

Book-51 Dr. 6

PLANS SURVEY
PART OF SIBLEY MEM. HY.
ROAD % No. 89

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed April 1923

File No.

~~5~~

2

R. 24-W.

School - 15

8584

40

Office of County Engr.
Hastings Minn.

N.E. 1/4 S.E. 1/4 Sec. 34
Dennis Mc Namara

Dot & Dash Line
 $\Delta = 24^{\circ}30'$
D-5+00
R-114+03
B.C. 62+07.3
E.C. 66+97.0

T=248.8

P.I. 49+57.8
 $\Delta = 27^{\circ}00'$
D-2+00
R-1432.5
B.C. 42+00
E.C. 56+50.0
T=687.8

$\Delta = 17^{\circ}10' L$
D-2+00
R-28650
B.C. 42+74.0
E.C. 51+32.4
Straight Line

S.W. 1/4 S.W. 1/4 Sec. 35
John O'Regan

75+15
75+18.3
Straight Line
 $\Delta = 26^{\circ}12'$
D-15+00
R-383.1
B.C. 71+25.4
E.C. 73+00.1

$\Delta = 40^{\circ}24'$
D-15+00
R-383.1
B.C. 70+37.9
E.C. 73+07.2
DOT & DASH LINE

S.E. 1/4 S.E. 1/4 Sec. 34
Dennis Mc Namara

S.W. 1/4 S.W. 1/4 Sec. 35

Alignment Change
on
Sibley Memorial Highway
East of Lyndale River
I-300 ft

T. 27-N.

T. 114-N

R-20-W

1320

34.35

Sibley Memorial Hy.

INDEX

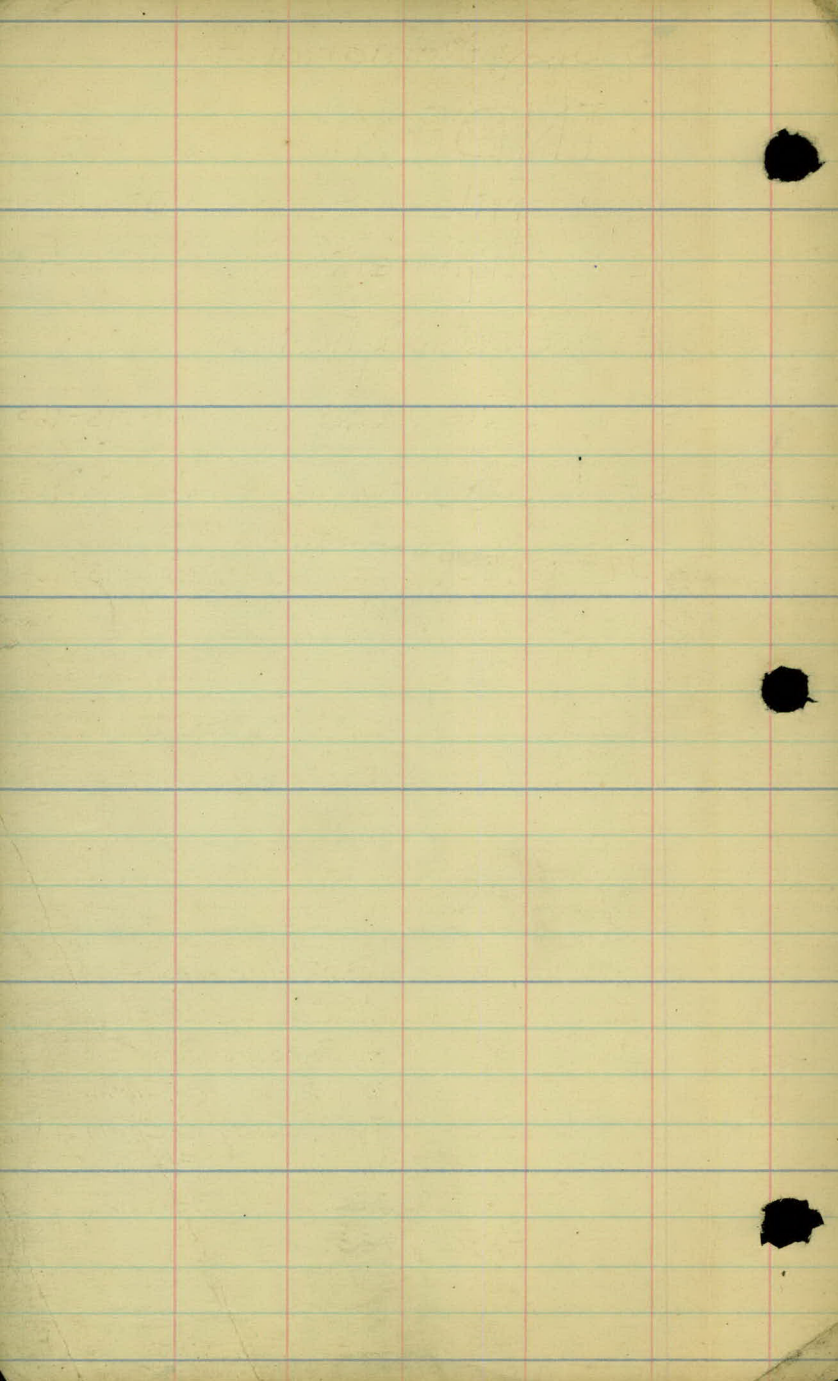
Page	Title	Sta.
1-12	Alignment	0+00 - 173+96.8
13-14	Section Ties	
15-28	± Elevations	0+00 - 173+96.8
29-54	X Sections	0+00 - 173+96.8
55-57	Check Levels	0+00 - 173+96.8

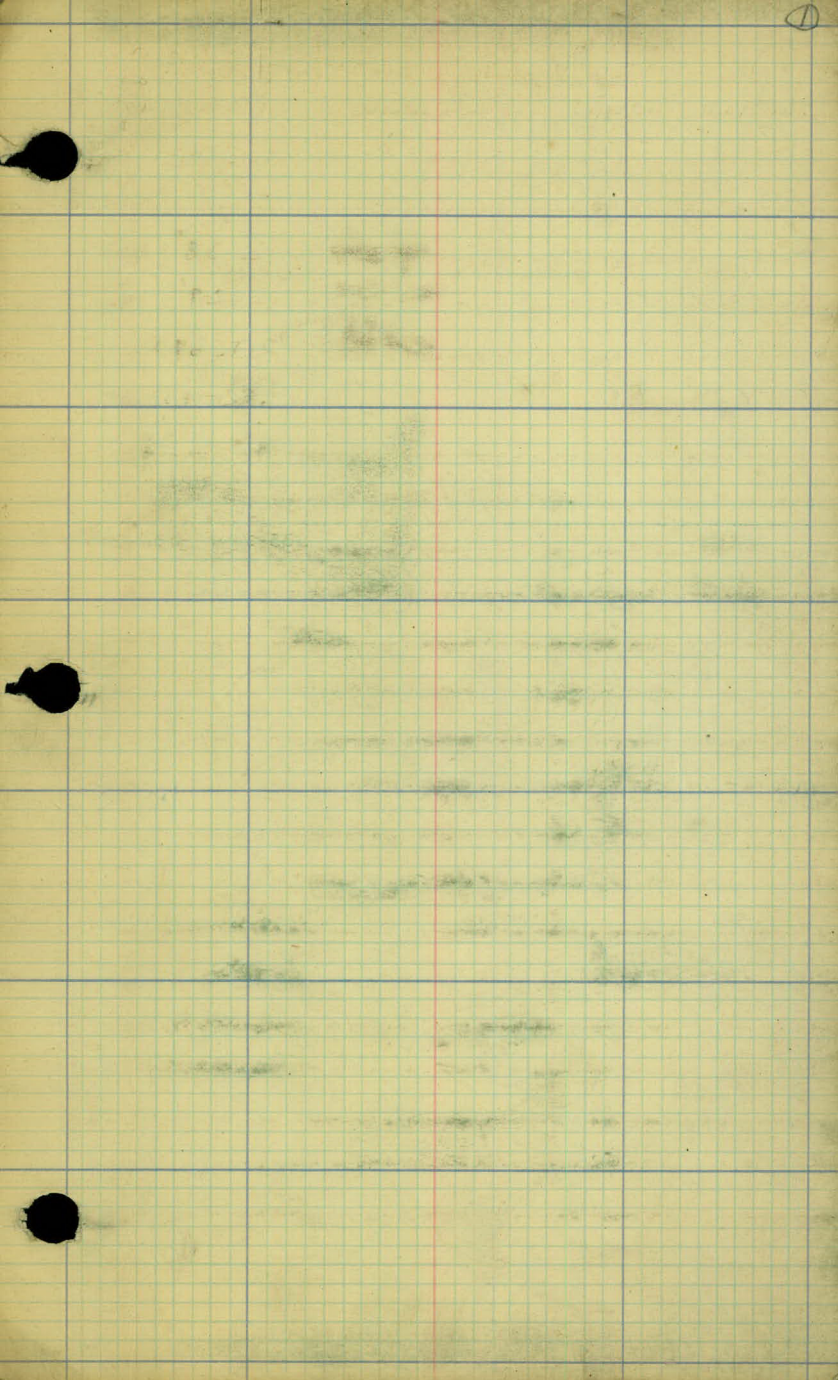
Proj 23:61

Wickor's Contract

G. Reiffer Inst ✓
 M. Carley Level ✓
 A. Parsons Rod
 D. Webber Hd Cham
 J. Mahoney Br Cham
 M. Galvin Flag
 J. Carr Stakes

April - 1923.





Sibley Memorial

4-12-23
Calc. Mag
Bearing

Station Point - Left. Right
53+09.9 Orig. sta. } Equation.
53+03.54 P.T. }

53

19°-20'

+50

18°-50'

Δ 38°-40'

52+40

P.I.

C 29°-00'

52

11°-35'

S.T. 69.80 ✓

51+70.2

P.C.

4°-20'

L.C. 133.34 ✓

S 39°-28'W S 35°-30'W

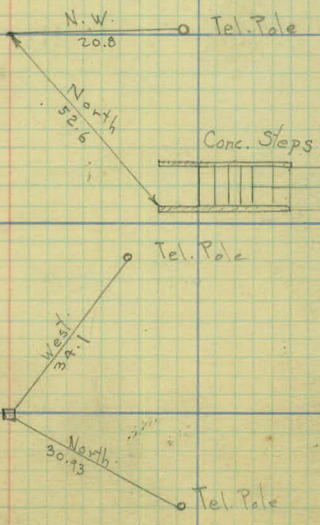
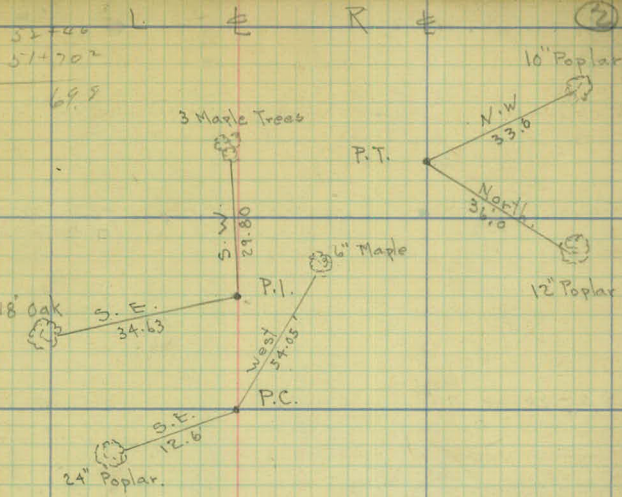
28+39.1

P.O.T.

S 39°-28'W S 35°-30'W

21+16.1

Mont. begin location



Station Point Left. & Right

Calc. Mag. Bearing

S63°05'W

$$\left. \begin{array}{l} 59 + 50.34 \text{ Orig. Sta.} \\ 59 + 38.41 \text{ P.T.} \\ \quad + 50.76 \end{array} \right\} \text{Equation}$$

$$\begin{array}{r} 8^{\circ} = 52' \\ 6^{\circ} = 35' \\ 6 = 56 \end{array}$$

58 + 53.23 P.I.

$\Delta 17^{\circ} - 43'$

$$\begin{array}{r} 4^{\circ} - 09' \\ 4^{\circ} - 41' \end{array}$$

C 9°-00

58

S.T. 99.33 .32

57 + 53.19 P.C.

L.C. 196.44 196.85

$$\begin{array}{r} 2^{\circ} - 04' \\ 2^{\circ} - 26' \end{array}$$

S45°22'W S41°10'W

$$\left. \begin{array}{l} 56 + 26.05 \text{ Orig. Sta.} \\ 56 + 20.60 \text{ P.T.} \\ \quad + 20 \end{array} \right\} \text{Equation}$$

$$\begin{array}{r} 16^{\circ} - 23' \\ 14^{\circ} - 20' \\ 15^{\circ} - 00' \end{array}$$

56

$\Delta 32^{\circ} - 46'$

+ 50

C 20°-00

55 + 41.5 P.I.

S.T. 84.65

55

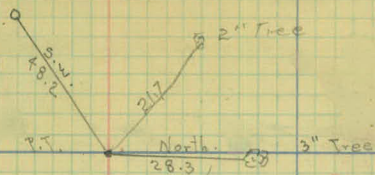
L.C. 163.85

54 + 50.35 P.C.

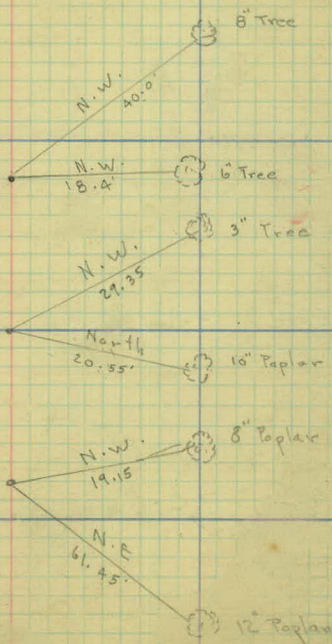
$$\begin{array}{r} 9^{\circ} - 20' \\ 10^{\circ} - 00' \\ 4^{\circ} - 20' \\ 5^{\circ} - 00' \end{array}$$

S78°08'W

6" Stump



7-8 9' Max



Station Point Left & Right Calc. Mag Bearing

$$\begin{array}{l} 65+37.53 \\ 65+34.81 \end{array} \left. \begin{array}{l} \text{orig. sta} \\ \text{P.T.} \end{array} \right\} \text{Equation}$$

78

S 49°-16' W S 43°-50' W

$$65+00 \quad 12^{\circ}-42'$$

Δ 25°-24'

$$64+65 \underline{73} \quad \text{P.I.} = 64+65 \pm$$

C 18°-00'

S.T. 12.03 .06

L.C. 14 L.W.

$$64+50 \quad 9^{\circ}-34'$$

$$63+93.7 \quad \text{P.C.} \quad 5^{\circ}-04'$$

S 74°-40' W

$$\begin{array}{l} 62+51.3 \\ 62+39.49 \end{array} \left. \begin{array}{l} \text{orig. sta} \\ \text{P.T.} \end{array} \right\} \text{Equation Transposed}$$

+51.38

1°32'

$$62$$

$$5^{\circ}-47' \quad 3^{\circ}-02'$$

$$+50$$

$$4^{\circ}-15' \\ 4^{\circ}-36'$$

$$4^{\circ}-22' \quad 5^{\circ}-47'$$

$$61+55 \underline{23} \quad \text{P.I.}$$

$$\Delta \quad 11^{\circ}-35'$$

$$C \quad 6^{\circ}-0'$$

$$61$$

$$2^{\circ}-45' \\ 3^{\circ}-05'$$

$$S.T. \quad 96.93 \quad \textcolor{red}{.90}$$

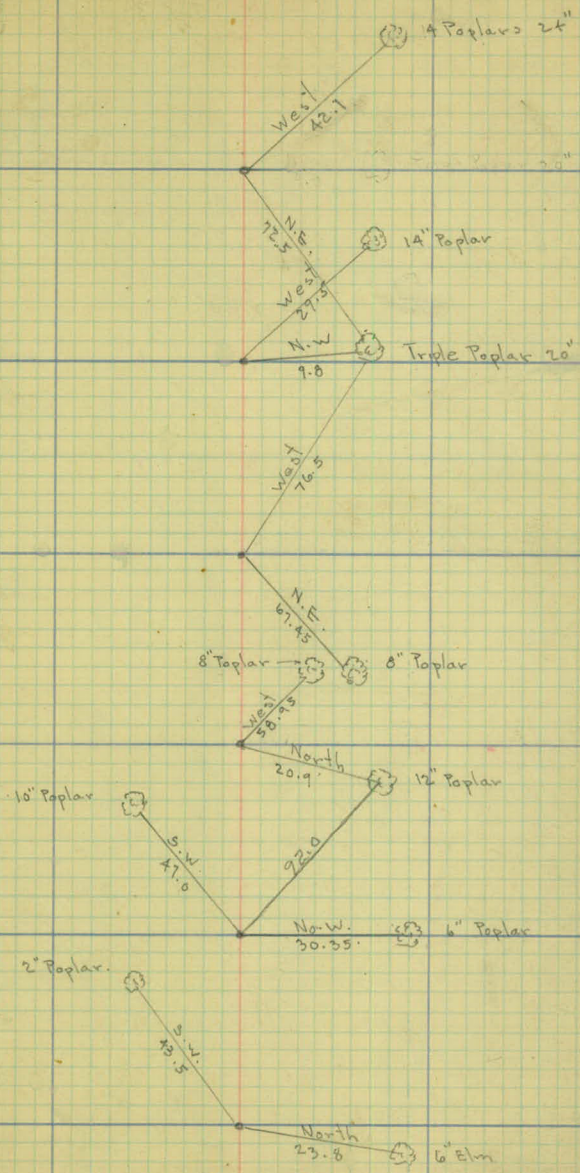
$$60+58 \underline{33} \quad \text{P.C.}$$

$$1^{\circ}-15' \\ 1^{\circ}-36'$$

$$L.C. \quad 193.00 \quad \textcolor{red}{.05}$$

S 63°-05' W

16
68
70



Statvan Point Left & Right

Calc. Mag.
Bearing

74+00.15 end Bridge

350°-29W

71+07.11 P.T.

+06.85

70+68.05 begin Bridge

70+50.55 P.I. Left.

$\Delta 7^{\circ}-54'$

C 7°-0

S.T. 56.56 ✓

L.C. 112.86 ✓

69+93.99 ✓ P.C.

358°-23W 353°-10W

68+73.55 Orig. Sta. } Equation

68+71.00 P.T. }
+12

+50

A°-33'

68+14.32 P.I.

$\Delta 9^{\circ}-07'$

C 8°-00

S.T. 57.10 .15 ✓

L.C. 114.00 113.95 ✓

68

3°-42'

67+57.2 P.C.

1°-42'

349°-16W

332.1
32.1
166.5



7' walks each side
19' Roadway
70+68.95 bridge end



Station Point Left Right Calc. Mag. Bearing

102 }
100 } 100' short sta.

S58°57'W

89+71.66 orig. sta.
89+70.39 P.T. } Equation
72

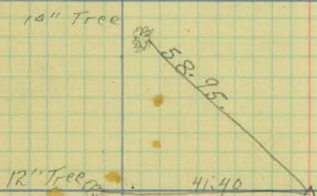
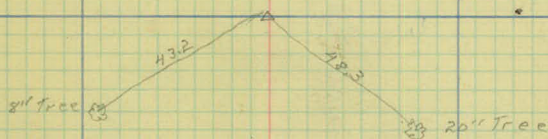
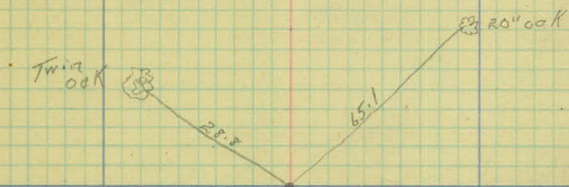
+50		3°-26'	
89		3°-02'	Δ 6°-53'
88+84.8	P.I.	6°-53'	C 4°-00'

S.T. 86.16
L.C. 171.75
172.08

88+50		2°-02'
87+98.64	P.C.	1°-02'

S52°04'W

79+15.6	P.I. } <u>Equation</u>	1°-35'	Δ 1°-35'
79+16.4 Orig. Sur.			C 1°-0'



Station Point Left & Right

Calc. Mag.
Bearing
$$\begin{array}{r} 108+38 \frac{51}{11} \\ 108+28 \frac{77}{11} \end{array} \left. \begin{array}{l} \text{Orig. Sta.} \\ \text{P.T.} \end{array} \right\} \underline{\text{Equation}}$$

S43°-21'W

106

21°-16'

107+48 $\frac{1}{1}$ P.I. $\Delta 42^{\circ}-37'$

C 25°-00'

+50

17°-43' S.T. 90.11 ✓

107

11°-28' L.C. 170 $\frac{48}{.47}$ 106+58 $\frac{29}{1}$ P.C.

5°-13'

S0°-44'W

$$\begin{array}{r} 105+37 \frac{66}{11} \\ 105+08 \frac{52}{11} \end{array} \left. \begin{array}{l} \text{Orig. Sta.} \\ \text{P.T.} \end{array} \right\} \underline{\text{Equation}}$$

105

29°-07'

+50

28°-09'

104

22°-39'

 $\Delta 58^{\circ}-13'$ 103+90 $\frac{00}{1}$ P.I.

C 22°-00' ✓

S.T. 145.86 $\frac{80}{.62}$

+50

17°-09'

L.C. 267.68 $\frac{62}{.62}$

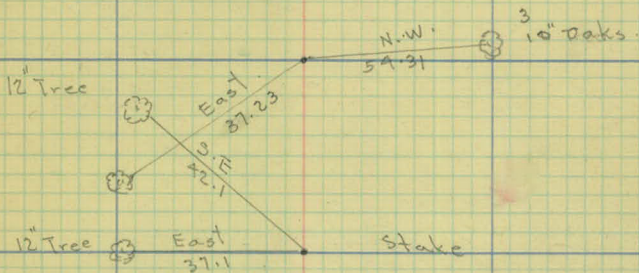
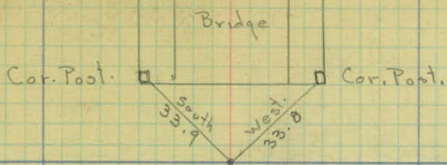
103

11°-39'

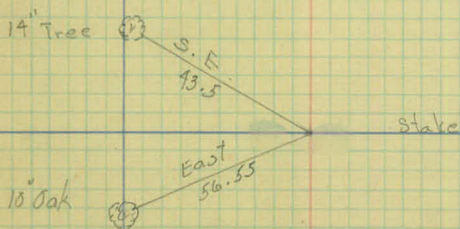
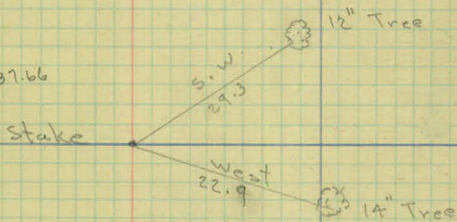
102+44 $\frac{14}{1}$ P.C.

6°-09'

S58°-57'W



Sta. 10.5 to 10.5 + 37.66
= 28.64' short



Station Point Left & Right

Calc. Bearing
4-20-23
Mag.

325°-40'W

122+80.39 orig. sta.
122+80.16 P.T. } Equation
.24

+50

2°-55'

122+07.4 P.I.

Δ 5°-50'

122

2°-19'

C 4°-0'

+50

1°-19'

S.T. 72.99

L.C. 145.75 .83

121+34.41 P.C.

0°-19'

331°-30'W

113+78.46 orig. sta.
113+77.49 P.T. } Equation
.41

+50

5°-55'

Δ 11°-51'

113+18.45 P.I.

C 10°-0'

S.T. 59.46 .54

L.C. 118.5

113

4°-33'

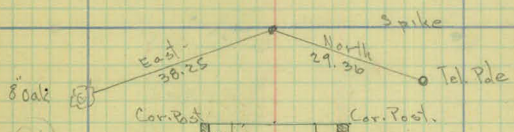
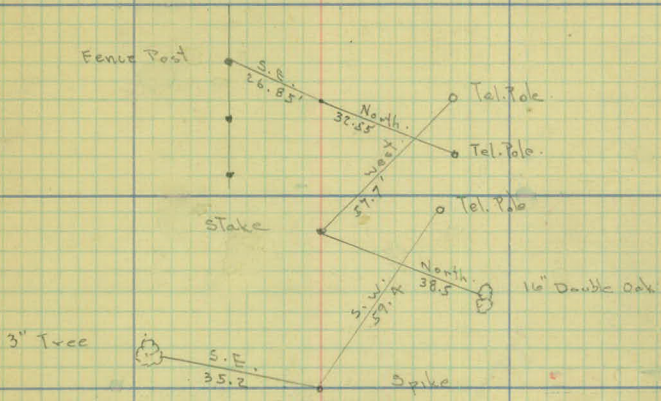
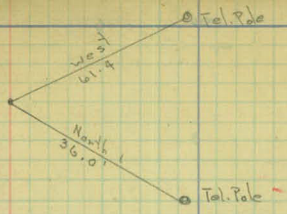
112+58.99 P.C.

2°-03'

112+70.4 End Bridge

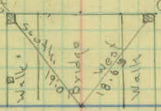
108+66.2 Begin Bridge

343°-21'W 338°-30'W



$$\begin{array}{r} 1127104 \\ 108662 \\ \hline 4.042 \end{array}$$

14



North End Bridge

18' Roadway
 8' walks each
 side
 34' W

Station

Point

Left & Right

Bearing

S 58° 51' W

S 54° 00' W

133+46 ⁸⁰ orig. sta. }
 133+45 ²⁰ P.T. } Equation

.83

133

1°-43'

+50

1°-29'

132

1°-14'

Δ 3°-26'

131+74 ⁵ P.L.

C 1°-0'

+50

0°-59'

S.T. 172 ³⁰ 171.8

131

0°-44'

L.C. 343 ²⁰ 335

+50

0°-29'

130+02 ²⁰ 5 P.C. 0°-14'

S 62°-17' W

126+35 ¹² (orig. sta.) }
 126+30 ⁹⁶ P.T. } Equation

+31.06

126

18°-19'

+50

15°-51'

Δ 36°-37'

125+21 ⁰⁵ P.L.

C 16°-0'

125

11°-51'

+50

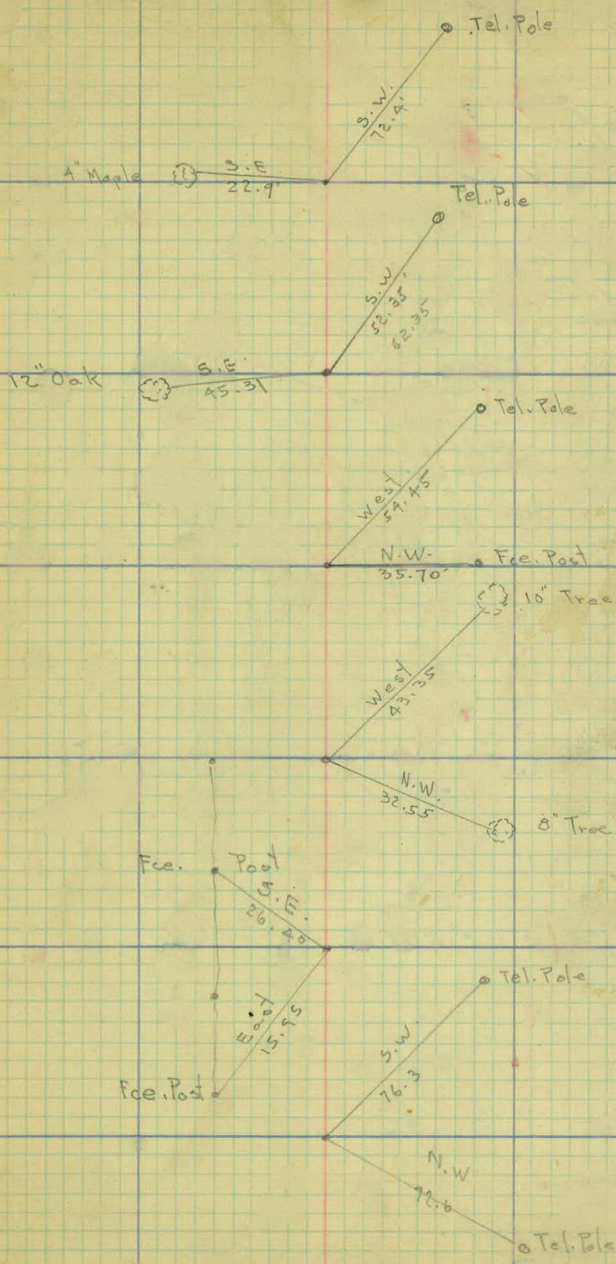
7°-51'

S.T. 118 ⁸⁸ 84C 228 ⁸¹

228.85

124+02 ¹⁷ 21 P.C.

3°-51'



Station	Point	Left. & Right	Calc. Bearing	Mag
---------	-------	---------------	---------------	-----

358°-49'W

140+76⁸⁸ P.T.

+50

4°-11'

Δ 8°-34'

140+234 P.I.

x

C 8°-00'

S.T. 53.68 ✓

L.C. 107.09 ✓

140 ✓

3°-12'

1°-12'

139+69⁷⁹ P.C.

S 50°-15'W

137+97⁸⁸ P.T.

+50

4°-18' 5

137

3°-20' 4

Δ 8°-36'

136+90⁶⁰ P.I.

C 4°-0'

S.T. 107.72 ✓

L.C. 215 ✓

+50

2°-20' 3

136

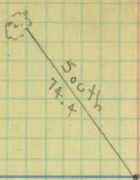
1°-20' 2

135+82⁸⁸ P.C.

0-20' 1

S 58°-51'W

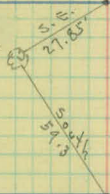
12" Bx. Elder



16" Bx Elder



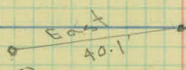
10" Tree



N. W.
19.20'

Tel. Pole

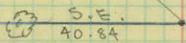
Cor. Fce. Post
16" Bx Elder



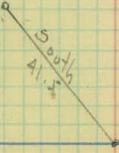
North
17.60'

Tel. Pole

12" Bx Elder



Mail Bx Post



S. W.
28.0'

Tel. Pole

Station Point Left & Right Calc Bearing

157+74 13 ⁸⁵ P.T.

S 50°-48'W

+ 50

7°-44'

157

6°-44'

Δ 15°-28'

156+78 85 P.I.

C 8°-00'

S.T. 97.36 ³⁴

+ 50

4°-44'

L.C. 193.34

156

2°-44'

155+81 49 ⁵¹ P.C.

0°-44'

S 66°-16'W

146+83 32 P.T.

+ 50

3°-44'

Δ 7°-27'

146+21 35 P.I.

C 6°-0'

S.T. 62.20

L.C. 124.17

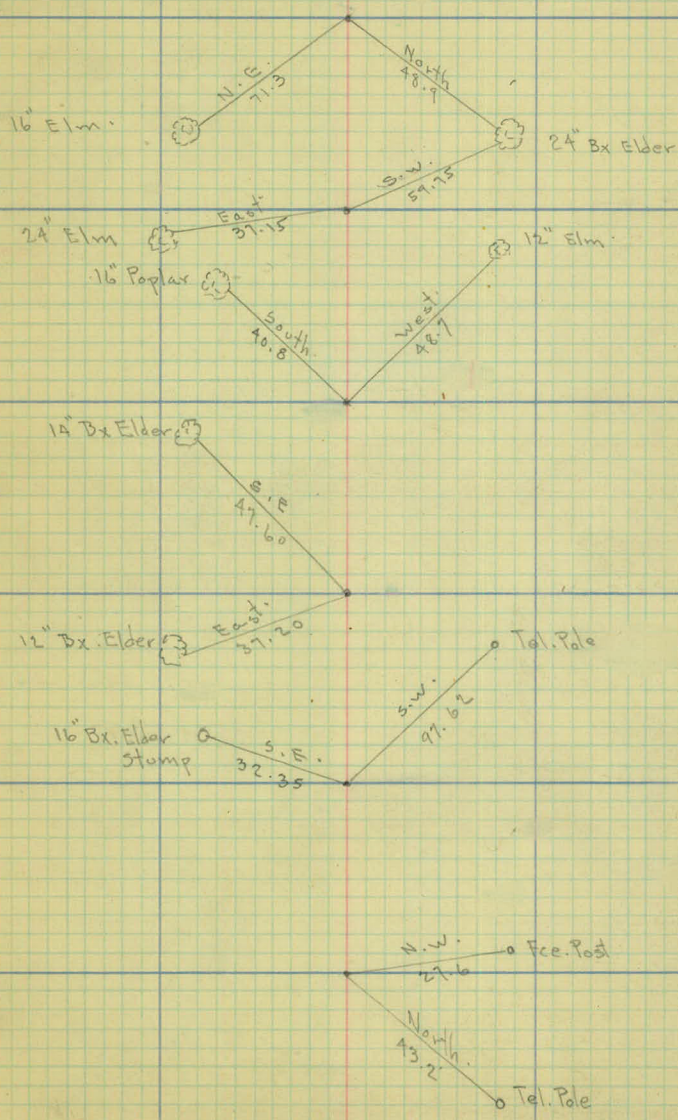
146

2°-44'

145+59 15 P.C.

1°-14'

S 58°-49'W S 54°-00'W



Sibley Memorial

Station	Point	Left. & Right	Calc. Bearing	Mag.
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173+96.8

S 38° 00' W

173+00 End Contract Grading

167+55.17 P.T.

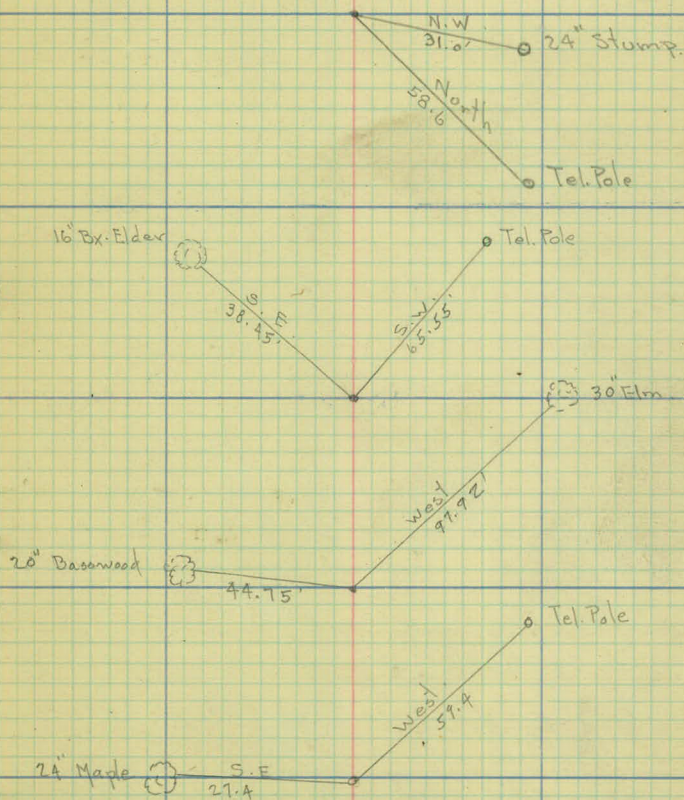
+50	4°-10'	Δ 8°-20'
167	4°-02'	C 5°-0'

166+72.50 P.I. S.T. 83.50 ✓

L.C. 166.67 ✓

+50	2°-47'
166	1°-32'

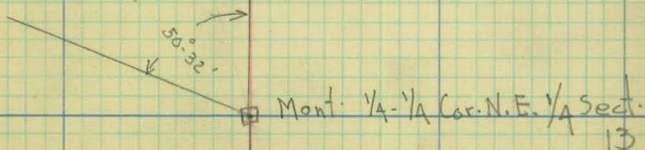
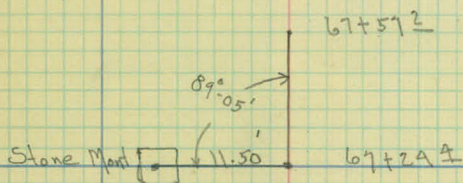
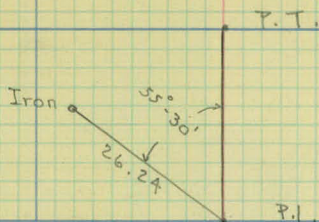
165+88.50 P.C. 0°-17' ✓



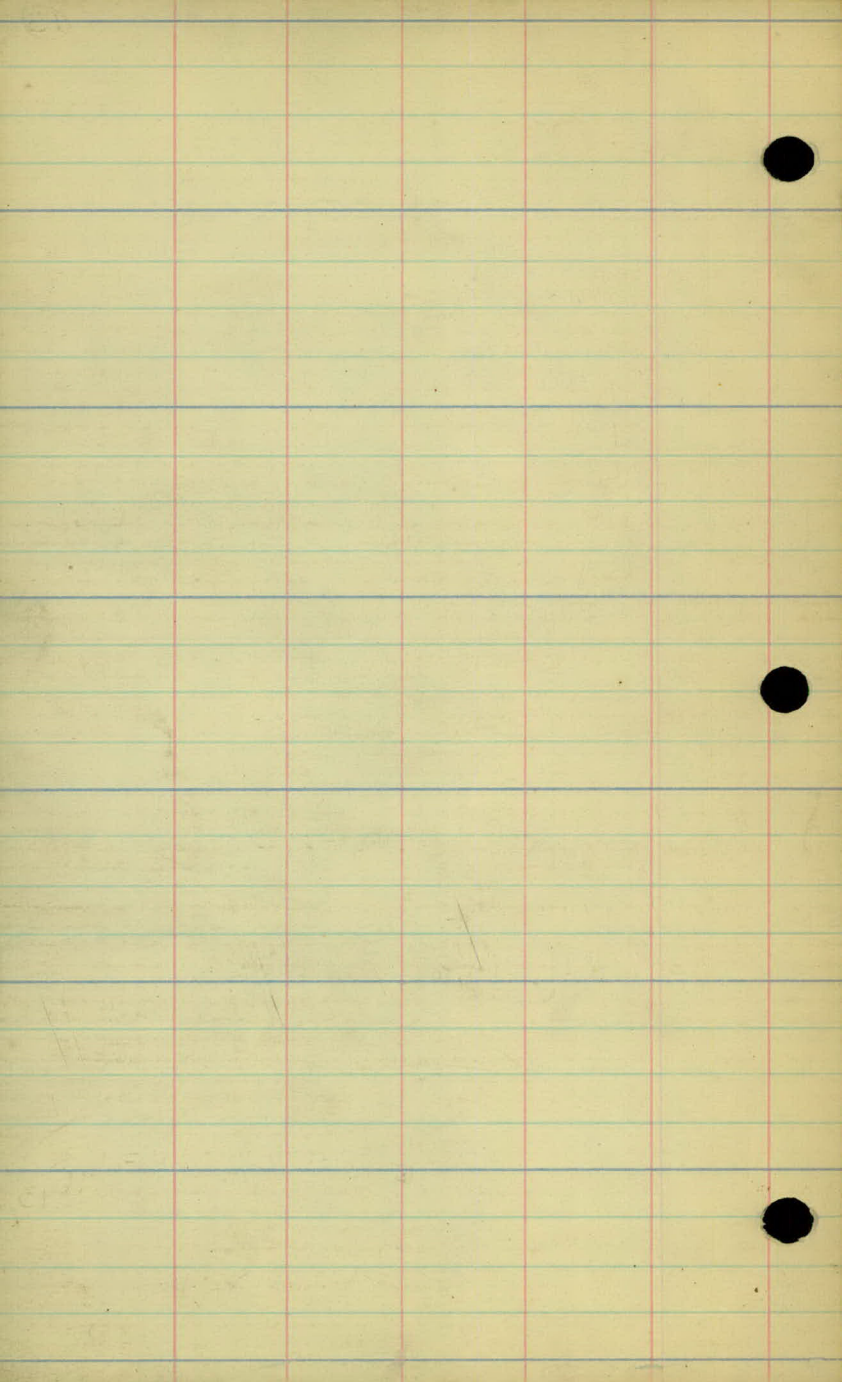
Ties to Sect. Cor.

140+76⁸⁸ P.T.140+23⁴¹ P.167+74²21+16¹

Mont



2 No. Line Sect. 13.



£ Levels on Mendota rd.

Carley T Persons

April 12, 25, 1923

4/12/23

Sheet #1 of sheets

Sta. + H.I. - Rod Elev

B.M. 1.91 279.42 277.51

B.M. 3.10 280.61 277.51

B.M. 5.27 275.34 ✓

21 +16.1 4.8 275.8 ✓

22 4.9 275.7 ✓

23 4.3 276.3 ✓

24 3.3 277.3 ✓

25 2.2 278.4 ✓

26 1.3 279.3 ✓

T.P. 5.11 284.92 0.80 279.81

27 5.0 279.9 ✓

28 4.2 280.7 ✓

29 5.8 279.1 ✓

30 8.0 276.9 ✓

31 10.7 274.2 ✓

32 13.0 271.9 ✓

T.P. 0.12 273.78 11.26 273.66

33 8.33 4.2 269.6 ✓

34 7.5 266.3 ✓

35 11.8 262.0 ✓

T.P. 0.53 262.41 11.90 261.88

23.96 23.96

8.33 277.51

15.63 261.88

15.63

Mendota rd. Levels Carley- π Persons ✓

75.8	76.1	76.1	75.6	75.7
<u>3.6</u>	<u>3.3</u>	<u>3.3</u>	<u>3.8</u>	<u>3.7</u>
50	100	150	200	300
75.7	74.0	72.9	70.2	69.9
<u>3.7</u>	<u>5.4</u>	<u>7.0</u>	<u>9.2</u>	<u>9.7</u>
50	100	150	200	260

rd. going east
" " North

(Edge of bridge)

Spike in tele pole R of sta 20+38
Top of men. sta 21+16.1

Top of stK. sta 26+00

4/12/23

Sheet #2 of sheets

Sta + H.L. - Rod Elev

0.53 262.41

36 4.7 257.7 ✓

37 9.7 252.7 ✓

B.M. 8.29 254.12 ✓

T.R. 1.04 251.17 12.28 250.13 ✓

38 2.8 248.4 ✓

39 5.7 245.5 ✓

40 7.7 243.5 ✓

41 8.9 242.3 ✓

42 9.6 241.6 ✓

T.R. 2.07 243.73 9.51 241.66

43 3.69 240.8 ✓

44 3.3 240.4 ✓

45 4.0 239.7 ✓

46 4.9 238.8 ✓

B.M. 6.98 236.75
28.77

41 / 23

B.M. 2.91 239.66

47 1.3 238.4 ✓

48 1.9 237.8 ✓

49 + 5.1 2.2 237.5 ✓

49 + 5.1 2.5 237.2 ✓

28.77 261.88

3.69 236.75

25.13 25.13

Mendota rd. Levels Carley & Persons!

Spike in tele pole Ref sta 37+03 (old elev 254.17)

R.R. spike in tele pole Ref sta 46+00

Farm entrance on L

4/16/23 Sheet #3 of 5

Sta	+	H.I.	-	Red	Elev.
	2.91	239.66			
50				3.6	236.1
51				5.6	234.1
52				10.5	229.2
T.P.	3.67	231.24	12.09		227.57
+50				5.0	226.2
53				7.7	223.5

$$\text{Equation } 53 + 03.54 = 53 + 09.9$$

B.M.	4.97	241.72			236.75
T.P.	1.77	231.41	12.08		229.64
53 +50				10.5	220.9
T.P.	0.22	222.00	9.63		221.78
54				4.3	217.7
+50				7.3	214.7
55				10.3	211.7
T.P.	0.69	211.21	11.48		210.52
+50	7.65			2.3	208.9
56				5.5	205.7
+50				7.9	203.3
57				10.5	200.7
T.P.	1.37	200.75	11.83		199.38
+50			45.02	2.7	198.1
	45.02		236.75		
	7.65		199.38		
	37.37		37.37		

Mendota rd. Levels Corley & Persons /

Sta. + H.I. - Rod Elev.

137 200.75

B.M.

3.83 196.92 ✓

58

6.1 199.7 ✓

+50

9.1 191.6 191.7

59

12.2 188.6 ✓

T.P.

0.54 189.32 11.97

188.78 ✓

+50

3.5 185.8 ✓

60

6.8 182.5 ✓

+50

9.9 179.4 ✓

T.P.

0.97 178.66 11.63

177.69 ✓

61

2.3 176.4 ✓

+50

5.9 172.8 ✓

62

8.5 170.2 ✓

T.P. +50

~~0.0~~ 167.98 10.68

167.98 ✓

+50

2.88

0.7 167.3 ✓

63

4.1 163.9 ✓

+50

7.1 160.9 ✓

64

9.9 158.1 ✓

T.P.

2.59 159.75 10.82

157.16 ✓

+50

45.10

4.7 155.1 ✓

65

7.9 151.9 ✓

45.10

199.38

2.88157.16

42.22

42.22

Mendota rd. Levels Corley & Persons /

spike in 6" elm stump Ref sta 57152

Sta	+	H.I.	-	Red Elev.
B.M.	0.0	167.64		167.64 ✓
T.P.	0.60	156.22	12.02	155.62 ✓
E.C. 65+37.65				7.3 148.9 ✓
+50				7.9 148.3 ✓
66				10.9 145.3 ✓
T.P.	0.77	146.57	10.92	145.80 ✓
+50				4.1 142.5 ✓
67				7.3 139.4 ✓
B.M. +				8.26 138.31 ✓
+50				10.1 136.6 136.5
T.P.	0.0	135.44	11.13	135.44 ✓
68		1.37		1.9 133.5 ✓
+50				5.1 130.3 ✓
69				8.1 127.3 ✓
+50				11.0 124.4 ✓
T.P.	0.0	124.52	10.92	124.52 ✓
70			44.49	2.6 121.9 ✓
+50				4.7 119.8 ✓
+1				5.60
71				6.2 118.3 ✓
72				7.5 117.0 ✓
73				8.8 115.7 ✓
74				10.1 114.4 ✓
		14.49	167.64	
		1.37	124.52	
		43.12	43.12	

Mendota rd. Levels Carley & Persons /
spike in poplar tree R of sta 62+35

Top of monument R of sta 67+

115.1
75
114 3 ✓

End of bridge

Sta + H.I. - Rod Elev.

0.0 124.52

B.M. 3.37 118.37 9.52 115.00 ✓

75 4.0 114.4 ✓

76 4.0 114.4 ✓

77 4.6 113.8 ✓

78 5.0 113.4 ✓

79 5.5 112.9 ✓

80 5.7 112.7 ✓

B.M. $\frac{2.42}{5.79}$ 115.99 4.80 113.57 ✓

81 3.7 112.3 ✓

82 4.1 111.9 ✓

83 4.3 111.7 ✓

84 4.6 111.4 ✓

85 5.1 (109.9) 110.9 ✓

86 5.2 (109.8) 110.8 ✓

B.M. 4.18 113.64 $\frac{6.53}{20.85}$ 109.46 ✓

+50 2.9 110.7 ✓

87 3.2 110.4 ✓

+50 3.5 110.1 ✓

88 3.8 109.8 ✓

+50 4.5 109.1 ✓

89 4.5 109.1 ✓

20.85 124.52

 $\frac{5.79}{15.06}$ $\frac{109.46}{15.06}$

15.06 15.06

Mendota rd. Levels Corley & Persons /

S.W. corner of SW abutment on bridge
Sta 74+00

Spike in 14" tree R. of Sta 80+96

spike in bass-wood tree R of Sta 87+60

Sta	+	H.I.	-	Red	Elev
	4.18	113.64			
+50				4.4	109.2 ✓
90				4.3	109.3 ✓
+50				4.5	109.1 ✓
91				4.5	109.1 ✓
+50				4.7	108.9 ✓
92				4.9	(108.8) 108.7
+50				5.0	108.6 ✓
93				5.1	108.5 ✓
B.M.				5.80	107.84 ✓
+50				5.3	108.3 ✓
94				5.4	108.2 ✓
+50				5.6	108.0 ✓
95				5.9	107.7 ✓
T.P.	3.80	112.11	5.33		108.31 ✓
+50				4.3	107.8 ✓
96				4.4	107.7 ✓
+50				4.5	107.6 ✓
97				4.9	107.2 ✓
+50				5.0	(106.1) 107.1
98				4.8	107.3 ✓
+50				4.9	107.2 ✓
99				5.5	106.6 ✓
	5.33		109.46		
	<u>4.18</u>		<u>108.31</u>		
	1.15		1.15		

Mendota rd. Levels Carley & Persons /

Spik* in twin elm R of sta 98+

Sta	+	H.L.	-	Rod Elev
	3.80	112.11		
99 +50				5.7 106.4 ✓
100 +00				6.1 106.0 ✓
100 +50				6.1 106.0 ✓
Equation sta 101 = sta 102				
102 +00				6.3 105.8 ✓
102 +50				6.3 105.8 ✓
103				6.5 105.6 ✓
B.M.	$\frac{3.18}{6.98}$	108.89	6.40	105.71 ✓
+50				3.6 105.3 ✓
104				3.9 105.0 ✓
+50				4.1 104.8 ✓
105				4.8 104.1 ✓

Equation 105 + 37.66 =

+50				4.9 104.0 ✓
106				5.9 103.0 ✓
+50				6.7 102.2 ✓
107				7.0 101.9 ✓
+50				7.3 101.6 ✓
108				7.5 101.4 ✓
T.P.	3.34	104.08	8.15	100.74 ✓
	14.55	108.31	$\frac{14.55}{6.98}$	
	<u>6.98</u>	<u>100.74</u>		
	7.57	7.57		

Mendota rd. Levels Carley & Persons'

spike in Large bass-wood tree R of sta 103+

Sta + H.T. - Rod Elev

3.34 104.08

108 +50

3.2 100.9 ✓

108 +68

3.7 100.9 ✓

109

4.0 100.1 ✓

110 +00

4.2 99.9 ✓

111

4.9 99.2 ✓

112

5.6 98.5 ✓

112 +10.2

6.0 98.1 ✓

113

5.7 98.4 ✓

+50

5.7 98.4 ✓

114

5.4 98.7 ✓

+50

115

4.8 99.3 ✓

B.M.

6.10 97.98 ✓

116

3.8 100.3 ✓

T.P.

6.43 107.06

3.45

100.63 ✓

+50

6.1 101.0 ✓

117

5.8 101.3 ✓

118

5.6 101.5 ✓

119

4.5 102.6 ✓

120

3.2 103.9 ✓

121

1.4 105.7 ✓

3.45

100.74

3.34

100.63

.11

.11

Mendota rd levels

End of bridge

End of bridge

S.W. cor of s. abbut on bridge sta 112+10

7/25/23 sheet #10 of sheets

Sta + H.I. - Rod Elev

6.43 107.06

T.P. 12.00 118.01 105 106.01 ✓

121 +50 11.1 106.9 ✓

122 9.5 108.5 ✓

+50 8.1 109.9 ✓

123 7.0 111.0 ✓

+50 6.1 111.9 ✓

124 5.5 112.5 ✓

+50 5.2 112.8 ✓

B.M. 7.97 119.79 5.69 6.69 112.32 ✓ 111.32

125 25.90 5.3 114.5 ✓

+50 4.9 113.9 114.9

126 4.6 115.2 ✓

P.T. +35 4.6 115.2 ✓

127 4.8 115.0 ✓

128 5.7 114.1 ✓

129 6.2 113.6 ✓

130 6.3 113.5 ✓

131 6.3 113.5 ✓

T.P. 4.03 117.14 6.68 113.11 ✓

132 15.42 3.8 113.4 113.3

+50 4.1 113.0 ✓

133 4.2 112.9 ✓

25.90 113.11

15.42 100.63

10.48 10.98

Mendota rd. levels

R.R. spike in tele. pole R of sta 129+75

1/25/23 Sheet #11 of sheets

Sta + H.I. - Rod Elev

4.03 117.14

EL. +46 4.5 112.6 ✓

134 4.9 112.2 ✓

135 4.8 112.3 ✓

+50 4.7 112.4 ✓

P.T. +82.88 4.6 112.5 ✓

136 4.5 112.6 ✓

+50 4.8 112.3 ✓

137 4.8 112.3 ✓

+50 5.0 112.1 ✓

138 4.9 112.2 ✓

139 4.3 112.8 ✓

PC +69 4.4 112.7 ✓

T.P. 5.71 118.11 4.74 112.40

140 9.74 5.2 112.9 ✓

141 5.0 113.1 ✓

B.M. 6.71 111.40 ✓ 110.90

142 11.45 4.5 113.6 ✓

143 3.8 114.3 ✓

144 4.9 113.2 ✓

+60 5.3 112.8 ✓

145 5.5 112.6 ✓

146 5.0 113.1 ✓

11.45 113.11

9.74 111.40

1.71 1.71

Mendoza rd. Levels Carley A Persons

R.R. spike in tele pole R of sta 141+60

Farm ent R

Farm ent L

Sta + H.I - Rod Elev

5.71 118.11

T.P. 6.23 119.21 5.13 112.98 ✓

146 + 50 6.1 113.1 ✓

147 6.0 113.2 ✓

148 5.6 113.6 ✓

149 4.8 114.4 ✓

150 3.6 115.6 ✓

151 2.8 116.4 ✓

152 1.1 118.1 ✓

B.M. $\frac{8.80}{20.74}$ 124.49 3.52 115.69 ✓

153 5.6 118.9 ✓

154 4.2 120.3 ✓

155 2.0 122.5 ✓

155 + 50 0.8 123.07

T.P. 5.32 125.33 4.48 120.01 ✓
13.13

Xroad L

156 1.9 123.4 ✓

+ 50 3.0 122.3 ✓

157 4.2 121.1 ✓

+ 50 5.4 129.9 ✓

158 5.9 119.4 ✓

159 6.1 119.2 ✓

160 6.8 118.5 ✓

20.74 120.01
13.13 112.40
7.61 7.61

Mendota rd. leve/s. Corley & Parsons ✓

R.R. spike in tele pole R of sta 152+

Xroad Left.

<u>1245</u>	<u>1265</u>	<u>1287</u>	<u>1340</u>	<u>1380</u>
15	26	42	92	152

-1/25/23

Sheet #13 of sheets

Sto + H.I. - Rod Elev.

5.32 125.33

161 6.4 118.9 ✓

T.P. 5.60 123.83 7.10 118.23 ✓

162 4.5 119.3 ✓

163 4.5 119.3 ✓

164 4.5 119.3 ✓

165 4.9 118.9 ✓

B.M. 6.87 124.73 5.97 117.86 ✓

165 + 88.5 B.C. 5.7 119.0 ✓

166 5.7 119.0 ✓

+50 5.7 119.0 ✓

167 5.1 119.6 ✓

168 4.4 120.3 ✓

169 3.0 121.7 ✓

170 1.6 123.1 ✓

T.P. 9.74 132.37 2.10 122.63 ✓

171 27.53 7.2 125.2 ✓

172 4.3 128.1 ✓

173 3.0 129.4 ✓

B.M. 5.82 126.55 ✓

20.99

27.53 126.55

20.99 120.01

6.54 6.54

Mendota rd. levels Carley & Persons /

R.R. spike in tele pole R of sta. 169+58

175.55

Spike in tele pole R of sta 173+70

4/25/23

Sheet # 19 of sheets

Sta.

+

H.I.

-

Red. Elev.

Mendota road Xsections

Carley - Recording
Persons - Hand-Level
Carr - Tape
Mahoney - Rod.

April 14, 25, 1923

Sta

Elev

+50

279.3

26

279.3

Heavy clay

+50

278.6

25

278.4

+50

277.9

24

277.3

clay

+50

276.6

23

276.3

+50

275.2

Heavy clay

22

275.7

+50

275.3

21 + 16.1

275.8

x

x

Mendoza rd. sections

(30)

$$\begin{array}{cccccccccccc} +1.5 & +0.9 & -1.0 & -1.0 & -0.2 & -0.6 & -2.0 & -2.0 & -1.5 & -2.5 & -2.5 \\ \hline 33 & 22 & 19 & 16 & 12 & 13 & 17 & 21 & 22 & 28 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.0 & +0.5 & -1.2 & -1.2 & 0.0 & -0.6 & -2.0 & -2.0 & -1.0 & -2.0 & -3.1 \\ \hline 33 & 29 & 22 & 15 & 12 & 13 & 17 & 20 & 21 & 24 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.5 & +1.0 & -1.0 & -0.9 & -0.5 & -0.7 & -1.5 & -1.4 & -1.5 & -3.0 & -3.0 \\ \hline 33 & 24 & 20 & 16 & 12 & 13 & 16 & 19 & 20 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +2.0 & +1.0 & -1.0 & -1.2 & -0.2 & -0.8 & -1.8 & -1.9 & -1.5 & -2.0 & -2.5 \\ \hline 33 & 26 & 22 & 15 & 12 & 14 & 17 & 20 & 21 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.5 & +1.0 & -1.5 & -1.2 & -0.2 & -0.5 & -1.3 & -1.2 & -1.0 & -1.2 & -0.5 \\ \hline 33 & 29 & 23 & 15 & 12 & 13 & 16 & 19 & 20 & 26 & 33 \end{array}$$

$$\begin{array}{cccccccccc} 0.0 & -1.5 & -1.5 & 0.0 & -0.7 & -1.3 & -1.4 & -0.9 & -0.5 \\ \hline 31 & 26 & 16 & 12 & 13 & 15 & 18 & 19 & 33 \end{array}$$

$$\begin{array}{cccccccccc} -2.0 & -2.0 & -2.0 & -0.2 & -0.1 & -1.0 & -1.0 & -0.8 & -1.0 \\ \hline 33 & 28 & 18 & 12 & 12 & 15 & 18 & 20 & 33 \end{array}$$

$$\begin{array}{cccccccccc} -2.5 & -3.0 & -2.5 & -0.4 & -0.5 & -1.4 & -1.4 & -1.0 & -1.0 \\ \hline 33 & 28 & 19 & 12 & 13 & 15 & 17 & 19 & 33 \end{array}$$

$$\begin{array}{cccccccc} -2.5 & -3.0 & -2.3 & -0.3 & -0.6 & -2.3 & -3.0 \\ \hline 33 & 24 & 19 & 13 & 11 & 16 & 33 \end{array}$$

$$\begin{array}{cccccccc} -2.0 & -0.0 & -3.2 & -0.9 & -0.4 & -5.0 & -31.0 \\ \hline 33 & 25 & 18 & 12 & 10 & 18 & 35 \end{array}$$

267.2 cu/v.

$$\begin{array}{cccccccc} -3.0 & -2.0 & -0.5 & -1.0 & -2.5 & -3.0 & -3.0 \\ \hline 33 & 19 & 12 & 11 & 18 & 26 & 33 \end{array}$$

$$\begin{array}{cccccccc} -1.0 & -1.4 & -1.4 & -0.7 & -0.5 & -0.7 & -0.5 & -0.5 \\ \hline 33 & 22 & 19 & 15 & 10 & 15 & 20 & 33 \end{array}$$

Sta.

Elev.

+50

270.9

32

271.9

+50

273.2

clay

31

274.2

+50

275.4

30

276.9

+50

278.1

Heavy Clay

29

279.1

+50

280.2

28

280.7

clay

+50

280.4

27

279.9

Mendota rd. sections

31

$$\begin{array}{ccccccccc} \frac{0.0}{33} & \frac{-0.5}{25} & \frac{-1.7}{23} & \frac{-1.7}{17} & \frac{-0.5}{13} & \frac{-0.7}{13} & \frac{-1.7}{15} & \frac{-2.0}{21} & \frac{-1.0}{22} & \frac{-1.0}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{0.0}{33} & \frac{-0.5}{33} & \frac{-2.0}{21} & \frac{-2.0}{15} & \frac{-0.5}{12} & \frac{-0.5}{14} & \frac{-2.0}{20} & \frac{-2.0}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+1.0}{33} & \frac{0.0}{24} & \frac{-1.0}{21} & \frac{-0.8}{14} & \frac{0.0}{11} & \frac{-0.5}{14} & \frac{-2.0}{18} & \frac{-2.2}{22} & \frac{-2.0}{23} & \frac{-2.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.5}{33} & \frac{-1.0}{24} & \frac{-0.5}{21} & \frac{-0.7}{13} & \frac{0.0}{11} & \frac{-0.2}{15} & \frac{-1.2}{17} & \frac{-1.0}{21} & \frac{-0.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.5}{33} & \frac{0.0}{24} & \frac{-1.5}{22} & \frac{-1.3}{15} & \frac{-0.3}{12} & \frac{-0.7}{13} & \frac{-1.7}{17} & \frac{-1.8}{21} & \frac{-0.5}{22} & \frac{-0.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+1.0}{33} & \frac{-0.2}{24} & \frac{-1.6}{23} & \frac{-1.5}{15} & \frac{-0.1}{12} & \frac{-0.5}{13} & \frac{-2.3}{18} & \frac{-2.2}{21} & \frac{-2.0}{22} & \frac{-1.5}{25} & \frac{-0.4}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-0.5}{33} & \frac{-1.0}{23} & \frac{-1.6}{21} & \frac{-1.5}{16} & \frac{0.0}{12} & \frac{-0.8}{14} & \frac{-2.0}{18} & \frac{-2.1}{24} & \frac{-1.5}{26} & \frac{-2.4}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+1.2}{33} & \frac{+0.5}{25} & \frac{-1.5}{23} & \frac{-1.5}{16} & \frac{0.0}{12} & \frac{-0.7}{12} & \frac{-1.5}{15} & \frac{-2.3}{17} & \frac{-1.5}{21} & \frac{-1.5}{27} & \frac{-1.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+2.0}{33} & \frac{+0.8}{23} & \frac{-1.1}{20} & \frac{-1.1}{15} & \frac{0.0}{12} & \frac{-0.5}{14} & \frac{-1.2}{16} & \frac{-1.5}{21} & \frac{-0.5}{23} & \frac{-2.0}{24} & \frac{0.0}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+1.5}{33} & \frac{+1.0}{24} & \frac{-0.9}{21} & \frac{-1.0}{15} & \frac{+0.1}{12} & \frac{-1.0}{13} & \frac{-1.5}{16} & \frac{-1.6}{20} & \frac{-1.2}{22} & \frac{-0.5}{31} & \frac{0.0}{35} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+2.5}{33} & \frac{+1.1}{24} & \frac{-0.5}{21} & \frac{-0.9}{15} & \frac{-0.3}{12} & \frac{-0.9}{14} & \frac{-1.6}{17} & \frac{-1.4}{21} & \frac{-0.5}{22} & \frac{-0.7}{24} & \frac{+0.1}{35} \end{array}$$

$$\begin{array}{ccccccccc} \frac{+1.5}{33} & \frac{+0.5}{22} & \frac{-0.5}{20} & \frac{-0.6}{15} & \frac{0.0}{12} & \frac{-0.5}{13} & \frac{-1.4}{17} & \frac{-1.5}{20} & \frac{-1.0}{21} & \frac{-1.0}{24} & \frac{0.0}{33} \end{array}$$

4/14/23

Sheet #3 of 3 sheets

Sta

Elev

X

X

+50

246.4

38

248.4

Clay - Heavy

+50

250.2

37

252.7

+50

255.3

36

257.4

Clay

+50

260.0

35

262.0

3

+50

263.8

34

266.3

Clay

+50

268.1

33

269.6

Mendota rd. sections

32

$$\frac{-0.5}{33} \quad \frac{-0.5}{21} \quad \frac{-0.9}{20} \quad \frac{-2.0}{16} \quad \frac{-0.3}{13} \quad \frac{-0.5}{13} \quad \frac{-1.5}{16} \quad \frac{-1.5}{18} \quad \frac{-0.7}{20} \quad \frac{-2.0}{28} \quad \frac{-2.0}{33}$$

$$\frac{+0.8}{33} \quad \frac{+0.2}{21} \quad \frac{-1.0}{20} \quad \frac{-1.0}{17} \quad \frac{0.0}{12} \quad \frac{-0.4}{11} \quad \frac{-1.5}{14} \quad \frac{-1.0}{19} \quad \frac{0.0}{20} \quad \frac{-0.5}{33}$$

$$\frac{+1.3}{33} \quad \frac{+1.0}{24} \quad \frac{-1.0}{22} \quad \frac{-0.5}{18} \quad \frac{0.0}{15} \quad \frac{-0.2}{9} \quad \frac{-1.4}{13} \quad \frac{-1.4}{15} \quad \frac{+0.5}{16} \quad \frac{0.0}{26} \quad \frac{0.0}{33}$$

$$\frac{+1.0}{33} \quad \frac{+1.0}{22} \quad \frac{-1.2}{17} \quad \frac{0.0}{12} \quad \frac{-0.5}{13} \quad \frac{-1.5}{16} \quad \frac{-1.5}{19} \quad \frac{+1.0}{21} \quad \frac{+1.5}{33}$$

$$\frac{+1.3}{33} \quad \frac{+1.3}{22} \quad \frac{-1.3}{15} \quad \frac{-0.2}{12} \quad \frac{-0.5}{12} \quad \frac{-1.4}{16} \quad \frac{-1.5}{18} \quad \frac{+1.0}{27} \quad \frac{+5.0}{33}$$

$$\frac{+1.5}{33} \quad \frac{+1.5}{24} \quad \frac{-1.5}{17} \quad \frac{-0.5}{13} \quad \frac{-0.5}{12} \quad \frac{-1.3}{14} \quad \frac{+1.5}{18} \quad \frac{+6.0}{28} \quad \frac{+6.5}{33}$$

$$\frac{+1.0}{33} \quad \frac{+1.0}{22} \quad \frac{-1.9}{16} \quad \frac{-0.5}{11} \quad \frac{-0.6}{14} \quad \frac{-1.2}{15} \quad \frac{-1.5}{20} \quad \frac{+0.5}{22} \quad \frac{+3.0}{28} \quad \frac{+3.0}{33}$$

$$\frac{0.0}{33} \quad \frac{0.0}{22} \quad \frac{-1.5}{19} \quad \frac{-1.5}{14} \quad \frac{-0.5}{12} \quad \frac{-0.2}{21} \quad \frac{-1.0}{23} \quad \frac{0.0}{33}$$

$$\frac{0.0}{33} \quad \frac{0.0}{21} \quad \frac{-1.0}{19} \quad \frac{-0.5}{14} \quad \frac{0.0}{12} \quad \frac{-0.5}{14} \quad \frac{-1.0}{50} \quad \frac{-1.5}{19} \quad \frac{-0.6}{21} \quad \frac{-0.6}{33}$$

$$\frac{0.0}{33} \quad \frac{-1.0}{23} \quad \frac{-2.1}{21} \quad \frac{-2.0}{15} \quad \frac{-0.5}{12} \quad \frac{-0.5}{13} \quad \frac{-1.0}{15} \quad \frac{-1.6}{19} \quad \frac{0.0}{21} \quad \frac{0.0}{33}$$

$$\frac{+1.6}{33} \quad \frac{+1.0}{30} \quad \frac{0.0}{22} \quad \frac{-1.3}{20} \quad \frac{-2.0}{15} \quad \frac{-0.4}{11} \quad \frac{-0.5}{14} \quad \frac{-1.0}{17} \quad \frac{-1.4}{21} \quad \frac{+1.0}{23} \quad \frac{+1.0}{33}$$

$$\frac{+1.0}{33} \quad \frac{+1.0}{22} \quad \frac{-1.2}{21} \quad \frac{-1.2}{13} \quad \frac{-0.1}{11} \quad \frac{-0.5}{13} \quad \frac{-1.5}{16} \quad \frac{-1.6}{19} \quad \frac{0.0}{21} \quad \frac{0.0}{33}$$

Sta

Elev.

+50

238.8

44

240.4

clay

+50

240.4

43

240.8

+50

241.0

42

241.6

clay

+50

241.8

41

242.3

light gravel

+50

242.7

40

243.5

+50

244.0

39

245.5

Mendoza rd. Xsections

$$\begin{array}{r} -3.2 \\ \hline 17 \end{array} \quad \begin{array}{r} -3.2 \\ \hline 17 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 13 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 13 \end{array} \quad \begin{array}{r} -3.5 \\ \hline 20 \end{array} \quad \begin{array}{r} -3.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -3.6 \\ 17 \end{array} \quad \begin{array}{r} -3.6 \\ 17 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.6 \\ 12 \end{array} \quad \begin{array}{r} -2.3 \\ 20 \end{array} \quad \begin{array}{r} -3.0 \\ 33 \end{array}$$

$\frac{-1.0}{33}$	$\frac{-9.0}{17}$	$\frac{-0.5}{12}$	$\frac{-0.7}{13}$	$\frac{-3.0}{20}$	$\frac{-2.5}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$$\begin{array}{r} -3.6 \\ 33 \end{array} \quad \begin{array}{r} -3.6 \\ 17 \end{array} \quad \begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -0.5 \\ 10 \end{array} \quad \begin{array}{r} -1.0 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 33 \end{array}$$

$\frac{-10}{33}$	$\frac{-17}{22}$	$\frac{-23}{21}$	$\frac{-23}{17}$	$\frac{-0.5}{12}$	$\frac{-0.4}{13}$	$\frac{-1.8}{19}$	$\frac{-1.8}{21}$	$\frac{-1.0}{22}$	$\frac{-0.5}{33}$
------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

10.5	0.0	-1.5	-1.5	-2.0	-2.0	-0.5	0.0	-2.0	-2.1	-1.5	-1.2
33	26	24	22	21	18	12	12	18	22	23	33

0.0	-0.5	-1.8	-1.5	-0.2	0.0	-2.0	-2.0	-1.5	-1.5
33	20	19	15	11	13	19	22	23	33

-0.7	-0.8	-1.5	-1.5	-0.2	-0.3	-2.3	-2.4	-2.4	-2.0	-2.0
33	22	21	16	12	13	16	30	22	23	33

$$\begin{array}{cccccccccccc} -0.7 & -0.7 & -1.3 & -1.3 & -0.4 & -0.5 & -2.3 & -2.3 & -2.0 & -3.1 & -3.1 \\ \hline 33 & 22 & 21 & 17 & 13 & 13 & 18 & 21 & 22 & 28 & 33 \end{array}$$

$$\frac{-1.0}{33} \quad \frac{-1.0}{21} \quad \frac{-1.5}{20} \quad \frac{-1.5}{15} \quad \frac{-0.5}{11} \quad \frac{-0.6}{12} \quad \frac{-2.0}{17} \quad \frac{-2.0}{21} \quad \frac{-3.1}{29} \quad \frac{-3.3}{33}$$

$\frac{-1.5}{33}$	$\frac{-1.0}{21}$	$\frac{-1.5}{19}$	$\frac{-1.0}{14}$	$\frac{-0.3}{12}$	$\frac{-0.5}{13}$	$\frac{-1.9}{18}$	$\frac{-2.0}{22}$	$\frac{-1.7}{23}$	$\frac{-2.0}{29}$	$\frac{-2.4}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$$\begin{array}{cccccccccccc} \frac{-1.0}{33} & \frac{-1.0}{21} & \frac{-2.0}{18} & \frac{-1.3}{15} & \frac{0.0}{12} & \frac{-0.5}{12} & \frac{-1.8}{16} & \frac{-2.0}{19} & \frac{-1.5}{20} & \frac{-2.2}{29} & \frac{-2.8}{33} \end{array}$$

Sta

Elev.

x

x

51

234.1

+50

235.3

50

236.1

clay

+50

236.4

49

237.2

+50

237.5

Some gravel

48

237.8

+50

237.7

47

238.4

+50

237.8

46

238.8

clay

+50

239.1

45

239.7

Mendota rd Xsections

34

$$\frac{+1.0}{33} \quad \frac{+0.6}{21} \quad \frac{-1.1}{19} \quad \frac{-1.0}{14} \quad \frac{-0.4}{12} \quad \frac{-0.5}{12} \quad \frac{-1.2}{14} \quad \frac{-1.3}{17} \quad \frac{+0.8}{19} \quad \frac{+1.0}{33}$$

$$\frac{+2.5}{33} \quad \frac{+2.0}{24} \quad \frac{-1.1}{17} \quad \frac{-1.0}{14} \quad \frac{-0.5}{12} \quad \frac{-0.5}{11} \quad \frac{-1.3}{13} \quad \frac{-1.4}{16} \quad \frac{+1.0}{19} \quad \frac{0.0}{33}$$

$$\frac{+5.0}{33} \quad \frac{+4.1}{24} \quad \frac{-0.6}{17} \quad \frac{-0.6}{14} \quad \frac{-0.2}{12} \quad \frac{-0.4}{12} \quad \frac{-1.0}{14} \quad \frac{-1.0}{16} \quad \frac{+0.5}{18} \quad \frac{+1.0}{33}$$

$$\frac{+5.0}{33} \quad \frac{+4.5}{26} \quad \frac{-0.4}{18} \quad \frac{-1.0}{14} \quad \frac{-0.5}{12} \quad \frac{-0.5}{11} \quad \frac{-1.2}{14} \quad \frac{-1.2}{16} \quad \frac{+3.0}{22} \quad \frac{+2.5}{33}$$

$$\frac{+5.3}{33} \quad \frac{+5.0}{32} \quad \frac{-1.3}{19} \quad \frac{-1.2}{14} \quad \frac{-0.5}{12} \quad \frac{-0.5}{12} \quad \frac{-1.0}{14} \quad \frac{-0.6}{18} \quad \frac{-0.6}{20} \quad \frac{+5.0}{28} \quad \frac{+5.0}{33}$$

$$\frac{+1.0}{35} \quad \frac{0.0}{31} \quad \frac{-0.2}{15} \quad \frac{0.0}{12} \quad \frac{-1.0}{13} \quad \frac{-0.8}{20} \quad \frac{+5.0}{27} \quad \frac{+5.0}{33}$$

$$\frac{+9.0}{35} \quad \frac{0.0}{20} \quad \frac{-0.8}{18} \quad \frac{-0.7}{16} \quad \frac{-0.3}{13} \quad \frac{-0.4}{14} \quad \frac{-0.8}{17} \quad \frac{+5.0}{34}$$

$$\frac{+3.5}{33} \quad \frac{+3.5}{23} \quad \frac{-1.6}{16} \quad \frac{-1.5}{14} \quad \frac{-0.5}{12} \quad \frac{-0.5}{13} \quad \frac{-1.5}{18} \quad \frac{+1.6}{28} \quad \frac{+1.0}{33}$$

$$\frac{-3.1}{33} \quad \frac{-3.1}{28} \quad \frac{-2.0}{21} \quad \frac{-1.0}{15} \quad \frac{-0.3}{12} \quad \frac{-0.5}{15} \quad \frac{-2.5}{21} \quad \frac{-2.5}{33}$$

$$\frac{-3.0}{33} \quad \frac{-1.5}{30} \quad \frac{-1.2}{18} \quad \frac{-0.3}{10} \quad \frac{-0.4}{13} \quad \frac{-2.1}{17} \quad \frac{-4.5}{33}$$

$$\frac{-5.5}{33} \quad \frac{-5.5}{23} \quad \frac{-0.4}{13} \quad \frac{-0.5}{11} \quad \frac{-5.0}{21} \quad \frac{-3.5}{27} \quad \frac{-1.0}{33}$$

$$\frac{-2.9}{33} \quad \frac{-2.5}{19} \quad \frac{-0.2}{12} \quad \frac{-0.5}{11} \quad \frac{-3.5}{21} \quad \frac{-1.5}{25} \quad \frac{-2.0}{33}$$

$$\frac{-2.5}{33} \quad \frac{-1.0}{21} \quad \frac{-1.5}{20} \quad \frac{-1.5}{17} \quad \frac{0.0}{12} \quad \frac{-0.1}{12} \quad \frac{-1.5}{17} \quad \frac{-2.5}{21} \quad \frac{-1.0}{26} \quad \frac{-1.0}{33}$$

Sta

Elev

57 200.7

+50 203.3

56 205.7

+50 208.9

55 211.7

+50 214.7

54 217.7

+50 220.9

53 223.5

+50 226.2

52 229.2

+50 231.5

yellow clay.

Heavy clay

Mendota rd X sections

Top of bank
about +250

$$\frac{+5.3}{23} \quad \frac{-0.4}{18} \quad \frac{-0.6}{15} \quad \frac{-0.3}{12} \quad \frac{-0.4}{14} \quad \frac{-1.8}{20} \quad \frac{-4.7}{33} \quad 0$$

$$\frac{+5.3}{23} \quad \frac{-0.1}{18} \quad \frac{-0.8}{14} \quad \frac{-0.3}{13} \quad \frac{-0.1}{14} \quad \frac{-1.1}{17} \quad \frac{-5.1}{33}$$

$$\frac{+5.3}{22} \quad \frac{-0.6}{18} \quad \frac{-1.1}{14} \quad \frac{-0.4}{13} \quad \frac{0.0}{12} \quad \frac{-1.0}{17} \quad \frac{-2.6}{27} \quad \frac{-5.0}{33}$$

Top of bank
about +150

$$\frac{+5.8}{20} \quad \frac{-0.3}{15} \quad \frac{-0.8}{11} \quad \frac{-0.6}{10} \quad \frac{+0.9}{14} \quad \frac{-0.3}{16} \quad \frac{-0.4}{18} \quad \frac{+0.3}{19} \quad \frac{-1.4}{33}$$

$$\frac{+5.8}{20} \quad \frac{-0.9}{15} \quad \frac{-0.8}{12} \quad \frac{-0.3}{11} \quad \frac{0.0}{12} \quad \frac{-1.0}{14} \quad \frac{-1.1}{17} \quad \frac{+7.5}{27} \quad \frac{+5.0}{33}$$

$$\frac{+5.8}{22} \quad \frac{-1.1}{17} \quad \frac{-1.1}{15} \quad \frac{-0.1}{10} \quad \frac{-0.3}{12} \quad \frac{-0.8}{14} \quad \frac{-0.9}{16} \quad \frac{+5.0}{23} \quad \frac{9.6}{29} \quad \frac{9.6}{33}$$

$$\frac{+11.3}{33} \quad \frac{+11.0}{30} \quad \frac{+5.0}{26} \quad \frac{-0.8}{17} \quad \frac{-0.9}{13} \quad \frac{0.0}{12} \quad \frac{-0.7}{12} \quad \frac{-1.1}{13} \quad \frac{-0.6}{16} \quad \frac{+5.0}{23} \quad \frac{+8.7}{28} \quad \frac{+8.7}{33}$$

$$\frac{+7.0}{33} \quad \frac{+6.8}{25} \quad \frac{-0.5}{18} \quad \frac{-0.6}{15} \quad \frac{+0.2}{14} \quad \frac{-0.7}{12} \quad \frac{-1.6}{13} \quad \frac{-1.6}{15} \quad \frac{+1.9}{18} \quad \frac{+1.0}{24} \quad \frac{-4.1}{33}$$

$$\frac{+5.6}{33} \quad \frac{+4.8}{25} \quad \frac{-0.8}{18} \quad \frac{-0.7}{16} \quad \frac{+0.4}{14} \quad \frac{-0.7}{12} \quad \frac{-1.6}{14} \quad \frac{-1.7}{17} \quad \frac{-0.2}{18} \quad \frac{-0.5}{25} \quad \frac{-4.7}{33}$$

$$\frac{+3.8}{33} \quad \frac{+3.3}{29} \quad \frac{+0.8}{22} \quad \frac{-1.0}{21} \quad \frac{-0.9}{18} \quad \frac{+0.5}{12} \quad \frac{-0.9}{14} \quad \frac{-1.8}{16} \quad \frac{-1.8}{17} \quad \frac{-1.4}{18} \quad \frac{-1.8}{33}$$

$$\frac{+5.3}{39} \quad \frac{+4.5}{29} \quad \frac{-1.1}{16} \quad \frac{-1.0}{14} \quad \frac{+0.4}{12} \quad \frac{-0.7}{12} \quad \frac{-5.3}{24} \quad \frac{-2.9}{33}$$

$$\frac{+2.6}{33} \quad \frac{+6.6}{20} \quad \frac{0.0}{18} \quad \frac{0.0}{15} \quad \frac{+0.3}{14} \quad \frac{-0.5}{13} \quad \frac{-1.6}{16} \quad \frac{-1.4}{19} \quad \frac{-0.6}{20} \quad \frac{-0.6}{33}$$

7/26/23

Sheet # 7 of Sheets

Sta

Elev

63

163.9

+50

167.3

62

170.2

+50

172.8

61

176.4

+50

179.4

Green soil

60

182.5

+50

185.8

Heavy clay

59

188.6

+50

191.6

58

194.7

+50

198.1

Mendota rd X sections

Top of bank about
+ 45.0

$$\left(\begin{array}{cccccc} \frac{+5.3}{26} & \frac{-1.0}{12} & \frac{0.0}{12} & \frac{-5.0}{21} \\ \frac{+5.3}{26} & \frac{0.0}{20} & \frac{-0.2}{10} & \frac{0.0}{16} & \frac{-5.0}{20} \\ \frac{+5.3}{18} & \frac{-0.9}{14} & \frac{-0.8}{12} & \frac{0.0}{11} & \frac{0.0}{16} & \frac{-5.0}{22} \\ \frac{+5.3}{21} & \frac{-0.9}{15} & \frac{-0.8}{11} & \frac{-0.1}{10} & \frac{-0.4}{14} & \frac{-5.0}{18} \end{array} \right)$$

Bottom of bank
4647-3570

Top of bank about
+45.0

$$\left(\begin{array}{cccccc} \frac{+5.3}{19} & \frac{-0.9}{14} & \frac{-1.0}{11} & \frac{-0.3}{9} & \frac{-0.3}{13} & \frac{-5.0}{18} \\ \frac{+5.0}{20} & \frac{0.0}{14} & \frac{-0.7}{12} & \frac{0.0}{10} & \frac{-0.3}{14} & \frac{-5.0}{20} \\ \frac{+5.3}{21} & \frac{+0.6}{17} & \frac{-0.7}{14} & \frac{-0.2}{12} & \frac{-0.3}{13} & \frac{-5.0}{20} \\ \frac{+5.3}{22} & \frac{-0.3}{18} & \frac{-0.9}{14} & \frac{-0.1}{12} & \frac{-0.3}{15} & \frac{-5.3}{20} \\ \frac{+5.3}{20} & \frac{0.0}{14} & \frac{-0.3}{12} & \frac{0.0}{11} & \frac{-0.8}{15} & \frac{-5.0}{20} \end{array} \right)$$

Bottom of bank about
-35.0

Top of bank
about 435

$$\left. \begin{array}{r} \frac{+5.0}{21} \quad \frac{-0.7}{17} \quad \frac{-0.7}{12} \quad \frac{-0.3}{11} \quad \frac{-0.1}{12} \quad \frac{-5.0}{19} \\ \frac{+5.3}{24} \quad \frac{-0.7}{17} \quad \frac{-1.3}{13} \quad \frac{-0.3}{12} \quad \frac{-0.2}{13} \quad \frac{-5.0}{18} \\ \frac{+5.3}{23} \quad \frac{-0.3}{18} \quad \frac{-0.8}{13} \quad \frac{-0.5}{12} \quad \frac{-0.2}{14} \quad \frac{-5.0}{20} \end{array} \right\}$$

Bottom about
- 35 -

Sta

Elev

65

157.9

X

+50

155.1

Green soil X

67

158.1

clay

+50

160.9

Top of bank about

+45.0

$\frac{+5.3}{22}$	$\frac{0.0}{17}$	$\frac{-0.8}{15}$	$\frac{-0.2}{14}$	$\frac{0.0}{11}$	$\frac{-2.1}{18}$	$\frac{-5.0}{23}$
$\frac{+5.3}{20}$	$\frac{-0.2}{16}$	$\frac{-0.3}{14}$	$\frac{0.0}{13}$	$\frac{0.0}{15}$	$\frac{-5.0}{26}$	
$\frac{+5.0}{20}$	$\frac{-0.2}{16}$	$\frac{-0.4}{13}$	$\frac{+0.3}{12}$	$\frac{0.0}{12}$	$\frac{-5.0}{17}$	
$\frac{+5.3}{19}$	$\frac{-0.5}{14}$	$\frac{-0.4}{13}$	$\frac{0.0}{12}$	$\frac{-0.2}{14}$	$\frac{-5.0}{20}$	

Bottom of bank
about

-35.0

Sta.	Elev.
+67	118.8
+50	119.8
70.	121.9
+50	124.4
69	127.3
+50	130.3
68	133.5
+50	136.6
67	139.4
+50	142.5
66	145.3
+50	148.3
65 + 37.5	178.9

clay

Heavy clay

Mendota rd. sections

38

$$\begin{array}{r} -4.0 \\ 33 \end{array} \quad \begin{array}{r} -2.5 \\ 20 \end{array} \quad \begin{array}{r} -0.2 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 13 \end{array} \quad \begin{array}{r} -7.1 \\ 23 \end{array} \quad \begin{array}{r} -7.2 \\ 33 \end{array}$$

$$\begin{array}{r} -2.5 \\ 33 \end{array} \quad \begin{array}{r} -3.5 \\ 20 \end{array} \quad \begin{array}{r} -0.3 \\ 12 \end{array} \quad \begin{array}{r} -0.4 \\ 14 \end{array} \quad \begin{array}{r} -4.3 \\ 21 \end{array} \quad \begin{array}{r} -4.4 \\ 33 \end{array}$$

$$\begin{array}{r} -3.5 \\ 34 \end{array} \quad \begin{array}{r} -5.1 \\ 32 \end{array} \quad \begin{array}{r} -5.0 \\ 27 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} -0.3 \\ 11 \end{array} \quad \begin{array}{r} -8.1 \\ 27 \end{array} \quad \begin{array}{r} -8.3 \\ 33 \end{array}$$

$$\begin{array}{r} -2.5 \\ 33 \end{array} \quad \begin{array}{r} -2.4 \\ 19 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.2 \\ 9 \end{array} \quad \begin{array}{r} -10.2 \\ 33 \end{array}$$

$$\begin{array}{r} +0.6 \\ 33 \end{array} \quad \begin{array}{r} -0.4 \\ 22 \end{array} \quad \begin{array}{r} -4.3 \\ 21 \end{array} \quad \begin{array}{r} -4.2 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -9.1 \\ 33 \end{array}$$

$$\begin{array}{r} +1.5 \\ 33 \end{array} \quad \begin{array}{r} +1.0 \\ 28 \end{array} \quad \begin{array}{r} 0.0 \\ 22 \end{array} \quad \begin{array}{r} -1.6 \\ 21 \end{array} \quad \begin{array}{r} -1.5 \\ 17 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -7.5 \\ 33 \end{array}$$

$$\begin{array}{r} +2.5 \\ 33 \end{array} \quad \begin{array}{r} +1.0 \\ 23 \end{array} \quad \begin{array}{r} -1.3 \\ 20 \end{array} \quad \begin{array}{r} -1.2 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} -1.0 \\ 15 \end{array} \quad \begin{array}{r} -8.1 \\ 33 \end{array}$$

$$\begin{array}{r} +6.1 \\ 30 \end{array} \quad \begin{array}{r} +5.0 \\ 26 \end{array} \quad \begin{array}{r} -0.5 \\ 16 \end{array} \quad \begin{array}{r} -0.2 \\ 14 \end{array} \quad \begin{array}{r} -0.2 \\ 12 \end{array} \quad \begin{array}{r} -0.5 \\ 15 \end{array} \quad \begin{array}{r} -2.0 \\ 23 \end{array} \quad \begin{array}{r} -5.0 \\ 33 \end{array}$$

$$\begin{array}{r} +5.9 \\ 33 \end{array} \quad \begin{array}{r} +5.5 \\ 30 \end{array} \quad \begin{array}{r} +3.5 \\ 21 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} +0.2 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} -10.6 \\ 33 \end{array}$$

$$\begin{array}{r} +10.0 \\ 28 \end{array} \quad \begin{array}{r} +5.0 \\ 23 \end{array} \quad \begin{array}{r} -0.5 \\ 18 \end{array} \quad \begin{array}{r} -0.5 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 14 \end{array} \quad \begin{array}{r} -0.5 \\ 14 \end{array} \quad \begin{array}{r} -1.5 \\ 23 \end{array} \quad \begin{array}{r} -7.0 \\ 33 \end{array}$$

$$\begin{array}{r} +15.0 \\ 31 \end{array} \quad \begin{array}{r} +5.0 \\ 22 \end{array} \quad \begin{array}{r} 0.0 \\ 17 \end{array} \quad \begin{array}{r} -0.4 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.3 \\ 13 \end{array} \quad \begin{array}{r} -1.0 \\ 16 \end{array} \quad \begin{array}{r} -3.0 \\ 23 \end{array} \quad \begin{array}{r} -9.1 \\ 33 \end{array}$$

$$\begin{array}{r} +9.4 \\ 25 \end{array} \quad \begin{array}{r} +5.0 \\ 21 \end{array} \quad \begin{array}{r} -0.6 \\ 16 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array} \quad \begin{array}{r} -0.4 \\ 10 \end{array} \quad \begin{array}{r} -1.1 \\ 14 \end{array} \quad \begin{array}{r} -2.5 \\ 20 \end{array} \quad \begin{array}{r} -10.0 \\ 30 \end{array}$$

4/1/33

Sheet # of sheets

Sta

Elev.

+50

112.5

78

113.4

+50

113.5

77

113.8

+50

113.9

76

114.4

+50

114.3

75

114.4

+50

113.7

74

114.4

73

115.7

72

117.0

71

118.3

Clay & rock

about 1' of clay over base rock

X

X

Bridge

Bridge

X

X

X

Mendota rd. X sections

39

$\frac{-0.5}{33}$ $\frac{-1.5}{25}$ $\frac{-2.4}{23}$ $\frac{-2.3}{16}$ $\frac{-0.4}{12}$ $\frac{-0.5}{12}$ $\frac{-2.0}{16}$ $\frac{-2.0}{22}$ $\frac{-1.1}{23}$ $\frac{-1.0}{33}$

$\frac{-1.5}{33}$ $\frac{-1.3}{26}$ $\frac{-2.4}{24}$ $\frac{-2.4}{17}$ $\frac{-0.4}{12}$ $\frac{-0.8}{12}$ $\frac{-2.5}{15}$ $\frac{-2.0}{23}$ $\frac{-1.6}{24}$ $\frac{-2.0}{30}$ $\frac{-4.5}{33}$

$\frac{-1.2}{33}$ $\frac{-2.5}{29}$ $\frac{-2.5}{16}$ $\frac{-0.4}{12}$ $\frac{-0.8}{11}$ $\frac{-2.8}{16}$ $\frac{-2.6}{22}$ $\frac{-2.2}{25}$ $\frac{-3.0}{33}$

$\frac{-1.0}{33}$ $\frac{-2.6}{30}$ $\frac{-3.0}{25}$ $\frac{-2.5}{16}$ $\frac{-0.5}{12}$ $\frac{-0.3}{11}$ $\frac{-2.1}{14}$ $\frac{-2.1}{21}$ $\frac{-1.7}{24}$ $\frac{-2.5}{30}$ $\frac{-7.0}{33}$

$\frac{-0.4}{33}$ $\frac{-0.5}{30}$ $\frac{-2.0}{23}$ $\frac{-2.0}{17}$ $\frac{-0.5}{12}$ $\frac{-0.5}{11}$ $\frac{-1.7}{14}$ $\frac{-1.8}{21}$ $\frac{-1.5}{23}$ $\frac{-7.0}{33}$

$\frac{0.0}{33}$ $\frac{-1.9}{24}$ $\frac{-2.1}{22}$ $\frac{-1.9}{16}$ $\frac{-0.4}{12}$ $\frac{-0.2}{11}$ $\frac{-1.4}{14}$ $\frac{-1.4}{19}$ $\frac{-0.5}{25}$ $\frac{-4.0}{33}$

$\frac{0.0}{33}$ $\frac{-1.5}{26}$ $\frac{-2.4}{23}$ $\frac{-2.0}{16}$ $\frac{-0.5}{12}$ $\frac{-0.3}{12}$ $\frac{-1.7}{15}$ $\frac{-1.5}{21}$ $\frac{-0.4}{25}$ $\frac{-0.5}{33}$

$\frac{-1.0}{33}$ $\frac{-1.3}{29}$ $\frac{-2.5}{24}$ $\frac{-1.2}{15}$ $\frac{-0.4}{12}$ $\frac{-0.5}{11}$ $\frac{-1.5}{14}$ $\frac{-1.5}{21}$ $\frac{0.0}{26}$ $\frac{-0.5}{33}$

$\frac{-1.4}{33}$ $\frac{-1.5}{28}$ $\frac{-2.0}{26}$ $\frac{-1.7}{16}$ $\frac{-0.5}{13}$ $\frac{-0.6}{11}$ $\frac{-1.4}{13}$ $\frac{-1.0}{21}$ $\frac{-4.4}{33}$

$\frac{-1.5}{33}$ $\frac{-1.5}{31}$ $\frac{-0.7}{16}$ $\frac{-0.2}{12}$ $\frac{0.0}{12}$ $\frac{-0.6}{15}$ $\frac{-5.0}{23}$ $\frac{-6.1}{33}$

550	Elev
85	109.9
+50	110.7
84	111.4
+50	111.5
83	111.7
+50	111.8
82	111.9
+50	112.0
81	112.3
+50	112.4
80	112.7
+50	112.8
79	112.9

about 1' or 2' of clay over loose rock

Mendota rd X sections

40

$\frac{0.0}{33}$ $\frac{-0.2}{23}$ $\frac{-1.0}{19}$ $\frac{-1.2}{15}$ $\frac{-0.3}{12}$ $\frac{-0.6}{13}$ $\frac{-3.0}{19}$ $\frac{-3.2}{26}$ $\frac{-1.5}{30}$ $\frac{-1.5}{33}$

$\frac{0.0}{33}$ $\frac{0.0}{29}$ $\frac{+0.2}{24}$ $\frac{-0.6}{21}$ $\frac{-1.5}{20}$ $\frac{-1.5}{16}$ $\frac{-0.5}{13}$ $\frac{-0.5}{12}$ $\frac{-1.5}{15}$ $\frac{-2.0}{24}$ $\frac{-0.5}{29}$ $\frac{-0.8}{33}$

$\frac{0.0}{33}$ $\frac{0.0}{24}$ $\frac{-1.0}{20}$ $\frac{-1.5}{15}$ $\frac{-0.1}{12}$ $\frac{-0.4}{12}$ $\frac{-1.5}{16}$ $\frac{-1.6}{28}$ $\frac{0.0}{30}$ $\frac{0.0}{33}$

$\frac{-1.0}{27}$ $\frac{-0.4}{21}$ $\frac{-1.6}{20}$ $\frac{-1.5}{15}$ $\frac{-0.4}{12}$ $\frac{-0.3}{12}$ $\frac{-1.0}{19}$ $\frac{-1.0}{26}$ $\frac{0.0}{32}$ $\frac{0.0}{33}$

$\frac{-1.1}{33}$ $\frac{-1.0}{23}$ $\frac{-1.9}{20}$ $\frac{-1.4}{15}$ $\frac{-0.5}{12}$ $\frac{-0.4}{12}$ $\frac{-1.0}{15}$ $\frac{-1.4}{28}$ $\frac{-0.5}{30}$ $\frac{-0.4}{33}$

$\frac{-0.5}{33}$ $\frac{-0.5}{26}$ $\frac{-1.5}{23}$ $\frac{-1.2}{16}$ $\frac{-0.4}{13}$ $\frac{-0.4}{12}$ $\frac{-1.0}{15}$ $\frac{-1.2}{27}$ $\frac{-0.5}{30}$ $\frac{-0.5}{33}$

$\frac{-1.0}{33}$ $\frac{-1.4}{14}$ $\frac{-0.3}{12}$ $\frac{-0.5}{12}$ $\frac{-1.4}{15}$ $\frac{-1.0}{28}$ $\frac{-0.5}{29}$ $\frac{-0.5}{33}$

$\frac{0.0}{33}$ $\frac{-0.5}{30}$ $\frac{-1.0}{23}$ $\frac{-1.1}{16}$ $\frac{0.0}{12}$ $\frac{-0.4}{12}$ $\frac{-1.5}{15}$ $\frac{-1.0}{29}$ $\frac{-0.2}{33}$

$\frac{-1.0}{33}$ $\frac{-1.0}{26}$ $\frac{-1.2}{25}$ $\frac{-1.1}{15}$ $\frac{-0.4}{12}$ $\frac{-0.3}{12}$ $\frac{-1.5}{18}$ $\frac{-1.6}{29}$ $\frac{+0.5}{31}$ $\frac{+0.4}{33}$

$\frac{+0.2}{33}$ $\frac{0.0}{23}$ $\frac{-0.2}{12}$ $\frac{-0.5}{12}$ $\frac{-1.3}{15}$ $\frac{-2.0}{27}$ $\frac{-1.0}{30}$ $\frac{-1.0}{33}$

$\frac{-0.9}{33}$ $\frac{-0.9}{20}$ $\frac{-1.6}{18}$ $\frac{-1.5}{14}$ $\frac{-0.3}{12}$ $\frac{-0.5}{11}$ $\frac{-1.4}{16}$ $\frac{-2.0}{28}$ $\frac{-1.5}{30}$ $\frac{-1.5}{33}$

$\frac{-1.1}{33}$ $\frac{-1.1}{27}$ $\frac{-2.1}{25}$ $\frac{-2.0}{14}$ $\frac{-0.4}{12}$ $\frac{-0.5}{11}$ $\frac{-1.5}{15}$ $\frac{-2.0}{21}$ $\frac{-1.3}{33}$

$\frac{-1.5}{27}$ $\frac{-2.2}{25}$ $\frac{-2.2}{16}$ $\frac{-0.5}{12}$ $\frac{-0.6}{11}$ $\frac{-2.0}{15}$ $\frac{-2.0}{18}$ $\frac{-1.5}{20}$ $\frac{-3.0}{33}$

4/19/23

Sheet # of sheets.

Sta

Elev

+50

108.9

91

109.1

+50

109.1

90

109.3

+50

109.2

89

109.1

+50

109.1

88

109.8

+50

110.1

87

110.4

+50

110.7

86

109.8

+50

109.8

Rock

clay

Mendota rd X sections

$$\begin{array}{ccccccccccc} -0.9 & -0.9 & -1.7 & -1.6 & -0.2 & -0.2 & -1.5 & -1.5 & -2.5 & -1.5 \\ \hline 83 & 25 & 24 & 17 & 13 & 13 & 16 & 22 & 28 & 34 \end{array}$$

$$\begin{array}{cccccccc} 7.1 & 1.7 & 1.6 & 0.0 & -0.1 & -1.4 & -1.9 & -1.5 \\ \hline 23 & 22 & 15 & 12 & 14 & 17 & 28 & 35 \end{array}$$

$$\begin{array}{ccccccccccc} 1.0 & -1.0 & -1.4 & -1.5 & 0.0 & -0.4 & -1.5 & -2.2 & -1.7 & -1.7 \\ \hline 33 & 22 & 20 & 16 & 12 & 12 & 15 & 27 & 29 & 33 \end{array}$$

$$\begin{array}{cccccccc} -1.2 & -1.8 & -1.7 & -0.3 & -0.3 & -1.5 & -2.0 \\ \hline 22 & 20 & 16 & 12 & 13 & 16 & 33 \end{array}$$

$$\begin{array}{cccccccc} -1.2 & -1.2 & -2.0 & -0.2 & -0.1 & -1.5 & -1.5 \\ \hline 33 & 19 & 16 & 11 & 13 & 16 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} -2.0 & -1.7 & -1.7 & -0.2 & -0.4 & -2.0 & -2.5 & -4.0 & -9.0 \\ \hline 21 & 20 & 16 & 12 & 12 & 17 & 22 & 30 & 33 \end{array}$$

$$\begin{array}{cccccccc} 1.6 & 1.6 & -2.1 & -2.0 & 0.0 & -0.1 & -1.6 & -2.4 \\ \hline 33 & 20 & 18 & 15 & 11 & 13 & 19 & 33 \end{array}$$

$$\begin{array}{cccccccc} -1.9 & -1.9 & -2.6 & -2.8 & -0.3 & -0.4 & -1.5 & -2.0 & -2.7 \\ \hline 33 & 19 & 17 & 14 & 12 & 12 & 14 & 23 & 33 \end{array}$$

$$\begin{array}{cccccccc} -2.2 & -2.2 & -2.6 & -0.4 & -0.3 & -1.1 & -2.0 \\ \hline 33 & 18 & 16 & 12 & 12 & 14 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} -2.5 & -2.5 & -3.1 & -0.5 & -0.3 & -2.4 & -2.0 & -3.0 & -3.0 & -2.5 \\ \hline 33 & 20 & 16 & 12 & 13 & 16 & 21 & 23 & 32 & 34 \end{array}$$

$$\begin{array}{cccccccc} -2.4 & -2.4 & -3.5 & -0.7 & -0.7 & -3.5 & -3.6 & -3.0 \\ \hline 33 & 21 & 16 & 12 & 13 & 23 & 33 & 34 \end{array}$$

$$\begin{array}{cccccccc} -1.6 & -2.3 & -2.3 & -0.5 & -0.5 & -2.0 & -3.0 & -2.7 \\ \hline 21 & 20 & 15 & 12 & 13 & 16 & 32 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} -0.5 & -0.5 & 1.4 & 1.5 & -0.1 & -0.5 & -1.8 & -3.1 & -2.0 & -2.0 \\ \hline 33 & 22 & 19 & 17 & 14 & 10 & 13 & 24 & 26 & 33 \end{array}$$

1/19/23

Sheet # of sheets

Sta.	Elev
98	107.3
150	106.1
97	107.2
150	107.6
96	107.7
150	107.8
95	107.7
150	108.0
94	108.2
150	108.3
93	108.5
150	108.6
92	108.8

Loose Rock covered by about 1' of clay

Mendota rd sections

42

$$\begin{array}{ccccccccc} \frac{-0.7}{33} & \frac{-0.8}{22} & \frac{-1.7}{20} & \frac{-1.6}{15} & \frac{-0.4}{12} & \frac{-0.6}{12} & \frac{-2.1}{16} & \frac{-2.1}{21} & \frac{-1.5}{24} & \frac{-2.4}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{0.0}{33} & \frac{0.0}{21} & \frac{-1.2}{20} & \frac{-1.3}{14} & \frac{-0.3}{11} & \frac{-0.2}{14} & \frac{-1.5}{18} & \frac{-1.4}{23} & \frac{-0.7}{25} & \frac{-0.9}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-0.5}{33} & \frac{-0.5}{22} & \frac{-1.6}{21} & \frac{-1.5}{16} & \frac{-0.1}{12} & \frac{-0.1}{13} & \frac{-2.0}{16} & \frac{-2.5}{24} & \frac{-1.6}{25} & \frac{-3.0}{31} & \frac{-4.1}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-0.4}{33} & \frac{-0.5}{17} & \frac{-1.1}{14} & \frac{-0.5}{12} & \frac{-0.2}{13} & \frac{-2.1}{17} & \frac{-2.5}{24} & \frac{-1.5}{29} & \frac{-1.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.1}{33} & \frac{-1.1}{22} & \frac{-1.6}{20} & \frac{-1.5}{17} & \frac{-0.9}{14} & \frac{-0.5}{12} & \frac{-2.5}{19} & \frac{-3.1}{24} & \frac{-2.1}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.1}{33} & \frac{-1.1}{21} & \frac{-2.4}{20} & \frac{-2.4}{17} & \frac{-0.5}{14} & \frac{-0.3}{13} & \frac{-1.2}{15} & \frac{-2.2}{24} & \frac{-1.1}{25} & \frac{-1.1}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.1}{33} & \frac{-1.1}{23} & \frac{-1.7}{22} & \frac{-1.6}{18} & \frac{0.0}{14} & \frac{-0.4}{12} & \frac{-2.0}{17} & \frac{-2.5}{23} & \frac{-1.0}{28} & \frac{-1.1}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.6}{33} & \frac{-1.5}{23} & \frac{-2.1}{22} & \frac{-2.1}{19} & \frac{-0.4}{15} & \frac{-0.4}{19} & \frac{-2.0}{18} & \frac{-2.1}{27} & \frac{-1.5}{30} & \frac{-1.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.2}{33} & \frac{-1.2}{22} & \frac{-1.5}{19} & \frac{-0.2}{14} & \frac{-0.1}{13} & \frac{-2.1}{17} & \frac{-2.3}{24} & \frac{-2.0}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.6}{33} & \frac{-1.5}{21} & \frac{-2.0}{19} & \frac{0.0}{14} & \frac{-0.5}{12} & \frac{-2.9}{16} & \frac{-2.4}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.5}{33} & \frac{-1.5}{22} & \frac{-2.1}{20} & \frac{-2.0}{17} & \frac{-0.2}{12} & \frac{-0.5}{12} & \frac{-2.5}{17} & \frac{-3.0}{27} & \frac{-2.5}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.1}{33} & \frac{-1.1}{21} & \frac{-2.2}{17} & \frac{-0.2}{13} & \frac{-0.4}{13} & \frac{-2.2}{17} & \frac{-3.1}{27} & \frac{-2.0}{36} \end{array}$$

$$\begin{array}{ccccccccc} \frac{-1.0}{33} & \frac{-1.1}{21} & \frac{-2.0}{20} & \frac{-2.0}{16} & \frac{0.0}{12} & \frac{-0.2}{12} & \frac{-1.5}{15} & \frac{-2.6}{27} & \frac{-2.0}{33} \end{array}$$

7/19/23 sheet# of sheets

Sta Elev
#05 104.1

+50 104.8

#04 105.0

+50 105.3

#03 105.6

+50 105.8

#02 105.8

Equation Sta 101 = 102

+50 106.0

100 106.0

+50 106.4

99 106.6

+50 107.2

Loose rock covered by about 1' of clay

Mendota rd. X-sections

0.0	+0.2	-1.3	-1.2	-0.5	+0.1	-0.8	-0.8	-0.2	0.0	-0.3	-0.3
33	20	17	16	14	13	10	17	19	21	25	33

-0.3	-0.6	-1.6	-1.5	-0.5	0.0	-1.5	-1.0	-0.9	-0.9
33	22	19	16	12	13	17	23	26	33

-0.9	-1.0	-1.5	-1.8	-0.7	0.0	-2.1	-2.0	-1.5	-1.5
33	27	26	16	13	12	19	30	31	33

-1.1	-1.5	-2.1	-1.8	-0.8	+0.1	-2.1	-2.5	-2.0	-2.5
33	25	23	15	13	11	17	26	28	33

Edge of berm 100' drop

-1.5	-1.5	-2.5	-2.4	-0.5	+0.1	-0.9	-1.8	-1.6	-1.5
23	32	27	20	13	12	14	19	28	33

-1.2	-2.4	-2.3	-0.8	+0.3	-1.5	-2.0	-1.5
33	28	21	14	12	17	28	33

-1.5	-1.5	-2.5	-2.5	-0.4	-0.2	-2.0	-2.0	-2.4
33	25	23	18	13	12	16	23	33

-1.3	-1.2	-1.9	-1.8	-0.3	-0.3	-1.7	-2.2	-5.5	-100
33	26	22	15	12	12	15	20	26	1

-0.7	-1.1	-1.0	-0.4	-0.5	-1.0	-1.5	-6.0
22	21	16	12	13	16	26	33

-1.1	-1.0	-1.3	-1.3	-0.5	0.0	-1.0	-2.1	-2.1	-2.5	-1.1
33	20	19	15	13	13	16	21	30	33	36

0.0	0.0	-1.1	-1.0	-0.4	-0.5	-1.6	-1.7	-1.5	-1.5
33	21	19	16	12	13	16	24	31	33

-1.1	-1.1	-1.5	-1.5	-0.5	-0.4	-2.0	-2.2	-1.1	-1.1
33	23	21	16	12	14	17	27	29	33

Bottom 100'

Sta

Elev

+70

98.4

X

X

112

98.5

111

99.2

110

99.9

109

100.1

X

X

+50

100.9

108

101.4

+50

101.6

107

101.9

+58

102.2

106

103.0

105 +50

104.0

Loose rock

Clay

Equation Sta 105 + 08.82 = 105 + 37.66

$$\begin{array}{ccccc} \text{L} & & \text{R} & & \\ \hline -2.0 & -2.1 & -0.2 & -0.2 & -4.2 \\ 22 & 19 & 16 & 13 & 18 \end{array}$$

$$\begin{array}{ccccccccc} +1.1 & +1.1 & -1.5 & -1.5 & 0.0 & -0.5 & -0.2 & -1.0 & -4.0 \\ 33 & 28 & 18 & 16 & 12 & 12 & 13 & 17 & 23 \end{array}$$

Bottom
about
-100.0

$$\begin{array}{ccccccccccc} +2.9 & +2.9 & -0.2 & -1.0 & -1.0 & +0.3 & -0.6 & -1.5 & -1.5 & +0.1 & -0.1 & -1.3 \\ 33 & 22 & 16 & 14 & 13 & 9 & 12 & 14 & 15 & 19 & 26 & 33 \end{array}$$

$$\begin{array}{ccccccccccccccc} +2.3 & +2.3 & +0.5 & -0.2 & +0.1 & +0.5 & -0.6 & -1.3 & -1.0 & -0.2 & +1.1 & +1.2 & 0.2-0.1 \\ 33 & 26 & 21 & 19 & 15 & 13 & 9 & 12 & 15 & 17 & 21 & 26 & 31 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} +0.9 & +1.2 & +0.2 & -0.1 & -0.1 & +0.3 & -0.3 & -0.8 & -0.8 & +0.6 & -1.0 \\ 33 & 23 & 21 & 17 & 13 & 12 & 10 & 12 & 15 & 19 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} +0.1 & -0.5 & -0.7 & -0.7 & -0.2 & -0.3 & -0.8 & -0.5 & +0.4 & +0.3 \\ 33 & 21 & 20 & 15 & 12 & 11 & 12 & 15 & 20 & 33 \end{array}$$

$$\begin{array}{ccccccccccccccc} +0.2 & -0.3 & -0.7 & -1.1 & -1.0 & -0.3 & -0.2 & -0.8 & -0.7 & +2.3 & +2.6 & +2.2 & +2.0 \\ 33 & 24 & 19 & 18 & 14 & 11 & 12 & 13 & 15 & 21 & 23 & 25 & 33 \end{array}$$

$$\begin{array}{ccccccccccc} +0.5 & +0.5 & +0.1 & -0.7 & -0.8 & -0.4 & +0.1 & -0.7 & -0.5 & +0.8 & +1.1 & +0.8 \\ 33 & 24 & 17 & 15 & 13 & 12 & 13 & 15 & 17 & 19 & 24 & 33 \end{array}$$

Sta.	Elev
122	108.5
+50	106.9
121	105.7
120	103.9
119	102.6
118	101.5
117	101.3
+50	100.8
116	100.3
115	99.3
114	98.7
+50	98.4
113	98.4

loose rock

clay

$$\begin{array}{cccccccccccc} +2.4 & +1.9 & +1.5 & -0.8 & -0.8 & -0.3 & -0.7 & -1.1 & -1.0 & -0.7 & -0.5 \\ 33 & 23 & 17 & 14 & 12 & 10 & 15 & 18 & 22 & 24 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +2.2 & +1.9 & -0.2 & -0.6 & -0.4 & -0.3 & -1.1 & -1.1 & -0.6 & +2.2 & +2.0 \\ 33 & 17 & 13 & 11 & 8 & 14 & 16 & 18 & 19 & 21 & 26 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.9 & +1.9 & +1.5 & -0.8 & -1.0 & -0.5 & -0.3 & -1.4 & -1.3 & +2.6 & +2.8 \\ 33 & 26 & 19 & 15 & 12 & 11 & 12 & 15 & 17 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} \phi \text{ of } x \text{ road} & -3.1 & -2.7 & -1.8 & -0.4 & -0.6 & -1.3 & -1.4 & +0.1 & +1.0 & +1.0 \\ 33 & 19 & 15 & 12 & 12 & 13 & 16 & 20 & 30 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -1.6 & -1.5 & -2.5 & -2.5 & -0.5 & -0.5 & -1.1 & -1.3 & 0.0 & 0.0 & +0.5 \\ 33 & 22 & 20 & 17 & 13 & 12 & 13 & 15 & 17 & 26 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -2.2 & -1.7 & -2.1 & -2.0 & -0.5 & -0.2 & -1.4 & -1.4 & 0.0 & 0.0 & +0.5 \\ 33 & 19 & 18 & 16 & 12 & 11 & 13 & 16 & 17 & 27 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -0.6 & +0.6 & -0.8 & -1.0 & -0.5 & -0.2 & -1.1 & -0.9 & +3.2 & +3.2 \\ 33 & 20 & 17 & 14 & 12 & 11 & 13 & 15 & 20 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +1.5 & +2.5 & -0.9 & -1.0 & -0.3 & -0.1 & -1.1 & -1.0 & +3.8 & +4.5 & +1.0 \\ 33 & 21 & 14 & 12 & 11 & 11 & 13 & 15 & 23 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} +3.0 & +3.2 & -0.7 & -0.6 & 0.0 & -0.3 & -0.6 & -0.7 & +0.6 & +3.1 & +2.5 & +3.0 \\ 33 & 24 & 15 & 13 & 12 & 12 & 14 & 15 & 18 & 23 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -1.0 & -1.0 & -2.1 & -2.0 & -0.9 & 0.0 & -0.8 & -1.0 & -0.5 & -0.7 & -1.0 \\ 33 & 19 & 18 & 15 & 11 & 11 & 13 & 16 & 17 & 29 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -1.0 & -1.5 & -1.6 & -2.0 & -1.6 & -0.8 & -0.3 & -1.2 & -1.1 & -0.4 & +0.9 & +1.5 \\ 33 & 23 & 18 & 16 & 12 & 11 & 11 & 13 & 16 & 19 & 25 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} -1.0 & -0.5 & +0.4 & -1.1 & -1.0 & -0.4 & 0.0 & -0.7 & -0.8 & -0.6 & -0.4 & +3.7 \\ 33 & 29 & 19 & 16 & 14 & 11 & 11 & 14 & 16 & 18 & 23 & 31 & 33 \end{array}$$

$$\begin{array}{cccccccccccc} \text{Drops} & -3.0 & -1.0 & -0.5 & -0.5 & -0.1 & -1.0 & -1.5 & -1.6 & -1.1 & +0.5 \\ \text{Down} & 33 & 22 & 12 & 10 & 9 & 13 & 17 & 29 & 31 & 33 \end{array}$$

Sibley Memorial

Sta

Elev

+50

112.8

X

X

121

112.5

+50

111.9

clay

Rock

123

111.0

+50

109.9

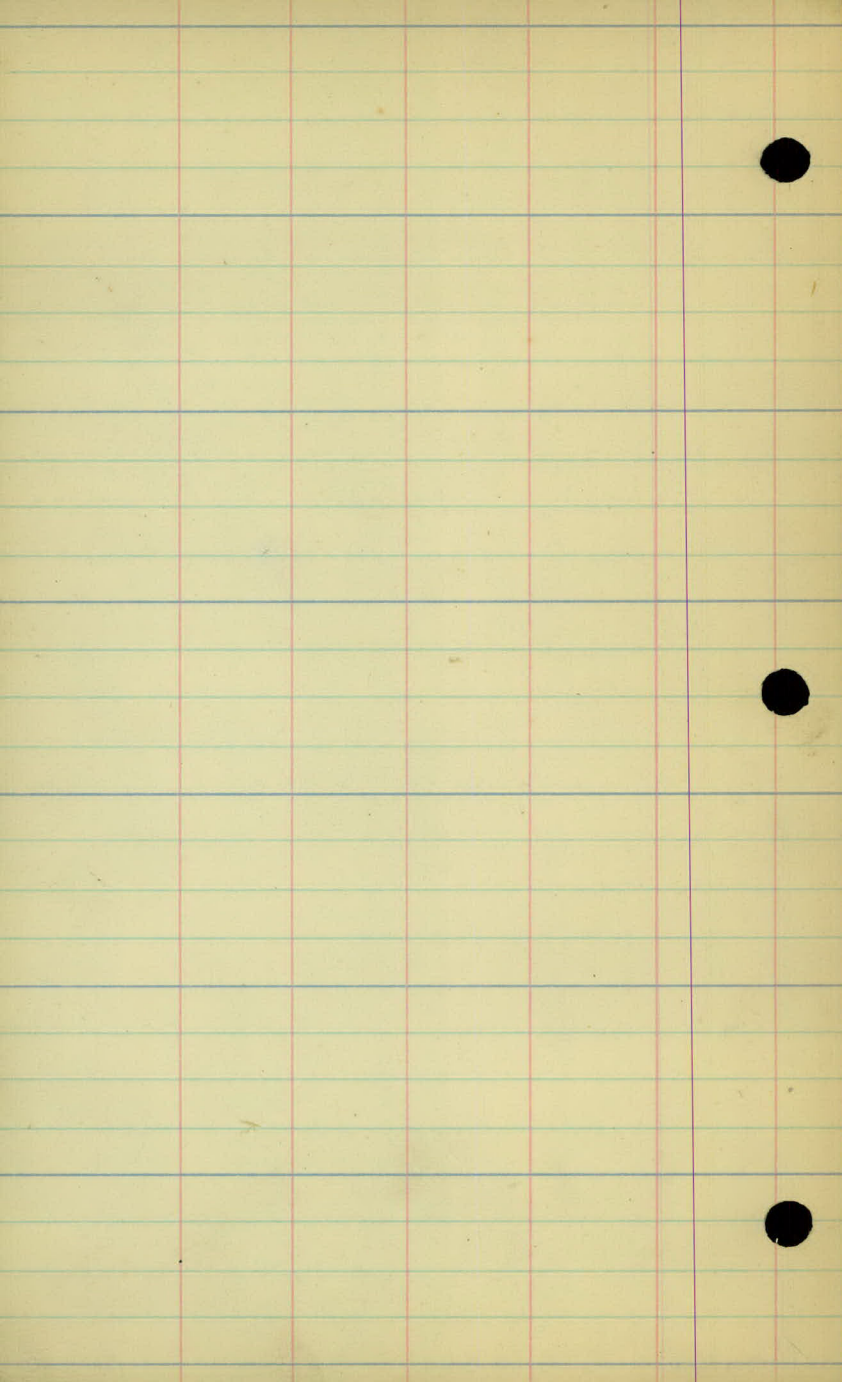
$$\begin{array}{ccccccccc} +0.2 & 0.0 & -0.5 & -0.5 & +0.2 & -0.7 & -1.5 & -1.5 & -2.9 & -3.0 \\ \hline 33 & 18 & 16 & 13 & 12 & 12 & 14 & 19 & 23 & 33 \end{array}$$

$$\begin{array}{ccccccccc} 0.0 & -0.1 & -0.9 & -0.9 & +0.1 & -0.5 & -1.8 & -2.0 & -1.8 & -2.7 \\ \hline 33 & 16 & 16 & 14 & 13 & 13 & 16 & 21 & 23 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +1.7 & 0.0 & +0.2 & -0.2 & -0.3 & -0.8 & -1.4 & -2.0 & -1.5 & -2.9 & -3.0 \\ \hline 33 & 30 & 17 & 16 & 12 & 12 & 14 & 20 & 21 & 26 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +2.5 & +2.3 & +2.0 & -0.3 & -0.5 & -0.3 & -0.5 & -1.4 & -2.0 & -1.5 & -2.9 \\ \hline 33 & 22 & 19 & 16 & 13 & 11 & 12 & 14 & 20 & 21 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +1.9 & +1.9 & +1.3 & -0.1 & -0.5 & -0.3 & -0.7 & -1.5 & -1.5 & -1.2 & -1.5 \\ \hline 33 & 24 & 20 & 16 & 14 & 12 & 12 & 15 & 21 & 23 & 33 \end{array}$$



+ 50

113.5

130

Drive ^{113.5} left.

+ 50

113.6

129

113.6

128

114.1

127

115.0

Rock

+ 50

115.0

126

115.2

+ 50

113.9

Clay

125

114.5

+ 50

112.8

124 + 00

112.5

$$\frac{+2.0}{31} \quad \frac{+0.9}{27} \quad \frac{-1.7}{22} \quad \frac{-2.1}{20} \quad \frac{-1.9}{13} \quad \frac{-0.4}{10}$$

$$\frac{-0.7}{14} \quad \frac{-5.2}{23} \quad \frac{-5.2}{28} \quad \frac{-4.1}{30} \quad \frac{-4.3}{33}$$

$$\frac{+3.5}{37} \quad \frac{0.0}{29} \quad \frac{-0.3}{25}$$

$$\frac{-0.5}{14} \quad \frac{-3.7}{22} \quad \frac{-4.6}{26} \quad \frac{-5.0}{33} \quad \frac{-4.0}{34}$$

$$\frac{+2.9}{39} \quad \frac{-1.7}{30} \quad \frac{-1.5}{19} \quad \frac{-0.5}{16}$$

$$\frac{-0.6}{10} \quad \frac{-1.0}{12} \quad \frac{-3.3}{17} \quad \frac{-5.0}{24} \quad \frac{-5.5}{29} \quad \frac{-3.3}{31-33}$$

$$\frac{+2.5}{33} \quad \frac{-0.1}{32} \quad \frac{-1.4}{30} \quad \frac{-1.7}{19} \quad \frac{-0.5}{14}$$

$$\frac{-0.6}{13} \quad \frac{-3.0}{19} \quad \frac{-3.9}{35} \quad \frac{-2.9}{35}$$

$$\frac{+2.4}{33} \quad \frac{-1.0}{27} \quad \frac{-0.8}{17} \quad \frac{-0.2}{16}$$

$$\frac{-0.6}{12} \quad \frac{-2.5}{17} \quad \frac{-2.9}{33}$$

$$\frac{+1.6}{33} \quad \frac{+1.7}{31} \quad \frac{-1.0}{27} \quad \frac{-1.3}{16} \quad \frac{-0.2}{13}$$

$$\frac{-0.5}{11} \quad \frac{-1.6}{14} \quad \frac{-2.1}{23} \quad \frac{-1.0}{26} \quad \frac{-2.5}{33}$$

$$\frac{+1.2}{33} \quad \frac{+1.5}{31} \quad \frac{-0.1}{28} \quad \frac{-0.5}{15} \quad \frac{+0.2}{13}$$

$$\frac{-0.5}{12} \quad \frac{-1.6}{15} \quad \frac{-1.8}{23} \quad \frac{-0.9}{25} \quad \frac{-2.0}{33}$$

$$\frac{+0.1}{33} \quad \frac{-0.3}{28} \quad \frac{-1.1}{19} \quad \frac{0.0}{13}$$

$$\frac{-1.0}{14} \quad \frac{-2.3}{20} \quad \frac{-2.2}{23} \quad \frac{-4.2}{33}$$

$$\frac{-0.2}{33} \quad \frac{-0.2}{31} \quad \frac{-1.0}{28} \quad \frac{-1.2}{25} \quad \frac{-0.9}{17} \quad \frac{0.0}{14}$$

$$\frac{-0.8}{12} \quad \frac{-1.7}{13} \quad \frac{-2.4}{23} \quad \frac{-3.8}{31} \quad \frac{-3.8}{23}$$

$$\frac{-0.6}{33} \quad \frac{-0.5}{26} \quad \frac{-0.4}{21} \quad \frac{-1.2}{20} \quad \frac{-1.2}{18} \quad \frac{+0.1}{14}$$

$$\frac{-0.4}{8} \quad \frac{-1.5}{13} \quad \frac{-2.9}{25} \quad \frac{-3.3}{33}$$

$$\frac{0.0}{33} \quad \frac{-0.2}{18} \quad \frac{-0.5}{17} \quad \frac{-0.5}{15} \quad \frac{0.0}{13}$$

$$\frac{-1.0}{12} \quad \frac{-1.6}{14} \quad \frac{-1.8}{20} \quad \frac{-2.7}{25} \quad \frac{-2.1}{33}$$

$$\frac{0.0}{33} \quad \frac{-0.3}{17} \quad \frac{-0.7}{16} \quad \frac{+0.1}{14}$$

$$\frac{-0.5}{12} \quad \frac{-2.0}{16} \quad \frac{-2.0}{22} \quad \frac{-1.8}{23} \quad \frac{-2.8}{27} \quad \frac{-2.9}{33}$$

Sibley

Mem

4-29-23

Sta

Elev.

137

112.3

+50

112.3

136

112.6
Driveway Left

+50

112.4

135

112.3

134

112.2

+50

112.6

133

112.9

+50

113.0

132

113.4

+50

113.5

131

113.5

Abt. 140.2' of Black Loam - Loose rock below

$$\frac{+5.0}{33} \quad \frac{-0.3}{24} \quad \frac{-1.7}{20} \quad \frac{-1.7}{16} \quad \frac{-0.3}{12} \quad \frac{-0.7}{11} \quad \frac{-3.1}{15} \quad \frac{-3.2}{19} \quad \frac{-3.7}{23} \quad \frac{-4.2}{33}$$

$$\frac{+4.4}{33} \quad \frac{+4.7}{27} \quad \frac{+3.8}{25} \quad \frac{-1.2}{15} \quad \frac{-1.3}{12} \quad \frac{-0.4}{9} \quad \frac{-0.8}{11} \quad \frac{-2.9}{15} \quad \frac{-3.1}{21} \quad \frac{-3.5}{24} \quad \frac{-4.1}{33}$$

$$\frac{+1.2}{33} \quad \frac{+0.5}{20} \quad \frac{+0.3}{13} \quad \frac{-0.7}{12} \quad \frac{-2.7}{16} \quad \frac{-2.9}{18} \quad \frac{-3.1}{21} \quad \frac{-3.8}{26} \quad \frac{4.1}{33}$$

$$\frac{+3.8}{33} \quad \frac{+1.2}{26} \quad \frac{-1.1}{20} \quad \frac{-1.1}{15} \quad \frac{-0.3}{13} \quad \frac{-0.3}{12} \quad \frac{-3.1}{17} \quad \frac{-3.3}{24} \quad \frac{-3.8}{28} \quad \frac{-3.8}{33}$$

$$\frac{+3.5}{33} \quad \frac{-0.3}{25} \quad \frac{-1.7}{20} \quad \frac{-1.8}{18} \quad \frac{-1.5}{15} \quad \frac{-0.4}{13} \quad \frac{-0.9}{13} \quad \frac{-3.3}{17} \quad \frac{-3.3}{22} \quad \frac{-3.1}{26} \quad \frac{-3.8}{30} \quad \frac{-3.8}{33}$$

$$\frac{+4.5}{33} \quad \frac{+2.2}{24} \quad \frac{-1.2}{18} \quad \frac{-1.4}{16} \quad \frac{-0.4}{12} \quad \frac{-0.4}{14} \quad \frac{-2.7}{18} \quad \frac{-2.8}{22} \quad \frac{-3.1}{28} \quad \frac{-4.0}{31} \quad \frac{-4.0}{33}$$

$$\frac{+2.2}{33} \quad \frac{+1.2}{28} \quad \frac{0.0}{22} \quad \frac{-1.5}{18} \quad \frac{-1.4}{15} \quad \frac{-0.6}{12} \quad \frac{-0.6}{12} \quad \frac{-2.6}{18} \quad \frac{-3.3}{21} \quad \frac{-3.1}{27} \quad \frac{-4.0}{33}$$

$$\frac{+0.5}{35} \quad \frac{-1.1}{32} \quad \frac{-2.5}{16} \quad \frac{-1.0}{12} \quad \frac{-0.4}{12} \quad \frac{-3.3}{18} \quad \frac{-3.7}{25} \quad \frac{-4.5}{28} \quad \frac{-4.8}{33}$$

$$\frac{-0.5}{35} \quad \frac{-2.2}{31} \quad \frac{-3.1}{18} \quad \frac{-0.9}{12} \quad \frac{-0.3}{12} \quad \frac{-3.4}{19} \quad \frac{-4.1}{28} \quad \frac{-4.5}{29} \quad \frac{-4.8}{33}$$

$$\frac{+2.5}{36} \quad \frac{+0.4}{32} \quad \frac{-0.7}{25} \quad \frac{-2.4}{22} \quad \frac{-2.6}{16} \quad \frac{-0.8}{11} \quad \frac{-0.3}{12} \quad \frac{-4.0}{19} \quad \frac{-4.2}{28} \quad \frac{-5.0}{30} \quad \frac{-5.0}{33}$$

$$\frac{+2.5}{33} \quad \frac{-0.6}{25} \quad \frac{-2.1}{22} \quad \frac{-2.7}{19} \quad \frac{-2.6}{15} \quad \frac{-0.8}{10} \quad \frac{-0.2}{14} \quad \frac{-4.3}{20} \quad \frac{-4.2}{29} \quad \frac{-4.5}{32} \quad \frac{4.5}{33}$$

$$\frac{+2.5}{33} \quad \frac{+2.0}{31} \quad \frac{-0.2}{27} \quad \frac{-0.5}{25} \quad \frac{-2.8}{19} \quad \frac{-2.6}{15} \quad \frac{-0.7}{10} \quad \frac{-0.4}{14} \quad \frac{-4.4}{21} \quad \frac{-4.8}{28} \quad \frac{-4.3}{31} \quad \frac{-4.6}{33}$$

Sibley Memorial

Sta

Elev.

1A7

113.2

+50

113.1

+40

Priv. Drive Right No. Culv.
113.1
196 Priv. Drive Left. New 12" Cor. 2. 30'

1A5

112.6

112.8

+60

Drive Right. No Culv.

1A4

113.2

1A3

114.3

1A2

113.6

1A1

113.1

+50

113.0

1A0

112.9

139

112.8

138

112.2

137+50

112.1

Abt 3'-0" Black loam over rock

$$\frac{+1.5}{40} \quad \frac{-2.3}{33} \quad \frac{-3.6}{20} \quad \frac{-0.7}{13} \quad \frac{-0.8}{12} \quad \frac{-4.1}{14} \quad \frac{-4.4}{25} \quad \frac{-4.6}{33}$$

$$\frac{+0.3}{33} \quad \frac{-2.3}{30} \quad \frac{-2.8}{17} \quad \frac{-0.6}{11} \quad \frac{-1.0}{12} \quad \frac{-3.2}{18} \quad \frac{-4.0}{25} \quad \frac{-4.2}{33}$$

$$\frac{-0.5}{33} \quad \frac{-2.3}{27} \quad \frac{-3.0}{16} \quad \frac{-0.5}{12} \quad \frac{-1.0}{12} \quad \frac{-2.7}{17} \quad \frac{-3.1}{25} \quad \frac{-3.5}{33}$$

$$\frac{+0.12}{38} \quad \frac{-2.4}{28} \quad \frac{-2.7}{16} \quad \frac{-0.5}{11} \quad \frac{-0.6}{12} \quad \frac{-3.2}{17} \quad \frac{-3.4}{33}$$

$$\frac{0.0}{33} \quad \frac{-2.2}{31} \quad \frac{-2.8}{19} \quad \frac{-1.5}{14} \quad \frac{-0.3}{11} \quad \frac{-0.7}{12} \quad \frac{-1.5}{14} \quad \frac{-2.5}{23} \quad \frac{-2.7}{33}$$

$$\frac{+1.5}{36} \quad \frac{-1.5}{33} \quad \frac{-2.2}{19} \quad \frac{-1.2}{16} \quad \frac{-0.2}{11} \quad \frac{-1.0}{13} \quad \frac{-3.2}{18} \quad \frac{-3.7}{24} \quad \frac{-3.5}{31} \quad \frac{-2.6}{33}$$

$$\frac{+0.5}{36} \quad \frac{-2.6}{33} \quad \frac{-3.0}{19} \quad \frac{+0.1}{11} \quad \frac{-0.8}{11} \quad \frac{-2.8}{16} \quad \frac{-3.0}{28} \quad \frac{-2.5}{29-33}$$

$$\frac{+0.5}{35} \quad \frac{-1.5}{33} \quad \frac{-2.2}{17} \quad \frac{-0.3}{12} \quad \frac{-0.9}{9} \quad \frac{-3.5}{15} \quad \frac{-4.1}{21} \quad \frac{-5.0}{33}$$

$$\frac{+1.6}{33} \quad \frac{-0.4}{27} \quad \frac{-1.8}{17} \quad \frac{-0.2}{12} \quad \frac{-1.0}{11} \quad \frac{-3.5}{14} \quad \frac{-4.2}{21} \quad \frac{-5.3}{33}$$

$$\frac{+1.9}{33} \quad \frac{+1.0}{29} \quad \frac{-1.4}{26} \quad \frac{-2.1}{16} \quad \frac{-0.4}{11} \quad \frac{-0.8}{12} \quad \frac{-3.5}{16} \quad \frac{-4.1}{23} \quad \frac{-4.9}{33}$$

$$\frac{+2.0}{33} \quad \frac{+1.8}{31} \quad \frac{-1.3}{28} \quad \frac{-2.7}{19} \quad \frac{-0.8}{11} \quad \frac{-0.8}{12} \quad \frac{-2.5}{14} \quad \frac{-4.5}{20} \quad \frac{-4.4}{29} \quad \frac{-3.2}{31-33}$$

$$\frac{+2.5}{35} \quad \frac{+1.0}{33} \quad \frac{-1.6}{21} \quad \frac{-1.5}{16} \quad \frac{-0.2}{13} \quad \frac{-0.5}{11} \quad \frac{-3.0}{17} \quad \frac{-3.3}{23} \quad \frac{-3.7}{33}$$

$$\frac{+4.1}{33} \quad \frac{+0.9}{28} \quad \frac{-1.1}{22} \quad \frac{-1.7}{17} \quad \frac{-0.2}{13} \quad \frac{-0.6}{10} \quad \frac{-3.1}{15} \quad \frac{-3.1}{17} \quad \frac{-3.2}{21} \quad \frac{-3.8}{33}$$

Sibley Memorial

570,	Elev.
158	119.4
+50	119.9
157	121.1
+50	112.3
156	123.4
+50	123.07
155	122.5
154	120.3
153	118.9
152	118.1
151	116.4
150	116.6
149	114.4
+75	24" Cor. I. 30' lg. Drains R.
148	113.6

Black Loam

$$\begin{array}{ccccccccc} +5.7 & +4.2 & -1.8 & -2.0 & -0.6 & -0.6 & -3.7 & -3.8 & -5.0 \\ \hline 33 & 30 & 23 & 16 & 13 & 12 & 17 & 25 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +2.9 & -1.8 & -2.0 & -0.6 & -0.1 & -3.2 & -2.4 & & \\ \hline 33 & 24 & 17 & 12 & 12 & 17 & 33 & & \end{array}$$

$$\begin{array}{ccccccccc} +1.7 & -0.4 & -2.0 & -0.6 & -0.4 & -3.5 & -3.0 & -3.0 & -3.5 \\ \hline 33 & 32 & 17 & 13 & 14 & 16-20 & 21 & 24 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +1.7 & +0.7 & -1.7 & -2.0 & -1.0 & -0.6 & -3.7 & -3.9 & -3.9 \\ \hline 33-30 & 26 & 21 & 15 & 16 & 16 & 22 & 24 & 26 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +0.9 & +0.7 & -0.3 & -0.8 & -0.3 & -0.5 & -6.0 & -6.3 & \\ \hline 33 & 29 & 26 & 18 & 12 & 15 & 25 & 33 & \\ +20.0 & +10.0 & +5.0 & 0 & -0.6 & -8.0 & -7.0 & & \\ \hline 200 & 25 & 33 & 10 & 18 & 27 & 33 & & \\ -2.0 & -2.4 & +0.1 & -0.7 & -7.4 & -7.5 & & & \\ \hline 33 & 21 & 15 & 15 & 27 & 33 & & & \end{array}$$

$$\begin{array}{ccccccccc} -1.1 & -3.2 & -3.1 & -1.6 & -0.8 & -1.5 & -6.2 & -6.4 & \\ \hline -0.7 & 31 & 26 & 18 & 14 & 15 & 26 & 33 & \\ 33 & & & & & & & & \end{array}$$

$$\begin{array}{ccccccccc} +1.9 & -0.4 & -2.6 & -2.9 & -1.5 & -0.5 & -1.2 & -4.8 & -5.3 & -6.8 \\ \hline 33 & 24 & 20 & 16 & 12 & 9 & 15 & 22 & 28 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +1.8 & +1.9 & 0 & -0.4 & -0.4 & -0.4 & -1.0 & -4.0 & -4.4 & -2.5 & -3.0 \\ \hline 33 & 23 & 20 & 18 & 14 & 13 & 15 & 21 & 24 & 29 & 33 \end{array}$$

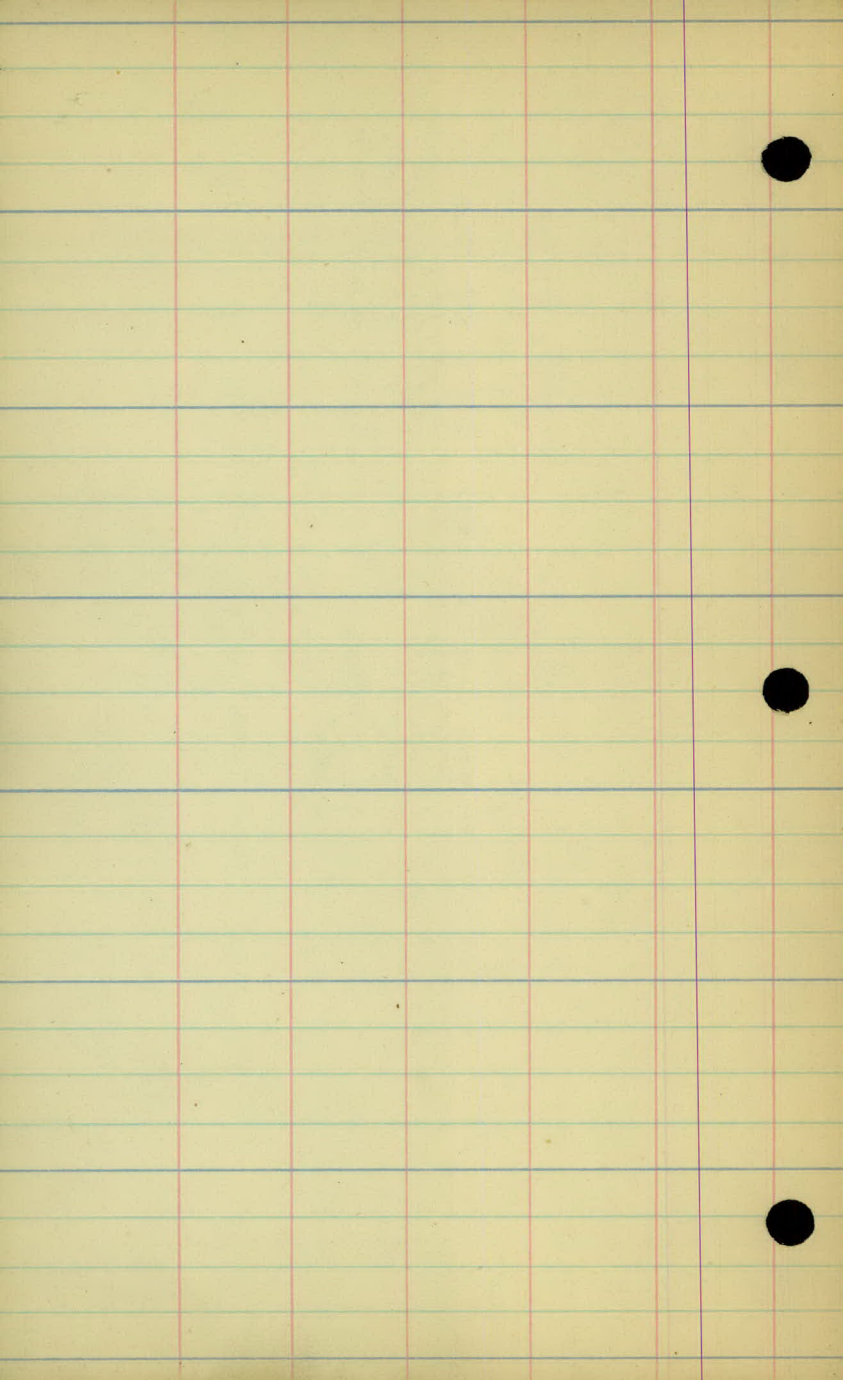
$$\begin{array}{ccccccccc} +3.5 & +3.2 & +1.9 & -1.8 & -1.6 & -0.5 & -0.5 & -3.0 & -3.9 & -2.8 & -3.4 & -4.2 \\ \hline 33 & 29 & 24 & 18 & 15 & 12 & 13 & 18 & 21 & 23 & 27 & 33 \end{array}$$

$$\begin{array}{ccccccccc} +2.2 & +1.8 & +0.6 & -2.2 & -2.1 & -0.3 & -0.5 & -3.0 & -3.9 & -4.2 & & \\ \hline 33 & 29 & 24 & 21 & 15 & 10 & 11 & 18 & 24 & 23 & & \end{array}$$

$$\begin{array}{ccccccccc} -0.3 & -1.8 & -2.7 & -0.7 & -0.3 & -1.0 & -2.1 & -3.1 & -3.4 & & \\ \hline 33 & 23 & 20 & 16 & 14 & 16 & 14 & 17 & 33 & & \end{array}$$

1 - 18' 12' 1

$$\begin{array}{ccccccccc} +1.3 & -1.3 & -2.7 & -1.0 & -0.5 & -0.8 & -3.8 & -4.4 & & & \\ \hline 40 & 33 & 22 & 17 & 15 & 7 & 16 & 33 & & & \end{array}$$



Sibley

Memoria

4-26-23

Sta.

Elev.

169

121.7

168

120.3

+50

120.0

167

119.6

166+50

119.0

166

119.0

+60

12" Cor. I. Cul. under Dr. R. Good Cond. 36

165

118.9

164

119.3

163

119.3

162

119.3

161

118.9

160

118.5

159

119.2

+76

12" Cor. I. Cul. under Rd.

Drains R

clay

limestone

Black loam over

$$\frac{+6.0}{33} \quad \frac{+5.0}{29} \quad \frac{-1.5}{21} \quad \frac{-1.7}{15} \quad \frac{-0.3}{11} \quad \frac{-0.4}{13} \quad \frac{-3.0}{18} \quad \frac{-3.5}{20} \quad \frac{-4.5}{23} \quad \frac{-4.5}{33}$$

$$\frac{+5.0}{33} \quad \frac{+3.5}{26} \quad \frac{-1.2}{20} \quad \frac{-1.5}{15} \quad \frac{-0.3}{13} \quad \frac{-0.9}{13} \quad \frac{-3.3}{16} \quad \frac{-3.1}{18-19} \quad \frac{-4.7}{33}$$

$$\frac{+4.9}{33} \quad \frac{+3.3}{27} \quad \frac{-1.8}{20} \quad \frac{-2.0}{16} \quad \frac{-0.8}{13} \quad \frac{-0.8}{13} \quad \frac{-3.3}{16} \quad \frac{-3.3}{17} \quad \frac{-2.7}{18} \quad \frac{-4.7}{33}$$

$$\frac{+4.8}{33} \quad \frac{+2.9}{25} \quad \frac{-1.7}{19} \quad \frac{-1.8}{15} \quad \frac{-0.5}{12} \quad \frac{-0.7}{13} \quad \frac{-3.5}{18} \quad \frac{-3.8}{21} \quad \frac{-4.1}{23} \quad \frac{-4.7}{33}$$

$$\frac{+2.9}{33} \quad \frac{+1.7}{26} \quad \frac{-2.2}{21} \quad \frac{-2.2}{16} \quad \frac{-0.7}{13} \quad \frac{-0.8}{14} \quad \frac{-4.2}{18} \quad \frac{-4.5}{22} \quad \frac{-4.0}{24} \quad \frac{-5.0}{33}$$

$$\frac{+1.9}{33} \quad \frac{+1.2}{24} \quad \frac{-2.2}{22} \quad \frac{-2.3}{16} \quad \frac{-0.8}{13} \quad \frac{-0.6}{14} \quad \frac{-3.8}{17} \quad \frac{-4.3}{24} \quad \frac{-4.5}{33}$$

$$\frac{+2.0}{33} \quad \frac{+1.0}{29} \quad \frac{-2.3}{24} \quad \frac{-2.9}{17} \quad \frac{-1.0}{13} \quad \frac{-0.9}{14} \quad \frac{-3.3}{19} \quad \frac{-4.0}{21} \quad \frac{-4.0}{26} \quad \frac{-4.0}{33}$$

$$\frac{+1.3}{33} \quad \frac{+0.6}{29} \quad \frac{-0.8}{28} \quad \frac{-2.5}{23} \quad \frac{-2.8}{18} \quad \frac{-0.6}{12} \quad \frac{-1.1}{14} \quad \frac{-3.1}{18} \quad \frac{-3.3}{20} \quad \frac{-2.7}{22} \quad \frac{-3.3}{33}$$

$$\frac{+2.9}{33} \quad \frac{+2.6}{26} \quad \frac{-0.5}{23} \quad \frac{-2.0}{20} \quad \frac{-2.0}{17} \quad \frac{-0.6}{14} \quad \frac{-1.0}{14} \quad \frac{-2.2}{18} \quad \frac{-2.9}{20} \quad \frac{-2.5}{33}$$

$$\frac{+2.2}{33} \quad \frac{+1.2}{26} \quad \frac{-2.5}{22} \quad \frac{-2.8}{17} \quad \frac{-0.9}{13} \quad \frac{-1.1}{13} \quad \frac{-4.5}{17} \quad \frac{-3.9}{20} \quad \frac{-5.0}{25} \quad \frac{-4.8}{33}$$

$$\frac{+4.3}{33} \quad \frac{+3.2}{27} \quad \frac{-1.7}{21} \quad \frac{-2.1}{16} \quad \frac{-0.5}{12} \quad \frac{-1.1}{15} \quad \frac{-4.2}{20} \quad \frac{-4.0}{20} \quad \frac{-4.5}{33}$$

$$\frac{+3.0}{33} \quad \frac{+2.0}{27} \quad \frac{-2.0}{23} \quad \frac{-2.3}{16} \quad \frac{-0.5}{11} \quad \frac{-1.0}{14} \quad \frac{-3.6}{20} \quad \frac{-4.2}{33}$$

$$\frac{+4.8}{33} \quad \frac{+3.2}{28} \quad \frac{-1.5}{24} \quad \frac{-2.4}{17} \quad \frac{-0.5}{12} \quad \frac{-1.0}{12} \quad \frac{-3.0}{16} \quad \frac{-3.6}{21} \quad \frac{-4.4}{33}$$

Sta

Elev

173

129.4

X

X

+66

128.8

172

128.1

+50

+0.2

126.7

clay

171

125.2

170

123.1

L

E

R

(54)

$$\begin{array}{r} +4.0 \\ 38 \end{array} \quad \begin{array}{r} +0.6 \\ 30 \end{array} \quad \begin{array}{r} 0.0 \\ 25 \end{array} \quad \begin{array}{r} -0.1 \\ 12 \end{array} \quad \begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -1.5 \\ 15 \end{array} \quad \begin{array}{r} -3.5 \\ 33 \end{array}$$

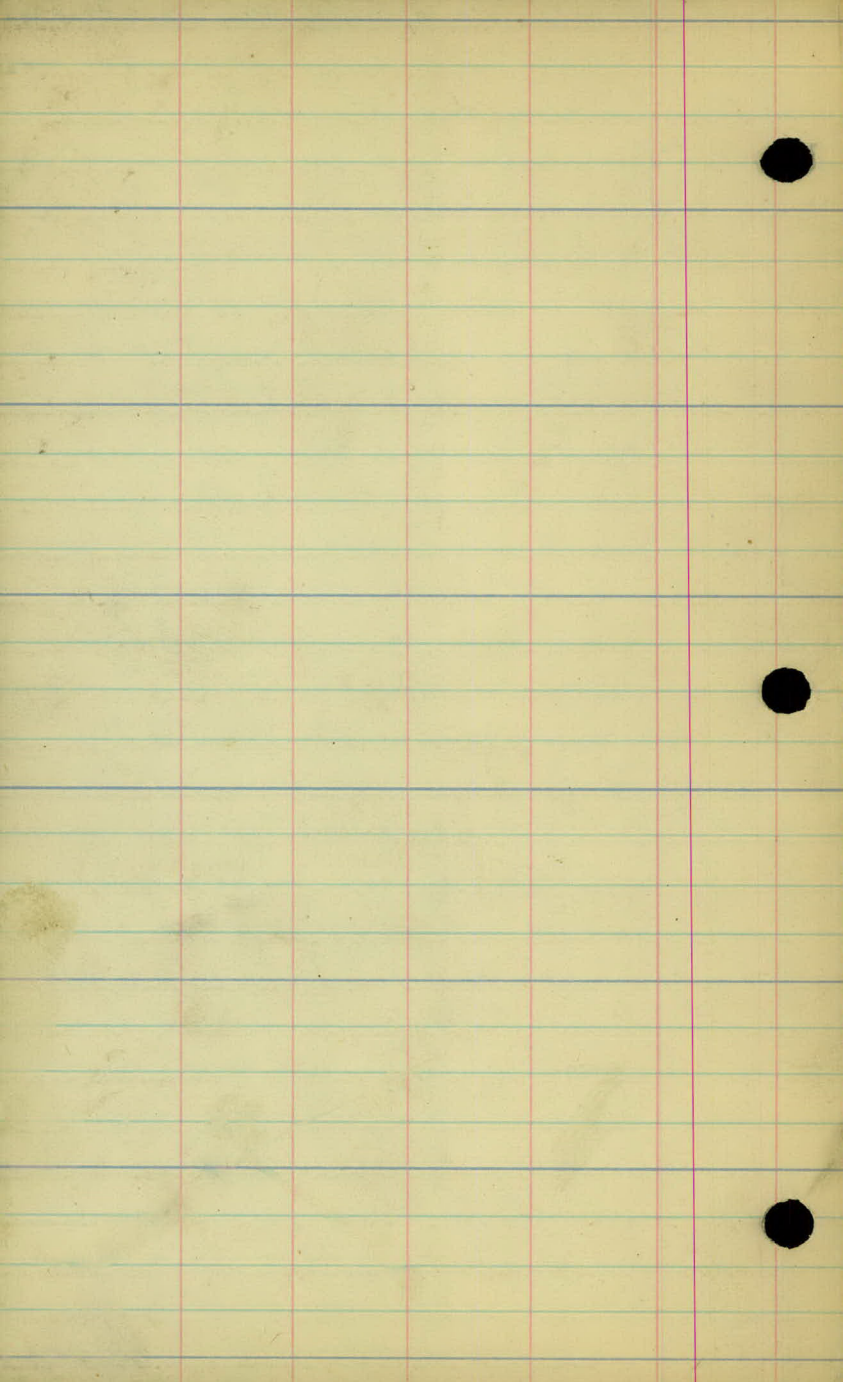
$$\begin{array}{r} +3.2 \\ 33 \end{array} \quad \begin{array}{r} +3.0 \\ 28 \end{array} \quad \begin{array}{r} 0.0 \\ 24 \end{array} \quad \begin{array}{r} -0.1 \\ 11 \end{array} \quad \begin{array}{r} -1.0 \\ 14 \end{array} \quad \begin{array}{r} -2.0 \\ 18 \end{array} \quad \begin{array}{r} -1.4 \\ 21 \end{array} \quad \begin{array}{r} -3.0 \\ 33 \end{array}$$

$$\begin{array}{r} +3.0 \\ 36 \end{array} \quad \begin{array}{r} -0.9 \\ 26 \end{array} \quad \begin{array}{r} -1.2 \\ 16 \end{array} \quad \begin{array}{r} -0.5 \\ 14 \end{array} \quad \begin{array}{r} -0.9 \\ 14 \end{array} \quad \begin{array}{r} -2.5 \\ 18 \end{array} \quad \begin{array}{r} -3.0 \\ 24 \end{array} \quad \begin{array}{r} -2.0 \\ 26 \end{array} \quad \begin{array}{r} -2.4 \\ 33 \end{array}$$

$$\begin{array}{r} +2.5 \\ 35 \end{array} \quad \begin{array}{r} -2.0 \\ 28 \end{array} \quad \begin{array}{r} -2.1 \\ 19 \end{array} \quad \begin{array}{r} -0.1 \\ 12 \end{array} \quad \begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -2.2 \\ 17 \end{array} \quad \begin{array}{r} -3.4 \\ 20 \end{array} \quad \begin{array}{r} -3.4 \\ 25 \end{array} \quad \begin{array}{r} -4.0 \\ 34 \end{array}$$

$$\begin{array}{r} +2.8 \\ 36 \end{array} \quad \begin{array}{r} -2.0 \\ 29 \end{array} \quad \begin{array}{r} -2.0 \\ 19 \end{array} \quad \begin{array}{r} -0.2 \\ 13 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -3.0 \\ 17 \end{array} \quad \begin{array}{r} -4.0 \\ 24 \end{array} \quad \begin{array}{r} -4.5 \\ 33 \end{array}$$

$$\begin{array}{r} +5.0 \\ 33 \end{array} \quad \begin{array}{r} +4.5 \\ 31 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -1.8 \\ 11 \end{array} \quad \begin{array}{r} -0.5 \\ 13 \end{array} \quad \begin{array}{r} -0.5 \\ 12 \end{array} \quad \begin{array}{r} -1.7 \\ 19 \end{array} \quad \begin{array}{r} -5.2 \\ 33 \end{array}$$



Check Levels

Sibley Memorial

Carley A Persons /

April 25, 1923

4/17/23

Check Levels 37 to

	+	H.I.	-	Elev.	B.M.
B.M.	1.47	255.59			254.12
T.P.	1.88	245.47	12.00	243.59	
B.M.	6.09	242.88	8.68	236.79	236.75
T.P.	0.46	232.45	10.89	231.99	
T.P.	0.17	220.93	11.69	220.96	
T.P.	0.88	210.89	10.92	210.01	
T.P.	0.33	199.02	12.20	198.69	
			2.11	196.91	196.88
T.P.	0.75	188.26	11.51	187.51	
T.P.	0.65	177.65	11.26	177.00	
B.M.	0.02	167.70	9.97	167.68	167.64
T.P.	1.63	157.56	11.77	155.93	
T.P.	1.24	146.95	11.85	145.71	
T.P.	0.30	135.71	11.54	135.41	
T.P.	0.02	124.37	11.36	124.35	
B.M.	2.37	117.37	9.92	114.95	115.00
B.M.			3.78	113.59	113.57
B.M.	3.49	112.95	7.92	109.45	109.46
B.M.	1.08	106.79	7.22	105.73	105.71
B.M.	9.18	108.16	8.80	98.99	98.98

S.W. Cor. of S. abut on bridge.

Tree L 80+96

" R 87+60

" R 103+

S.W. Cor of S. abut on bridge

Sta	+	H.I.	-	Elev	B.M.
	9.18	108.16			
T.P.	12.10	119.91	0.35	107.81	
B.M.	7.07	119.39	6.57	112.34	112.32
T.P.	4.41	116.90	6.90	112.49	
B.M.	6.43	117.83	6.50	111.40	111.40
B.M.	8.87	124.56	2.14	115.69	115.69
T.P.	5.45	125.45	4.56	120.00	
T.P.	5.23	123.40	7.28	118.17	
B.M.			5.54	117.86	117.86
T.P.	8.76	131.34	.82	122.58	
B.M.			4.84	126.50	126.55

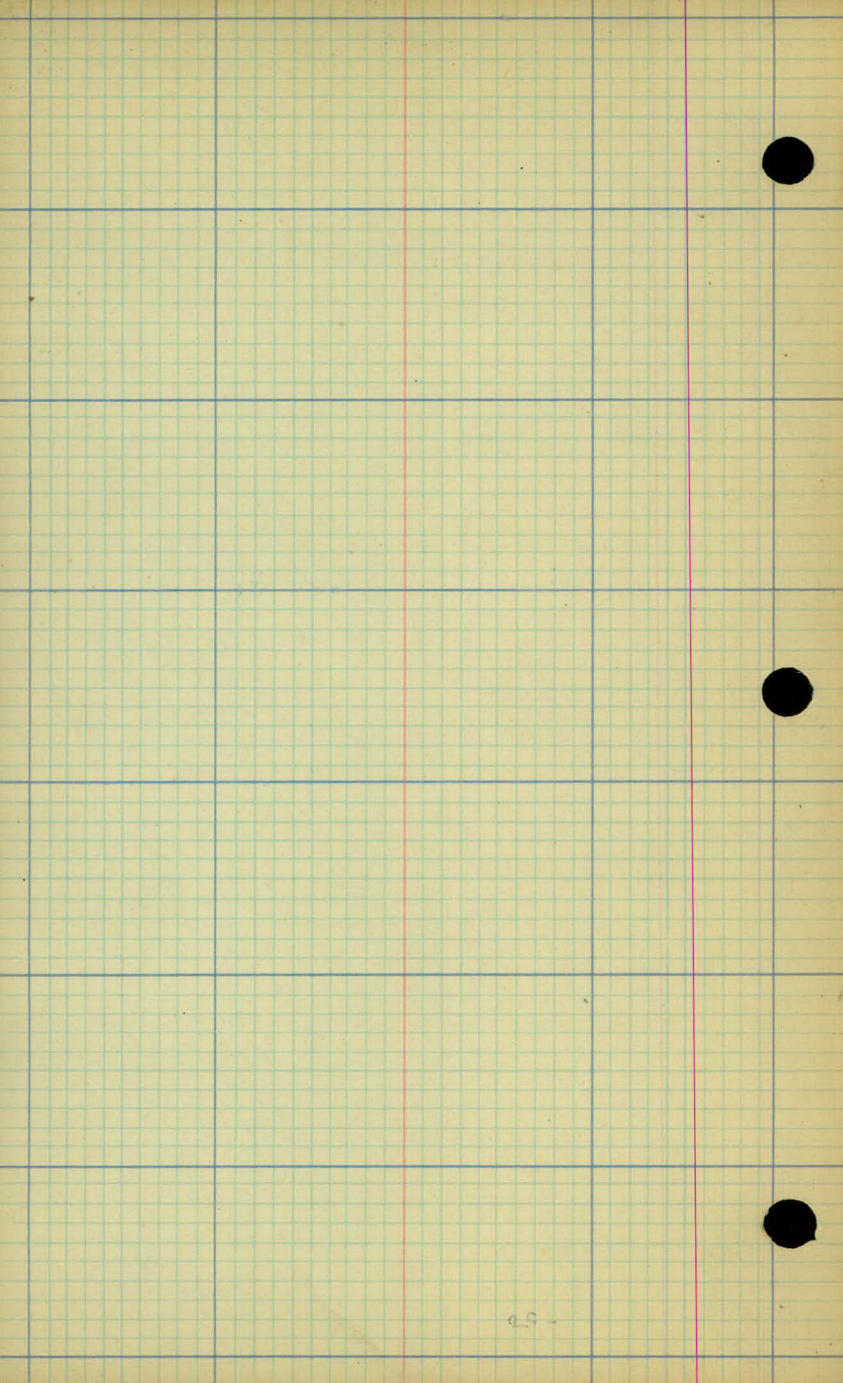
Spike in Tele Pole Rot 124+

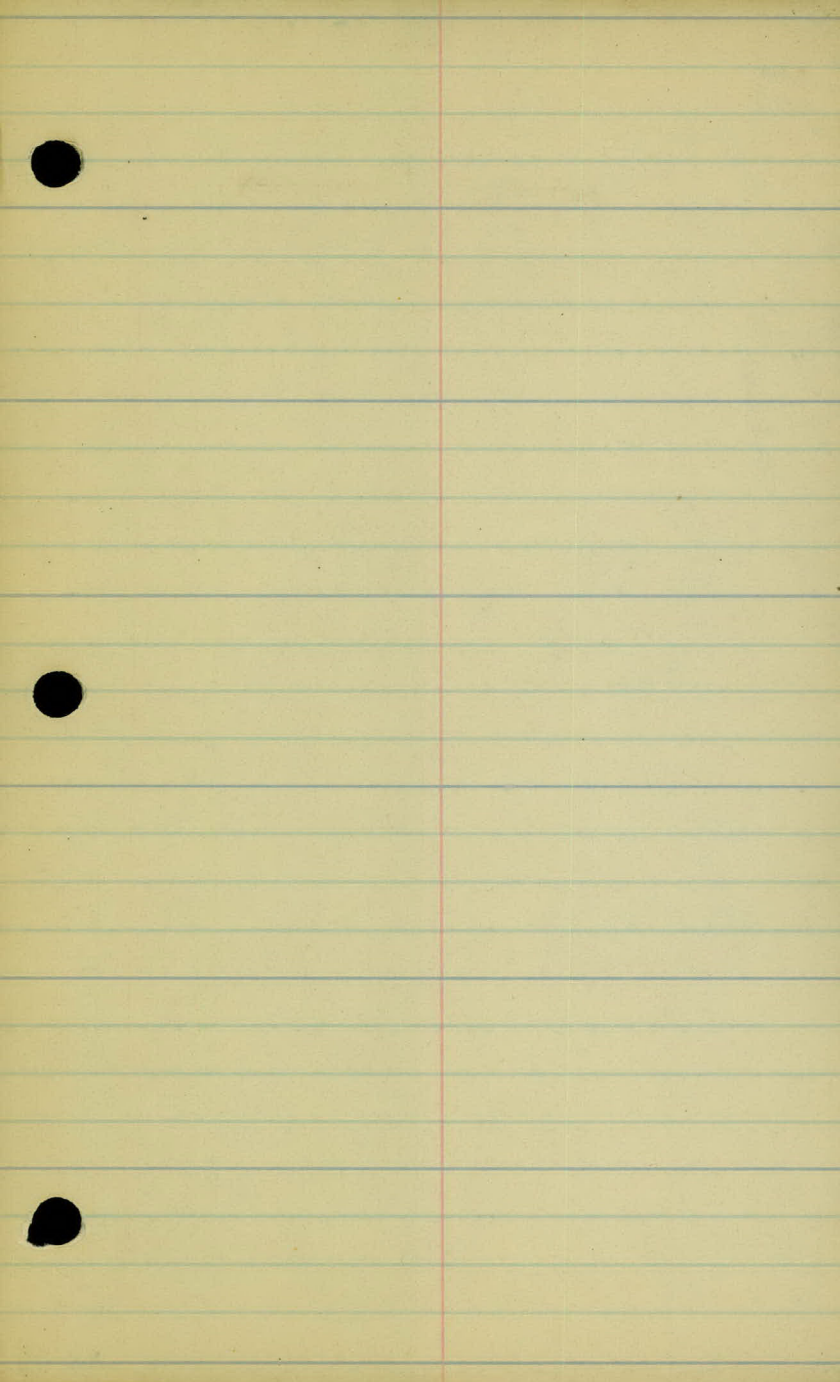
Spike in Tele Pole R 141+

" " " " " 152+

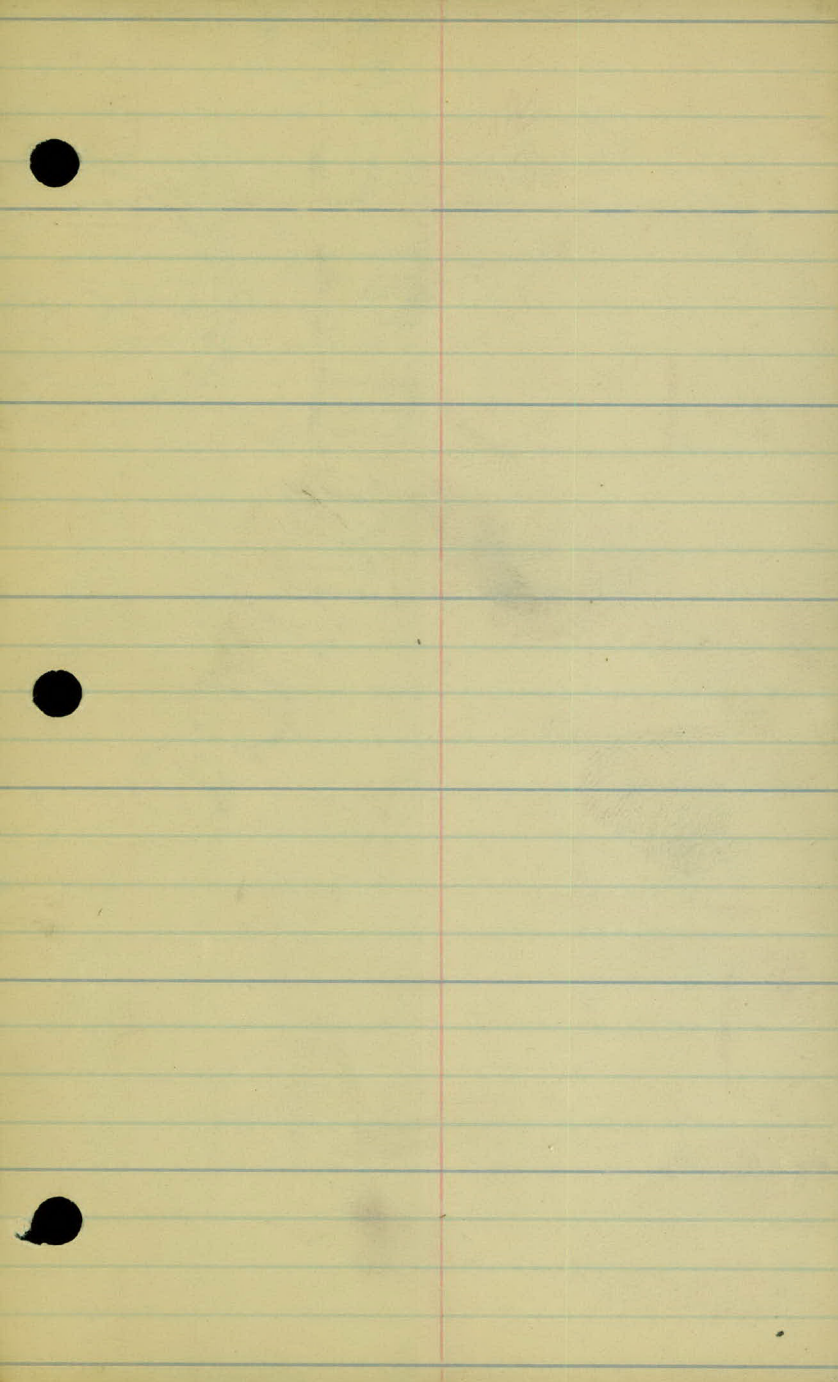
" " " " " 165+

Last B.M.

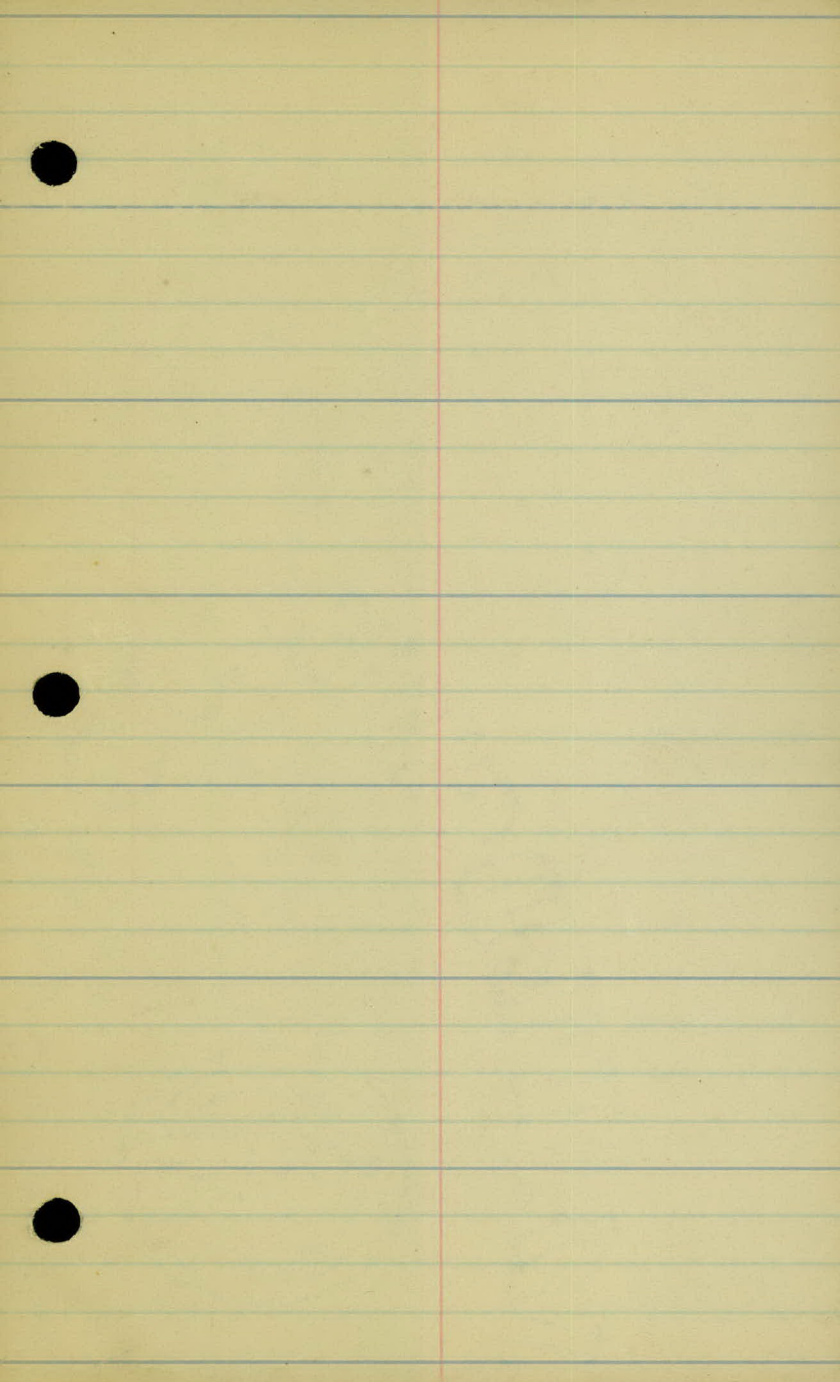




Sta	+	HT	-	Flev	Grade
B.M.	4.23	281.74	✓	277.51	4
21				6.1	275.64 274.5
22				6.0	275.7 275.4
23				5.4	276.3 276.2
24				4.4	277.3 277.1
25				3.3	278.4 278.0
26				2.4	279.3 278.8
27				1.8	279.9 279.7
T.P.	1.82	281.62	✓	1.94	279.80
+50				1.0	280.6 280.1
28				0.9	280.7 280.5
+50				1.2	280.9 281.0
29				2.5	279.1 279.6
+50				3.7	277.9 278.4



Sta		H.L.		Elev	Grade
29		1.82	281.62		
30				4.7	276.9 277.1
31				7.4	274.2 274.5
32				9.5	272.1 271.9
33				12.0	268.6 269.3
	T.P.	0.13	270.43	✓ 11.32	270.30
34				4.2	266.2 266.2
35				8.5	261.9 262.1
	T.P.	1.66	260.67	✓ 11.42	259.01
36				2.9	257.8 257.5
37			251.17	7.8	252.9 253.0
	+50			0.4	250.74 250.74
38				2.7	248.4 248.7
	B.M.			6.50	254.17 254.12
39				5.7	245.5 245.4
	T.P.	3.47	253.09	✓ 11.05	249.62
40				7.8	243.4 243.7
		0.97	251.17	✓ 2.89	250.20
	+50			8.4	242.8 242.8



Sta + H.I. - Elev Grade

41 8.8 242.4 242.4

TP 3.89 245.29 9.77 241.40

42 3.6 241.7 241.7

43 4.4 240.9 241.0

44 5.0 240.3 240.2

45 5.4 239.5 239.5

46 6.3 239.0 238.9

B.M. 5.61 242.36 236.75

47 4.0 238.4 238.3

48 4.6 237.8 237.7

49 5.2 237.2 237.1

50 5.5 236.9 236.5

51 7.3 235.1 234.6

TP 0.63 232.67 10.32 232.04

52 3.3 229.4 229.9

+50 6.2 226.5 226.0

L

E

R

CO.1

CO.1f

CO.4.

CO.5

Sta + H.I. - Elev Grade

0.63 232.67

53 9.2 223.5 223.9

T.P. 0.25 222.29 10.63 222.04

+50 221.1

54 4.5 217.8 218.3

T.P. 0.44 211.04 11.69 210.60

55 212.1 212.4

+50 2.3 208.7 209.4

56 5.4 205.6 206.4

57 10.4 200.6 200.7

T.P. 0.27 199.55 11.76 199.28

58 4.7 194.8 194.8

+50 8.0 191.8

59 11.1 188.8

T.P. 0.24 188.68 11.11 188.44

60 6.2 182.1

T.P. 0.15 177.10 11.73 176.95

61 1.0 176.1 176.1

+50 4.0 173.1 173.1

L R

0.0

F0.4

F1.1

F0.3

F0.5

F1.0

F1.1

F0.3

F0.7

F1.0

F0.7

F0.6

F0.6

F0.8

F0.7

F0.4

F0.1

F0.3

0.0

0.0

0.0

F1.0

F0.3

0.0

0.0

F0.3

0.0

C0.2

C0.4

C0.5

F0.5

0.0

C0.3

F0.4

0.0

C0.2

Sta + H.I. - Elev Grade

0.15 177.10

62 6.9 170.1
 B.M. 0.36 167.90 9.46 167.64 (167.64)

63 4.4 163.4

64 10.5 157.4 157.4

T.P. 0.86 158.25 10.51 157.39

+50 4.1 154.5

65 7.2 151.5

T.P. 1.43 148.52 11.16 147.09

66 3.4 145.6

67 9.1 139.7

T.P. 0.34 137.07 11.79 136.73

68 3.8 133.7

+50 10.5 130.8

69 10.1 127.0 0.9

T.P. 1.30 126.67 11.70 125.37

70 4.9 121.8 121.0 0.9

+70 7.7 119.5 118.5

B.M. 3.71 118.71 11.70 114.97 (115.00)

71 4.3 114.4 113.35

75 4.3 114.4 114.1

L E R

F0.1

C0.1

C0.3

S.E

C1.1

C0.1

C0.3

0.0

0.0

F0.8

0.0

F0.3

0.0

0.0

F0.4

0.0

F0.1

C0.5

F0.5

F0.2

F0.3

F0.8

0.0

F0.4

F0.4

F0.2

F0.4

F0.9

C 0.9

F0.1

C 0.9

C0.8

E0.8

C0.8

Sta + H.I. - Elev Grade

3.71 118.71

76 4.6 114.1 113.8

77 4.9 113.8 113.5

78 5.5 113.2 113.2

79 5.8 112.9 112.9

80 6.1 112.6 112.6

B.M. 2.79 116.36 5.14 113.57

81 4.2 112.2 112.2

82 4.5 111.9 111.9

83 4.8 111.6 111.6

84 5.1 111.3 111.3

85 5.5 110.9 111.0

86 5.6 110.8 110.7

87 6.1 110.3 110.3

B.M. 4.11 113.57 6.90 109.46

5.14

87 + 60 R

6.90

Sta + H.I. - Elev Grade

4.11 113.57

88 3.8 109.8 110.0

89 4.4 109.2 109.7

90 4.2 109.4 109.4

91 4.5 109.1 109.1

92 4.8 108.8 108.7

93 5.0 108.6 108.4

94 5.3 108.3 108.1

95 5.8 107.8 107.8

96 6.0 107.6 107.5

97 6.3 107.3 107.3

- T.P. 3.38 110.65 6.30 107.27

98 3.4 107.3 107.0

99 4.1 106.6 106.7

Sibley memorial

5/28/23

Sta I H.I. Elev Grade

3.38 110.65

100 4.6 106.1 106.3

102 4.9 105.8 105.8

103 5.1 105.6 105.3

+50 5.2 105.5 105.0

104 5.7 104.7

+50 6.0 104.2

105 6.8 103.9 103.7

106 7.7 103.0 103.0

T.P. 4.63 107.16 8.12 102.53

107 5.5 102.0

+50 5.4 101.5

108 5.8 101.0

+66.2 7.0 100.4

109 (Sta 108+68.2 to 112+70)
Bridge

110

B.M. 9.18

(97.98)

112+70 97.95

L

C

R

+	T	—	Elev
	219.41	3.04	216.37
217	218.54		
		(7.89)	210.65
		12.01	206.53
113	207.66	6.63	201.03
		6.63	216.37
918	210.21	10.53	199.68
12.48		322.1	216.64
		12.48	199.25
		19.73	
1189	211.18		
		99.5	201.23
614	207.37		
		1.00	206.73
701	213.74		
		2.99	210.75

172 + 72

15" x 30' C.M. imp

165 + 60

12" x 32' C.M. imp ✓

158 + 96

12" x 28' C.M. imp ✓

155 + 50

Road Int. R
No culv. req ✓

148 + 79

24" x 28' C.M. imp ✓

146 + 00

Ent. L. 12" x 28' C.M. imp ✓

146 + 33 Ent. R

No culv. req ✓

145 + 76

12" x 28' C.M. imp ✓

144 + 60

Ent. R.

No culv. req ✓

139 + 15

12" x 28' C.M. imp ✓

136 + 00

Ent. L.

No culv. req ✓

132 + 84

12" x 30' C.M. imp ✓

129 + 60

Ent. L. No culv. imp. ✓

Culv. reqd. pl. 12" x 25' cm

128+20 Ent. R.

No culv. regd ✓

125+10 12" X 26' C.M. imp ✓

123+40 Road Int. L ✓

No culv. regd

122+14 Ent. R.

No culv. imp

Culv. regd Pl. 12" X 25' C.M. ✓

121+35 Road Int. L

No culv. regd ✓

118+40 Road Int. L

No culv. imp ✓

Culv. regd 12" X 25' C.M.

114+64 Ent. R. ✓

Culv. regd 12" X 25' C.M.

97+10 12" X 32' C.M. imp ✓

88+88 12" X 28' C.M. imp ✓

80+27 12" X 30' C.M. imp ✓

81+45 Road Int. L ✓
Culv. reqd 12" x 30' CM

79+15 12" x 30' C.M. imp ✓

74+20 Ent. L
12" x 18' C.M. imp ✓

58+80 15" x 24' C.M. imp ✓

62+25 12" x 28' C.M. imp ✓

55+30 No culv. imp
None reqd ✓

52+12 No culv. imp
Culv. reqd 12" x 32' CM.

48+50 Ent. L.
P. Culv. reqd 12" x 25' CM.

46+40 Ent. L.
12" x 30' C.M. imp ✓

46 + 20

15" x 36' V.P. imp ✓

Extensions
necessary
both ends
3' each end

offtake ditch
on right needs
cleaning

43 + 00

Ent. R.

No culv. imp

Culv. reg'd ✓ 12" x 25'

37 + 85 Ent L.

Culv. reg'd. ✓ 12" x 25' C.M.

34 + 70 Ent L.

12" x 18' C.M. imp ✓

35 + 05 Ent. R.

12" x 18' C.M. imp ✓

26 + 75 Ent R.

Culv. reg'd ✓ 12" x 25' C.M.

23+20 ✓ Ent. R.

Culv. regd 12" x 25 cm

21+91 ✓

15" x 66" V.P. 17p

