

Book # 4-Dr. 6

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

Preliminary Survey

LITTLE CANADA ROAD.

From McMenemy St. To 1000' East.

Road Acc't. No. 7

Date Filed 10-15-34

File 6

LITTLE CANADA RD.

ALIGNMENT.

Ang Lt Ang Rt.

10+40.22

11° 11'

8+44.59

10° 16'

5+50.59

3° 43'

0+91.65

0+00

= P.I. 73+81.70.

294.0

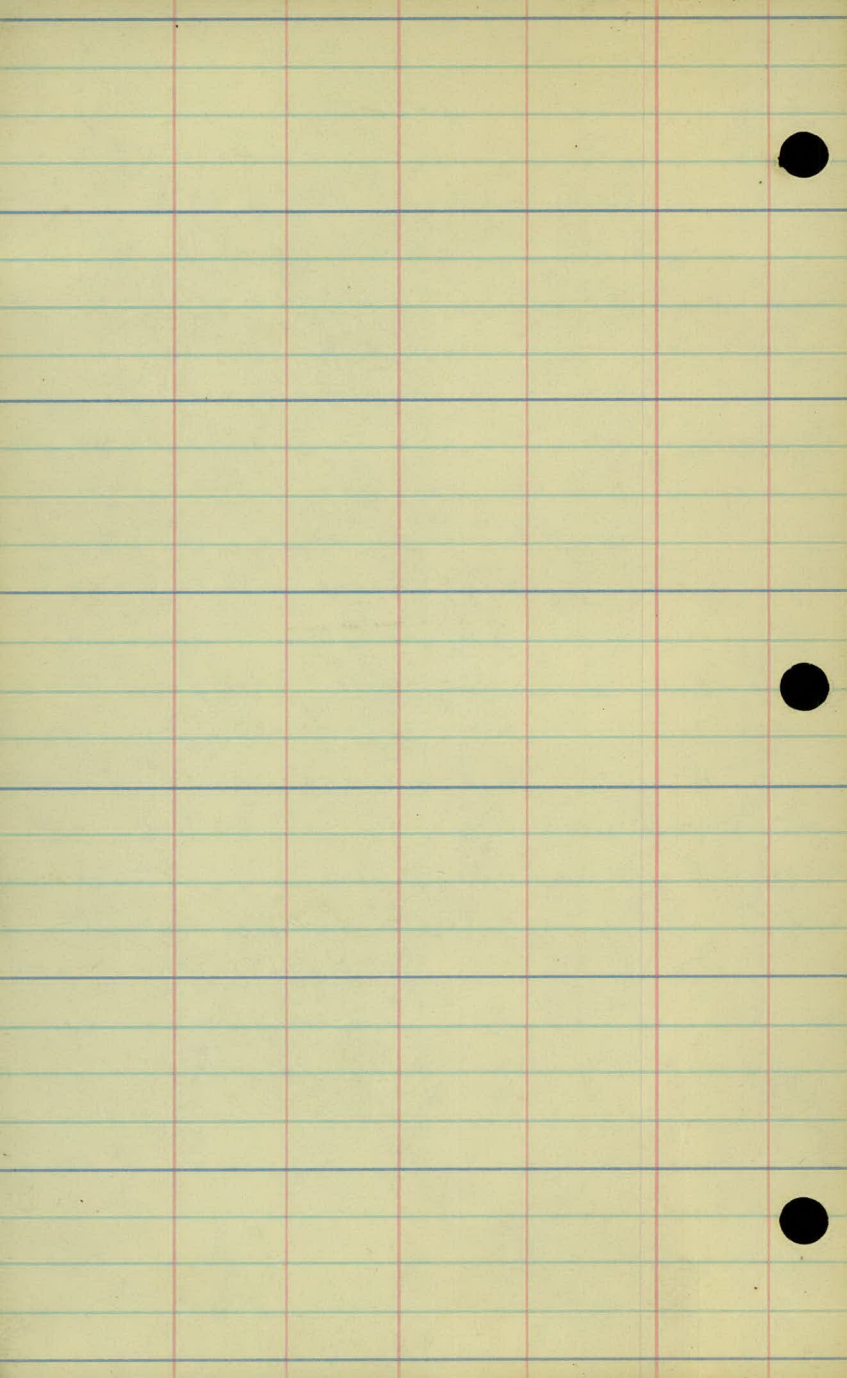
33'

23° 57'

85° 48'

32.7  
65.6

P.I. = 64+07.85



# TOPOGRAPHY

5

4

3

2

1

0 + 00

+98 T.P. 13'

ipuek

+38-20" B. Not 41

{ +98-15" Map 23  
 +83-15" Oak 26'  
 +83 T.P. 15'

+50-12" Map. 24

+01-8" Map 25

+85-18" Map 25

+51-20" Map. 26'

+49 T.P. 18'

+57-15" Map. 26'

+20-12" Map. 27'

+17 Cor School 88.8

+88-18" Map. 27'

+58 Cor. School 92.8

+57-15" Map. 27'

+19 T.P. 20'

School Grounds

+29 R.T. Sq 18'

+01 End Cul. 35'

+96 T.P. 25'

+87 W.V. Service Rd.

+45 int Side Dr.

+24-24" Stomp 32'

± Side Dr. 35'

N.W. Dr.

20'

± Present Rd. 20' W.V. Service Rd.

+83 P.P. 38'

+47  
+45 Headwall

+32 End Cul. 9'  
12" X 84" C.I.P.

± Present Rd. 40'

Cem'ty

+29 F. Cor 35'

+29 End 14'

+18-20" Map. 35'

± Present Rd. 11'

+94-24" Map. 35'

± Present Rd. 8'

Cult.

+39-15" Map. 32'

+10-24" Map. 31'

Present Rd. 5' R.H.

+82 End G.R. 21

+69 Beg Cult

+27-8" T.W. R.P. 32'

Present Rd. 6' G.R. 22'

N.W. Dr.

11

10

9

8

7

6

+140  $\pm$  Rd 3'  
+22 T.P. 26

+34 T.P. 11'  
+27 Cor. G.P. 26'  
+19.125 P. 22

+13 Cor. G.P. 24

old ch. r.

+85 Drive way

+72 T.P. 28'

+49 Cor. Ho. 33

+48-10" B.E. 26'

+34 T.P. 24'

+99 End Row Post 28'

+90 T.P. 22

+14-15" B.E. 21'

+01 T.P. 19

+95 Row 11 Posts 30'

+52 T.P. 17'

+32  $\pm$  P. Dr

12" x 20" C.P. 14'

Bay Cliff

Gordon

Scattered Rocks

+40 F. 34'  
+30 P.P. 27

F41'  $\pm$  Rd 13'

+40-10" B.E. 46

+11 G.P. 46

$\pm$  Rd 11 F. 59

+94 Light P. 40

+74 F. Cor. 66'

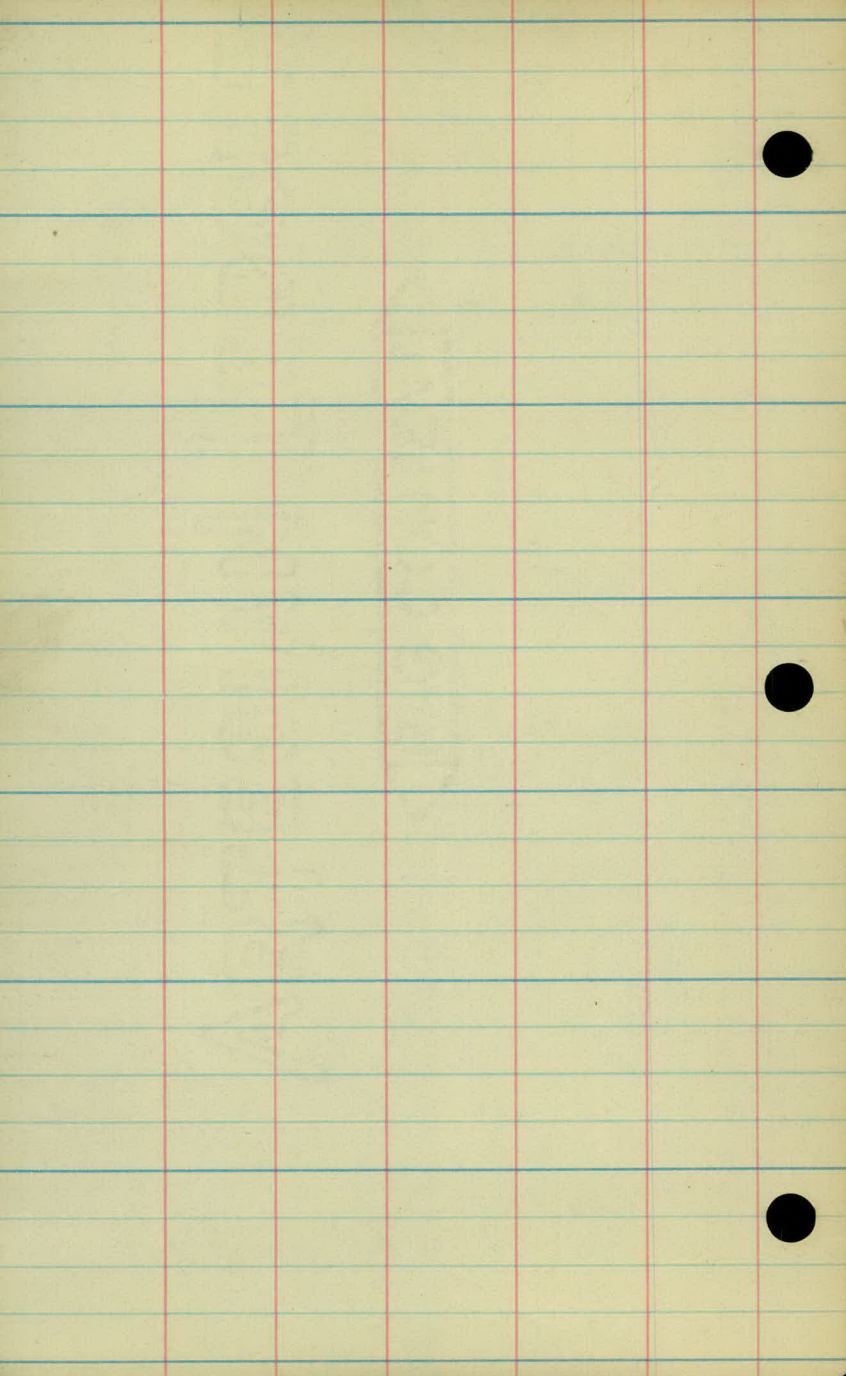
+44 Cor F 88

$\pm$  Rd 12' F. 36'

F. 36'  $\pm$  Rd 10'

+94  $\pm$  Cam. Dr.

$\pm$  Rd 13' F. 36'



## CROSS SECTIONS

| Station | +     | H.I.   | -    | Elev.          |
|---------|-------|--------|------|----------------|
| B.M.    | 5.66  | 208.66 |      | 200.00 Assumed |
| T.P.    | 10.75 | 218.16 | 1.25 | 207.41         |
| B.M.    |       |        | 7.34 | 210.82         |

0 +00

+50

+80

1

|      |      |        |      |        |
|------|------|--------|------|--------|
| B.M. | 0.66 | 211.48 | 7.34 | 210.82 |
|------|------|--------|------|--------|

+ 15

+50

2

+50

+68

3

|      |      |        |      |        |
|------|------|--------|------|--------|
| T.P. | 3.35 | 205.94 | 8.89 | 202.59 |
|------|------|--------|------|--------|

+50

4

LEFT      ≠      RIGHT.  
Top Mont 5+50=33' Rt.      × ± Rt

Spk in T.P. 25' Lt 0+96'      ×  
 $\begin{array}{r} 28 \\ 50 \end{array}$   $\begin{array}{r} 23 \\ 37 \end{array}$   $\begin{array}{r} 27 \\ 25 \end{array}$  34  $\begin{array}{r} 37 \\ 8 \end{array}$   $\begin{array}{r} 63 \\ 17 \end{array}$   $\begin{array}{r} 63 \\ 20 \end{array}$   $\begin{array}{r} 59 \\ 24 \end{array}$   $\begin{array}{r} 57 \\ 38 \end{array}$   $\begin{array}{r} 64 \\ 50 \end{array}$

inv. Culv. Red. = 7.78

$\begin{array}{r} 86 \\ 50 \end{array}$   $\begin{array}{r} 74 \\ 23 \end{array}$  6.8  $\begin{array}{r} 67 \\ 21 \end{array}$   $\begin{array}{r} 77 \\ 34 \end{array}$   $\begin{array}{r} 99 \\ 50 \end{array}$

$\begin{array}{r} 85 \\ 50 \end{array}$   $\begin{array}{r} 76 \\ 22 \end{array}$  7.6  $\begin{array}{r} 76 \\ 14 \end{array}$   $\begin{array}{r} 82 \\ 27 \end{array}$   $\begin{array}{r} 113 \\ 37 \end{array}$   $\begin{array}{r} 126 \\ 50 \end{array}$

inv. Culv. 12.5

$\begin{array}{r} 126 \\ 50 \end{array}$   $\begin{array}{r} 103 \\ 31 \end{array}$   $\begin{array}{r} 82 \\ 26 \end{array}$   $\begin{array}{r} 89 \\ 5 \end{array}$  8.6  $\begin{array}{r} 84 \\ 13 \end{array}$   $\begin{array}{r} 100 \\ 50 \end{array}$

25 above.

$\begin{array}{r} 98 \\ 50 \end{array}$   $\begin{array}{r} 50 \\ 30 \end{array}$   $\begin{array}{r} 24 \\ 14 \end{array}$  2.5  $\begin{array}{r} 24 \\ 10 \end{array}$   $\begin{array}{r} 30 \\ 30 \end{array}$   $\begin{array}{r} 35 \\ 50 \end{array}$

New Fill

$\begin{array}{r} 60 \\ 50 \end{array}$   $\begin{array}{r} 43 \\ 33 \end{array}$  3.7  $\begin{array}{r} 37 \\ 6 \end{array}$   $\begin{array}{r} 41 \\ 17 \end{array}$   $\begin{array}{r} 44 \\ 32 \end{array}$   $\begin{array}{r} 4.9 \\ 50 \end{array}$

$\begin{array}{r} 57 \\ 50 \end{array}$   $\begin{array}{r} 55 \\ 34 \end{array}$  5.0  $\begin{array}{r} 50 \\ 6 \end{array}$   $\begin{array}{r} 58 \\ 27 \end{array}$   $\begin{array}{r} 14.0 \\ 40 \end{array}$

$\begin{array}{r} 50 \\ 50 \end{array}$   $\begin{array}{r} 57 \\ 36 \end{array}$   $\begin{array}{r} 67 \\ 22 \end{array}$  6.1  $\begin{array}{r} 61 \\ 5 \end{array}$   $\begin{array}{r} 74 \\ 26 \end{array}$   $\begin{array}{r} 15.6 \\ 41 \end{array}$

$\begin{array}{r} 4.9 \\ 50 \end{array}$   $\begin{array}{r} 58 \\ 40 \end{array}$   $\begin{array}{r} 60 \\ 27 \end{array}$   $\begin{array}{r} 72 \\ 22 \end{array}$  6.6  $\begin{array}{r} 66 \\ 5 \end{array}$   $\begin{array}{r} 76 \\ 21 \end{array}$   $\begin{array}{r} 99 \\ 37 \end{array}$   $\begin{array}{r} 10.9 \\ 50 \end{array}$

$\begin{array}{r} 52 \\ 50 \end{array}$   $\begin{array}{r} 64 \\ 32 \end{array}$   $\begin{array}{r} 64 \\ 26 \end{array}$   $\begin{array}{r} 84 \\ 21 \end{array}$  7.4  $\begin{array}{r} 74 \\ 6 \end{array}$   $\begin{array}{r} 9.3 \\ 35 \end{array}$   $\begin{array}{r} 11.1 \\ 50 \end{array}$

10.2 over 41.

$\begin{array}{r} 10.2 \\ 50 \end{array}$   $\begin{array}{r} 0.5 \\ 1.7 \end{array}$   $\begin{array}{r} 1.0 \\ 32 \end{array}$   $\begin{array}{r} 15 \\ 25 \end{array}$   $\begin{array}{r} 40 \\ 20 \end{array}$   $\begin{array}{r} 34 \\ 11 \end{array}$  3.1  $\begin{array}{r} 3.0 \\ 6 \end{array}$   $\begin{array}{r} 3.5 \\ 18 \end{array}$   $\begin{array}{r} 41 \\ 23 \end{array}$   $\begin{array}{r} 35 \\ 26 \end{array}$   $\begin{array}{r} 5.3 \\ 37 \end{array}$   $\begin{array}{r} 6.3 \\ 50 \end{array}$

$\begin{array}{r} 23 \\ 50 \end{array}$   $\begin{array}{r} 28 \\ 23 \end{array}$   $\begin{array}{r} 47 \\ 16 \end{array}$  4.0  $\begin{array}{r} 40 \\ 8 \end{array}$   $\begin{array}{r} 4.7 \\ 24 \end{array}$   $\begin{array}{r} 4.4 \\ 31 \end{array}$   $\begin{array}{r} 6.5 \\ 50 \end{array}$

205.94

+50

5

+50 ΔPT. opposite Mont

B.M.

5.94

200.00

200.00

6

+50

7

T.P.

4.80

204.14

6.60

99.34

+50

8

+50

9

+50

B.M.

5.31

207.89

1.56

202.58

10

+40

End Proj

B.M.

5.31

202.58

LEFT

4

RIGHT

$$\begin{array}{ccccccc} \frac{3.2}{50} & \frac{3.3}{24} & \frac{5.3}{18} & 4.7 & \overset{x}{\frac{4.5}{8}} & \frac{5.4}{25} & \frac{5.0}{32} & \frac{6.0}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{4.2}{50} & \frac{4.7}{24} & \frac{6.4}{18} & \frac{6.3}{11} & \frac{5.6}{6} & 5.3 & \overset{x}{\frac{4.9}{11}} & \frac{5.7}{25} & \frac{5.2}{36} & \frac{5.5}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{5.1}{50} & \frac{5.9}{31} & \frac{6.3}{7} & 5.8 & \overset{x}{\frac{5.3}{12}} & \frac{6.0}{28} & \frac{5.5}{31} & \frac{5.0}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{7.1}{50} & \frac{7.1}{30} & \frac{7.3}{12} & \frac{6.2}{3} & 6.0 & \overset{x}{\frac{5.6}{11}} & \frac{6.3}{28} & \frac{5.6}{31} & \frac{4.7}{36} & \frac{4.2}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{7.2}{50} & \frac{7.6}{28} & \frac{7.7}{10} & \frac{6.4}{3} & 6.2 & \overset{y}{\frac{5.7}{10}} & \frac{6.2}{25} & \frac{5.3}{31} & \frac{4.4}{36} & \frac{4.1}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{8.1}{50} & \frac{7.6}{27} & \frac{8.3}{21} & \frac{8.4}{12} & \frac{6.7}{4} & 6.4 & \overset{x}{\frac{6.0}{10}} & \frac{6.4}{25} & \frac{5.2}{31} & \frac{4.6}{36} & \frac{4.4}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{8.0}{50} & \frac{7.0}{29} & \frac{7.5}{21} & \frac{6.7}{10} & \frac{5.5}{5} & 5.2 & \overset{y}{\frac{4.9}{10}} & \frac{5.3}{24} & \frac{4.0}{31} & \frac{3.2}{38} & \frac{3.2}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{10.3}{50} & \frac{9.2}{34} & \frac{8.0}{29} & \frac{8.7}{23} & \frac{5.9}{4} & 5.7 & \overset{y}{\frac{5.4}{11}} & \frac{5.7}{26} & \frac{4.6}{31} & \frac{3.7}{38} & \frac{3.5}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{10.3}{50} & \frac{8.7}{29} & \frac{9.1}{23} & \frac{8.1}{17} & \frac{6.8}{7} & 6.4 & \overset{y}{\frac{5.9}{6}} & \frac{5.7}{15} & \frac{6.2}{29} & \frac{5.2}{39} & \frac{4.2}{50} \end{array}$$

$$\begin{array}{ccccccc} \text{O10 Rd.} & \frac{10.7}{50} & \frac{8.0}{18} & 6.2 & \overset{x}{\frac{5.6}{12}} & \frac{5.8}{25} & \frac{7.1}{36} & \frac{4.8}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{9.2}{50} & \frac{8.0}{33} & \frac{6.9}{13} & \frac{5.8}{8} & 5.2 & \frac{4.9}{10} & \frac{5.5}{21} & \frac{6.2}{26} & \frac{4.1}{39} & \frac{1.7}{47} & \frac{1.7}{50} \end{array}$$

Spk in T.R 26' 2" + 10 + 22

$$\begin{array}{ccccccc} \frac{9.0}{50} & \frac{7.7}{29} & \frac{7.5}{16} & \frac{8.1}{11} & 7.7 & \frac{7.6}{5} & \frac{8.6}{20} & \frac{6.4}{31} & \frac{3.7}{38} & \frac{3.3}{50} \end{array}$$

$$\begin{array}{ccccccc} \frac{6.0}{50} & \frac{4.7}{29} & \frac{7.7}{18} & \frac{7.1}{6} & 7.0 & \frac{7.5}{12} & \frac{5.0}{19} & \frac{4.4}{23} & \frac{2.2}{29} & \frac{2.1}{50} \end{array}$$

