

Book - 44- Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Prepared by
Road Map Survey

TURTLE LAKE RD.

From Hodgson Rd. To N. County Line

NORTH CO. LINE RD.

From Turtle Lake Rd. To Centerville Rd.

Road Acc't. No. 62-63

Date Filed 2-16-25

File

2-16-25

RELOCATION ROAD 62463

FROM HODGSON RD. TO CENTERVILLE R.

Alignment & Sec. Ties

an "L" LINE

Sta 0+00 to 232+84.98

Feb. 2, 1925 to Feb. 13, 1925

TRANSIT

P. R. Banister - Asst. Eng.

A. E. Austin - Transit

D. Skooglund - Hd. Chain

A. McEntyre - Riv. "

T. Franke - Appraiser

A. Berthiaume - Stakes

A. Janboski - Riv. Flag.

LEVELS.

P. Crane - Levelman

W. H. Huse - Rodman

NOTE.

Level Datum produced from Lake Improvement Bench mark at Hamline & Lexington as established in 1924 by Ramsey Co. Lake Improvement Dept.
LAKE IMPROVEMENT DATUM

tion

Ang. ht. Ang. R4.

23+386 P.O.T.

N. 23° 34' E.

22+662 P.T.

21+22.5 P.I. 66° 26'

19+340 P.C.

E45T

0+00 Mont & Hodgson. Road

LATITUDE & DEPARTURE CHART.

Proj. ROAD #62863 From Hodgson Road

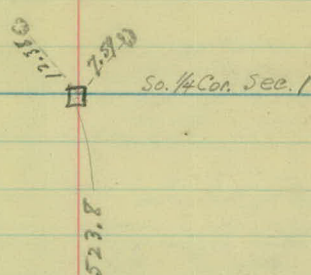
To Centerville Rd.

Sta.	Dist.	Deflection		Course	Latitude		Departure		Totals	
		L.	R.		+ N	- S	+ E	- W	Latitude	Departure
0+00									0	0
	2122.5 ✓			East ✓			2122.5			
1 21+22.5		66°26' ✓							0	2122.5
	1294.9 ✓			N. 23°34'E ✓	1186.9 ✓		517.7 ✓			
2 33+72.6		23°51' ✓							1186.9	2640.2
	1475.8 ✓			N. 00°17'W. ✓	1475.8 ✓			7.3 ✓		
3 48+44.5		89°46' ✓							2662.7	2632.9
	2638.8 ✓			N. 89°29'E. ✓	23.8 ✓		2638.7 ✓			
4 73+58.5		2°14' ✓							2686.5	5271.6
	2555.8 ✓			S. 88°17'E. ✓		76.6 ✓	2554.7 ✓			
5 99+14.2		91°49' ✓							2609.9	7826.3
	3150.2 ✓			N. 00°06'W. ✓	3150.2 ✓			5.5 ✓		
6 129+29.1		90°40' ✓							5760.1	7820.8
	2637.4 ✓			S. 89°26'E. ✓		26.1 ✓	2637.3 ✓			
7 154+37.2		0°22' ✓							5734.0	10458.1
	3976.6 ✓			S. 89°48'E. ✓		13.9 ✓	3976.6 ✓			
8 194+13.8		38°05' ✓							5720.1	14434.7
	2160.4 ✓			N. 52°07'E. ✓	1326.6 ✓		1705.1 ✓			
9 215+41.8		38°12' ✓							7046.7	16139.8
	1630.7 ✓			S. 89°41'E. ✓		9.0 ✓	1630.7 ✓			
10 231+35.3		71°03' ✓							7037.7	17770.5
	205.57 ✓			S. 18°38'E. ✓		194.8 ✓	65.7 ✓			
11 232+84.98									6842.9 ✓	17836.2 ✓

Computed by *W. Van Dusen* (T)
 Checked by *W. Van Dusen* (S.C.)

L nine

2



SE. MEE

- 19+34 - 0000
- +50 - 1036
- 20+00 - 6036
- +50 - 11036
- 21+00 - 16036
- +50 - 21036
- 22+00 - 26036
- +50 - 31036
- +662 - 33013

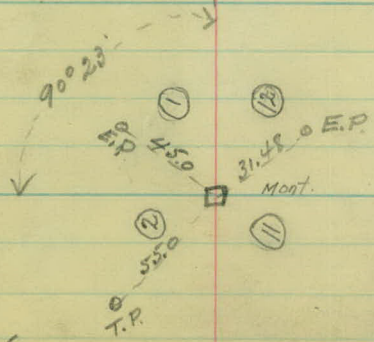
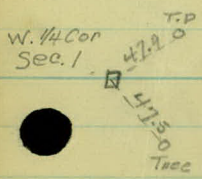
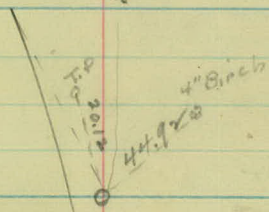
20° Curve ht

$\Delta = 66^{\circ}26'$

Rad = 287.94 ✓

Tang = 188.54 ✓

Length = 332.16 ✓



← North.

Station

Ang. ht. Ang. RI.

N. 89° 29' E.

50+06.5 ✓ P.T.

48+44.5 P.I.

89° 46'

45+57.7 ✓ P.C.

N. 00° 17' W.

34+89.9 ✓ P.T.

33+72.6 P.I. 23° 51'

32+51.4 ✓ P.C.

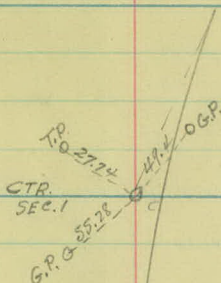
N. 23° 34' E.

h hinc

2

Sta. - Def

45+57.7 - 0°00'
 46+00 - 40°14'
 +50 - 90°14'
 47+00 - 140°14'
 +50 - 190°14'
 48+00 - 240°14'
 +50 - 290°14'
 49+00 - 340°14'
 +50 - 390°14'
 50+00 - 440°14'
 +06.5 - 440°53'



20° Curve. R4

$\Delta = 89°46'$

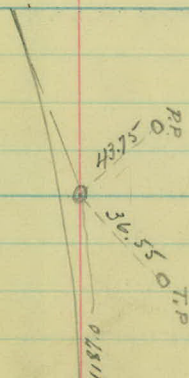
Rad = 287.94 ✓

Tang = 286.77 ✓

Length = 448.83 ✓

Sta. Def

32+51.4 - 0°00'
 33+00 - 20°26'
 +50 - 40°56'
 34+00 - 70°26'
 +50 - 90°56'
 +69.9 - 110°55½'



10° Curve. R4

$\Delta = 23°51'$

Rad. = 573.69 ✓

Tang = 121.15 ✓

Length = 238.50 ✓

So. 1/4 Cor. Sec. 1

E

Station

Ang. ht. Ang RA.

110+83.4 P.O.T

N.00°06'W.

100+76.1 ✓ P.T.

99+14.2 P.I. 91°49'

96+170 ✓ P.C.

82+00 P.O.T

S.88°17'E.

74+70.1 ✓ P.T.

73+58.5 P.I. 2°14'

72+46.8 ✓ P.C.

N.89°29'E.

h" nine

24" 47.3 32.4558"

Sta - Def

96+17 - 0000

+50 - 30°18'

97+00 - 80°18'

+50 - 13°18'

98+00 - 18°18'

+50 - 23°18'

99+00 - 28°18'

+50 - 33°18'

100+00 - 38°18'

+50 - 43°18'

+76' - 45°54 1/2

20° Curve Lt

$\Delta = 91°49'$

Rad = 287.94 ✓

Tang = 297.22 ✓

Length = 459.08 ✓

31.65
IRON PIN
Center
#6 Sec. 6

1° Curve Rt.

$\Delta = 2°14'$

R. 5739.65 ✓

T. 111.67 ✓

L. 223.33 ✓

42.15° F.P.

299.50 54°

T.P. 48.97

Mont. East 1/4 Cor. Sec. 1

Station.

Ang. ht. Ang. Pt.

178+80.5 P.O.T.

161+00 P.O.T.

154+37.2 P.I. $0^{\circ} 22'$

142+58.7 P.O.T.

130+91.1 P.T.

129+29.1 P.I.

126+57.8 P.C.

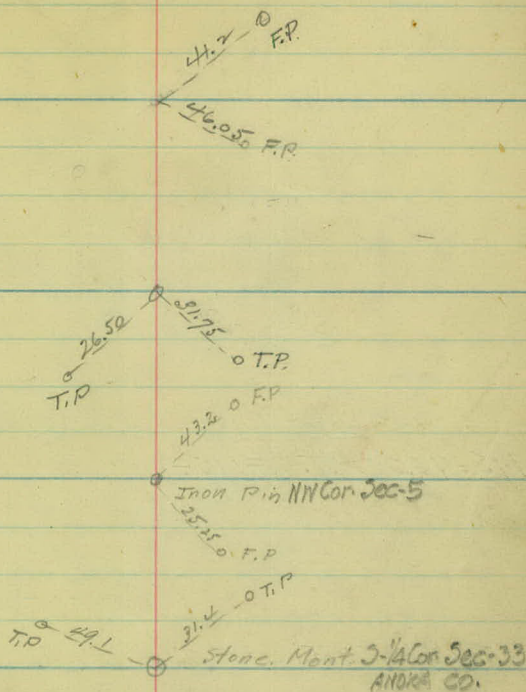
5.89° 48' E.

5.89° 26' E.

$90^{\circ} 40'$

N. 00° 06' W.

"L" HINC



Sta. - Def

126+37.8 - 0000'

+50 - 10'13"

127+00 - 60'13"

+50 - 110'13"

128+00 - 160'13"

+50 - 210'13"

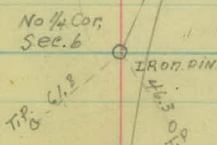
129+00 - 260'13"

+50 - 310'13"

130+00 - 360'13"

+50 - 410'13"

130+91' - 450'20"



20° Curve Rt.

$\Delta = 90^\circ 40'$

Rad = 287.94 ✓

Tan g = 291.30 ✓

Length = 453.33 ✓

Station

Ang. ht. Ang. Rt.

EQUATION

195+96.6 $\checkmark$ P.T. = 195+79.4
(End of Curve) (Tangent Ahead)

$\checkmark$ N. 52° 07' E.

194+13.8 P.I. 36° 05'

192+15.8 $\checkmark$ P.C.

180+77.3 P.O.T

$\checkmark$ S. 89° 48' E.

Sta - Def

192+58 - 0000

+50 - 10 42 1/2'

193+00 - 40 12 1/2'

+50 - 60 42 1/2'

194+00 - 90 12 1/2'

+50 - 110 42 1/2'

195+00 - 140 12 1/2'

+50 - 160 42 1/2'

195+96.6 - 190 02 1/2'

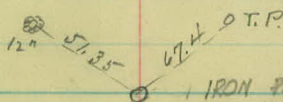
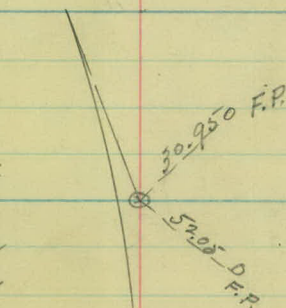
10° Curve ht.

$\Delta = 38^\circ 05'$

Rad. = 573.69 ✓

Tang. = 198.00 ✓

Length = 380.83 ✓



IRON PIN

N 1/4 Cor. Sec. 5

{ Estab. - 2640' E. from
Iron Pin N 1/4 Cor. Sec. 5
running E to N 1/4 Cor. Sec. 4.
2-B-25 PRB }

Station

Ang. ht. Ang. Pt.

232+84.28

P.T. (on E. Centerville Road)

5.18° 38' E.

231+35.3

P.I.

71° 03'

229+29.73

P.C.

5.89° 41' E.

220+00.7

P.T.

215+41.8

P.I.

38° 12'

210+45.7

P.C.

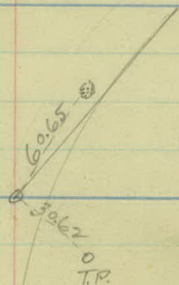
N. 52.87° E.

6" line t

(See sketch back of this sheet.)
2-13-25 PRB.

Sta - Def

229+29⁷³ - 0°00'
+50 - 2°01½'
230+00 - 7°01½'
+50 - 12°01½'
231+00 - 17°01½'
+50 - 22°01½'
232+00 - 27°01½'
+50 - 32°01½'
232+80⁹⁸ - 35°31½'



20° Curve, RT.

$\Delta = 71°03'$

Rad = 287.94 ✓

Tang = 205.57 ✓

Length = 355.25 ✓

Sta - Def

210+45.7 - 0°00'
211+00 - 1°05'
212+00 - 3°05'
213+00 - 5°05'
214+00 - 7°05'
215+00 - 9°05'
216+00 - 11°05'
217+00 - 13°05'
218+00 - 15°05'
219+00 - 17°05'
219+00.7 - 19°06'



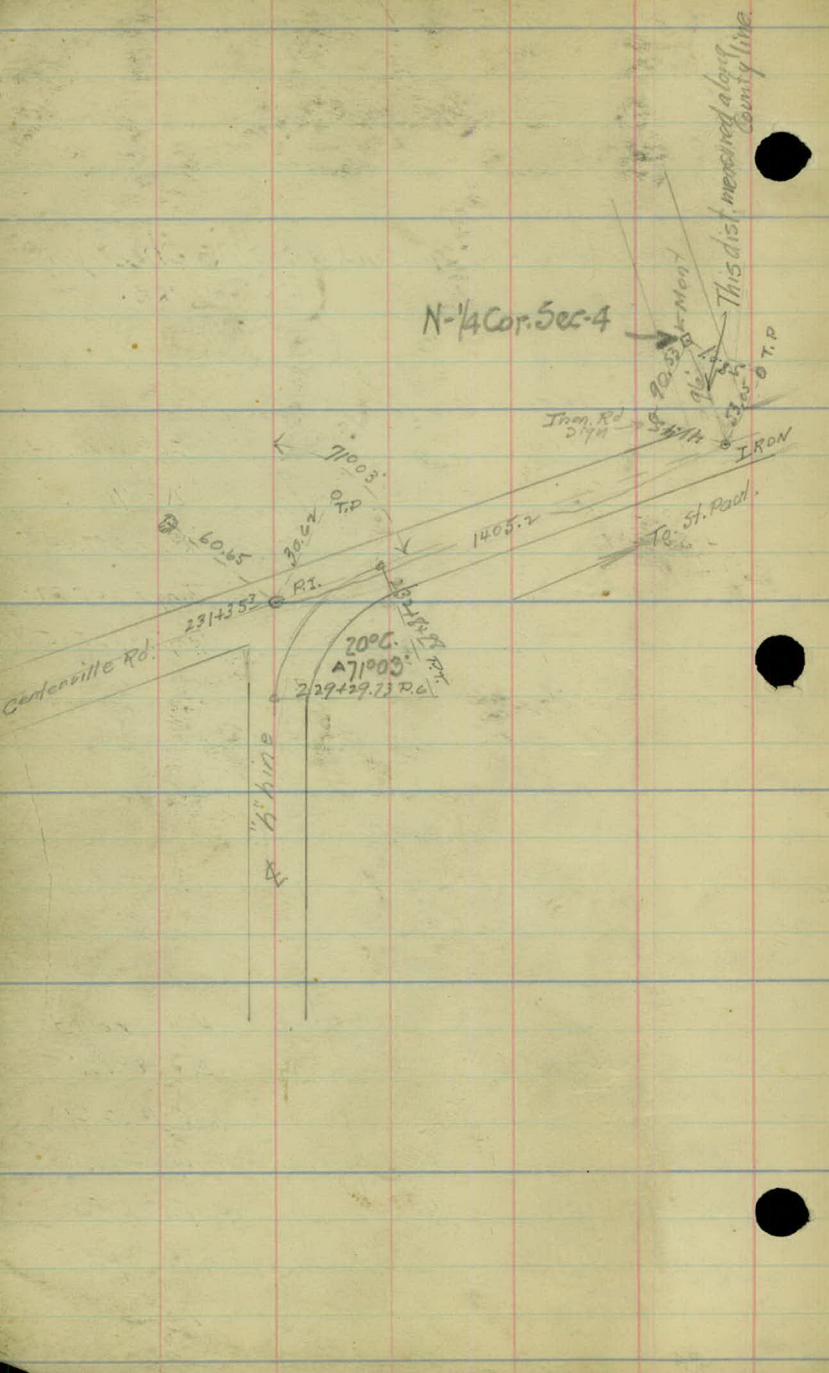
4° Curve, RT.

$\Delta = 38°12'$

Rad = 1432.69 ✓

Tang = 496.11 ✓

Length = 955.00 ✓

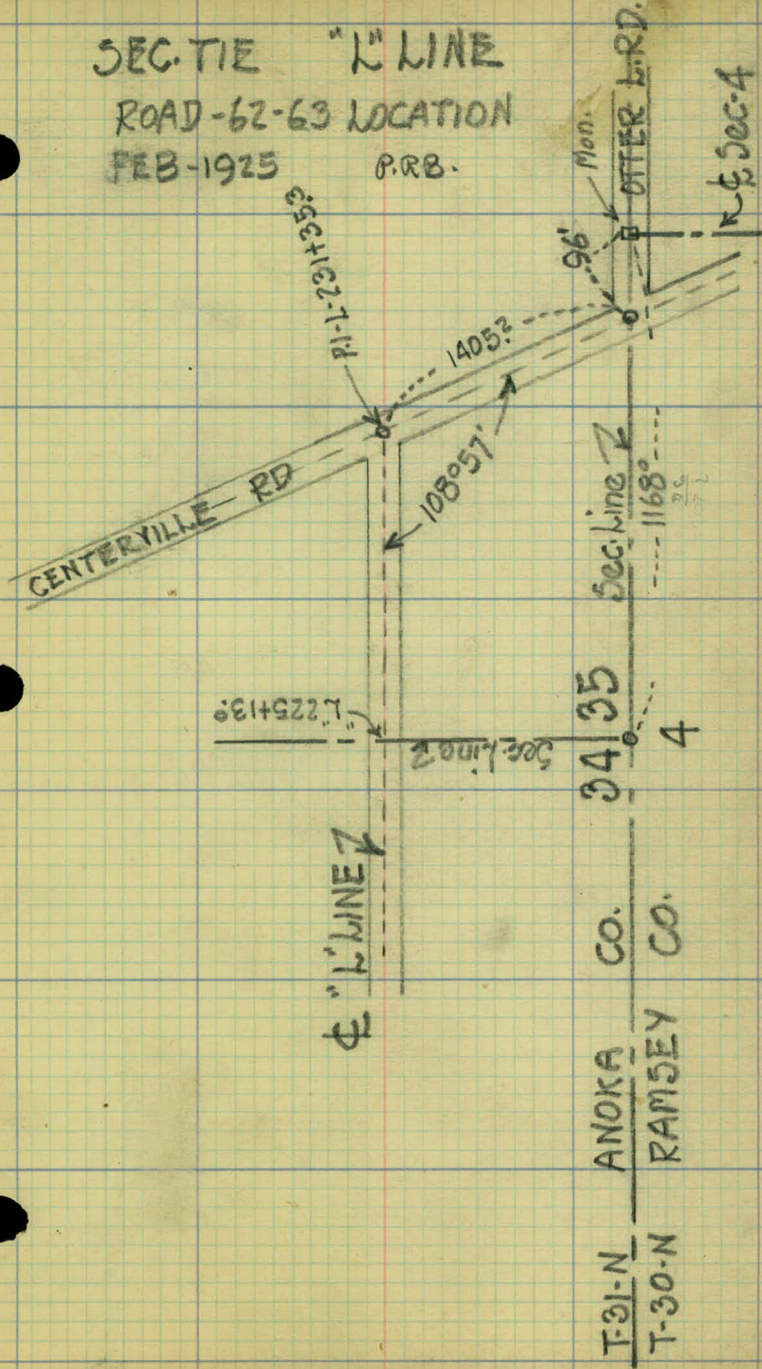


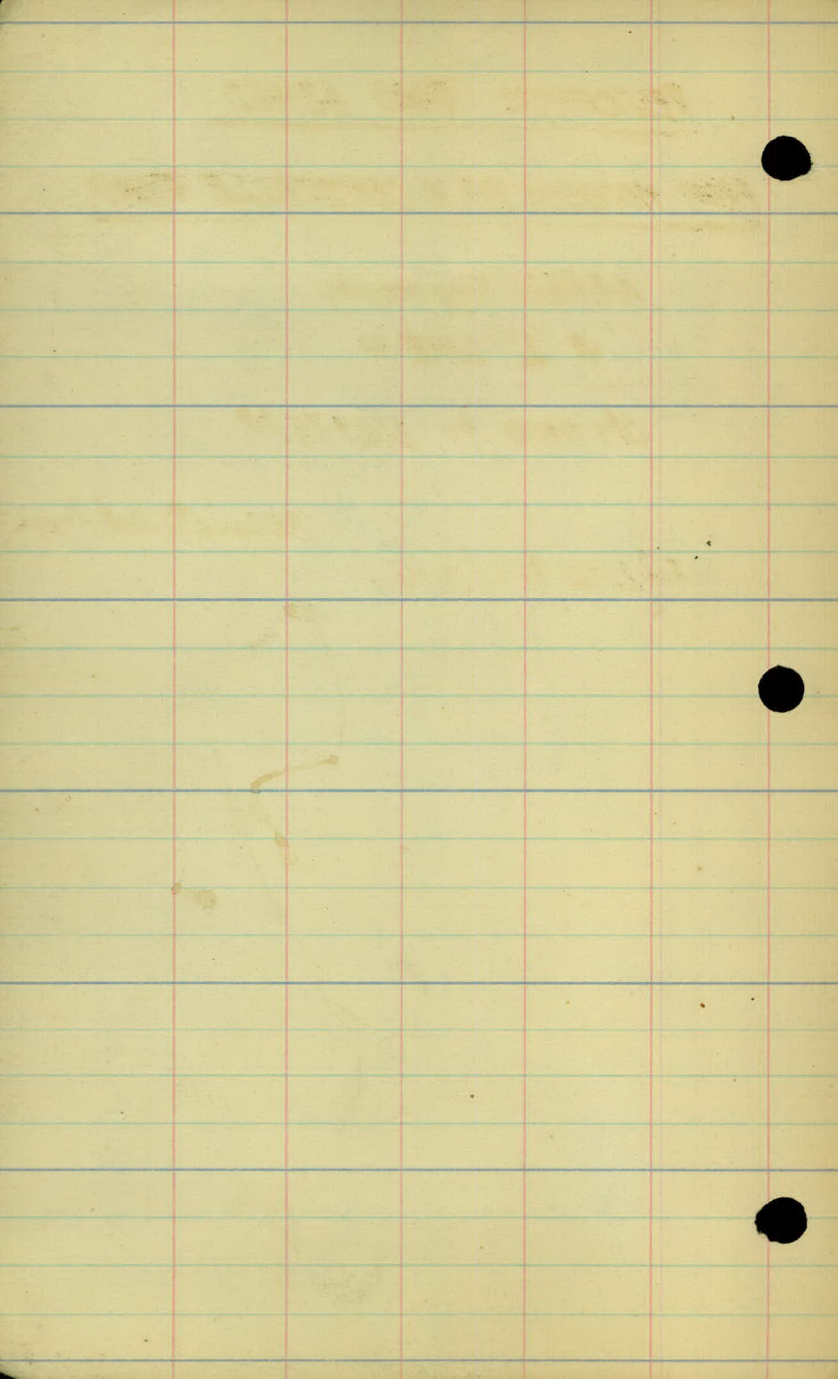
SEC. TIE "L" LINE

ROAD-62-63 LOCATION

FEB-1925

P.R.B.





RELOCATION ROAD 62463

FROM HODGSON RD TO CENTERVILLE ROAD

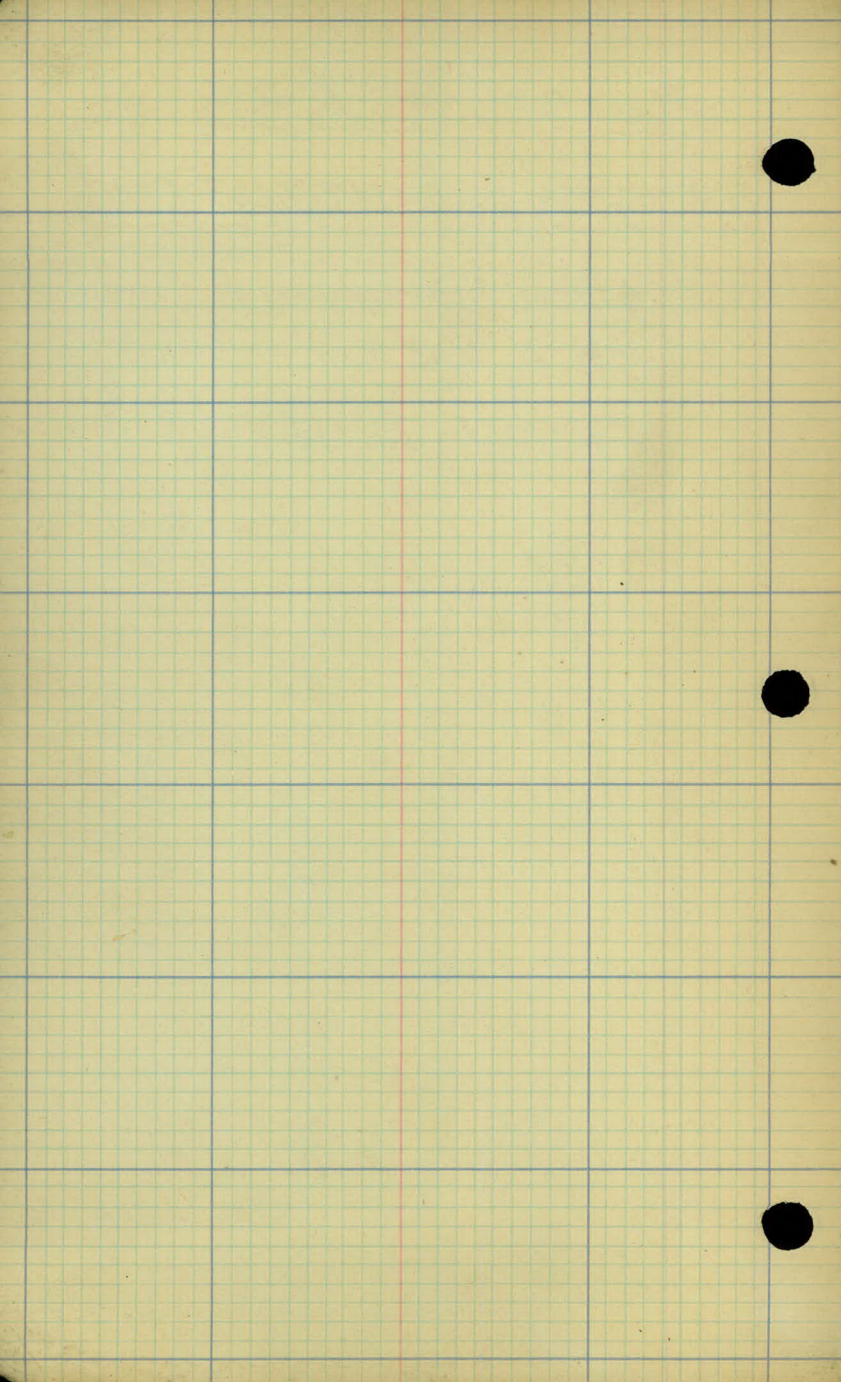
Artificial Topography

A "L" LINE B

Sta 0+00 to 232+84.98

P.R. Banister Asst. Engr.

Feb. 2, 1925 to Feb. 13, 1925



"L" LINE

6+00

+73 P.P. 25.0'

+54 T.P. 23' R/L

5+00

+40 P.P. 25' R/L

+32 T.P. 23' R/L

4+00

+10 P.P. 24.5 R/L

+18 T.P. 23' R/L

3+00

Waste band

+60 P.P. 22' R/L

+10 Water Main Xing

2+00

+80 T.P. 21' R/L

Cultivated

32.5

32.5

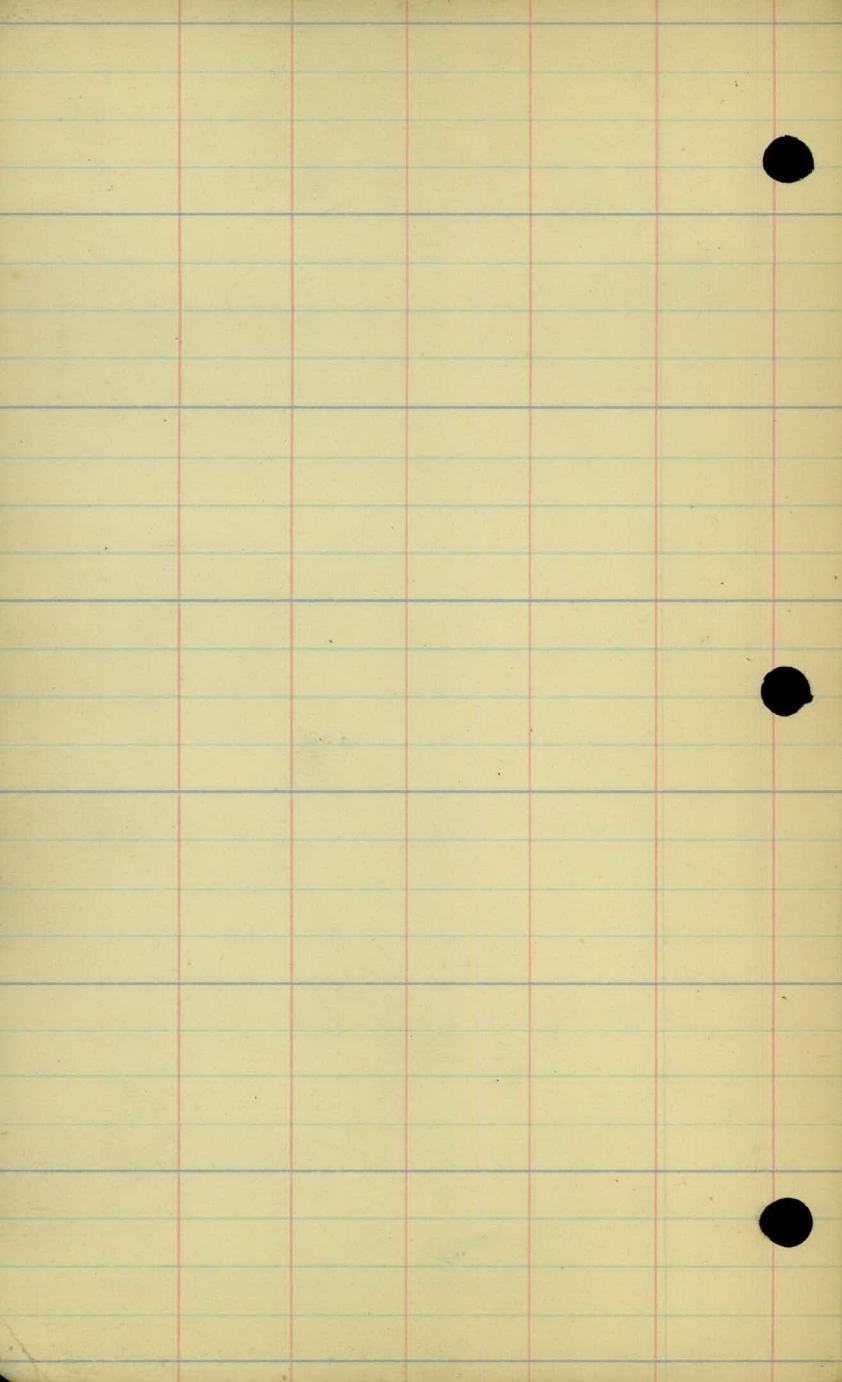
1+00

+55 T.P. 21' R/L

+22 P.P. 22.5 R/L
+17 Rd. Sign 26'

+32 32.5

0+00



L line

13+00

+15 R.P. 29' ht.

+170 Overhead Power line

+56 Road

+60

+61 Mail Box 15' R.P.

12+00

+96 T.P. 26' R.P.

+12 R.P. 28' ht.

11+00

+66 T.P.

(15 - 2x12 Floor
 2 - 12x12x24 Caps
 2 - 6 Pile Bents
 11 - 6" I Beams 16' long)

+86 Beg. Fence 29.5 R.P.

10+00

+00

8' 10.5

+99 End. Bridge
+91.5 End. Bridge

+74 R.P. 27' ht.

+46 T.P. 25' R.P.

9+00

+39 R.P. 26' ht.

+19 T.P. 24' R.P.

8+00

+01 R.P. 26' ht.

7+00

+54 T.P. 23.5 R.P.

6+00

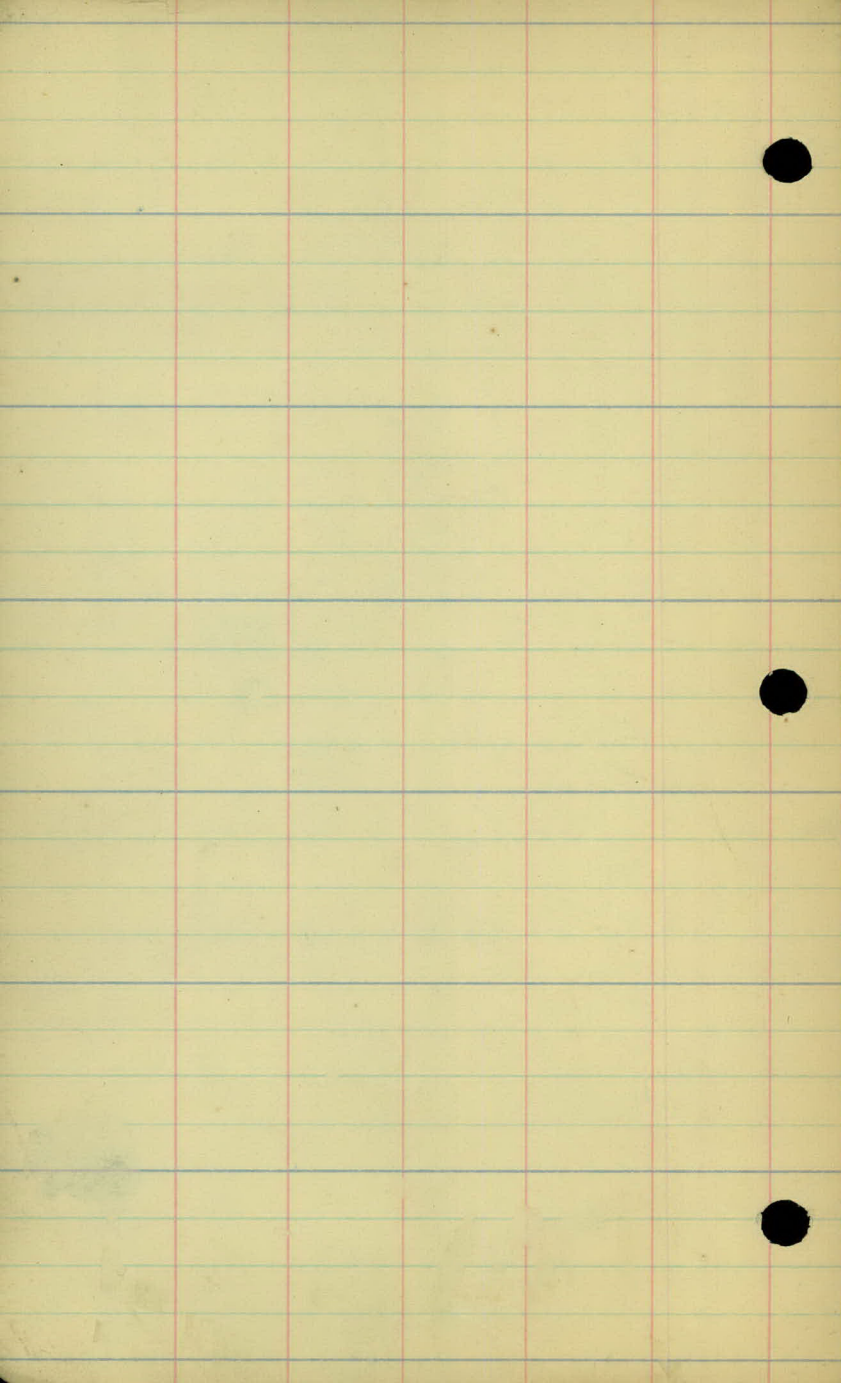
Bottom land

Bottom land

Bottom land

Brush

Bottom land



"L" line

20+00

Evergreen
+09 P.P. 26.5
+66 @ 24.5 M.

+58 T.P. 20'

19+00

+13 T.P. 22.5 R.L.

18+00

+35 P.P. 28' H

+45 @ 23' R.L. (18')

+91 @ 32' (18" Oak)
+93 T.P. 24' R.L.

17+00

+79 P.P. 29' H

+67 T.P. 24' R.L.

16+00

+87 Ence. Cor.

15+00

+14 T.P. 29' H

+47 T.P. 26' R.L.

14+00

+24 T.P. 26.5
+22

13+00

Cut Hatched land.

Continued

4
old. Rd. 4
ht. 25' 510. Rd.
R7

28'

29'

29'

28'

19'

17'

7.0

00.175

15

81

25

10'

h line 27+00

+92 T.P. 13' h/

+29 P.P. 4' h/

+66 T.P. 15' h/

+60 P.P. 48' h/
+50 T.P. 10' h/

+31 T.P. 4' h/

+87 P.P. 39' h/

+75 F.E

F.E

Cultivated Field

+18 Fence Xing

+45 Drive

+11 T.P. 5' R/

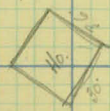
+78 ± Road Xing

+32 P.P. 1' R/

+11 T.P. 52' R/

+78 P.P. 7' R/

+45 T.P. 4 1/2' R/



26+00

25+00

24+00

23+00

22+00

21+00

20+00

16

32

50

72

92

100

96

78

53

25

130

20.0

"H" line

100 Power line Xing 34+00

+90 drive

+59 R.P. 09 ht.

+42 T.P. 36' R/L

33+00

+85 T.P. 75' R/L
+25 R.P. 59' R/L

32+00

+95 Cor.

Cultivated Field

Road

Road

+25 T.P. 125' R/L
+17

31+00

+90 R.P. 71' R/L

+25 T.P. 110' R/L

30+00

+40 R.P. 18' R/L

+23 T.P. 55' R/L

29+00

+47 R/L Road

+12 T.P. 09' R/L

28+00

+88 R.P. 36' R/L

+65 Fence Xing

+37

27+00

20

07

"L" line

4400

+71 T.P. 17' R1

+58

+12 P.P. 24' H1

40100

+90 Cop
+75 P.P. 17' R1

+43 T.P. 17' R1

39400

+45 P.P. 23' H1

Postone

+22 T.P. 17' R1

38400

+32 P.P. 24' H1

+05 T.P. 17' R1

37400

Postone

36400

+82 T.P. 17' R1

+45

+19 P.P. 23.5' H1

35700

Cultivated

Cultivated

+57 T.P. 18' R1

+10 P.P. 36' R1
+05 P.P. 41' R1

34400

86
93 +87
92 +70

75

44

17.0

5.0

"L" line

 $\frac{4}{5} + 00$

197 T.D 54' 49"

+80 P.D 1454+

487 Fence, con.

+ 59 T.P. 5/11

450 P.P. 97 1/2

+70

+69 P.P. 48 h +

+ 79 T.P. 08. kt.

+60 Fence Xing

+24 P.P. 23.5A

456 T.P. 17.5 R4

457 P.P. 24/67.

436 T. P. 17 R.

+16 T.P. 17' R.L.

182 R.R. 24th lot

490 T. P. 16. 2

47400

46400

 $45 + 00$

44,00

43400

4200

41400.

Cultivated

Cultivated

26

20

50

"L" line

55+00

54+00

+80 P.R. 19' AT 90

+81 T.P. 20' RT

53+00

+64 T.P. 25' RT

+11 P.R. 18' AT

52+00

60'

26' +70

+70 T.P. 26' RT

51+00

42'

26'

Meadow hand.

+42 P.R. 17' AT

+11 T.P. 26' RT

50+00

34'

26'

Confined

37'

21'

+15 F.E.

+93 P.R. 39' AT

49+00

Road

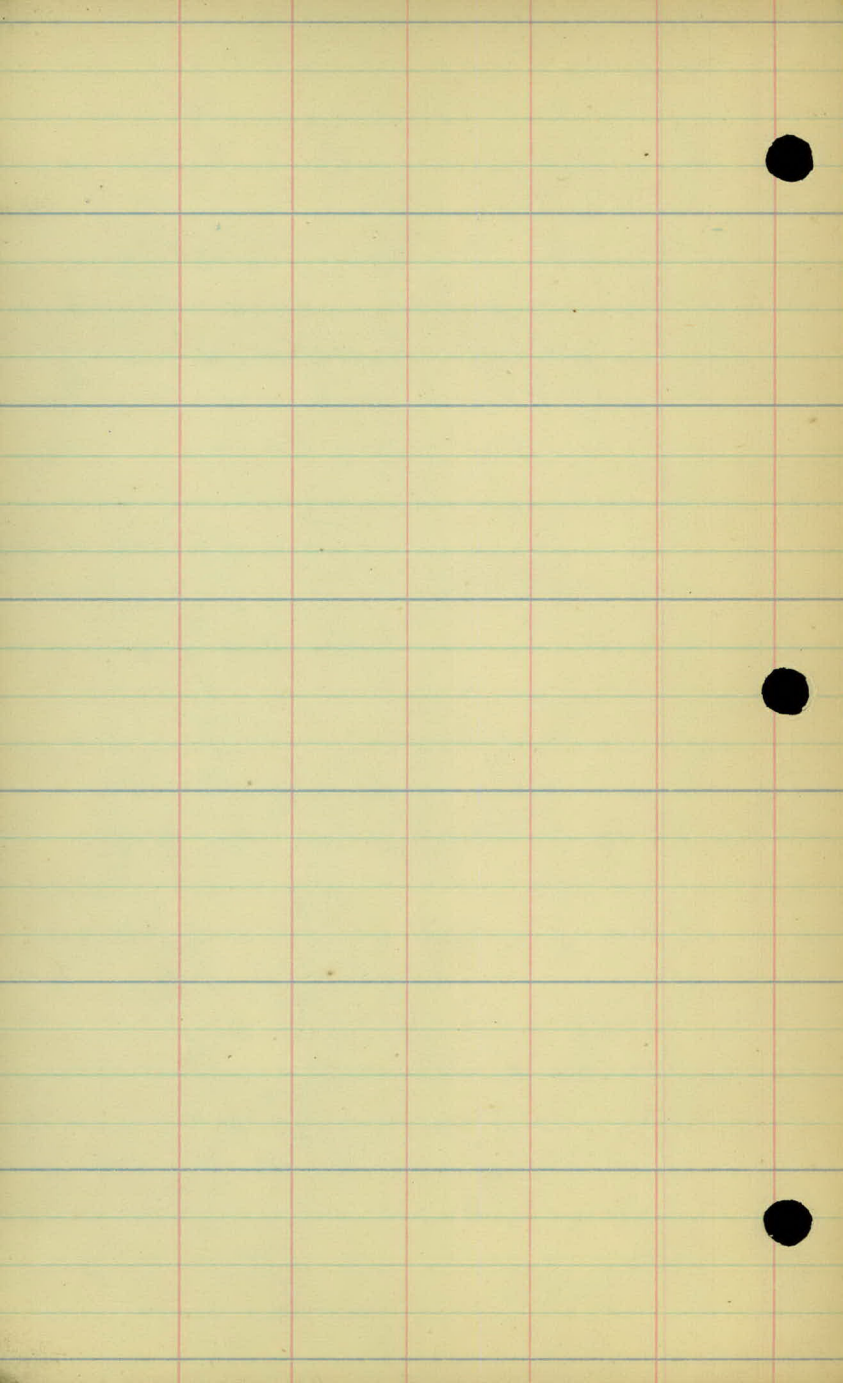
+82 Fencing

+82 T.P. 2'

18'

+17 G.P. 100' LT

48+00



"L" line

62+00

+86 P.P. 23' Ht.

+92 T.P. 21.5' Ht.

61+00

+100

+14 -26'

Concrete steps.

60+00

+92 T.P. 22'

Church.

Grounds.

59+00

+70 T.P. 22' Ht.

58+00

+60 P.P. 22' Ht.

+45 T.P. 23' Ht.

57+00

+00 P.P. 21' Ht.

Meadow land

Continued

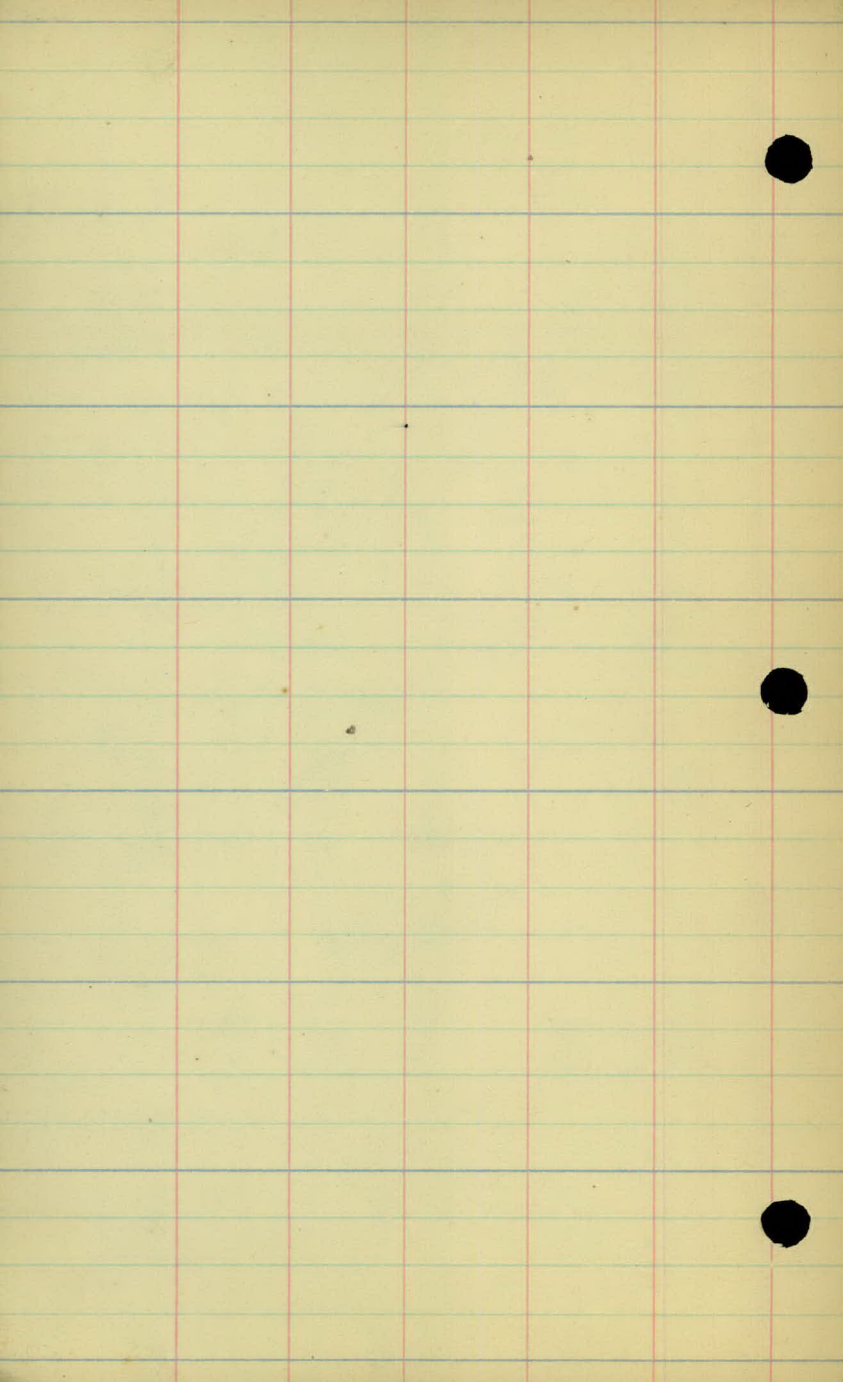
+25 T.P. 23' Ht.

56+00

+57 P.P. 20' Ht.

+03 T.P. 25' Ht.

55+00



"L" line

69+00

20'

68+00

25'

+32 R.P. 26' H.

67+00

23'

Cultivated

66+00

24'

+43 R.P. 27' H.

65+00

25'

Cultivated

O
 O
 O O O O O
 O O O O O
 O O O O O
 ----- +23 Walk

64+00

25'

ORCHARD

+94 T.P. 21' End.

DRIVE

+47 R.P. 23' H.

63+00

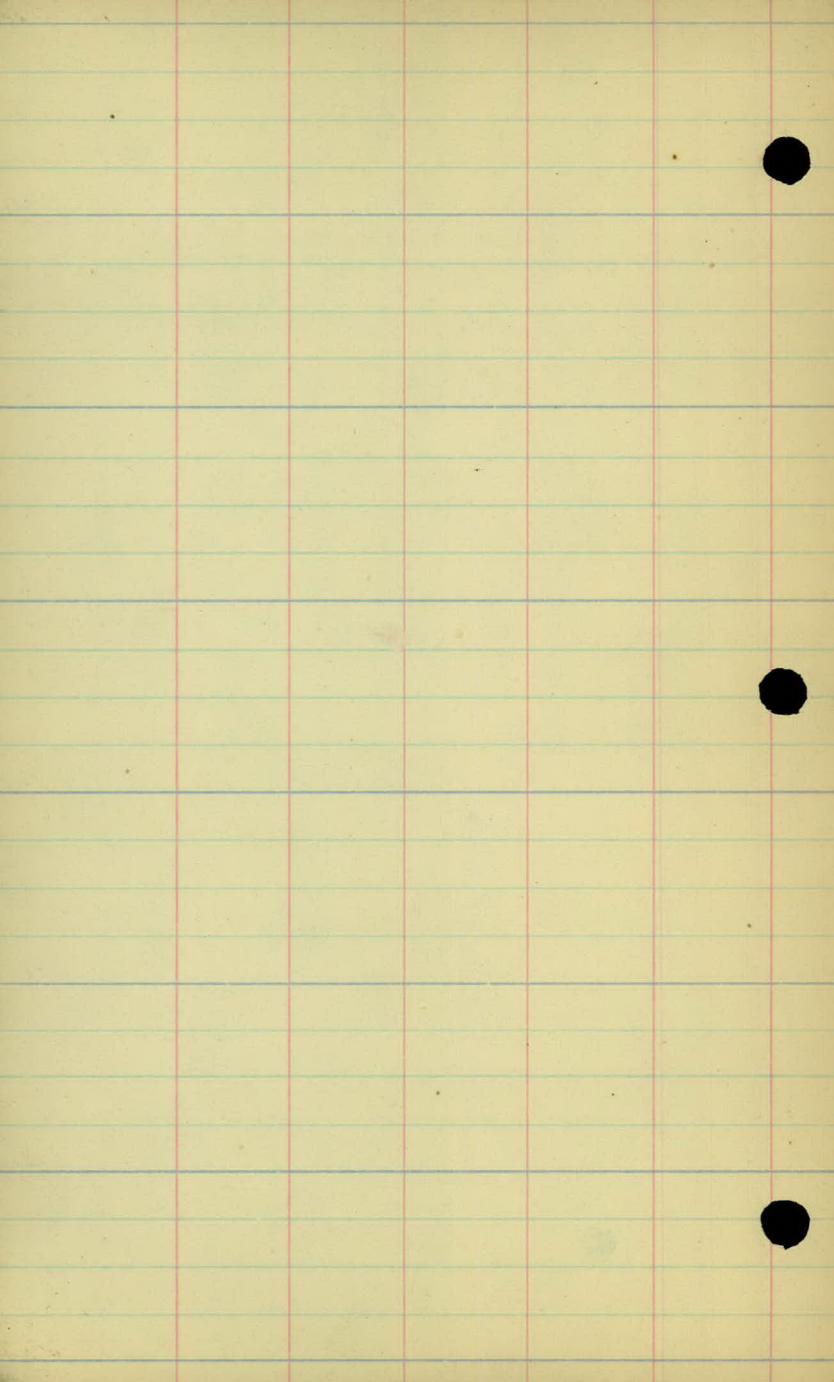
24'

MEADOW land

+53 T.P. 22' H.

62+00

25'



"L" line

76+00

Cultivated land.

+98 P.P. 28' Ht.

75+00

Timber

74+00

+58.5 --- +58.5
+50 Drive

+17 P.P. 27' Ht.

73+00

Cultivated

+10 Drive

72+00

+51 Power line Limb
Over Road.

+52 RR 92' Ht.
+49 RR 36' Ht.
+39 P.P. 26' Ht.

+14 P.P. 26' Ht.

71+00

Cultivated

+34 - +85 Power line Tower

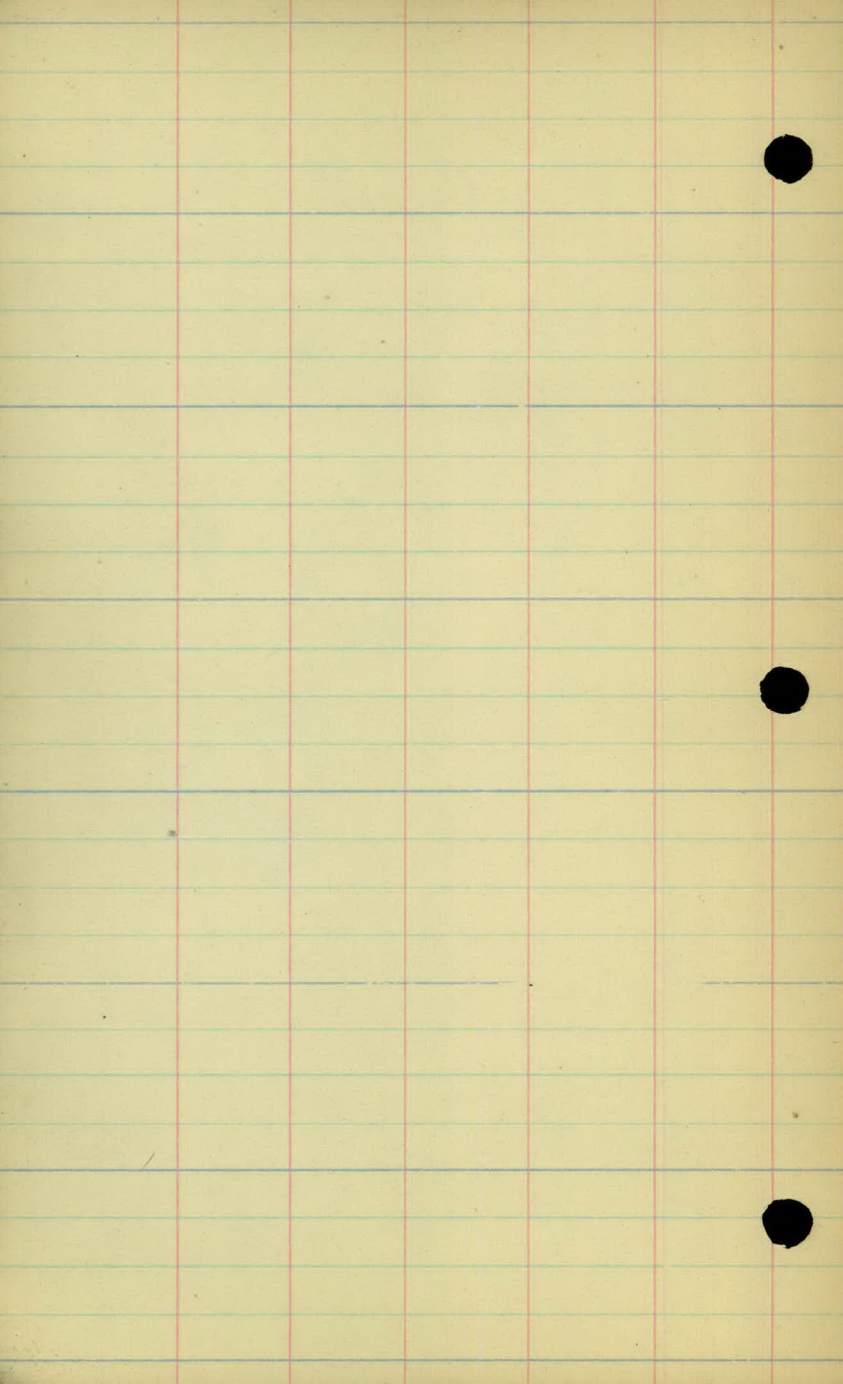
70+00

+72 Drive

+25 P.P. 26' Ht.

69+00

24'



+90 P.P. 34' ht.

"L" line

83+00

34

32

82+00

+56 P.P. 33' ht.

33

81+00

Cultivated

33

80+00

+93 P.P. 32' ht.

32

79+00

Cultivated

32

78+00

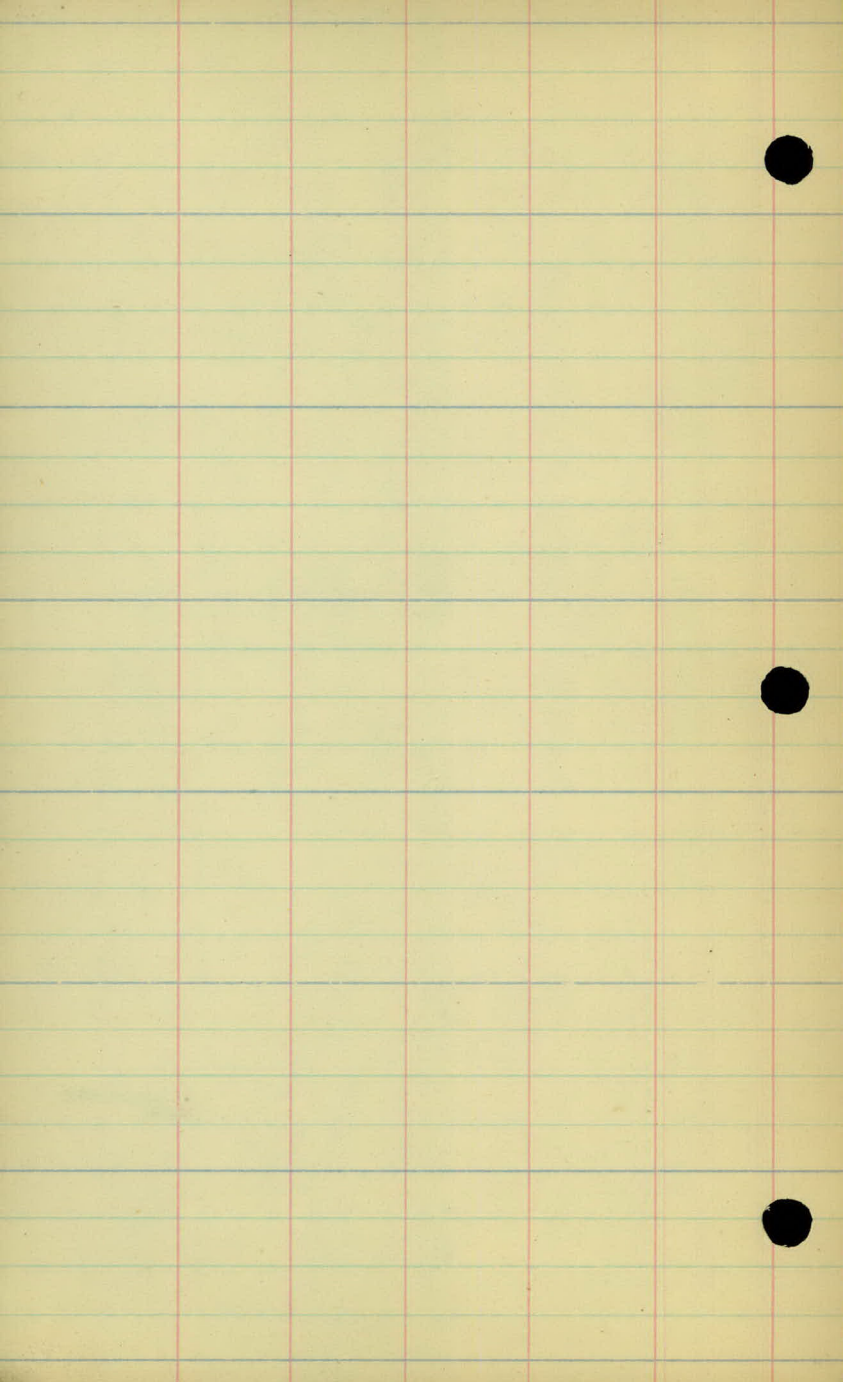
Timber

+97 P.P. 30' ht.

33

77+00

76+00



"L" line

90+00

+80 P.P. 34' 1/2

89+00

88+00

+80 P.P. 33' 1/2

87+00

86+00

+60 P.P. 34' 1/2

85+00

84+00

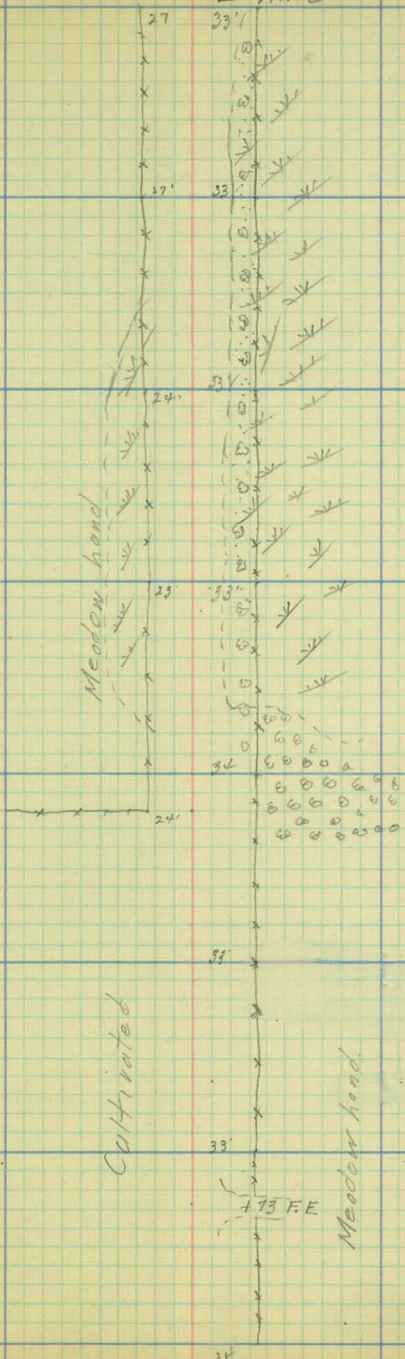
83+00

Meadow hand

Cultivated

Meadow hand

+73 F.E.



14

03

+70 P.P. 26' Ht

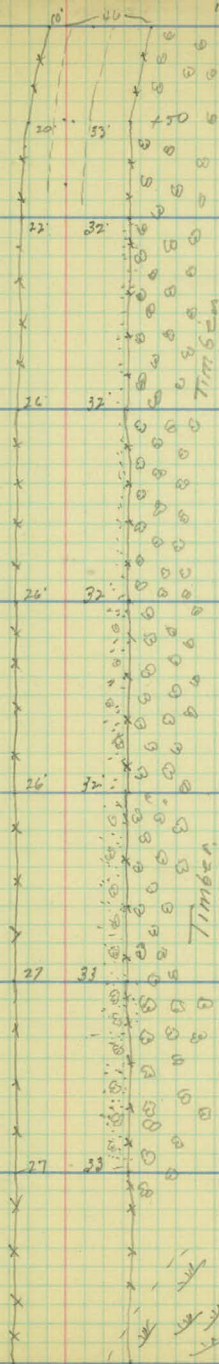
+71 P.P. 31' Ht

+77 P.P. 31' Ht

+80 P.P. 33' Ht

Cultivated

Meadow land



"L" line

97+00

96+00

95+00

94+00

93+00

92+00

91+00

90+00

3.0

2.0

2.0

08

29

68.

98

75

37

left & right
8.0

8.0

7.1

6.5

4.0

3.0

3.0

"L" line

111+00

+23 P.P. 33' ht.

Post one

33'

20' 15" +90

Small Trees

110+00

+26 P.P. 35' ht.

33'

24'

109+00

32'

26'

108+00

Meadow land

Post one

Road

30'

26'

107+00

+40 P.P. 30' ht.

30'

25'

106+00

+60 Drive

30'

26'

Meadow land

Cultivated

28'

25'

105+00

+47 P.P. 30' ht.

104+00

Rd. 67 - 2 Rd. P1
5.0

6.0

5.0

5.0

5.0

7.0

7.0

"L" line

118+00

+59 T.P. 16' RT.

117+00

Cultivated

Posture.

+31 T.P. 16' RT.

+24 T.P. 38' RT.

116+00

Road

Posture.

+06 T.P.

115+00

Cultivated

+11 DRIVE
POWER LINE ROAD

+62 P.P. 28' RT.
+48 P.P. 24' RT.
+41 P.P. 20' RT.
+20 T.P. 34' RT.

114+00

+84 T.P. 15' RT.



Cultivated

113+00

+52 T.P. 14' RT.

+32 P.P. 34' RT.



Farm pond

40' x 40' UNIT

112+00



+37

+20 DRIVE

+15 DRIVE

111+00

1.0

1.5

2.0

2.0

3.0

4.0

4.0

"L" line

125+00

+100 T.P. 27' 6"

124+00

+82 T.P. 19' R+.

24'

123+00

+111 T.P. 29' 11"

24'

122+00

+135 T.P. 18' R+.

24'

121+00

+13 T.P. 30' 6"

Cultivated

25'

120+00

3+42

25'

+39

Road

pasture

+22 T.P. 31' 4"

7'

119+00

+84 T.P. 17' R1

118+00

02.5

140

40

85.0

461

105.0

100.0

54.0

23.0

7.0

1.0

"L" line

132+00

+58 P.R. 24' Ht.

+00 T.P. 14' R.H. 131+00

Cultivated

130+00

+85 P.P. 49' Ht.

+69 T.P. 04' Ht.

CEMETERY

75' Pool

+50

129+00

+75 T.P. 79' Ht.

+61 T.P. 153' Ht.

+46 T.P. 68' Ht.

129

128+00

+81 T.P. 66' Ht.

+55 T.P. 3' Ht.

Pool

Waste land

127+00

+13 T.P. 24' Ht.

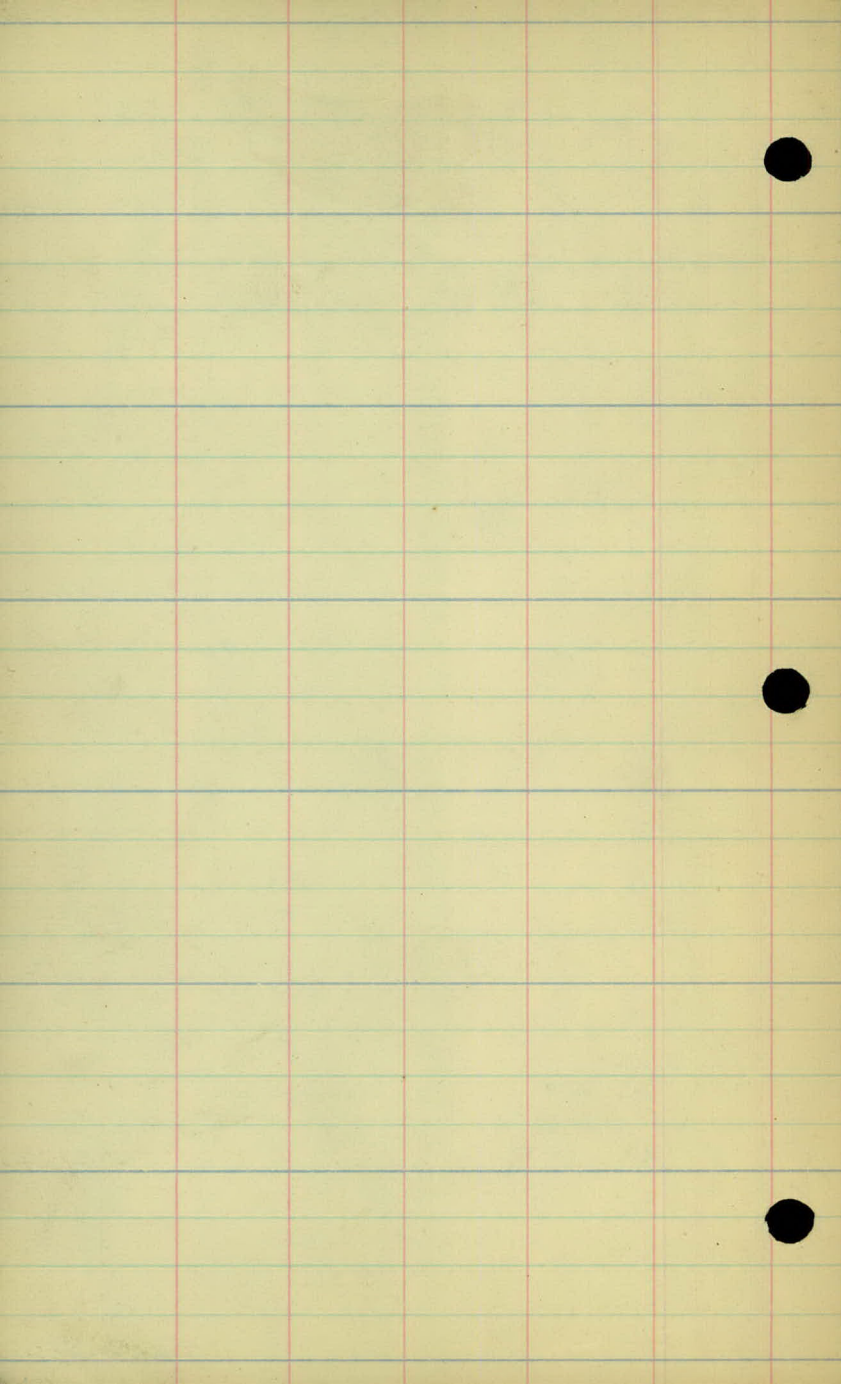
+29 T.P. 20'

126+00

Cultivated

Cultivated

+06 T.P. 20' R.H. 125+00



"L" hide

+98 T.P. 14' R₁

139

138

+69 T.P. 14' R₁

+39 P.P. 23.5 ft

137

+35 T.P. 14' R₁

136

+45 P.P. 24' ft

135 12
135 12

Meadow hood

Meadow hood

+50 Wood. Box
Culvert.
Caved In.

+02 T.P. 14' R₁

135

134

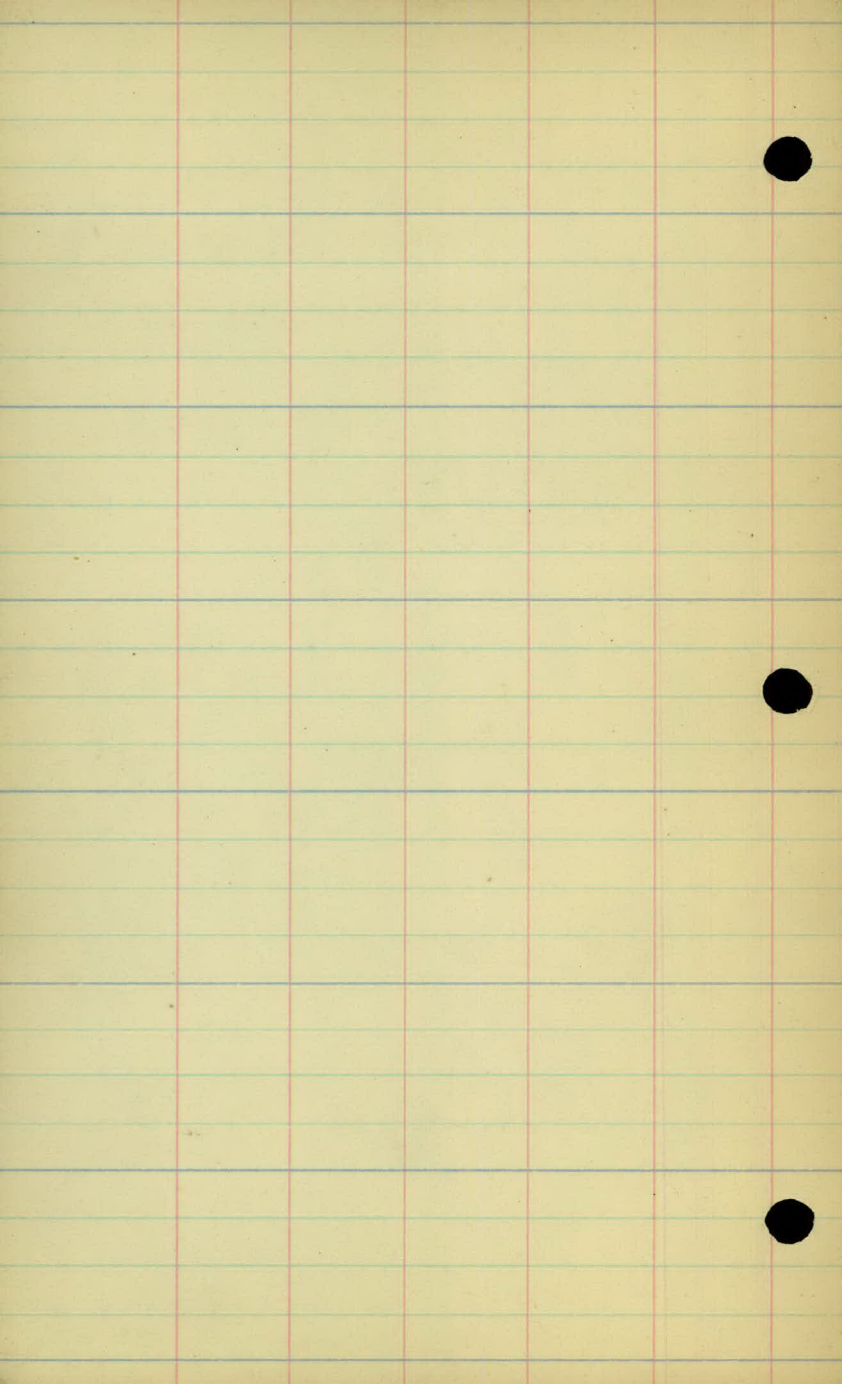
+72 T.P. 14.5'

+50 P.P. 24.5 ft

133

+34 T.P. 14.5' R₁

152+00



448 P.P. 25 H

Pasture.

Pasture

457 P.P 24.5

457

+ 38.7 £ Road

467 T.P. 14.5 Rf.

+38.7¢ Drive

465 T. P. 14' R4.

429 R.P. 24.5 hr

Meadow. hand.

Meadow land.

+ 31 T. P. 14' R.

431 P.P. 24.5 Lt.

139

50

5.0

"L" line

153

452 T.P. 16.5 R.

152

+34 R.P. 25.5 ft

456 T.P. 15.5 R.

151

Meadow land

Meadow land

+06 T.P. 15 R.

150

+60 R.P. 34 ft.
+50 R.P. 25 ft.

+49

149

+96 Power line X 109

+72 T.P. 13.5 R.

+45 Power line
Tower 37.5 R.

+12 R.P. 25.5 ft.

+39

148

+68 T.P. 14.5 R.

Pasture.

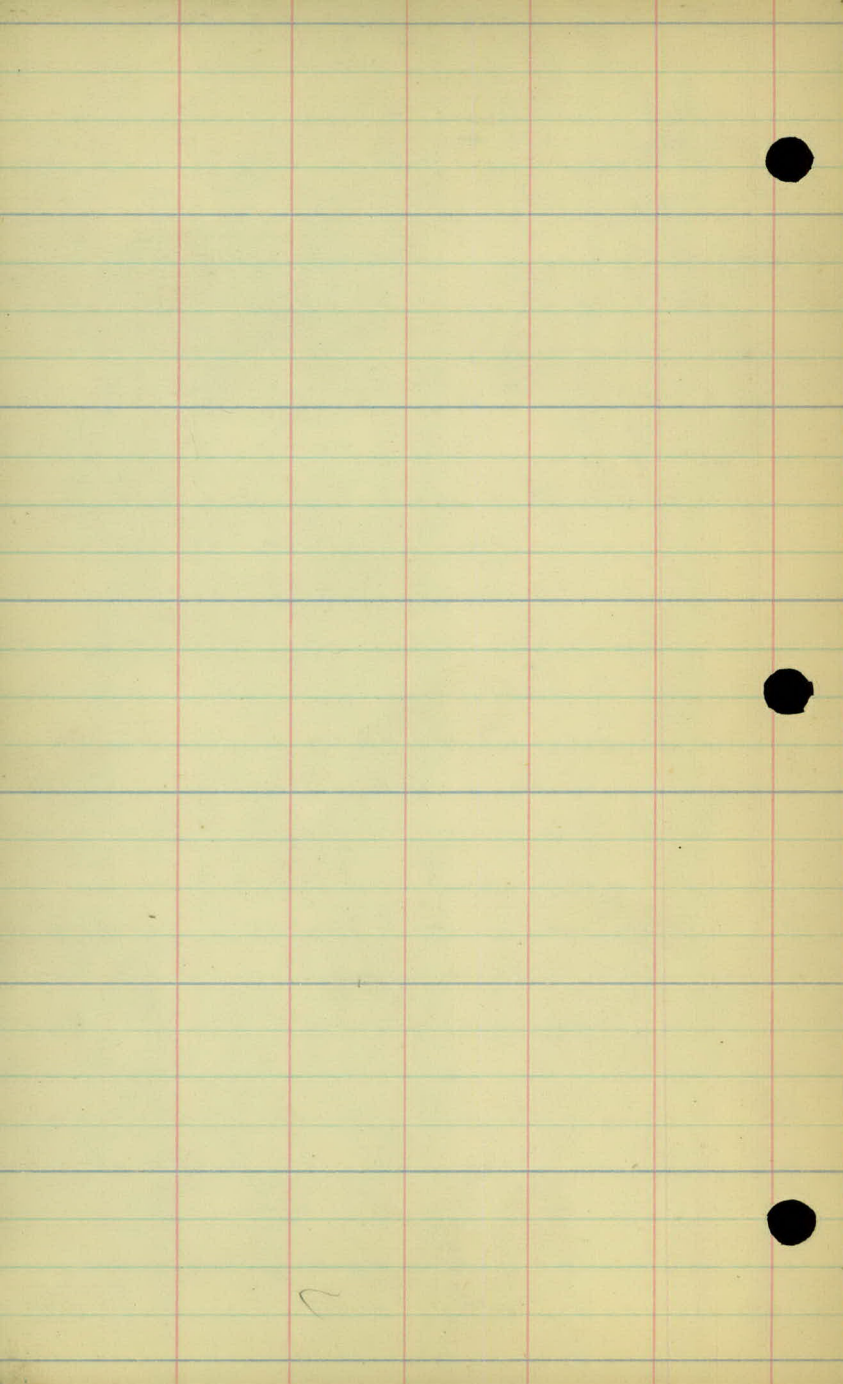
Pasture

147

+32 R.P. 25 ft.

+36 T.P. 14 R.

146



"L" line

155 32.5

160

169 Form. E

165 32.0

159

+83 T.P. 22.5 R.

+49 P.P. 23.8 Lt.

175 31.5

158

+57 T.P. 20.8 R.

180 31.0

157

+73 P.P. 24.1

Cultivated

Hill Farm

+31 T.P. 19.5 R.

170 30.5

156

175 25.5

+95 P.P. 25.5 Lt.

+02 T.P. 18.5 R.

155

Meadow land

Meadow land

137 30

154

+81 T.P. 17.5 R.

+18 P.P. 25.5

153

0.0

3.0

1.0

0.2

0.0

"L" line

167

16° 36.2

Cultivated

+24 T.P. 27.5

166

18° 36°

+78 R.P. 21.9 Lt.

17.7 358

+105 T.P. 27.3 Rt.

165

+50 — x x x — 18.5 — 450

16A+00 P.D.T.

+84 R.P. 21.5 Lt.

18.5 348

+26.5 31.75

+61 T.P. 26.0 Rt.

164

Hill Farm.

16' 45

163

+56 T.P. 25.0 Rt.

14.8 33.7

+91 R.P. 22.3 Lt.

Cultivated

+29 T.P. 23.9

162

14.6 32.9

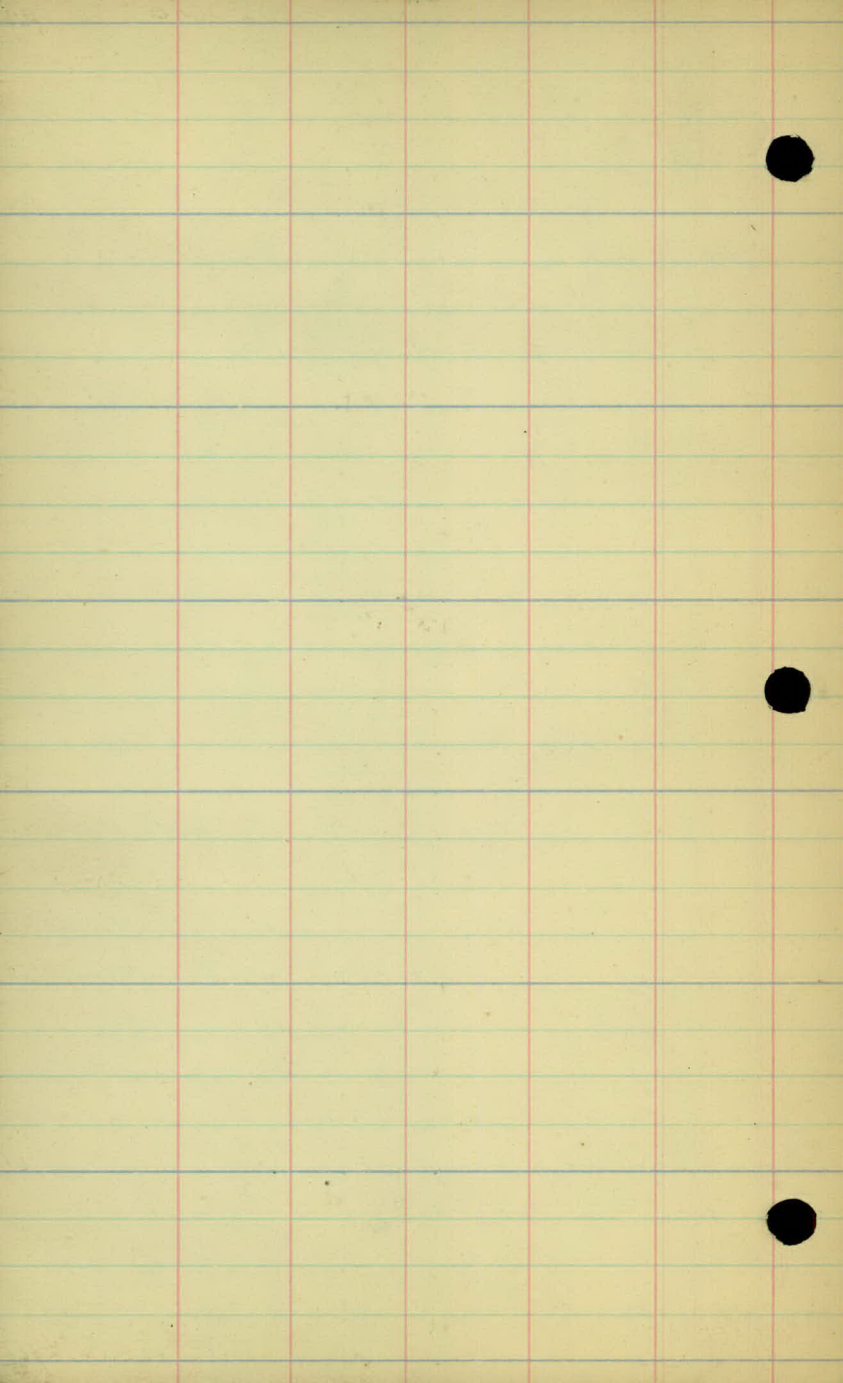
161

+19 R.P. 22.5 Lt.

15.5 32.5

+105 T.P. 23.5 Rt.

160



+72 PP-19.1 Lt.

CULT.

+70 Fence Cor-13.7 Lt.

+78 PP-18.2 Lt.

+92 Driveway + Gate

+76 PP-19.5 L

+42 Cor. Ho. 48.7 L.

+28 FC-13' L.

+54 End Fc.

+76 PP-20.0 L

354

361

363

138

368

110

370

175

365

145

135

362

16

362

1" LINE

+83 TP-28.0 R.

+59 TP-28.6 R.

CULT.

+30 TP-28.8 R.

+02 TP-28.0 R.

CULT.

+79 TP-28.9 R.

+50 TP-28.0 R.

174

173

172

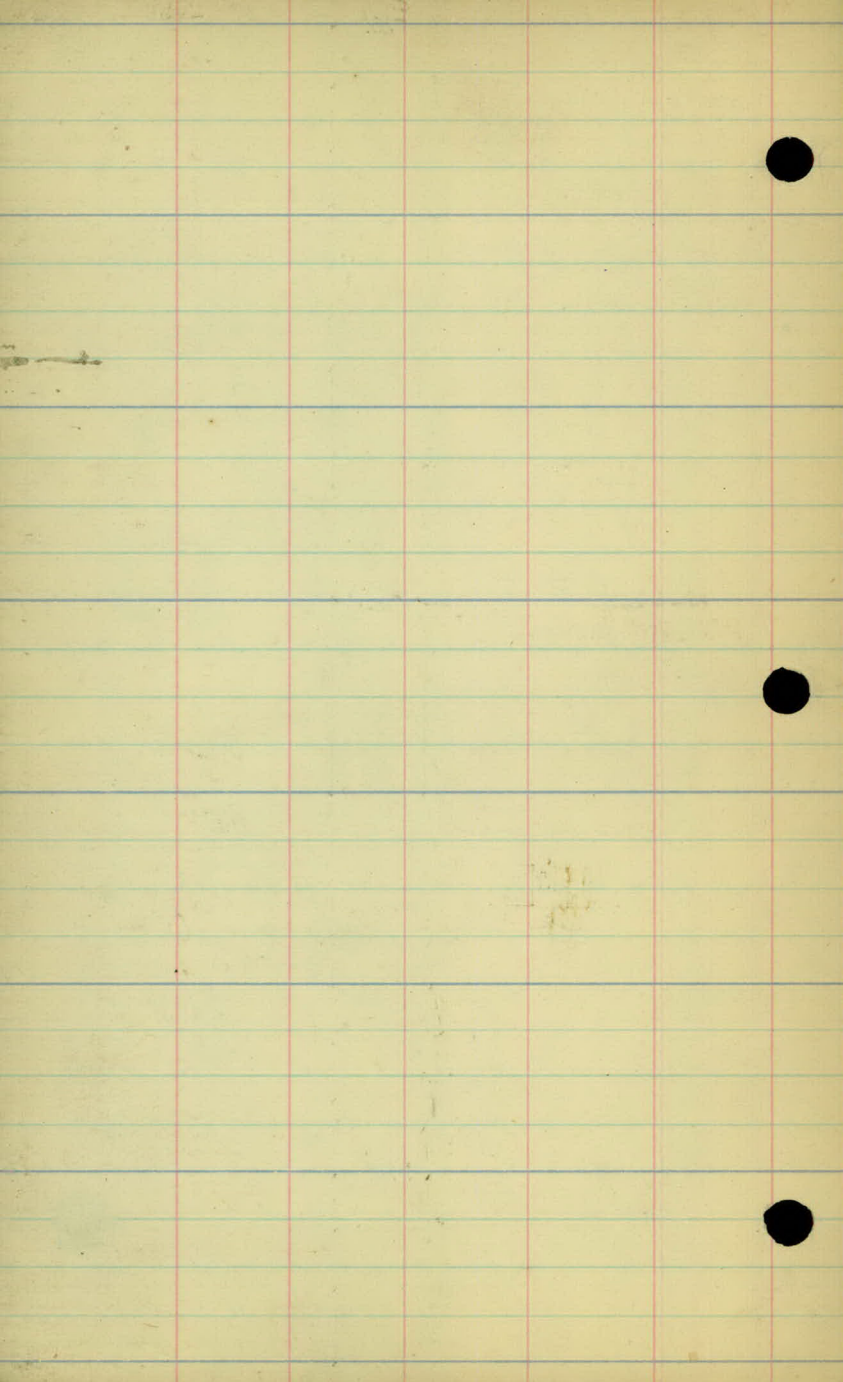
171

170

169

168

167



+95 Tree-42'
+00 Rd-5'R.
+77² IRON POT.

Est. N 1/4 Cor. Sec. 5

Rd-5'R
+56 PR-17.7L

CULT.
Rd.
178+80.5 POT.

+00 Rd.

+64 PR-18.6L.

CULT.

+71 PR-19.0L

33
5/35.0-67.4

LINE.
181+40 T.P-27'R.

181

+15 T.P. 27.5'R

180

33

42 F.R.
Const. Road (Not Used)
+91 T.P. 28.1'R
46.05 F.R.

179

33.2

178

+64 T.P. 28.2'R.

+16-12" C.M.-19'g.
N.E. 1/4-25'R

177

CULT.

+58 T.P. 27.8'R.

33.4

34.1

176

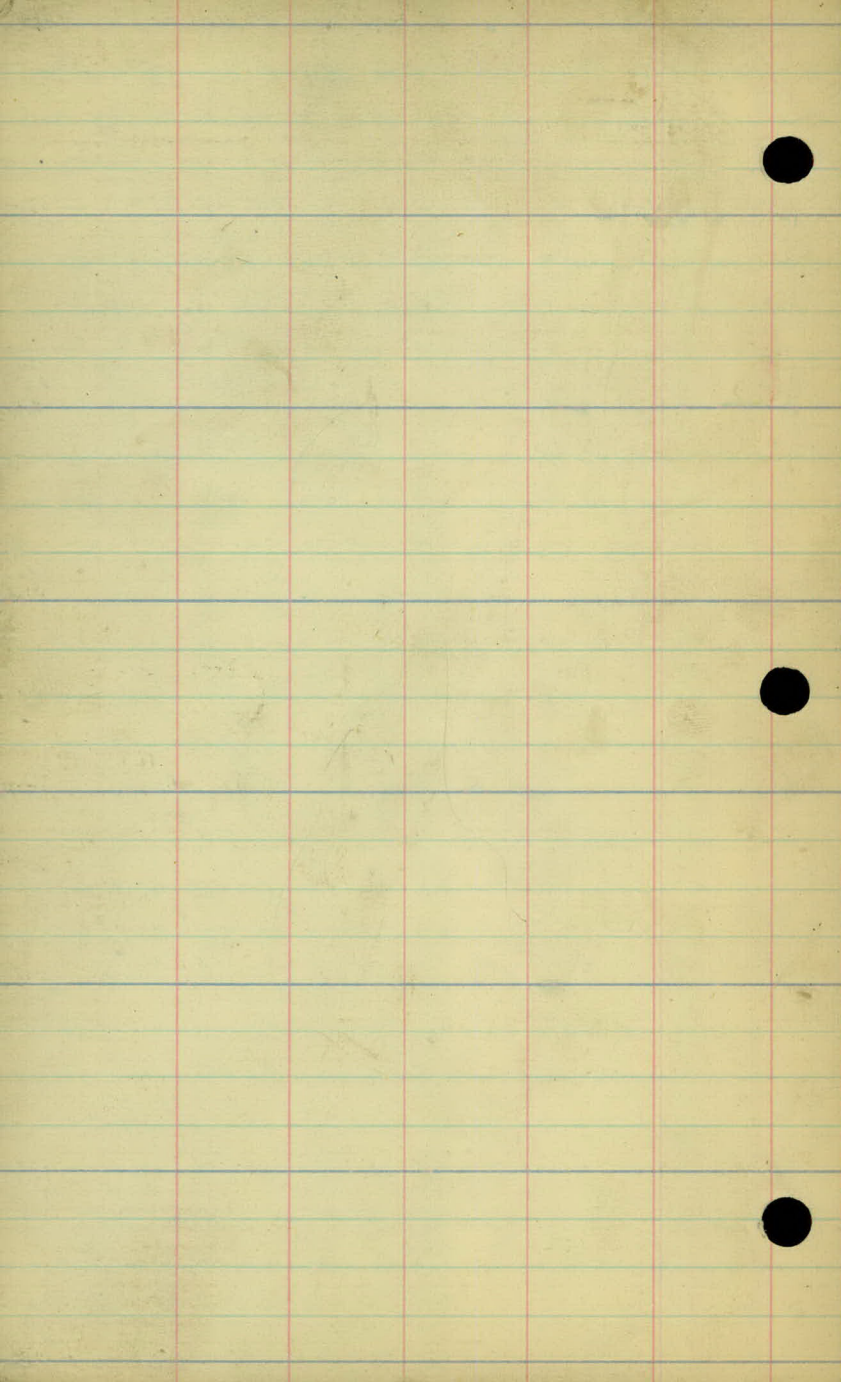
34.7

+11 T.P. 27.8'R.

175

35.4

174



± Rd-2'L

E 30.7

"L" LINE

188

+34-PP-15.5'L

+67 T.P. 26'R

± Rd-2'L

30.8

187

+48 T.P. 26'R.

± Rd-4'L

31.4

186

+50 PP-15.8'L

± Rd-3'L

32'

185

+18 T.P. 27'R.

CULT.

CULT.

32

± Rd-2'R

184

+92 T.P. 27R

+57 P.P. 16.0'L

32.3

± Rd-6'R

183

+67 T.P. 27'R.

+80 End Fc. 8.3'L

32.3

± Rd-8'R

182

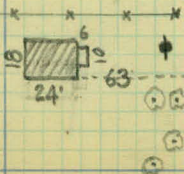
+61 PP-15'L

+48-Cor. School
SW. Cor. 63'L

+40 T.P. 27'R.

± Rd-5'R

181



Z ←

£

30.95° F.P.

10°C.
Δ 38005" L.

194+138

1498.0

52.05

192+158 P.C.

3+80.8

• F.P.

EQUATION 195+96.6 P.T. = 193+79.4

+100 Rd-12'R.

+97 I.P. 48'R + Fc 195
+82 P.P. 55'R

+50 $\frac{1}{2}$ Rd-39'R.
+50 Fc-83.5'R

+92 P.P. 17.5'R
+82 Rd-34'R + Fc-63' 194
+90 T.P. 51'R

+50 $\frac{1}{2}$ Rd-21' + Fc-46'

+15 $\frac{1}{2}$ Gate-16' W
+82 Rd-13.5'R + Fc-35.5' 193
+80 T.P. 28'R

+50 Fc-30.5'R

+16 $\frac{1}{2}$ Rd-7'R.
+16 Fc-29.5'R 192

+59 T.P. 24'R

+30 Fc-29.5'R.

+82 Rd-3'R. 191
+100 Fc-29.5'R

+18 T.P. 25.5'R
+100 Fc-30.5'R 190

$\frac{1}{2}$ Rd.

CULT.

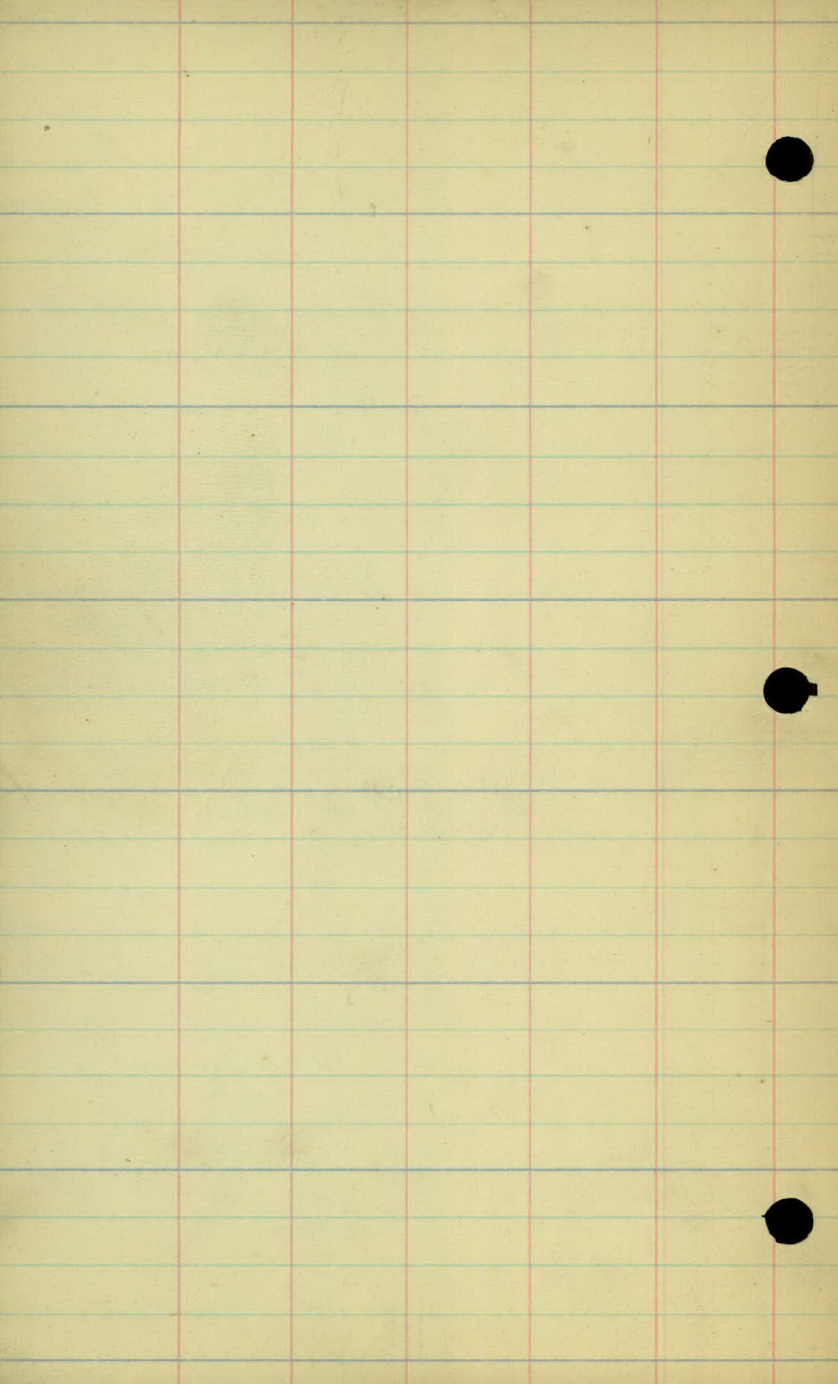
CULT.

+34 P.P. 15'L

$\frac{1}{2}$ Rd 2'L.

Fc-30.5'R 189
+90 T.P. 25.5'R.

Fc-30.7'R. 188



"L" LINE

202

33

33

201

33

200

33

199

345

198

345

197

34

196

EQUATION

$$195 + 96.5 RT = 195 + 79.9$$

+56 { T.P. 48%
ERD-62

+10 ERD

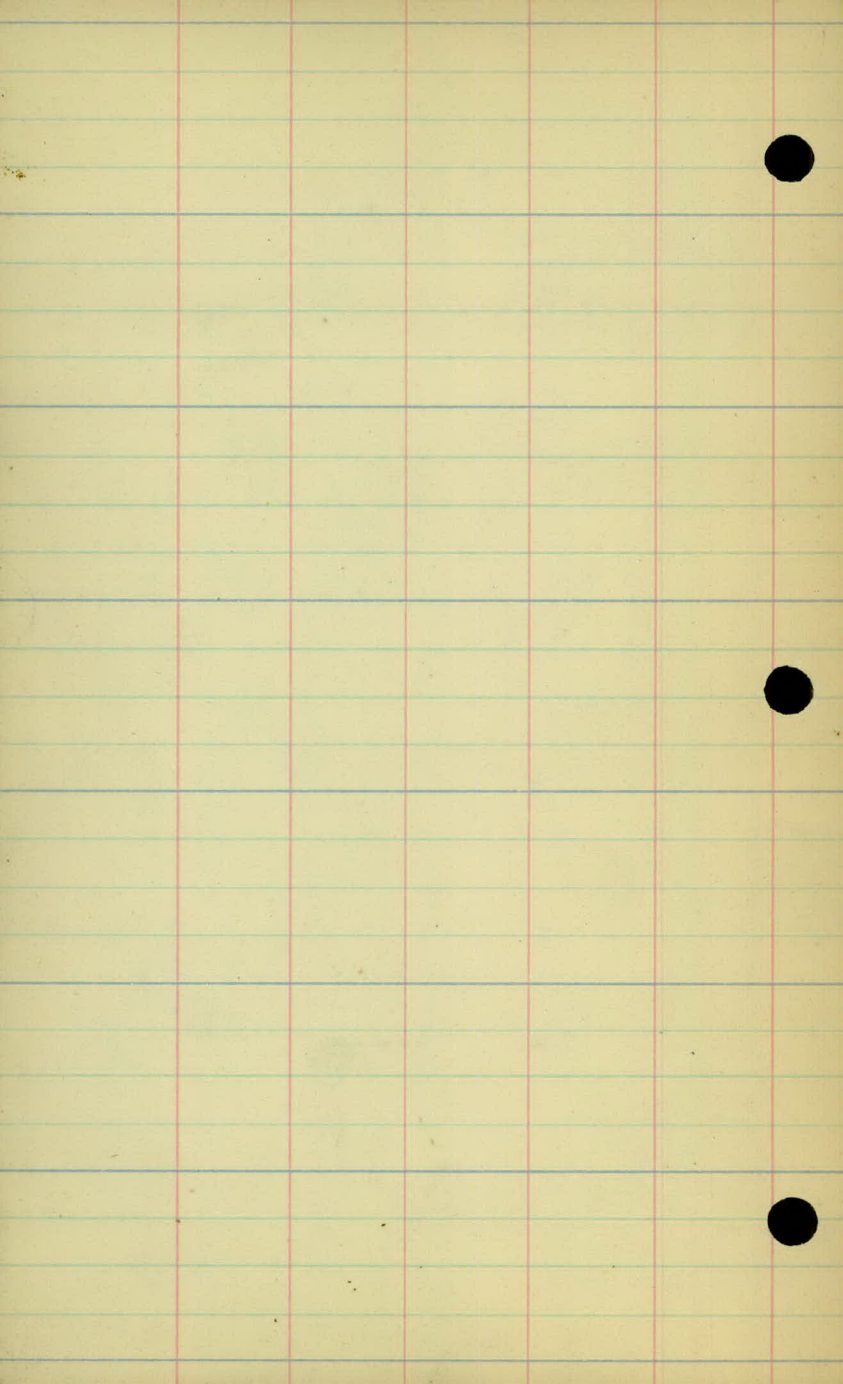
Cultivated land

SWAMP & MEADOW

+965 345 R.

+50 FC-395 R.

195



209

50

208

50

207

50

Ritch

206

51

205

55

Postage

204

54.5

+66.5 Fence Xing
+60

+38 F.E

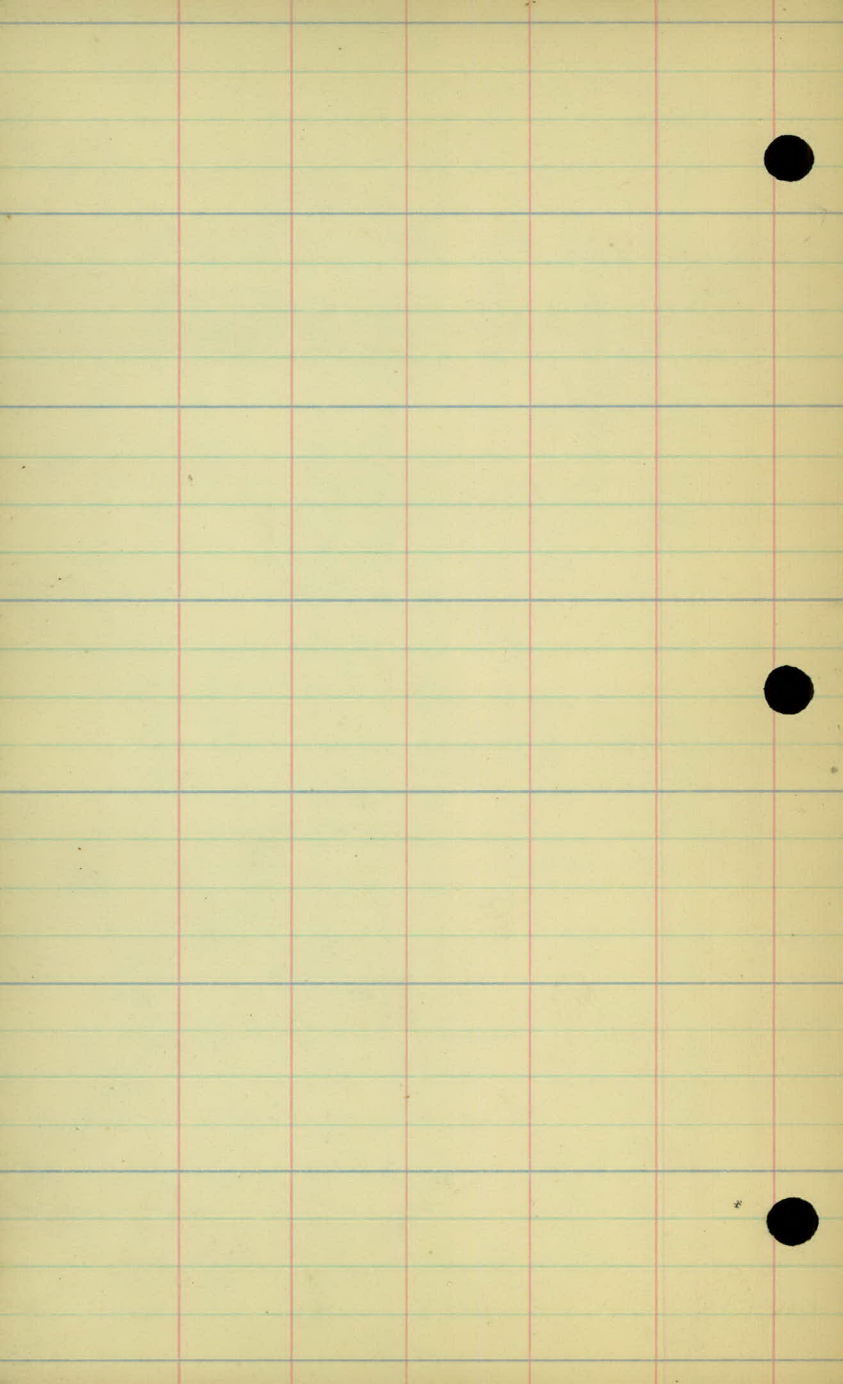
203

33

cultivated

202

33



216

215

21st

213

212

211

210

209

Cultivated hand

+85 Fence Lin. g

+75 cattle Road

52.3

best

130.

50

2

...

11

+73 Fonce Xing

145L

425

Res. 2

22

30

42

67

223+00 { ϕ Rd-10
Fc-37.5

+50 Fc. Cor.
+42 TP-27.5L

+21 Cor. Barn-61'L

222+00 { Fc 35.5L
G.Rd 10.5L

Conc. Silo

21 Barn

14'

22'

P.R.B 2/9/25
+96 Cor Fc-9'R
+88 ϕ 16' Gate

+100 Fc-9'R

221+00 { ϕ Rd 11'L
Fc-35'L

+100 Fc-9'R

+54 TP-27'L

PT+00.8 ϕ Rd 8'L
220 Fc-33.5

+00.8 Fc-9'R

219+00 Fc. { ϕ Rd-11'L
Fc-38'L

+100 Fc-6'R.

+57 TP-21'L
+55 Fc-41'L
G.Rd-16'L

+55 Fc. Cor-2'R

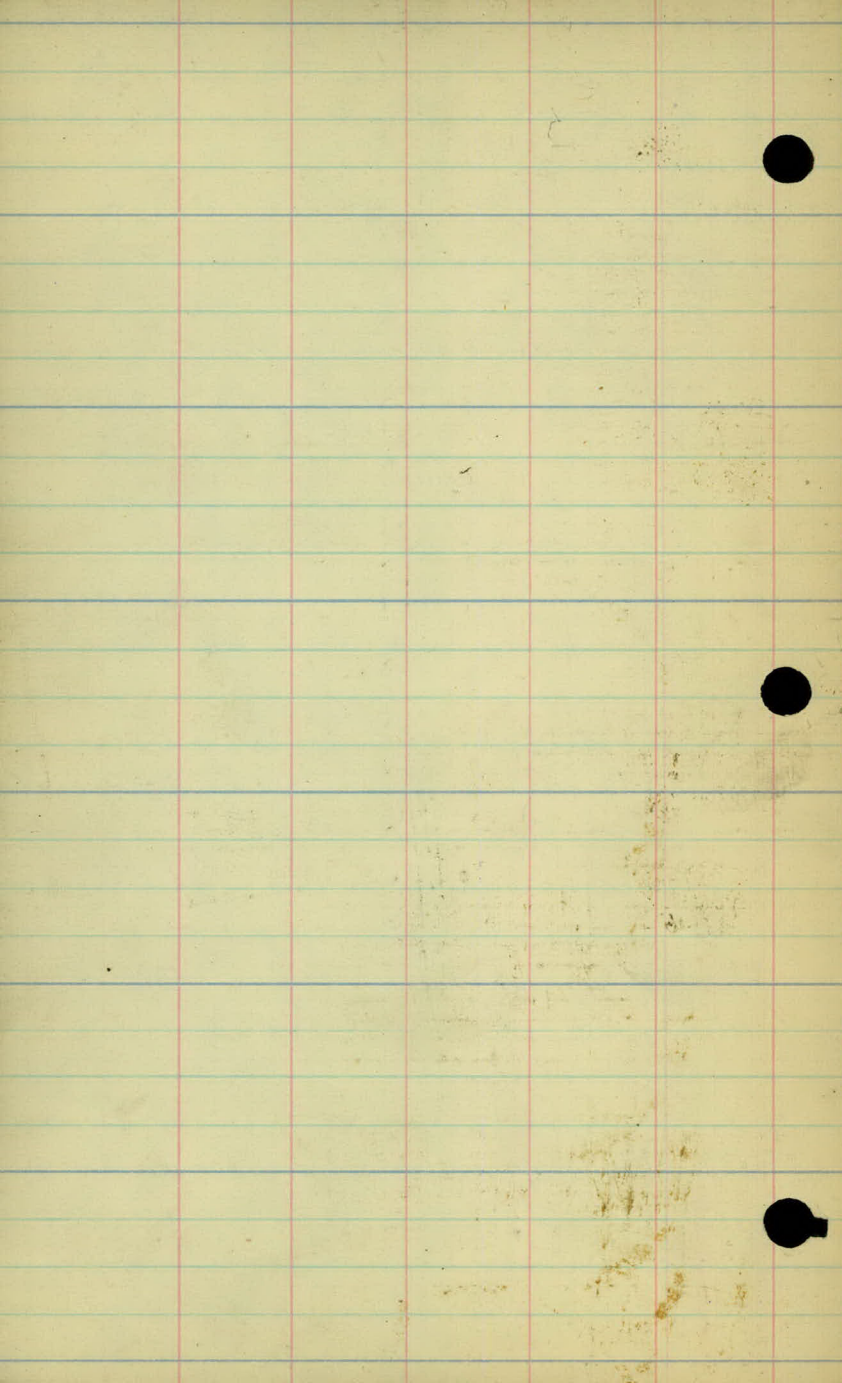
218+00 { Fc-48
G.Rd-22

Fc N+S.

217+00 { Fc-72
G.Rd-42

+69 TP-61'L

216+00 { Fc-98
G.Rd-67



230+00

PRB-29-25

+56 TP-TP-30'L

+108 CULV

12" Cor. 1P-22"lg.

229+00 $\frac{1}{2}$ Rd.

PASTURE

228+00 $\frac{1}{2}$ Rd.

+89 TP-30'L

CULT.

227+00 $\frac{1}{2}$ Rd. 3'L

+103 TP-30'L

226+00 $\frac{1}{2}$ Rd. 6.5'L

CULT.

+13 End Trees-41'L

225+00 $\frac{1}{2}$ Rd-10'L

Trees 41'L

+114 TP-28.5'L

224+00 $\frac{1}{2}$ Rd-10'L

Cor Ho+90-75'L

+83 $\frac{1}{2}$ Drive-L

+70 End Fc. 37.5'L

+59 Cor. Shad Apph.

+05 $\frac{1}{2}$ 16' Gate L

223+00

HO.

95'

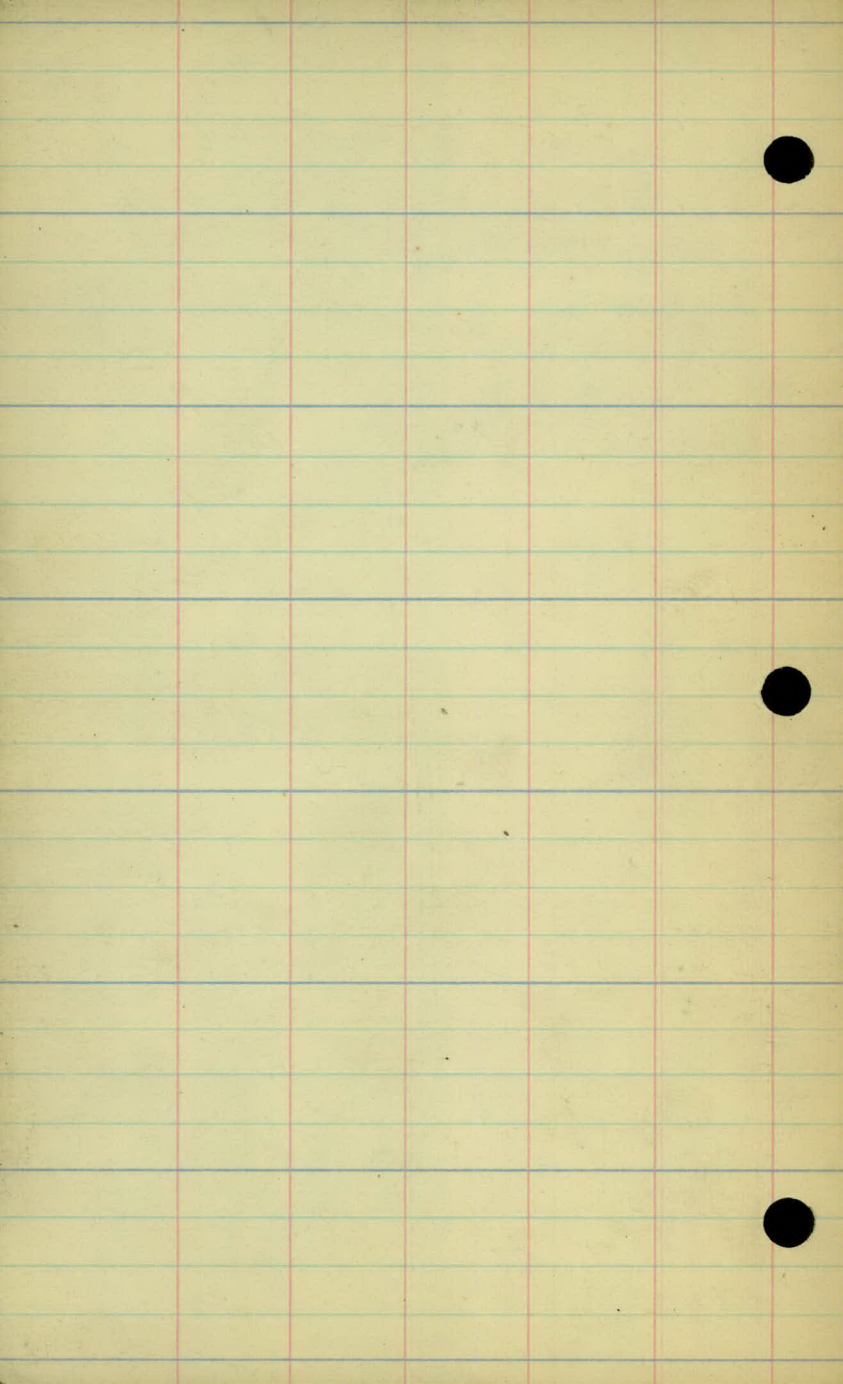
28.5'

14'

CULT. FIELD.

+13 FC-21.5R-N+5

CULT. FIELD



L. Line.

234

233

+85 F. Ent. 11
 +76 T. 44 L.
 +59 T. 24 L.
 +50 T. 46 L.
 +39 T. 47 L.
 +22 T. 50 L.
 +16 T. 20 R.
 Rd. 13 L.

Farm Yard

+76 F. Cor. 33 N.
 +62 T. 20 N.
 +50 F. 30 N.

F. 19 N. 232

+50 Rd. 32 L.
 +32 T. 14 L.
 +10 Rd. 64 L.
 +17 T. 215 L.
 F. 10 L.
 +92 T. 5 L.
 +
 +64 P.P. 68 L.
 +50 Rd. 23 L.

+72 T. 8 N.
 +54 F.

231

+84 F.

+50 F. Cor. 16 N.

230

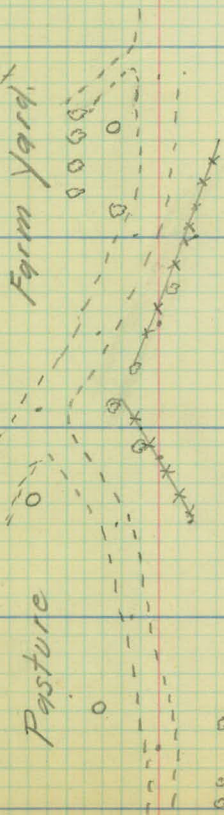
Rd. 7 L.

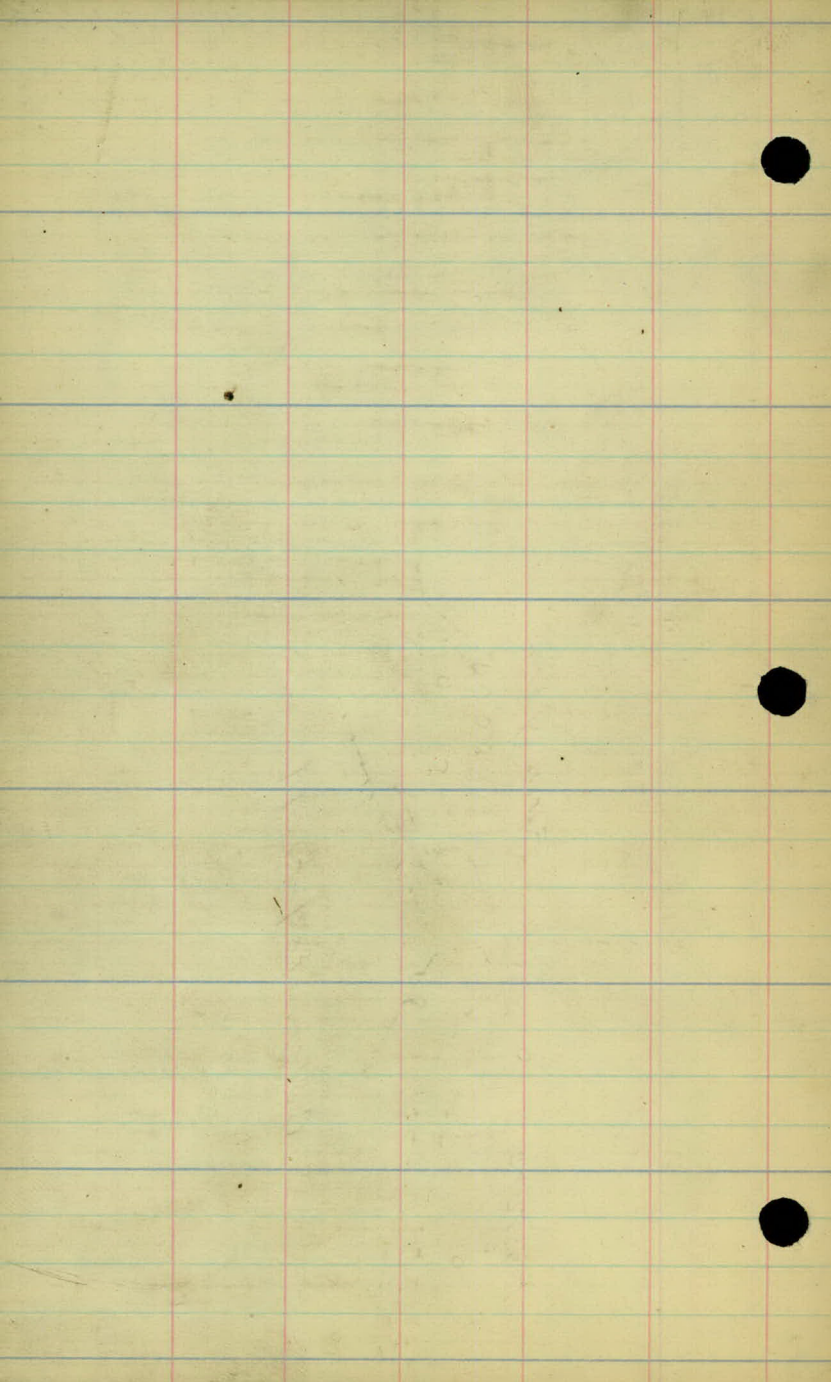
Pasture

+50 P.P. 315 L.

229

Cultivated field





L. line

Center line levels on
L. line from Sta. 0+00 to
End of Proj.

Sta.	+	H.I.	-	Rod.	Elev.
B.M.	3.16	715.43		712.27	
- 3+00				7.7	907.7.
- 2+00				6.8	908.4.
- 1+00				6.2	909.2.
- 0+50				5.5	909.9.
0+00	Center of Hodgson Rd.			4.6	910.8.
0+50				5.5	909.9.
01				6.1	909.3.
+50				6.8	908.4.
02				7.4	908.0.
+50				8.2	907.2.
03				9.1	906.3.
+50				9.7	905.7.
T.P.	1.93	907.55	7.81	905.62	
04				2.3	905.3.
+50				3.0	904.4.
05				3.9	903.7.
+50				4.9	902.7.
06				6.3	901.3.
+50				7.0	900.4.
07				7.3	900.3.
+50				7.4	900.2.
08				7.1	900.5.
T.I.	5.53	905.47	7.61	899.94	
+50				5.2	900.3.
09				5.2	900.3.
+50				4.9	900.4.

2/3/25.

On top of conc. step. N.E. Cor. of school House:

<u>5.0</u>	<u>4.7</u>	<u>5.0</u>	<u>5.0</u>	<u>4.9</u>	<u>4.5</u>	<u>3.4</u>	<u>2.4</u>
100	100	100	50	50	100	100	300

Sta.	+	H.I.	-	Red.	Elev.
		705.47 ✓			
10				4.3	901.2.
	+50			4.4	900.9.
11				5.1	900.4.
	+50			4.9	900.4.
12				4.7	900.8.
	+50			3.4	901.9.
13				2.4	902.9.
	+50			2.4	903.1.
14				1.7	903.8.
	+50			1.5	904.0.
15				0.9 ✓	904.4.
T.P.	7.58	712.01 ✓	0.84	904.43	
	+50			6.9	905.1.
16				6.3	905.7.
	+50			5.5	904.5.
B.M.				4.08	907.93 ✓
17				5.3	906.7.
	+50			5.0	907.0.
18				4.7	907.3.
	+50			4.5	907.5.
19				4.3	907.7.
	+50			3.9	908.1.
20				3.9	908.1.
	+39			3.5	908.5.
	+50			1.7 ✓	910.3.
T.P.	7.71	919.44 ✓	2.24	909.75 ✓	

2/3/25

Spk. in 24" Oak. 30' Rt. Sta. 16 + 85.

Sta.	+	H.I. 719.44	-	Red.	Elev.
	+40			5.8	913.7.
21				4.7	914.8.
	+31			4.7	914.8.
	+40			7.6	911.9.
	+50			7.9	911.6.
22				4.2	913.3.
	+50			5.0	914.5.
	+66			5.2	914.3.
23				3.0	916.5.
	+35			1.4	918.1.
	+50			1.5	918.0.
24				1.8	917.7.
	+50			1.9	917.6.
25				2.9	916.6.
	+50			3.9	915.4. 915.6
26				3.9	915.4.
T.P.	4.07	919.95	3.58	915.88	
	+50			4.1	915.9.
27				4.4	915.6.
	+50			5.7	914.3.
28				5.6	914.4.
	+50			4.6	915.4.
29				4.5	915.5.
	+50			4.3	915.7.
B.M.				3.97	915.98✓
30				6.6	913.4.

2/3/25

spk. in T.P.W. Sta. 19 + 35.

Sta.	+	H.I. ✓	-	Rod.	Elev.
		919.95			
	+50			8.4	911.4.
	+80			10.3	909.7.
31				10.8	909.2.
	+50			9.4	910.4.
32.				7.7	912.3.
	+51			6.0	914.0.
33				4.2	915.8.
	+38			3.5	916.5.
	+50			5.3	914.7.
T.P.	3.58	919.70 ✓	4.43	915.52 ✓	
34				4.1	915.0.
	+50			3.8	915.3.
	+90			4.0	915.1.
35				4.0	915.1.
	+50			4.2	914.9.
36				4.2	914.9.
	+50			4.2	914.9.
37				4.6	914.5.
	+50			4.8	914.3.
38				5.5	913.4.
	+50			5.9	913.2.
39				6.8	912.3.
	+50			7.4	911.5.
40				8.4	910.7.
T.P.	0.88	911.34 ✓	8.64	910.44 ✓	
	+50			1.9	909.5.

1/3/25

Sta.	+	H.I. ✓ 911.54	-	Rod.	Elev.
41				2.8	908.5
	+50			3.4	907.9
42				4.4	906.9
B.M.				4.38	906.94
	+50			5.1	906.2
43				6.2	905.1
	+50			7.0	904.3
44				7.8	903.5
	+50			8.4	902.9
45				9.0	902.3
	+57			9.4	901.7
46				10.0	901.3
T.P.	2.49	904.24 ✓	9.57	901.77 ✓	
	+38			4.0	900.3
	+50			5.9	898.4
47				5.6	898.7
	+50			4.1	900.2
48				3.6	900.7
	+25			4.1	900.2
	+50			5.1	899.2
49				8.7	895.6
	+12			6.9	897.4
	+24			5.3	899.0
	+50			5.1	899.2
50				5.0	899.3
	+50			4.8	899.5

2/3/25

Spl. in 30" Oak. 50 lb. Sta. 42 + 25.

Sta.	+	H.I.	-	Red.	E/CV.
		904.26			
51				4.9	899.4
	+50			5.1	899.2
52				5.2	899.1
	+50			5.4	899.9 898.
53				5.4	899.9 898.
T.P.	4.57	903.43	5.40	898.86	
	+50			4.3	899.1
54				4.4	899.0
	+50			4.3	899.1
55				4.4	899.0
	+50			4.5	899.9 898.
56				4.8	898.4
	+50			4.8	898.4
57				4.8	898.4
	+50			4.8	898.6
58				4.4	898.8
	+50			4.2	899.2
59				3.8	899.6
B.M.	4.78	906.09	4.12	899.31	
	+50			4.2	899.9
60				5.9	900.2
	+50			5.3	900.8
61				4.9	901.2
	+50			4.5	901.6
62				3.8	902.3
	+50			3.2	902.9

1/3/25

SpK. in 14" Oak. 45 Lt. 5+9, 59+30.

Sta.	+	H.I.	-	Rod	Elev.
		906.09			
63				1.5	903.4
+50				1.0	904.1
64				0.9	905.2
T.P.	10.50	915.41	0.98	905.11	
+50				9.4	906.0
65				8.7	906.9
+50				7.6	908.0
66				6.4	909.2
+50				5.5	910.1
67				4.4	911.2
+50				3.5	912.2
68				2.2	913.4
+50				1.4	914.0
T.P.	9.31	923.65	1.27	914.94	
69				8.4	915.1
+50				7.8	915.9
70				6.7	917.0
+50				6.3	917.4
71				5.5	918.2
B.M.				3.63	920.02
+50				5.1	918.4
72				5.3	918.4
+50				5.3	918.4
73				5.8	917.9
+50				6.4	917.3
74				4.8	917.9

912.1

916.9

2/4/25

spk. in 24" Oqk. 30 ft. sta. 70 + 70.

Sta.	+	H.I. ✓ 923.45	-	Red.	Elev.
+50				7.5 ✓	914.2
T.P.	3.08	919.43 ✓	7.30	916.35	
75				3.8	915.6
+50				4.2	915.2
76				4.3	915.1
+50				4.5	914.9
77				4.8	914.4
+50				4.8	914.4
78				4.8	914.4
+50				4.6	914.8
79				4.4	915.0
+50				4.4	915.0
80				4.2	915.2
+50				4.1 ✓	915.3
T.P.	1.30	916.82 ✓	3.91	915.51	
81				1.8	915.0
+50				2.9	913.9
82				4.2	912.6
+50				5.3	911.5
83				4.4	910.2
B.M.				0.58	916.24 ✓
+50				7.3	909.5
84				8.3	908.5
+50				9.0	907.8
85				10.3	906.5
+50				11.9	914.9 904.9

2/4/25

Spk. in T.P. 40' Lt. Sta. 83+00.

Stg.	+	H.I. ✓	-	Red.	Elev.
		916.82 ✓			
T.P.	0.55	906.20 ✓	11.17	905.65 ✓	
86				2.7	902.5 ✓ 903.5
	+50			3.9	902.3.
87				4.9	901.3.
	+50			5.7	900.5.
88				5.5	900.7.
	+50			5.5	900.7.
89				5.4	900.8.
	+50			5.1	901.1.
90				4.9 ✓	901.3.
T.P.	7.33	908.53 ✓	5.00	901.20	
	+50			7.0	901.5.
91				6.5	902.0.
	+50			6.0	902.5.
92				5.8	902.7.
	+50			5.4	903.1.
93				5.0	903.5.
	+50			4.4	904.1.
94				3.9	904.6.
	+50			3.4	905.1.
95				2.8	905.7.
	+50			2.4	906.1.
96				2.0 ✓	906.5.
T.P.	4.25	912.94 ✓	1.84	906.69	
B.M.				2.83	910.11 ✓
	+50			6.0	906.9.

2/4/25

Spk. in 10" Oak. 40' Rt. Sta. 96 + 40

Sta.	+	H.I. / 712.94	-	Rod	Elev.
97				4.2	904.7.
+40				6.6	906.3.
+45				4.1	908.8.
+50				4.0	908.9.
98				4.1	908.8.
+50				5.5	907.4.
99				7.0	905.9.
+50				7.1	905.8.
+63				7.1	905.8.
+67				8.3	904.6.
100				7.3	905.4.
+50				6.8	906.1.
+72				6.8	906.1.
101				6.7	906.2.
+50				6.5	906.4.
102				4.7	906.2.
T.P.	8.44	914.94	4.44	906.30	
+50				8.7	906.3.
103				8.5	906.5.
+50				7.8	907.2.
104				6.8	908.2.
+50				5.5	909.5.
105				3.7	911.3.
+50				2.0	913.0.
106				0.6	914.4.
T.P.	10.14	924.48	0.44	914.32	

2/4/25

S+g.	+	H.I. / 724.48	-	Red.	Elev
+50				8.9	915.4
107				7.6	914.9
+50				4.1	918.4
108				4.4	919.9
+50				2.8	921.7
109				1.2	923.3
+50				0.3	924.2
T.P.	3.79	728.18	0.29	924.19	
110				3.5	924.7
+50				3.2	925.0
111				3.2	925.0
B.M.				2.51	925.67
+50				3.7	924.3
112				5.3	922.9
+50				6.4	921.8
113				7.8	920.4
+50				7.2	919.0
114				10.6	917.6
+50				11.7	916.5
T.P.	0.59	917.14	11.63	916.55	
115				2.0	915.1
+50				3.9	914.2
116				4.2	914.9
+50				4.9	912.2
117				5.9	911.2
+50				6.5	910.6

912.8

2/9/25

Spl. in 50" Daff. 40' Lt. Sta. 111 + 10.

Sta.	+	H.I. ✓ 917.14	-	Red.	Elev.
118				6.9	910.2
+50				7.3	909.8
119				7.4	909.5
+50				7.5 ✓	909.4
T.P.	3.46	913.11 ✓	7.49	909.65	
120				3.6	909.5
+50				3.9	909.2
121				4.1	909.0
+50				4.4	908.7
122				4.4	908.5
+50				4.9	908.2
123				5.2	907.9
+50				5.1	908.0
124				5.5	907.6
+50				5.8	907.3
125				6.0 ✓	907.1
B.M.	4.33	911.77 ✓	5.67	907.44	
+50				4.7	907.1
126				4.8	907.0
+50				4.7	907.1
127				5.1	906.7
+28				5.6	906.2
+33				6.9	904.9
+40				6.6	905.2
+44				5.2	906.6
+50				5.1	906.7

2/4/25

Spk. in T.P. Rt. Sta. 125+07.

Sta.	+	H.I. ✓ 911.77	-	Red.	Elev.
128				3.0	908.8
+50				1.4	910.4
129				1.5	910.3
+50				2.4	909.4
130				5.1	906.7
T.P.	1.45	908.65	4.57	907.20	
+50				1.8	906.9
131				2.4	906.1
+50				3.5	905.2
132				4.3	904.4
+50				4.7	904.0
133				4.5	904.2
+50				4.8	903.9
134				5.1	903.6
+50				5.8	902.9
135				6.4	902.3
+50				6.8	901.9
136				7.5	901.2
T.P.	6.22	907.22	7.45	901.00	
+50				6.3	900.9
137				6.2	901.0
+50				6.0	901.2
138				5.3	901.9
+50				4.9	902.3
139				4.7	902.5
+50				4.7	902.5

2/4/85

Sta.	+	H.I.	-	Red.	Elev.
		907.22 ✓			
140				4.4	902.8.
+50				4.7	902.5.
141				4.9	902.3.
+50				5.2	902.0.
142				5.2	902.0.
+38.7	Road on Lt.			4.9	902.3.
143				5.5	901.7.
+50				5.3 ✓	901.9.
B.M.	4.78	907.84 ✓	4.14	903.06	
144				5.7	902.1.
+50				5.4	902.4.
145				4.2	903.4.
+50				2.5 ✓	905.3.
T.P.	11.13	918.51 ✓	0.44	907.38	
146				10.8 ✓	907.7.
T.P.	8.43	918.98 ✓	7.94	910.55	
+50				7.4	909.4.
147				7.4	911.4.
+50				5.6	913.4.
148				5.1	913.9.
+50				5.3	913.7.
149				4.9	914.1.
+50				4.8	914.2.
150				4.3	914.7.
+50				3.5	915.5.
151				2.4	916.6.

2/6/25

$\frac{2.7}{150}$ $\frac{4.1}{100}$ $\frac{4.8}{50}$

$\frac{4.0}{50}$ $\frac{2.7}{100}$

Farm Rd. on Rt.

SpK. in 30" Oak. 40' Rt. Sta. 143+50.

Sta.	T	H.I. ✓	-	Red. ✓	Elev.
		918.98 ✓			
T.P.	10.93	927.74 ✓	2.15	916.83 ✓	
+50				10.5	917.3.
152				9.3	918.5.
+50				7.7	920.1.
153				6.4	921.4.
+50				4.7 ✓	923.1.
B.M.	8.78	933.48 ✓	3.04	924.70 ✓	
154				7.5	926.0.
+50				4.1	927.4.
155				5.3	928.2.
+50				5.2	928.3.
156				4.9	928.6.
+50				4.7	928.8.
157				4.9	928.6.
+50				4.0	927.5.
158				7.0	926.5.
+50				6.8	926.7.
159				6.8	926.7.
+50				5.9 ✓	927.4.
T.P.	6.80	934.43 ✓	5.85	927.63	
160				4.1	928.3.
+50				5.0	929.4.
161				3.2	931.2.
+50				2.4	931.8.
162				3.2	931.2.
+50				4.5	929.9.

2/15/25

SpK. in T. P. Rt. Sta. 153+85.

Sta.	+	H.I. ✓ 934.43	-	Red.	Elev.
163				5.0	929.4.
	+50			4.6	929.8.
164				4.1	930.3.
	+50			5.4	930.8.
165				4.5	929.9.
	+50			4.3	928.1.
166				9.2 ✓	925.2.
T.P.	6.07	931.57 ✓	8.93	925.50	
	+50			4.9	924.7.
167				8.1	923.5.
	+50			8.7	922.9.
168				8.1	923.4.
	+50			7.2	924.4.
169				5.9	925.7.
B.M.				3.06	918.51 ✓
	+50			4.0	927.6.
170				3.5	928.1.
	+50			5.0	926.6.
171				4.0	925.6.
	+50			4.3	925.3.
172				6.0	925.6.
	+50			5.5 ✓	926.1.
T.P.	1.16	927.62 ✓	5.11	926.46	
173				1.7	925.9.
	+50			1.2	925.4.
174				3.9	923.7.

2/13/25

Spk. in 24" Oak. 35' Lt. Sta. 169+15.

Sta.	+	H.I.	-	Req.	Elev.
		927.42			
	+50			4.4	923.2
175				5.4	922.2
	+50			5.5	922.1
176				5.7	921.9
	+50			5.9	921.7
177				4.8	920.8
	+50			4.7	920.7
178				5.2	922.4
	+50			4.5	923.1
179				4.7	922.9
T.P.	0.70	924.44	3.88	923.74	
	+50			2.7	921.7
180				4.4	919.8
	+50			4.7	917.7
181				8.2	916.2
B.M.			8.42	916.02	
	+50			8.8	915.6
182				9.2	915.2
	+50			8.7	915.7
183				8.4	916.0
	+50			8.8	915.6
T.P.	4.62	920.22	8.84	915.60	
184				4.7	915.5
	+50			4.4	915.6
185				4.9	915.3
	+50			4.7	915.3

2/13/25

SpK. in 18" Flm. 35' Lt. Sta. 181 + 35.

Sta.	+	H.I.	-	Rod.	Elev.
		920.22			
186				5.1	915.1
	+50			5.1	915.1
187				5.1	915.1
	+50			7.3	912.9
188				10.2	910.0
	+50			12.0	908.2
T.P.	3.97	912.80	11.39	908.83	
189				5.9	906.9
	+50			6.8	906.0
190				7.0	905.8
	+50			6.2	906.6
191				3.9	908.9
	+50			4.0	908.8
192				4.5	908.3
	+50			5.2	907.6
193				6.4	906.4
	+50			8.3	904.5
194				7.4	903.4
	+50			10.2	902.6
195				10.0	902.8
	+10	center of Road		7.5	903.3
	+50			10.4	902.4
195 + 96 ⁶ = 195 + 79 ⁴				12.3	900.5
B.M.	3.44	905.77	10.47	902.33	
196				5.4	900.2
	+50			5.3	900.3

900.5

2/7/25

$$\begin{array}{r} 6.4 \\ 100. \end{array} \quad \begin{array}{r} 8.5 \\ 50 \end{array}$$

SpK. in 12" O.K. 60 Rt. Stg. 194 + 65.

Sta.	T	H.T. ✓	-	Red.	Elev.
		905.79			
197				5.0	900.8.
+50				5.8	900.8 900.0
198.		✓		4.3 ✓	899.5.
T.P.	5.73	908.06	3.46	902.33	
+50				7.3	900.8.
+55 ⁵ P.O.T.				7.2	900.9.
199		✓		7.4 ✓	900.7.
T.P.	4.47	905.22	7.31	900.75	
+50				6.4	898.8.
200				7.3	897.9.
+50				6.6	898.6.
201				6.9	898.3.
+25				7.2	898.0.
+50				6.3	898.9.
202				5.5	899.7.
+50				4.9	900.3.
203				5.5	899.7.
+50				6.7	898.5.
204				7.8	897.4.
+50				8.4	896.8.
205				8.6	896.6.
+50				9.1	896.1.
206		✓		9.7 ✓	895.5.
T.P.	4.84	900.71	9.35	895.87	
+50				5.5	895.2.
207				5.5	895.2.

2/9/22

Sta.	+	H.I.	-	Red.	Elev.
		900.71			
+50				5.3	895.4.
208				4.8	895.9.
+50				5.1	895.6.
209				5.0	895.7.
+59				5.2	895.5.
+61				5.7	895.0.
+48				4.2	894.5.
+71				5.4	895.3.
210				5.4	895.3.
+44				5.4	895.3.
211				5.4	895.3.
+50				4.6	896.1.
+83				1.8.	897.9.
+84				2.0	898.7.
212				0.8	899.9.
T.P.	4.13	906.23	0.61	900.10	
+50				4.1	902.1.
B.M.				5.01	901.22
213				4.2	902.0.
+50				4.9	901.3.
214				5.4	900.4.
+50				7.0	899.2.
215				7.0	899.2.
+50				5.5	900.7.
214				2.5	903.7.
T.P.	5.33	910.74	0.82	905.41	

2/7/22

Spk. in 18" Elm 60 ft. Sta. 211+90

Sta.	+	H.I. 910.74	-	Red.	E/cv
+50				3.8	906.9
+77				1.8	908.9
217				2.1	908.6
+50				3.7	907.0
218				4.5	904.2
+50				8.8	901.9
219				7.1	903.6
+50				4.2	904.5
220				6.7	904.0
+50				7.5	903.2
221				6.5	904.2
T.P.	10.81	914.42	5.13	905.61	
+50				10.5	905.9
222				8.0	908.4
+50				6.6	909.8
223				6.0	910.4
+50				5.8	910.6
224				5.1	911.3
B.M.				3.01	913.41
+50				4.5	911.9
225				3.2	913.2
+50				0.8	915.4
T.P.	7.82	923.53	0.71	915.71	
226				5.5	918.0
+50				4.0	919.5
227				3.8	919.7

2/9/25

On Conc. Porch S.E. Cor. H. 5+9. 224+18.

Sta.	+	H.I. ✓	-	Rod.	Elev.
		923.53			
	+50			3.9	919.4
228				4.9	918.4
	+50			5.7	917.8
229				5.7 ✓	917.8
B.M.	7.35	918.45 ✓	2.43	721.10	
	+29 ³			11.1	917.4
	+50			10.6	917.9
230				10.9	917.4
	+12			11.4	917.1
	+27			11.8	916.7
	+50			11.2	917.3
231				9.4	918.9
	+50			7.2	921.3
	+70			6.7	921.8
	+82			8.9	919.4
232				8.1	920.4
	+50			5.7	922.8
	+84 ⁹⁸	P.T		5.0	923.5
233				4.9	923.4
	+50			3.8	924.7
234				3.0	925.5
	+50			2.4	926.1
235				1.7 ✓	926.8
B.M.			7.35	921.10	

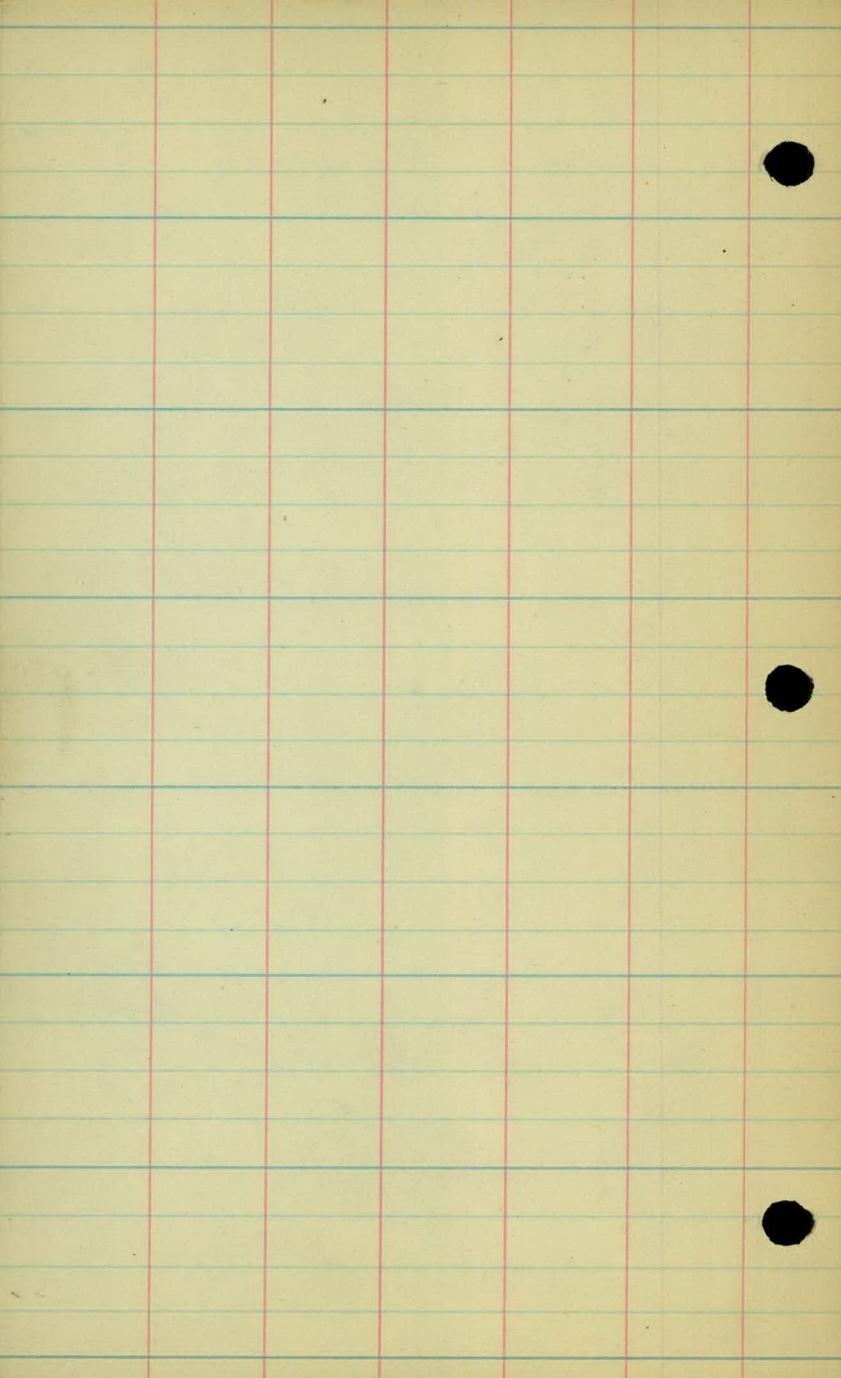
2/13/25

L. Line.

Spk. in 30" Tree N.E. Cor. of Intersection.

Q of Rd. $\frac{6.7}{13}$
Q of Rd. $\frac{5.7}{2}$

Spk. in 30" Tree N.E. Cor. of Intersection.



Levels from Lex. & Ham. to
Co. Rd. I. & Hodgson.

Sta.	t	H.I.	-	Elev.
B.M.	8.85	901.29		872.44
	9.73	910.19	0.85	900.46
	4.55	910.74	3.98	906.21
	1.53	905.41	4.88	903.88
	4.44	902.95	6.90	898.51
	4.62	902.01	6.54	896.39
	1.85	901.87	2.99	900.02

B.M.			2.60	899.27
	3.09	899.54	5.42	896.45
	8.38	903.92	4.00	895.54
	2.74	904.09	2.79	901.13
	3.29	898.24	7.12	894.95

B.M.	3.94	895.93	4.15	891.99
	4.28	895.54	6.65	889.28
	5.27	897.60	3.23	892.33
	3.18	896.25	4.53	893.07
	4.19	895.90	4.54	891.71
	6.80	898.45	4.25	891.65
	8.84	906.48	0.81	897.64
	2.08	913.54	1.00	905.48

B.M.			1.29	912.27
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2/2/25

B.M. # 61. Top of conc. base Rd. sign post
on W. side of post at Hamline & Lexington.

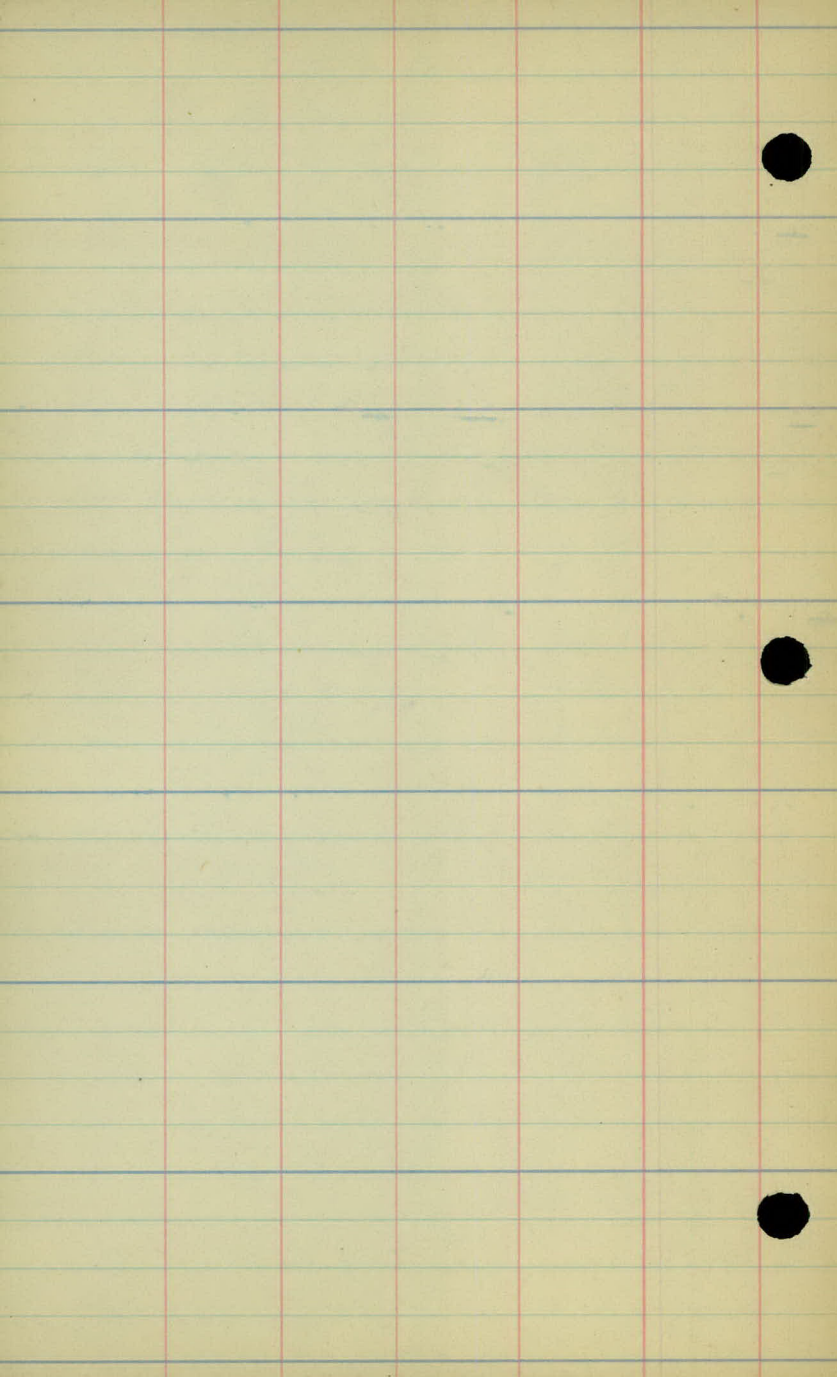
SpK. in 30" Oak 100' Lt. on 1st curve N. of Lex. & Co. Rd. I.

SpK. in T.P. S.E. Cor. of Lexington & Co. Rd. I.

School House

B.M. 

On top of conc. step N.E. Cor. of school House.



Levels from Co. Rd I. &
Hodgson to Ham. & Lex.

Sta.	+	H.I.	-	Elev.
B.M.	1.36	913.63 ✓		912.27 ✓
	1.33	906.78 ✓	8.18	905.45 ✓
	0.79	898.43 ✓	7.14	897.64 ✓
	4.40	896.05 ✓	4.78	891.65 ✓
	4.55	896.24 ✓	4.34	891.71 ✓
	4.58	897.65 ✓	3.19	893.07 ✓
	4.45	896.54 ✓	5.54	892.09 ✓
	4.44	896.54 ✓	4.42	890.12 ✓
B.M.	6.34	898.31 ✓	4.59	891.97 ✓ 891.99
	8.35	906.01 ✓	0.65	897.64 ✓
	1.78	901.58 ✓	4.21	897.80 ✓
	4.87	901.70 ✓	4.75	894.93 ✓ 894.83
B.M.	4.68	903.93 ✓	2.45	899.25 ✓ 899.27
	2.13	901.24 ✓	4.82	897.11 ✓
	5.34	905.27 ✓	3.31	897.93 ✓
	8.55	910.44 ✓	1.34	901.91 ✓
	4.49	910.54 ✓	4.41	904.05 ✓
	0.98	902.44 ✓	9.04	901.48 ✓
B.M.			10.02	892.44 ✓ 892.44

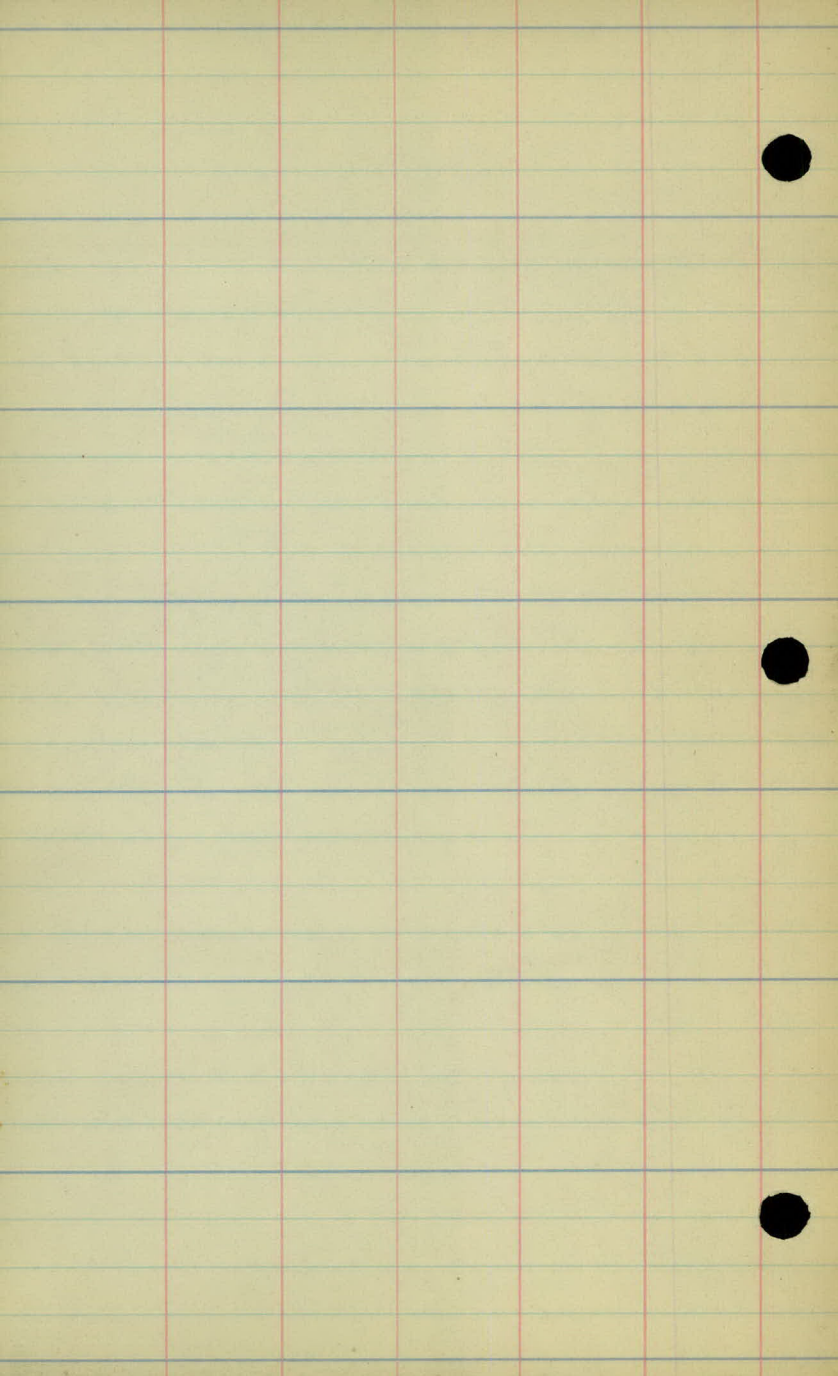
2/3/26

On top of conc. step N.E. Cor. of school house.

Spk. in T.P. S.E. Cor. of Lexington & Co. Rd. I.

Spk. in 30" Ogk. 150' H. on 1st Curve N. of Lex. & Co. Rd. I.

B.M. #41.



2/4/25

L. Line

Check Levels on L. Line
from Sta. 0+00 to end of Proj.

Sta.	+	H.I.	-	Elev.	
B.M.	1.98	914.25		912.27	
	2.03	907.84	8.42	905.83	
	4.88	905.22	7.47	900.39	
	8.12	911.81	1.58	903.69	
B.M.	4.01	911.95	3.88	907.93	907.93
	7.35	919.54	1.76	910.19	
	3.38	920.67	2.25	917.29	
B.M.	4.24	920.24	4.67	916.00	915.98
	5.03	919.85	5.42	914.82	
	0.17	912.88	7.14	912.71	
B.M.	3.38	910.34	5.90	906.98	906.96
	2.79	904.58	8.57	901.79	
	4.64	903.82	5.40	899.18	
B.M.	6.71	906.04	4.49	899.33	899.31
	10.02	915.58	0.48	905.54	
	9.25	913.58	1.25	914.33	
B.M.			3.55	910.03	910.02
	3.58	919.54	7.62	915.96	
	1.00	916.43	4.11	915.43	
B.M.			0.17	916.26	916.24
	0.37	905.65	11.15	915.28	
	6.95	908.44	4.14	901.49	
	7.44	913.71	2.17	906.27	
B.M.	3.65	913.77	3.59	910.12	910.11
	8.22	914.40	7.59	906.18	
	10.85	924.22	1.03	913.37	
	4.13	927.65	0.70	923.52	

2/5/25

On Top of conc. step N.E. Cor. of school house.

SpK. in 24" Oak. 30' Rt. Sta. 16+85.

SpK. in T.P. 65' Rt. Sta. 29+35.

SpK. in 30" Oak. 50' Lt. Sta. 42+25.

SpK. in 24" Oak. 45' Lt. Sta. 59+30.

899.53
11.44
910.97
2.56

908.21 N.E. Cor. of 1st Landing on Church steps.

SpK. in 24" Oak. 30' Lt. Sta. 70+90.

SpK. in T.P. 40' Lt. Sta. 83+00.

SpK. in 10" Oak. 40' Rt. Sta. 96+40.

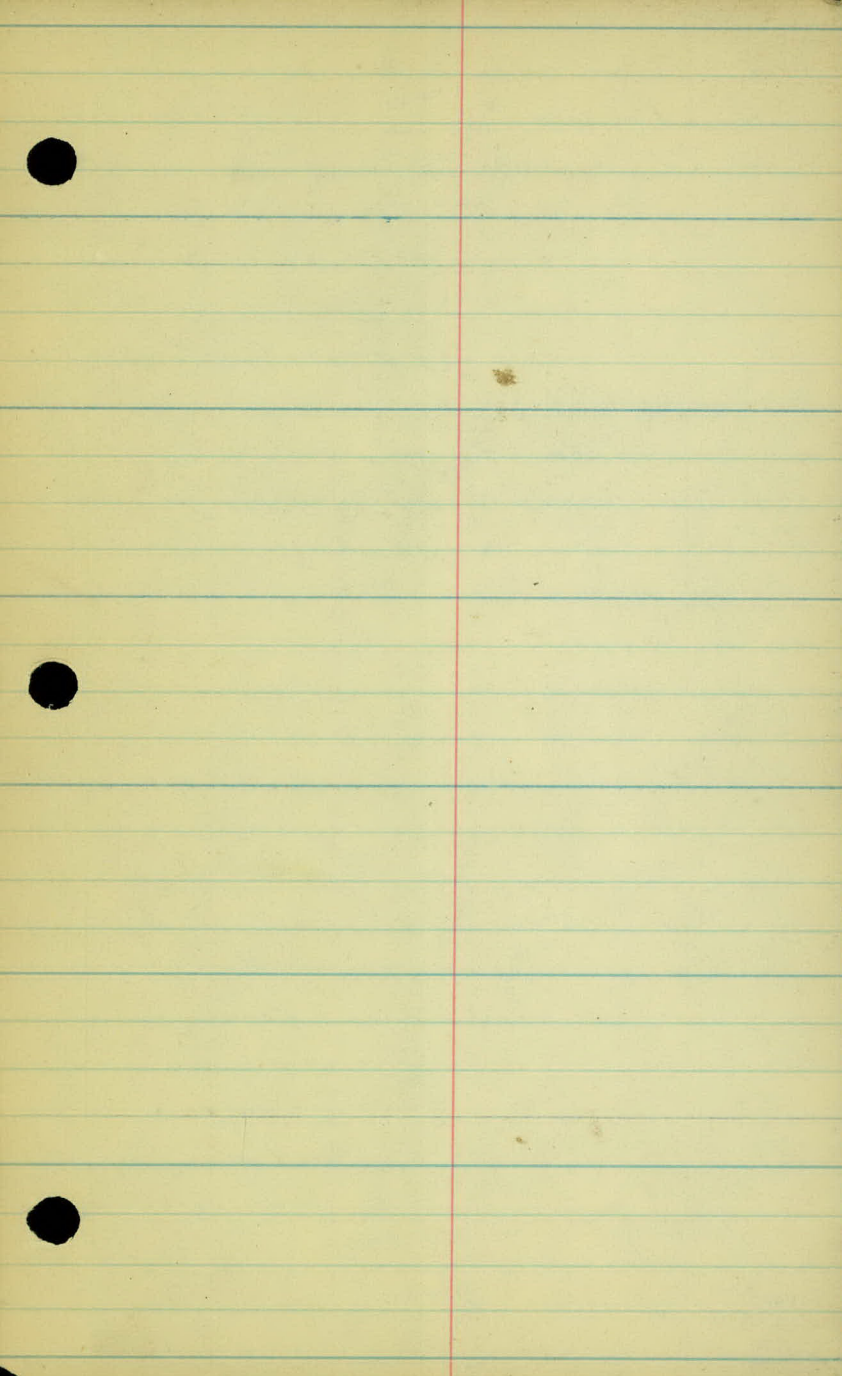
Sta.	+	H.I.	-	Elev.
		917.65		

B.M.			2.00	915.65	915.67
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	0.77	917.11	11.31	916.34	
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	3.43	913.12	7.42	909.69	
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B.M.			5.71	907.41	907.44
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Sta.	+	H.I.	-	E/cv.	
B.M.	4.63	912.07		907.44	
	2.73	908.26	6.54	905.53	
	6.50	907.53	7.23	901.03	
B.M.	4.50	907.56	4.47	903.06	903.04
	11.47	918.30	0.73	906.83	
	10.27	916.21	2.36	915.94	
B.M.	8.82	933.52	1.51	924.70	924.70
	6.17	934.31	5.38	928.14	
	4.03	931.50	6.84	927.47	
B.M.			2.97	928.53	928.51
	1.20	927.54	5.14	926.36	
	0.83	923.01	5.38	922.18	
B.M.			6.78	916.03	916.02
	4.47	920.09	2.39	915.62	
	4.10	913.81	10.38	909.71	
	3.93	906.77	10.97	902.84	
B.M.			4.45	902.32	902.33
	3.86	904.52	6.11	900.46	
	4.82	901.08	8.26	894.26	
	7.85	906.28	2.65	898.43	
B.M.			5.08	901.20	901.22
	3.88	909.51	0.65	905.63	
	8.03	916.75	0.79	918.72	
B.M.			3.34	913.39	913.41
	4.62	922.72	0.65	916.10	
B.M.			1.64	921.08	921.10

2/10/25

Spk. in T.P. Rt. Sta. 125+07.

Spk. in 30" Oak. 40' Rt. Sta. 143+50.

Spk. in T.P. 20' Rt. Sta. 153+85.

Spk. in 24" Oak. 35' Lt. Sta. 169+15.

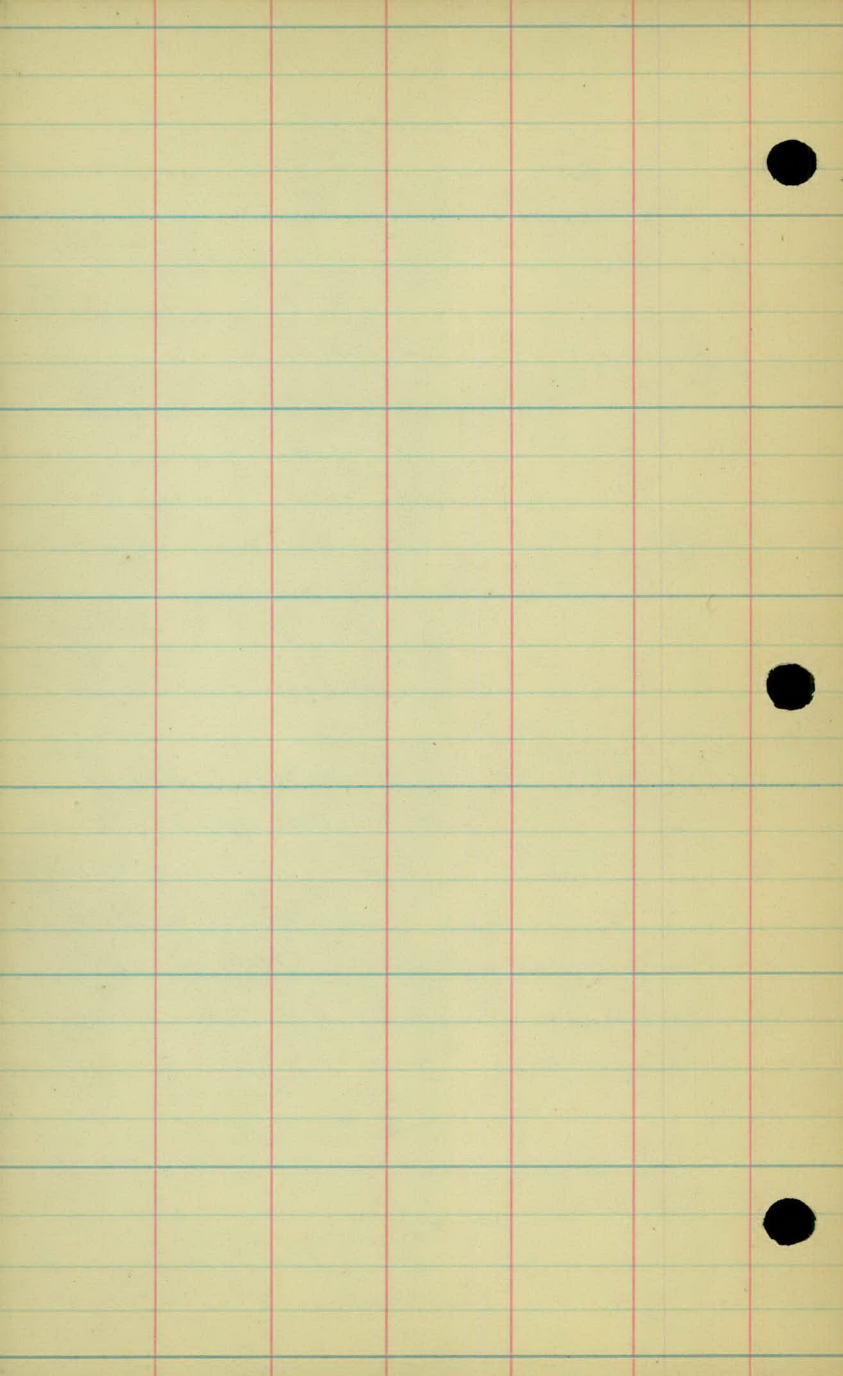
Spk. in 18" Elm 35' Lt. Sta. 181+35.

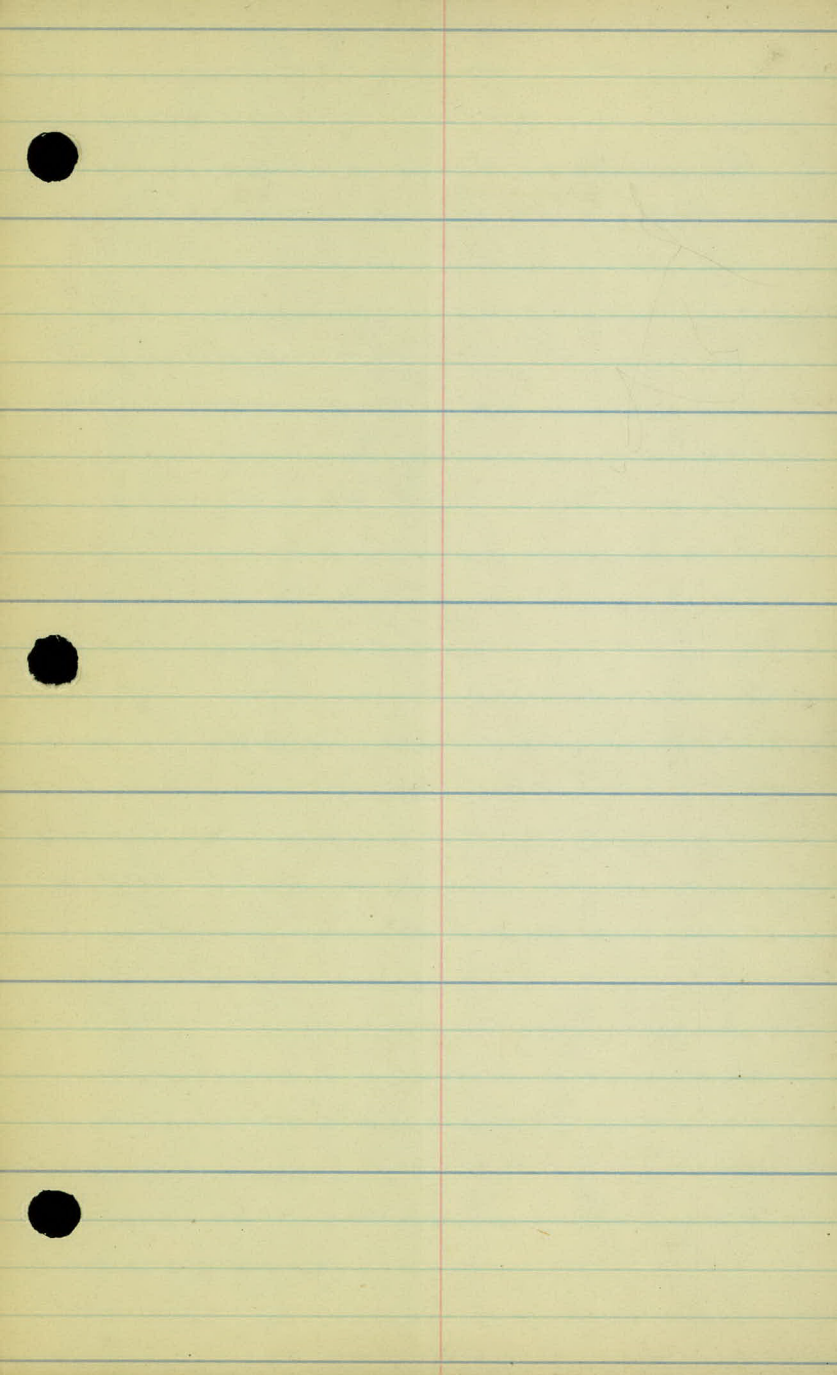
Spk. in 12" Oak. 60' Rt. Sta. 194+65.

Spk. in 18" Elm 60' Rt. Sta. 211+90.

On conc. porch S.E. Cor. Lt. Sta. 224+18.

Spk. in 30" Tree N.E. Cor.



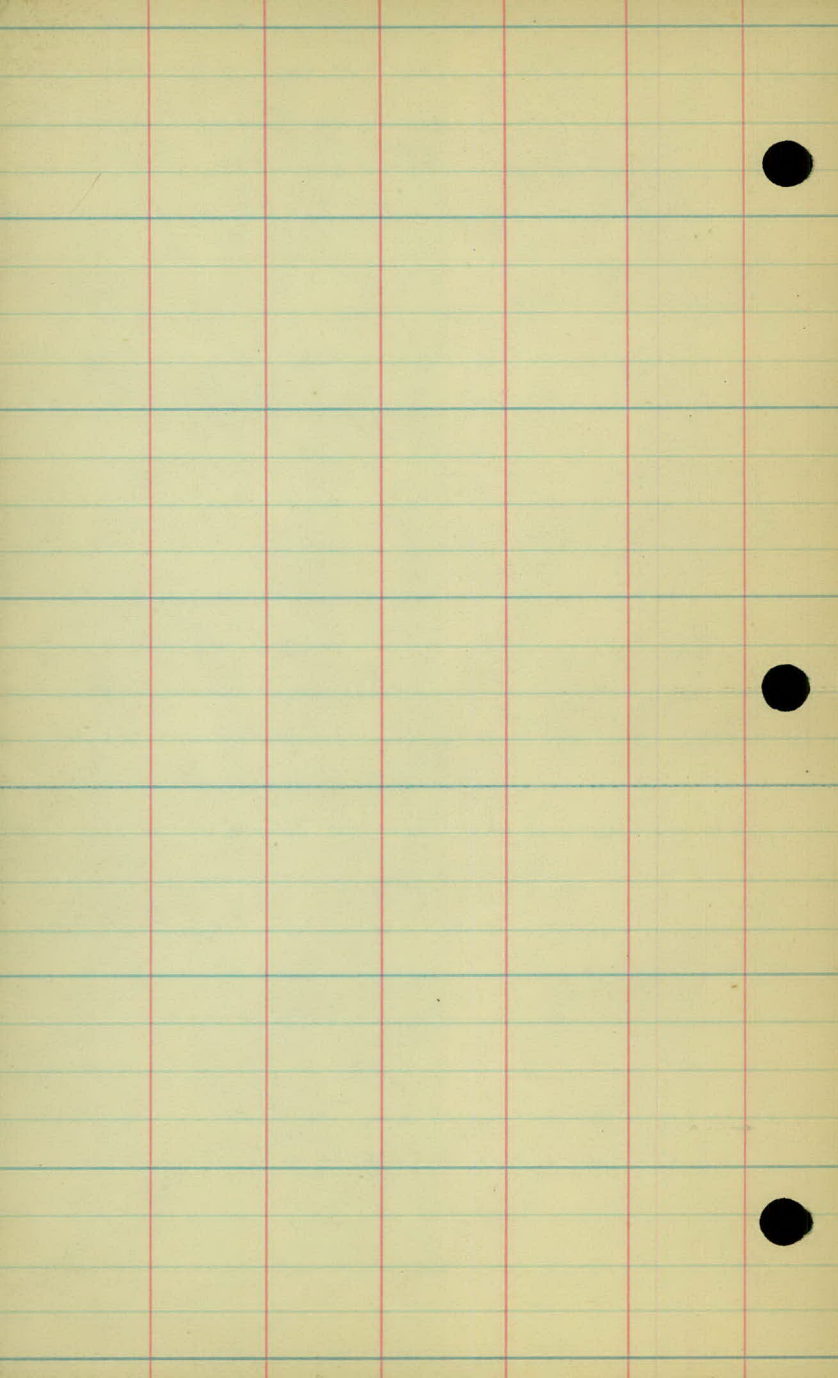


B.M.	1.98	714.25		912.27
	2.03	907.84	8.42	905.83
	4.88	905.27	7.47	900.39
	8.12	711.81	1.58	903.69
B.M.			3.88	907.93
	9.82	720.04	1.59	910.22
	3.26	910.24	3.06	916.98
B.M.			4.22	916.02
	5.03	919.85	5.42	914.82
	0.17	912.58	7.14	912.71
B.M.			5.08	907.00

2/5/25

SpK. in 30" Oak. 40' Lt. Stg. 111+10.

SpK. in T.P. Rt. Stg. 125+07.



Road. 62 + 63.
X-Sections
4" line

"L" line

Station	+	H.I.	=	Rod	Elev.
B.M.	2.00	914.27			912.27
0+00					
+50					
1+00					
+79					
2+00					
+11				9.00	905.27
+40					
3+00					
+50					
4+00					
T.P.	0.38	905.32	9.33	904.94	
+50					
5+00					
+50					
6+00					

6" nine

4

2-10-25

0+100

On top concrete step N.E. Cor. School House

$\frac{4.0}{50.0}$ $\frac{4.0}{25.0}$ 3.7 $\frac{3.6}{25.0}$ $\frac{3.8}{50.0}$

$\frac{4.3}{33.0}$ $\frac{4.8}{15.0}$ 4.3 $\frac{4.9}{9.0}$ $\frac{5.9}{15.0}$ $\frac{6.2}{26.0}$ $\frac{4.1}{31.0}$ $\frac{4.1}{33.0}$

$\frac{4.6}{33.0}$ $\frac{5.2}{17.0}$ 5.0 $\frac{5.4}{9.0}$ $\frac{7.0}{13.0}$ $\frac{7.5}{20.0}$ $\frac{7.0}{24.0}$ $\frac{3.7}{32.0}$ $\frac{3.7}{33.0}$

$\frac{5.0}{33.0}$ $\frac{5.6}{23.0}$ $\frac{5.8}{8.0}$ 6.0 $\frac{6.1}{8.0}$ $\frac{7.0}{12.0}$ $\frac{7.9}{17.0}$ $\frac{7.9}{22.0}$ $\frac{3.2}{32.0}$ $\frac{3.5}{33.0}$

$\frac{5.5}{33.0}$ $\frac{5.8}{21.0}$ $\frac{6.1}{8.0}$ 6.3 $\frac{6.0}{14.0}$ $\frac{5.7}{33.0}$

APPOX Top. Water Main

$\frac{6.0}{33.0}$ $\frac{7.7}{21.0}$ $\frac{7.7}{14.0}$ $\frac{7.2}{11.0}$ 6.9 $\frac{7.4}{12.0}$ $\frac{7.1}{33.0}$

$\frac{3.0}{34.0}$ $\frac{7.0}{29.0}$ $\frac{10.1}{24.0}$ $\frac{10.2}{19.0}$ $\frac{8.7}{11.0}$ 8.0 $\frac{8.5}{18.0}$ $\frac{10.8}{19.0}$ $\frac{10.7}{33.0}$

$\frac{1.5}{40.0}$ $\frac{6.2}{31.0}$ $\frac{9.2}{27.0}$ $\frac{10.5}{24.0}$ $\frac{10.7}{18.0}$ $\frac{9.5}{13.0}$ $\frac{9.0}{10.0}$ 8.5 $\frac{9.0}{7.0}$ $\frac{9.6}{12.0}$ $\frac{11.5}{19.0}$ $\frac{10.7}{33.0}$

$\frac{6.4}{34.0}$ $\frac{11.0}{26.0}$ $\frac{11.8}{21.0}$ $\frac{11.4}{18.0}$ $\frac{10.3}{14.0}$ $\frac{9.6}{11.0}$ 9.0 $\frac{9.5}{11.0}$ $\frac{12.4}{17.0}$ $\frac{12.0}{33.0}$

$\frac{4.5}{33.0}$ $\frac{4.1}{25.0}$ $\frac{3.7}{20.0}$ $\frac{1.2}{10.0}$ 0.7 $\frac{1.4}{9.0}$ $\frac{3.9}{16.0}$ $\frac{4.2}{24.0}$ $\frac{4.8}{33.0}$

$\frac{5.2}{33.0}$ $\frac{5.1}{17.0}$ $\frac{3.0}{12.0}$ $\frac{2.3}{9.0}$ 1.4 $\frac{2.3}{10.0}$ $\frac{4.4}{15.0}$ $\frac{5.0}{23.0}$ $\frac{5.2}{33.0}$

$\frac{5.2}{33.0}$ $\frac{5.3}{20.0}$ $\frac{5.4}{17.0}$ $\frac{3.6}{10.0}$ 2.7 $\frac{3.2}{9.0}$ $\frac{3.6}{11.0}$ $\frac{5.4}{15.0}$ $\frac{5.8}{18.0}$ $\frac{5.4}{33.0}$

$\frac{5.7}{33.0}$ $\frac{6.2}{15.0}$ $\frac{4.6}{10.0}$ 4.0 $\frac{4.6}{11.0}$ $\frac{6.7}{15.0}$ $\frac{6.0}{26.0}$ $\frac{5.8}{33.0}$

Station + H.I. - Rod Elev.

905.32

7+00

8+00

9+00

9+87 - Cross-section in Drainage Notes

~~10+00~~

~~10+03~~

T.P.

6.57 907.03 4.86 900.46

11+00

12+00

13+65

13+00

T.P. 10.29 913.20 4.12 902.91

+50

14+00

+50

15+00

16+00

"L" line

7400

				7.8										
7.1	7.8	10.2	10.2	7.2	5.6									
38.0	38.0	19.0	16.0	11.0	9.0	5.1	5.7	7.0	11.5	7.2	7.0			
							9.0	11.0	18.5	25.0	33.			

			2.4							2.4	2.4		
7.5	7.8	7.5	10.5	7.4	5.6	5.4				5.8	7.1	10.5	10.5
38.0	29.0	20.0	15.6	11.0	9.0	7.0	5.0	10.0	12.0	17.0	19.0	23	35.0

7.2	7.8	10.3	10.8	7.3	5.8	6.1	7.2	10.3	10.8	7.3	7.1
33.0	28.0	18.0	16.0	11.0	8.0	5.2	10.0	11.0	7.0	19.0	23
33.0	28.0	18.0	16.0	11.0	8.0	5.2	10.0	11.0	7.0	19.0	23

6.8	6.5	7.0	7.0	7.2	4.5	4.8	9.0	8.4	8.4	6.8
38.0	25.0	17.0	12.0	14.0	7.0	4.2	9.0	16.0	17.0	20.0

[illegible][illegible]

$\frac{7.5}{38.0}$	$\frac{7.3}{20.0}$	$\frac{9.5}{19.0}$	$\frac{6.4}{14.0}$	$\frac{6.5}{11.0}$	$\frac{5.2}{8.0}$	4.7	$\frac{5.5}{12.0}$	$\frac{7.0}{17.0}$	$\frac{7.1}{22.0}$	$\frac{7.0}{33.0}$
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<u>7.0</u>	<u>6.8</u>	<u>7.7</u>	<u>7.4</u>	<u>5.3</u>		<u>4.3</u>	<u>5.4</u>	<u>6.1</u>	<u>6.9</u>	<u>7.1</u>	<u>7.0</u>
33.0	19.0	17.0	13.0	9.0	4.3	6.0	14.0	18.0	19.0	27.0	33.0

Nail in T.P. 20' Rt. Sto 13+20

13.5	13.1	13.0	11.0		10.6	12.8	13.0	12.2	11.8
23.0	25.0	14.0	9.0	10.0	10.0	17.0	21.0	28.0	33.0

4.3	82	12.2	12.3	10.1		10.3	12.0	12.2	11.1	5.6	4.5
33.0	30.0	21.0	13.0	7.0	9.6	12.0	15.0	21.0	23.0	32.0	34.0

3.0	5.7	9.8	11.2	11.6	9.8	9.5	10.0	11.3	11.3	1.3
26.5	25.0	20.0	22.0	13.5	9.0	9.3	12.5	17.0	20.0	33

<u>1.7</u>	<u>7.9</u>	<u>10.8</u>	<u>10.8</u>	<u>9.4</u>	<u>9.2</u>		<u>9.1</u>	<u>10.6</u>	<u>10.6</u>	<u>6.2</u>	<u>0.0</u>
39.0	51.0	21.0	17.0	13.0	7.0	8.8	13.0	17.5	20.0	27.0	34.0

3.0	6.6	9.3	9.8	9.4	8.0	7.6	8.2	9.7	9.1	8.0	2.5
35.0	29.0	23.0	16.0	11.0	6.5		14.0	17.5	22.0	24.0	33.0

Station	+	H.I.	-	Rod Elev.	
		913.20			
16+50					
B.M.	4.19	912.12		5.27	907.93 907.93
17+00					
+50					
18+00					
+50					
19+00					
+50					
T.P.	8.52	916.73	3.91	908.21	
20+00					
+40					
+62					
21+00					
+32					
+43					

H.

t.

R.

L' line

16+50

$\frac{6.1}{33.0}$	$\frac{6.4}{31.0}$	$\frac{9.3}{16.0}$	$\frac{9.3}{11.0}$	$\frac{7.2}{5.0}$	$\frac{6.9}{6.9}$	$\frac{6.8}{2.7}$	$\frac{7.4}{12.0}$	$\frac{9.4}{17.5}$	$\frac{9.4}{20.5}$	$\frac{8.0}{26.0}$	$\frac{4.8}{33.0}$	$\frac{4.1}{35.0}$
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S/p. 17 24" OAK 30 R+ 349 16+85

$\frac{6.0}{33.0}$	$\frac{6.5}{18.0}$	$\frac{7.6}{15.0}$	$\frac{7.6}{10.0}$	$\frac{6.7}{8.0}$	$\frac{5.8}{6.0}$	$\frac{5.4}{5.4}$	$\frac{5.3}{2.0}$	$\frac{6.1}{13.0}$	$\frac{8.0}{17.0}$	$\frac{7.8}{20.0}$	$\frac{5.6}{24.0}$	$\frac{4.8}{33.0}$
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$\frac{6.2}{33.0}$	$\frac{6.6}{22.0}$	$\frac{7.5}{15.5}$	$\frac{7.8}{12.5}$	$\frac{5.7}{7.0}$	$\frac{5.1}{5.1}$	$\frac{5.6}{11.0}$	$\frac{7.0}{15.0}$	$\frac{7.5}{19.0}$	$\frac{4.3}{21.0}$	$\frac{6.3}{27.0}$	$\frac{6.2}{33.0}$
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$\frac{6.7}{33.0}$	$\frac{7.6}{20.0}$	$\frac{7.2}{12.0}$	$\frac{6.8}{8.5}$	$\frac{5.4}{6.5}$	$\frac{5.0}{5.0}$	$\frac{4.8}{1.5}$	$\frac{5.3}{12.0}$	$\frac{7.7}{18.0}$	$\frac{8.0}{29.0}$	$\frac{7.7}{33.0}$
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$\frac{6.0}{33.0}$	$\frac{7.0}{21.0}$	$\frac{7.2}{15.0}$	$\frac{5.6}{9.0}$	$\frac{5.1}{7.0}$	$\frac{4.7}{4.7}$	$\frac{4.5}{1.0}$	$\frac{5.3}{10.0}$	$\frac{8.5}{17.5}$	$\frac{8.7}{26.0}$	$\frac{8.7}{33.0}$
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$\frac{3.7}{33.0}$	$\frac{4.0}{28.0}$	$\frac{5.0}{19.0}$	$\frac{5.6}{16.0}$	$\frac{5.1}{10.0}$	$\frac{4.5}{4.5}$	$\frac{4.4}{1.5}$	$\frac{5.2}{12.5}$	$\frac{8.0}{19.0}$	$\frac{8.0}{22.0}$	$\frac{7.0}{26.0}$	$\frac{7.0}{33.0}$
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$\frac{1.1}{39.0}$	$\frac{2.0}{29.5}$	$\frac{2.5}{22.0}$	$\frac{2.9}{19.0}$	$\frac{5.6}{15.0}$	$\frac{5.7}{12.5}$	$\frac{4.7}{8.0}$	$\frac{4.0}{4.0}$	$\frac{4.5}{4.5}$	$\frac{5.2}{10.5}$	$\frac{7.0}{14.5}$	$\frac{7.2}{19.0}$	$\frac{4.4}{23.0}$	$\frac{4.4}{28.0}$	$\frac{4.4}{33.0}$
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$\frac{4.2}{34.0}$	$\frac{4.2}{29.0}$	$\frac{5.4}{14.5}$	$\frac{7.5}{11.5}$	$\frac{9.3}{6.0}$	$\frac{8.6}{8.6}$	$\frac{7.9}{9.0}$	$\frac{8.3}{18.0}$	$\frac{9.0}{21.5}$	$\frac{11.2}{26.5}$	$\frac{11.3}{30.5}$	$\frac{12.7}{34.0}$	$\frac{6.5}{36.5}$
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$\frac{2.1}{33.0}$	$\frac{2.5}{23.0}$	$\frac{3.6}{8.5}$	$\frac{6.0}{5.0}$	$\frac{8.2}{8.2}$	$\frac{8.5}{2.5}$	$\frac{7.7}{7.5}$	$\frac{7.0}{20.0}$	$\frac{9.5}{28.0}$	$\frac{10.5}{38.0}$
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$\frac{1.0}{33.0}$	$\frac{2.0}{13.0}$	$\frac{3.0}{3.0}$	$\frac{4.8}{0.5}$	$\frac{7.2}{6.0}$	$\frac{7.8}{10.0}$	$\frac{7.4}{13.5}$	$\frac{6.4}{28.0}$	$\frac{7.2}{39.0}$	$\frac{10.2}{48.0}$
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$\frac{0.0}{33.0}$	$\frac{0.4}{21.0}$	$\frac{1.9}{15.5}$	$\frac{3.0}{16.0}$	$\frac{4.7}{17.0}$	$\frac{6.3}{21.5}$	$\frac{6.8}{35.0}$	$\frac{5.3}{43.0}$	$\frac{5.6}{50.0}$	$\frac{7.0}{50.0}$
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$\frac{0.0}{33.0}$	$\frac{0.8}{16.0}$	$\frac{2.2}{2.0}$	$\frac{3.5}{6.0}$	$\frac{5.5}{10.0}$	$\frac{6.0}{13.0}$	$\frac{5.8}{24.0}$	$\frac{4.9}{34.0}$	$\frac{5.2}{40.0}$	$\frac{7.0}{46.0}$	$\frac{7.3}{43.0}$
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$\frac{0.0}{33.0}$	$\frac{0.8}{21.0}$	$\frac{1.6}{7.0}$	$\frac{5.5}{4.0}$	$\frac{5.6}{6.5}$	$\frac{5.2}{20.0}$	$\frac{4.7}{21.5}$	$\frac{5.1}{33.0}$	$\frac{6.5}{35.0}$	$\frac{6.5}{37.0}$	$\frac{5.0}{37.0}$
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Station	+	H.I.	-	Rod Elev.
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916.73

22 +00

T.P.	8.44	922.46	2.51	914.22
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+50

23 +00

+25

24 +00

25 +00

26 +00

+50

27 +00

T.P.	8.82	918.48	8.00	914.66
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+50

28 +00

28 +00

+50

+50

29 +00

B.M.

2.48 916.00 916.00

22+100

"L" line

0.2 0.6 1.5 3.9 4.1 3.6 3.1 3.4 3.7 4.8 4.8 3.0 3.0 3.8
33.0 29.0 28.5 24.0 20.5 16.0 6.0 9.4 4.5 9.5 11.5 16.0 17.0 33.0

5.0 8.2 8.3 8.0 8.6 9.3 9.3 6.6 7.2 8.0
40.0 34.0 26.0 15.0 6.5 3.0 9.3 1.0 5.5 20.0 33.0

4.8 7.8 8.3 7.6 8.2 8.3 7.9 6.5 5.0 5.8 6.5
42.0 35.5 31.0 19.0 7.5 7.0 3.0 2.0 22.0 33.0

6.5 7.5 8.0 7.4 7.9 7.7 6.1 5.3 6.1
40.0 35.0 32.0 22.0 14.0 8.0 3.0 4.7 16.0 33.0

5.0 6.5 6.6 6.1 6.6 6.6 6.2 4.9 5.6 6.2
45.0 48.0 37.0 27.0 18.0 14.5 10.5 7.0 5.0 17.0 33.0

5.0 5.8 5.3 5.7 5.7 7.6 8.7
47.0 38.0 29.0 21.0 12.0 6.3 20.0 33.0

5.2 6.0 6.2 5.8 6.3 6.6 9.0 10.5
48.0 41.0 37.0 28.0 20.0 12.0 7.3 17.0 33.0

5.8 6.4 6.6 6.0 6.6 6.5 8.2 9.5
48.0 46.0 36.0 26.0 17.0 10.0 6.9 16.0 33.0

6.4 7.0 6.7 6.4 6.8 6.7 8.6 10.0
42.0 37.0 34.0 25.0 16.5 11.0 7.1 18.0 33.0

1.5 2.4 2.2 2.4 3.2 3.5 3.6 5.7 6.8
41.0 38.0 31.0 22.0 13.0 8.0 5.0 4.0 17.0 33.0

2.2 3.2 3.2 2.9 3.5 5.0 6.0 7.0
37.0 32.0 23.0 15.5 4.0 4.1 9.0 20.0 33.0

2.6 2.7 3.3 3.2 3.3 3.7 4.9 5.6 6.4
39.0 28.0 23.0 16.0 9.0 3.1 11.0 18.0 24.5 36.0

2.3 2.1 3.0 3.4 3.0 3.7 4.2
33.0 18.0 3.0 11.0 23.0 33.0 33.0

5/2 in T.R 41 RT. STA 29+25

Station	+	H.I.	-	Red.	Elev.
		918.48			
B.M	2.45	918.45	2.48	916.00	
29+50					
30+00					
+50					
31+00					
+50					
32+00					
+50					
33+00					
T.P.	6.20	922.70	1.95	916.50	
+38					
+55					
34+00					
+50					

29+50

ht.

±

RT.

"A" line

Sp. in T.P. 40 RT. Sta 29+25

$\frac{2.2}{33.0}$	$\frac{2.3}{21.0}$	2.8	$\frac{3.2}{28.0}$	$\frac{3.6}{41.0}$	$\frac{3.4}{48.0}$
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$\frac{4.3}{35.0}$	$\frac{4.5}{27.0}$	5.0	$\frac{4.6}{33.0}$	$\frac{4.4}{33.0}$
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$\frac{6.4}{33.0}$	$\frac{6.5}{18.0}$	7.2	$\frac{7.2}{20.0}$	$\frac{6.9}{33.0}$
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$\frac{8.0}{33.0}$	$\frac{8.5}{30.0}$	$\frac{8.6}{18.0}$	9.3	$\frac{8.8}{21.0}$	$\frac{8.6}{33.0}$
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$\frac{6.4}{33.0}$	$\frac{7.0}{9.0}$	$\frac{7.7}{7.0}$	7.8	$\frac{9.0}{20.0}$	$\frac{8.0}{33.0}$
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$\frac{5.2}{33.0}$	$\frac{5.6}{20.0}$	6.2	$\frac{6.9}{17.0}$	$\frac{7.0}{33.0}$
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$\frac{3.3}{33.0}$	$\frac{4.0}{21.0}$	4.5	$\frac{5.0}{18.0}$	$\frac{4.7}{30.0}$	$\frac{5.2}{35.0}$
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$\frac{1.6}{33.0}$	$\frac{2.0}{19.0}$	2.8	$\frac{3.0}{13.0}$	$\frac{4.8}{16.0}$	$\frac{5.0}{19.0}$	$\frac{4.0}{22.0}$	$\frac{3.4}{33.0}$	$\frac{3.9}{48.0}$
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$\frac{4.3}{33.0}$	$\frac{5.0}{19.0}$	$\frac{5.8}{2.5}$	6.4	$\frac{8.7}{4.0}$	$\frac{9.1}{7.0}$	$\frac{8.1}{10.5}$	$\frac{7.5}{20.0}$	$\frac{7.8}{31.0}$	$\frac{8.8}{34.0}$
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$\frac{4.0}{33.0}$	$\frac{4.6}{12.0}$	$\frac{5.3}{6.0}$	8.6	$\frac{9.0}{2.5}$	$\frac{7.9}{6.0}$	$\frac{7.5}{15.0}$	$\frac{7.8}{26.0}$	$\frac{8.4}{29.0}$	$\frac{8.4}{31.0}$	7.3
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$\frac{2.8}{33.0}$	$\frac{3.4}{17.0}$	$\frac{7.0}{12.0}$	$\frac{7.3}{7.5}$	$\frac{8.5}{6.5}$	$\frac{7.7}{3.0}$	7.6	$\frac{7.3}{7.0}$	$\frac{7.8}{18.0}$	$\frac{7.6}{25.0}$	$\frac{6.9}{33.0}$
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$\frac{4.3}{33.0}$	$\frac{4.3}{21.0}$	$\frac{7.7}{16.0}$	$\frac{9.0}{12.5}$	$\frac{7.8}{7.0}$	7.3	$\frac{8.0}{11.0}$	$\frac{9.0}{14.0}$	$\frac{8.0}{17.0}$	$\frac{7.9}{33.0}$
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Station	+	H.I.	-	Rod. Elev	
		922.70			
35+00					
+50					
36+00					
37+00					
38+00					
+50					
39+00					
+50					
T.P.	3.65	914.33	12.02	910.68	
40+00					
41+00					
+50					
42+00					
43+00					
B.M.	2.75	909.71	7.37	906.96	7.37 906.96

Station	+	H.I.	-	Rod	Elev.
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909.7'

43+00

44+00

45+00

+57

46+00

+38

T.P.	4.74	904.16	10.29	899.42
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+50

47+00

+50

48+00

+50

49+00

43460

H.

A

R.H.

"h" line

10.2 9.5 6.2 6.2 8.7 9.0 9.2
33.0 19.0 12.0 5.4 11.0 16.0 23.0 33.0

10.1 9.1 6.9 6.9 8.9 9.1
33.0 17.0 11.5 6.2 12.0 17.0 33.0

10.6 10.1 8.0 8.2 10.2 10.2 10.2
33.0 17.0 10.0 11.5 15.5 17.5 33.0

9.7 9.6 9.1 8.6 8.0 8.5 9.1 10.4 10.2 10.6
33.0 16.0 15.0 10.5 8.0 8.5 12.0 14.5 20.0 33.0

11.0 10.9 10.4 9.9 9.2 9.4 9.9 10.9 10.2 9.8
33.0 25.0 19.0 15.0 5.0 7.5 11.5 17.0 33.0

2Rd
11.7 11.6 9.3 9.6 9.1 9.6 11.3 11.2 10.8
33.0 29.0 24.0 14.5 3.5 4.0 11.5 33.0

2Rd
5.6 3.9 3.0 3.6 4.2 5.7 6.0 5.3 5.4
33.0 29.0 17.0 8.0 4.0 1.0 5.7 5.5 23.0 33.0

2Rd
6.0 4.0 3.2 3.8 6.0 5.7 5.8 5.5 5.6 5.4
59.0 33.0 41.0 28.5 25.5 22.0 12.0 5.5 20.0 33.0

3.7 3.5 4.0 4.2 4.4
37.0 18.0 17.0 33.0

4.2 3.8 3.5 3.1 2.9
33.0 17.0 20.0 33.0

2Rd
4.4 4.9 7.1 7.8 7.7 9.3 9.3 6.0 4.4 3.6
47.0 32.0 30.0 25.5 22.0 19.0 13.0 5.2 18.0 33.0

2Rd
4.8 6.5 5.3 4.7 5.2 6.5 4.5 9.5 8.1 8.3 8.8 6.3 6.5 5.1
41.0 37.0 31.5 22.0 11.0 5.5 1.5 2.0 4.0 6.0 8.5 10.5 14.0 33.0

Station	+	H.I.	—	Rod Elev.
		904.16		
49+22				
+50				
T.P.	4.93	903.54	5.55	898.61
50+00				
51+00				
52+00				
53+00				
54+00				
55+00				
56+00				
T.P.	5.56	904.18	4.92	898.62
57+00				
58+00				
59+00				
B.M.			4.91	899.50

ht.

A

ht.

"h" line

(49122)

$\frac{9.4}{39.0}$ $\frac{9.3}{21.0}$ $\frac{5.6}{25.0}$ $\frac{4.7}{12.5}$ $\frac{5.0}{5.0}$ $\frac{7.5}{4.5}$ $\frac{8.9}{8.0}$ $\frac{8.8}{9.0}$ $\frac{8.0}{11.5}$ $\frac{8.5}{16.0}$ $\frac{9.3}{18.5}$ $\frac{6.3}{21.5}$

$\frac{9.6}{35.0}$ $\frac{9.0}{29.0}$ $\frac{8.8}{23.0}$ $\frac{5.7}{17.0}$ $\frac{4.9}{6.0}$ $\frac{5.0}{5.0}$ $\frac{5.5}{8.0}$ $\frac{8.0}{12.0}$ $\frac{4.2}{16.0}$ $\frac{9.3}{18.0}$ $\frac{9.0}{22.0}$ $\frac{8.9}{25.5}$ $\frac{6.8}{28.0}$

Nail in T.R. Rt. sta 50+10

$\frac{8.6}{32.0}$ $\frac{9.0}{30.0}$ $\frac{8.6}{22.0}$ $\frac{8.0}{16.0}$ $\frac{5.0}{11.5}$ $\frac{4.2}{4.2}$ $\frac{5.2}{12.0}$ $\frac{6.5}{14.0}$ $\frac{7.8}{18.0}$ $\frac{9.2}{25.0}$ $\frac{7.8}{31.0}$ $\frac{6.2}{33.0}$

$\frac{5.7}{37.0}$ $\frac{5.5}{31.5}$ $\frac{7.9}{28.0}$ $\frac{7.3}{23.5}$ $\frac{9.3}{22.0}$ $\frac{7.2}{18.0}$ $\frac{4.8}{12.0}$ $\frac{4.2}{11.0}$ $\frac{8.0}{15.0}$ $\frac{8.4}{21.0}$ $\frac{7.8}{24.0}$ $\frac{6.8}{28.0}$ $\frac{4.7}{31.0}$ $\frac{4.7}{33.0}$

$\frac{7.7}{33.0}$ $\frac{8.1}{30.0}$ $\frac{7.7}{28.0}$ $\frac{7.8}{21.5}$ $\frac{7.9}{17.5}$ $\frac{5.0}{13.0}$ $\frac{4.4}{4.4}$ $\frac{5.2}{16.0}$ $\frac{7.9}{14.5}$ $\frac{8.0}{28.0}$ $\frac{7.8}{33.0}$

$\frac{9.1}{33.0}$ $\frac{8.2}{24.0}$ $\frac{7.8}{19.0}$ $\frac{5.7}{13.5}$ $\frac{5.1}{11.0}$ $\frac{4.6}{4.6}$ $\frac{5.4}{10.0}$ $\frac{7.8}{14.0}$ $\frac{8.0}{19.0}$ $\frac{8.0}{33.0}$

$\frac{7.8}{30.5}$ $\frac{8.8}{29.0}$ $\frac{7.9}{27.0}$ $\frac{7.3}{23.0}$ $\frac{7.3}{17.0}$ $\frac{5.5}{13.0}$ $\frac{4.6}{4.6}$ $\frac{5.0}{7.5}$ $\frac{5.0}{10.0}$ $\frac{8.0}{16.0}$ $\frac{8.0}{33.0}$

$\frac{9.3}{33.0}$ $\frac{8.2}{30.0}$ $\frac{9.0}{28.0}$ $\frac{9.0}{27.0}$ $\frac{8.1}{20.0}$ $\frac{7.8}{15.5}$ $\frac{5.4}{12.5}$ $\frac{4.6}{4.6}$ $\frac{4.8}{11.5}$ $\frac{7.0}{16.0}$ $\frac{6.8}{21.0}$ $\frac{6.3}{33.0}$

$\frac{8.5}{33.0}$ $\frac{9.3}{30.0}$ $\frac{9.8}{28.0}$ $\frac{8.0}{27.0}$ $\frac{8.2}{17.0}$ $\frac{5.6}{12.0}$ $\frac{5.0}{5.0}$ $\frac{5.3}{10.0}$ $\frac{8.0}{15.0}$ $\frac{8.7}{18.0}$ $\frac{8.5}{33.0}$

$\frac{9.0}{31.0}$ $\frac{10.0}{28.5}$ $\frac{9.0}{27.5}$ $\frac{8.9}{20.0}$ $\frac{8.4}{17.0}$ $\frac{6.4}{12.0}$ $\frac{6.0}{10.0}$ $\frac{5.6}{5.6}$ $\frac{6.0}{10.5}$ $\frac{9.0}{16.0}$ $\frac{8.6}{33.0}$

$\frac{9.9}{33.0}$ $\frac{9.2}{18.0}$ $\frac{8.6}{15.0}$ $\frac{6.0}{10.5}$ $\frac{5.4}{5.4}$ $\frac{5.8}{10.5}$ $\frac{8.4}{15.0}$ $\frac{8.5}{19.0}$ $\frac{8.1}{33.0}$

$\frac{7.8}{33.0}$ $\frac{7.5}{25.0}$ $\frac{6.9}{14.5}$ $\frac{5.3}{11.5}$ $\frac{4.6}{4.6}$ $\frac{5.1}{11.5}$ $\frac{4.3}{16.0}$ $\frac{6.8}{18.0}$ $\frac{6.9}{24.0}$ $\frac{5.3}{27.0}$ $\frac{5.0}{33.0}$

Spike in 24" Oak 40 ft. sta 39+30

Station	+	H.I.	-	Rob.	Elev.
		904.18			
T.P.	7.45	907.85	3.78	900.40	
60+00					
61+00					
T.P.	5.11	908.69	4.27	903.58	
62+00					
63+00					
64+00					
65+00					
T.P.	9.57	916.80	1.46	907.23	
66+00					
+60					
67+00					
68+00					
T.P.	6.52	922.18	1.12	915.66	
69+00					
B.M				2.17	920.01

60400

67

E

R.

"h" hime

8.7	9.7	9.5	8.9	8.4		8.1	8.5	10.1	8.6	7.9	7.0
33.0	28.0	13.5	13.0	12.0	7.7	10.0	63.0	16.5	18.0	23.0	25.0
								2.0	2.8	5.0	
								33.0	27.0	28.0	

9.5	9.4	8.6	8.3	7.3	7.2	7.2	7.5	8.5	8.6	7.3	5.8	4.0
33.0	23.0	20.0	15.0	12.5	10.0	6.7	10.0	11.5	14.0	20.0	24.0	29.0
											2.7	
											33.0	

Nail in T.P. Rt. Sta 61 + 25

9.6	7.6	8.1	8.0	6.8		6.9	8.3	8.4	7.1	4.8
33.0	17.5	16.0	14.0	11.0	6.5	11.0	14.0	18.0	21.0	33.0

9.1	7.6	5.7		5.8	6.6	6.9	6.2
33.0	18.5	12.5	5.2	11.0	13.0	18.0	33.0

6.2	5.7	4.4	3.9		3.9	4.9	5.0	3.0	1.5
33.0	17.0	12.5	7.0	3.5	10.5	13.0	14.5	17.0	33.0

4.1	3.8	3.9	2.7	2.0		2.2	3.0	3.1	2.6	2.0
33.0	21.0	15.0	11.5	5.0	1.8	8.5	12.0	14.0	15.0	33.0

9.9	9.9	9.1	9.9	8.3	8.0	8.0	9.9	9.6	8.5	5.9	5.8
33.0	18.0	15.5	14.5	11.0	6.0	7.6	11.0	15.0	18.0	22.0	24.5
											33.0

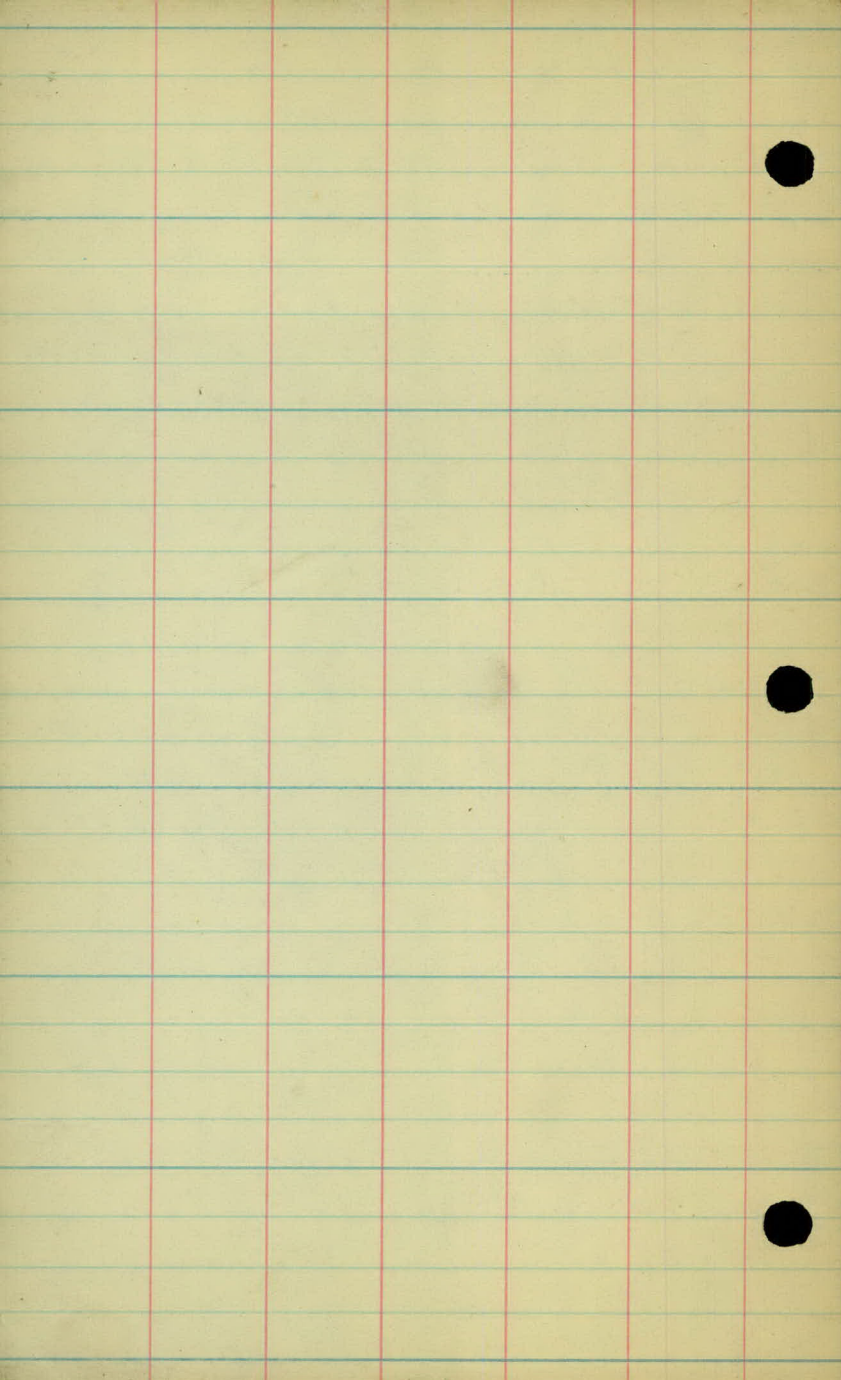
9.7	7.5	7.8	6.9	8.3	7.3	7.0	7.0	9.4	8.5	7.3	7.0	6.0	5.5
33.0	23.0	17.5	15.5	13.5	12.0	9.0	11.0	14.5	16.0	17.0	21.5	23.0	33.0

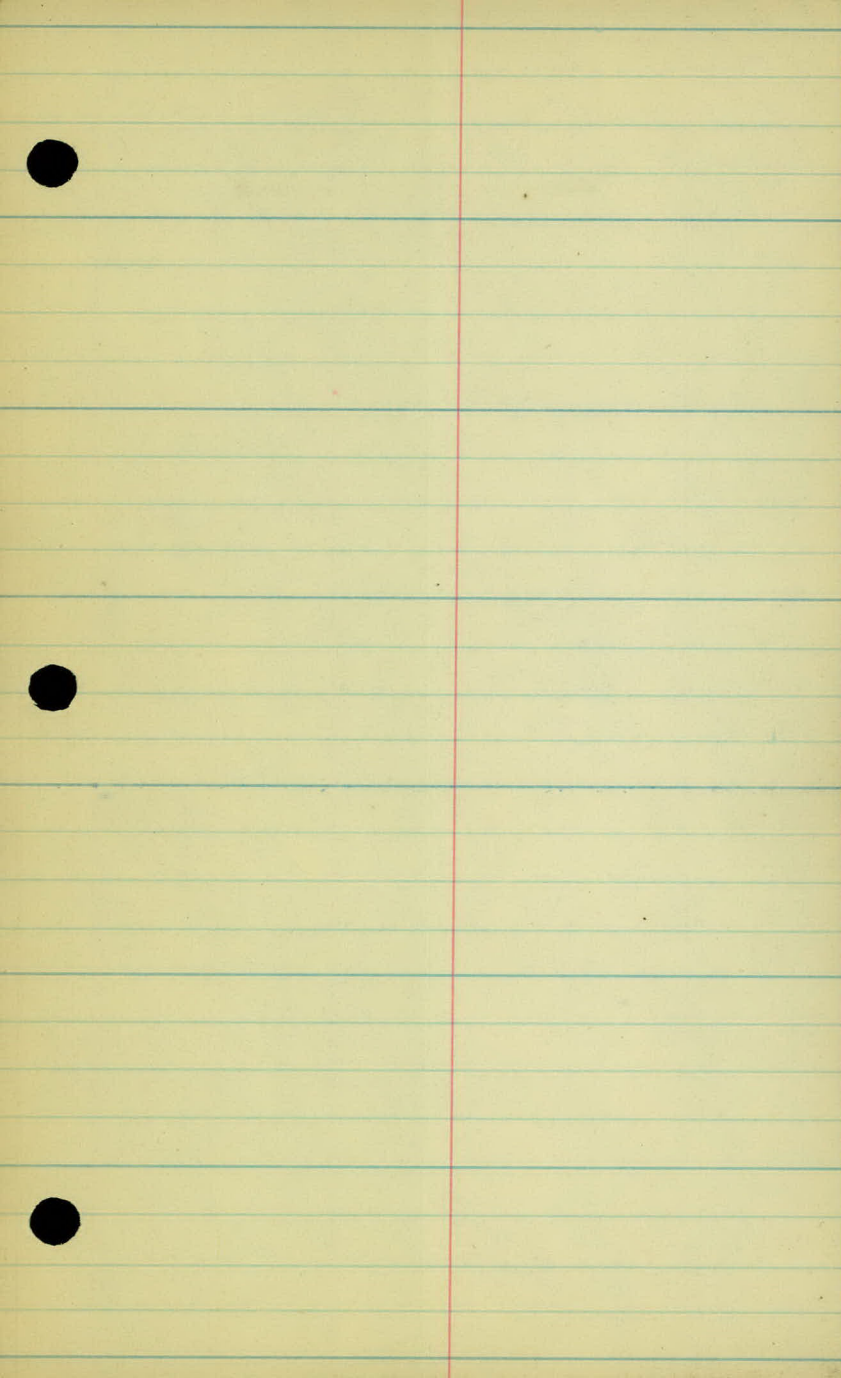
6.0	5.6	5.9	7.3	6.2		6.1	7.4	7.5	6.4	5.9	5.0
33.0	25.0	17.0	15.0	11.0	5.6	11.0	14.0	17.0	22.0	24.0	33.0

8.5	9.4	3.5	5.1	5.1	4.0	4.0	5.4	5.4	4.6	4.5
33.0	24.0	16.0	14.0	13.0	12.0	3.4	12.0	15.0	16.0	17.5
										33.0

9.2	7.3	7.8	8.0	8.0	7.3	7.9	9.0	8.9	8.0	7.6
33.0	21.0	15.0	14.0	12.0	11.0	7.1	13.0	16.0	18.0	20.0
										33.0

Sp. in 30" OAK Lt Sta 70 + 90





Sta	+	H.I.	-	Elev.
B.M.	2.64	922.66		920.02

70

+44

71

+37

72

+60

73

+60

74

+50

75

T.P.	5.59	919.56	8.69	913.97
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+50

74

2/12/25

SPK in 24" Oak 30' Lt. Sta. 70+90.

5.2	5.1	7.3	5.9		6.2	7.2	7.1	5.6	5.0
33	14	14	4	5.7	10	15	18	25	33

4.7	4.2	4.0	6.0	5.3		5.5	6.5	6.2	3.2	2.5
33	24	15	12	9	5.1	13	17	22	24	33

4.1	3.7	3.6	5.5	5.2		4.9	4.1	5.8	3.0	2.7
33	25	15	13	10	4.4	12	16	24	28	33

2.7	3.3	4.9	5.0	4.5		4.3	4.2	4.3		
33	16	14	10	4	4.3	13	22	33		

4.2	4.1	4.0	4.4		4.8	5.1				
33	23	17	7	4.1	12	33				

3.5	3.6	5.4	4.5		4.8	4.9	5.0			
33	19	17	9	4.3	11	16	33			

4.1	4.9	6.0	5.3	5.1		5.2	5.8	5.6		
33	16	15	11	8	4.8	13	14	33		

5.9	6.0	6.5	5.9		5.4	5.8	6.3	6.0	6.6	
33	17	12	9	5.4	4	13	15	18	33	

7.4	7.2	6.3			6.1	6.9	4.9	4.0	4.9	
33	13	10	5.8		12	17	20	28	33	

8.8	8.3	7.2	6.8		6.8	7.3	8.5	7.8	3.8	3.3
33	15	13	7	6.3	10	13	15	21	25	33

7.9	7.6	6.3	7.6		7.3	8.1	8.8	8.7	6.6	5.6
33	18	14	10	7.0	11	14	16	17	20	33

8.1	8.1	7.0	5.2		5.2	4.6	6.4	5.5	4.8	
33	22	15	11	4.5	14	17	19	21	33	

4.8	7.6	5.1			4.9	6.2	6.2	4.8	5.0	
33	14	11	4.4		14	17	19	23	33	

Sta. + H.I. - Elev.

919.54

+50

77

78

+50

T.P. 7.79 923.47 3.89 915.67

79

+50

80

+44

81

+47

82

B.M. 1.10 917.34 7.20 916.27 914.24

+50

83

2/12/25

$\frac{6.7}{33}$	$\frac{8.0}{14}$	$\frac{5.2}{10}$	4.4	$\frac{5.1}{13}$	$\frac{7.2}{15}$	$\frac{7.8}{21}$	$\frac{6.2}{15}$	$\frac{7.2}{33}$
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$\frac{9.5}{33}$	$\frac{9.1}{18}$	$\frac{5.6}{12}$	4.9	$\frac{5.4}{12}$	$\frac{8.8}{18}$	$\frac{8.1}{33}$
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$\frac{8.2}{33}$	$\frac{8.4}{19}$	$\frac{5.7}{13}$	4.9	$\frac{5.0}{13}$	$\frac{7.1}{15}$	$\frac{6.8}{33}$
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$\frac{6.3}{33}$	$\frac{6.4}{30}$	$\frac{7.2}{28}$	$\frac{6.6}{14}$	$\frac{5.5}{12}$	4.7	$\frac{5.1}{13}$	$\frac{5.9}{14}$	$\frac{5.9}{14}$	$\frac{4.9}{19}$	$\frac{4.1}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{7.7}{33}$	$\frac{7.8}{31}$	$\frac{9.7}{28}$	$\frac{9.6}{14}$	$\frac{9.1}{13}$	8.4	$\frac{8.7}{11}$	$\frac{9.4}{13}$	$\frac{9.2}{14}$	$\frac{7.3}{20}$	$\frac{7.1}{33}$
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$\frac{5.9}{34}$	$\frac{10.2}{27}$	$\frac{9.4}{14}$	$\frac{8.8}{13}$	8.4	$\frac{8.8}{11}$	$\frac{9.5}{13}$	$\frac{9.9}{15}$	$\frac{5.8}{19}$	$\frac{6.2}{33}$
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+2

-2

$\frac{4.9}{33}$	$\frac{10.7}{25}$	$\frac{10.2}{18}$	$\frac{8.9}{11}$	8.2	$\frac{8.3}{14}$	$\frac{9.0}{15}$	$\frac{9.1}{14}$	$\frac{4.4}{23}$	$\frac{4.1}{33}$
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+1

-1

$\frac{4.7}{34}$	$\frac{8.7}{29}$	$\frac{7.8}{22}$	$\frac{7.5}{14}$	$\frac{9.1}{15}$	8.0	$\frac{8.4}{14}$	$\frac{9.4}{18}$	$\frac{9.2}{20}$	$\frac{3.7}{22}$	$\frac{3.7}{33}$
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$\frac{5.5}{35}$	$\frac{8.8}{31}$	$\frac{9.4}{28}$	$\frac{10.0}{22}$	$\frac{9.9}{14}$	$\frac{9.0}{14}$	8.5	$\frac{9.1}{11}$	$\frac{9.8}{13}$	$\frac{9.2}{23}$	$\frac{5.5}{27}$	$\frac{5.1}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.6}{34}$	$\frac{10.5}{24}$	$\frac{11.0}{21}$	$\frac{10.6}{16}$	$\frac{10.1}{15}$	9.5	$\frac{10.1}{10}$	$\frac{11.0}{12}$	$\frac{11.1}{15}$	$\frac{7.1}{22}$	$\frac{6.4}{33}$
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$\frac{6.9}{33}$	$\frac{10.8}{24}$	$\frac{12.3}{21}$	$\frac{12.5}{17}$	$\frac{11.6}{16}$	10.9	$\frac{11.3}{10}$	$\frac{12.0}{11}$	$\frac{11.7}{15}$	$\frac{8.3}{18}$	$\frac{8.9}{33}$
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Spk. in T.P. 40' Lt. Sta. 83+00.

$\frac{1.0}{34}$	$\frac{4.3}{29}$	$\frac{6.7}{24}$	$\frac{7.2}{18}$	$\frac{6.1}{16}$	5.9	$\frac{6.8}{11}$	$\frac{7.4}{12}$	$\frac{7.2}{15}$	$\frac{5.1}{16}$	$\frac{5.1}{33}$
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$\frac{2.5}{33}$	$\frac{3.2}{28}$	$\frac{8.2}{22}$	$\frac{8.3}{14}$	$\frac{7.4}{13}$	7.2	$\frac{7.8}{12}$	$\frac{8.5}{14}$	$\frac{8.4}{15}$	$\frac{7.5}{16}$	$\frac{8.8}{33}$
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Sta. + H.I. - Elev.

917.34

+50

84

+45

85

T.P. 3.04 909.48 10.94 906.42

+46

86

T.P. 5.45 905.31 9.62 899.86

87

88

89

90

91

T.P. 7.57 909.36 3.52 901.79

92

93

$\frac{4.2}{33}$	$\frac{4.7}{24}$	$\frac{9.1}{31}$	$\frac{8.6}{14}$	8.0	$\frac{8.5}{12}$	$\frac{9.3}{14}$	$\frac{9.5}{16}$	$\frac{8.4}{17}$	$\frac{9.4}{33}$
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$\frac{4.3}{33}$	$\frac{5.2}{26}$	$\frac{9.6}{19}$	$\frac{9.0}{12}$	8.8	$\frac{9.3}{11}$	$\frac{9.9}{13}$	$\frac{10.2}{17}$	$\frac{9.5}{21}$	$\frac{8.0}{22}$	$\frac{8.6}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{4.9}{33}$	$\frac{4.0}{24}$	$\frac{11.5}{20}$	$\frac{10.5}{15}$	$\frac{9.8}{12}$	7.4	$\frac{9.9}{12}$	$\frac{10.9}{14}$	$\frac{11.0}{20}$	$\frac{8.9}{23}$	$\frac{7.0}{26}$	$\frac{7.3}{33}$
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$\frac{6.5}{33}$	$\frac{7.5}{26}$	$\frac{10.5}{24}$	$\frac{12.0}{20}$	$\frac{11.7}{13}$	10.9	$\frac{11.3}{12}$	$\frac{12.6}{13}$	$\frac{13.2}{23}$	$\frac{11.5}{31}$	$\frac{10.4}{33}$
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$\frac{1.0}{33}$	$\frac{1.5}{26}$	$\frac{5.4}{20}$	$\frac{5.5}{15}$	$\frac{4.7}{12}$	4.5	$\frac{5.0}{13}$	$\frac{5.8}{15}$	$\frac{5.4}{22}$	$\frac{2.6}{26}$	$\frac{2.6}{33}$
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$\frac{7.5}{33}$	$\frac{7.2}{16}$	$\frac{6.6}{14}$	6.0	$\frac{6.6}{13}$	$\frac{7.2}{15}$	$\frac{7.6}{33}$
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Nail in T.R. 14. Sta. 86+80

$\frac{7.4}{33}$	$\frac{7.2}{18}$	$\frac{5.5}{14}$	$\frac{4.4}{9}$	4.0	$\frac{4.4}{11}$	$\frac{7.2}{17}$	$\frac{7.5}{33}$
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$\frac{7.2}{33}$	$\frac{7.1}{16}$	$\frac{5.4}{13}$	$\frac{5.0}{10}$	4.6	$\frac{4.8}{10}$	$\frac{5.2}{13}$	$\frac{7.3}{18}$	$\frac{7.2}{33}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{4.9}{33}$	$\frac{6.9}{16}$	$\frac{5.4}{13}$	$\frac{5.0}{9}$	4.5	$\frac{4.6}{11}$	$\frac{5.5}{14}$	$\frac{6.8}{17}$	$\frac{7.3}{33}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

$\frac{6.6}{33}$	$\frac{6.8}{17}$	$\frac{4.9}{13}$	$\frac{4.5}{9}$	4.0	$\frac{4.4}{10}$	$\frac{5.1}{14}$	$\frac{4.8}{17}$	$\frac{7.3}{33}$
------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------

$\frac{6.8}{33}$	$\frac{6.3}{17}$	$\frac{4.0}{13}$	$\frac{3.7}{9}$	3.2	$\frac{3.5}{11}$	$\frac{3.8}{14}$	$\frac{5.7}{18}$	$\frac{5.6}{33}$
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$\frac{10.7}{33}$	$\frac{9.9}{19}$	$\frac{7.6}{13}$	6.6	$\frac{7.2}{13}$	$\frac{8.1}{15}$	$\frac{8.2}{20}$	$\frac{7.6}{24}$	$\frac{7.2}{33}$
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$\frac{8.9}{33}$	$\frac{8.2}{17}$	$\frac{6.7}{14}$	5.8	$\frac{6.3}{11}$	$\frac{7.1}{14}$	$\frac{7.1}{18}$	$\frac{4.7}{10}$	$\frac{3.9}{33}$
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Sta. + H.I. - Elev.

909.34

94

95

T.P. 7.45 913.53 3.28 906.08

96

B.M. 3.44 913.55 3.44 910.09 910.11

+50

97

+34

+50

98

+50

99

+50

+66

100

2/14/25

$$\begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 13 \end{array} \quad 4.7 \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 6.1 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 2.3 \\ 22 \end{array} \quad \begin{array}{r} 1.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 22 \end{array} \quad \begin{array}{r} 5.8 \\ 20 \end{array} \quad \begin{array}{r} 5.7 \\ 15 \end{array} \quad \begin{array}{r} 4.7 \\ 14 \end{array} \quad 3.5 \quad \begin{array}{r} 4.0 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad \begin{array}{r} 4.3 \\ 20 \end{array} \quad \begin{array}{r} 1.4 \\ 24 \end{array} \quad \begin{array}{r} 0.8 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 8.4 \\ 14 \end{array} \quad \begin{array}{r} 7.8 \\ 13 \end{array} \quad 7.0 \quad \begin{array}{r} 7.4 \\ 13 \end{array} \quad \begin{array}{r} 7.9 \\ 15 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \end{array} \quad \begin{array}{r} 5.8 \\ 23 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

SPX in 10" Oak 40' Pt. 5th 96 + 40.

$$\begin{array}{r} 3.4 \\ 33 \end{array} \quad \begin{array}{r} 3.3 \\ 21 \end{array} \quad \begin{array}{r} 6.6 \\ 19 \end{array} \quad \begin{array}{r} 7.1 \\ 9 \end{array} \quad 6.5 \quad \begin{array}{r} 6.8 \\ 8 \end{array} \quad \begin{array}{r} 7.1 \\ 14 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 26 \end{array} \quad \begin{array}{r} 3.4 \\ 30 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 3.7 \\ 33 \end{array} \quad \begin{array}{r} 3.6 \\ 12 \end{array} \quad \begin{array}{r} 7.8 \\ 6 \end{array} \quad 6.8 \quad \begin{array}{r} 6.2 \\ 15 \end{array} \quad \begin{array}{r} 6.6 \\ 23 \end{array} \quad \begin{array}{r} 8.1 \\ 28 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 2.5 \\ 43 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 3.4 \\ 20 \end{array} \quad \begin{array}{r} 4.2 \\ 5 \end{array} \quad 7.8 \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 6.1 \\ 27 \end{array} \quad \begin{array}{r} 6.3 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \end{array} \quad 4.5 \quad \begin{array}{r} 7.8 \\ 5 \end{array} \quad \begin{array}{r} 8.0 \\ 19 \end{array} \quad \begin{array}{r} 7.0 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 4.9 \\ 14 \end{array} \quad 4.8 \quad \begin{array}{r} 4.3 \\ 21 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad 6.0 \quad \begin{array}{r} 5.3 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad 7.4 \quad \begin{array}{r} 7.6 \\ 14 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad 7.4 \quad \begin{array}{r} 7.8 \\ 5 \end{array} \quad \begin{array}{r} 8.4 \\ 7 \end{array} \quad \begin{array}{r} 9.2 \\ 9 \end{array} \quad \begin{array}{r} 9.4 \\ 13 \end{array} \quad \begin{array}{r} 8.1 \\ 17 \end{array} \quad \begin{array}{r} 7.6 \\ 31 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 7.7 \\ 3 \end{array} \quad 8.9 \quad \begin{array}{r} 8.8 \\ 4 \end{array} \quad \begin{array}{r} 8.4 \\ 8 \end{array} \quad \begin{array}{r} 7.6 \\ 22 \end{array} \quad \begin{array}{r} 8.0 \\ 33 \end{array}$$

$$\begin{array}{r} 5.6 \\ 33 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 9.6 \\ 10 \end{array} \quad \begin{array}{r} 9.0 \\ 5 \end{array} \quad \begin{array}{r} 8.1 \\ 3 \end{array} \quad 7.9 \quad \begin{array}{r} 7.5 \\ 11 \end{array} \quad \begin{array}{r} 7.9 \\ 21 \end{array} \quad \begin{array}{r} 8.1 \\ 24 \end{array} \quad \begin{array}{r} 9.2 \\ 33 \end{array}$$

Sta. + H.I. - E/cv.

913.55

+50

101

T.P. 5.26 911.27 7.54 706.01

+50

102

+48

103

+27

104

+45

T.P. 10.99 911.01 1.25 910.02

105

+70

106

107

T.P. 10.66 929.24 2.43 918.58

2/14/25

$\frac{5.4}{33}$	$\frac{4.0}{24}$	$\frac{8.8}{19}$	$\frac{8.8}{14}$	$\frac{7.9}{12}$	7.3	$\frac{7.7}{8}$	$\frac{7.7}{12}$	$\frac{8.3}{14}$	$\frac{8.3}{14}$	$\frac{7.4}{19}$	$\frac{7.8}{33}$
------------------	------------------	------------------	------------------	------------------	-------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.0}{33}$	$\frac{6.0}{25}$	$\frac{9.1}{21}$	$\frac{9.0}{18}$	$\frac{7.9}{14}$	7.3	$\frac{7.5}{9}$	$\frac{8.1}{11}$	$\frac{7.9}{13}$	$\frac{7.2}{15}$	$\frac{7.2}{33}$
------------------	------------------	------------------	------------------	------------------	-------	-----------------	------------------	------------------	------------------	------------------

$\frac{4.0}{33}$	$\frac{5.9}{25}$	$\frac{7.4}{23}$	$\frac{7.1}{20}$	$\frac{5.5}{14}$	$\frac{4.9}{5}$	4.9	$\frac{5.4}{8}$	$\frac{6.6}{11}$	$\frac{6.3}{14}$	$\frac{6.8}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-------	-----------------	------------------	------------------	------------------

$\frac{6.3}{33}$	$\frac{6.4}{15}$	$\frac{7.4}{23}$	$\frac{7.6}{21}$	$\frac{6.9}{19}$	$\frac{5.8}{15}$	$\frac{5.0}{7}$	5.1	$\frac{5.3}{4}$	$\frac{5.7}{9}$	$\frac{7.3}{13}$	$\frac{8.9}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-------	-----------------	-----------------	------------------	------------------

$\frac{5.9}{33}$	$\frac{6.2}{26}$	$\frac{7.5}{23}$	$\frac{7.5}{22}$	$\frac{6.8}{20}$	$\frac{5.7}{14}$	$\frac{5.0}{5}$	5.1	$\frac{5.5}{8}$	$\frac{7.5}{13}$	$\frac{9.0}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-------	-----------------	------------------	------------------

$\frac{7.9}{33}$	$\frac{7.2}{20}$	$\frac{5.4}{15}$	$\frac{4.8}{4}$	5.0	$\frac{5.4}{4}$	$\frac{6.0}{9}$	$\frac{9.2}{14}$	$\frac{9.8}{33}$
------------------	------------------	------------------	-----------------	-------	-----------------	-----------------	------------------	------------------

$\frac{7.0}{33}$	$\frac{8.7}{14}$	$\frac{7.1}{20}$	$\frac{5.2}{14}$	$\frac{4.7}{5}$	4.8	$\frac{5.1}{4}$	$\frac{5.8}{10}$	$\frac{8.5}{16}$	$\frac{7.8}{33}$
------------------	------------------	------------------	------------------	-----------------	-------	-----------------	------------------	------------------	------------------

$\frac{6.2}{33}$	$\frac{5.6}{20}$	$\frac{3.6}{19}$	$\frac{3.1}{5}$	3.2	$\frac{3.7}{8}$	$\frac{5.6}{14}$	$\frac{5.7}{23}$	$\frac{5.7}{28}$	$\frac{6.5}{33}$
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$\frac{1.7}{33}$	$\frac{1.6}{26}$	$\frac{4.3}{22}$	$\frac{4.2}{19}$	$\frac{2.5}{15}$	$\frac{2.0}{5}$	2.0	$\frac{2.6}{8}$	$\frac{4.7}{15}$	$\frac{4.7}{19}$	$\frac{1.9}{23}$	$\frac{1.8}{27}$	$\frac{2.7}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.2}{33}$	$\frac{6.7}{17}$	$\frac{11.5}{20}$	$\frac{10.4}{17}$	$\frac{9.8}{4}$	10.0	$\frac{10.6}{8}$	$\frac{12.5}{14}$	$\frac{12.7}{17}$	$\frac{8.3}{23}$	$\frac{8.4}{33}$
------------------	------------------	-------------------	-------------------	-----------------	--------	------------------	-------------------	-------------------	------------------	------------------

$\frac{7.2}{33}$	$\frac{7.3}{26}$	$\frac{8.8}{24}$	$\frac{8.7}{19}$	$\frac{7.6}{4}$	7.7	$\frac{8.1}{6}$	$\frac{8.7}{11}$	$\frac{8.5}{33}$
------------------	------------------	------------------	------------------	-----------------	-------	-----------------	------------------	------------------

$\frac{7.4}{33}$	$\frac{7.7}{15}$	$\frac{8.4}{21}$	$\frac{7.2}{14}$	$\frac{6.8}{5}$	6.9	$\frac{7.4}{4}$	$\frac{8.0}{8}$	$\frac{7.7}{33}$
------------------	------------------	------------------	------------------	-----------------	-------	-----------------	-----------------	------------------

$\frac{5.4}{33}$	$\frac{5.7}{21}$	$\frac{4.8}{17}$	$\frac{4.2}{5}$	4.4	$\frac{4.7}{4}$	$\frac{6.6}{11}$	$\frac{6.1}{33}$
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Sta.	+	H.I.	-	E/cv.	
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929.24

B.M.	3.95	929.62	3.58	925.66	925.67
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108

+44

109

110

+14

111

112

+59

113

T.R	0.08	918.83	10.87	918.75	
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114

115

114

2/14/23

SpK. in 30" OqK 40' Lt. Stg. 111+10.

9.8	10.7	10.0	9.7	10.5	12.6	12.4
33	40	18	7.10.1	6	9	33

<u>7.6</u>	<u>8.3</u>	<u>9.1</u>	<u>9.1</u>	<u>8.4</u>	<u>8.1</u>		<u>8.6</u>	<u>9.4</u>	<u>9.0</u>	<u>8.7</u>
33	24	21	19	14	4	8.4	3	7	11	33

<u>5.2</u>	<u>5.7</u>	<u>6.9</u>	<u>6.6</u>	<u>6.3</u>		<u>6.7</u>	<u>7.4</u>	<u>4.4</u>	<u>3.8</u>
3.3	2.5	1.9	1.8	7	6.7	4	6	11	3.3

<u>2.6</u>	<u>3.1</u>	<u>6.0</u>	<u>6.1</u>	<u>5.2</u>	<u>5.0</u>		<u>5.6</u>	<u>6.1</u>	<u>5.7</u>	<u>2.3</u>	<u>2.6</u>
33	28	24	22	19	8	5.4	3	6	8	10	33

<u>2.3</u>	<u>2.5</u>	<u>5.7</u>	<u>5.7</u>	<u>5.1</u>	<u>4.8</u>		<u>4.9</u>	<u>5.5</u>	<u>5.4</u>	<u>2.6</u>	<u>3.2</u>
2.3	2.8	2.5	2.1	1.9	7	5.1	4	4	9	11	3.3

$\frac{4.9}{33}$	$\frac{4.8}{24}$	$\frac{5.7}{22}$	$\frac{5.7}{20}$	$\frac{5.4}{18}$	$\frac{4.7}{8}$	$\frac{4.6}{3}$	$\frac{5.2}{4}$	$\frac{5.2}{7}$	$\frac{3.5}{10}$	$\frac{3.2}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------

<u>6.0</u>	<u>5.9</u>	<u>7.6</u>	<u>7.8</u>	<u>7.1</u>	<u>6.7</u>		<u>7.0</u>	<u>7.8</u>	<u>7.6</u>	<u>6.7</u>	<u>6.8</u>
<u>33</u>	<u>14</u>	<u>22</u>	<u>10</u>	<u>18</u>	<u>7</u>	<u>6.9</u>	<u>3</u>	<u>6</u>	<u>8</u>	<u>10</u>	<u>33</u>

<u>8.3</u>	<u>8.8</u>	<u>9.6</u>	<u>9.6</u>	<u>9.0</u>	<u>8.2</u>		<u>8.5</u>	<u>9.4</u>	<u>9.3</u>	<u>8.2</u>	<u>7.5</u>
33	24	23	21	19	7	8.4	4	6	8	10	33

$\frac{9.1}{33} \quad \frac{9.6}{24} \quad \frac{10.4}{22} \quad \frac{10.3}{19} \quad \frac{9.7}{17} \quad \frac{9.2}{6} \quad 9.4$ $\frac{9.4}{5} \quad \frac{10.3}{7} \quad \frac{10.1}{9} \quad \frac{9.6}{11} \quad \frac{9.0}{33}$

<u>1.8</u>	1.8	<u>2.7</u>	<u>2.6</u>	<u>1.9</u>	<u>1.3</u>		<u>1.4</u>	<u>2.6</u>	<u>2.6</u>	<u>1.9</u>	<u>2.0</u>
33	23	22	20	18	7	1.4	5	9	10	12	33

<u>5.3</u>	<u>4.9</u>	<u>4.1</u>	<u>3.7</u>		<u>4.1</u>	<u>5.4</u>	<u>5.4</u>	<u>4.9</u>	<u>4.8</u>
33	20	17	6	3.8	7	10	12	14	33

$\frac{7.9}{33}$ $\frac{7.8}{25}$ $\frac{7.7}{21}$ $\frac{6.8}{18}$ $\frac{6.0}{6}$ 6.0 $\frac{6.3}{7}$ $\frac{7.2}{10}$ $\frac{7.3}{13}$ $\frac{6.6}{14}$ $\frac{6.4}{33}$

5+9. + H.I. - E/cy

918.83

117

118

T.P. 3.77 913.35 9.25 909.58

119

+37

120

+58

121

122

123

124

B.M. 6.53 913.77 5.93 907.42 907.44

125

124

+50

2/16/25

$\frac{7.0}{33}$	$\frac{8.1}{22}$	$\frac{9.2}{21}$	$\frac{9.2}{19}$	$\frac{8.3}{17}$	$\frac{7.6}{5}$	7.7	$\frac{8.1}{8}$	$\frac{8.8}{10}$	$\frac{8.6}{12}$	$\frac{8.2}{14}$	$\frac{7.6}{33}$
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$\frac{10.2}{33}$	$\frac{10.1}{23}$	$\frac{10.7}{22}$	$\frac{10.8}{19}$	$\frac{9.5}{17}$	$\frac{8.7}{5}$	8.7	$\frac{9.0}{8}$	$\frac{10.1}{10}$	$\frac{10.4}{13}$	$\frac{9.4}{15}$	$\frac{8.9}{33}$
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$\frac{7.0}{33}$	$\frac{6.6}{22}$	$\frac{4.5}{14}$	$\frac{3.8}{5}$	3.9	$\frac{4.3}{8}$	$\frac{6.3}{12}$	$\frac{6.2}{14}$	$\frac{5.5}{15}$	$\frac{5.0}{33}$
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$\frac{6.8}{33}$	$\frac{6.4}{21}$	$\frac{4.2}{15}$	$\frac{3.7}{4}$	3.8	$\frac{4.3}{9}$	$\frac{5.7}{13}$	$\frac{5.4}{20}$	$\frac{4.9}{22}$	$\frac{5.1}{33}$
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$\frac{4.1}{33}$	$\frac{3.9}{29}$	$\frac{6.2}{24}$	$\frac{6.7}{23}$	$\frac{5.7}{19}$	$\frac{4.3}{15}$	$\frac{3.7}{4}$	3.8	$\frac{4.2}{8}$	$\frac{5.6}{12}$	$\frac{5.6}{19}$	$\frac{1.9}{24}$	$\frac{1.9}{33}$
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$\frac{4.8}{33}$	$\frac{4.7}{28}$	$\frac{6.5}{25}$	$\frac{6.9}{21}$	$\frac{6.3}{19}$	$\frac{4.6}{15}$	$\frac{4.2}{3}$	4.3	$\frac{4.7}{8}$	$\frac{5.8}{12}$	$\frac{6.2}{14}$	$\frac{6.0}{18}$	$\frac{5.2}{33}$
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$\frac{6.8}{33}$	$\frac{6.5}{24}$	$\frac{6.8}{23}$	$\frac{6.8}{20}$	$\frac{5.0}{15}$	$\frac{4.4}{3}$	4.5	$\frac{4.9}{9}$	$\frac{6.0}{12}$	$\frac{6.2}{15}$	$\frac{5.7}{17}$	$\frac{5.5}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------

$\frac{6.6}{33}$	$\frac{5.9}{21}$	$\frac{6.5}{19}$	$\frac{6.2}{17}$	$\frac{5.2}{14}$	$\frac{4.8}{3}$	4.9	$\frac{5.1}{10}$	$\frac{6.2}{13}$	$\frac{6.4}{15}$	$\frac{5.0}{17}$	$\frac{5.2}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{6.7}{33}$	$\frac{6.6}{22}$	$\frac{7.4}{21}$	$\frac{7.3}{17}$	$\frac{6.3}{15}$	$\frac{5.4}{3}$	5.5	$\frac{5.9}{10}$	$\frac{6.9}{12}$	$\frac{7.0}{15}$	$\frac{6.0}{18}$	$\frac{5.6}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{6.6}{33}$	$\frac{6.7}{21}$	$\frac{7.6}{19}$	$\frac{7.3}{14}$	$\frac{6.5}{14}$	5.8	$\frac{6.1}{9}$	$\frac{7.3}{12}$	$\frac{7.2}{14}$	$\frac{6.5}{17}$	$\frac{6.1}{33}$
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Spk. in T.P. Pt. Sta. 125 + 07.

$\frac{8.0}{33}$	$\frac{8.8}{19}$	$\frac{8.3}{18}$	$\frac{8.1}{14}$	$\frac{7.5}{15}$	6.9	$\frac{7.4}{11}$	$\frac{8.6}{13}$	$\frac{8.6}{15}$	$\frac{7.7}{17}$	$\frac{7.2}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{8.9}{33}$	$\frac{8.8}{14}$	$\frac{7.7}{12}$	7.0	$\frac{7.7}{10}$	$\frac{8.7}{13}$	$\frac{8.6}{14}$	$\frac{7.7}{19}$	$\frac{7.2}{33}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{8.1}{33}$	$\frac{7.8}{17}$	$\frac{8.5}{14}$	$\frac{8.5}{14}$	$\frac{7.5}{12}$	6.7	$\frac{7.5}{10}$	$\frac{8.9}{14}$	$\frac{8.8}{17}$	$\frac{6.5}{22}$	$\frac{5.8}{33}$
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Sta.	+	H.I.	-	Elev
		713.97		

127

+25

+37

+50

128

+50

129

+50

+81

130

+50

131

T.P.	3.39	708.84	8.52	705.45
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+33

2/16/25

$$\begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 8.4 \\ 24 \end{array} \quad \begin{array}{r} 8.8 \\ 25 \end{array} \quad \begin{array}{r} 7.6 \\ 20 \end{array} \quad \begin{array}{r} 6.8 \\ 9 \end{array} \quad 7.2 \quad \begin{array}{r} 7.5 \\ 5 \end{array} \quad \begin{array}{r} 8.7 \\ 8 \end{array} \quad \begin{array}{r} 8.6 \\ 12 \end{array} \quad \begin{array}{r} 6.3 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 9.1 \\ 33 \end{array} \quad \begin{array}{r} 7.6 \\ 29 \end{array} \quad \begin{array}{r} 6.9 \\ 15 \end{array} \quad 7.8 \quad \begin{array}{r} 8.9 \\ 4 \end{array} \quad \begin{array}{r} 8.9 \\ 11 \end{array} \quad \begin{array}{r} 6.8 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.6 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 7.6 \\ 7 \end{array} \quad \begin{array}{r} 8.5 \\ 4 \end{array} \quad 9.0 \quad \begin{array}{r} 8.5 \\ 3 \end{array} \quad \begin{array}{r} 6.9 \\ 7 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.4 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 24 \end{array} \quad \begin{array}{r} 7.7 \\ 12 \end{array} \quad \begin{array}{r} 8.7 \\ 7 \end{array} \quad \begin{array}{r} 7.8 \\ 5 \end{array} \quad 7.2 \quad \begin{array}{r} 7.0 \\ 4 \end{array} \quad \begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 25 \end{array} \quad \begin{array}{r} 5.8 \\ 17 \end{array} \quad 5.2 \quad \begin{array}{r} 5.1 \\ 16 \end{array} \quad \begin{array}{r} 4.4 \\ 23 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 4.5 \\ 14 \end{array} \quad 3.6 \quad \begin{array}{r} 2.9 \\ 16 \end{array} \quad \begin{array}{r} 2.6 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad 3.7 \quad \begin{array}{r} 3.5 \\ 16 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 6.9 \\ 13 \end{array} \quad \begin{array}{r} 6.4 \\ 7 \end{array} \quad 4.7 \quad \begin{array}{r} 3.7 \\ 12 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 20 \end{array} \quad \begin{array}{r} 6.9 \\ 12 \end{array} \quad 7.4 \quad \begin{array}{r} 6.7 \\ 4 \end{array} \quad \begin{array}{r} 5.9 \\ 12 \end{array} \quad \begin{array}{r} 4.3 \\ 23 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.1 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 27 \end{array} \quad \begin{array}{r} 6.6 \\ 22 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} 7.1 \\ 5 \end{array} \quad 7.3 \quad \begin{array}{r} 7.6 \\ 5 \end{array} \quad \begin{array}{r} 7.1 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 28 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} 5.4 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 19 \end{array} \quad \begin{array}{r} 7.7 \\ 13 \end{array} \quad \begin{array}{r} 7.2 \\ 8 \end{array} \quad 7.1 \quad \begin{array}{r} 8.7 \\ 18 \end{array} \quad \begin{array}{r} 7.5 \\ 33 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 18 \end{array} \quad \begin{array}{r} 8.8 \\ 11 \end{array} \quad \begin{array}{r} 8.6 \\ 5 \end{array} \quad 8.0 \quad \begin{array}{r} 9.1 \\ 14 \end{array} \quad \begin{array}{r} 9.8 \\ 17 \end{array} \quad \begin{array}{r} 10.4 \\ 24 \end{array} \quad \begin{array}{r} 9.6 \\ 27 \end{array} \quad \begin{array}{r} 10.3 \\ 33 \end{array}$$

$$\begin{array}{r} 3.1 \\ 33 \end{array} \quad \begin{array}{r} 4.1 \\ 17 \end{array} \quad \begin{array}{r} 3.9 \\ 13 \end{array} \quad \begin{array}{r} 3.6 \\ 8 \end{array} \quad 3.2 \quad \begin{array}{r} 3.8 \\ 4 \end{array} \quad \begin{array}{r} 4.7 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array}$$

Sta. + H.I. - E/ev.

708.84

132

133

+57

134

135

136

T.P. 6.53 707.47 7.90 900.94

137

138

139

140

141

142

P.M. 8.68 911.74 4.41 903.04 903.04

+58.2

2/14/25

7.7	8.0	8.0	6.3	4.6	4.7	5.9	8.5	8.9	8.7
33	24	17	13	4	4.5	5	13	18	33

7.7	7.5	7.4	7.0	5.4	5.1	6.0	6.7	6.2
33	23	18	15	9	4.7	8	12	15

6.0	5.5	5.2	5.3	5.7	6.0	4.7	5.6
33	10	7	4.7	8	12	14	18

6.2	6.1	5.7	5.6	6.6	7.3	6.8	6.9
33	11	7	5.3	7	12	15	17

8.6	8.7	8.9	8.0	6.8	6.9	7.9	8.7	9.2
33	20	14	14	7	6.5	8	12	14

9.4	9.3	8.6	8.0	7.7	8.7	9.2	9.3
33	17	13	4	7.4	7	11	19

8.0	8.1	7.6	6.6	6.8	7.3	8.1	8.2	7.9	8.7	8.7	7.9
33	20	12	7	6.5	7	10	13	14	31	31.5	33.5

7.4	7.5	5.8	5.9	6.4	7.5	7.8	8.3	8.3	7.8
33	17	7	5.5	4	10	14	31	31.5	33.5

4.9	5.5	6.4	6.5	5.2	5.3	6.4	7.0	7.9	7.9	7.0
33	22	18	13	8	5.0	7	11	31	31.5	33.5

4.9	5.7	6.0	6.3	5.0	5.1	6.1	7.2	8.0	8.0	7.2
33	22	17	15	8	4.7	7	12	30	30.5	32.5

6.6	7.2	7.2	6.6	6.7	5.6	6.4	7.1	7.4	8.0	8.0	7.4
33	23	17	13	9	5.2	7	9	13	30	31.5	32.5

7.1	7.4	6.4	5.9	5.9	6.8	7.1	7.1	8.2	8.2	7.1
33	17	13	9	5.4	8	12	20	30	30.5	32.5

SpK. in 30" D.K. 40' RT. ST. 14.5 + 5.0

7.5	9.5	7.1	8.7
33	16	7.2	14

Sta. + H.I. - Elev.

911.74

+56

143

144

145

+50

T.P. 9.17 918.80 2.11 909.63

146

147

+50

148

+40

149

150

T.P. 9.52 926.91 1.41 917.39

151

2/17/25

$\frac{11.0}{33}$	$\frac{10.9}{20}$	$\frac{10.3}{17}$	$\frac{10.0}{10}$		$\frac{8.9}{11}$	$\frac{10.8}{19}$	$\frac{10.6}{33}$
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$\frac{11.4}{33}$	$\frac{11.6}{17}$	$\frac{11.4}{10}$	$\frac{10.2}{8}$	$\frac{10.2}{6}$	$\frac{10.0}{10.0}$	$\frac{11.5}{7}$	$\frac{11.4}{10}$	$\frac{11.3}{12}$	$\frac{11.3}{24}$	$\frac{11.0}{26}$	$\frac{10.8}{33}$
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$\frac{11.4}{33}$	$\frac{11.2}{17}$	$\frac{11.1}{12}$	$\frac{10.1}{9}$	$\frac{9.5}{7}$	$\frac{9.4}{9.4}$	$\frac{10.1}{8}$	$\frac{10.7}{10}$	$\frac{10.7}{14}$	$\frac{10.2}{19}$	$\frac{10.0}{33}$
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$\frac{10.8}{33}$	$\frac{10.6}{17}$	$\frac{10.2}{12}$	$\frac{8.4}{9}$	$\frac{8.3}{8.3}$	$\frac{8.0}{3}$	$\frac{8.6}{7}$	$\frac{8.4}{18}$	$\frac{7.3}{33}$
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$\frac{8.3}{33}$	$\frac{6.7}{14}$	$\frac{6.5}{8}$	$\frac{6.4}{6.4}$	$\frac{6.2}{2}$	$\frac{6.6}{4}$	$\frac{6.5}{9}$	$\frac{6.6}{12}$	$\frac{4.6}{16}$	$\frac{3.3}{33}$
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$\frac{12.0}{33}$	$\frac{11.0}{18}$	$\frac{11.8}{14}$	$\frac{11.7}{14}$	$\frac{11.2}{7}$	$\frac{11.2}{11.2}$	$\frac{11.1}{9}$	$\frac{10.4}{15}$	$\frac{8.3}{18}$	$\frac{6.8}{33}$
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$\frac{4.2}{33}$	$\frac{6.0}{21}$	$\frac{6.7}{17}$	$\frac{7.2}{15}$	$\frac{7.1}{9}$	$\frac{7.4}{2}$	$\frac{8.3}{8.3}$	$\frac{8.7}{2}$	$\frac{8.8}{7}$	$\frac{8.9}{12}$	$\frac{3.3}{17}$	$\frac{3.3}{33}$
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$\frac{4.5}{33}$	$\frac{4.6}{17}$	$\frac{5.6}{15}$	$\frac{5.6}{10}$	$\frac{6.0}{2}$	$\frac{6.5}{6.5}$	$\frac{7.5}{3}$	$\frac{7.9}{7}$	$\frac{7.7}{11}$	$\frac{1.8}{16}$	$\frac{1.4}{33}$
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$\frac{5.4}{33}$	$\frac{4.9}{17}$	$\frac{5.3}{14}$	$\frac{4.9}{5}$	$\frac{4.9}{4.9}$	$\frac{4.7}{8}$	$\frac{5.2}{9}$	$\frac{5.6}{13}$	$\frac{3.3}{16}$	$\frac{3.2}{33}$
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$\frac{6.3}{33}$	$\frac{6.0}{20}$	$\frac{5.7}{17}$	$\frac{5.2}{14}$	$\frac{4.8}{7}$	$\frac{5.0}{5.0}$	$\frac{4.8}{6}$	$\frac{5.0}{10}$	$\frac{4.7}{33}$
------------------	------------------	------------------	------------------	-----------------	-------------------	-----------------	------------------	------------------

$\frac{5.9}{33}$	$\frac{5.6}{20}$	$\frac{4.8}{14}$	$\frac{4.8}{8}$	$\frac{4.8}{4.8}$	$\frac{4.9}{7}$	$\frac{6.7}{11}$	$\frac{6.0}{33}$
------------------	------------------	------------------	-----------------	-------------------	-----------------	------------------	------------------

$\frac{3.9}{33}$	$\frac{4.0}{24}$	$\frac{4.2}{10}$	$\frac{4.0}{4.0}$	$\frac{5.0}{14}$	$\frac{5.4}{33}$
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$\frac{9.9}{33}$	$\frac{10.0}{26}$	$\frac{9.9}{14}$	$\frac{10.2}{12}$	$\frac{10.5}{10.5}$	$\frac{10.7}{8}$	$\frac{11.0}{18}$	$\frac{10.7}{33}$
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Sta.	+	H.I.	-	Elev.
		724.91		

152

153

+60

154

B.M.	10.24	734.94	2.21	724.70	724.70
+40					

155

156

157

158

+50

159

+50

T.P.	7.84	735.17	7.57	727.37
160				

2/17/25

$\frac{8.5}{33}$ $\frac{8.7}{32}$ $\frac{8.5}{16}$ $\frac{8.7}{10}$ 8.6 $\frac{9.3}{7}$ $\frac{9.4}{17}$ $\frac{8.9}{33}$

$\frac{6.2}{33}$ $\frac{5.9}{13}$ 5.5 $\frac{6.3}{7}$ $\frac{6.3}{18}$ $\frac{6.1}{33}$

$\frac{5.9}{33}$ $\frac{3.7}{13}$ 3.4 $\frac{4.3}{8}$ $\frac{4.3}{18}$ $\frac{4.1}{33}$

$\frac{1.7}{33}$ $\frac{1.8}{14}$ $\frac{1.9}{3}$ $\frac{1.3}{2}$ 0.9 $\frac{1.7}{8}$ $\frac{2.5}{19}$ $\frac{1.9}{33}$

SpK. in T. 10. Mt. St. 9. 153 + 85
 $\frac{9.0}{33}$ $\frac{8.8}{24}$ $\frac{8.4}{16}$ $\frac{8.4}{5}$ 7.8 $\frac{9.0}{11}$ $\frac{9.0}{14}$ $\frac{9.3}{17}$ $\frac{9.6}{33}$

$\frac{8.7}{33}$ $\frac{8.3}{18}$ $\frac{7.3}{11}$ $\frac{7.0}{4}$ 6.8 $\frac{7.4}{10}$ $\frac{5.8}{13}$ $\frac{5.1}{33}$

$\frac{10.2}{33}$ $\frac{8.1}{14}$ $\frac{8.4}{13}$ $\frac{8.0}{11}$ $\frac{6.4}{4}$ 6.3 $\frac{6.8}{11}$ $\frac{5.5}{14}$ $\frac{4.6}{33}$

$\frac{7.3}{33}$ $\frac{6.9}{21}$ $\frac{7.1}{12}$ $\frac{7.8}{11}$ $\frac{6.9}{7}$ 6.6 $\frac{6.5}{7}$ $\frac{7.4}{12}$ $\frac{6.2}{14}$ $\frac{5.4}{33}$

$\frac{9.0}{33}$ $\frac{8.3}{20}$ $\frac{8.7}{14}$ $\frac{7.3}{12}$ $\frac{9.2}{10}$ $\frac{8.5}{8}$ 8.1 $\frac{8.2}{9}$ $\frac{8.4}{12}$ $\frac{8.4}{15}$ $\frac{6.5}{20}$ $\frac{6.4}{33}$

$\frac{10.0}{33}$ $\frac{9.2}{17}$ $\frac{9.3}{13}$ $\frac{7.0}{8}$ 8.3 $\frac{8.5}{8}$ $\frac{8.9}{10}$ $\frac{9.1}{14}$ $\frac{8.8}{18}$ $\frac{8.0}{23}$ $\frac{8.1}{33}$

$\frac{9.5}{33}$ $\frac{8.8}{17}$ $\frac{9.1}{10}$ $\frac{8.5}{8}$ 8.2 $\frac{8.9}{10}$ $\frac{8.0}{15}$ $\frac{7.5}{21}$ $\frac{7.3}{33}$

$\frac{7.7}{33}$ $\frac{8.0}{19}$ $\frac{8.0}{12}$ $\frac{8.6}{10}$ $\frac{7.8}{7}$ 7.3 $\frac{7.5}{4}$ $\frac{7.7}{13}$ $\frac{6.6}{14}$ $\frac{5.7}{22}$ $\frac{5.6}{33}$

$\frac{7.2}{33}$ $\frac{8.5}{21}$ $\frac{7.9}{12}$ $\frac{8.4}{11}$ $\frac{7.8}{8}$ 7.1 $\frac{6.9}{5}$ $\frac{7.1}{12}$ $\frac{6.6}{14}$ $\frac{5.5}{21}$ $\frac{5.5}{33}$

Sta. + H.I. - E/cv.

935.19

141

+40

142

+70

143

+50

144

+50

145

+29

T.P. 5.67 731.05 7.81 925.38

146

B.M. 4.10 932.41 2.52 928.53 928.51

+50

147

2/17/25

5.5	4.0	4.7	3.9		4.1	4.6	4.6	4.0	4.4
33	12	11	3	4.0	10	12	13	15	33

5.0	3.8	3.9	4.2	3.2		3.4	3.9	4.2	3.8	3.3	3.8
33	14	12	10	3	3.2	8	12	13	15	20	33

4.9	4.4	4.5	4.9	5.1	4.5		4.1	4.3	4.7	4.0	3.5	4.2	4.2
33	19	11	10	8	5	4.1	8	12	13	15	18	22	33

6.6	6.0	6.2	6.9	6.4	6.1	5.7		6.2	5.8	6.3	5.6	5.6
33	18	13	9	7	4	2	5.7	9	11	14	17	33

6.6	6.2	6.4	6.6	6.4		5.9	5.7	6.4	5.7	6.4	6.2
33	18	12	10	8	5.7	9	10	14	18	28	33

6.6	5.8	4.9	5.5	6.7	6.0	5.3		5.7	5.3	6.0	5.4	6.4	6.0
33	23	18	14	12	5	3	5.4	7	7	14	21	29	33

7.7	6.5	5.2	5.8	5.5		5.0	4.5	4.2	3.9
33	25	19	16	6	4.8	8	9	17	33

1.5
33

7.3	4.8	4.5	4.7		4.6	4.0	4.1	4.7	5.2	5.4	1.9
33	20	15	5	4.4	7	8	12	15	17	22	25

7.9	6.6	4.6	4.9	5.6		5.2	5.9	2.3	1.9
33	22	18	14	6	5.3	11	14	19	33

8.4	7.3	5.3	5.5	6.7	7.1		6.8	7.0	7.2	4.8	4.8
33	24	19	16	11	5	6.7	3	8	15	16	33

8.0	6.7	6.3		6.0	5.5	5.3	5.2
33	17	7	5.7	8	9	15	33

SPK in 24" Oak 35' LK 5' + 9.169 + 10'

9.8	9.1	8.8	9.1		8.5	8.1	7.6	7.5
33	19	14	5	8.1	9	10	22	33

10.3	9.9	9.8	9.8		9.6	9.4	10.3	10.0	9.8
33	18	14	7	7.2	9	10	15	17	33

Sta. + H.I. ~ E/cv

932.41

+57

168

169

+70

170

+50

171

172

T.P. 0.53 927.68 5.44 927.15

173

174

175

176

+45

2/18/25

$$\frac{10.8}{33} \quad \frac{10.4}{18} \quad \frac{10.5}{11} \quad 9.7 \quad \frac{10.4}{10} \quad \frac{10.7}{13} \quad \frac{10.6}{18} \quad \frac{10.8}{25} \quad \frac{10.8}{33}$$

$$\frac{7.0}{33} \quad \frac{9.2}{18} \quad \frac{8.8}{14} \quad \frac{9.3}{10} \quad 9.4 \quad \frac{9.4}{9} \quad \frac{9.6}{15} \quad \frac{9.8}{23} \quad \frac{10.2}{33}$$

$$\frac{5.5}{33} \quad \frac{5.6}{7} \quad \frac{6.9}{3} \quad 6.9 \quad \frac{6.5}{12} \quad \frac{6.4}{14} \quad \frac{6.5}{27} \quad \frac{7.3}{33}$$

$$\frac{3.4}{50} \quad \frac{3.4}{28} \quad \frac{4.0}{10} \quad \frac{4.4}{7} \quad 4.5 \quad \frac{4.4}{11} \quad \frac{3.9}{12} \quad \frac{4.4}{19} \quad \frac{4.4}{33}$$

$$\frac{3.4}{33} \quad \frac{4.0}{7} \quad \frac{4.4}{5} \quad 4.5 \quad \frac{4.4}{10} \quad \frac{4.4}{14} \quad \frac{4.5}{18} \quad \frac{4.8}{25} \quad \frac{5.0}{33}$$

$$\frac{4.4}{33} \quad \frac{5.2}{7} \quad \frac{5.6}{5} \quad 5.8 \quad \frac{6.4}{14} \quad \frac{6.0}{15} \quad \frac{7.0}{28} \quad \frac{7.3}{33}$$

$$\frac{6.1}{33} \quad \frac{6.3}{12} \quad \frac{7.0}{7} \quad 7.0 \quad \frac{7.0}{13} \quad \frac{7.3}{20} \quad \frac{7.5}{33}$$

$$\frac{6.0}{33} \quad \frac{6.3}{4} \quad 6.9 \quad \frac{6.7}{8} \quad \frac{7.2}{13} \quad \frac{7.2}{25} \quad \frac{7.0}{33}$$

$$\frac{1.1}{33} \quad \frac{1.3}{22} \quad \frac{1.5}{10} \quad 1.9 \quad \frac{2.1}{11} \quad \frac{2.3}{14} \quad \frac{1.8}{15} \quad \frac{2.0}{33}$$

$$\frac{3.5}{33} \quad \frac{3.6}{14} \quad \frac{3.9}{6} \quad 3.8 \quad \frac{4.0}{13} \quad \frac{4.0}{23} \quad \frac{3.4}{33}$$

$$\frac{5.4}{33} \quad \frac{5.4}{8} \quad 5.9 \quad \frac{5.6}{13} \quad \frac{5.9}{17} \quad \frac{5.5}{33}$$

$$\frac{5.2}{33} \quad \frac{5.2}{18} \quad \frac{5.3}{4} \quad 5.4 \quad \frac{6.0}{14} \quad \frac{5.6}{17} \quad \frac{6.5}{23} \quad \frac{6.8}{33}$$

$$\frac{6.2}{33} \quad \frac{6.1}{13} \quad 6.3 \quad \frac{6.0}{15} \quad \frac{6.0}{23} \quad \frac{6.3}{28} \quad \frac{5.9}{33}$$

Sta. + H.I. ~ Elev.

727.68

177

178

T. 1.54 724.91 4.31 723.37

+50

179

+48

180

+57

181

182

+50

B.M. 4.22 720.24 8.90 716.01 714.02

183

184

185

2/18/25

$$\begin{array}{r} 4.9 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 7.0 \\ 7 \end{array} \quad 6.8 \quad \begin{array}{r} 6.7 \\ 20 \end{array} \quad \begin{array}{r} 6.7 \\ 29 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array}$$

$$\begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 5.1 \\ 6 \end{array} \quad \begin{array}{r} 5.5 \\ 2 \end{array} \quad 5.4 \quad \begin{array}{r} 6.0 \\ 16 \end{array} \quad \begin{array}{r} 6.8 \\ 24 \end{array} \quad \begin{array}{r} 6.3 \\ 33 \end{array}$$

$$\begin{array}{r} 1.9 \\ 33 \end{array} \quad \begin{array}{r} 1.8 \\ 7 \end{array} \quad \begin{array}{r} 2.2 \\ 5 \end{array} \quad 1.7 \quad \begin{array}{r} 2.2 \\ 8 \end{array} \quad \begin{array}{r} 1.6 \\ 10 \end{array} \quad \begin{array}{r} 2.2 \\ 20 \end{array} \quad \begin{array}{r} 1.3 \\ 33 \end{array}$$

$$\begin{array}{r} 2.5 \\ 33 \end{array} \quad \begin{array}{r} 2.3 \\ 20 \end{array} \quad \begin{array}{r} 2.4 \\ 8 \end{array} \quad 1.8 \quad \begin{array}{r} 2.2 \\ 5 \end{array} \quad \begin{array}{r} 1.5 \\ 4 \end{array} \quad \begin{array}{r} 1.2 \\ 13 \end{array} \quad \begin{array}{r} 1.5 \\ 18 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 1.8 \\ 13 \end{array} \quad \begin{array}{r} 3.3 \\ 7 \end{array} \quad 3.1 \quad \begin{array}{r} 3.7 \\ 5 \end{array} \quad \begin{array}{r} 3.1 \\ 6 \end{array} \quad \begin{array}{r} 2.2 \\ 17 \end{array} \quad \begin{array}{r} 1.6 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 23 \end{array} \quad \begin{array}{r} 4.5 \\ 14 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad 4.9 \quad \begin{array}{r} 5.6 \\ 3 \end{array} \quad \begin{array}{r} 6.0 \\ 7 \end{array} \quad \begin{array}{r} 4.2 \\ 10 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 8.4 \\ 33 \end{array} \quad \begin{array}{r} 8.2 \\ 23 \end{array} \quad \begin{array}{r} 8.5 \\ 5 \end{array} \quad \begin{array}{r} 9.0 \\ 3 \end{array} \quad 8.9 \quad \begin{array}{r} 9.0 \\ 10 \end{array} \quad \begin{array}{r} 8.6 \\ 14 \end{array} \quad \begin{array}{r} 8.7 \\ 19 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array}$$

$$\begin{array}{r} 10.1 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 20 \end{array} \quad \begin{array}{r} 10.2 \\ 5 \end{array} \quad \begin{array}{r} 9.7 \\ 2 \end{array} \quad 9.4 \quad \begin{array}{r} 10.0 \\ 16 \end{array} \quad \begin{array}{r} 10.5 \\ 21 \end{array} \quad \begin{array}{r} 10.9 \\ 26 \end{array} \quad \begin{array}{r} 10.9 \\ 33 \end{array}$$

$$\begin{array}{r} 10.0 \\ 33 \end{array} \quad \begin{array}{r} 9.9 \\ 20 \end{array} \quad \begin{array}{r} 10.0 \\ 3 \end{array} \quad 9.6 \quad \begin{array}{r} 9.6 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 22 \end{array} \quad \begin{array}{r} 10.2 \\ 33 \end{array}$$

$$\begin{array}{r} 8.5 \\ 33 \end{array} \quad \begin{array}{r} 8.7 \\ 16 \end{array} \quad 7.3 \quad \begin{array}{r} 9.2 \\ 18 \end{array} \quad \begin{array}{r} 8.7 \\ 33 \end{array}$$

Spk in 18" E/Wm. 35' Lt. Sta. 181+35

$$\begin{array}{r} 3.7 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 3 \end{array} \quad 4.4 \quad \begin{array}{r} 4.0 \\ 12 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad \begin{array}{r} 3.4 \\ 24 \end{array} \quad \begin{array}{r} 2.8 \\ 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad \begin{array}{r} 5.2 \\ 4 \end{array} \quad 4.7 \quad \begin{array}{r} 4.7 \\ 9 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 4.7 \\ 21 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 7 \end{array} \quad \begin{array}{r} 5.4 \\ 5 \end{array} \quad 5.0 \quad \begin{array}{r} 5.3 \\ 6 \end{array} \quad \begin{array}{r} 6.3 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 12 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array}$$

Sta. + H.I. - Elev.

710.14

184

+48

187

T.P. 0.80 715.88 5.14 715.08

T.P. 1.49 715.84 1.51 714.37

+55

188

189

+45

190

+45

T.P. 3.10 712.04 6.90 708.94

191

192

+50

193

2/19/25

$$\begin{array}{r} 4.5 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 5.1 \\ 5.1 \end{array} \quad \begin{array}{r} 5.3 \\ 3 \end{array} \quad \begin{array}{r} 5.2 \\ 8 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 5.7 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 17 \end{array} \quad \begin{array}{r} 4.6 \\ 20 \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 25 \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 5.2 \\ 5.2 \end{array} \quad \begin{array}{r} 5.5 \\ 5 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array}$$

$$\begin{array}{r} 4.5 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 15 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad \begin{array}{r} 5.0 \\ 5.0 \end{array} \quad \begin{array}{r} 5.2 \\ 7 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 4.4 \\ 18 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 3.7 \\ 33 \end{array} \quad \begin{array}{r} 3.6 \\ 28 \end{array} \quad \begin{array}{r} 3.7 \\ 12 \end{array} \quad \begin{array}{r} 3.6 \\ 7 \end{array} \quad \begin{array}{r} 3.4 \\ 3.4 \end{array} \quad \begin{array}{r} 3.7 \\ 4 \end{array} \quad \begin{array}{r} 2.4 \\ 8 \end{array} \quad \begin{array}{r} 2.7 \\ 18 \end{array} \quad \begin{array}{r} 1.3 \\ 22 \end{array} \quad \begin{array}{r} 1.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 6.8 \\ 9 \end{array} \quad \begin{array}{r} 6.1 \\ 6 \end{array} \quad \begin{array}{r} 5.9 \\ 5.9 \end{array} \quad \begin{array}{r} 6.2 \\ 5 \end{array} \quad \begin{array}{r} 5.8 \\ 9 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 4.9 \\ 21 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} 8.7 \\ 33 \end{array} \quad \begin{array}{r} 9.5 \\ 13 \end{array} \quad \begin{array}{r} 9.0 \\ 9 \end{array} \quad \begin{array}{r} 9.5 \\ 8 \end{array} \quad \begin{array}{r} 9.0 \\ 9.0 \end{array} \quad \begin{array}{r} 9.3 \\ 4 \end{array} \quad \begin{array}{r} 9.2 \\ 10 \end{array} \quad \begin{array}{r} 8.7 \\ 13 \end{array} \quad \begin{array}{r} 8.7 \\ 22 \end{array} \quad \begin{array}{r} 8.7 \\ 33 \end{array}$$

$$\begin{array}{r} 9.4 \\ 33 \end{array} \quad \begin{array}{r} 10.7 \\ 14 \end{array} \quad \begin{array}{r} 10.9 \\ 13 \end{array} \quad \begin{array}{r} 10.3 \\ 9 \end{array} \quad \begin{array}{r} 10.1 \\ 5 \end{array} \quad \begin{array}{r} 9.7 \\ 9.7 \end{array} \quad \begin{array}{r} 9.9 \\ 6 \end{array} \quad \begin{array}{r} 10.6 \\ 10 \end{array} \quad \begin{array}{r} 11.6 \\ 33 \end{array}$$

$$\begin{array}{r} 11.9 \\ 33 \end{array} \quad \begin{array}{r} 11.7 \\ 13 \end{array} \quad \begin{array}{r} 10.3 \\ 9 \end{array} \quad \begin{array}{r} 9.9 \\ 9.9 \end{array} \quad \begin{array}{r} 10.3 \\ 4 \end{array} \quad \begin{array}{r} 11.8 \\ 10 \end{array} \quad \begin{array}{r} 11.9 \\ 21 \end{array} \quad \begin{array}{r} 11.9 \\ 33 \end{array}$$

$$\begin{array}{r} 10.0 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 13 \end{array} \quad \begin{array}{r} 10.1 \\ 11 \end{array} \quad \begin{array}{r} 9.9 \\ 8 \end{array} \quad \begin{array}{r} 9.5 \\ 9.5 \end{array} \quad \begin{array}{r} 10.2 \\ 6 \end{array} \quad \begin{array}{r} 10.2 \\ 10 \end{array} \quad \begin{array}{r} 9.7 \\ 12 \end{array} \quad \begin{array}{r} 9.6 \\ 33 \end{array}$$

$$\begin{array}{r} 1.9 \\ 33 \end{array} \quad \begin{array}{r} 3.2 \\ 13 \end{array} \quad \begin{array}{r} 3.3 \\ 6 \end{array} \quad \begin{array}{r} 3.7 \\ 5 \end{array} \quad \begin{array}{r} 3.2 \\ 3.2 \end{array} \quad \begin{array}{r} 3.6 \\ 7 \end{array} \quad \begin{array}{r} 4.0 \\ 11 \end{array} \quad \begin{array}{r} 3.2 \\ 13 \end{array} \quad \begin{array}{r} 3.4 \\ 23 \end{array} \quad \begin{array}{r} 2.7 \\ 25 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array}$$

$$\begin{array}{r} 1.4 \\ 33 \end{array} \quad \begin{array}{r} 3.3 \\ 3 \end{array} \quad \begin{array}{r} 3.6 \\ 2 \end{array} \quad \begin{array}{r} 3.5 \\ 3.5 \end{array} \quad \begin{array}{r} 3.3 \\ 4 \end{array} \quad \begin{array}{r} 4.0 \\ 13 \end{array} \quad \begin{array}{r} 3.8 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 19 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 1.0 \\ 33 \end{array} \quad \begin{array}{r} 2.7 \\ 9 \end{array} \quad \begin{array}{r} 3.6 \\ 2 \end{array} \quad \begin{array}{r} 5.1 \\ 5.1 \end{array} \quad \begin{array}{r} 5.0 \\ 4 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 5.0 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 2.6 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 5.7 \\ 5.7 \end{array} \quad \begin{array}{r} 4.1 \\ 4 \end{array} \quad \begin{array}{r} 7.4 \\ 5 \end{array} \quad \begin{array}{r} 7.0 \\ 11 \end{array} \quad \begin{array}{r} 7.7 \\ 20 \end{array} \quad \begin{array}{r} 7.2 \\ 24 \end{array} \quad \begin{array}{r} 7.6 \\ 33 \end{array}$$

Sta. + H.I. - Elev.

912.04

+50

194

+50

B.M.

9.74 902.30 902.33

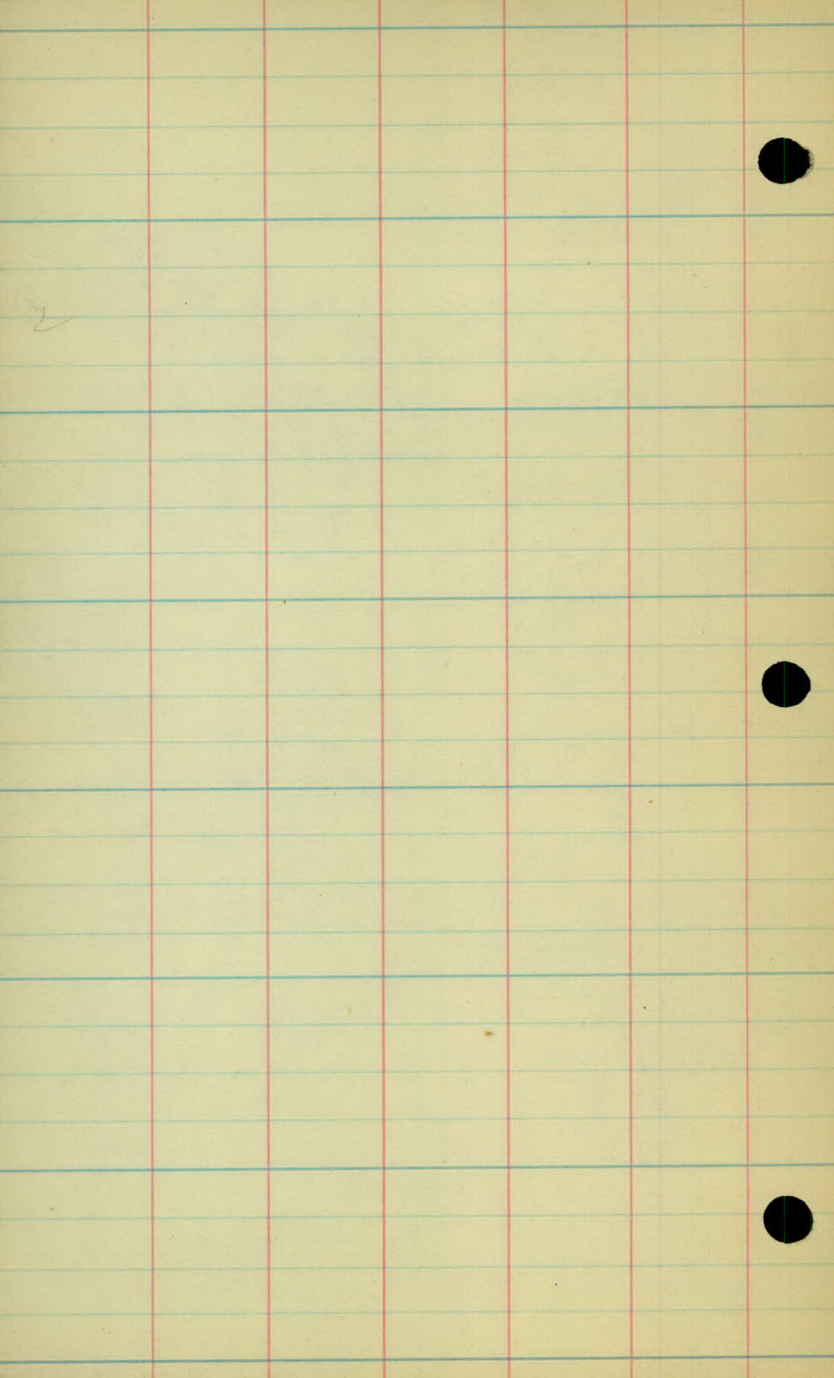
2/19/05

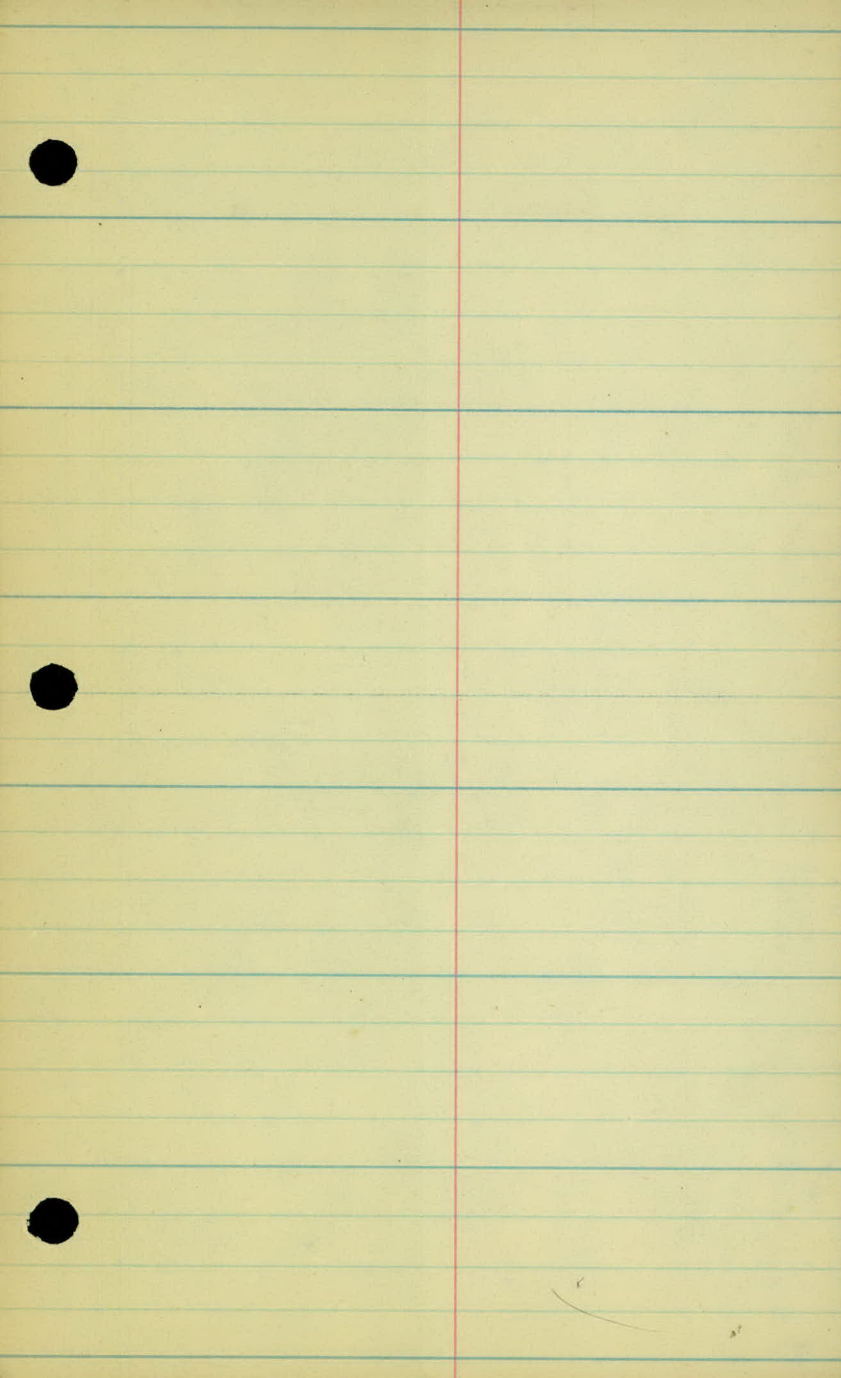
$\frac{4.6}{33}$	$\frac{5.9}{17}$	7.6	$\frac{8.5}{10}$	$\frac{9.3}{15}$	$\frac{9.3}{28}$	$\frac{10.3}{33}$
------------------	------------------	-----	------------------	------------------	------------------	-------------------

$\frac{6.6}{33}$	$\frac{8.0}{8}$	8.7	$\frac{9.7}{12}$	$\frac{10.3}{17}$	$\frac{11.0}{24}$	$\frac{10.8}{27}$	$\frac{10.3}{33}$
------------------	-----------------	-----	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{7.5}{33}$	$\frac{8.7}{14}$	9.5	$\frac{10.3}{14}$	$\frac{10.9}{33}$
------------------	------------------	-----	-------------------	-------------------

SPK in 12" Oak 60' Rt Sta 194 + 65





Sta.	+	H.I.	-	E/cv.
B.M.	3.70	906.03		902.33
195				

+50

194

197

+75

198

+55

199

+50

T.P.	7.07	905.90	7.20	898.83
200				

+65

201

+15

2/17/25

S.P.K. in 12" O.K. 60' Rt. Sta. 194 + 65.

$\frac{1.2}{33}$	$\frac{2.4}{13}$	3.0	$\frac{3.2}{12}$	$\frac{3.6}{21}$	$\frac{5.7}{29}$	$\frac{6.1}{33}$
------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{2.5}{33}$	$\frac{3.2}{14}$	3.7	$\frac{4.8}{21}$	$\frac{6.8}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{4.7}{33}$	$\frac{5.6}{14}$	5.8	$\frac{6.0}{14}$	$\frac{7.1}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{4.7}{33}$	$\frac{4.7}{13}$	5.2	$\frac{5.4}{16}$	$\frac{6.4}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{5.1}{33}$	$\frac{6.0}{14}$	6.7	$\frac{6.7}{14}$	$\frac{7.6}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{5.9}{33}$	$\frac{6.4}{14}$	6.5	$\frac{6.3}{14}$	$\frac{6.9}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{4.6}{33}$	$\frac{5.0}{14}$	5.1	$\frac{4.9}{14}$	$\frac{5.9}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{4.7}{33}$	$\frac{4.9}{14}$	5.4	$\frac{5.4}{16}$	$\frac{6.2}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{6.0}{33}$	$\frac{6.5}{14}$	7.2	$\frac{7.4}{14}$	$\frac{7.8}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{7.5}{33}$	$\frac{7.9}{14}$	8.0	$\frac{7.9}{14}$	$\frac{8.4}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{7.1}{33}$	$\frac{7.0}{14}$	7.1	$\frac{7.5}{14}$	$\frac{8.4}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{7.4}{33}$	$\frac{7.5}{14}$	7.4	$\frac{7.6}{14}$	$\frac{8.5}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{7.3}{33}$	$\frac{7.6}{14}$	7.9	$\frac{8.0}{14}$	$\frac{8.6}{33}$
------------------	------------------	-----	------------------	------------------

Sta. + H.I. = E/cv.

905.90

202

+50

203

204

205

206

T.P. 4.65 901.23 9.32 896.58

207

208

+65 Rec. 36"

209

210

211

+52

212

T.P. 5.75 906.71 0.27 900.94

2/17/25

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 14 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ 33 \end{array} \quad \begin{array}{r} 4.9 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} 8.4 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad \begin{array}{r} 8.5 \\ 14 \end{array} \quad \begin{array}{r} 9.5 \\ 33 \end{array}$$

$$\begin{array}{r} 8.6 \\ 33 \end{array} \quad \begin{array}{r} 8.9 \\ 14 \end{array} \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} 10.2 \\ 33 \end{array}$$

$$\begin{array}{r} 9.4 \\ 33 \end{array} \quad \begin{array}{r} 9.8 \\ 14 \end{array} \quad \begin{array}{r} 10.3 \\ 14 \end{array} \quad \begin{array}{r} 10.5 \\ 33 \end{array}$$

$$\begin{array}{r} 5.6 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array}$$

$$\begin{array}{r} 5.1 \\ 33 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array}$$

$$\begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 1.9 \\ 33 \end{array} \quad \begin{array}{r} 1.4 \\ 14 \end{array} \quad \begin{array}{r} 1.3 \\ 14 \end{array} \quad \begin{array}{r} 1.5 \\ 33 \end{array}$$

Stg. + H.I. - E/cy.

906.71

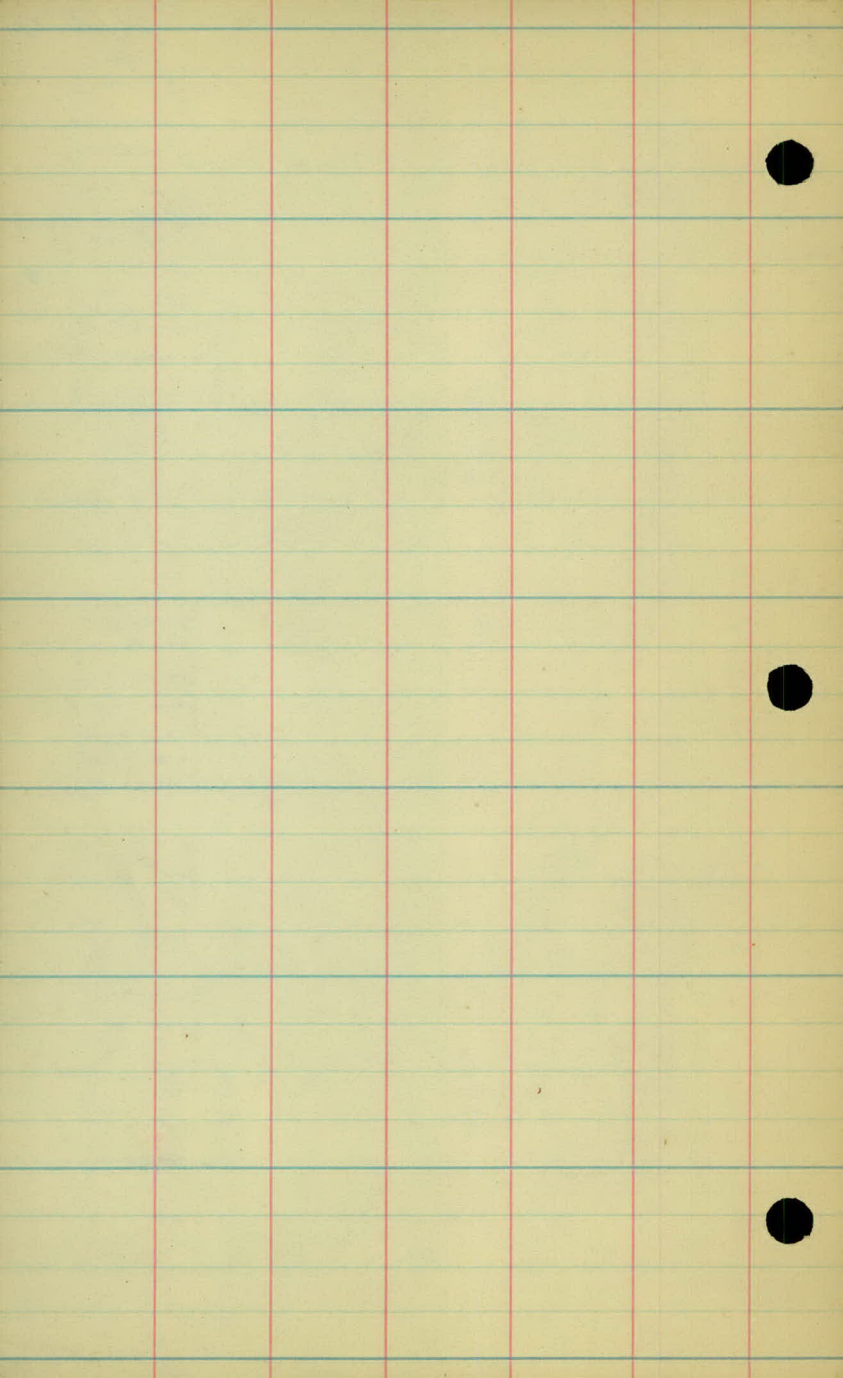
B.M.

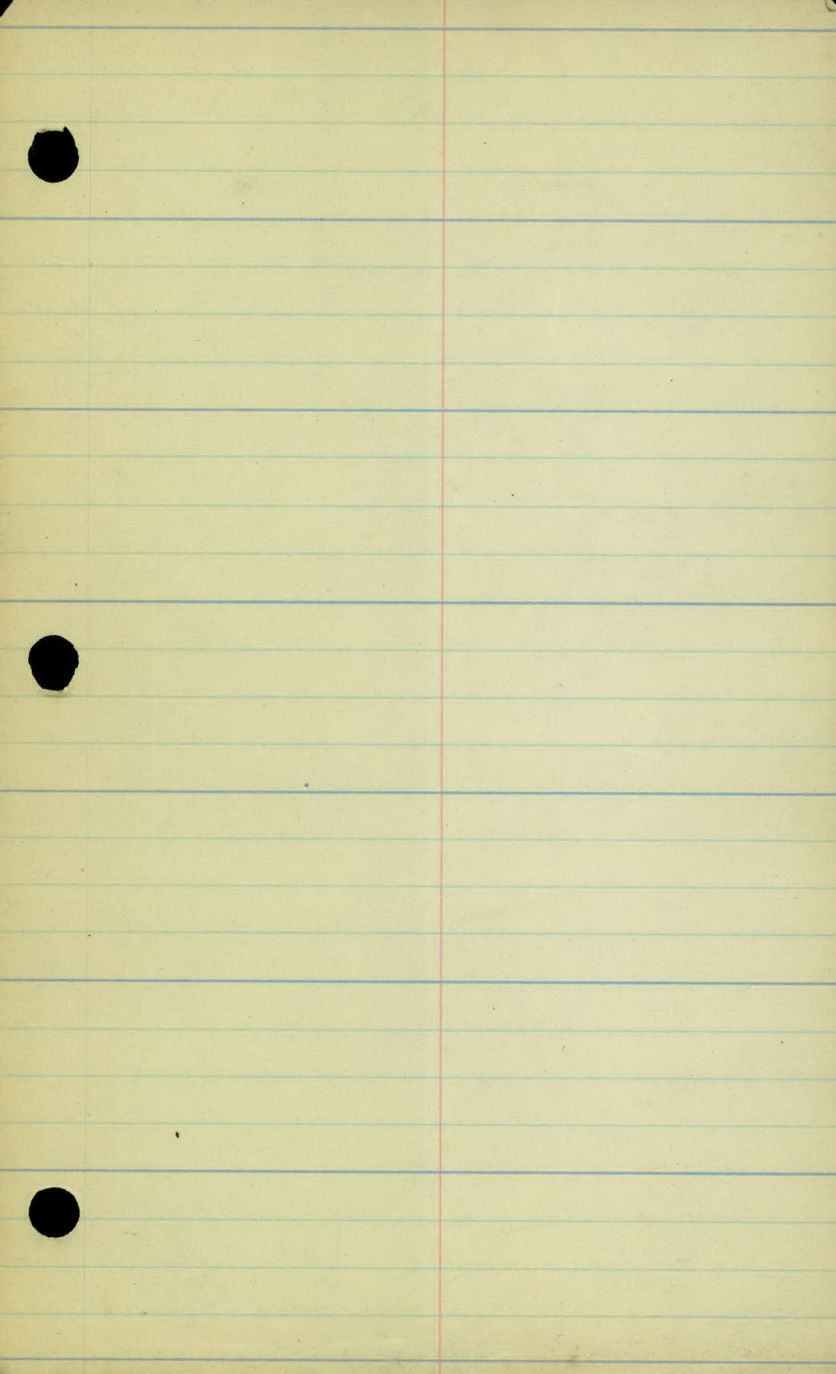
5,49 901.22 901.22

104 + 40 R. 24"

2/17/25

SpK. in 18" E/m 40' Rt. Sta. 211 + 90.





Station	+	H.I.	-	Rod.	Elev
B.M.	5.21	906.43			901.22
212+50					
213+00					
+50					
214+00					
+50					
215+00					
+60					
216+00					
T.P.	7.37	912.26	1.54	904.89	
+75					
217+00					
+50					
218+00					
+45					

212+50

ht.

±

RT.

"h" line

Spike in Tree. Rt. Sta 211+90

$\frac{5.3}{33.0}$	$\frac{4.9}{20.0}$	4.4	$\frac{4.3}{20.0}$	$\frac{4.5}{33.0}$
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$\frac{4.1}{33.0}$	$\frac{4.3}{16.0}$	4.5	$\frac{4.3}{16.0}$	$\frac{4.5}{33.0}$
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$\frac{5.9}{33.0}$	$\frac{5.2}{16.0}$	5.1	$\frac{5.2}{17.0}$	$\frac{5.3}{33.0}$
--------------------	--------------------	-----	--------------------	--------------------

$\frac{7.2}{33.0}$	$\frac{7.0}{21.0}$	$\frac{6.1}{9.0}$	5.8	$\frac{5.5}{10.0}$	$\frac{5.4}{33.0}$
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$\frac{8.1}{33.0}$	$\frac{7.8}{15.0}$	7.3	$\frac{6.8}{17.0}$	$\frac{6.8}{33.0}$
--------------------	--------------------	-----	--------------------	--------------------

$\frac{6.2}{33.0}$	$\frac{7.0}{16.0}$	7.2	$\frac{7.0}{17.0}$	$\frac{6.7}{33.0}$
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$\frac{4.3}{33.0}$	$\frac{4.7}{17.0}$	5.0	$\frac{5.7}{18.0}$	$\frac{5.8}{33.0}$
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$\frac{1.6}{33.0}$	$\frac{2.0}{17.0}$	2.7	$\frac{3.4}{17.0}$	$\frac{4.0}{33.0}$
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$\frac{3.2}{34.0}$	$\frac{2.3}{28.0}$	$\frac{1.6}{22.0}$	$\frac{2.6}{12.0}$	3.4	$\frac{4.6}{14.0}$	$\frac{6.4}{33.0}$
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$\frac{3.7}{34.0}$	$\frac{2.8}{30.0}$	$\frac{2.0}{18.0}$	$\frac{2.7}{7.0}$	$\frac{3.3}{5.0}$	3.6	$\frac{4.1}{8.0}$	$\frac{5.6}{21.0}$	$\frac{6.2}{33.0}$
--------------------	--------------------	--------------------	-------------------	-------------------	-----	-------------------	--------------------	--------------------

± Rt

$\frac{5.6}{40.0}$	$\frac{5.0}{35.0}$	$\frac{4.7}{30.0}$	$\frac{5.2}{24.0}$	$\frac{6.0}{19.0}$	$\frac{5.7}{17.0}$	$\frac{4.8}{6.5}$	5.3	$\frac{6.0}{16.0}$	$\frac{6.6}{33.0}$
--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	-------------------	-----	--------------------	--------------------

± Rt

$\frac{7.6}{40.0}$	$\frac{7.6}{34.0}$	$\frac{7.3}{30.0}$	$\frac{6.7}{23.0}$	$\frac{7.1}{15.0}$	$\frac{8.1}{9.0}$	8.1	$\frac{8.5}{17.0}$	$\frac{8.7}{33.0}$
--------------------	--------------------	--------------------	--------------------	--------------------	-------------------	-----	--------------------	--------------------

± Rt

$\frac{10.8}{40.0}$	$\frac{10.4}{27.0}$	$\frac{8.3}{21.0}$	$\frac{7.7}{15.0}$	$\frac{8.3}{8.0}$	$\frac{9.8}{4.0}$	10.4	$\frac{9.3}{18.0}$	$\frac{9.9}{33.0}$
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Station	+	H.I.	—	Rod Elev.	
		912.26			
219+00					
+50					
220+00					
+60					
221+00					
T.P.	11.00	916.74	6.52	905.74	
222+00					
+75					
223+00					
224+00					
B.M.	9.09	922.50	3.33	913.41	913.41
225+00					
226+00					
226+50					
227+00					

219700

H

F

K4.

"L" line

$\frac{9.5}{27.0} \frac{10.2}{25.5} \frac{10.2}{23.5} \frac{8.8}{20.0} \frac{7.8}{11.0} \frac{8.2}{3.0} 8.5 \frac{8.4}{6.0} \frac{7.8}{22.0} \frac{7.7}{33.0}$
 $\frac{9.8}{32.0} \frac{9.4}{37.0}$

$\frac{9.1}{32.0} \frac{8.8}{29.0} \frac{9.0}{24.0} \frac{10.0}{22.5} \frac{8.9}{19.0} \frac{7.8}{15.5} \frac{7.6}{9.0} 7.6 \frac{7.6}{2.0} \frac{8.2}{3.0} \frac{7.7}{8.0} \frac{7.4}{20.0} \frac{7.4}{33.0}$

$\frac{10.0}{33.0} \frac{9.7}{28.0} \frac{9.6}{25.0} \frac{10.1}{21.0} \frac{8.3}{16.0} \frac{7.7}{8.5} \frac{8.0}{2.0} 8.3 \frac{8.4}{8.5} \frac{8.4}{22.0} \frac{8.3}{33.0}$

$\frac{8.6}{33.0} \frac{8.8}{28.0} \frac{8.2}{21.0} \frac{7.8}{16.0} \frac{7.6}{11.0} \frac{7.8}{4.0} 8.8 \frac{9.5}{4.5} \frac{9.0}{7.0} \frac{9.2}{15.0} \frac{10.2}{7.0} \frac{10.3}{29.0} \frac{10.3}{34.0}$

$\frac{7.3}{34.0} \frac{8.0}{31.0} \frac{7.7}{23.0} \frac{7.7}{19.0} \frac{6.8}{15.0} \frac{6.7}{11.0} \frac{7.0}{5.0} 8.0 \frac{8.2}{6.0} \frac{8.2}{9.0} \frac{8.8}{21.0} \frac{9.0}{33.0}$

$\frac{8.0}{32.0} \frac{9.4}{31.0} \frac{9.9}{29.0} \frac{9.1}{25.0} \frac{9.1}{18.5} \frac{8.4}{16.0} \frac{8.3}{10.0} 8.2 \frac{8.2}{8.5} \frac{9.4}{33.0}$

$\frac{6.6}{35.0} \frac{6.6}{32.0} \frac{7.2}{30.0} \frac{6.8}{28.0} \frac{7.0}{21.0} \frac{7.0}{16.0} \frac{6.5}{10.5} 6.4 \frac{6.7}{1.5} \frac{6.2}{4.0} \frac{6.0}{18.0} \frac{5.7}{33.0}$

$\frac{7.3}{32.0} \frac{6.6}{20.0} \frac{6.5}{10.0} 6.4 \frac{6.0}{7.0} \frac{5.1}{19.0} \frac{4.8}{33.0}$

$\frac{6.0}{35.0} \frac{6.4}{27.0} \frac{5.8}{15.0} \frac{5.6}{6.0} 5.4 \frac{5.5}{6.0} \frac{5.3}{13.0} \frac{4.3}{33.0}$

S.E. Con Concrete Porch. Ht. Sta. 924+18

$\frac{8.5}{33.0} \frac{8.5}{23.0} \frac{9.1}{22.0} \frac{8.8}{16.0} \frac{8.4}{8.0} \frac{8.6}{3.5} 9.4 \frac{9.4}{4.0} \frac{8.9}{22.0} \frac{8.7}{33.0}$

$\frac{4.4}{33.0} \frac{4.8}{30.0} \frac{4.5}{15.0} \frac{4.5}{6.0} 4.5 \frac{4.7}{2.0} \frac{5.3}{6.0} \frac{5.4}{18.0} \frac{5.1}{27.0} \frac{5.3}{33.0}$

$\frac{2.7}{38.0} \frac{3.3}{19.0} \frac{3.0}{14.0} \frac{2.8}{4.0} 2.9 \frac{3.3}{6.0} \frac{3.7}{13.0} \frac{3.1}{25.0} \frac{3.3}{33.0}$

$\frac{3.2}{33.0} \frac{3.3}{18.0} \frac{2.9}{13.0} \frac{2.6}{3.0} 2.7 \frac{2.9}{7.0} \frac{3.1}{12.0} \frac{2.2}{24.0} \frac{2.4}{33.0}$

STATION	+	H.I.	-	Rob.	Elev.
		922.50			
227+50					
228+00					
229+00					
T.P	7.57	915.59	4.48	919.02	
+60					
230+00					
+50					
231+00					
+62					
+79					
232+00					
+50					
+84.98					
B.M.				4.50	921.09

227+50

ht.

A

R7.

"h" hie

$\frac{4.1}{33.0}$	$\frac{3.7}{35.0}$	$\frac{3.7}{15.0}$	$\frac{3.3}{11.0}$	$\frac{2.8}{3.0}$	2.9	$\frac{3.0}{10.0}$	$\frac{3.8}{14.0}$	$\frac{3.8}{18.0}$	$\frac{2.2}{23.0}$	$\frac{2.3}{33.0}$
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$\frac{5.2}{33.0}$	$\frac{4.8}{16.0}$	$\frac{4.3}{11.0}$	3.8	$\frac{4.3}{11.0}$	$\frac{4.9}{17.0}$	$\frac{4.2}{19.0}$	$\frac{3.7}{33.0}$
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$\frac{6.9}{33.0}$	$\frac{6.8}{19.0}$	$\frac{6.1}{15.0}$	$\frac{5.8}{8.0}$	$\frac{4.9}{5.0}$	4.6	$\frac{5.0}{10.0}$	$\frac{5.6}{15.0}$	$\frac{4.8}{33.0}$
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$\frac{9.4}{33.0}$	$\frac{8.9}{14.0}$	$\frac{9.3}{12.0}$	$\frac{8.2}{5.5}$	7.7	$\frac{8.1}{9.0}$	$\frac{9.8}{17.0}$	$\frac{9.8}{19.0}$	$\frac{8.8}{21.0}$	$\frac{8.8}{33.0}$
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$\frac{8.9}{33.0}$	$\frac{8.7}{22.0}$	$\frac{8.9}{20.0}$	$\frac{7.9}{13.0}$	$\frac{7.6}{7.0}$	8.0	$\frac{9.3}{7.0}$	$\frac{9.3}{9.0}$	$\frac{9.0}{16.0}$	$\frac{9.4}{33.0}$
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R6

$\frac{8.1}{10.0}$	$\frac{7.4}{33.0}$	$\frac{7.1}{25.0}$	$\frac{7.5}{16.0}$	$\frac{8.5}{10.0}$	$\frac{8.5}{8.0}$	$\frac{8.0}{6.0}$	8.4	$\frac{8.7}{16.0}$	$\frac{8.7}{33.0}$
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$\frac{6.9}{34.0}$	$\frac{7.0}{31.0}$	$\frac{7.3}{28.0}$	$\frac{7.3}{26.0}$	$\frac{6.7}{25.0}$	$\frac{6.5}{11.0}$	6.8	$\frac{6.9}{8.0}$	$\frac{7.1}{33.0}$
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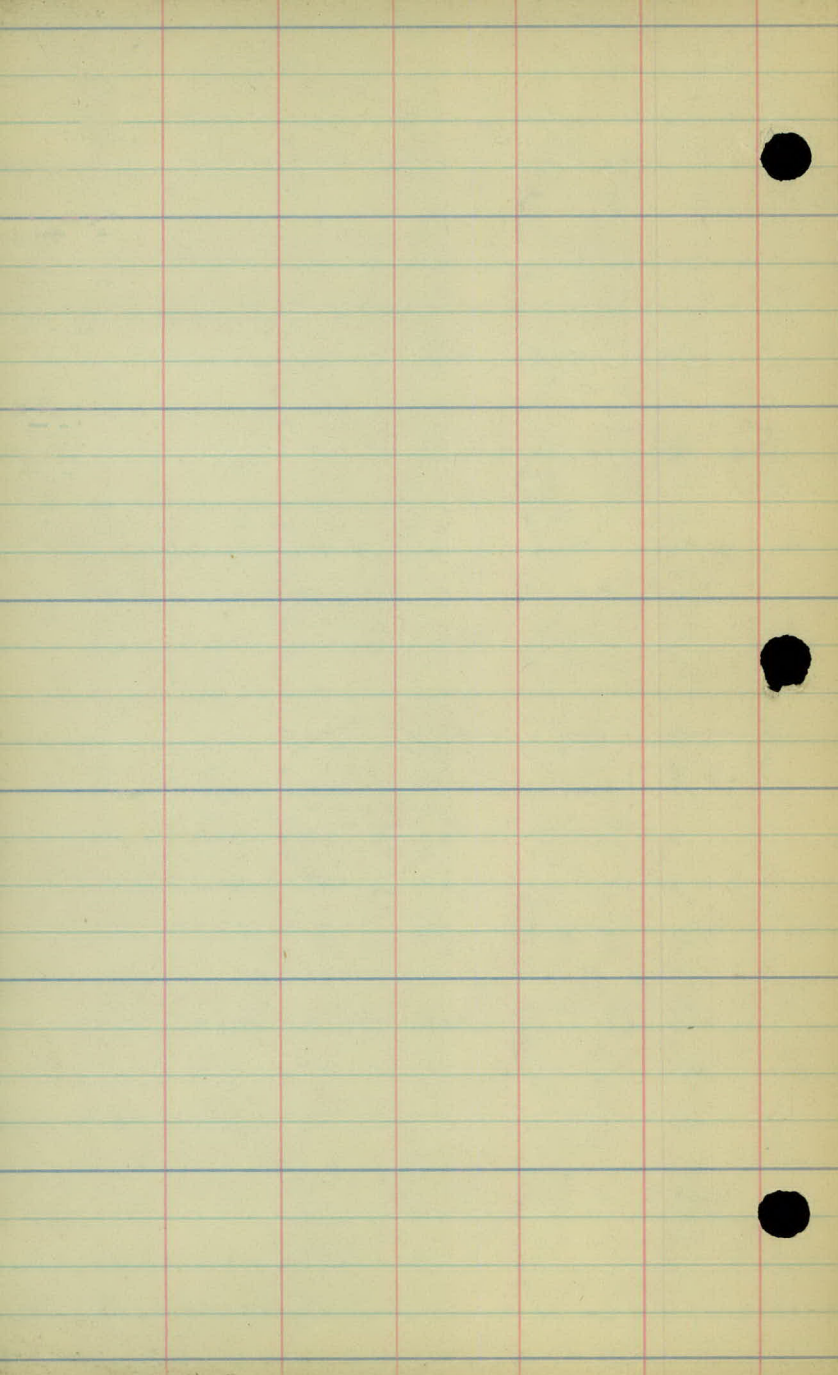
$\frac{5.2}{33.0}$	$\frac{4.8}{28.0}$	$\frac{5.0}{18.0}$	$\frac{5.7}{14.5}$	$\frac{6.5}{10.5}$	$\frac{6.4}{7.5}$	$\frac{5.2}{6.0}$	3.7	$\frac{3.3}{7.0}$	$\frac{3.5}{19.0}$	$\frac{4.0}{33.0}$
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$\frac{5.1}{33.0}$	$\frac{4.4}{20.0}$	$\frac{4.7}{11.5}$	$\frac{4.9}{8.0}$	$\frac{6.1}{3.0}$	6.1	$\frac{3.3}{7.0}$	$\frac{2.5}{12.0}$	$\frac{3.0}{23.0}$	$\frac{3.3}{33.0}$
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$\frac{4.2}{33.0}$	$\frac{4.8}{31.5}$	$\frac{4.9}{27.0}$	$\frac{4.4}{25.0}$	$\frac{4.0}{14.0}$	$\frac{4.3}{5.5}$	$\frac{4.7}{2.0}$	5.3	$\frac{5.9}{2.5}$	$\frac{6.0}{6.0}$	$\frac{5.3}{9.5}$	$\frac{2.5}{16.0}$	$\frac{2.4}{23.0}$	$\frac{3.0}{33.0}$
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$\frac{2.0}{35.0}$	$\frac{2.4}{26.0}$	$\frac{3.4}{29.0}$	$\frac{4.0}{14.5}$	$\frac{3.4}{12.0}$	3.0	$\frac{3.1}{7.0}$	$\frac{3.6}{19.5}$	$\frac{4.5}{13.0}$	$\frac{3.6}{16.5}$	$\frac{3.4}{24.0}$	$\frac{3.1}{33.0}$
--------------------	--------------------	--------------------	--------------------	--------------------	-----	-------------------	--------------------	--------------------	--------------------	--------------------	--------------------

$\frac{1.9}{33.0}$	$\frac{1.6}{29.0}$	$\frac{2.9}{19.0}$	$\frac{2.4}{7.0}$	2.3	$\frac{2.5}{8.0}$	$\frac{3.1}{13.5}$	$\frac{3.3}{15.5}$	$\frac{2.5}{22.0}$	$\frac{2.0}{33.0}$
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Drainage notes
on the L. Line.

103+27 Cross Drain. 18" x 37' C.M. Good Cond.
Extends 22⁵ Lt. & 14³ Rt.

119+01 Cross Drain 18" x 32⁵ C.M. Good Cond
Extends 21 Lt. & 11⁵ Rt.

135+51 Cross Drain 6" x 12" x 25' Plank. Box
Extends 12' Lt. & 13' Rt. Poor Cond.

141+13 Cross Drain 6" x 12" x 25' Plank. Box.
Extends 12' Lt. & 13' Rt. Poor Cond.

104+40 Cross Drain Requires 24"
Drains Rt.

108+65 Cross Drain Requires 36"
Drains Rt.

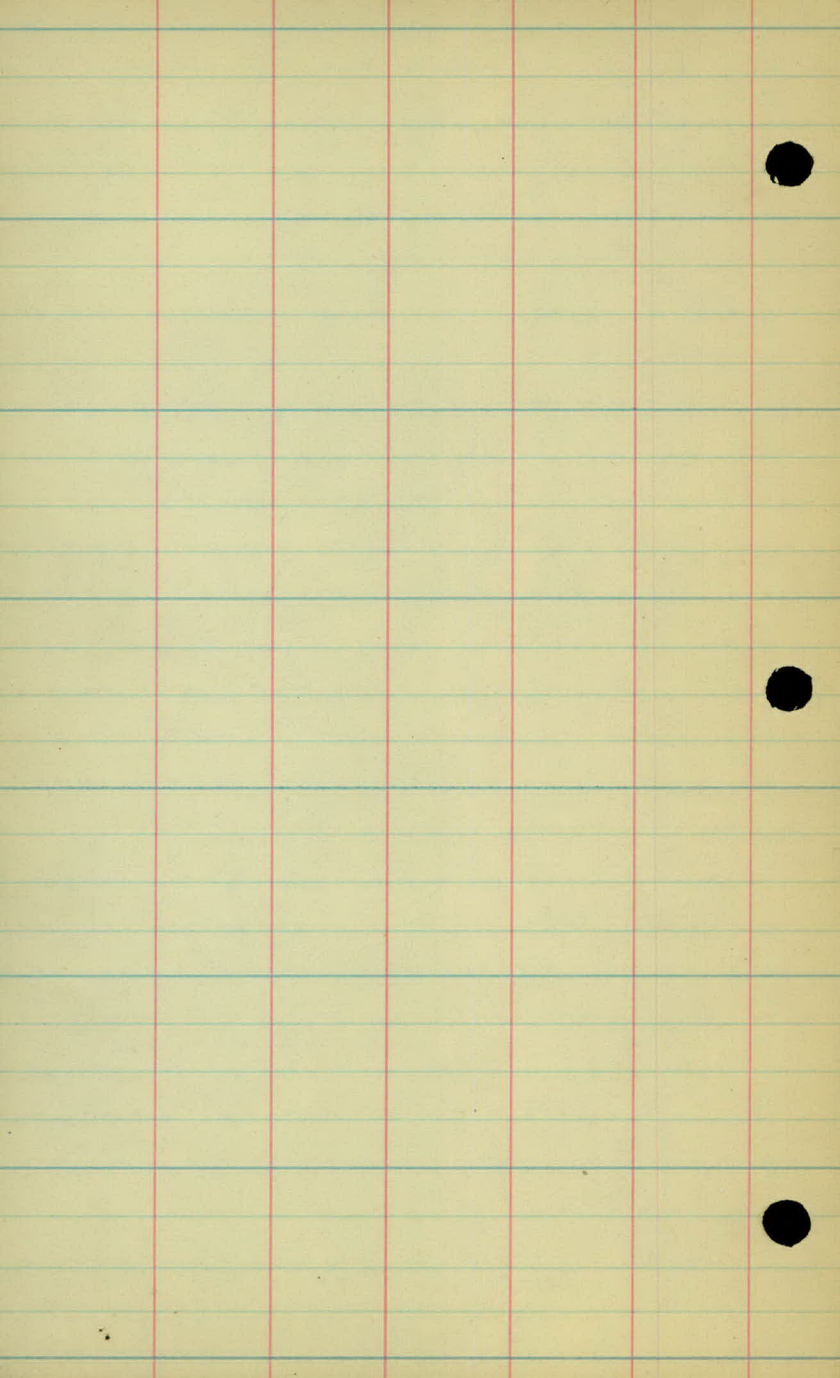
L. Line.

Invert Elev. = 901.81 $\frac{901.5}{33}$ $\frac{901.3}{50}$
Drains Rt.

Invert Elev. = 906.39 $\frac{905.8}{50}$ $\frac{905.0}{75}$
Drains Lt.

Invert Elev. = 899.1 $\frac{898.8}{50}$ $\frac{898.6}{100}$
Drains Lt.

Invert Elev. = 899.6 $\frac{899.5}{50}$
Drains Rt.



L. Line

Drainaged notes on the L. Line

Sta.	+	H.I.	-	Elev.
B.M.	1.45	909.38		907.93
T.P.	2.71	905.53	6.54	902.82

9+87 Edge of bridge

9+95 Center of bridge.

10+03 Edge of bridge.

53+47 Cross Drain 18" x 31' C.M. Good Cond.
Extends 15' Lt. & 16' Rt.

54+33 Cross Drain 18" x 37' C.M. Good Cond.
Extends 19⁶' Lt. & 17⁴' Rt.

229+50 Cross Drain 12" x 22' ? C.M.
Extends 13' Rt. & ? Lt.

230+30 Requires 12" C.M.

L. Line

900.93 = El. of Plan King.

898.2 = El. Top of ice.

896.6 = El. Bottom of ditch.

6.9	6.6	7.1	7.7	7.2	4.4		4.5	8.1	8.1	7.0	7.0
33	20	18	14	13	4	43	9	14	18	22	33

7.0	7.0	8.4	8.4	7.4	4.9		4.8	8.3	8.3	7.0	7.0
33	20	17	14	13	8	4.5	11	14	19	20	33

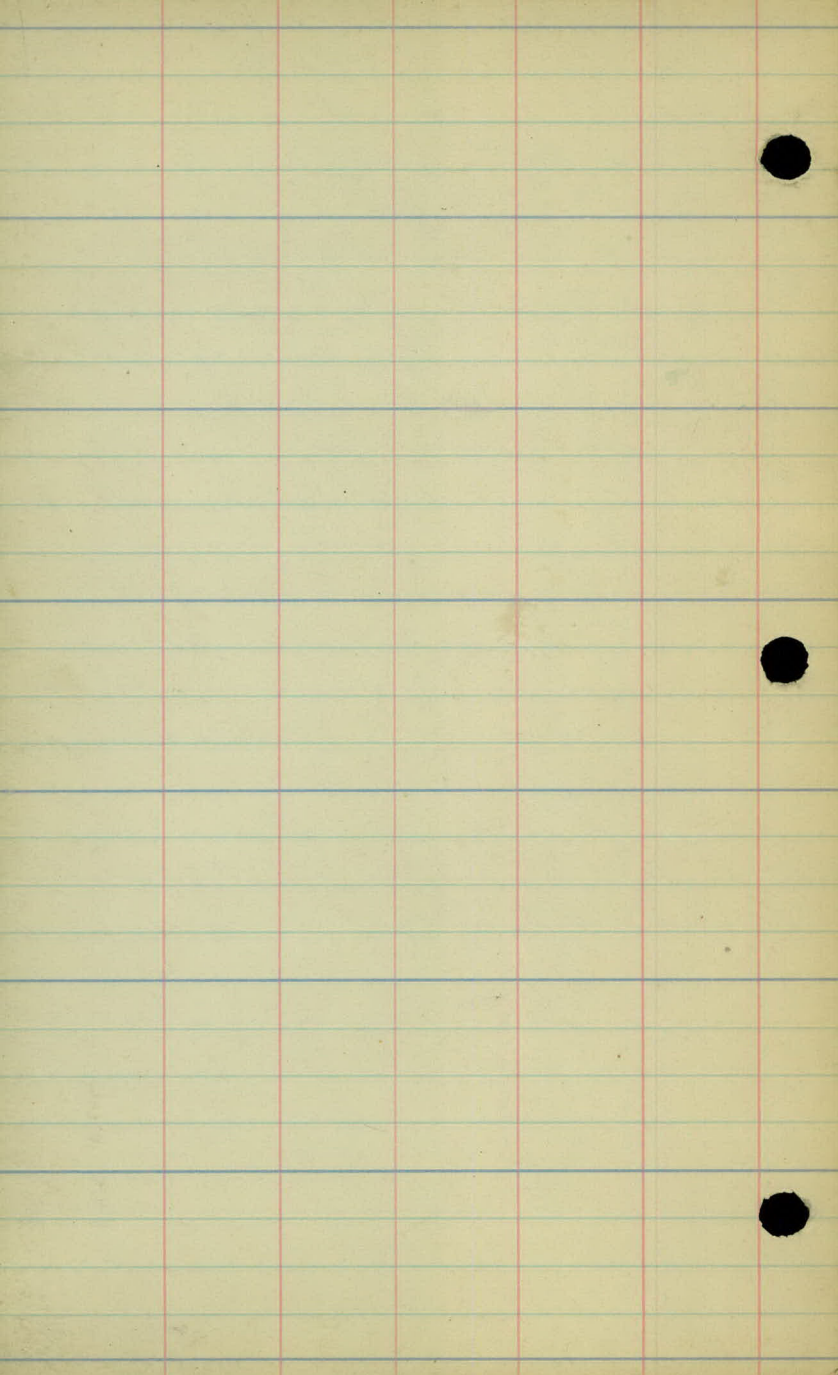
Inv. Elev. = 894.8

Drains Lt.

Inv. Elev. 894.7

Drains Lt.

Drains Lt.



Road. 62+63.

"41" line. Alignment.

"L"-line.

Station

Ang. ht. Ang. Rt.

$221 + 13^{\circ} 41' = 220 + 00.7$ P.T. "h" line

$208 + 67.1$ ✓ P.T.

✓
S. 89° 46' E.

$206 + 74.2$ P.I.

45° 08'

$204 + 35.8$ ✓ P.C.

$200 + 00$ P.O.T.

✓
N. 45° 12' E.

$190 + 24.4$ ✓ P.T.

$188 + 12.0$ P.I. 45° 00' = 188 + 12.0 P.O.T. "L" LINE

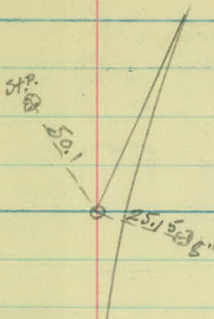
$185 + 74.2$ ✓ P.C.

✓
S. 89° 48' E.

"L" - line

Sta. - Def.

204+35.8 - 0°00'
 +50 - 0°43'
 205+00 - 3°13'
 +50 - 5°43'
 206+00 - 8°13'
 +50 - 10°43'
 207+00 - 13°13'
 +50 - 15°43'
 208+00 - 18°13'
 +50 - 20°43'
 209+00 - 22°34'



10° Curve RT.

$\Delta = 45.08^\circ$

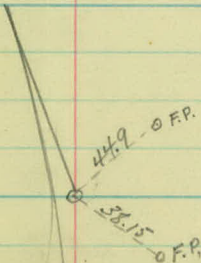
Rad. = 573.69 ✓

Tang. = 239.4 ✓

Length = 451.3 ✓

Sta. - Def.

185+74.7 - 0°00'
 186+00 - 1°17'
 +50 - 3°47'
 187+00 - 6°17'
 +50 - 8°47'
 188+00 - 11°17'
 +50 - 13°47'
 189+00 - 16°17'
 +50 - 18°47'
 190+00 - 21°17'
 191+00 - 22°30'



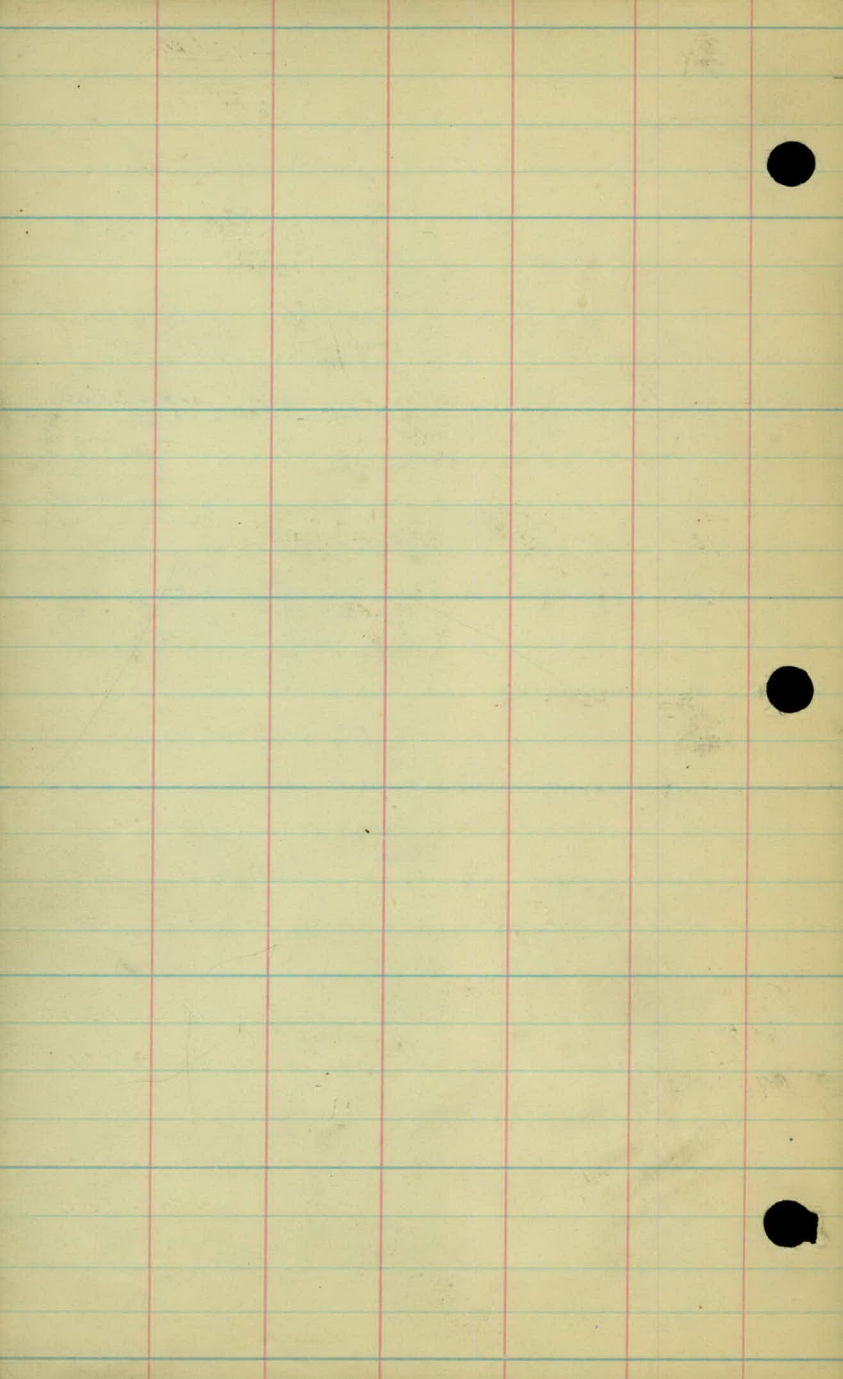
10° Curve. ht.

$\Delta = 45.00^\circ$

Rad. = 573.69 ✓

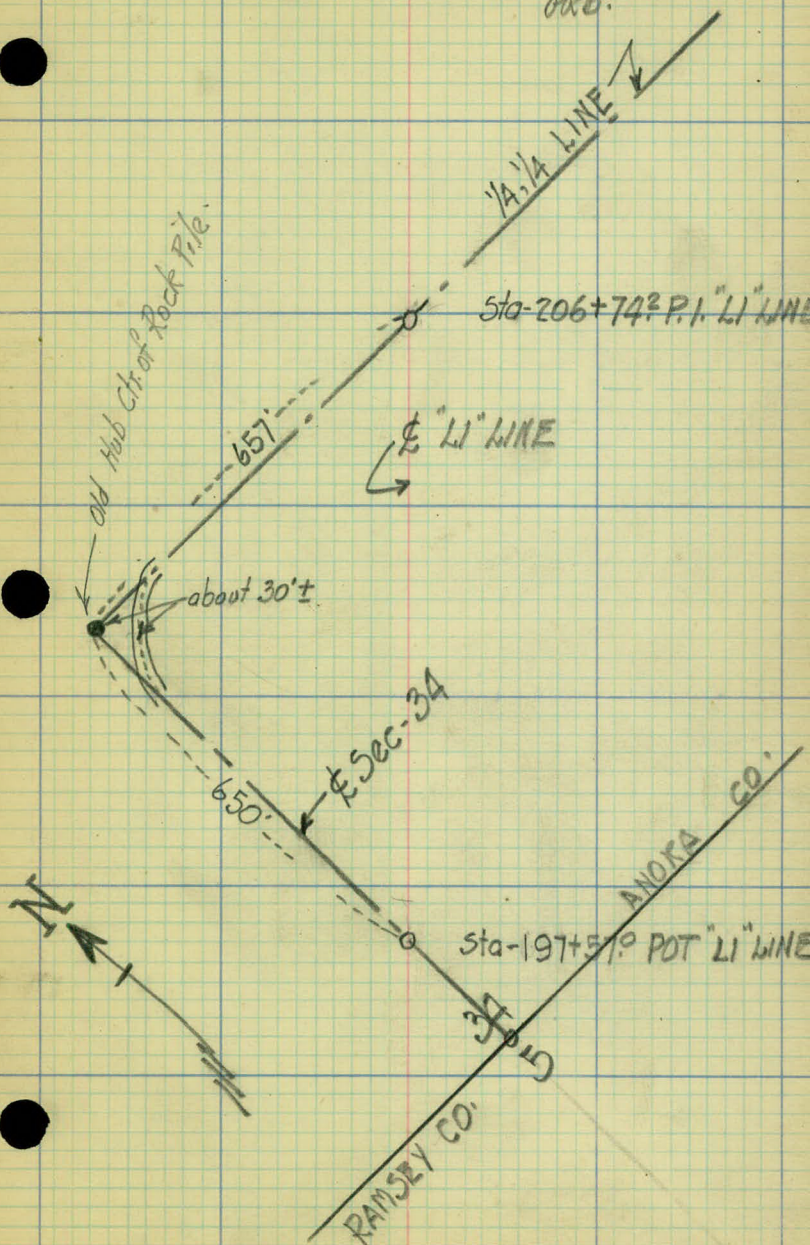
Tang. = 237.6 ✓

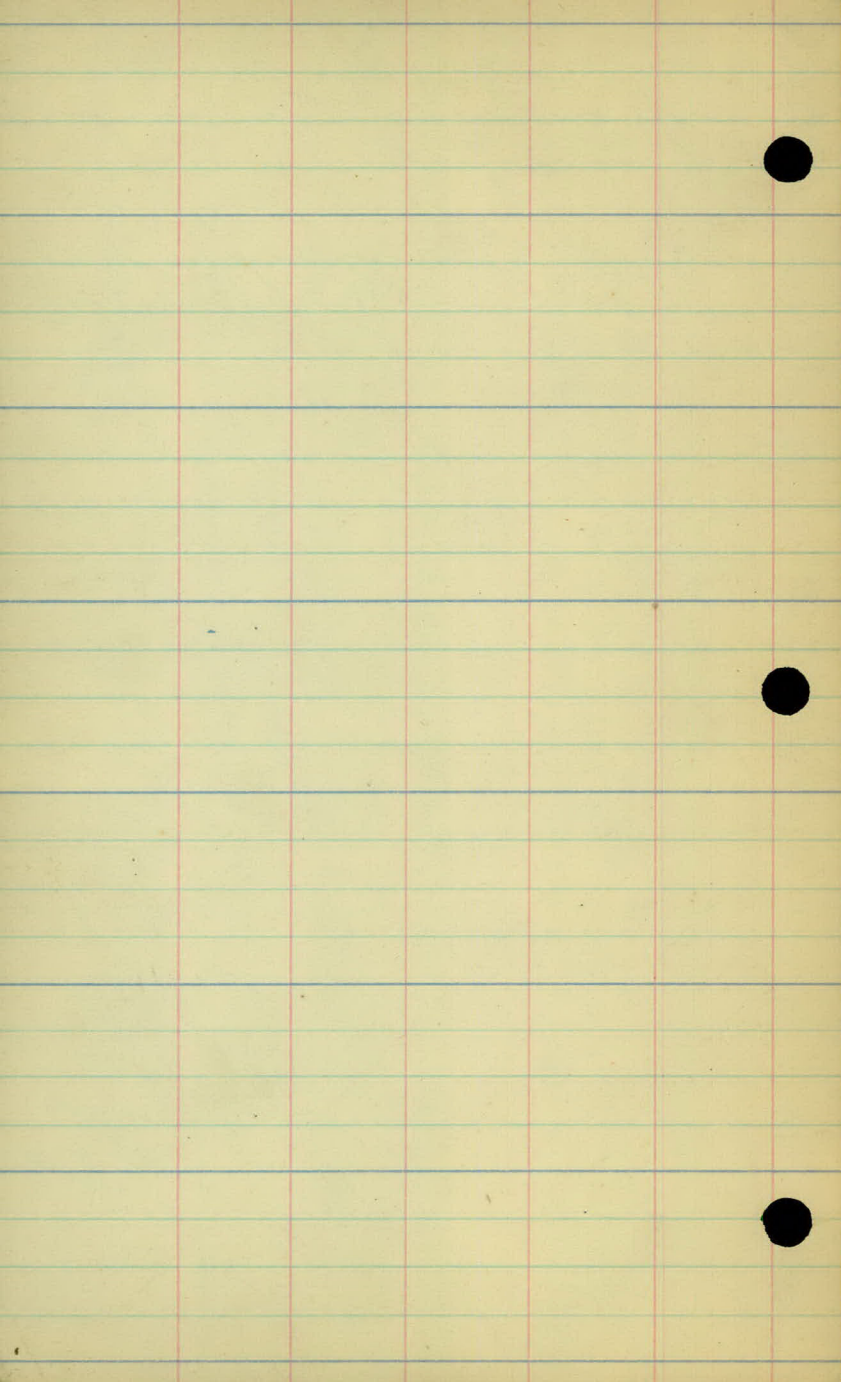
Length = 450.0 ✓



SEC. T1E

"LI" LINE
ORR.





191

L

"LI" LINE

PRB 2-20-25

LI-PT-190+244

190

CULTIVATED FIELD

189

188

SEE "L" LINE
FOR TOPOG. ON THIS
SIDE PRO.

L "LI" LINE

187

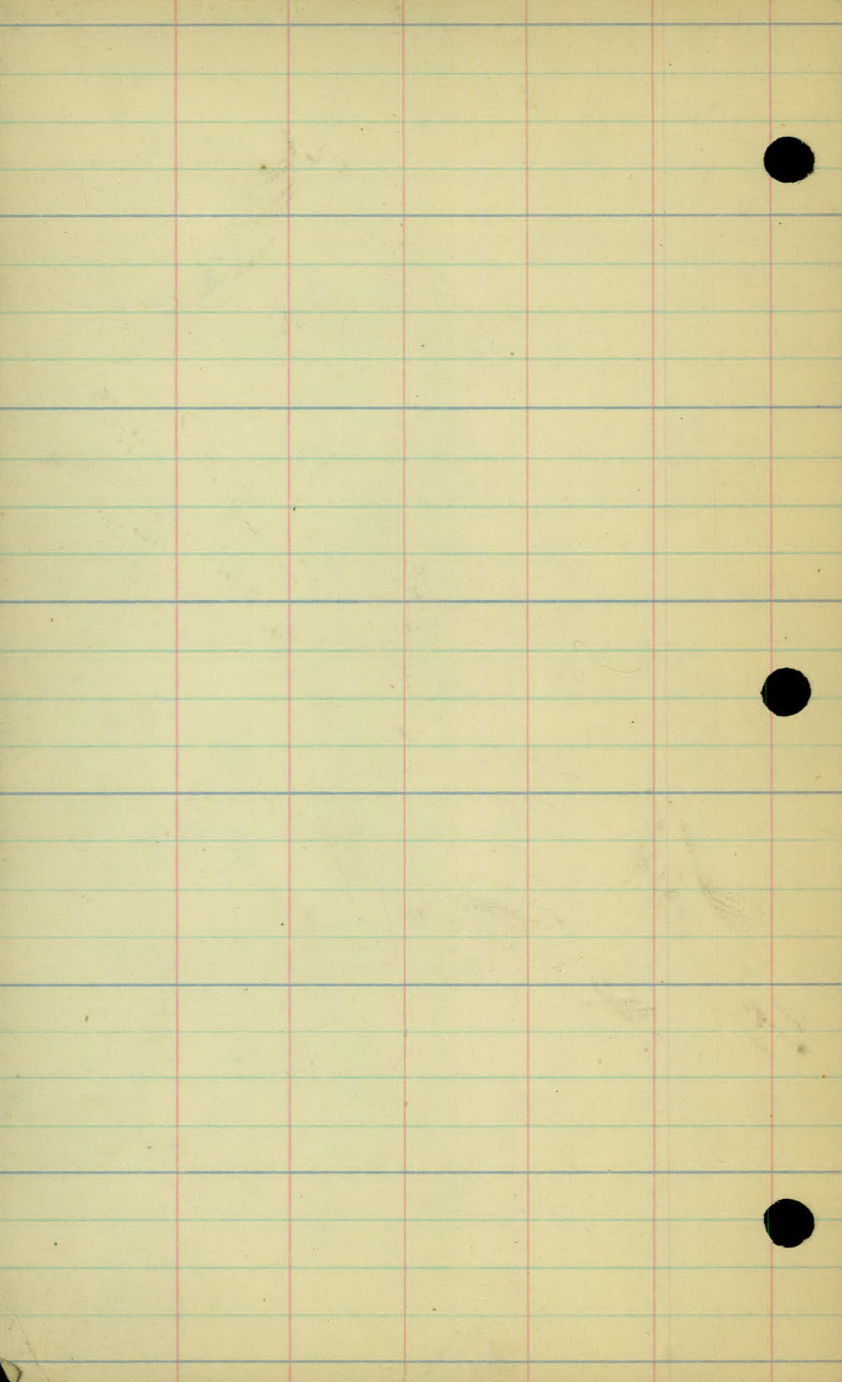
186

LI-185+744 P.C.
L-185+744 POT.

L "L" LINE

TIES TO P.I.

P.I. LI-188+120 =
L-188+120 POT.449 F.P.
38.15 F.P.10° CL.
Δ 45° 00'
ST-237.6
L-450.0



198

"L1" LINE PRB-2-20-25

+57.0¢ Road

+50¢ 16' Gate L

old Ho. Fdn

+30 T.P. 42' R.

+26 Fc. Xing

+08 PP+Fc Cor 24' R

+04 Fc. Cor 15' R

197

6. 14

+855 E Cor Shed 152' L

Pump

+33 T.P. 121' R.

+00 Fc. 114' R

+00¢ Rd 130

196

+95 SE Cor Barn 121' L

195

PASTURE
(Boggy)+85 Fc. 42' R
(Tree)

+34 Fc. X.

+34 Fc. 120' L

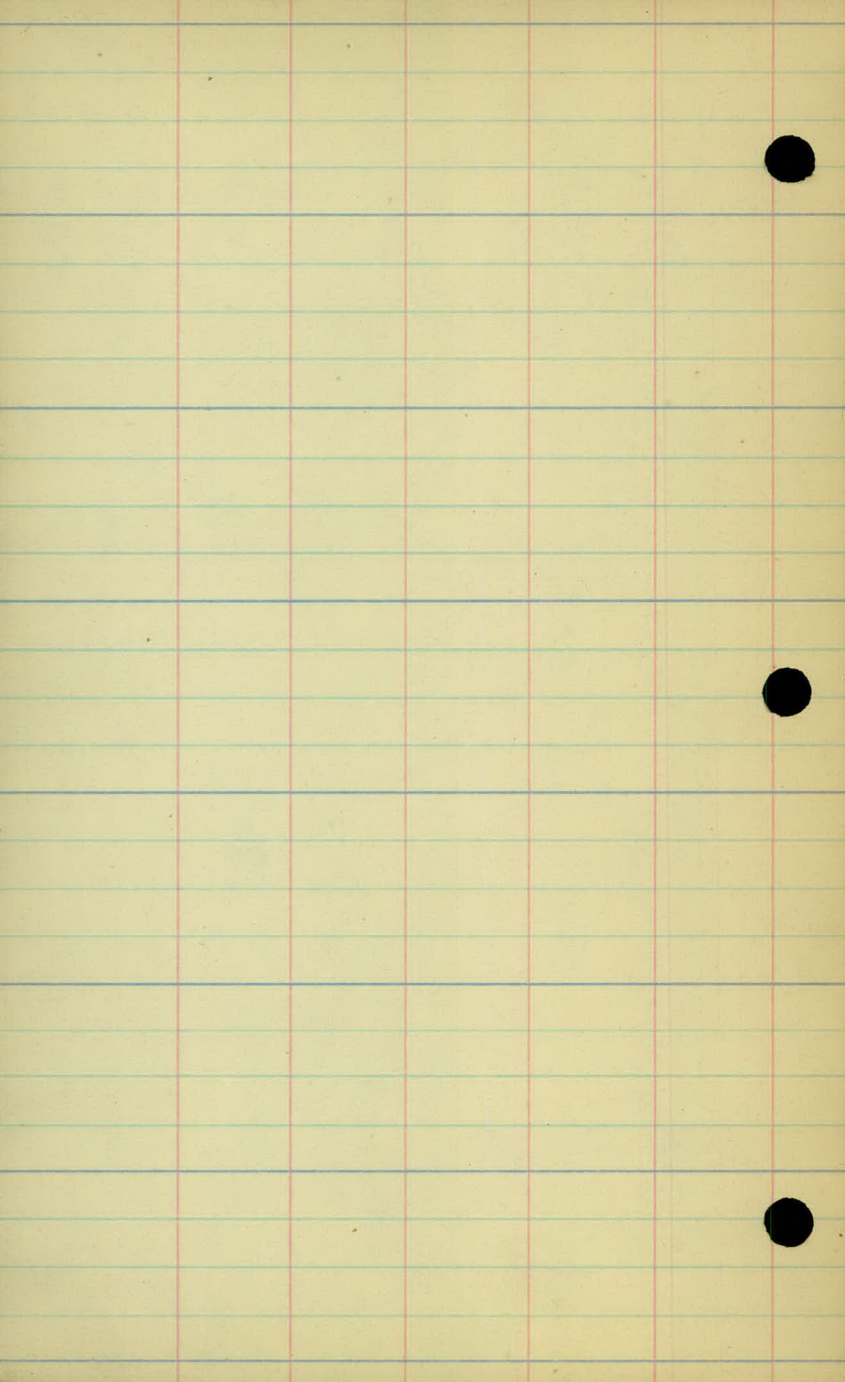
194 Fc. Cor. 39' L

193

CULTIVATED
FIELD

192

191



205

£

"LI" LINE

2-20-25

P&B.

PC 204+35.8

204

203

202

201

200

CULTIVATED FIELD

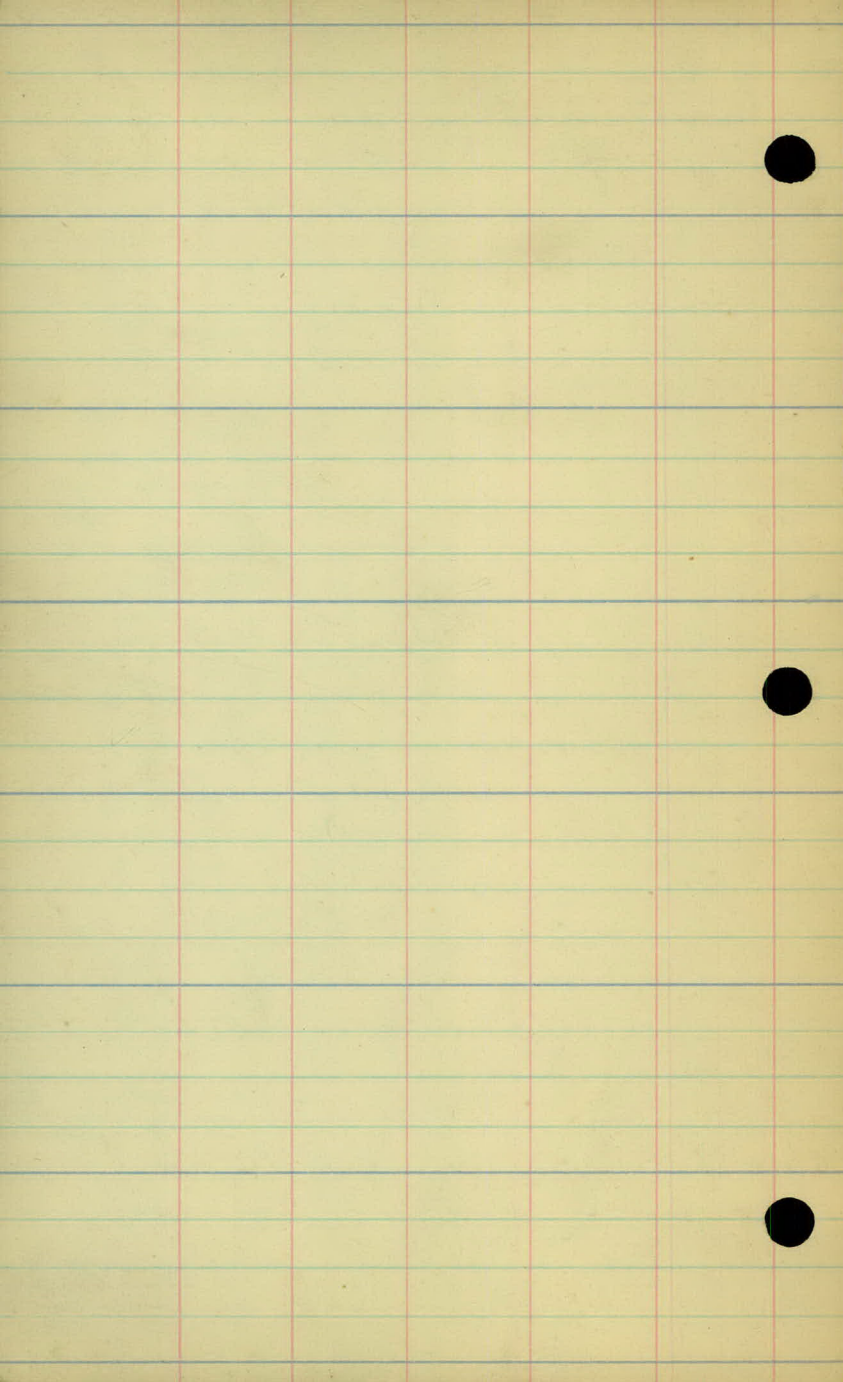
199

+34 P.P. 90° L

+21 T.P. 42° L End Fc.

198 +100 Fc-65 L

197 25° L



212

1" LINE

211

+52 P.P. 25.5

210

209

+0.3 P.P. 23.5

FT-208-87'

+50 { Rd-3'
Fc-32'

208

+00 { Rd-6
Fc-33'

+50 { Rd-18' + Fc-42'

+20 { Rd-25' + PP-46

+20 Fc-Xing.

+00 { Rd-33'

+00 Fc-82

207

+95 T.P. 19'

206

+50 { Fc-29
Rd-56

+17 T.P. 66

+15 PP 101

+11 Fc-32'

+10 { T.P. + Fc-142

+00 { Rd-160

205

+15 - 24° C.M.P. 30' long

+19 21' P+

+35 36' +15 Silo +38 15' Lido
+26 23' +26 Rep. Fence 94

+77 75 100 30'

+66 DRIVE 60 60 60

+26 26' 102' 14' Brick Ho

+70 102' 14'

+50 Fc-22'

+00 Fc-17

+85 T.P. 6'R

+50 Fc-8.5R

CULTIVATED
FIELD

7.0

9.0

8.5

8.0

6.5

4.5

6' line

219

33

x
x
x
x
x

32.5

218

+72 P.P. 22' H

x
x
x
x
x

31

217

+94 P.P. 21' H

x
x
x
x
x

30

216

x
x
x
x
x

29

215

+96 P.P. 19.5

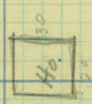
x x x

x
x
x
x
x

28

214

Cultivated



x
x
x
x
x

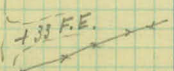
27.5

213

+51 P.P. 20' H
+33 ± D.I.I.E
+26 ± 27.5 H

x
x
x
x
x

+71 ± 18' R.I



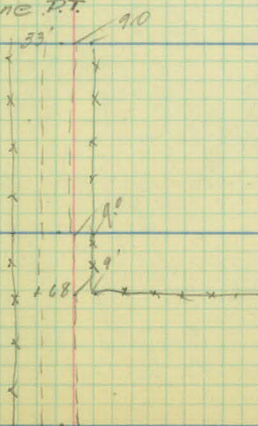
+17 F.E. 19.5

212

7.0

7.5

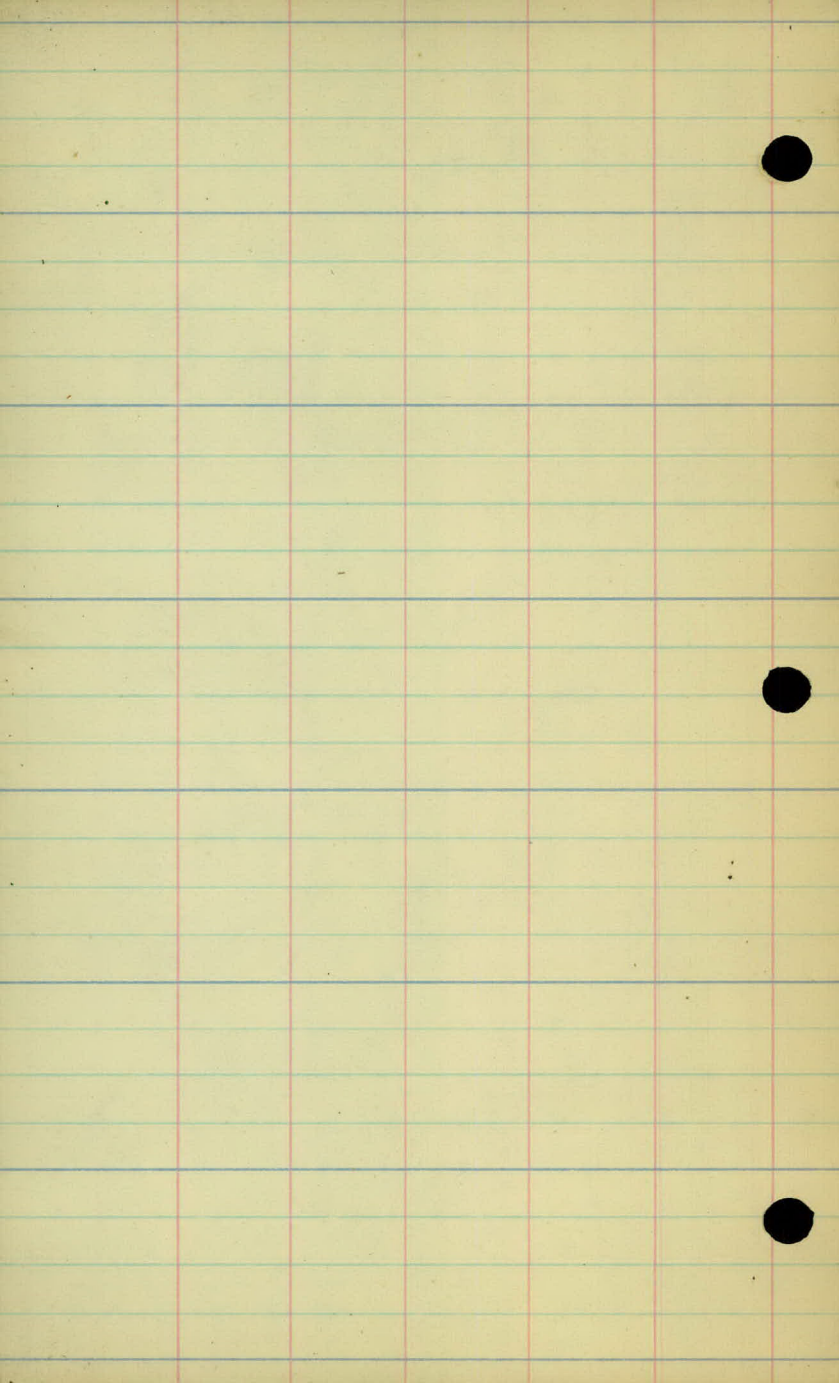
$$221 + 13.0 L_1 = 220 + 00.8 L_1 \text{ hinc. P.T.}$$



221

220

219



L' Line

Center levels on the
L' Line from Sta. 185+74⁺
to Sta. 221+13⁰.

Sta.	+	M.I.	-	Red.	Elev.
B.M.	4.43	710.45		914.02	
185+74 ⁴	P.C.			5.5	915.0.
186				5.3	915.2.
+50				5.2	915.3.
187				5.3	915.2.
+15				5.4	915.1.
+50				7.4	913.1.
T.P	1.64	711.82	10.27	910.18	
188				3.6	908.2.
+50				6.0	905.8.
189				4.2	905.6.
+50				6.2	905.6.
190				6.6	905.2.
+24 ⁴				8.1	903.7.
+50				8.0	903.8.
+62				7.3	904.5.
+74				7.4	904.4.
191				8.7	903.1.
+25				9.2	902.6.
+50				8.3	903.5.
192				5.6	904.2.
+15				4.3	907.5.
+50				3.6	908.2.
193				4.9	906.9.
T.P.	0.94	908.08	4.70	907.12	
+50				2.4	905.7.
194				3.6	904.5.

2/20/20

L'Line

Sp. in 18" Elm 35' Lt. Sta. 181+35

Sta.	+	H.I. ✓	-	Red.	Elev.
		708.08			
+50				4.9	703.2.
195				5.2	702.9.
+50				5.4	702.5.
196				5.6	702.5.
+50				4.8	703.3.
B.M.				2.84	705.24 ✓
197				3.5	704.4.
+34				1.5	706.4.
+42				0.4 ✓	707.5.
T.P.	10.34	714.17 ✓	2.25	705.83	
+54	Center of cross Rd.			8.2	708.0.
+81				7.3	706.9.
198				6.2	710.0.
+50				4.2	712.0.
199				3.7	712.5.
+50				3.4	712.4.
200				4.4	711.8.
+50				6.3	709.9.
201				8.2	708.0.
+50				8.5	707.7.
202				8.0 ✓	708.2.
T.P.	2.84	711.08 ✓	7.93	702.24	
+50				4.4	706.7.
203				4.4	706.7.
+50				4.9	706.2.
+70				5.0	706.1.

2/20/25

L' Line

Spk. in 14" Oak, 55' Lt. Sta. 194 + 40.

<u>11.7</u>	<u>10.5</u>	<u>9.9</u>	<u>9.3</u>
200	150	100	50

<u>8.4</u>	<u>9.2</u>	<u>9.6</u>	<u>9.8</u>
50	100	150	200

Sta.	+	H.I.	-	Elev.
		711.08		
	+92			4.8 904.3
204				4.6 904.5
	+50			4.4 904.5
205				4.9 904.2
	+50			4.5 904.4
206				5.1 905.9
	+50			4.1 905.0
207				5.5 905.6
	+45			4.2 906.9
	+50			4.2 904.9
208				4.5 904.4
T.P.	1.09	905.94	6.23	904.85
	+50			2.3 903.6
209				3.1 902.7
	+50			4.4 901.3
B.M.				1.63 904.31
210				5.9 900.0
B.M.	0.35	905.94	0.35	905.59
	+50			6.7 899.2
211				4.8 899.1
	+50			4.7 899.2
212				6.4 899.5
	+50			5.4 900.5
T.P.	5.67	906.47	5.14	900.80
213				4.7 901.8
	+50			4.4 902.1

2/20/28

L' Line

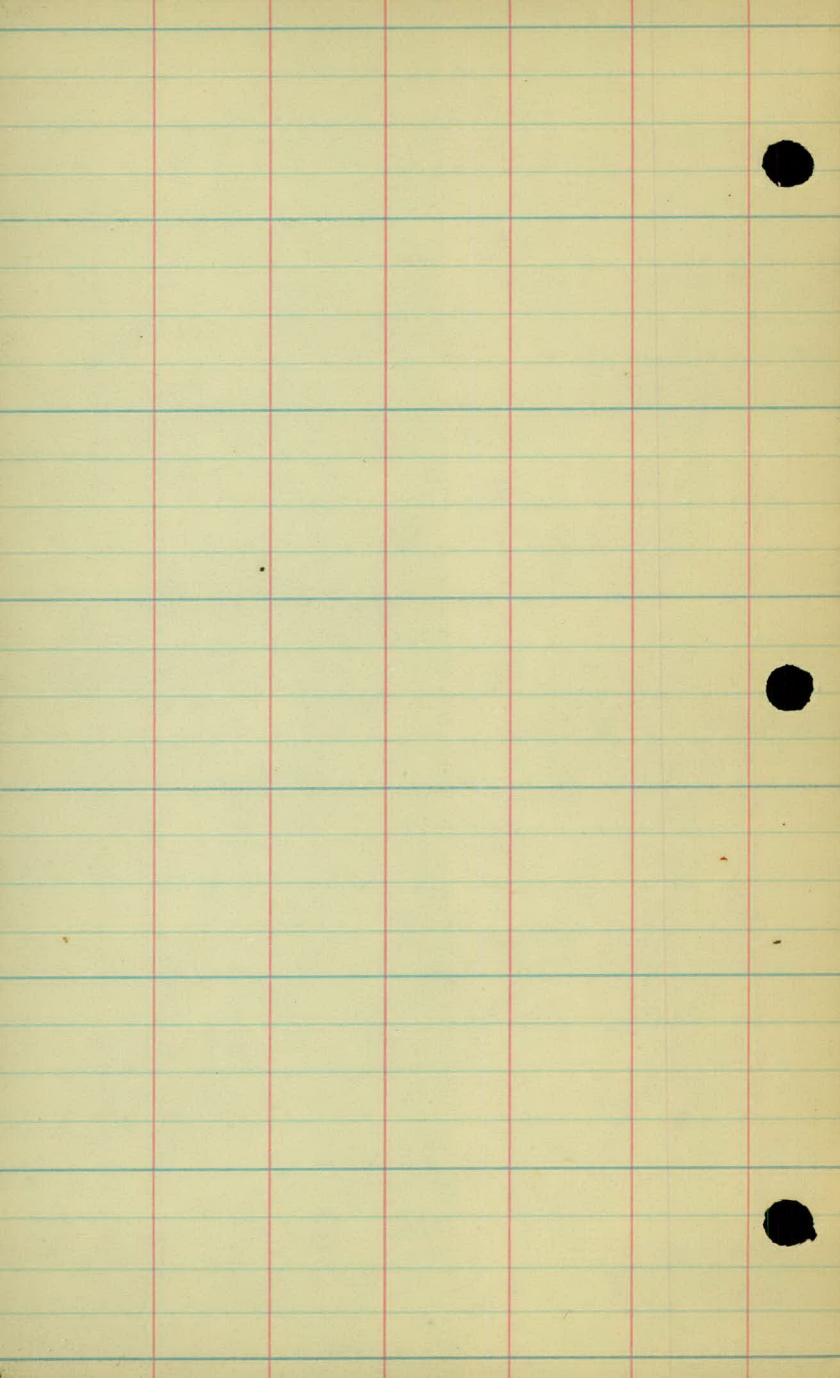
spl. in 40" cottonwood Rt. Sta. 209+35.

On Top of lower conc. step N.E. Cor. Rt. Sta. 209+20.

Sta.	+	H.I.	-	Elev.
		906.47		
214				5.3 901.2.
+50				5.2 901.3.
215				5.5 901.0.
+50				5.7 900.8.
214				4.4 901.9.
+50				3.0 903.5.
217				0.5 904.0.
T.P.	5.68	911.38	0.77	905.90
+50				3.3 908.1.
218				2.4 908.8.
+50				4.2 907.2.
219				6.4 905.0.
+50				7.6 903.8.
220				7.5 903.9.
+50				4.4 904.8.
221				7.1 904.3.
221 + 13° = 220 + 00.8			L. Line	7.4 903.0 904.0
T.P.	10.79	914.84	7.31	904.07
B.M.			1.44	913.42 913.41

L1 Line.

2/20/25



L' Line,

x sec. on the L' Line,
from Sta. 185+74² to Sta. 220+63.

Sta.	T	H.I.	-	Elev.
185 + 74 ⁴	4.23	710.25		716.02

186

+50

187

+50

T.P.	2.84	712.07	11.04	709.11
------	------	--------	-------	--------

188

+50

189

+50

190

+35

+47

191

L' Line.

1/21/22

$$\begin{array}{ccccccccc} \frac{5.5}{33} & \frac{5.5}{19} & \frac{5.8}{13} & \frac{5.2}{7} & 5.2 & \frac{5.4}{3} & \frac{5.7}{4} & \frac{5.3}{12} & \frac{4.9}{22} & \frac{4.8}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{5.3}{33} & \frac{5.3}{19} & \frac{5.6}{13} & \frac{5.1}{7} & 5.1 & \frac{5.1}{3} & \frac{5.2}{4} & \frac{5.6}{16} & \frac{4.4}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{5.2}{33} & \frac{5.6}{10} & \frac{5.3}{5} & 4.9 & \frac{5.4}{7} & \frac{5.3}{16} & \frac{5.6}{16} & \frac{5.9}{33} \end{array}$$

$$\begin{array}{ccccccccc} \frac{4.4}{33} & \frac{4.2}{17} & \frac{4.9}{3} & 5.1 & \frac{4.9}{7} & \frac{5.3}{17} & \frac{5.2}{22} & \frac{5.7}{28} & \frac{5.1}{33} \end{array}$$

$$\begin{array}{ccccccc} \frac{7.9}{33} & \frac{7.4}{14} & 7.2 & \frac{7.4}{10} & \frac{7.8}{14} & \frac{8.2}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{4.1}{33} & \frac{4.3}{16} & 3.8 & \frac{3.2}{14} & \frac{3.5}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{6.5}{33} & \frac{6.6}{16} & 6.3 & \frac{6.2}{14} & \frac{5.5}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{7.5}{33} & \frac{7.0}{14} & 6.5 & \frac{5.7}{14} & \frac{4.8}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{8.4}{33} & \frac{7.6}{14} & 6.4 & \frac{5.4}{14} & \frac{4.8}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{8.8}{33} & \frac{8.4}{22} & \frac{8.0}{20} & \frac{7.7}{14} & 6.8 & \frac{6.5}{14} & \frac{6.6}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{8.9}{33} & \frac{8.8}{14} & 8.4 & \frac{8.1}{14} & \frac{7.7}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{9.1}{33} & \frac{9.1}{12} & \frac{8.6}{17} & 7.4 & \frac{7.7}{14} & \frac{7.8}{33} \end{array}$$

$$\begin{array}{cccccc} \frac{9.4}{33} & \frac{8.9}{14} & 7.0 & \frac{8.9}{14} & \frac{8.8}{33} \end{array}$$

Sta. + H.I. - Elev.

912.07

+24

192

+50

193

194

195

196

B.M. 9.30 914.54 6.83 905.14 905.14

197

+57

+78

98

+35

99

L' Line.

2/21/25

$$\begin{array}{r} 10.0 \\ 33 \end{array} \quad \begin{array}{r} 9.5 \\ 14 \end{array} \quad 7.8 \quad \begin{array}{r} 9.5 \\ 14 \end{array} \quad \begin{array}{r} 9.3 \\ 33 \end{array}$$

$$\begin{array}{r} 8.0 \\ 33 \end{array} \quad \begin{array}{r} 6.8 \\ 14 \end{array} \quad 5.8 \quad \begin{array}{r} 5.0 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad 3.9 \quad \begin{array}{r} 3.2 \\ 14 \end{array} \quad \begin{array}{r} 3.3 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad 5.1 \quad \begin{array}{r} 4.7 \\ 14 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 8.2 \\ 33 \end{array} \quad \begin{array}{r} 8.3 \\ 14 \end{array} \quad 7.7 \quad \begin{array}{r} 6.3 \\ 14 \end{array} \quad \begin{array}{r} 7.4 \\ 33 \end{array}$$

$$\begin{array}{r} 9.8 \\ 33 \end{array} \quad \begin{array}{r} 9.6 \\ 14 \end{array} \quad 9.2 \quad \begin{array}{r} 9.0 \\ 14 \end{array} \quad \begin{array}{r} 9.0 \\ 33 \end{array}$$

$$\begin{array}{r} 9.3 \\ 33 \end{array} \quad \begin{array}{r} 9.5 \\ 14 \end{array} \quad 9.5 \quad \begin{array}{r} 9.6 \\ 14 \end{array} \quad \begin{array}{r} 9.5 \\ 33 \end{array}$$

SpK in 24" Oak 55' 14.5 Sta 196 + 40.

$$\begin{array}{r} 10.9 \\ 33 \end{array} \quad \begin{array}{r} 10.8 \\ 14 \end{array} \quad 9.8 \quad \begin{array}{r} 8.9 \\ 14 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array}$$

$$\begin{array}{r} 8.2 \\ 33 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \end{array} \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad 6.6 \quad \begin{array}{r} 7.1 \\ 12 \end{array} \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad \begin{array}{r} 7.3 \\ 13 \end{array} \quad \begin{array}{r} 5.1 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 33 \end{array}$$

$$\begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 7.8 \\ 12 \end{array} \quad 7.7 \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad \begin{array}{r} 4.7 \\ 15 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 2 \end{array} \quad 4.4 \quad \begin{array}{r} 3.7 \\ 14 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array}$$

$$\begin{array}{r} 5.1 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 30 \end{array} \quad \begin{array}{r} 3.5 \\ 14 \end{array} \quad 2.7 \quad \begin{array}{r} 2.6 \\ 14 \end{array} \quad \begin{array}{r} 2.8 \\ 33 \end{array}$$

$$\begin{array}{r} 3.9 \\ 33 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad 2.1 \quad \begin{array}{r} 1.7 \\ 14 \end{array} \quad \begin{array}{r} 2.0 \\ 33 \end{array}$$

Sta. + H.I. - Elev.
914.54

+43

100

T.P. 3.47 912.51 5.50 909.04

+40

101

+50

102

+50

103

+70

104

+50

105

+50

L'Line.

2/21/23

$$\begin{array}{r} 2.6 \\ 33 \end{array} \quad \begin{array}{r} 2.4 \\ 14 \end{array} \quad 2.0 \quad \begin{array}{r} 1.7 \\ 14 \end{array} \quad \begin{array}{r} 1.3 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 2.9 \\ 14 \end{array} \quad 2.7 \quad \begin{array}{r} 2.7 \\ 14 \end{array} \quad \begin{array}{r} 2.6 \\ 33 \end{array}$$

$$\begin{array}{r} 2.9 \\ 33 \end{array} \quad \begin{array}{r} 3.0 \\ 14 \end{array} \quad 2.7 \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad 4.5 \quad \begin{array}{r} 4.7 \\ 14 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad 4.8 \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.1 \\ 33 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad 4.3 \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad 5.8 \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad 5.9 \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 7.9 \\ 33 \end{array} \quad \begin{array}{r} 7.4 \\ 22 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad 6.2 \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 7.6 \\ 4 \end{array} \quad 7.9 \quad \begin{array}{r} 8.7 \\ 7 \end{array} \quad \begin{array}{r} 7.6 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad 8.0 \quad \begin{array}{r} 8.8 \\ 10 \end{array} \quad \begin{array}{r} 9.1 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad 6.3 \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 7.1 \\ 33 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 5.9 \\ 14 \end{array} \quad 6.0 \quad \begin{array}{r} 6.3 \\ 14 \end{array} \quad \begin{array}{r} 6.6 \\ 33 \end{array}$$

Sta. + H.T. - Elev.

912.51

206

+50

207

T.P. 3.08 909.61 5.98 906.53

+43

+69

208

+50

209

+48

+56

B.N.

5.33 904.18 904.31

L' Line.

2/21/25

$$\begin{array}{r} 7.5 \\ 33 \end{array} \quad \begin{array}{r} 6.8 \\ 16 \end{array} \quad 6.4 \quad \begin{array}{r} 6.5 \\ 14 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array}$$

$$\begin{array}{r} 8.4 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 27 \end{array} \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad 7.5 \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 28 \end{array} \quad \begin{array}{r} 7.7 \\ 24 \end{array} \quad \begin{array}{r} 7.7 \\ 14 \end{array} \quad 6.9 \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 6.8 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 29 \end{array} \quad \begin{array}{r} 4.4 \\ 11 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 5.9 \\ 5 \end{array} \quad 2.9 \quad \begin{array}{r} 2.7 \\ 6 \end{array} \quad \begin{array}{r} 2.6 \\ 11 \end{array} \quad \begin{array}{r} 3.1 \\ 14 \end{array} \quad \begin{array}{r} 3.4 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 6.8 \\ 29 \end{array} \quad \begin{array}{r} 6.7 \\ 27 \end{array} \quad \begin{array}{r} 4.0 \\ 22 \end{array} \quad \begin{array}{r} 4.3 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 4 \end{array} \quad 5.7 \quad \begin{array}{r} 2.7 \\ 4 \end{array} \quad \begin{array}{r} 3.2 \\ 20 \end{array} \quad \begin{array}{r} 3.4 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 31 \end{array} \quad \begin{array}{r} 7.1 \\ 26 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 4.5 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 14 \end{array} \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad 4.9 \quad \begin{array}{r} 5.8 \\ 9 \end{array} \quad \begin{array}{r} 5.8 \\ 7 \end{array} \quad \begin{array}{r} 4.1 \\ 11 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

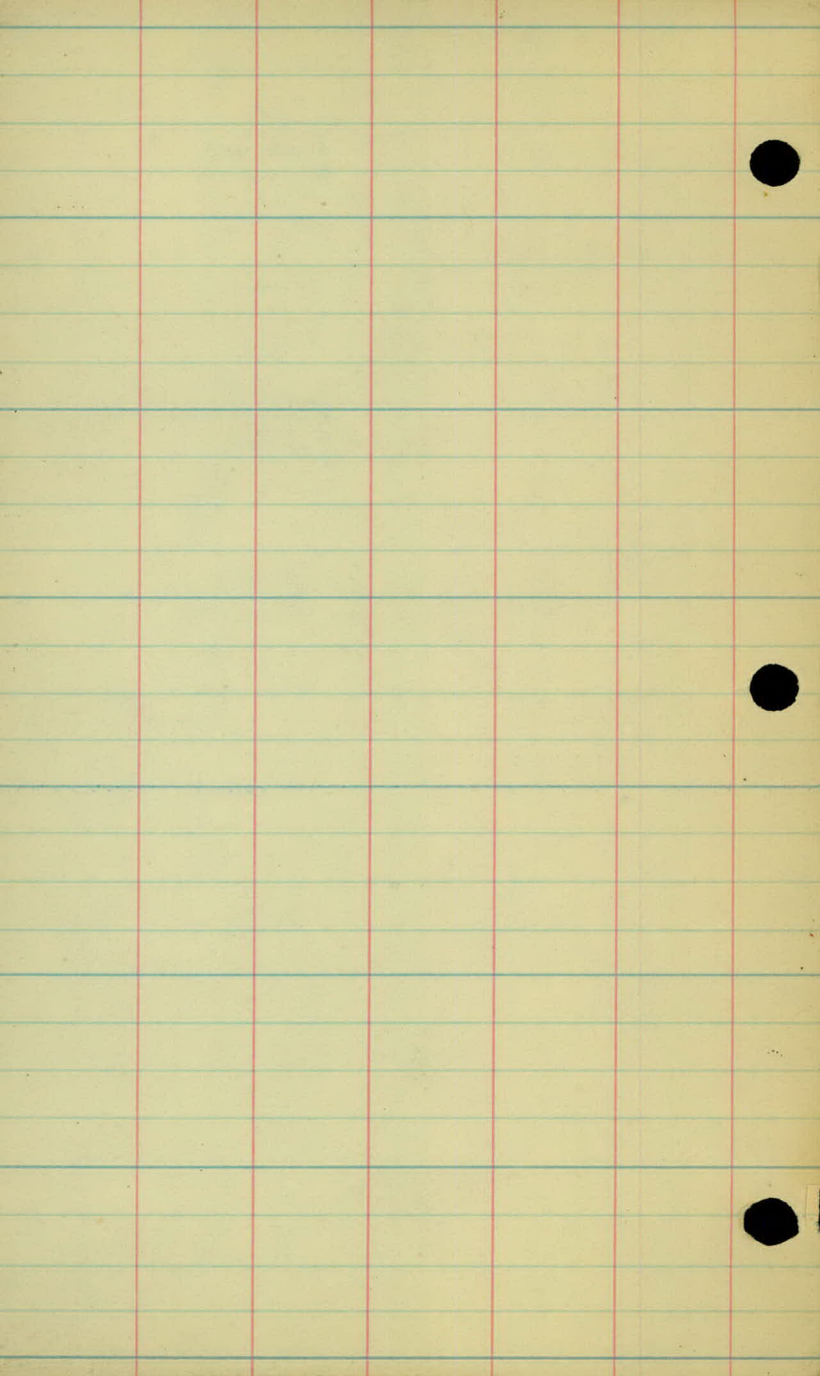
$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 28 \end{array} \quad \begin{array}{r} 8.2 \\ 21 \end{array} \quad \begin{array}{r} 8.0 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad 6.0 \quad \begin{array}{r} 5.9 \\ 6 \end{array} \quad \begin{array}{r} 6.8 \\ 9 \end{array} \quad \begin{array}{r} 6.7 \\ 13 \end{array} \quad \begin{array}{r} 4.5 \\ 16 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array}$$

$$\begin{array}{r} 8.1 \\ 33 \end{array} \quad \begin{array}{r} 7.9 \\ 22 \end{array} \quad \begin{array}{r} 9.1 \\ 19 \end{array} \quad \begin{array}{r} 8.8 \\ 14 \end{array} \quad \begin{array}{r} 7.4 \\ 12 \end{array} \quad 4.9 \quad \begin{array}{r} 7.1 \\ 8 \end{array} \quad \begin{array}{r} 7.8 \\ 12 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 33 \end{array} \quad \begin{array}{r} 8.5 \\ 21 \end{array} \quad \begin{array}{r} 7.6 \\ 18 \end{array} \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 8.1 \\ 11 \end{array} \quad 8.2 \quad \begin{array}{r} 8.7 \\ 14 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 7.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 24 \end{array} \quad \begin{array}{r} 8.6 \\ 21 \end{array} \quad \begin{array}{r} 9.9 \\ 18 \end{array} \quad \begin{array}{r} 8.6 \\ 15 \end{array} \quad \begin{array}{r} 8.2 \\ 11 \end{array} \quad \begin{array}{r} 8.5 \\ 10 \end{array} \quad 8.5 \quad \begin{array}{r} 8.8 \\ 20 \end{array} \quad \begin{array}{r} 8.5 \\ 33 \end{array}$$

Spk. in 40" Cottonwood Rt. Sta. 209+35



Road. 62 + 63.

"h₁" line X-Sections.

Li line

Station	+	H.I.	-	Rod.	Elev.
B.M.	0.09	904.40			904.31
210 + 00					
+ 47					
211 + 00					
+ 37					
212 + 00					
+ 43					
213 + 00					
+ 44					
T.P.	7.27	909.66	2.01	902.39	
214 + 00					
215 + 00					
216 + 00					
217 + 00					
T.P.	8.74	915.76	2.64	907.02	

210+00

K-1

L

R-1

"hj"-line

Splice in Cottonwood Rd. Sta. 209+35

<u>4.5</u>	<u>4.2</u>	<u>5.6</u>	<u>5.1</u>	<u>4.3</u>	<u>4.2</u>	<u>4.5</u>	<u>4.4</u>
33.0	17.5	18.0	14.5	13.0	8.5	4.5	33.0

<u>5.6</u>	<u>5.9</u>	<u>6.3</u>	<u>6.0</u>	<u>5.3</u>	<u>5.5</u>	<u>6.2</u>
33.0	21.0	18.0	14.0	9.5	5.3	33.0

<u>8.2</u>	<u>7.6</u>	<u>7.2</u>	<u>5.2</u>	<u>5.7</u>	<u>7.2</u>	<u>7.3</u>	<u>7.8</u>	<u>7.3</u>
33.0	25.0	12.0	6.0	5.3	11.5	16.0	21.0	33.0

<u>7.6</u>	<u>7.9</u>	<u>7.8</u>	<u>7.5</u>	<u>5.8</u>	<u>5.4</u>	<u>7.0</u>	<u>8.4</u>	<u>8.4</u>	<u>7.0</u>	<u>6.7</u>	<u>7.2</u>
33.0	26.0	16.5	13.5	8.0	5.2	6.0	11.0	15.0	17.0	20.5	33.0

<u>5.8</u>	<u>5.6</u>	<u>5.0</u>	<u>4.9</u>	<u>5.0</u>	<u>6.4</u>	<u>7.7</u>	<u>7.7</u>	<u>6.8</u>	<u>5.8</u>	<u>6.0</u>
33.0	17.0	9.0	4.9	8.0	13.0	15.0	16.0	17.0	20.0	29.0
									<u>6.8</u>	<u>35.0</u>

<u>3.2</u>	<u>3.7</u>	<u>4.4</u>	<u>4.6</u>	<u>4.0</u>	<u>3.9</u>	<u>4.0</u>	<u>5.5</u>	<u>7.3</u>	<u>7.3</u>	<u>5.9</u>	<u>5.6</u>
33.0	19.5	18.0	16.0	14.0	3.0	4.0	6.0	15.0	17.5	19.0	33.0

<u>0.0</u>	<u>1.8</u>	<u>3.1</u>	<u>3.2</u>	<u>2.2</u>	<u>2.5</u>	<u>2.7</u>	<u>4.5</u>	<u>7.0</u>	<u>7.0</u>	<u>6.3</u>	<u>5.0</u>
33.0	22.0	16.5	14.0	3.0	2.5	8.0	14.0	18.0	19.0	25.0	33.0

<u>0.0</u>	<u>0.3</u>	<u>1.3</u>	<u>3.4</u>	<u>3.4</u>	<u>2.5</u>	<u>2.1</u>	<u>2.6</u>	<u>3.6</u>	<u>6.7</u>	<u>6.3</u>	<u>5.5</u>	<u>3.8</u>	<u>2.8</u>
33.0	28.0	21.0	18.0	16.0	10.0	4.0	2.4	7.5	10.5	16.0	18.5	34.0	37.0

<u>8.7</u>	<u>9.0</u>	<u>9.3</u>	<u>9.3</u>	<u>8.7</u>	<u>8.3</u>	<u>8.5</u>	<u>9.5</u>	<u>12.0</u>	<u>10.6</u>	<u>9.0</u>	<u>8.8</u>
33.0	24.0	22.0	18.0	12.0	5.0	8.6	2.0	10.0	15.0	16.0	33.0

<u>11.9</u>	<u>11.3</u>	<u>10.8</u>	<u>8.5</u>	<u>7.9</u>	<u>8.2</u>	<u>10.5</u>	<u>11.3</u>	<u>11.1</u>	<u>11.7</u>	<u>11.3</u>	<u>11.3</u>
33.0	25.0	20.0	14.0	7.0	7.5	8.6	3.5	8.0	10.5	14.0	33.0

<u>7.1</u>	<u>8.0</u>	<u>8.7</u>	<u>7.9</u>	<u>7.3</u>	<u>7.6</u>	<u>8.5</u>	<u>8.6</u>	<u>8.4</u>	<u>9.2</u>
33.0	27.0	24.0	19.0	8.5	2.5	8.1	3.0	8.0	15.0

<u>1.9</u>	<u>1.8</u>	<u>3.2</u>	<u>3.9</u>	<u>3.4</u>	<u>3.2</u>	<u>4.2</u>	<u>4.7</u>	<u>4.8</u>	<u>4.6</u>	<u>6.0</u>
33.0	27.5	26.5	23.0	18.0	8.0	3.6	2.0	6.0	11.0	33.0

"L" line

Station	+	HI	-	Rod	Elev
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915.76

217+66

218+00

+59

219+00

T.P.	4.64	909.23	11.17	904.59
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+61

220+00

+63

T.P.

3.51

905.92

old T. Rod "L" line

H.

4

77.
hi-line

217+66

$$\left\{ \begin{array}{cccccccc} 1.3 & 5.8 & 6.8 & 7.6 & 6.8 & 6.8 & 7.4 & 6.8 & 6.1 & 7.7 \\ 29.5 & 26.5 & 25.0 & 20.0 & 15.0 & 9.0 & 7.2 & 4.0 & 7.0 & 14.0 & 33.0 \\ 0.7 & & & & & & & & & & \\ 33.0 & & & & & & & & & & \end{array} \right.$$

$$\begin{array}{cccccccc} 0.6 & 3.5 & 6.3 & 7.7 & 7.6 & 7.0 & 6.4 & 7.3 & 6.7 & 5.4 & 5.8 & 6.8 \\ 35.0 & 30.0 & 26.0 & 22.0 & 20.0 & 16.0 & 9.0 & 7.2 & 11.5 & 5.5 & 14.0 & 22.0 & 33.0 \end{array}$$

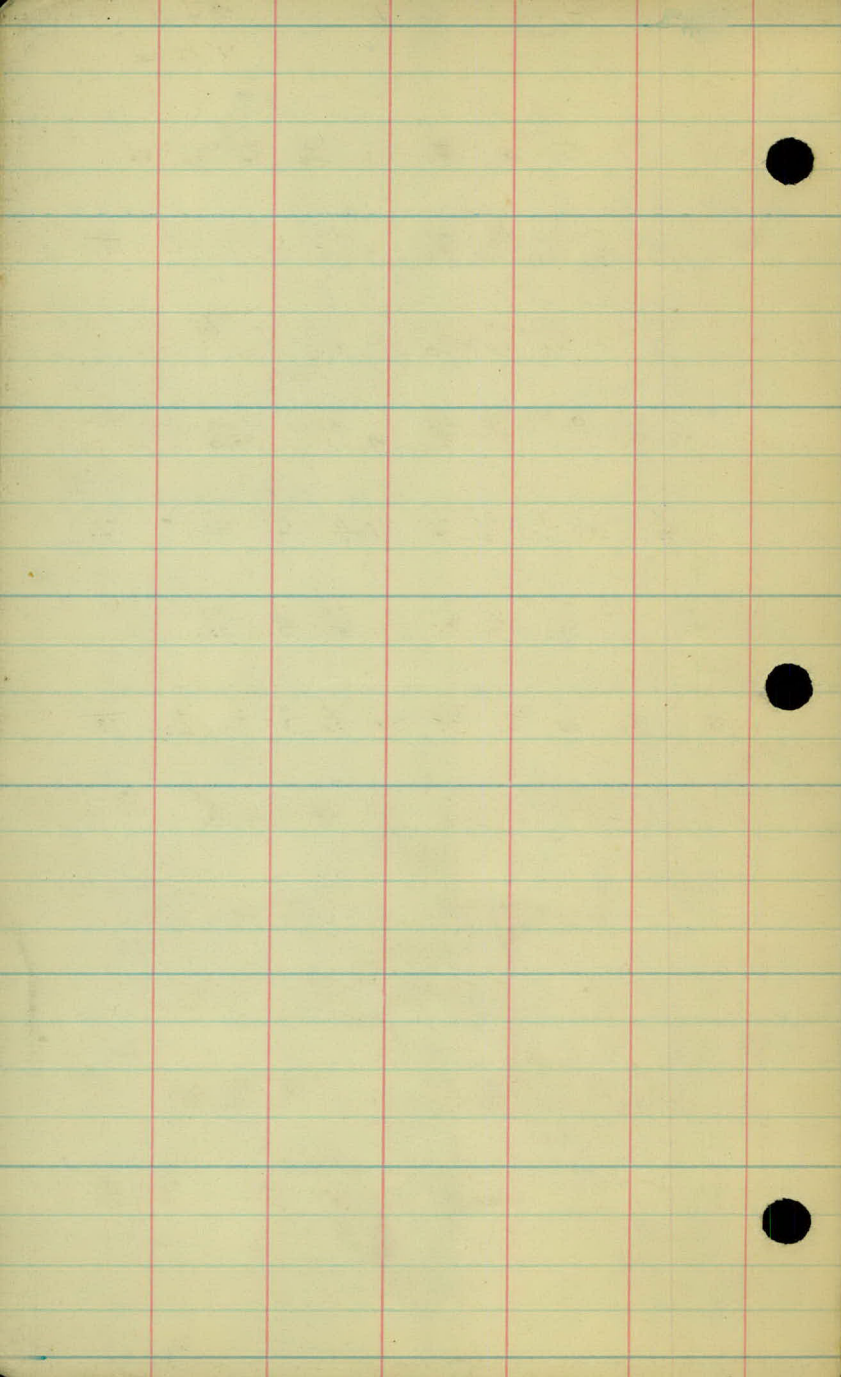
$$\begin{array}{cccccccc} 7.0 & 7.4 & 9.4 & 9.1 & 8.6 & 8.2 & 8.8 & 9.4 & 8.8 & 9.1 \\ 33.0 & 27.0 & 21.0 & 16.0 & 13.0 & 7.0 & 1.0 & 9.0 & 3.5 & 16.0 & 33.0 \end{array}$$

$$\begin{array}{cccccccc} 11.0 & 10.8 & 11.5 & 10.8 & 10.4 & 10.0 & 10.3 & 11.0 & 11.2 \\ 33.0 & 23.0 & 22.0 & 19.0 & 14.0 & 7.0 & 2.0 & 10.9 & 10.0 & 33.0 \end{array}$$

$$\begin{array}{cccccccc} 8.1 & 8.0 & 7.2 & 5.2 & 4.6 & 5.5 & 7.1 & 7.3 & 6.9 & 6.6 & 6.4 \\ 33.0 & 27.0 & 19.0 & 13.0 & 7.0 & 5.5 & 4.0 & 7.0 & 11.5 & 20.0 & 33.0 \end{array}$$

$$\begin{array}{cccccccc} 6.7 & 7.3 & 7.3 & 5.3 & 5.0 & 5.3 & 5.8 & 6.0 & 5.3 \\ 33.0 & 29.0 & 21.0 & 14.0 & 8.5 & 5.3 & 3.0 & 14.0 & 33.0 \end{array}$$

$$\begin{array}{cccccccc} 6.0 & 5.8 & 6.9 & 5.1 & 4.4 & 4.5 & 4.6 & 5.1 & 5.1 & 4.8 & 4.3 \\ 33.0 & 24.0 & 22.0 & 16.0 & 7.5 & 4.5 & 3.0 & 3.5 & 6.0 & 6.5 & 33.0 \end{array}$$



L'Line.

Drainaged notes on L'Line.

Sta.

207+70 Requires 12" C.M. if old road
is maintained.

211+15 Cross Drain 24" X 32" C.M. Good Cond.
Extends 15' Lt. & 17' Rt.

Inv. Elev. = 892.4

Drains Rt.

