

Book-32- Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

C.W.A. CONST. Survey

KELLER PKWY & ARCADE ST.

From To

Road Acc't. No. 42 & 43

Date Filed 1934 File

Cross X
Keller Rd.

Sta	+	H.I.	-	Elev.
B.M.				870.00
B.M.	1.45	901.45		900.00

0+00

+50

1+00

+50

2+00

+50

3+00

T.P.	2.35	894.85	8.95	892.50
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+50

4+00

+50

5+00

+50

A. Windy Cold 2/12/34 1

Spike in P.P. ^{Void} NE. of Co. Rd. B & 5TH No. 1

Spike in P.P. 36° Rt Sta. 0+93

$\frac{63}{40} \frac{7.1}{34} \frac{6.9}{29} \frac{4.2}{18} \frac{4.4}{12} \frac{4.4}{4.2} \frac{4.5}{12} \frac{6.8}{19} \frac{7.1}{26} \frac{7.3}{39} \frac{7.3}{45}$

$\frac{11.6}{50} \frac{10.4}{43} \frac{4.0}{24} \frac{3.7}{19} \frac{3.5}{14} \frac{3.8}{14} \frac{3.8}{21} \frac{3.9}{30} \frac{0.3}{36} \frac{+0.2}{40}$

$\frac{12.0}{50} \frac{10.9}{41} \frac{4.4}{29} \frac{3.3}{19} \frac{3.1}{2} \frac{3.1}{31} \frac{3.2}{22} \frac{3.2}{32} \frac{1.8}{40}$

$\frac{12.4}{50} \frac{11.4}{41} \frac{4.3}{25} \frac{3.4}{12} \frac{2.7}{12} \frac{2.4}{12} \frac{2.4}{38} \frac{2.0}{46}$

$\frac{12.7}{50} \frac{11.1}{36} \frac{5.3}{22} \frac{4.1}{11} \frac{3.1}{36} \frac{1.0}{36} \frac{1.2}{50}$

$\frac{12.7}{40} \frac{12.1}{33} \frac{7.0}{19} \frac{6.0}{10} \frac{5.4}{11} \frac{5.6}{11} \frac{5.8}{15} \frac{7.5}{23} \frac{7.1}{28} \frac{2.3}{40}$

$\frac{7.3}{F19/21.8}$

$\frac{28.0}{F5.0} \frac{133}{138} \frac{134}{40} \frac{98}{29} \frac{9.0}{17} \frac{9.0}{11} \frac{8.3}{10} \frac{8.7}{15} \frac{9.1}{21} \frac{11.5}{40} \frac{11.5}{40} \frac{11.9}{F3.6} \frac{25.2}{25.2}$

$\frac{25.2}{F3.6} \frac{7.6}{40} \frac{7.4}{23} \frac{5.1}{16} \frac{4.6}{11} \frac{3.8}{10} \frac{4.1}{16} \frac{4.7}{24} \frac{7.1}{32} \frac{7.1}{40} \frac{7.0}{40} \frac{7.1}{F3.3} \frac{24.6}{24.6}$

$\frac{24.6}{F3.3} \frac{7.9}{40} \frac{7.8}{32} \frac{7.7}{22} \frac{7.9}{19} \frac{6.2}{7} \frac{5.2}{7} \frac{4.6}{46} \frac{4.9}{9} \frac{5.5}{15} \frac{7.4}{20} \frac{7.5}{40} \frac{7.5}{F2.9} \frac{23.8}{23.8}$

$\frac{25.9}{F3.5} \frac{8.1}{40} \frac{8.2}{25} \frac{8.1}{21} \frac{6.5}{12} \frac{5.1}{12} \frac{4.6}{46} \frac{4.8}{9} \frac{5.6}{17} \frac{7.6}{21} \frac{7.5}{40} \frac{7.5}{F2.9} \frac{23.8}{23.8}$

$\frac{24.6}{F2.2} \frac{8.2}{40} \frac{8.1}{36} \frac{8.0}{26} \frac{5.8}{16} \frac{5.2}{12} \frac{4.7}{47} \frac{4.8}{9} \frac{5.9}{21} \frac{7.5}{25} \frac{7.5}{40} \frac{6.2}{F1.5} \frac{21.0}{21.0}$

$\frac{24.9}{F3.4} \frac{7.8}{40} \frac{8.1}{15} \frac{7.7}{19} \frac{7.9}{14} \frac{5.6}{12} \frac{5.9}{12} \frac{4.4}{44} \frac{4.7}{10} \frac{5.7}{20} \frac{7.5}{24} \frac{7.5}{40} \frac{7.5}{F3.1} \frac{24.2}{24.2}$

Sta + H.L. - Elev

894.85

T.P. 6.13 898.16 2.82 892.03

6+00

+50

+89

7+00

T.P. 7.95 902.17 3.94 894.22

+38

+78

B.M. 9.06 903.86 7.37 894.80

8+00

+39

T.P. 4.95 899.75 9.06 894.80

+65

9+00

+50

+78

2/12/34

2

$$26 \frac{105}{F41} \frac{110}{40} \frac{106}{29} \frac{104}{20} \frac{75}{14} \frac{69}{9} 64 \frac{65}{11} \frac{69}{16} \frac{75}{21} \frac{78}{26} \frac{78}{40} \frac{78}{F34/248}$$

$$27 \frac{97}{F48} \frac{103}{40} \frac{100}{29} \frac{96}{20} \frac{61}{12} \frac{56}{10} 51 \frac{54}{12} \frac{58}{16} \frac{84}{23} \frac{88}{26} \frac{84}{38} \frac{83}{40} \frac{87}{F36/252}$$

$$\frac{90}{40} \frac{87}{27} \frac{81}{19} \frac{52}{12} \frac{48}{8} 44 \frac{47}{13} \frac{49}{17} \frac{39}{21} \frac{55}{28} \frac{48}{40}$$

$$36 \frac{84}{F42} \frac{88}{40} \frac{84}{26} \frac{78}{19} \frac{49}{12} \frac{45}{8} 42 \frac{45}{13} \frac{46}{16} \frac{30}{23} \frac{35}{29} \frac{39}{32} \frac{30}{40} \frac{36}{F40/200}$$

$$26 \frac{81}{DC11} \frac{75}{40} \frac{85}{28} \frac{66}{18} \frac{83}{14} \frac{80}{8} 77 \frac{81}{13} \frac{71}{22} \frac{35}{00} \frac{+31}{40} \frac{+21}{C28} \frac{476}{476} \frac{+22}{50}$$

$$34 \frac{42}{C33} \frac{58}{40} \frac{30}{28} \frac{80}{14} \frac{77}{8} 75 \frac{78}{12} \frac{79}{16} \frac{46}{25} \frac{25}{29} \frac{+15}{50} \frac{79}{C154/58.8}$$

Spike in PR 21' R4 54 9+28 Cold 2/13/34

$$34 \frac{57}{C33} \frac{66}{40} \frac{52}{32} \frac{56}{27} \frac{100}{16} \frac{93}{8} 90 \frac{94}{13} \frac{93}{17} \frac{66}{24} \frac{11}{35} \frac{+58}{49} \frac{+60}{C150/58.0}$$

105

$$24 \frac{101}{DC04} \frac{120}{40} \frac{115}{33} \frac{102}{26} \frac{98}{20} \frac{107}{17} \frac{97}{14} \frac{94}{9} 90 \frac{93}{12} \frac{97}{19} \frac{73}{25} \frac{16}{27} \frac{0.2}{C8.8} \frac{45.6}{45.6}$$

$$25 \frac{91}{F39} \frac{92}{40} \frac{90}{30} \frac{88}{20} \frac{58}{11} \frac{55}{8} 52 \frac{55}{12} \frac{60}{20} \frac{49}{24} \frac{32}{40} \frac{41}{C11} \frac{292}{292}$$

$$25 \frac{92}{F39} \frac{92}{40} \frac{72}{26} \frac{88}{19} \frac{61}{12} \frac{56}{7} 54 \frac{57}{13} \frac{75}{21} \frac{78}{26} \frac{61}{39} \frac{60}{40} \frac{75}{F21/22.2}$$

$$22 \frac{73}{F21} \frac{73}{40} \frac{77}{38} \frac{73}{17} \frac{61}{13} \frac{55}{8} 52 \frac{57}{12} \frac{61}{17} \frac{55}{25} \frac{50}{33} \frac{57}{36} \frac{61}{40} \frac{52}{C06/20}$$

64

$$29 \frac{39}{C10} \frac{25}{40} \frac{31}{35} \frac{33}{31} \frac{60}{17} \frac{52}{11} \frac{50}{8} 49 \frac{54}{12} \frac{58}{17} \frac{54}{25} \frac{51}{31} \frac{55}{40} \frac{52}{DC17/264}$$

Sta + H.I. - Elev.

899.75

10+00

T.P. 10.80 907.42 3.13 896.62

+49

+68

11+00

+21

+81

12+00

+50

13+00

T.P. 6.84 903.46 10.80 896.62

+50

14+00

+50

61

$$41.6 / \begin{array}{c} +2.8 \\ 07.4 \end{array} \quad \begin{array}{c} 0.0 \\ 32 \end{array} \quad \begin{array}{c} 2.1 \\ 26 \end{array} \quad \begin{array}{c} 4.8 \\ 15 \end{array} \quad \begin{array}{c} 4.7 \\ 8 \end{array} \quad 46 \quad \begin{array}{c} 5.0 \\ 12 \end{array} \quad \begin{array}{c} 5.4 \\ 20 \end{array} \quad \begin{array}{c} 5.1 \\ 27 \end{array} \quad \begin{array}{c} 5.4 \\ 36 \end{array} \quad \begin{array}{c} 5.9 \\ 40 \end{array} \quad \begin{array}{c} 5.2 \\ 00.9 \end{array} / 25.8$$

$$\begin{array}{c} +1.8 \\ 55.3 \end{array} \quad \begin{array}{c} 0.2 \\ 40 \end{array} \quad \begin{array}{c} 2.2 \\ 34 \end{array} \quad \begin{array}{c} 9.9 \\ 22 \end{array} \quad \begin{array}{c} 12.0 \\ 13 \end{array} \quad \begin{array}{c} 12.0 \\ 9 \end{array} \quad 11.7 \quad \begin{array}{c} 12.0 \\ 11 \end{array} \quad \begin{array}{c} 12.6 \\ 20 \end{array} \quad \begin{array}{c} 13.1 \\ 40 \end{array} \quad \text{Hemway}$$

$$\begin{array}{c} +3.2 \\ 90 \end{array} \quad \begin{array}{c} +0.8 \\ 47 \end{array} \quad \begin{array}{c} 3.2 \\ 40 \end{array} \quad \begin{array}{c} 8.2 \\ 29 \end{array} \quad \begin{array}{c} 11.8 \\ 13 \end{array} \quad \begin{array}{c} 11.7 \\ 9 \end{array} \quad 11.4 \quad \begin{array}{c} 11.8 \\ 11 \end{array} \quad \begin{array}{c} 12.3 \\ 19 \end{array} \quad \begin{array}{c} 12.1 \\ 23 \end{array} \quad \begin{array}{c} 13.0 \\ 40 \end{array}$$

$$\begin{array}{c} +2.5 \\ 60 \end{array}$$

$$51.0 / \begin{array}{c} +2.5 \\ 013.5 \end{array} \quad \begin{array}{c} +2.8 \\ 50 \end{array} \quad \begin{array}{c} +2.9 \\ 44 \end{array} \quad \begin{array}{c} 0.0 \\ 40 \end{array} \quad \begin{array}{c} 9.0 \\ 21 \end{array} \quad \begin{array}{c} 11.5 \\ 14 \end{array} \quad \begin{array}{c} 11.4 \\ 9 \end{array} \quad 11.0 \quad \begin{array}{c} 11.4 \\ 11 \end{array} \quad \begin{array}{c} 11.7 \\ 17 \end{array} \quad \begin{array}{c} 10.0 \\ 25 \end{array} \quad \begin{array}{c} 12.4 \\ 36 \end{array} \quad \begin{array}{c} 12.7 \\ 40 \end{array} \quad \begin{array}{c} 10.7 \\ 00.3 \end{array} / 27.6$$

$$\begin{array}{c} +2.8 \\ 60 \end{array} \quad \begin{array}{c} +3.1 \\ 013.9 \end{array} \quad \begin{array}{c} +3.2 \\ 50 \end{array} \quad \begin{array}{c} +3.3 \\ 47 \end{array} \quad \begin{array}{c} 0.0 \\ 40 \end{array} \quad \begin{array}{c} 11.2 \\ 14 \end{array} \quad \begin{array}{c} 11.1 \\ 10 \end{array} \quad 10.8 \quad \begin{array}{c} 11.1 \\ 12 \end{array} \quad \begin{array}{c} 11.5 \\ 18 \end{array} \quad \begin{array}{c} 10.7 \\ 24 \end{array} \quad \begin{array}{c} 11.7 \\ 33 \end{array} \quad \begin{array}{c} 13.5 \\ 40 \end{array} \quad \begin{array}{c} 11.3 \\ 00.10 \end{array} / 26.0$$

$$39.1 / \begin{array}{c} 4.7 \\ 05.8 \end{array} \quad \begin{array}{c} 3.9 \\ 50 \end{array} \quad \begin{array}{c} 4.7 \\ 40 \end{array} \quad \begin{array}{c} 6.7 \\ 25 \end{array} \quad \begin{array}{c} 11.2 \\ 16 \end{array} \quad \begin{array}{c} 10.7 \\ 10 \end{array} \quad 10.5 \quad \begin{array}{c} 10.9 \\ 11 \end{array} \quad \begin{array}{c} 12.2 \\ 19 \end{array} \quad \begin{array}{c} 14.8 \\ 26 \end{array} \quad \begin{array}{c} 15.4 \\ 28 \end{array} \quad \begin{array}{c} 16.0 \\ 40 \end{array} \quad \begin{array}{c} 15.2 \\ 04.7 \end{array} / 24$$

$$43.0 / \begin{array}{c} 3.1 \\ 02.5 \end{array} \quad \begin{array}{c} 3.0 \\ 50 \end{array} \quad \begin{array}{c} 3.4 \\ 40 \end{array} \quad \begin{array}{c} 4.7 \\ 29 \end{array} \quad \begin{array}{c} 11.2 \\ 17 \end{array} \quad \begin{array}{c} 10.8 \\ 9 \end{array} \quad 10.6 \quad \begin{array}{c} 11.1 \\ 11 \end{array} \quad \begin{array}{c} 11.6 \\ 15 \end{array} \quad \begin{array}{c} 15.6 \\ 28 \end{array} \quad \begin{array}{c} 16.0 \\ 40 \end{array} \quad \begin{array}{c} 15.6 \\ 05.0 \end{array} / 28.0$$

$$49.7 / \begin{array}{c} 0.2 \\ 010.6 \end{array} \quad \begin{array}{c} 0.2 \\ 50 \end{array} \quad \begin{array}{c} 0.7 \\ 40 \end{array} \quad \begin{array}{c} 2.2 \\ 31 \end{array} \quad \begin{array}{c} 11.2 \\ 16 \end{array} \quad \begin{array}{c} 10.9 \\ 10 \end{array} \quad 10.8 \quad \begin{array}{c} 11.3 \\ 11 \end{array} \quad \begin{array}{c} 15.8 \\ 28 \end{array} \quad \begin{array}{c} 16.1 \\ 40 \end{array} \quad \begin{array}{c} 15.8 \\ 05.0 \end{array} / 28.0$$

$$42 / \begin{array}{c} 3.6 \\ 07.1 \end{array} \quad \begin{array}{c} 4.0 \\ 50 \end{array} \quad \begin{array}{c} 3.8 \\ 40 \end{array} \quad \begin{array}{c} 4.4 \\ 29 \end{array} \quad \begin{array}{c} 10.6 \\ 21 \end{array} \quad \begin{array}{c} 11.1 \\ 11 \end{array} \quad 10.9 \quad \begin{array}{c} 11.4 \\ 10 \end{array} \quad \begin{array}{c} 12.0 \\ 19 \end{array} \quad \begin{array}{c} 11.9 \\ 21 \end{array} \quad \begin{array}{c} 15.1 \\ 30 \end{array} \quad \begin{array}{c} 5.1 \\ 40 \end{array}$$

8.7

$$\begin{array}{c} 1.8 \\ 50 \end{array} \quad 40.2 / \begin{array}{c} 1.1 \\ 06.1 \end{array} \quad \begin{array}{c} 1.1 \\ 40 \end{array} \quad \begin{array}{c} 1.2 \\ 29 \end{array} \quad \begin{array}{c} 2.8 \\ 17 \end{array} \quad \begin{array}{c} 7.4 \\ 11 \end{array} \quad 7.2 \quad \begin{array}{c} 7.4 \\ 9 \end{array} \quad \begin{array}{c} 8.1 \\ 18 \end{array} \quad \begin{array}{c} 7.8 \\ 20 \end{array} \quad \begin{array}{c} 11.0 \\ 37 \end{array} \quad \begin{array}{c} 11.4 \\ 40 \end{array} \quad \begin{array}{c} 8.7 \\ 00.00 \end{array} / 40$$

8.9

$$36.2 / \begin{array}{c} 3.3 \\ 04.1 \end{array} \quad \begin{array}{c} 3.3 \\ 40 \end{array} \quad \begin{array}{c} 3.5 \\ 23 \end{array} \quad \begin{array}{c} 8.1 \\ 17 \end{array} \quad \begin{array}{c} 7.7 \\ 11 \end{array} \quad 7.4 \quad \begin{array}{c} 7.7 \\ 10 \end{array} \quad \begin{array}{c} 8.6 \\ 21 \end{array} \quad \begin{array}{c} 9.7 \\ 40 \end{array} \quad \begin{array}{c} 8.8 \\ 00.01 \end{array} / 4.2$$

9.1

$$29.8 / \begin{array}{c} 6.2 \\ 01.4 \end{array} \quad \begin{array}{c} 6.9 \\ 40 \end{array} \quad \begin{array}{c} 5.9 \\ 20 \end{array} \quad \begin{array}{c} 8.5 \\ 15 \end{array} \quad \begin{array}{c} 7.9 \\ 10 \end{array} \quad 7.6 \quad \begin{array}{c} 7.9 \\ 12 \end{array} \quad \begin{array}{c} 8.8 \\ 17 \end{array} \quad \begin{array}{c} 8.6 \\ 19 \end{array} \quad \begin{array}{c} 10.1 \\ 40 \end{array} \quad \begin{array}{c} 8.9 \\ 00.02 \end{array} / 4.4$$

Sta + H.I. - Elev

903.46

15+00

+50

16+00

B.I. 2.84 897.99 8.31 895.15

+50

17+00

+50

18+00

+50

19+00

T.P. 13.77 902.11 465 893.34

+50

+87

20+00

$$25.4 / \begin{array}{c} 8.9 \\ \hline 0007 \end{array} \quad \begin{array}{c} 8.8 \\ \hline 40 \end{array} \quad \begin{array}{c} 8.7 \\ \hline 17 \end{array} \quad \begin{array}{c} 9.2 \\ \hline 14 \end{array} \quad \begin{array}{c} 8.5 \\ \hline 10 \end{array} \quad 8.1 \quad \begin{array}{c} 8.2 \\ \hline 11 \end{array} \quad \begin{array}{c} 9.5 \\ \hline 21 \end{array} \quad \begin{array}{c} 9.6 \\ \hline 33 \end{array} \quad \begin{array}{c} 10.5 \\ \hline 40 \end{array} \quad \begin{array}{c} 9.1 \\ \hline 0005 \end{array} / 25.0$$

$$27.8 / \begin{array}{c} 8.3 \\ \hline 00.4 \end{array} \quad \begin{array}{c} 8.4 \\ \hline 40 \end{array} \quad \begin{array}{c} 8.4 \\ \hline 19 \end{array} \quad \begin{array}{c} 9.4 \\ \hline 15 \end{array} \quad \begin{array}{c} 9.4 \\ \hline 11 \end{array} \quad 2.7 \quad \begin{array}{c} 9.7 \\ \hline 10 \end{array} \quad \begin{array}{c} 9.0 \\ \hline 14 \end{array} \quad \begin{array}{c} 9.6 \\ \hline 19 \end{array} \quad \begin{array}{c} 9.2 \\ \hline 22 \end{array} \quad \begin{array}{c} 9.8 \\ \hline 26 \end{array} \quad \begin{array}{c} 9.0 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.9 \\ \hline 0008 \end{array} / 28$$

$$26.4 / \begin{array}{c} 9.7 \\ \hline 0001.2 \end{array} \quad \begin{array}{c} 10.3 \\ \hline 40 \end{array} \quad \begin{array}{c} 9.4 \\ \hline 20 \end{array} \quad \begin{array}{c} 10.3 \\ \hline 16 \end{array} \quad \begin{array}{c} 10.5 \\ \hline 12 \end{array} \quad 9.4 \quad \begin{array}{c} 9.4 \\ \hline 8 \end{array} \quad \begin{array}{c} 9.9 \\ \hline 16 \end{array} \quad \begin{array}{c} 10.3 \\ \hline 20 \end{array} \quad \begin{array}{c} 9.1 \\ \hline 25 \end{array} \quad \begin{array}{c} 10.0 \\ \hline 40 \end{array} \quad \begin{array}{c} 9.2 \\ \hline 00.2 \end{array} / 27.4$$

Splice in PP 27' Lft. Sta. 15+98

$$24.4 / \begin{array}{c} 6.8 \\ \hline 0002 \end{array} \quad \begin{array}{c} 6.8 \\ \hline 40 \end{array} \quad \begin{array}{c} 6.1 \\ \hline 31 \end{array} \quad \begin{array}{c} 5.8 \\ \hline 16 \end{array} \quad \begin{array}{c} 5.3 \\ \hline 11 \end{array} \quad 4.7 \quad \begin{array}{c} 4.8 \\ \hline 8 \end{array} \quad \begin{array}{c} 5.0 \\ \hline 14 \end{array} \quad \begin{array}{c} 5.5 \\ \hline 20 \end{array} \quad \begin{array}{c} 5.9 \\ \hline 40 \end{array} \quad \begin{array}{c} 5.3 \\ \hline 0009 \end{array} / 25.8$$

$$24.3 / \begin{array}{c} 7.1 \\ \hline 15.1 \end{array} \quad \begin{array}{c} 8.1 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.0 \\ \hline 20 \end{array} \quad \begin{array}{c} 5.3 \\ \hline 15 \end{array} \quad \begin{array}{c} 5.1 \\ \hline 10 \end{array} \quad 5.0 \quad \begin{array}{c} 5.1 \\ \hline 8 \end{array} \quad \begin{array}{c} 5.6 \\ \hline 17 \end{array} \quad \begin{array}{c} 6.1 \\ \hline 30 \end{array} \quad \begin{array}{c} 6.2 \\ \hline 40 \end{array} \quad \begin{array}{c} 6.0 \\ \hline 0005 \end{array} / 25.0$$

$$26.4 / \begin{array}{c} 7.8 \\ \hline 15.1 \end{array} \quad \begin{array}{c} 8.4 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.6 \\ \hline 23 \end{array} \quad \begin{array}{c} 4.9 \\ \hline 14 \end{array} \quad \begin{array}{c} 5.0 \\ \hline 8 \end{array} \quad 5.0 \quad \begin{array}{c} 5.3 \\ \hline 9 \end{array} \quad \begin{array}{c} 6.0 \\ \hline 15 \end{array} \quad \begin{array}{c} 7.3 \\ \hline 22 \end{array} \quad \begin{array}{c} 7.2 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.3 \\ \hline 15.3 \end{array} / 24.6$$

$$24.0 / \begin{array}{c} 6.7 \\ \hline 15.0 \end{array} \quad \begin{array}{c} 8.0 \\ \hline 40 \end{array} \quad \begin{array}{c} 6.9 \\ \hline 33 \end{array} \quad \begin{array}{c} 6.3 \\ \hline 20 \end{array} \quad \begin{array}{c} 4.8 \\ \hline 13 \end{array} \quad \begin{array}{c} 4.7 \\ \hline 9 \end{array} \quad 4.8 \quad \begin{array}{c} 5.4 \\ \hline 10 \end{array} \quad \begin{array}{c} 5.9 \\ \hline 14 \end{array} \quad \begin{array}{c} 7.1 \\ \hline 20 \end{array} \quad \begin{array}{c} 7.2 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.4 \\ \hline 15.6 \end{array} / 25.8$$

$$27.0 / \begin{array}{c} 4.5 \\ \hline 00.0 \end{array} \quad \begin{array}{c} 4.9 \\ \hline 40 \end{array} \quad \begin{array}{c} 4.2 \\ \hline 24 \end{array} \quad \begin{array}{c} 5.2 \\ \hline 19 \end{array} \quad \begin{array}{c} 4.8 \\ \hline 15 \end{array} \quad \begin{array}{c} 4.4 \\ \hline 9 \end{array} \quad 4.5 \quad \begin{array}{c} 5.2 \\ \hline 11 \end{array} \quad \begin{array}{c} 5.7 \\ \hline 15 \end{array} \quad \begin{array}{c} 6.9 \\ \hline 20 \end{array} \quad \begin{array}{c} 7.5 \\ \hline 30 \end{array} \quad \begin{array}{c} 7.7 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.5 \\ \hline 15.0 \end{array} / 27.0$$

$$30.1 / \begin{array}{c} 3.1 \\ \hline 01.6 \end{array} \quad \begin{array}{c} 2.3 \\ \hline 40 \end{array} \quad \begin{array}{c} 3.1 \\ \hline 27 \end{array} \quad \begin{array}{c} 5.0 \\ \hline 19 \end{array} \quad \begin{array}{c} 5.1 \\ \hline 16 \end{array} \quad \begin{array}{c} 4.6 \\ \hline 10 \end{array} \quad 4.7 \quad \begin{array}{c} 5.5 \\ \hline 12 \end{array} \quad \begin{array}{c} 5.8 \\ \hline 16 \end{array} \quad \begin{array}{c} 7.1 \\ \hline 20 \end{array} \quad \begin{array}{c} 7.5 \\ \hline 27 \end{array} \quad \begin{array}{c} 7.5 \\ \hline 40 \end{array} \quad \begin{array}{c} 7.5 \\ \hline 15.8 \end{array} / 26.4$$

$$4.7 / \begin{array}{c} 4.7 \\ \hline 80 \end{array} \quad \begin{array}{c} 6.0 \\ \hline 7.6 \end{array} \quad \begin{array}{c} 6.0 \\ \hline 39 \end{array} \quad \begin{array}{c} 14.3 \\ \hline 16 \end{array} \quad \begin{array}{c} 13.8 \\ \hline 10 \end{array} \quad 13.6 \quad \begin{array}{c} 13.9 \\ \hline 10 \end{array} \quad \begin{array}{c} 14.2 \\ \hline 16 \end{array} \quad \begin{array}{c} 16.0 \\ \hline 24 \end{array} \quad \begin{array}{c} 16.3 \\ \hline 40 \end{array} \quad \begin{array}{c} 16.0 \\ \hline 15.4 \end{array} / 25.2$$

$$52.6 / \begin{array}{c} 0.9 \\ \hline 12.8 \end{array} \quad \begin{array}{c} 0.9 \\ \hline 50 \end{array} \quad \begin{array}{c} 1.8 \\ \hline 41 \end{array} \quad \begin{array}{c} 14.2 \\ \hline 15 \end{array} \quad \begin{array}{c} 14.1 \\ \hline 10 \end{array} \quad 13.8 \quad \begin{array}{c} 14.1 \\ \hline 10 \end{array} \quad \begin{array}{c} 14.6 \\ \hline 16 \end{array} \quad \begin{array}{c} 16.0 \\ \hline 24 \end{array} \quad \begin{array}{c} 16.5 \\ \hline 40 \end{array}$$

$$52.6 / \begin{array}{c} 1.2 \\ \hline 0128 \end{array} \quad \begin{array}{c} 1.7 \\ \hline 47 \end{array} \quad \begin{array}{c} 2.8 \\ \hline 41 \end{array} \quad \begin{array}{c} 14.1 \\ \hline 18 \end{array} \quad \begin{array}{c} 14.4 \\ \hline 16 \end{array} \quad \begin{array}{c} 14.3 \\ \hline 10 \end{array} \quad 14.0 \quad \begin{array}{c} 14.6 \\ \hline 10 \end{array} \quad \begin{array}{c} 15.2 \\ \hline 17 \end{array} \quad \begin{array}{c} 16.1 \\ \hline 24 \end{array} \quad \begin{array}{c} 16.6 \\ \hline 40 \end{array} \quad \begin{array}{c} 16.0 \\ \hline 15.0 \end{array} / 24.0$$

Sta + H.I. - Elev

907.11

+50

TP 752 885.82 13.77 893.34

21+00

+50

22+00

+50

B.M. 524 883.53 7.53 878.29

23+00.

+50

24+00

+50

25+00

+19

TP 12.14 892.13 3.54 879.99

+50

$$44.8 / \frac{56}{68.9} \frac{5.3}{49} \frac{6.2}{39} \frac{14.6}{16} \frac{14.5}{10} \frac{16.0}{14.5} \frac{14.9}{11} \frac{15.4}{16} \frac{16.2}{20} \frac{16.2}{27} \frac{16.8}{40} \frac{16.3}{F11.72}$$

$$38.4 / \frac{2.5}{65.7} \frac{14}{50} \frac{2.5}{38} \frac{8.4}{17} \frac{8.2}{13} \frac{8.3}{8} \frac{8.3}{8.3} \frac{8.9}{11} \frac{9.4}{16} \frac{10.3}{22} \frac{10.6}{40} \frac{10.3}{F2.9} \frac{14.0}{24.0}$$

$$34.8 / \frac{4.3}{63.9} \frac{3.5}{50} \frac{4.3}{35} \frac{5.6}{27} \frac{8.6}{15} \frac{8.4}{12} \frac{8.3}{8} \frac{8.2}{8.2} \frac{8.9}{11} \frac{9.5}{17} \frac{10.5}{23} \frac{10.6}{40} \frac{10.4}{F2.2} \frac{24.6}{24.6}$$

$$31.6 / \frac{5.8}{62.3} \frac{6.5}{50} \frac{5.8}{30} \frac{8.1}{16} \frac{8.7}{13} \frac{8.4}{8} \frac{8.1}{8.1} \frac{8.3}{11} \frac{8.7}{17} \frac{10.0}{25} \frac{10.5}{40} \frac{10.0}{F1.9} \frac{23.7}{23.7}$$

$$25.8 / \frac{9.2}{60.9} \frac{9.2}{40} \frac{9.2}{20} \frac{9.2}{16} \frac{9.0}{12} \frac{8.9}{8} \frac{8.6}{8.6} \frac{8.9}{10} \frac{9.2}{15} \frac{10.6}{20} \frac{11.2}{40} \frac{11.3}{F2.7} \frac{26.1}{26.1}$$

Spike in P.P. 16' Lt 5ft, 22+45

$$25.0 / \frac{7.8}{60.9} \frac{7.7}{40} \frac{7.5}{21} \frac{7.2}{13} \frac{7.0}{9} \frac{6.8}{6.8} \frac{7.0}{10} \frac{7.6}{14} \frac{11.1}{23} \frac{10.3}{40} \frac{11.1}{F4.3} \frac{30.9}{30.9}$$

$$25.0 / \frac{8.0}{60.5} \frac{8.2}{40} \frac{7.6}{14} \frac{7.5}{10} \frac{7.1}{7.1} \frac{7.4}{9} \frac{7.7}{14} \frac{11.2}{21} \frac{10.8}{26} \frac{10.7}{40} \frac{10.7}{F3.6} \frac{28.8}{28.8}$$

$$25.0 / \frac{8.6}{60.5} \frac{8.4}{40} \frac{8.4}{22} \frac{7.9}{14} \frac{8.0}{10} \frac{7.6}{7.6} \frac{7.7}{9} \frac{8.2}{15} \frac{10.4}{22} \frac{10.9}{40} \frac{11.7}{F3.1} \frac{27.3}{27.3}$$

$$24.0 / \frac{7.7}{60.0} \frac{8.1}{40} \frac{7.7}{23} \frac{6.9}{13} \frac{6.6}{10} \frac{6.2}{6.2} \frac{6.4}{10} \frac{7.0}{14} \frac{10.5}{21} \frac{10.2}{30} \frac{10.2}{40} \frac{10.2}{F4.2} \frac{30.0}{30.0}$$

$$24.0 / \frac{6.7}{60.0} \frac{7.5}{40} \frac{7.1}{29} \frac{6.6}{23} \frac{5.8}{14} \frac{5.4}{9} \frac{5.2}{5.2} \frac{5.4}{8} \frac{5.5}{12} \frac{5.4}{17} \frac{4.8}{29} \frac{3.9}{40}$$

$$6.9 / \frac{6.9}{40} \frac{6.0}{22} \frac{5.3}{14} \frac{5.1}{9} \frac{4.9}{8} \frac{5.2}{8} \frac{5.5}{16} \frac{5.3}{21} \frac{4.7}{26} \frac{2.3}{32} \frac{2.1}{40} \frac{2.3}{C26.7} \frac{2.3}{2.3}$$

$$21.4 / \frac{13.2}{60.6} \frac{14.5}{40} \frac{13.5}{21} \frac{13.1}{15} \frac{13.0}{10} \frac{12.8}{12.8} \frac{13.3}{10} \frac{13.6}{15} \frac{11.7}{22} \frac{11.0}{27} \frac{7.4}{34} \frac{6.3}{40} \frac{6.3}{C6.5} \frac{6.3}{6.3}$$

Sta + H.I. - Elev

892.13

26+00

T.P. 12.21 892.10 12.14 879.99

+50

27+00

+50

28+00

T.P. 513 885.61 11.62 880.48

+50

29+00

+50

30+00

+46

31+00

817

2.28 883.33

$$25.4 / \frac{12.8}{DC0.7} \frac{13.6}{40} \frac{12.6}{20} \frac{12.4}{14} \frac{12.2}{10} \frac{13.5}{12.0} \frac{12.5}{10} \frac{12.8}{14} \frac{12.2}{16} \frac{4.2}{30} \frac{3.3}{40} \frac{2.0}{C10.0} \frac{4.2}{4.2}$$

$$25.4 / \frac{12.5}{DC0.7} \frac{13.5}{40} \frac{12.5}{25} \frac{12.1}{15} \frac{12.0}{14} \frac{11.7}{11.7} \frac{12.1}{9} \frac{12.1}{13} \frac{9.0}{21} \frac{2.8}{31} \frac{0.5}{50} \frac{0.5}{11.2} \frac{0.5}{4.2}$$

$$27.2 / \frac{12.7}{DC0.1} \frac{13.8}{40} \frac{12.3}{21} \frac{11.5}{11} \frac{11.3}{11.3} \frac{11.8}{9} \frac{11.8}{18} \frac{10.0}{18} \frac{2.0}{32} \frac{0.8}{50} \frac{0.8}{C10.5} \frac{0.8}{4.2}$$

$$27.0 / \frac{12.9}{DC0.9} \frac{13.8}{40} \frac{13.5}{19} \frac{12.0}{13} \frac{11.7}{9} \frac{11.4}{11.4} \frac{12.1}{13} \frac{12.0}{18} \frac{4.6}{32} \frac{3.6}{56} \frac{4.1}{C7.3} \frac{4.1}{4.2}$$

$$25.0 / \frac{12.6}{DC0.5} \frac{12.9}{40} \frac{12.4}{21} \frac{11.9}{11} \frac{11.6}{11.6} \frac{12.3}{14} \frac{12.5}{18} \frac{8.2}{26} \frac{8.1}{45} \frac{7.9}{C3.7} \frac{7.9}{3.44}$$

$$24.8 / \frac{6.6}{DC0.4} \frac{13.7}{49} \frac{7.0}{34} \frac{6.8}{19} \frac{5.7}{12} \frac{5.5}{5.5} \frac{6.2}{11} \frac{6.9}{16} \frac{7.7}{19} \frac{7.2}{34} \frac{7.0}{40} \frac{7.2}{F2.2} \frac{7.2}{2.66}$$

$$24.3 / \frac{8.0}{F2.1} \frac{14.8}{40} \frac{12.6}{32} \frac{6.8}{21} \frac{6.2}{18} \frac{6.1}{11} \frac{5.9}{5.9} \frac{6.1}{9} \frac{6.5}{12} \frac{9.6}{19} \frac{11.8}{24} \frac{11.2}{32} \frac{11.2}{40} \frac{11.4}{F5.5} \frac{11.4}{3.44}$$

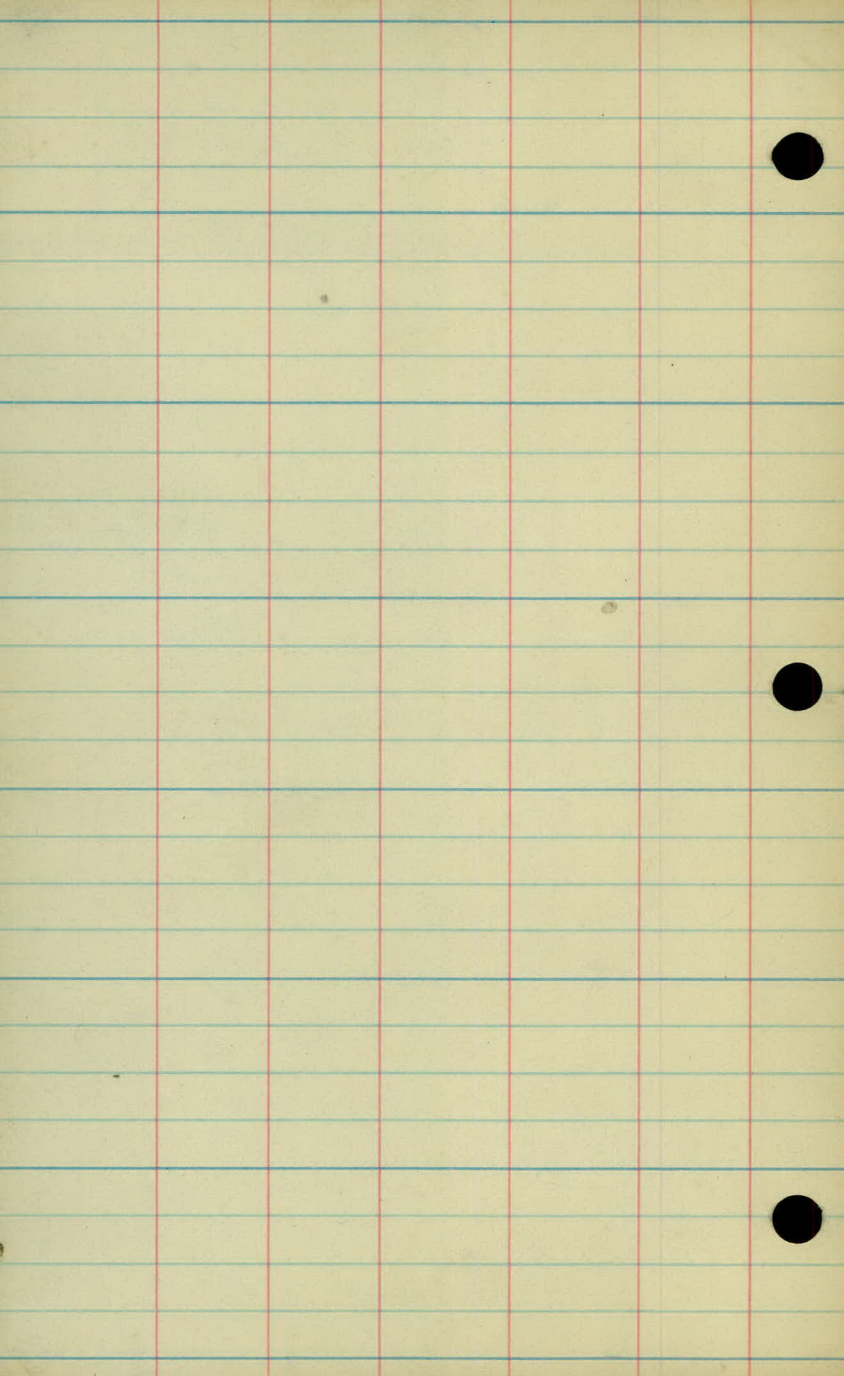
$$24.4 / \frac{2.5}{DC0.7} \frac{8.9}{45} \frac{8.0}{39} \frac{7.1}{17} \frac{6.6}{10} \frac{6.2}{6.2} \frac{6.2}{10} \frac{6.6}{16} \frac{12.6}{25} \frac{11.8}{28} \frac{12.0}{32} \frac{12.0}{40} \frac{12.0}{40.5} \frac{12.0}{4.2}$$

$$24.2 / \frac{7.2}{DC0.1} \frac{7.5}{40} \frac{6.8}{18} \frac{6.2}{10} \frac{5.8}{5.8} \frac{5.9}{10} \frac{6.0}{13} \frac{10.0}{25} \frac{10.2}{35} \frac{10.7}{40} \frac{10.4}{14.6} \frac{10.4}{3.44}$$

$$\frac{5.8}{40} \frac{4.9}{32} \frac{4.1}{21} \frac{4.6}{9} \frac{4.8}{4.8} \frac{5.2}{10} \frac{5.7}{17} \frac{4.1}{22} \frac{4.8}{40} \frac{4.5}{C13} \frac{4.5}{2.76}$$

$$\frac{3.0}{45} \frac{3.7}{24} \frac{4.1}{10} \frac{4.3}{4.3} \frac{4.7}{10} \frac{5.8}{18} \frac{0.0}{28} \frac{+5.2}{37} \frac{+6.1}{50} \frac{6.1}{C10.4} \frac{6.1}{4.2}$$

Spike in PP60 Lt Sta 30+70



	+	H.I.	-	Elev.
B.M.	3.41	886.74		883.33
31+48				

32+00

+50

T.P.	6.25	882.96	1000	876.71
33+00				

+50

34+00

+50

35+00

T.P.	7.71	885.99	4.68	878.28
+50				

36+00

+50

37+00

TP	7.67	885.99	7.67	878.32
B.M.	5.77	884.66	7.10	878.89

$$\begin{array}{cccccccccccc} 10.1 & 7.1 & 6.8 & 6.2 & & 6.5 & 6.2 & 7.4 & 3.5 & 2.1 & 3.2 \\ 40 & 34 & 28 & 10 & 6.2 & 8 & 12 & 20 & 30 & 40 & C3.0/3.0 \end{array}$$

$$\begin{array}{cccccccccccccccc} 24.0 & 10.9 & 11.2 & 10.6 & 8.9 & 8.4 & 7.9 & 9.2 & 10.6 & 10.8 & 9.9 & 8.1 & 10.4 \\ F3.0 & 40 & 21 & 16 & 11 & 11 & 14 & 18 & 23 & 28 & 40 & F2.5/23.0 \end{array}$$

$$\begin{array}{cccccccccccccccc} 22.4 & 11.4 & 12.1 & 11.3 & 10.0 & 9.8 & 9.2 & 9.5 & 9.9 & 12.1 & 12.0 & 11.9 & 11.7 & 12.2 \\ F2.2 & 40 & 17 & 13 & 10 & 10 & 14 & 20 & 25 & 27 & 40 & F3.0/24.0 \end{array}$$

7.8

$$\begin{array}{cccccccccccccccc} 22.0 & 8.3 & 8.8 & 7.6 & 6.9 & 6.6 & 6.3 & 6.4 & 6.6 & 8.9 & 8.9 & 8.9 & 8.9 \\ F2.0 & 40 & 16 & 13 & 9 & 10 & 15 & 22 & 29 & 40 & F2.6/23.2 \end{array}$$

$$\begin{array}{cccccccccccccccc} 22.4 & 8.6 & 9.4 & 8.2 & 7.2 & 6.7 & 6.4 & 6.6 & 7.0 & 8.9 & 8.9 & 8.7 & 8.4 \\ F2.2 & 40 & 18 & 11 & 8 & 11 & 19 & 24 & 31 & 40 & F2.2/22.4 \end{array}$$

7.3

$$\begin{array}{cccccccccccccccc} 24.2 & 7.2 & 7.6 & 6.7 & 6.4 & 5.8 & 5.9 & 6.3 & 7.6 & 8.4 & 9.3 & 8.6 \\ D.C.O.1 & 40 & 12 & 9 & 5.8 & 11 & 16 & 21 & 22 & 40 & F2.8/23.6 \end{array}$$

6.4

$$\begin{array}{cccccccccccccccc} 21.8 & 6.8 & 7.2 & 6.0 & 5.6 & 4.9 & 5.2 & 5.4 & 6.0 & 7.9 & 7.3 & 6.5 & 8.0 \\ F1.9 & 40 & 12 & 9 & 4.9 & 11 & 15 & 18 & 24 & 29 & 40 & F3.1/24.2 \end{array}$$

$$\begin{array}{cccccccccccccccc} 21.4 & 6.2 & 7.0 & 6.3 & 5.4 & 5.0 & 4.5 & 4.9 & 5.3 & 6.4 & 6.4 & 4.9 & 0.7 & 4.0 \\ F1.7 & 40 & 18 & 11 & 9 & 4.5 & 10 & 15 & 20 & 21 & 24 & 40 & C0.5/27.1 \end{array}$$

$$\begin{array}{cccccccccccc} 21.4 & 7.2 & 9.6 & 9.0 & 8.3 & 7.9 & 7.5 & 7.9 & 8.3 & 8.9 & 8.8 & 5.1 \\ F1.7 & 40 & 15 & 13 & 10 & 11 & 16 & 18 & 21 & 25 \end{array}$$

$$\begin{array}{cccccccccccc} 21.7 & 8.9 & 9.3 & 8.7 & 7.8 & 7.7 & 7.3 & 7.8 & 8.3 & 8.8 & 8.9 & 8.0 & 7.5 & 4.4 \\ F1.6 & 40 & 17 & 13 & 11 & 7.3 & 11 & 16 & 17 & 19 & 21 & 24 & 28 \end{array}$$

$$\begin{array}{cccccccccccc} 21.8 & 9.0 & 9.4 & 8.6 & 7.8 & 7.5 & 7.1 & 7.6 & 7.9 & 8.4 & 7.6 & 7.2 & 3.5 \\ F1.9 & 40 & 15 & 13 & 10 & 7.1 & 14 & 16 & 19 & 22 & 25 & 30 \end{array}$$

$$\begin{array}{cccccccccccc} 22.0 & 8.9 & 9.4 & 8.3 & 7.5 & 7.3 & 6.9 & 7.4 & 8.1 & 3.4 & 0.8 \\ F2.0 & 40 & 15 & 13 & 10 & 6.9 & 12 & 19 & 27 & 37 \end{array}$$

Sta + H.I. - Elev.

884.66

37+50

38+00

38+47.50

39+00

+50

B.M. 6.43 885.32 5.77 878.89

40+00

+50

41+00

+50

42+00

+50

43+00

T.P. 3.29 883.32 5.29 880.03

+50

$$\frac{8.7}{40} \frac{7.363}{16} \frac{6.0}{12} \frac{5.2}{9} \frac{4.1}{11} \frac{6.3}{17} \frac{6.5}{21} \frac{5.3}{24} \frac{4.0}{26} \frac{0.6}{35}$$

$$\frac{8.2}{40} \frac{7.4}{16} \frac{6.1}{12} \frac{5.9}{9} \frac{5.5}{11} \frac{6.1}{17} \frac{6.2}{23} \frac{6.4}{28} \frac{4.0}{37} \frac{2.6}{43} \frac{0.0}{48}$$

$$\frac{8.4}{40} \frac{6.8}{16} \frac{6.0}{14} \frac{5.8}{12} \frac{5.3}{10} \frac{5.9}{18} \frac{6.4}{21} \frac{6.5}{25} \frac{5.4}{30} \frac{4.4}{37} \frac{0.0}{47}$$

$$\frac{8.0}{40} \frac{6.5}{17} \frac{5.8}{10} \frac{5.6}{13} \frac{5.1}{10} \frac{5.7}{14} \frac{5.8}{17} \frac{6.1}{19} \frac{5.1}{21} \frac{5.3}{26} \frac{5.0}{36} \frac{0.0}{46}$$

$$\frac{7.5}{40} \frac{7.0}{22} \frac{5.8}{16} \frac{5.3}{14} \frac{5.2}{12} \frac{4.8}{10} \frac{5.4}{16} \frac{5.8}{20} \frac{5.0}{25} \frac{0.7}{33}$$

$$\frac{7.9}{40} \frac{7.6}{25} \frac{6.3}{17} \frac{5.7}{15} \frac{5.5}{12} \frac{5.2}{10} \frac{5.6}{9} \frac{5.8}{13} \frac{6.4}{17} \frac{6.2}{20} \frac{5.0}{30} \frac{1.9}{37}$$

$$\frac{7.8}{40} \frac{7.6}{25} \frac{6.9}{19} \frac{5.5}{13} \frac{5.2}{12} \frac{4.9}{9} \frac{5.2}{14} \frac{5.7}{18} \frac{6.3}{28} \frac{4.9}{34} \frac{1.9}{44}$$

$$\frac{7.6}{40} \frac{7.0}{24} \frac{5.9}{19} \frac{5.2}{15} \frac{5.0}{12} \frac{4.6}{10} \frac{5.0}{10} \frac{5.4}{14} \frac{6.4}{18} \frac{5.3}{27} \frac{2.1}{34}$$

$$\frac{7.2}{40} \frac{6.9}{24} \frac{4.9}{15} \frac{4.8}{11} \frac{4.4}{10} \frac{4.9}{10} \frac{5.1}{13} \frac{6.2}{19} \frac{5.4}{28} \frac{2.5}{42}$$

$$\frac{6.9}{40} \frac{6.1}{21} \frac{5.4}{19} \frac{4.9}{14} \frac{4.8}{10} \frac{4.4}{11} \frac{5.0}{11} \frac{5.5}{16} \frac{6.3}{19} \frac{5.2}{28} \frac{2.3}{32}$$

$$\frac{7.1}{40} \frac{6.6}{23} \frac{5.8}{16} \frac{5.2}{14} \frac{5.0}{10} \frac{4.7}{11} \frac{5.1}{11} \frac{6.4}{20} \frac{6.3}{24} \frac{4.9}{29} \frac{2.1}{42}$$

$$\frac{6.8}{40} \frac{6.6}{31} \frac{6.1}{18} \frac{5.6}{13} \frac{5.3}{10} \frac{5.0}{11} \frac{5.4}{11} \frac{5.8}{15} \frac{6.5}{21} \frac{5.7}{29} \frac{3.0}{32}$$

$$\frac{5.4}{40} \frac{4.7}{33} \frac{4.6}{17} \frac{4.0}{14} \frac{3.8}{11} \frac{3.4}{11} \frac{3.9}{11} \frac{5.1}{23} \frac{4.0}{29} \frac{4.0}{40}$$

883.3v

44+00

+50

45+00

BM

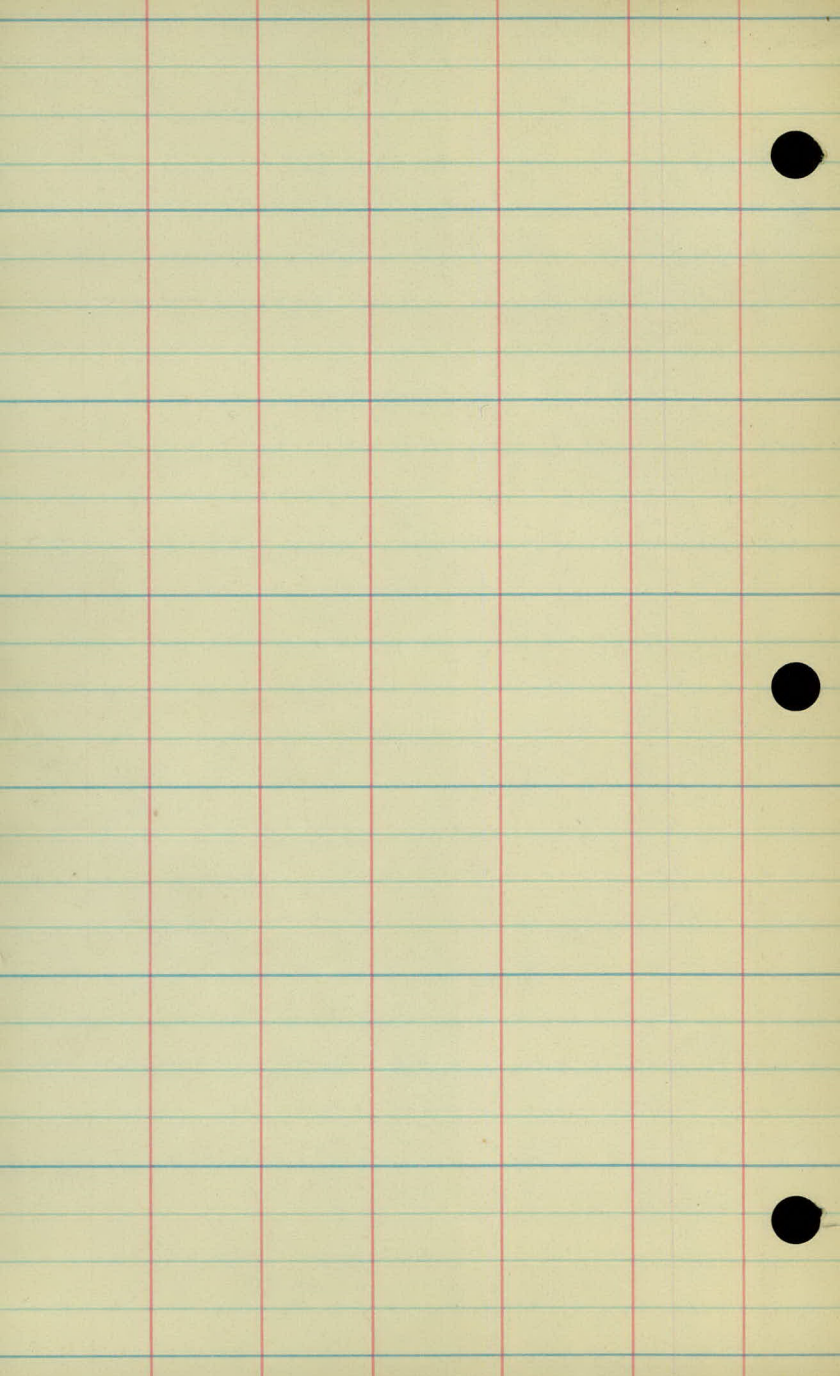
5.94 877.38

$$\frac{5.3}{40} \quad \frac{5.1}{33} \quad \frac{5.0}{21} \quad \frac{5.8}{18} \quad \frac{4.6}{13} \quad \frac{4.1}{10} \quad 3.8 \quad \frac{4.2}{10} \quad \frac{4.5}{13} \quad \frac{7.0}{26} \quad \frac{6.7}{40}$$

$$\frac{5.9}{40} \quad \frac{6.2}{29} \quad \frac{6.6}{25} \quad \frac{5.3}{22} \quad \frac{6.6}{17} \quad \frac{4.9}{13} \quad 4.2 \quad \frac{4.8}{11} \quad \frac{5.0}{13} \quad \frac{9.0}{24} \quad \frac{9.1}{40}$$

$$\frac{6.9}{40} \quad \frac{6.9}{32} \quad \frac{7.2}{26} \quad \frac{5.9}{22} \quad \frac{6.8}{19} \quad \frac{5.6}{13} \quad 4.6 \quad \frac{5.3}{12} \quad \frac{5.7}{14} \quad \frac{7.8}{17} \quad \frac{9.0}{22} \quad \frac{9.5}{25} \quad \frac{9.8}{40}$$

Spike in P.P. Rpt. of 45 + 30



Alignment
Arcade St.

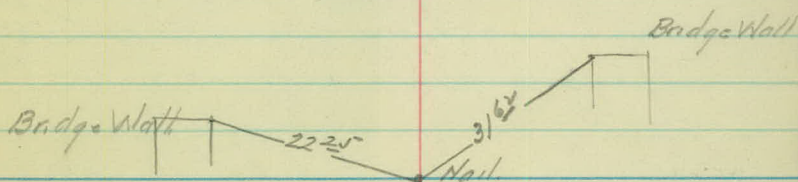
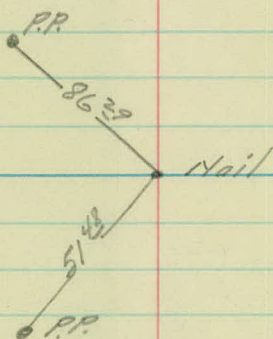
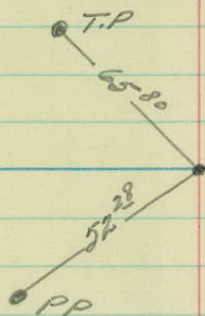
Sta Point Alt Art.

10+40⁰⁸

0°-03'

5+17³³

0+00



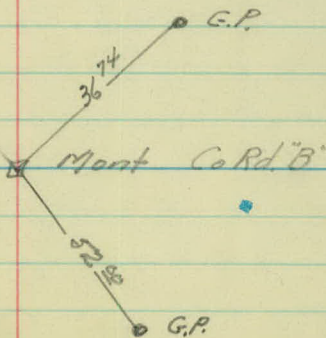
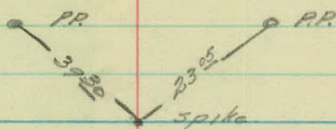
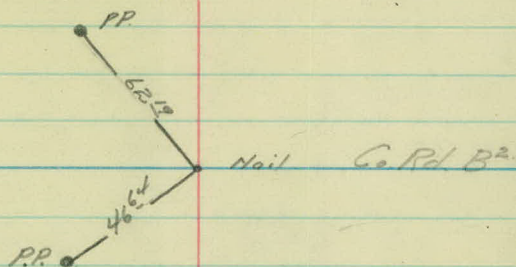
Sta Point L+Δ R+Δ

56+37⁵² P.O.T.

43+71⁴¹ P.O.T.

36+68⁷² P.I.

0°-03'



Sta. Point Alt. A.Rt.

67+82⁸⁰

65+46⁸¹

P.T.

16°-18'

65+00

14°-15'

+50

12°-25'

64+00

10°-25'

+50

8°-25'

63+00

6°-25'

63+48⁸¹

P.I.

32°-36'

+50

4°-25'

62+00

2°-25'

+50

0°-25'

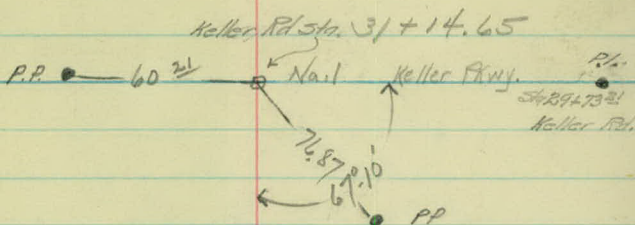
61+39⁸¹

P.C.

0°-00'

See page 6 New alignment

62+98⁸¹



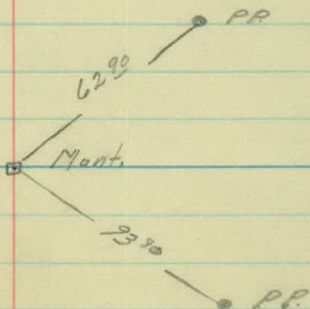
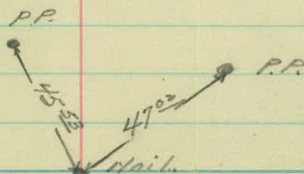
$\Delta 32^\circ - 36'$

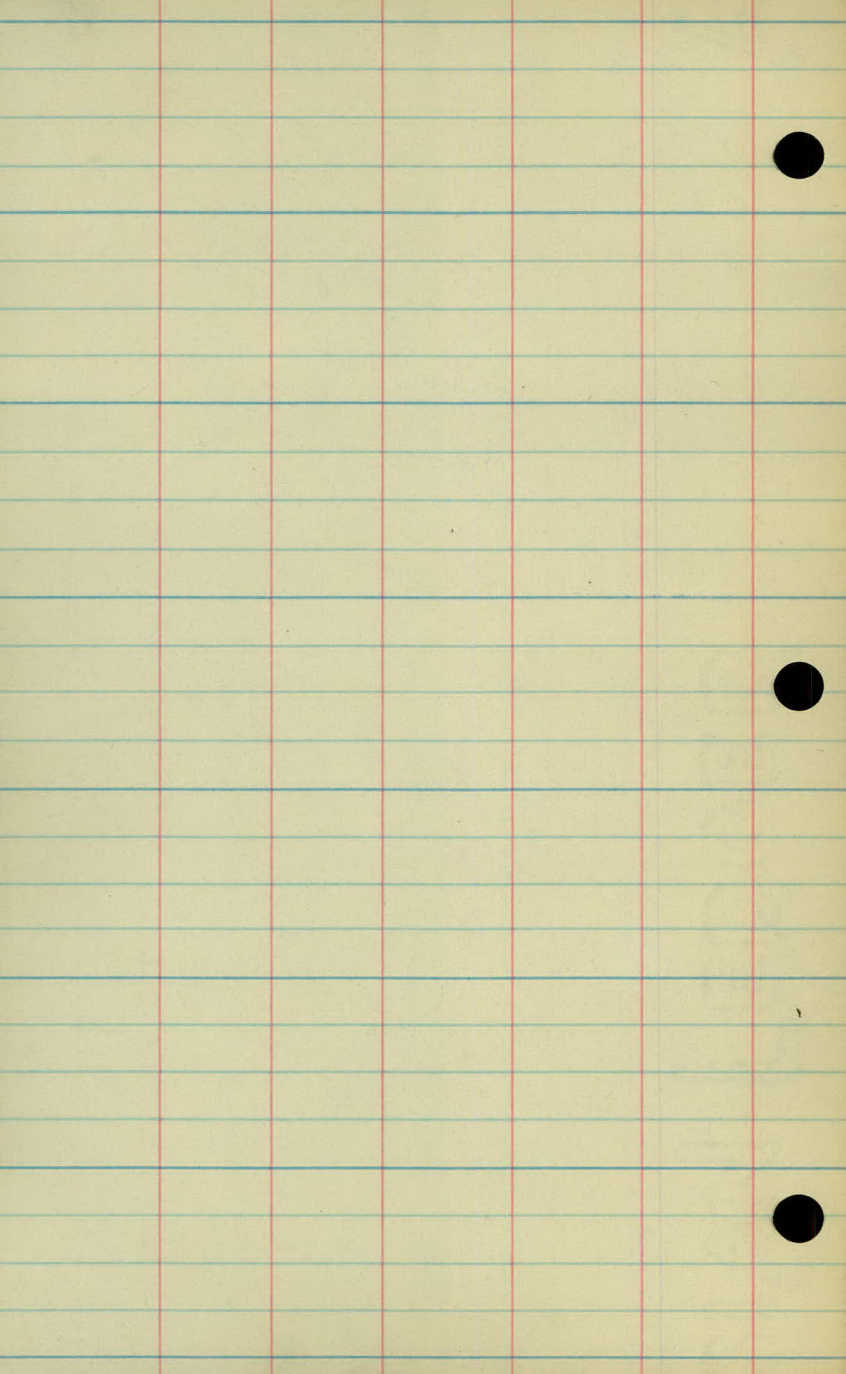
$\angle 8^\circ - 00'$

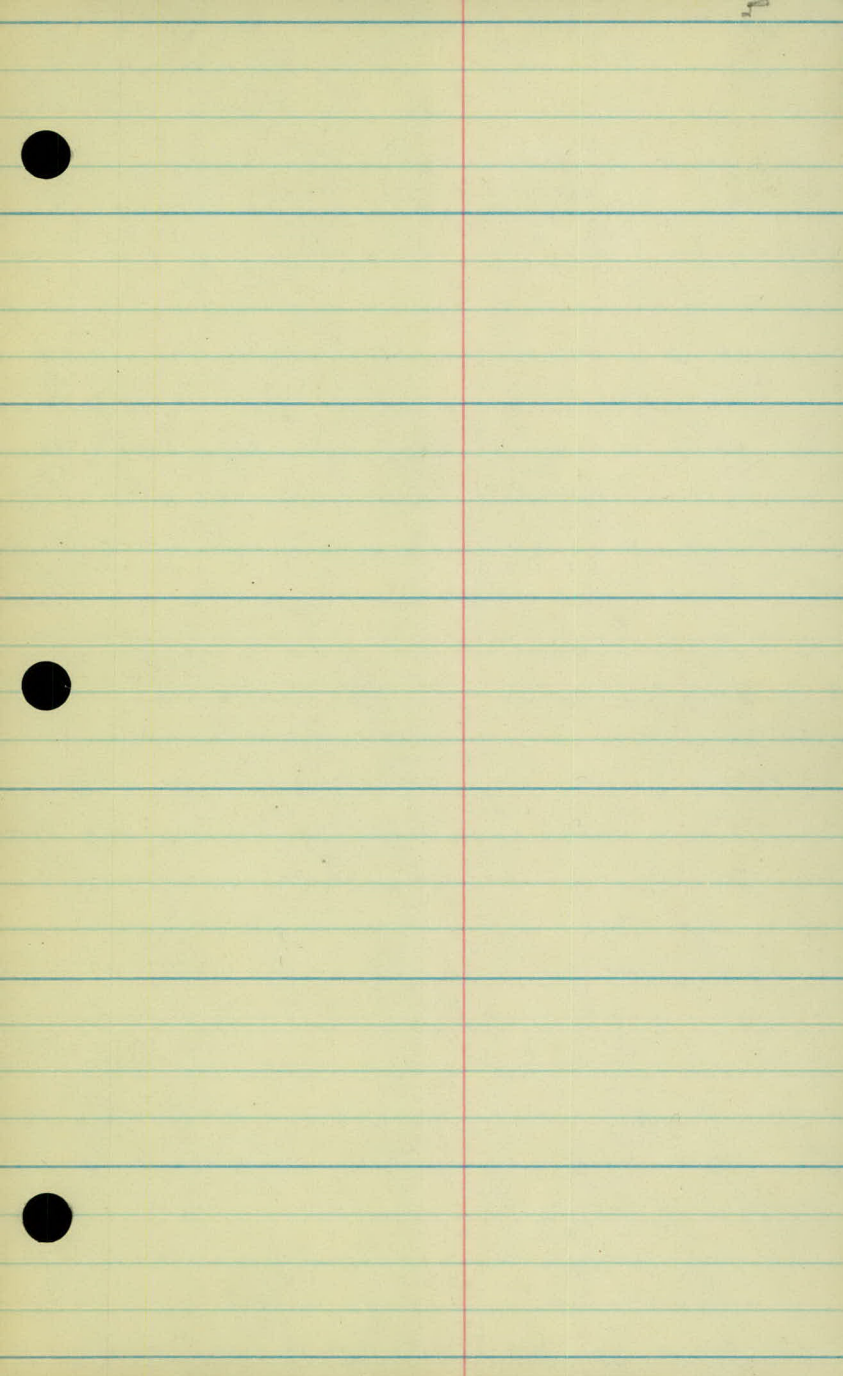
$T. 209.60$

$b. 407.50$

aid







Sta Point Alt. Δ Pt.

65+18.25[✓] P.T. 13°-18'

65+00 12°-21.2

+50 9°-51.2

64+00 7°-21.2

63+88.37[✓] P.I. 26°-36' 16'

+50 4°-51.2

63+00 3°-21.2[✓]62+52.25[✓] P.C. 0°-00'61+95.25[✓] P.T. 2°-49.5

+50 1°-40.8

61+39.31[✓] P.I. 5°-39' 1.5

61+00 0°-25.8

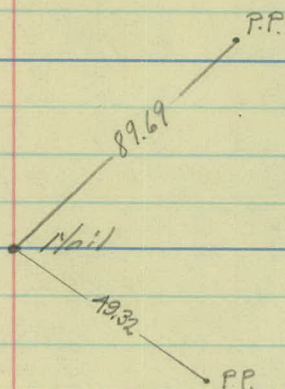
60+82.25[✓] P.C. 0°-00'

A $26^{\circ}-36'$

D $10^{\circ}-00'$

T. 135.62

h. 2660

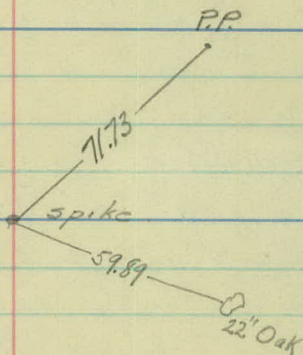


A $5^{\circ}-39'$

D $5^{\circ}-00'$

T. 56.56

h. 113.00



Sta. Point

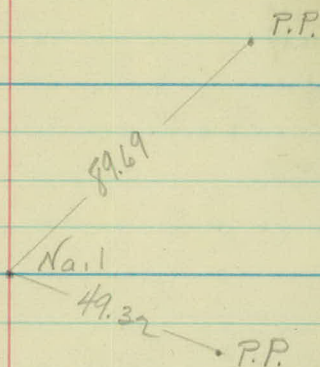
 Δ Rt.65+20.33 P.T. $13^{\circ}-27'$ 65+00 $12^{\circ}-26'$ 64+50 $9^{\circ}-56^{\circ}$ 64+00 $7^{\circ}-26^{\circ}$ 63+88.37 P.I. $26^{\circ}54'$ 63+50 $4^{\circ}-56'$ 63+00 $2^{\circ}-26'$ 62+51.33 P.C. $0^{\circ}-00'$

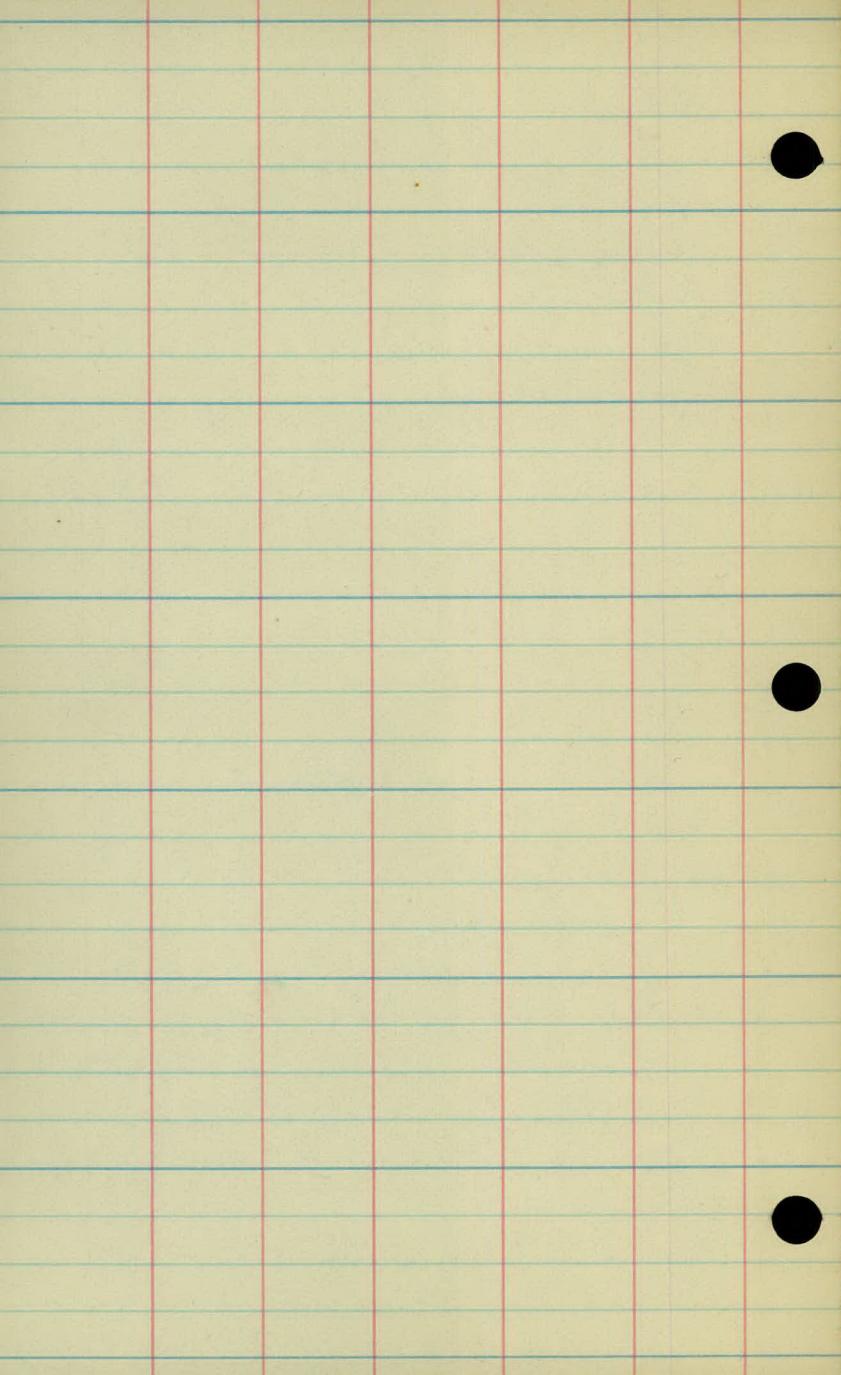
Δ 26°-54'

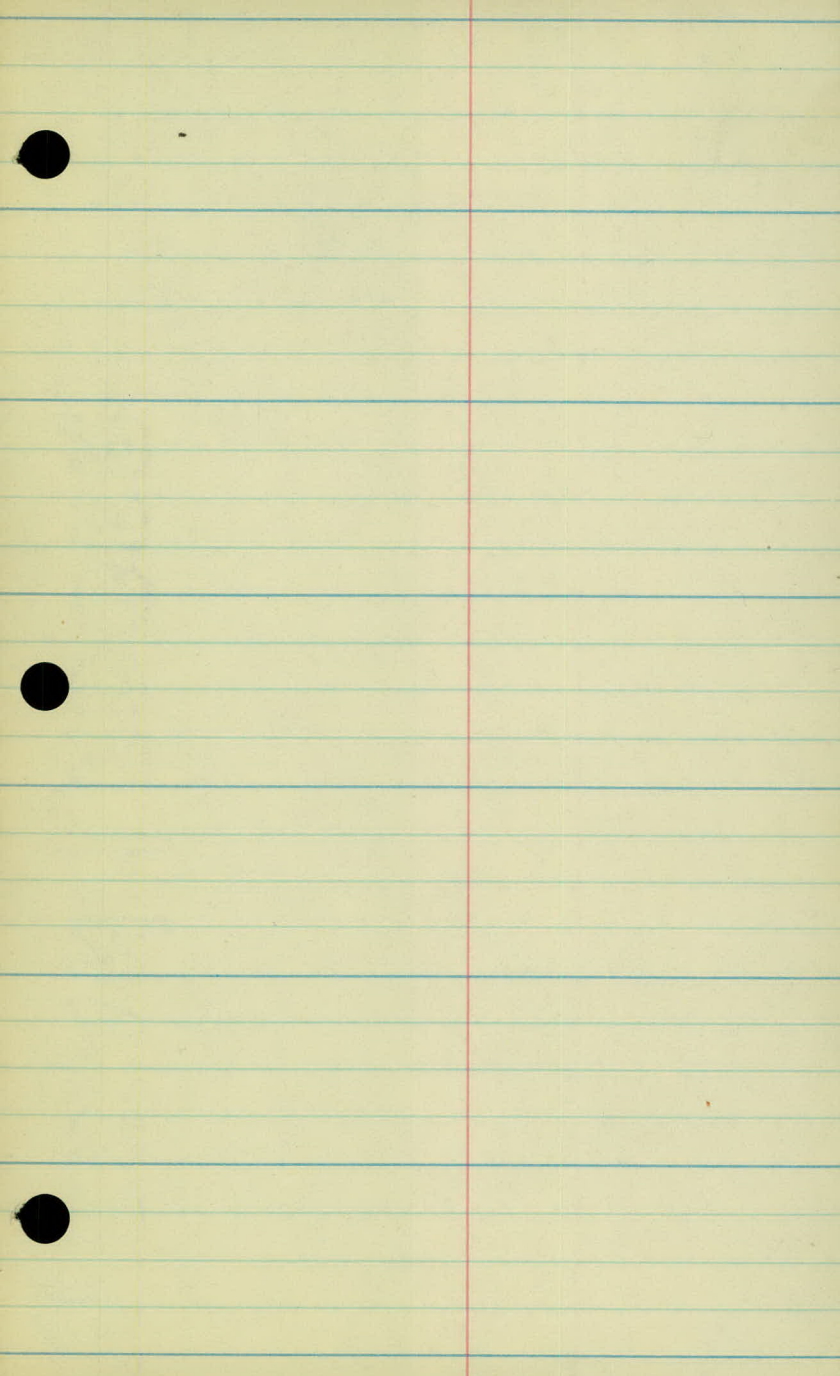
D 10°

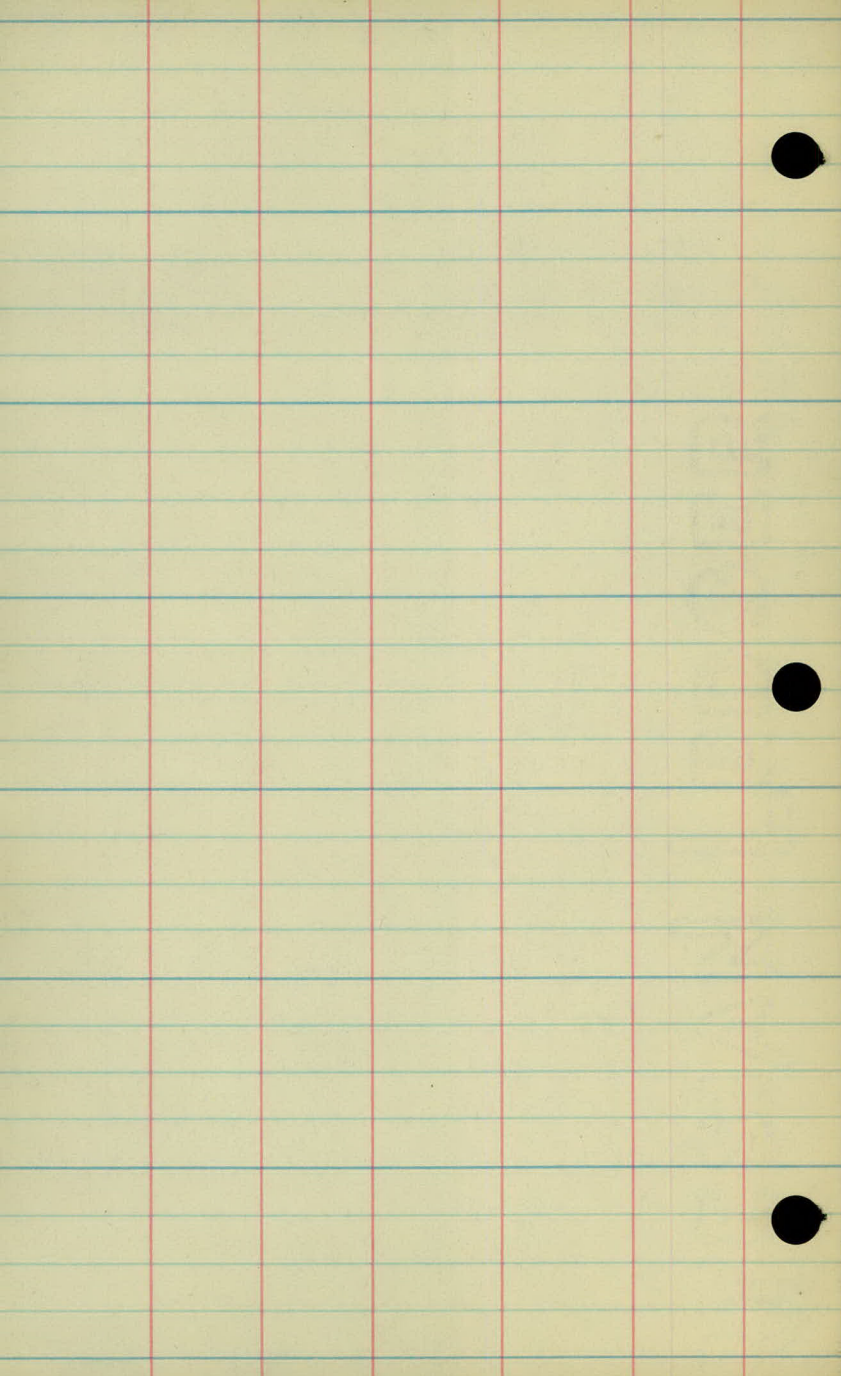
T 137.04

L 269.00









Cross Sect.

Arcade St.

0+00 -

Sta	+	Ht	-	Elev.
B.M.	11.11 7.11	899.63 895.63		888.52
T.P.	13.52	912.89 908.89	0.26	899.37 895.37
B.M.	1.46	911.93 907.93	2.42	910.47 906.47
0+00				09.9

+26				09.8
-----	--	--	--	------

+50				10.0
-----	--	--	--	------

1+00				10.5
------	--	--	--	------

+29				10.7
-----	--	--	--	------

+39				10.8
-----	--	--	--	------

2+00				11.3
T.P.	7.76	918.23 914.23	1.46	910.47 906.47
+09				11.3

+19		918.19 914.19		11.4
B.M.	7.72	898.75	7.76	910.47 906.47
+50				11.7

3+00		925.39 921.39		12.0
T.P.	12.86	906.05	5.66	912.53 908.53 893.19

906.87
888.52
18.35

Spike in PP. NW Cor First Ave & Arcade St.

Spike in PP. 18' ht of St 0+50

Bridge $\frac{20}{12} \frac{23}{14} \frac{20}{12} \frac{22}{14} \frac{18}{12}$ Bridge

$\frac{82}{50} \frac{115}{49} \frac{41}{41} \frac{129}{F107} \frac{129}{41} \frac{20}{19} \frac{22}{123} 21 \frac{25}{117} \frac{20}{16} \frac{27}{19} \frac{128}{30} \frac{223}{54} \frac{243}{60} \frac{122}{125}$

$\frac{21}{50} \frac{37}{41} \frac{481}{32} \frac{78}{F63} \frac{62}{31} \frac{19}{25} \frac{20}{17} \frac{20}{123} 19 \frac{22}{117} \frac{18}{15} \frac{122}{37} \frac{295}{53} \frac{227}{F205} \frac{287}{610} \frac{287}{69}$

$\frac{19}{50} \frac{68}{38} \frac{68}{30} \frac{71}{F51} \frac{16}{34} \frac{17}{19} \frac{17}{123} 14 \frac{16}{117} \frac{10}{17} \frac{127}{41} \frac{141}{F141} \frac{178}{410} \frac{178}{53}$

$\frac{28}{50} \frac{41}{47} \frac{80}{28} \frac{55}{F40} \frac{52}{28} \frac{11}{20} \frac{15}{123} 12 \frac{13}{117} \frac{10}{18} \frac{57}{30} \frac{49}{36} \frac{84}{50} \frac{49}{44} \frac{49}{90}$

$\frac{04}{50} \frac{03}{36} \frac{09}{24} \frac{14}{123} 11 \frac{13}{117} \frac{09}{18} \frac{58}{31} \frac{42}{29} \frac{64}{50}$

Driveway

$\frac{14}{50} \frac{06}{41} \frac{00}{26} \frac{08}{123} \frac{06}{117} \frac{08}{15} \frac{06}{20} \frac{25}{25} \frac{23}{29} \frac{15}{33} \frac{03}{36} \frac{12}{39} \frac{10}{50}$

$\frac{44}{50} \frac{57}{35} \frac{65}{22} \frac{70}{123} \frac{69}{117} \frac{72}{19} \frac{70}{24} \frac{87}{30} \frac{87}{35} \frac{70}{35} \frac{38}{40} \frac{44}{50}$

$\frac{43}{50} \frac{82}{42} \frac{106}{33} \frac{91}{26} \frac{65}{18} \frac{70}{123} \frac{68}{117} \frac{71}{18} \frac{71}{21} \frac{85}{27} \frac{92}{35} \frac{80}{42} \frac{32}{50} \frac{35}{50} \frac{91}{F20} \frac{91}{40}$

$\frac{29}{50} \frac{114}{F46} \frac{36}{55} \frac{66}{50} \frac{113}{42} \frac{115}{35} \frac{114}{28} \frac{66}{17} \frac{68}{123} \frac{68}{117} \frac{63}{18} \frac{84}{25} \frac{87}{28} \frac{82}{33} \frac{20}{43} \frac{22}{50} \frac{85}{F20} \frac{40}{210}$

$\frac{26}{50} \frac{95}{F33} \frac{11}{50} \frac{09}{46} \frac{43}{39} \frac{93}{29} \frac{94}{25} \frac{63}{18} \frac{64}{123} \frac{64}{117} \frac{64}{17} \frac{72}{21} \frac{73}{27} \frac{49}{35} \frac{42}{41} \frac{49}{50} \frac{93}{F20} \frac{93}{260}$

2+0 + ~~914.39~~ ✓ - 15/20
 921.39
 906.05

3+39 12.1

+56 12.3

4+00 12.1

+50 11.8

5+00 11.5

+50

~~916.98~~ ✓

10.8
~~912.53~~ ✓

T.P

4.45

917.98
 892.64

12.86

908.53
 893.19

6+00

09.9

+34

09.3

+50

08.9

7+00

~~911.33~~ ✓

07.8

T.P

4.65

907.33

~~906.68~~ ✓

891.99

10.30

902.68

887.34

+50

06.9

8+00

06.1

$$47.1 \frac{41}{9.2} \frac{41}{50} \frac{38}{44} \frac{134}{37} \frac{144}{31} \frac{130}{18} \frac{134}{123} 133 \frac{135}{117} \frac{128}{21} \frac{142}{25} \frac{101}{36} \frac{106}{42} \frac{111}{50} \frac{113}{93} /$$

$$44.7 \frac{30}{61.01} \frac{30}{50} \frac{29}{42} \frac{122}{29} \frac{143}{24} \frac{142}{22} \frac{130}{18} \frac{133}{123} 131 \frac{133}{117} \frac{126}{20} \frac{111}{29} \frac{24}{39} \frac{24}{50} \frac{24}{107} / 50.4$$

$$46.6 \frac{45}{68.8} \frac{41}{50} \frac{42}{41} \frac{114}{32} \frac{133}{20} \frac{134}{123} 133 \frac{135}{117} \frac{128}{20} \frac{141}{24} \frac{140}{28} \frac{126}{33} \frac{45}{43} \frac{45}{50} \frac{45}{68.8} /$$

$$50.0 \frac{31}{61.5} \frac{31}{50} \frac{27}{40} \frac{124}{25} \frac{133}{19} \frac{137}{123} 136 \frac{137}{117} \frac{127}{21} \frac{116}{31} \frac{108}{34} \frac{06}{43} \frac{06}{50} \frac{08}{61.8} / 54.6$$

$$50.2 \frac{3.3}{61.06} \frac{31}{49} \frac{125}{35} \frac{130}{25} \frac{141}{123} 13.9 \frac{140}{117} \frac{133}{22} \frac{36}{38} \frac{3.7}{50} \frac{3.6}{61.3} / 49.6$$

$$\frac{94}{50} \frac{138}{39} \frac{148}{123} \frac{146}{117} \frac{148}{27} \frac{133}{32} \frac{131}{43} \frac{36}{50} \frac{3.8}{61.06} \frac{38}{50} /$$

$$\frac{6.6}{50} \frac{7.2}{46} \frac{7.1}{26} \frac{7.2}{123} 7.1 \frac{7.2}{117} \frac{6.5}{18} \frac{5.4}{29} \frac{1.7}{36} \frac{0.3}{50} \frac{11}{66.9} / 41.2$$

$$\frac{9.0}{50} \frac{8.1}{25} \frac{8.0}{123} 7.7 \frac{7.8}{117} \frac{7.5}{19} \frac{8.4}{23} \frac{7.6}{30} \frac{6.4}{33} \frac{4.4}{50} \frac{7.6}{61.1} / 27.2$$

$$27.6 \frac{112}{13.8} \frac{132}{50} \frac{131}{37} \frac{119}{27} \frac{8.4}{19} \frac{8.4}{123} 8.1 \frac{8.3}{117} \frac{8.1}{18} \frac{9.0}{21} \frac{9.1}{27} \frac{6.7}{50} \frac{9.1}{61.05} / 27.0$$

$$32.7 \frac{15.4}{16.2} \frac{15.4}{50} \frac{15.4}{29} \frac{9.9}{18} \frac{9.6}{123} 9.2 \frac{9.4}{117} \frac{9.1}{18} \frac{12.1}{26} \frac{12.7}{29} \frac{11.5}{50} \frac{12.4}{13.2} / 26.4$$

59

$$29.4 \frac{9.1}{14.7} \frac{9.0}{50} \frac{9.3}{33} \frac{9.0}{29} \frac{4.6}{17} \frac{4.5}{123} 4.4 \frac{4.5}{117} \frac{4.3}{17} \frac{5.1}{26} \frac{5.7}{50} \frac{5.7}{61.08} / 27.6$$

$$27.6 \frac{9.1}{13.8} \frac{9.1}{50} \frac{9.2}{32} \frac{8.2}{24} \frac{5.3}{18} \frac{5.3}{123} 5.2 \frac{5.3}{117} \frac{5.0}{19} \frac{6.7}{23} \frac{6.0}{32} \frac{4.1}{50} \frac{6.7}{61.00} / 26.0$$

5+9	+	871.33 ✓ 907.33 891.99	-	Eleu
8+50		911.28 ✓ 907.29		08.1 906.68 ✓ 902.68
TR	461	891.95	465	887.34
9+00				04.0
TR				
+50				02.6
10+00		903.35 ✓ 899.35		900.8 902.34 ✓ 898.34
BT	101	884.01	895	883.00
11+00				897.1
+50				95.4
12+00				93.3
+50		891.4 ✓ 889.4 ✓		90.9 890.59 ✓ 886.59
TR	0.83	872.08	12.76	871.25
13+00				88.0
+50				85.3
14+00		883.04 ✓ 879.04		83.0 882.67 ✓ 878.67
TR	0.37	863.70	8.75	863.33
+50				80.9

12+50
1.25

27.5/59 66 67 58 76 79 65 64 6.2 6.5 6.2 83 8.5 92 84 8.7/2.50
C0.3 50 33 26 23 21 17 12.3

31.8/54 34 53 51 88 87 75 7.5 7.3 7.7 7.5 7.5 105 10.7 104 8.8
C1.9 50 36 26 22 20 18 12.3 11.7 19 27 34 40 50 F1.5/2

37.2/46 4.0 52 98 102 89 8.9 8.7 90 8.9 12.0 12.2 63 55 12.1/2.50
C4.1 50 30 23 21 17 12.3 11.7 20 26 36 45 50 F3.4/2.50

93 98 101 106 105 106 103 145 12.7 33 135/26.0
50 39 26 12.3 11.7 22 32 39 50

spike in PR 18 R124 9+80

Clear - Gold.

Filling 3.4 4.6 5.3 5.9 4.3 7.2 8.4 8.3 12.4 12.7
33 25 13 13 28 34 46 50

6.8 7.6 8.0 8.3 9.1 10.2 11.8
22 12 15 28 41 58

6.2 8.1 9.5 10.6 10.3 10.1 10.3 11.1
50 26 23 17 10 14 50

33.2/94 7.9 10.7 12.2 12.5 12.5 12.6 12.5 12.7 13.4 14.1
C3.1 50 21 18 16 13 9 11 27 44

29.8/1.0 0.1 1.2 3.6 3.5 3.4 9.8 4.1 6.2 8.1 6.2/2.50
C2.4 40 25 17 6 10 17 24 50 F2.8/2.50

28.4/54 50 4.3 52 56 63 6.3 6.2 6.1 6.2 6.7 9.4 7.7 9.4
C0.7 50 33 29 22 19 16 6 9 16 23 40 F3.3/2.4.6
99

25.8/90 8.4 9.2 8.8 8.5 8.4 8.5 9.0 11.8 11.5 11.6/4.4
C0.9 40 24 13 8 10 15 21 40 F3.2/2

24.4/3.4 3.7 3.5 2.4 2.2 2.1 2.2 2.5 5.6 5.2 5.6/2.50
C0.2 40 25 19 9 6 13 18 40 F3.8/2.50

Sta	+	883.04	-	Elev
		879.04		
		863.70		

15+00

+50

874.24	874.15
870.24	870.15
854.90	854.81

T.P. 0.09 8.89

16+00

+50

17+00

870.12	866.22
866.12	862.22
850.78	846.88

T.P. 2.90 8.02

+50

18+00

868.27	862.39
864.27	858.39
848.93	843.05

B.M. 5.88 7.73

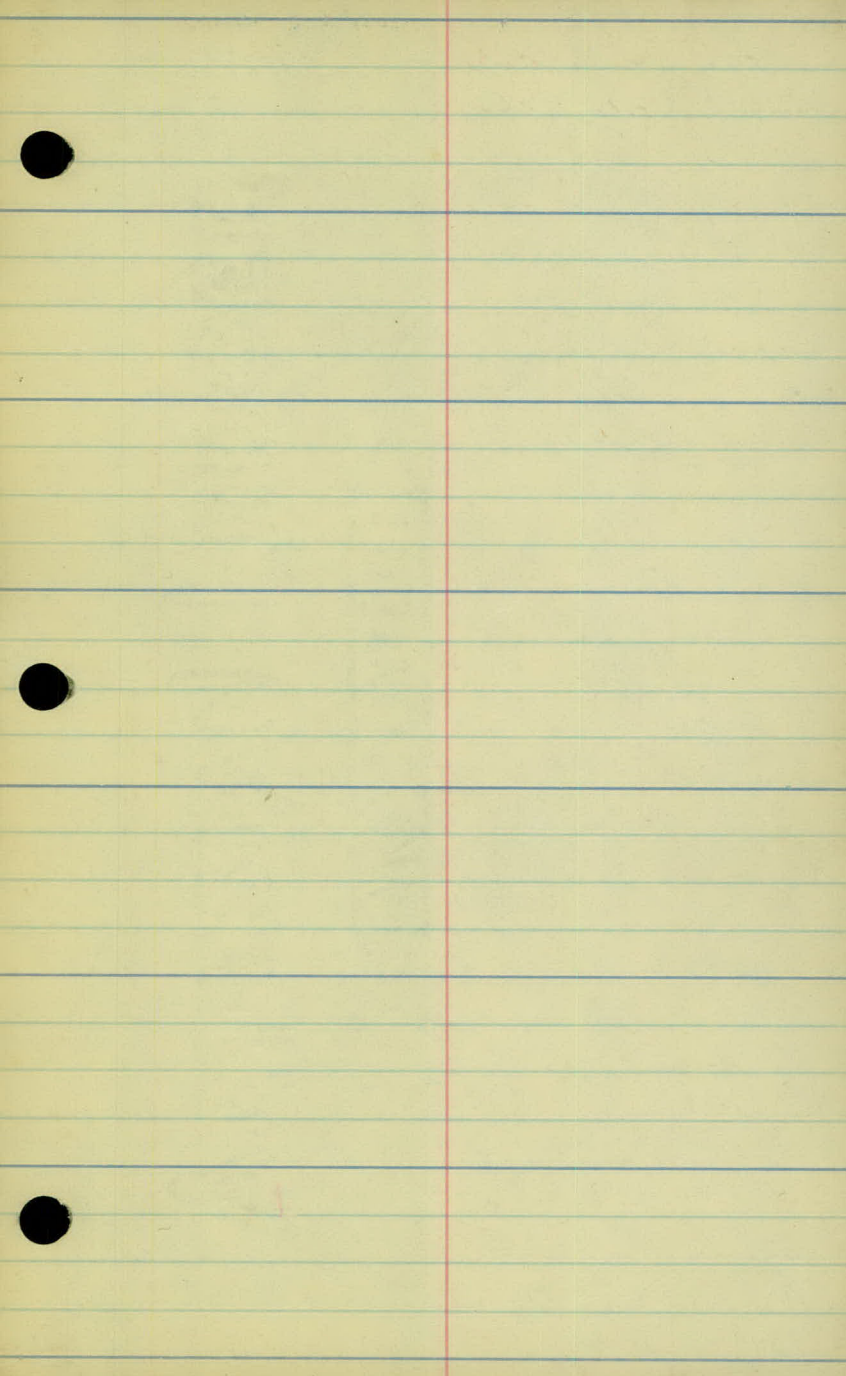
+50

19+00

+50

20+00

+50



Sta	+	848.58	-	856.89
		851.58		858.39
B.M.	13.19	856.24		843.05
23+00				52.3

+50				53.9
-----	--	--	--	------

24+00		886.70		855.76
		884.70		857.56
T.P.	11.14	867.36	0.02	856.22
+17				856.4

+50				857.4
-----	--	--	--	-------

25+00				859.2
-------	--	--	--	-------

+50				60.7
-----	--	--	--	------

26+00				61.8
-------	--	--	--	------

+50				62.8
-----	--	--	--	------

27+00				63.8
-------	--	--	--	------

+23				64.8
-----	--	--	--	------

+58				64.7
-----	--	--	--	------

28+00				886.54
				886.49
B.M.			2.21	865.15

21-00-D.C.

26.3 g 00 Gut.

3.9

2.3

0.5

$\frac{12.2}{11.0}$

$\frac{12.2}{0.01242}$

$\frac{11.5}{10.0}$

$\frac{11.2}{0.03246}$

8.2

6.7

5.6

4.6

3.6

3.1

2.7

2.0

B.M.	10.02	894.51 890.51 875.17		884.49 880.49 865.15
27+58				
27+23		904.11 900.11		894.35 890.35
T.P.	9.76	884.77	0.16	875.01
27+00				63.8
+50				62.8
26+00				61.8
28+00				65.4
27+58				64.7
27+23				64.3
25+50		906.98 902.96		906.98 897.14
T.P.	5.84	887.64	2.77	881.80
26+00				61.8
+50				60.7
25+00				59.2
+50				57.4

$$354/4.1 \checkmark$$

18.5

$$404/16 \checkmark$$

110

$$456/8.1$$

C12.9

(210)

$$4.9/504 \checkmark$$

$$52/515 \checkmark$$

$$548/30$$

C190

(220)

(230)

$$7.8/49.1$$

(194)

$$11.3/38.4 \checkmark$$

(20.1)

$$8.2/44.2 \checkmark$$

(20.5)

$$5.7/48.5 \checkmark$$

(24.1)

$$12.3/44.0$$

$$61.3/2.5$$

C23.3

(258)

$$63.5/2.1$$

C24.8

(26.9)

$$62.3/4.4$$

C24.0

(28.4)

$$63.8/5.2$$

C250

(30.2)

Sta	+	966.98	-	Elev
		902.98		
		887.64		

24+00		895.67		557
		891.67		891.50
T.P.	0.17	876.33	11.48	876.16
23+50				53.9

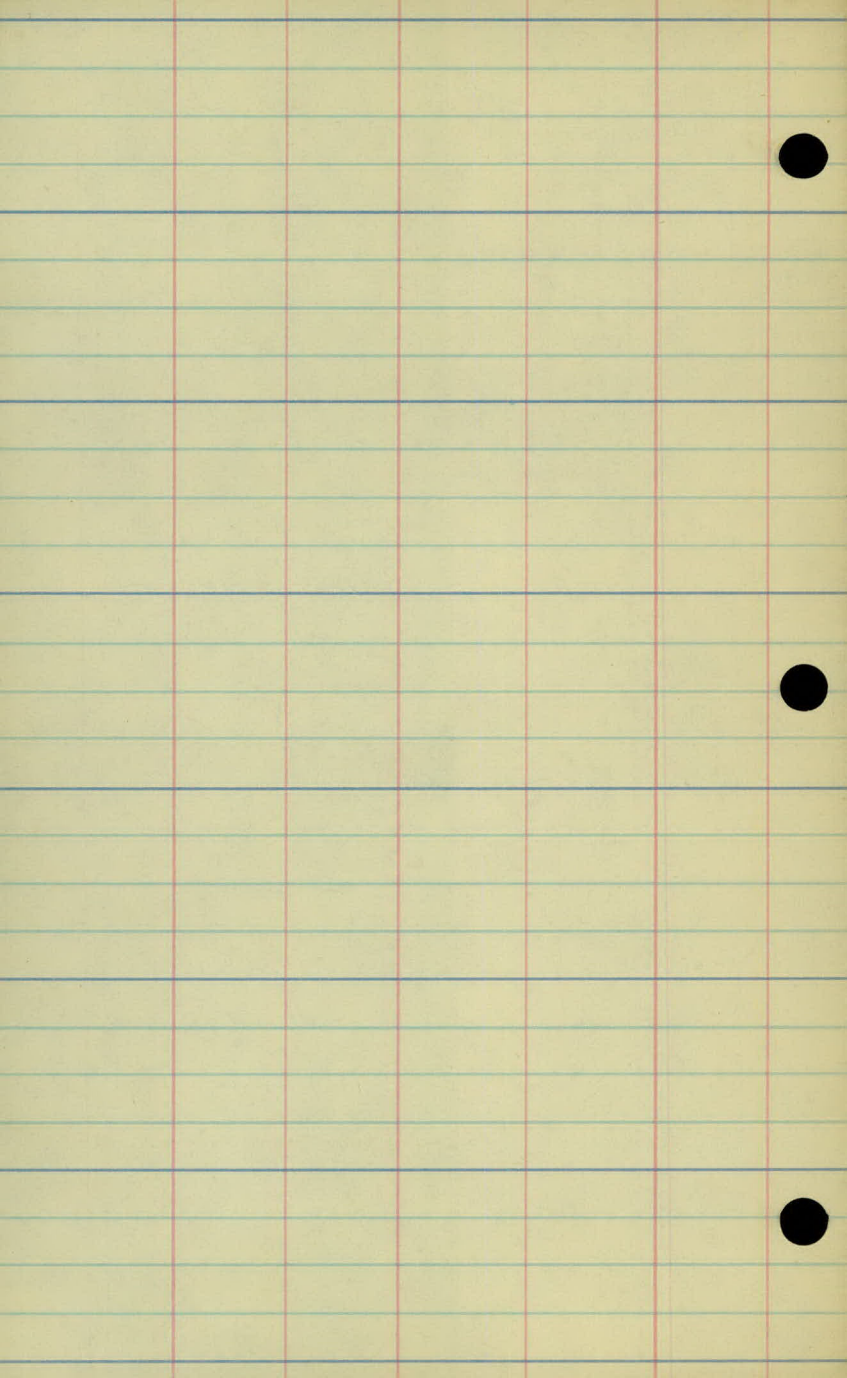
25+00		893.05		59.2
		874.05		878.73
T.P.	0.32	863.71	12.94	863.39
		870.54		867.82
T.P.	2.72	855.20	11.23	852.48
B.M.			12.18	858.36
				843.02 = 843.05

$$61.7 / \frac{83}{C 23.6} \quad 31.9$$

$$55.1 / \frac{32}{C 19.2} \quad 22.4$$

$$17.1$$

$$\frac{9.0}{C 81} / 38.4$$



Sta	+	41.8756 ✓	Even
B.M.	4.02	874.21	889.53
		870.21	870.19
35+00			86.6

+50		88.1
-----	--	------

36+00		89.7
	9.33	898.86 ✓
		879.52 ✓ 402
		889.53 ✓
		870.19 ✓

+29		90.6
-----	--	------

+43		91.1
-----	--	------

+69	Co. R.D. "B"	92.0
-----	--------------	------

+82		92.3
-----	--	------

+91		92.6
-----	--	------

37+00		92.9
		873.5

+50		94.2
		74.8

38+00		95.5
		76.1

+59		97.0
		77.6

T.P.	11.24	909.79	0.31	898.55
		890.45 ✓		879.21 ✓

R.R. spike in P.P. 19' R+5 to 36+02.

31.0/123 143 130 7.7 7.3 7.0 7.2 7.2 140 158
F65 40 24 12 8 12 19 32 40

32.9/140
F72

28.0/105 108 9.5 6.4 5.7 5.5 5.7 6.9 11.9 13.9 13.0/31.0
F50 40 21 13 8 11 20 31 40 F65

24.0/54 7.6 7.2 6.2 4.9 4.7 4.2 3.9 4.1 4.8 7.5 9.0
DC00 40 31 27 20 14 8 12 21 30 40

107 109 96 86 101 9.0 8.5 8.3 8.5 8.9 10.1 8.5 11.1
40 32 26 20 15 13 8 11 20 23 28 40

6.5 7.3 8.2 7.8 7.8 7.8
40 28 16 10 29 40

5.7 6.3 6.9 6.9 7.1 7.6 8.7 6.6
40 25 8 9 19 22 28 Stone Wall

5.9 6.2 6.5 4.6 6.7 7.2 6.3 5.5
40 21 8 9 16 26 33

6.6 6.8 6.2 6.3 6.6 6.7 5.6 5.0
40 30 26 10 16 31 40

3.5 3.6 6.9 6.2 6.2 6.0 6.4 6.7 6.3 0.5
40 29 20 19 14 11 19 25 35

2.4 5.8 5.2 3.0 4.7 5.2 5.3 5.8 5.1 1.2
22 17 12 8 11 18 20 23 28

1.1 3.7 4.1 3.6 3.4 3.8 4.1 3.0 0.2
20 17 15 8 11 20 26 29

0.6 2.2 2.1 1.9 2.1 1.8 0.9
18 15 8 12 21 28

Sta

+

H.I.
909.79
890.45

-

Elev

37+00

92.9

+50

94.2

38+00

95.5

+59

97.0

+66

97.2

+75

97.5

+82

97.6

39+00

98.2

T.P.

559

904.14
887.80

1124

898.55
879.21

✓

+50

99.0

40+00

99.4

+50

99.3

41+00

99.3

$$(16.9) \quad \frac{74}{36} \frac{68}{40} \frac{81}{60} \frac{70}{C100} / 42.0$$

$$\frac{45.0}{C12.0} \frac{3.7}{60} \frac{3.5}{60} \frac{87}{40} \frac{3.2}{32} (15.6) \frac{5.6}{33} \frac{60}{40} \frac{73}{60} \frac{60}{C9.7} / 40.6$$

$$\frac{42.1}{C13.4} \frac{1.0}{60} \frac{0.9}{40} \frac{0.5}{32} (14.3) \frac{4.0}{36} \frac{4.3}{40} \frac{6.6}{60} \frac{4.6}{C9.8} / 41.7$$

$$\frac{47.2}{C13.5} \frac{+0.6}{60} \frac{+0.7}{40} \frac{+0.6}{40} \frac{+0.1}{32} (12.8) \frac{2.6}{40} \frac{3.5}{50} \frac{5.1}{60} \frac{2.3}{C10.6} / 42.9$$

$$\frac{+0.3}{60} \frac{+0.4}{40} \frac{0.2}{31} \frac{9.9}{21} \frac{12.8}{15} \frac{12.8}{9} 12.6 \frac{12.8}{12} \frac{12.8}{17} \frac{12.0}{29} \frac{10.1}{40}$$

$$\frac{+0.2}{60} \frac{+0.1}{40} \frac{0.3}{31} \frac{7.1}{25} \frac{12.2}{16} \frac{12.9}{9} 12.3 \frac{12.6}{12} \frac{13.0}{18} \frac{11.9}{26} \frac{9.9}{40}$$

$$\frac{+0.2}{60} \frac{+0.2}{40} \frac{0.3}{31} \frac{9.6}{21} \frac{12.4}{17} \frac{12.3}{8} 12.2 \frac{12.4}{12} \frac{12.9}{17} \frac{13.2}{21} \frac{10.8}{28} \frac{9.7}{33} \frac{5.2}{40}$$

$$\frac{5.0}{C2.5} / 31.8$$

$$\frac{42.9}{C12.0} \frac{1.5}{60} \frac{2.7}{60} \frac{1.5}{40} \frac{1.9}{23} \frac{9.1}{21} \frac{13.2}{15} \frac{11.8}{9} \frac{11.6}{11} \frac{12.0}{16} \frac{12.4}{21} \frac{13.1}{25} \frac{11.6}{29} \frac{7.5}{40} \frac{8.3}{39} \frac{7.5}{32.9}$$

$$31.2 \frac{2.3}{C2.8} \frac{4.1}{40} \frac{2.3}{32} \frac{1.5}{24} \frac{4.7}{21} \frac{6.0}{17} \frac{5.7}{13} \frac{5.4}{8} 5.1 \frac{5.5}{12} \frac{5.9}{17} \frac{6.6}{22} \frac{5.1}{26} \frac{7.9}{40} \frac{5.1}{C2.0} / 27.0$$

6.2

$$\frac{26.9}{C2.10} \frac{5.2}{40} \frac{7.8}{40} \frac{6.6}{33} \frac{4.5}{21} \frac{5.7}{17} \frac{5.2}{11} \frac{5.0}{8} 4.7 \frac{5.1}{11} \frac{5.5}{19} \frac{6.2}{22} \frac{5.3}{25} \frac{5.2}{32} \frac{8.6}{40} \frac{5.2}{C2.12} / 27.0$$

6.3

$$\frac{9.9}{40} \frac{9.0}{34} \frac{6.1}{22} \frac{5.7}{13} \frac{5.1}{8} 4.8 \frac{5.2}{12} \frac{5.9}{20} \frac{6.7}{22} \frac{5.4}{25} \frac{5.5}{32} \frac{9.1}{40} \frac{5.4}{C2.09} / 25.8$$

$$\frac{28.4}{F5.2} \frac{10.0}{40} \frac{10.6}{40} \frac{10.4}{33} \frac{9.3}{24} \frac{5.4}{16} \frac{5.1}{9} 4.8 \frac{5.2}{11} \frac{5.7}{17} \frac{6.7}{23} \frac{8.6}{40}$$

Sta + H.I. - Elev.
 904.14
 884.80

41+50 99.5

42+00 99.6

+50 899.8

T.P. 9.46 909.06 889.72 454 899.60 880.26

B.M. 12.57 909.02 889.68 12.61 896.45 877.11

43+00 900.0

+50 899.9

44+00 99.7

+40 899.2

45+00 899.64 880.50 907.1 897.7

T.P. 3.19 780.30 12.57 896.45 877.11

+50 896.4

46+00 95.2

T.P. 2.11 898.56 879.22 3.19 896.45 877.11

+50 94.2

$$24\frac{80}{134} \cdot \frac{80}{40} \quad \frac{78}{33} \frac{82}{28} \quad \frac{75}{22} \frac{53}{15} \frac{48}{8} \quad 46 \quad \frac{52}{13} \frac{56}{17} \frac{64}{21} \frac{123}{33} \frac{133}{40} \frac{123}{F77} / 30.4$$

$$21\frac{44}{60.1} \frac{32}{40} \frac{3.5}{34} \frac{46}{26} \frac{58}{21} \frac{59}{19} \frac{53}{15} \frac{48}{9} \quad 45 \quad \frac{49}{11} \frac{53}{17} \frac{63}{21} \frac{102}{27} \frac{113}{31} \frac{119}{32} \frac{134}{40} \frac{119}{F79} / 32$$

$$35\frac{20.2}{104.1} \frac{104}{40} \frac{25}{32} \frac{5.4}{28} \frac{5.7}{18} \frac{49}{12} \frac{47}{9} \quad 43 \quad \frac{46}{11} \frac{52}{17} \frac{58}{21} \frac{68}{27} \frac{78}{40} \frac{58}{1000} / 4.0$$

Br. spike in GP 19' 6" 5' 9" 45' + 29.

$$49\frac{28}{106.2} \frac{28}{40} \frac{3.4}{33} \frac{5.9}{30} \frac{8.1}{26} \frac{102}{20} \frac{98}{17} \frac{95}{11} \quad 90 \quad \frac{95}{11} \frac{99}{17} \frac{109}{22} \frac{87}{26} \frac{77}{40} \frac{8.8}{100} / 27.4$$

$$360\frac{46}{104.5} \frac{46}{40} \frac{4.9}{32} \frac{101}{22} \frac{102}{19} \frac{98}{17} \frac{95}{11} \quad 91 \quad \frac{97}{12} \frac{99}{16} \frac{107}{21} \frac{105}{24} \frac{74}{27} \frac{80}{40} \frac{76}{100} / 30$$

$$72\frac{31.6}{102.5} \frac{27}{40} \frac{20}{32} \frac{8.1}{30} \frac{8.2}{28} \frac{10.8}{21} \frac{104}{18} \frac{98}{12} \quad 93 \quad \frac{97}{11} \frac{100}{15} \frac{107}{21} \frac{36}{31} \frac{36}{40} \frac{36}{100} / 39.4$$

$$118\frac{40}{120.0} \frac{75}{40} \frac{90}{31} \frac{115}{28} \frac{120}{25} \frac{111}{18} \frac{105}{13} \quad 98 \quad \frac{102}{11} \frac{104}{15} \frac{108}{18} \frac{98}{22} \frac{17}{32} \frac{13}{40} \frac{11}{100} / 44$$

$$270\frac{1.8}{100.0} \frac{1.8}{40} \frac{1.8}{25} \frac{36}{23} \frac{23}{12} \quad 19 \quad \frac{23}{10} \frac{26}{15} \frac{32}{18} \frac{3.1}{21} \frac{2.2}{23} \frac{12}{32} \frac{0.7}{40} \frac{19}{1000} / 27$$

$$21\frac{47}{115} \frac{4.9}{40} \frac{4.9}{29} \frac{4.9}{23} \frac{3.6}{11} \quad 32 \quad \frac{3.8}{11} \frac{40}{15} \frac{51}{21} \frac{6.6}{26} \frac{70}{32} \frac{6.5}{40} \frac{6.4}{100} / 24$$

$$27\frac{4.3}{101} \frac{4.3}{40} \frac{4.2}{25} \frac{5.5}{21} \frac{5.0}{17} \frac{4.7}{12} \quad 44 \quad \frac{4.8}{10} \frac{5.1}{16} \frac{7.8}{25} \frac{8.3}{30} \frac{8.4}{40} \frac{7.9}{100} / 25.0$$

$$310\frac{1.4}{130.0} \frac{91.8}{40} \frac{1.8}{26} \frac{5.5}{21} \frac{4.9}{16} \frac{4.6}{10} \quad 44 \quad \frac{4.8}{10} \frac{5.3}{14} \frac{80}{32} \frac{87}{40} \frac{6.9}{100} / 23.0$$

349

+

N.I.

-

E/CV.

898.56

879.22

47+00

93.3

T.P

0.69

892.63

878.29

662

891.94

872.60

+50

92.6

48+00

92.3

+50

92.1

49+00

92.2

+50

92.4

50+00

92.5

+50

92.3

T.P.

4.11

895.81

876.47

0.93

891.70

872.36

51+00

91.9

+19

+50

71.9

91.2

52+00

71.6

90.9

+50

71.0

90.3

T.P.

76

82

$$28.4/5.5 \quad \frac{26}{40} \quad \frac{46}{29} \quad \frac{53}{25} \quad \frac{65}{22} \quad \frac{58}{16} \quad \frac{55}{10} \quad 53 \quad \frac{57}{9} \quad \frac{62}{15} \quad \frac{101}{22} \quad \frac{125}{33} \quad \frac{131}{40} \quad \frac{125}{17.4/32.4}$$

$$28.0/5.0 \quad \frac{34}{40} \quad \frac{50}{30} \quad \frac{42}{23} \quad \frac{09}{17} \quad \frac{04}{11} \quad 20 \quad \frac{04}{9} \quad \frac{09}{15} \quad \frac{101}{30} \quad \frac{110}{40} \quad \frac{110}{11.0/42.0}$$

$$28.4/5.5 \quad \frac{39}{40} \quad \frac{54}{29} \quad \frac{51}{24} \quad \frac{13}{17} \quad \frac{10}{15} \quad \frac{07}{12} \quad 03 \quad \frac{06}{9} \quad \frac{12}{14} \quad \frac{112}{32} \quad \frac{124}{40} \quad \frac{128}{12.5/43.0}$$

$$30.4/6.7 \quad \frac{55}{40} \quad \frac{67}{28} \quad \frac{62}{26} \quad \frac{10}{16} \quad \frac{07}{11} \quad 05 \quad \frac{08}{10} \quad \frac{15}{15} \quad \frac{102}{29} \quad \frac{113}{34} \quad \frac{117}{40} \quad \frac{117}{17.2/40.4}$$

$$29.8/6.3 \quad \frac{51}{40} \quad \frac{63}{31} \quad \frac{59}{25} \quad \frac{19}{18} \quad \frac{11}{15} \quad \frac{08}{10} \quad 04 \quad \frac{08}{10} \quad \frac{13}{16} \quad \frac{94}{31} \quad \frac{104}{40} \quad \frac{104}{11.0/38.0}$$

$$27.8/5.1 \quad \frac{47}{40} \quad \frac{51}{29} \quad \frac{41}{23} \quad \frac{18}{18} \quad \frac{16}{17} \quad \frac{12}{15} \quad \frac{06}{10} \quad 02 \quad \frac{06}{10} \quad \frac{10}{15} \quad \frac{31}{20} \quad \frac{32}{22} \quad \frac{56}{29} \quad \frac{56}{40}$$

$$22.4/2.3 \quad \frac{30}{40} \quad \frac{28}{28} \quad \frac{08}{16} \quad \frac{05}{10} \quad 01 \quad \frac{08}{14} \quad \frac{24}{24} \quad \frac{44}{40} \quad \frac{24}{12.3/26}$$

$$27.4/5.0 \quad \frac{50}{40} \quad \frac{46}{24} \quad \frac{14}{15} \quad \frac{07}{9} \quad 03 \quad \frac{08}{10} \quad \frac{15}{20} \quad \frac{69}{28} \quad \frac{92}{40} \quad \frac{83}{11.0/34.0}$$

$$22.6/6.2 \quad \frac{65}{40} \quad \frac{63}{26} \quad \frac{60}{22} \quad \frac{53}{19} \quad \frac{46}{14} \quad \frac{42}{9} \quad 39 \quad \frac{43}{10} \quad \frac{45}{13} \quad \frac{48}{18} \quad \frac{52}{21} \quad \frac{50}{25} \quad \frac{61}{35} \quad \frac{78}{40} \quad \frac{80}{60.4/46.0}$$

$$\frac{00.0}{27}$$

$$\frac{40}{15} \quad \frac{48}{13} \quad \frac{47}{8} \quad 46 \quad \frac{49}{11} \quad \frac{53}{18} \quad \frac{27}{32} \quad \frac{26}{40} \quad \frac{26}{12.0/31.0}$$

$$\frac{00}{21} \quad \frac{49}{13} \quad \frac{51}{8} \quad 49 \quad \frac{51}{10} \quad \frac{55}{18} \quad \frac{28}{31} \quad \frac{27}{40} \quad \frac{28}{02} \quad \frac{28}{31.2}$$

$$\frac{15}{22} \quad \frac{57}{15} \quad \frac{58}{12} \quad \frac{56}{8} \quad 55 \quad \frac{58}{10} \quad \frac{61}{15} \quad \frac{53}{23} \quad \frac{33}{31} \quad \frac{31}{40} \quad \frac{33}{12.2/31.4}$$

219	+	41. 895.81 876.47	-	15/60	
53+00				69.9	89.2
+50				68.9	88.2
B.M.	0.03	888.19 868.85	7.65	888.16 868.82	
54+00				67.5	86.8
T.P.					
+50				66.1	85.4
55+00				64.8	84.1
+50				63.5	82.8
56+00				62.2	81.5
B.M.	13.42	901.58 882.24	0.03	888.16 868.82	
51+50				71.9	91.2
T.P.	13.68	914.98 895.64	0.28	901.30 881.96	
52+00				71.6	90.9
+50				71.0	90.3
53+00				69.9	89.2
T.P.	1.89	916.49 897.15	0.38	914.60 895.26	
+50				68.9	88.2

26.3

$$\begin{array}{cccccccccccc} 2.3 & 46 & 66 & 68 & 66 & 6.8 & 72 & 6.8 & 44 & 4.8 & 4.4 & \\ 21 & 18 & 15 & 8 & & 11 & 16 & 20 & 29 & 40 & 0.22 & /31.4 \end{array}$$

$$\begin{array}{cccccccccccc} 35 & 5.9 & 76 & 81 & 79 & 70 & 80 & 82 & 5.8 & 70 & 60 & \\ 20 & 17 & 15 & 11 & 8 & & 12 & 18 & 26 & 40 & 0.16 & /30.2 \end{array}$$

$$\begin{array}{cccccccccccc} 16 & 15 & 15 & & 29 & 18 & 22 & 24 & 00 & 26 & 29 & 63 & 17 \\ 17 & 13 & 18 & 14 & & 11 & 15 & 20 & 22 & 28 & 31 & 40 & 0.12/26 \\ & & & \uparrow & & & & & & & & & \\ & & & 8 & & & & & & & & & \end{array}$$

$$\begin{array}{cccccccccccc} 10 & 29 & 29 & 28 & 34 & 38 & 47 & 137 & 232 & 266 & 60 & \\ 22 & 17 & 8 & & 11 & 19 & 22 & 43 & 63 & 70 & 132 & /244 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{C6.1} & 34.1/4.11 & +18 & 10 & 45 & 43 & 4.1 & 46 & 52 & 59 & 134 & 238 & 264 & 241 \\ 39.2 & C5.2 & 40 & 23 & 18 & 9 & & 10 & 19 & 20 & 31 & 54 & 70 & F20.58 \end{array}$$

$$\begin{array}{cccccccccccc} 2.4/52 & 33 & 52 & 59 & 58 & 56 & 54 & 60 & 64 & 133 & 232 & 256 & 256 \\ C0.2 & 40 & 28 & 24 & 15 & 10 & & 11 & 15 & 26 & 44 & 59 & F20.2/58.4 \end{array}$$

82

$$\begin{array}{cccccccccccc} 250/27 & 73 & 73 & 77 & 73 & 68 & 67 & 72 & 80 & 137 & 200 & 242 & 237 \\ D605 & 40 & 27 & 23 & 20 & 10 & & 9 & 16 & 25 & 33 & 54 & F170/52.0 \end{array}$$

$$\begin{array}{cccccccc} \textcircled{C4.2} & 32.6/61 & 67 & 61 & 54 & 10.4 \\ 35.4 & C4.2 & 50 & 36 & 19 \end{array}$$

$$\begin{array}{cccccccc} \textcircled{C11.4} & 44.5/11.7 & 12.2 & 11.4 & 103 & 24.1 \\ 49.8 & C12.1 & 50 & 39 & 25 \end{array}$$

$$\begin{array}{cccccccc} \textcircled{C17.4} & 55.7/50 & 68 & 56 & 43 & 24.7 \\ 61.8 & 196 & 60 & 50 & 38 \end{array}$$

$$\begin{array}{cccccccc} \textcircled{C22.2} & 61.7/21 & 19 & 09 & 00 & 25.8 \\ 71.4 & C23.6 & 60 & 50 & 70 \end{array}$$

$$\begin{array}{cccccccc} \textcircled{C23.0} & 62.4/44 & 40 & 35 & 38 & 28.3 \\ 73.0 & 23.9 & 60 & 50 & 37 \end{array}$$

54	+	H.I. 916.49 897.15	-	Elev	
54+00				6.25	86.8
T.P.	0.08	903.55 884.21	12.02	903.47 884.13	
+50				66.1	85.4
T.P.	1.81	895.67 876.33	7.67	893.86 874.52	
B.M.	0.22	888.36 869.04	7.53	888.14 868.80	= 868.82
B.M.	4.63	880.94 861.62	12.05	876.31 856.99	
56+18					880.9
+37					80.3
+60					79.7
	5.37	881.48 862.36	4.63	876.31 856.99	
57+00					78.8
+50					77.6
B.M.	2.72	879.03 859.71	5.37	876.31 856.99	
58+00					76.7
+50					75.9
59+00					75.4
+50					75.0
B.M.	4.71	879.38 860.06	4.36	874.67 855.35	

$$\begin{array}{r} 25.1 \\ 77.2 \\ \hline 6.45 \end{array} \quad \begin{array}{r} 42 \\ 62.5 \end{array} \quad \begin{array}{r} 40 \\ 70 \end{array} \quad \begin{array}{r} 45 \\ 60 \end{array} \quad \begin{array}{r} 56 \\ 50 \end{array} \quad \begin{array}{r} 86 \\ 36 \end{array} \quad (29.7)$$

$$\begin{array}{r} 17.9 \\ 62.8 \end{array} \quad \begin{array}{r} 48.5 \\ 61.48 \end{array} \quad \begin{array}{r} 35 \\ 60 \end{array} \quad \begin{array}{r} 26 \\ 50 \end{array} \quad \begin{array}{r} 63 \\ 38 \end{array} \quad \begin{array}{r} 74 \\ 34 \end{array} \quad (18.1)$$

spike in PP 14' Rt Sta 57+76

$$\begin{array}{r} +12 \\ 50 \end{array} \quad \begin{array}{r} +06 \\ 45 \end{array} \quad \begin{array}{r} +04 \\ 35 \end{array} \quad \begin{array}{r} +03 \\ 18 \end{array} \quad \begin{array}{r} 00 \\ 9 \end{array} \quad 00 \quad \begin{array}{r} 05 \\ 9 \end{array} \quad \begin{array}{r} 11 \\ 15 \end{array} \quad \begin{array}{r} 15.5 \\ 39 \end{array} \quad \begin{array}{r} 16.7 \\ 50 \end{array}$$

$$\begin{array}{r} +20 \\ 50 \end{array} \quad \begin{array}{r} 00 \\ 25 \end{array} \quad \begin{array}{r} 06 \\ 10 \end{array} \quad 06 \quad \begin{array}{r} 11 \\ 9 \end{array} \quad \begin{array}{r} 13 \\ 11 \end{array} \quad \begin{array}{r} 20 \\ 16 \end{array} \quad \begin{array}{r} 15.1 \\ 37 \end{array} \quad \begin{array}{r} 16.6 \\ 42 \end{array} \quad \begin{array}{r} 17.1 \\ 50 \end{array}$$

$$\frac{18.0}{168} / 51.6$$

$$\begin{array}{r} 05 \\ 40 \end{array} \quad \begin{array}{r} 12 \\ 34 \end{array} \quad \begin{array}{r} 09 \\ 30 \end{array} \quad \begin{array}{r} 12 \\ 16 \end{array} \quad \begin{array}{r} 12 \\ 10 \end{array} \quad 12 \quad \begin{array}{r} 18 \\ 9 \end{array} \quad \begin{array}{r} 20 \\ 11 \end{array} \quad \begin{array}{r} 30 \\ 17 \end{array} \quad \begin{array}{r} 43 \\ 32 \end{array} \quad \begin{array}{r} 13.5 \\ 38 \end{array} \quad \begin{array}{r} 16.3 \\ 42 \end{array} \quad \begin{array}{r} 18.1 \\ 52 \end{array} \quad \begin{array}{r} 18.3 \\ 60 \end{array}$$

$$\begin{array}{r} 792.9 \\ 600 \end{array} \quad \begin{array}{r} 12 \\ 40 \end{array} \quad \begin{array}{r} 31 \\ 30 \end{array} \quad \begin{array}{r} 27 \\ 26 \end{array} \quad \begin{array}{r} 33 \\ 21 \end{array} \quad \begin{array}{r} 35 \\ 20 \end{array} \quad \begin{array}{r} 33 \\ 11 \end{array} \quad 2.9 \quad \begin{array}{r} 33 \\ 8 \end{array} \quad \begin{array}{r} 35 \\ 10 \end{array} \quad \begin{array}{r} 46 \\ 18 \end{array} \quad \begin{array}{r} 13.7 \\ 33 \end{array} \quad \begin{array}{r} 17.2 \\ 39 \end{array} \quad \begin{array}{r} 18.9 \\ 50 \end{array} \quad \begin{array}{r} 19.3 \\ 60 \end{array} \quad \begin{array}{r} 19.9 \\ F160 \end{array}$$

56

$$\begin{array}{r} 25.8 \\ 1000.9 \end{array} \quad \begin{array}{r} 4.7 \\ 40 \end{array} \quad \begin{array}{r} 2.8 \\ 30 \end{array} \quad \begin{array}{r} 4.8 \\ 35 \end{array} \quad \begin{array}{r} 5.0 \\ 28 \end{array} \quad \begin{array}{r} 4.7 \\ 26 \end{array} \quad \begin{array}{r} 4.8 \\ 20 \end{array} \quad \begin{array}{r} 4.3 \\ 11 \end{array} \quad 4.1 \quad \begin{array}{r} 4.7 \\ 8 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 13.6 \\ 26 \end{array} \quad \begin{array}{r} 17.0 \\ 31 \end{array} \quad \begin{array}{r} 18.7 \\ 42 \end{array} \quad \begin{array}{r} 19.4 \\ 60 \end{array} \quad \begin{array}{r} 19.0 \\ F160 \end{array}$$

3.8

$$\begin{array}{r} 24.0 \\ 1000 \end{array} \quad \begin{array}{r} 3.8 \\ 40 \end{array} \quad \begin{array}{r} 3.0 \\ 35 \end{array} \quad \begin{array}{r} 4.4 \\ 26 \end{array} \quad \begin{array}{r} 4.1 \\ 21 \end{array} \quad \begin{array}{r} 2.9 \\ 17 \end{array} \quad \begin{array}{r} 2.8 \\ 11 \end{array} \quad 2.3 \quad \begin{array}{r} 2.8 \\ 8 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad \begin{array}{r} 13.0 \\ 27 \end{array} \quad \begin{array}{r} 14.4 \\ 31 \end{array} \quad \begin{array}{r} 16.1 \\ 50 \end{array} \quad \begin{array}{r} 15.9 \\ F136 \end{array} / 47.2$$

3:1 Slope F. 11

$$\begin{array}{r} 25.8 \\ 1226 \end{array} \quad \begin{array}{r} 5.7 \\ 40 \end{array} \quad \begin{array}{r} 6.0 \\ 25 \end{array} \quad \begin{array}{r} 5.6 \\ 21 \end{array} \quad \begin{array}{r} 4.1 \\ 18 \end{array} \quad \begin{array}{r} 3.5 \\ 11 \end{array} \quad \begin{array}{r} 3.3 \\ 11 \end{array} \quad 3.1 \quad \begin{array}{r} 3.6 \\ 8 \end{array} \quad \begin{array}{r} 4.3 \\ 13 \end{array} \quad \begin{array}{r} 13.6 \\ 28 \end{array} \quad \begin{array}{r} 14.8 \\ 36 \end{array} \quad \begin{array}{r} 15.7 \\ 50 \end{array} \quad \begin{array}{r} 15.2 \\ F126 \end{array} / 45.2$$

$$\begin{array}{r} 28.5 \\ 1735 \end{array} \quad \begin{array}{r} 6.9 \\ 40 \end{array} \quad \begin{array}{r} 6.6 \\ 24 \end{array} \quad \begin{array}{r} 4.0 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 11 \end{array} \quad 3.6 \quad \begin{array}{r} 4.2 \\ 8 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 13.0 \\ 25 \end{array} \quad \begin{array}{r} 14.5 \\ 34 \end{array} \quad \begin{array}{r} 15.3 \\ 50 \end{array} \quad \begin{array}{r} 15.0 \\ F11.4 \end{array} / 40.8$$

$$\begin{array}{r} 17.4 \\ 103.2 \end{array} \quad \begin{array}{r} 7.2 \\ 40 \end{array} \quad \begin{array}{r} 7.4 \\ 35 \end{array} \quad \begin{array}{r} 7.1 \\ 25 \end{array} \quad \begin{array}{r} 5.1 \\ 20 \end{array} \quad \begin{array}{r} 4.5 \\ 17 \end{array} \quad \begin{array}{r} 4.2 \\ 11 \end{array} \quad 4.0 \quad \begin{array}{r} 4.4 \\ 7 \end{array} \quad \begin{array}{r} 5.1 \\ 14 \end{array} \quad \begin{array}{r} 12.5 \\ 25 \end{array} \quad \begin{array}{r} 13.8 \\ 34 \end{array} \quad \begin{array}{r} 15.1 \\ 40 \end{array} \quad \begin{array}{r} 14.2 \\ F10.2 \end{array} / 38.4$$

spike in PP 18' Rt Sta 62+01

Sta

+

H.I.

-

Elev

879.38
860.06

60+00

74.7

+50

B.M.

4.16

878.83
859.51

4.71

874.67
855.31

74.7

60+82.75 P.C.

74.8

61+00

74.8

+50

74.6

+95.75 P.T.

74.5

62+52.75 P.C.

74.4

63+00

74.2

+50

64+00

+50

65+00

+18.75 P.T.

3:1

$$\begin{array}{r} 4.7 \\ 7.3 \\ 2.6 \end{array} \begin{array}{r} 5.5 \\ 4.0 \\ 1.5 \end{array} \begin{array}{r} 7.0 \\ 3.2 \\ 3.8 \end{array} \begin{array}{r} 7.3 \\ 2.6 \\ 4.7 \end{array} \begin{array}{r} 6.1 \\ 2.2 \\ 3.9 \end{array} \begin{array}{r} 5.6 \\ 1.9 \\ 3.7 \end{array} \begin{array}{r} 5.2 \\ 1.6 \\ 3.6 \end{array} \begin{array}{r} 4.9 \\ 1.2 \\ 3.7 \end{array} \begin{array}{r} 4.7 \\ 7.0 \\ 2.3 \end{array} \begin{array}{r} 5.0 \\ 1.2 \\ 3.8 \end{array} \begin{array}{r} 5.7 \\ 1.2 \\ 4.5 \end{array} \begin{array}{r} 13.3 \\ 2.7 \\ 10.6 \end{array} \begin{array}{r} 15.1 \\ 5.0 \\ 10.1 \end{array} \begin{array}{r} 14.1 \\ 9.4 \\ 4.7 \end{array} \begin{array}{r} 36.8 \\ 27.4 \\ 9.4 \end{array}$$

$$\begin{array}{r} 0.7 \\ 4.7 \\ 4.0 \end{array} \begin{array}{r} 1.7 \\ 4.0 \\ 2.3 \end{array} \begin{array}{r} 4.1 \\ 3.0 \\ 1.1 \end{array} \begin{array}{r} 6.6 \\ 3.8 \\ 2.8 \end{array} \begin{array}{r} 6.0 \\ 2.2 \\ 3.8 \end{array} \begin{array}{r} 5.6 \\ 1.8 \\ 3.8 \end{array} \begin{array}{r} 5.2 \\ 1.5 \\ 3.7 \end{array} \begin{array}{r} 4.9 \\ 1.2 \\ 3.7 \end{array} \begin{array}{r} 4.7 \\ 7.0 \\ 2.3 \end{array} \begin{array}{r} 5.1 \\ 1.2 \\ 3.9 \end{array} \begin{array}{r} 5.8 \\ 1.3 \\ 4.5 \end{array} \begin{array}{r} 10.4 \\ 2.3 \\ 8.1 \end{array} \begin{array}{r} 12.2 \\ 3.4 \\ 8.8 \end{array} \begin{array}{r} 13.0 \\ 5.0 \\ 8.0 \end{array} \begin{array}{r} 12.2 \\ 7.5 \\ 4.7 \end{array} \begin{array}{r} 33.0 \\ 27.5 \\ 5.5 \end{array}$$

$$\begin{array}{r} C5.3 \\ +1.3 \\ 37.6 \end{array} \begin{array}{r} 2.54 \\ +1.4 \\ 34.4 \end{array} \begin{array}{r} 0.2 \\ 2.8 \end{array} \begin{array}{r} 4.5 \\ 2.4 \end{array} \begin{array}{r} 5.1 \\ 2.1 \end{array} \begin{array}{r} 5.1 \\ 1.8 \end{array} \begin{array}{r} 4.5 \\ 1.5 \end{array} \begin{array}{r} 4.2 \\ 1.1 \end{array} \begin{array}{r} 4.0 \\ 1.0 \end{array} \begin{array}{r} 4.6 \\ 1.0 \end{array} \begin{array}{r} 5.0 \\ 1.4 \end{array} \begin{array}{r} 8.2 \\ 2.3 \end{array} \begin{array}{r} 8.8 \\ 2.7 \end{array} \begin{array}{r} 9.6 \\ 4.0 \end{array}$$

$$\begin{array}{r} 0.7.0 \\ +3.0 \\ 4.1 \end{array} \begin{array}{r} 2.6.2 \\ +2.2 \\ 35.6 \end{array} \begin{array}{r} 1.1 \\ 3.0 \end{array} \begin{array}{r} 5.1 \\ 2.0 \end{array} \begin{array}{r} 5.1 \\ 1.9 \end{array} \begin{array}{r} 4.6 \\ 1.5 \end{array} \begin{array}{r} 4.3 \\ 1.1 \end{array} \begin{array}{r} 4.0 \\ 1.0 \end{array} \begin{array}{r} 4.7 \\ 1.2 \end{array} \begin{array}{r} 5.3 \\ 1.7 \end{array} \begin{array}{r} 6.8 \\ 2.3 \end{array} \begin{array}{r} 8.3 \\ 4.0 \end{array}$$

$$\begin{array}{r} C10.0 \\ +5.8 \\ 4.7 \end{array} \begin{array}{r} 2.91 \\ +4.9 \\ 4.0 \end{array} \begin{array}{r} 1.3 \\ 2.9 \end{array} \begin{array}{r} 3.3 \\ 2.3 \end{array} \begin{array}{r} 4.3 \\ 2.0 \end{array} \begin{array}{r} 4.4 \\ 1.3 \end{array} \begin{array}{r} 4.2 \\ 1.2 \end{array} \begin{array}{r} 4.6 \\ 1.0 \end{array} \begin{array}{r} 4.9 \\ 1.7 \end{array} \begin{array}{r} 5.3 \\ 2.1 \end{array} \begin{array}{r} 5.2 \\ 2.5 \end{array} \begin{array}{r} 6.5 \\ 4.0 \end{array}$$

$$\begin{array}{r} C17.7 \\ +13.4 \\ 62.4 \end{array} \begin{array}{r} 2.129 \\ +8.6 \\ 47.1 \end{array} \begin{array}{r} 1.2 \\ 3.4 \end{array} \begin{array}{r} 5.0 \\ 2.0 \end{array} \begin{array}{r} 5.2 \\ 1.7 \end{array} \begin{array}{r} 4.6 \\ 1.0 \end{array} \begin{array}{r} 4.3 \\ 1.3 \end{array} \begin{array}{r} 4.7 \\ 1.2 \end{array} \begin{array}{r} 5.0 \\ 1.5 \end{array} \begin{array}{r} 5.2 \\ 1.8 \end{array} \begin{array}{r} 5.6 \\ 2.4 \end{array} \begin{array}{r} 5.4 \\ 2.8 \end{array} \begin{array}{r} 7.2 \\ 4.0 \end{array}$$

$$\begin{array}{r} C25.6 \\ +21.2 \\ 78.2 \end{array} \begin{array}{r} 2.19.2 \\ +14.8 \\ 55.1 \end{array} \begin{array}{r} 1.1.9 \\ 4.3 \end{array} \begin{array}{r} 4.6 \\ 2.3 \end{array} \begin{array}{r} 5.2 \\ 2.1 \end{array} \begin{array}{r} 5.4 \\ 1.8 \end{array} \begin{array}{r} 4.6 \\ 1.1 \end{array} \begin{array}{r} 4.4 \\ 1.0 \end{array} \begin{array}{r} 4.9 \\ 1.2 \end{array} \begin{array}{r} 5.1 \\ 1.5 \end{array} \begin{array}{r} 5.9 \\ 2.4 \end{array} \begin{array}{r} 8.9 \\ 3.2 \end{array} \begin{array}{r} 12.5 \\ 4.4 \end{array}$$

$$\begin{array}{r} C28.5 \\ +23.9 \\ 84 \end{array} \begin{array}{r} 2.24.3 \\ +19.7 \\ 62.7 \end{array} \begin{array}{r} 1.1.6 \\ 5.1 \end{array} \begin{array}{r} 4.6 \\ 2.2 \end{array} \begin{array}{r} 5.2 \\ 2.1 \end{array} \begin{array}{r} 5.4 \\ 1.8 \end{array} \begin{array}{r} 5.0 \\ 1.0 \end{array} \begin{array}{r} 5.0 \\ 1.0 \end{array} \begin{array}{r} 4.6 \\ 1.2 \end{array} \begin{array}{r} 5.1 \\ 1.5 \end{array} \begin{array}{r} 5.4 \\ 1.6 \end{array} \begin{array}{r} 6.5 \\ 2.6 \end{array} \begin{array}{r} 11.5 \\ 4.0 \end{array} \begin{array}{r} 13.1 \\ 5.0 \end{array}$$

$$\begin{array}{r} C28.4 \\ +23.5 \\ 83.8 \end{array} \begin{array}{r} 2.28.1 \\ +20.2 \\ 64 \end{array} \begin{array}{r} 1.1.8 \\ 5.1 \end{array} \begin{array}{r} 1.1.3 \\ 5.5 \end{array} \begin{array}{r} 5.5 \\ 2.4 \end{array} \begin{array}{r} 6.3 \\ 2.1 \end{array} \begin{array}{r} 5.4 \\ 1.6 \end{array} \begin{array}{r} 5.3 \\ 1.1 \end{array} \begin{array}{r} 4.9 \\ 1.2 \end{array} \begin{array}{r} 5.6 \\ 1.1 \end{array} \begin{array}{r} 5.9 \\ 1.7 \end{array} \begin{array}{r} 6.8 \\ 2.7 \end{array} \begin{array}{r} 9.5 \\ 3.6 \end{array} \begin{array}{r} 12.7 \\ 5.0 \end{array}$$

$$\begin{array}{r} C19.7 \\ +14.4 \\ 46.4 \end{array} \begin{array}{r} 2.20.5 \\ +15.5 \\ 56.7 \end{array} \begin{array}{r} 1.1.4 \\ 5.1 \end{array} \begin{array}{r} 6.2 \\ 2.2 \end{array} \begin{array}{r} 7.2 \\ 2.3 \end{array} \begin{array}{r} 6.1 \\ 1.6 \end{array} \begin{array}{r} 5.6 \\ 1.1 \end{array} \begin{array}{r} 5.3 \\ 1.2 \end{array} \begin{array}{r} 6.0 \\ 1.2 \end{array} \begin{array}{r} 6.1 \\ 1.5 \end{array} \begin{array}{r} 6.9 \\ 3.0 \end{array} \begin{array}{r} 9.4 \\ 3.7 \end{array} \begin{array}{r} 9.7 \\ 4.5 \end{array}$$

$$\begin{array}{r} +24 \\ 44 \end{array} \begin{array}{r} 6.6 \\ 2.9 \end{array} \begin{array}{r} 7.4 \\ 2.4 \end{array} \begin{array}{r} 6.5 \\ 1.7 \end{array} \begin{array}{r} 6.0 \\ 1.2 \end{array} \begin{array}{r} 5.6 \\ 1.2 \end{array} \begin{array}{r} 6.3 \\ 1.2 \end{array} \begin{array}{r} 6.0 \\ 1.2 \end{array} \begin{array}{r} 6.4 \\ 1.2 \end{array} \begin{array}{r} 6.9 \\ 1.2 \end{array} \begin{array}{r} 8.6 \\ 3.1 \end{array} \begin{array}{r} 11.1 \\ 4.5 \end{array}$$

$$\begin{array}{r} 9.6 \\ 40 \end{array} \begin{array}{r} 8.0 \\ 2.9 \end{array} \begin{array}{r} 7.7 \\ 2.1 \end{array} \begin{array}{r} 6.7 \\ 1.6 \end{array} \begin{array}{r} 6.3 \\ 1.0 \end{array} \begin{array}{r} 6.0 \\ 1.0 \end{array} \begin{array}{r} 6.4 \\ 1.0 \end{array} \begin{array}{r} 6.9 \\ 1.6 \end{array} \begin{array}{r} 8.6 \\ 2.5 \end{array} \begin{array}{r} 11.1 \\ 4.5 \end{array}$$

$$\begin{array}{r} 11.4 \\ 36.6 \end{array} \begin{array}{r} 8.3 \\ 2.1 \end{array} \begin{array}{r} 6.8 \\ 1.5 \end{array} \begin{array}{r} 6.2 \\ 1.2 \end{array} \begin{array}{r} 7.0 \\ 1.3 \end{array} \begin{array}{r} 7.5 \\ 1.8 \end{array} \begin{array}{r} 8.5 \\ 2.5 \end{array} \begin{array}{r} 11.4 \\ 4.5 \end{array}$$

Sta.	+	H.I.	-	Elev.
BM	5.99	916.46 912.46		910.47 906.47
2+00				
+50				
+74				07.9
3+00				
+39				
+56				08.2 ✓
4+00				08.1 ✓
+12				08.0 ✓
+50				07.9 ✓
+64				07.8 ✓
T.P.	3.18	914.78 910.78	4.86	911.60 907.60
5+00				07.5
+18				07.3

spike in PP18'ht 5/4 0+50

$$5.2 \quad \frac{2.7}{0.2.5} / 40.0$$

$$4.8 \quad \frac{0.4}{0.4.4} / 47.6$$

$$4.6 \quad \frac{+0.5}{0.5.1} / 50.4$$

$$4.5 \quad \frac{2.5}{0.2.0} / 38.0$$

$$4.4 \quad \frac{1.7}{0.2.7} / 40.8$$

$$4.3$$

$$4.4$$

$$4.5$$

$$4.6$$

$$4.7$$

$$3.3$$

$$3.5$$

Sta + H.I. - Elev.

914.78
910.28

+50

06.8

6+00

060

+34

T.P.

12.49

927.22
923.22

005

914.73
910.73

+3+56

082

4+00

08.1

+18

08.0

+50

07.9

+64

07.8

5+00

07.5

+18

07.3

+50

06.8

6+00

T.P.

2.91

918.22
914.78

11.41

060
915.81
911.81
910.50
906.50

B.M.

8.22

91073
1249
923.22

4.0

4.8

5.5

$\frac{4.0}{0.15}/36.0$

(15.0)

$\frac{7.5}{7.5}/60.0$

(15.1)

$\frac{7.1}{8.0}/62.0$

(15.2)

$\frac{7.4}{0.78}/61.2$

(15.3) ✓

(15.4)

$\frac{3.2}{12.2}/78.8$

(15.7)

$\frac{5.6}{10.1}/70.4$

(15.9)

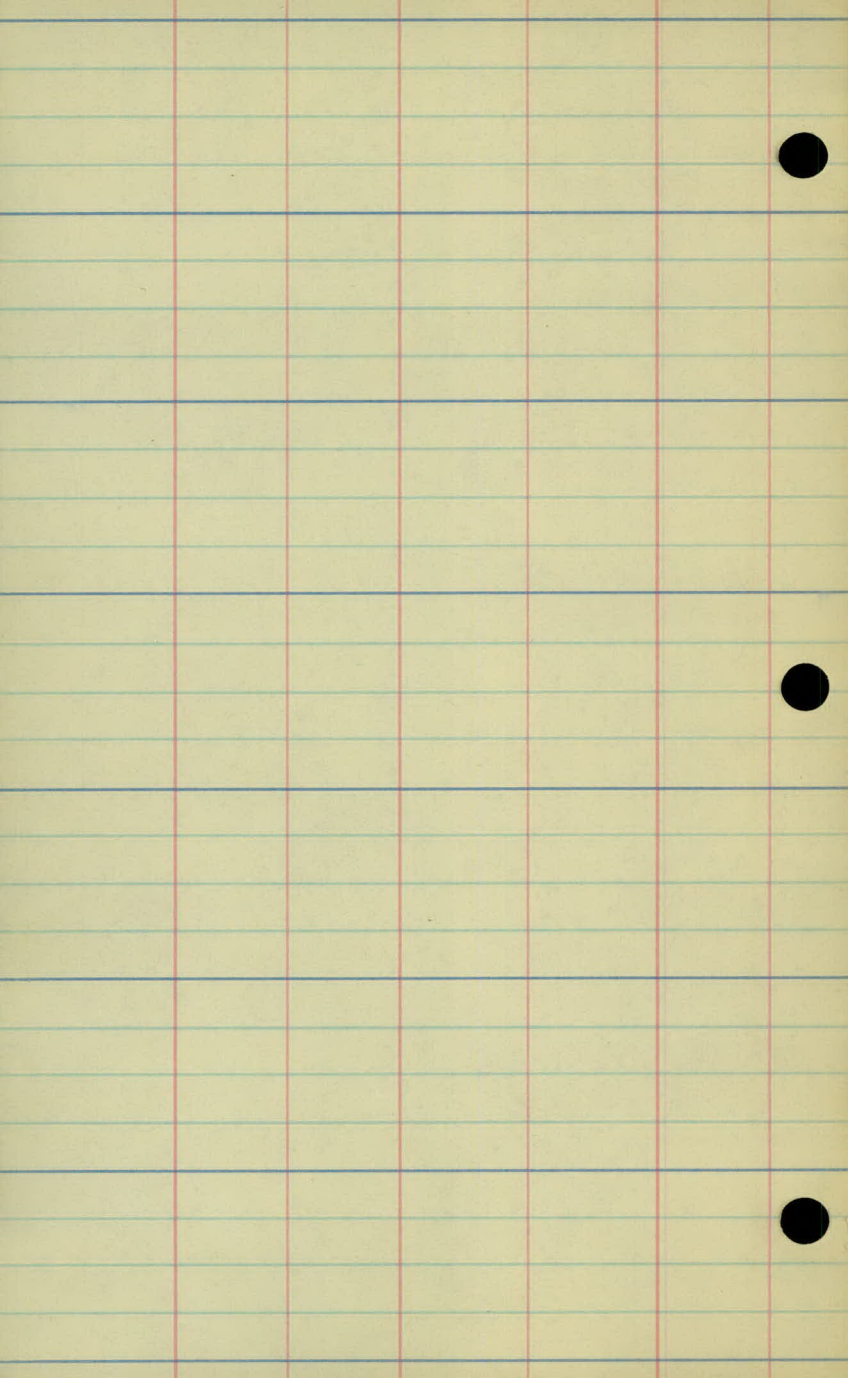
$\frac{6.6}{0.93}/62.2$

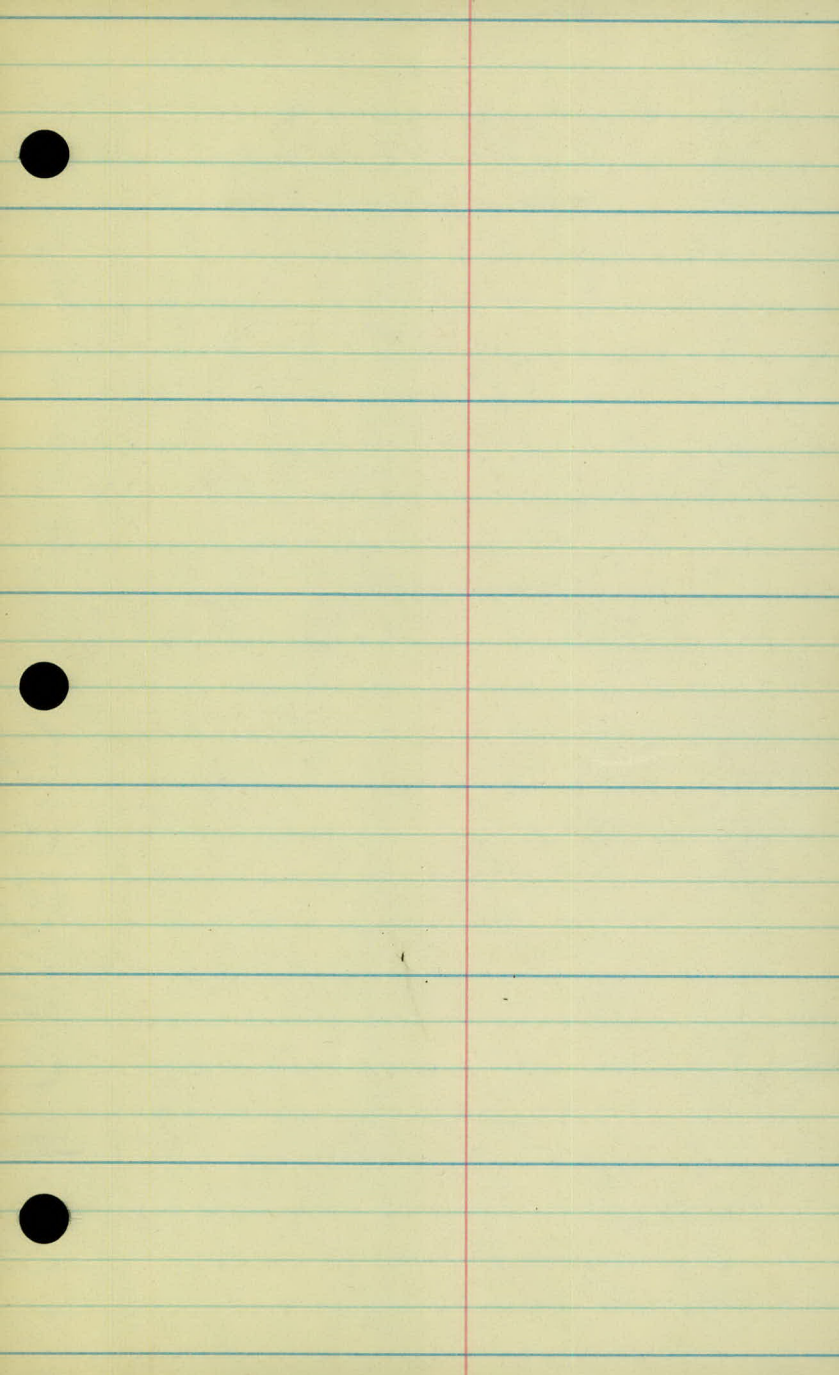
(16.4)

$\frac{5.8}{0.106}/72.4$

(17.2)

$\frac{10.0}{0.72}/58.4$





Sta.	+	H.I.	-	Elev.
B.M.				910.47 906.47

0+26

0+50

1+00

1+25

3/21/34

Spoke in PP 18' Lt Sta. 0+50

3:1

F25.2

95.6

3:1

F26.2

98.6

F23.2

89.6

4:1

F23.8

115.2

4:1

F26.9

127.6

F30.5

142.0

F26.6

126.4

Check Levels

B.M.	12.43	900.95		888.52
	13.34	913.96	0.33	900.62
B.M.			3.50	910.46
	3.27	915.16	2.07	911.89
	0.27	904.68	10.75	904.41
			7.60	897.08
B.M.			2.33	902.35
			1.76	902.92
	0.38	891.92	13.14	891.54
	0.69	879.04	13.57	878.35
	8.12	873.97	13.19	865.85
B.M.			11.50	862.47
	12.49	885.85	0.61	873.36
B.M.	0.09	884.70	1.24	884.61
	9.64	893.75	0.59	884.11
B.M.			4.23	889.52
	9.82	903.41	0.16	893.59
	5.40	904.29	4.52	898.89
B.M.	1.36	897.80	7.85	896.44
	4.62	896.30	6.12	891.68
B.M.	0.16	888.32	8.14	888.16
B.M.	3.08	879.43	11.97	876.35
B.M.	0.01	874.71	4.73	874.70
B.M.			10.43	864.28

● Spike in P.P. N.W. Cor. Payne Av. Conn & Arcade.

✓ ✓ ✓ 18' L. Sta. 0+50

✓ ✓ ✓ 18' R. Sta. 9+80

✓ ✓ ✓ S.W. Cor. Frost & Arcade.

✓ ✓ ✓ 18' R. Sta. 19+95

✓ ✓ ✓ 18' R. Sta. 28+95

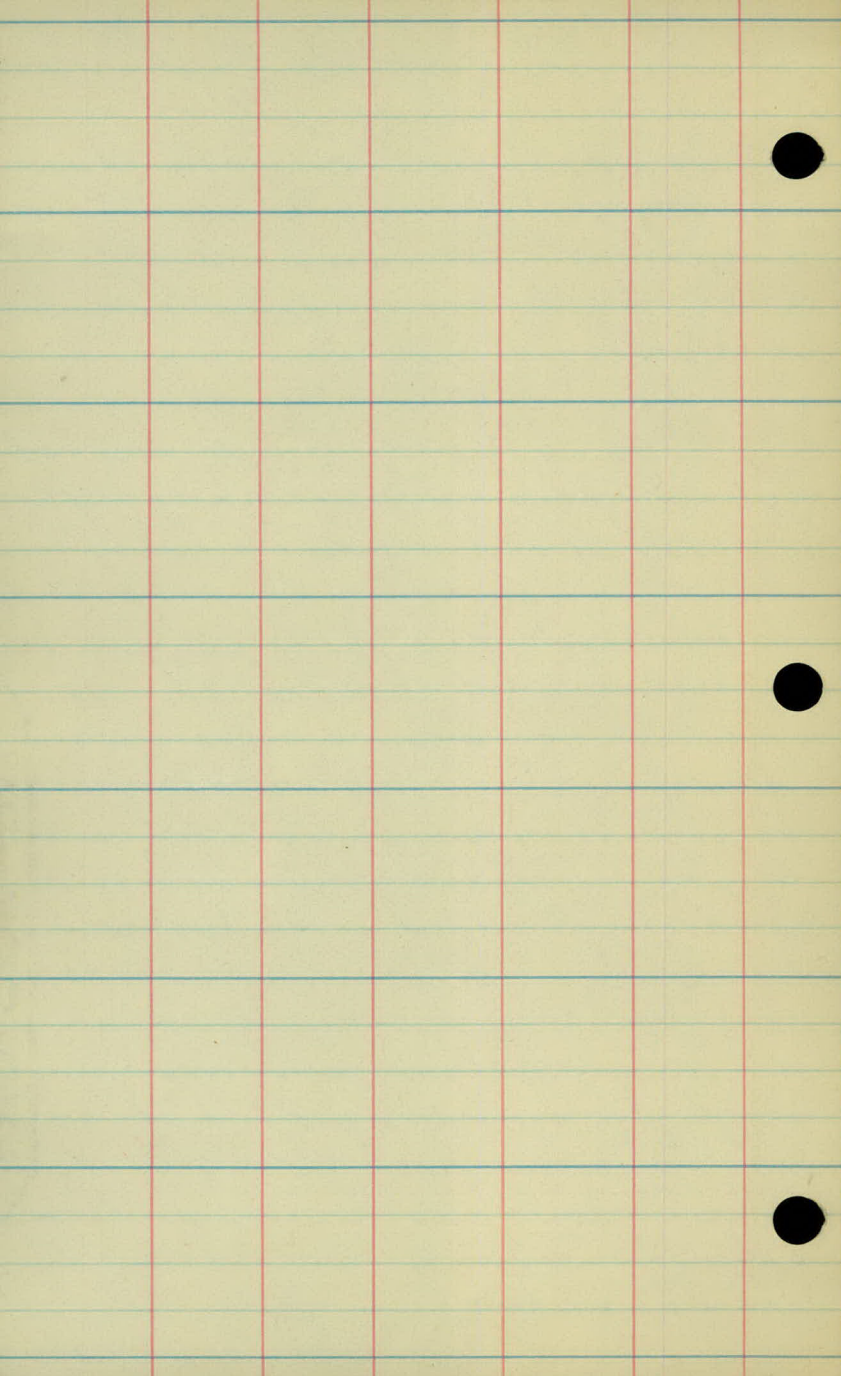
✓ ✓ ✓ 19' R. Sta. 36+02

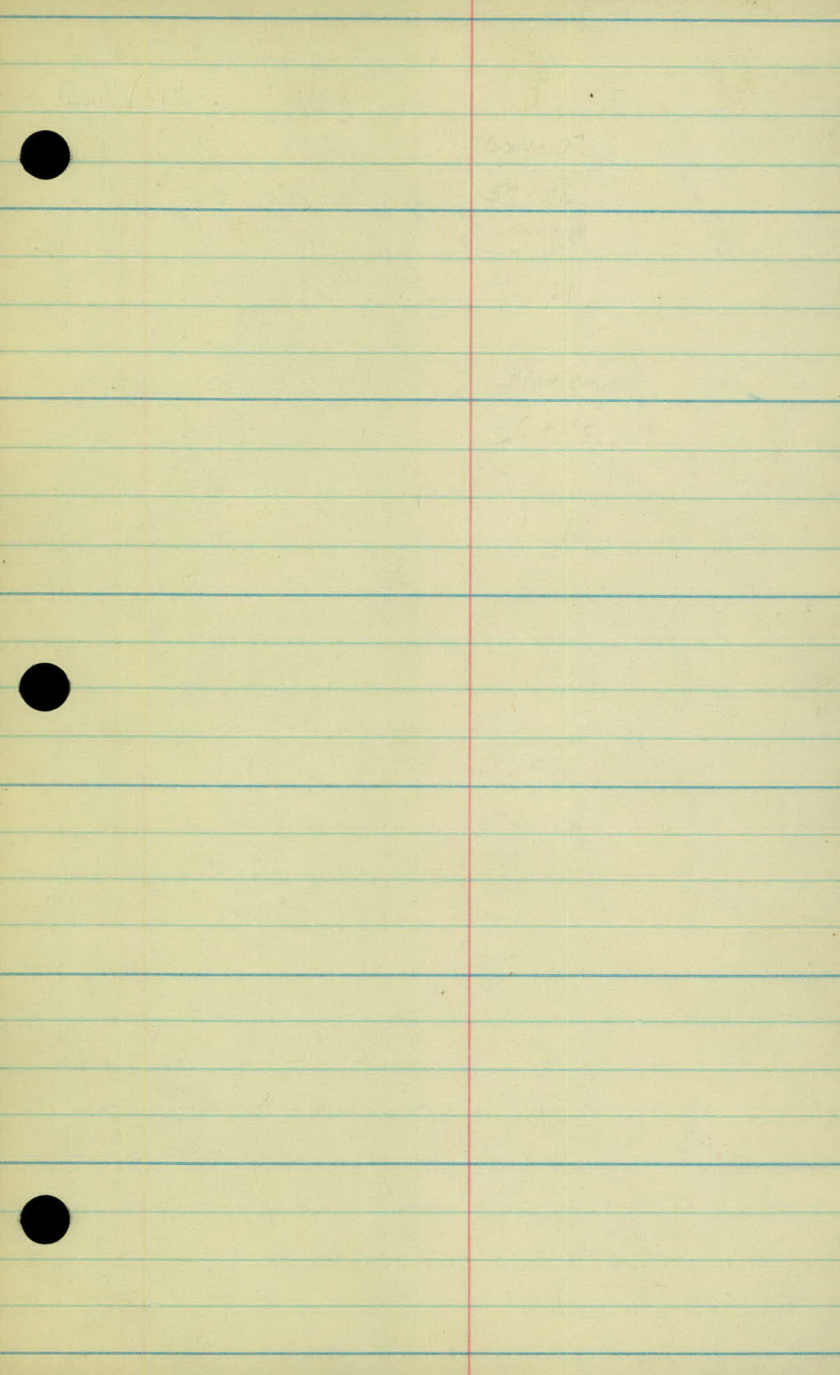
✓ ✓ G.P. 19' L. Sta. 45+29

✓ ✓ P.P. 18' R. Sta. 53+58

✓ ✓ P.P. 14' R. Sta. 57+76

✓ ✓ P.P. 18' R. Sta. 62+07





Sta.	+	H.I.	-	Elev.
B.M.	1.04	903.38 ✓		902.34
	0.25	889.87 ⁸⁷	13.76	889.62 ✓
	0.34	878.77	10.94	878.43
		878.27		878.93
15+00				78.9
+ 50				76.5
16+00				74.1
+ 50				71.5
	6.91	869.30 ✓		862.39
17+00				69.5
+ 50				67.8
18+00				66.2
+ 50				65.1
19+00				64.5
+ 50				63.4
20+00				63.1

Spike in P.P. 18' Rt Sta. 9+80

$\frac{4.4}{40} \frac{4.2}{38} \frac{5.5}{26} \frac{4.2}{24} \frac{4.2}{19} \frac{1.1}{14} \frac{0.6}{9} 0.4 \frac{0.7}{9} \frac{0.8}{11} \frac{5.0}{20} \frac{5.3}{39}$

$\frac{10.4}{40} \frac{9.8}{30} \frac{10.7}{27} \frac{9.8}{26} \frac{9.7}{22} \frac{3.4}{14} \frac{2.9}{9} 2.8 \frac{2.8}{8} \frac{3.2}{12} \frac{8.8}{21} \frac{9.6}{46}$

$\frac{14.1}{40} \frac{13.6}{27} \frac{12.7}{23} \frac{5.7}{13} \frac{5.3}{9} 5.2 \frac{5.3}{9} \frac{6.7}{11} \frac{11.0}{20} \frac{13.0}{27} \frac{14.3}{38}$

$\frac{15.7}{40} \frac{15.5}{28} \frac{7.9}{14} \frac{7.4}{10} 7.5 \frac{7.4}{8} \frac{7.9}{13} \frac{15.4}{25} \frac{18.0}{40}$

Spike in P.P. 18' Rt Sta. 19+95

$\rightarrow \frac{8.0}{40} \frac{7.3}{28} \frac{6.2}{24} \frac{0.5}{15} \frac{0.0}{11} +0.2 \frac{0.0}{9} \frac{1.0}{13} \frac{6.9}{23} \frac{9.2}{32} \frac{10.2}{41}$

$\frac{9.0}{40} \frac{8.6}{27} \frac{7.6}{22} \frac{2.0}{14} \frac{1.7}{11} 1.5 \frac{1.8}{9} \frac{2.3}{12} \frac{8.8}{23} \frac{10.5}{32} \frac{11.3}{40}$

$\frac{8.6}{40} \frac{8.9}{26} \frac{7.4}{19} \frac{3.7}{14} \frac{3.3}{11} 3.1 \frac{3.2}{8} \frac{3.7}{12} \frac{9.6}{22} \frac{10.9}{29} \frac{11.3}{40}$

$\frac{8.4}{40} \frac{8.6}{28} \frac{8.9}{25} \frac{7.7}{19} \frac{4.6}{13} \frac{4.3}{10} 4.2 \frac{4.5}{9} \frac{4.9}{12} \frac{10.0}{22} \frac{11.3}{46}$

$\frac{8.2}{40} \frac{8.5}{28} \frac{9.2}{24} \frac{8.6}{21} \frac{5.5}{13} \frac{5.2}{10} 5.0 \frac{5.4}{9} \frac{5.8}{13} \frac{9.8}{21} \frac{10.7}{26} \frac{11.4}{40}$

$\frac{9.1}{40} \frac{9.6}{24} \frac{8.6}{19} \frac{6.5}{14} \frac{6.2}{10} 5.9 \frac{6.2}{9} \frac{6.6}{14} \frac{10.8}{22} \frac{11.8}{40}$

$\frac{9.5}{40} \frac{10.0}{31} \frac{10.5}{25} \frac{9.1}{19} \frac{6.8}{14} \frac{6.3}{10} 6.2 \frac{6.6}{9} \frac{7.0}{13} \frac{10.4}{20} \frac{11.2}{24} \frac{12.0}{40}$

Sta	+	H.I.	-	E.L.
		869.30		
20+50				63.4
21+00				64.5
+50				66.2
22+00				68.2
T.P.	6.24	875.50	0.04	869.26
22+50				70.0
23+00				71.7
+50				73.3
+66				
24+00				75.1
T.P.	12.72	886.68	1.54	873.96
+10				75.5
+15				75.6
+50				76.7
25+00				78.4
+50				80.1

$$\begin{array}{r} 8.9 \\ 40 \end{array} \quad \begin{array}{r} 9.0 \\ 24 \end{array} \quad \begin{array}{r} 8.6 \\ 18 \end{array} \quad \begin{array}{r} 6.2 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 10 \end{array} \quad 5.9 \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 2.5 \\ 13 \end{array} \quad \begin{array}{r} 9.6 \\ 19 \end{array} \quad \begin{array}{r} 10.6 \\ 24 \end{array} \quad \begin{array}{r} 10.8 \\ 40 \end{array}$$

$$\begin{array}{r} 7.9 \\ 40 \end{array} \quad \begin{array}{r} 7.7 \\ 31 \end{array} \quad \begin{array}{r} 7.1 \\ 23 \end{array} \quad \begin{array}{r} 6.3 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad 4.8 \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 5.8 \\ 14 \end{array} \quad \begin{array}{r} 9.3 \\ 20 \end{array} \quad \begin{array}{r} 10.2 \\ 24 \end{array} \quad \begin{array}{r} 10.8 \\ 40 \end{array}$$

$$\begin{array}{r} 6.4 \\ 40 \end{array} \quad \begin{array}{r} 5.9 \\ 25 \end{array} \quad \begin{array}{r} 3.8 \\ 17 \end{array} \quad \begin{array}{r} 3.3 \\ 10 \end{array} \quad 3.1 \quad \begin{array}{r} 3.5 \\ 9 \end{array} \quad \begin{array}{r} 4.2 \\ 15 \end{array} \quad \begin{array}{r} 8.2 \\ 21 \end{array} \quad \begin{array}{r} 9.0 \\ 26 \end{array} \quad \begin{array}{r} 9.7 \\ 35 \end{array} \quad \begin{array}{r} 10.4 \\ 40 \end{array}$$

$$\begin{array}{r} 3.0 \\ 40 \end{array} \quad \begin{array}{r} 2.9 \\ 30 \end{array} \quad \begin{array}{r} 0.3 \\ 24 \end{array} \quad \begin{array}{r} 1.1 \\ 10 \end{array} \quad 1.1 \quad \begin{array}{r} 1.5 \\ 9 \end{array} \quad \begin{array}{r} 2.1 \\ 15 \end{array} \quad \begin{array}{r} 7.0 \\ 26 \end{array} \quad \begin{array}{r} 9.7 \\ 35 \end{array} \quad \begin{array}{r} 10.3 \\ 40 \end{array}$$

$$\begin{array}{r} 0.0 \\ 40 \end{array} \quad \begin{array}{r} 1.4 \\ 30 \end{array} \quad \begin{array}{r} 4.4 \\ 24 \end{array} \quad \begin{array}{r} 6.2 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 10 \end{array} \quad 5.5 \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 13.2 \\ 29 \end{array} \quad \begin{array}{r} 13.8 \\ 34 \end{array} \quad \begin{array}{r} 16.0 \\ 46 \end{array}$$

$$\begin{array}{r} 882.6 \\ 52 \end{array} \quad \begin{array}{r} 882.8 \\ 37 \end{array} \quad \begin{array}{r} 3.9 \\ 22 \end{array} \quad \begin{array}{r} 3.8 \\ 19 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad \begin{array}{r} 4.0 \\ 9 \end{array} \quad 3.8 \quad \begin{array}{r} 4.0 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 6.2 \\ 22 \end{array} \quad \begin{array}{r} 9.1 \\ 28 \end{array} \quad \begin{array}{r} 11.3 \\ 36 \end{array} \quad \begin{array}{r} 13.0 \\ 43 \end{array}$$

$$\begin{array}{r} 893.3 \\ 60 \end{array} \quad \begin{array}{r} 891.6 \\ 43 \end{array} \quad \begin{array}{r} 2.5 \\ 17 \end{array} \quad \begin{array}{r} 2.3 \\ 9 \end{array} \quad 2.2 \quad \begin{array}{r} 2.4 \\ 10 \end{array} \quad \begin{array}{r} 4.1 \\ 23 \end{array} \quad \begin{array}{r} 4.0 \\ 30 \end{array} \quad \begin{array}{r} 9.1 \\ 40 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} 898.5 \\ 60 \end{array} \quad \begin{array}{r} 894.5 \\ 43 \end{array}$$

$$\begin{array}{r} 899.9 \\ 65 \end{array} \quad \begin{array}{r} 898.0 \\ 45 \end{array} \quad \begin{array}{r} 0.4 \\ 16 \end{array} \quad \begin{array}{r} 0.4 \\ 9 \end{array} \quad 0.4 \quad \begin{array}{r} 0.6 \\ 11 \end{array} \quad \begin{array}{r} 1.4 \\ 18 \end{array} \quad \begin{array}{r} 2.7 \\ 22 \end{array} \quad \begin{array}{r} 3.3 \\ 40 \end{array}$$

$$11.2 \quad \begin{array}{r} 11.6 \\ 11 \end{array} \quad \begin{array}{r} 12.3 \\ 15 \end{array} \quad \begin{array}{r} 13.7 \\ 28 \end{array} \quad \begin{array}{r} 14.2 \\ 47 \end{array}$$

$$11.1 \quad \begin{array}{r} 11.5 \\ 11 \end{array} \quad \begin{array}{r} 12.2 \\ 18 \end{array} \quad \begin{array}{r} 13.3 \\ 27 \end{array} \quad \begin{array}{r} 8.6 \\ 33 \end{array} \quad \begin{array}{r} 12.9 \\ 42 \end{array}$$

$$\begin{array}{r} 903.0 \\ 68 \end{array} \quad \begin{array}{r} 901.2 \\ 45 \end{array} \quad \begin{array}{r} 9.7 \\ 19 \end{array} \quad \begin{array}{r} 10.1 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 9 \end{array} \quad 10.0 \quad \begin{array}{r} 10.3 \\ 11 \end{array} \quad \begin{array}{r} 10.8 \\ 17 \end{array} \quad \begin{array}{r} 11.2 \\ 24 \end{array} \quad \begin{array}{r} 10.4 \\ 27 \end{array} \quad \begin{array}{r} 5.2 \\ 35 \end{array} \quad \begin{array}{r} 8.9 \\ 42 \end{array}$$

$$\begin{array}{r} 903.5 \\ 70 \end{array} \quad \begin{array}{r} 902.5 \\ 44 \end{array} \quad \begin{array}{r} 5.3 \\ 24 \end{array} \quad \begin{array}{r} 8.6 \\ 17 \end{array} \quad \begin{array}{r} 8.8 \\ 13 \end{array} \quad \begin{array}{r} 8.3 \\ 8 \end{array} \quad 8.1 \quad \begin{array}{r} 8.4 \\ 11 \end{array} \quad \begin{array}{r} 8.9 \\ 17 \end{array} \quad \begin{array}{r} 9.8 \\ 22 \end{array} \quad \begin{array}{r} 9.1 \\ 28 \end{array} \quad \begin{array}{r} 6.4 \\ 32 \end{array} \quad \begin{array}{r} +1.9 \\ 34.5 \end{array} \quad \begin{array}{r} 0.0 \\ 35.1 \end{array} \quad \begin{array}{r} 2.5 \\ 45 \end{array}$$

$$\begin{array}{r} 905.6 \\ 70 \end{array} \quad \begin{array}{r} 904.1 \\ 44 \end{array} \quad \begin{array}{r} 2.9 \\ 25 \end{array} \quad \begin{array}{r} 5.9 \\ 19 \end{array} \quad \begin{array}{r} 6.9 \\ 10 \end{array} \quad 6.6 \quad \begin{array}{r} 6.9 \\ 11 \end{array} \quad \begin{array}{r} 7.5 \\ 20 \end{array} \quad \begin{array}{r} 5.9 \\ 27 \end{array} \quad \begin{array}{r} +5.9 \\ 39.5 \end{array} \quad \begin{array}{r} +5.2 \\ 44.0 \end{array} \quad \begin{array}{r} +3.8 \\ 50 \end{array}$$

886.68

26+00

81.2

+50

81.9

27+00

83.2

+26

83.7

+31

Drive Rt.

83.7

+50

✓ ✓

84.0

+59

84.1

28+00

84.7

2.13 884.55

$$\begin{array}{r} 905.0 \\ 70 \end{array} \quad \begin{array}{r} 902.9 \\ 41 \end{array} \quad \begin{array}{r} 1.2 \\ 27 \end{array} \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad 5.5 \quad \begin{array}{r} 5.9 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 0.0 \\ 34 \end{array} \quad \begin{array}{r} +1.0 \\ 40 \end{array} \quad \begin{array}{r} +11.2 \\ 41.1 \end{array} \quad \begin{array}{r} +9.7 \\ 49.1 \end{array} \quad \begin{array}{r} +8.5 \\ 55 \end{array}$$

$$\begin{array}{r} 901.7 \\ 60 \end{array} \quad \begin{array}{r} 901.3 \\ 43 \end{array} \quad \begin{array}{r} 898.6 \\ 35 \end{array} \quad \begin{array}{r} 4.7 \\ 17 \end{array} \quad 4.8 \quad \begin{array}{r} 4.9 \\ 11 \end{array} \quad \begin{array}{r} 4.9 \\ 18 \end{array} \quad \begin{array}{r} 0.7 \\ 30 \end{array} \quad \begin{array}{r} +5.3 \\ 41 \end{array} \quad \begin{array}{r} +13.1 \\ 44.5 \end{array} \quad \begin{array}{r} +12.0 \\ 51.5 \end{array} \quad \begin{array}{r} +11.3 \\ 55 \end{array}$$

$$\begin{array}{r} 896.4 \\ 50 \end{array} \quad \begin{array}{r} 897.4 \\ 36 \end{array} \quad \begin{array}{r} 896.2 \\ 31 \end{array} \quad \begin{array}{r} 1.9 \\ 23 \end{array} \quad \begin{array}{r} 3.7 \\ 15 \end{array} \quad 3.5 \quad \begin{array}{r} 3.9 \\ 17 \end{array} \quad \begin{array}{r} 2.7 \\ 22 \end{array} \quad \begin{array}{r} 2.3 \\ 27 \end{array} \quad \begin{array}{r} 0.0 \\ 32 \end{array} \quad \begin{array}{r} +14.1 \\ 36 \end{array} \quad \begin{array}{r} +12.6 \\ 50.4 \end{array} \quad \begin{array}{r} +11.3 \\ 55 \end{array}$$

$$3.0 \quad \begin{array}{r} 3.1 \\ 17 \end{array} \quad \begin{array}{r} 2.0 \\ 26 \end{array} \quad \begin{array}{r} +3.8 \\ 38 \end{array}$$

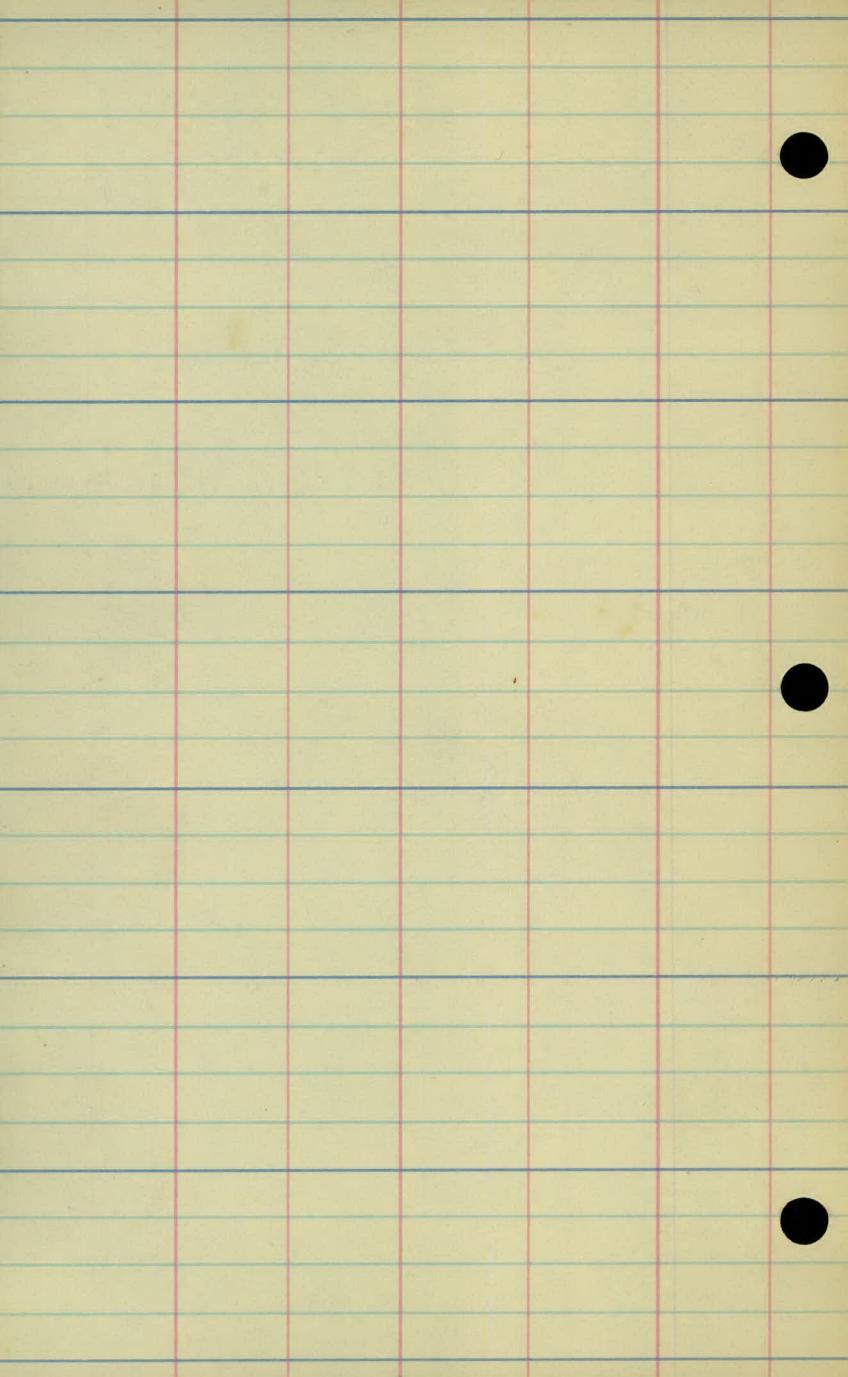
$$\text{Drive.}$$

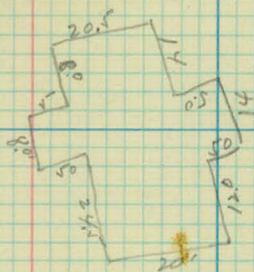
$$3.0 \quad \begin{array}{r} 3.1 \\ 13 \end{array} \quad \begin{array}{r} 2.5 \\ 24 \end{array} \quad \begin{array}{r} 1.4 \\ 45 \end{array}$$

$$\begin{array}{r} 889.5 \\ 50 \end{array} \quad \begin{array}{r} 891.0 \\ 33 \end{array} \quad \begin{array}{r} 892.0 \\ 27 \end{array} \quad \begin{array}{r} 3.5 \\ 19 \end{array} \quad \begin{array}{r} 3.1 \\ 15 \end{array} \quad 2.7 \quad \begin{array}{r} 2.5 \\ 17 \end{array} \quad \begin{array}{r} 1.4 \\ 45 \end{array}$$

$$2.6 \quad \begin{array}{r} 2.9 \\ 16 \end{array} \quad \begin{array}{r} +1.6 \\ 27 \end{array}$$

$$\begin{array}{r} 0.5 \\ 40 \end{array} \quad \begin{array}{r} +1.1 \\ 31 \end{array} \quad \begin{array}{r} +2.1 \\ 30 \end{array} \quad \begin{array}{r} +3.1 \\ 26 \end{array} \quad \begin{array}{r} 2.8 \\ 17 \end{array} \quad \begin{array}{r} 2.3 \\ 13 \end{array} \quad 2.0 \quad \begin{array}{r} 2.5 \\ 17 \end{array} \quad \begin{array}{r} +0.6 \\ 28 \end{array}$$

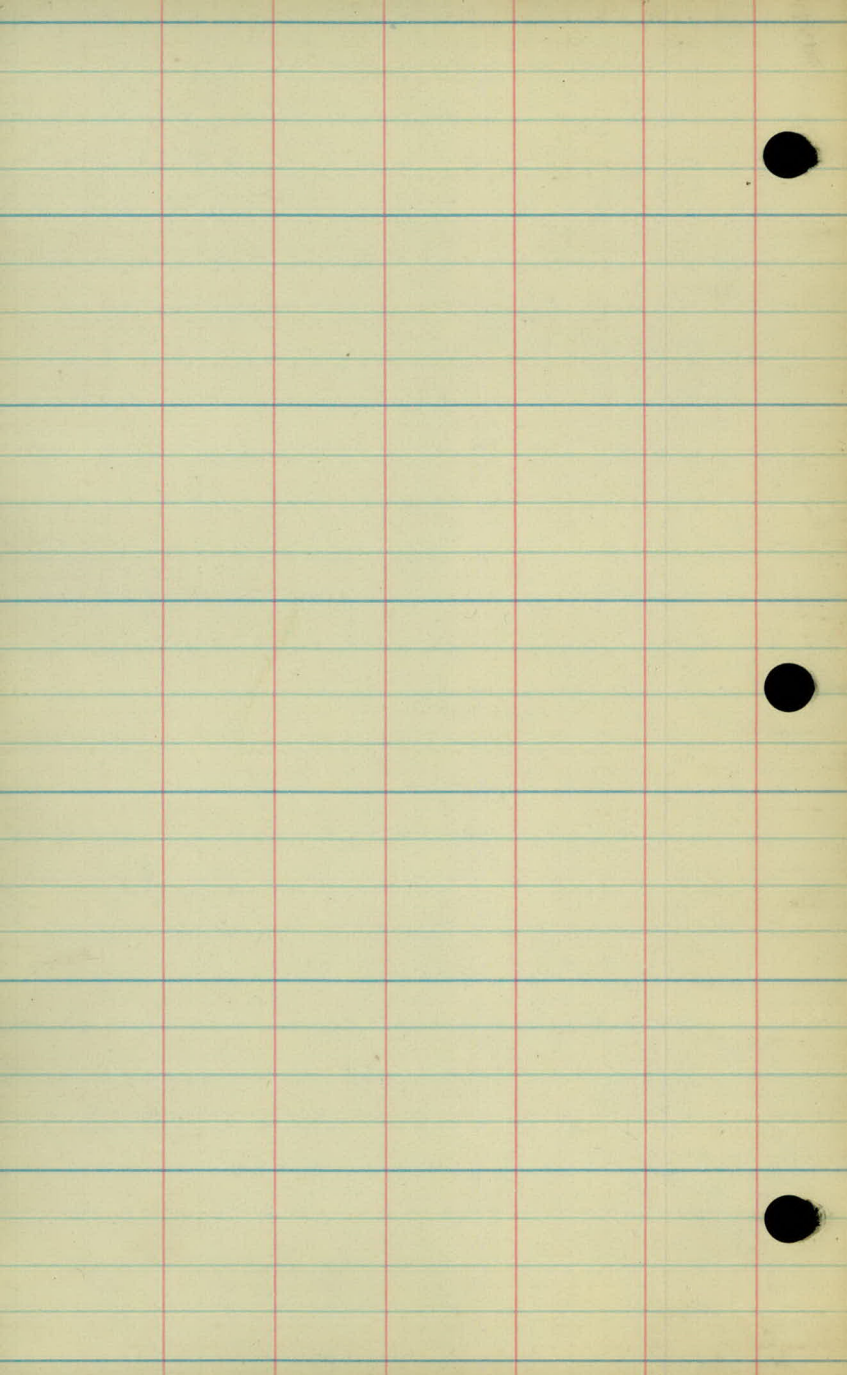


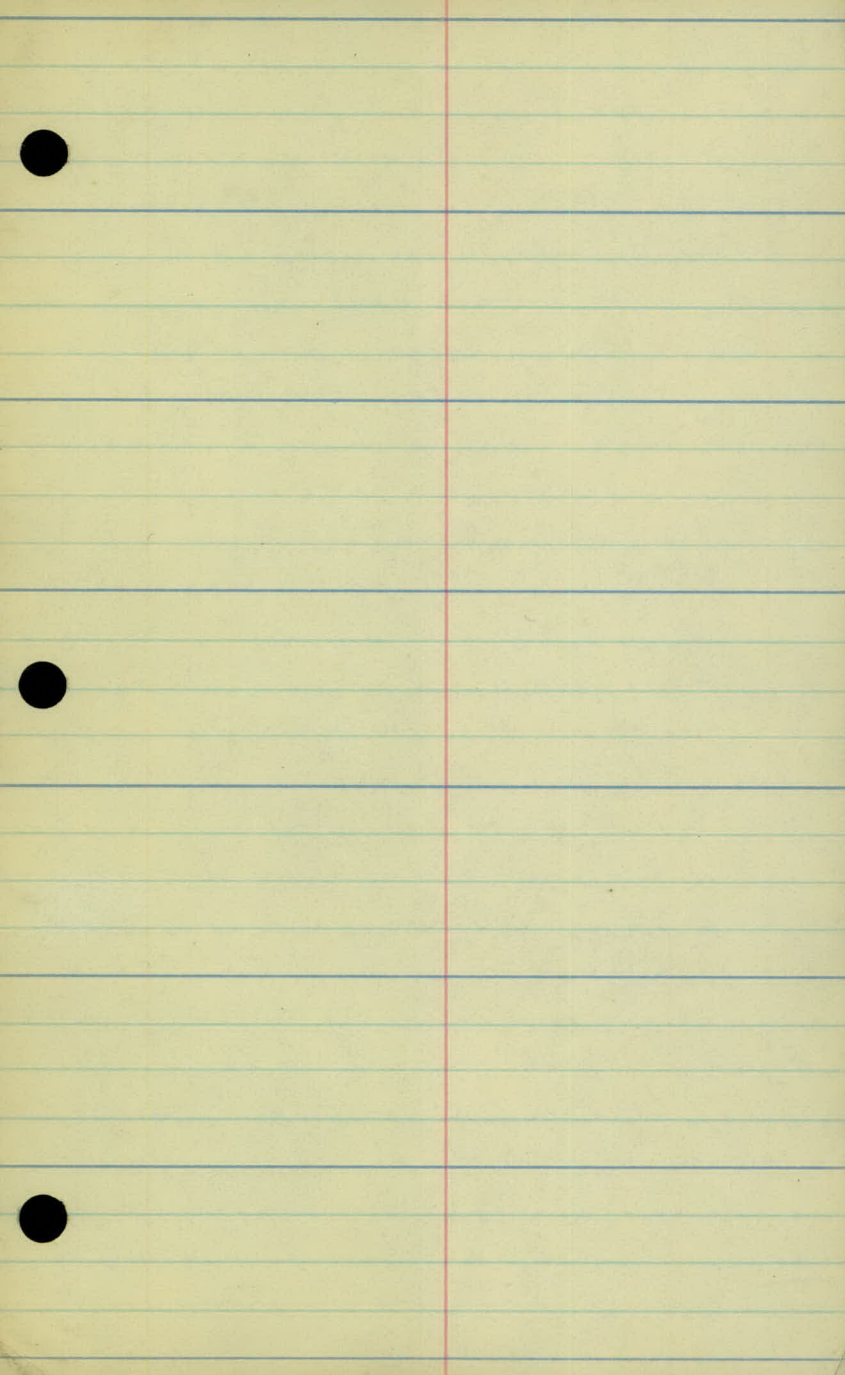


+15 Tr. 53'
+03 Tr. 22'

+97 Tr. 64
+85 Tr. 71
+78 Cor. House 62'
+68 Cor. House 72'
+65 Steps 18'
+48 Tr. 6" 42'
+70 Flower Box 41'
160 " " 42'

15-10" Oak in 2:1 Cut 51+50 to 55+50





$5^{\circ} 39'$
 $3+00$ (12.8) $26\ 56'$ $32^{\circ} 35'$ $\frac{C5.2}{598}$

$+39$ (12.0) $\frac{C8.1}{62.4}$

$+63$ (12.1) $\frac{C9.5}{68.0}$

$+100$ (12.1) $\frac{C7.8}{61.2}$

$+23$ (12.1) $\frac{C9.7}{69.8}$

$+50$ (12.3) $\frac{C9.5}{65.8}$

$+74$ (12.4) $\frac{C10.6}{72.4}$

$+100$ (12.7) $\frac{C11.0}{74.0}$

$+16$ (13.0) $\frac{C14.3}{71.2}$

$+50$ (13.3) $\frac{C6.9}{68.4}$

$+82$ 13.8

Alignment
Keller Rd.

Sta Point Δ Lt Δ Rt

6+09⁴⁵ 22°-06⁵ P.T.

6+00 21°-26⁸

+50 17°-56⁸

5+00 14°-26⁸

+50 10°-56⁸

4+60²⁷ P.I. 44°-13'

4+00 7°-26⁸

+50 3°-56⁸

3+00 0°-26⁸

2+93⁶² 0°-0' P.C.

2+91²⁷ 18°-15' P.T.

+50 15°-37⁵

2+00 12°-30'

1+50²³ P.I. 36°-23'

+50 9°-22⁵

1+00 6°-15'

+50 3°-07⁵

0+00 0°-0' P.C.

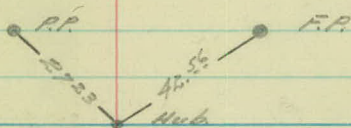
A 44° 13'

Δ 14° 0' Lt.

T 166.65

L. 315.83

R 410.28



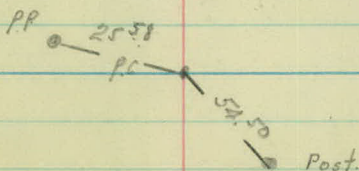
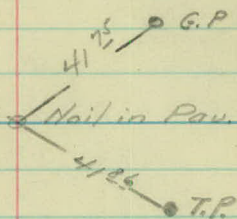
A 36° 23'

Δ 12° 30' Lt

T. 150.93

L 291.07

R 459.28



Sta Point Aht ART

19+04²⁹ P.T. 21°-48'

19+00 21°-17'

18+18⁸¹ P.I. 43°36'

+50 15°-17'

18+00 9°-17'

+50 3°-17'

17+22⁶² P.C. 0°-00'

16+23⁶⁸ P.T. 14°-35.5'

16 13°-24.5'

+50 10°-54.5'

15 8°-24.5'

14+81¹³ P.I. 29°-11'

+50 5°-54.5'

14 3°-24.5'

+50 0°-54.5'

13+31⁸⁴ P.C.

Top 2nd Iron Post
from Cor.

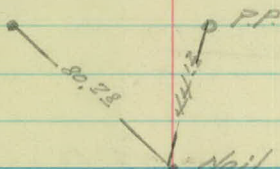
$\Delta 43^{\circ} 36'$

D 349.0' RT

T. 96.19

L. 181.67

R. 240.49



$\Delta 29^{\circ} 11'$

$\Delta 10^{\circ}$ Lt.

T 149.34

L 291.84

R 573.69

14" Cottonwood.

Q
15.28

PP 36.39

Nail



340 Point Alt A Rt

28+01²⁴ PT 23°-55'

28+00 23°-46'

+50 18°-01'

27+04⁴⁶ P.I. 47°-51' 23'

27+00 12°-16'

+50 6°-31'

26+00 0°-46'

25+93²⁰ P.C. 0°-00'

24+79²⁵ P.T. 8°-34'

+50 7°-22'

24+00 5°-22'

23+73⁵⁶ P.I. 17°-00'

+50 3°-22'

23+00 1°-32'

22+65⁵⁸ P.C. 0°-00'

27+90 $\swarrow$ 26.07 $\nearrow$ 15" Oak
 Property Iron
 $\searrow$ 31.66 $\nearrow$ 10" Box E.

10" Willow $\nearrow$ 70.30 $\swarrow$ Nail
 12" Willow $\nearrow$ 95.25 $\swarrow$ 47° 51'
 D 23° 00'
 T 111.26
 L 208.04
 P. 250.79
 E. 23.57

PC 25+93.70
 53.32 $\nearrow$ Property Iron
 25+52 $\swarrow$ 61.63
 T.R.

Iron Post. $\nearrow$ 55.40 $\swarrow$ Nail
 Wood Post. $\nearrow$ PP 2180 $\swarrow$ 17° 08'
 Iron Post. $\nearrow$ 48.26 $\swarrow$ D 8° 00'
 T. 107.98
 L. 214.17
 R. 716.78
 E. 8.09

Sta Point ALT Δ Rt.

31+90⁸² PT 7° 56'

31+69⁸² PI 15° 52' 15

+50 0° 22⁹⁶

31+47⁸³ PC 0° 00'

30+36⁴⁵ P.T. 5° 43'

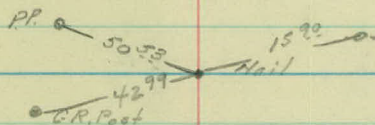
30+00 4° 04'

29+73²¹ PI 11° 26' 3'

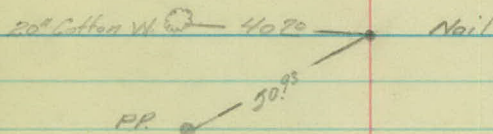
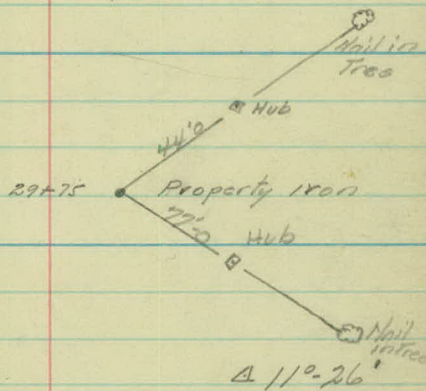
+50 1° 49'

29+09⁴⁴ PC 0° 00'

$\Delta 16^{\circ}26'$
 $D. 40^{\circ}00'$
 $T. 21.14$
 $L. 4.08$
 $R. 146.19$
 $E. 1.52$



$\Delta 15^{\circ}52'$
 $D. 37^{\circ}00'$
 $P.P.T. 21.94$
 $L. 42.89$



$\Delta 11^{\circ}26'$
 $D. 90^{\circ}00'$
 $T. 63.80$
 $L. 127.04$
 $R. 637.28$
 $E. 3.18$

Sta. Point Alt. A.R.

53+13.47 P.T. 11°-07'

53+00 10°-15'

+50 7°-00'

52+29.12 P.I. 22°-15'

52+00 3°-45'

+50 0°-30'

51+42.32 P.C. 0°-0'

38+47.50^{1.473} P.T. 9°-03'

38+00 6°-40'

+50 4°-10'

37+57.88 P.I. 18°-06'

37+00 1°-40'

36+66.50 P.C. 0°-00'

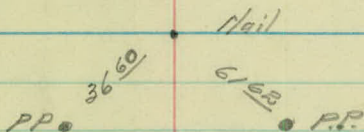
589'

$\Delta 22^{\circ}-15'$

$D 13^{\circ}-00'$

$T. 86.85$

$L. 171.15$



$\Delta 18^{\circ}-06'$

$D. 100.0'$

$T. 91.38$

$L. 181.0$

$E. 7.2$

