

Book - 28 - Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

COUNTY ROAD "C"

From Rice St. To $\frac{1}{2}$ Mi. E.

Road Acc't. No. 52

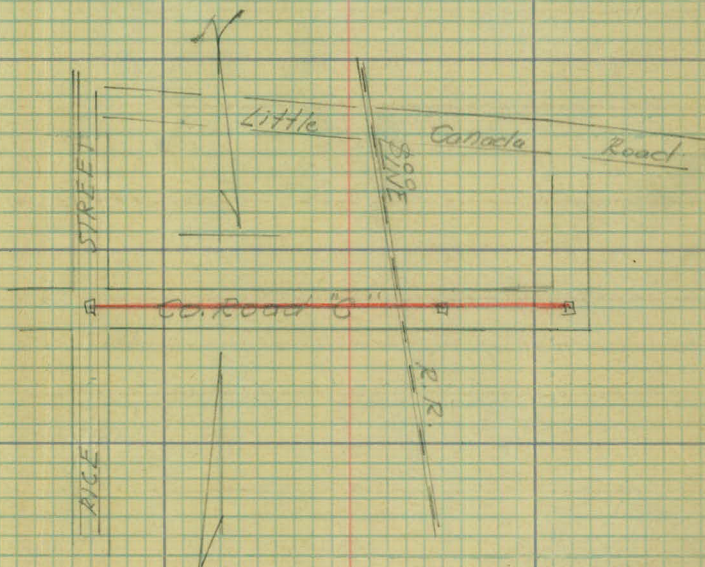
Date Filed. 1-6-36

File 6

Plan Survey

County Road "C"

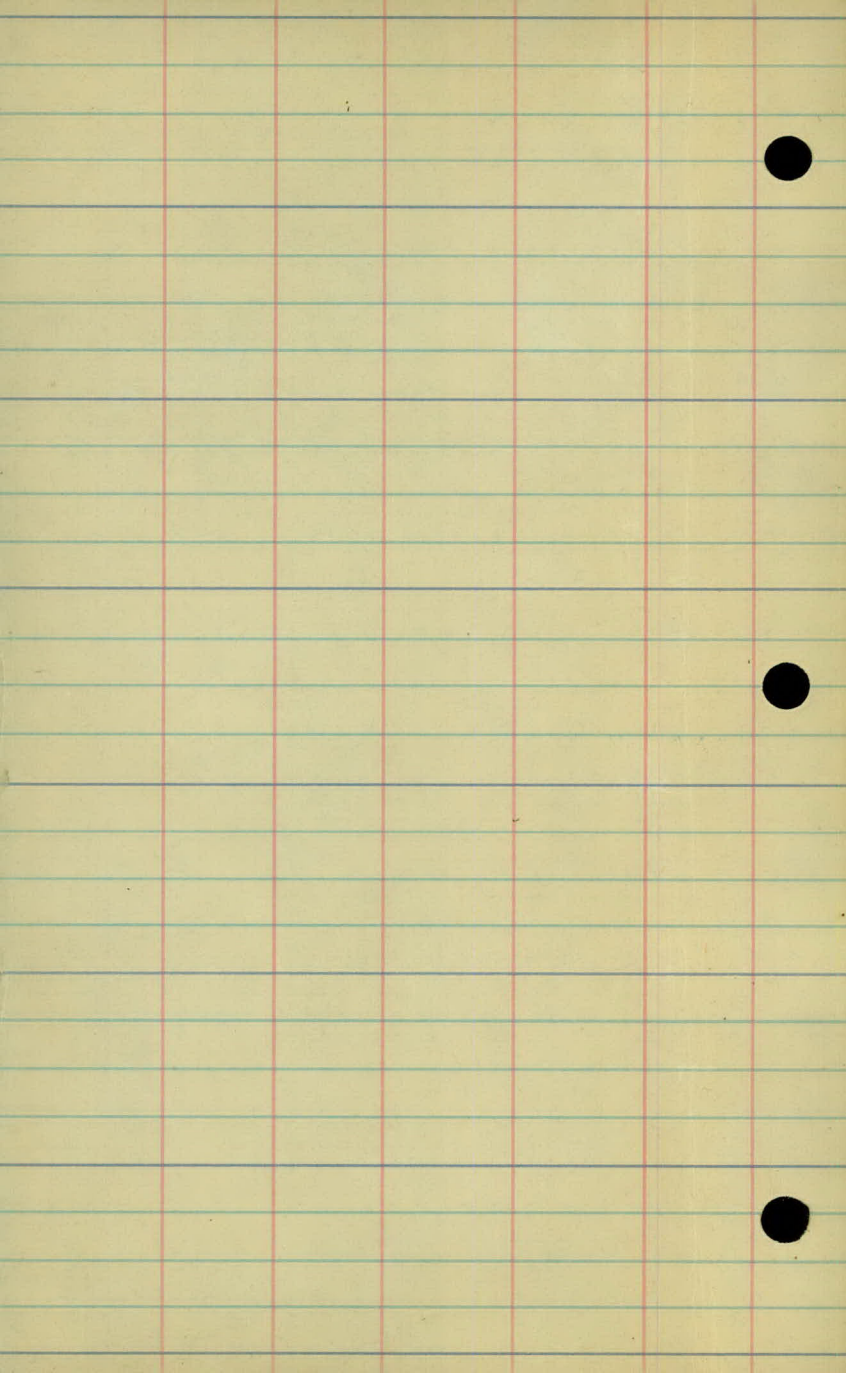
from Rice St. to Lake St.



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W. H. Carlson
Nov. 21, 1935



alignment

Station Point ^{Angle}
Lt - Rt.

309+19.82 Mon.

302+19.62 P.I. 0°24'

300+91.85 - $\angle$ $\frac{500}{\text{LINE}}$ R.R. $\frac{1}{2}$

296+54.52 P.O.T.

277+97.6 Mon. $\angle$ Rice.

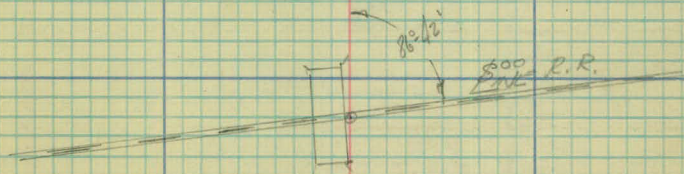
W.H.C.
H.A.W.
K.A.
L.B.H. 11/20/35 2

Mont.

II

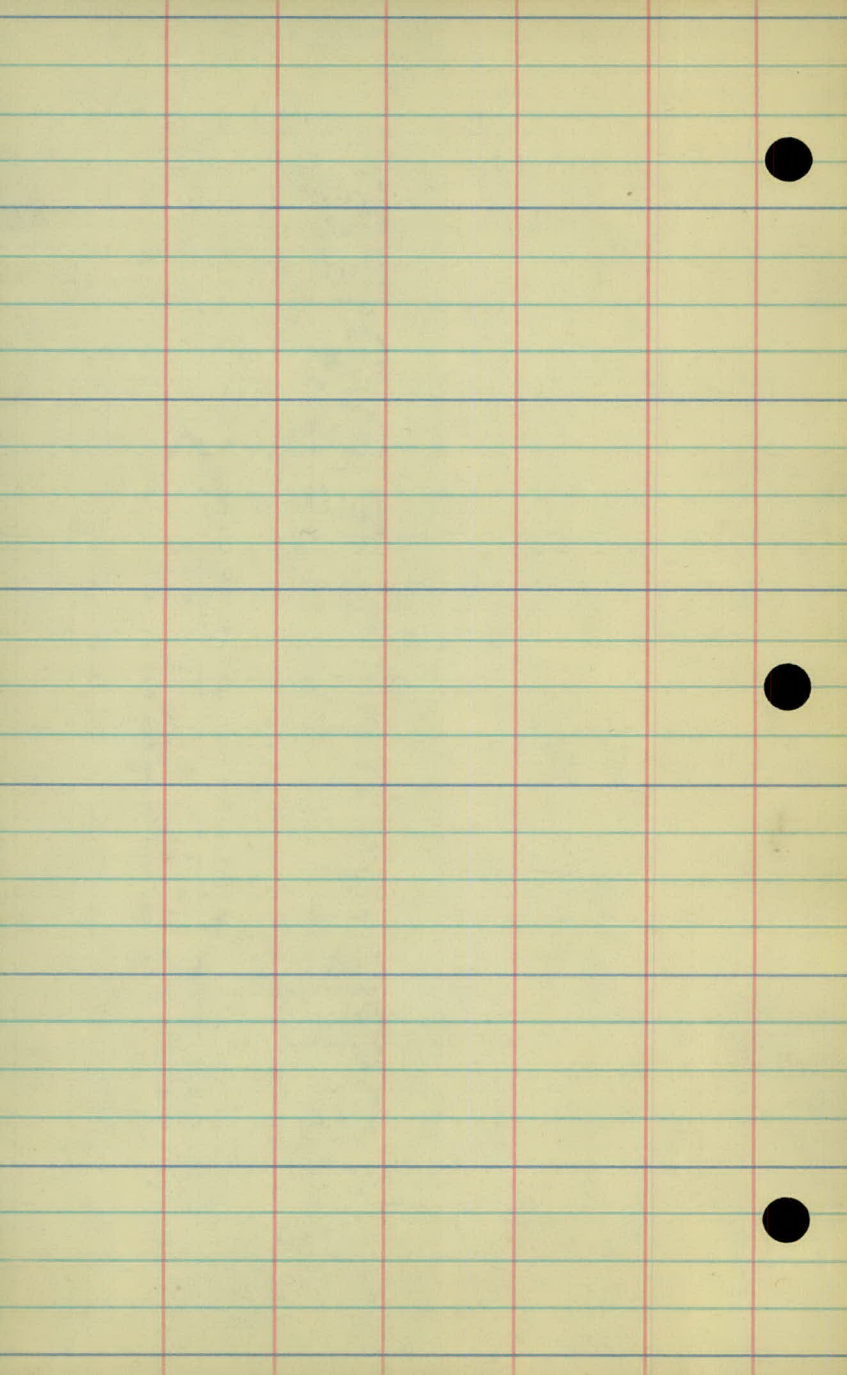
Mont.

II



North-
E Rico St.

II



Topography

15' - 4'

282

16' - 4'

281

15' - 7'

280

15' - 5'

279

17' - 8'

+40 - 17-13

+20 29-29'

278

+97.6

Mon. & Rice St.

277

+94-F. Line 25'

+94-F. Line 25'

+45-Ent. M. Cor. W.

+32-T.P. -18'-24'

+18-Ent. 12'x12' Ent. 9'

+18-N.E. Cor. 2-S.F. 54'

+97-N.W. Cor. 2-S.F. 54'

+84-N.E. Cor. 2-S.F. 6'

+18-N.W. Cor. 2-S.F. 6'

+57-6" S.M. -26'

+45-Ent. 12'x20' C.W.

11'

+66-T.P. 21'

+69-E.P. 23'

+55-2-S.F. 150'

+20-Ent.

+92-F. Cor. 34'

+70-T.P. 20'

+155

15-C. H.

+143-N.W. Cor. 64'

+28-Ent.

+80-Ent.

+46-N.E. Cor. 36'

+47-T.P. 20'

+46-N.W. Cor. 36' Frame 75'

+23-T.P. 43'

+97.6-Edge Pav.

+41-14" Maple 40'

+17-Ent. 12'x20' C.W.

+68-18" Maple 36'

+93-Tri 6" Apple 51'

+90-14" Maple 36'

Cult.

+60

Rice St.

Conc. Pav.

27'-7"

289

26'-6"

288

25'-6"

+58- 8" x 31' VIT TITE
30' E-1'

287

23'-4"

286

21'-1"

2

285

19'-0"

284

18'-2"

283

71-4 } H.P. 61'
190-W. Mar. }

460-T.P. 21'-25'

(5)

cut

197-25 Fr. South

445-T.P. 21'

Marsh

433-T.P. 21'

420-20" Oak-38'

cut

480-E. St. South 12'x12'
468-T.P. 21' 15'

478-T.P. 21'
466-5' 19'x12' 25'
477-NE. Cor. 3' 15'x5'
451-N.W. Cor. 1'
447-4" Box 1' 23'
439-ENT 12'x12' CNL
13'

455-T.P. 21'

70-1

296

27'-3'

295

24'-5'

294

25'-5'

293

26'-5'

292

27'-8'

291

26'-8'

290

Range 710 448
+55-5.43



+11-T.P. 23'

+59-d St. South
No culv.

+77-T.P. 22'

+10-T.P. 22'

+81 N.E. Cor. } 15.F.62
+61 N.W. Cor. }

+52-T.P. 22'

+25-Ent.

culv.

+31-T.P. 22'
B.M.

+38-Ent.

to arch

+75-T.P. 22'

+70-T.P. 22'

+25-Ent.

+38-Ent.

16'-0

303

20'-0

19.62- Mon.

302

21'-0'

301

19.85 ⁵⁰⁰ LINE R.R. { See P. 17 for
Detail of Bridge

300

18'-4'

299

21'-4'

298

20'-1'

2

297

F-28
+98-T.R. 24'

F-25'

+63-T.P. 23'

+244-Bt. 22'-3.9

+23.3-Bent

+93.7-Bent

+82.5-Bent

+62.5-Bent

+61.5-Bt. 20'-1.2'

+54-R.R.T.P. 46'

+40-T.P. 23'
+30-F.C.N. 23'

+48-T.P. 23'

+47-T.P. 22'

+44-T.P. 22'

+32 S.E. Cor. 85' } 1+5.F

+99-S.W. Cor. 80'

+42-T.P. 23'

Hay Meadow

310

+19.82 mod.

58' 19" - 120

329

28' - 5'

20 - 8 + 80

308

14' - 8

307

13' - 8'

306

15' 4

108-12" Vit x 31' 28' ^E - 8'

305

17 3/4 - 3'

304

+99-T.P. 61'
+98-F.C. 24'
+93-12' out 56'

L40-Field Ent

+48-14' oak 33'
+75-B. Fed 33'

+93-94 y 19 k 26'
+65-Fed. Cor 31'
+55-Field Ent.
+44-T.P. 24'

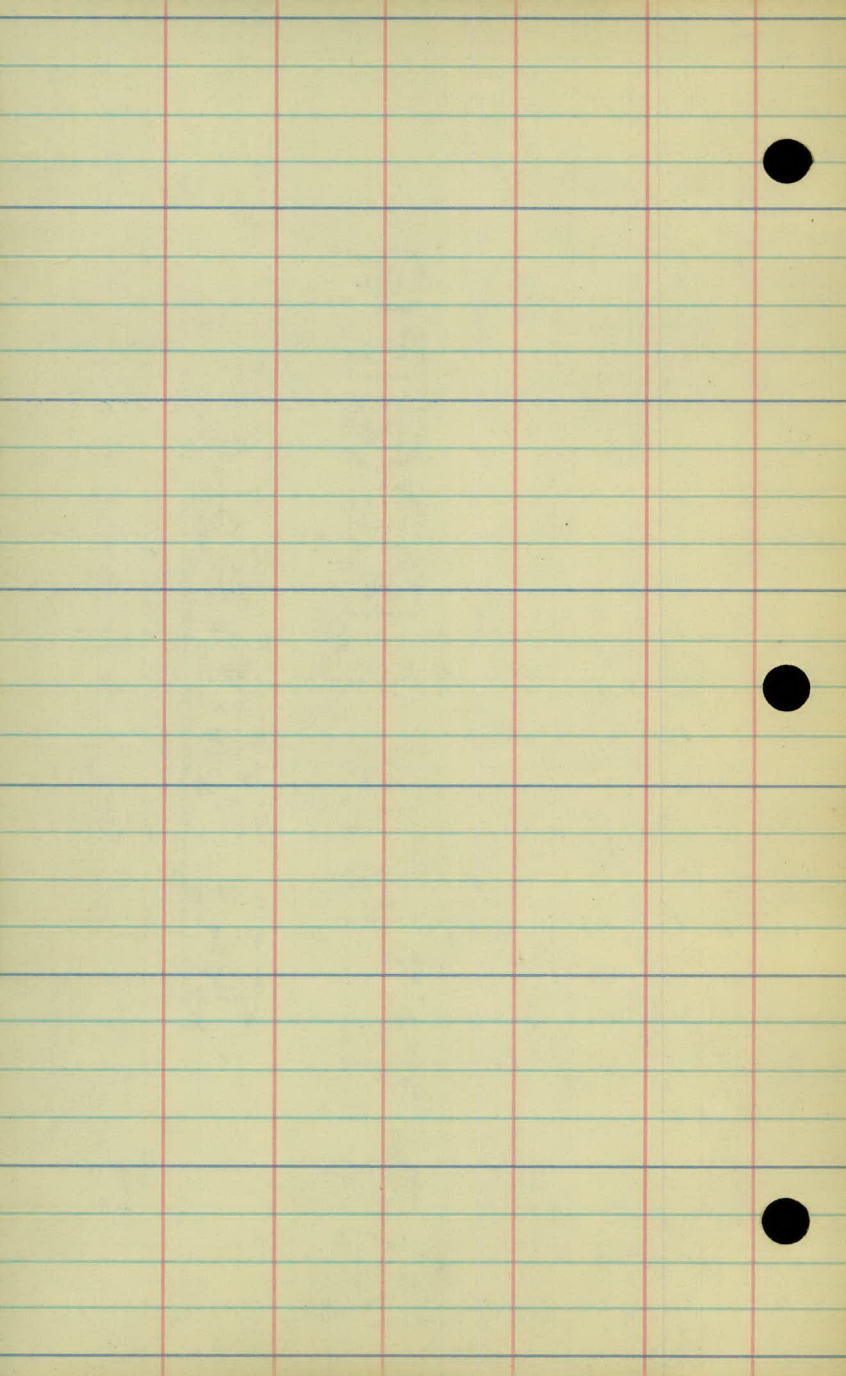
+67-T.P. 25'

+13-T.P. 26'

+60-T.P. 25'

+28-T.P. 24'

+00-Ring Fed 0'
+95-F. Cor 25'



Cross-sections.

Sta.	+	π	-	Elev.
B.M.	3.92	961.83 ✓		957.91 ✓
277 + 97.6				57.9.
278 + 09.6 - 6250 Av.				57.8.
+30				57.9.
279				56.3.
+40				55.5.
280				54.0.
+40				53.4.
281				52.5.
+55				51.0.
282				49.4.
T.P.	0.06	950.19. ✓	11.70	950.13. ✓
+50				48.3.
283				47.0.

Lt.

Z

Rt.

Top Mon. Rice & Co. Road "C"

3.82 $\frac{43}{50}$ $\frac{400}{50}$ $\frac{41}{50}$ $\frac{39}{33}$ $\frac{45}{20}$ $\frac{39}{10}$ $\frac{41}{23}$ $\frac{48}{40}$ $\frac{40}{40}$ $\frac{51}{33}$ $\frac{67}{22}$ $\frac{62}{17}$ $\frac{56}{8}$ $\frac{55}{6}$ $\frac{58}{7}$ $\frac{55}{7}$ $\frac{36}{33}$ $\frac{66}{33}$ $\frac{56}{25}$ $\frac{21}{21}$ $\frac{65}{16}$ $\frac{62}{8}$ $\frac{63}{5}$ $\frac{67}{6}$ $\frac{62}{19}$ $\frac{49}{33}$ $\frac{46}{33}$ $\frac{100}{33}$ $\frac{74}{30}$ $\frac{90}{16}$ $\frac{82}{14}$ $\frac{77}{6}$ $\frac{78}{10}$ $\frac{82}{15}$ $\frac{74}{25}$ $\frac{77}{25}$ $\frac{86}{33}$ $\frac{88}{33}$ $\frac{93}{22}$ $\frac{95}{20}$ $\frac{95}{16}$ $\frac{87}{14}$ $\frac{83}{7}$ $\frac{84}{6}$ $\frac{86}{15}$ $\frac{95}{15}$ $\frac{98}{33}$ $\frac{87}{33}$ $\frac{88}{24}$ $\frac{96}{22}$ $\frac{102}{16}$ $\frac{96}{14}$ $\frac{92}{6}$ $\frac{93}{13}$ $\frac{96}{18}$ $\frac{65}{33}$ $\frac{67}{50}$ $\frac{67}{50}$ $\frac{107}{33}$ $\frac{104}{25}$ $\frac{118}{16}$ $\frac{111}{15}$ $\frac{108}{7}$ $\frac{108}{6}$ $\frac{108}{12}$ $\frac{74}{19}$ $\frac{54}{50}$ $\frac{126}{33}$ $\frac{124}{21}$ $\frac{123}{20}$ $\frac{128}{18}$ $\frac{128}{15}$ $\frac{124}{7}$ $\frac{124}{6}$ $\frac{122}{9}$ $\frac{127}{13}$ $\frac{124}{17}$ $\frac{98}{50}$ $\frac{60}{50}$ $\frac{27}{33}$ $\frac{25}{25}$ $\frac{31}{21}$ $\frac{35}{20}$ $\frac{34}{18}$ $\frac{23}{15}$ $\frac{19}{6}$ $\frac{19}{6}$ $\frac{20}{10}$ $\frac{26}{12}$ $\frac{26}{16}$ $\frac{06}{33}$ $\frac{00}{50}$ $\frac{47}{33}$ $\frac{41}{20}$ $\frac{46}{18}$ $\frac{34}{15}$ $\frac{31}{7}$ $\frac{32}{6}$ $\frac{33}{9}$ $\frac{42}{13}$ $\frac{37}{16}$ $\frac{23}{24}$ $\frac{17}{50}$ $\frac{10}{50}$

Station	+	π ✓	-	Elev.
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950.19 ✓

283+45				46.1 -
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284				45.3 -
-----	--	--	--	--------

+50				44.9 -
-----	--	--	--	--------

+75				44.9 -
-----	--	--	--	--------

285				44.7 -
-----	--	--	--	--------

+50				44.0 -
-----	--	--	--	--------

286				43.8 -
-----	--	--	--	--------

+32				43.0 -
-----	--	--	--	--------

+62				42.9 -
-----	--	--	--	--------

287				41.7 -
-----	--	--	--	--------

288				40.4 -
-----	--	--	--	--------

+50				42.5 -
-----	--	--	--	--------

T.P.	7.62	951.75 ✓	6.06	944.13 ✓
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Lt.

Z

Rt.

11

$$\begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 4.3 \\ 16 \end{array} \quad \begin{array}{r} 4.0 \\ 8 \end{array} \quad \begin{array}{r} 4.1 \\ 41 \end{array} \quad \begin{array}{r} 4.2 \\ 6 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 5.0 \\ 79 \end{array} \quad \begin{array}{r} 4.9 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 24 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 4.8 \\ 9 \end{array} \quad \begin{array}{r} 4.9 \\ 49 \end{array} \quad \begin{array}{r} 5.1 \\ 5 \end{array} \quad \begin{array}{r} 6.8 \\ 10 \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array}$$

$$\begin{array}{r} 5.4 \\ 42 \end{array} \quad \begin{array}{r} 6.9 \\ 37 \end{array} \quad \begin{array}{r} 7.1 \\ 27 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 5.3 \\ 53 \end{array} \quad \begin{array}{r} 5.2 \\ 4 \end{array} \quad \begin{array}{r} 6.3 \\ 7 \end{array} \quad \begin{array}{r} 6.5 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array} \quad \text{No. rel}$$

$$\begin{array}{r} 4.6 \\ 42 \end{array} \quad \begin{array}{r} 6.2 \\ 37 \end{array} \quad \begin{array}{r} 6.8 \\ 25 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 5.3 \\ 53 \end{array} \quad \begin{array}{r} 5.8 \\ 2 \end{array} \quad \begin{array}{r} 6.9 \\ 8 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ 42 \end{array} \quad \begin{array}{r} 6.2 \\ 37 \end{array} \quad \begin{array}{r} 6.8 \\ 26 \end{array} \quad \begin{array}{r} 5.9 \\ 19 \end{array} \quad \begin{array}{r} 5.4 \\ 9 \end{array} \quad \begin{array}{r} 5.5 \\ 53 \end{array} \quad \begin{array}{r} 5.8 \\ 4 \end{array} \quad \begin{array}{r} 7.0 \\ 8 \end{array} \quad \begin{array}{r} 7.4 \\ 16 \end{array} \quad \begin{array}{r} 6.5 \\ 18 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.1 \\ 40 \end{array} \quad \begin{array}{r} 7.7 \\ 36 \end{array} \quad \begin{array}{r} 7.8 \\ 27 \end{array} \quad \begin{array}{r} 6.5 \\ 19 \end{array} \quad \begin{array}{r} 6.0 \\ 10 \end{array} \quad \begin{array}{r} 6.2 \\ 42 \end{array} \quad \begin{array}{r} 6.4 \\ 4 \end{array} \quad \begin{array}{r} 7.5 \\ 9 \end{array} \quad \begin{array}{r} 7.9 \\ 19 \end{array} \quad \begin{array}{r} 7.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 41 \end{array} \quad \begin{array}{r} 6.4 \\ 30 \end{array} \quad \begin{array}{r} 7.4 \\ 27 \end{array} \quad \begin{array}{r} 7.4 \\ 25 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 6.0 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 1 \end{array} \quad \begin{array}{r} 6.4 \\ 53 \end{array} \quad \begin{array}{r} 7.2 \\ 2 \end{array} \quad \begin{array}{r} 7.9 \\ 13 \end{array} \quad \begin{array}{r} 7.4 \\ 22 \end{array} \quad \begin{array}{r} 5.1 \\ 28 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array}$$

$$\begin{array}{r} 7.4 \\ 33 \end{array} \quad \begin{array}{r} 7.4 \\ 30 \end{array} \quad \begin{array}{r} 8.3 \\ 28 \end{array} \quad \begin{array}{r} 8.2 \\ 26 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 12 \end{array} \quad \begin{array}{r} 7.2 \\ 72 \end{array} \quad \begin{array}{r} 7.8 \\ 2 \end{array} \quad \begin{array}{r} 8.4 \\ 12 \end{array} \quad \begin{array}{r} 8.2 \\ 21 \end{array} \quad \begin{array}{r} 5.4 \\ 27 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 9.3 \\ 38 \end{array} \quad \begin{array}{r} 8.7 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 22 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 6.7 \\ 2 \end{array} \quad \begin{array}{r} 7.3 \\ 73 \end{array} \quad \begin{array}{r} 7.8 \\ 5 \end{array} \quad \begin{array}{r} 9.4 \\ 13 \end{array} \quad \begin{array}{r} 8.8 \\ 20 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array}$$

$$\begin{array}{r} 10.0 \\ 33 \end{array} \quad \begin{array}{r} 9.8 \\ 30 \end{array} \quad \begin{array}{r} 6.9 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 7.0 \\ 3 \end{array} \quad \begin{array}{r} 8.5 \\ 35 \end{array} \quad \begin{array}{r} 10.0 \\ 3 \end{array} \quad \begin{array}{r} 10.0 \\ 33 \end{array}$$

Drains No.

10.3

C.V.V.

10.1

$$\begin{array}{r} 8.7 \\ 37 \end{array} \quad \begin{array}{r} 8.5 \\ 31 \end{array} \quad \begin{array}{r} 6.6 \\ 26 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 6.9 \\ 6 \end{array} \quad \begin{array}{r} 9.8 \\ 98 \end{array} \quad \begin{array}{r} 10.3 \\ 73 \end{array} \quad \begin{array}{r} 10.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 37 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 6.6 \\ 5 \end{array} \quad \begin{array}{r} 7.7 \\ 77 \end{array} \quad \begin{array}{r} 8.7 \\ 33 \end{array}$$

Station + π ✓ - E/lev.

951.75 ✓

288+80

44.1 .

289

44.7 .

+13

44.5 .

+21

44.4 .

+65

43.8 .

290

43.5 .

+18

44.2
~~44.2~~

+35

44.3 .

+65

42.3 .

291

40.5 .

+50

40.1

292

41.2 .

Lt.

E

Rt.

$$\begin{array}{r} 53 \\ 44 \end{array} \quad \begin{array}{r} 85 \\ 36 \end{array} \quad \begin{array}{r} 79 \\ 28 \end{array} \quad \begin{array}{r} 76 \\ 76 \end{array} \quad \begin{array}{r} 77 \\ 77 \end{array} \quad \begin{array}{r} 7.2 \\ 15. \end{array} \quad \begin{array}{r} 6.9 \\ 33 \end{array}$$

$$\begin{array}{r} 66 \\ 38 \end{array} \quad \begin{array}{r} 83 \\ 31 \end{array} \quad \begin{array}{r} 78 \\ 27 \end{array} \quad \begin{array}{r} 7.5 \\ 16 \end{array} \quad \begin{array}{r} 7.1 \\ 7.1 \end{array} \quad \begin{array}{r} 6.0 \\ 24 \end{array} \quad \begin{array}{r} 54 \\ 50 \end{array}$$

$$\begin{array}{r} 59 \\ 43 \end{array} \quad \begin{array}{r} 81 \\ 30 \end{array} \quad \begin{array}{r} 7.7 \\ 26 \end{array} \quad \begin{array}{r} 74 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 7.3 \end{array} \quad \begin{array}{r} 6.9 \\ 24 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 6.0 \\ 41 \end{array} \quad \begin{array}{r} 8.0 \\ 30 \end{array} \quad \begin{array}{r} 7.7 \\ 26 \end{array} \quad \begin{array}{r} 74 \\ 16 \end{array} \quad \begin{array}{r} 74 \\ 8 \end{array} \quad \begin{array}{r} 7.8 \\ 0 \end{array} \quad \begin{array}{r} 6.8 \\ 6 \end{array} \quad \begin{array}{r} 1.0 \\ 15 \end{array} \quad \begin{array}{r} 0.8 \\ 50 \end{array}$$

$$\begin{array}{r} 48 \\ 41 \end{array} \quad \begin{array}{r} 56 \\ 34 \end{array} \quad \begin{array}{r} 7.5 \\ 30 \end{array} \quad \begin{array}{r} 73 \\ 17 \end{array} \quad \begin{array}{r} 74 \\ 4 \end{array} \quad \begin{array}{r} 8.1 \\ 2 \end{array} \quad \begin{array}{r} 8.0 \\ 8.0 \end{array} \quad \begin{array}{r} 0.8 \\ 11 \end{array} \quad \begin{array}{r} +0.6 \\ 24 \end{array} \quad \begin{array}{r} +0.8 \\ 50 \end{array}$$

$$\begin{array}{r} 58 \\ 44 \end{array} \quad \begin{array}{r} 74 \\ 33 \end{array} \quad \begin{array}{r} 84 \\ 24 \end{array} \quad \begin{array}{r} 78 \\ 27 \end{array} \quad \begin{array}{r} 7.5 \\ 17 \end{array} \quad \begin{array}{r} 7.7 \\ 5 \end{array} \quad \begin{array}{r} 84 \\ 2 \end{array} \quad \begin{array}{r} 8.3 \\ 8.3 \end{array} \quad \begin{array}{r} 8.3 \\ 2 \end{array} \quad \begin{array}{r} 1.5 \\ 10 \end{array} \quad \begin{array}{r} 0.6 \\ 18 \end{array} \quad \begin{array}{r} +0.8 \\ 24 \end{array} \quad \begin{array}{r} +0.8 \\ 50 \end{array}$$

$$\begin{array}{r} 87 \\ 38 \end{array} \quad \begin{array}{r} 79 \\ 27 \end{array} \quad \begin{array}{r} 76 \\ 17 \end{array} \quad \begin{array}{r} 7.6 \\ 7.6 \end{array} \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad \begin{array}{r} 2.5 \\ 12 \end{array} \quad \begin{array}{r} 1.6 \\ 18 \end{array} \quad \begin{array}{r} +0.7 \\ 22 \end{array} \quad \begin{array}{r} +0.7 \\ 50 \end{array}$$

$$\begin{array}{r} 90 \\ 33 \end{array} \quad \begin{array}{r} 8.2 \\ 26 \end{array} \quad \begin{array}{r} 7.8 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 7.5 \end{array} \quad \begin{array}{r} 6.7 \\ 26 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.1 \\ 35 \end{array} \quad \begin{array}{r} 11.1 \\ 32 \end{array} \quad \begin{array}{r} 8.7 \\ 27 \end{array} \quad \begin{array}{r} 84 \\ 17 \end{array} \quad \begin{array}{r} 8.5 \\ 5 \end{array} \quad \begin{array}{r} 7.5 \\ 7.5 \end{array} \quad \begin{array}{r} 10.7 \\ 4 \end{array} \quad \begin{array}{r} 10.6 \\ 16 \end{array} \quad \begin{array}{r} 9.8 \\ 33 \end{array}$$

$$\begin{array}{r} 11.8 \\ 35 \end{array} \quad \begin{array}{r} 11.8 \\ 32 \end{array} \quad \begin{array}{r} 8.8 \\ 27 \end{array} \quad \begin{array}{r} 8.8 \\ 18 \end{array} \quad \begin{array}{r} 8.8 \\ 5 \end{array} \quad \begin{array}{r} 11.3 \\ 11.3 \end{array} \quad \begin{array}{r} 12.0 \\ 9 \end{array} \quad \begin{array}{r} 12.0 \\ 33 \end{array}$$

$$\begin{array}{r} 11.2 \\ 33 \end{array} \quad \begin{array}{r} 8.5 \\ 27 \end{array} \quad \begin{array}{r} 8.3 \\ 17 \end{array} \quad \begin{array}{r} 8.5 \\ 5 \end{array} \quad \begin{array}{r} 11.7 \\ 11.7 \end{array} \quad \begin{array}{r} 12.6 \\ 3 \end{array} \quad \begin{array}{r} 12.8 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 33 \end{array} \quad \begin{array}{r} 9.5 \\ 31 \end{array} \quad \begin{array}{r} 7.9 \\ 27 \end{array} \quad \begin{array}{r} 7.5 \\ 17 \end{array} \quad \begin{array}{r} 7.7 \\ 5 \end{array} \quad \begin{array}{r} 10.6 \\ 10.6 \end{array} \quad \begin{array}{r} 11.5 \\ 3 \end{array} \quad \begin{array}{r} 11.9 \\ 20 \end{array} \quad \begin{array}{r} 12.1 \\ 33 \end{array}$$

Station	+	Σ ✓	-	Elev.
20		951.75		
29250				44.1.
B.M.			9.01	942.74. ✓
293		✓		45.3.
T.P	7.53	958.66	0.62	951.13 ✓
+55				47.1.
294				47.6.
+50				49.2.
295				50.3.
+45				52.3. ✓
+71				53.4. ✓
+77				53.4. ✓
296				54.5.
+75				55.0.
+65				53.6.

21.

8

121.

13

$$\begin{array}{r} 76 \\ 33 \end{array} \quad \begin{array}{r} 76 \\ 74 \end{array} \quad \begin{array}{r} 69 \\ 76 \end{array} \quad \begin{array}{r} 67 \\ 17 \end{array} \quad \begin{array}{r} 68 \\ 2 \end{array} \quad \begin{array}{r} 77 \\ 7 \end{array} \quad \begin{array}{r} 83 \\ 3 \end{array} \quad \begin{array}{r} 85 \\ 33 \end{array}$$

$$\begin{array}{r} 54 \\ 33 \end{array} \quad \begin{array}{r} 59 \\ 26 \end{array} \quad \begin{array}{r} 57 \\ 16 \end{array} \quad \begin{array}{r} 62 \\ 3 \end{array} \quad \begin{array}{r} 65 \\ 7 \end{array} \quad \begin{array}{r} 69 \\ 1 \end{array} \quad \begin{array}{r} 69 \\ 7 \end{array} \quad \begin{array}{r} 62 \\ 9 \end{array} \quad \begin{array}{r} 40 \\ 33 \end{array}$$

Role #3-

$$\begin{array}{r} 128 \\ 33 \end{array} \quad \begin{array}{r} 117 \\ 27 \end{array} \quad \begin{array}{r} 116 \\ 16 \end{array} \quad \begin{array}{r} 119 \\ 7 \end{array} \quad \begin{array}{r} 116 \\ 7 \end{array} \quad \begin{array}{r} 106 \\ 14 \end{array} \quad \begin{array}{r} 87 \\ 18 \end{array} \quad \begin{array}{r} 82 \\ 25 \end{array} \quad \begin{array}{r} 61 \\ 33 \end{array} \quad \begin{array}{r} 56 \\ 50 \end{array}$$

$$\begin{array}{r} 124 \\ 33 \end{array} \quad \begin{array}{r} 109 \\ 26 \end{array} \quad \begin{array}{r} 107 \\ 15 \end{array} \quad \begin{array}{r} 111 \\ 7 \end{array} \quad \begin{array}{r} 107 \\ 11 \end{array} \quad \begin{array}{r} 84 \\ 14 \end{array} \quad \begin{array}{r} 62 \\ 28 \end{array} \quad \begin{array}{r} 58 \\ 50 \end{array}$$

$$\begin{array}{r} 113 \\ 33 \end{array} \quad \begin{array}{r} 96 \\ 25 \end{array} \quad \begin{array}{r} 95 \\ 15 \end{array} \quad \begin{array}{r} 95 \\ 7 \end{array} \quad \begin{array}{r} 94 \\ 12 \end{array} \quad \begin{array}{r} 75 \\ 15 \end{array} \quad \begin{array}{r} 50 \\ 35 \end{array} \quad \begin{array}{r} 50 \\ 50 \end{array}$$

125.
774.52

$$\begin{array}{r} 93 \\ 33 \end{array} \quad \begin{array}{r} 79 \\ 26 \end{array} \quad \begin{array}{r} 79 \\ 15 \end{array} \quad \begin{array}{r} 84 \\ 7 \end{array} \quad \begin{array}{r} 81 \\ 17 \end{array} \quad \begin{array}{r} 59 \\ 32 \end{array} \quad \begin{array}{r} 58 \\ 50 \end{array}$$

$$\begin{array}{r} 65 \\ 33 \end{array} \quad \begin{array}{r} 59 \\ 24 \end{array} \quad \begin{array}{r} 66 \\ 23 \end{array} \quad \begin{array}{r} 61 \\ 14 \end{array} \quad \begin{array}{r} 64 \\ 7 \end{array} \quad \begin{array}{r} 46 \\ 31 \end{array} \quad \begin{array}{r} 43 \\ 50 \end{array}$$

$$\begin{array}{r} 43 \\ 37 \end{array} \quad \begin{array}{r} 62 \\ 33 \end{array} \quad \begin{array}{r} 55 \\ 25 \end{array} \quad \begin{array}{r} 52 \\ 13 \end{array} \quad \begin{array}{r} 53 \\ 7 \end{array} \quad \begin{array}{r} 43 \\ 25 \end{array} \quad \begin{array}{r} 38 \\ 50 \end{array}$$

7.853.83
+ 11.73
7865.56

$$\begin{array}{r} 37 \\ 39 \end{array} \quad \begin{array}{r} 63 \\ 32 \end{array} \quad \begin{array}{r} 55 \\ 25 \end{array} \quad \begin{array}{r} 51 \\ 13 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 52 \\ 20 \end{array}$$

$$\begin{array}{r} 59 \\ 79 \end{array} \quad \begin{array}{r} 65 \\ 50 \end{array} \quad 5.5$$

$$\begin{array}{r} 27 \\ 39 \end{array} \quad \begin{array}{r} 59 \\ 33 \end{array} \quad \begin{array}{r} 50 \\ 24 \end{array} \quad \begin{array}{r} 43 \\ 12 \end{array} \quad \begin{array}{r} 42 \\ 7 \end{array} \quad \begin{array}{r} 47 \\ 10 \end{array} \quad \begin{array}{r} 41 \\ 20 \end{array}$$

$$\begin{array}{r} 38 \\ 29 \end{array} \quad \begin{array}{r} 48 \\ 50 \end{array} \quad 5.5$$

$$\begin{array}{r} 1.8 \\ 3.9 \end{array} \quad \begin{array}{r} 5.2 \\ 32 \end{array} \quad \begin{array}{r} 5.2 \\ 26 \end{array} \quad \begin{array}{r} 46 \\ 24 \end{array} \quad \begin{array}{r} 40 \\ 13 \end{array} \quad \begin{array}{r} 42 \\ 3 \end{array} \quad \begin{array}{r} 37 \\ 9 \end{array} \quad \begin{array}{r} 41 \\ 14 \end{array} \quad \begin{array}{r} 48 \\ 20 \end{array} \quad \begin{array}{r} 44 \\ 20 \end{array}$$

$$\begin{array}{r} 2.5 \\ 30 \end{array} \quad \begin{array}{r} 3.9 \\ 50 \end{array} \quad 5.5$$

$$\begin{array}{r} 53 \\ 33 \end{array} \quad \begin{array}{r} 55 \\ 28 \end{array} \quad \begin{array}{r} 48 \\ 12 \end{array} \quad \begin{array}{r} 51 \\ 20 \end{array} \quad \begin{array}{r} 47 \\ 20 \end{array}$$

$$\begin{array}{r} 26 \\ 30 \end{array} \quad \begin{array}{r} 43 \\ 50 \end{array} \quad \begin{array}{r} 85 \\ 75 \end{array}$$

Station	+	π /	-	Elev.
297		958.66 ✓		53.1.

+50.				52.4.
------	--	--	--	-------

298				52.8.
-----	--	--	--	-------

T.P.	2.93	956.74 ✓	4.85	853.81 ✓
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+35				52.4.
-----	--	--	--	-------

+70				50.3.
-----	--	--	--	-------

299				49.5.
-----	--	--	--	-------

+50				48.6.
-----	--	--	--	-------

300				47.4.
-----	--	--	--	-------

+61				47.7.
-----	--	--	--	-------

+62				41.4.
-----	--	--	--	-------

Profile Bridge No. of E

" " " " "

" " " " "

" " " " "

T.P.	2.79	946.03	13.50 ✓	943.24 ✓
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Lt.

E

Rt.

$T = 865.56$

12.5

$\frac{5.7}{33}$	$\frac{5.6}{22}$	$\frac{5.0}{11}$	$\frac{5.6}{9}$	$\frac{5.0}{17}$	$\frac{4.0}{29}$	$\frac{4.7}{50}$	$\frac{6.0}{75}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

-13.2

Yard-

$\frac{5.1}{33}$	$\frac{6.1}{24}$	$\frac{6.0}{10}$	$\frac{6.3}{10}$	$\frac{5.8}{15}$	$\frac{6.0}{15}$	$\frac{4.2}{27}$	$\frac{5.3}{31}$	$\frac{6.9}{50}$	$\frac{10.2}{75}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------

12.8

$\frac{5.5}{33}$	$\frac{5.6}{20}$	$\frac{5.4}{11}$	$\frac{5.9}{2}$	$\frac{5.9}{11}$	$\frac{7.0}{13}$	$\frac{6.7}{24}$	$\frac{7.5}{32}$	$\frac{9.8}{50}$	$\frac{12.2}{75}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	-------------------

Top of Stake 298

$\frac{4.0}{33}$	$\frac{3.7}{23}$	$\frac{3.4}{11}$	$\frac{3.7}{1}$	$\frac{4.3}{1}$	$\frac{4.8}{3}$	$\frac{4.9}{12}$	$\frac{3.7}{18}$	$\frac{3.3}{27}$	$\frac{4.4}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7.7}{33}$	$\frac{7.7}{29}$	$\frac{4.8}{22}$	$\frac{4.6}{12}$	$\frac{4.9}{3}$	$\frac{6.4}{3}$	$\frac{7.5}{3}$	$\frac{8.4}{18}$	$\frac{9.0}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{9.1}{33}$	$\frac{8.8}{29}$	$\frac{5.5}{22}$	$\frac{5.3}{12}$	$\frac{5.6}{3}$	$\frac{7.2}{3}$	$\frac{9.0}{3}$	$\frac{9.4}{15}$	$\frac{10.5}{27}$	$\frac{11.4}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{8.8}{33}$	$\frac{8.5}{26}$	$\frac{6.8}{21}$	$\frac{6.4}{12}$	$\frac{6.7}{3}$	$\frac{8.1}{3}$	$\frac{10.5}{8}$	$\frac{11.0}{28}$	$\frac{12.2}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{11.0}{33}$	$\frac{9.8}{24}$	$\frac{7.5}{19}$	$\frac{7.2}{11}$	$\frac{7.6}{3}$	$\frac{9.3}{3}$	$\frac{11.9}{8}$	$\frac{13.2}{20}$	$\frac{13.7}{33}$
-------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{12.7}{50}$	$\frac{12.7}{38}$	$\frac{12.5}{25}$	$\frac{10.7}{19}$	$\frac{6.8}{11}$	$\frac{6.4}{3}$	$\frac{6.8}{3}$	$\frac{8.8}{3}$	$\frac{12.9}{8}$	$\frac{14.9}{23}$	$\frac{15.2}{50}$
-------------------	-------------------	-------------------	-------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{12.7}{50}$	$\frac{15.3}{27}$	$\frac{15.3}{50}$	$\frac{15.3}{50}$
-------------------	-------------------	-------------------	-------------------

W. End. $6.9 = 949.9$

W. top. $4.1 = 952.7$

E. Top $4.0 = 952.8$

E. End $7.8 = 949.0$

Sta. + 7, - Elev.
946.03 ✓

300+80.

300+91.85 - 2 Track

2945 ✓

301+02

301+20

40.8.

T.P. 7.05 950.29 ✓ 2.79 943.24 ✓

301+75

46.7.

+65

45.5.

302

42.4.

B.M. +19.62 0.30 940.99 7.60 940.69 ✓

+50

38.3.

303

34.9 ✓

Lt

±

Rt

$$\begin{array}{r} 18.2 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 918.2 \\ \underline{17.8} \end{array}$$

$$\begin{array}{r} 17.8 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 16.48 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 16.58 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 16.74 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 18.9 \\ \underline{50} \end{array}$$

$$\begin{array}{r} 929.0 \\ \underline{17.1} \end{array}$$

$$\begin{array}{r} 18.3 \\ \underline{50} \end{array}$$

41.5 / 46-Mud Sil W. end

Silid brks
Sandy/clay.

40.0
6.05 " 1. E end.

$\begin{array}{r} 51 \\ \underline{50} \end{array}$	$\begin{array}{r} 42 \\ \underline{31} \end{array}$	$\begin{array}{r} 6.0 \\ \underline{27} \end{array}$	$\begin{array}{r} 6.0 \\ \underline{4} \end{array}$	$\begin{array}{r} 19.8 \\ \underline{5.2} \end{array}$	$\begin{array}{r} 3.1 \\ \underline{5} \end{array}$	$\begin{array}{r} 4.7 \\ \underline{15} \end{array}$	$\begin{array}{r} 8.6 \\ \underline{23} \end{array}$	$\begin{array}{r} 6.1 \\ \underline{29} \end{array}$	$\begin{array}{r} 5.5 \\ \underline{50} \end{array}$
---	---	--	---	--	---	--	--	--	--

$\begin{array}{r} 7.2 \\ \underline{50} \end{array}$	$\begin{array}{r} 8.7 \\ \underline{37} \end{array}$	$\begin{array}{r} 1.0 \\ \underline{22} \end{array}$	$\begin{array}{r} 1.3 \\ \underline{5} \end{array}$	$\begin{array}{r} 3.6 \\ \underline{4} \end{array}$	$\begin{array}{r} 6.3 \\ \underline{16} \end{array}$	$\begin{array}{r} 7.8 \\ \underline{16} \end{array}$	$\begin{array}{r} 10.2 \\ \underline{29} \end{array}$	$\begin{array}{r} 9.7 \\ \underline{50} \end{array}$
--	--	--	---	---	--	--	---	--

$\begin{array}{r} 10.9 \\ \underline{40} \end{array}$	$\begin{array}{r} 10.1 \\ \underline{33} \end{array}$	$\begin{array}{r} 4.4 \\ \underline{22} \end{array}$	$\begin{array}{r} 4.8 \\ \underline{4} \end{array}$	$\begin{array}{r} 8.3 \\ \underline{7} \end{array}$	$\begin{array}{r} 10.2 \\ \underline{16} \end{array}$	$\begin{array}{r} 9.6 \\ \underline{27} \end{array}$	$\begin{array}{r} 9.7 \\ \underline{40} \end{array}$
---	---	--	---	---	---	--	--

$\begin{array}{r} 13.3 \\ \underline{43} \end{array}$	$\begin{array}{r} 12.5 \\ \underline{31} \end{array}$	$\begin{array}{r} 2.7 \\ \underline{23} \end{array}$	$\begin{array}{r} 7.9 \\ \underline{1} \end{array}$	$\begin{array}{r} 7.9 \\ \underline{1} \end{array}$	$\begin{array}{r} 10.7 \\ \underline{9} \end{array}$	$\begin{array}{r} 11.3 \\ \underline{17} \end{array}$	$\begin{array}{r} 11.0 \\ \underline{33} \end{array}$
---	---	--	---	---	--	---	---

Top Mon.

$\begin{array}{r} 8.4 \\ \underline{40} \end{array}$	$\begin{array}{r} 7.2 \\ \underline{30} \end{array}$	$\begin{array}{r} 2.3 \\ \underline{22} \end{array}$	$\begin{array}{r} 2.7 \\ \underline{4} \end{array}$	$\begin{array}{r} 5.1 \\ \underline{7} \end{array}$	$\begin{array}{r} 6.5 \\ \underline{14} \end{array}$	$\begin{array}{r} 5.9 \\ \underline{17} \end{array}$	$\begin{array}{r} 5.6 \\ \underline{33} \end{array}$
--	--	--	---	---	--	--	--

$\begin{array}{r} 10.4 \\ \underline{33} \end{array}$	$\begin{array}{r} 10.0 \\ \underline{29} \end{array}$	$\begin{array}{r} 5.7 \\ \underline{21} \end{array}$	$\begin{array}{r} 6.1 \\ \underline{1} \end{array}$	$\begin{array}{r} 6.1 \\ \underline{1} \end{array}$	$\begin{array}{r} 10.8 \\ \underline{9} \end{array}$	$\begin{array}{r} 11.6 \\ \underline{23} \end{array}$	$\begin{array}{r} 11.1 \\ \underline{33} \end{array}$
---	---	--	---	---	--	---	---

Sta. + π - Elev.

940.99 ✓

303 +50

32.3

304

30.5

T.P.

0.47

931.89 ✓

9.59

931.40 ✓

+30

~~38.9~~

29.8

305

~~37.4~~

28.3

+50

~~36.5~~

27.4

306

~~36.0~~

26.9

307

~~34.8~~

25.7

+60

~~33.9~~

24.8

308

~~33.3~~

24.2

+50

~~32.3~~

23.2

309

~~31.1~~

22.0

+1982

~~30.5~~

21.33

B.M.

1054

921.33

H.

L

Rt.

16

$\frac{10.6}{33}$	$\frac{10.1}{26}$	$\frac{8.5}{17}$	$\frac{8.4}{9}$	$\frac{8.1}{1}$	$\frac{8.7}{1}$	$\frac{11.9}{10}$	$\frac{13.0}{18}$	$\frac{13.2}{33}$
-------------------	-------------------	------------------	-----------------	-----------------	-----------------	-------------------	-------------------	-------------------

$\frac{13.8}{33}$	$\frac{13.7}{24}$	$\frac{10.5}{17}$	$\frac{10.2}{8}$	$\frac{10.5}{1}$	$\frac{10.5}{1}$	$\frac{12.5}{6}$	$\frac{12.7}{19}$	$\frac{12.5}{33}$
-------------------	-------------------	-------------------	------------------	------------------	------------------	------------------	-------------------	-------------------

$\frac{5.9}{33}$	$\frac{5.6}{23}$	$\frac{2.4}{16}$	$\frac{2.0}{7}$	$\frac{2.1}{1}$	$\frac{7.3}{2}$	$\frac{4.2}{7}$	$\frac{3.2}{23}$	$\frac{2.9}{33}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{6.8}{33}$	$\frac{6.8}{29}$	$\frac{7.0}{24}$	$\frac{3.5}{18}$	$\frac{3.4}{8}$	$\frac{3.6}{3}$	$\frac{6.2}{8}$	$\frac{7.1}{16}$	$\frac{7.4}{23}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{7.3}{33}$ — culvert $\frac{7.15}{33}$

$\frac{18}{50}$	$\frac{1.2}{35}$	$\frac{6.4}{27}$	$\frac{6.5}{23}$	$\frac{4.2}{19}$	$\frac{4.5}{1}$	$\frac{4.7}{4}$	$\frac{7.2}{11}$	$\frac{7.1}{33}$
-----------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------

$\frac{41.0}{50}$	$\frac{41.0}{35}$	$\frac{6.0}{25}$	$\frac{6.3}{22}$	$\frac{5.2}{19}$	$\frac{5.2}{5}$	$\frac{5.0}{1}$	$\frac{5.4}{2}$	$\frac{8.1}{13}$	$\frac{8.6}{21}$	$\frac{7.0}{24}$	$\frac{7.4}{33}$
-------------------	-------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{40.7}{50}$	$\frac{40.7}{34}$	$\frac{7.0}{23}$	$\frac{7.3}{20}$	$\frac{6.0}{14}$	$\frac{6.2}{1}$	$\frac{6.6}{8}$	$\frac{8.3}{13}$	$\frac{9.2}{20}$	$\frac{6.5}{23}$	$\frac{7.0}{33}$
-------------------	-------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{6.0}{50}$	$\frac{6.0}{33}$	$\frac{2.1}{26}$	$\frac{8.2}{24}$	$\frac{8.1}{19}$	$\frac{7.0}{17}$	$\frac{7.1}{1}$	$\frac{2.7}{9}$	$\frac{9.3}{14}$	$\frac{9.3}{21}$	$\frac{8.0}{23}$	$\frac{8.0}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

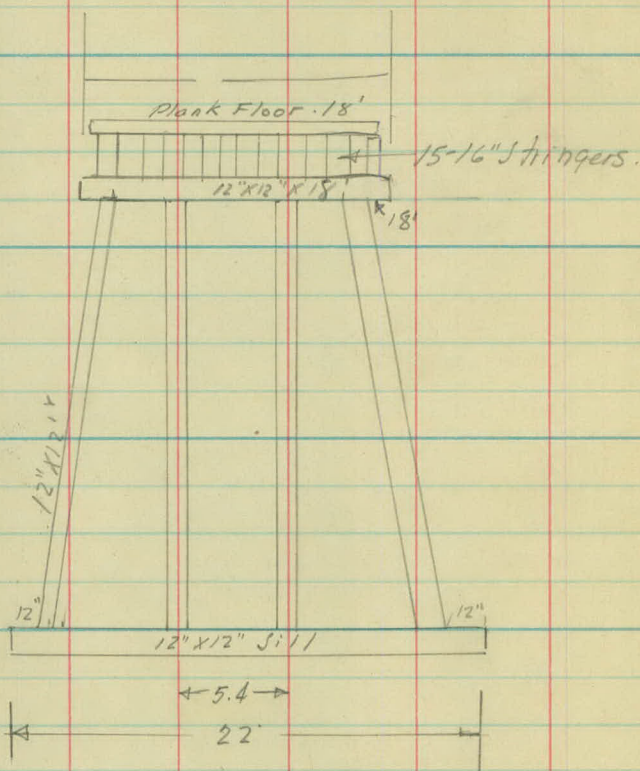
$\frac{7.3}{50}$	$\frac{7.3}{29}$	$\frac{8.6}{26}$	$\frac{8.7}{22}$	$\frac{7.4}{18}$	$\frac{7.7}{1}$	$\frac{8.0}{9}$	$\frac{9.4}{12}$	$\frac{9.7}{18}$	$\frac{8.2}{22}$	$\frac{8.1}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{8.0}{50}$	$\frac{8.1}{33}$	$\frac{8.8}{29}$	$\frac{8.3}{18}$	$\frac{9.0}{14}$	$\frac{8.7}{1}$	$\frac{9.3}{17}$	$\frac{10.1}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	-------------------

$\frac{8.7}{50}$	$\frac{9.9}{27}$	$\frac{9.4}{13}$	$\frac{9.9}{1}$	$\frac{10.4}{33}$
------------------	------------------	------------------	-----------------	-------------------

$\frac{9.8}{50}$	$\frac{9.5}{33}$	$\frac{10.54}{1}$	$\frac{10.8}{33}$
------------------	------------------	-------------------	-------------------

Top Stone Mon. Sta. 309 + 19.82



(7)

949.9

300 + 61.5
+ 62.5 - 2 Bent
#1

Top Sil
Elev. 949.5

+ 928.3

12" x 12"

952.7

300 + 82.5 - 2 Bent
#2

Top Rail Elev. 929.47

300 + 91.85 - 2 Track

16" Stringers

+ 929.0

Frame Bents

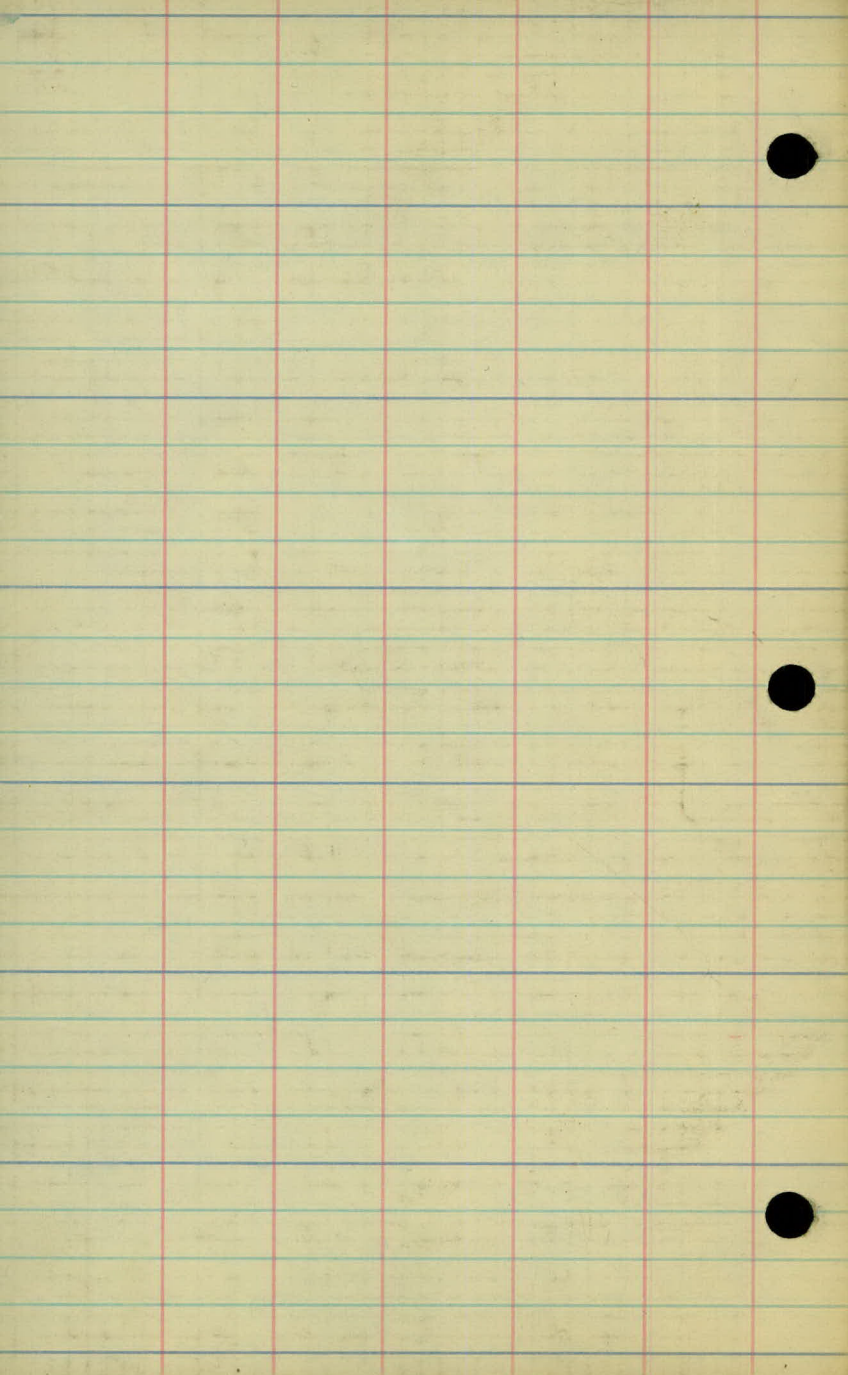
952.8

301 + 03.7 - 2 Bent
#3

949.0

#4
+ 23.3 - 2 Bent
301 + 24.4 Elev

Top Sil
Elev. 949.0



Co. Rd 'C'

Rice to Lake St.

Slope stakes.

32' Top

3:1 Fill

2' Deep Ditch

Var-Both

1:1 Back Slope.

Ditch 1' Deep on South Side

288- to Bridges

33- Lt. + Rt.

Sta.	+	-	Grade
	3.07	960.98	957.91
277 + 97.6			

278 to 9.6 - Edge Row.

278 + 30			57.5
----------	--	--	------

279			56.5
-----	--	--	------

1.1

+40			56.2
-----	--	--	------

280			55.0
-----	--	--	------

+40			54.4
-----	--	--	------

281			53.0
-----	--	--	------

+55			51.7
			53.8

7

T.P.	3.02	953.92	10.08	950.90
------	------	--------	-------	--------

282			50.7
-----	--	--	------

+50			49.7
-----	--	--	------

283			48.7
-----	--	--	------

Mon @ Rice St.

$$3.5 \quad 33' \frac{31}{104} \quad \frac{31}{104}$$

$$4.5 \quad 33' \frac{43}{102} \quad \frac{43}{102}$$

$$4.8 \quad 33' \frac{54}{1014} \quad \frac{55}{107} \quad \frac{39}{109} / 33$$

$$6.0 \quad 33' \frac{83}{102} \quad \frac{71}{111} \quad \frac{80}{100} / 376$$

$$6.6 \quad 33' \frac{79}{1007} \quad 214 \frac{64}{118} \quad \frac{75}{109} \quad \frac{88}{122} / 226$$

$$8.0 \quad 33' \frac{79}{101} \quad \frac{84}{104} \quad \frac{60}{120} / 33$$

$$9.2 \quad 33' \frac{98}{1011} \quad ? \quad \frac{101}{109} \quad ? \quad \frac{55}{137} / 33 \quad ? \quad 849 \quad 702$$

$$3.2 \quad 33' \frac{46}{1006} \quad \frac{44}{112} \quad \frac{02}{130} / 33$$

$$4.2 \quad 33' \frac{62}{1000} \quad 222 \frac{66}{221} \quad \frac{57}{115} \quad \frac{35}{107} / 33$$

$$5.2 \quad 33' \frac{82}{100} \quad \frac{70}{118} \quad \frac{52}{120} / 33 \quad \text{①}$$

95392

283+45

478

284

469

+50

462

T.P.

+75

458

T.P.

3.68

948.50

9.10

944.82

285

455

+50

449

286

444

+32

441

+62

439

287

436

+50

433

288

431

+50

430

6.1	$28.2 \begin{array}{r} 1.5 \\ -7.1 \end{array}$	$\begin{array}{r} 7.9 \\ -1.8 \end{array}$	$\begin{array}{r} 8.9 \\ -2.8 \end{array} / 24.4$	
7.0	$26.8 \begin{array}{r} 1.06 \\ -3.6 \end{array}$	$\begin{array}{r} 8.6 \\ -1.6 \end{array}$	$\begin{array}{r} 10.5 \\ -3.5 \end{array} / 26.5$	
7.7	$25.0 \begin{array}{r} 1.07 \\ -2.0 \end{array}$	$\begin{array}{r} 9.0 \\ -1.3 \end{array}$	$\begin{array}{r} 9.4 \\ -1.7 \end{array} / 21.1$	$\begin{array}{r} 9.5 \\ 10.2 \end{array} / 33$
3.0	$28 \begin{array}{r} 4.7 \\ 100.3 \end{array}$	$20.5 \begin{array}{r} 4.5 \\ -1.5 \end{array}$	$\begin{array}{r} 3.8 \\ -0.8 \end{array}$	$\begin{array}{r} 4.8 \\ -1.8 \end{array} / 21.4$
3.6	$20 \begin{array}{r} 5.6 \\ 100.3 \end{array}$	$19.3 \begin{array}{r} 4.7 \\ -1.1 \end{array}$	$\begin{array}{r} 4.5 \\ -0.9 \end{array}$	$\begin{array}{r} 6.1 \\ 7.1 \end{array} / 20.5$
4.1	$23 \begin{array}{r} 4.7 \\ 101.4 \end{array}$	$\begin{array}{r} 4.6 \\ -0.5 \end{array}$	$\begin{array}{r} 5.7 \\ -1.6 \end{array} / 20.8$	$\begin{array}{r} 3.2 \\ 10.9 \end{array} / 33$
4.1	$23 \begin{array}{r} 5.6 \\ 100.8 \end{array}$	$\begin{array}{r} 5.2 \\ -0.4 \end{array}$	$\begin{array}{r} 6.3 \\ -1.9 \end{array} / 21.7$	$\begin{array}{r} 3.6 \\ 10.8 \end{array} / 33$
4.6	$22.7 \begin{array}{r} 6.6 \\ 100 \end{array}$	$\begin{array}{r} 5.5 \\ -0.9 \end{array}$	$\begin{array}{r} 7.0 \\ -2.4 \end{array} / 23.2$	$\begin{array}{r} 6.6 \\ 10.6 \end{array} / 33$
4.9	$26.8 \begin{array}{r} 6.9 \\ 100.0 \end{array}$	$\begin{array}{r} 6.4 \\ -2.0 \end{array}$	$\begin{array}{r} 8.4 \\ -3.5 \end{array} / 26.5$	
5.2	$29.6 \begin{array}{r} 7.2 \\ 100.0 \end{array}$	$\begin{array}{r} 7.3 \\ -2.1 \end{array}$	$\begin{array}{r} 9.2 \\ -4.0 \end{array} / 28.0$	
5.4	$23 \begin{array}{r} 7.0 \\ 100.4 \end{array}$	$\begin{array}{r} 8.1 \\ -2.7 \end{array}$	$\begin{array}{r} 8.8 \\ -3.4 \end{array} / 26.2$	
5.5	$23 \begin{array}{r} 5.1 \\ 10.1 \end{array}$	$\begin{array}{r} 8.4 \\ 10.4 \end{array}$	$\begin{array}{r} 6.9 \\ -1.4 \end{array} / 20.2$	

1464
1150

948.50

288480

42.9

11.73

956.05

4.18

944.32

289

42.9

+13

43.0

+21

43.0

+65

42.9

290

43.0

+18

43.1

+35

43.2

T.P

8.63

951.37

13.31

942.76

+65

43.3

291

43.5

+50

44.1

292

44.6

B.M.

9th Road

$$5.6 \quad 33 \overline{) \frac{5.4}{0.2}}$$

$$\frac{1.5}{11.1}$$

$$\frac{3.5}{12.1} / 33$$

13.2

13.1

$$13.1 \quad 33 \overline{) \frac{11.5}{+1.6}}$$

$$\frac{11.9}{11.2}$$

$$\frac{5.1}{18.1} / 33$$

$$13.2 \quad 33 \overline{) \frac{10.3}{1.9}}$$

$$\frac{12.4}{10.8}$$

$$\frac{3.4}{19.8} / 33$$

$$13.1 \quad 33 \overline{) \frac{11.8}{1.3}}$$

$$\frac{12.7}{10.4}$$

$$\frac{3.4}{19.7} / 33$$

240.40
(9)

13.0

$$\frac{12.0}{11.0}$$

$$\frac{4.0}{19.0} / 33$$

14.9 13.9

$$12.9 \quad 33 \overline{) \frac{12.0}{10.9}}$$

$$\frac{11.8}{11.1}$$

$$\frac{10.7}{11.2} / 33$$

350
270

10.1

$$8.1 \quad 22.0 \overline{) \frac{10.1}{10.0}}$$

$$\frac{9.3}{11.2}$$

$$\frac{7.4}{10.7} / 33$$

(9)

9.9

$$7.9 \quad 28.8 \overline{) \frac{9.9}{10.0}}$$

$$\frac{10.5}{12.7}$$

$$\frac{11.7}{13.8} / 27.4$$

9.3

$$7.3 \quad 29.9 \overline{) \frac{9.3}{10.0}}$$

$$\frac{10.9}{13.6}$$

$$\frac{12.6}{15.3} / 31.9$$

$$6.3 \quad 29.5 \overline{) \frac{11}{10.0}}$$

$$\frac{10.2}{13.4}$$

$$\frac{11.8}{15.0} / 31.0$$

rt - Rt.

(942.74) RR sp. in T.P. 742 + 25

951.13 #3

951.87

292+50

45.3

293

46.2

T.P.

10.86

958.00

4.23

947.14

+55

47.2

294

48.1

+50

49.5

295

50.1

+45

51.0

T.P.

8.37

964.34 - 2.03

955.97

+71

51.5

+77

51.6

296

52.1

+25

52.6

+65

53.4

$$\begin{array}{r} 8.1 \\ 61 \overline{) 529} \end{array} \begin{array}{r} 71 \\ 00.08 \end{array}$$

$$\begin{array}{r} 17.9 \\ -1.2 \end{array}$$

$$\begin{array}{r} 9.2 \\ -2.9 \end{array} \begin{array}{r} 22.7 \\ 00.00 \end{array}$$

$$\begin{array}{r} 5.6 \\ 40.14 \overline{) 22.0} \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \overline{) 171} \end{array}$$

$$\begin{array}{r} 41 \\ -0.9 \end{array}$$

$$\begin{array}{r} 46 \\ 10.6 \overline{) 33} \end{array}$$

$$\begin{array}{r} 10.8 \\ 33 \overline{) 359} \end{array}$$

$$\begin{array}{r} 44 \\ -0.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ 15.3 \overline{) 33} \end{array}$$

$$\begin{array}{r} 9.9 \\ 33 \overline{) 327} \end{array}$$

$$\begin{array}{r} 10.5 \\ -0.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ 14.3 \overline{) 33} \end{array}$$

948.61 - Nadin RD. Rt. Sta. 244

$$\begin{array}{r} 8.9 \\ 33 \overline{) 297} \end{array}$$

$$\begin{array}{r} 8.9 \\ 0.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ 14.2 \overline{) 33} \end{array}$$

$$\begin{array}{r} 7.9 \\ 33 \overline{) 212} \end{array}$$

$$\begin{array}{r} 7.9 \\ 0.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ 12.7 \overline{) 33} \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \overline{) 113} \end{array}$$

$$\begin{array}{r} 5.7 \\ +1.3 \end{array}$$

$$\begin{array}{r} 4.0 \\ 12.0 \overline{) 33} \end{array}$$

Top Large Boulder.

$$12.8$$

$$\begin{array}{r} 11.2 \\ +1.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ 13.3 \overline{) 33} \end{array}$$

$$\begin{array}{r} 12.7 \\ 33 \overline{) 118} \end{array}$$

$$\begin{array}{r} 11.0 \\ +1.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ 17.5 \overline{) 33} \end{array}$$

$$\begin{array}{r} 12.2 \\ 33 \overline{) 113} \end{array}$$

$$\begin{array}{r} 7.9 \\ +2.3 \end{array}$$

$$\begin{array}{r} 2.8 \\ 19.4 \overline{) 33} \end{array}$$

$$\begin{array}{r} 11.7 \\ 33 \overline{) 103} \end{array}$$

$$\begin{array}{r} 9.2 \\ +2.5 \end{array}$$

$$\begin{array}{r} 1.5 \\ 10.2 \overline{) 33} \end{array}$$

$$\begin{array}{r} 10.9 \\ 33 \overline{) 10.8} \end{array}$$

$$\begin{array}{r} 10.8 \\ +0.1 \end{array}$$

$$\begin{array}{r} 1.6 \\ 19.3 \overline{) 33} \end{array}$$

964.34

297

54.0

+50

54.7

298

55.1

390 957.44 10.80

983.54

+35

55.3

+70

55.4

299

55.4

+50

55. ✓

300

54.8

(+47-Brid)

2.22 949.55

10.11

54.2

+61

8.85

948.69

→ topman

+62

+80

301

$$\begin{array}{r} 12.3 \\ 10.3 \end{array}$$

$$\begin{array}{r} 11.4 \\ 33 \overline{) 381} \\ 330 \\ \hline 51 \end{array}$$

$$\begin{array}{r} 11.2 \\ 10.9 \end{array}$$

$$\begin{array}{r} 3.2 \\ 7.1 \overline{) 37} \end{array}$$

$$\begin{array}{r} 11.6 \\ 9.6 \end{array}$$

$$\begin{array}{r} 10.8 \\ 33 \overline{) 358} \\ 330 \\ \hline 28 \end{array}$$

$$\begin{array}{r} 11.9 \\ 11.3 \end{array}$$

$$\begin{array}{r} 4.3 \\ 15.3 \overline{) 33} \end{array}$$

$$\begin{array}{r} 11.2 \\ 9.2 \end{array}$$

$$\begin{array}{r} 11.2 \\ 33 \overline{) 370} \\ 330 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 11.5 \\ 11.3 \end{array}$$

$$\begin{array}{r} 6.3 \\ 12.9 \overline{) 33} \end{array}$$

$$2.1$$

$$\begin{array}{r} 4.4 \\ 20.6 \overline{) 23} \end{array}$$

$$\begin{array}{r} 5.1 \\ 5.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ 2.7 \overline{) 21.4} \end{array}$$

$$2.0$$

$$\begin{array}{r} 8.1 \\ 28.2 \overline{) 6.1} \end{array}$$

$$\begin{array}{r} 7.3 \\ 5.3 \end{array}$$

$$\begin{array}{r} 10.1 \\ 8.1 \overline{) 32.2} \end{array}$$

$$2.0$$

$$\begin{array}{r} 9.5 \\ 31 \overline{) 7.5} \end{array}$$

$$\begin{array}{r} 7.8 \\ 5.8 \end{array}$$

$$\begin{array}{r} 12.9 \\ 10.9 \overline{) 37.8} \end{array}$$

$$2.2$$

$$\begin{array}{r} 6.4 \\ 20.4 \overline{) 7.2} \end{array}$$

$$\begin{array}{r} 9.0 \\ 6.8 \end{array}$$

$$\begin{array}{r} 12.3 \\ 11.9 \overline{) 38.2} \end{array}$$

$$2.6$$

$$\begin{array}{r} 11.7 \\ 34.2 \overline{) 9.1} \end{array}$$

$$\begin{array}{r} 10.0 \\ 7.4 \end{array}$$

$$\begin{array}{r} 15.1 \\ 12.5 \overline{) 41.0} \end{array}$$

$$3.2$$

$$\begin{array}{r} 12.5 \\ 36.6 \overline{) 10.3} \end{array}$$

$$\begin{array}{r} 9.8 \\ 4.6 \end{array}$$

$$\begin{array}{r} 15.0 \\ 11.8 \overline{) 39.8} \end{array}$$

301+37-(Brid)

+65

302

+50

303

+50

304

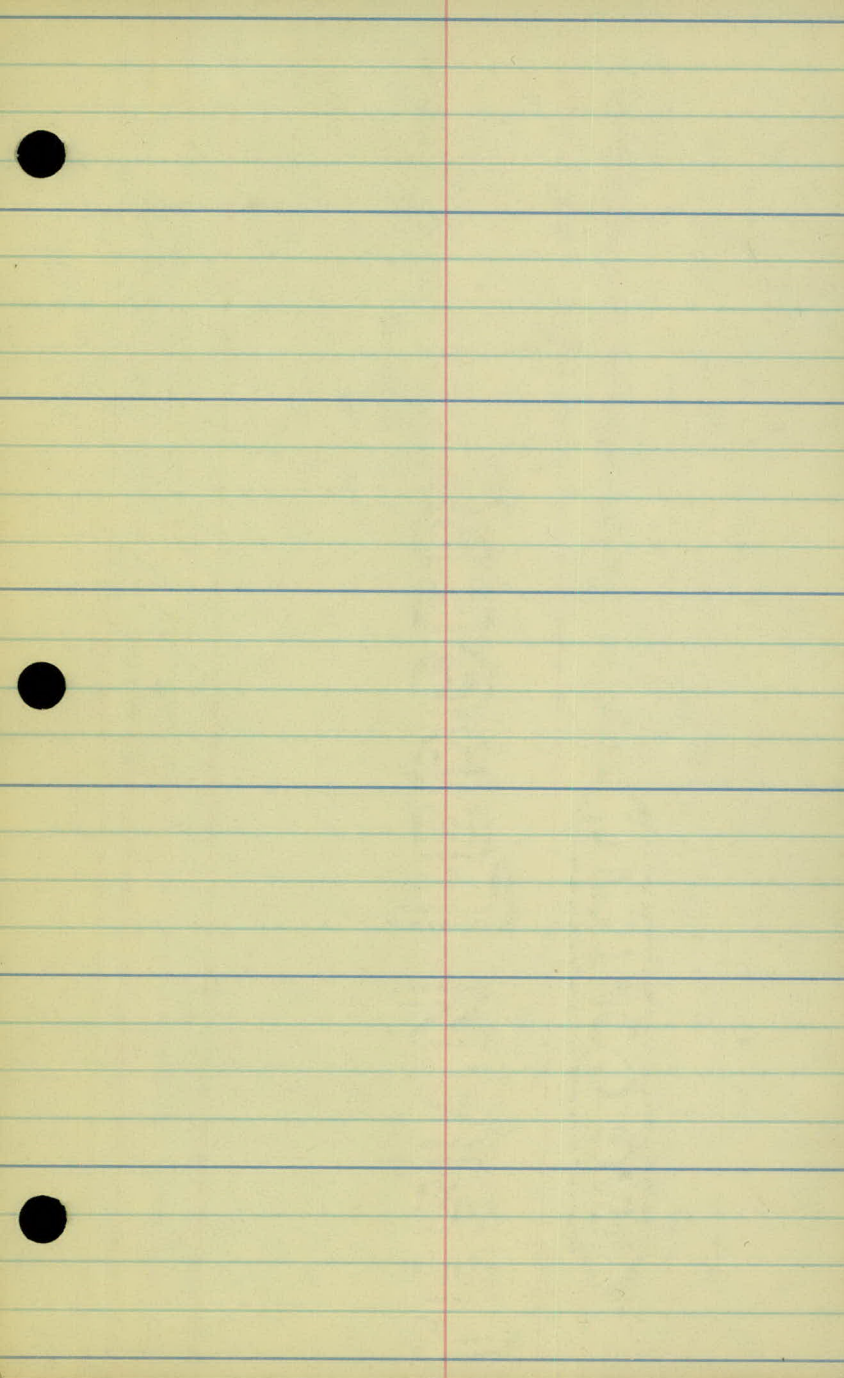
+30

3

305

+50

306



306 f50

307

+60

308

+50

309

+19.82

Dr. 6-BK 26

Co. Rd. C"

Borrow Pit X Sections

Sta	+	-	Elev
B.M.	18.93	953.62	940.69
I.P.	4.88	958.00 953.50	953.12
B.M.		6.31	952.19 → 951.69
292.			44.8
	+50		45.7
293			46.5
	+50		47.3
294			48.2
	+50		49.3
295			50.3
	+50		51.4
296			52.5
	+50		53.5

ht.

£

Top Mont 302+19.62

Spike in P.P. 21' RH. 295+12

41.2	41.9	42.2	42.4	44.4	44.8
$\frac{168}{100}$	$\frac{161}{50}$	$\frac{158}{28}$	$\frac{156}{21}$	$\frac{136}{150}$	$\frac{132}{13.2}$

42.4	42.5	44.2	43.3	43.7	46.3	46.7
$\frac{156}{100}$	$\frac{155}{60}$	$\frac{138}{33}$	$\frac{147}{32}$	$\frac{143}{21}$	$\frac{127}{16}$	$\frac{123}{12.3}$

42.8	46.2	46.5	44.3	44.6	46.0	46.5
$\frac{152}{100}$	$\frac{118}{50}$	$\frac{115}{34}$	$\frac{127}{31}$	$\frac{124}{21}$	$\frac{120}{16}$	$\frac{115}{11.5}$

41.6	46.2	45.9	44.8	45.3	47.0	47.3
$\frac{162}{100}$	$\frac{128}{50}$	$\frac{121}{34}$	$\frac{132}{32}$	$\frac{127}{21}$	$\frac{110}{16}$	$\frac{107}{10.7}$

41.7	45.0	46.3	45.9	46.3	47.9	48.2
$\frac{163}{100}$	$\frac{130}{50}$	$\frac{117}{33}$	$\frac{121}{32}$	$\frac{117}{21}$	$\frac{101}{16}$	$\frac{98}{9.8}$

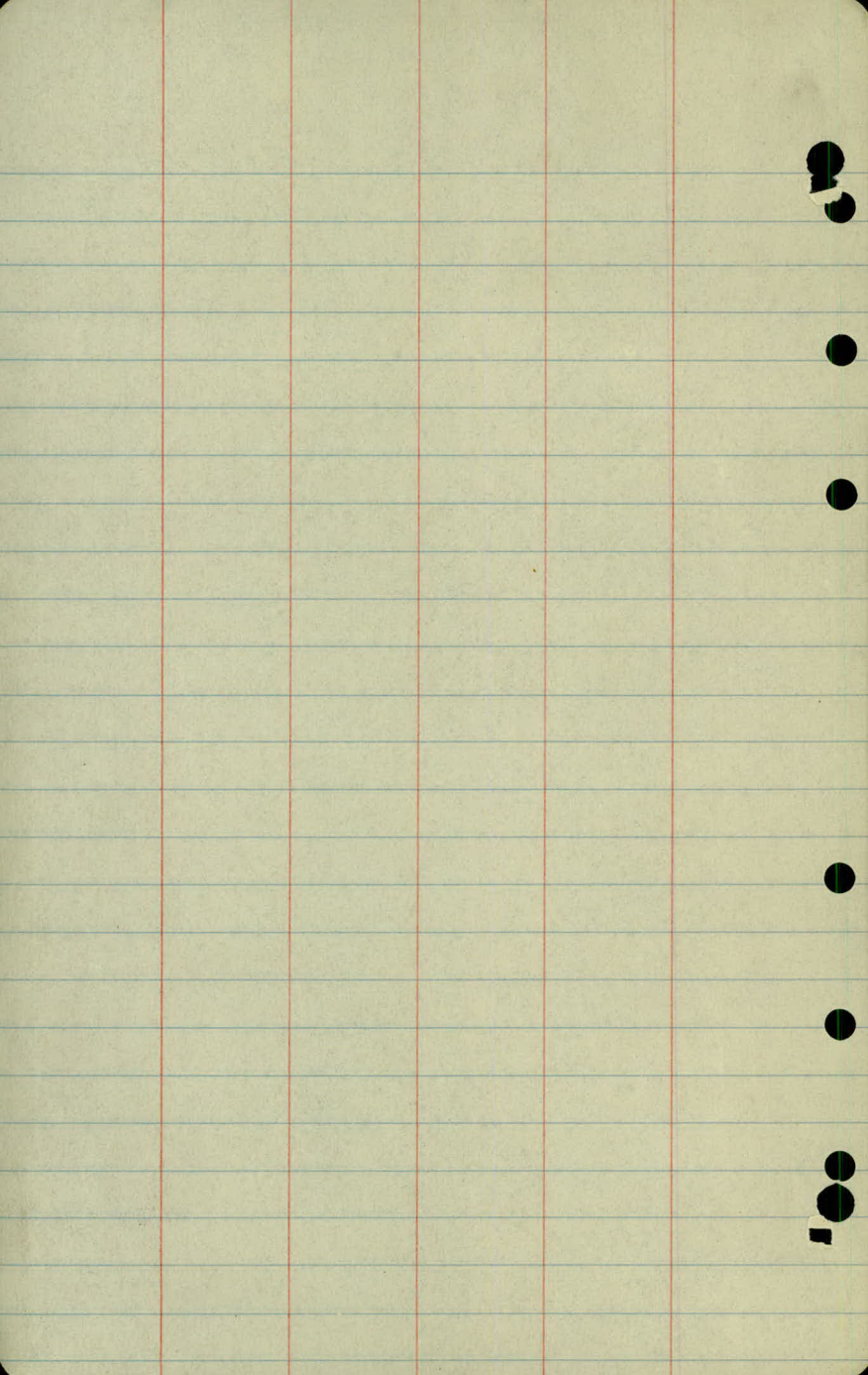
43.7	46.2	47.3	46.8	47.1	49.0	49.3
$\frac{143}{100}$	$\frac{118}{72}$	$\frac{107}{33}$	$\frac{112}{32}$	$\frac{109}{21}$	$\frac{90}{16}$	$\frac{87}{8.7}$

44.2	45.4	47.6	48.6	49.3	48.0	49.3	50.2	50.3
$\frac{138}{200}$	$\frac{126}{139}$	$\frac{109}{100}$	$\frac{94}{80}$	$\frac{87}{33}$	$\frac{100}{32}$	$\frac{97}{21}$	$\frac{78}{16}$	$\frac{77}{7.7}$

46.9	50.5	51.9	52.5	52.7	49.0	49.2	51.1	51.4
$\frac{111}{200}$	$\frac{75}{102}$	$\frac{61}{100}$	$\frac{53}{37}$	$\frac{53}{34}$	$\frac{90}{29}$	$\frac{88}{22}$	$\frac{69}{16}$	$\frac{66}{6.6}$

47.0	54.0	54.9	55.0	55.6	50.3	50.6	52.2	52.5
$\frac{110}{184}$	$\frac{40}{129}$	$\frac{31}{100}$	$\frac{30}{75}$	$\frac{24}{38}$	$\frac{77}{30}$	$\frac{74}{21}$	$\frac{58}{15}$	$\frac{55}{5.5}$

55.4	57.0	51.4	51.5	53.1	53.5
$\frac{26}{63.0}$	$\frac{10}{41}$	$\frac{46}{30}$	$\frac{65}{21}$	$\frac{49}{15}$	$\frac{45}{4.5}$



Additional X Sections

Co. Rd C" Borrow Pit.

Feb 2, 1988

Sta	+	π	-	Elev.
B.M.	3.40	955.09		951.69

294 +50

49.3

295

50.3

+50

51.4

Lt.

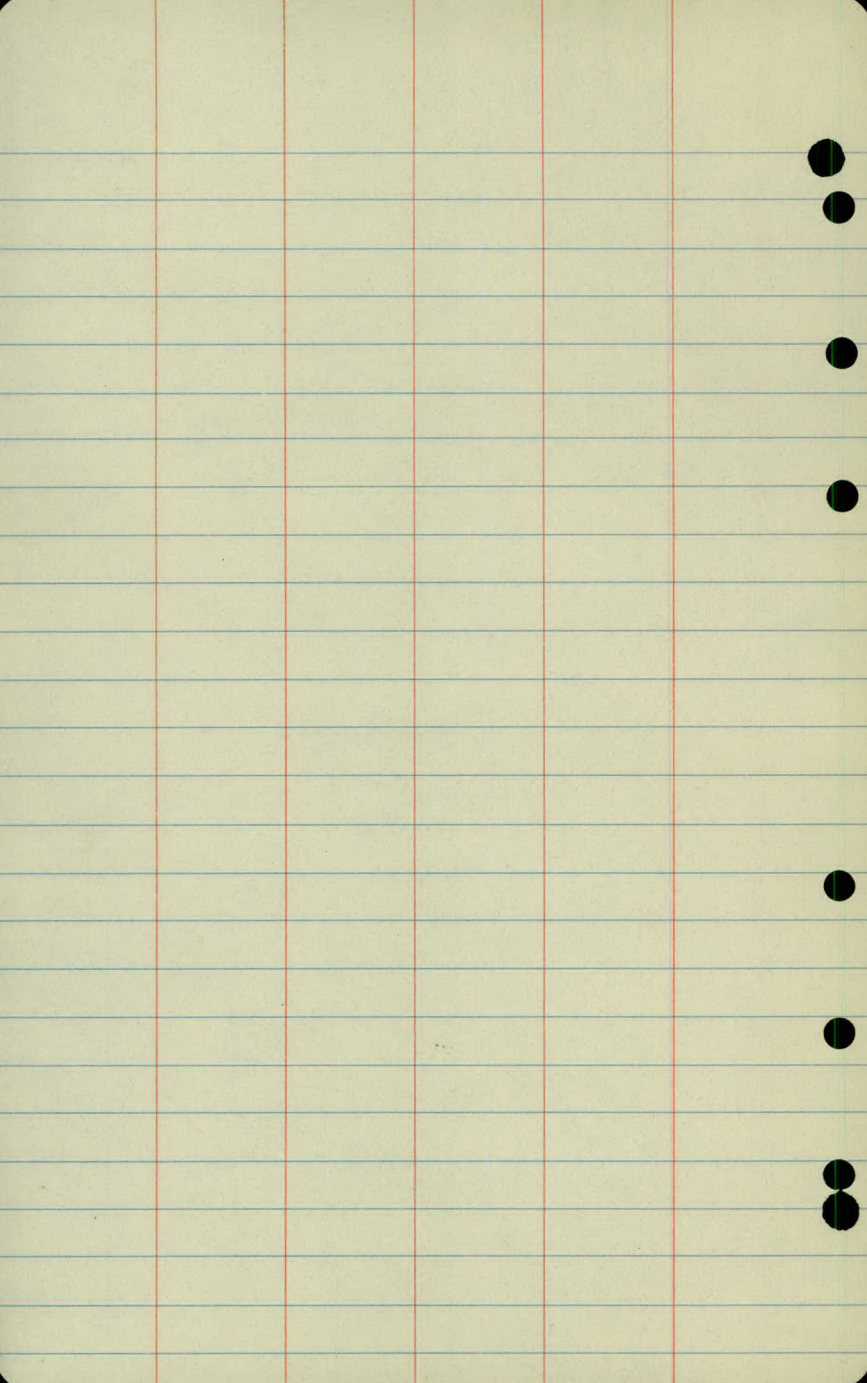
L.

Spike in T.P. Rt sta 295+12

	39.4	40.6	40.7	39.9	40.5	42.2	
Edge Asparagus	15.7	14.5	14.4	15.2	14.6	12.9	
Field	→ 308	293	250	213	172	185	(5.8)

	37.7	39.3	40.6	42.3	
	→ 310	263	245		
Fe. →	12.4	15.8	14.5	12.8	
	351	300	263	245	(4.8)

	39.1	40.7	41.9	42.1	44.5	
Edge Asparagus	14.0	14.4	13.2	18.0	10.6	
Fe. →	354	329	312	300	270	289
						(3.7)



BORROW PIT
Alignment & Topog.
C.O.R.D.C.

Feb. 2, 1938

H. Andrie

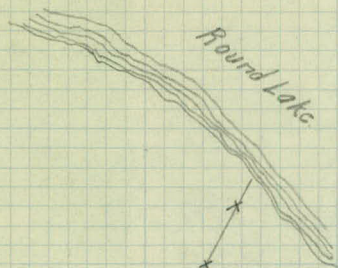
3

469.5 = Lot 1,000 #18

2

1

0400 = Nail & Red in Top of Cop. Fg. Post.



Round Lake

+15-15" Oak 21'
+09-12" Oak 21'
Fc. 13.5

Iron Fc. Post 2.45'

9.2-12" Oak

+71-15" Oak 4'

+72-15" Oak 0.5'

Rosepherry's

206'

89'

Fc. 05 23.4'

+90 Fc. 05 0.5'

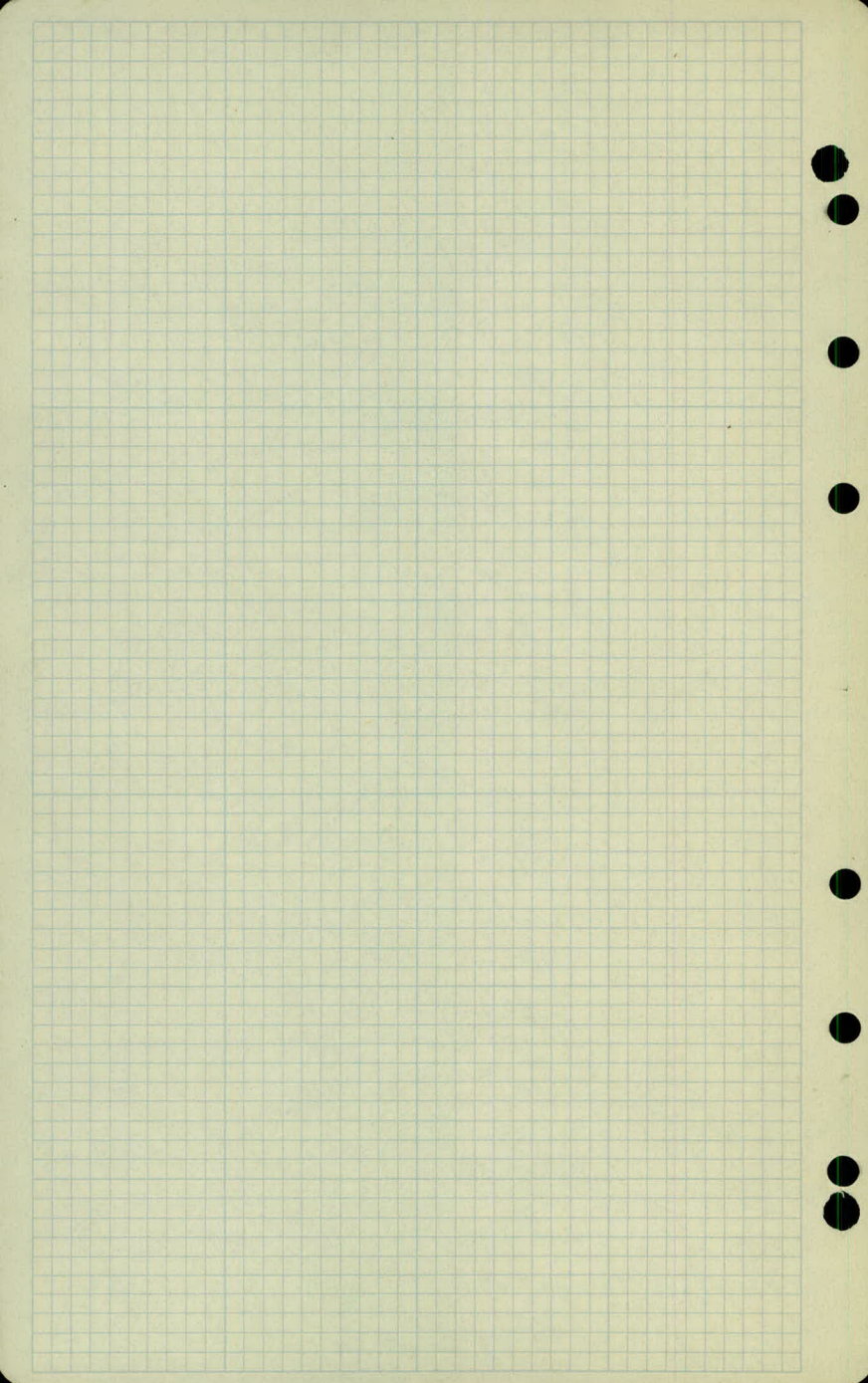
Fc. 0.5'

+25 Fc. 15'

+28 Fc. 05 0.5'

Fc. 05 0.00





X Sections

Borrow Pit Co. Rd. "G"

Approx. 500' to sta 295

Sta	+	π	-	Elev.
B.M.	2.40	935.09 ✓		931.69
I.P.	-1.21	940.51 ✓	13.37	941.72 ✓

0 +25

+70

1

+50

2

+45

I.P.	1.87	934.36 ✓	8.02	932.49 ✓
------	------	----------	------	----------

+70

3

+56

T.M.

+70

B.M.			19.3	932.43 ✓
------	--	--	------	----------

Lt.

E

Rt.

Spt in T.P.Rt Sta 2954.12

29.8	29.4	28.4
<u>10.7</u>	<u>11</u>	<u>12.1</u>
25		25

28.8	34.1	32.5	28.6	28.5
<u>11.7</u>	<u>6.9</u>	<u>8.0</u>	<u>11.9</u>	<u>12.0</u>
50	14		37	50

28.2	29.2	31.3	34.9	35.7	32.0	29.0
<u>12.3</u>	<u>11.3</u>	<u>9.2</u>	<u>5.6</u>	<u>4.8</u>	<u>8.5</u>	<u>13.5</u>
72	44	27		15	40	70

21.5	34.5	34.5	34.4	30.1	26.0
<u>13.0</u>	<u>6.0</u>	<u>4</u>	<u>6.1</u>	<u>10.9</u>	<u>14.5</u>
85	16		15	45	70

27.9	33.3	33.5	31.5	26.5	22.0
<u>12.6</u>	<u>7.2</u>	<u>7.0</u>	<u>7.0</u>	<u>14.0</u>	<u>18.5</u>
85	33		25	62	85

23.2	23.9	27.2	28.9	35.4	25.1	33.2	27.0	19.5	15.5
<u>17.9</u>	<u>16.6</u>	<u>13.3</u>	<u>11.6</u>	<u>5.1</u>	<u>5.4</u>	<u>7.3</u>	<u>13.5</u>	<u>21.0</u>	<u>25.0</u>
218	200	119	95	23		15	42	89	95

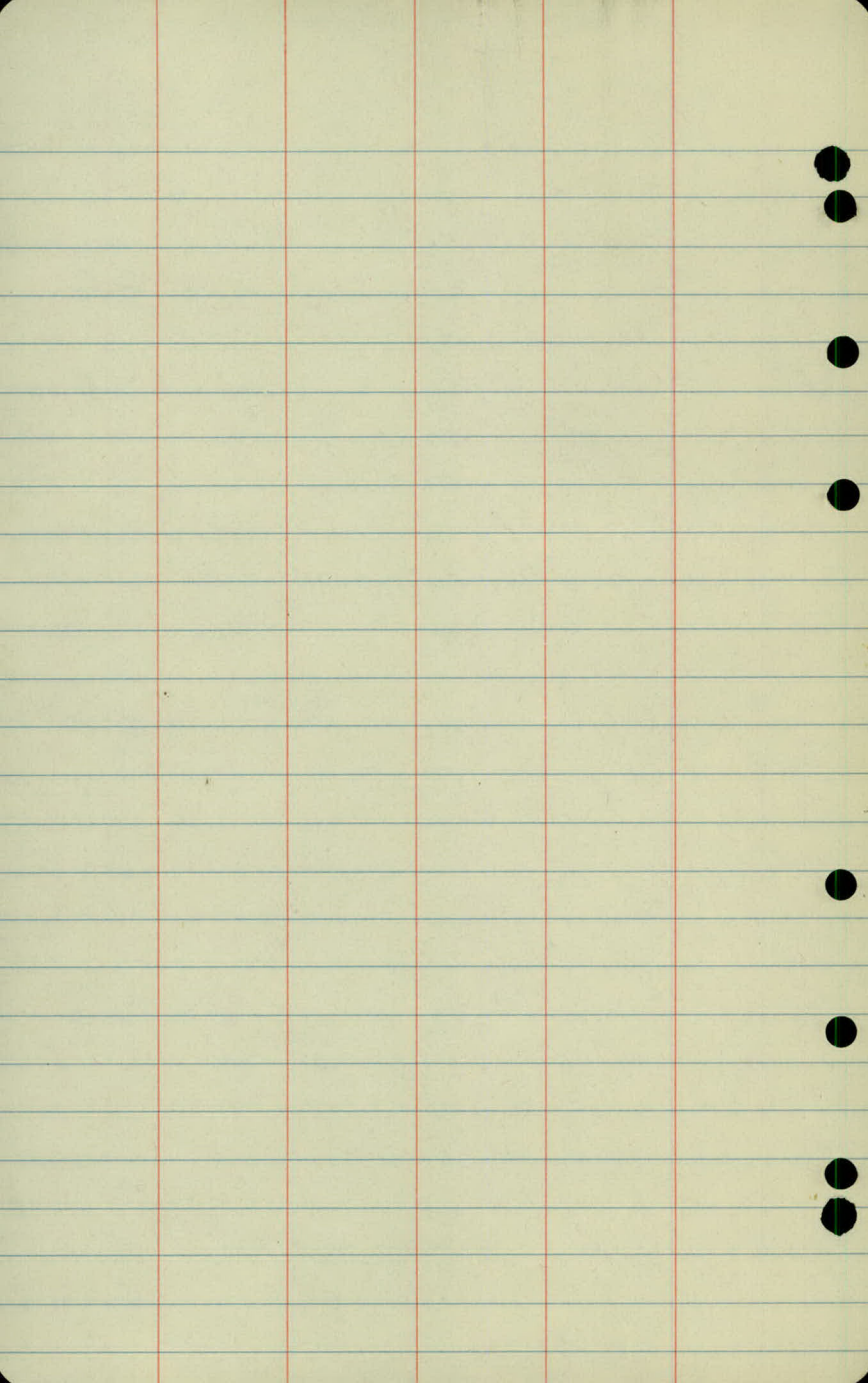
22.2	23.0	24.1	27.6	29.1	32.0	33.7	32.0	29.8	25.4	20.9	15.4
<u>12.2</u>	<u>11.9</u>	<u>5.9</u>	<u>6.8</u>	<u>5.3</u>	<u>1.4</u>	<u>0.7</u>	<u>2.4</u>	<u>4.6</u>	<u>9.0</u>	<u>13.5</u>	<u>19.0</u>
209	200	165	118	100	40	18		15	40	72	88

19.4	22.6	25.3	27.7	29.5	28.7	27.0	25.8	22.1	16.7
<u>15.0</u>	<u>11.8</u>	<u>9.1</u>	<u>6.7</u>	<u>4.9</u>	<u>5.7</u>	<u>7.4</u>	<u>8.6</u>	<u>12.3</u>	<u>17.7</u>
210	200	175	160	58	21		17	55	76

15.4	19.6	22.4	22.9	23.8	23.2	21.6	18.2
<u>19.0</u>	<u>14.8</u>	<u>12.0</u>	<u>16.5</u>	<u>10.6</u>	<u>11.2</u>	<u>12.8</u>	<u>16.2</u>
170	161	142	100	80	39		13

19.4	20.8	17.6
<u>15.0</u>	<u>13.6</u>	<u>16.8</u>
100	40	25

Top Let Iron #18 Sta 69.5



BORROW PIT SURVEY

Co. Rd. "C" at Bridge

Alignment

&
Topog.

Dec 25, 1928

Private Index

INDEX.

Align- P. 1

Prop Line - 2

X Sections
Co Rd "C" 3-4

Borrow Pit
X Sections 5-8

Not
used.
A.P.C.
3-8-38

6

5

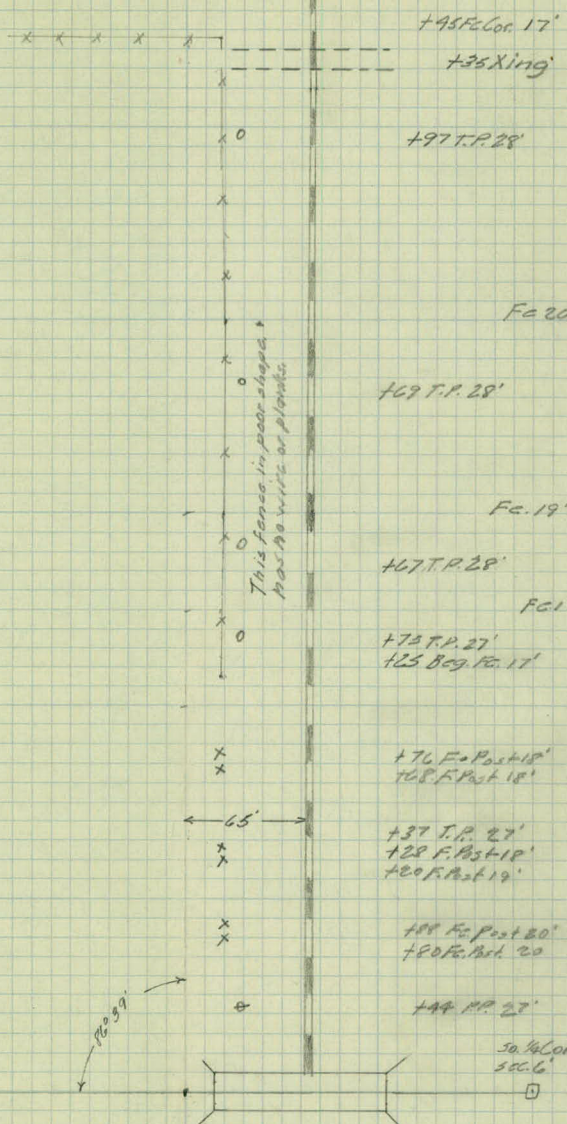
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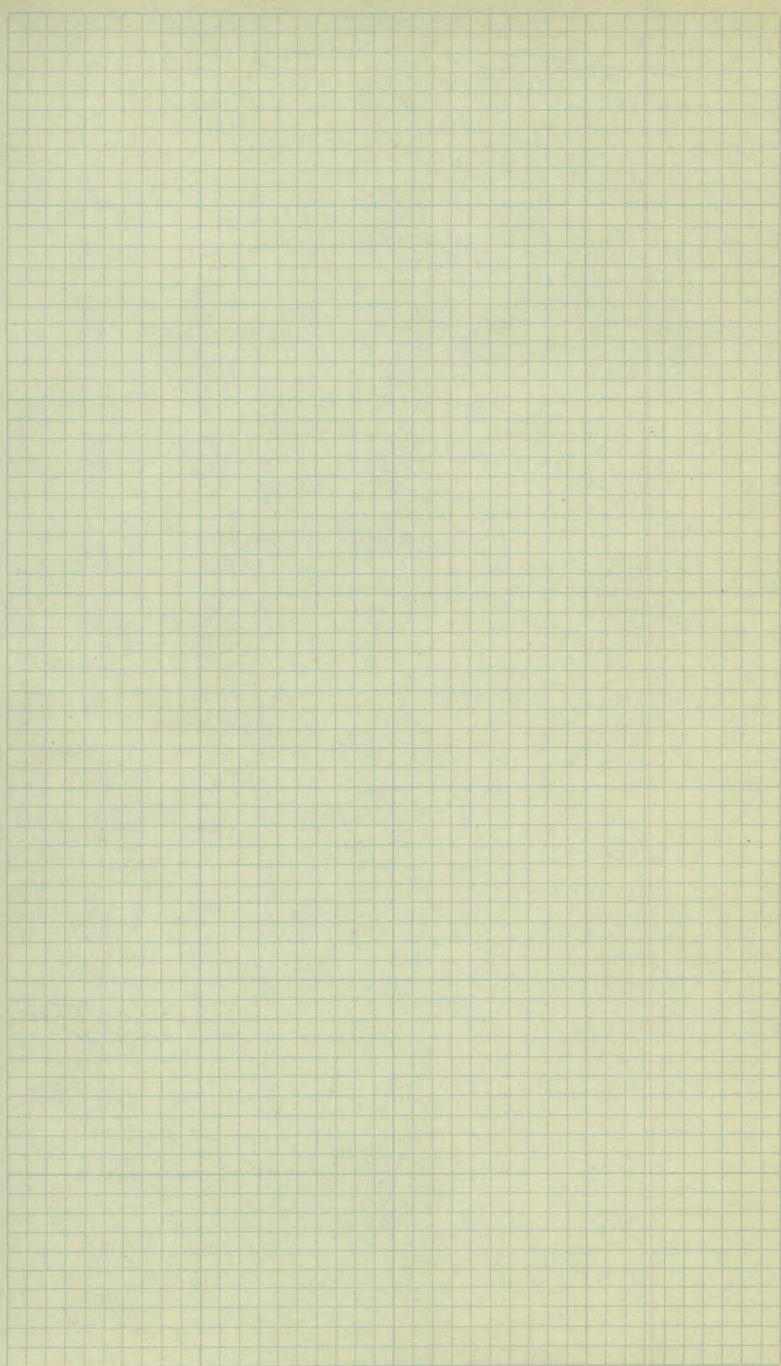
3

2

1

0+00 = & Co. Rd. "C" sta. 300+27.37





Round Lake.

Found Old Iron

25° 44'
← M605.

108.78 M

Found Old Iron

Fe Cor. = 00 to Borrow Pit.

45 M

177.81 ft.

177.81 ft.

37'

Pl. Iron

2.08'

Pl. Iron

32'
shed.946.40 = 1st floor
Elev of HO.

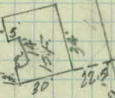
Pl. Iron

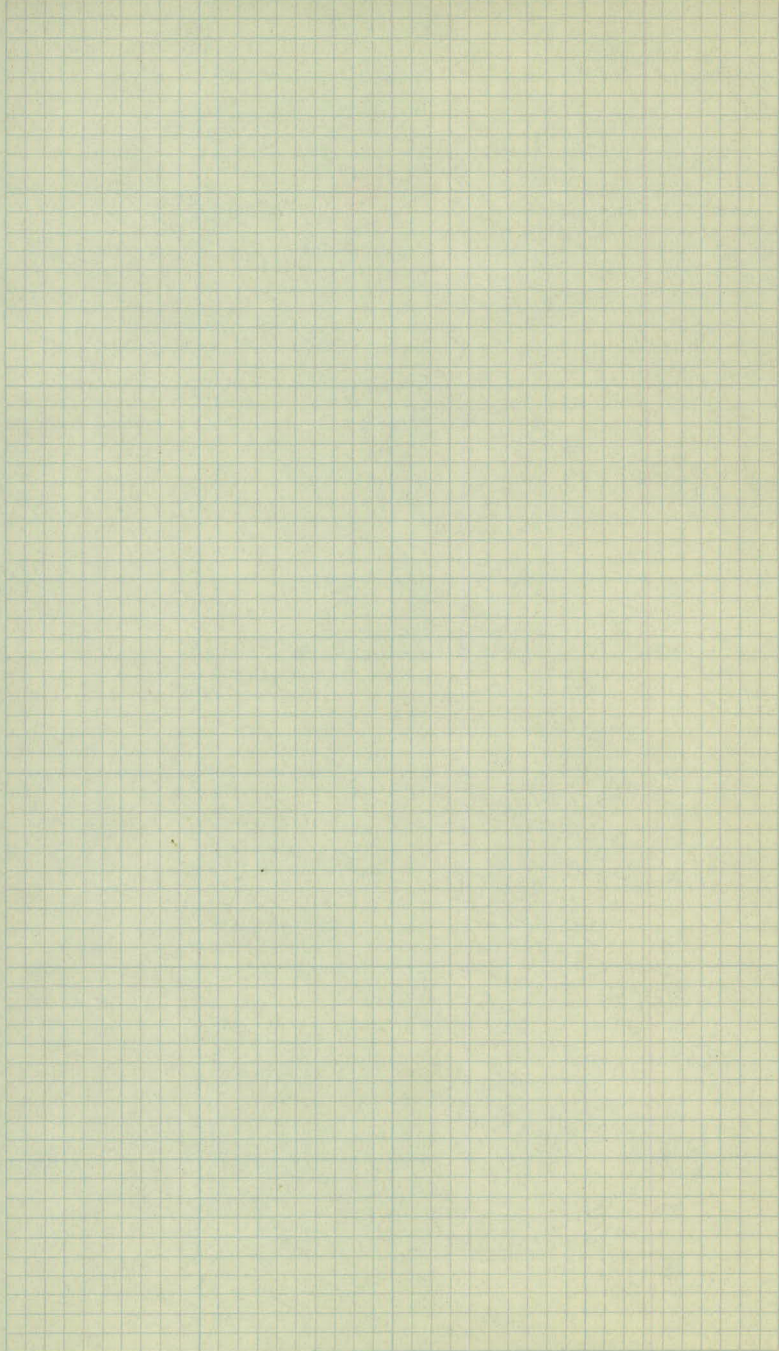
Co. Rd "C"

Pl. Iron

554.89'

298472.73'

50 1/2 Cor
500.6'



X section 3

Co. Rd. "C"

298+70 to Bridge

Sta	+	Δ	-	Elev
B. 17	11.80	752.99		940.69

298 + 70

299

+50

300

+48 = West End of Bridge

Lt.

E

Rt.

Top Mont 302+19.62

Summers	+0.4	0.0	48
Hours		20	34

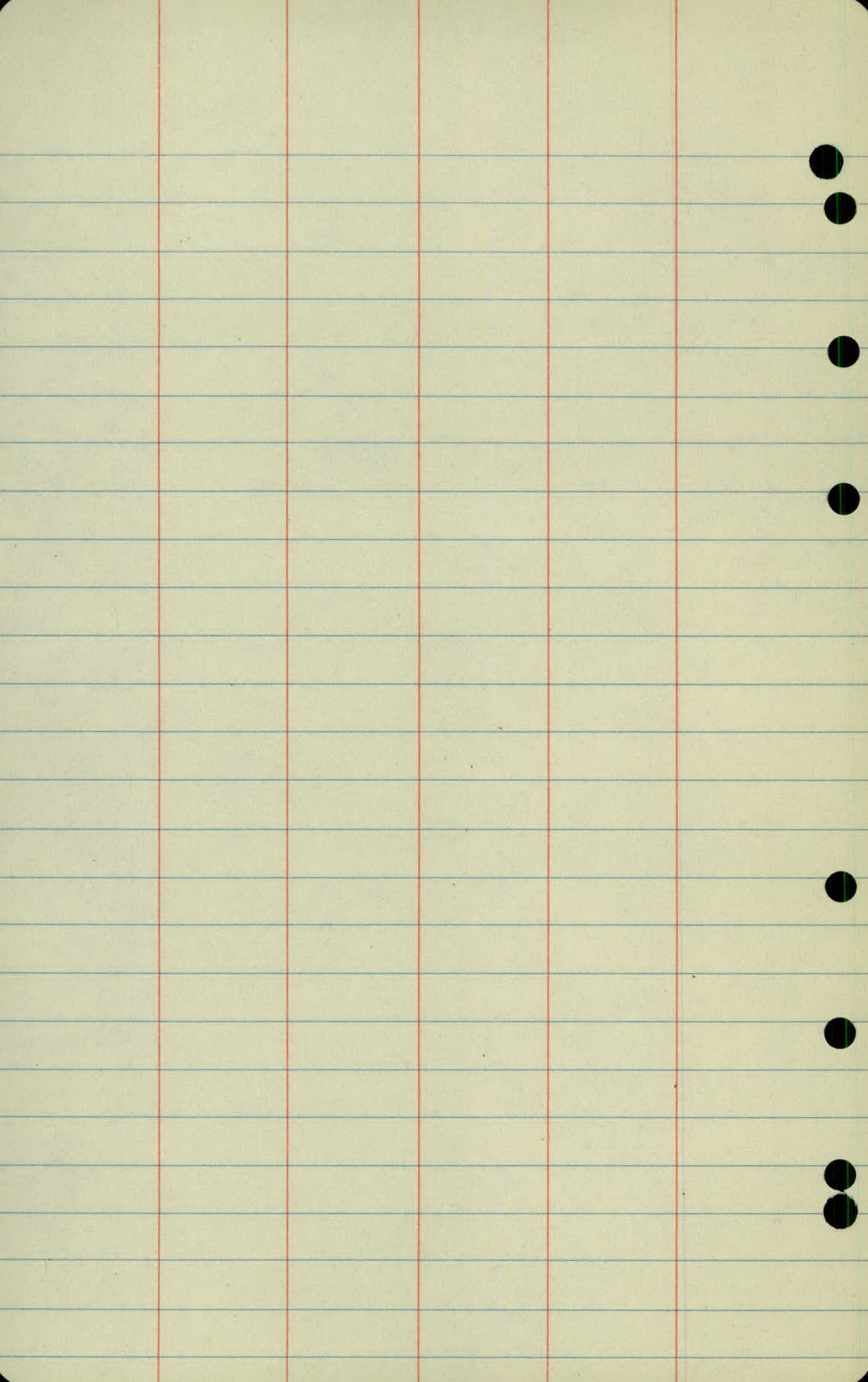
44	12	08	13	74
33	23		18	37

13	22	18	29	78
30	20		20	38

64	27	26	34	90
30	21		18	36

954.60 = Elev. W. End Bridge.

951.95 = Elev. E. End Bridge.



BORROW PIT

X Sections

Sto	+	T	-	Elev
B.M.	11.80	952.99		940.69

0+00				49.8
------	--	--	--	------

+22				49.2
-----	--	--	--	------

+25				46.7
-----	--	--	--	------

+46				45.7
-----	--	--	--	------

T.P	4.07	950.97	3.59	946.90
-----	------	--------	------	--------

1				46.0
---	--	--	--	------

+50				46.7
-----	--	--	--	------

2				44.3
---	--	--	--	------

+25				43.4
-----	--	--	--	------

B.M.	1.47	948.57		946.90
------	------	--------	--	--------

+50				42.3
-----	--	--	--	------

+75				41.2
-----	--	--	--	------

3				38.7
---	--	--	--	------

Lt

E

Rt

Top Mont. sta 302+

954.60 = Elev. W. End Bridge

27

951.95 = Elev. E. End Bridge

33

$\frac{3.3}{168}$	$\frac{4.3}{150}$	$\frac{5.0}{100}$	$\frac{5.0}{50}$	$\frac{6.4}{14}$	$\frac{5.8}{-}$	$\frac{7.7}{26}$
-------------------	-------------------	-------------------	------------------	------------------	-----------------	------------------

$\frac{3.9}{165}$	$\frac{4.5}{150}$	$\frac{5.3}{125}$	$\frac{5.1}{100}$	$\frac{3.2}{70}$	$\frac{3.7}{50}$	$\frac{6.2}{13}$	$\frac{4.8}{-}$	$\frac{8.4}{32}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------

Nail in T.P.

$\frac{2.3}{173}$	$\frac{3.8}{150}$	$\frac{5.3}{123}$	$\frac{5.2}{100}$	$\frac{4.0}{75}$	$\frac{3.9}{50}$	$\frac{5.0}{-}$	$\frac{5.0}{10}$	$\frac{7.1}{31}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	-----------------	------------------	------------------

$\frac{0.7}{182}$	$\frac{1.8}{163}$	$\frac{3.5}{150}$	$\frac{4.2}{135}$	$\frac{6.0}{117}$	$\frac{6.0}{84}$	$\frac{6.0}{50}$	$\frac{5.7}{35}$	$\frac{4.3}{-}$	$\frac{3.8}{7}$	$\frac{5.2}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	-----------------	------------------

$\frac{1.8}{193}$	$\frac{4.1}{176}$	$\frac{3.2}{150}$	$\frac{4.8}{121}$	$\frac{3.8}{89}$	$\frac{5.0}{50}$	$\frac{5.6}{25}$	$\frac{6.7}{-}$	$\frac{6.0}{11}$	$\frac{5.3}{32}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------

$\frac{2.2}{198}$	$\frac{1.9}{179}$	$\frac{4.3}{150}$	$\frac{5.4}{126}$	$\frac{4.0}{100}$	$\frac{3.8}{87}$	$\frac{5.8}{50}$	$\frac{6.6}{24}$	$\frac{7.6}{-}$	$\frac{7.3}{15}$	$\frac{7.7}{35}$
-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------

Nail in T.P.

$\frac{1.6}{204}$	$\frac{2.1}{171}$	$\frac{4.3}{151}$	$\frac{4.4}{116}$	$\frac{3.5}{90}$	$\frac{3.2}{61}$	$\frac{5.0}{12}$	$\frac{6.1}{-}$	$\frac{7.1}{20}$	$\frac{7.6}{38}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------

$\frac{4.4}{209}$	$\frac{6.2}{148}$	$\frac{7.7}{134}$	$\frac{7.7}{100}$	$\frac{6.1}{74}$	$\frac{5.3}{61}$	$\frac{5.6}{14}$	$\frac{7.2}{-}$	$\frac{8.2}{10}$	$\frac{9.7}{37}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	------------------

$\frac{6.6}{214}$	$\frac{7.7}{200}$	$\frac{8.4}{163}$	$\frac{11.5}{133}$	$\frac{11.3}{100}$	$\frac{9.4}{83}$	$\frac{7.8}{51}$	$\frac{8.7}{70}$	$\frac{9.7}{-}$	$\frac{10.9}{11}$	$\frac{12.2}{43}$
-------------------	-------------------	-------------------	--------------------	--------------------	------------------	------------------	------------------	-----------------	-------------------	-------------------

Sta	+	T	-	Elev
		984.37		
T.P.	-0.14	936.60	11.63	936.74
3	+90			31.9
	+80			29.9
4				30.0
	+90			31.4
5				24.2
	+50			21.6
6				20.6
	+32 = E Xing			22.2
T.P.	3.84	939.99	6.45	930.15
0	+35			46.7
	+46			45.7
1				46.0

Lt.

R

Rt.

$$\begin{array}{r} 12.0 \\ 325 \end{array} \quad \begin{array}{r} 34 \\ 194 \end{array} \quad \begin{array}{r} 16 \\ 165 \end{array} \quad \begin{array}{r} 54 \\ 134 \end{array} \quad \begin{array}{r} 48 \\ 100 \end{array} \quad \begin{array}{r} 23 \\ 53 \end{array} \quad \begin{array}{r} 34 \\ 17 \end{array} \quad \begin{array}{r} 47 \\ 7 \end{array} \quad \begin{array}{r} 49 \\ 37 \end{array} \quad \begin{array}{r} 59 \\ 41 \end{array} \quad \begin{array}{r} 49 \\ 48 \end{array} \quad \begin{array}{r} 53 \\ 54 \end{array} \quad \begin{array}{r} 94 \\ 60 \end{array} \quad \begin{array}{r} 79 \\ 60 \end{array}$$

$$\begin{array}{r} 2.6 \\ 230 \end{array} \quad \begin{array}{r} 8.5 \\ 193 \end{array} \quad \begin{array}{r} 7.7 \\ 179 \end{array} \quad \begin{array}{r} 8.3 \\ 137 \end{array} \quad \begin{array}{r} 4.8 \\ 100 \end{array} \quad \begin{array}{r} 3.1 \\ 86 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 26 \end{array} \quad \begin{array}{r} 6.7 \\ 10 \end{array} \quad \begin{array}{r} 7.3 \\ 39 \end{array} \quad \begin{array}{r} 7.7 \\ 42 \end{array} \quad \begin{array}{r} 6.8 \\ 49 \end{array} \quad \begin{array}{r} 7.2 \\ 54 \end{array} \quad \begin{array}{r} 9.3 \\ 60 \end{array} \quad \begin{array}{r} 8.1 \\ 60 \end{array}$$

$$\begin{array}{r} 5.9 \\ 235 \end{array} \quad \begin{array}{r} 10.9 \\ 194 \end{array} \quad \begin{array}{r} 10.2 \\ 175 \end{array} \quad \begin{array}{r} 10.8 \\ 152 \end{array} \quad \begin{array}{r} 9.1 \\ 129 \end{array} \quad \begin{array}{r} 4.7 \\ 83 \end{array} \quad \begin{array}{r} 4.0 \\ 46 \end{array} \quad \begin{array}{r} 5.3 \\ 25 \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 7.2 \\ 30 \end{array} \quad \begin{array}{r} 7.5 \\ 40 \end{array} \quad \begin{array}{r} 7.6 \\ 44 \end{array} \quad \begin{array}{r} 6.5 \\ 49 \end{array} \quad \begin{array}{r} 7.0 \\ 54 \end{array} \quad \begin{array}{r} 9.4 \\ 60 \end{array} \quad \begin{array}{r} 8.2 \\ 60 \end{array}$$

$$\begin{array}{r} 10.7 \\ 242 \end{array} \quad \begin{array}{r} 15.9 \\ 195 \end{array} \quad \begin{array}{r} 14.6 \\ 144 \end{array} \quad \begin{array}{r} 11.5 \\ 100 \end{array} \quad \begin{array}{r} 10.0 \\ 83 \end{array} \quad \begin{array}{r} 6.8 \\ 21 \end{array} \quad \begin{array}{r} 5.2 \\ 27 \end{array} \quad \begin{array}{r} 4.8 \\ 37 \end{array} \quad \begin{array}{r} 4.9 \\ 47 \end{array} \quad \begin{array}{r} 4.9 \\ 53 \end{array} \quad \begin{array}{r} 9.6 \\ 53 \end{array} \quad \begin{array}{r} 8.2 \\ 60 \end{array}$$

$$\begin{array}{r} 17.8 \\ 100 \end{array} \quad \begin{array}{r} 15.2 \\ 48 \end{array} \quad \begin{array}{r} 13.8 \\ 25 \end{array} \quad \begin{array}{r} 13.2 \\ 10 \end{array} \quad \begin{array}{r} 12.9 \\ 13 \end{array} \quad \begin{array}{r} 11.4 \\ 40 \end{array} \quad \begin{array}{r} 10.1 \\ 47 \end{array} \quad \begin{array}{r} 8.1 \\ 54 \end{array} \quad \begin{array}{r} 9.9 \\ 60 \end{array} \quad \begin{array}{r} 8.3 \\ 60 \end{array}$$

$$\begin{array}{r} 21.8 \\ 100 \end{array} \quad \begin{array}{r} 18.4 \\ 45 \end{array} \quad \begin{array}{r} 17.5 \\ 27 \end{array} \quad \begin{array}{r} 15.0 \\ 16 \end{array} \quad \begin{array}{r} 13.6 \\ 39 \end{array} \quad \begin{array}{r} 12.8 \\ 53 \end{array} \quad \begin{array}{r} 10.1 \\ 60 \end{array} \quad \begin{array}{r} 8.5 \\ 60 \end{array}$$

$$\begin{array}{r} 5.5 \\ 51 \end{array} \quad \begin{array}{r} 19.8 \\ 6 \end{array} \quad \begin{array}{r} 17.2 \\ 6 \end{array} \quad \begin{array}{r} 14.0 \\ 10 \end{array} \quad \begin{array}{r} 14.7 \\ 15 \end{array} \quad \begin{array}{r} 13.6 \\ 48 \end{array} \quad \begin{array}{r} 12.8 \\ 54 \end{array} \quad \begin{array}{r} 9.6 \\ 54 \end{array} \quad \begin{array}{r} 8.6 \\ 60 \end{array}$$

T.Rail

$$\begin{array}{r} 19.6 \\ 46 \end{array} \quad \begin{array}{r} 14.4 \\ 18 \end{array} \quad \begin{array}{r} 12.9 \\ 53 \end{array} \quad \begin{array}{r} 8.5 \\ 53 \end{array} \quad \begin{array}{r} 7.95 \\ 62.5 \end{array}$$

Top Rail Rt 4400

$$+ \textcircled{12.7} \quad \begin{array}{r} 5.4 \\ 56 \end{array} \quad \begin{array}{r} 4.8 \\ 60 \end{array} \quad \begin{array}{r} 4.89 \\ \text{Top Rail} \end{array}$$

$$+ \textcircled{11.7} \quad \begin{array}{r} 5.4 \\ 54 \end{array} \quad \begin{array}{r} 5.5 \\ 58 \end{array} \quad \begin{array}{r} 4.9 \\ 60 \end{array}$$

$$+ \textcircled{12.0} \quad \begin{array}{r} 5.4 \\ 53 \end{array} \quad \begin{array}{r} 5.7 \\ 56 \end{array} \quad \begin{array}{r} 4.9 \\ 60 \end{array}$$

833.99

1 +50

46.7.

2

44.3.

+25

43.4.

+50

42.3.

+75

41.2.

3

38.7.

$$+ \textcircled{12.7} \begin{array}{r} 4.5 \\ 50 \end{array} \begin{array}{r} 5.6 \\ 56 \end{array} \begin{array}{r} 4.9 \\ 60 \end{array}$$

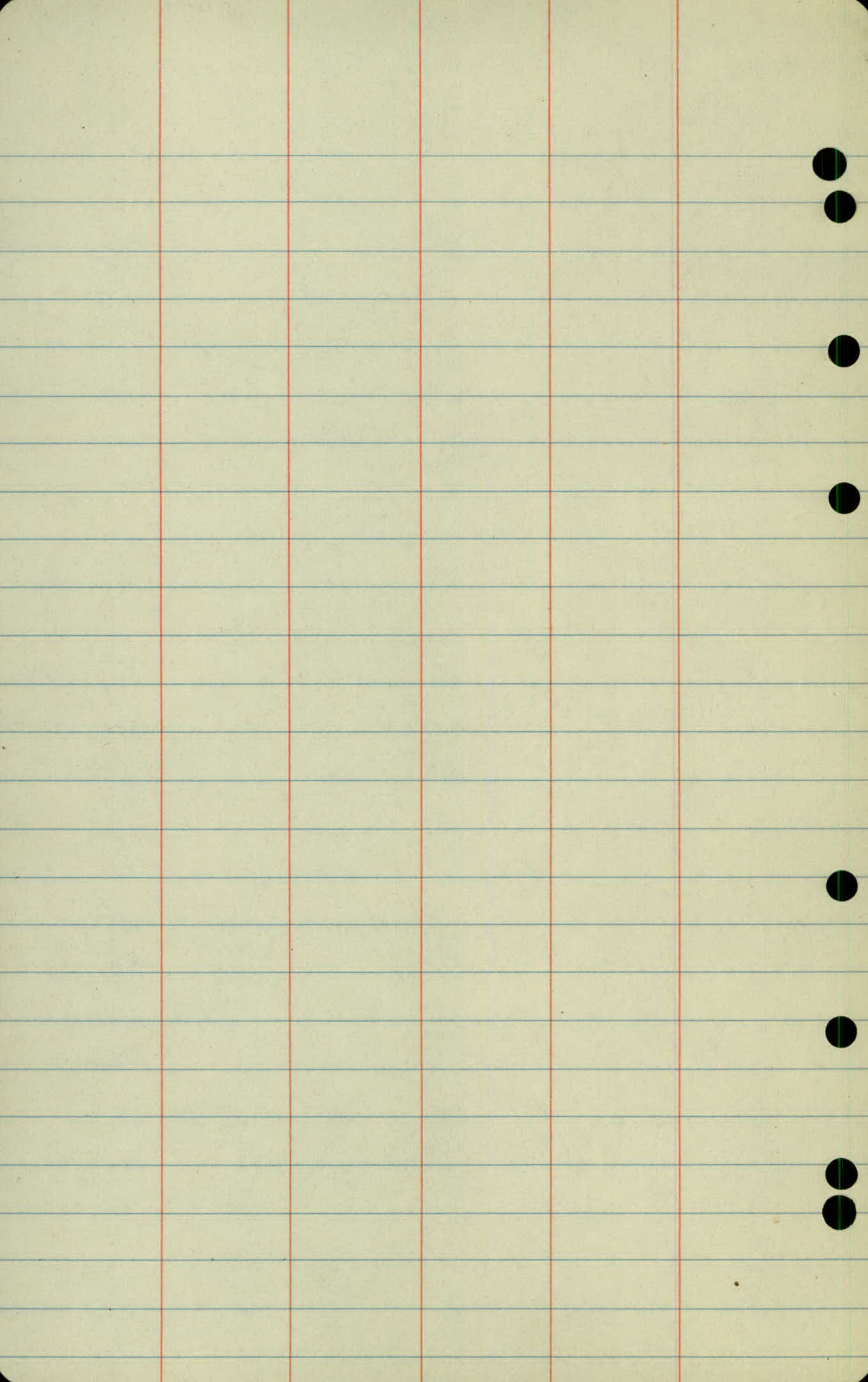
$$+ \textcircled{10.3} \begin{array}{r} 2.3 \\ 46 \end{array} \begin{array}{r} 5.5 \\ 57 \end{array} \begin{array}{r} 5.1 \\ 60 \end{array} \begin{array}{r} 4.43 \\ \text{Top Rail} \end{array}$$

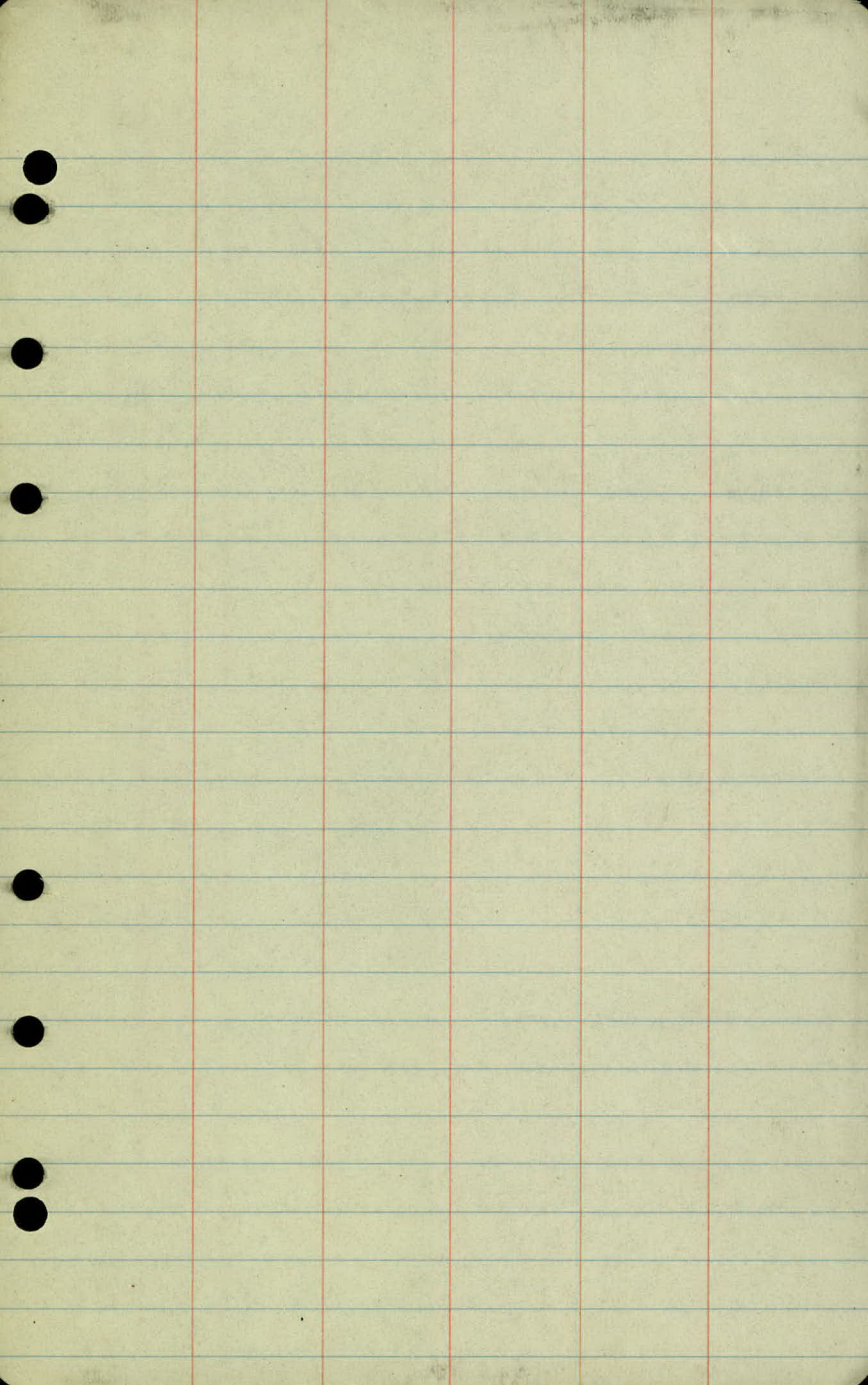
$$+ \textcircled{9.4} \begin{array}{r} 0.9 \\ 45 \end{array} \begin{array}{r} 5.6 \\ 57 \end{array} \begin{array}{r} 5.1 \\ 60 \end{array}$$

$$+ \textcircled{8.3} \begin{array}{r} 10.8 \\ 44 \end{array} \begin{array}{r} 2.5 \\ 49 \end{array} \begin{array}{r} 5.7 \\ 57 \end{array} \begin{array}{r} 5.2 \\ 60 \end{array}$$

$$+ \textcircled{7.2} \begin{array}{r} 1.9 \\ 74 \end{array} \begin{array}{r} 3.6 \\ 50 \end{array} \begin{array}{r} 5.7 \\ 58 \end{array} \begin{array}{r} 5.3 \\ 60 \end{array}$$

$$+ \textcircled{11.7} \begin{array}{r} 6.4 \\ 53 \end{array} \begin{array}{r} 6.1 \\ 57 \end{array} \begin{array}{r} 5.5 \\ 60 \end{array} \begin{array}{r} 4.63 \\ \text{Top Rail} \end{array}$$





B.M. 925.71 Co Rd "C" & N.B. Rd.
Top Mont

B.M. 927.05 Co Rd "D"

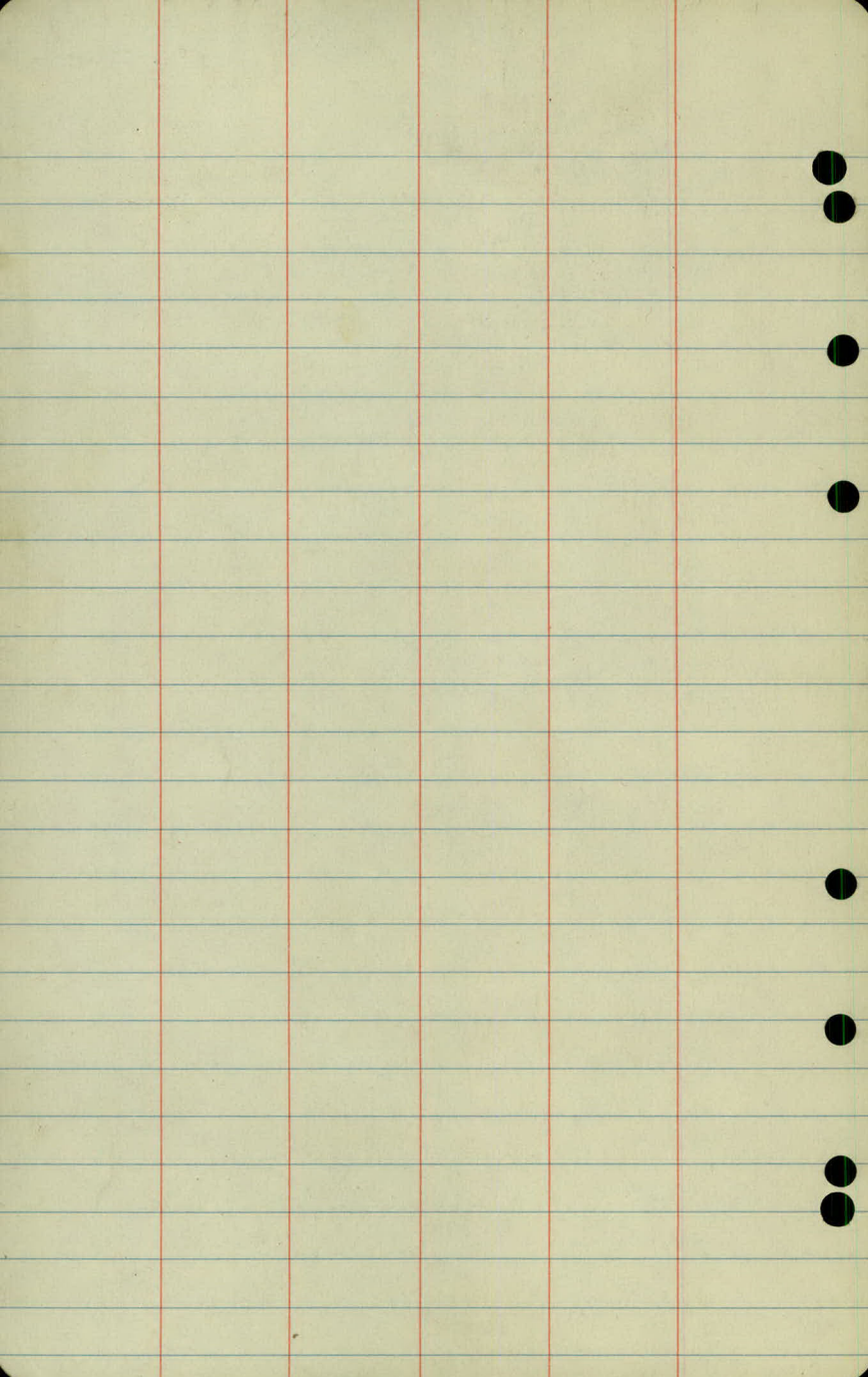
R.R. 77°13' N.E. 32+45.51
32+45.51 R Track.

68.
B. 925.71
Top

17

£

121



Co. Rd. E"

Barrow Pit #1

Slope Stakes.

Sta	+	↑	-	Grade.
B.M.	13.07	953.76		940.69
I.P.	3.84	957.23	0.37	953.39
B.M.	1.33	953.00	3.56	951.67

292 943.00

+50 43.5

293 94.0

+50 44.5

294 95.0

+50 45.5

295 951.67

295 46.0

3.83 957.50

+50 46.5

296 47.0

+50 47.5

Lt.

4

Top Mart

skin P.P.

8.0

$$\begin{array}{r} 9.0 \\ 9.1 \\ +0.0/60.1 \\ \hline 4.8 \end{array}$$

7.5

$$\begin{array}{r} 9.5 \\ 9.3 \\ +0.2/0 \\ \hline 3.7 \end{array}$$

7.0

$$\begin{array}{r} 12.2 \\ 12.4 \\ +0.0/20 \\ \hline 12.0 \\ 11.2 \\ +0.8/0 \\ \hline 11.0 \\ 9.9 \\ +1.1/0 \\ \hline 10.0 \\ 8.3 \\ +1.7/0 \\ \hline 9.0 \\ 5.8 \\ +3.2/0 \\ \hline 8.9 \\ 2.9 \\ +2.9/50 \\ \hline 2.7 \end{array}$$

11.0

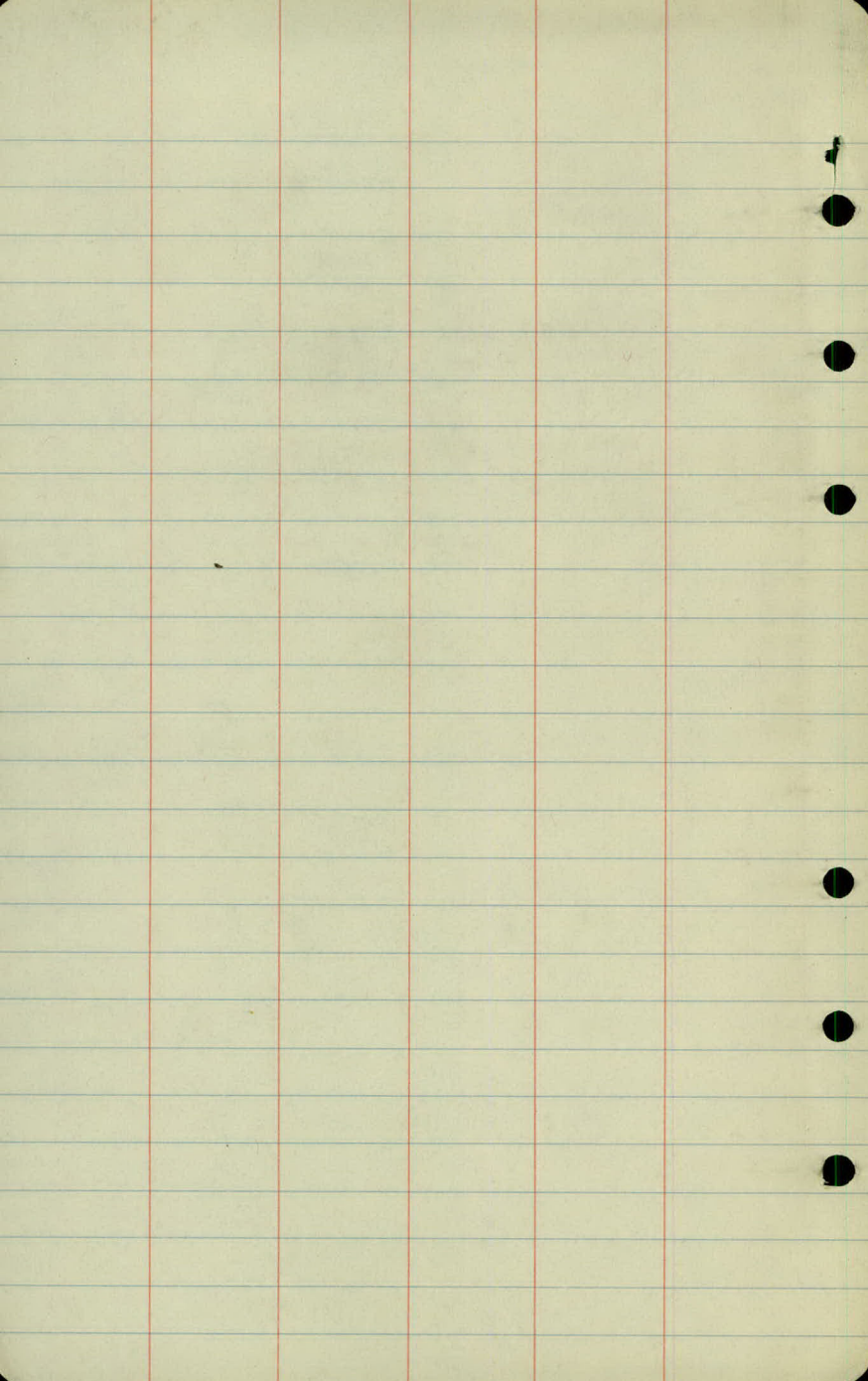
$$\begin{array}{r} 18.0 \\ 18.5 \\ +0.0/0 \\ \hline 17.0 \\ 15.8 \\ +1.2/0 \\ \hline 16.0 \\ 13.0 \\ +2.2/0 \\ \hline 15.0 \\ 10.5 \\ +4.5/0 \\ \hline 14.0 \\ 6.6 \\ +7.4/0 \\ \hline 13.0 \\ 5.7 \\ +7.3/0 \\ \hline 12.0 \\ 4.0 \\ +8.0/0 \\ \hline 4.1 \end{array}$$

10.5

$$\begin{array}{r} 12.6 \\ 12.6 \\ +1.0/23.4 \\ \hline 14.5 \\ 11.5 \\ +3.0/0 \\ \hline 13.5 \\ 6.4 \\ +6.9/0 \\ \hline 12.5 \\ 2.6 \\ +9.9/0 \\ \hline 11.5 \\ 1.9 \\ +9.6/0 \\ \hline 5.0 \end{array}$$

10.0

$$\begin{array}{r} 0.6 \\ 19.4 \\ +0.0/50. \\ \hline 4.0 \end{array}$$



Slope stakes

Co. Rd. "C"

Sta 296 East.

Sta.	+	-	Grade
B.M.	6.88	758.55	751.67

295			50.1
-----	--	--	------

+45			51.0
-----	--	--	------

+55			51.2
-----	--	--	------

+70			51.5
-----	--	--	------

+77			51.6
-----	--	--	------

96,			52.0
-----	--	--	------

+25			52.5
-----	--	--	------

+65			53.1
-----	--	--	------

97			53.6
----	--	--	------

+50			54.2
-----	--	--	------

98			54.6
----	--	--	------

Gr. Rod.

Lt.

£

Rt

Spk in R.P.

6.6

50

1.4

4.0

45

42

45

$\frac{55}{15} / 19.0$

Sta.	+	Δ	-	Grade
		988.55		

298	+3.5			54.8
-----	------	--	--	------

	+70			55.0
--	-----	--	--	------

299				55.1
-----	--	--	--	------

	+50			55.2
--	-----	--	--	------

	+55			55.2
--	-----	--	--	------

300				55.2
-----	--	--	--	------

	+48.64			54.8
--	--------	--	--	------

T.P	0.09	951.97	6.67	951.88
-----	------	--------	------	--------

	+62.31			54.42
--	--------	--	--	-------

B.M.			11.30	940.67
------	--	--	-------	--------

301	+21.4			52.25
-----	-------	--	--	-------

	+40.07			51.27
--	--------	--	--	-------

B.M.	6.09	946.78		940.69
------	------	--------	--	--------

	+65			49.75
--	-----	--	--	-------

Gr. Rod.

Lt.

E

Rt.

3.8

$$\frac{50}{-12}$$

$$\frac{38}{-20} / 20.0$$

3.6

$$\frac{22.0}{-2.0} / \frac{66}{-2.0}$$

$$\frac{58}{-22}$$

$$\frac{11.0}{-74} / 20.8$$

3.5

$$\frac{27.2}{-56} / \frac{71}{-56}$$

$$\frac{67}{-32}$$

$$\frac{136}{-101} / 36.2$$

3.4

$$\frac{29.4}{-67} / \frac{101}{-67}$$

$$\frac{80}{-46}$$

$$\frac{142}{-108} / 37.6$$

3.4

3.4

$$\frac{34.6}{-99} / \frac{127}{-99}$$

$$\frac{88}{-54}$$

$$\frac{159}{-125} / 41.0$$

0.0
48

$$\frac{27.0}{-35} / \frac{55}{-35}$$

$$\frac{121}{-121} / 40.2$$

Top Mount.

0.4

$$\frac{35.2}{-9.6} / \frac{10.0}{-9.6}$$

$$\frac{117}{-113} / 38.6$$

-20

$$\frac{36.2}{-10.1} / \frac{21}{-10.1}$$

$$\frac{11}{-44}$$

$$\frac{6.4}{-79} / 34.8$$

Sta.	+	π	-	Grade
		946.78		
302				47.2
	+50			43.4
B.M.	1.28	941.97		940.69
303				39.9
	+50			36.9
T.P.	1.84	933.06	10.75	931.62
304				34.2
	+30			32.8
	+			
305				30.0
	+50			28.4
306				27.2
	+50			26.2

Sr. Rod.

Lt.

R.

Rt.

$$-0.4 \quad \frac{38.6}{-88} / \frac{84}{-88} \quad -80/390 \quad \frac{4.4}{-48} \quad \frac{82}{-86} / 33.2$$

$$3.4 \quad \frac{31.0}{-10.5} / \frac{13.9}{-10.5} \quad -100/340 \quad \frac{84}{-5.0} \quad \frac{11.5}{-8.1} / 32.2 \quad -8.1/30.2$$

Top Mant.

$$2.1 \quad \frac{34.4}{-9.2} / \frac{11.5}{-9.2} \quad -72/32.4 \quad \frac{71}{-5.0} \quad \frac{12.1}{-10.0} / 36.0 \quad -10.0/34.0$$

$$6.1 \quad \frac{25.6}{-9.8} / \frac{10.2}{-9.8} \quad -43/22.1 \quad \frac{9.9}{-3.8} \quad \frac{14.1}{-8.0} / 32.0 \quad -8.0/30.0$$

$$-1.1 \quad \frac{30.4}{-7.2} / \frac{6.1}{-7.2} \quad -7.2/28.9 \quad \frac{2.6}{-3.8} \quad \frac{4.5}{-5.6} / 27.2 \quad -5.7/25.4$$

$$9.3 \quad \frac{30.2}{-7.1} / \frac{7.4}{-7.1} \quad -7.1/28.2 \quad \frac{3.4}{-3.1} \quad \frac{4.5}{-4.2} / 24.4 \quad -4.2/22.4$$

$$3.1 \quad \frac{36.2}{-3.1} / \frac{8.2}{-3.1} \quad -5.1/24.2 \quad \frac{4.8}{-1.7} \quad \frac{8.5}{-5.4} / 26.8 \quad -5.4/24.8$$

$$4.7 \quad \frac{17.6}{-0.8} / \frac{5.5}{-0.8} \quad -28/16.6 \quad \frac{5.7}{-1.0} \quad \frac{10.0}{-5.3} / 26.6 \quad -5.0/24.0$$

$$5.9 \quad \frac{33.0}{+4.4} / \frac{1.5}{+4.4} \quad \frac{6.3}{-0.4} \quad \frac{8.9}{-3.0} / 22.0 \quad -3.5/2.0$$

$$6.9 \quad \frac{33.0}{+6.6} / \frac{0.3}{+6.6} \quad \frac{6.8}{+0.1} \quad \frac{8.1}{+0.5} / 33.0$$

Sta	+	Δ	-	Grade
		993.06		
307				25.4
T.P.	2.43	928.40	7.09	925.97
+60				24.6
308				24.1
+50				23.6
309				23.2
+19.82				23.1
B.M.			7.07	921.31 921.33

Gr. Rod.

Lt

2

Rt.

7.7

$$33.0 / \frac{.08}{+.69}$$

$$\frac{7.3}{+.04}$$

$$\frac{8.2}{29.5 / 33.0}$$

2.8

$$33.0 / \frac{2.6}{+.12}$$

$$\frac{3.7}{+.01}$$

$$\frac{4.7}{21.1 / 33.0}$$

4.2

$$33.0 / \frac{3.8}{+.05}$$

$$\frac{4.2}{+.01}$$

$$\frac{4.9}{29.1 / 33.0}$$

4.8

$$33.0 / \frac{4.5}{+.03}$$

$$\frac{5.3}{+.05}$$

$$\frac{6.6}{20.2 / 33.0}$$

5.2

$$\frac{7.2}{20.0 / 33.0}$$

Total Month

