

Book - 40 - Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

C.R.A. CONST. Survey

HAMLIN AVE.

From Co. Rd. "A" To Co. Rd. "B"

Road Acc't. No. 2

Date Filed 1934 File

CROSS SECTIONS

HAMLIN AVE.

Co Rd "A" TO

0+00 to 61+50

Jay ANDREWS

D. Roche He

H. Daly.

L. Nickle.

E. Golisch.

Feb-1934.

FS. HI BS Elev.

BM Spike Hamline 408 104.08 100.00

+ Cord "A"

0+00 R "A" Men 4.83

0+10 Edge Pav "A" 4.98

0+30 Break R. 4.91

0+50 4.82

1+00 4.22

1+50 3.28

1+66 R Drive R 20' W 3.05

2+00 2.62

2+26 L Drive L 20' W 2.28

2+50 1.96

3+00 1.45

① 304 105.68 1.44 102.64

HAMLIN
CO Rd A

AVE.

EDGE
PAV

EDGE
PAV

8" Crown

00

00 00 00

X	F	F	F	F	C	C						X
0.7	0.9	1.6	1.6	0.4	0.6							
32.4	33	31	28	26	21	00						

X	F	F	F	F	F	C	C					X
0.9	0.9	0.5	1.3	6.2	0.3	0.4	0.5					
34.4	33	25	24	21	19	18	15	00				

X	F	F	F	F	F	C	C					X
0.8	0.8	0.5	1.4	1.4	0.9	0.0	0.3					
34.6	33	24	22	20	19	18	14	00				

X	F	F	F	F	F	C	C					X
1.5	1.5	1.5	1.3	0.4	0.2							
36	33	23	19	18	13	00						

F	F	F	F	F	F	C						X
1.3	1.3	0.7	1.4	1.4	0.1	0.4						
35.6	33	23	21	19	18	13	00					

X	F	F	F	F	F	C						X
0.8	0.8	0.6	1.5	1.5	0.3	0.2						
34.6	33	23	22	19	18	12	00					

X	F	F	F	F	C						X
0.0	0.3	0.8	0.8	0.0	0.2						
3.2	23	22	19	18	13						

105.68

3+50

2.94

3+86 Drive L-20'W

3.13

4+00

3.22

4+50 Drive L-20'W

3.79

4+60

4+97 Drive L-20'W

4.89

5+00

4.95

+10

5+50

6.21

5+65.20 Drive L-20'W

6.44

5+86 Break R

6.63

6+00

6.97

6+27 Drive L-20'W

7.41

6+50

7.75

⑤

284

106.79

7.73

97.95

L.

R.

[illegible]

$\frac{X}{c}$	c	c	F	F	c	c	c	F	F	c	c	c	X
0.7	0.7	0.7	0.8	0.7	0.7	0.5	0.4	0.1	0.5	0.5	0.3	0.3	1.7
34.4	33	23	21	19	18	16	80	17	13	15	16	18	30.4

	C	F	L	C ⁴	C	C	C
	0.4	0.0	0.4	0.1	0.4	0.9	1.8
	8.6	12	15	17	18	21	24
							30.6

C	C	C	F	F	C	C	0.0
0.9	0.9	0.6		0.6	0.3	0.5	
54.8	53	23	21	19	18	12	0.0

[illegible]

$\frac{0.0}{0.0} \quad \frac{0.0}{24}$
 Reset at 3.1
 $\frac{0.0}{10} \quad \frac{0.3}{18} \quad \frac{0.5}{23} - \frac{3.1}{27.3}$

X	$\frac{X^2}{35}$	$\frac{X^3}{20}$	$\frac{X^4}{10}$	$\frac{X^5}{5}$	$\frac{X^6}{2}$	$\frac{X^7}{1}$	$\frac{X^8}{1}$
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.1	0.07	0.03	0.01	0.0008	0.0001	0.00001	0.000001
0.2	0.12	0.08	0.02	0.0016	0.0002	0.00002	0.000002
0.3	0.17	0.13	0.03	0.0024	0.0003	0.00003	0.000003
0.4	0.22	0.18	0.04	0.0032	0.0004	0.00004	0.000004
0.5	0.27	0.23	0.05	0.0040	0.0005	0.00005	0.000005
0.6	0.32	0.28	0.06	0.0048	0.0006	0.00006	0.000006
0.7	0.37	0.33	0.07	0.0056	0.0007	0.00007	0.000007
0.8	0.42	0.38	0.08	0.0064	0.0008	0.00008	0.000008
0.9	0.47	0.43	0.09	0.0072	0.0009	0.00009	0.000009
1.0	0.52	0.48	0.10	0.0080	0.0010	0.00010	0.000010
1.1	0.57	0.53	0.11	0.0088	0.0011	0.00011	0.000011
1.2	0.62	0.58	0.12	0.0096	0.0012	0.00012	0.000012
1.3	0.67	0.63	0.13	0.0104	0.0013	0.00013	0.000013
1.4	0.72	0.68	0.14	0.0112	0.0014	0.00014	0.000014
1.5	0.77	0.73	0.15	0.0120	0.0015	0.00015	0.000015
1.6	0.82	0.78	0.16	0.0128	0.0016	0.00016	0.000016
1.7	0.87	0.83	0.17	0.0136	0.0017	0.00017	0.000017
1.8	0.92	0.88	0.18	0.0144	0.0018	0.00018	0.000018
1.9	0.97	0.93	0.19	0.0152	0.0019	0.00019	0.000019
2.0	1.02	0.98	0.20	0.0160	0.0020	0.00020	0.000020
2.1	1.07	1.03	0.21	0.0168	0.0021	0.00021	0.000021
2.2	1.12	1.08	0.22	0.0176	0.0022	0.00022	0.000022
2.3	1.17	1.13	0.23	0.0184	0.0023	0.00023	0.000023
2.4	1.22	1.18	0.24	0.0192	0.0024	0.00024	0.000024
2.5	1.27	1.23	0.25	0.0200	0.0025	0.00025	0.000025
2.6	1.32	1.28	0.26	0.0208	0.0026	0.00026	0.000026
2.7	1.37	1.33	0.27	0.0216	0.0027	0.00027	0.000027
2.8	1.42	1.38	0.28	0.0224	0.0028	0.00028	0.000028
2.9	1.47	1.43	0.29	0.0232	0.0029	0.00029	0.000029
3.0	1.52	1.48	0.30	0.0240	0.0030	0.00030	0.000030
3.1	1.57	1.53	0.31	0.0248	0.0031	0.00031	0.000031
3.2	1.62	1.58	0.32	0.0256	0.0032	0.00032	0.000032
3.3	1.67	1.63	0.33	0.0264	0.0033	0.00033	0.000033
3.4	1.72	1.68	0.34	0.0272	0.0034	0.00034	0.000034
3.5	1.77	1.73	0.35	0.0280	0.0035	0.00035	0.000035
3.6	1.82	1.78	0.36	0.0288	0.0036	0.00036	0.000036
3.7	1.87	1.83	0.37	0.0296	0.0037	0.00037	0.000037
3.8	1.92	1.88	0.38	0.0304	0.0038	0.00038	0.000038
3.9	1.97	1.93	0.39	0.0312	0.0039	0.00039	0.000039
4.0	2.02	1.98	0.40	0.0320	0.0040	0.00040	0.000040
4.1	2.07	2.03	0.41	0.0328	0.0041	0.00041	0.000041
4.2	2.12	2.08	0.42	0.0336	0.0042	0.00042	0.000042
4.3	2.17	2.13	0.43	0.0344	0.0043	0.00043	0.000043
4.4	2.22	2.18	0.44	0.0352	0.0044	0.00044	0.000044
4.5	2.27	2.23	0.45	0.0360	0.0045	0.00045	0.000045
4.6	2.32	2.28	0.46	0.0368	0.0046	0.00046	0.000046
4.7	2.37	2.33	0.47	0.0376	0.0047	0.00047	0.000047
4.8	2.42	2.38	0.48	0.0384	0.0048	0.00048	0.000048
4.9	2.47	2.43	0.49	0.0392	0.0049	0.00049	0.000049
5.0	2.52	2.48	0.50	0.0400	0.0050	0.00050	0.000050

HI
100.79

6+88 Drive-L-20'W

3.30

7+00

3.40

7+09 12" C.I. Pipe 49-14

3.46

7+16

3.96

7+50

7+64 Drive-L-20'W

4.08

8+00

4.12

8+22 Fire Hy.L

4.21

8+45 Drive-L-20'W

4.44

8+50

4.50

8+55 Break-L

4.52

8+87

9+00

4.79

9+50

5.19

9+59 Corr Iron
Pipe 49-16

5.25

10+00

5.32

0

6.21

101.68

5.32

95.49

R

[illegible]

X	C	F	P	C	C	C	OC	OC	X
0.8	0.7	0.7	0.6	0.1	0.5	0.2	0.0	1.1	0.8
34.6	33	23	19	18	11.5	8.0	18	21	25.6

C	C	C	C	C	C	F	PC	DC	K
1.3	1.8	0.5	1.1	0.8	0.3	0.2	1.5	1.5	0.9
3.56	3.3	10	18	11.0	9.0	18	21	24	24.8

χ^2	C	C	F	C	C
3.2	3.1	2.3	0.1	0.7	0.7
39.6	33	26	19	18	11.5
					0.0

$\frac{30}{290}$	$\frac{79}{53}$	$\frac{22}{26}$	$\frac{06}{22}$	$\frac{05}{19}$	$\frac{03}{18}$	$\frac{06}{117}$	$\frac{03}{80}$	$\frac{03}{18}$	$\frac{26}{24}$
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X	C	C	F	F	L	C	C	F	F	X
33	37	22	10	05	0.4	0.7	-	03	1.1	5.6
396	33	26	22	19	18	12.2	00	80	18	35.2

X	C	C	C	F	C	C	F	F	X
20	19	24	0.0	0.1	0.6	0.7	0.4	0.5	9.6
270	28	25	22	13	18	12	0.0	80	37.4

101.68

10+50

5.95

11+00

5.19

11+31 - End of City Sec on Left

11+43 2 Drive L-20'W

4.88

11+50

4.88

12+00

4.97

12+50

5.05

12+89 S. L. Garden

5.16

13+00

5.18

13+08 - 12" C.I. Pipe

13+22 ^{East} ~~25~~ Garden Rd way 26'W.

5.03

13+50

4.98

13+54 N.L. Garden

5.00

14+00

4.57

D.

5.89

103.00

4.57

97.11

X	C	C	C	C	C	C	C	C	F	F	F	X
20	1.9	1.2	0.1	0.0	0.7	0.8	0.3	0.9	1.1	1.1	6.1	
37.0	22	24	21	19	18	11.5	0.0	8.0	16	18	30.2	

X	C	C	F	C	C	C	C	F	F	F	X
20	1.9	0.2	0.6	0.7	0.3	0.0	0.9	1.1	1.1	6.1	
27.0	33	19	18	14	0.0	8.0	13	18	23.8		
X	C	C	C	C	C	C	C	C	C	C	C
1.1	1.0	0.6	0.4	0.1	0.9						
35.2	33	27	19	18	7.5						

X	C	C	C	C	C	C	C	F	F	X
1.1	1.4	1.2	1.0	0.8	0.4	0.9	2.5			
30.0	24	21	18	9.5	0.0	8.0	18	23.0		

X	C	C	C	C	C	C	F	F	F	X
1.8	1.2	1.0	0.7	0.6	0.3	1.0	1.6	0.1	0.1	
30.6	24	21	18	11.0	0.0	8.0	18	21	30.2	

(Reset)
3-1-

X	C	C	C	C	C	C	F	F	F	X
1.3	0.9	0.7	0.3	0.2	0.3	0.3	1.1	3.6		
29.6	24	21	18	0.0	2.7	12	18	25.2		

X	C	C	C	C	C	C	C	C	C	C	C
0.8	0.6	0.6	0.6	0.6	0.6	0.5	0.2	1.0	0.5	0.5	
28.6	24	21	18	22.4	0.0	7.0	18	21	24	25	

X	C	C	C	C	C	C	C	F	C	C	C	X
0.5	0.6	0.5	1.1	0.0	0.3	0.3	0.6	0.5	0.4	0.9	1.1	1.5
28.2	24	22	21	18	17	12	0.0	7.2	15	18	21	27.0

X	C	C	C	C	C	C	C	F	F	C	C	C	C	X
1.5	1.5	1.5	1.0	0.2	0.4	0.4	0.4	0.2	0.2	0.3	0.9	0.8	1.1	1.5
27	24	22	21	18	13.6	0.0	7.0	12	17	18	19	21	24	29.4

103.00

14+50

5.39

15+00

5.03

15+50

5.01

16+00

4.79

16+45

4.63

16+50

16+59 Drive R-20'W

4.59

16+70

17+00

4.54

17+50

4.35

17+80

17+90 Z Drive R-20'W

4.15

18+00

4.09

18+50

3.66

19+00

3.13

⊙

901

102.83

3.13

99.87

$\frac{x}{DC}$	$\frac{BC}{AC}$	$\frac{DC}{AC}$	$\frac{C}{AB}$	$\frac{A}{CB}$	$\frac{F}{AB}$	$\frac{F}{AC}$	$\frac{D}{AB}$	$\frac{C}{AB}$	$\frac{C}{AC}$	$\frac{C}{AB}$	$\frac{x}{AB}$
$\frac{1.3}{26.6}$	$\frac{0.5}{24}$	$\frac{0.8}{21}$	$\frac{0.0}{18}$	$\frac{0.5}{14}$	$\frac{0.7}{13}$	$\frac{0.9}{14}$	$\frac{0.0}{17}$	$\frac{1.5}{18}$	$\frac{1.8}{21}$	$\frac{1.6}{24}$	$\frac{1.9}{30.8}$

X													
DC	C	C	DC	F	C	F	F	C	C	C		X	
1.2	0.3	0.1	1.0	0.1	0.4	0.5	0.0	0.8	0.8	1.4	1.4	1.6	2.0
2.7	2.4	2.3	1.9	1.8	2.6	7.0	1.2	13	17	18	21	24	31.0

$\bar{X}$	$\bar{Y}$	$\bar{X}^2$	$\bar{Y}^2$	$\bar{X}\bar{Y}$	$\bar{X} - \bar{X}_0$	$\bar{Y} - \bar{Y}_0$	$(\bar{X} - \bar{X}_0)^2$	$(\bar{Y} - \bar{Y}_0)^2$	$(\bar{X} - \bar{X}_0)(\bar{Y} - \bar{Y}_0)$
1.0	1.0	1.0	1.0	1.0	0.6	0.0	0.36	0.00	0.00
1.2	1.2	1.44	1.44	1.44	0.8	0.2	0.64	0.04	0.16
1.4	1.4	1.96	1.96	1.96	1.0	0.4	1.00	0.16	0.40
1.6	1.6	2.56	2.56	2.56	1.2	0.6	1.44	0.36	0.72
1.8	1.8	3.24	3.24	3.24	1.4	0.8	1.96	0.64	1.12
2.0	2.0	4.00	4.00	4.00	1.6	1.0	2.56	1.00	1.60
2.2	2.2	4.84	4.84	4.84	1.8	1.2	3.24	1.44	2.16
2.4	2.4	5.76	5.76	5.76	2.0	1.4	4.00	1.96	2.80
2.6	2.6	6.76	6.76	6.76	2.2	1.6	4.84	2.56	3.52
2.8	2.8	7.84	7.84	7.84	2.4	1.8	5.76	3.24	4.32
3.0	3.0	9.00	9.00	9.00	2.6	2.0	6.76	4.00	5.28
3.2	3.2	10.24	10.24	10.24	2.8	2.2	7.84	4.84	6.16
3.4	3.4	11.56	11.56	11.56	3.0	2.4	9.00	5.76	7.20
3.6	3.6	12.96	12.96	12.96	3.2	2.6	10.24	6.76	8.32
3.8	3.8	14.44	14.44	14.44	3.4	2.8	11.56	7.84	9.52
4.0	4.0	16.00	16.00	16.00	3.6	3.0	12.96	9.00	10.80
4.2	4.2	17.64	17.64	17.64	3.8	3.2	14.44	10.24	12.16
4.4	4.4	19.36	19.36	19.36	4.0	3.4	16.00	11.56	13.60
4.6	4.6	21.16	21.16	21.16	4.2	3.6	17.64	12.96	15.12
4.8	4.8	23.04	23.04	23.04	4.4	3.8	19.36	14.44	16.72
5.0	5.0	25.00	25.00	25.00	4.6	4.0	21.16	16.00	18.40
5.2	5.2	27.04	27.04	27.04	4.8	4.2	23.04	17.64	20.16
5.4	5.4	29.16	29.16	29.16	5.0	4.4	25.00	19.36	22.00
5.6	5.6	31.36	31.36	31.36	5.2	4.6	27.04	21.16	23.92
5.8	5.8	33.64	33.64	33.64	5.4	4.8	29.16	23.04	25.92
6.0	6.0	36.00	36.00	36.00	5.6	5.0	31.36	25.00	28.00
6.2	6.2	38.44	38.44	38.44	5.8	5.2	33.64	27.04	30.16
6.4	6.4	40.96	40.96	40.96	6.0	5.4	36.00	29.16	32.40
6.6	6.6	43.56	43.56	43.56	6.2	5.6	38.44	31.36	34.72
6.8	6.8	46.24	46.24	46.24	6.4	5.8	40.96	33.64	36.96
7.0	7.0	49.00	49.00	49.00	6.6	6.0	43.56	36.00	39.60
7.2	7.2	51.84	51.84	51.84	6.8	6.2	46.24	38.44	42.16
7.4	7.4	54.76	54.76	54.76	7.0	6.4	49.00	40.96	44.80
7.6	7.6	57.76	57.76	57.76	7.2	6.6	51.84	43.56	47.52
7.8	7.8	60.64	60.64	60.64	7.4	6.8	54.76	46.24	50.24
8.0	8.0	63.60	63.60	63.60	7.6	7.0	57.76	49.00	52.96
8.2	8.2	67.24	67.24	67.24	7.8	7.2	60.64	51.84	55.68
8.4	8.4	70.56	70.56	70.56	8.0	7.4	63.60	54.76	58.40
8.6	8.6	73.96	73.96	73.96	8.2	7.6	66.96	57.76	61.12
8.8	8.8	77.44	77.44	77.44	8.4	7.8	70.56	60.64	63.84
9.0	9.0	81.00	81.00	81.00	8.6	8.0	73.96	63.60	66.56
9.2	9.2	84.64	84.64	84.64	8.8	8.2	77.44	66.96	69.28
9.4	9.4	88.36	88.36	88.36	9.0	8.4	81.00	70.56	72.00
9.6	9.6	92.16	92.16	92.16	9.2	8.6	84.64	73.96	74.72
9.8	9.8	96.04	96.04	96.04	9.4	8.8	88.36	77.44	77.44
10.0	10.0	100.00	100.00	100.00	9.6	9.0	92.16	81.00	80.16
10.2	10.2	104.04	104.04	104.04	9.8	9.2	96.04	84.64	82.88
10.4	10.4	108.16	108.16	108.16	10.0	9.4	100.00	88.36	85.60
10.6	10.6	112.36	112.36	112.36	10.2	9.6	104.04	92.16	88.32
10.8	10.8	116.64	116.64	116.64	10.4	9.8	108.16	96.04	91.04
11.0	11.0	121.00	121.00	121.00	10.6	10.0	112.36	100.00	93.76
11.2	11.2	125.44	125.44	125.44	10.8	10.2	116.64	104.04	96.48
11.4	11.4	130.00	130.00	130.00	11.0	10.4	121.00	108.16	99.20
11.6	11.6	134.64	134.64	134.64	11.2	10.6	125.44	112.36	101.92
11.8	11.8	139.36	139.36	139.36	11.4	10.8	130.00	116.64	104.64
12.0	12.0	144.00	144.00	144.00	11.6	11.0	134.64	121.00	107.36
12.2	12.2	148.84	148.84	148.84	11.8	11.2	139.36	125.44	110.08
12.4	12.4	153.76	153.76	153.76	12.0	11.4	144.00	130.00	112.80
12.6	12.6	158.76	158.76	158.76	12.2	11.6	148.84	134.64	115.52
12.8	12.8	163.84	163.84	163.84	12.4	11.8	153.76	139.36	118.24
13.0	13.0	169.00	169.00	169.00	12.6	12.0	158.76	144.00	120.96
13.2	13.2	174.24	174.24	174.24	12.8	12.2	163.84	148.84	123.68
13.4	13.4	179.56	179.56	179.56	13.0	12.4	169.00	153.76	126.40
13.6	13.6	185.00	185.00	185.00	13.2	12.6	174.24	158.76	129.12
13.8	13.8	190.44	190.44	190.44	13.4	12.8	179.56	163.84	131.84
14.0	14.0	196.00	196.00	196.00	13.6	13.0	185.00	169.00	134.56
14.2	14.2	201.64	201.64	201.64	13.8	13.2	190.44	174.24	137.28
14.4	14.4	207.36	207.36	207.36	14.0	13.4	196.00	179.56	140.00
14.6	14.6	213.16	213.16	213.16	14.2	13.6	201.64	185.00	142.72
14.8	14.8	219.04	219.04	219.04	14.4	13.8	207.36	190.44	145.44
15.0	15.0	225.00	225.00	225.00	14.6	14.0	213.16	196.00	148.16
15.2	15.2	231.04	231.04	231.04	14.8	14.2	219.04	201.64	150.88
15.4	15.4	237.16	237.16	237.16	15.0	14.4	225.00	207.36	153.60
15.6	15.6	243.36	243.36	243.36	15.2	14.6	231.04	213.16	156.32
15.8	15.8	249.64	249.64	249.64	15.4	14.8	237.16	219.04	159.04
16.0	16.0	256.00	256.00	256.00	15.6	15.0	243.36	225.00	161.76
16.2	16.2	262.44	262.44	262.44	15.8	15.2	249.64	231.04	164.48
16.4	16.4	269.00	269.00	269.00	16.0	15.4	256.00	237.16	167.20
16.6	16.6	275.64	275.64	275.64	16.2	15.6	262.44	243.36	169.92
16.8	16.8	282.36	282.36	282.36	16.4	15.8	269.00	249.64	172.64
17.0	17.0	289.00	289.00	289.00	16.6	16.0	275.64	256.00	175.36
17.2	17.2	295.84	295.84	295.84	16.8	16.2	282.36	262.44	178.08
17.4	17.4	302.76	302.76	302.76	17.0	16.4	289.00	269.00	180.80
17.6	17.6	309.76	309.76	309.76	17.2	16.6	295.84	275.64	183.52
17.8	17.8	316.84	316.84	316.84	17.4	16.8	302.76	282.36	186.24
18.0	18.0	324.00	324.00	324.00	17.6	17.0	309.76	289.00	188.96
18.2	18.2	331.24	331.24	331.24	17.8	17.2	316.84	295.84	191.68
18.4	18.4	338.56	338.56	338.56	18.0	17.4	324.00	302.76	194.40
18.6	18.6	345.96	345.96	345.96	18.2	17.6	331.24	309.76	197.12
18.8	18.8	353.44	353.44	353.44	18.4	17.8	338.56	316.84	199.84
19.0	19.0	361.00	361.00	361.00	18.6	18.0	345.96	324.00	202.56
19.2	19.2	368.64	368.64	368.64	18.8	18.2	353.44	331.24	205.28
19.4	19.4	376.36	376.36	376.36	19.0	18.4	361.00	338.56	208.00
19.6	19.6	384.16	384.16	384.16	19.2	18.6	368.64	345.96	210.72
19.8	19.8	392.04	392.04	392.04	19.4	18.8	376.36	353.44	213.44
20.0	20.0	400.00	400.00	400.00	19.6	19.0	384.16	361.00	216.16
20.2	20.2	408.04	408.04	408.04	19.8	19.2	392.04	368.64	218.88
20.4	20.4	416.16	416.16	416.16	20.0	19.4	400.00	376.36	221.60
20.6	20.6	424.36	424.36	424.36	20.2	19.6	408.04	384.16	224.32
20.8	20.8	432.64	432.64	432.64	20.4	19.8	416.16	392.04	227.04
21.0	21.0	441.00	441.00	441.00	20.6	20.0	424.36	400.00	229.76
21.2	21.2	449.44	449.44	449.44	20.8	20.2	432.64	408.04	232.48
21.4	21.4	458.00	458.00	458.00	21.0	20.4	441.00	416.16	235.20
21.6	21.6	466.56	466.56	466.56	21.2	20.6	449.44	424.36	237.92
21.8	21.8	475.24	475.24	475.24	21.4	20.8	458.00	432.64	240.64
22.0	22.0	484.00	484.00	484.00	21.6	21.0	466.56	441.00	243.36
22.2	22.2	492.84	492.84	492.84	21.8	21.2	475.24	449.44	246.08
22.4	22.4	501.76	501.76	501.76	22.0	21.4	484.00	458.00	248.80
22.6	22.6	510.76	510.76	510.76	22.2	21.6	492.84	466.56	251.52
22.8	22.8	519.84	519.84	519.84	22.4	21.8	501.76	475.24	254.24
23.0	23.0	529.00	529.00	529.00	22.6	22.0	510.76	484.00	256.96
23.2	23.2	538.24	538.24	538.24	22.8	22.2	519.84	492.84	259.68
23.4	23.4	547.56	547.56	547.56	23.0	22.4	529.00	501.76	262.40
23.6	23.6	556.96	556.96	556.96	23.2	22.6	538.24	510.76	265.12
23.8	23.8	566.44	566.44	566.44	23.4	22.8	547.56	519.84	267.84
24.0	24.0	576.00	576.00	576.00	23.6	23.0	556.96	529.00	270.56
24.2	24.2	585.64	585.64	585.64	23.8	23.2	566.44	538.24	273.28
24.4	24.4	595.36	595.36	595.36	24.0	23.4	576.00	547.56	276.00
24.6	24.6	605.16	605.16	605.16	24.2	23.6	585.64	556.96	278.72
24.8	24.8	615.04	615.04	615.04	24.4	23.8	595.36	566.44	281.44
25.0	25.0								

X	DC	DC	DC	F	C		F	F	C	C	C	X
0.3	0.3	0.5	0.4	0.0	0.4		0.7	0.7	0.7	0.8	0.7	0.8
746	74	21	18	17	13	00	12	12	17	18	21	24

[illegible][illegible][illegible]

X	0.0	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0
$\frac{0.0}{25.4}$	$\frac{0.0}{24}$	$\frac{0.2}{21}$	$\frac{0.4}{18}$	$\frac{0.6}{13.0}$	$\frac{0.8}{7.0}$	$\frac{1.0}{1.8}$	$\frac{1.2}{2.1}$	$\frac{1.4}{2.4}$	$\frac{1.6}{2.6}$	$\frac{1.8}{2.8}$	$\frac{2.0}{2.8}$

[illegible]

K	OC	OC	OC	F	OC	F	F	F	F	OC	OC	K
0.1	0.1	0.2	0.7	0.3	0.5	0.8	0.7	0.3	1.2	1.3	1.4	OC
244	24	21	18	15	11	12	14	15	18	21	24	26

108.88

19+50

8.42

19+68 Drive R.

8.13

19+78

20+00

7.64

20+50

6.98

21+00

6.20

21+50

5.27

21+64 Drive R

5.10

+75

22+00

4.59

22+50

3.93

23+00

3.60

23+50

3.33

23+61 Drive L

3.78

23+73

23+89 ✓ R

3.33

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.0	0.5	0.9	0.0	0.4	0.4	0.1	0.6	0.6	0.1	0.5	1.1	1.1	
24	21	18	15	12	00	70	12	13	15	18	21	24	29.7

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.5	0.5	0.6	0.7	0.4	0.4	0.2	0.6	0.6	0.7	0.7	0.8	1.1	2.0
24	21	18	15	12	00	70	11	12	14	16	18	21	31.0

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.6	0.6	0.6	0.7	0.3	0.5	0.5	0.8	0.8	0.8	0.3	1.2	1.1	1.8
25.2	24	21	18	12	00	74	12	13	15	17	18	21	26.3

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
1.4	1.5	0.8	0.5	0.8	0.3	0.5	0.4	0.0	1.0	1.0	0.3	1.2	2.3
26.8	26.0	24	21	20	18	16	12	00	80	12	13	15	31.6

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.4	0.4	1.3	0.9	0.6	0.5	0.5	0.5	0.1	0.9	0.9	0.8	1.5	2.2
27.8	24	21	20	18	15	00	80	13	14	16	18	21	31.6

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.4	0.6	0.9	0.6	0.5	0.5	0.5	0.0	0.8	0.8	0.4	1.5	1.0	1.9
27.8	24	21	18	15	00	80	13	14	16	18	21	24	30.8

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.2	0.6	0.5	0.7	0.4	0.4	0.0	0.2	1.4	1.1	0.1	1.8	2.5	2.6
27.6	24	21	18	12	00	84	13	16	18	21	24	26	32.2

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.7	0.8	0.5	0.8	0.3	0.4	0.5	0.2	0.9	0.7	0.3	1.5	3.7	4.8
28.4	24	21	18	17	15	00	80	11	14	18	21	24	35.6

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
0.3	0.2	0.6	0.3	0.4	0.4	0.4	0.3	1.0	0.4	0.1	0.7	0.9	
27.6	24	21	18	16	00	80	12	15	18	21	24	28.8	

X	DC	DC	F	F	C	C	C	F	F	C	C	C	X
1.5	0.1	0.5	0.2	0.6	0.6	0.0	0.0	0.7	0.0	1.5	0.2	0.2	
27.0	24	21	18	15	00	86	13	15	18	21	24	27.6	

108.88

24+00

3.32

24+20

①

5.13

110.71

3.30

105.58

24+30

5.10

24+40 Drive R.

5.10

24+50

5.09

25+00

5.00

25+50

4.76

26+00

4.30

26+12.50 L "A"

4.02

26+33.50 No Line Par

3.69

26+44.6 L "A"

3.44

26+55 Spike "A"

7.26

113.24

4.73

105.98

26+75 No Line Par

5.85

26+75 No Line "A"

5.58

41
113.24

27+00

5.49

27+50

4.33

27+75

28+00

2.46

28+50

1.14

○

5.99

118.09

1.14

112.10

29+00

5.11

29+50

4.53

30+00 - P.O.T. Nail

4.61

30+50

4.77

31+00

5.07

31+50

5.23

32+00

5.50

32+50

6.09

$$\begin{array}{cccccccccccc} X & F & F & F & C & & C & C & F & F & C & C & X \\ 2.0 & 0.8 & 0.3 & 0.2 & & 0.5 & 0.0 & 0.7 & 1.0 & 0.5 & 1.0 & 0.7 \\ 272 & 18 & 17 & 14 & 0.0 & 7.0 & 12 & 14 & 18 & 21 & 24 & 25.8 \end{array}$$

$$\begin{array}{cccccccccccc} X & F & F & F & C & & C & C & F & F & C & C & X \\ 1.9 & 0.6 & 0.1 & & 0.4 & 0.1 & 1.3 & 0.4 & 1.3 & 0.4 & 0.4 & 0.3 \\ 218 & 18 & 13 & 0.0 & 7.0 & 11 & 14 & 18 & 21 & 24 & 27.6 \\ X & & & & & & & & & & & & \\ 2.0 & & & & & & & & & & & & \\ 24 & & & & & & & & & & & & \\ X & & & & & & & & & & & & \\ 2.5 & 0.5 & 0.0 & 0.5 & C & & C & C & C & C & C & X \\ 21 & 18 & 14 & 0.0 & 7.0 & 15 & 18 & 21 & 24 & - & 1.3 & 29.6 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & F & F & C & & C & C & F & C & C & X \\ 1.3 & 1.5 & 0.9 & 1.0 & 0.2 & 0.4 & & 0.4 & 0.2 & 0.2 & 0.8 & 1.1 & 3.1 \\ 24.6 & 24 & 21 & 18 & 16 & 14 & 0.0 & 7.0 & 11 & 13 & 18 & 21 & 24 & 33.2 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & F & C & & C & C & F & C & C & C & X \\ 3.4 & 3.9 & 1.2 & 0.9 & 1.0 & 0.1 & & 0.4 & 0.3 & 0.2 & 0.2 & 0.3 & 0.6 & 0.7 & 5.5 \\ 338 & 25 & 21 & 20 & 18 & 17 & 0.0 & 8.0 & 12 & 15 & 18 & 21 & 24 & 28 & 38.2 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 5.6 & 6.7 & 0.6 & 0.9 & 0.7 & 0.2 & 0.2 & 0.6 & 0.0 & 0.2 & 0.4 & 1.3 & 4.7 & 6.5 \\ 382 & 28 & 27 & 26 & 21 & 18 & 12.5 & 0.0 & 7.0 & 12 & 18 & 21 & 24 & 28 & 39.4 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 2.0 & 8.7 & 1.3 & 0.8 & 1.5 & 0.0 & 0.5 & & 0.3 & 0.4 & 0.4 & 2.1 & 4.5 & 5.2 \\ 43.0 & 39 & 28 & 24 & 21 & 18 & 12.5 & 0.0 & 8.0 & 18 & 21 & 24 & 26 & 38.2 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 10.3 & 11.0 & 8.0 & 1.0 & 0.3 & 0.1 & 0.4 & & 0.4 & 0.4 & 0.4 & 0.6 & 0.8 & 4.1 & 4.4 \\ 47.6 & 37 & 35 & 24 & 21 & 18 & 14.0 & 0.0 & 8.0 & 18 & 21 & 24 & 26 & 27 & 34.8 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 11.5 & 11.6 & 8.1 & 0.8 & 0.3 & 0.0 & 0.3 & & 0.4 & 0.1 & 0.5 & 0.7 & 1.0 & 2.0 & 4.7 & 4.8 \\ 50.0 & 36 & 34 & 24 & 21 & 18 & 11.6 & 0.0 & 8.0 & 15 & 18 & 21 & 24 & 27 & 28 & 32.6 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 7.9 & 7.8 & 3.7 & 1.2 & 0.4 & 0.3 & 0.3 & 0.5 & & 0.4 & 0.1 & 0.5 & 1.1 & 3.5 & 3.7 \\ 428 & 34 & 31 & 29 & 24 & 21 & 18 & 12.4 & 0.0 & 8.0 & 18 & 21 & 24 & 30 & 34.4 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 4.9 & 5.7 & 3.2 & 2.0 & 0.2 & 0.2 & 0.2 & & 0.5 & 0.3 & 0.7 & 0.4 & 0.5 & 1.0 & 1.3 \\ 36.8 & 27 & 26 & 24 & 21 & 18 & 11.6 & 0.0 & 8.0 & 12 & 15 & 18 & 21 & 24 & 24.6 \end{array}$$

$$\begin{array}{cccccccccccc} X & C & C & C & F & C & & C & C & C & C & C & X \\ 2.9 & 3.6 & 3.0 & 0.5 & 0.0 & & & & 0.3 & 0.2 & 0.1 & 0.9 & 1.2 & - & 1.3 \\ 32.4 & 25 & 24 & 21 & 18 & 12 & 0.0 & & 8.0 & 15 & 18 & 21 & 24 & - & 29.6 \end{array}$$

118.09

32+88

33+00

c

6.08

0

0.83

112.44

6.48

111.61

33+09.42 Rgn Av

0.91

33+36

1.25

33+50

1.49

34+00

2.27

34+50

3.07

+ 83

35+00

4.32

054-35 Nail

4.32

108.12

	$\frac{C}{0.4}$	$\frac{C}{0.2}$	$\frac{F}{0.3}$	$\frac{F}{0.4}$	$\frac{C}{0.7}$	$\frac{C}{1.0}$	$\frac{C}{1.2}$	$\frac{X}{1.3}$
00	9.2	12	15	17	18	21	24	29.6

$\frac{X}{2.0}$	$\frac{C}{3.0}$	$\frac{C}{3.1}$	$\frac{DC}{1.1}$	$\frac{00}{18}$	$\frac{00}{15}$	$\frac{0.3}{11.5}$	0.0
31.0	28	24	21	18	15	11.5	0.0

	$\frac{C}{0.4}$	$\frac{C}{0.1}$	$\frac{F}{0.6}$	$\frac{F}{0.5}$	$\frac{0.3}{2.9}$	$\frac{X}{3.3}$
00	10.2	14	16	18	21	33.2

$\frac{X}{0.9}$	$\frac{C}{0.3}$	$\frac{DC}{1.5}$	$\frac{00}{18}$	$\frac{0.4}{11}$	0.0	$\frac{C}{0.2}$	$\frac{C}{0.1}$	$\frac{F}{0.8}$	$\frac{F}{0.8}$	$\frac{C}{0.1}$	$\frac{C}{3.2}$	$\frac{X}{3.4}$
28.8	24	21	18	11	0.0	10.2	13	15	18	21	24	33.8

$\frac{X}{1.4}$	$\frac{DC}{1.2}$	$\frac{DC}{0.9}$	$\frac{F}{0.6}$	$\frac{00}{15}$	$\frac{0.3}{11.0}$	0.0	$\frac{C}{0.3}$	$\frac{F}{1.1}$	$\frac{F}{1.1}$	$\frac{DC}{1.5}$	$\frac{C}{4.4}$	$\frac{X}{3.8}$
26.8	24	21	18	15	11.0	0.0	10.2	15	18	21	25	34.6

$\frac{X}{0.8}$	$\frac{DC}{0.8}$	$\frac{DC}{1.3}$	$\frac{F}{0.3}$	$\frac{0.5}{11}$	0.0	$\frac{C}{0.3}$	$\frac{00}{13}$	$\frac{F}{1.4}$	$\frac{F}{1.4}$	$\frac{DC}{2.4}$	$\frac{C}{1.5}$	$\frac{C}{4.3}$	$\frac{X}{4.7}$
21.6	24	21	18	11	0.0	9.6	13	17	18	21	24	30	36.4

	$\frac{F}{0.5}$	$\frac{C}{0.1}$	$\frac{0.6}{11}$	0.0
—	27	18	11	0.0

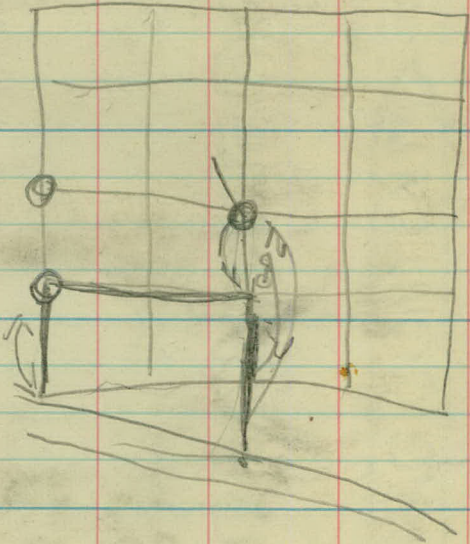
$\frac{X}{2.5}$	$\frac{F}{0.5}$	$\frac{00}{16}$	$\frac{C}{0.4}$	0.0	$\frac{C}{0.4}$	$\frac{C}{0.1}$	$\frac{F}{1.1}$	$\frac{DC}{0.5}$	$\frac{DC}{0.8}$	$\frac{X}{0.8}$
23.0	18	16	11	0.0	9.3	13	18	21	24	25.6

$$\begin{array}{r}
 116.88 \\
 4.81 \\
 \hline
 112.07 \\
 7.21 \\
 \hline
 1119.28
 \end{array}$$

$$\begin{array}{r}
 8.39 \\
 7.9 \\
 \hline
 49
 \end{array}$$

2.8

199



CROSS-SECTIONS

HAMLIN AVE

Sta 35+50 to 61+50

G.J. Murphy
E.J. Topley
L.O. Pratt
W. White
M. Groetch.

March - 1924

Sta

+

π

-

Elev.

B.M.

2.03

110.15

108.12

35+50

36+00

36+50

37+00

3-14-34

B.M.

2.05

110.17

108.12

37+50

Nail in pavement Sta 35+00

$$\begin{array}{r} 6.5 \\ \hline 50 \end{array} - \begin{array}{r} 2.8 \\ \hline 26.1 \end{array} \begin{array}{r} 3.8 \\ \hline 18 \end{array} \begin{array}{r} 3.8 \\ \hline 9 \end{array} \begin{array}{r} 3.4 \\ \hline 0 \end{array} \begin{array}{r} 3.5 \\ \hline 10 \end{array} \begin{array}{r} 3.4 \\ \hline 19 \end{array} - \begin{array}{r} 4.6 \\ \hline 31.8 \end{array} \begin{array}{r} 7.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.9 \\ \hline 50 \end{array} - \begin{array}{r} 2.7 \\ \hline 25.8 \end{array} \begin{array}{r} 4.3 \\ \hline 18 \end{array} \begin{array}{r} 4.1 \\ \hline 10 \end{array} \begin{array}{r} 4.1 \\ \hline 0 \end{array} \begin{array}{r} 4.4 \\ \hline 10 \end{array} \begin{array}{r} 4.3 \\ \hline 19 \end{array} - \begin{array}{r} 4.7 \\ \hline 32.1 \end{array} \begin{array}{r} 9.4 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.7 \\ \hline 50 \end{array} - \begin{array}{r} 2.5 \\ \hline 25.5 \end{array} \begin{array}{r} 5.0 \\ \hline 13 \end{array} \begin{array}{r} 4.6 \\ \hline 10 \end{array} \begin{array}{r} 4.4 \\ \hline 0 \end{array} \begin{array}{r} 4.7 \\ \hline 10 \end{array} \begin{array}{r} 4.6 \\ \hline 18 \end{array} - \begin{array}{r} 3.0 \\ \hline 27.0 \end{array} \begin{array}{r} 8.3 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 1.1 \\ \hline 21.3 \end{array} \begin{array}{r} 5.8 \\ \hline 50 \end{array} \begin{array}{r} 5.6 \\ \hline 23 \end{array} \begin{array}{r} 6.2 \\ \hline 11 \end{array} \begin{array}{r} 5.1 \\ \hline 14 \end{array} \begin{array}{r} 4.6 \\ \hline 10 \end{array} \begin{array}{r} 4.4 \\ \hline 0 \end{array} \begin{array}{r} 4.9 \\ \hline 11 \end{array} \begin{array}{r} 5.2 \\ \hline 18 \end{array} - \begin{array}{r} 2.7 \\ \hline 26.1 \end{array} \begin{array}{r} 6.6 \\ \hline 31 \end{array} \begin{array}{r} 5.8 \\ \hline 50 \end{array}$$

Nail in pavement at 35+00

$$\begin{array}{r} 6.0 \\ \hline 50 \end{array} \begin{array}{r} 6.2 \\ \hline 18 \end{array} \begin{array}{r} 4.9 \\ \hline 13 \end{array} \begin{array}{r} 4.4 \\ \hline 11 \end{array} \begin{array}{r} 4.4 \\ \hline 0 \end{array} \begin{array}{r} 4.8 \\ \hline 11 \end{array} \begin{array}{r} 7.2 \\ \hline 23 \end{array} \begin{array}{r} 7.3 \\ \hline 26 \end{array} \begin{array}{r} 6.9 \\ \hline 50 \end{array}$$

Sta	+	A	-	Elev
38.00		110.17	✓	108.12

38+50

39+00

B.M.	2.15	✓ 110.27		✓ 108.12
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X	6.17	✓ 110.69	5.75	✓ 104.52
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39+50

40+00

40+50

41+00

41+50

$$\begin{array}{r} C \\ 0.8 \\ \hline 23.6 \end{array} \quad \begin{array}{r} 3.9 \\ \hline 50 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 25 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 19 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.7 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 20 \end{array} \quad \begin{array}{r} 6.7 \\ \hline 24 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 3.4 \\ \hline 50 \end{array} \quad \text{Private Drive} \quad \begin{array}{r} 4.7 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.4 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.3 \\ \hline 19 \end{array} \quad \begin{array}{r} 6.8 \\ \hline 28 \end{array} \quad \begin{array}{r} 7.5 \\ \hline 50 \end{array} \quad \begin{array}{r} F1.5 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} C \\ 0.7 \\ \hline 21.4 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 24 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 20 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 19 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 12 \end{array} \quad \begin{array}{r} 4.4 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 10 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 18 \end{array} \quad \begin{array}{r} 6.8 \\ \hline 26 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 50 \end{array} \quad \begin{array}{r} F1.9 \\ \hline 23.7 \end{array}$$

Spike in pavement 26+00

$$\begin{array}{r} \text{Private} \\ \text{Driveway} \end{array} \quad \begin{array}{r} 5.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 19 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 10 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 0 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 9 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 19 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 24 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 50 \end{array} \quad \begin{array}{r} D.C \\ 0.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} F. \\ 1.5 \\ \hline 21.0 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 19 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 16 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 0 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 10 \end{array} \quad \begin{array}{r} 6.0 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.0 \\ \hline 50 \end{array} \quad \begin{array}{r} C. \\ 0.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} F. \\ 2.1 \\ \hline 21.3 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 20 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 15 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 10 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 17 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 21 \end{array} \quad \begin{array}{r} 1.7 \\ \hline 50 \end{array} \quad \begin{array}{r} C. \\ 2.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} F. \\ 2.3 \\ \hline 24.9 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.9 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.4 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 9 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 15 \end{array} \quad \begin{array}{r} 3.2 \\ \hline 50 \end{array} \quad \text{Private Driveway}$$

$$\begin{array}{r} F. \\ 1.7 \\ \hline 23.1 \end{array} \quad \begin{array}{r} 6.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 0 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 10 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 15 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 19 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 50 \end{array} \quad \begin{array}{r} F. \\ 1.4 \\ \hline 22.2 \end{array}$$

110,69

$4\frac{1}{2} + 50$

43 + 00

43 + 50

44 + 00

44 + 50

145700

$$\begin{array}{r}
 F, 2.2 \\
 \hline
 24.6
 \end{array}
 \quad
 \begin{array}{r}
 6.1 \\
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$$\begin{array}{r}
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 7.4 \\
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 \end{array}
 \quad
 \begin{array}{r}
 D.C \\
 0.9 \\
 \hline
 25.8
 \end{array}$$

Sta + P. = Elev.
114.60 ✓

45+50

✓

✓

B.M. 6.36 115.40 5.56 109.04

46+00

46+50

47+00

47+50

48+00

48+50

✓

✓

X 6.04 116.94 4.50 110.90

C. $\frac{0.1}{24.8}$ $\frac{4.8}{50}$ $\frac{5.1}{22}$ $\frac{6.7}{19}$ $\frac{5.3}{11}$ $\frac{4.9}{0}$ $\frac{5.2}{8}$ $\frac{6.5}{15}$ $\frac{5.4}{18}$ $\frac{5.7}{33}$ $\frac{6.0}{50}$ D.C. $\frac{1.2}{26.4}$

D.C. $\frac{1.5}{27.0}$ $\frac{4.9}{50}$ $\frac{4.1}{23}$ $\frac{6.2}{19}$ $\frac{5.2}{12}$ $\frac{4.8}{9}$ $\frac{6.2}{8}$ $\frac{6.3}{15}$ $\frac{4.4}{18}$ $\frac{7.1}{50}$ D.C. $\frac{1.8}{27.6}$

D.C. $\frac{1.0}{26.0}$ $\frac{5.5}{50}$ $\frac{5.2}{24}$ $\frac{6.4}{19}$ $\frac{4.9}{13}$ $\frac{4.4}{0}$ $\frac{4.7}{8}$ $\frac{5.1}{14}$ $\frac{3.9}{19}$ $\frac{4.1}{50}$ C. $\frac{0.8}{28.6}$

D.C. 6.3 5.3 6.1 4.6 4.1 4.3 5.3 3.7 3.0 3.0 C.
0.4 50 24 20 14 6 10 14 19 35 50 1.1
24.8

D.C
0.2
 $\frac{0.2}{26.4}$

$\frac{6.1}{50}$ $\frac{5.1}{23}$ $\frac{5.8}{20}$ $\frac{4.4}{11}$ $\frac{3.9}{0}$ $\frac{4.2}{10}$ $\frac{5.4}{15}$ $\frac{4.7}{19}$ $\frac{4.0}{36}$ $\frac{3.9}{50}$

D.C
1.3
 $\frac{1.3}{26.4}$

D.C. $\frac{0.3}{24.6}$ $\frac{5.8}{50}$ $\frac{5.1}{24}$ $\frac{5.7}{20}$ $\frac{3.9}{12}$ $\frac{3.7}{0}$ $\frac{4.0}{8}$ $\frac{5.4}{15}$ $\frac{4.2}{19}$ $\frac{3.6}{35}$ $\frac{3.8}{50}$ D.C. $\frac{1.3}{26.6}$

Private Driveway

$\frac{4.0}{50}$ $\frac{3.6}{12}$ $\frac{3.4}{0}$ $\frac{3.4}{10}$ $\frac{4.7}{15}$ $\frac{4.2}{15}$ $\frac{4.6}{34}$ $\frac{4.7}{50}$ D.C
 $\frac{1.0}{26.0}$

3-20-34

Sta.	+	T.	✓	Elev.
BM	5.98	116.88	✓	110.90

49+00

49+50

50+00

50+50

		↓	✓	
X	7.21	119.28	4.81	112.07

51+00

51+50

52+00

Top of No End of Culv 48150

C. 1.7
30.4

DC 1.1 / 26.2 4.6 / 50 5.3 / 17 4.7 / 12 4.5 / 10 4.8 / 8 5.5 / 15 2.2 / 21 2.4 / 27 4.6 / 50

DC 1.1 / 26.2 4.6 / 50 4.5 / 25 5.1 / 17 4.4 / 11 4.1 / 10 4.3 / 8 4.7 / 23 5.7 / 50 DC 1.0 / 26.0

C 1.4 / 29.8 4.1 / 50 3.1 / 22 4.9 / 17 4.4 / 10 4.0 / 6 4.4 / 8 4.9 / 13 8.7 / 35 9.6 / 50 F. 1.5 / 21.0

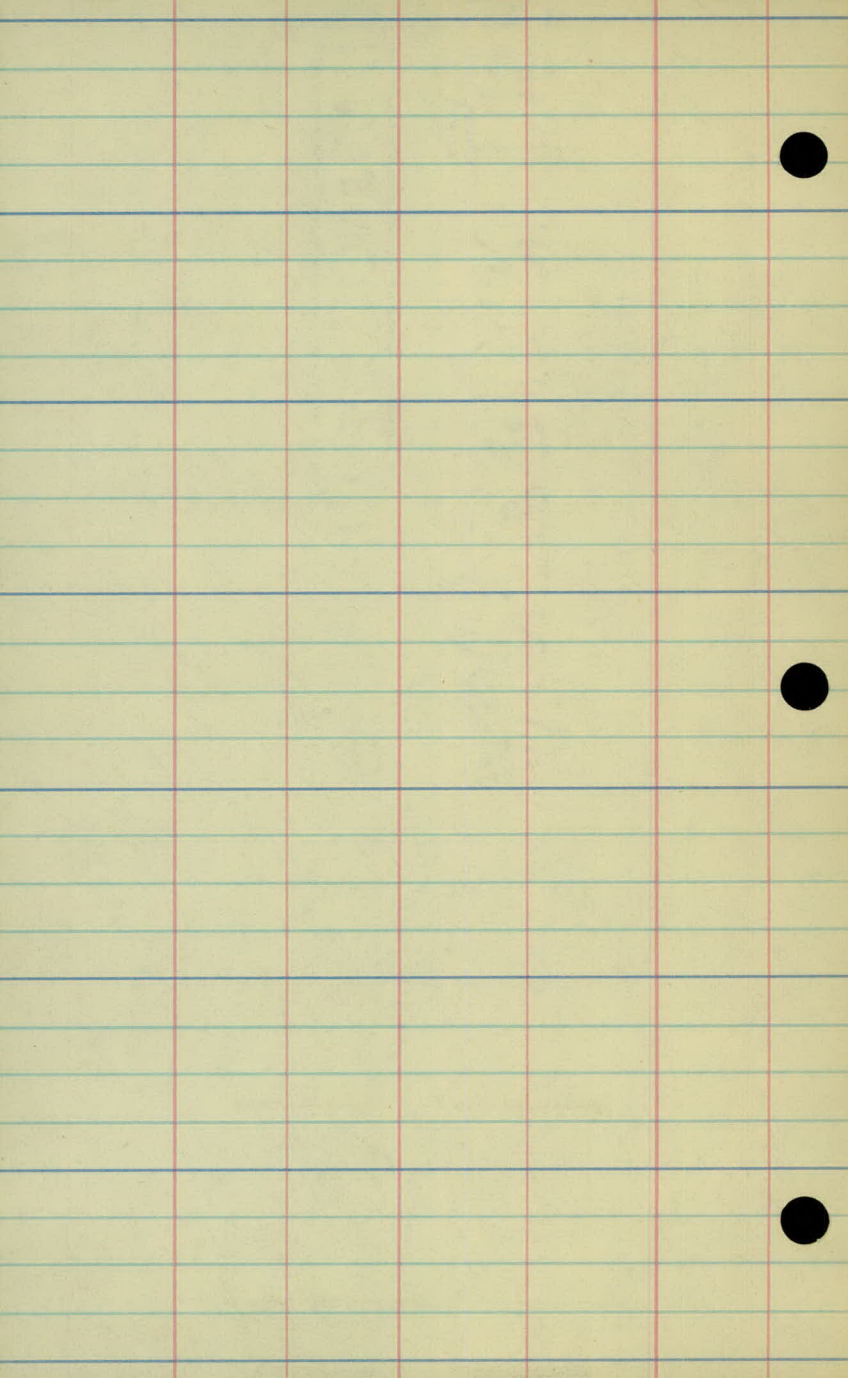
-2.5 / 23.0 5.0 / 50 4.9 / 32 6.7 / 27 6.9 / 20 5.0 / 15 4.4 / 10 4.1 / 10 4.6 / 8 5.0 / 12 6.8 / 17 6.6 / 50 F. 1.5 / 21.0

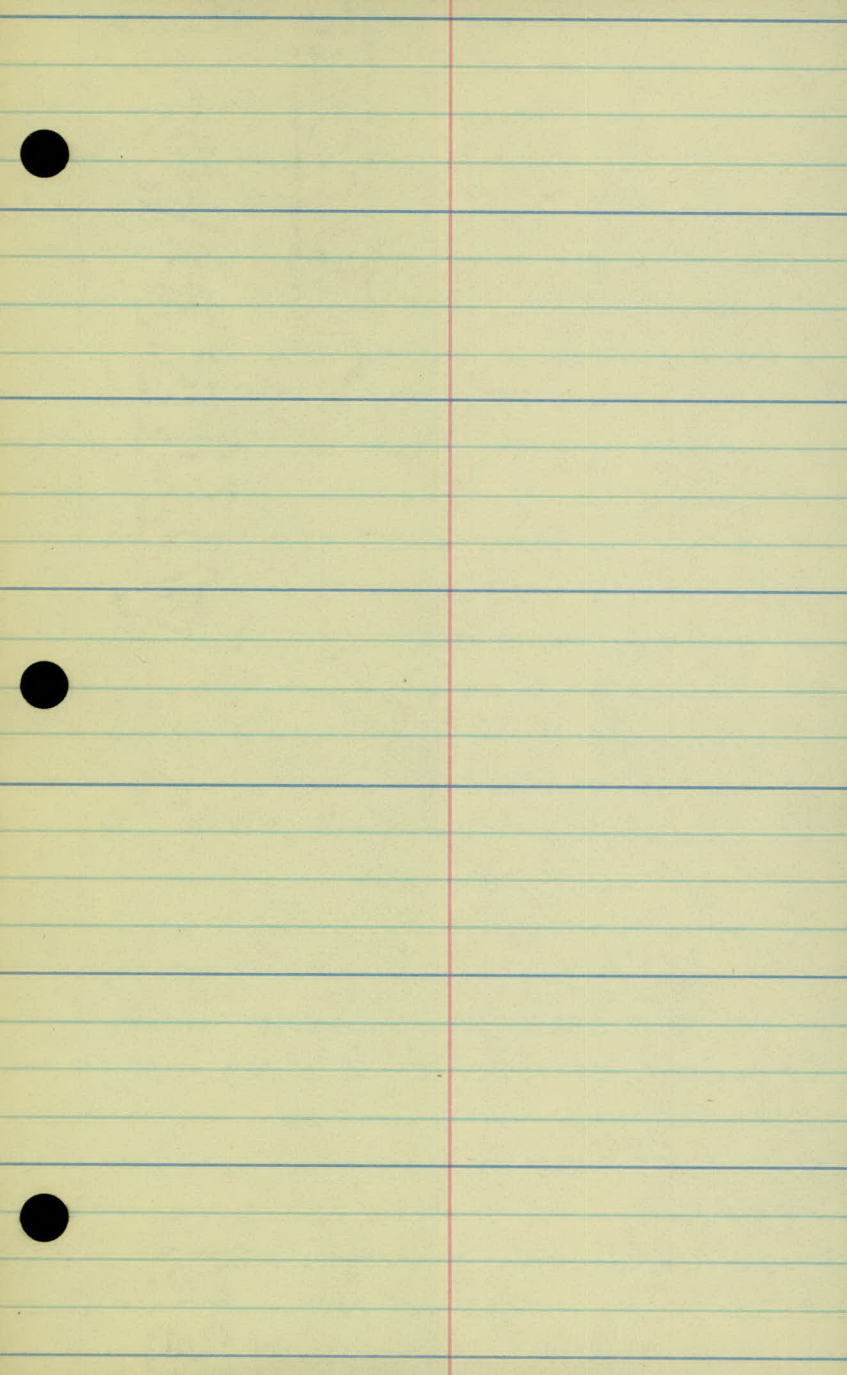
C. 6.4
39.8

F. 1.5 / 21.0 8.4 / 50 8.9 / 20 7.8 / 15 7.5 / 11 7.2 / 10 7.5 / 8 8.4 / 15 7.6 / 22 2.0 / 27 0.5 / 50

F. 4.0 / 30.0 12.9 / 50 12.3 / 30 10.9 / 19 8.9 / 14 8.3 / 10 7.9 / 10 8.2 / 8 8.8 / 16 7.6 / 24 2.0 / 33 1.1 / 50 C. 6.7 / 40.4

F. 4.5 / 31.5 14.3 / 50 13.3 / 21 9.8 / 15 9.2 / 11 8.8 / 10 9.4 / 9 9.4 / 50 11 complete





Sta. + π - Elev.

BM. 534 116.24 110.90

X 358 113.29 653 109.71

53+50

54+00

54+50

55+00

55+50

Top of No End Cyl. 5/8 48+50

$\frac{1.0}{29.0}$ $\frac{2.9}{50}$ $\frac{2.4}{33}$ $\frac{4.7}{19}$ $\frac{4.0}{13}$ $\frac{3.7}{0}$ $\frac{4.0}{8}$ $\frac{4.3}{16}$ $\frac{3.6}{50}$ Filling Sta
yard.

DC $\frac{0.8}{25.6}$ $\frac{4.6}{50}$ $\frac{3.9}{32}$ $\frac{5.0}{20}$ $\frac{4.2}{13}$ $\frac{3.7}{0}$ $\frac{4.1}{9}$ $\frac{4.7}{18}$ $\frac{3.9}{23}$ $\frac{3.9}{50}$ DC $\frac{1.5}{27}$

DC $\frac{0.3}{25.0}$ $\frac{5.1}{50}$ $\frac{5.3}{29}$ $\frac{5.3}{19}$ $\frac{4.5}{13}$ $\frac{4.1}{0}$ $\frac{4.4}{10}$ $\frac{5.0}{18}$ $\frac{3.5}{23}$ $\frac{2.5}{50}$ C $\frac{1.3}{29.6}$

DC $\frac{0.8}{25.6}$ $\frac{6.4}{50}$ $\frac{5.5}{25}$ $\frac{5.8}{19}$ $\frac{5.0}{13}$ $\frac{4.6}{0}$ $\frac{4.9}{9}$ $\frac{5.5}{17}$ $\frac{4.2}{25}$ $\frac{3.0}{50}$ C $\frac{0.9}{28.8}$

DC $\frac{0.2}{2.4}$ $\frac{7.5}{50}$ $\frac{7.0}{29}$ $\frac{6.4}{18}$ $\frac{5.6}{13}$ $\frac{5.0}{0}$ $\frac{5.2}{9}$ $\frac{6.0}{16}$ $\frac{4.8}{25}$ $\frac{3.8}{50}$ C $\frac{0.6}{28.2}$

Sta + π - Elev

113.29 ✓

56+00

' X 4.06 ✓ 111.65 5.70 ✓ 107.59

56+50 ←

57+00

57+50

58+00

58+50

$$DC \frac{0.2}{24.4} \quad 7.8 \frac{1}{50} \quad 7.2 \frac{1}{28} \quad 6.8 \frac{1}{18} \quad 5.8 \frac{1}{13} \quad 5.3 \frac{1}{9} \quad 5.5 \frac{1}{9} \quad 6.1 \frac{1}{18} \quad 5.2 \frac{1}{24} \quad 4.5 \frac{1}{50} \quad C \frac{0.7}{28.4}$$

$$\rightarrow DC \frac{0.2}{24.4} \quad 6.7 \frac{1}{50} \quad 6.0 \frac{1}{27} \quad 4.7 \frac{1}{12} \quad 4.2 \frac{1}{9} \quad 4.3 \frac{1}{9} \quad 4.9 \frac{1}{17} \quad 3.4 \frac{1}{20} \quad 1.7 \frac{1}{50} \quad C \frac{2.3}{31.6}$$

$$DC \frac{0.2}{24.4} \quad 7.1 \frac{1}{50} \quad 6.4 \frac{1}{31} \quad 6.0 \frac{1}{17} \quad 5.1 \frac{1}{12} \quad 4.6 \frac{1}{10} \quad 4.8 \frac{1}{10} \quad 5.1 \frac{1}{17} \quad 3.3 \frac{1}{20} \quad 1.1 \frac{1}{50} \quad C \frac{2.8}{32.6}$$

$$DC \frac{0.5}{25.0} \quad 7.5 \frac{1}{50} \quad 6.9 \frac{1}{31} \quad 6.7 \frac{1}{17} \quad 5.9 \frac{1}{12} \quad 5.4 \frac{1}{9} \quad 5.5 \frac{1}{12} \quad 6.1 \frac{1}{17} \quad 4.3 \frac{1}{22} \quad 2.9 \frac{1}{50} \quad C \frac{1.7}{30.4}$$

(0.5 added to ditch depth)

$$DC \frac{0.5}{25.0} \quad 8.8 \frac{1}{50} \quad 7.6 \frac{1}{17} \quad 6.5 \frac{1}{11} \quad 6.0 \frac{1}{10} \quad 6.0 \frac{1}{10} \quad 6.7 \frac{1}{18} \quad 4.8 \frac{1}{22} \quad 2.9 \frac{1}{50} \quad C \frac{1.7}{30.4}$$

(0.5 added to ditch depth)

$$DC \frac{0.2}{24.4} \quad 10.1 \frac{1}{50} \quad 8.6 \frac{1}{22} \quad 7.0 \frac{1}{10} \quad 6.6 \frac{1}{9} \quad 6.7 \frac{1}{9} \quad 7.2 \frac{1}{18} \quad 5.1 \frac{1}{22} \quad 3.4 \frac{1}{50} \quad C \frac{2.7}{32.4}$$

Sta + π - Elev
 111.65 ✓

59+00

T.P. 2.65 ✓ 3-21-34 112.36 109.71 ✓

X 2.94 ✓ 108.17 7.13 105.23 ✓

59+50

60+00

60+50

61+00

(0.5 added to
ditch depth)

DC $\frac{0.3}{24.6}$ $\frac{10.6}{50}$ $\frac{9.1}{21}$ $\frac{7.5}{10}$ $\frac{7.2}{0}$ $\frac{7.3}{10}$ $\frac{7.6}{18}$ $\frac{6.3}{23}$ $\frac{4.3}{50}$ $\frac{0.9}{30.8}$

DC $\frac{1.5}{27.0}$ $\frac{4.9}{50}$ $\frac{4.6}{25}$ $\frac{5.3}{16}$ $\frac{4.7}{10}$ $\frac{4.3}{0}$ $\frac{4.4}{9}$ $\frac{4.6}{17}$ $\frac{4.2}{20}$ $\frac{2.9}{50}$ $\frac{0.9}{28.8}$

DC $\frac{0.2}{27.4}$ $\frac{5.0}{50}$ $\frac{4.7}{20}$ $\frac{5.5}{16}$ $\frac{5.1}{10}$ $\frac{4.8}{0}$ $\frac{5.0}{10}$ $\frac{5.6}{19}$ $\frac{5.1}{21}$ $\frac{3.1}{50}$ $\frac{0.1}{29.0}$

DC $\frac{0.2}{27.4}$ $\frac{6.7}{50}$ $\frac{5.9}{21}$ $\frac{6.4}{14}$ $\frac{6.1}{11}$ $\frac{5.8}{0}$ $\frac{5.9}{9}$ $\frac{6.0}{12}$ $\frac{5.0}{28}$ $\frac{4.0}{50}$ $\frac{1.5}{30.0}$

DC $\frac{1.2}{26.4}$ $\frac{8.3}{50}$ $\frac{7.6}{23}$ $\frac{7.8}{16}$ $\frac{7.4}{11}$ $\frac{7.1}{0}$ $\frac{7.1}{8}$ $\frac{8.1}{20}$ $\frac{7.2}{21}$ $\frac{5.6}{34}$ $\frac{4.8}{50}$ $\frac{1.1}{29.0}$

Sta + π - Elev.

108.17

61+50

3-22-34

X

9.65 98.52 ✓

62+00

62+50

63+00

$$\begin{array}{cccccccccccc}
 -1.7 & 112 & 108 & 9.1 & 8.9 & 9.2 & 9.7 & 7.4 & 6.2 & 0 & 1.6 \\
 \hline
 23.1 & 50 & 24 & 11 & 0 & 9 & 20 & 32 & 50 & 30.2
 \end{array}$$

