

Book - 28 - On 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

C.W.A. CONST. Survey

COUNTY ROAD "C"

From Cleveland To Snelling

Road Acc't. No. 7

Date Filed 1934

File _____

Alignment Notes

CO RD C

Cleveland to Snelling

(Copy)

sta Point Lt Rt

59+19³⁰ PT

N 84-33' E

58+13¹⁰ PI 4° 15'

X

57+06⁸⁰ PC

N. 88° 40' E

51+50⁶³ PT

50+9+⁰⁰ PI 1° 08'

↓

50+37³⁰ PC

57 + 06.80 0°-56' 45.7
 58. 0°-56' F.C.
 59 1°-56' T.P.
 +193 2°-07½'

Δ 4°-15'
 D 2° Lt
 T 106 ³
 L 212 ⁵⁰
 R 2864 ⁹³

Cleveland Ave S-E Cor Sec 5

T.P. 206.65 43.14 F.P.
 24.38

Δ 1°-08'
 D 1° Lt
 T 56 ²⁰
 L 113 ³³
 R 5729 ⁶⁵

Sta	Point	Lt	Rt.
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69+65.45	PT		
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69+06.88	PI		2°-20'
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68+48.55	PC		
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N 78° 22' E

61+96.74	PT		
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60+94.35	PI		6°-09'
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59+91.74	PC		
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8-25-25

H L W

(Copy)

6" Stamp (3)

0 TP N^o 18768

32° 1'

61
56

Δ 2° 20'

D 2° Rt

T 58 33

L 116 9

R 2864 93

59+91.74

650 0° 07.4'

TP
0

Δ 6° 09'

+450 0° 52.4'

34.3

D 3° Lt

61 1° 37.4'

T 102 61

+50 2° 22.4'

29 ⁹⁵

L 205 00

+96 ⁷⁴ 3° 04.5'

Δ
Hub

R 1910 08

Sta	Point	Lt	Rt
88+30.00	PI	0°-08'	
79+47.65	POT		Sec line
79+47.50	PT		
78+75.9	PI		5°-44'
78+04.2	PC		
73+51.24	PT		
72+02.90	PI		5°-58'
70+53.58	PC		

↑

S 87°-34'E

X

N 86°-42'E

Y

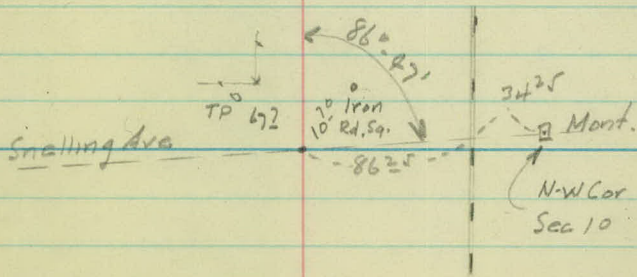
105486-1 P1

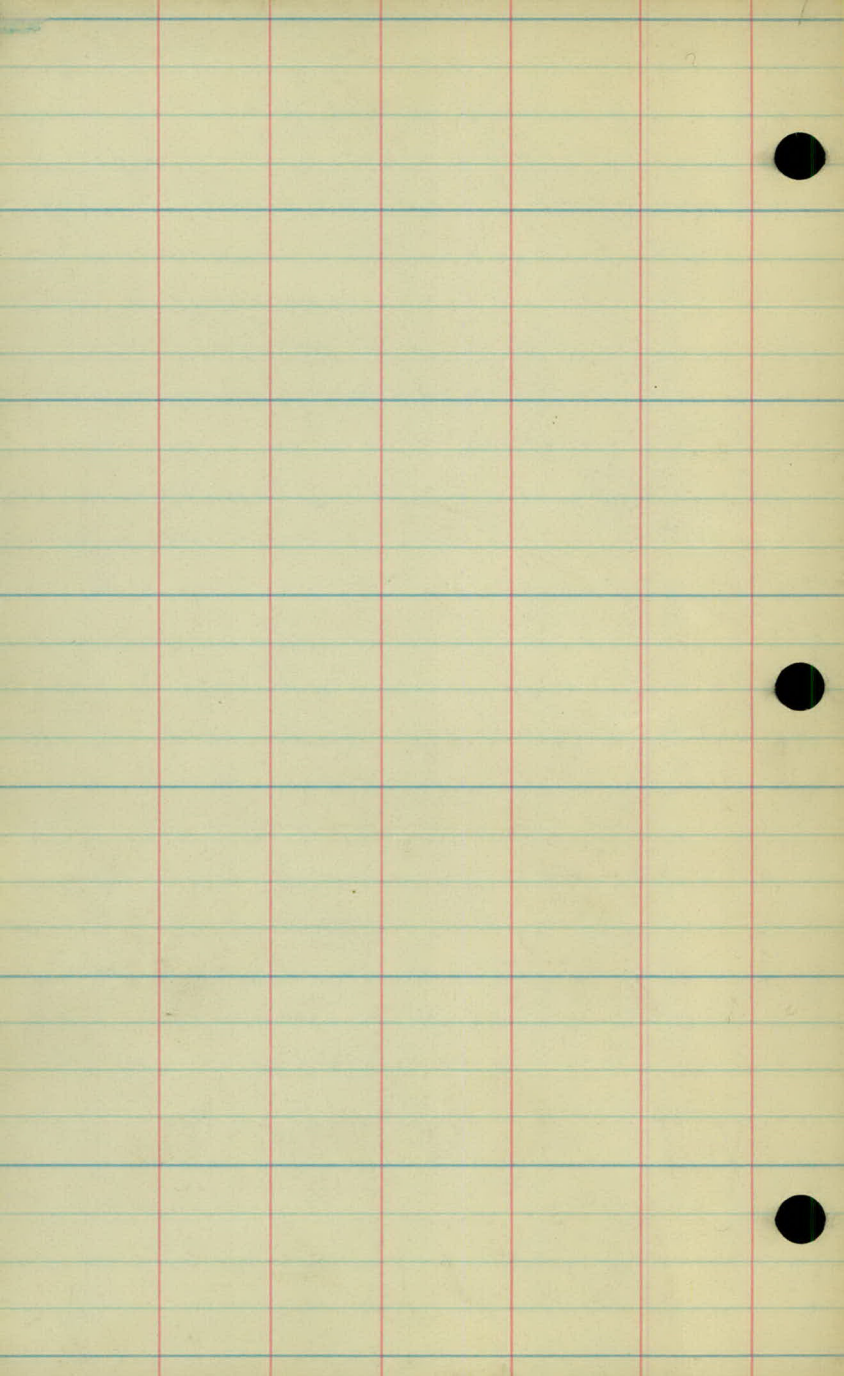
0°02'

Sec Line

587°22'E

587°42'E - 4





County Road "C" - Cleveland Ave West
Alignment Cleveland to Snelling
Sta 53+00³⁵ to 105+84⁴⁵

Sta	Point	Lt.	Rt.	Lt.	Rt.
59+19 ²⁰	P.T.	2°07 ¹ / ₂			
59		1°56'		Δ 4°15'	
+50		1°26'		D 2° Lt	
58+13 ¹⁰	P.I.			T 106.3	
58		0°56'		L 212 ⁵⁰	
+50		0°26'		R 2864 ⁹³	
57+06 ⁸⁰	P.C.	0°00'			

53+00³⁵

51+50 ⁶³	P.T.	0°34'			
51		0°19'		Δ 1°08'	
				D 1° Lt	
				T 56.20	
50+94 ²⁰	P.I.			L 113 ³³	
				R 5729 ⁶⁵	
+50		0°04'			
50+37 ³⁰	P.C.	0°00'			

West

Tangents Run out 2/12/34

Curves Run 2/14/34

P.P. o 26.5 spk 570 o T.P.

± Cleveland Ave.

4'

S.E. Cor Sec. 5

206.65

P.P. o

29.7 spk

26.2

o T.P.

County Road "C"

5+9 Point Lt Rt Lt Rt.

69+65⁷⁵ P.T. 1° 10'

+50

1° 01'

Δ 2° 20'

D 2° Rt

T 58³³

69+06⁸⁸ P.I.

L 116²

R 2864⁷³

69 0° 31'

+50

0° 01'

68+48⁵⁵ P.C.

0° 00'

61+96⁷⁹ P.T. 3° 04¹/₂'

+50

2° 22¹/₂'

Δ 6° 09'

61

1° 37¹/₂'

D 3° Lt

T 102⁶¹

60+94³⁵ P.I.

L 205°

R 1910⁰⁸

+50

0° 52¹/₂'

60

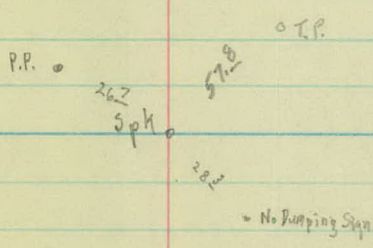
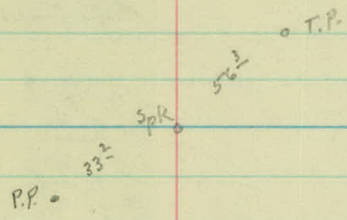
0° 07¹/₂'

59+91⁷⁴ P.C.

0° 00'

Tangents Run Out 2/12/34

Curves Run 2/14/34



Tangents Run Out 2/12/34

Curves Run 2/13/34

P.P. o

426

396

o T.P.

Spk o

9825

759

1857

9477

Curves Run 2/14/34

P.P. o

297

Spk

210

o T.P.

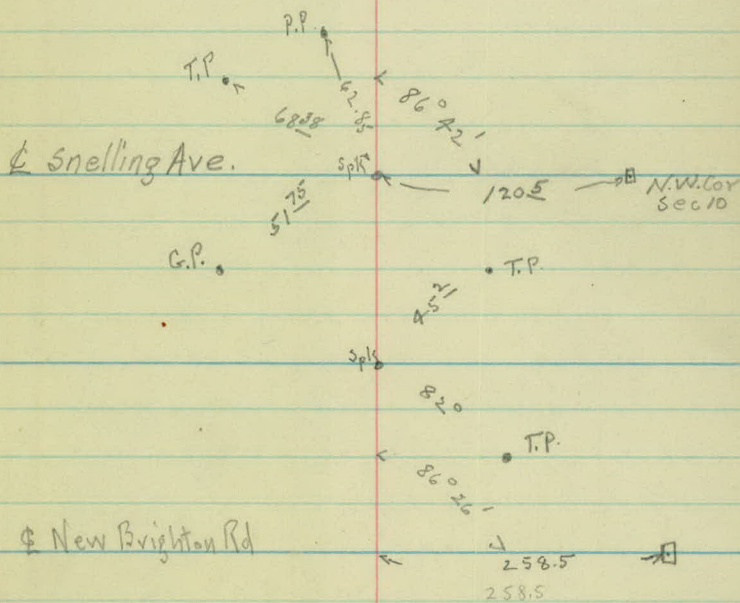
8
Sta Point Lt Rt Lt Rt

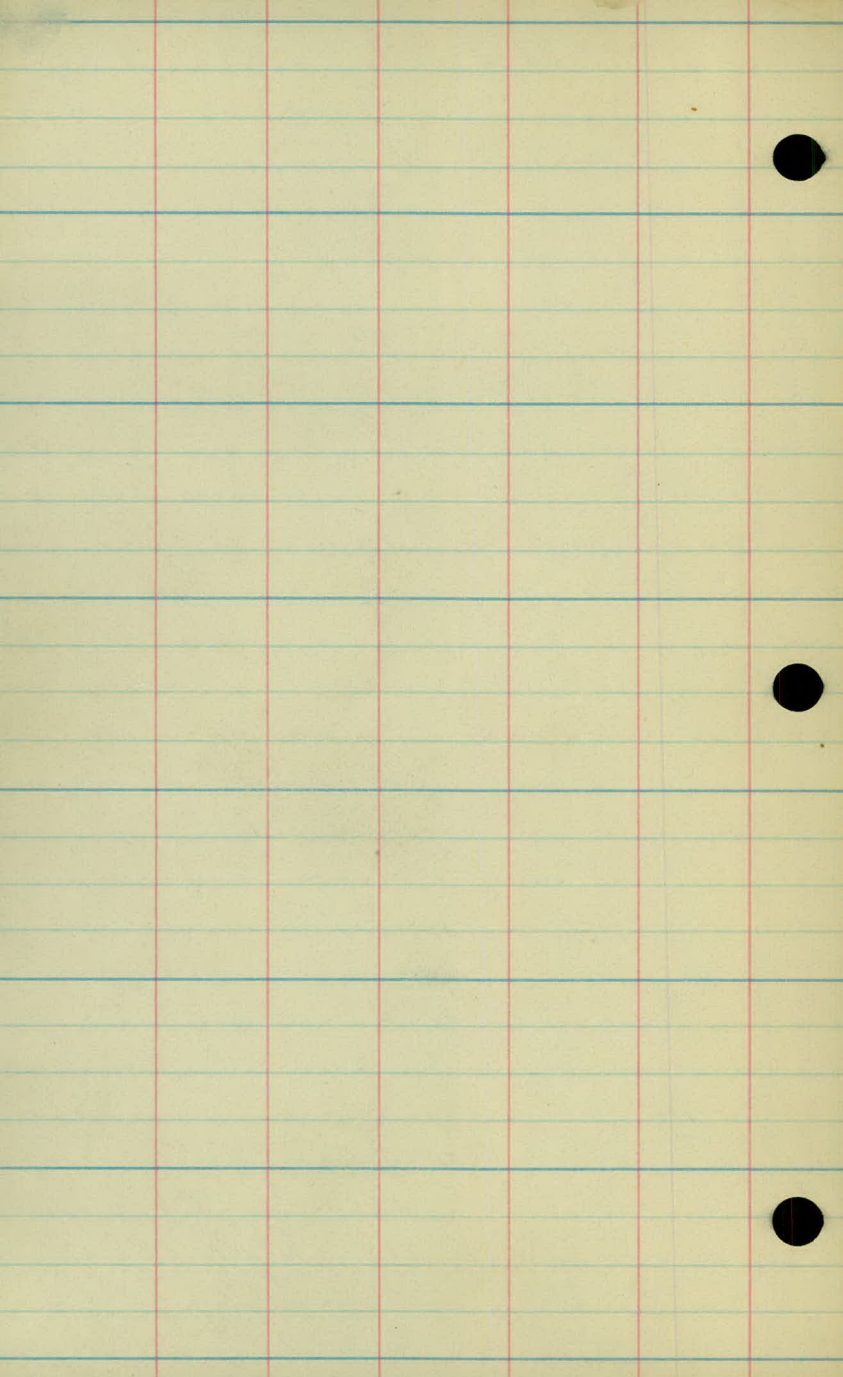
105+84⁴⁵ P.I.

88+30⁰⁰ P.I. 0°04'

52⁴ feet from P.I. on Forward Semi Tangent

9
Q Run 2/13/34





County Road "C" - Cleveland West.

Fences to be Removed.

Cleveland Ave to Hamline St.

Fences to Remove

County Road "G" - Snelling to Hamline

108+75 to 110+50 Left Side

175 feet 48" Woven Wire Poor

175 " Barbed Wire Poor

15 - Good 4" posts - 5 Poor 4" Posts

109+50 to 114 Right Side

450 ft (Total 1800 ft) 4 Strand Barbed Wire

26 - Good 6" posts

8 - Bad 6" "

117+25 to 119 Left Side

175 feet 48" Woven Wire - Poor

175 " 1 Strand Barbed Wire - Poor

3 Good 6" Posts - 4 Bad 6" Posts

5 " 3" " - 4 " 3" "

119 to 131+50 Left Side

1250 ft (Total 2500 ft) 2 Strand Barbed Wire

9 - Good 6" Posts 3 - Bad 6" Posts

37 - " 3" " 16 - " 3" "

County Road "C" - Cleveland Ave West
Cross-sections & Slope stakes.
Cleveland Ave to Snelling Ave
Sta 53+00 to 105+85

Assumed Elev. 1000.00

B.M.

Station + H.I. - Elev Grade Rd.

9.18 1009.18

53+50

8.0

54

9.1
7.6

+50

6.3

+85

9.2
5.8

55

5.3

+50

4.4

+58

40'-12" C.M.P.

Extension Required
12' Right
18' Left.

4.3

56

3.6

+45

End of Fence on Left 25ft out

+50

2.3

57

1.0

T.P.

10.75

1018.70

1.23

1008.95

+25

N.B.-D.C. Grade on Lt 12.4 - 38' R.B.

11.7
10.2

+50

N.B.-D.C. Grade on Lt 11.9 - 36' R.B.

9.7

19.0

58

A=2045

8.5

41.3

Spike in Oak Tree 35ft left of 52+70

2/14/34

$\frac{12.1}{F4.1}$	$\frac{12.1}{F4.1}$	$\frac{12.2}{40}$	$\frac{12.2}{33}$	$\frac{11.7}{21}$	$\frac{8.1}{14}$	$\frac{10.3}{7.7}$	$\frac{8.0}{10}$	$\frac{7.7}{17}$	$\frac{11.7}{30}$	$\frac{11.7}{37}$	$\frac{11.7}{40}$
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$\frac{8.2}{P.C.0.9}$	$\frac{8.2}{25.8}$	$\frac{8.8}{40}$	$\frac{8.7}{53}$	$\frac{8.0}{17}$	$\frac{7.5}{12}$	$\frac{10.5}{7.1}$	$\frac{7.3}{10}$	$\frac{8.4}{25}$	$\frac{8.8}{27}$	$\frac{8.2}{30}$	$\frac{8.2}{40}$	$\frac{2.5}{P.C.0.6}$	$\frac{8.5}{2.5}$
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$\frac{5.0}{C.1.3}$	$\frac{5.0}{29.6}$	$\frac{6.7}{40}$	$\frac{5.6}{33}$	$\frac{3.9}{22}$	$\frac{6.6}{18}$	$\frac{6.5}{12}$	$\frac{10.5}{5.8}$	$\frac{6.3}{10}$	$\frac{6.9}{14}$	$\frac{8.7}{20}$	$\frac{9.6}{27}$	$\frac{9.2}{35}$	$\frac{2.8}{43}$	$\frac{3.2}{56}$	$\frac{2.6}{9.6}$	$\frac{9.6}{F3.3}$
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$\frac{8.5}{F3.2}$	$\frac{8.5}{26.4}$	$\frac{9.8}{40}$	$\frac{9.1}{31}$	$\frac{8.1}{21}$	$\frac{5.4}{13}$	$\frac{5.3}{9}$	$\frac{10.3}{5.0}$	$\frac{5.4}{10}$	$\frac{5.7}{13}$	$\frac{8.2}{19}$	$\frac{7.8}{25}$	$\frac{8.4}{32}$	$\frac{6.6}{35}$	$\frac{6.6}{40}$	$\frac{2.5}{7.8}$	$\frac{7.8}{F2.5}$
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$\frac{12.7}{F8.3}$	$\frac{12.7}{31.6}$	$\frac{F8.1}{32.2}$	$\frac{12.8}{40}$	$\frac{12.0}{29}$	$\frac{11.0}{23}$	$\frac{4.6}{12}$	$\frac{10.3}{4.1}$	$\frac{4.3}{9}$	$\frac{4.6}{12}$	$\frac{9.4}{21}$	$\frac{9.9}{29}$	$\frac{11.0}{40}$	$\frac{3.1}{9.9}$	$\frac{9.9}{F5.5}$
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$\frac{12.9}{F8.6}$	$\frac{12.9}{37.2}$	$\frac{F8.3}{32.5}$	$\frac{12.1}{40}$	$\frac{12.1}{28}$	$\frac{5.0}{20}$	$\frac{4.5}{12}$	$\frac{10.3}{4.0}$	$\frac{4.4}{10}$	$\frac{4.4}{12}$	$\frac{5.0}{20}$	$\frac{9.9}{23}$	$\frac{10.0}{32}$	$\frac{10.1}{40}$	$\frac{3.1}{10.0}$	$\frac{10.0}{F5.7}$
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$\frac{11.1}{F7.5}$	$\frac{11.1}{35.0}$	$\frac{F7.3}{31.5}$	$\frac{11.5}{40}$	$\frac{11.2}{33}$	$\frac{10.4}{26}$	$\frac{10.0}{24}$	$\frac{4.0}{12}$	$\frac{10.3}{3.3}$	$\frac{3.4}{10}$	$\frac{3.7}{13}$	$\frac{8.2}{21}$	$\frac{8.5}{29}$	$\frac{8.6}{40}$	$\frac{2.9}{8.5}$	$\frac{8.5}{F4.9}$
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$\frac{7.3}{F5.0}$	$\frac{7.3}{30.0}$	$\frac{7.4}{40}$	$\frac{7.2}{52}$	$\frac{7.0}{23}$	$\frac{2.7}{12}$	$\frac{10.3}{2.0}$	$\frac{2.3}{10}$	$\frac{2.4}{13}$	$\frac{5.2}{17}$	$\frac{5.1}{25}$	$\frac{5.0}{40}$	$\frac{2.5}{5.1}$	$\frac{5.1}{F2.8}$
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$\frac{4.1}{F3.1}$	$\frac{4.1}{26.2}$	$\frac{5.2}{40}$	$\frac{4.3}{32}$	$\frac{4.0}{20}$	$\frac{1.6}{16}$	$\frac{1.2}{12}$	$\frac{10.3}{0.7}$	$\frac{1.2}{10}$	$\frac{1.5}{13}$	$\frac{3.6}{17}$	$\frac{3.7}{29}$	$\frac{3.4}{40}$	$\frac{2.5}{3.9}$	$\frac{3.9}{F2.9}$
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P.C. Gd Stake. 57+06⁶

$\frac{11.3}{P.C.1.1}$	$\frac{11.3}{28.0}$	$\frac{11.4}{40}$	$\frac{11.7}{33}$	$\frac{10.3}{26}$	$\frac{12.4}{24}$	$\frac{10.7}{22}$	$\frac{10.3}{20}$	$\frac{10.3}{13}$	$\frac{10.3}{9.7}$	$\frac{10.3}{11}$	$\frac{10.3}{14}$	$\frac{11.0}{17}$	$\frac{11.3}{29}$	$\frac{11.6}{40}$	$\frac{14.6}{11.9}$	$\frac{11.9}{P.C.0.3}$
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$\frac{9.8}{P.C.2.5}$	$\frac{9.8}{30.2}$	$\frac{10.3}{40}$	$\frac{9.6}{32}$	$\frac{9.3}{25}$	$\frac{11.9}{24}$	$\frac{11.9}{22}$	$\frac{10.2}{21}$	$\frac{9.6}{12}$	$\frac{10.5}{9.2}$	$\frac{9.4}{10}$	$\frac{9.6}{13}$	$\frac{10.3}{15}$	$\frac{8.0}{19}$	$\frac{7.7}{33}$	$\frac{8.2}{31}$	$\frac{8.3}{40}$	$\frac{30.2}{9.8}$	$\frac{9.8}{P.C.1.6}$
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$\frac{8.1}{C.0.4}$	$\frac{8.1}{27.2}$	$\frac{8.7}{40}$	$\frac{8.4}{33}$	$\frac{8.0}{26}$	$\frac{9.7}{23}$	$\frac{8.7}{13}$	$\frac{10.5}{8.0}$	$\frac{8.3}{10}$	$\frac{8.3}{12}$	$\frac{8.6}{13}$	$\frac{11.1}{16}$	$\frac{1.5}{20}$	$\frac{2.3}{29}$	$\frac{8.6}{40}$	$\frac{27.6}{8.2}$	$\frac{8.2}{C.0.3}$
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Station	+	H.I	-	Elev	Grade Rd
58 + 50		1018.70	A = 24.04	50.2	7.2
59			A = 30.16	44.4	6.2
T.P.	10.22	1027.77	1.15	1017.58	15.4
+ 50			A = 17.78	15.9	13.9
+ 70			A = 25.11	41.2	13.4
60			A = 48.99	87.5	13.5
+ 50			A = 45.51	76.2	13.0
61			A = 36.74	27.2	13.5
T.P.	2.66	1018.87	11.56	1016.21	12.0
61 + 40			100	40.2	3.1
+ 50					3.2
+ 75					3.4
62					3.4
+ 35					3.4
+ 50					3.6

2/14/34

$$\frac{4.8}{C2.4} \frac{3.8}{3.8}$$

$$\frac{4.8}{40} \frac{4.8}{27} \frac{7.6}{24} \frac{7.2}{12} \frac{7.2}{6.7} \frac{7.0}{10} \frac{7.2}{13} \frac{7.6}{14} \frac{7.6}{16} \frac{7.6}{23} \frac{7.6}{31} \frac{8.2}{40}$$

$$\frac{2.6}{2.6} \frac{7.6}{D.C.1.1}$$

$$\frac{2.2}{C4.0} \frac{0.1}{3.5}$$

$$\frac{C3.8}{33.0}$$

$$\frac{4.7}{40} \frac{2.1}{19} \frac{6.3}{25} \frac{6.1}{11} \frac{7.0}{5.7} \frac{5.9}{12} \frac{6.5}{15} \frac{6.0}{17} \frac{6.7}{28} \frac{7.1}{40}$$

$$\frac{2.6}{2.6} \frac{6.4}{D.C.1.3}$$

On Slope Stake Lt side 59+00

$$\frac{4.5}{C9.4} \frac{0.8}{3.8}$$

$$\frac{C9.1}{33.0}$$

$$\frac{4.4}{50} \frac{4.4}{40} \frac{4.4}{32} \frac{12.8}{25} \frac{14.1}{18} \frac{13.7}{11} \frac{10.5}{12.4} \frac{12.6}{12} \frac{12.9}{15} \frac{14.7}{18} \frac{15.0}{28} \frac{14.6}{39} \frac{10.9}{45} \frac{12.4}{50}$$

$$\frac{2.8}{2.8} \frac{15.0}{D.C.0.7}$$

$$\frac{3.6}{50} \frac{3.7}{40} \frac{3.3}{38} \frac{13.0}{29} \frac{13.4}{17} \frac{13.1}{11} \frac{10.5}{12.9} \frac{13.1}{13} \frac{14.2}{16} \frac{14.0}{21} \frac{13.6}{29} \frac{12.9}{36} \frac{12.2}{43} \frac{13.3}{45} \frac{13.3}{50}$$

$$\frac{3.4}{C9.6} \frac{2}{3.8}$$

$$\frac{C8.9}{33.0}$$

$$\frac{3.3}{50} \frac{3.6}{40} \frac{4.5}{31} \frac{12.6}{20} \frac{13.0}{16} \frac{12.8}{12} \frac{10.5}{12.5} \frac{12.8}{12} \frac{13.2}{16} \frac{13.2}{24} \frac{12.9}{32} \frac{12.3}{39} \frac{8.4}{42} \frac{15.4}{50}$$

$$\frac{2.6}{2.6} \frac{13.3}{D.C.1.2}$$

$$\frac{3.4}{C8.8} \frac{0.6}{3.8}$$

$$\frac{C8.0}{33.0}$$

$$\frac{1.3}{50} \frac{3.8}{40} \frac{4.7}{27} \frac{11.7}{22} \frac{12.2}{17} \frac{12.0}{13} \frac{10.5}{11.7} \frac{12.1}{11} \frac{13.0}{15} \frac{13.1}{23} \frac{12.9}{31} \frac{7.7}{36} \frac{8.1}{39} \frac{18.0}{50}$$

$$\frac{2.5}{2.5} \frac{13.1}{D.C.0.6}$$

$$\frac{4.4}{C2.6} \frac{1}{3.8}$$

$$\frac{9.6}{40} \frac{9.4}{32} \frac{9.1}{24} \frac{12.0}{19} \frac{12.0}{15} \frac{11.8}{12} \frac{10.5}{11.5} \frac{11.8}{11} \frac{12.9}{16} \frac{13.0}{22} \frac{12.5}{29} \frac{7.0}{35} \frac{7.2}{57} \frac{14.7}{50}$$

$$\frac{2.5}{2.5} \frac{12.9}{D.C.0.6}$$

On Stake 15ft Lt of 61+10

2/15/34

$$\frac{3.6}{D6.0} \frac{0}{2.6}$$

$$\frac{5.2}{40} \frac{4.2}{30} \frac{3.1}{18} \frac{3.1}{14} \frac{3.0}{12} \frac{10.5}{2.6} \frac{2.9}{11} \frac{3.6}{14} \frac{0.4}{20} \frac{4.1}{28} \frac{4.4}{35} \frac{7.1}{50}$$

$$\frac{4.1}{4.1} \frac{3.1}{0.0}$$

$$\frac{4.4}{F1.2} \frac{4}{2.2}$$

$$\frac{6.1}{40} \frac{5.6}{32} \frac{5.2}{25} \frac{3.2}{14} \frac{3.0}{11} \frac{10.5}{2.7} \frac{3.0}{11} \frac{4.0}{14} \frac{0.9}{19} \frac{4.2}{27} \frac{4.6}{36} \frac{3.0}{41} \frac{7.7}{50}$$

$$\frac{3.6}{3.6} \frac{4.4}{C6.6}$$

$$\frac{7.0}{F3.6} \frac{1}{2.2}$$

$$\frac{7.4}{40} \frac{7.1}{33} \frac{4.5}{21} \frac{3.4}{14} \frac{10.5}{2.9} \frac{3.3}{12} \frac{4.4}{14} \frac{2.4}{20} \frac{1.1}{28} \frac{0.8}{35} \frac{4.6}{40} \frac{8.4}{50}$$

$$\frac{5.2}{F1.8} \frac{0}{2.3}$$

$$\frac{4.8}{40} \frac{4.8}{31} \frac{4.9}{17} \frac{3.4}{13} \frac{10.5}{2.9} \frac{3.3}{11} \frac{4.0}{15} \frac{2.6}{19} \frac{1.8}{28} \frac{1.2}{37} \frac{5.6}{44} \frac{8.1}{50}$$

$$\frac{3.0}{3.0} \frac{1.7}{C1.7}$$

$$\frac{3.2}{50} \frac{3.2}{29} \frac{3.1}{21} \frac{4.6}{19} \frac{4.6}{16} \frac{3.6}{13} \frac{10.5}{2.9} \frac{3.3}{12} \frac{4.0}{14} \frac{2.4}{17} \frac{1.9}{19} \frac{1.2}{29} \frac{5.2}{39} \frac{7.2}{45} \frac{7.2}{50}$$

$$\frac{3.3}{C0.3} \frac{1}{2.6}$$

$$\frac{3.0}{40} \frac{3.2}{31} \frac{3.3}{21} \frac{4.6}{18} \frac{4.6}{16} \frac{3.6}{13} \frac{10.5}{3.1} \frac{3.3}{12} \frac{4.0}{14} \frac{2.6}{17} \frac{1.4}{19} \frac{5.9}{30} \frac{5.9}{41} \frac{5.9}{50}$$

$$\frac{2.7}{2.7} \frac{2.2}{C1.4}$$

Station	+	H.I	-	Elev	Grade Rd.
62+75		1018.87			5.3 3.8
63					3.9
+50					4.2
64					4.4
+50					4.8
65					5.2
+50					5.4
66					6.9 5.4
+40		85			7.8 5.9
+50					6.0
67					6.3
B.M.	7.31	1019.93	6.25	1012.62	
+50					8.0
68					7.8

2/10/34

$\frac{4.9}{D.C.4}$
248

$\frac{5.0}{40}$ $\frac{5.0}{31}$ $\frac{4.9}{19}$ $\frac{5.2}{19}$ $\frac{5.2}{16}$ $\frac{3.9}{13}$ $+0.6$ $\frac{3.9}{12}$ $\frac{4.9}{15}$ $\frac{4.9}{18}$ $\frac{4.1}{20}$ $\frac{4.3}{32}$ $\frac{4.0}{40}$ $\frac{1.7}{46}$ $\frac{3.6}{50}$ $\frac{5.4}{59}$ $\frac{26.6}{2}$ $\frac{4.2}{D.C.1}$

$\frac{6.6}{F2.7}$
254

$\frac{6.3}{40}$ $\frac{6.5}{28}$ $\frac{6.7}{19}$ $\frac{4.2}{13}$ $+0.3$ $\frac{4.1}{10}$ $\frac{6.1}{15}$ $\frac{6.3}{28}$ $\frac{6.1}{40}$ $\frac{6.1}{50}$ $\frac{34.8}{2}$ $\frac{6.3}{F2.4}$

$\frac{7.1}{F2.9}$
258

$\frac{6.8}{40}$ $\frac{7.1}{31}$ $\frac{7.1}{18}$ $\frac{4.4}{13}$ $+0.3$ $\frac{4.6}{12}$ $\frac{11.1}{16}$ $\frac{7.5}{27}$ $\frac{7.3}{40}$ $\frac{26.4}{2}$ $\frac{7.4}{F3.2}$

$\frac{6.4}{F2.0}$
240

$\frac{6.1}{40}$ $\frac{6.2}{28}$ $\frac{6.9}{17}$ $\frac{4.6}{13}$ $+0.3$ $\frac{4.7}{11}$ $\frac{7.0}{15}$ $\frac{7.6}{28}$ $\frac{7.3}{40}$ $\frac{24.6}{2}$ $\frac{7.7}{F3.3}$

$\frac{7.2}{F2.4}$
248

$\frac{7.0}{40}$ $\frac{7.1}{29}$ $\frac{7.3}{17}$ $\frac{5.0}{13}$ $+0.3$ $\frac{5.1}{4.5}$ $\frac{7.9}{16}$ $\frac{8.0}{30}$ $\frac{8.0}{40}$ $\frac{26.6}{2}$ $\frac{8.1}{F3.3}$

$\frac{7.9}{F2.7}$
254

$\frac{7.7}{40}$ $\frac{7.8}{31}$ $\frac{7.9}{18}$ $\frac{5.4}{13}$ $+0.3$ $\frac{5.3}{9.9}$ $\frac{8.1}{11}$ $\frac{8.1}{17}$ $\frac{7.9}{30}$ $\frac{7.9}{40}$ $\frac{25.8}{2}$ $\frac{8.1}{F2.9}$

$\frac{7.6}{F2.2}$
244

$\frac{7.4}{40}$ $\frac{7.4}{31}$ $\frac{7.6}{23}$ $\frac{7.8}{17}$ $\frac{5.6}{14}$ $+0.3$ $\frac{5.3}{5.1}$ $\frac{7.7}{12}$ $\frac{7.9}{17}$ $\frac{7.7}{30}$ $\frac{7.7}{40}$ $\frac{25.0}{2}$ $\frac{7.9}{F2.5}$

$\frac{6.9}{D.C.0.0}$
240

$\frac{6.5}{40}$ $\frac{6.7}{34}$ $\frac{6.7}{27}$ $\frac{7.1}{17}$ $\frac{5.7}{14}$ $+0.3$ $\frac{5.3}{5.1}$ $\frac{5.7}{11}$ $\frac{6.9}{13}$ $\frac{7.2}{15}$ $\frac{7.0}{27}$ $\frac{7.0}{40}$ $\frac{25.6}{2}$ $\frac{7.2}{F2.8}$

$\frac{4.4}{40}$ $\frac{4.2}{37}$ $\frac{5.4}{30}$ $\frac{4.4}{24}$ $\frac{5.0}{19}$ $\frac{7.1}{17}$ $\frac{5.7}{14}$ $\frac{70.5}{5.4}$ $\frac{5.7}{11}$ $\frac{6.4}{14}$ $\frac{7.1}{16}$ $\frac{5.6}{18}$ $\frac{6.5}{24}$ $\frac{6.3}{32}$ $\frac{5.9}{40}$ $\frac{26.0}{2}$ $\frac{6.4}{D.C.1.0}$

$\frac{5.4}{C.0.6}$
28.2

$\frac{4.5}{40}$ $\frac{4.6}{30}$ $\frac{5.4}{28}$ $\frac{4.8}{26}$ $\frac{4.6}{19}$ $\frac{7.2}{16}$ $\frac{5.7}{14}$ $\frac{70.5}{5.5}$ $\frac{5.8}{10}$ $\frac{6.2}{12}$ $\frac{7.3}{13}$ $\frac{4.2}{17}$ $\frac{5.1}{31}$ $\frac{4.8}{40}$ $\frac{28.6}{2}$ $\frac{5.2}{C.0.8}$

$\frac{5.1}{C.1.2}$
29.4

$\frac{5.0}{40}$ $\frac{5.0}{36}$ $\frac{4.3}{33}$ $\frac{5.9}{31}$ $\frac{5.9}{30}$ $\frac{3.4}{27}$ $\frac{3.4}{23}$ $\frac{8.1}{18}$ $\frac{6.5}{15}$ $\frac{70.5}{5.8}$ $\frac{6.0}{8}$ $\frac{7.0}{12}$ $\frac{1.0}{18}$ $\frac{0.4}{21}$ $\frac{0.0}{30}$ $\frac{+0.2}{40}$ $\frac{40.0}{2}$ $\frac{+0.2}{C.6.5}$

30 ft Lt of 67+30 spk in P.P.

$\frac{10.8}{F2.8}$
256

$\frac{11.4}{40}$ $\frac{10.8}{30}$ $\frac{11.2}{23}$ $\frac{10.0}{17}$ $\frac{5.9}{14}$ $\frac{70.5}{7.5}$ $\frac{8.0}{10}$ $\frac{9.0}{12}$ $\frac{7.4}{15}$ $\frac{6.6}{27}$ $\frac{5.9}{32}$ $\frac{5.1}{40}$ $\frac{30.8}{2}$ $\frac{6.1}{C.1.9}$

$\frac{14.1}{F6.3}$
32.6

$\frac{14.2}{40}$ $\frac{12.2}{33}$ $\frac{12.0}{26}$ $\frac{12.3}{19}$ $\frac{8.2}{13}$ $\frac{70.5}{7.5}$ $\frac{8.1}{11}$ $\frac{12.4}{21}$ $\frac{12.6}{32}$ $\frac{12.1}{40}$ $\frac{29.8}{2}$ $\frac{12.7}{F4.9}$

1019.93

Station + H.I - Elev Grade Rd

68+49 P.C. 7.9

+62 36'-20" C.M.P. Extension Required
Rt. side 12 ft
Lt " 16 " 7.9

69 7.9

+35 7.6

+50 7.6 Rt
7.8 Lt

+75 7.7

70 7.6 Rt
7.8 Lt

+30 7.8

+54 7.7

71 7.5 Rt
7.7 Lt+50 7.5 Rt
7.7 Lt

T.P. 5.03 1017.93 7.01 1012.92

72 5.0 7.01 1012.92 5.7 Rt
5.9 Lt

+50 6.1 7.0

2/15/34

$$\frac{13.4}{F5.5} \bigg| \frac{3}{3.0}$$

$$\frac{13.6}{40} \frac{13.4}{32} \frac{12.8}{19} \frac{8.1}{12} +0.3 \frac{8.2}{7.6} \frac{13.7}{12} \frac{13.9}{22} \frac{14.0}{31} \frac{14.0}{40}$$

$$\frac{32.0}{F6.0} \bigg| \frac{13.9}{13.9}$$

$$\frac{13.2}{F5.3} \bigg| \frac{3}{30.6}$$

$$\frac{13.2}{40} \frac{13.2}{27.0} \frac{12.8}{19} \frac{8.1}{15} \frac{8.2}{11} +0.3 \frac{8.2}{7.6} \frac{13.7}{12} \frac{13.9}{22} \frac{14.0}{31} \frac{14.0}{40}$$

$$\frac{32.0}{F6.0} \bigg| \frac{13.9}{13.9}$$

$$\frac{12.4}{F4.5} \bigg| \frac{2}{29.0}$$

$$\frac{11.7}{40} \frac{12.3}{31} \frac{12.6}{22} \frac{12.1}{18} \frac{8.0}{12} +0.3 \frac{8.2}{7.6} \frac{12.6}{11} \frac{13.9}{18} \frac{14.0}{25} \frac{14.0}{34} \frac{14.0}{40}$$

$$\frac{32.0}{F6.1} \bigg| \frac{14.0}{14.0}$$

$$\frac{8.1}{40} \frac{8.4}{32} \frac{8.8}{26} \frac{10.7}{22} \frac{10.7}{16} \frac{7.9}{12} +0.3 \frac{8.1}{7.3} \frac{12.3}{12} \frac{12.9}{20} \frac{13.2}{27} \frac{13.6}{35} \frac{14.0}{40}$$

$$\frac{4.5}{C1.3} \bigg| \frac{2}{29.6}$$

$$\frac{6.2}{40} \frac{6.4}{31} \frac{4.6}{26} \frac{9.9}{20} \frac{9.9}{16} \frac{7.9}{13} +0.5 \frac{7.9}{7.3} \frac{10.4}{12} \frac{11.3}{18} \frac{12.5}{28} \frac{14.0}{40}$$

$$\frac{27.2}{F3.6} \bigg| \frac{11.2}{11.2}$$

$$\frac{3.2}{40} \frac{2.5}{29} \frac{8.0}{33} \frac{8.6}{16} \frac{7.8}{14} +0.5 \frac{7.8}{7.2} \frac{11.1}{12} \frac{10.9}{19} \frac{9.4}{27} \frac{10.4}{29} \frac{10.4}{40}$$

$$\frac{1.7}{C6.1} \bigg| \frac{3}{39.2}$$

$$\frac{1.8}{40} \frac{6.0}{29} \frac{7.6}{24} \frac{8.2}{16} \frac{7.8}{14} +0.5 \frac{7.9}{7.3} \frac{10.1}{12} \frac{10.9}{17} \frac{10.6}{23} \frac{8.0}{27} \frac{8.1}{31} \frac{8.1}{40}$$

$$\frac{26.0}{F3.0} \bigg| \frac{10.6}{10.6}$$

$$\frac{1.8}{40} \frac{1.2}{29} \frac{6.9}{24} \frac{7.8}{16} \frac{7.7}{12} +0.5 \frac{7.7}{7.3} \frac{8.7}{11} \frac{9.8}{17} \frac{6.2}{26} \frac{7.1}{31} \frac{7.9}{50}$$

$$\frac{3.7}{C4.0} \bigg| \frac{3}{35.0}$$

$$\frac{4.1}{40} \frac{3.0}{28} \frac{6.3}{23} \frac{8.0}{16} \frac{7.6}{12} +0.5 \frac{7.8}{7.2} \frac{9.2}{11} \frac{9.7}{14} \frac{9.0}{19} \frac{5.2}{24} \frac{5.8}{30} \frac{6.9}{40} \frac{6.9}{50}$$

$$\frac{32.2}{C2.6} \bigg| \frac{5.1}{5.1}$$

$$\frac{5.4}{C2.5} \bigg| \frac{3}{31.6}$$

$$\frac{6.0}{40} \frac{6.0}{32} \frac{4.9}{31} \frac{4.9}{29} \frac{9.0}{23} \frac{7.6}{18} \frac{7.6}{14} +0.5 \frac{7.8}{7.2} \frac{9.1}{11} \frac{8.7}{14} \frac{9.4}{20} \frac{7.0}{28} \frac{7.9}{32} \frac{9.1}{40} \frac{9.1}{50}$$

$$\frac{23.4}{F1.7} \bigg| \frac{9.2}{9.2}$$

$$\frac{5.9}{C1.8} \bigg| \frac{3}{30.6}$$

$$\frac{7.0}{40} \frac{6.7}{33} \frac{5.8}{32} \frac{5.8}{30} \frac{9.5}{24} \frac{9.7}{17} \frac{7.5}{13} \frac{7.5}{7.2} \frac{7.8}{11} \frac{9.2}{15} \frac{10.1}{25} \frac{9.7}{30} \frac{8.2}{33} \frac{8.7}{40} \frac{10.3}{50}$$

$$\frac{25.2}{F2.6} \bigg| \frac{10.1}{10.1}$$

On Rock 35ft Rt of 71+65

$$\frac{3.1}{C2.8} \bigg| \frac{3}{32.6}$$

$$\frac{3.9}{40} \frac{3.8}{34} \frac{3.1}{33} \frac{3.0}{25} \frac{6.4}{16} \frac{5.8}{13} \frac{5.4}{5.4} \frac{5.9}{11} \frac{7.7}{16} \frac{9.0}{22} \frac{7.9}{26} \frac{6.2}{31} \frac{6.4}{33} \frac{7.6}{40} \frac{8.7}{50}$$

$$\frac{25.0}{F2.5} \bigg| \frac{8.2}{8.2}$$

$$\frac{1.2}{C4.9} \bigg| \frac{3}{36.8}$$

$$\frac{1.3}{40} \frac{1.2}{32} \frac{1.8}{25} \frac{7.4}{18} \frac{7.4}{16} \frac{6.1}{13} \frac{5.6}{5.6} \frac{6.2}{11} \frac{7.4}{15} \frac{7.8}{21} \frac{6.7}{23} \frac{7.3}{31} \frac{6.0}{40} \frac{8.6}{50}$$

$$\frac{25.4}{P0.07} \bigg| \frac{6.9}{6.9}$$

Station +		H. 1	-	Elev	Grade Rod
73					6.7 Rt 6.6 Lt
+52	P.T.				6.6 Lt 6.8 Rt 8.3
74					7.1 Lt 7.3 Rt
+50					7.4
75					7.6
+50					7.9
+62	26' - 10" C.M.P			Extension Required 10' + Rt. Side 12' - Lt -	7.9 Lt 8.1 Rt 8.6
76					7.8 Lt 8.0 Rt
+50					7.8 Lt 8.0 Rt
B.M.				6.92	1011.03
	2.50	1013.53			
77					4.0
+50					4.3
+90					4.5

2/15/34

$$\frac{6.2}{C.O.A} \left| \begin{array}{l} 27.8 \\ 27.8 \end{array} \right.$$

$$\frac{5.7 \ 5.5 \ 6.4 \ 7.1 \ 7.3 \ 6.4}{40 \ 32 \ 22 \ 20 \ 16 \ 14 \ 6.1}$$

$$\frac{6.6 \ 8.1 \ 8.8 \ 9.8 \ 9.8 \ 9.9}{10 \ 14 \ 24 \ 32 \ 40 \ 50}$$

$$\frac{2.5}{2.5} \left| \begin{array}{l} 9.2 \\ F2.8 \end{array} \right.$$

$$\frac{9.1}{F2.5} \left| \begin{array}{l} 25.0 \\ 25.0 \end{array} \right.$$

$$\frac{10.1 \ 9.8 \ 9.3 \ 8.4 \ 7.0}{40 \ 35 \ 27 \ 17 \ 14 \ 6.3}$$

$$\frac{6.8 \ 8.1 \ 7.4 \ 6.7 \ 6.4 \ 6.2 \ 6.1}{10 \ 13 \ 15 \ 24 \ 32 \ 40 \ 50}$$

$$\frac{2.7}{2.7} \left| \begin{array}{l} 6.6 \\ C.O.2 \end{array} \right.$$

$$\frac{10.3}{F3.2} \left| \begin{array}{l} 26.4 \\ 26.4 \end{array} \right.$$

$$\frac{10.7 \ 10.5 \ 9.5 \ 9.2 \ 7.3}{40 \ 28 \ 24 \ 16 \ 13 \ 6.8}$$

$$\frac{7.5 \ 8.1 \ 7.3 \ 6.8 \ 7.1 \ 7.3}{11 \ 12 \ 14 \ 28 \ 40 \ 50}$$

$$\frac{2.8}{2.8} \left| \begin{array}{l} 6.8 \\ C.O.5 \end{array} \right.$$

$$\frac{11.6}{F4.2} \left| \begin{array}{l} 28.4 \\ 28.4 \end{array} \right.$$

$$\frac{12.0 \ 12.0 \ 11.4 \ 10.4 \ 7.6 \ 40.3}{40 \ 36 \ 26 \ 17 \ 13 \ 7.1}$$

$$\frac{7.7 \ 10.2 \ 10.1 \ 9.7 \ 9.1}{11 \ 15 \ 28 \ 40 \ 50}$$

$$\frac{2.5}{2.5} \left| \begin{array}{l} 10.2 \\ F2.8 \end{array} \right.$$

$$\frac{11.7}{F4.1} \left| \begin{array}{l} 28.2 \\ 28.2 \end{array} \right.$$

$$\frac{12.1 \ 11.9 \ 11.4 \ 7.9 \ 40.3 \ 8.0 \ 10.0 \ 10.0 \ 9.7 \ 9.1 \ 7.9}{40 \ 30 \ 19 \ 14 \ 7.3 \ 11 \ 15 \ 23 \ 29 \ 40 \ 50}$$

$$\frac{2.4}{2.4} \left| \begin{array}{l} 10.0 \\ F2.4 \end{array} \right.$$

$$\frac{11.8}{F3.9} \left| \begin{array}{l} 27.8 \\ 27.8 \end{array} \right.$$

$$\frac{11.8 \ 11.7 \ 11.5 \ 8.0 \ 40.3 \ 8.2 \ 9.9 \ 9.6 \ 9.6 \ 7.4 \ 6.3}{40 \ 31 \ 20 \ 14 \ 7.6 \ 11 \ 14 \ 18 \ 28 \ 40 \ 50}$$

$$\frac{2.2}{2.2} \left| \begin{array}{l} 9.0 \\ F1.1 \end{array} \right.$$

$$\frac{11.5}{F3.6} \left| \begin{array}{l} 27.2 \\ 27.2 \end{array} \right.$$

$$\frac{12.1 \ 11.7 \ 11.4 \ 10.7 \ 6.4 \ 8.2}{40 \ 31 \ 20 \ 17 \ 15 \ 14 \ 7.6}$$

$$\frac{8.0 \ 6.6 \ 10.0 \ 9.4 \ 8.4 \ 7.3 \ 6.1}{10 \ 11 \ 13 \ 23 \ 29 \ 40 \ 50}$$

$$\frac{2.4}{2.4} \left| \begin{array}{l} 9.3 \\ C.O.3 \end{array} \right.$$

$$\frac{11.2}{F3.4} \left| \begin{array}{l} 26.8 \\ 26.8 \end{array} \right.$$

$$\frac{11.8 \ 11.4 \ 11.0 \ 8.2}{40 \ 28 \ 19 \ 14 \ 7.5}$$

$$\frac{8.1 \ 9.4 \ 9.8 \ 9.1 \ 7.5 \ 5.3}{10 \ 13 \ 21 \ 29 \ 40 \ 50}$$

$$\frac{2.4}{2.4} \left| \begin{array}{l} 9.5 \\ C.O.0 \end{array} \right.$$

$$\frac{10.8}{F3.0} \left| \begin{array}{l} 26.0 \\ 26.0 \end{array} \right.$$

$$\frac{11.3 \ 11.2 \ 10.5 \ 8.3}{45 \ 32 \ 18 \ 14 \ 7.5}$$

$$\frac{7.9 \ 8.9 \ 8.9 \ 7.6 \ 6.7 \ 5.6 \ 4.4 \ 3.9 \ 5.6}{11 \ 14 \ 16 \ 19 \ 25 \ 29 \ 40 \ 43 \ 50}$$

$$\frac{3.2}{3.2} \left| \begin{array}{l} 5.4 \\ C2.6 \end{array} \right.$$

30 ft Rt of 79 + 15 Spike in Tel Pole.

2/19/34

$$\frac{5.0}{C.O.5} \left| \begin{array}{l} 25.0 \\ 25.0 \end{array} \right.$$

$$\frac{4.5 \ 4.4 \ 5.2 \ 5.0 \ 2.8}{40 \ 36 \ 30 \ 18 \ 14 \ 3.5}$$

$$\frac{3.8 \ 3.6 \ 2.1 \ 1.0 \ 1.4 \ 2.0 \ 2.2}{11 \ 15 \ 18 \ 30 \ 42 \ 46 \ 50}$$

$$\frac{3.3}{3.3} \left| \begin{array}{l} 9.6 \\ C1.4 \end{array} \right.$$

$$\frac{3.3}{C1.0} \left| \begin{array}{l} 29.0 \\ 29.0 \end{array} \right.$$

$$\frac{2.7 \ 2.4 \ 3.2 \ 3.3 \ 4.1 \ 4.7 \ 4.0}{40 \ 28 \ 30 \ 17 \ 16 \ 14 \ 13 \ 3.8}$$

$$\frac{4.2 \ 2.7 \ 1.8 \ 1.1 \ 1.8}{11 \ 17 \ 30 \ 40 \ 50}$$

$$\frac{3.2}{3.2} \left| \begin{array}{l} 4.7 \\ C2.6 \end{array} \right.$$

$$\frac{1.1 \ 1.2 \ 1.8 \ 2.4 \ 3.1 \ 4.1 \ 4.3 \ 4.3}{40 \ 34 \ 31 \ 19 \ 17 \ 15 \ 14 \ 12 \ 4.0}$$

$$\frac{4.3 \ 4.3 \ 4.6 \ 4.2 \ 3.9 \ 3.9 \ 3.4}{11 \ 13 \ 15 \ 25 \ 34 \ 40 \ 50}$$

78

4.6

+24

4.7

+50

5.1

+80

5.1

79

4.4

+28

+33

+50

+65

+75

80

+35

5.7

+50

6.3

7.8

2/19/34

$$\frac{1.9}{02.7} \bigg| \frac{22.2}{2}$$

$$\frac{1.3}{40} \frac{1.3}{37} \frac{2.0}{32} \frac{2.5}{26} \frac{2.8}{19} \frac{5.0}{14} \frac{5.0}{15} \frac{4.9}{13} \frac{4.1}{4.1}$$

$$\frac{4.5}{10} \frac{5.7}{17} \frac{4.7}{19} \frac{4.6}{30} \frac{4.9}{40} \frac{4.0}{50}$$

$$\frac{26}{4} \bigg| \frac{4.9}{26.12}$$

$$\frac{3.1}{01.6} \bigg| \frac{30.2}{2}$$

$$\frac{2.7}{40} \frac{2.5}{34} \frac{3.2}{31} \frac{3.6}{18} \frac{5.3}{14} \frac{5.3}{14} \frac{4.6}{14} \frac{4.2}{4.2}$$

$$\frac{4.6}{12} \frac{5.3}{14} \frac{6.0}{23} \frac{6.0}{30} \frac{6.1}{40} \frac{5.9}{50}$$

$$\frac{24}{4} \bigg| \frac{6.0}{26.02}$$

$$\frac{2.7}{00.4} \bigg| \frac{27.8}{2}$$

$$\frac{4.4}{40} \frac{4.3}{34} \frac{4.6}{33} \frac{4.7}{27} \frac{4.3}{20} \frac{4.9}{17} \frac{6.8}{16} \frac{6.8}{14} \frac{5.0}{13} \frac{4.6}{4.6}$$

$$\frac{4.8}{11} \frac{5.0}{13} \frac{4.6}{15} \frac{4.6}{24} \frac{5.0}{37} \frac{5.4}{45} \frac{5.5}{50}$$

$$\frac{27.8}{4} \bigg| \frac{4.7}{26.04}$$

$$\frac{6.1}{00.00} \bigg| \frac{24.0}{2}$$

$$\frac{6.2}{40} \frac{6.0}{34} \frac{6.3}{26} \frac{6.8}{19} \frac{6.0}{16} \frac{5.7}{14} \frac{5.1}{12} \frac{4.6}{4.6}$$

$$\frac{4.9}{11} \frac{4.9}{13} \frac{4.2}{16} \frac{4.1}{26} \frac{4.5}{35} \frac{4.8}{45} \frac{4.8}{50}$$

$$\frac{6.7}{40} \frac{6.7}{36} \frac{6.7}{29} \frac{5.6}{24} \frac{4.8}{18} \frac{4.3}{13} \frac{4.3}{4.3}$$

$$\frac{4.5}{12} \frac{4.8}{24} \frac{4.6}{24} \frac{4.6}{34} \frac{3.4}{4.3} \frac{5.0}{5.0}$$

$$\frac{26.1}{4} \bigg| \frac{4.9}{26.12}$$

$$\frac{6.5}{52} \frac{2.8}{40} \frac{2.8}{30} \frac{3.0}{20} \frac{2.8}{10} \frac{2.8}{2.8}$$

$$\frac{2.8}{10} \frac{3.0}{20} \frac{3.1}{26} \frac{4.4}{32} \frac{4.6}{40}$$

$$\frac{2.7}{40} \frac{2.8}{30} \frac{2.8}{20} \frac{2.7}{10} \frac{2.8}{2.8}$$

$$\frac{2.6}{10} \frac{2.8}{20} \frac{2.9}{30} \frac{2.4}{40}$$

$$\frac{2.8}{40} \frac{2.8}{30} \frac{2.7}{20} \frac{2.7}{10} \frac{2.7}{2.7}$$

$$\frac{2.7}{10} \frac{2.7}{20} \frac{2.6}{30} \frac{2.6}{40}$$

$$\frac{3.0}{40} \frac{2.7}{30} \frac{2.9}{20} \frac{2.8}{10} \frac{2.8}{2.8}$$

$$\frac{2.8}{10} \frac{2.9}{20} \frac{2.9}{30} \frac{2.8}{40}$$

$$\frac{4.2}{42} \frac{3.1}{35} \frac{2.2}{20} \frac{2.1}{20} \frac{3.0}{10} \frac{2.9}{2.9}$$

$$\frac{3.1}{10} \frac{3.3}{20} \frac{3.0}{25} \frac{3.2}{32} \frac{4.8}{40}$$

$$\frac{3.4}{40} \frac{3.9}{32} \frac{6.9}{24} \frac{4.8}{16} \frac{4.8}{3.7}$$

$$\frac{4.0}{12} \frac{4.5}{22} \frac{4.9}{35} \frac{5.4}{40}$$

$$\frac{6.1}{00.11} \bigg| \frac{26.2}{2}$$

$$\frac{3.3}{42} \frac{4.2}{36} \frac{6.0}{27} \frac{8.2}{19} \frac{8.1}{17} \frac{6.2}{14} \frac{5.6}{12} \frac{5.2}{5.2}$$

$$\frac{5.7}{10} \frac{6.0}{14} \frac{6.1}{17} \frac{7.7}{21} \frac{5.0}{24} \frac{4.2}{38} \frac{4.5}{40} \frac{4.3}{50}$$

$$\frac{29.0}{4} \bigg| \frac{4.7}{26.10}$$

$$\frac{6.7}{00.11} \bigg| \frac{26.2}{2}$$

$$\frac{4.0}{40} \frac{5.8}{32} \frac{6.9}{25} \frac{8.8}{18} \frac{8.8}{16} \frac{6.8}{14} \frac{6.3}{12} \frac{5.8}{5.8}$$

$$\frac{6.3}{10} \frac{6.8}{13} \frac{8.7}{17} \frac{8.7}{22} \frac{4.1}{25} \frac{5.8}{36} \frac{5.5}{50}$$

$$\frac{27.4}{4} \bigg| \frac{6.1}{26.02}$$

81

7.4

8.9

+25

7.4

7.6

9.1

+50

7.5

T.P.

9.99

1003.54

82

5.04

1008.58

3.2 Lt

5.64

1009.18

2.4 Rt

+36

51' 24" C.M.P.

Extension Required
Rt Side 14 ft
Lt " 14 "

3.9

+50

4.2

83

4.6

+49

End of 2-Strand Barbed Wire fence Rt

+50

Good Galv Wire

3.6

3" Posts

3

84

1.5

3

0.57

1008.61

+50

5.40

1014.01

4.8

3

85

3.4

1

+25

3.0

9.5

T.P.

0.49

1012.52

1

End of

2/19/34

$$\frac{7.6}{D6.13} \left| \frac{1.6}{2} \right.$$

$$\frac{40}{40} \frac{67}{32} \frac{20}{25} \frac{95}{19} \frac{95}{17} \frac{25}{13} \frac{7.5}{6.9} \frac{7.4}{11} \frac{7.7}{15} \frac{9.5}{19} \frac{9.5}{22} \frac{26}{24} \frac{28}{38} \frac{2.7}{50}$$

$$\frac{27.2}{2} \left| \frac{7.3}{D6.16} \right.$$

$$\frac{9.3}{F1.9} \left| \frac{23.8}{2} \right.$$

$$\frac{40}{40} \frac{27}{35} \frac{88}{27} \frac{102}{19} \frac{24}{11} \frac{7.1}{7.1} \frac{7.6}{11} \frac{7.7}{14} \frac{10.4}{20} \frac{9.4}{24} \frac{9.6}{32} \frac{11.2}{42} \frac{11.6}{50}$$

$$\frac{24}{24} \left| \frac{9.6}{D6.00} \right.$$

$$\frac{11.2}{F3.7} \left| \frac{27.4}{2} \right.$$

$$\frac{40}{40} \frac{11.5}{33} \frac{11.6}{20} \frac{11.1}{12} \frac{7.5}{7.2} \frac{7.6}{10} \frac{7.7}{12} \frac{13.0}{26} \frac{14.4}{37} \frac{12.0}{43} \frac{15.7}{50}$$

$$\frac{83.4}{83.4} \left| \frac{14.2}{F6.7} \right.$$

On Lt 6/ope Stake 81+50

$$\frac{12.7}{F9.5} \left| \frac{29.0}{2} \right.$$

$$\frac{40}{40} \frac{12.8}{33} \frac{12.0}{27} \frac{3.4}{12} \leftarrow 2.9 \frac{2.4}{2.1} \frac{3.1}{12} \frac{7.2}{15} \frac{11.5}{20} \frac{11.9}{29} \frac{10.9}{40}$$

$$\frac{37.2}{37.2} \left| \frac{11.0}{F8.6} \right.$$

$$\frac{13.3}{F9.4} \left| \frac{38.8}{2} \right.$$

$$\frac{40}{40} \frac{13.3}{34} \frac{13.3}{33} \frac{14.6}{25} \frac{14.7}{25} \frac{E.C.}{13} \frac{4.3}{11} \frac{4.1}{3.6} \frac{4.1}{12} \frac{E.C.}{26} \frac{14.8}{26} \frac{14.5}{30} \frac{15.7}{32} \frac{13.4}{40}$$

$$\frac{38.6}{38.6} \left| \frac{13.2}{F9.3} \right.$$

$$\frac{14.6}{F10.4} \left| \frac{40.8}{2} \right.$$

$$\frac{50}{50} \frac{14.1}{42} \frac{13.6}{42} \frac{14.6}{40} \frac{14.5}{36} \frac{12.8}{31} \frac{12.0}{24} \frac{11.8}{13} \frac{4.5}{11} \frac{4.2}{3.9} \frac{4.3}{12} \frac{8.4}{22} \frac{12.7}{26} \frac{13.7}{33} \frac{13.6}{40}$$

$$\frac{38.8}{38.8} \left| \frac{13.6}{F9.4} \right.$$

$$\frac{13.5}{F8.9} \left| \frac{37.8}{2} \right.$$

$$\frac{40}{40} \frac{13.5}{36} \frac{13.4}{26} \frac{12.4}{12} \frac{4.7}{4.8} \frac{4.7}{12} \frac{11.7}{24} \frac{13.0}{32} \frac{13.3}{40}$$

$$\frac{37.2}{37.2} \left| \frac{13.2}{F8.6} \right.$$

$$\frac{13.7}{F10.1} \left| \frac{40.2}{2} \right.$$

$$\frac{40}{40} \frac{13.7}{36} \frac{13.6}{28} \frac{12.0}{18} \frac{3.7}{3.3} \frac{3.7}{12} \frac{4.7}{16} \frac{12.5}{30} \frac{13.4}{36} \frac{13.5}{40}$$

$$\frac{39.8}{39.8} \left| \frac{12.5}{F9.9} \right.$$

$$\frac{13.6}{F12.1} \left| \frac{44.2}{2} \right.$$

$$\frac{40}{40} \frac{13.5}{36} \frac{12.3}{30} \frac{11.9}{13} \frac{1.9}{12} \frac{1.6}{1.2} \frac{1.4}{11} \frac{1.8}{16} \frac{11.8}{33} \frac{12.0}{41}$$

$$\frac{43.2}{43.2} \left| \frac{13.1}{F11.6} \right.$$

Top of Stake 12ft Rt of 84+70

$$\frac{16.9}{F12.1} \left| \frac{44.2}{2} \right.$$

$$\frac{44}{44} \frac{16.9}{31} \frac{16.4}{15} \frac{5.3}{12} \frac{4.8}{4.5} \frac{4.7}{11} \frac{5.5}{18} \frac{14.9}{35} \frac{15.3}{42}$$

$$\frac{41.0}{41.0} \left| \frac{15.3}{F10.5} \right.$$

$$\frac{10.6}{F9.2} \left| \frac{34.4}{2} \right.$$

$$\frac{40}{40} \frac{11.0}{33} \frac{10.4}{28} \frac{10.1}{18} \frac{4.3}{13} \frac{3.6}{3.1} \frac{3.5}{12} \frac{4.7}{18} \frac{8.6}{25} \frac{10.0}{34} \frac{9.4}{40} \frac{2.0}{50}$$

$$\frac{33.0}{33.0} \left| \frac{9.9}{F6.5} \right.$$

$$\frac{4.5}{D6.00} \left| \frac{24.0}{2} \right.$$

$$\frac{40}{40} \frac{5.3}{34} \frac{5.0}{28} \frac{4.4}{20} \frac{4.6}{15} \frac{3.4}{13} \frac{3.1}{2.5} \frac{2.9}{11} \frac{3.3}{16} \frac{3.8}{19} \frac{3.3}{23} \frac{2.7}{31} \frac{2.0}{40} \frac{1.6}{50}$$

$$\frac{2.7}{2.7} \left| \frac{3.0}{0.0} \right.$$

On Stake 40ft Rt 85+25

T.P.

10.86 1024.38

1018.52

85+50

12.7

86

11.3

T.P.

4.93

1027.67

1.64

1022.74

+30

13.9

+50

$$\frac{11}{5} \text{ Post}$$

$$\frac{19}{19}$$

13.3

87

+34

End of 2 Wire 3" Posts

11.9

Add 24-ft Cross Fence.
 Cor of Woven Wire Fence - 1 strand Barb
 Good 6" Posts
 Poor Wire

+50

10.9

88

10.3

+30

+50

10.1

89

10.2

+50

10.7

90

11.4

+50

12.4

Top of Stake 40' Rt 85+2.5

2/20/34

9.6
C31.8

106 10.9 9.6 1.5 12.2 13.5 12.9 12.8
40 33 33 2.9 23 17 15 13 12.2

12.8 12.6 13.5 9.1 9.8 9.6 9.7 13.5 12.6
12 17 24 32 43 50 53 60 67

34.2
10 23
C3.5

3.6
C7.7

F
4.2 3.1 2.5 1.0 12.0 11.5
50 38 34 28 17 14 10.8

11.3 12.3 12.6 2.3 2.2 22 3.0 14.7
11.0 15 27 38 44 50 54 69

4.4
2.6
C8.7

on Rt Slope Stake 86+00

7.1 9.0 3.2 2.9 13.0 14.4 13.9 12.6 13.8 14.5 12.8 3.6 3.5 3.8 17.3
50 9.7 39 34 22 17 14 13.4 11 13 15 23 35 42 51 70

2.9
C10.4

F
2.9 2.4 2.1 12.0 13.6 13.3 13.1 14.0 11.5 3.2 3.0 3.3 17.1
46 40 35 24 17 14 12.8 14 16 26 34 43 50 71

4.7
3.1
C10.2

2.2
C9.7

F
2.2 2.2 11.4 12.1 11.9 11.8 12.6 11.3 2.6 2.4 2.8 7.9 11.0 17.1
40 32 20 16 14 11.4 13 17 27 36 42 50 56 62 71

4.0
2.4
C9.5

2.2
C8.7

F
2.2 2.0 3.1 10.6 11.0 10.8 10.1 1.9 1.6 1.9 6.9 11.2 14.7
40 32 28 21 13 10 4 13 22 31 40 46 52 62 71

4.5
1.9
C9.0

2.8
C7.5

F
2.9 3.0 3.3 10.0 10.2 10.4 10.5 2.5 6.5 2.8 3.2 8.6 12.1 16.2
40 32 27 18 14 9.8 13 20 28 33 38 46 53 62 69

4.1
2.8
C7.5

F
3.5 3.4 3.4 9.7 10.4 10.1 10.2 8.8 3.5 3.5 3.7 8.1 11.9 14.0
40 32 28 20 16 14 9.7 14 23 33 39 45 49 59 69

4.0
C6.1

F
4.0 3.8 3.6 9.5 10.3 10.1 10.1 10.5 9.8 4.3 4.1 4.3 8.8 13.7 16.5
40 32 28 20 16 14 9.6 13 16 19 27 35 44 52 62 71

3.9
4.0
C6.1

4.6
C5.6

F
4.6 4.6 4.7 9.3 10.2 10.2 10.6 9.6 4.8 4.8 5.2 14.7 17.1
40 31 26 19 14 9.7 14 16 19 24 36 46 61 71

3.7
5.1
C5.1

5.5
C5.2

F
5.5 5.3 5.6 9.6 10.3 10.7 10.2 11.2 10.6 5.9 6.5 6.5 6.8 13.1 16.5
40 31 26 19 16 13 10.2 14 17 20 24 28 36 49 57 63

3.5
6.4
C4.3

7.0
C4.4

F
7.0 6.7 6.3 10.7 11.2 11.2 11.4 11.6 11.1 11.6 6.8 6.8 12.3 16.6
40 31 28 24 17 15 13 10.9 12 15 18 25 35 45 54 65

3.6
6.7
C4.7

7.6
C4.6

F
7.0 7.7 7.5 12.0 12.2 12.2 12.4 12.4 11.3 7.8 7.2 7.6 16.1
40 31 24 16 14 11 11.9 12 15 20 25 36 49 63

3.7
7.2
C5.2

1027.67

#8 Woven Wire

91

25-6" Posts to here

13.6

T.P.

0.17

1020.11

7.73

1019.94

+50

7.2

92

8.3

+50

9.1

93

10.1

+50

11.3

+75

11.9

+80

Fence Removed to Here Total 41 Posts

94

12.4

B.M.

2.38

1008.77

13.72

1006.39

+50

2.2 Lt
2.0 Rt

95

3.2

+50

4.4

96

5.1

+50

5.7

2/20/34

8.4	8	8.3	7.9	7.9	10.5	12.6	13.5	13.5	13.7	13.3	8.4	8.8	9.4	18.5	36.6	8.8
CS.2	2	40	31	24	21	16	12	13.1	12	15	18	24	36	50	69	24.8

Slope stake Rt Side 91400

$\frac{2.6}{CA.6}$	$\frac{2}{2}$	$\frac{2.5}{40}$	$\frac{2.2}{31}$	$\frac{2.5}{24}$	$\frac{4.3}{22}$	$\frac{6.6}{16}$	$\frac{7.1}{12}$	6.7	$\frac{7.1}{13}$	$\frac{7.6}{16}$	$\frac{3.0}{22}$	$\frac{3.3}{37}$	$\frac{2.5}{50}$	$\frac{10.7}{56}$	$\frac{35.4}{CA.2}$	$\frac{3.0}{66}$

F

4.1	4	4.1	4.1	4.0	4.2	7.7	8.1	8.2	8.3	9.0	3.7	4.2	4.0	4.1	4.9	7.3	11.3	35.8	3.9
CA.2	2	40	34	31	25	18	15	12	7.8	14	16	24	26	36	50	58	64	69	CA.4

F

4.9	4	4.8	4.9	4.6	5.2	7.0	8.3	9.1	9.2	10.0	5.3	5.3	5.2	5.5	8.4	11.0	34.8	5.2
CA.2	2	40	33	31	32	20	15	12	8.6	13	16	22	34	50	58	65	71	CA.9

F

6.5	6	6.5	6.5	6.1	6.6	9.9	10.1	10.2	10.6	6.6	7.0	7.0	6.8	7.2	9.0	12.0	33.6	6.8
CA.6	2	40	33	31	23	16	12	9.6	13	16	21	26	37	50	61	66	72	CA.3

F

8.5	8	8.6	8.3	8.4	8.9	11.1	11.2	11.2	11.9	10.2	9.9	10.2	10.2	10.5	12.9	29.6	10.0
CA.8	2	40	31	26	19	15	13	10.8	13	16	19	28	42	50	64	70	CA.3

F

9.9	10.2	10.4	10.5	11.6	11.6	11.8	13.4	11.8	11.8	12.0	12.1	27.9	11.9
40	31	24	17	14	12	11.4	12	18	25	35	44	50	00

F

11.8	12	11.6	12.0	12.0	12.5	12.2	12.3	14.0	14.1	12.6	11.9	14.2	24.0	13.9
CA.6	2	31	24	18	15	12	11.9	12	18	23	28	37	50	DC.00

Spike in Tel. Pole = 254 + Rt 94465

3.7	3	3.5	3.6	3.7	3.2	2.1	4.2	4.7	4.6	4.5	2.5	4.7
DL.00	2	31	25	18	12	1.7	12	18	29	40	50	4.7

F

5.6	5	5.7	5.6	5.2	3.7	3.3	3.4	5.1	5.0	5.8	6.7	24.6	5.5
F2.4	2	31	28	19	15	13	2.9	12	17	22	27	40	F2.3

F

7.1	7	7.0	7.2	6.8	4.4	4.4	7.2	7.0	7.5	7.8	2.5	7.1
F1.7	2	31	24	19	13	4.1	11	19	26	33	40	F2.7

F

8.1	8	7.9	8.1	7.7	5.3	5.3	7.4	8.2	8.3	8.4	2.6	8.2
F3.0	2	31	25	18	13	4.8	11	17	25	33	40	F3.1

F

9.0	9	8.4	9.0	8.2	6.0	5.8	8.8	9.3	9.2	2.7	9.2
F3.3	2	31	26	19	13	5.4	11	18	28	40	F3.6

97

6.1

+50

6.6

98

6.8

+50

7.0

99

7.0

+50

7.0

100

6.9

T.P.

6.24

1002.53

3.61

1006.14

+50

4.3

+90

End of Fence

101

4.2

+50

4.3

102

4.5

+50

4.7

2/20/34

9.7
F3.6 27.2

F
9.5 9.8 9.1 6.4 6.2 9.4 10.1 10.2 10.2
31 25 19 13 5.8 11 18 25 34 40

28.2 10.2
F4.1

10.0
F3.4 26.8

F
9.7 10.2 9.6 6.2 6.7 7.1 10.5 10.8 11.0
31 24 19 13 6.3 10 12 19 27 40

28.8 11.0
F4.4

10.0
F3.2 26.4

F
9.8 10.1 9.8 7.2 6.9 10.2 11.0 10.9 11.0
31 23 18 13 6.5 11 19 27 35 40

28.4 11.0
F4.2

10.0
F3.0 26.0

F
9.6 10.0 11.1 9.5 7.2 7.1 9.6 10.4 10.4 10.4
31 26 23 17 13 6.7 11 17 27 34 40

26.8 10.4
F3.4

10.0
F3.0 26.0

F
9.4 10.0 11.2 9.7 7.2 7.0 10.0 9.8 10.2 10.2
31 26 22 18 13 6.7 11 19 28 30 40

26.0 10.0
F3.0

9.8
F2.8 25.6

F
8.8 9.5 11.0 9.7 7.0 7.1 7.3 9.6 10.0 9.6 10.4 10.1
31 26 22 19 13 6.7 10 13 18 25 27 31 40

25.8 9.9
F2.9

9.4
F2.5 25.0

F
8.4 9.2 10.5 10.8 9.7 7.1 7.2 10.0 9.5 10.1 9.8
32 26 24 22 19 13 6.6 12 21 28 31 40

25.8 9.8
F2.9

On Guard Stake Sta 100+00

2/21/34

7.2
F2.9 25.8

F
5.7 5.4 7.3 7.9 8.0 7.0 4.4 4.5 4.5 5.1 8.6 9.0 6.5 7.5 7.7 6.5 6.2
32 28 25 24 20 18 14 11 4.0 11 14 18 23 27 30 32 34 40

28.0 8.2
F4.0

6.4
F2.6 25.2

6.1 5.9 8.0 8.2 7.1 4.5 4.6 8.4 6.6 8.5 6.7 7.1 6.2 6.0
40 27 24 20 17 12 3.9 12 18 24 25 28 32 34 40

26.5 7.5
F3.3

6.1
F2.4 24.8

6.3 5.6 8.0 8.0 7.2 4.5 4.6 4.8 8.0 8.4 7.3 7.1 8.0 7.1 9.3
40 27 23 20 16 13 4.0 10 13 18 24 27 30 32 35 40

26.1 7.4
F3.1

7.6
F3.1 26.2

6.3 6.4 7.7 7.7 8.5 8.5 7.5 6.0 4.5 4.5 8.2 8.0 8.3 7.8 8.2 8.5 8.0 8.0
40 30 28 24 25 23 21 16 12 4.2 11 18 21 25 26 30 32 35 40

26.0 7.8
F3.3

8.3
F3.6 27.2

6.5 7.1 8.8 9.7 9.8 4.6 7.7 8.0 8.0 8.8 8.2 8.3
42 28 25 19 12 4.4 11 17 19 28 31 35 40

26.5 8.0
F3.3

103

4.7

+50

4.7

104

4.3

+11

Extension Required
 Rt. side 15 ft.
 31 ft 1' X 2' Limestone box 4' 12"

4.2

+50

4.1

105

4.0

+40

4.0

+50

+60

+85

4 Snelling Ave.

3.7

B.M.

3.87

1002.27

+85

$$\frac{8.2}{F3.5} \bigg| 27.0$$

$$\frac{4.5 \ 7.2 \ 8.2 \ 8.4 \ 8.0 \ 4.9}{45 \ 34 \ 27 \ 24 \ 19 \ 13 \ 4 \ 4} \quad \frac{4.7 \ 8.6 \ 9.2 \ 9.7 \ 9.7}{11 \ 18 \ 25 \ 34 \ 40}$$

$$\frac{29.6}{F4.8} \bigg| 9.5$$

$$\frac{7.7}{F3.0} \bigg| 26.0$$

$$\frac{4.5 \ 6.8 \ 7.6 \ 8.0 \ 8.2 \ 5.7 \ 4.7}{40 \ 31 \ 27 \ 23 \ 19 \ 16 \ 11 \ 4.4} \quad \frac{4.8 \ 8.6 \ 9.5 \ 10.0 \ 10.5}{11 \ 18 \ 26 \ 33 \ 40}$$

$$\frac{30.4}{F5.2} \bigg| 9.9$$

$$\frac{7.3}{F3.0} \bigg| 26.0$$

$$\frac{6.2 \ 7.1 \ 7.8 \ 8.2 \ 7.8 \ 4.4}{40 \ 27 \ 24 \ 22 \ 20 \ 12 \ 4.0} \quad \frac{4.5 \ 8.6 \ 9.6 \ 10.2}{11 \ 18 \ 27 \ 40}$$

$$\frac{31.0}{F5.5} \bigg| 9.8$$

$$\frac{7.5}{F3.3} \bigg| 26.6$$

$$\frac{6.1 \ 6.8 \ 7.7 \ 8.5 \ 9.6 \ 5.6 \ 4.7}{40 \ 31 \ 25 \ 22 \ 15 \ 15 \ 12 \ 3.9} \quad \frac{4.3 \ 4.8 \ 5.6 \ 9.3 \ 9.3 \ 10.1}{8 \ 12 \ 16 \ 18 \ 28 \ 40}$$

$$\frac{30.8}{F5.4} \bigg| 9.6$$

$$\frac{7.2}{F3.6} \bigg| 27.2$$

$$\frac{4.6 \ 7.0 \ 7.9 \ 8.3 \ 8.0 \ 4.2}{40 \ 32 \ 26 \ 23 \ 19 \ 13 \ 3.8} \quad \frac{4.0 \ 8.6 \ 10.0 \ 10.5 \ 10.8}{10 \ 17 \ 23 \ 31 \ 40}$$

$$\frac{32.8}{F6.4} \bigg| 10.5$$

$$\frac{7.9}{F3.9} \bigg| 27.8$$

$$\frac{7.2 \ 7.4 \ 8.0 \ 8.9 \ 8.0 \ 4.4}{40 \ 34 \ 27 \ 21 \ 18 \ 12 \ 3.7} \quad \frac{4.0 \ 4.7 \ 9.8 \ 10.5 \ 11.1}{9 \ 11 \ 20 \ 31 \ 40}$$

$$\frac{33.2}{F6.6} \bigg| 10.6$$

$$\frac{7.8}{F3.3} \bigg| 26.6$$

$$\frac{8.7 \ 7.7 \ 7.5 \ 4.4}{40 \ 29 \ 31 \ 13 \ 3.7} \quad \frac{4.3 \ 4.8 \ 9.8 \ 10.8 \ 11.2}{10 \ 12 \ 21 \ 31 \ 40}$$

$$\frac{33.6}{F6.8} \bigg| 11.0$$

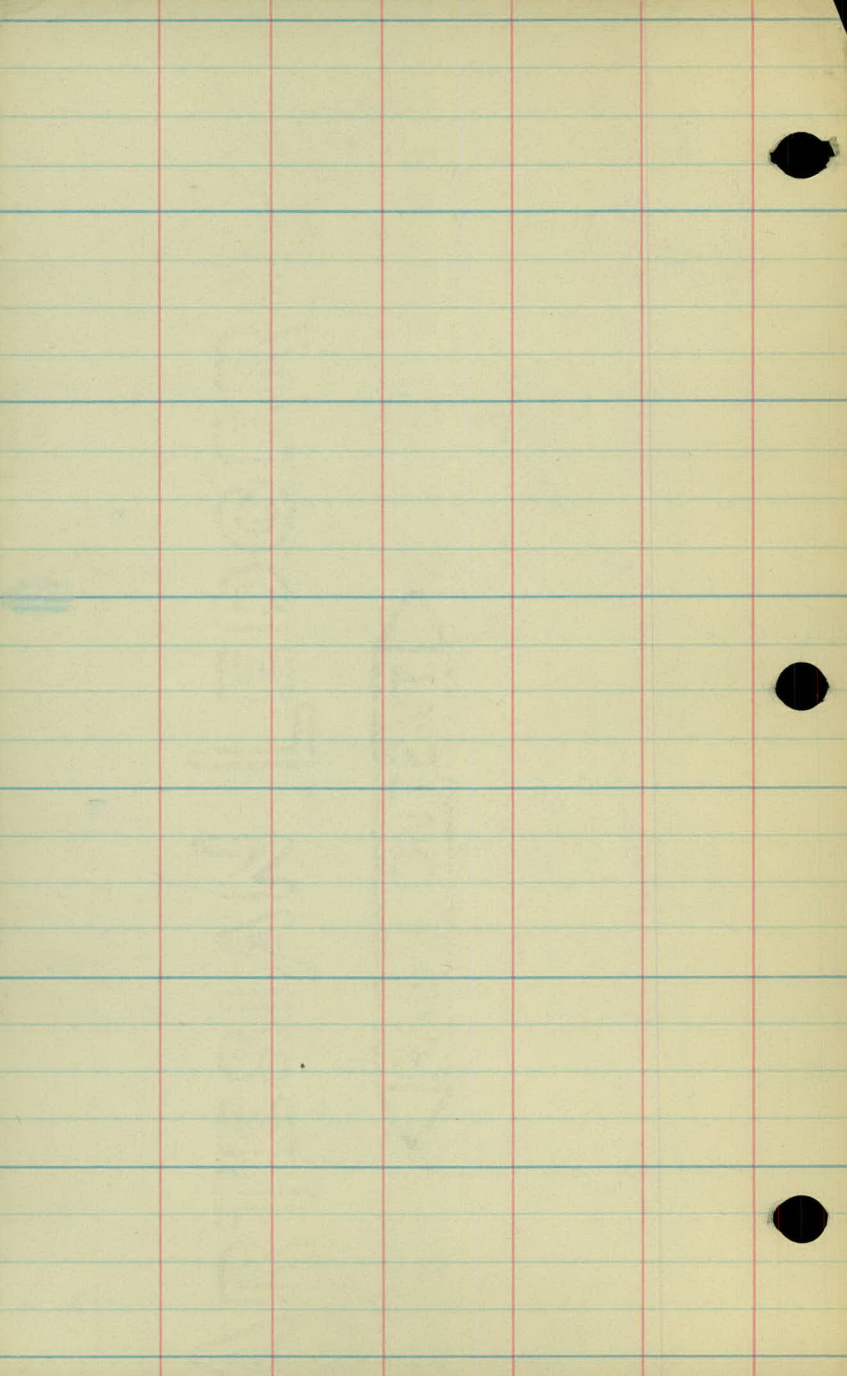
$$\frac{8.0 \ 7.0 \ 4.2 \ 4.1}{40 \ 32 \ 24 \ 13 \ 3.7} \quad \frac{4.6 \ 9.8 \ 10.7 \ 11.1}{11 \ 23 \ 29 \ 40}$$

$$\frac{4.1 \ 3.9 \ 4.1 \ 2.8}{40 \ 30 \ 21 \ 12 \ 3.6} \quad \frac{4.1 \ 4.9 \ 9.5 \ 10.8 \ 11.1}{10 \ 12 \ 21 \ 31 \ 40}$$

$$\frac{3.4 \ 3.5 \ 3.4 \ 3.4}{40 \ 30 \ 20 \ 10 \ 3.4} \quad \frac{4.1 \ 4.7 \ 9.8 \ 10.8 \ 10.9}{10 \ 12 \ 23 \ 33 \ 40}$$

$$\frac{34.0}{F7.0} \bigg| 10.7$$

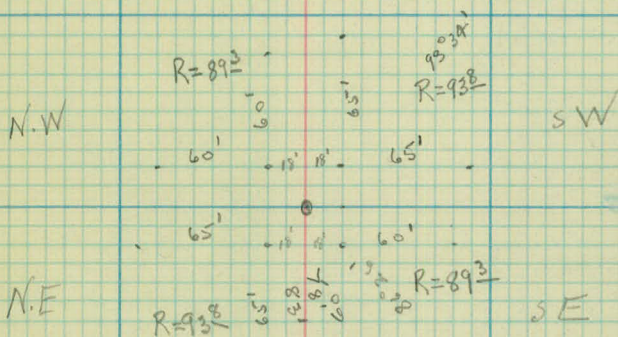
Spike in Tel Pole #18738R

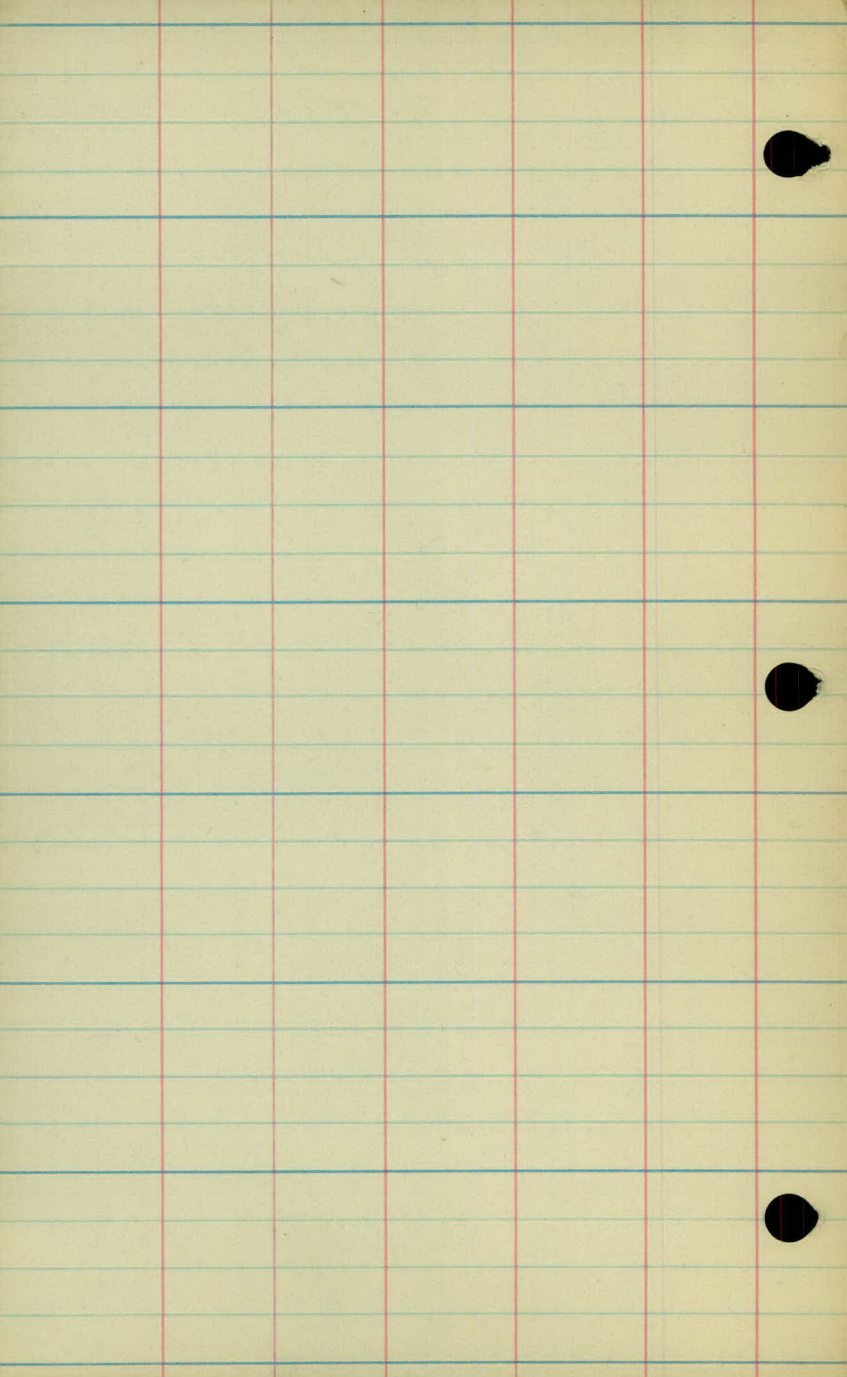


$$S.W \quad 0 = 78 + 67$$

$$S.E \quad 0 = 80 + 25$$

$$N.E \quad 0 = 80 + 30$$





County Road "C" - Cleveland Ave West.
Radii at Co Rd "C" & New Brighton Rd.

B.M

5.86 10/6.39

10/11.03

North West

D.C.

$$0+00 = 78+72-18F+Lr$$

7.8

9.5

0+20

7.36

9.1

0+40

6.92

8.6

0+60

6.48

8.2

0+84

6.0

7.7

South West

$$0+00 = 78+67-18F+Rt$$

7.8

9.5

0+20

7.34

9.0

0+40

6.88

8.6

0+60

6.42

8.1

0+80

5.96

7.7

0+95

5.6

7.3

50% in 100 ft

30' R+79+15

2/26/34
Radii at Intersection New Brighton Rd

Northwest Corner

$$\frac{8.2}{D.C.10} \quad 7.5$$

$$\frac{F.2.2}{9.6}$$

$$\frac{9.6}{F.2.7}$$

$$\frac{9.6}{F.3.1}$$

$$\frac{9.6}{F.3.6} \quad 5.7$$

$$7.5 \quad \frac{7.1}{D.C.1.4}$$

$$\frac{7.2}{D.C.4.8}$$

$$\frac{7.1}{D.C.1.5}$$

$$\frac{6.5}{D.C.1.6}$$

$$\frac{5.7}{D.C.2.0}$$

$$5.5$$

South East

0+00 =	80+25-18FtRt	7.9	9.4
0+20		7.34	9.0
0+40		6.78	8.5
0+60		6.22	7.9
0+84		5.6	7.3

North East

0+00 =	80+30-18FtLt	8.15	9.9
0+20		7.71	9.4
0+40		7.27	9.0
0+60		6.83	8.5
0+80		6.39	8.1
0+95		6.0	7.7

2/26/34

$$\begin{array}{r} 7.1 \\ 61.0 \overline{) 0} \end{array}$$

$$\begin{array}{r} 7.4 \\ 86 \overline{) 6.6} \end{array}$$

$$\begin{array}{r} 8.5 \\ 86.00 \overline{) 0} \end{array}$$

$$\begin{array}{r} 6.8 \\ 86.11 \overline{) 0} \end{array}$$

5.3

7.85

$$\begin{array}{r} 9.2 \\ 86.07 \overline{) 0} \end{array}$$

$$\begin{array}{r} 7.6 \\ 86.16 \overline{) 0} \end{array}$$

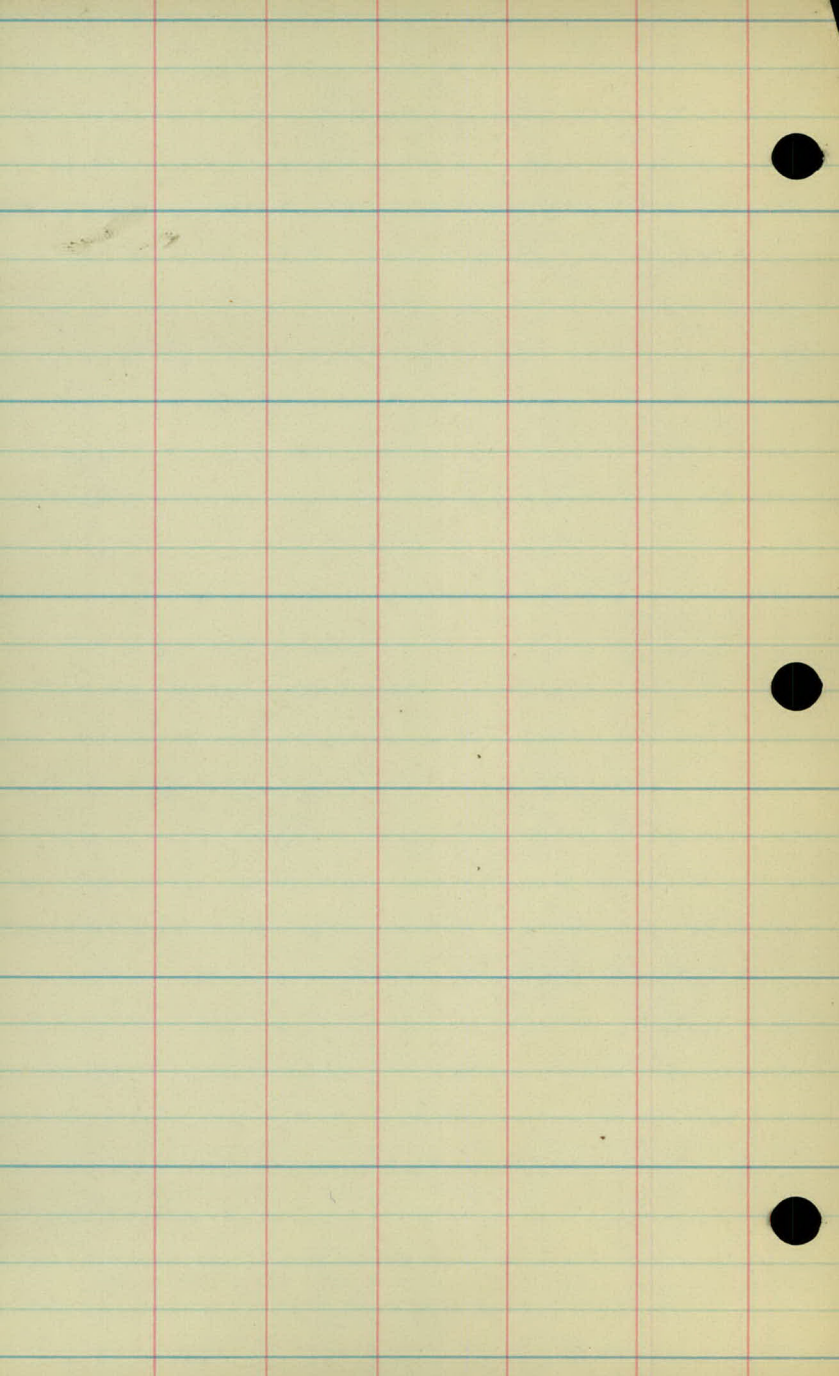
$$\begin{array}{r} 6.2 \\ 86.27 \overline{) 0} \end{array}$$

$$\begin{array}{r} 6.3 \\ 86.22 \overline{) 0} \end{array}$$

$$\begin{array}{r} 6.1 \\ 86.12 \overline{) 0} \end{array}$$

5.7

D.C.O.O



County Road "C" - Cleveland Ave West
Alignment - Snelling to Hamline
Station 105+86¹ to 132+07²

Station	Point	$\angle L+$	$\angle R+$	$\angle +$	$R+$
---------	-------	-------------	-------------	------------	------

132+07 ⁸	P.I.				
---------------------	------	--	--	--	--

120+00 ¹⁷	P.T.	0° 58'			
----------------------	------	--------	--	--	--

+50		0° 43'			
-----	--	--------	--	--	--

119+03 ⁵²	P.I.				
----------------------	------	--	--	--	--

119		0° 28'			
-----	--	--------	--	--	--

+50		0° 13'			
-----	--	--------	--	--	--

118+06 ⁶⁴	P.G.	0° 00'			
----------------------	------	--------	--	--	--

106+86 ¹	P.I.				
---------------------	------	--	--	--	--

			0° 21' R		
--	--	--	----------	--	--

$\Delta 1^{\circ} 56'$

$D 1^{\circ} 00' L$

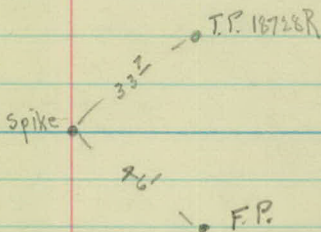
$T 96.68$

$\angle 193^{\circ} 33'$

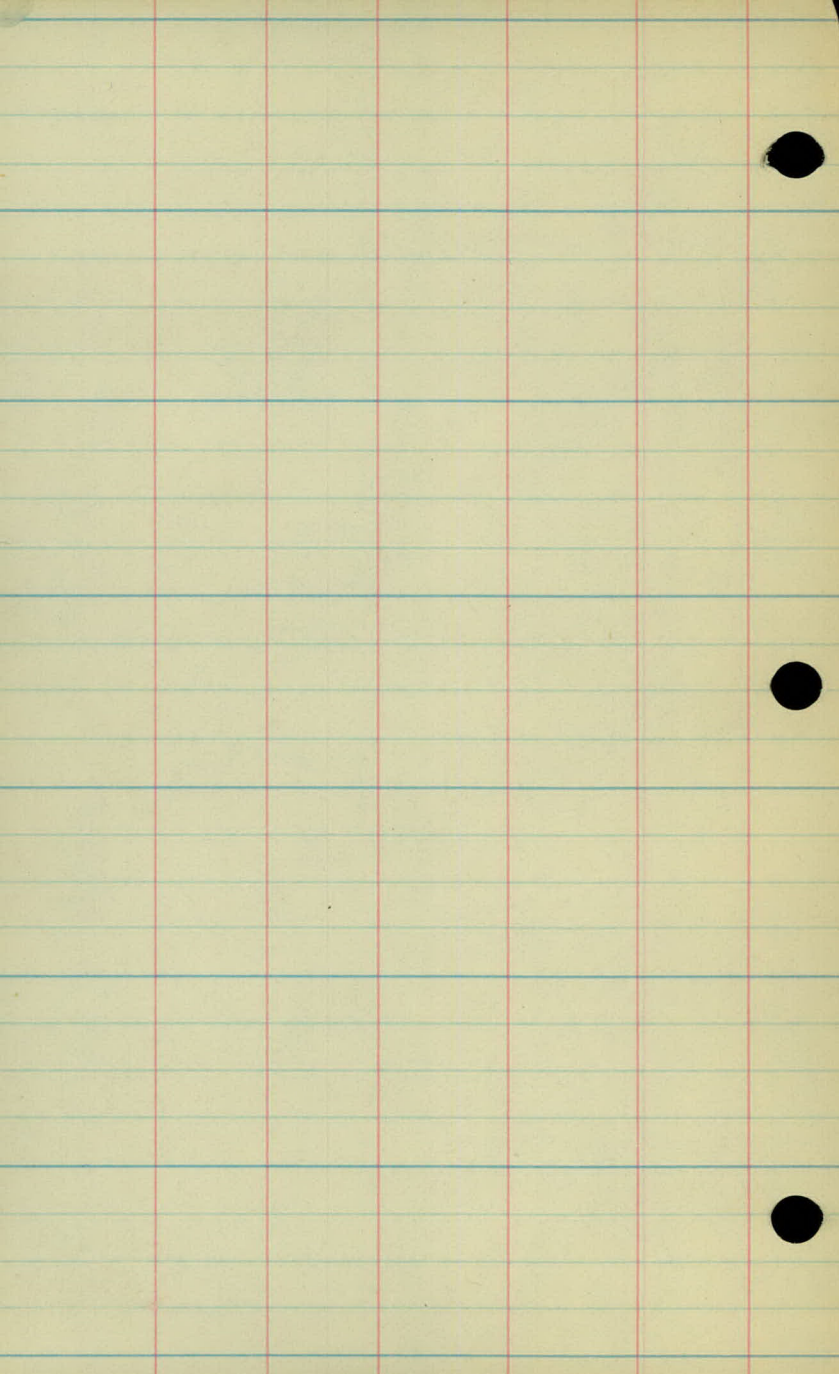
$R. 5729.58$

Hamline Ave.

Monument



Snelling Ave.



County Road "C" Cleveland Ave West

Restaking Rt Side Ex'n on 10:1 Slope

Station 54+00 to 62+80

" 66+50 to 74+00

" 75+33 " 78+24

" 85+25 " 94+00

Restaking Rt Side Ex'n on 4:1 Slope

Station 80+35 " 81+25

Restaking Right Side County Rd "C" Excn on Daylight Slope
B.M. Assumed. 1000.00

54+00	29	8.4
+50	5.7	7.2
55+00	48	6.3
	6.	
57.+50	1.45	7.95
58	5.25	6.75
+50	4.0	5.5
59	3.0	4.5
+50	10.2	11.7
60	9.3	10.8
+50	8.6	10.1
61	8.4	9.9

Re Staking County "C" Excn on Daylight Slope
Spike in Oak Tree 35 ft of 52+70 3/12/34

$$6.4 \quad \begin{array}{r} 390 \overline{) 71} \\ \underline{76.1.3} \end{array}$$

$$5.2 \quad \begin{array}{r} 640 \overline{) 34} \\ \underline{76.38} \end{array}$$

$$4.3 \quad \begin{array}{r} 34 \overline{) 4.3} \\ \underline{76.00} \end{array}$$

$$5.95 \quad \begin{array}{r} 501 \overline{) 5.6} \\ \underline{76.624} \end{array}$$

$$4.75 \quad \begin{array}{r} 401 \overline{) 5.4} \\ \underline{76.114} \end{array}$$

$$3.5 \quad \begin{array}{r} 330 \overline{) 4.8} \\ \underline{76.07} \end{array}$$

$$2.5 \quad \begin{array}{r} 33 \overline{) 3.8} \\ \underline{76.07} \end{array}$$

$$9.7 \quad \begin{array}{r} 510 \overline{) 9.2} \\ \underline{76.2.5} \end{array}$$

$$8.8 \quad \begin{array}{r} 461 \overline{) 8.8} \\ \underline{76.2.0} \end{array}$$

$$8.1 \quad \begin{array}{r} 431 \overline{) 8.1} \\ \underline{76.1.7} \end{array}$$

$$1.9 \quad \begin{array}{r} 430 \overline{) 8.3} \\ \underline{76.1.6} \end{array}$$

61+50

8.4

9.9

62

8.6

10.1

+50

8.8

10.3

+80

9.2

10.7

66+50

7.95

9.95

67

8.3

9.8

+50

8.8

10.3

70

5.2

6.7

+54

5.1

6.6

71

5.1

6.6

+50

5.0

7.6

72

2.9

5.4

$$7.9 \quad \begin{array}{r} 4 \overline{) 8.5} \\ 10 \overline{) D.C. 1.5} \end{array}$$

$$8.1 \quad \begin{array}{r} 4 \overline{) 8.7} \\ 10 \overline{) D.C. 1.4} \end{array}$$

$$8.3 \quad \begin{array}{r} 4 \overline{) 8.4} \\ 10 \overline{) D.C. 1.7} \end{array}$$

$$8.7 \quad \begin{array}{r} 5 \overline{) 8.1} \\ 10 \overline{) D.C. 1.6} \end{array}$$

$$7.45 \quad \begin{array}{r} 6 \overline{) 5.3} \\ 10 \overline{) D.C. 9.2} \end{array}$$

$$7.8 \quad \begin{array}{r} 7 \overline{) 5.4} \\ 10 \overline{) D.C. 9.4} \end{array}$$

$$8.3 \quad \begin{array}{r} 6 \overline{) 6.7} \\ 10 \overline{) D.C. 9.3} \end{array}$$

$$4.7 \quad \begin{array}{r} 3 \overline{) 5.8} \\ 10 \overline{) D.C. 0.9} \end{array}$$

$$4.6 \quad \begin{array}{r} 5 \overline{) 4.2} \\ 10 \overline{) D.C. 2.4} \end{array}$$

$$4.6 \quad \begin{array}{r} 4 \overline{) 5.2} \\ 10 \overline{) D.C. 1.4} \end{array}$$

28' to outside ditch

$$4.5 \quad \begin{array}{r} 4 \overline{) 6.2} \\ 10 \overline{) D.C. 1.3} \end{array}$$

$$2.4 \quad \begin{array}{r} 3 \overline{) 4.4} \\ 10 \overline{) D.C. 1.0} \end{array}$$

72 + 50

3.1

5.4

+ 80

3.4

5.9

73

3.7

+ 52

3.8

5.3

74

4.3

5.8

75 + 33

+ 50

5.25

6.75

76

5.2

6.7

+ 50

5.2

6.7

77

5.5

7.0

+ 50

5.8

7.3

78

6.8

+ 24

1.0

$$2.6 \quad \begin{array}{r} 6 \\ 5 \overline{) 9.9} \\ \underline{5} \\ 4.9 \\ \underline{4} \\ .9 \\ \underline{.5} \\ .4 \\ \underline{.3} \\ .1 \\ \underline{.0} \\ .1 \end{array}$$

$$2.9 \quad \begin{array}{r} 2 \\ 8 \overline{) 5.9} \\ \underline{16} \\ 23 \\ \underline{16} \\ 7 \\ \underline{6} \\ 1 \end{array}$$

$$3.1$$

$$3.3 \quad \begin{array}{r} 5 \\ 10 \overline{) 2.7} \\ \underline{20} \\ 7 \\ \underline{6} \\ 1 \end{array}$$

$$3.8 \quad \begin{array}{r} 4 \\ 10 \overline{) 4.1} \\ \underline{40} \\ 1 \end{array}$$

$$4.65 \quad \begin{array}{r} 2 \\ 10 \overline{) 6.65} \\ \underline{20} \\ 6 \\ \underline{6} \\ 0 \end{array}$$

$$4.75 \quad \begin{array}{r} 6 \\ 10 \overline{) 8.2} \\ \underline{60} \\ 22 \\ \underline{20} \\ 2 \end{array}$$

$$4.7 \quad \begin{array}{r} 6 \\ 10 \overline{) 2.7} \\ \underline{20} \\ 7 \end{array}$$

$$4.7 \quad \begin{array}{r} 6 \\ 10 \overline{) 8.2} \\ \underline{60} \\ 22 \\ \underline{20} \\ 2 \end{array}$$

$$5.0 \quad \begin{array}{r} 5 \\ 10 \overline{) 4.0} \\ \underline{50} \\ 0 \end{array}$$

$$5.3 \quad \begin{array}{r} 6 \\ 10 \overline{) 4.1} \\ \underline{60} \\ 1 \end{array}$$

$$4.6 \quad \begin{array}{r} 4 \\ 10 \overline{) 5.3} \\ \underline{40} \\ 13 \\ \underline{10} \\ 3 \end{array}$$

$$5.0 \quad \begin{array}{r} 2 \\ 10 \overline{) 6.8} \\ \underline{20} \\ 6 \end{array}$$

85+25

12.6

+50

11.5

86

10.1

+50

12.8

87

11.4

+50

10.4

88

11.9

+50

11.7

89

11.6

+50

12.2

90

12.9

+50

13.9

$$10.1 \quad \begin{array}{r} 540 \\ 10 \end{array} \left| \begin{array}{r} 9.3 \\ \hline D.C.2.8 \end{array} \right.$$

$$9.5 \quad \begin{array}{r} 550 \\ 10 \end{array} \left| \begin{array}{r} 8.6 \\ \hline D.C.2.9 \end{array} \right.$$

$$8.1 \quad \begin{array}{r} 610 \\ 10 \end{array} \left| \begin{array}{r} 6.6 \\ \hline D.C.3.5 \end{array} \right.$$

$$10.8 \quad \begin{array}{r} 610 \\ 10 \end{array} \left| \begin{array}{r} 9.3 \\ \hline D.C.3.5 \end{array} \right.$$

$$9.4 \quad \begin{array}{r} 590 \\ 10 \end{array} \left| \begin{array}{r} 8.1 \\ \hline D.C.3.3 \end{array} \right.$$

$$8.4 \quad \begin{array}{r} 560 \\ 10 \end{array} \left| \begin{array}{r} 7.4 \\ \hline D.C.3.0 \end{array} \right.$$

$$9.9 \quad \begin{array}{r} 540 \\ 10 \end{array} \left| \begin{array}{r} 8.1 \\ \hline D.C.2.8 \end{array} \right.$$

$$9.7 \quad \begin{array}{r} 520 \\ 10 \end{array} \left| \begin{array}{r} 9.3 \\ \hline D.C.2.6 \end{array} \right.$$

$$9.6 \quad \begin{array}{r} 500 \\ 10 \end{array} \left| \begin{array}{r} 9.2 \\ \hline D.C.2.4 \end{array} \right.$$

$$10.2 \quad \begin{array}{r} 520 \\ 10 \end{array} \left| \begin{array}{r} 9.6 \\ \hline D.C.2.6 \end{array} \right.$$

$$10.9 \quad \begin{array}{r} 510 \\ 10 \end{array} \left| \begin{array}{r} 10.4 \\ \hline D.C.2.5 \end{array} \right.$$

$$11.9 \quad \begin{array}{r} 550 \\ 10 \end{array} \left| \begin{array}{r} 11.0 \\ \hline D.C.2.9 \end{array} \right.$$

91+00

7.4

+50

8.5

92

9.7

+50

10.5

93

11.4

+50

12.6

94+75

5.6

80+35

7.3

+50

8.0

81

9.0

+25

9.2

3/13/34

$$5.4 \quad \begin{array}{r} 5.5 \\ 10 \overline{) 4.5} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 4.5 \\ 10 \overline{) 0.0} \end{array}$$

$$6.5 \quad \begin{array}{r} 5.9 \\ 10 \overline{) 5.2} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 5.2 \\ 10 \overline{) 0.0} \end{array}$$

$$7.7 \quad \begin{array}{r} 6.1 \\ 10 \overline{) 6.2} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 6.2 \\ 10 \overline{) 0.0} \end{array}$$

$$8.5 \quad \begin{array}{r} 6.1 \\ 10 \overline{) 7.0} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 7.0 \\ 10 \overline{) 0.0} \end{array}$$

$$9.4 \quad \begin{array}{r} 6.2 \\ 10 \overline{) 7.8} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 7.8 \\ 10 \overline{) 0.0} \end{array}$$

$$10.6 \quad \begin{array}{r} 5.1 \\ 10 \overline{) 10.1} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 10.1 \\ 10 \overline{) 0.0} \end{array}$$

$$3.6 \quad \begin{array}{r} 2.6 \\ 10 \overline{) 5.6} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 5.6 \\ 10 \overline{) 0.0} \end{array}$$

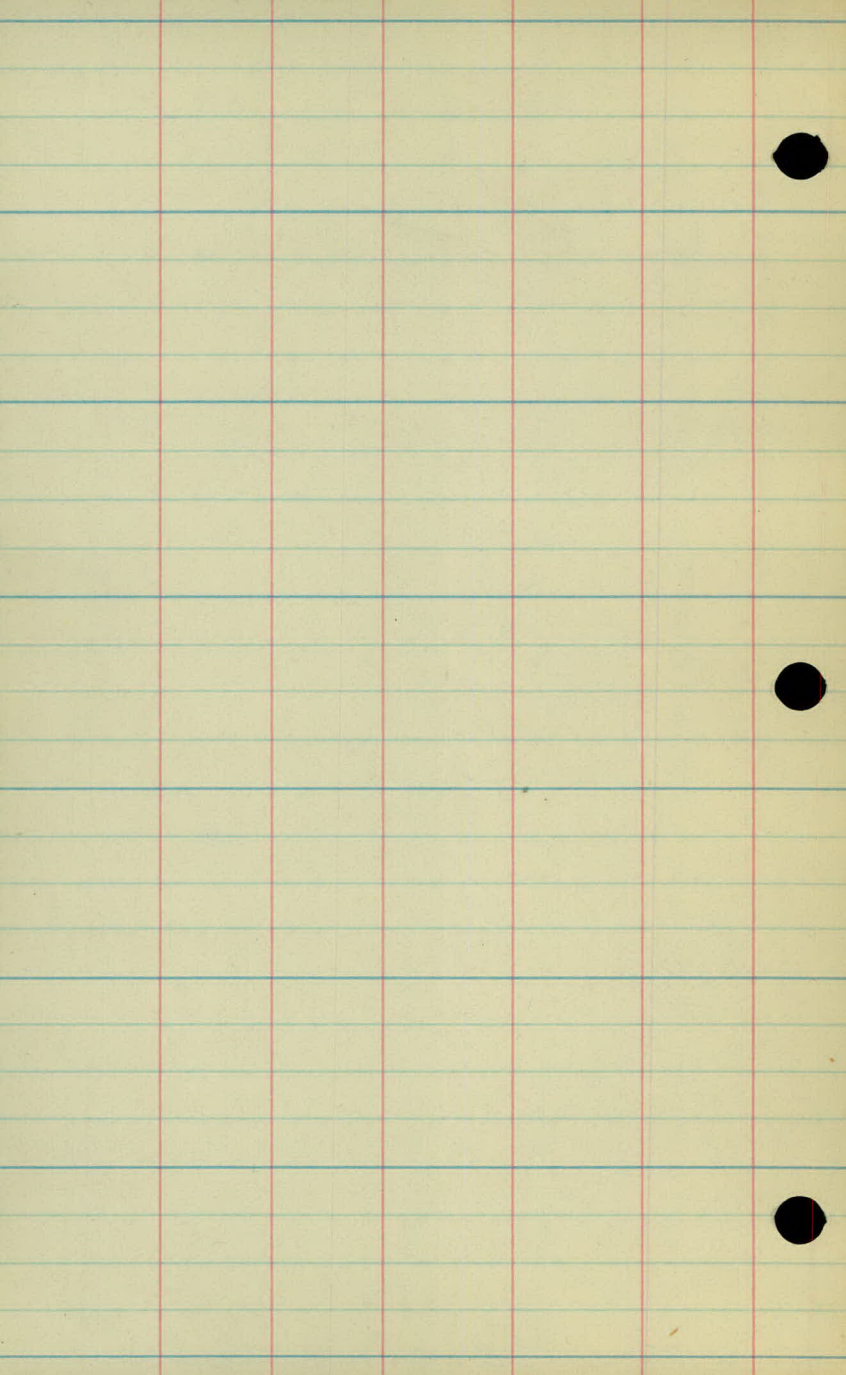
4:1 Slope 20 lb.

$$5.3 \quad \begin{array}{r} 6.1 \\ 10 \overline{) 4.7} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 4.7 \\ 10 \overline{) 0.0} \end{array}$$

$$6.0 \quad \begin{array}{r} 3.3 \\ 10 \overline{) 6.2} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 6.2 \\ 10 \overline{) 0.0} \end{array}$$

$$7.0 \quad \begin{array}{r} 3.1 \\ 10 \overline{) 7.7} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 7.7 \\ 10 \overline{) 0.0} \end{array}$$

$$7.2 \quad \begin{array}{r} 2.6 \\ 10 \overline{) 9.2} \\ \underline{0.0} \end{array} \quad \begin{array}{r} 9.2 \\ 10 \overline{) 0.0} \end{array}$$



County Road "C" - Cleveland Ave West
Location of Pole Lines
Cleveland Ave to Hamline Ave.

Location of Pole Lines
County Road "G"

59

58

57

56

55

54

53

3/5/34

25' out P.P. @ +50

+88 @ T.P. 26' out

21' out P.P. @ +62
21' W.P. @ +91

20-15' C.M.P. $\left[\begin{array}{l} \text{7' } 23' \text{ out} \\ +52 \end{array} \right]$ +66 @ T.P. 23' out

21' P.P. @ +50

+32 @ T.P. 24'

+71 @ No Pump 15'

21' out P.P. @ +95

+65 @ T.P. 25'

+15 @ T.P. 27'

P.P. 23' @ +41

+80 @ T.P. 28' out

67

66

65

64

63

62

61

60

3/5/34

+58 @T.P. 26' out

27' out P.P. @ +71

+22 @T.P. 26' out

27' out P.P. @ +11 +09 @T.P. 24' out
 26' - 10' CMP 27' out
 +79

+29 @T.P. 24' out

25' P.P. @ +60

+47 @T.P. 24' out

23' out P.P. @ +02

+71 @Dumping Prob 19' out

+02 @T.P. 24' out

79

73

72

71

70

69

68

67

3/5/34

25' out P.P. @ +36

+00 @ 19' out

26' out P.P. @ +42
16' out G.P. @ +40

+95 @ T.P. 20' out

27' out P.P. @ +45

+56 @ T.P. 26' out

27' out P.P. @ +88

+71 @ T.P. 26' out

28' out P.P. @ +79

81

80

79

78

77

76

75

74

3/5/34

20 XRd sign
38' out G.P.
41' out G.P.

+96
+86
+78 +70

OT.P. 27' out
St. Paul sign 28'
Hd. Mark 30'

35' out P.P.

+28
+25
+21
+05

OT.P. 29' out
OT.P. 29' out
OT.P. 29' out
OT.P. 29' out

20' out P.P.

+71

+94

OT.P. 29' out

+66

OT.P. 29' out

29' out P.P.

+24

+49

OT.P. 25' out

+33

OT.P. 25' out

29' out P.P.

+80

+77

OT.P. 25' out

88

87

86

85

84

83

82

81

3/5/34

+52 @ Tel. Pole 28' out

+25 @ O.P. 25' & 30' out

+34 @ T.P. 27' out

21' X R 1590 +89 +91 @ T.P. 29' out

+58 @ 27' out T.P.

+02 @ No Damp fig 18

+23 @ T.P. 26' out

95

94

93

92

91

90

89

88

3/5/34

+75 @ Tel. Pole 30' out

+92 @ 0 Db | Tel. Pole 26' & 31' out

+29 @ Tel. Pole 29' out

+04 @ Tel. Pole 29' out

+84 @ Tel. Pole 28' out

+66 @ Tel. Pole 28' out

102

101

100

99

98

97

96

95

3/5/34

35' out to Private Tel. Pole @
32'-12" CMP $\left\{ \begin{array}{l} +98 \\ +93 \\ \leftarrow 21' \text{ out} \\ +66 \end{array} \right.$

+12 @ Tel. Pole 31' out.

+78 @ Old Tel. Pole 28' & 33' out

+58 @ Tel. Pole 30' out

+0 @ Tel. Pole 28' out

+32 @ Tel. Pole 28' out

+00 @ Tel. Pole 28' out

109

108

107

106

105

104

103

102

3/5/34

+97

○ Tel. Pole 31' out

+16

○ Tel. Pole 31' out

26' out Guide P ○

+62

+33
+28

○ Tel Pole 33' out
Power Pole 41' out

28' out Power P ○

+43

+67 ○ End of Gd. Rail 10' out

+58

○ ○ Db. Tel. Pole 30' & 36' out

+25 ○ No Dump sign 12' out

+92 Rd. Marker 10' out

30' out Power P ○

+41

Post in end of Rail

+99

○ 33' out Tel. Pole.

14' out 24" Vee ○ +76

+58 End of Gd. Rail 10' out

+32

○ Tel. Pole 33' out

+65

○ Tel. Pole 34' out

+76 ○ Rd sign 15' out

+36

○ Tel. Pole 31' out

116

115

114

113

112

111

110

109

3/5/34

+35 ⊙ Tel Pole 29' out

+04 ⊙ Tel Pole 29' out

+38 ⊙ Tel Pole 29' out

+74 ⊙ ⊙ Db Tel Pole 26' & 23' out

20' out RR Sign ⊙ +47 +47 ⊙ Tel Pole 27' out

20' out X Rd Sign ⊙ +56

+17 ⊙ Tel Pole 30' out

123

122

121

120

119

118

117

116

3/5/34

+80

⊙ Tel Pole 36' out

+50

⊙ Tel Pole 30' out

+27

⊙ ⊙ Dbl Tel Pole 25' & 30' out

+91

⊙ Tel Pole 28' out



+21' out No jump ⊙

+51 f66

⊙ Tel Pole 28' out

130

129

128

127

126

125

124

123

3/5/34

+58

○Tel Pole 59' out

+87 ○XRd Sign 18' out

+25

○Tel Pole 55' out

+95

○Tel Pole 51' out

+63

○DBI Tel Pole 45' & 50' out

+37

○Tel Pole 43' out

+06

○Tel Pole 39' out

137

136

135

134

133

132

131

130

3/5/34

32' out to Rd Mark
26' out to P.P. ©

+88 +85 +85

+66

© Pole 70' out

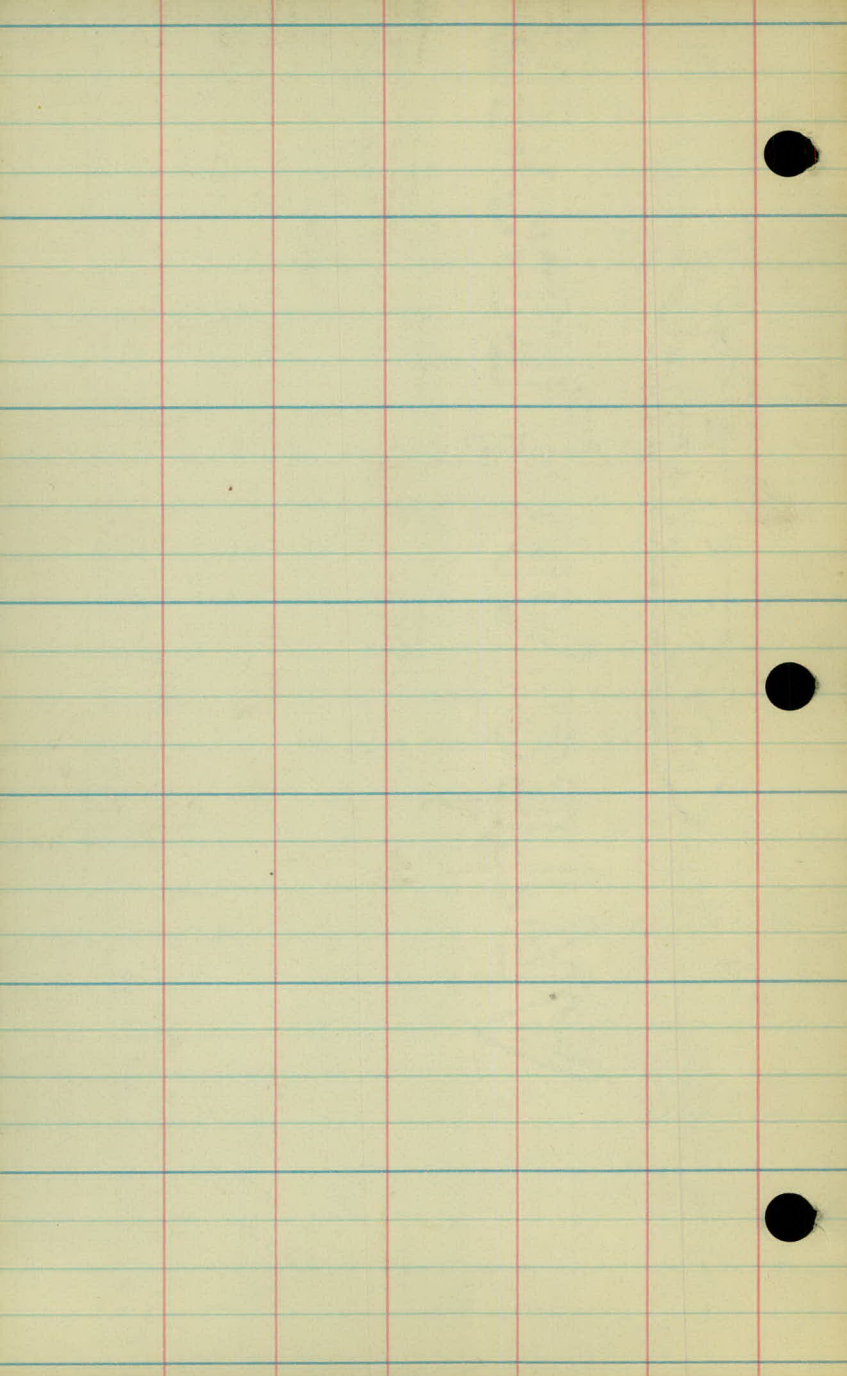
© Pole 64' out

+29 © Tractor Prohibit Sign 17' out

+88

© Pole 63' out

+01 © R Sign 19' out



County Road "C" - Cleveland Ave West

Cross-sections & Slope Stakes.

Snelling Ave to Hamline Ave

Station 106 to 131+50

Extension of Cross-sections Rt. Side

Station 109 to 114+60

" 117+25 to 121+00

" 124+00 to 131+50

B.M

1002.27

6.47 1008.74

106

6.3

+15

+43

40' -

15" C.M.P.

Extension Required

At 10 ft

At 10 ft

6.3

+50

6.3

+75

107

6.4

7.9

+50

6.3

108

5.8

+20

+35

+50

5.2 Rt
5.4 Lt

109

6.3

+50

5.0

Spike in Tel. Pole 18738R. 30' Rt of 106+65

2/28/34

$\frac{6.0}{40} \frac{5.2}{30} \frac{5.9}{20} \frac{6.1}{10} 6.0$ $\frac{6.1}{9} \frac{7.2}{13} \frac{11.3}{20} \frac{12.7}{24} \frac{12.2}{34} \frac{15.3}{40}$

$\frac{33.8}{13.2}$
F6.7

$\frac{7.3}{40} \frac{6.7}{30} \frac{6.1}{20} \frac{6.1}{10} 6.0$ $\frac{6.5}{9} \frac{7.2}{15} \frac{10.0}{19} \frac{11.7}{26} \frac{12.1}{32} \frac{12.8}{40}$

$\frac{8.6}{F2.3}$
24.6

F
 $\frac{E.C.}{20} \frac{8.6}{40} \frac{8.3}{32} \frac{8.5}{27} \frac{8.8}{23} \frac{7.2}{19} \frac{6.4}{10} 6.0$ $\frac{6.6}{9} \frac{7.4}{14} \frac{E.C.}{20} \frac{10.4}{20} \frac{11.5}{28} \frac{11.9}{40}$

$\frac{30.4}{11.5}$
F5.2

$\frac{8.8}{F2.5}$
25.0

F
 $\frac{8.5}{40} \frac{8.6}{32} \frac{8.8}{22} \frac{7.6}{19} \frac{7.0}{16} 6.0$ $\frac{6.5}{9} \frac{6.5}{15} \frac{11.3}{33} \frac{11.5}{40}$

$\frac{10.3}{10.3}$
F4.0

F
 $\frac{7.9}{40} \frac{8.0}{33} \frac{7.7}{23} \frac{8.2}{17} \frac{6.7}{11} 6.1$ $\frac{6.2}{9} \frac{6.4}{20} \frac{6.6}{29} \frac{10.8}{42} \frac{11.1}{50}$

$\frac{7.5}{D.C.O.A.}$
24.8

F
 $\frac{7.2}{40} \frac{7.3}{33} \frac{7.4}{23} \frac{8.0}{17} \frac{6.6}{11} 6.1$ $\frac{6.5}{12} \frac{6.6}{25} \frac{6.8}{42}$

N.S

$\frac{5.6}{C.O.7}$
28.2

F
 $\frac{6.1}{40} \frac{5.9}{33} \frac{5.6}{28} \frac{6.2}{22} \frac{8.2}{18} \frac{8.4}{16} \frac{6.2}{11} 5.8$ $\frac{6.0}{10} \frac{6.3}{20} \frac{6.4}{30} \frac{6.7}{40}$

N.S

$\frac{5.2}{C.O.6}$
28.2

F
 $\frac{5.2}{40} \frac{5.4}{33} \frac{5.2}{28} \frac{5.6}{24} \frac{7.7}{21} \frac{7.9}{17} \frac{5.9}{11} 5.3$ $\frac{5.6}{10} \frac{5.7}{20} \frac{5.8}{30} \frac{6.0}{40}$

N.S

F
 $\frac{9.6}{40} \frac{4.4}{33} \frac{4.6}{26} \frac{7.5}{20} \frac{7.7}{16} \frac{5.6}{11} 5.1$ $\frac{5.4}{10} \frac{6.0}{20} \frac{6.1}{30} \frac{6.0}{40}$

F
 $\frac{4.1}{40} \frac{4.1}{32} \frac{4.2}{25} \frac{7.6}{19} \frac{7.6}{16} \frac{5.6}{12} 5.0$ $\frac{5.6}{13} \frac{5.7}{21} \frac{7.5}{27} \frac{8.2}{40}$

$\frac{8.6}{C.18}$
30.6

F
 $\frac{3.7}{40} \frac{3.6}{32} \frac{3.4}{27} \frac{5.5}{21} \frac{7.6}{19} \frac{7.6}{16} \frac{5.5}{11} 4.9$ $\frac{5.4}{12} \frac{5.6}{15} \frac{7.9}{19} \frac{8.2}{31} \frac{8.1}{40}$

$\frac{2.5}{8.0}$
F2.8

$\frac{1.7}{C.6}$
34.2

F
 $\frac{1.9}{40} \frac{1.8}{32} \frac{2.1}{27} \frac{7.3}{19} \frac{7.3}{16} \frac{5.3}{13} 4.8$ $\frac{5.3}{12} \frac{7.3}{17} \frac{7.3}{25} \frac{3.6}{31} \frac{3.9}{40}$

$\frac{2.9}{5.3}$
29.0

$\frac{0.9}{C.A.2}$
35.4

F
 $\frac{0.9}{40} \frac{1.1}{32} \frac{1.0}{29} \frac{7.8}{20} \frac{7.0}{16} \frac{5.1}{13} 4.9$ $\frac{4.9}{12} \frac{7.0}{18} \frac{6.9}{25} \frac{5.6}{33} \frac{1.8}{40}$

$\frac{3.5}{1.6}$
C3.5

110

4.8

+50

4.7

111

4.5

6.0

+50

3.9 LT
4.1 R

T.P.

0.46

1008.28

2.19

1010.47

112

5.9 LT
6.1 RT

+50

5.6 LT
5.9 RT

113

5.4 LT
5.6 RT

+50

5.3

6.6

114

5.2

6.7

+50

5.0
5.2

6.7

2.13

1010.61

+60

5.5 LT
5.3 RT

6.8

115

5.0

2/28/34

$$\frac{1.3}{C.3.5} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{1.4}{40} \frac{1.4}{32} \frac{5.7}{26} \frac{7.3}{20} \frac{7.3}{18} \frac{5.3}{13} \frac{4.8}{11} \frac{4.7}{4.3} \frac{7.1}{11} \frac{6.9}{18} \frac{1.4}{22} \frac{1.2}{21} \frac{1.3}{35} \frac{1.3}{40}$$

$$F \quad \frac{1.2}{C.3.6} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{2.2}{C.2.5} \left| \frac{32.0}{32.0} \right. \quad \frac{3.7}{40} \frac{3.2}{35} \frac{2.5}{34} \frac{2.2}{32} \frac{2.2}{28} \frac{6.5}{21} \frac{7.0}{19} \frac{4.8}{18} \frac{4.5}{13} \frac{4.7}{11} \frac{4.2}{4.7} \frac{7.0}{11} \frac{6.8}{18} \frac{5.0}{22} \frac{1.3}{25} \frac{1.1}{30} \frac{1.1}{34} \frac{1.1}{40}$$

$$F \quad \frac{1.0}{C.3.7} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{5.0}{D.C.10} \left| \frac{36.0}{36.0} \right. \quad \frac{6.6}{40} \frac{6.2}{35} \frac{5.5}{34} \frac{5.1}{32} \frac{4.9}{26} \frac{6.5}{20} \frac{4.6}{17} \frac{4.7}{14} \frac{4.3}{11} \frac{4.0}{4.0} \frac{4.4}{11} \frac{6.5}{18} \frac{7.0}{22} \frac{6.7}{25} \frac{1.7}{31} \frac{1.4}{34} \frac{1.3}{40}$$

$$F \quad \frac{1.3}{C.3.2} \left| \frac{35.0}{35.0} \right.$$

$$F \quad \frac{7.7}{F.3.8} \left| \frac{27.6}{27.6} \right. \quad \frac{8.5}{40} \frac{7.6}{32} \frac{7.7}{30} \frac{6.4}{22} \frac{6.0}{16} \frac{4.4}{13} \frac{4.2}{11} \frac{3.6}{3.6} \frac{4.1}{11} \frac{6.4}{17} \frac{6.2}{22} \frac{4.9}{26} \frac{1.3}{30} \frac{1.0}{35} \frac{1.0}{40}$$

$$F \quad \frac{1.0}{C.3.1} \left| \frac{35.0}{35.0} \right.$$

Top of stake 30 ft R + at 112+00

3/1/34

$$F \quad \frac{9.5}{F.3.6} \left| \frac{27.2}{27.2} \right. \quad \frac{10.8}{40} \frac{10.6}{35} \frac{9.7}{32} \frac{9.6}{27} \frac{8.6}{21} \frac{8.2}{17} \frac{6.4}{13} \frac{5.9}{12} \frac{5.6}{5.6} \frac{5.6}{11} \frac{7.8}{17} \frac{8.1}{21} \frac{7.6}{24} \frac{5.8}{29} \frac{3.2}{35} \frac{3.0}{40}$$

$$F \quad \frac{3.2}{C.2.9} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{9.2}{F.3.6} \left| \frac{27.2}{27.2} \right. \quad \frac{10.4}{40} \frac{9.9}{34} \frac{9.2}{31} \frac{8.7}{23} \frac{8.3}{18} \frac{6.1}{13} \frac{5.8}{11} \frac{5.4}{5.4} \frac{5.7}{11} \frac{7.8}{15} \frac{7.7}{17} \frac{7.5}{20} \frac{4.3}{25} \frac{3.1}{25} \frac{2.9}{40}$$

$$F \quad \frac{3.1}{C.2.8} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{7.7}{F.2.3} \left| \frac{24.6}{24.6} \right. \quad \frac{8.4}{40} \frac{7.7}{34} \frac{7.7}{31} \frac{7.7}{24} \frac{7.4}{17} \frac{5.6}{12} \frac{5.1}{5.1} \frac{5.4}{11} \frac{7.1}{14} \frac{7.4}{18} \frac{7.0}{21} \frac{4.1}{25} \frac{2.5}{35} \frac{2.5}{40}$$

$$F \quad \frac{2.7}{C.2.9} \left| \frac{34.0}{34.0} \right.$$

$$F \quad \frac{6.4}{D.C.0.4} \left| \frac{24.8}{24.8} \right. \quad \frac{7.5}{40} \frac{6.7}{34} \frac{6.7}{31} \frac{6.4}{23} \frac{6.4}{18} \frac{6.2}{14} \frac{5.1}{12} \frac{4.8}{4.8} \frac{4.8}{10} \frac{5.3}{12} \frac{7.1}{16} \frac{7.3}{17} \frac{6.8}{20} \frac{3.2}{23} \frac{3.0}{34} \frac{2.5}{40}$$

$$F \quad \frac{3.0}{C.2.8} \left| \frac{33.0}{33.0} \right.$$

$$F \quad \frac{6.7}{D.C.0.0} \left| \frac{24.0}{24.0} \right. \quad \frac{7.4}{40} \frac{7.7}{36} \frac{7.1}{35} \frac{6.9}{31} \frac{6.7}{24} \frac{6.0}{18} \frac{6.1}{15} \frac{5.0}{12} \frac{4.7}{4.7} \frac{5.0}{9} \frac{5.4}{12} \frac{6.4}{16} \frac{6.7}{19} \frac{5.1}{21} \frac{4.1}{24} \frac{3.4}{34} \frac{3.2}{40}$$

$$F \quad \frac{3.6}{C.1.6} \left| \frac{32.0}{32.0} \right.$$

$$F \quad \frac{7.8}{F.2.8} \left| \frac{25.6}{25.6} \right. \quad \frac{8.3}{40} \frac{7.9}{34} \frac{8.1}{31} \frac{7.7}{24} \frac{7.4}{17} \frac{5.3}{12} \frac{4.7}{4.7} \frac{5.0}{12} \frac{7.9}{19} \frac{7.8}{22} \frac{6.1}{25} \frac{6.5}{34} \frac{5.5}{40}$$

$$F \quad \frac{5.9}{D.C.0.8} \left| \frac{27.6}{27.6} \right.$$

$$F \quad \frac{8.6}{40} \frac{7.8}{34} \frac{8.2}{31} \frac{8.3}{24} \frac{7.8}{16} \frac{5.3}{11} \frac{4.8}{4.8} \frac{5.2}{12} \frac{8.1}{19} \frac{8.5}{24} \frac{7.0}{28} \frac{6.7}{34} \frac{6.4}{40}$$

$$F \quad \frac{6.8}{D.C.0.0} \left| \frac{26.0}{26.0} \right.$$

$$F \quad \frac{8.1}{F.3.1} \left| \frac{26.2}{26.2} \right. \quad \frac{8.1}{40} \frac{7.4}{39} \frac{8.3}{30} \frac{8.2}{28} \frac{8.0}{18} \frac{5.2}{11} \frac{4.7}{4.7} \frac{5.1}{11} \frac{8.1}{18} \frac{8.4}{26} \frac{8.4}{34} \frac{8.1}{40}$$

$$F \quad \frac{8.6}{F.3.6} \left| \frac{27.2}{27.2} \right.$$

115+50

4.7

116

3.9

+50

3.1

117

2.7
2.5

4.2

+25

2.1

3.6

7.07

101903

0.85

1009.96

+50

9.9

118

9.1

+25

8.8

+50

8.9

+75

119

7.7

+20

7.3

+50

7.0

B.M.

7.96

1011.07

$$\frac{8.6}{F.2.9} \bigg| 27.8$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 88 & 87 & 83 & 85 & 86 & 78 & 48 & & 48 & 88 & 73 & 92 & 93 \\ 40 & 35 & 34 & 30 & 25 & 18 & 12 & 4.4 & 11 & 19 & 27 & 24 & 40 \end{array}$$

$$\frac{24.2}{F.4.6} \bigg| 9.3$$

$$\frac{3.3}{F3A} \bigg| 2.68$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 85 & 80 & 84 & 86 & 76 & 41 & & 40 & 47 & 85 & 85 & 86 & 82 \\ 40 & 34 & 30 & 24 & 18 & 12 & 3.6 & 11 & 16 & 22 & 28 & 34 & 40 \end{array}$$

$$\frac{29.2}{F4.6} \bigg| 8.5$$

$$\frac{7.2}{F4.1} \bigg| 2.82$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 70 & 67 & 72 & 76 & 78 & 30 & & 32 & 51 & 82 & 80 & 81 \\ 40 & 33 & 30 & 25 & 19 & 10 & 2.8 & 12 & 17 & 24 & 33 & 40 \end{array}$$

$$\frac{30.2}{F5.1} \bigg| 8.2$$

$$\frac{4.2}{D.C.00} \bigg| 2.40$$

$$\begin{array}{cccccccccccc} & F & & & P2P & & & & & & & & \\ 42 & 37 & 40 & 42 & 53 & 28 & & 26 & 63 & 65 & 64 & 63 \\ 40 & 33 & 30 & 22 & 17 & 11 & 2.2 & 12 & 19 & 29 & 34 & 40 \end{array}$$

$$\frac{27.4}{F3.7} \bigg| 6.2$$

$$\frac{2.1}{00} \bigg| 270$$

$$\begin{array}{cccccccccccc} & F & & & Pen & & & & & & & & \\ 17 & 16 & 20 & 19 & 22 & 24 & 21 & & 21 & 28 & 34 & 36 & 42 \\ 40 & 33 & 30 & 23 & 16 & 14 & 12 & 1.6 & 14 & 16 & 24 & 34 & 40 \end{array}$$

$$\frac{240}{D.C.00} \bigg| 3.6$$

$$\frac{7.0}{C2.1} \bigg| 32.8$$

$$\begin{array}{cccccccccccc} & F & & & Pen & & & & & & & & \\ 75 & 70 & 75 & 78 & 78 & 99 & 101 & 97 & & 99 & 104 & 104 & 98 \\ 40 & 33 & 29 & 25 & 19 & 15 & 14 & 11 & 9.4 & 14 & 16 & 20 & 24 \\ & & & & & & & & & & & & 33 & 40 \end{array}$$

$$\frac{270}{00} \bigg| 9.9$$

$$\frac{3.5}{C5.6} \bigg| 38.2$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 32 & 36 & 36 & 33 & 37 & 90 & 90 & 87 & & 90 & 99 & 96 & 70 \\ 40 & 36 & 32 & 30 & 27 & 19 & 18 & 13 & 8.6 & 14 & 16 & 19 & 23 \\ & & & & & & & & & & & & 33 & 40 \end{array}$$

$$\frac{30.6}{C1.8} \bigg| 7.3$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 27 & 28 & 21 & 27 & 30 & 79 & 91 & 87 & & 86 & 94 & 93 & 67 \\ 40 & 36 & 32 & 30 & 27 & 21 & 16 & 12 & 8.3 & 13 & 16 & 19 & 23 \\ & & & & & & & & & & & & 33 & 40 \end{array}$$

$$\frac{3.1}{C5.5} \bigg| 37.6$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 31 & 24 & 29 & 34 & 64 & 84 & 82 & & 83 & 84 & 86 & 58 & 63 \\ 40 & 31 & 30 & 25 & 21 & 14 & 11 & 7.9 & 13 & 16 & 18 & 22 & 33 \\ & & & & & & & & & & & & 40 \end{array}$$

$$\frac{31.6}{C2.3} \bigg| 6.1$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 46 & 41 & 44 & 49 & 83 & 82 & 79 & & 80 & 84 & 84 & 52 & 56 \\ 40 & 31 & 29 & 21 & 16 & 14 & 12 & 7.6 & 13 & 15 & 17 & 21 & 33 \\ & & & & & & & & & & & & 40 \end{array}$$

$$\frac{6.4}{C1.3} \bigg| 29.6$$

$$\begin{array}{cccccccccccc} & F & F & & & & & & & & F & & \\ 61 & 64 & 62 & 67 & 80 & 80 & 76 & & 76 & 80 & 50 & 52 & 52 \\ 40 & 30 & 28 & 18 & 15 & 14 & 12 & 7.2 & 14 & 16 & 19 & 23 & 35 \\ & & & & & & & & & & & & 40 \end{array}$$

$$\frac{32.4}{C2.7} \bigg| 5.0$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 80 & 62 & 75 & 71 & 70 & 78 & 73 & & 71 & 78 & 57 & 47 & 44 \\ 40 & 32 & 26 & 17 & 16 & 14 & 12 & 6.8 & 14 & 16 & 20 & 23 & 36 \\ & & & & & & & & & & & & 40 \end{array}$$

$$\frac{6.7}{C0.3} \bigg| 27.6$$

$$\begin{array}{cccccccccccc} & F & & & F & & & & & & & & \\ 13 & 10 & 14 & 61 & 59 & 61 & 70 & 67 & & 67 & 73 & 48 & 40 \\ 40 & 32 & 24 & 23 & 18 & 16 & 14 & 11 & 6.5 & 13 & 17 & 21 & 23 \\ & & & & & & & & & & & & 30 & 36 & 40 \end{array}$$

$$\frac{33.4}{C3.2} \bigg| 3.8$$

Spike in Tel Pole 20Fht of 121 + 76

119+75

6.7

120

6.7

+30

6.8

+50

6.8

+75

7.0

8.5

121

7.0 Rt
6.8 Lt

+35

+50

7.1

122

6.4

+50

6.0

123

5.8

+50

5.8 Lt
5.6 Rt 7.3

124

5.4 Lt
5.2 Rt

L

F

$$\begin{array}{r} 5.9 \ 5.5 \ 4.7 \ 4.8 \ 6.4 \ 6.5 \\ 40 \ 25 \ 21 \ 17 \ 13 \ 11 \end{array} \quad \begin{array}{r} 6.5 \ 7.3 \ 7.1 \ 4.8 \ 3.6 \ 3.7 \ 2.0 \\ 13 \ 16 \ 18 \ 21 \ 25 \ 27 \ 40 \end{array}$$

2/1/34

F

F

$$\begin{array}{r} 5.3 \ 5.2 \ 4.4 \ 4.5 \ 6.4 \ 6.5 \\ 40 \ 29 \ 21 \ 18 \ 13 \ 10 \end{array} \quad \begin{array}{r} 6.5 \ 7.4 \ 7.1 \ 4.7 \ 3.6 \ 3.5 \ 3.4 \\ 13 \ 17 \ 19 \ 23 \ 32 \ 36 \ 40 \end{array}$$

F

$$\begin{array}{r} 3.3 \ 3.6 \\ 2 \ 1 \end{array} \quad \begin{array}{r} 3.6 \\ 1 \end{array}$$

F

$$\begin{array}{r} 5.7 \ 5.1 \ 4.8 \ 5.2 \ 6.6 \ 6.5 \\ 40 \ 27 \ 22 \ 18 \ 13 \ 10 \end{array} \quad \begin{array}{r} 6.8 \ 7.6 \ 7.5 \ 5.1 \ 4.3 \ 4.6 \ 5.0 \\ 14 \ 17 \ 20 \ 23 \ 27 \ 36 \ 40 \end{array}$$

F

F

$$\begin{array}{r} 6.4 \ 6.7 \ 5.4 \ 5.5 \ 5.4 \ 6.7 \\ 40 \ 26 \ 22 \ 18 \ 17 \ 14 \end{array} \quad \begin{array}{r} 6.7 \ 7.6 \ 7.5 \ 5.6 \ 5.0 \ 5.5 \ 5.3 \\ 13 \ 17 \ 19 \ 24 \ 28 \ 37 \ 40 \end{array}$$

F

$$\begin{array}{r} 5.0 \ 5.1 \\ 1 \ 1 \end{array} \quad \begin{array}{r} 5.1 \\ 1 \end{array}$$

F

$$\begin{array}{r} 8.5 \ 8.4 \ 8.5 \ 7.7 \ 7.8 \ 7.2 \ 6.8 \\ 40 \ 30 \ 25 \ 23 \ 19 \ 16 \end{array} \quad \begin{array}{r} 6.8 \ 8.1 \ 8.2 \ 6.3 \ 6.2 \ 6.4 \\ 14 \ 19 \ 21 \ 27 \ 38 \ 40 \end{array}$$

F

F

$$\begin{array}{r} 10.5 \ 10.1 \ 10.6 \ 10.3 \ 9.6 \ 9.2 \ 7.1 \ 6.9 \\ 40 \ 34 \ 25 \ 23 \ 20 \ 18 \ 14 \ 11 \end{array} \quad \begin{array}{r} 6.9 \ 9.3 \ 9.3 \ 8.5 \ 7.9 \ 8.1 \ 8.2 \\ 13 \ 19 \ 21 \ 24 \ 28 \ 38 \ 40 \end{array}$$

F

$$\begin{array}{r} 2.4 \ 8.5 \\ 10 \ 10 \end{array} \quad \begin{array}{r} 8.5 \\ 1 \end{array}$$

F

$$\begin{array}{r} 11.6 \ 11.6 \ 11.3 \ 9.7 \ 7.0 \\ 40 \ 25 \ 22 \ 18 \ 12 \end{array} \quad \begin{array}{r} 7.2 \ 10.7 \ 11.6 \ 11.8 \\ 13 \ 27 \ 30 \ 39 \end{array}$$

F

F

$$\begin{array}{r} 11.7 \ 11.7 \ 11.0 \ 9.3 \ 7.0 \\ 40 \ 25 \ 21 \ 18 \ 13 \end{array} \quad \begin{array}{r} 7.0 \ 9.1 \ 11.7 \ 11.8 \ 11.8 \\ 12 \ 20 \ 25 \ 33 \ 40 \end{array}$$

F

$$\begin{array}{r} 2.9 \ 11.8 \\ 4 \ 4 \end{array} \quad \begin{array}{r} 11.8 \\ 1 \end{array}$$

F

$$\begin{array}{r} 10.9 \ 10.6 \ 10.0 \ 9.2 \ 6.5 \\ 40 \ 25 \ 20 \ 18 \ 13 \end{array} \quad \begin{array}{r} 6.7 \ 8.0 \ 8.5 \ 9.5 \ 9.1 \ 8.6 \\ 12 \ 16 \ 21 \ 24 \ 32 \ 41 \end{array}$$

F

$$\begin{array}{r} 2.6 \ 9.6 \\ 4 \ 4 \end{array} \quad \begin{array}{r} 9.6 \\ 1 \end{array}$$

F

$$\begin{array}{r} 10.8 \ 9.5 \ 8.5 \ 5.9 \\ 40 \ 21 \ 18 \ 13 \end{array} \quad \begin{array}{r} 6.0 \ 6.7 \ 7.6 \ 7.8 \ 8.1 \\ 10 \ 15 \ 24 \ 34 \ 42 \end{array}$$

F

$$\begin{array}{r} 2.3 \ 7.5 \\ 10 \ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 1 \end{array}$$

F

$$\begin{array}{r} 9.8 \ 9.7 \ 8.7 \ 5.6 \\ 40 \ 23 \ 18 \ 13 \end{array} \quad \begin{array}{r} 5.8 \ 6.2 \ 8.2 \ 9.0 \ 9.9 \ 9.4 \\ 11 \ 13 \ 16 \ 28 \ 31 \ 44 \end{array}$$

F

$$\begin{array}{r} 2.6 \ 9.1 \\ 6 \ 6 \end{array} \quad \begin{array}{r} 9.1 \\ 1 \end{array}$$

F

$$\begin{array}{r} 6.9 \ 6.6 \ 5.6 \\ 40 \ 18 \ 13 \end{array} \quad \begin{array}{r} 5.7 \ 8.0 \ 8.9 \ 9.4 \ 9.8 \\ 12 \ 20 \ 31 \ 36 \ 45 \end{array}$$

F

$$\begin{array}{r} 2.0 \ 8.6 \\ 10 \ 10 \end{array} \quad \begin{array}{r} 8.6 \\ 1 \end{array}$$

F

$$\begin{array}{r} 4.2 \ 4.0 \ 4.0 \ 4.6 \ 4.9 \\ 40 \ 29 \ 18 \ 15 \ 12 \end{array} \quad \begin{array}{r} 5.3 \ 6.7 \ 8.2 \ 8.0 \ 6.1 \ 6.5 \\ 12 \ 15 \ 23 \ 33 \ 36 \ 47 \end{array}$$

F

$$\begin{array}{r} 2.6 \ 8.3 \\ 10 \ 10 \end{array} \quad \begin{array}{r} 8.3 \\ 1 \end{array}$$

1019.03

124+50

4.8 Lt
4.6 Rt

T.P.

5.23

1018.44

5.82

1013.21

125

4.1 Lt
3.9 Rt

+50

4.1 Lt
3.9 Rt

126

4.1 5.6

+50

4.0 5.5

127

3.8 5.3

+50

3.5 5.0

128

3.4 4.9

+50

3.4 4.9

129

3.1 4.6

B.M.

4.20

1014.24

3/1/34

$$\begin{array}{r} 2.9 \\ C.1.9 \end{array} \bigg| \begin{array}{r} 20.8 \\ 20.8 \end{array}$$

$$\begin{array}{r} F \\ 3.0 \ 2.9 \ 2.8 \ 4.1 \ 4.5 \\ 4.0 \ 2.9 \ 1.8 \ 1.5 \ 1.1 \end{array} \bigg| \begin{array}{r} 4.3 \\ 4.3 \end{array}$$

$$\begin{array}{r} F \\ 4.7 \ 6.6 \ 7.2 \ 6.7 \ 4.3 \\ 1.3 \ 1.9 \ 2.9 \ 3.8 \ 4.8 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 7.3 \\ 7.2 \end{array}$$

Top of Stake 30' Rt of 125+00

$$\begin{array}{r} 2.4 \\ C.1.7 \end{array} \bigg| \begin{array}{r} 20.8 \\ 20.8 \end{array}$$

$$\begin{array}{r} F \\ 2.2 \ 2.4 \ 2.5 \ 3.5 \ 3.6 \\ 4.0 \ 3.0 \ 1.8 \ 1.3 \ 1.0 \end{array} \bigg| \begin{array}{r} 3.6 \\ 3.6 \end{array}$$

$$\begin{array}{r} F \\ 4.2 \ 5.4 \ 6.4 \ 6.3 \ 3.2 \\ 1.6 \ 1.4 \ 3.3 \ 3.9 \ 5.1 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 6.7 \\ 6.6 \end{array}$$

$$\begin{array}{r} 2.7 \\ C.1.4 \end{array} \bigg| \begin{array}{r} 2.98 \\ 2.98 \end{array}$$

$$\begin{array}{r} F \\ 2.5 \ 2.7 \ 2.3 \ 2.4 \ 3.6 \\ 4.0 \ 3.0 \ 1.8 \ 1.6 \ 1.1 \end{array} \bigg| \begin{array}{r} 3.6 \\ 3.6 \end{array}$$

$$\begin{array}{r} F \\ 3.9 \ 5.0 \ 6.3 \ 6.1 \ 3.0 \ 2.5 \\ 1.2 \ 1.6 \ 2.4 \ 3.2 \ 4.0 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.4 \\ 2.4 \end{array} \bigg| \begin{array}{r} 6.3 \\ 6.2 \end{array}$$

$$\begin{array}{r} 3.6 \\ C.0.5 \end{array} \bigg| \begin{array}{r} 28.0 \\ 28.0 \end{array}$$

$$\begin{array}{r} F \\ 3.6 \ 3.6 \ 3.6 \ 2.9 \ 3.4 \ 3.7 \\ 4.0 \ 3.1 \ 2.4 \ 1.8 \ 1.5 \ 1.2 \end{array} \bigg| \begin{array}{r} 3.6 \\ 3.6 \end{array}$$

$$\begin{array}{r} F \\ 4.0 \ 4.8 \ 4.4 \ 6.3 \ 5.2 \\ 1.2 \ 2.1 \ 3.1 \ 3.8 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 4.8 \\ 4.0 \end{array}$$

$$\begin{array}{r} 3.9 \\ C.0.1 \end{array} \bigg| \begin{array}{r} 27.2 \\ 27.2 \end{array}$$

$$\begin{array}{r} F \\ 3.6 \ 3.9 \ 3.6 \ 3.5 \ 3.5 \ 3.7 \\ 4.0 \ 2.4 \ 2.1 \ 1.8 \ 1.4 \ 1.1 \end{array} \bigg| \begin{array}{r} 3.5 \\ 3.5 \end{array}$$

$$\begin{array}{r} F \\ 4.0 \ 4.9 \ 4.5 \ 4.1 \ 4.9 \ 6.3 \ 5.2 \\ 1.2 \ 1.5 \ 2.1 \ 3.0 \ 3.6 \ 4.0 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ 2.6 \end{array} \bigg| \begin{array}{r} 9.5 \\ 9.0 \end{array}$$

$$\begin{array}{r} 3.5 \\ C.0.3 \end{array} \bigg| \begin{array}{r} 27.6 \\ 27.6 \end{array}$$

$$\begin{array}{r} F \\ 3.1 \ 3.4 \ 3.7 \ 2.9 \ 3.1 \ 3.6 \\ 4.0 \ 3.2 \ 2.4 \ 1.8 \ 1.4 \ 1.2 \end{array} \bigg| \begin{array}{r} 3.3 \\ 3.3 \end{array}$$

$$\begin{array}{r} F \\ 3.6 \ 5.1 \ 4.5 \ 3.9 \ 5.3 \ 3.9 \\ 1.2 \ 1.7 \ 2.3 \ 3.2 \ 4.0 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 4.4 \\ 4.0 \end{array}$$

$$\begin{array}{r} 3.2 \\ C.0.3 \end{array} \bigg| \begin{array}{r} 27.6 \\ 27.6 \end{array}$$

$$\begin{array}{r} F \\ 2.7 \ 3.1 \ 3.3 \ 2.8 \ 2.8 \ 3.3 \\ 4.0 \ 3.2 \ 2.3 \ 1.8 \ 1.5 \ 1.2 \end{array} \bigg| \begin{array}{r} 3.0 \\ 3.0 \end{array}$$

$$\begin{array}{r} F \\ 3.4 \ 4.2 \ 4.3 \ 3.6 \ 4.6 \ 4.9 \\ 1.0 \ 1.4 \ 1.9 \ 3.2 \ 4.2 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 4.1 \\ 4.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ C.0.6 \end{array} \bigg| \begin{array}{r} 28.2 \\ 28.2 \end{array}$$

$$\begin{array}{r} F \\ 2.6 \ 2.9 \ 3.0 \ 2.6 \ 2.7 \ 3.2 \\ 4.0 \ 3.1 \ 2.4 \ 1.8 \ 1.6 \ 1.3 \end{array} \bigg| \begin{array}{r} 2.9 \\ 2.9 \end{array}$$

$$\begin{array}{r} F \\ 3.5 \ 4.1 \ 4.3 \ 3.5 \ 3.5 \ 4.2 \ 3.5 \\ 1.1 \ 1.3 \ 1.7 \ 2.9 \ 3.8 \ 4.3 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ 2.6 \end{array} \bigg| \begin{array}{r} 5.6 \\ 5.0 \end{array}$$

$$\begin{array}{r} 3.0 \\ C.0.4 \end{array} \bigg| \begin{array}{r} 27.8 \\ 27.8 \end{array}$$

$$\begin{array}{r} F \\ 2.9 \ 3.0 \ 3.0 \ 2.9 \\ 4.0 \ 2.9 \ 1.9 \ 1.3 \ 2.9 \end{array}$$

$$\begin{array}{r} F \\ 3.4 \ 4.2 \ 3.6 \ 3.3 \ 3.6 \ 3.0 \\ 1.1 \ 1.4 \ 1.8 \ 2.5 \ 3.7 \ 5.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ 2.6 \end{array} \bigg| \begin{array}{r} 3.6 \\ 3.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ 7.0.0 \end{array} \bigg| \begin{array}{r} 0.1 \\ 2.4 \end{array}$$

$$\begin{array}{r} F \\ 4.5 \ 4.7 \ 3.7 \ 2.7 \ 2.8 \\ 4.0 \ 2.6 \ 1.9 \ 1.6 \ 1.3 \end{array} \bigg| \begin{array}{r} 2.6 \\ 2.6 \end{array}$$

$$\begin{array}{r} F \\ 3.3 \ 4.1 \ 3.9 \ 3.7 \ 4.2 \\ 1.1 \ 1.3 \ 2.6 \ 3.7 \ 4.1 \end{array}$$

$$\begin{array}{r} 2.5 \\ 2.5 \end{array} \bigg| \begin{array}{r} 4.0 \\ 4.0 \end{array}$$

Spike in West Side of Pow Pole 25 ft ht 131+85

B.M.

1014.24

5.29 101953

B.M.

5.51

1014.02

5.51 101953

129+50

38 Lt 55
40 Rt

130

4.2 Lt 59
4.4 Rt

+50

4.8 Lt 65
5.0 Rt

131

5.3 Lt
5.5 Rt

+50

5.7 Lt
5.9 Rt

B.M.

1014.02

2.92 1016.94

B.M.

7.06 1009.88

Spike in West Side of Pow Pole 25ft left 131+85

Spike in East Side of Pow Pole 25ft left 131+85

$\frac{6.0}{F2.2} \left \begin{array}{l} 244 \\ 244 \end{array} \right.$	$\begin{array}{cccccccc} & F & & & & & & \\ 6.0 & 6.9 & 5.9 & 4.8 & 3.8 & 3.8 & 3.9 & 4.2 & 4.2 & 4.1 & 4.3 \\ 40 & 31 & 23 & 19 & 16 & 12 & 3.5 & 11 & 20 & 30 & 40 & 50 \end{array}$	$\frac{4.2}{D.C.1.3} \left \begin{array}{l} 28.6 \\ 28.6 \end{array} \right.$
$\frac{6.1}{F1.9} \left \begin{array}{l} 23.8 \\ 23.8 \end{array} \right.$	$\begin{array}{cccccccc} & F & & & & & & \\ 6.4 & 6.2 & 6.0 & 4.9 & 4.6 & 4.1 & 4.3 & 4.4 & 4.2 & 4.7 & 5.1 \\ 40 & 31 & 22 & 19 & 18 & 13 & 3.9 & 10 & 20 & 30 & 40 & 50 \end{array}$	$\frac{3.9}{D.C.2.0} \left \begin{array}{l} 28.1 \\ 28.1 \end{array} \right.$
$\frac{7.0}{F2.2} \left \begin{array}{l} 24.2 \\ 24.2 \end{array} \right.$	$\begin{array}{cccccccc} & F & & & & & & \\ 7.0 & 7.1 & 6.9 & 6.4 & 5.5 & 4.8 & 4.9 & 4.6 & 5.0 & 4.5 & 4.9 & 4.5 & 4.3 & 5.1 \\ 40 & 33 & 23 & 20 & 18 & 14 & 4.5 & 10 & 15 & 18 & 21 & 34 & 33 & 46 & 50 \end{array}$	$\frac{4.9}{D.C.1.6} \left \begin{array}{l} 27.2 \\ 27.2 \end{array} \right.$
$\frac{6.8}{F1.5} \left \begin{array}{l} 23.1 \\ 23.1 \end{array} \right.$	$\begin{array}{cccccccc} & F & & & & & & \\ 7.3 & 7.0 & 7.0 & 6.7 & 5.7 & 5.3 & 5.3 & 4.3 & 4.0 & 4.1 & 4.0 \\ 40 & 30 & 22 & 19 & 18 & 14 & 5.0 & 9 & 15 & 23 & 36 & 47 \end{array}$	$\frac{9.2}{C1.3} \left \begin{array}{l} 26.6 \\ 26.6 \end{array} \right.$
$\frac{6.5}{F0.8} \left \begin{array}{l} 21.6 \\ 21.6 \end{array} \right.$	$\begin{array}{cccccccc} & F & & & & & & \\ 7.4 & 6.6 & 6.3 & 5.1 & 5.8 & 5.7 & 5.1 & 5.2 & 5.3 & 5.0 & 5.3 \\ 40 & 27 & 19 & 15 & 13 & 5.4 & 11 & 14 & 21 & 30 & 40 & 50 \end{array}$	$\frac{5.2}{C0.7} \left \begin{array}{l} 28.4 \\ 28.4 \end{array} \right.$

Spike in East Side of Pow. Pole 25ft left 131+85

Spike in Guide Pole 20ft left 139+20

Extension of Xsecs on Rt. Side

109

+50

110

+50

111

+50

112

+50

113

+50

114

+50

+60

Extension of Xsecs on RT Side

$$5.6 \begin{array}{r} 4.8 \quad 5.4 \quad 6.5 \quad 7.7 \\ 50 \quad 57 \quad 67 \quad 68 \end{array}$$

$$5.3 \begin{array}{r} 2.4 \quad 3.2 \quad 5.2 \quad 6.9 \\ 50 \quad 55 \quad 60 \quad 64 \end{array}$$

$$5.1 \begin{array}{r} 2.2 \quad 6.5 \\ 50 \quad 59 \end{array}$$

$$5.1 \begin{array}{r} 2.0 \quad 4.5 \quad 6.0 \\ 45 \quad 51 \quad 53 \end{array}$$

$$4.8 \begin{array}{r} 2.4 \quad 5.8 \\ 50 \quad 58 \end{array}$$

$$4.6 \begin{array}{r} 2.0 \quad 5.9 \\ 45 \quad 55 \end{array}$$

$$5.7 \begin{array}{r} 2.7 \quad 5.0 \quad 6.2 \\ 46 \quad 50 \quad 55 \end{array}$$

$$5.6 \begin{array}{r} 3.0 \quad 5.0 \quad 6.3 \\ 46 \quad 50 \quad 54 \end{array}$$

$$5.3 \begin{array}{r} 2.6 \quad 6.1 \\ 46 \quad 53 \end{array}$$

$$5.0 \begin{array}{r} 2.5 \quad 5.8 \\ 47 \quad 54 \end{array}$$

$$5.0 \begin{array}{r} 3.4 \quad 6.3 \\ 47 \quad 54 \end{array}$$

$$4.9 \begin{array}{r} 5.6 \quad 4.7 \\ 50 \quad 58 \end{array}$$

$$4.9 \begin{array}{r} 6.0 \quad 4.9 \\ 50 \quad 58 \end{array}$$

117+25

+50

118

+25

+50

+75

119

+20

+50

+75

120

+30

+50

$$8.0 \quad \frac{9.4}{50} \quad \frac{9.9}{56} \quad \frac{10.5}{61}$$

$$7.2 \quad \frac{7.1}{50} \quad \frac{7.4}{51} \quad \frac{9.4}{55}$$

$$6.9 \quad \frac{6.9}{50} \quad \frac{7.2}{51} \quad \frac{9.5}{55}$$

$$4.5 \quad \frac{6.3}{50} \quad \frac{6.6}{52} \quad \frac{9.2}{56}$$

$$6.1 \quad \frac{5.2}{47} \quad \frac{8.9}{55}$$

$$5.7 \quad \frac{4.5}{48} \quad \frac{8.7}{57}$$

$$5.5 \quad \frac{3.4}{47} \quad \frac{8.3}{55}$$

$$5.1 \quad \frac{2.8}{45} \quad \frac{7.8}{53}$$

$$4.8 \quad \frac{2.4}{46} \quad \frac{7.8}{55}$$

$$4.8 \quad \frac{2.9}{48} \quad \frac{7.7}{55}$$

$$4.9 \quad \frac{4.1}{50} \quad \frac{8.2}{56}$$

$$5.0 \quad \frac{4.3}{50} \quad \frac{8.4}{57}$$

120+75

121

124

+50

125

+50

126

+50

129

+50

128

+50

129

$$5.1 \frac{5.7}{51} \frac{8.8}{58}$$

$$5.2 \frac{6.2}{54} \frac{8.2}{61}$$

$$6.0 \frac{8.6}{62} \frac{10.3}{65}$$

$$5.6 \frac{6.1}{61} \frac{9.3}{70}$$

$$5.1 \frac{5.1}{61} \frac{8.7}{71}$$

$$5.1 \frac{4.0}{63} \frac{9.2}{73}$$

$$5.7 \frac{7.4}{50} \frac{6.3}{69} \frac{10.2}{76}$$

$$5.1 \frac{5.7}{70} \frac{8.6}{77}$$

$$4.9 \frac{6.1}{71} \frac{8.6}{76}$$

$$4.7 \frac{6.7}{64} \frac{7.5}{74} \frac{8.2}{79}$$

$$4.5 \frac{5.7}{74} \frac{6.9}{76}$$

$$4.2 \frac{4.1}{52} \frac{4.3}{72} \frac{6.9}{76}$$

$$4.2 \frac{4.4}{44} \frac{4.7}{50} \frac{5.7}{55} \frac{4.4}{58} \frac{5.1}{66} \frac{7.0}{70}$$

$$129 + 50$$

$$130$$

$$+ 50$$

$$131$$

$$+ 7$$

$$+ 50$$

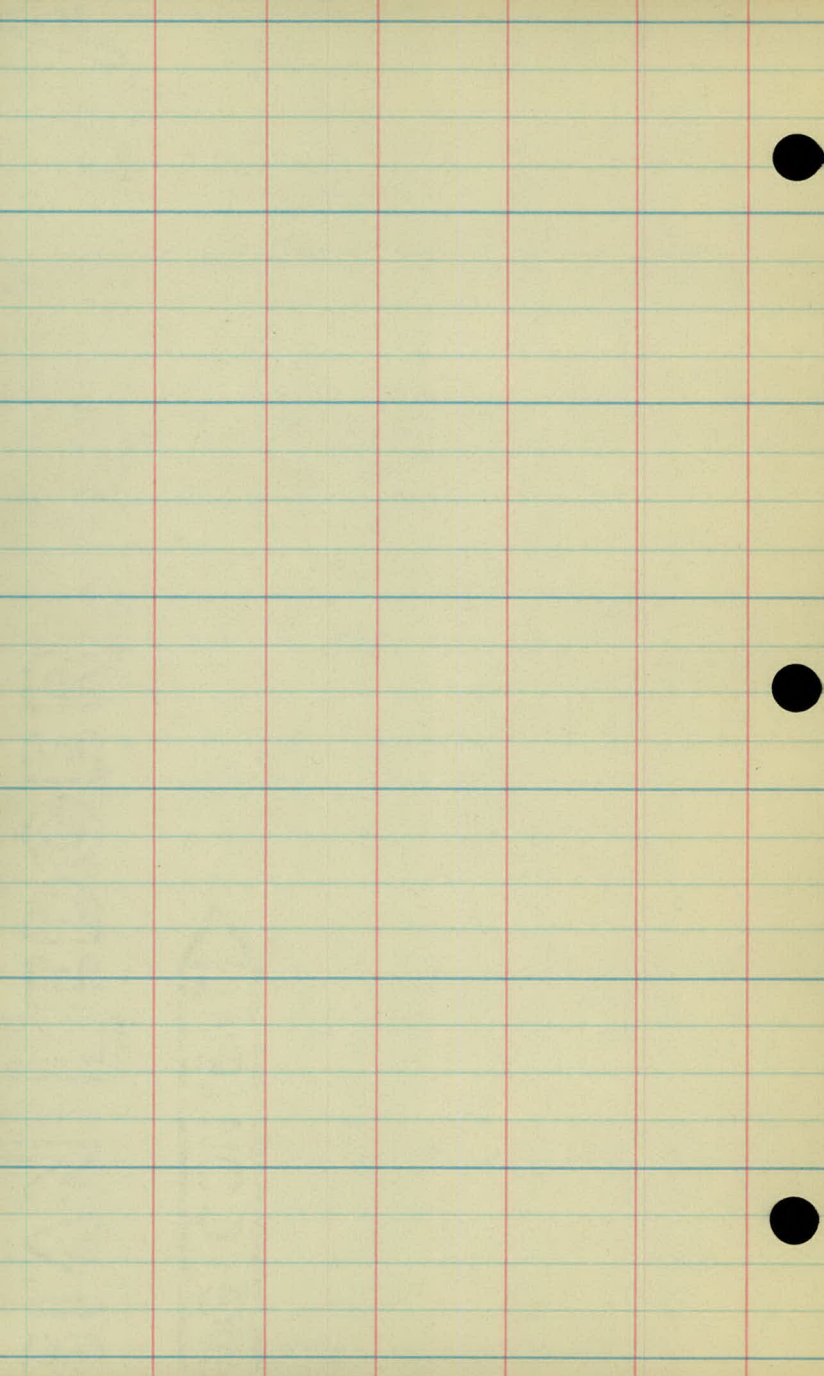
$$4.1 \quad \frac{4.6}{65} \quad \frac{5.4}{78} \quad \frac{7.9}{82}$$

$$4.7 \quad \frac{5.5}{53} \quad \frac{5.4}{78} \quad \frac{9.6}{87}$$

$$5.3 \quad \frac{4.8}{55} \quad \frac{4.1}{61} \quad \frac{4.2}{80} \quad \frac{8.5}{89}$$

$$5.9 \quad \frac{3.5}{50} \quad \frac{4.6}{53} \quad \frac{3.5}{57} \quad \frac{2.8}{78} \quad \frac{6.5}{85} \quad \frac{8.7}{91}$$

$$6.1 \quad \frac{5.0}{56} \quad \frac{4.7}{69} \quad \frac{4.5}{84} \quad \frac{7.6}{94}$$



County Road "C" - Cleveland Ave West.

Scattered Remeasurements

Cleveland Ave to New Brighton Rd.

Station 53+50 to 78+80

Remeasurements County Road "C"

53+50

54

+50

+90

55

+50

+58

56

+50

57

+25

+50

58

Remeasurements County Road "C"

$$\begin{array}{r} 0.6 \\ 28 \end{array} \frac{97}{20} \frac{93}{12} 89$$

$$\begin{array}{r} 9.6 \\ 25 \end{array} \frac{11.0}{24} \frac{99}{21} \frac{86}{18} \frac{84}{8} 8.3$$

$$\begin{array}{r} 0.6 \\ 29 \end{array} \frac{88}{24} \frac{88}{21} \frac{73}{18} \frac{74}{10} 7.1$$

00

$$\begin{array}{r} 0.6 \\ 27 \end{array} \frac{66}{20} \frac{64}{9} 6.2$$

$$\begin{array}{r} 0.6 \\ 28 \end{array} \frac{4.3}{26} \frac{4.4}{22} \frac{19}{19} \frac{18}{11} 1.5$$

$$\begin{array}{r} 0.6 \\ 28 \end{array} \frac{3.7}{24} \frac{3.5}{21} \frac{13}{18} \frac{12}{11} 0.9$$

$$\begin{array}{r} 0.6 \\ 28 \end{array} \frac{10.7}{25} \frac{10.7}{21} \frac{9.8}{18} \frac{8.9}{10} 8.6$$

58+50

59

+50

+70

60

+50

61

+40

+50

+75

62

+35

+50

L C R

$$\begin{array}{r} 0.6 \quad 9.0 \quad 9.1 \quad 7.5 \quad 7.6 \\ 31.7 \quad 25 \quad 21.5 \quad 18 \quad 10 \end{array} \quad 7.4$$

$$\begin{array}{r} 0.6 \quad 7.5 \quad 7.9 \quad 6.4 \quad 6.5 \\ 33 \quad 25 \quad 21 \quad 18 \quad 9 \end{array} \quad 6.3$$

$$\begin{array}{r} 0.6 \quad 6.4 \quad 6.5 \quad 5.0 \quad 5.0 \\ 34 \quad 23 \quad 20 \quad 18 \quad 9 \end{array} \quad 4.9$$

$$\begin{array}{r} 0.6 \quad 6.0 \quad 6.0 \quad 4.6 \quad 4.5 \\ 35 \quad 23 \quad 20 \quad 18 \quad 9 \end{array} \quad 4.5$$

$$\begin{array}{r} 0.6 \quad 5.7 \quad 6.4 \quad 4.2 \quad 4.1 \\ 34 \quad 23 \quad 20 \quad 18 \quad 8 \end{array} \quad 4.1$$

$$\begin{array}{r} 0.6 \quad 5.0 \quad 5.0 \quad 3.5 \quad 3.3 \\ 35 \quad 23 \quad 20 \quad 18 \quad 8 \end{array} \quad 3.3$$

$$\begin{array}{r} 0.6 \quad 4.9 \quad 4.9 \quad 3.4 \quad 3.2 \\ 32 \quad 24 \quad 21 \quad 18 \quad 8 \end{array} \quad 3.1$$

$$\begin{array}{r} 0.6 \quad 4.7 \quad 4.6 \quad 3.4 \quad 3.3 \\ 35 \quad 24 \quad 21 \quad 18 \quad 9 \end{array} \quad 3.1$$

62+75

63

+50

64

+50

65

+50

66

+40

+50

67

+50

68

$$4.0 \quad \frac{4.1}{9} \quad \frac{4.3}{20} \quad \frac{0.6}{26.6}$$

$$4.4 \quad \frac{4.6}{9} \quad \frac{4.7}{20} \quad \frac{0.6}{25.8}$$

$$4.6 \quad \frac{4.7}{10} \quad \frac{4.9}{20} \quad \frac{0.6}{25.0}$$

$$\frac{0.6}{22.8} \quad \frac{4.8}{19} \quad \frac{5.0}{14} \quad 4.5 \quad \frac{4.7}{10} \quad \frac{4.8}{20} \quad \frac{6.7}{25.2}$$

$$\frac{0.6}{2.8} \quad \frac{6.7}{2.4} \quad \frac{6.7}{2.1} \quad \frac{5.3}{18} \quad \frac{5.1}{14} \quad 4.9 \quad \frac{5.1}{}$$

$$\frac{0.6}{2.7.8} \quad \frac{6.8}{2.4} \quad \frac{6.8}{2.1} \quad \frac{5.2}{18} \quad \frac{5.1}{14} \quad 5.1$$

$$\frac{0.6}{2.9.2} \quad \frac{7.4}{2.4} \quad \frac{7.4}{11} \quad \frac{5.9}{18} \quad \frac{5.8}{14} \quad 5.4$$

$$68+49$$

$$+62$$

$$69$$

$$+35$$

$$+50$$

$$+75$$

$$70$$

$$+30$$

$$+54$$

$$71$$

$$+50$$

$$72$$

$$+50$$

$$\begin{array}{r} 0.6 \quad 6.7 \quad 6.7 \quad 5.1 \quad 5.1 \\ 292 \quad 24 \quad 21 \quad 18 \quad 14 \quad 4.8 \end{array}$$

$$\begin{array}{r} 0.6 \quad 4.5 \quad 6.5 \quad 5.1 \quad 5.1 \\ 342 \quad 24 \quad 21 \quad 18 \quad 13 \quad 4.7 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.5 \quad 6.6 \quad 5.2 \quad 5.0 \\ 39 \quad 24 \quad 21 \quad 18 \quad 12 \quad 4.8 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.4 \quad 6.4 \quad 5.0 \quad 5.0 \\ 362 \quad 24 \quad 21 \quad 18 \quad 10 \quad 4.7 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.5 \quad 6.5 \quad 5.0 \quad 4.9 \\ 342 \quad 24 \quad 21 \quad 18 \quad 10 \quad 4.7 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.5 \quad 6.5 \quad 5.1 \quad 4.9 \\ 312 \quad 24 \quad 21 \quad 18 \quad 10 \quad 4.7 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.6 \quad 4.7 \quad 5.0 \quad 4.8 \\ 302 \quad 25 \quad 21 \quad 18 \quad 10 \quad 4.6 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.5 \quad 6.5 \quad 5.2 \quad 5.0 \\ 322 \quad 24 \quad 21 \quad 18 \quad 11 \quad 4.8 \end{array}$$

$$\begin{array}{r} 0.6 \quad 6.7 \quad 6.6 \quad 5.5 \quad 5.3 \\ 362 \quad 24 \quad 22 \quad 18 \quad 11 \quad 5.1 \end{array}$$

73

+52

74

+50

75

+50

1 +62

76

+50

77

+50

+90

78

$$\begin{array}{r} 0.5 \quad 6.2 \quad 6.2 \quad 4.9 \quad 4.7 \\ 27 \quad 24 \quad 21 \quad 18 \quad 11 \end{array} \quad \begin{array}{r} 4.7 \\ 11 \end{array} \quad 4.5$$

$$\begin{array}{r} 0.5 \quad 5.1 \quad 5.1 \\ 25 \quad 19 \quad 11 \end{array} \quad 4.8$$

$$\begin{array}{r} 0.6 \quad 6.3 \quad 6.2 \\ 27.2 \quad 20 \quad 11 \end{array} \quad 6.0$$

$$\begin{array}{r} 0.6 \quad 6.3 \quad 6.2 \\ 28 \quad 20 \quad 11 \end{array} \quad 6.0$$

$$\begin{array}{r} 0.6 \quad 6.3 \quad 6.3 \\ 27.0 \quad 20 \quad 11 \end{array} \quad 6.0$$

$$\begin{array}{r} 0.6 \quad 6.3 \quad 6.3 \\ 26.3 \quad 19 \quad 11 \end{array} \quad 6.0$$

$$\begin{array}{r} 0.6 \quad 8.2 \quad 8.2 \quad 6.7 \quad 6.6 \\ 24.9 \quad 24 \quad 21 \quad 18 \quad 11 \end{array} \quad 6.2$$

$$\begin{array}{r} 0.5 \quad 6.9 \quad 7.0 \quad 5.6 \quad 5.2 \\ 28.9 \quad 23.2 \quad 21.5 \quad 17.5 \quad 11 \end{array} \quad 5.2$$

$$\begin{array}{r} 0.6 \quad 7.0 \quad 7.0 \quad 5.6 \quad 5.5 \\ 31.5 \quad 23.8 \quad 20.2 \quad 18 \quad 11 \end{array} \quad 5.5$$

$$\begin{array}{r} 0.6 \quad 7.1 \quad 7.1 \quad 5.8 \quad 5.6 \\ 31.5 \quad 24 \quad 21 \quad 18 \quad 11 \end{array} \quad 5.5$$

$$78 + 24$$

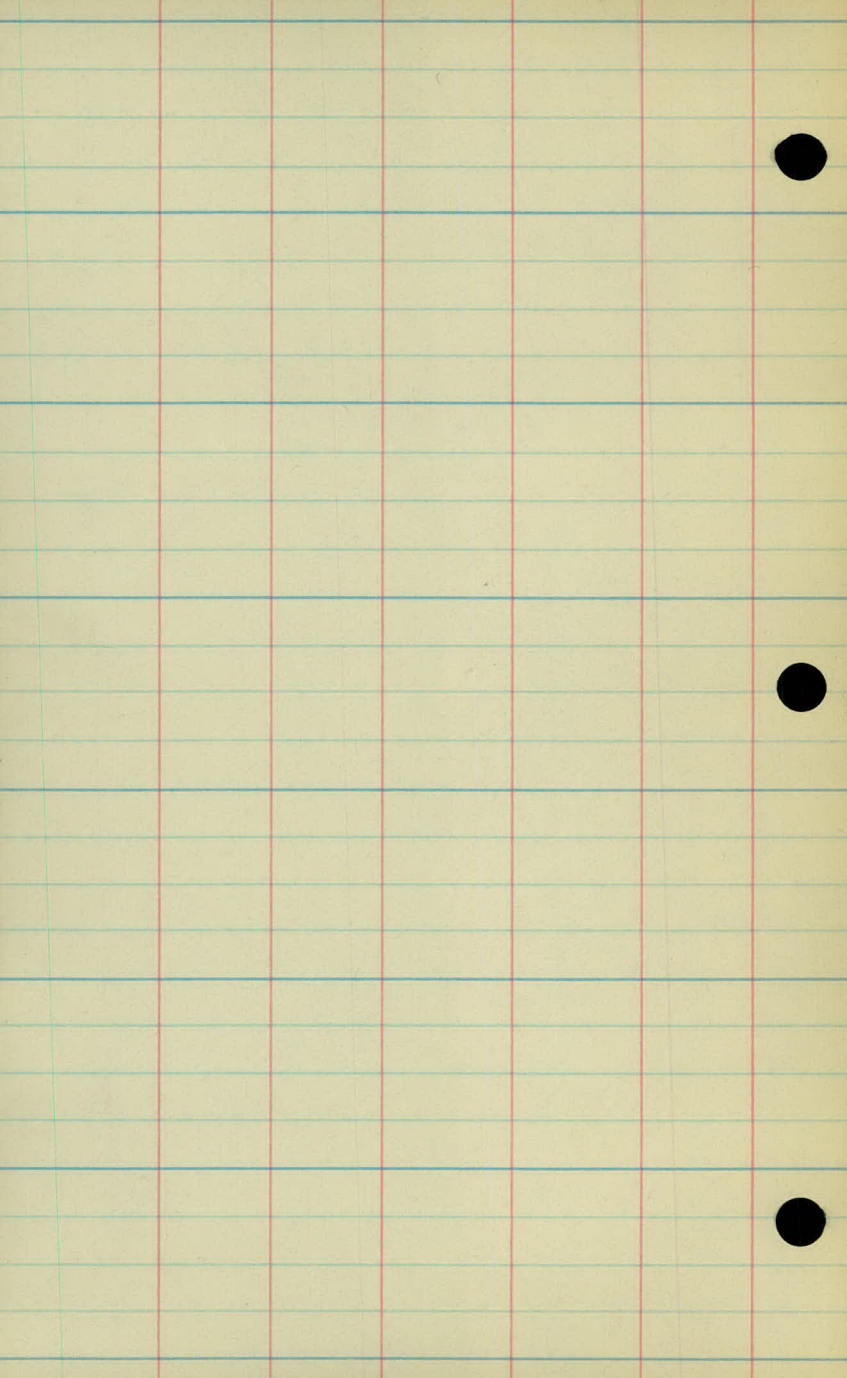
$$+ 50$$

$$+ 80$$

$$\begin{array}{r} 0.6 \quad 7.4 \quad 7.4 \quad 6.1 \quad 5.9 \\ 30 \div 24 \quad 21 \quad 18 \quad 11 \quad 5.7 \end{array}$$

$$\begin{array}{r} 0.6 \quad 7.8 \quad 7.8 \quad 4.3 \quad 6.2 \\ 27 \div 24 \quad 21 \quad 18 \quad 11 \quad 6.0 \end{array}$$

$$\begin{array}{r} 0.8 \quad 8.3 \quad 8.2 \quad 4.7 \quad 6.4 \\ 28 \div 27 \quad 25 \quad 22 \quad 11 \quad 6.0 \end{array}$$



County Road "C" - Cleveland Ave West
Alignment - Hamline Ave to Lexington Ave,
Station 132+07⁶⁵ to 165+71⁰⁵

Station	Point	ΔL	ΔR	Lt	Rt
---------	-------	------------	------------	----	----

165+71 ⁰⁵	P.I.	0° 54'			
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162+91 ⁹	P.O.T.				
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143+16 ⁷	P.O.T.				
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139+49 ⁸⁸	P.I.		90° 55' R		
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132+07 ⁶⁵	P.I.	91° 35' L			
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3/15/34
- Windy.

Intersection Lexington Ave & Cor'd "C"

Light Pole 45° Spike 337 746¹⁰ Tel Pole Monument

Spike 666 Tel Pole

515 Tel Pole

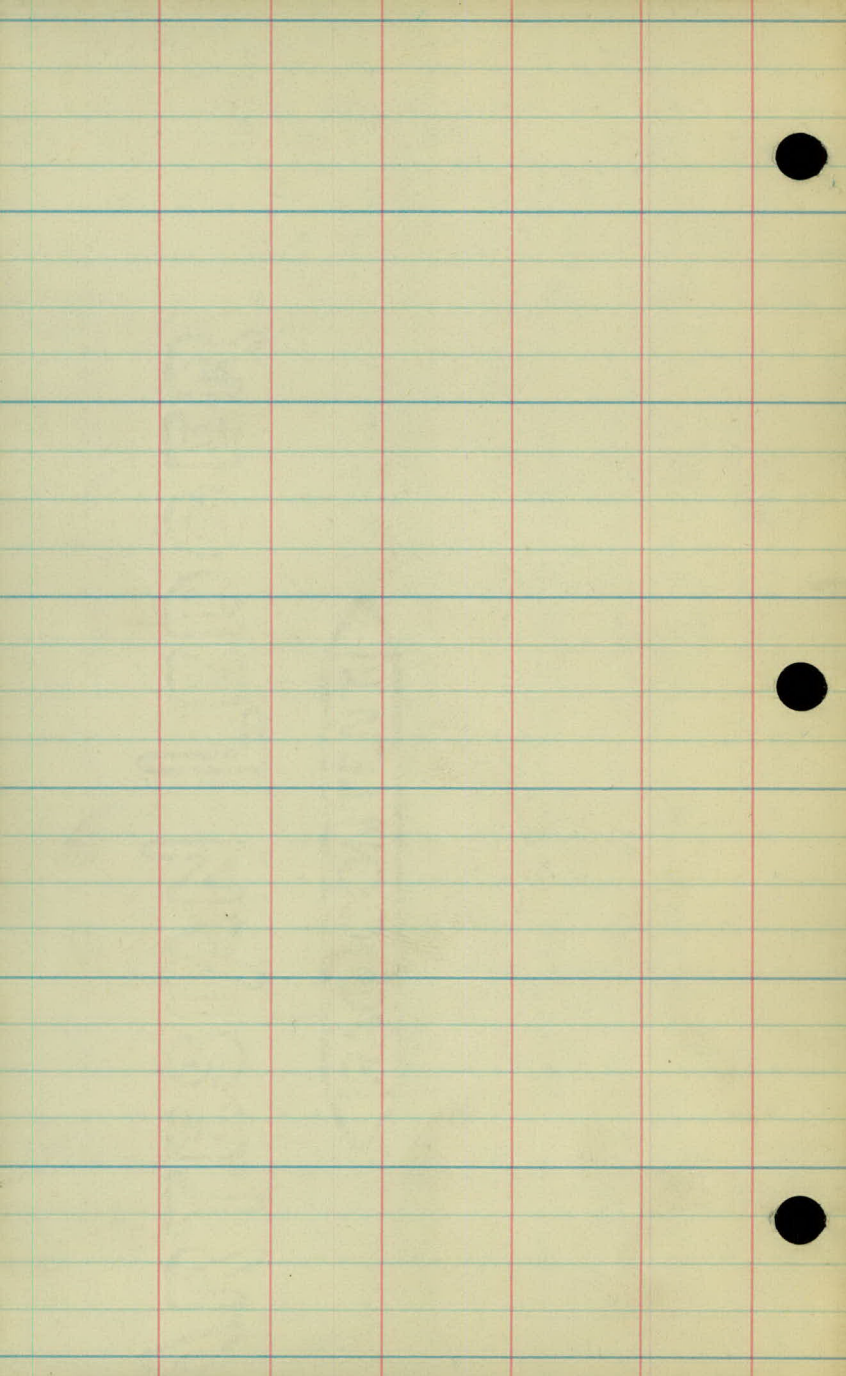
Pow Pole 602 Spike 242 Tel Pole

530

Intersection Hamline & Cor'd "C" East

G.P. 32

Intersection Hamline & Cor'd "C" West Monument



County Road "C" - Cleveland Ave West

Cross-sections & Slope Stakes.

Hamline Ave West.

Station 139+50 to 142+00

B.M.

1009.88

3.95 1013.83

39+50

+64

+77

Beginning 36" Woven Wire 1 Strand Barbed.

40

5.2 6.7

+50

5.3 6.8

41

5.3 6.8

+50

5.3 6.8

42

5.3 6.8

T.P.

4.01 1009.82

Spike in Guide Pole 20ft left / 39+20

5.0 4.9 4.8 4.5 4.4
50 40 30 20 10 4.2 10 20 30 40

5.3 5.2 5.1 4.9 4.8
50 40 30 20 10 4.6 10 20 30

6.2 6.1 5.8 5.4 5.4 4.9
50 40 30 25 20 10 4.7 10 25 28 34 50

5.5 7.3 6.8 6.5 5.5 5.5 5.5 5.3 5.4 5.1 4.7 4.6
D.C.1.2 26.4 50 41 31 27 24 19 15 4.7 13 17 26 40 50 27 4.9
10 C.0.3

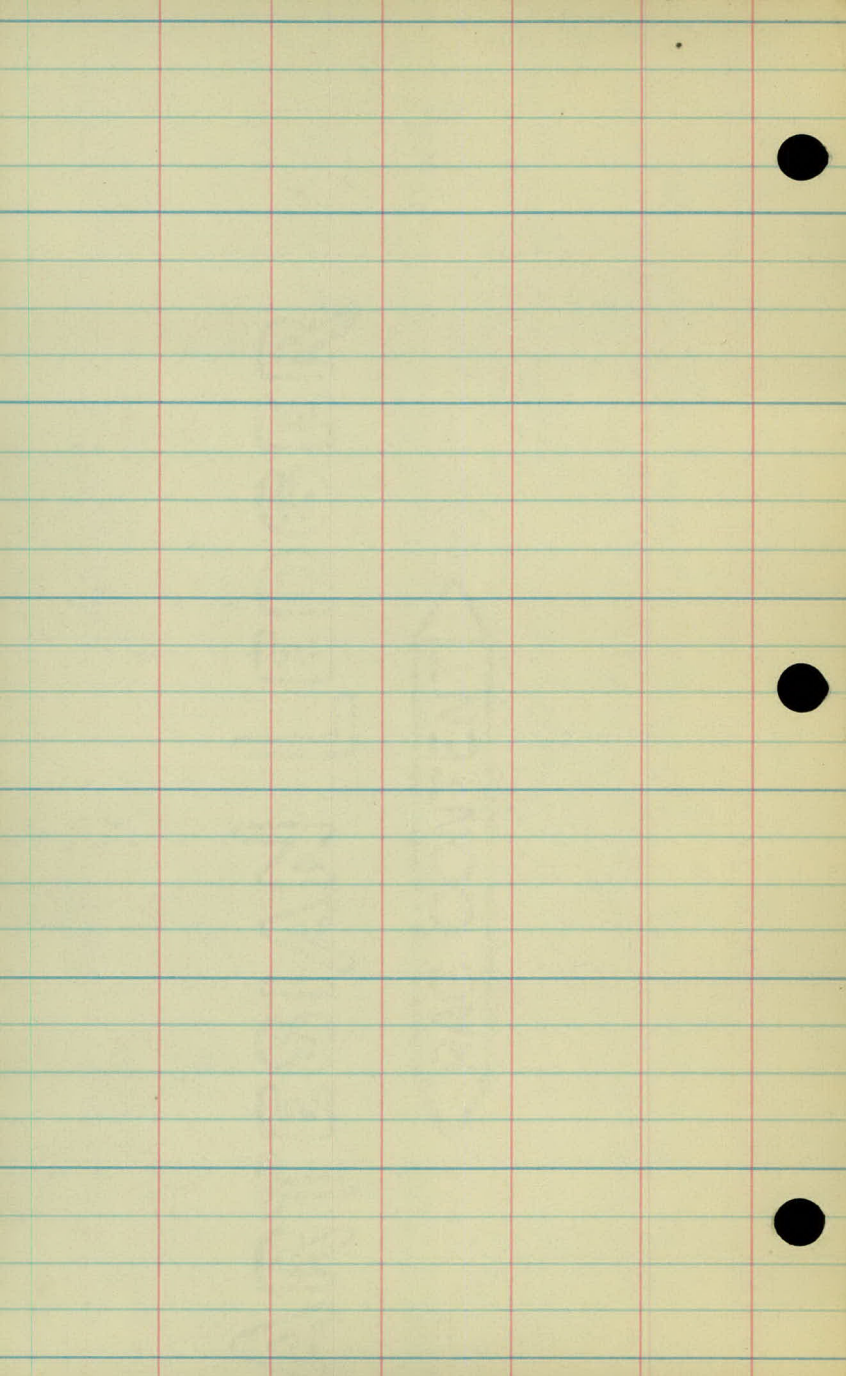
5.4 7.2 6.7 6.4 5.6 5.2 5.6 5.9 5.2 5.2 5.3 5.8 5.0 4.4 4.0
D.C.1.4 26.8 50 40 35 30 28 24 17 16 12 4.8 12 14 16 25 40 50 28 4.8
10 C.0.5

6.8 8.0 7.6 7.6 7.8 7.0 6.8 6.8 5.2 5.2 5.5 5.9 5.6 4.8 4.4
D.C.0.0 27.0 50 40 32 21 28 24 17 12 4.8 11 14 16 25 40 50 26.4 5.6
P.C.1.2

6.6 7.0 7.3 7.3 7.0 6.8 7.3 7.5 5.3 5.3 5.8 6.0 5.7
D.C.0.0 27.0 50 40 28 27 24 21 20 12 4.8 12 20 36 50

6.0 6.1 6.3 6.0 6.0 6.3 5.2 5.0 5.3 6.2 5.8 5.4 5.4
D.C.0.8 25.6 50 40 29 28 24 17 13 4.8 11 12 17 26 35 50 26 5.8
P.C.1.0

on Gd stake 15ft left / 43+16.7 P.O.T.



Road A² near New Brighton Rd.
Grade & Slope Stakes Rt. Side
Station 90 to 92+50

Back D.L.

Excav
GradeShoulder
GradeDitch
Grade

90+00

8.10

7.90

9.8

+50

6.90

6.70

9.98

91

6.55

6.35

10.16

+50

29²

6.45

6.25

10.34

92

7.20

7.00

10.52

+50

8.15

7.95

10.7

Voice/S

$$7.60 \quad \begin{array}{r} 9 \\ 10 \overline{) 85} \\ \underline{D.C.1.3} \end{array} \quad \begin{array}{r} 14 \\ 12 \overline{) 9.0} \\ \underline{D.C.0.4} \end{array}$$

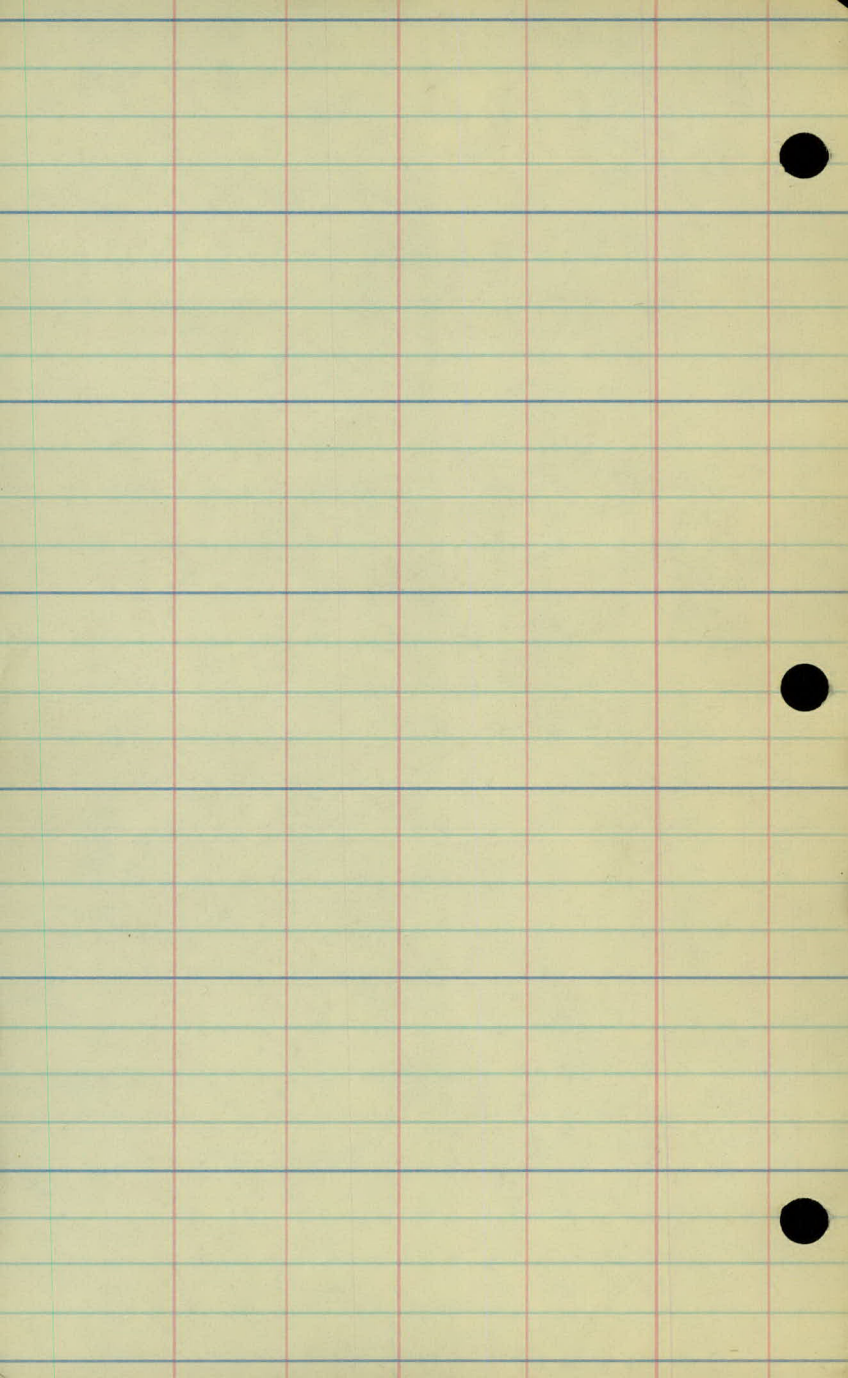
$$6.40 \quad \begin{array}{r} 35 \\ 14 \overline{) 49} \\ \underline{D.C.3.1} \end{array} \quad \begin{array}{r} 8.2 \\ \underline{D.C.0.0} \end{array}$$

$$6.05 \quad \begin{array}{r} 4 \\ 1.4 \overline{) 4.6} \\ \underline{D.C.6.6} \end{array} \quad \begin{array}{r} 2 \\ 20 \overline{) 8.1} \\ \underline{D.C.0.0} \end{array}$$

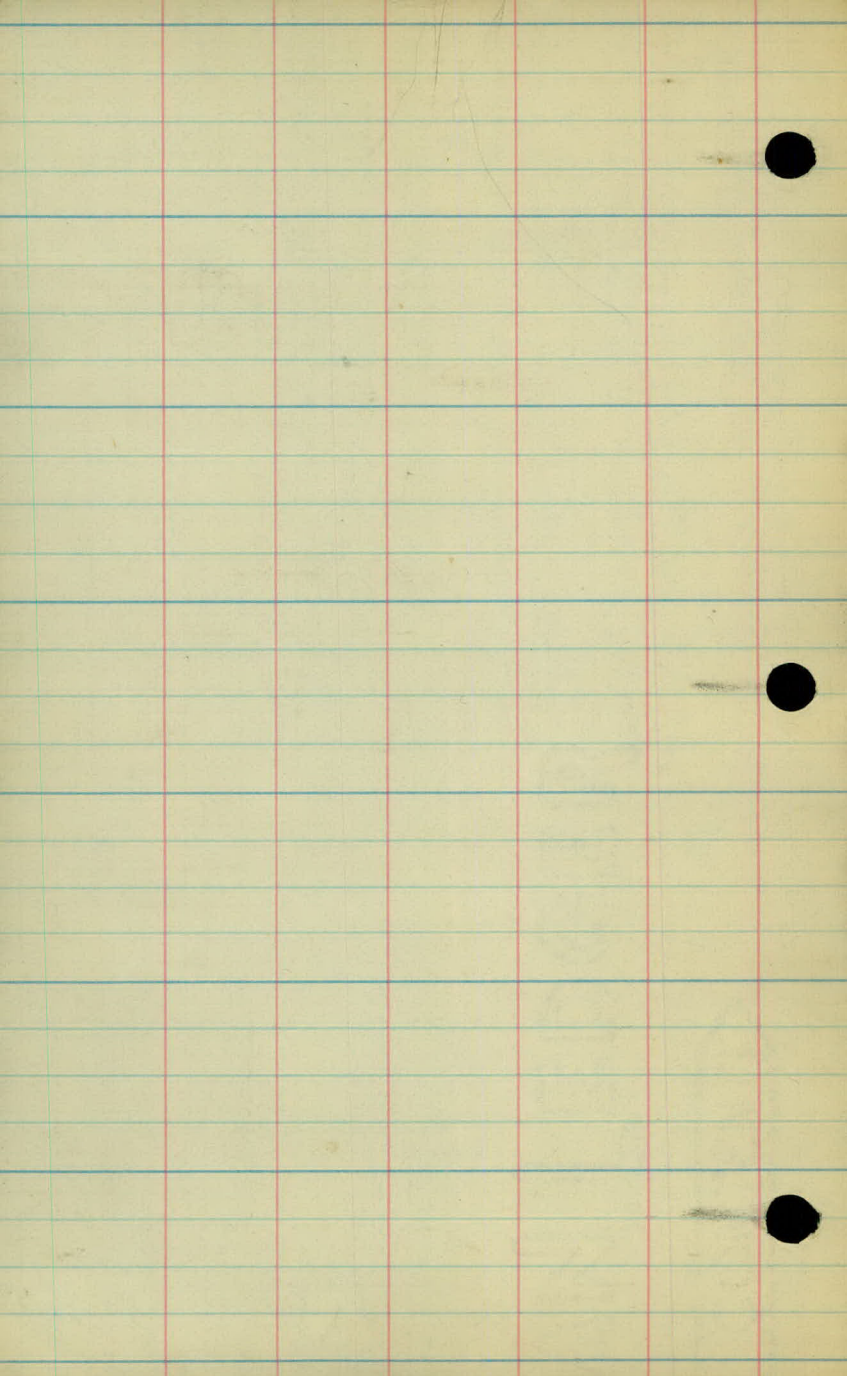
$$5.95 \quad \begin{array}{r} 40 \\ 15 \overline{) 46} \\ \underline{D.C.5.7} \end{array} \quad \begin{array}{r} 30 \\ 10 \overline{) 5.0} \\ \underline{D.C.3.0} \end{array}$$

$$6.70 \quad \begin{array}{r} 39 \\ 12 \overline{) 65} \\ \underline{D.C.5.0} \end{array} \quad \begin{array}{r} 30 \\ 12 \overline{) 5.6} \\ \underline{D.C.3.1} \end{array}$$

$$7.65 \quad \begin{array}{r} 34 \\ 14 \overline{) 80} \\ \underline{D.C.2.7} \end{array} \quad \begin{array}{r} 27 \\ 14 \overline{) 80} \\ \underline{D.C.1.7} \end{array}$$



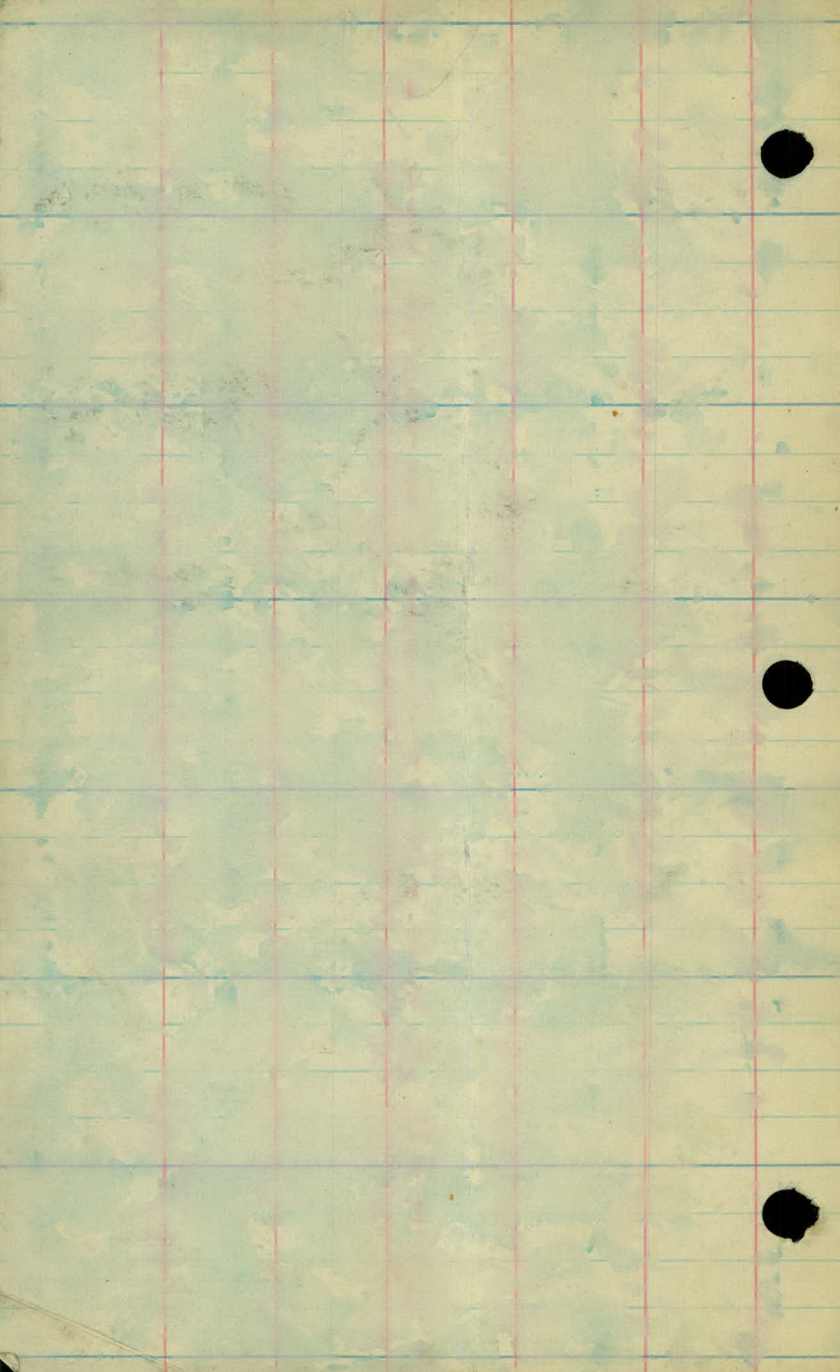
GRADE STAKE NOTES
COUNTY ROAD "C"



SEC. TIES

Co. Rd. "C."

From S.T.M. #1 to
East Co. Liite





105+00.45

P.P.
32.32 28.74
85.22
T.P. 12.10

S.W. Cor. Sec. 2

78+73.15

T.P.
47.55 39.03
47.70
P.P.
T.P. E.P.

S. 1/4 Cor. Sec. 3
Rock St.

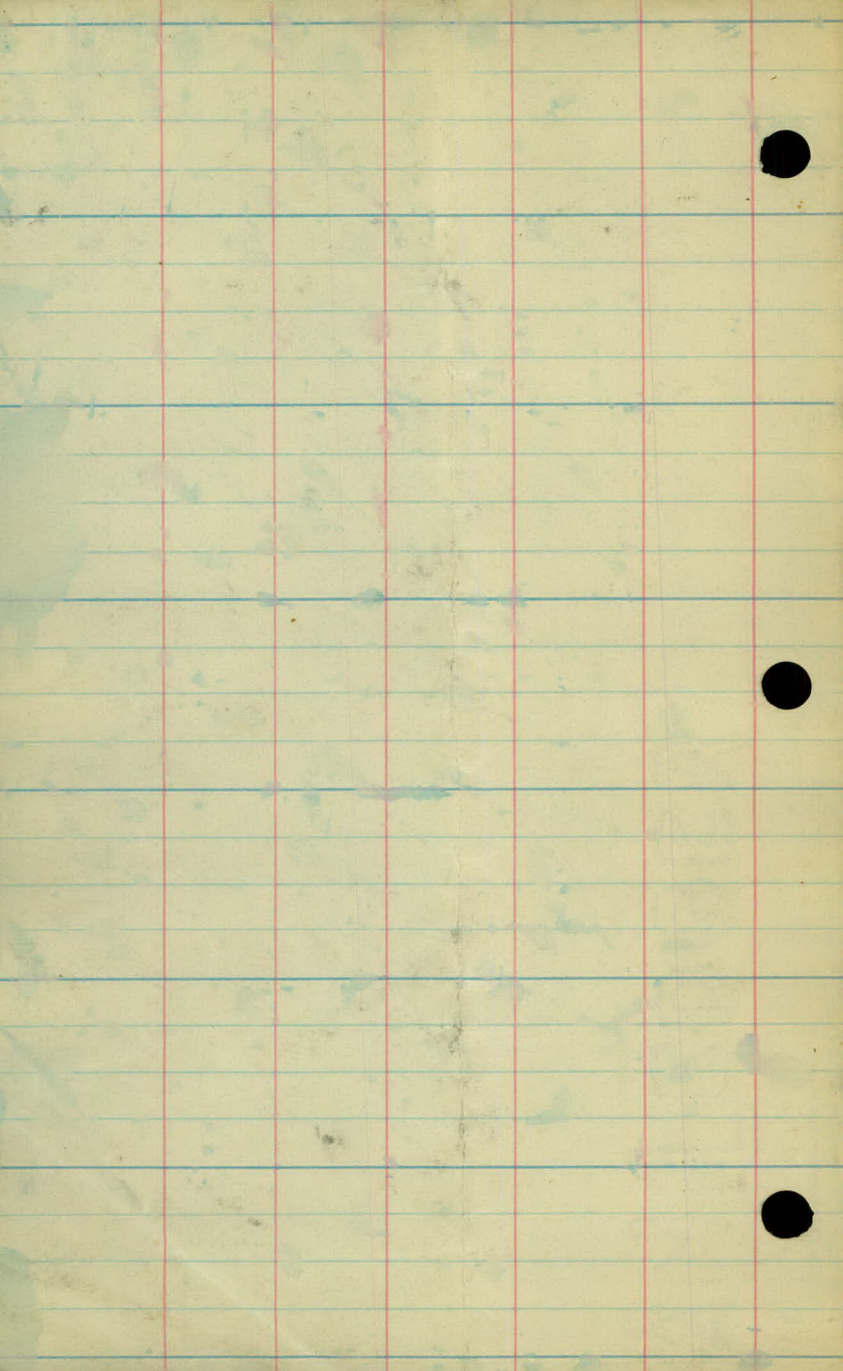
52+41.10

30.22 71.9
39.13
T.P.

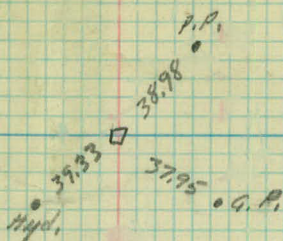
S.W. Cor. Sec. 3

38+48.6

S. T. H. No. 1



Sta. 209+81.8
E. Co. Line.

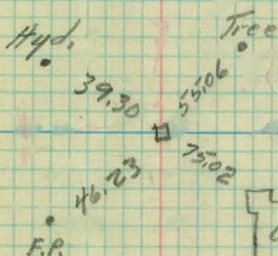


S.E. Cor. Sec.

P.O.T. 189+00

Hub

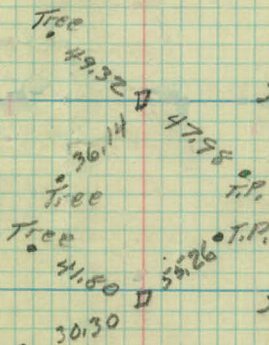
183+71.6



So. 1/4 Cor. Sec. 1

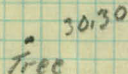
church

157+59.6



S.W. 1/4 Cor. Sec. 1

131+34.0



S. 1/4 Cor. Sec. 2

Cod. 2600

6-00

7-20

8-50

E

$$\begin{array}{r} F. 2.2 \\ \hline 21.3 \end{array}$$

$$\begin{array}{r} F. 5.1 \\ \hline 25.1 \end{array}$$

$$\begin{array}{r} F. 2.7 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} F. 4.0 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} F. 1.8 \\ \hline 20.7 \end{array}$$

$$\begin{array}{r} F. 3.4 \\ \hline 23.1 \end{array}$$

Dec. 9 - Cloudy - Snow
 1933 120 above
 Von Hippel - Chief
 Jay. A. ROBERTS - Notes
 Rachetto - Red
 Michell - Green
 Morrison - ✓

Road C^u

39+50	50 Gr.	
40+00	50	
40+33	2	Conc. Steps 2.4' 1 slope
40+50	50	21.5' from E
41+00	50	
41+40 + 44	50	
41+50	50	
42+00	50	
42+50	50	
43+00	50	
43+50	50	
43+60	50	
44+00	50	
44+50	50	

NoRoad "C"
LSo~~C.O. 2~~
27.4~~F. 2.0~~
26.0~~C. 2.9~~
~~32.8~~C 3.3
30.6 2:1~~P.C. 0.6~~ ✓
28.2~~C. 4.8~~
~~36.6~~C 5.6
32.2 2:1~~O.C. 1.2~~ ✓
26.4~~C. 4.0~~
~~35.0~~C 4.6
33.2 2:1C.O. 3
27.6

C. 3.2

34.4

C. 1.2

C 3.8
31.6 2:1

36.0

C. 1.8
30.6C. 2.4
31.8C. 1.8
30.6C. 3.3
33.6C. 1.7
30.4C. 3.8
34.6~~O. 0~~
27.0C. 2.6
32.2P.C. 0.8
25.6C. 1.5
30.0F. 1.6
24.8C. 0.9
28.8

Road "C"

44+90

5.0

45+50

5.0

46+00

5.0

46+50

5.0

47+00

5.0

47+50

5.0

48+00

5.0

48+50

5.0

49+00

5.0

49+50

5.0

49+75

50+00

5.0

50+25

50+50

50+75

51+00

50+75

Road C⁴₂

2

$$\begin{array}{r} F.1.6 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} DC.1.4 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} DC.0.3 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} DC.0.5 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} DC.0.4 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} DC.0.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} DC.0.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} DC.0.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} F.3.3 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} DC.1.3 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} F.4.8 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} DC.0.2 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} F.5.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} F.1.6 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} F.5.7 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} F.2.5 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} DC.0.5 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} F.8.7 \\ \hline 29.1 \end{array}$$

$$\begin{array}{r} 1/2:1 \\ \hline C.1.3 \\ \hline 27.5 \end{array}$$

$$\begin{array}{r} 1/2:1 \rightarrow \\ \hline C.2.0 \\ \hline 41.5 \end{array}$$

$$\begin{array}{r} 1/2:1 \\ \hline C.1.6 \\ \hline 47.5 \end{array}$$

$$\begin{array}{r} C.14.3 \\ \hline 44.9 \end{array}$$

Stakes changed by Carley

$$\begin{array}{r} C.1.9 \\ \hline 30.5 \\ \hline C.8.8 \\ \hline 42.3 \\ \hline C.13.6 \\ \hline 51.3 \\ \hline C.16.1 \\ \hline 56.0 \\ \hline C.16.7 \\ \hline 56.6 \\ \hline C.10.1 \\ \hline 47.2 \\ \hline C.14.2 \\ \hline 53.4 \end{array}$$

$$1.8:1$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$(1.8:1)$$

$$\begin{array}{r} F.3.7 \\ \hline 29.9 \end{array}$$

$$\begin{array}{r} C.0.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} C.5.9 \\ \hline 38.8 \end{array}$$

$$\begin{array}{r} C.12.6 \\ \hline 54.2 \end{array}$$

Hard

Log of "C"

51+30	$\frac{1}{2} \cdot 1$ C. 6.7 32.8	$\frac{C. 6.7}{40.8} (2.1)$ 5.0	C. 13.3 55.6
51+50			
51+60		$\frac{C. 6.7}{40.4} (2.1)$ 5.0	
51+90	D.C. 1.0 23.5	5.0	C. 9.8 46.6
52+00		$\frac{C. 4.7}{36.4} (2.1)$ 5.0	
52+60	D.C. 0.1 24.2	5.0	F 3.2 27.6
53+00	F 6.7 38.1	5.0	F 6.6 37.8
53+50	F 7.7 41.7	5.0	F 7.3 29.6
54+00	F 8.0 42.0	5.0	F 7.0 39.0
54+50	F 5.9 35.7	5.0	F 5.8 35.4
55+00	F 2.9 26.7	5.0	F 3.0 27.0
55+50	F 2.4 25.2	5.0	F 1.8 23.4
56+00	F 1.6 22.8	5.0	C 0.2 27.4
56+50	F 3.0 27.0	5.0	C 1.8 30.6
57+00	F 3.5 28.5	5.0	C 2.8 32.0

Dec - 11th - Sub. Zero.
15-18 Below.
Sharp Wind.

$$57+50 \quad \frac{F.3.0}{27.0} \quad \text{Road } 764 \quad 50 \quad \frac{0.24}{29.8} \quad 3$$

$$58+10 \quad \frac{F.5.9}{35.7} \quad 50 \quad \frac{0.15}{27.0}$$

$$58+50 \quad \frac{F.6.3}{36.9} \quad 50 \quad \frac{0.07}{27.4}$$

$$59+00 \quad \frac{F.5.9}{35.7} \quad 50 \quad \frac{0.3.1}{34.1}$$

$$59+50 \quad \frac{06.00}{27.5} \quad 50 \quad \frac{0.35}{33.4}$$

$$60+00 \quad \frac{0.0.05}{48.0} \quad 50 \quad \frac{0.2.8}{37.8}$$

$$60+50 \quad \frac{0.2.7}{37.4} \quad 50 \quad \frac{0.4.0}{35.0}$$

$$61+00 \quad \frac{0.5.5}{39.8} \quad 50 \quad \frac{0.6.1}{39.2}$$

$$61+50 \quad \frac{0.6.4}{39.8} \quad 50 \quad \frac{0.7.7}{42.4}$$

$$62+00 \quad \frac{0.6.7}{39.4} \quad 50 \quad \frac{0.7.9}{37.8}$$

$$62+50 \quad \frac{0.1.0}{29.0} \quad 50 \quad \frac{F.1.5}{27.5}$$

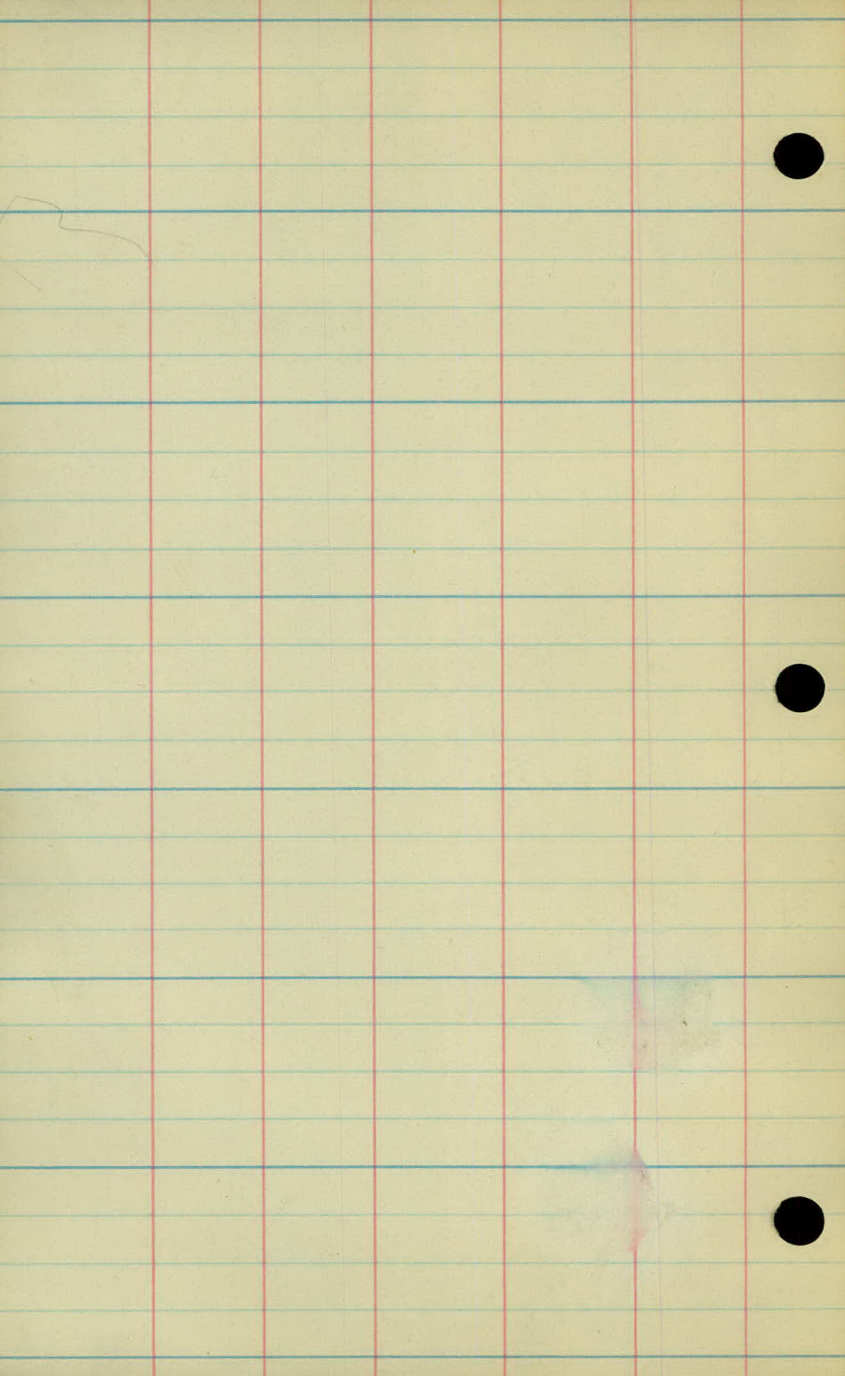
$$63+00 \quad \frac{06.0.6}{75.9} \quad 50 \quad \frac{06.1.5}{27.0}$$

12 100

Road C

4

63+50	F.28 28.4	5.0	C.3.3 33.6
64+10	F.78 76.4	5.0	C.2.3 31.6
64+50	F.2.8 28.5	F.3.6 78.8	5.0
			F.1.9 22.2
			F.7.1 74.3
65+00	F.5.1 28.8	F.4.1 30.3	5.0
			F.1.4 21.1
			F.6.3 36.9
66+20	F.6.6 27.0	F.4.8 32.4	5.0
66+00		F.7.7 41.1	5.0
66+50		Bridge	5.0
67+00		Bridge	5.0
67+50	F.22.1 14.3	5.0	
68+00	F.9.4 30.1	F.15.3 62.9	5.0
68+50	F.5.8 16.7	F.4.5 31.5	5.0
			F.10.4 32.0
			F.13.8 59.4
69+00	F.5.3 11.9	F.3.9 29.7	5.0
69+50	F.11.9 11.9	F.3.0 27.0	5.0
70+00	✓ F.2.5 25.5		F.3.9 22.7
			F.2.8 26.4
70+50	F.1.9 28.7	5.0	F.3.1 27.3
71+00	F.3.2 27.6	5.0	F.3.0 27.0



Road C^u

5

71+65	$\frac{F 2.9}{26.7}$	5.0	$\frac{F 2.8}{26.4}$
72+00	$\frac{F 2.7}{24.6}$	5.0	$\frac{F 2.3}{24.9}$
72+50	$\frac{DC 0.2}{24.4}$	5.0	$\frac{DC 0.7}{25.4}$
73+00	$\frac{DC 0.5}{25.0}$	5.0	$\frac{DC 1.3}{26.6}$
73+50	$\frac{DC 1.0}{26.0}$	5.0	$\frac{C 0.6}{28.2}$
74+00	$\frac{C 1.6}{30.2}$	5.0	$\frac{C 1.6}{30.2}$
74+65	$\frac{C 2.0}{31.0}$	5.0	$\frac{C 2.6}{32.2}$
75+00	$\frac{C 1.8}{30.6}$	5.0	$\frac{C 3.0}{33.0}$
75+50	$\frac{C 2.0}{31.0}$	5.0	$\frac{C 2.0}{31.0}$
76+00	$\frac{C 1.2}{29.4}$	5.0	$\frac{C 0.9}{28.8}$
76+50	$\frac{C 1.7}{30.4}$	5.0	$\frac{C 1.7}{30.4}$
77+00	$\frac{C 1.3}{29.6}$	5.0	$\frac{C 2.5}{32.0}$
77+50	$\frac{C 0.8}{28.6}$	5.0	$\frac{C 1.9}{30.2}$

E. Line N + S Road

W' ✓ ✓ ✓

No. Road C.V.

50 6

78+00 $\frac{C.O.1}{27.2}$ 5.0 $\frac{C.2.2}{31.4}$

78+44 $\frac{DC.1.4}{26.8}$ 5.0 $\frac{C.2.9}{32.8}$

79+00 $\frac{F.3.4}{78.1}$ $\frac{5.4}{30.2}$ 5.0 $\frac{C.O.4}{26.3}$

79+50 $\frac{F.5.8}{35.4}$ 5.0 $\frac{C.1.3}{27.4}$

80+00 $\frac{DC.O.2}{24.4}$ 5.0 $\frac{C.1.8}{30.6}$

80+50 $\frac{C.1.6}{30.2}$ 5.0 $\frac{C.2.1}{31.2}$

81+00 $\frac{F.1.6}{27.8}$ 5.0 $\frac{F.2.9}{26.7}$

81+50 $\frac{F.5.2}{35.6}$ 5.0 $\frac{F.5.8}{35.4}$

82+00 $\frac{F.4.7}{32.1}$ 5.0 $\frac{F.4.1}{36.5}$

82+50 $\frac{F.3.3}{27.9}$ 5.0 $\frac{F.4.9}{32.7}$

83+00 $\frac{DC.O.5}{35.0}$ 5.0 $\frac{F.3.2}{27.6}$

83+50 $\frac{C.O.3}{27.6}$ 5.0 $\frac{DC.O.1}{24.2}$

84+00 $\frac{C.1.8}{20.6}$ 5.0 $\frac{C.4.9}{30.8}$

84+50 $\frac{C.4.4}{25.8}$ 5.0 $\frac{C.5.1}{37.2}$

85+00 $\frac{C.6.0}{39.0}$ 5.0 $\frac{C.6.1}{39.2}$

$\frac{C.2.1}{30.2}$

$\frac{C.5.2}{34.8}$

$\frac{C.6.4}{36.6}$

26.8 1X.

14.4 5.

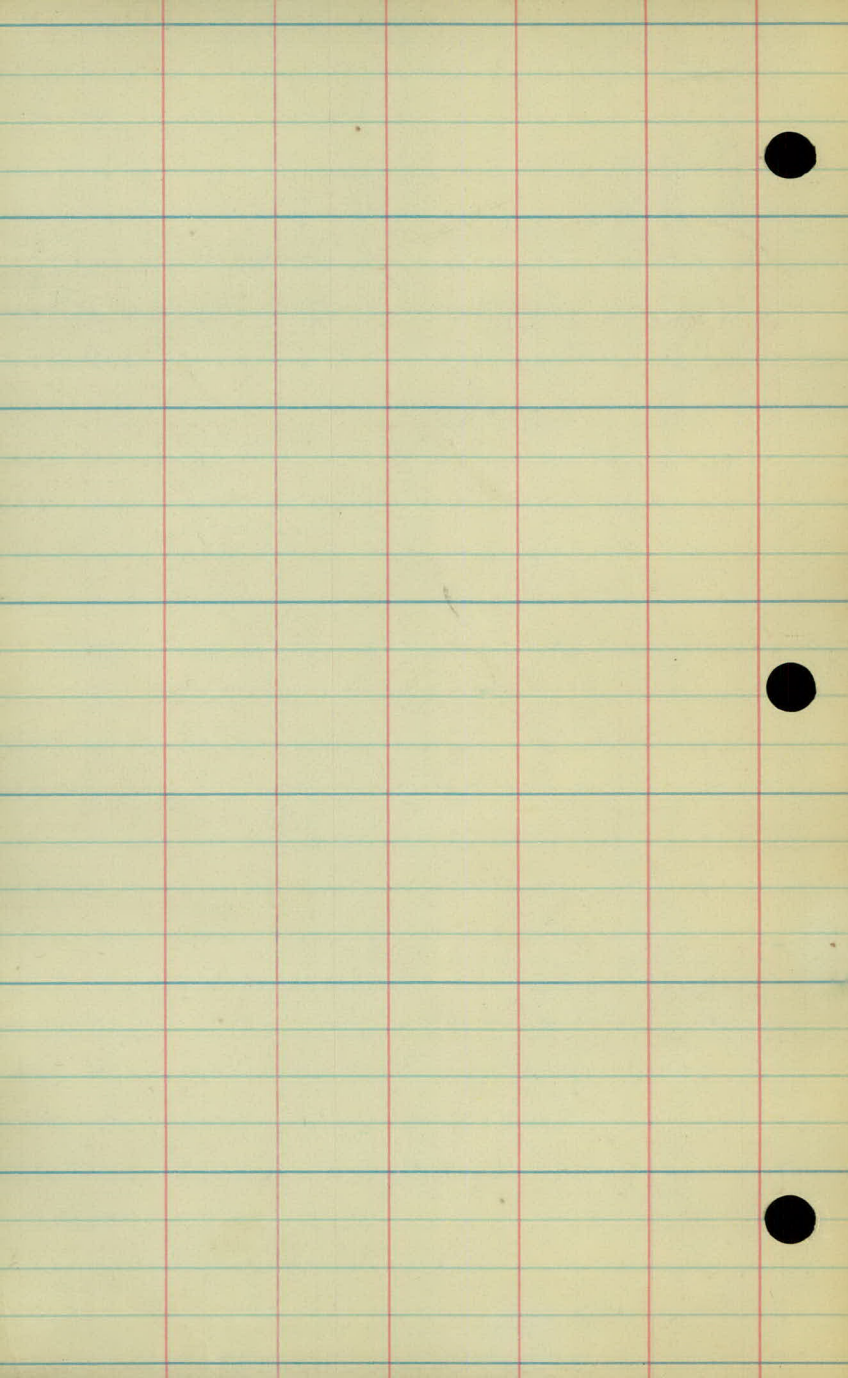
12.4 1X.

No. Road "C" 50
 55+50 $\frac{C. 8.2}{43.4}$ $\frac{C. 7.1}{41.1}$ $\frac{C. 6.9}{37.4}$ 7
 56+00 $\frac{C. 8.6}{43.4}$ $\frac{C. 5.7}{38.4}$ $\frac{C. 5.8}{35.7}$

Dec. 12 - Light Snow - 5. above - Sun Shining?

86+50	$\frac{C. 7.2}{41.4}$	5.0	$\frac{C. 4.3}{35.6}$	$\frac{C. 4.6}{33.9}$
87+00	$\frac{C. 4.4}{35.8}$	5.0	$\frac{C. 2.2}{31.4}$	$\frac{C. 2.4}{30.6}$
87+50	$\frac{C. 3.2}{33.4}$	5.0	$\frac{C. 1.5}{30.0}$	$\frac{C. 1.5}{29.3}$
88+00	$\frac{C. 1.8}{30.6}$	5.0	$\frac{C. 1.6}{29.0}$	$\frac{C. 1.0}{28.7}$
89+50	$\frac{DC. 1.1}{26.2}$	5.0	$\frac{C. 1.5}{30.0}$	$\frac{C. 1.4}{29.1}$
89+00	$\frac{DC. 0.9}{25.8}$	5.0	$\frac{C. 1.3}{29.6}$	$\frac{C. 1.3}{29.0}$
89+50	$\frac{F. 4.3}{30.9}$	5.0	$\frac{F. 1.8}{23.4}$	
90+00	$\frac{F. 5.6}{34.8}$	5.0	$\frac{F. 4.3}{30.9}$	<u>4.3</u>
90+50	$\frac{F. 4.5}{31.5}$	5.0	$\frac{F. 5.4}{34.2}$	
91+00	$\frac{F. 4.5}{31.5}$	5.0	$\frac{F. 4.4}{31.2}$	<u>4.4</u>
91+50	$\frac{F. 3.8}{32.4}$	5.0	$\frac{F. 1.6}{27.8}$	
92+00	$\frac{F. 1.8}{23.4}$	5.0	$\frac{DC. 1.5}{26.2}$	
92+50	$\frac{C. 3.2}{33.4}$	5.0	$\frac{C. 4.5}{36.0}$	
93+00	$\frac{C. 3.0}{33.0}$	5.0	$\frac{C. 6.5}{40.0}$	
93+50	$\frac{DC. 0.6}{25.4}$	5.0	$\frac{C. 6.2}{39.6}$	

Slope changed 1/2. 1/2.



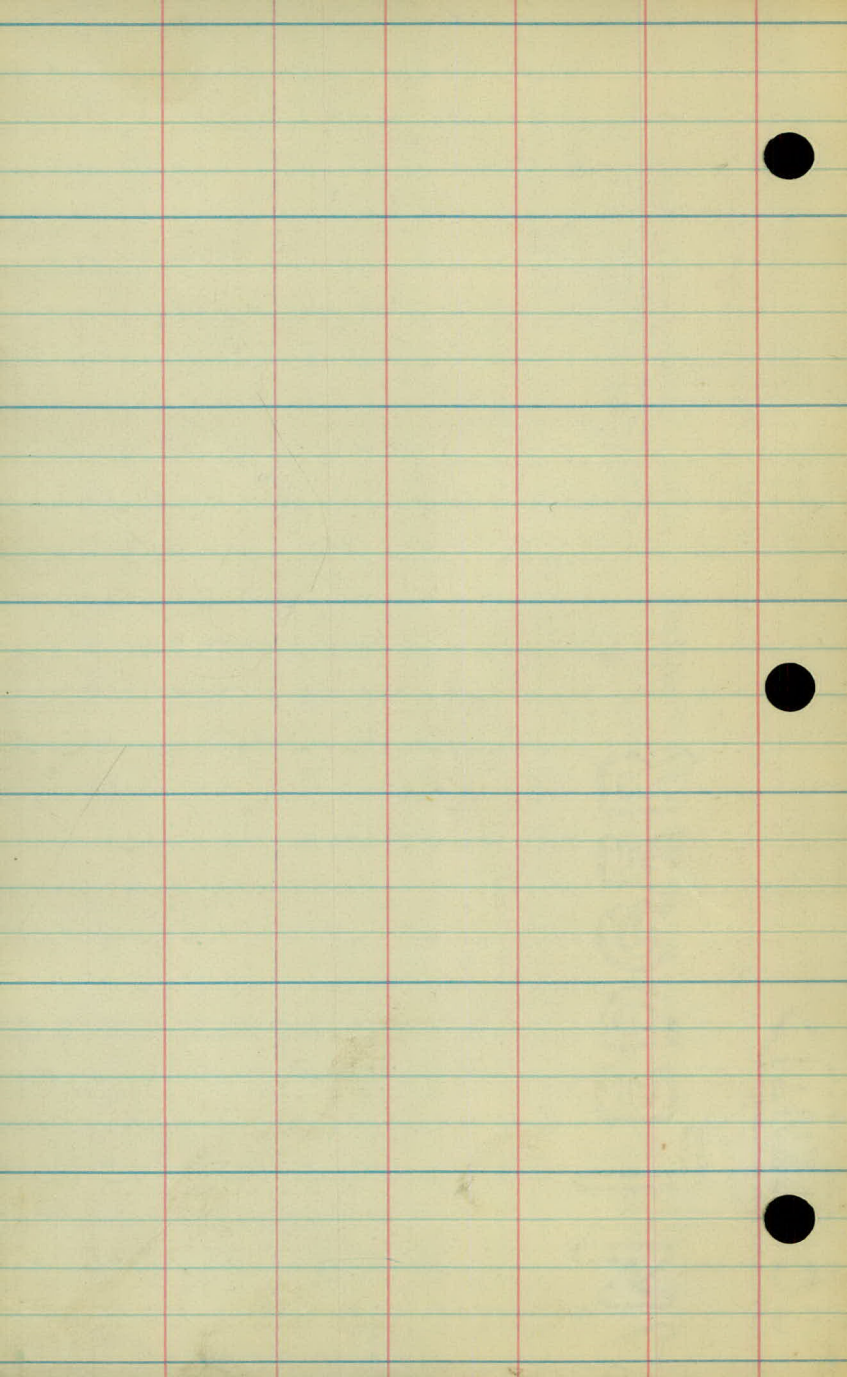
Road CU

8

94+00	$\frac{F.57}{33.6}$	5.0	$\frac{C.7.3}{41.6}$
94+50	$\frac{F.6.8}{38.4}$	5.0	$\frac{C.4.1}{39.2}$
95+00	$\frac{F.7.2}{39.6}$	5.0	$\frac{C.4.6}{36.2}$
95+50	$\frac{F.6.7}{38.1}$	5.0	$\frac{C.1.8}{30.6}$
96+00	$\frac{F.7.0}{39.0}$	5.0	$\frac{DC.1.1}{26.2}$
96+50	$\frac{F.7.3}{39.9}$	5.0	$\frac{DC.1.4}{26.8}$
97+00	$\frac{F.6.9}{38.7}$	5.0	$\frac{DC.1.4}{26.8}$
97+50	$\frac{F.5.7}{36.1}$	5.0	$\frac{DC.1.1}{26.2}$
98+00	$\frac{F.4.4}{31.2}$	5.0	$\frac{DC.1.2}{26.4}$
98+50	$\frac{F.3.8}{29.7}$	5.0	$\frac{C.0.3}{27.6}$
99+00	$\frac{F.3.4}{27.6}$	5.0	$\frac{C.0.4}{27.8}$
99+50	$\frac{F.2.4}{25.2}$	5.0	$\frac{C.1.7}{30.4}$
100+00	$\frac{F.1.8}{23.4}$	5.0	$\frac{C.0.7}{28.4}$
100+50	$\frac{F.1.5}{22.8}$	5.0	$\frac{DC.0.9}{25.8}$
101+00	$\frac{F.3.2}{27.6}$	5.0	$\frac{DC.1.0}{25.0}$
101+50	$\frac{F.4.1}{36.3}$	5.0	$\frac{0.3.3}{33.6}$
102+00	$\frac{F.2.1}{24.2}$	5.0	$\frac{C.4.4}{35.8}$
102+50	$\frac{C.0.2}{27.4}$	5.0	$\frac{C.4.1}{35.2}$
103+00	$\frac{C.0.5}{28.0}$	5.0	$\frac{0.4.4}{35.8}$

110+40 E I Beam Masonry Culvert 6x8'
Plank Floor

103+50	$\frac{C.1.9}{30.8}$	5.0	$\frac{C.1.5}{30.0}$	
104+00	$\frac{C.2.9}{32.8}$	5.0	$\frac{C.1.9}{30.8}$	
104+50	$\frac{C.3.7}{34.4}$	5.0	$\frac{C.1.9}{30.8}$	
105+00	$\frac{C.5.0}{37.0}$	5.0	$\frac{C.4.0}{35.0}$	
105+50	$\frac{C.6.6}{40.2}$	5.0	$\frac{C.6.2}{39.4}$	
106+00	$\frac{C.8.6}{44.2}$	5.0	$\frac{C.8.2}{43.4}$	
106+50	$\frac{C.7.9}{42.8}$	5.0	$\frac{C.8.9}{44.8}$	
107+00	$\frac{C.7.3}{41.6}$	5.0	$\frac{C.9.0}{45.0}$	
107+50	$\frac{C.5.6}{38.2}$	5.0	$\frac{C.8.5}{44.0}$	
108+00	$\frac{C.1.2}{29.4}$	5.0	$\frac{C.4.8}{36.6}$	
108+20	$\frac{F.2.1}{24.2}$		$\frac{C.0.1}{27.2}$	
108+50	$\frac{F.8.6}{43.8}$	5.0	$\frac{C.0.2}{27.4}$	
109+00	$\frac{F.15.7}{47.4}$	5.0	$\frac{F.2.5}{25.5}$	
109+50	$\frac{F.17.6}{50.8}$	5.0	$\frac{F.6.2}{36.6}$	
110+00	$\frac{F.14.7}{47.4}$	5.0	$\frac{F.8.4}{43.2}$	
110+50	$\frac{F.10.7}{39.4}$	5.0	$\frac{F.11.5}{41.0}$	
111+00	$\frac{F.12.6}{37.8}$	5.0	$\frac{F.10.5}{39.0}$	
111+50	$\frac{F.3.2}{27.6}$	5.0	$\frac{F.6.3}{30.6}$	
112+00	$\frac{F.2.2}{24.6}$	5.0	$\frac{F.6.0}{30.0}$	
112+50	$\frac{F.2.0}{24.0}$	5.0	$\frac{F.5.0}{28.0}$	



Roach

10

113+00

$$\begin{array}{r} F1.7 \\ 23.1 \end{array}$$

$$\begin{array}{r} F2.9 \\ 26.7 \end{array}$$

$$\begin{array}{r} 2.9 \\ 23.8 \end{array}$$

113+50

$$\begin{array}{r} F1.8 \\ 23.4 \end{array}$$

$$\begin{array}{r} DC.03 \\ 24.6 \end{array}$$

114+00

$$\begin{array}{r} C.0.2 \\ 27.4 \end{array}$$

$$\begin{array}{r} DC.0.9 \\ 25.8 \end{array}$$

114+50

$$\begin{array}{r} C1.2 \\ 29.4 \end{array}$$

$$\begin{array}{r} DC.1.0 \\ 26.0 \end{array}$$

Dec. 13. Cloudy - 15 above.

115+00

$$\begin{array}{r} C.2.6 \\ 32.2 \end{array}$$

$$\begin{array}{r} DC.1.5 \\ 27.0 \end{array}$$

115+50

$$\begin{array}{r} C.6.9 \\ 40.8 \end{array}$$

$$\begin{array}{r} C1.9 \\ 30.8 \end{array}$$

116+00

$$\begin{array}{r} C.8.9 \\ 44.8 \end{array}$$

$$\begin{array}{r} C.4.6 \\ 36.2 \end{array}$$

116+50

$$\begin{array}{r} C.6.1 \\ 39.2 \end{array}$$

$$\begin{array}{r} DC.1.0 \\ 26.0 \end{array}$$

117+00

$$\begin{array}{r} DC.0.9 \\ 25.8 \end{array}$$

$$\begin{array}{r} F.5.8 \\ 35.4 \end{array}$$

117+50

$$\begin{array}{r} F.2.1 \\ 24.3 \end{array}$$

$$\begin{array}{r} F.6.4 \\ 37.2 \end{array}$$

118+00

$$\begin{array}{r} F.9.3 \\ 24.1 \end{array}$$

$$\begin{array}{r} F.5.4 \\ 32.2 \end{array}$$

118+50

$$\begin{array}{r} F.2.4 \\ 26.2 \end{array}$$

$$\begin{array}{r} F.3.7 \\ 29.1 \end{array}$$

119+00

$$\begin{array}{r} DC.1.1 \\ 26.2 \end{array}$$

$$\begin{array}{r} F.2.8 \\ 26.4 \end{array}$$

119+50

$$\begin{array}{r} C.1.8 \\ 20.6 \end{array}$$

$$\begin{array}{r} F.2.6 \\ 25.8 \end{array}$$

W Line White Bear Ave

E ✓ ✓ ✓ ✓

Road C

11

120+00	$\frac{C. 2.2}{31.4}$	$\frac{F. 4.2}{30.6}$
120+50	$\frac{C. 2.3}{31.6}$	$\frac{F. 3.2}{27.6}$
121+00	$\frac{C. 1.2}{29.4}$	
121+65	$\frac{C. 0.4}{27.8}$	$\frac{C. 1.2}{27.4}$
122+00	$\frac{C. 3.8}{31.6}$	$\frac{C. 2.0}{31.0}$
122+50	$\frac{C. 2.6}{32.2}$	$\frac{C. 1.5}{30.0}$
123+00	$\frac{C. 2.5}{32.0}$	$\frac{C. 0.6}{28.2}$
123+50	$\frac{C. 4.4}{32.8}$	$\frac{C. 0.6}{28.2}$
124+00	$\frac{C. 4.5}{36.0}$	$\frac{C. 1.0}{29.0}$
124+50	$\frac{C. 0.8}{28.6}$	$\frac{C. 1.5}{27.0}$
125+00	$\frac{F. 2.8}{26.4}$	$\frac{F. 2.5}{25.5}$
125+50	$\frac{F. 2.7}{26.1}$	$\frac{F. 3.8}{29.4}$
126+00	$\frac{C. 0.8}{25.6}$	$\frac{F. 4.1}{30.3}$
126+50	$\frac{C. 0.3}{27.6}$	$\frac{F. 3.7}{29.1}$
127+00	$\frac{C. 1.3}{26.6}$	$\frac{F. 4.6}{31.8}$

129+40 - 12" Galv C/V

Road G4

⊕
12

$$127+50 \quad \frac{C.O.6}{28.2}$$

$$\frac{F.5.2}{32.6}$$

$$128+00 \quad \frac{C.1.0}{29.0}$$

$$\frac{F.3.7}{34.5}$$

$$128+50 \quad \frac{C.1.2}{29.6}$$

$$\frac{F.4.2}{30.6}$$

$$129+00 \quad \frac{DC.0.4}{24.8}$$

$$\frac{F.4.6}{31.8}$$

$$129+50 \quad \frac{F.2.1}{26.3}$$

$$\frac{F.3.3}{27.9}$$

$$130+00 \quad \frac{DC.0.2}{24.0}$$

$$\frac{DC.1.1}{25.2}$$

$$130+05$$

$$130+50 \quad \frac{DC.0.7}{25.4}$$

$$\frac{DC.1.0}{26.0}$$

$$131+00 \quad \frac{DC.0.7}{25.6}$$

$$\frac{F.2.0}{24.0}$$

$$131+50 \quad \frac{C.O.6}{28.4}$$

$$\frac{DC.0.8}{25.6}$$

$$132+00 \quad \frac{C.1.5}{30.0}$$

$$\frac{F.1.5}{27.5}$$

$$132+50 \quad \frac{F.2.2}{31.4}$$

$$\frac{C.O.1}{27.2}$$

$$133+00 \quad \frac{DC.0.7}{25.4}$$

$$\frac{DC.1.3}{26.6}$$

$$133+50 \quad \frac{C.1.9}{30.8}$$

$$\frac{C.O.1}{27.2}$$

$$134+00 \quad \frac{DC.1.1}{26.2}$$

$$\frac{DC.1.5}{26.8}$$

$$134+50 \quad \frac{F.2.5}{25.5}$$

$$\frac{C.O.2}{21.4}$$

136+10 - 18" Galv Pipe

$$135+00 \quad \frac{DC 0.7}{25.4}$$

$$\frac{C 1.0}{29.0}$$

$$135+50 \quad \frac{DC 0.3}{24.6}$$

$$\frac{C 0.6}{28.2}$$

$$136+00 \quad \frac{F 6.0}{36.0}$$

$$\frac{C 0.1}{27.2}$$

$$136+50 \quad \frac{F 8.4}{43.2}$$

$$\frac{DC 1.2}{26.4}$$

$$137+00 \quad \frac{F 6.9}{38.7}$$

$$\frac{DC 0.9}{25.8}$$

$$137+50 \quad \frac{F 4.0}{30.0}$$

$$\frac{DC 0.7}{25.4}$$

$$138+00$$

$$\frac{C 0.1}{27.2}$$

$$138+05 \quad \frac{C 0.1}{27.2}$$

$$138+50 \quad \frac{C 2.2}{37.4}$$

$$\frac{C 1.5}{30.0}$$

$$139+00 \quad \frac{C 2.4}{32.8}$$

$$\frac{C 0.3}{27.6}$$

$$139+50 \quad \frac{F 3.6}{28.8}$$

$$\frac{DC 1.3}{26.6}$$

$$140+00 \quad \frac{F 5.2}{33.6}$$

$$\frac{DC 1.0}{26.0}$$

$$140+50 \quad \frac{F 4.2}{30.6}$$

$$\frac{DC 1.2}{26.6}$$

$$141+00 \quad \frac{F 1.6}{22.8}$$

$$\frac{DC 0.7}{25.4}$$

$$141+50 \quad \frac{F 1.5}{24.6}$$

$$\frac{C 3.1}{33.2}$$

$$142+00 \quad \frac{F 2.6}{28.8}$$

$$\frac{C 0.8}{26.6}$$

146498 P.O.T.

142+50

$$\begin{array}{r} F.35 \\ 78.5 \end{array}$$

$$\begin{array}{r} DC.08 \\ 25.6 \end{array}$$

144

143+00

$$\begin{array}{r} DC.06 \\ 25.2 \end{array}$$

$$\begin{array}{r} DC.08 \\ 26.0 \end{array}$$

143+50

$$\begin{array}{r} DC.10 \\ 26.0 \end{array}$$

$$\begin{array}{r} DC.1.2 \\ 26.4 \end{array}$$

144+00

$$\begin{array}{r} C.22 \\ 31.2 \end{array}$$

$$\begin{array}{r} C.50 \\ 37.0 \end{array}$$

144+50

$$\begin{array}{r} C.0.8 \\ 28.6 \end{array}$$

$$\begin{array}{r} C.6.6 \\ 40.2 \end{array}$$

145+00

$$\begin{array}{r} F.2.5 \\ 25.5 \end{array}$$

$$\begin{array}{r} C.3.5 \\ 34.0 \end{array}$$

145+50

$$\begin{array}{r} DC.1.3 \\ 26.6 \end{array}$$

$$\begin{array}{r} C.3.4 \\ 33.8 \end{array}$$

146+00

$$\begin{array}{r} DC.1.4 \\ 26.8 \end{array}$$

$$\begin{array}{r} C.4.6 \\ 36.2 \end{array}$$

146+50

$$\begin{array}{r} DC.0.0 \\ 24.0 \end{array}$$

$$\begin{array}{r} C.2.8 \\ 32.6 \end{array}$$

147+00

$$\begin{array}{r} DC.0.3 \\ 24.6 \end{array}$$

$$\begin{array}{r} C.2.4 \\ 31.8 \end{array}$$

147+50

$$\begin{array}{r} DC.0.7 \\ 25.4 \end{array}$$

$$\begin{array}{r} C.2.0 \\ 31.0 \end{array}$$

148+00

$$\begin{array}{r} C.0.2 \\ 27.4 \end{array}$$

$$\begin{array}{r} C.2.3 \\ 31.6 \end{array}$$

148+50

$$\begin{array}{r} C.0.9 \\ 28.8 \end{array}$$

$$\begin{array}{r} C.3.3 \\ 33.6 \end{array}$$

149+00

$$\begin{array}{r} C.1.2 \\ 29.4 \end{array}$$

$$\begin{array}{r} C.3.1 \\ 33.2 \end{array}$$

149+50

$$\begin{array}{r} C.1.5 \\ 30.0 \end{array}$$

Dec-18. Cloudy

C.1.4

25 above

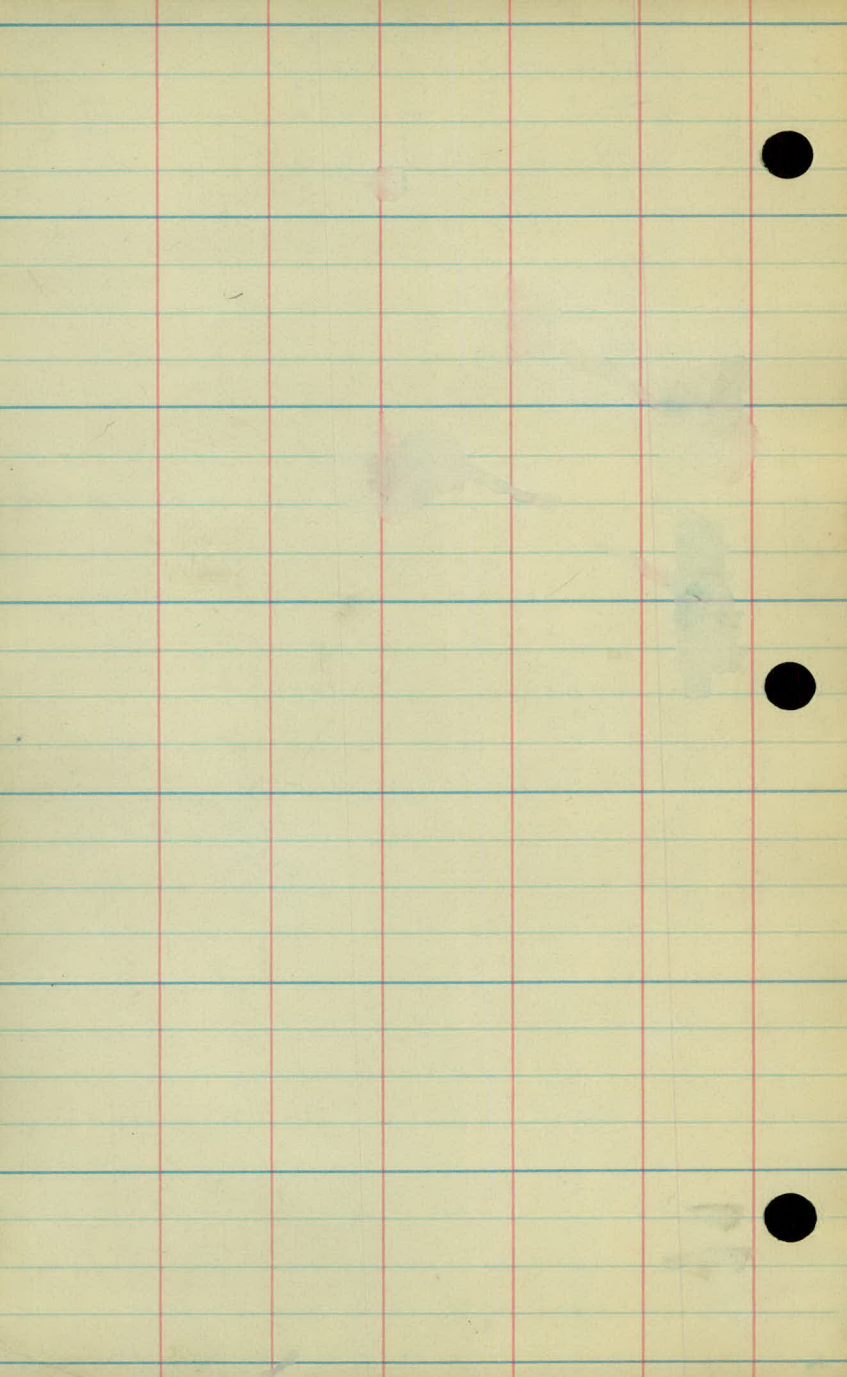
29.8

150+00

$$\begin{array}{r} C.1.8 \\ 25.6 \end{array}$$

J.V. Andrews - Chief
 Nonison - Int
 Rosette - Rep
 Daly - Chron
 Nickle

$$\begin{array}{r} C.0.2 \\ 27.4 \end{array}$$



150+45	$\frac{DC 1.0}{26.0}$	$\frac{DC 1.3}{26.6}$
150+50	$\frac{DC 0.3}{24.6}$	$\frac{C.O. 3}{27.6}$
151+0	$\frac{DC 1.2}{26.4}$	$\frac{C.O. 4}{27.8}$
152+00	$\frac{F. 1.6}{22.8}$	$\frac{C.O. 1}{27.2}$
152+50	$\frac{DC 0.3}{24.6}$	$\frac{DC 0.0}{27.0}$
153+00	$\frac{C.O. 2}{27.4}$	$\frac{DC 0.6}{28.2}$
153+50	$\frac{DC 0.0}{24.0}$	
153+60		$\frac{C.O. 5}{28.0}$
154+08	$\frac{F. 2.3}{24.9}$	$\frac{C. 1.0}{29.0}$
154+50	$\frac{F. 1.9}{23.7}$	$\frac{C.O. 6}{28.2}$
155+00	$\frac{DC 1.5}{27.0}$	$\frac{DC 0.2}{24.4}$
155+50	$\frac{C.O. 1}{27.2}$	$\frac{F. 2.4}{28.2}$
156+00	$\frac{DC 1.2}{26.4}$	$\frac{F. 3.1}{27.3}$
156+50	$\frac{C.O. 3}{27.6}$	$\frac{F. 2.3}{24.9}$
157	$\frac{C. 1.3}{29.6}$	$\frac{DC 1.0}{26.0}$
157+37	$\frac{C. 3.5}{34.0}$	
157+78	$\frac{C. 5.7}{38.4}$	$\frac{C.O. 8}{28.6}$
158+00	$\frac{C. 6.4}{39.8}$	$\frac{C.O. 8}{28.6}$

$$\begin{array}{r} 46 \\ 3 \\ \hline 76 \end{array}$$

$$\begin{array}{r} 29 \\ 3 \\ \hline 87 \end{array}$$

$$\begin{array}{r} 37 \\ 3 \\ \hline 11 \end{array}$$

46

$$\begin{array}{r} 7 \\ 5 \\ \hline 1 \end{array}$$

31

164 + 80 18" Corr Pipe

Road C^u

16

$$158+50 \quad \frac{63}{39.6}$$

$$\frac{C.O.7}{75.4}$$

$$159 \quad \frac{61.8}{30.4}$$

$$\frac{DC.1.0}{76.0}$$

$$159+50 \quad \frac{60.3}{27.6}$$

$$\frac{DC.O.O}{74.0}$$

$$160 \quad \frac{DC.O.9}{25.8}$$

$$\frac{DC.O.9}{25.8}$$

$$160+50 \quad \frac{60.1}{27.2}$$

$$\frac{DC.1.0}{26.0}$$

$$161 \quad \frac{DC.1.0}{26.0}$$

$$\frac{F.2.7}{26.7}$$

$$161+50 \quad \frac{F.2.1}{24.3}$$

$$\frac{F.3.7}{29.1}$$

$$162 \quad \frac{F.2.2}{24.6}$$

$$\frac{F.1.7}{22.1}$$

$$162+50 \quad \frac{F.2.0}{24.0}$$

$$\frac{F.2.6}{25.2}$$

$$163 \quad \frac{DC.O.9}{25.8}$$

$$\frac{F.4.6}{31.8}$$

$$+50 \quad \frac{DC.1.5}{27.05}$$

$$\frac{F.2.7}{26.1}$$

$$164 \quad \frac{DC.O.1}{24.2}$$

$$\frac{F.1.7}{23.1}$$

$$+50 \quad \frac{F.3.2}{27.6}$$

$$\frac{F.4.1}{30.3}$$

$$165 \quad \frac{F.3.3}{27.9}$$

$$\frac{F.3.0}{27.0}$$

$$+50 \quad \frac{F.2.0}{24.0}$$

$$\frac{DC.O.1}{24.2}$$

28
10

27

Road Cu

17

$$166 \quad \frac{DC.0.6}{25.7}$$

$$\frac{C.0.1}{27.2}$$

$$+50 \quad \frac{C.0.3}{27.6}$$

$$\frac{C.0.9}{28.8}$$

$$167 \quad \frac{C.1.0}{29.0}$$

$$\frac{C.1.6}{30.2}$$

$$+50 \quad \frac{DC.1.5}{27.0}$$

$$\frac{DC.1.5}{27.0}$$

$$168 \quad \frac{DC.0.5}{25.0} \quad \text{Dec-19. Clear} \quad \frac{C.0.2}{27.4}$$

25 Above

$$+50 \quad \frac{DC.0.5}{25.0}$$

$$\frac{C.2.8}{32.6}$$

$$169 \quad \frac{DC.1.0}{26.0}$$

$$\frac{C.4.8}{36.6}$$

$$+50 \quad \frac{DC.1.5}{27.0}$$

$$\frac{C.5.9}{38.8}$$

$$170 \quad \frac{C.0.1}{27.2}$$

$$\frac{C.7.5}{42.0}$$

$$+50 \quad \frac{DC.0.1}{24.7}$$

$$\frac{C.5.4}{37.8}$$

$$171 \quad \frac{F.3.9}{29.7}$$

$$\frac{C.1.5}{30.0}$$

$$+50 \quad \frac{F.4.8}{32.4}$$

$$\frac{DC.1.5}{27.0}$$

$$172 \quad \frac{F.4.3}{30.9}$$

$$\frac{F.1.7}{23.1}$$

$$+50 \quad \frac{DC.0.2}{24.4}$$

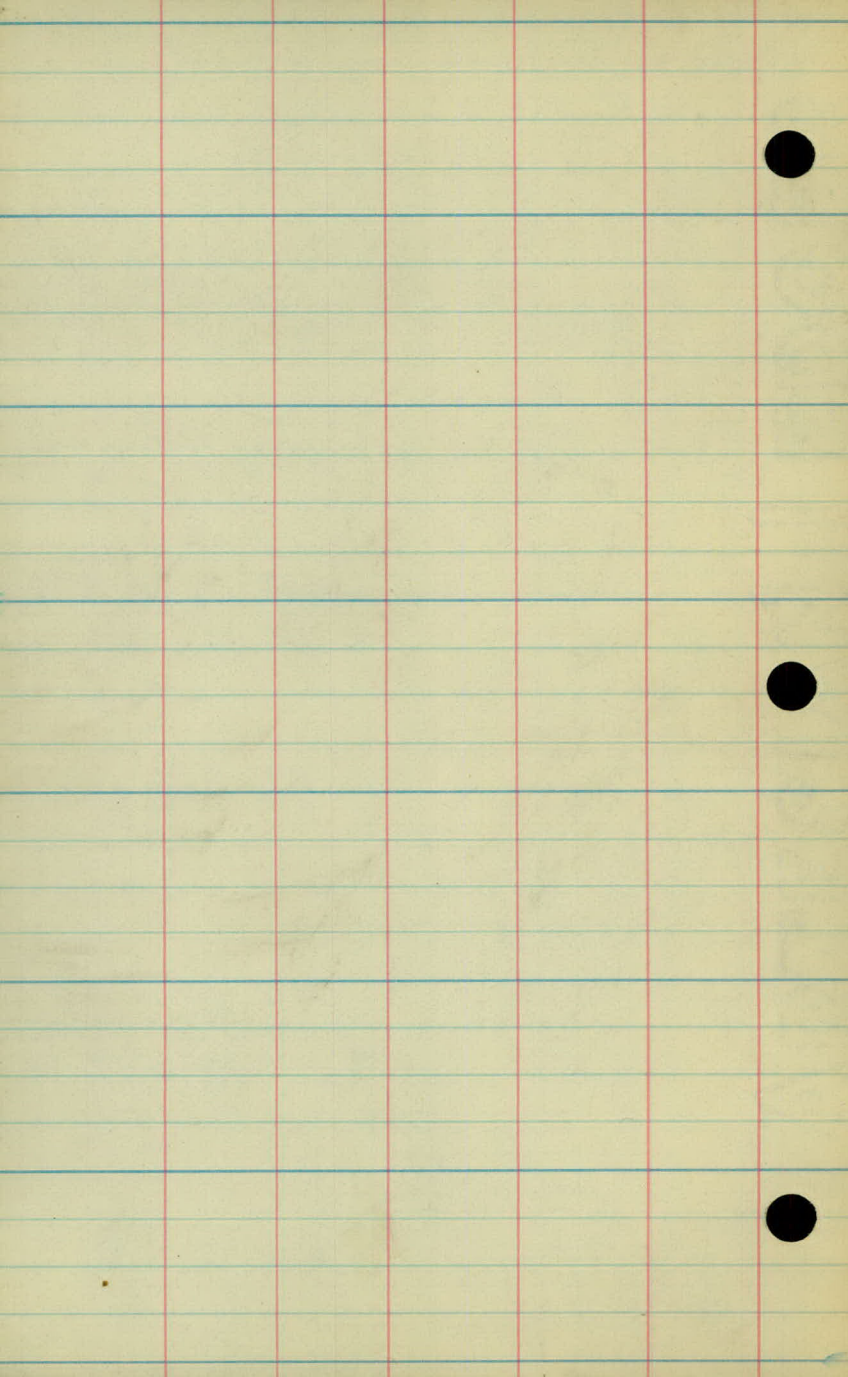
$$\frac{DC.0.3}{24.6}$$

$$173 \quad \frac{C.0.4}{29.8}$$

$$\frac{DC.1.5}{27.0}$$

$$+50 \quad \frac{C.2.6}{32.2}$$

$$\frac{C.2.0}{31.0}$$



Road 6

18

$$174 \quad \frac{F1.6}{22.8}$$

$$\frac{F1.6}{22.8}$$

$$+50 \quad \frac{F2.6}{25.8}$$

$$\frac{F2.6}{25.8}$$

$$175 \quad \frac{F3.7}{29.1}$$

$$\frac{F2.8}{26.4}$$

$$+50 \quad \frac{F2.5}{25.5}$$

$$\frac{F2.8}{26.4}$$

$$176 \quad \frac{DC0.8}{25.6}$$

$$\frac{F2.8}{26.4}$$

$$+50 \quad \frac{C0.1}{27.2}$$

$$\frac{F1.9}{26.7}$$

$$177 \quad \frac{DC1.3}{26.6}$$

$$+30$$

$$\frac{C1.8}{30.6}$$

$$+50 \quad \frac{C0.2}{27.4}$$

$$\frac{C1.6}{30.2}$$

$$178 \quad \frac{DC0.2}{24.0}$$

$$\frac{C1.4}{29.8}$$

$$+50 \quad \frac{DC0.0}{24.0}$$

$$\frac{C0.3}{27.6}$$

$$179 \quad \frac{C1.4}{29.8}$$

$$\frac{C0.8}{28.6}$$

$$+50 \quad \frac{C1.7}{30.4}$$

$$\frac{DC1.0}{26.0}$$

$$180 \quad \frac{C1.2}{29.4}$$

$$\frac{DC0.4}{24.8}$$

$$+50 \quad \frac{F3.8}{29.4}$$

$$\frac{F5.2}{33.6}$$

$$181 \quad \frac{F4.0}{30.0}$$

$$\frac{F7.0}{39.0}$$

$$+50 \quad \frac{DC1.0}{26.0}$$

$$\frac{DC1.5}{27.0}$$

Line Maple Trees - 23' So

184+35- Conc Steps 27' N

Line Maple Trees - 34' N

185+25 Brick Steps - 27' N

Conc Steps - Yard Fence 30' - So.

Road C⁴

19

$$182 \quad \frac{C.26}{32.2}$$

$$\frac{C.23}{31.6}$$

$$+50 \quad \frac{C.14}{29.8}$$

$$\frac{C.36}{34.2}$$

$$183 \quad \frac{C.10}{29.0}$$

$$\frac{C.20}{31.0}$$

$$+35$$

$$\frac{C.10}{29.0}$$

$$+45 \quad \frac{C.21}{31.2}$$

+64 L Road.

$$184 \quad \frac{C.46}{36.2}$$

23'

$$\frac{DC.09}{25.8}$$

$$+10$$

$$\frac{C.20}{31.0}$$

$$+50 \quad \frac{C.43}{35.6}$$

$$\frac{C.24}{31.8}$$

$$185 \quad \frac{C.46}{36.2}$$

$$\frac{C.02}{27.4}$$

$$+50 \quad \frac{C.42}{35.0}$$

$$\frac{DC.10}{26.0}$$

$$186 \quad \frac{DC.10}{26.0}$$

$$\frac{F29}{26.7}$$

$$+50 \quad \frac{F28}{26.4}$$

$$\frac{F3.9}{29.7}$$

$$187 \quad \frac{F27}{25.1}$$

$$\frac{F2.9}{26.7}$$

$$+50 \quad \frac{F2.5}{24.9}$$

$$\frac{F44}{31.2}$$

19430

Conc Walk to ho - S. Side

Line Maple Trees - No Side - 34' out

190+70 Conc Walk - 27' N + 24.50

190+76 Fire Hy - 22' N

193+20 Conc Steps 50

Road Cu

20

$$188 \quad \frac{F1.9}{23.7} \quad \bullet \quad 23' \quad \bullet \quad \frac{F6.1}{36.3}$$

$$+50 \quad \frac{DC1.5}{27.0} \quad \bullet \quad \bullet \quad \frac{F3.1}{27.5}$$

$$189 \quad \frac{F2.5}{25.5} \quad \bullet \quad \bullet \quad \frac{DC0.4}{24.8}$$

$$+50 \quad \frac{DC0.3}{24.6} \quad \bullet \quad \bullet \quad \frac{F4.1}{30.3}$$

$$190 \quad \frac{DC1.1}{26.2} \quad \bullet \quad 34' \quad 23' \quad \bullet \quad \frac{F3.1}{27.3}$$

Dec - 20th - Clear - 250 bore

$$191 \quad \frac{DC0.0}{24.0} \quad \bullet \quad \bullet \quad \frac{C3.1}{33.2}$$

$$+50 \quad \frac{F2.8}{26.4} \quad \bullet \quad \bullet \quad \frac{C3.9}{34.8}$$

$$192 \quad \frac{F4.6}{31.8} \quad \bullet \quad \bullet \quad \frac{C4.8}{26.6}$$

$$+50 \quad \frac{F5.0}{33.0} \quad \bullet \quad \bullet \quad \frac{DC1.1}{26.2}$$

$$193 \quad \frac{F3.3}{27.9} \quad \bullet \quad \bullet \quad \frac{DC1.1}{26.2}$$

$$+50 \quad \frac{C2.1}{31.2} \quad \bullet \quad \bullet \quad \frac{DC0.9}{25.8}$$

$$194 \quad \frac{C2.2}{31.4} \quad \bullet \quad \bullet \quad \frac{DC0.4}{24.8}$$

$$+50 \quad \frac{DC0.5}{25.0} \quad \bullet \quad \bullet \quad \frac{F2.0}{24.0}$$

196+30 W End E+W^o Walk - 27⁴/₁N

Line Maple Trees - 21' S_o

196+60 WE. Conc Walk - 25²/₅ S_o

196+90 Fire Hy - 25' N + ^{E END CONC WALK} 25²/₅ - S_o

196+98 E END Conc Walk - 27⁴/₁N

197+25 - Car Tracks

201 - Conc Drive - 24' N

$$195 \quad \frac{F1.9}{23.7}$$

$$\bullet \quad \frac{F3.2}{27.6} \quad 21$$

$$+50 \quad \frac{F3.1}{27.3}$$

$$\bullet \quad \frac{DC0.0}{24.0}$$

$$196 \quad \frac{C0.2}{28.2}$$

$$\bullet \quad \frac{DC0.2}{24.6}$$

$$+50 \quad \text{conc walk}$$

$$\frac{DC0.4}{24.8}$$

$$197 \quad \frac{C0.1}{27.2}$$

$$\frac{DC0.5}{25.0}$$

$$+50 \quad \frac{C0.1}{27.2}$$

$$\frac{DC1.2}{26.4}$$

$$198 \quad \frac{C6.4}{39.8}$$

$$\frac{DC1.4}{26.8}$$

$$+50 \quad \frac{C9.4}{45.8}$$

$$\frac{DC1.5}{27.0}$$

$$199 \quad \frac{C7.9}{42.8}$$

$$\frac{DC1.3}{26.6}$$

$$+50 \quad \frac{C3.1}{33.2}$$

$$\frac{DC0.6}{25.2}$$

$$200 \quad \frac{DC1.2}{26.4}$$

$$\frac{F1.5}{22.5}$$

$$+50 \quad \frac{DC0.4}{24.8}$$

$$\frac{F2.2}{24.6}$$

201

$$\frac{F7.0}{24.0}$$

$$+10 \quad \frac{DC0.9}{25.8}$$

+40

$$+50 \quad \frac{DC0.9}{25.8}$$

$$\frac{DC0.1}{24.2}$$

204+05

Fire Hy- 22' N

204+25

conc Steps- 28' 14"

205+07

-

-

✓

205+70

-

-

16' 30"

205+80

✓

-

-

218+30 Corr. Pipe-24'

$$202 \quad \frac{DC1.2}{26.4}$$

$$\frac{DC0.4}{24.8}$$

$$+50 \quad \frac{DC1.0}{26.0}$$

$$\frac{DC0.9}{25.8}$$

$$203 \quad \frac{DC0.9}{25.8}$$

$$\frac{DC1.5}{27.0}$$

$$+50 \quad \frac{DC1.1}{26.2}$$

$$\frac{DC1.5}{27.0}$$

$$204 \quad \frac{DC1.5}{27.0}$$

$$\frac{C4.6}{40.2}$$

$$+50 \quad \frac{DC1.1}{26.2}$$

$$\frac{C4.9}{36.8}$$

$$205 \quad \frac{DC1.2}{26.4}$$

$$\frac{DC1.2}{26.4}$$

$$+50 \quad \frac{DC1.5}{27.0}$$

$$\frac{C3.0}{35.0}$$

$$+95 \quad \frac{C2.8}{32.6}$$

$$+0.5$$

$$+50 \quad \frac{DC0.0}{26.0}$$

$$\frac{C8.4}{37.8}$$

$$\frac{C2.0}{31.0}$$

$$207 \quad \frac{DC0.7}{25.4}$$

$$\frac{F1.7}{23.1}$$

$$+45 \quad \frac{DC0.5}{25.0}$$

$$+50$$

$$\frac{F3.4}{28.2}$$

$$208 \quad \frac{DC0.6}{25.2}$$

$$\frac{F4.0}{30.0}$$

$$+50 \quad \frac{DC0.0}{24.0}$$

$$\frac{F3.4}{28.2}$$

Fire Hy. +50 - 21' N

East Countyline Road.

209

$$\begin{array}{r} F2.3 \\ \hline 74.9 \end{array}$$

$$\begin{array}{r} F1.8 \\ \hline 21.6 \end{array}$$

23

+50

$$\begin{array}{r} DE0.2 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} DC1.0 \\ \hline 26.0 \end{array}$$

209+73.9

Clearance

$$39 + 86$$

$$20.3$$

$$40 + 33$$

$$21.5$$

$$5.7$$

$$5.6$$

$$1.8$$

$$5.06$$

$$1.18$$

$$3.80$$

$$235 \text{ use } 2.4$$

$$21.500$$

$$276$$

$$1370$$

$$1164$$

$$2260$$

$$1940$$

$$320$$

$$10.3$$

$$9.3$$

$$5.5$$

$$3.8$$

$$2.0$$

$$4.0$$

$$4.4$$

$$2.0$$

$$1.8$$

$$9.2$$

$$10.0$$

$$2.0$$

$$2.0$$

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$$2.0$$

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$$2.0$$

$$2.0$$

$$2.4$$

$$5.3$$

$$12.7$$

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$$67 : 24 : 50.1$$

$$2.4$$

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$$67/1200$$

$$2.4$$

$$5.3$$

$$12.7$$

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$$12.7$$

$$67/2.50$$

$$20.1$$

$$4.90$$

$$4.64$$

$$3.10$$

$$2.6$$

$$0.37$$

$$5.0$$

$$16.50$$

$$16.50$$

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$$27.1$$

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$$9.6$$

$$H+$$

$$3.1$$

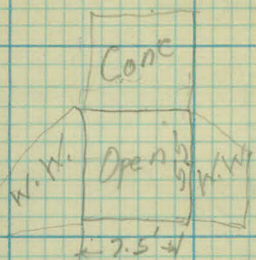
$$9.0$$

5.24 S. End
538
 14 N. End

44
20
 38
60

31.14
.46

110 + 43



11 - 6" I-Beams
 1/2 Corr. Panels
 26.7'

Stone Masonry Walls 10" thick
 Conc. Wing Walls

50

N.

$$\begin{array}{r}
 110 + 43 \quad \begin{array}{r} 165.22 \\ 14.3 \end{array} \quad \begin{array}{r} 3.2 \\ 13.3 \end{array} \quad \begin{array}{r} 3.5 \\ 13.3 \end{array} \quad \begin{array}{r} 3.4 \\ 0.0 \end{array} \quad \begin{array}{r} 36.34 \\ 11.3 \end{array} \quad \begin{array}{r} 3.4 \\ 11.3 \end{array} \quad \begin{array}{r} 3.4 \\ 12.3 \end{array} \quad \begin{array}{r} 17.1 \\ 12.3 \end{array} \\
 \hline
 \begin{array}{r} 16.0 \\ 175 \end{array} \quad \begin{array}{r} 16.0 \\ 125 \end{array} \quad \begin{array}{r} 16.4 \\ 75 \end{array} \quad \begin{array}{r} 18.0 \\ 65 \end{array} \quad \begin{array}{r} 18.8 \\ 115 \end{array} \quad \begin{array}{r} 20.0 \\ 165 \end{array}
 \end{array}$$

New C.M. Culv. 116' Long

N. End 0.6' lower than S. End.

7.5

7.2

Sta.

£

Ditch

7.10

-0.04
K7.71
7.67
4

0+00

6.4

6.9 ✓

~~+50~~~~6.3~~~~6.8~~

1+00

6.2
5.86.7 ✓
6.3 ✓

+50

5.0

5.5 ✓

2+00

4.3

4.8 ✓

~~+50~~~~4.0~~~~4.5~~

3+00

4.0
3.54.5 ✓
4.0 ✓

+50

3.3

3.8

4+00

3.0

3.5

4+50

3.0

5+00

2.9

67
33
100
263
373

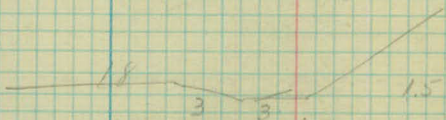
$$\begin{array}{r} 8.5 \\ 8 \\ \hline 680 \\ 83 \\ \hline 153 \end{array}$$

20.4

$$\begin{array}{r} 4.47 \\ 233 \\ \hline 210 \end{array}$$

$$\begin{array}{r} 2.4 \\ 214 \\ \hline 508 \\ 428 \\ \hline 720 \end{array}$$

$$\begin{array}{r} 3.8 \\ 6 \\ \hline 54 \end{array}$$



$$\begin{array}{r} 1.5 \\ 2.2 \\ \hline 2.2 \\ 2.2 \\ \hline 4.3 \end{array}$$

$$\begin{array}{r} 10 \\ 12 \\ \hline 12 \\ 12 \\ \hline 24 \end{array}$$

50.79