

Book-53 Dr. 6

**LOCATION  
CENTRAL AVENUE  
CUT-OFF**

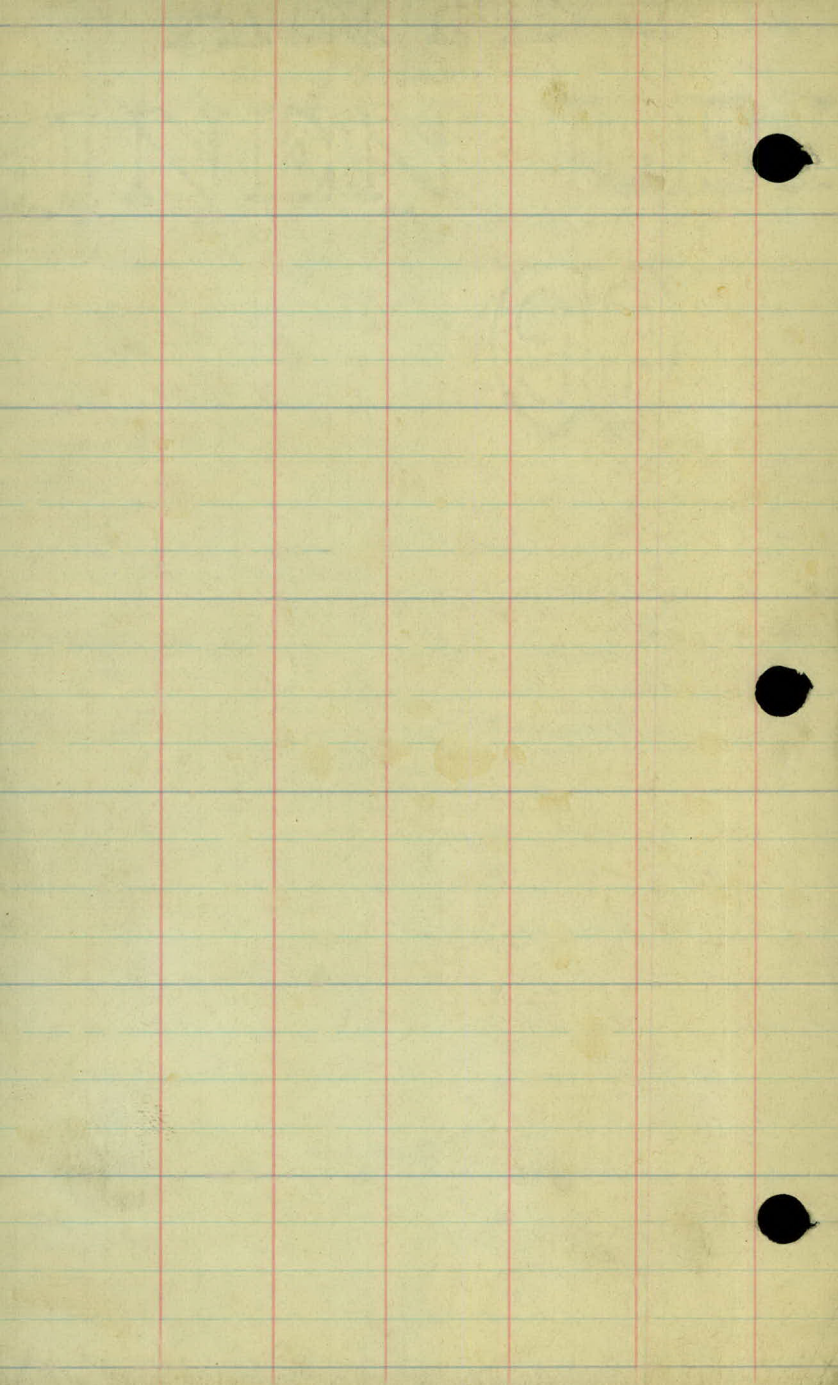
*D.O. Weber  
1928*

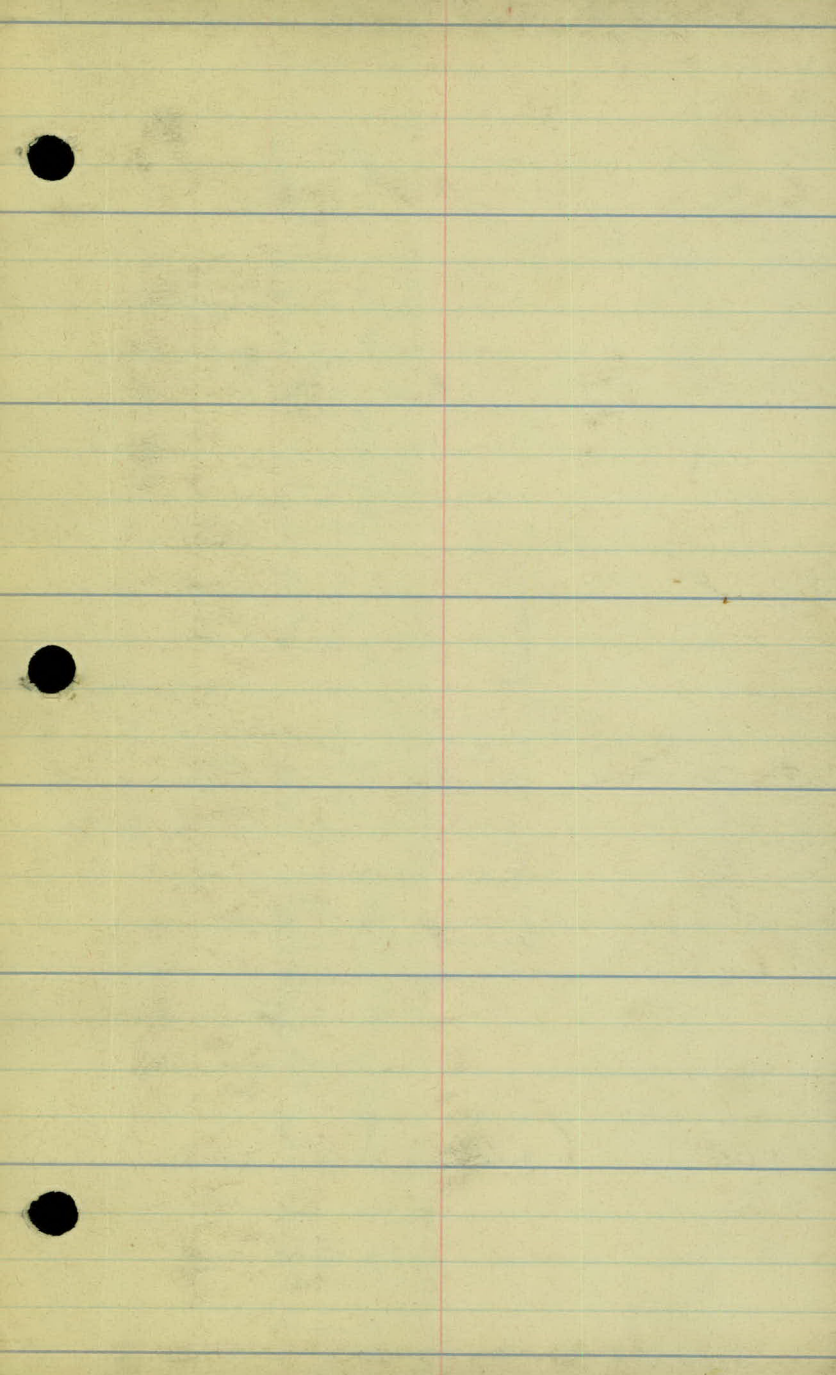
PRELIMINARY LOCATION  
OF CENTRAL AVE. CUT-OFF  
FROM LARPELLEUR AVE.  
TO CENTRAL AVE.

D.O. Weber

Completed 6-4-28









Sta. Point

47+73.2 P.O.T.  $\pm$  Hamline Ave.

32+55.4 P.O.T.

29+03. P.O.T.

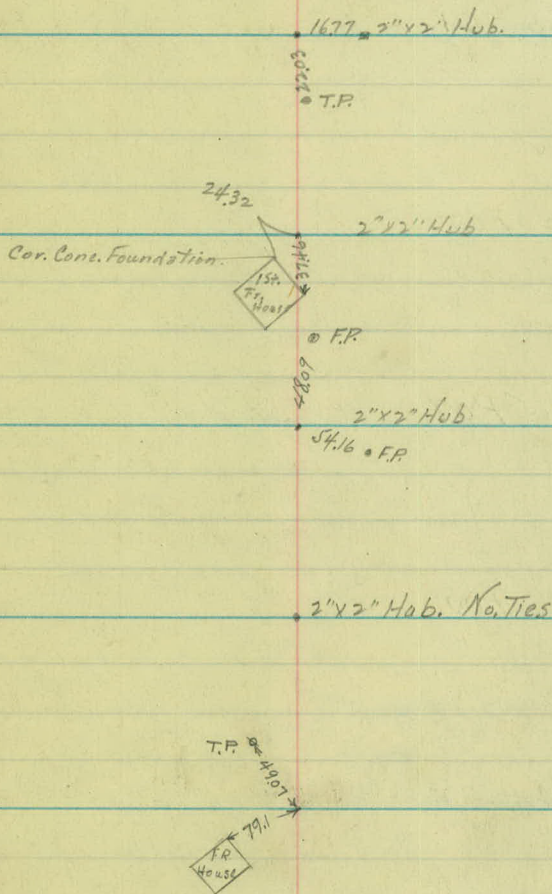
17+03.9 P.O.T.

0+00 =  $\pm$  Carpenter Ave.

5-1-28

Fair-Warm

{ D. Weber  
Beaton  
Haeusler  
Thompson



Sta. Point

131+26.63 P.O.T.  $\pm$  New Brighton Pave.

128+33.18 P.O.T.

97+13.2 P.O.T. No. Ties

89+33.65 P.O.T.  $\pm$  Snelling Ave.

68+57.5 P.O.T.

50+14.76 P.O.T.



5-2-28  
Cloudy & Cool

{ Weber  
Beaton  
Wheeler  
Thompson

Hole in Pavement

33.2  
4" W.O.

54.16  
14" B.O.

53.27  
14" W.O.  
2" x 2" Hub.

60.64  
14" W.O.

T.P. 8

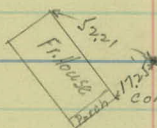
29.31

Spike

53.88  
12" W.O.

5.0  
14" W.O.  
2" x 2" Hub.

3.32  
2" x 2" Hub. under Fence.



2" x 2" Hub

conc. cor. Porch.

209+97.44 Pot.

207+43.28

188+40.25 Hike No Ties

173+52.85  $\pm$  Cleveland Ave.

165+15.91

153+07.

136+77.1

24.36 2"x2" Hub.  
 14" B.O. @ 11.48  
 2"x2" Hub.  
 13.82 @ 10" B.O.

Light  
 Born

Co Rd. D

38° 24' Arc  
 2171.03

40' EP @ 39.48

Cleve.

3 1/4" TP

800' So Cleveland.

2"x2" Hub.

No. of Co R. E. 1500'

2"x2" Hub.

2"x2" Hub.

No Tics

264+41.33 Equation (264+41.33=264+51.33)

231+47.57 = ("Equa" = 237+57.57)

231+46.05 Hub 2"x2"

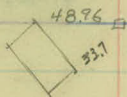
223+76.5 Hub 2"x2"

216+57.3 Hub

75.9

215+81.4





2" x 2" Hub.

2" x 2" Hub.

No Ties

2" x 2" Hub. Top of Slope.

± Long Lake Rd. (Pavement?)

305 + 1446

302 + 2253 P.O.T. 2" x 2" Hub.

299 + 157 P.O.T. 2" x 2" Hub

295 + 110 P.O.T. 2" x 2" Hub.

286 + 55.1 P.O.T. 2" x 2" Hub

272 + 6125 P.O.T. 2" x 2" Hub. ←

→ Equation  $(272 + 5125 = 272 + 6125)$

1936 @ 8" Oak

1944 @ 10" W.O.

50' from E. of Silver Lake Rd. (Sec. Line.)

200' S.E. of Fairchild Ave.

Near Fence.

200' ft So. of Co. Rd. E.

340+56.75 " 2"x2" Hub.

339+07.95 P.O.T. 2"x2" Hub.

337+05.4 P.O.T. 2"x2" Hub.

334+87.69 P.O.T. 2"x2" Hub.

333+19.55 P.O.T. 2"x2" Hub.

327+56.0 POT. 2"x2" Hub.

326+00 = Beg. Woods.

320+39.5 P.O.T. 2"x2" Hub.



= Intersection of West Co. Line.

(No Ties)

Point  $\Delta$  Lt  $\Delta$  Rt

397+91.47 P.O.T. 2" x 2" Hub

393+80.85 P.O.T. 2" x 2" Hub (No Ties)

388+31.95 P.O.T. 2" x 2" Hub. (No Ties)

376+68.27 =  $\Delta = 38^{\circ}40'$

375+81.8

360+89.08 P.O.T. 1" x 2" Hub

352+29.63 P.O.T. 2" x 2" Hub.

347+90.8 Hub 2" x 2" Hub

Burnt stamp 12"  
17.43  
11" B.O.

Nail in 2"x2" Hub.  
21.93  
12" B.O.  
8" B.O.

8" B.O.  
13.31  
10" B.O.

West of Lake in woods

17.76  
6.41  
12" B.O.

|      |        |      |                          |          |
|------|--------|------|--------------------------|----------|
| B.S. | H.I. ✓ | F.S. | Mon. at Dale +<br>Larps. | Elev ✓   |
| 4.92 | 923.85 | 3.88 |                          | → 918.93 |
|      |        |      |                          | 919.97   |

|      |        |      |                      |        |
|------|--------|------|----------------------|--------|
| 5.59 | 925.56 | 3.63 | Mon. & M. W. of Dale | 921.93 |
|------|--------|------|----------------------|--------|

|      |        |      |  |        |
|------|--------|------|--|--------|
| 1.59 | 923.32 | 7.58 |  | 915.74 |
|------|--------|------|--|--------|

|      |        |      |                |          |
|------|--------|------|----------------|----------|
| 5.11 | 920.85 | 0.90 | Mon. & M. Dale | 919.95 ✓ |
|------|--------|------|----------------|----------|

|      |        |      |  |        |
|------|--------|------|--|--------|
| 6.39 | 926.34 | 0.22 |  | 926.12 |
|------|--------|------|--|--------|

|       |        |      |  |        |
|-------|--------|------|--|--------|
| 12.34 | 938.46 | 0.68 |  | 937.78 |
|-------|--------|------|--|--------|

|      |        |      |  |        |
|------|--------|------|--|--------|
| 6.99 | 944.77 | 2.01 |  | 942.76 |
|------|--------|------|--|--------|

|      |        |      |  |          |
|------|--------|------|--|----------|
| 3.60 | 946.36 | 2.96 |  | 939.40 ✓ |
|------|--------|------|--|----------|

$$\begin{array}{r} 46.33 \\ 25.86 \\ \hline 20.47 \end{array} \checkmark$$

$$\begin{array}{r} 939.40 \\ 918.93 \\ \hline 20.47 \end{array} \checkmark$$

R.R. Spite opp. Station

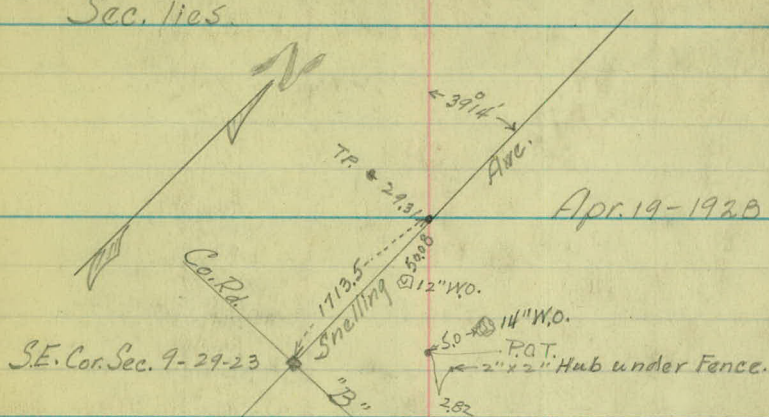
Levels from Dale St. to 0+00



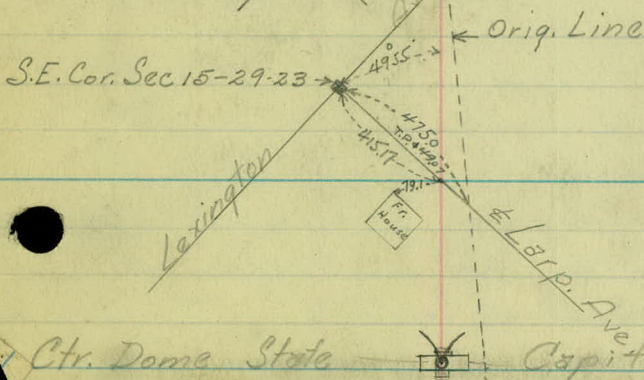
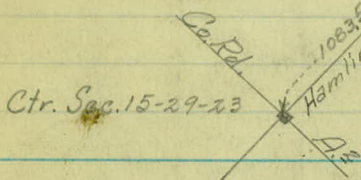
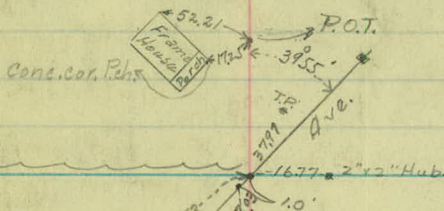
Cloudy & Cold.

Weber &  
Beaton Rod  
Haeussler H.C.  
Thompson R.C.

Sec. Ties.

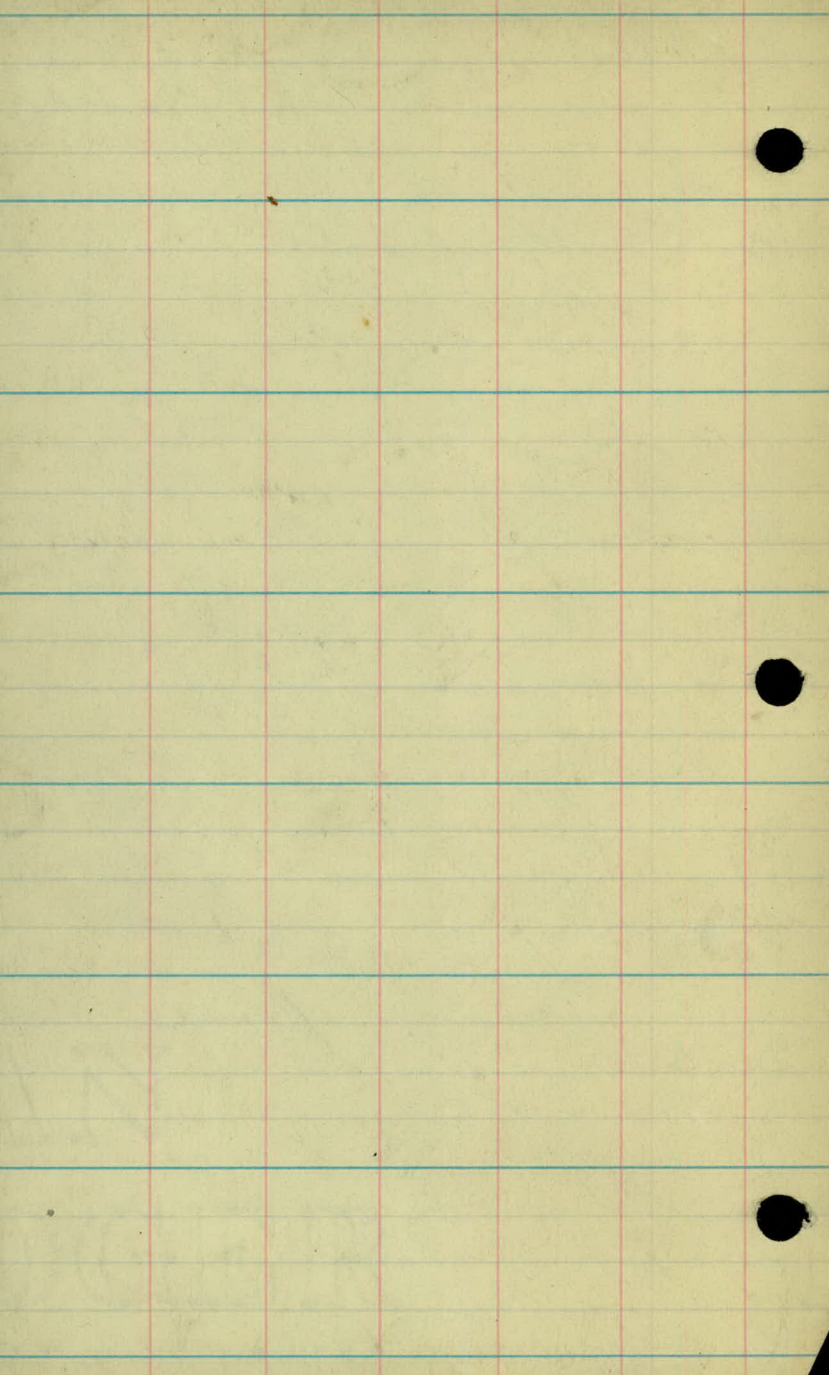


Apr. 19-1920



Ctr. Dome State

Capitol.



Cloudy - Cold  
Sec. Ties

Ctr Sec. 32-27-23

(2)

Weber  
Beaton  
Hoesler  
Thompson

39° 14' Rd.

5342 @ 3" Maple.

5342 @ 6" Maple

Apr. 21

N.W. Cor. Sec. 4-29-23

Co. Rd.

Long Lake

Co. Rd.

'S'

Ave.

W 1/4 Cor. Sec. 4-29-23

Cleveland

P.O.T.

12' @ 10" W.O.

554 @ 10" W.O.

Apr. 20

39° 01' Rd.

N. 1/4 Cor. Sec. 9-29-23

51005

332

5416

14" W.O.

4" W.O.

P.O.T.

5327 @ 14" W.O.

6064 @ 14" W.O.

Apr. 19-

Ctr Sec. 9-29-23

New Brighton

V.V.

West of Silver Lake Road.  
Mon. 61.45 W. of  $\pm$  Rd.

About 200' SE. Co Rd. E."

Halfway Between Long Lake Rd. & Co. Rd. E."



Fair & Cool

N.W. Cor. Sec 30

14" B.O. ⊗

20" B.O. ⊗

West Co.

Apr. 24-28

Line { Weber ③  
Beaton  
Hoesler  
Thompson

38°  
3827  
16.77  
541.57

W. 1/4 cor. Sec 30

Edge of Woods

P.O.T.

1593 ⊗ 24" B.O.

342.9

⊗ 14" B.O.

⊗ 8" B.O.

N.W. of Barn

P.O.T.

19.37

19.45 ⊗ 8" W.O.

Ctr Sec. 30

3856

Apr. 23-28

722.32

296.0

2417.0 F.P.

Co. R. E.

30 1/4 Cor. Sec. 30

P.O.T.

228 ⊗ 12" W.O.

32.16

12" W.O. ⊗

P.O.T. 30.63 ⊗ 24" B.O.

27.21

⊗ 14" Maple

No. Edge of woods about 100' S.E. of intersection

300' So. of No. Edge Woods

about 500' S.E. of Lake in Woods

Clear & Cool

38+85.0

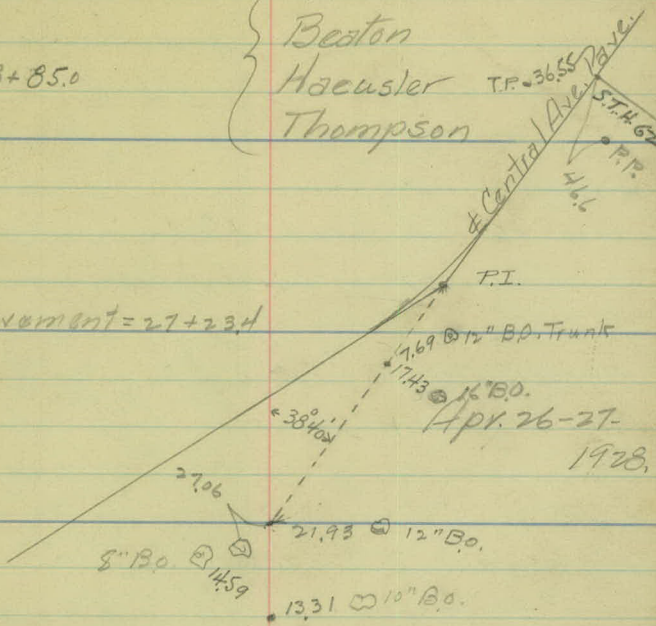
Weber  
Beaton  
Haeusler  
Thompson

T.P. 36.55  
S.T.H. 62  
P.P.  
4.66

P.I.

Edge Pavement = 27+23.4

0+00



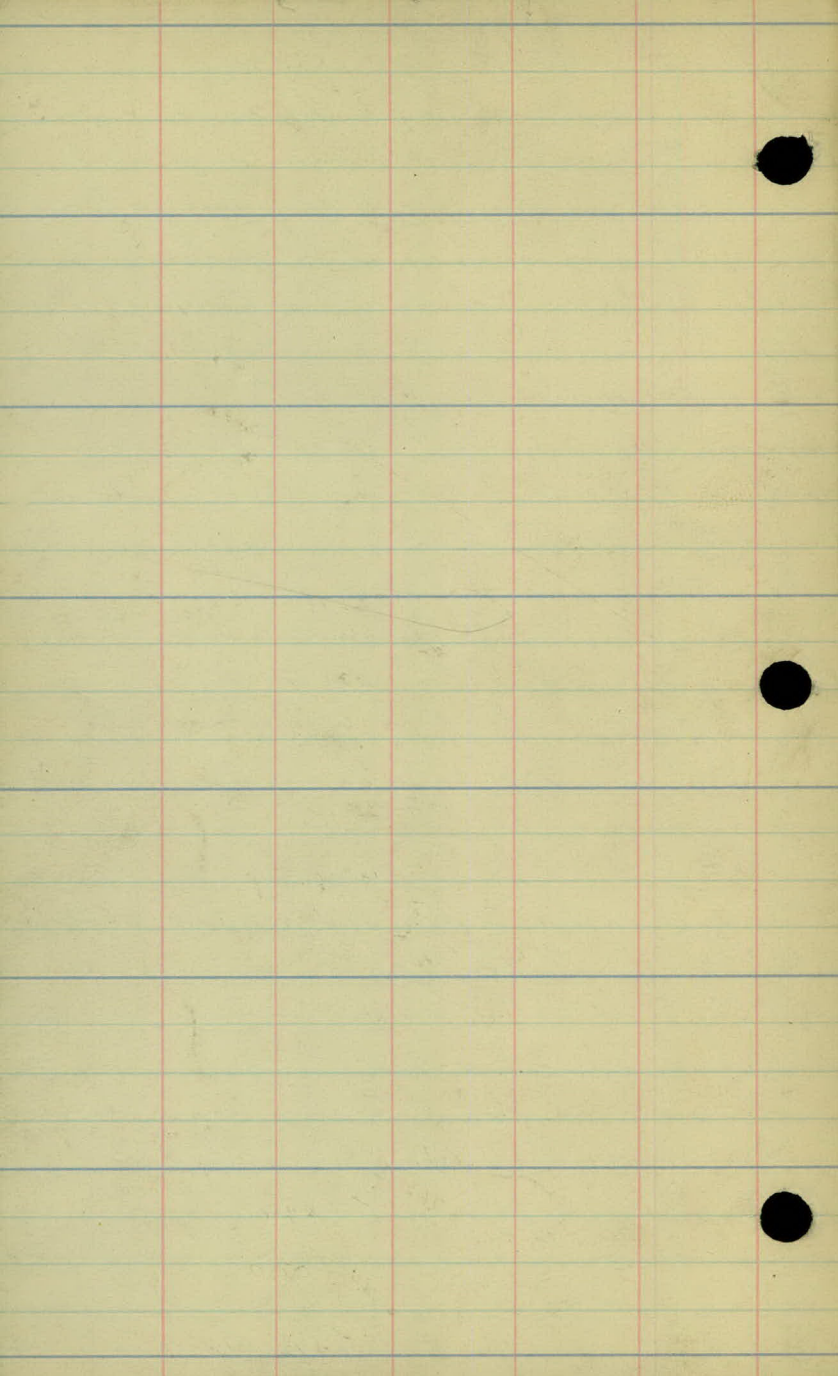
Apr. 26-27-1928

14" B.O.  
13.14  
10" B.O. 10.44

Apr. 25-28

P.O.T.

12" B.O. 7.63  
14" B.O. 12.97  
8" B.O. 14.4  
12" B.O. 2.74





5+00

4-30-28

Sta. 6+00

+63 P.P. 32'

D. Weber  
Beaton,  
Haeussler  
Thompson

Clear-Warm

5+00

# Topography Notes

St. T. H. #62

4+00

Cultivated

Cultivated

3+00

2+00

1+00

Cultivated

Cultivated

+42 = T.R. 19'  
+38 = Rtsign 30'

0+00

+13 = Edge of Pavg.  
20' Pavement.

11

10

9

8

7

6+00

(Cultivated)

(Cultivated)

(Cultivated)

(Cultivated)

• +50 = P. 3.50' 24"

• +38 = T.P. 37'

7+00

= 28' R1 Edge Pave.

Edge of Pave = 6+68

27.

Edge of Pavement 6+00 22'

+23 = Edge of Pavement  
Lexington Ave

23

22

21

20

19

18

17

16

15

14

13

12



(Cultivated)

(Cultivated)

(Cultivated)

(Cultivated)

29

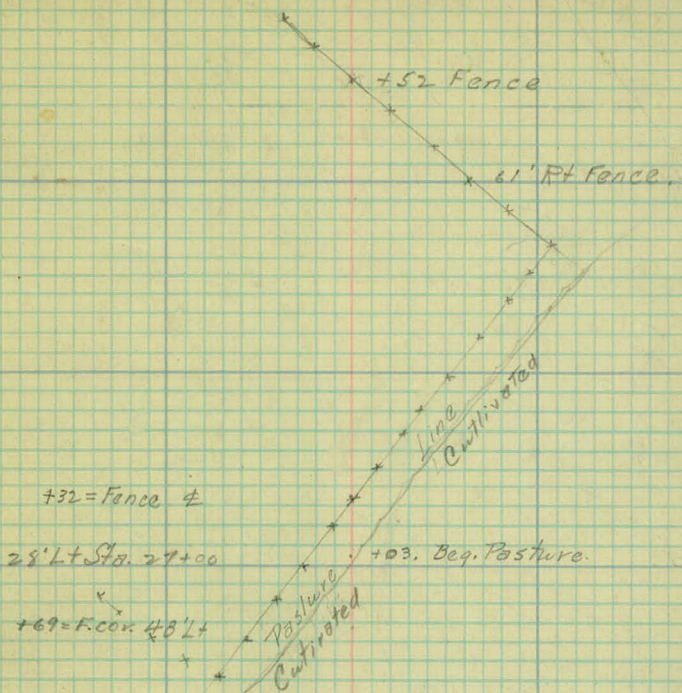
28

27

26

25

24



(Cultivated)

(Cultivated)



37131

+

34

33

32

+30

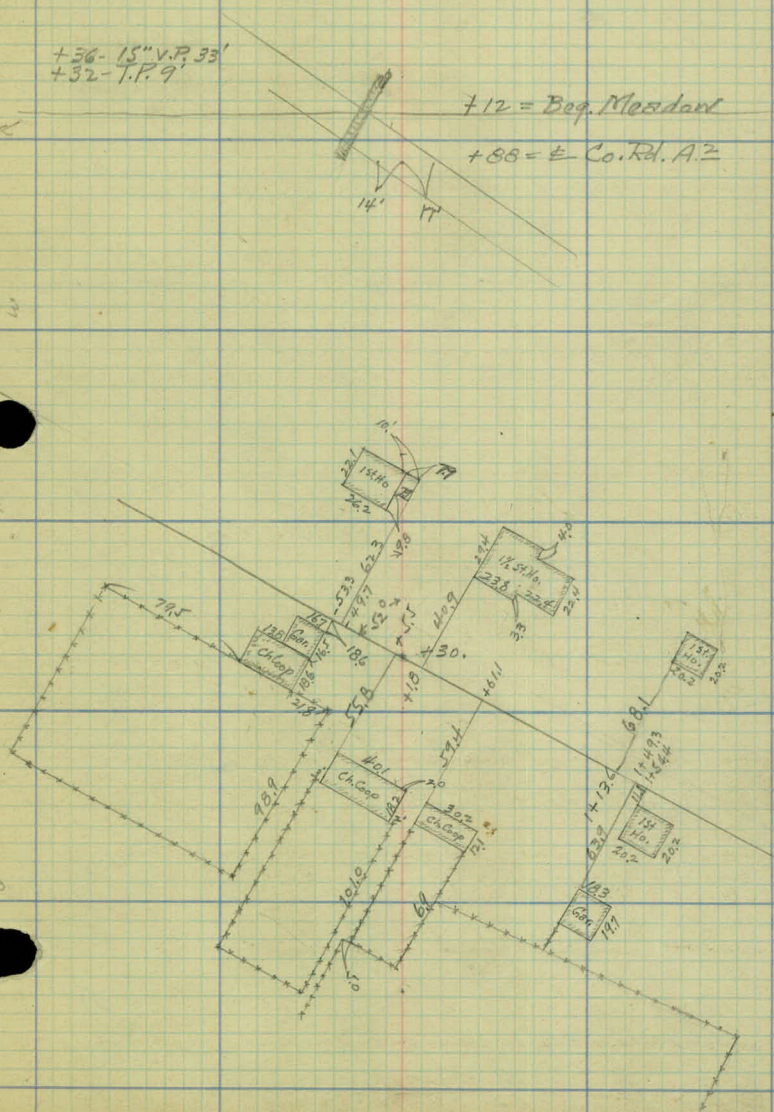
31

30



Weber  
Beaton  
Thompson  
Wheeler

+36-15" V.P. 33'  
+32-T.P. 9'

 $+88 = \pm \text{Co. Rd. A. 2}$ 

41

40

39

38

37

36

Cultivated Field.

Cultivated Field

Meadow

Meadow



47

46

45

44

43

42



+50 T.P. 1' Lt + 44

(Cultivated)

(Cultivated)

Parallel with Cordaz

+27 ± Farm Ent N' side

53

52

51

50

49

48

Cloudy - Cool

5-3-28

Weber  
Beaton  
Thompson  
Wheeler

Beg. Cultivated Field.  
End. Pasture

+71 - Apple Tree 26'

+61 - Beg. Pasture

+09.

+88



+15-10" Elm 40'

+53-4" Maple 18'

+42 ± F.E. 8' Wide

+62-18" Elm 19'

+25-W Shoulder Rd. 33'

+11 - R.P. 5'



66

65

64

63

62

61

60

59

58

57

56

55

54



Cultivated

Cultivated

Cultivated

Cultivated

84

83

82

81

80

79

78

77

76

75

74

73

72

71

70

69

68

67

84+25-

Fence

35' RT of Sta. 84+00

Pasture.

+59-12" B.O. 4'  
+52 Fence Int.

Pasture

+20-8" W.O. 20'  
+10 F. Cor 24'

+90-F.P. 25'

+63 Fence

+38 T.P. 50' +40 E Co. Rd. "B"

+30 P.P. 4'

Cultivated

+64 T.P. 50'

Cultivated



102

+70

101

100+00

90

89

+84

88

87

86

85



(Cultivated)

(Cultivated)

+15-Fence

101+00 F=15'

+160-F-50'

+0.8-Fence

100+00 Fence 8'

Cultivated

Cultivated

Clear-Cool

5-4-28

{ Weber  
Bealon  
Thompson  
Wheeler

+49-TR=27'

+24-18"C.M. 44'

18"x50'

+89=18"C.M. 5'

88+84

+82=10"W.O. 12'

+29-12"W.O. 31'

+14=8"W.O. 26'

+06=6"W.O. 20'

89+06 Fence 15'

120

119+00

118

117

115+00

114+00

Low  
Mo  
nd

115+00 Fence 49'

Pasture

+ 27 Fence

+ 54.5 Fence

118+00 Fence 37'

Pasture

234+

119+02 - Ditch 4' Wide.

62'

67.5

Ditch

1101

1102

1103

1104

1105



127

126

125+00

24

23

121+00



128+00

127+03- 03. Lt.

126+00

100' Lt

Fence

Pasture

Pasture

63'

+77. Fence Cor.

36'

123+55. Fence

Pasture

Pasture

133

132

131+26.63  $\pm$  New Brighton Road.

131+00

130+00

129+00

128+00

Clear - Cool

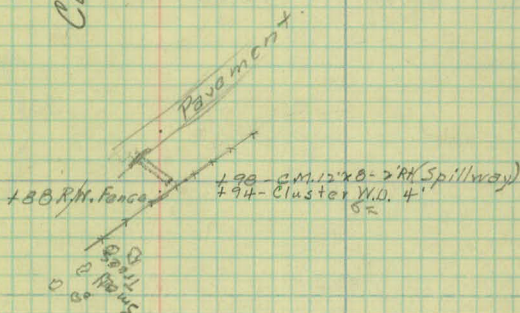
134

{ D. Weber  
Beaton  
Thompson  
Wheeler.

5-4-28

Cultivated

Cultivated



Pasture

Pasture.  
192 2' x 2' 4' W.D.  
193 14' x 14' W.D.



40

40

139

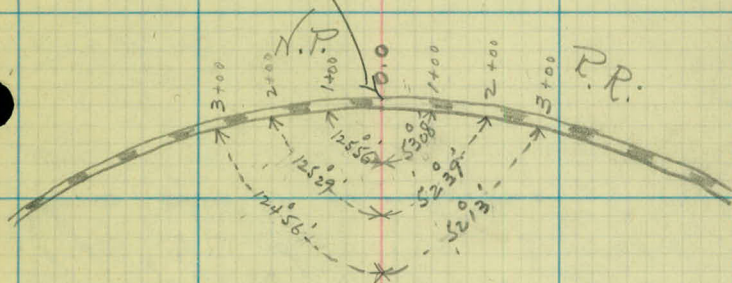
138

137

136



Sta. 137+45.3 = No. Rail.



40

40

139

138

137

$$\begin{array}{r} 68 \\ 24 \\ \hline 92 \\ 30 \\ \hline 122 \\ 2 \end{array}$$

136

$$\begin{array}{r} 68 \\ 74 \\ \hline 142 \end{array}$$

322

5-6-28

141  
(Fair-Highwind)

D. Weber  
M.A. Beaman  
F.R. Thompson  
Wheeler

Pasture

Marsh

Co. Rd. "C"

+43 = ± Co. Rd. "C"

+15 - Rd. Sgn. 17'

+02 - Fence

+88 - T.R. 24'

N.P. R.R.

+45.3 - No. Rail of N.P. Track

137+00 - Fence 27'

+80 - R.R. R/W Fence.

147

146

45

44

43

142

141



148

Swampy

+63

Ditch

+22

37

Low  
Land.

Cultivated

(Cultivated)

(Cultivated)

40

Pasture

+25 - Cultivated

156

155

154

152

151

150

49

148

156+00  
cultivated

Pasture

+32-20" W.O.B.

Cultivated

Garden

40'

+75

150  
Berry Patch

Pasture

+25

150+00  
+22' Rt.  
+50-Brush 75'  
+42' Rt.  
+50-Brush 18'  
+90-Brush 29' End  
+75-10" maple-24'  
+50-20" W.O. 5' Rt.  
Beg. Brush.

+08.

Swamp

100'



166

165

164

63

62

161

60

59

158+00

156+00



167 200'  
400' Swamp  
+00 = Edge of Swamp

Pasture  
+40 Edge  
Pasture

Stripe of Woods  
163+00 = Edge of Woods  
200' Lx

(Cultivated)

Cultivated

Cultivated

+00 Edge Woods

Cultivated

Woods

+27' - Beg Woods

180

174

+56.83

173

70

69

168

167

Alfalfa.

Alfalfa.

+ 10.0 Fence

Cleveland

+ 14 T.P. 2'

Pasture

Pasture

54' Ditch

SWAMP

SWAMP

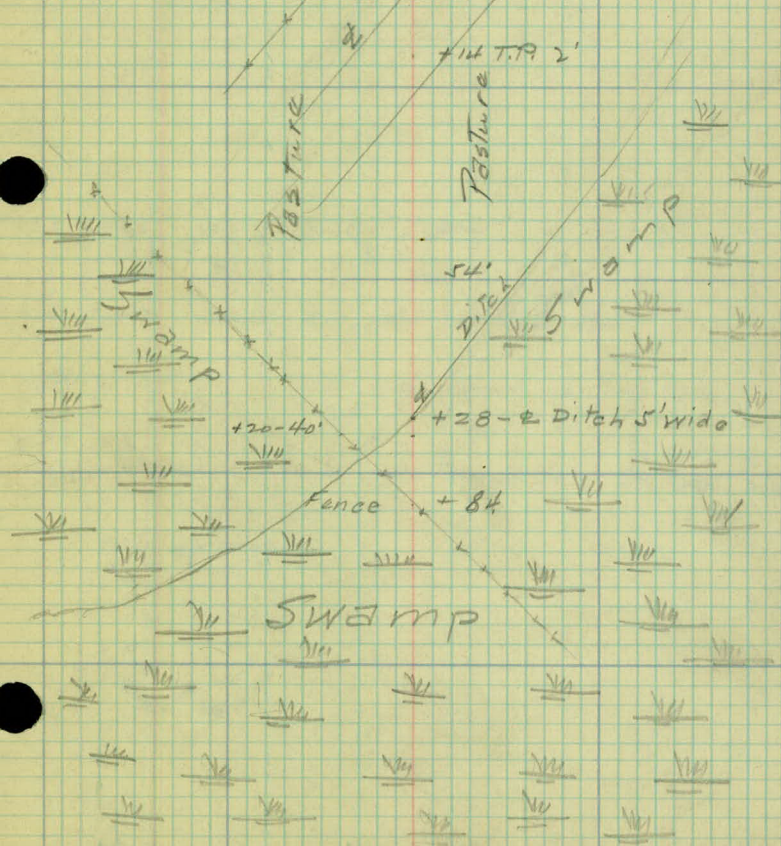
+ 20-40'

+ 28-2 Ditch 5' wide

Fence

+ 84

SWAMP





198

197+00

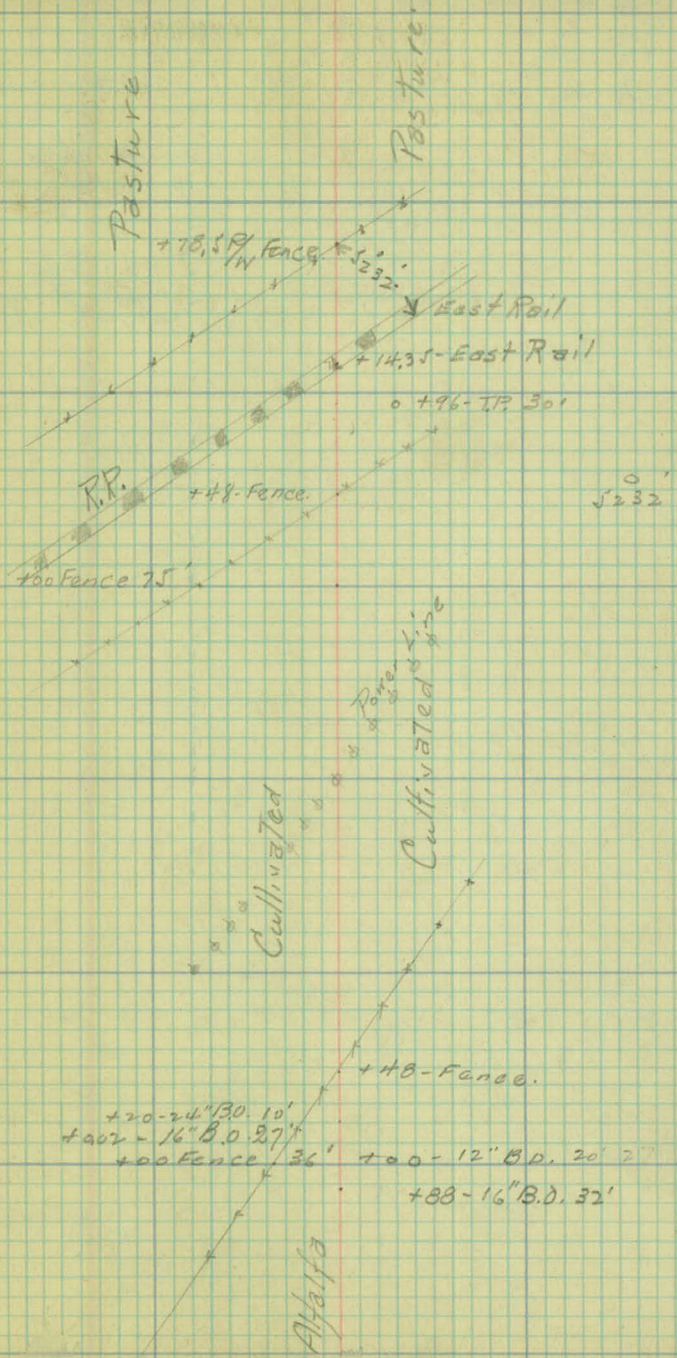
196+00

190+00

181+00

180+00





208+00

207+00

206

199+00





224

223

219

216

215+00

+88

210



Marsh

+80 - Fence.

100'

- 101. -

Fence

Cultivated

Cultivated

+14 = E Ditch  
+10.12 "B.F. 10'

27'

5' Wide

+47 - T.R. 8'

+07.4 = Edge Pave.

+63.4 = Edge Pave.

+72 = 3" Box Elm 28'

+50 = 3" Box Elm 15'

+45 = E F.E. = 9' Wide.

+27.6 Box Elm. 2'

+22 T.R. 3'

+12 = 8" Box Elm 15'

54'

Truck Garden

Truck Garden.

211 - Fence 14.55

Fence - 210 + 88

Pasture

Pasture

233

228

227

226

225

224+00

223+00





240+00

239+00

238+00

(Equation)  $237 + 47.57 = 237 + 57.57$

237

236.00

235



241 + 07. Fence 12  
Cor.

4' Ditch

+72 Fence 20'  
+60

Cultivated (Cultivated)

(Cultivated)

+50-16" Tree 34'

Cultivated

Cultivated

+18-14" Tree 29'  
+20-20" Tree 34'

+40-10" " 15'  
+30-10" Apple 21'

+46 End Trees 25'

+95' Line of Trees

+14 Trees 12"

+40- Bay Row Maple Tree 14-39'  
+15-10" Tree 40

Cultivated

Cultivated

246 + 00

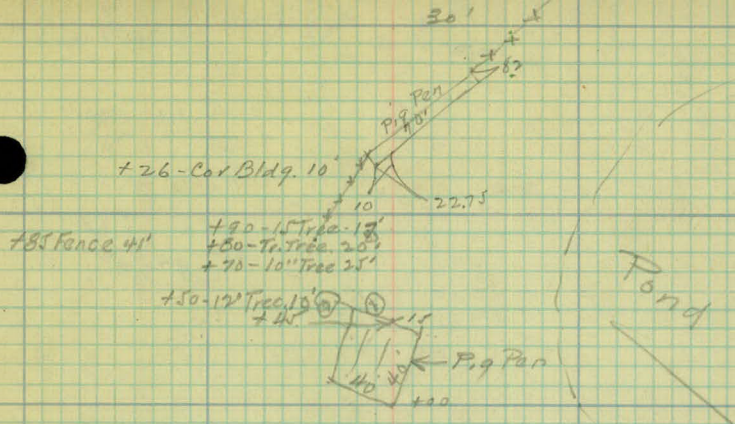
245

244

243

242

241

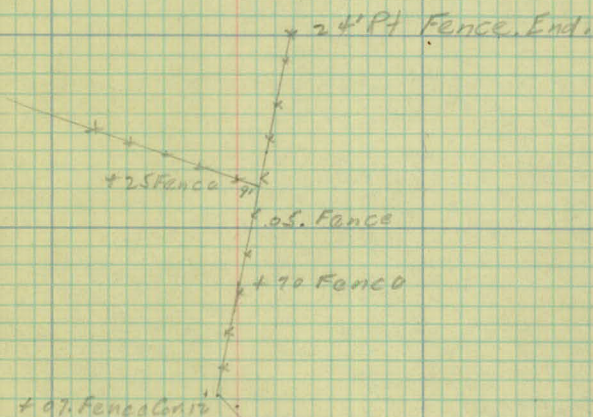


+50' @ 65'-10"

+35' @ 65'-14"

+40' @ 66'-14"

+60, 14' @ 40'





257

252+00

+50-T.P. 4' Lt.

+16-Jog in  $R \frac{1}{4}$  Fence 65' Lt.

251

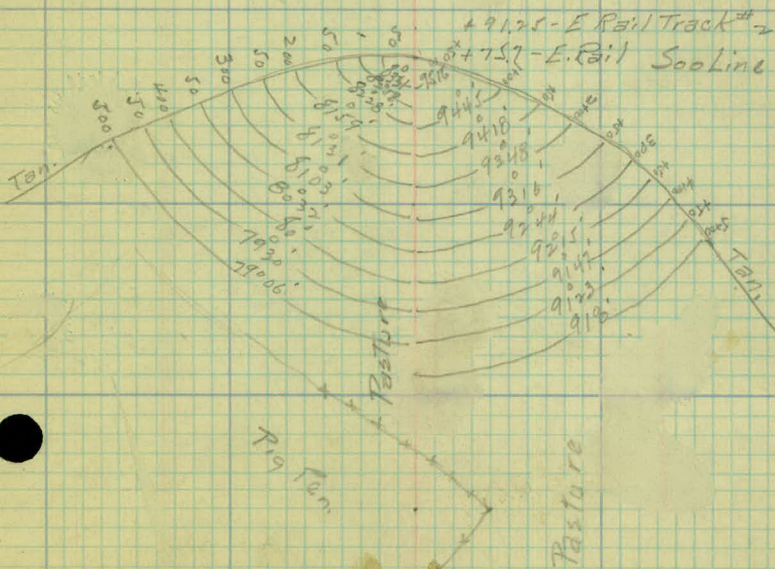
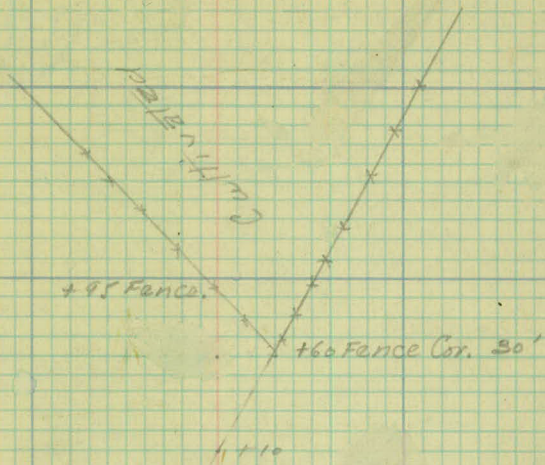
+82=RR.  $R \frac{1}{4}$  Fence.

+65'=Cor Fence. Jog. in  $R \frac{1}{4}$  55' Lt.

250+00

247





267

265

264

263

262

Madison

Farm Entrance 15' wide

+75 E.F.F.

+60 - T.B. 14'

50'

Cultivated

Cultivated



+25 Car House 11'

+05 House 100'

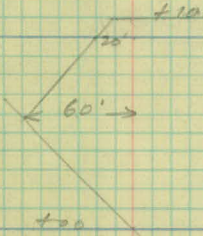
+74 " " 78' Gar.

+65 Car Bldg 35'

Con Barn Tile +57 well - 36'

+17 Bldg 24' Gr.

+05 Bldg 34' Gr.



Pig Pen

+50 Pig Pen 50'



278

275

274

273

272

271



278+00

Cultivated

+50-10" B.P. 15'

VII

VII

VII

VII

VII

VII

VII

VII

VII

VII

VII

VII

VII

12'

+90 = G.R. + 90 - P.P. 12'

+77 - 4 Co P.P. E.

+65 - G.R.

+50' Cluster of 3-14" Oaks

+30 Edge B.P.

+30-12" W.D. 10'

Berry Patch

+76 - 1'

+61-12" W.D. 2'

+25-12" W.D. 20'

+20-12" W.D. 6'

+00-10" W.D. 4'

+20-6" W.D. 20'

289

288

287

286

280

279

278

Cultivated

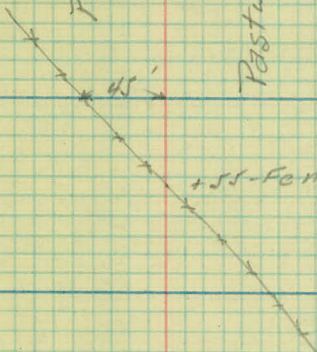
Cultivated

Pasture.

Pasture

45'

+ 55' Fence.





296

295

294

293

292

291

290

289



+ 30 Fence +

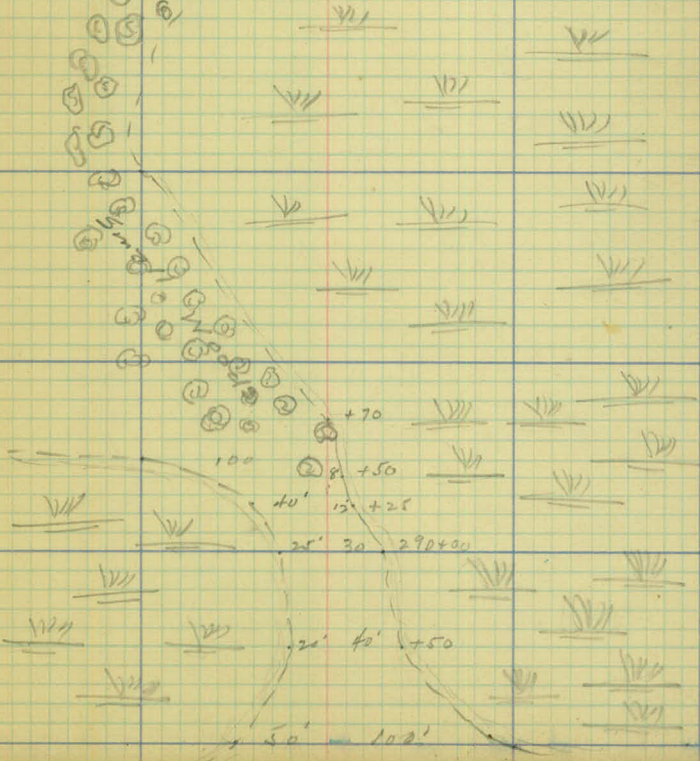
Calleryna

30'

Pasura

Pasura

293 + 20 Edge Swamp.



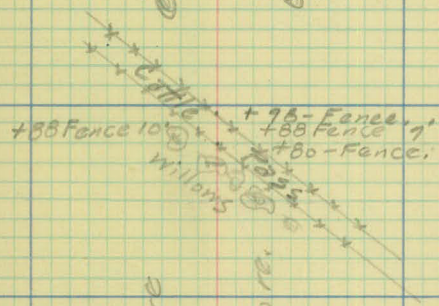
300

299

288

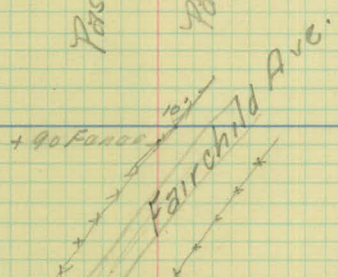
Apple Orchard

Apple Orchard



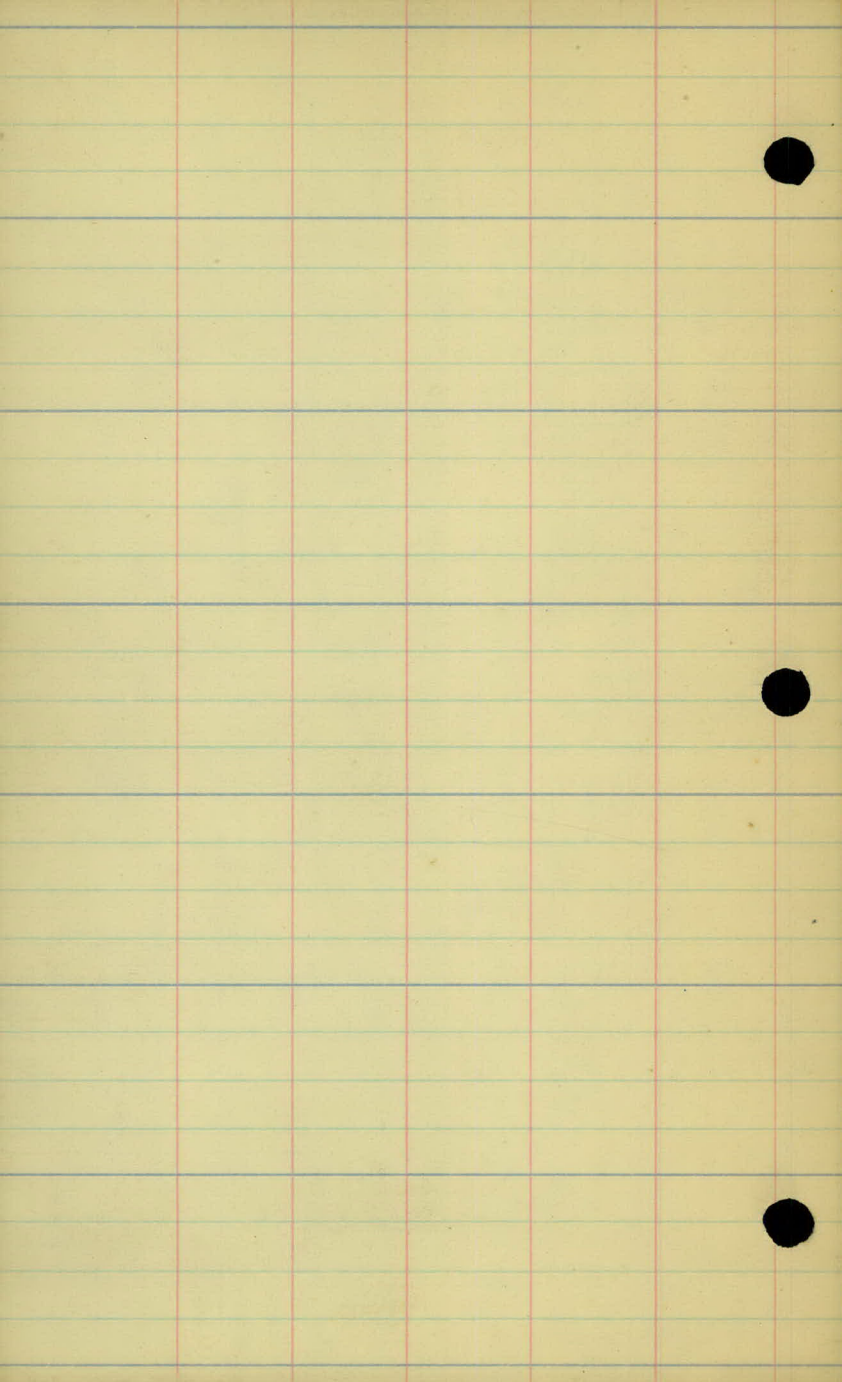
Pasture

Pasture

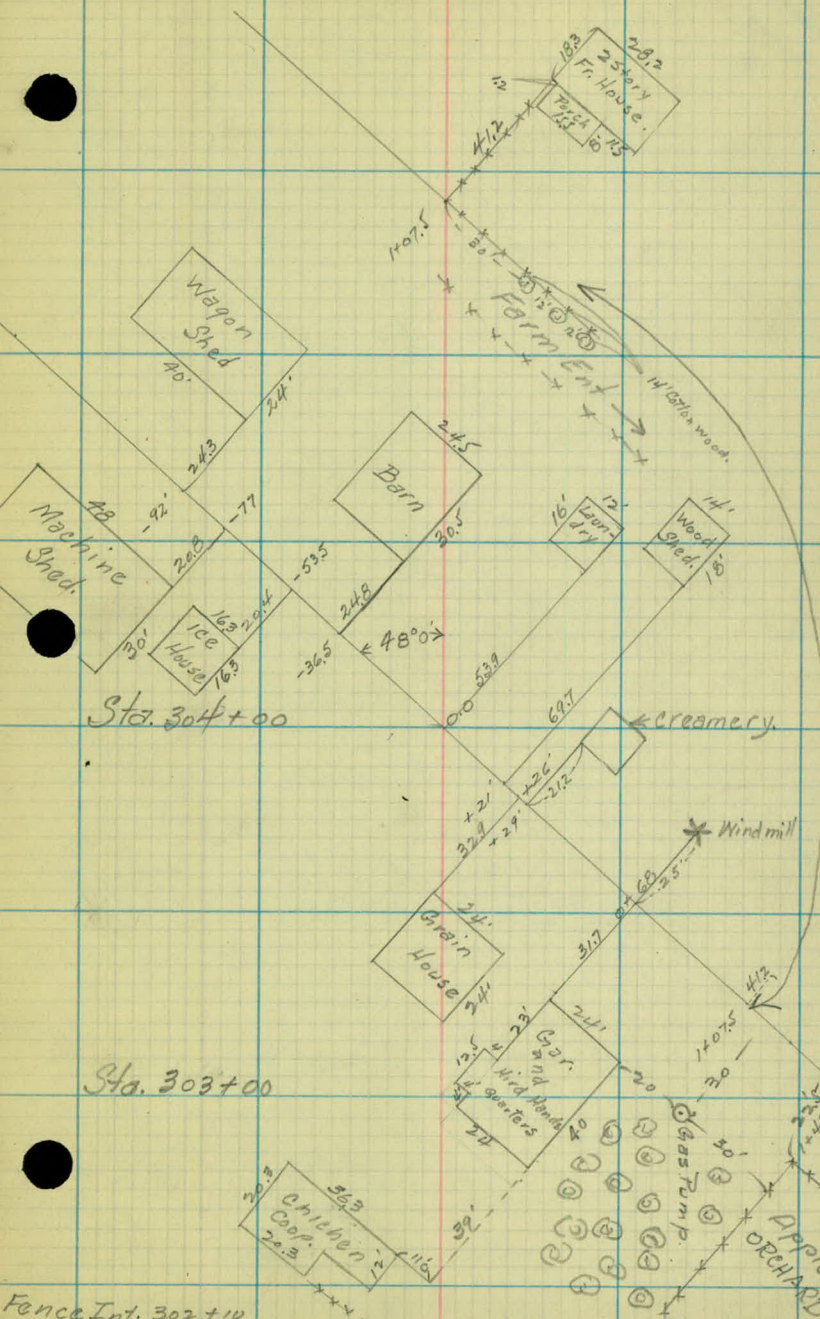


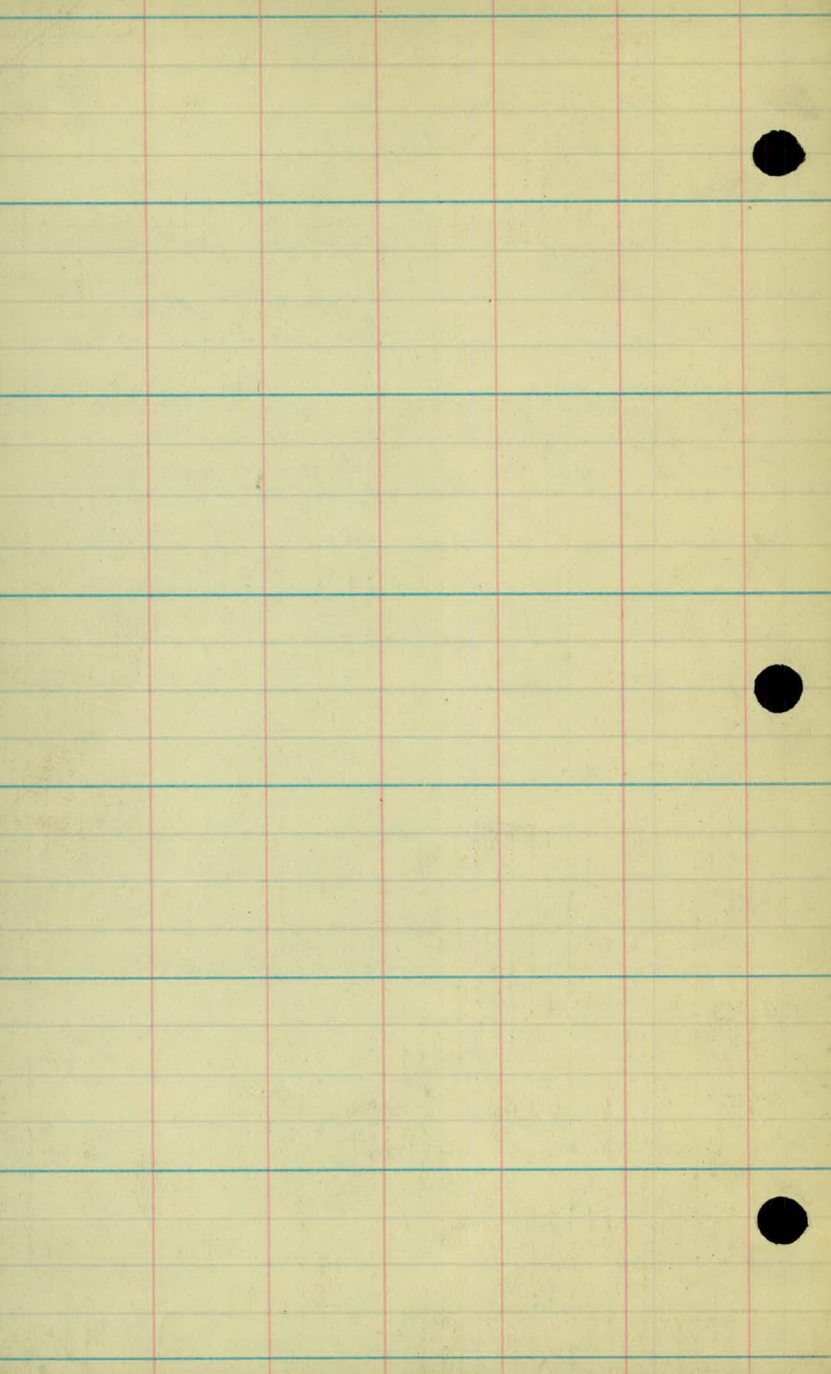
298 top Fence 4'

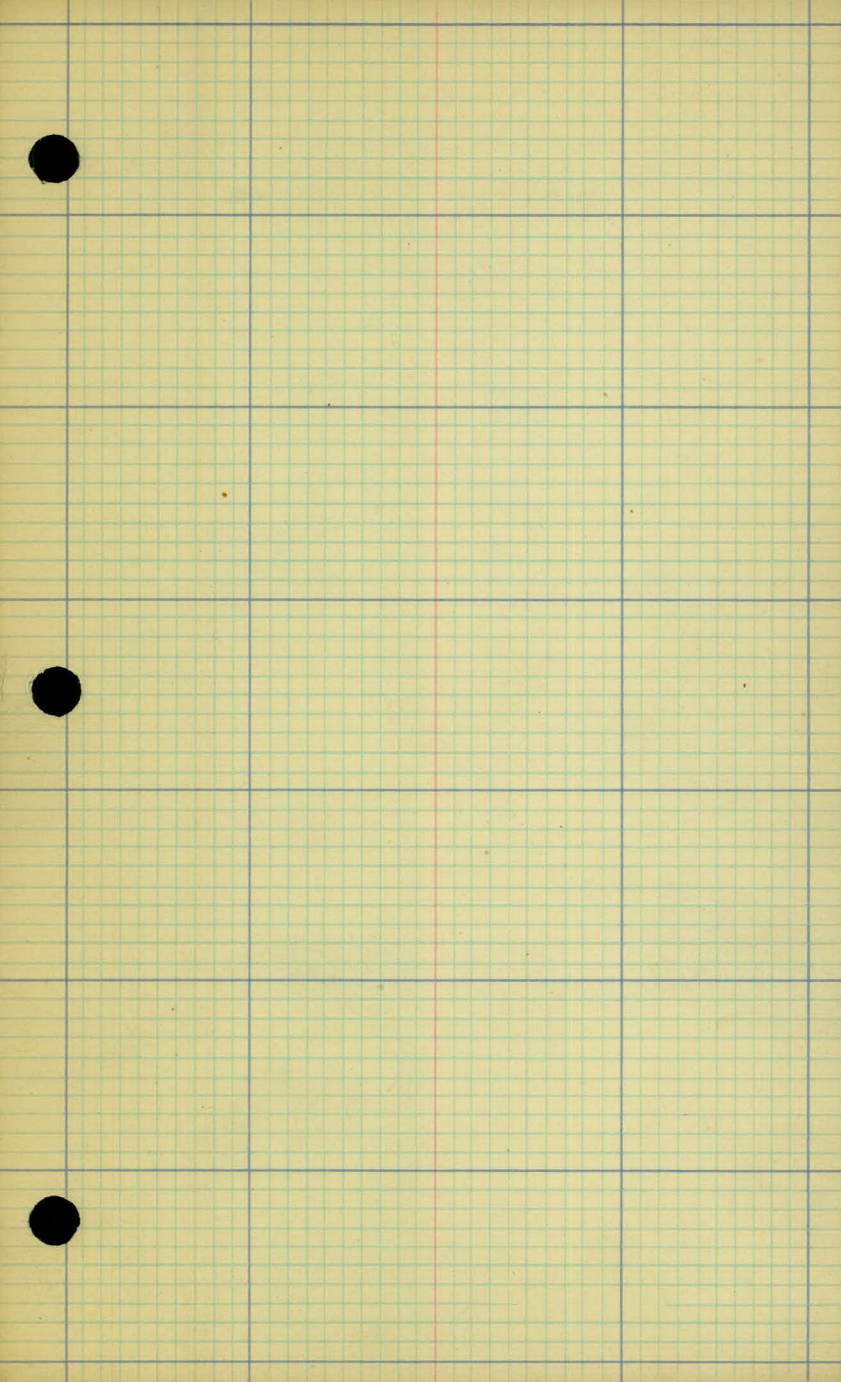
+ 07 Fence











334

326

325

324

323

+80

=

322

1°

306



53.7  
+87.63 = Fence N. Co. Line

= Beg. Woods

+80. End.

+15 Beg.

Cultivated

30'

+80

Cultivated

377

368

365

360

352

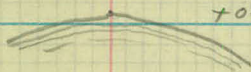
Cultivated

Cultivated.

x x x x x x x x x x +20-Fence.

Woods

No.



+05. = Edge of Pond



+30 = Edge of Pond

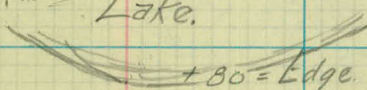
Woods

Woods



+50 = Edge of Lake.

Lake.



+80 = Edge. of Lake.

Woods

Woods

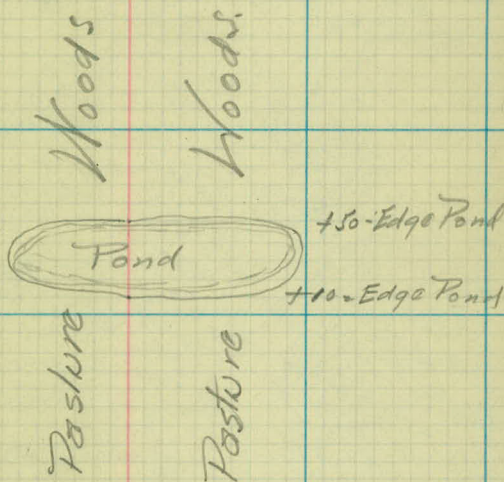
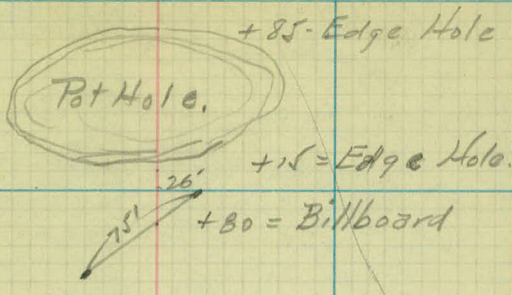
401

400

396

393





\* \* \* \* \* +80 - Fence.

Cultivated

Cultivated

407

End of Project. 5/14/62

406

405

404

403

402

401

407

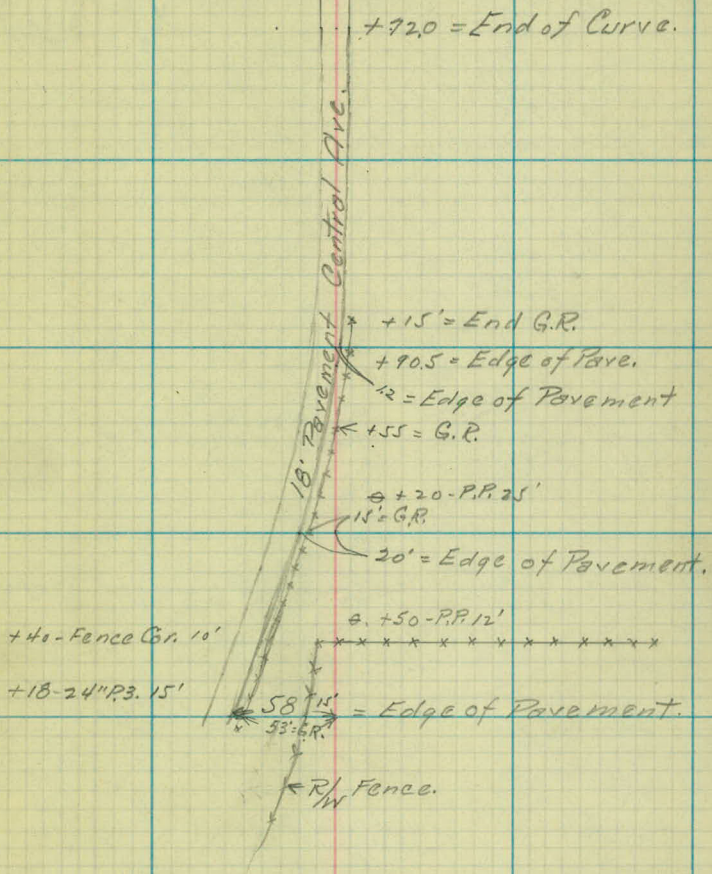
406

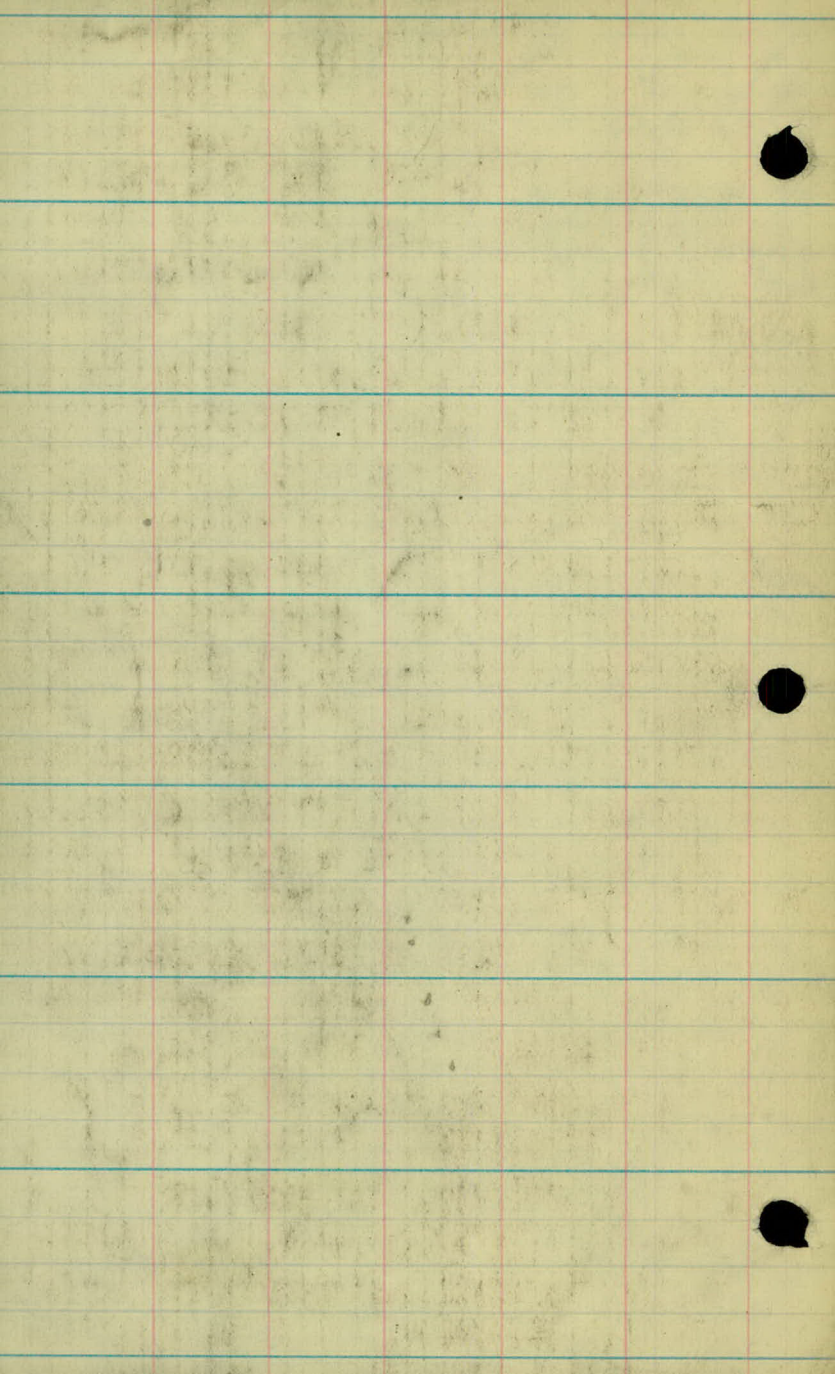
405

404

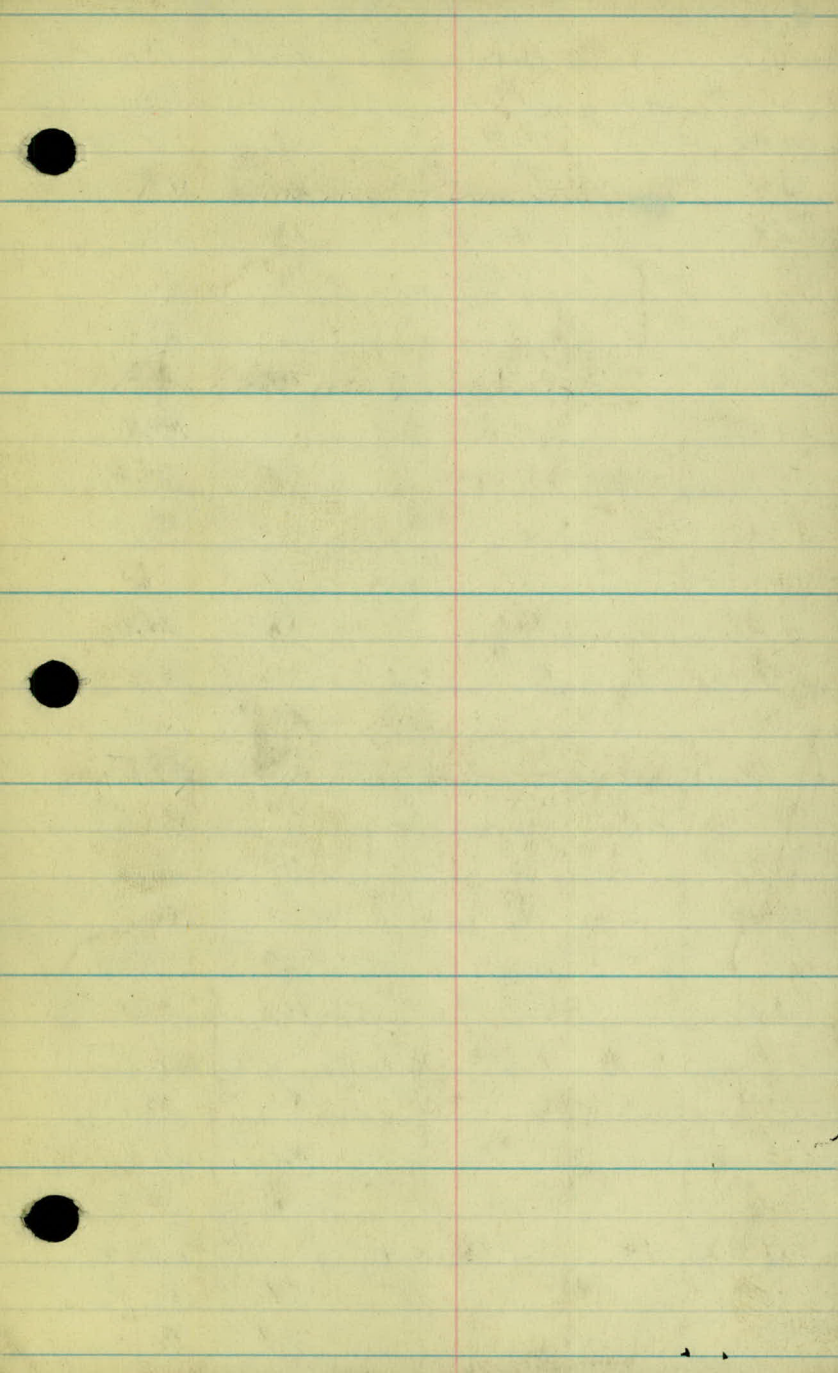
403

402









| Sta.  | +     | H.I.   | -    | Rod  | Elev.  |
|-------|-------|--------|------|------|--------|
|       |       |        |      |      | 939.40 |
| 0+00  | 4.51  | 943.91 |      | 4.49 | 939.42 |
| +21   |       |        |      | 4.9  | 939.0  |
| +27.5 |       |        |      | 6.7  | 37.2   |
| 1+00  |       |        |      | 7.5  | 36.4   |
| 2+00  |       |        |      | 6.4  | 37.5   |
| 3+00  |       |        |      | 4.7  | 39.2   |
| 4+00  |       |        |      | 3.2  | 940.7  |
| 5+00  |       |        |      | 8.5  | 35.4   |
| 6+05  |       |        |      | 13.9 | 930.0  |
| +20   |       |        |      | 8.1  | 35.8   |
| +45.5 |       |        |      | 8.3  | 35.6   |
| T.P.  | 1.23  | 937.99 | 7.15 |      | 936.76 |
| +73.0 |       |        |      | 3.0  | 935.00 |
| +88.0 |       |        |      | 8.1  | 29.9   |
| 7+00  |       |        |      | 7.7  | 30.3   |
| 8+00  |       |        |      | 7.7  | 30.3   |
| 9+00  |       |        |      | 7.5  | 30.5   |
| 10+00 |       |        |      | 6.7  | 31.3   |
| 11    |       |        |      | 4.9  | 33.1   |
| T.P.  | 12.03 | 945.83 | 4.19 |      | 933.80 |
| 12    |       |        |      | 8.1  | 37.7   |
| 13    |       |        |      | 4.1  | 41.7   |
| 14    |       |        |      | 1.0  | 44.8   |
| T.P.  | 8.40  | 953.83 | 0.40 |      | 945.43 |
| 15    |       |        |      | 5.8  | 48.0   |
| 16    |       |        |      | 2.8  | 51.0   |

5-1-1928

Fair-Warm.

R.R. in T.P. 75' Rt.

± Larpenteur Ave.

Shoulder Larp Ave.

Top of Slope

{ D. Weber &  
M.A. Bealon  
Haeusler  
Thompson

Toe of Slope

East Shoulder

± Pavement Lexington Ave

West Shoulder

Toe of Slope

-376 +

Top of Stake Sta. 11+00

| Sta.  | +     | H.I.   | -     | Rod  | Elev.  |
|-------|-------|--------|-------|------|--------|
| 17+00 |       | 953.83 |       | 2.1  | 51.7   |
| 18+00 |       |        |       | 38   | 50.0   |
| 19    |       |        |       | 12.3 | 41.5   |
| T.P.  | 1.29  | 943.72 | 11.40 |      | 942.43 |
| 20    |       |        |       | 8.1  | 35.6   |
| 21    |       |        |       | 10.2 | 33.5   |
| 22    |       |        |       | 10.3 | 33.4   |
| 23    |       |        |       | 12.2 | 31.5   |
| T.P.  | 10.40 | 942.37 | 11.75 |      | 931.97 |
| 24    |       |        |       | 9.4  | 33.0   |
| 25    |       |        |       | 4.4  | 38.0   |
| T.P.  | 9.72  | 951.51 | 0.58  |      | 941.79 |
| 26    |       |        |       | 8.9  | 42.6   |
| 27    |       |        |       | 6.3  | 45.2   |
| 28    |       |        |       | 5.3  | 46.2   |
| 29    |       |        |       | 5.5  | 46.0   |
| 30    |       |        |       | 3.4  | 48.1   |
| B.M.  | 1.13  | 949.10 | 3.54  |      | 947.97 |
| 31    |       |        |       | 1.1  | 48.0   |
| 32    |       |        |       | 5.3  | 43.8   |
| +55   |       |        |       | 7.0  | 42.1   |
| 33+00 |       |        |       | 9.0  | 40.1   |
| +61   |       |        |       | 9.2  | 39.9   |
| +70   |       |        |       | 6.8  | 42.3   |
| +89   |       |        |       | 6.6  | 42.5   |
| 34    |       |        |       | 6.9  | 42.2   |



5-1-28

Fair-Warm

D.W.

Beaton

Haeussler

Thompson

Top Stake Sta. 19+00

Top of Stake Sta. 23+00

Guy Pole 200' East Sta. 32+55.4

Toe of Slope

So. Shoulder

& Co. Rd. A. 2

| Sta     | +    | H.I.   | -    | Rod  | Elev   |
|---------|------|--------|------|------|--------|
| 34+06.0 |      | 949.10 |      | 7.0  | 42.1   |
| +11.0   |      |        |      | 9.0  | 40.1   |
| 35+00   |      |        |      | 8.4  | 40.7   |
| 36      |      |        |      | 2.7  | 46.4   |
| +50     |      |        |      | 2.4  | 46.7   |
| 37      |      |        |      | 2.4  | 46.7   |
| 38.     |      |        |      | 0.9  | 48.2   |
| T.P.    | 5.70 | 954.50 | 0.30 |      | 948.80 |
| 39      |      |        |      | 3.2  | 51.3   |
| +50     |      |        |      | 3.8  | 50.7   |
| 40      |      |        |      | 5.0  | 49.5   |
| 41      |      |        |      | 5.9  | 48.6   |
| 42      |      |        |      | 6.0  | 48.5   |
| 43      |      |        |      | 2.7  | 51.8   |
| +50     |      |        |      | 1.2  | 53.3   |
| 44      |      |        |      | 2.2  | 52.3   |
| 45      |      |        |      | 5.7  | 48.8   |
| T.P.    | 9.03 | 958.41 | 5.12 |      | 949.38 |
| 46      |      |        |      | 12.5 | 45.9   |
| 47      |      |        |      | 8.7  | 49.7   |
| +38.5   |      |        |      | 9.3  | 49.1   |
| +55     |      |        |      | 7.0  | 51.4   |
| +73.2   |      |        |      | 6.7  | 51.7   |
| +90.6   |      |        |      | 6.9  | 51.5   |
| +97     |      |        |      | 8.8  | 49.6   |
| B.M.    |      |        |      |      | 952.22 |
|         |      |        |      |      | (.20)  |

$$\begin{array}{r}
 63.44 \checkmark \\
 50.62 \checkmark \\
 \hline
 12.82 \checkmark
 \end{array}$$

$$\begin{array}{r}
 952.22 \\
 939.40 \\
 \hline
 12.82 \checkmark
 \end{array}$$

May 1-1928

6.19

Don

5-1-28

Faint + Warm

No. Shoulder Co. Rd. A2

{ D. Weber.

Toe of Slope.

{ M. A. Beaton

{ Haessler

{ Thompson

Top of Stake Sta. 38+00

Top of Stake Sta. 45+00

Toe of Slope

Top Shoulder

± Hamline Ave

Top Shoulder

Toe Slope.

T.P. 5' Rt Sta 48+00.

| Sta   | +    | H.I.   | -    | Red  | Elev.  |
|-------|------|--------|------|------|--------|
| B.M.  | 7.42 | 959.64 |      |      | 952.22 |
| 48+00 |      |        |      | 10.2 | 49.4   |
| 49    |      |        |      | 5.0  | 54.6   |
| +42   |      |        |      | 5.9  | 53.7   |
| 50    |      |        |      | 2.1  | 57.4   |
| +15   |      |        |      | 1.8  | 57.8   |
| 51    |      |        |      | 4.0  | 55.6   |
| 52    |      |        |      | 6.1  | 53.5   |
| 53    |      |        |      | 5.8  | 53.8   |
| 54    |      |        |      | 6.4  | 53.2   |
| T.P.  | 0.0  | 952.90 | 6.74 |      | 952.90 |
| 55    |      |        |      | 3.1  | 49.8   |
| 56    |      |        |      | 5.1  | 47.8   |
| 57    |      |        |      | 5.4  | 47.5   |
| 58    |      |        |      | 6.4  | 46.5   |
| 59    |      |        |      | 7.2  | 45.7   |
| T.P.  | 5.70 | 951.58 | 7.02 |      | 945.88 |
| 60    |      |        |      | 6.4  | 45.2   |
| 61    |      |        |      | 6.1  | 45.5   |
| 62    |      |        |      | 5.0  | 46.6   |
| 63    |      |        |      | 6.2  | 45.4   |
| 64    |      |        |      | 6.8  | 44.8   |
| 65    |      |        |      | 7.2  | 44.4   |
| T.P.  | 6.99 | 951.52 | 7.05 |      | 944.53 |
| 66    |      |        |      | 4.8  | 46.7   |
| 67    |      |        |      | 3.9  | 47.6   |



5-2-28

Cloudy - Warm  
T.P. S' Rt Sta. 4B+00

{ D. Weber  
M.A. Beaton  
Haeasler  
Thompson

Top of Stake Sta. 54+00

|         |      | H.I.                        |            | Rod  | Elev                        |
|---------|------|-----------------------------|------------|------|-----------------------------|
| 67+04.0 |      | 951.52                      |            | 42   | 47.3                        |
| +07.0   |      |                             |            | 61   | 45.4                        |
| +15.0   |      |                             |            | 63   | 45.2                        |
| +23     |      |                             |            | 35   | 48.0                        |
| 39      |      |                             | ± C. Rd B  | 29   | 48.6                        |
| 59      |      |                             |            | 32   | 48.3                        |
| 65      |      |                             |            | 45   | 47.0                        |
| 68+00   |      |                             |            | 39   | 47.6                        |
| B.M.    |      |                             |            |      |                             |
| 69      | 2.99 | <del>953.79</del><br>952.79 | Apr. May 2 | 5.6  | 48.2                        |
| 70      |      |                             | 1.72       | 5.9  | 47.9                        |
| 71      |      |                             |            | 5.6  | 48.2                        |
| 72      |      |                             |            | 4.0  | 49.8                        |
| 73      |      |                             |            | 2.4  | 51.4                        |
| +78     |      |                             |            | 1.0  | 52.8                        |
| 74      |      |                             |            | 3.2  | 50.6                        |
| T.P.    | 7.95 | <del>954.11</del><br>958.11 | 2.63       |      | <del>951.16</del><br>950.16 |
| +80     |      |                             |            | 12.6 | 46.5                        |
| 75      |      |                             |            | 11.0 | 48.1                        |
| +30     |      |                             |            | 6.9  | 52.2                        |
| +72     |      |                             |            | 5.4  | 53.7                        |
| +82     |      |                             |            | 3.7  | 55.4                        |
| +95     |      |                             |            |      | 759.91                      |
| 76      |      |                             |            | 00   | 59.1                        |
| +33     |      |                             |            | 8.4  | 50.7                        |
| +88     |      |                             |            | 11.2 | Water 47.9                  |
| 77      |      |                             |            |      |                             |

2253  
20.11  
2.42 ✓

95222  
949.80 ✓  
2.42

949.80 ✓  
950.79 ✓  
48.2

5-2-28  
Cloudy - Warm

{ D. Weber.  
M.A. Beaton  
Haeuser  
Thompson }

R.R. spk. in 12" B.O. 5' Rt. Sta. 68+57.5

5-3-28  
Cloudy - Cool

D. Weber  
Beaton  
Thompson  
Wheeler

Top Slake Sta. 74+00

So. Edge of Pond.

|            |      |                                        |      |      |                                        |
|------------|------|----------------------------------------|------|------|----------------------------------------|
| Sta.       | +    | H I ✓                                  | —    |      |                                        |
| 77 + 94    |      | <del>959.11</del><br><del>958.11</del> |      | 11.2 | Water 47.9                             |
| 78         |      |                                        |      | 10.4 | 48.7                                   |
| + 50       |      |                                        |      | 6.4  | 52.7                                   |
| 79         |      |                                        |      | 3.4  | 55.7                                   |
| + 50       |      |                                        |      | 8.9  | 50.2                                   |
| 80         |      |                                        |      | 10.0 | 49.1                                   |
| T.P.       | 3.69 | 953.29<br><del>952.39</del>            | 9.51 |      | <del>949.60</del><br><del>948.70</del> |
| 81         |      |                                        |      | 1.6  | 51.7                                   |
| 82         |      |                                        |      | 2.1  | 51.2                                   |
| + 62       |      |                                        |      | 7.8  | 45.5                                   |
| 83         |      |                                        |      | 8.1  | 45.2                                   |
| 84         |      |                                        |      | 4.5  | 48.8                                   |
| + 50       |      |                                        |      | 2.6  | 50.7                                   |
| 85         |      |                                        |      | 3.5  | 49.8                                   |
| T.P.       | 7.10 | 957.30<br><del>956.40</del>            | 3.09 |      | <del>950.20</del><br><del>949.30</del> |
| + 75       |      |                                        |      | 10.6 | 46.7                                   |
| 86         |      |                                        |      | 10.3 | 47.0                                   |
| 87         |      |                                        |      | 5.9  | 51.4                                   |
| + 30       |      |                                        |      | 5.6  | 51.7                                   |
| 88         |      |                                        |      | 8.7  | 48.6                                   |
| 89         |      |                                        |      | 7.8  | 49.5                                   |
| +          |      |                                        |      | 2.8  | 54.5                                   |
| 89 + 33.65 |      |                                        |      | 2.0  | 55.3                                   |
| + 60       |      |                                        |      | 2.5  | 54.8                                   |
| + 71       |      |                                        |      | 5.9  | 51.4                                   |
| B.M.       |      |                                        | 3.79 |      | <del>953.51</del><br><del>952.61</del> |



5-3-28

Cloudy. Cool  
No Edge of Pond.

D. Weber  
Beaton  
Thompson  
Wheeler

Top of Stake Sta. 80+00

Top Stake Sta. 85+00  
→

Toe of Slope

Top of Shoulder So.

≠ Spelling

Top of Shoulder No.

Toe of Slope.

Spike on Stump. 89+80-6' R4.

| Sta.   | +     | H.I.                        | -     | Rod  | Elev.                       |
|--------|-------|-----------------------------|-------|------|-----------------------------|
| B.M.   | 10.14 | <del>963.65</del><br>962.75 |       |      | <del>953.51</del><br>952.61 |
| 90     |       |                             |       | 11.2 | 52.5                        |
| +85    |       |                             |       | 10.5 | 53.2                        |
| 91     |       |                             |       | 8.4  | 55.3                        |
| +35    |       |                             |       | 6.2  | 57.5                        |
| 92     |       |                             |       | 7.1  | 56.6                        |
| 93     |       |                             |       | 3.7  | 60.0                        |
| 94     |       |                             |       | 6.7  | 57.0                        |
| 95     |       |                             |       | 5.2  | 57.5                        |
| 96     |       |                             |       | 0.6  | 63.1                        |
| T.P.   | 1.90  | <del>965.13</del><br>964.23 | 0.42  |      | <del>963.23</del><br>962.33 |
| 97     |       |                             |       | 0.0  | 65.1                        |
| +30    |       |                             |       | 0.4  | 64.7                        |
| 98     |       |                             |       | 5.1  | 60.0                        |
| +40    |       |                             |       | 6.7  | 58.4                        |
| 99     |       |                             |       | 4.6  | 60.5                        |
| +60    |       |                             |       | 5.2  | 59.9                        |
| 100+00 |       |                             |       | 8.2  | 56.9                        |
| T.P.   | 0.48  | <del>955.84</del><br>954.14 | 9.77  |      | <del>955.36</del><br>954.46 |
| 101    |       |                             |       | 11.6 | 44.2                        |
| +70    |       |                             |       | 10.7 | 35.6                        |
| T.P.   | 1.33  | <del>946.25</del><br>944.35 | 10.92 |      | <del>944.92</del><br>944.02 |
| 102    |       |                             |       | 12.3 | 34.0                        |
| 103    |       |                             |       | 17.1 | 29.2                        |
| 104    |       |                             |       | 13.7 | 32.6                        |
| 105    |       |                             |       | 12.7 | 33.6                        |

5-4-28

Fair - Cool

Spike on Stump 89+80, 6' Rt.

{ Weber  
Beaton  
Thompson  
Wheeler

Top Stake Sta. 96+00

|       |      |                                                  |       |      |                                                  |
|-------|------|--------------------------------------------------|-------|------|--------------------------------------------------|
| Sta.  | +    | H.T.                                             | -     | Rod  | Elev                                             |
| 106.  |      | <del>946.25</del><br><del>945.35</del><br>938.15 |       | 12.1 | <del>934.15</del><br><del>933.25</del><br>934.35 |
| T.P.  | 3.80 | <del>937.25</del>                                | 11.90 |      | <del>933.75</del>                                |
| 107   |      |                                                  |       | 2.5  | 35.7                                             |
| +50   |      |                                                  |       | 2.1  | 36.1                                             |
| 108   |      |                                                  |       | 3.2  | 35.0                                             |
| 9     |      |                                                  |       | 1.3  | 36.9                                             |
| 10    |      |                                                  |       | 2.0  | 36.2                                             |
| 11    |      |                                                  |       | 0.6  | 37.6                                             |
| 12    |      |                                                  |       | 2.6  | 35.6                                             |
| T.P.  | 1.39 | <del>937.11</del><br><del>936.21</del>           | 2.43  |      | <del>935.72</del><br><del>934.82</del>           |
| +85   |      |                                                  |       | 3.6  | 33.5                                             |
| 13    |      |                                                  |       | 2.0  | 35.1                                             |
| +70   |      |                                                  |       | 0.0  | 37.1                                             |
| 14    |      |                                                  |       | 1.7  | 35.4                                             |
| +60   |      |                                                  |       | 5.7  | 31.4                                             |
| 15    |      |                                                  |       | 7.2  | 29.9                                             |
| +54.5 |      |                                                  |       | 8.4  | 28.7                                             |
| 16    |      |                                                  |       | 13.3 | 23.8                                             |
| T.P.  | 0.92 | <del>926.74</del><br><del>925.84</del>           | 11.29 |      | <del>925.82</del><br><del>924.92</del>           |
| 17    |      |                                                  |       | 7.3  | 19.4                                             |
| -18   |      |                                                  |       | 8.6  | 18.1                                             |
| 119   |      |                                                  |       | 8.1  | 18.6                                             |
| +02   |      |                                                  |       | 8.1  | 18.6                                             |
| +04   |      |                                                  |       | 9.8  | 16.9                                             |
| +08   |      |                                                  |       | 8.4  | 18.3                                             |



5-4-28

Top Stake Sta. 106+00

Top of Stake Sta. 112+00

Fence Line

Rock 115+85' 2' Lt.

± Ditch

| Sta.   | +     | H.T.                                   | -    | Rd   | Elev.                       |
|--------|-------|----------------------------------------|------|------|-----------------------------|
|        |       | <del>926.74</del><br><del>925.84</del> |      |      |                             |
| 120+00 |       |                                        |      | 9.3  | 17.4                        |
| 21     |       |                                        |      | 9.8  | 16.9                        |
| 22     |       |                                        |      | 8.2  | 18.5                        |
| T.P.   | 12.12 | 930.87<br><del>929.97</del>            | 7.99 |      | 916.75<br><del>917.85</del> |
| +15    |       |                                        |      | 11.9 | 19.0                        |
| +85    |       |                                        |      | 6.0  | 24.9                        |
| 23     |       |                                        |      | 5.5  | 25.4                        |
| +45    |       |                                        |      | 5.4  | 25.5                        |
| 24     |       |                                        |      | 9.1  | 21.8                        |
| +10    |       |                                        |      | 9.6  | 21.3                        |
| +30    |       |                                        |      | 8.8  | 22.1                        |
| +90    |       |                                        |      | 12.7 | 18.2                        |
| 125+00 |       |                                        |      | 12.3 | 18.6                        |
| 26     |       |                                        |      | 4.2  | 26.7                        |
| +15    |       |                                        |      | 3.8  | 27.1                        |
| +50    |       |                                        |      | 6.1  | 24.8                        |
| T.P.   | 8.32  | 938.87<br><del>937.97</del>            | 0.32 |      | 930.55<br><del>929.65</del> |
| 127+00 |       |                                        |      | 3.3  | 35.6                        |
| +25    |       |                                        |      | 2.2  | 36.7                        |
| +90    |       |                                        |      | 3.7  | 35.2                        |
| 128    |       |                                        |      | 2.9  | 36.0                        |
| +33    |       |                                        |      | 1.3  | 37.6                        |
| 129    |       |                                        |      | 4.9  | 34.0                        |
| 130    |       |                                        |      | 10.7 | 28.2                        |

5-4-28

Top Stake Sta. 122+00

| Sta.             | +    | HI<br><del>938.87</del><br><del>937.75</del> | -     | Pod  | Elev                                   |
|------------------|------|----------------------------------------------|-------|------|----------------------------------------|
| 130 + 95         |      |                                              |       | 8.4  | 30.5                                   |
| 131 + 00         |      |                                              |       | 6.5  | 32.4                                   |
| 04               |      |                                              |       | 5.5  | 33.4                                   |
| 09.              |      |                                              |       | 5.4  | 33.5                                   |
| 18.5             |      |                                              |       | 5.5  | 33.4                                   |
|                  |      |                                              |       | 5.9  | 33.0                                   |
|                  |      |                                              |       | 5.9  | 33.0                                   |
|                  |      |                                              |       | 10.5 | 28.4                                   |
| B.M.             | 4.74 | <del>936.79</del><br><del>935.89</del>       | 6.82  |      | <del>932.05</del><br><del>931.15</del> |
| 131 + 80 (Water) |      |                                              |       | 10.2 | 26.6                                   |
| 32 + 80          |      |                                              |       | 9.8  | 27.0                                   |
| 33               |      |                                              |       | 8.2  | 28.6                                   |
| 34               |      |                                              |       | 7.5  | 29.3                                   |
| + 50             |      |                                              |       | 5.9  | 30.9                                   |
| 35               |      |                                              |       | 0.5  | 36.3                                   |
| + 35             |      |                                              |       | 0.0  | 36.8                                   |
| + 72             |      |                                              |       | 3.3  | 33.5                                   |
| 36               |      |                                              |       | 4.4  | 32.4                                   |
| + 77             |      |                                              |       | 0.7  | 36.1                                   |
| 37               |      |                                              |       | 5.3  | 31.5                                   |
| T.P.             | 3.64 | <del>929.74</del><br><del>928.84</del>       | 10.69 |      | <del>926.10</del><br><del>925.20</del> |
| + 22             |      |                                              |       |      | 929.84                                 |
| + 36             |      |                                              |       | 5.4  | 24.3                                   |
| + 45             |      |                                              |       | 3.52 | 26.2                                   |
| + 58             |      |                                              |       | 4.8  | 24.9                                   |
| + 64             |      |                                              |       | 3.0  | 26.7                                   |



5-4-28

Clear-Cool

Toe of Slope

Top Shoulder

Edge of Pavement

± Pavement New Brighton Road.

Edge of Pavement

Top of Shoulder

Toe of Slope.

Top of C.M.P. 12" 50' Lt. Sta. 131+26.63 ± Pave.

Fair (Windy)

7/11/28

Weber  
Thompson  
Wheeler  
Kinster

Top of Cut.

Toe of Cut

Top of No. Rail "N.P."

Toe of Cut

Top of Cut

| Sta.         | +5   | 1/2 I.                      | -5   | Rod  | Elev.                       |
|--------------|------|-----------------------------|------|------|-----------------------------|
| 138+00       |      | <del>929.74</del><br>928.64 |      | 7.5  | 22.2                        |
| +24          |      |                             |      | 8.5  | 21.2                        |
| +33          |      |                             |      | 5.6  | 24.1                        |
| +55          |      |                             |      | 5.3  | 24.4                        |
| No. Shoulder |      |                             |      | 5.8  | 23.9                        |
| +62          |      |                             |      | 10.0 | 19.7                        |
| 139          |      |                             |      | 10.1 | 19.6                        |
| 140          |      |                             |      | 10.3 | 19.4                        |
| +50          |      |                             |      | 9.8  | 19.9                        |
| +90          |      |                             |      | 8.2  | 21.5                        |
| 41           |      |                             |      | 7.2  | 22.5                        |
| +23          |      |                             |      | 5.8  | 23.9                        |
| 142          |      |                             |      | 7.9  | 21.8                        |
| 43           |      |                             |      | 7.6  | 22.1                        |
| 44           |      |                             |      | 8.6  | 21.1                        |
| T.P.         | 0.90 | <del>922.52</del><br>921.62 | 8.52 |      | <del>921.22</del><br>920.32 |
| 145          |      |                             |      | 6.2  | 15.9                        |
| +17          |      |                             |      | 6.5  | 15.6                        |
| +21          |      |                             |      | 9.4  | 12.7                        |
| +30          |      |                             |      | 5.3  | 16.8                        |
| 146          |      |                             |      | 6.4  | 15.7                        |
| +75          |      |                             |      | 12.7 | 09.4                        |
| 148+20       |      |                             |      | 12.7 | 09.4                        |
| +50          |      |                             |      | 11.5 | 10.6                        |
| +70          |      |                             |      | 9.7  | 12.4                        |
| 149          |      |                             |      | 10.2 | 11.9                        |
| 150          |      |                             |      | 11.0 | 11.1                        |

Toe of Slope

Top of Shoulder

£ Co. Rd. "C"

Top of Shoulder.

Toe of Shoulder.

Edge of Ditch

£ " "

Edge of "

Edge of Swamp

" " "

|        |       |                   |                  |      |                   |
|--------|-------|-------------------|------------------|------|-------------------|
| 578.   | +5    | <del>923.66</del> | <del>10.78</del> | Red  | <del>911.34</del> |
| T.P.   | 12.32 | <del>922.76</del> | 10.78            |      | <del>910.44</del> |
| 151    |       |                   |                  | 13.8 | 09.9              |
| 152    |       |                   |                  | 10.8 | 12.9              |
| +60    |       |                   |                  | 4.8  | 18.9              |
| T.P.   | 7.15  | <del>930.37</del> | <del>0.44</del>  |      | <del>923.22</del> |
| 153    |       |                   |                  | 6.3  | 24.1              |
| 54     |       |                   |                  | 16.0 | 14.4              |
| 155    |       |                   |                  | 16.5 | 13.9              |
| 156    |       |                   |                  | 12.2 | 18.2              |
| +50    |       |                   |                  | 5.2  | 25.2              |
| 157    |       |                   |                  | 3.0  | 27.4              |
| +35    |       |                   |                  | 3.8  | 26.6              |
| 158    |       |                   |                  | 10.5 | 19.9              |
| +40    |       |                   |                  | 12.0 | 18.4              |
| 159    |       |                   |                  | 9.4  | 21.0              |
| 60     |       |                   |                  | 6.6  | 23.8              |
| T.P.   | 5.90  | <del>929.63</del> | <del>6.64</del>  |      | <del>923.73</del> |
| 161    |       |                   |                  | 2.8  | 26.8              |
| 62     |       |                   |                  | 3.0  | 26.6              |
| 63     |       |                   |                  | 4.0  | 25.6              |
| 164    |       |                   |                  | 5.2  | 24.4              |
| +92    |       |                   |                  | 11.2 | 18.4              |
| 165    |       |                   |                  | 12.9 | 16.7              |
| B.M.   | 0.49  | <del>917.93</del> | <del>12.19</del> |      | <del>917.44</del> |
| +17    |       |                   |                  | 4.2  | 13.7              |
| +40    |       |                   |                  | 11.3 | 06.6              |
| T.P.   | 0.40  | <del>907.31</del> | <del>11.02</del> |      | <del>906.91</del> |
| 166+00 |       |                   |                  | 5.6  | 901.7             |



Edge of Woods

2 Nails in Stump 30' Lt Sta. 164 + 05

| Sta.   | + 5   | HI.                                    | - 5  | Rod  | Elev.                                  |
|--------|-------|----------------------------------------|------|------|----------------------------------------|
| 167+00 |       | <del>907.31</del><br><del>106.41</del> |      | 8.8  | 98.5                                   |
| 169+20 |       |                                        |      | 8.8  | 98.5                                   |
| +28    |       |                                        |      | 10.0 | 97.3                                   |
| +33    |       |                                        |      | 8.6  | 98.7                                   |
| 170+00 |       |                                        |      | 7.8  | 99.5                                   |
| 171    |       |                                        |      | 5.9  | 901.4                                  |
| 172    |       |                                        |      | 4.4  | 02.9                                   |
| 173    |       |                                        |      | 4.9  | 02.4                                   |
| +15    |       |                                        |      | 6.5  | 900.8                                  |
| +25    |       |                                        |      | 3.8  | 03.5                                   |
| +40    |       |                                        |      | 3.3  | 04.0                                   |
| B.M.   | 8.26  | <del>910.93</del><br><del>110.03</del> | 4.64 |      | <del>902.67</del><br><del>101.77</del> |
| +70    |       |                                        |      | 7.1  | 03.8                                   |
| +80    |       |                                        |      | 10.1 | 900.8                                  |
| 174+00 |       |                                        |      | 9.0  | 901.3                                  |
| +14    |       |                                        |      | 6.7  | 04.2                                   |
| 175    |       |                                        |      | 5.6  | 05.3                                   |
| 176    |       |                                        |      | 6.4  | 04.5                                   |
| 77     |       |                                        |      | 7.8  | 03.1                                   |
| 78     |       |                                        |      | 6.6  | 04.3                                   |
| 79     |       |                                        |      | 5.1  | 05.8                                   |
| 180    |       |                                        |      | 2.7  | 08.2                                   |
| T.P.   | 11.34 | <del>920.42</del><br><del>911.50</del> | 1.85 |      | <del>907.08</del><br><del>70.818</del> |
| 181    |       |                                        |      | 9.0  | 11.4                                   |
| 82     |       |                                        |      | 7.6  | 12.8                                   |
| 83     |       |                                        |      | 6.7  | 13.7                                   |

35.54  
 981.15  
 901.77  
 2938  
 64.92  
 35.54  
 2938  
 (Don)

So. Edge Swamp

No. Edge " also Edge of Ditch  
± Ditch

" " "

Toe of Slope:

90177

826

Top of Shoulder

91003

± Cleveland Ave.

Spike in T.P. 2' Rt. Sta. 173+10

#24

W. Shoulder

Weber

Toe Slope

Thompson

Fair & Warm.

Wheeler

Kinstler

5/14/28

Top Stake Sta. 180+00

| Sta.   | + s  | H.I.                                   | - s   | Rod  | Elev.                                  |
|--------|------|----------------------------------------|-------|------|----------------------------------------|
| 184+00 |      | <del>920.42</del><br><del>919.52</del> |       | 4.3  | 16.1                                   |
| 85     |      |                                        |       | 1.5  | 18.9                                   |
| T.P.   | 8.30 | <del>927.37</del><br><del>926.47</del> | 1.35  |      | <del>919.07</del><br><del>918.17</del> |
| 186    |      |                                        |       | 6.9  | 20.5                                   |
| 87     |      |                                        |       | 4.6  | 22.8                                   |
| 188    |      |                                        |       | 4.0  | 23.4                                   |
| +33    |      |                                        |       | 3.8  | 23.6                                   |
| 189    |      |                                        |       | 6.4  | 21.0                                   |
| +50    |      |                                        |       | 8.8  | 18.6                                   |
| 190    |      |                                        |       | 9.4  | 18.0                                   |
| 91     |      |                                        |       | 11.4 | 16.0                                   |
| 92     |      |                                        |       | 11.7 | 15.7                                   |
| T.P.   | 3.33 | <del>919.20</del><br><del>918.30</del> | 11.50 |      | <del>915.87</del><br><del>914.97</del> |
| 93     |      |                                        |       | 3.4  | 15.8                                   |
| +34    |      |                                        |       | 3.0  | 16.2                                   |
| 94     |      |                                        |       | 5.6  | 13.6                                   |
| +28    |      |                                        |       | 6.1  | 13.1                                   |
| 95     |      |                                        |       | 3.6  | 15.6                                   |
| +62    |      |                                        |       | 0.6  | 18.6                                   |
| 96     |      |                                        |       | 2.2  | 17.0                                   |
| +50    |      |                                        |       | 3.8  | 15.4                                   |
| +75    |      |                                        |       | 6.7  | 18.5                                   |
| +94    |      |                                        |       | 6.1  | 13.1                                   |
| 197+05 |      |                                        |       | 11.5 | 07.7                                   |
| +14.2  |      |                                        |       | 9.58 | 09.62                                  |
| +21    |      |                                        |       | 9.61 | 09.59                                  |



Top Stake Sta. 185+00

Top Stake Sta. 192

Top of Cut R.R.  
Top of Slope  
East Rail  
West Rail.

| Sta.   | + S   | H.T.                                   | - S  | Rod  | Elev.                                  |
|--------|-------|----------------------------------------|------|------|----------------------------------------|
| 197    |       | <del>919.20</del><br><del>918.30</del> |      |      |                                        |
| +28.6  |       |                                        |      | 11.4 | 07.8                                   |
| +38    |       |                                        |      | 8.8  | 10.4                                   |
| 198+00 |       |                                        |      | 12.1 | 07.1                                   |
| 99     |       |                                        |      | 15.0 | 04.2                                   |
| T.P.   | 3.24  | <del>911.54</del><br><del>910.64</del> | 10.9 |      | <del>908.30</del><br><del>907.40</del> |
| +09.   |       |                                        |      | 7.2  | 04.3                                   |
| +12    |       |                                        |      | 9.6  | 901.9                                  |
| +15    |       |                                        |      | 6.8  | 04.7                                   |
| 200+00 |       |                                        |      | 6.5  | 05.0                                   |
| 01     |       |                                        |      | 5.6  | 05.9                                   |
| 02     |       |                                        |      | 5.5  | 06.0                                   |
| 03     |       |                                        |      | 4.0  | 07.5                                   |
| 04     |       |                                        |      | 1.7  | 09.8                                   |
| T.P.   | 12.38 | <del>922.34</del><br><del>921.44</del> | 1.58 |      | <del>909.96</del><br><del>909.</del>   |
| 205+00 |       |                                        |      | 10.5 | 11.8                                   |
| 206    |       |                                        |      | 6.1  | 16.2                                   |
| +42    |       |                                        |      | 2.4  | 19.9                                   |
| +47    |       |                                        |      | 5.4  | 16.9                                   |
| +81    |       |                                        |      | 1.9  | 20.4                                   |
| 207+00 |       |                                        |      | 2.2  | 20.1                                   |
| +05.   |       |                                        |      | 4.0  | 18.3                                   |
| T.P.   | 12.10 | <del>934.01</del><br><del>933.44</del> | 0.43 |      | <del>924.91</del><br><del>924.44</del> |
| +23    |       |                                        |      | 7.0  | 27.0                                   |
| 208+00 |       |                                        |      | 4.6  | 29.4                                   |
| +05.   |       |                                        |      | 3.7  | 30.3                                   |

Toe of Slope  
Top of Cut.

Edge Ditch

Edge "

Top Sta. 204 + 00

R/W Fence

Toe Slope

Co Rd. "D"

Toe Slope

Top Sl

| Sta.       | + s  | H.I.                                   | - s                                  | Pod   | Elev.                                  |
|------------|------|----------------------------------------|--------------------------------------|-------|----------------------------------------|
|            |      | <del>934.01</del><br><del>933.11</del> |                                      |       |                                        |
| 209+00     |      | 58.95<br>27.71<br>31.24 ✓              | 27.71<br>933.01<br>901.77<br>31.24 ✓ | 1.7   | 32.3                                   |
| + 47.8     |      |                                        |                                      | 0.7   | 33.3                                   |
| T.P.       | 7.83 | <del>941.74</del><br><del>940.81</del> | 0.10                                 |       | <del>932.91</del><br><del>932.01</del> |
| + 52       |      |                                        |                                      | 3.0   | 38.7                                   |
| 210        |      |                                        |                                      | 4.1   | 37.6                                   |
| + 48       |      |                                        |                                      | 2.7   | 39.0                                   |
| 211        |      |                                        |                                      | 5.4   | 36.3                                   |
| + 65 ✓     |      |                                        |                                      | 4.1   | 37.6                                   |
| 212        |      |                                        |                                      | 5.6   | 36.1                                   |
| 13         |      |                                        |                                      | 11.6  | 30.1                                   |
| + 30       |      |                                        |                                      | 11.5  | 30.2                                   |
| 214        |      |                                        |                                      | 6.6   | 35.1                                   |
| 215        |      |                                        |                                      | 4.8   | 36.9                                   |
| T.P.       | 5.33 | <del>944.93</del><br><del>944.03</del> | 2.14                                 |       | <del>939.60</del><br><del>938.70</del> |
| + 23       |      |                                        |                                      | 6.9   | 38.0                                   |
| + 32       |      |                                        |                                      | 4.5   | 40.4                                   |
| + 66       |      |                                        |                                      | 4.6   | 40.3                                   |
| 216 + 05.0 |      |                                        |                                      | 7.2   | 37.7                                   |
| + 12       |      |                                        |                                      | 7.0   | 37.9                                   |
| + 23       |      |                                        |                                      | 9.7   | 35.2                                   |
| + 42       |      |                                        |                                      | - 1.0 | <del>945.93</del><br><del>945.03</del> |
| 217        |      |                                        |                                      | 2.4   | 42.5                                   |
| 218        |      |                                        |                                      | 2.0   | 42.9                                   |
| 219        |      |                                        |                                      | 4.9   | 40.0                                   |
| + 08.      |      |                                        |                                      | 5.2   | 39.7                                   |
| + 14       |      |                                        |                                      | 9.3   | 35.6                                   |



Cloudy + Warm

5/17/28



D. Weber  
F.P. Thompson  
Wheeler

= Face of Barn

Top Iron Post 20' Lt - 208 + 90

Edge Dr. way

E " Pavement

W. " "

" Shoulder.

Ditch

Top of Cut.

} Long Lake Rd.

Edge Ditch

E ...

| Sta    | + s   | H.I                                    | - s   | Rod | Elev                                   |
|--------|-------|----------------------------------------|-------|-----|----------------------------------------|
| 219+20 |       | <del>944.93</del><br><del>944.03</del> |       | 5.2 | 39.7                                   |
| 220    |       |                                        |       | 5.8 | 39.1                                   |
| 221    |       |                                        |       | 5.2 | 39.7                                   |
| T.P.   | 4.57  | <del>944.45</del><br><del>943.55</del> | 5.05  |     | <del>939.88</del><br><del>938.98</del> |
| +38    |       |                                        |       | 3.7 | 40.8                                   |
| 222    |       |                                        |       | 6.4 | 38.1                                   |
| +8v    |       |                                        |       | 4.9 | 39.6                                   |
| 223    |       |                                        |       | 3.1 | 41.4                                   |
| +15    |       |                                        |       | 2.0 | 42.5                                   |
| +76.5  |       |                                        |       | 1.9 | 42.6                                   |
| +90    |       |                                        |       | 3.5 | 41.0                                   |
| 225    |       |                                        |       | 5.1 | 39.4                                   |
| +57    |       |                                        |       | 5.2 | 39.3                                   |
| +84    |       |                                        |       | 6.0 | 38.5                                   |
| 226    |       |                                        |       | 7.2 | 37.3                                   |
| B.M.   | 4.68. | <del>941.88</del><br><del>940.20</del> | 7.25  |     | <del>937.20</del><br><del>936.30</del> |
| 227    |       |                                        |       | 7.2 | 34.7                                   |
| 228    |       |                                        |       | 7.7 | 34.2                                   |
| +68    |       |                                        |       | 7.6 | 34.3                                   |
| 229    |       |                                        |       | 5.7 | 36.2                                   |
| 30     |       |                                        |       | 1.3 | 40.6                                   |
| 31     |       |                                        |       | 3.1 | 38.8                                   |
| +25    |       |                                        |       | 4.3 | 37.6                                   |
| T.P.   | 1.19  | <del>931.65</del><br><del>930.25</del> | 11.42 |     | <del>930.46</del><br><del>929.06</del> |
| 23v    |       |                                        |       | 4.2 | 27.5                                   |
| T.P.   | 2.01  | <del>921.63</del><br><del>920.73</del> | 12.03 |     | <del>919.62</del><br><del>918.72</del> |

Edge of Ditch

Top of Stake Sta. 221+00

Face of Barn.

Hub. 2" x 2"

Spike in Cor. Barn. - 227+33 - 30' Lt.

| Sta. | + s                                           | H.I.             | - s  | Rd.  | Elev.            |
|------|-----------------------------------------------|------------------|------|------|------------------|
|      |                                               | 921.63<br>920.73 |      |      |                  |
| 233  |                                               |                  |      | 6.9  | 14.7             |
| 234  |                                               |                  |      | 7.8  | 13.8             |
| +76  |                                               |                  |      | 5.3  | 16.3             |
| 235  | 47.56 933.01<br>25.61 911.06<br>(21.95) 21.95 | 47.56            |      | 6.0  | 15.6             |
| 236  |                                               |                  |      | 9.2  | 12.4             |
| B.M. | 0.70 712.66<br>911.70                         | 7.67             |      |      | 911.96<br>911.06 |
| 237  | (Equation)<br>(237 + 47.57 = 237 + 57.57)     |                  |      | 1.3  | 11.4             |
| +40  |                                               |                  |      | 2.2  | 10.5             |
| 238  |                                               |                  |      | 6.8  | 05.9             |
| 239  |                                               |                  |      | 10.2 | 02.5             |
| 240  |                                               |                  |      | 8.6  | 04.1             |
| +58  |                                               |                  |      | 11.3 | 901.4            |
| +60  |                                               |                  |      | 12.0 | 99.7             |
| +63  |                                               |                  |      | 12.0 | 900.7            |
| 241  |                                               |                  |      | 12.7 | 900.0            |
| 242  |                                               |                  |      | 13.0 | 99.7             |
| 243  |                                               |                  |      | 10.8 | 901.9            |
| T.P. | 1.83                                          | 907.16<br>906.26 | 7.33 |      | 905.33<br>904.43 |
| 244  |                                               |                  |      | 7.7  | 99.5             |
| 245  |                                               |                  |      | 7.5  | 99.7             |
| 246  |                                               |                  |      | 7.6  | 99.6             |
| 247  |                                               |                  |      | 4.4  | 02.8             |
| 248  |                                               |                  |      | 8.2  | 99.0             |
| 249  |                                               |                  |      | 8.9  | 98.3             |
| 250  |                                               |                  |      | 8.9  | 98.3             |



Top of Boulder 136+80.  $\pm$

Cloudy + Rainy  
5/18-28.

D. Weber  $\pi$   
F.P. Thompson  
Wheeler.

Edge Ditch

$\pm$  "

Edge Ditch

| Sta.   | + s   | H.I.                                   | - s  | Pod. | Elev.                                  |
|--------|-------|----------------------------------------|------|------|----------------------------------------|
|        |       | <del>907.16</del><br><del>906.26</del> |      |      |                                        |
| 250+88 |       |                                        |      | 5.5  | 901.7                                  |
| 251    |       |                                        |      | 8.1  | 99.1                                   |
| T.P.   | 12.50 | <del>919.07</del><br><del>910.17</del> | 0.59 |      | <del>906.57</del><br><del>905.17</del> |
| +72    |       |                                        |      | 1.4  | 17.7                                   |
| +75    |       |                                        |      | 0.74 | 18.4                                   |
| +95    |       |                                        |      | 0.49 | 18.6                                   |
| 252    |       |                                        |      | 1.0  | 18.1                                   |
| +20    |       |                                        |      | 15.5 | 03.6                                   |
| +72    |       |                                        |      | 15.0 | 04.1                                   |
| 253    |       |                                        |      | 12.0 | 07.1                                   |
| 254    |       |                                        |      | 3.2  | 15.9                                   |
| T.P.   | 11.26 | <del>929.60</del><br><del>928.70</del> | 0.75 |      | <del>918.34</del><br><del>917.44</del> |
| 255    |       |                                        |      | 11.8 | 17.8                                   |
| +31    |       |                                        |      | 12.4 | 17.2                                   |
| 256    |       |                                        |      | 9.0  | 20.6                                   |
| 257    |       |                                        |      | 5.4  | 24.2                                   |
| T.P.   | 12.45 | <del>941.35</del><br><del>940.45</del> | 0.70 |      | <del>928.90</del><br><del>928.00</del> |
| +30    |       |                                        |      | 16.0 | 25.4                                   |
| +32    |       |                                        |      | 14.0 | 27.4                                   |
| 258    |       |                                        |      | 10.5 | 20.9                                   |
| 259    |       |                                        |      | 2.2  | 39.2                                   |
| 260    |       |                                        |      | 0.3  | 41.1                                   |
| T.P.   | 11.74 | <del>952.94</del><br><del>952.04</del> | 0.15 |      | <del>941.20</del><br><del>940.20</del> |
| 261    |       |                                        |      | 9.6  | 43.3                                   |
| 262    |       |                                        |      | 5.6  | 47.3                                   |
| T.P.   | 12.44 | <del>964.82</del><br><del>963.92</del> | 0.56 |      | <del>952.38</del><br><del>951.48</del> |

Top Stake 251+54 -  $\frac{1}{2}$  = Toe of R.R. Fill (East)

Top of Fill

Top of East Rail } 500 Line.

" " W. Rail

Toe of Slope R.R. (West)

Top Stake Sta. 260+00

Fig Sheet

| Sta.   | + s   | HT                                     | - s   | Rod  | Elev.                                  |
|--------|-------|----------------------------------------|-------|------|----------------------------------------|
|        |       | <del>964.82</del><br><del>963.92</del> |       |      |                                        |
| 263+00 |       |                                        |       | 6.7  | 58.1                                   |
| T.P.   | 7.12  | <del>971.83</del><br><del>970.92</del> | 0.11  |      | <del>964.71</del><br><del>963.81</del> |
| 264    |       |                                        |       | 3.7  | 68.1                                   |
| +40    |       |                                        |       | 0.4  | 71.4                                   |
| 265    |       |                                        |       | 4.9  | 66.9                                   |
| 266    |       |                                        |       | 14.0 | 57.8                                   |
| T.P.   | 2.55  | <del>961.89</del><br><del>960.99</del> | 12.49 |      | <del>959.34</del><br><del>958.44</del> |
| 267    |       |                                        |       | 7.8  | 54.1                                   |
| +50    |       |                                        |       | 8.2  | 53.7                                   |
| 268    |       |                                        |       | 7.8  | 54.1                                   |
| 269    |       |                                        |       | 7.0  | 54.9                                   |
| +30    |       |                                        |       | 6.0  | 55.9                                   |
| 270    |       |                                        |       | 8.6  | 53.3                                   |
| +55    |       |                                        |       | 7.7  | 54.2                                   |
| 271    |       |                                        |       | 4.9  | 57.0                                   |
| B.M.   | 11.48 | <del>972.95</del><br><del>972.05</del> | 0.42  |      | <del>961.47</del><br><del>960.57</del> |
| 272    |       |                                        |       | 5.7  | 67.3                                   |
| +60    |       |                                        |       | 2.0  | 71.0                                   |
| 273.   |       |                                        |       | 5.2  | 67.8                                   |
| T.P.   | 1.11  | <del>964.35</del><br><del>963.45</del> | 9.71  |      | <del>963.24</del><br><del>962.34</del> |
| 274    |       |                                        |       | 13.3 | 51.1                                   |
| +25    |       |                                        |       | 12.5 | 51.9                                   |
| +45    |       |                                        |       | 13.7 | 50.7                                   |
| +55    |       |                                        |       | 17.4 | 47.0                                   |
| +65    |       |                                        |       | 14.1 | 50.3                                   |

$$\begin{array}{r}
 72.59 \\
 23.08 \\
 \hline
 49.51 \\
 \end{array}
 \quad
 \begin{array}{r}
 960.87 \\
 911.06 \\
 \hline
 49.51 \\
 \end{array}
 \quad
 23.08$$



R.R. spike in Oak Swamp 271 + 44.5 - 123' Rt.

Fair & Warm

Feb 28

D. Weber

Boston

Thompson

Wheeler.

Top of Cut

Bottom Ditch

Top of Shoulder

| Sta.   | + s   | H.I.                                   | - s   | Pod. | Elev.                                  |
|--------|-------|----------------------------------------|-------|------|----------------------------------------|
| 274+74 |       | <del>964.35</del><br><del>963.45</del> |       | 13.8 | 50.6                                   |
| +90    |       |                                        |       | 14.1 | 50.3                                   |
| T.P.   | 0.52  | <del>953.94</del><br><del>953.04</del> | 10.93 |      | <del>953.42</del><br><del>952.2</del>  |
| 275    |       |                                        |       | 9.0  | 44.9                                   |
| +08.   |       |                                        |       | 13.2 | 40.7                                   |
| +32    |       |                                        |       | 17.6 | 36.3                                   |
| 276    |       |                                        |       | 18.1 | 35.8                                   |
| 277    |       |                                        |       | 18.2 | 35.7                                   |
| 278    |       |                                        |       | 18.4 | 35.5                                   |
| +45    |       |                                        |       | 17.0 | 36.9                                   |
| 279    |       | <del>965.51</del>                      |       | 8.2  | 45.7                                   |
| T.P.   | 11.86 | <del>964.61</del>                      | .29   |      | <del>953.65</del><br><del>952.75</del> |
| +65    |       |                                        |       | 10.7 | 54.8                                   |
| 280+00 |       |                                        |       | 10.7 | 54.8                                   |
| +55    |       |                                        |       | 14.2 | 51.3                                   |
| 281    |       |                                        |       | 11.9 | 53.6                                   |
| +45    |       |                                        |       | 6.8  | 58.7                                   |
| 282    |       |                                        |       | 5.1  | 60.4                                   |
| 283    |       |                                        |       | 8.1  | 57.4                                   |
| 284    |       |                                        |       | 9.0  | 64.5                                   |
| T.P.   | 11.45 | <del>973.51</del><br><del>972.61</del> | 3.45  |      | <del>962.06</del><br><del>961.16</del> |
| 285    |       |                                        |       | 5.5  | 68.0                                   |
| 286    |       |                                        |       | 6.2  | 67.3                                   |
| +50    |       |                                        |       | 5.8  | 67.7                                   |
| +57    |       |                                        |       | 7.0  | 66.5                                   |
| 287    |       |                                        |       | 7.8  | 65.7                                   |
| +42    |       |                                        |       | 11.9 | 61.6                                   |

2 Co. Rd. E.

Top of Shoulder.

Toe of Slope.

} Swamp.

|        |       |                                        |       |                                        |
|--------|-------|----------------------------------------|-------|----------------------------------------|
|        |       | <del>773.51</del><br><del>772.61</del> |       |                                        |
| T.P.   | 0.08  | <del>962.22</del><br><del>961.32</del> | 11.37 | <del>962.14</del><br><del>961.24</del> |
| 288    |       |                                        | 12.4  | 49.8                                   |
| T.P.   | 0.33  | <del>950.44</del><br><del>949.54</del> | 12.11 | <del>950.11</del><br><del>949.21</del> |
| 289    | 36.83 | 960.57<br>937.42<br>23.15              | 14.0  | 36.4                                   |
| 290    |       | 5999<br>36.83<br>23.15                 | 14.0  | 36.4                                   |
| B.M.   | 4.57  | <del>944.79</del><br><del>942.89</del> | 12.12 | <del>938.32</del><br><del>937.42</del> |
| +50    |       |                                        | 6.2   | 36.7                                   |
| +75    |       |                                        | 8.3   | 34.6                                   |
| 293+20 |       |                                        | 8.3   | 34.6                                   |
| +60    |       |                                        | 6.7   | 36.2                                   |
| 294    |       |                                        | 4.9   | 38.0                                   |
| +50    |       |                                        | 3.3   | 39.6                                   |
| T.P.   | 12.20 | <del>954.45</del><br><del>953.55</del> | 0.64  | <del>942.25</del><br><del>941.35</del> |
| 295    |       |                                        | 10.5  | 44.0                                   |
| +45    |       |                                        | 4.6   | 49.9                                   |
| 296    |       |                                        | 4.8   | 49.6                                   |
| +50    |       |                                        | 6.5   | 48.0                                   |
| +65    |       |                                        | 3.9   | 50.6                                   |
| 297    |       |                                        | 3.7   | 50.8                                   |
| +92    |       |                                        | 2.9   | 51.6                                   |
| 298    |       |                                        | 0.8   | 53.7                                   |
| +07    |       |                                        | 0.8   | 53.7                                   |
| T.P.   | 11.24 | <del>965.23</del><br><del>964.33</del> | 0.46  | <del>953.99</del><br><del>953.09</del> |
| +23    |       |                                        | 4.3   | 60.9                                   |
| +38    |       |                                        | 2.4   | 62.8                                   |
| +53    |       |                                        | 2.4   | 62.8                                   |
| 298+80 |       |                                        | 10.3  | 54.9                                   |



Nail in Top of Stump Sta. 289+45-40' Rt.

Edge of Swamp.

{ D. Weber  $\pi$   
MA Beaton Rd

Fair + Warm 5/26/28

Toe of Slope.

Top of Stake Sta. 298+00

Top of Shoulder

~~to Silver Lake Rd.~~ Fairchild Ave

Top of Shoulder

Toe of Slope.

| Sta.   | + s  | H.T.                                   | - s  | Rad. | Elev.                                  |
|--------|------|----------------------------------------|------|------|----------------------------------------|
|        |      | <del>985.23</del><br><del>964.93</del> |      |      |                                        |
| 299    |      |                                        |      | 10.5 | 54.7                                   |
| +50    |      |                                        |      | 5.5  | 59.7                                   |
| 300+00 |      |                                        |      | 2.7  | 62.5                                   |
| +50    |      |                                        |      | 3.0  | 62.2                                   |
| +90    |      |                                        |      | 0.0  | 65.2                                   |
| T.P.   | 1204 | <del>976.98</del><br><del>976.08</del> | 0.29 |      | <del>964.94</del><br><del>964.84</del> |
| 301.   |      |                                        |      | 10.5 | 66.5                                   |
| +20    |      |                                        |      | 10.0 | 67.0                                   |
| T.P.   | 1197 | <del>988.95</del><br><del>988.05</del> | 0.00 |      | <del>976.98</del><br><del>976.08</del> |
| 302    |      |                                        |      | 7.1  | 81.9                                   |
| +25    |      |                                        |      | 3.5  | 85.5                                   |
| 303    |      |                                        |      | 0.0  | 89.0                                   |
| +60    | ?    |                                        |      |      | <del>291.05</del><br><del>988.57</del> |
| T.P.   | 941  | <del>997.98</del><br><del>997.08</del> | 0.38 |      | <del>987.67</del><br><del>994.47</del> |
| B.M.   |      |                                        | 3.51 |      | <del>992.57</del>                      |
| 304+50 |      |                                        |      | 4.3  | 93.7                                   |
| 305    |      |                                        |      | 8.1  | 89.9                                   |
| T.P.   | 7.35 | <del>996.17</del><br><del>995.27</del> | 9.16 |      | <del>988.82</del><br><del>987.92</del> |
| 306.   |      |                                        |      | 10.8 | 85.4                                   |
| +50    |      |                                        |      | 10.1 | 86.1                                   |
| 307    |      |                                        |      | 12.0 | 84.2                                   |
| +50    |      |                                        |      | 9.2  | 87.0                                   |
| 308    |      |                                        |      | 9.6  | 86.6                                   |
| 309    |      |                                        |      | 6.7  | 89.5                                   |
| 310    |      |                                        |      | 4.0  | 92.2                                   |

= ~~L~~ Cattle Pass

Top of Stake 20' Rt Sta 301 + 00

Edge of Stucco Bldg.

S.E. Cor. Conc. Step. (Laundry Bldg.)  
Edge Barn.

|        |       |                   |       |      |                   |
|--------|-------|-------------------|-------|------|-------------------|
| 310    | +     | 996.17            |       |      |                   |
|        |       | <del>995.27</del> |       |      |                   |
| 310+60 |       |                   |       | 1.3  | 94.9              |
| 311    |       |                   |       | 3.4  | 92.8              |
| 312    |       |                   |       | 6.7  | 89.5              |
| 313    |       | 999.09            |       | 9.9  | 86.3              |
| T.P.   | 12.5  | <del>998.19</del> | 9.58  |      | <del>786.59</del> |
| 314    |       |                   |       | 15.5 | 83.6              |
| 315    |       |                   |       | 14.6 | 85.1              |
| 316    |       |                   |       | 9.6  | 89.5              |
| 317    |       |                   |       | 5.3  | 93.8              |
| 318    |       |                   |       | 6.3  | 92.8              |
| 319    |       |                   |       | 8.2  | 90.9              |
| 320    |       |                   |       | 7.0  | 92.1              |
| +40    |       |                   |       | 4.3  | 94.8              |
| 321    | 81.28 | 993.88            | 24.82 | 6.6  | 92.5              |
| 22     | 24.82 | 937.42            |       | 13.4 | 85.7              |
|        | 56.46 | 56.46             |       |      | <del>774.78</del> |
| T.P.   | 2.32  | 996.2             | 4.31  |      | <del>772.58</del> |
| +90    |       | 997.10            |       | 20.2 | 76.9              |
| 323    |       |                   |       | 18.7 | 78.4              |
| +65    |       |                   |       | 12.1 | 85.0              |
| T.P.   | 4.35  | 990.00            | 11.45 |      | <del>785.65</del> |
| 24     |       | 989.10            |       | 13.2 | 76.8              |
| +15    |       |                   |       | 18.3 | 71.7              |
| +80    |       |                   |       | 18.3 | 71.7              |
| 325    |       |                   |       | 15.1 | 74.9              |
| +75    |       |                   |       | 7.3  | 82.7              |
| 326    |       |                   |       | 7.1  | 82.9              |



Fair + Warm

5/29/28

{ D Weber &  
M.A. Beaton Red

| Sta.      | +     | HT                                     | - s   | Pod. | Elev.                                  |
|-----------|-------|----------------------------------------|-------|------|----------------------------------------|
| 327       |       | <del>990.00</del><br><del>989.10</del> | 1     | 2.4  | 87.6                                   |
| 28        |       | <del>989.77</del>                      |       | 2.0  | 88.0                                   |
| T.P.      | 1.42  | <del>988.87</del>                      | 1.65  |      | <del>988.35</del><br><del>987.44</del> |
| +70       |       |                                        |       | 4.3  | 85.5                                   |
| 329       |       |                                        |       | 2.6  | 87.2                                   |
| +50       |       |                                        |       | 3.2  | 86.6                                   |
| +80       |       |                                        |       | 11.3 | 78.5                                   |
| 330 + 0.5 |       |                                        |       | 11.3 | 78.5                                   |
| +25       |       |                                        |       | 5.5  | 84.3                                   |
| 331       |       |                                        |       | 5.3  | 84.5                                   |
| 332       |       |                                        |       | 5.2  | 84.6                                   |
| 333       |       |                                        |       | 4.9  | 84.9                                   |
| +35       |       |                                        |       | 6.0  | 83.8                                   |
| T.P.      | 2.24  | <del>984.76</del><br><del>983.06</del> | 7.25  |      | <del>982.52</del><br><del>981.62</del> |
| 334       |       |                                        |       | 8.7  | 76.1                                   |
| +30       |       |                                        |       | 15.4 | 69.4                                   |
| +50       |       |                                        |       | 14.4 | 70.4                                   |
| +87.63    |       |                                        |       | 14.6 | 70.2                                   |
| T.P.      | 1.39  | <del>975.05</del><br><del>974.15</del> | 11.10 |      | <del>973.66</del><br><del>972.76</del> |
| 335       |       |                                        |       | 6.4  | 68.7                                   |
| +50       |       |                                        |       | 10.1 | 65.0                                   |
| 336       |       |                                        |       | 5.9  | 69.2                                   |
| 337       |       |                                        |       | 2.4  | 72.7                                   |
| 338       |       |                                        |       | 11.9 | 63.2                                   |
| 339       |       |                                        |       | 7.9  | 67.2                                   |
| T.P.      | 12.48 | <del>980.28</del><br><del>979.38</del> | 7.25  |      | <del>967.80</del><br><del>966.90</del> |

Top Stake Sta 328+00

West Co. Line.

Top Stake 4' R4 Sta. 339+50

| Sta.   |       | H.T.                                     |       | P.A  | Elev                                     |
|--------|-------|------------------------------------------|-------|------|------------------------------------------|
| 339+50 |       | <del>980.28</del><br><del>979.32</del>   |       | 10.8 | 69.5                                     |
| 340    |       |                                          |       | 2.4  | 77.9                                     |
| T.P.   | 10.15 | <del>990.31</del><br><del>989.41</del>   | 0.12  |      | <del>980.16</del><br><del>979.26</del>   |
| +45    |       |                                          |       | 1.2  | 89.1                                     |
| +60    |       |                                          |       | 0.0  | 90.3                                     |
| 341    |       |                                          |       | 1.0  | 89.3                                     |
| 342    |       |                                          |       | 6.6  | 83.7                                     |
| 343    |       |                                          |       | 9.9  | 80.4                                     |
| 344    |       |                                          |       | 0.0  | 90.3                                     |
| T.P.   | 12.38 | <del>1001.69</del><br><del>1000.79</del> | 1.0   |      | <del>989.31</del><br><del>988.41</del>   |
| B.M.   |       |                                          | 10.4  |      | <del>991.29</del><br><del>990.39</del>   |
| +55    |       |                                          |       | 9.7  | 92.0                                     |
| 345    |       |                                          |       | 3.3  | 98.4                                     |
| T.P.   | 12.06 | <del>1013.13</del><br><del>1012.23</del> | 0.62  |      | <del>1001.07</del><br><del>1000.17</del> |
| +50    |       |                                          |       | 6.2  | 06.9                                     |
| 346    |       |                                          |       | 3.1  | 10.0                                     |
| 347    |       |                                          |       | 2.7  | 10.4                                     |
| 348    |       |                                          |       | 5.1  | 08.0                                     |
| +45    |       |                                          |       | 8.5  | 04.6                                     |
| 349    |       |                                          |       | 18.8 | 94.3                                     |
| T.P.   | 0.07  | <del>1001.65</del><br><del>1000.75</del> | 11.55 |      | <del>1001.58</del><br><del>1000.68</del> |
| T.P.   | 0.02  | <del>989.21</del><br><del>988.31</del>   | 12.46 |      | <del>989.19</del><br><del>988.29</del>   |
| 350    |       |                                          |       | 8.2  | 81.0                                     |
| +70    |       |                                          |       | 11.2 | 78.0                                     |
| 351    |       |                                          |       | 10.2 | 79.0                                     |
| T.P.   | 0.04  | <del>978.40</del><br><del>977.50</del>   | 10.85 |      | <del>978.36</del><br><del>977.46</del>   |



12" B.O. 4' Lt Sta. 344.00

| Sta    | + s   | H.T.                                   | - s   | Red  | Elev.                       |
|--------|-------|----------------------------------------|-------|------|-----------------------------|
|        |       | <del>978.40</del><br><del>977.50</del> |       |      |                             |
| 352    |       |                                        |       | 4.0  | 74.4                        |
| +30    |       |                                        |       | 7.4  | 71.0                        |
| T.P.   | 0.08  | 966.60<br><del>965.70</del>            | 11.88 |      | 966.52<br><del>964.62</del> |
| +50    |       |                                        |       | 2.0  | 64.6                        |
| +65    |       |                                        |       | 9.0  | 57.6                        |
| +80    |       |                                        |       | 12.3 | 54.3                        |
| T.P.   | 564   | 963.82<br><del>962.92</del>            | 8.42  |      | 958.18<br><del>957.28</del> |
| 360+50 |       |                                        |       | 9.5  | 54.3                        |
| +65    |       |                                        |       | 7.4  | 56.4                        |
| +90    |       |                                        |       | 4.9  | 58.9                        |
| 361    |       |                                        |       | 5.2  | 58.6                        |
| +50    |       |                                        |       | 8.55 | 55.27                       |
| 362    |       |                                        |       | 8.0  | 55.8                        |
| +50    |       | 966.79                                 |       | 2.4  | 61.4                        |
| T.P.   | 8.53  | <del>965.89</del>                      | 5.56  |      | 958.26<br><del>957.36</del> |
| 363    |       |                                        |       | 1.0  | 65.8                        |
| +60    |       |                                        |       | 8.8  | 58.0                        |
| 364    |       |                                        |       | 8.0  | 58.8                        |
| +70    |       |                                        |       | 4.2  | 62.6                        |
| 365    |       |                                        |       | 7.2  | 59.6                        |
| +30    |       |                                        |       | 9.9  | 56.9                        |
| T.P.   | 11.26 | 969.31<br><del>968.41</del>            | 8.74  |      | 958.05<br><del>957.15</del> |
| 368+05 |       |                                        |       | 12.5 | 56.8                        |
| +50    |       |                                        |       | 5.6  | 63.7                        |
| 369    |       |                                        |       | 3.3  | 66.0                        |

Edge of Water (Water Level.)

West End of Lake.

Little Swamp. (Water Level.)

362 + 30 - 15' Rt.

Water Level Swamp

W. Water Level

I

| Sta. | + s  | <del>1/2 T</del><br><del>969.31</del><br>968.41 | -     | Pod Elev.                              |
|------|------|-------------------------------------------------|-------|----------------------------------------|
| 370  |      |                                                 |       | 2.7 66.6                               |
| 371  |      |                                                 |       | 3.4 65.9                               |
| T.P. | 2.88 | <del>969.12</del><br><del>968.22</del>          | 3.07  | <del>966.24</del><br><del>968.24</del> |
| 372  |      |                                                 |       | 7.1 62.0                               |
| T.P. | 5.85 | <del>974.97</del><br><del>974.07</del>          | 0.0   | <del>969.12</del><br><del>968.22</del> |
| +50  |      |                                                 |       | 4.6 70.4                               |
| 373  |      |                                                 |       | 3.3 71.7                               |
| +50  |      |                                                 |       | 5.4 69.6                               |
| +85  |      |                                                 |       | 4.8 70.2                               |
| 374  |      |                                                 |       | 6.7 68.3                               |
| +50  |      |                                                 |       | 15.4 59.6                              |
| 375  |      |                                                 |       | 9.5 65.5                               |
| +50  |      |                                                 |       | 2.8 72.2                               |
| 376  |      |                                                 |       | 2.2 72.8                               |
| T.P. | 1.55 | <del>974.42</del><br><del>973.52</del>          | 2.10  | <del>972.87</del><br><del>971.97</del> |
| +68  |      |                                                 |       | 8.8 65.6                               |
| T.P. | 0.58 | <del>962.48</del><br><del>961.58</del>          | 12.52 | <del>961.90</del><br><del>961.00</del> |
| 377  |      |                                                 |       | 1.4 61.1                               |
| 378  |      |                                                 |       | 5.8 56.7                               |
| +70  |      |                                                 |       | 8.5 54.0                               |
| 79.  |      |                                                 |       | 11.8 50.7                              |
| 380  |      |                                                 |       | 13.5 49.0                              |
| +50  |      |                                                 |       | 10.5 52.0                              |
| 381  |      |                                                 |       | 12.1 50.4                              |
| T.P. | 0.92 | <del>951.66</del><br><del>950.76</del>          | 11.74 | <del>950.74</del><br><del>949.84</del> |



Top of Stake 376+00 3' Rt.

P.I. 4 Central Ave.  
1"

| Station | +    | H.I.                               | -     | Rod Elev.                          |
|---------|------|------------------------------------|-------|------------------------------------|
| 381     |      | <del>950.76</del><br><b>951.66</b> |       |                                    |
| +50     |      |                                    | 1.2   | 50.5                               |
| 382     |      |                                    | 4.9   | 46.8                               |
| +50     |      |                                    | 7.5   | 44.2                               |
| 383     |      |                                    | 6.0   | 45.7                               |
| +15     |      |                                    | 5.5   | 46.2                               |
| 384     |      |                                    | 11.8  | 39.9                               |
| T.P.    | 3.77 | <del>942.53</del><br><b>943.43</b> | 12.0  | <del>938.76</del><br><b>939.66</b> |
| 385     |      | 99.98                              | 2.5   | 35.9                               |
| 386     |      | 993.88                             | 7.0   | 36.4                               |
| 387     |      | 940.68                             | 4.7   | 38.7                               |
| 388     |      | <del>532.0</del><br><b>948.52</b>  | 2.1   | <del>940.68</del><br><b>941.58</b> |
| B.M.    | 6.94 | <del>947.62</del><br><b>948.52</b> | 18.5  |                                    |
| 389     |      |                                    | 6.9   | 41.6                               |
| 390     |      |                                    | 9.8   | 38.7                               |
| +35     |      |                                    | 10.4  | 38.1                               |
| 391     |      |                                    | 6.1   | 42.4                               |
| 392     |      |                                    | 5.0   | 43.5                               |
| 393     |      |                                    | 5.3   | 43.2                               |
| 394     |      |                                    | 5.7   | 42.8                               |
| +50     |      |                                    | 7.5   | 41.0                               |
| 395     |      |                                    | 11.2  | 37.3                               |
| T.P.    | 0.79 | <del>937.35</del><br><b>938.25</b> | 11.06 | <del>936.56</del><br><b>937.46</b> |
| 396     |      |                                    | 13.8  | 24.5                               |
| +10     |      |                                    | 18.5  | 19.8                               |
| +50     |      |                                    | 18.5  | 19.8                               |

Top of 2"x2" Stake 1' RT Sta. 388+32.0

Fair & Warm

5/31/28

D. Weber  $\pi$   
M.A. Beaton Red.

Edge of Pot Hole  
Edge " " "

| Sta.  | +     | H.I.<br><del>938.25</del><br><del>937.35</del> | -                                 | Pod. | Elev                        |
|-------|-------|------------------------------------------------|-----------------------------------|------|-----------------------------|
| 397   |       |                                                |                                   | 12.0 | 26.3                        |
| +40   |       |                                                |                                   | 7.8  | 30.5                        |
| 398   |       |                                                |                                   | 13.2 | 25.1                        |
| T.P.  | 1.37  | 927.59<br><del>926.69</del>                    | 12.03                             |      | 926.22<br><del>925.32</del> |
| +55   |       |                                                |                                   | 15.0 | 12.6                        |
| 399   |       |                                                |                                   | 15.8 | 11.8                        |
| 400   |       |                                                |                                   | 12.3 | 15.3                        |
| T.P.  | 2.71  | 919.64<br><del>918.74</del>                    | 10.66                             |      | 916.93<br><del>916.03</del> |
| +70   |       |                                                |                                   | 8.5  | 11.1                        |
| T.P.  | 2.94  | 910.76<br><del>909.86</del>                    | 11.82                             |      | 907.82<br><del>906.92</del> |
| 401   |       |                                                |                                   | 7.7  | 03.1                        |
| +15   |       |                                                |                                   | 18.1 | 92.7                        |
| +85   |       |                                                |                                   | 18.1 | 92.7                        |
| 402   |       |                                                |                                   | 17.9 | 92.9                        |
| 403   |       |                                                |                                   | 14.5 | 96.3                        |
| +50   |       |                                                |                                   | 4.7  | 906.1                       |
| +90.5 |       |                                                |                                   | 4.33 | 06.43                       |
|       |       |                                                |                                   | 4.92 | 05.84                       |
| 404   |       |                                                |                                   | 5.55 | 05.21                       |
| 405   |       |                                                |                                   | 3.18 | 07.58                       |
| 406   |       |                                                |                                   | 2.4  | 08.4                        |
| 407   |       |                                                |                                   | 3.0  | 07.8                        |
| B.M.  |       |                                                |                                   |      | 908.10<br><del>907.20</del> |
|       | 14.75 | 940.68<br>907.20<br>33.48                      | 2.66<br>48.23<br>14.75<br>33.48 ✓ |      |                             |



} Pot. Hole.

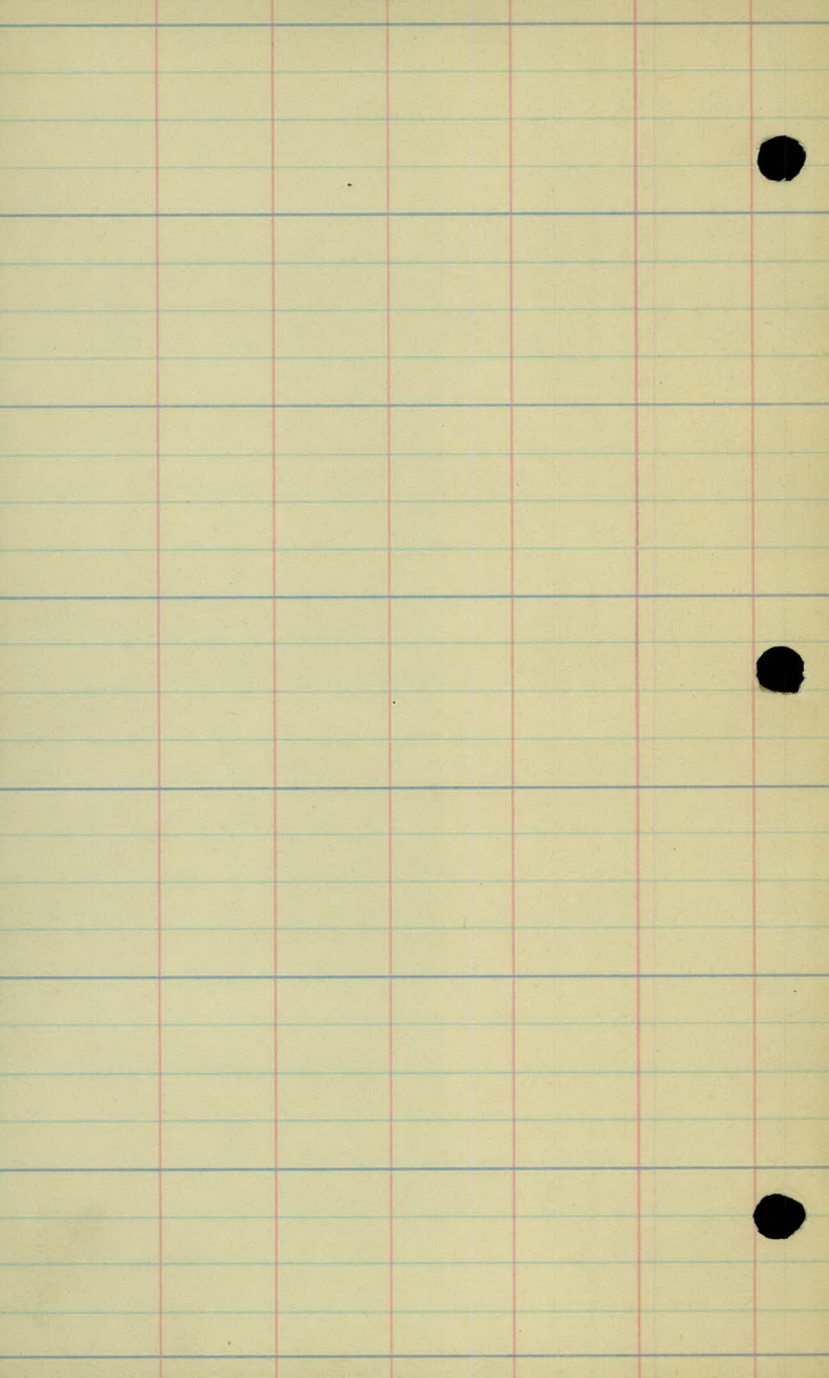
= Toe of Slope.

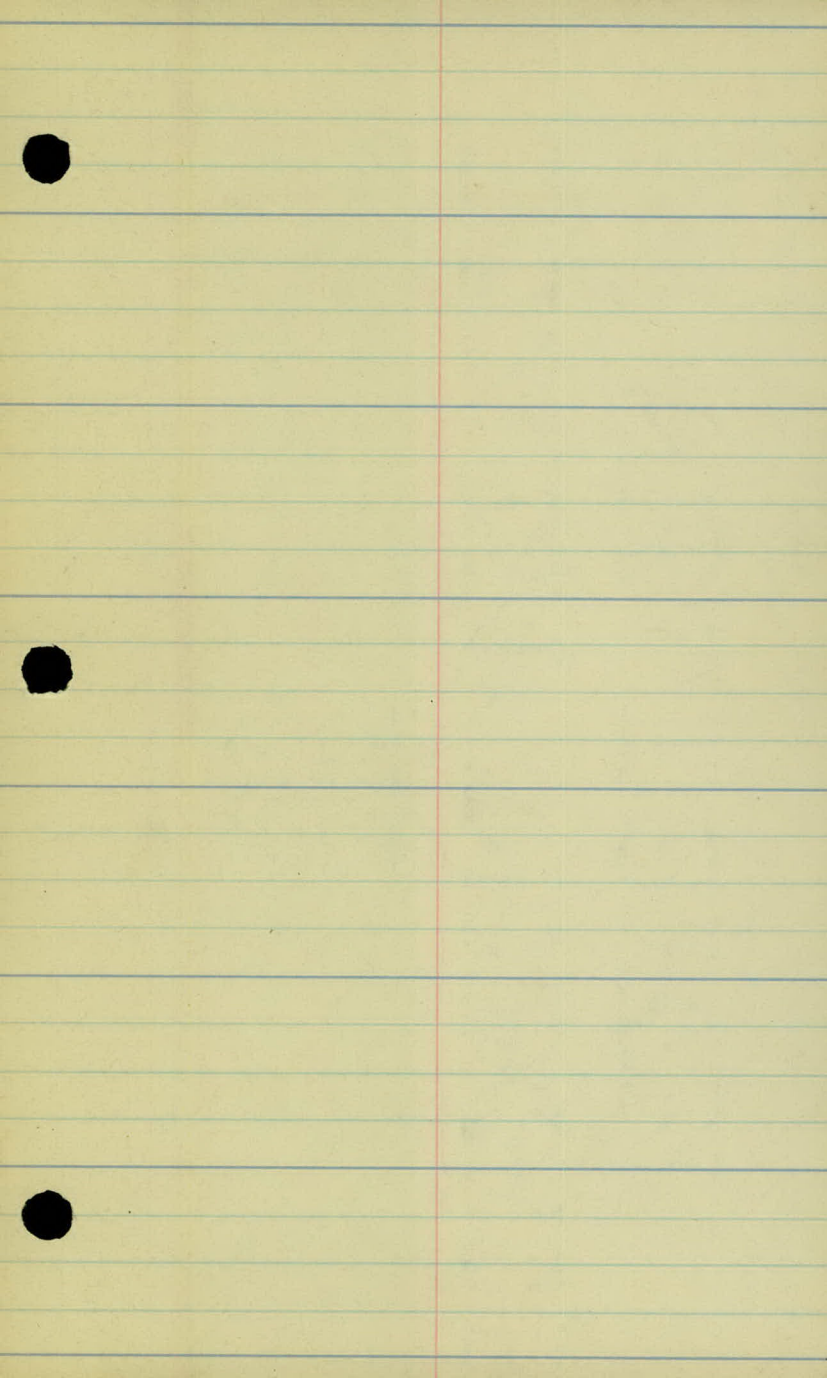
= Top of Shoulder.

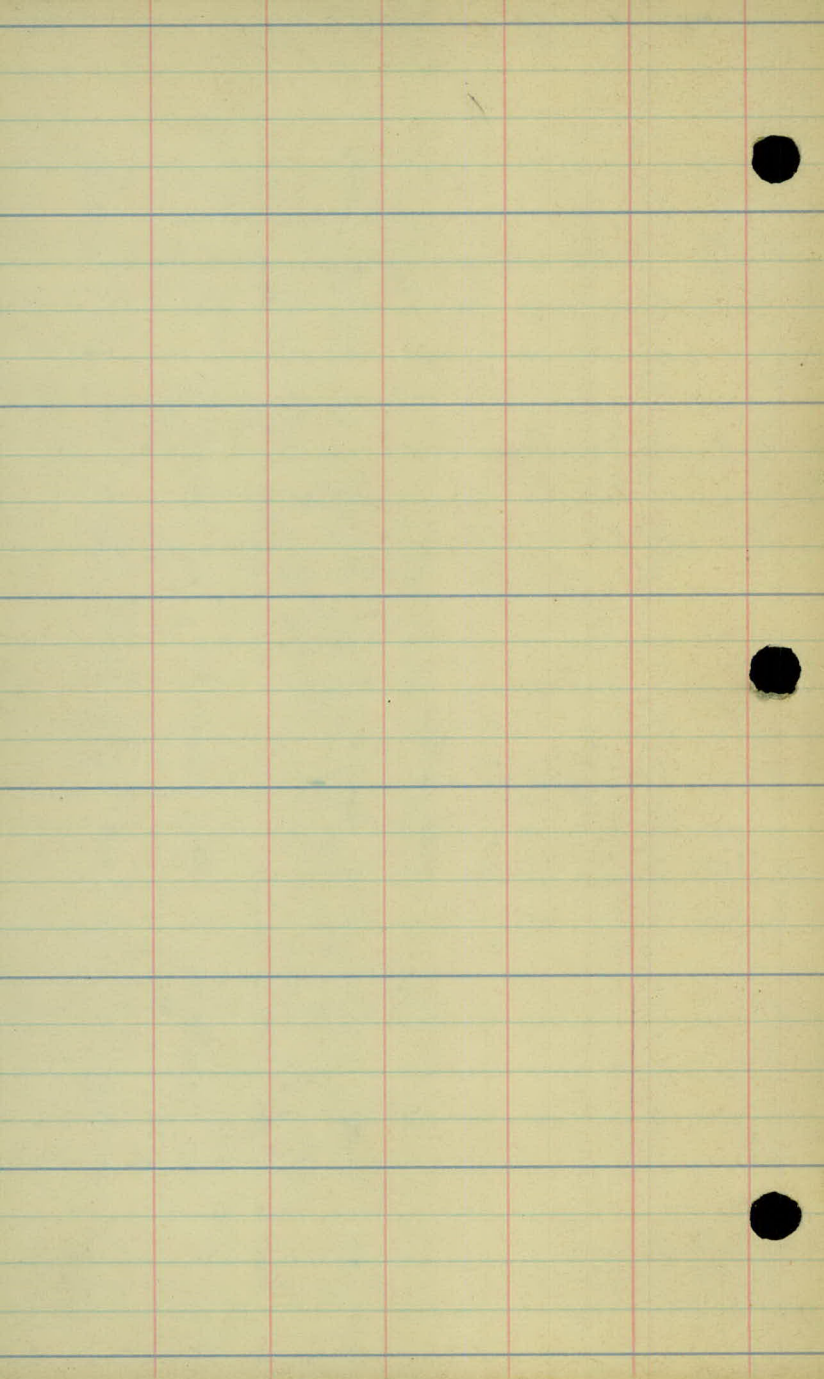
Edge of Pav.

$$\begin{array}{r}
 555 \\
 \underline{9} \\
 533 \\
 \underline{9} \\
 \end{array}
 \begin{array}{r}
 492 \\
 \underline{9} \\
 433 \\
 \underline{9} \\
 425 \\
 \underline{9} \\
 \end{array}
 \begin{array}{r}
 433 \\
 \underline{9} \\
 425 \\
 \underline{9} \\
 \end{array}
 \begin{array}{l}
 \text{Central Ave.} \\
 \text{= our } \pounds
 \end{array}$$

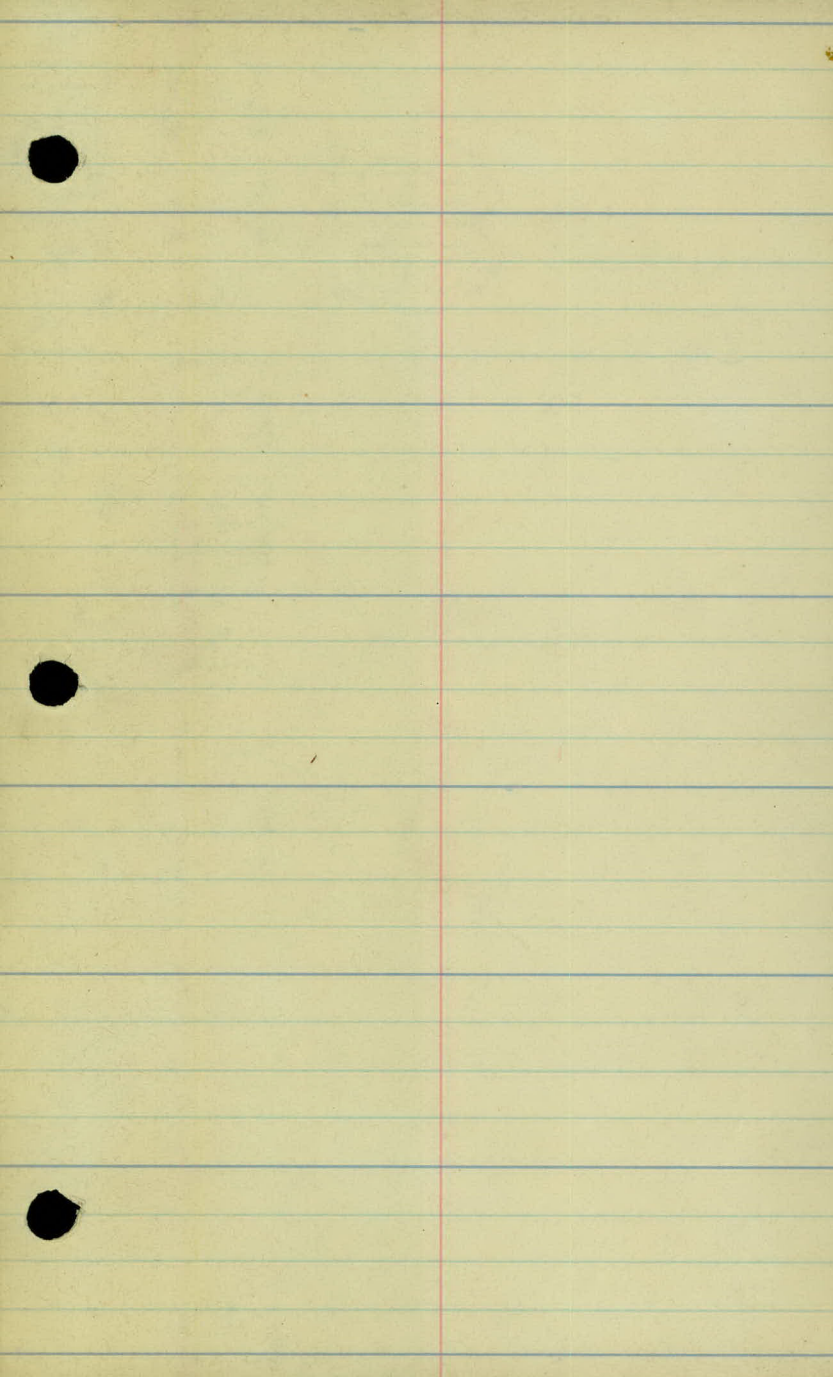
R.R. spike in P.R. 20' R.R. 405+18











5

4

3

2

1

0 + 00