

Book - 25 - Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- Plan ----- Survey

----- COUNTY ROAD "D" -----

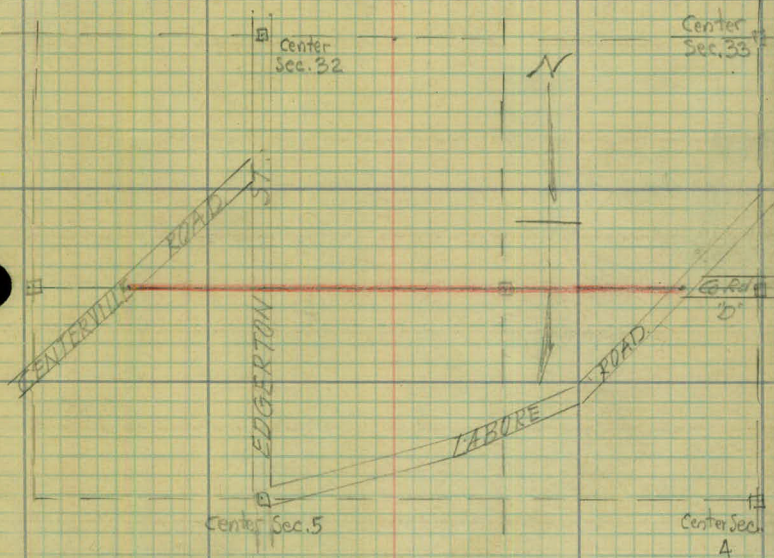
From Centerville Rd. To. Labarre Rd.

Road Acc't. No. -----

Date Filed. 1-6-36

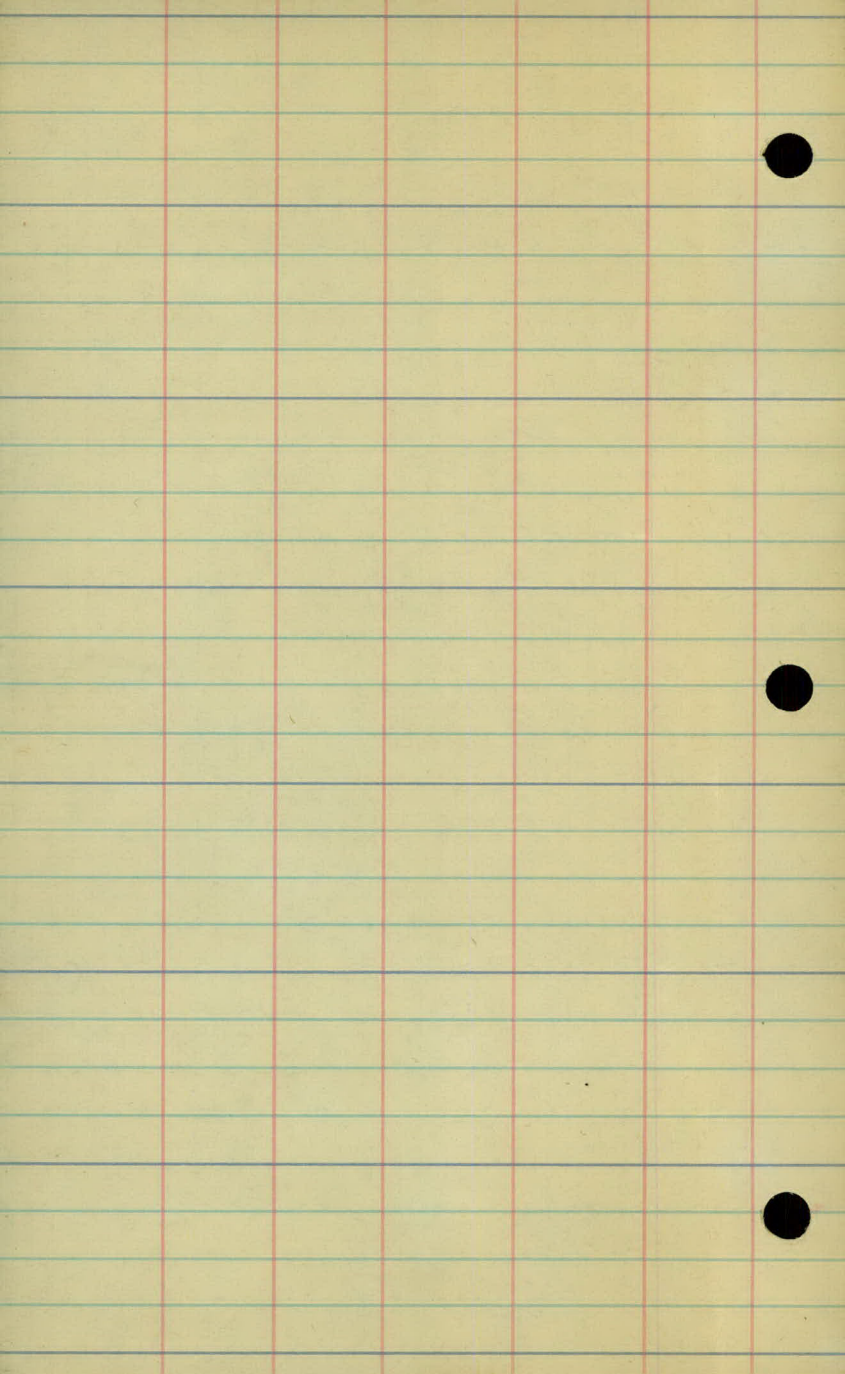
File 6

Plan Survey
County Road "D"
Centerville Rd to Labore Rd.



Index	
alignment	P1 - P4
topography	P. 5 - P. 15
Cross Sections	18 - 28
Bench Levels	16 - 17

W. A. Carlson Oct. 30, 1935



1
alignment.

Station Point Lt. ^A Et.

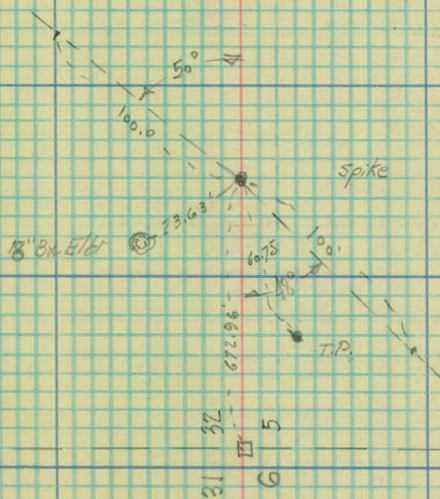
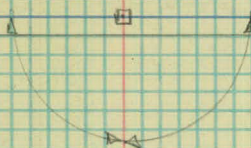
191574 Nor. 0°-09'

0700 = 2 Centerville Road

Nor.

2 Edgerton

20' One Course Conc.



Station	Point	St. ^A	Alt.
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45489.2			
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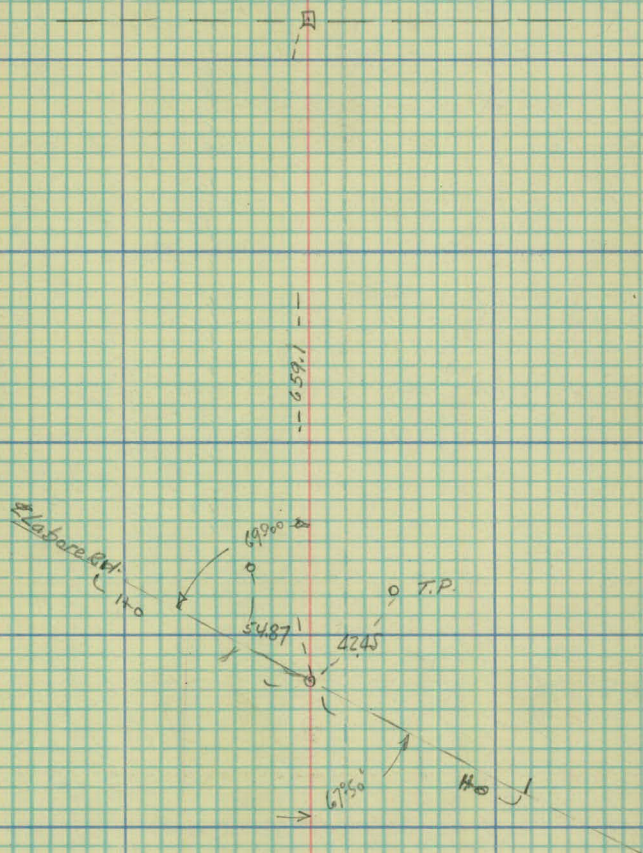
	0°04'		
--	-------	--	--

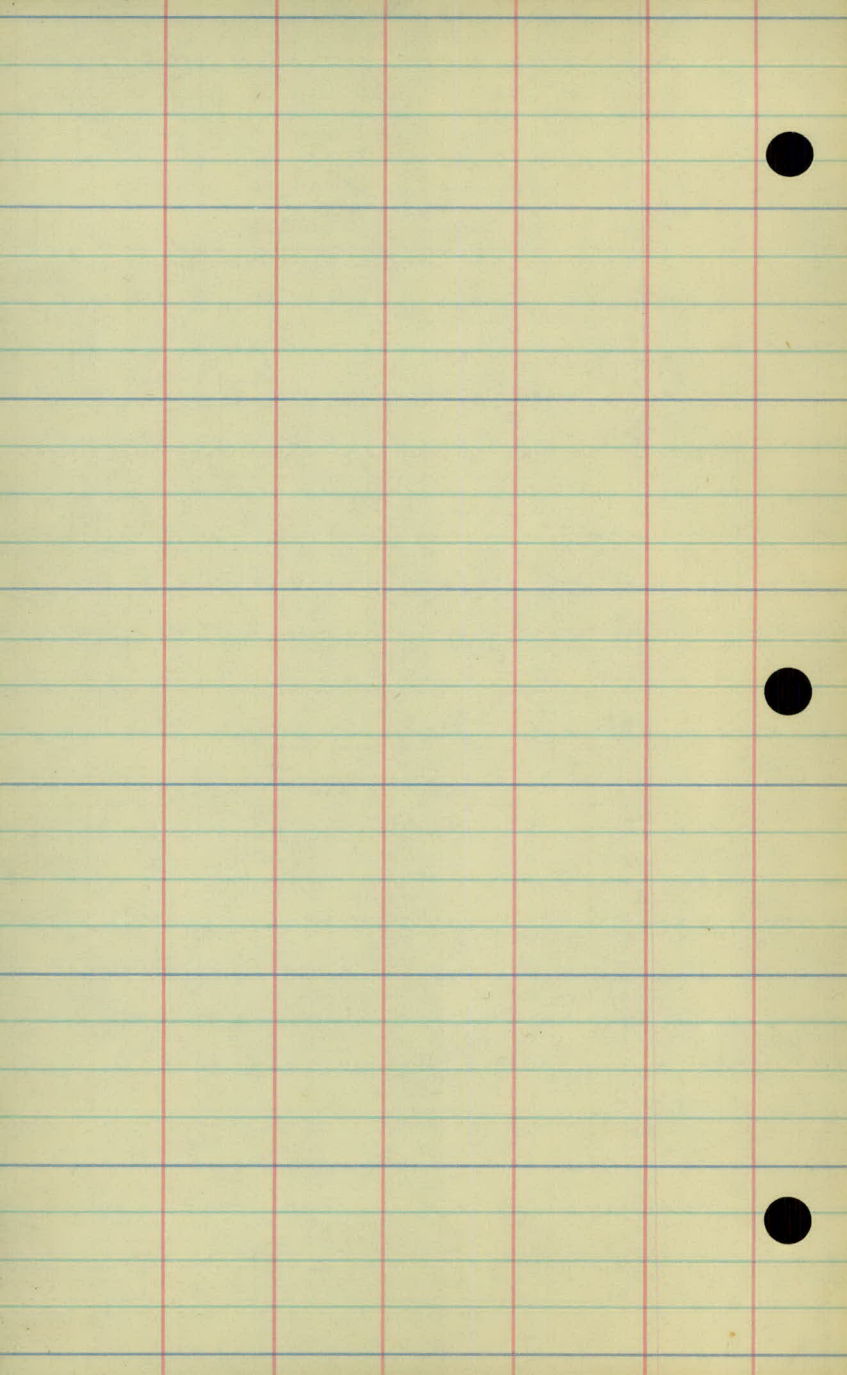
32 33
5 4

Station Point Lt. ^A Rt.

65476.32

65476.32





Topography.

3

2

1

0 to

Note: Scoop Sections
for Elev. of Ditch Bottom

+150-A in Fence 6'
+30- Beg Fence 27'

Small Trees
Thick

Hay
Wooded

Elev. 893.4

+181-Fence Cor. 1'

+137-14" W Willow 0'
+134-Ditch XS E

+107- 8" 1/2 3'

+120-2 Ditch 78'
5' Both.

Waste
Land

Cultivated.

Elev. 892.0

+38-P.P. 7'

Tarvia 165

-01145 Edge Tarvia - 0'

Gen Tarvia Beat

Back to Road

0173 - Tarvin 165
0204 - Cor. 111 1/2 of 141
0127-8" Maple 8'
0124 - Lilac 85.3'
01145-Edge Tarvia 9'
0100- 8" Maple 47'
Tarvia 165

-0112-Lilac Edge 43'

Tarvia 20' wide

10

9

8

7

6

5

4

El. 898.6

El Ditch 197

190-800 F. 4

x

x

Hay Meadow

A

Cultivated

50 A in Ditch

El. 896.0

Ditch 186-183

V

Prod.

El. 896.0

17

16

15

14

13

12

11

150-1 Ditch 123' Elev. 900.6

125-2 Ditch 192' Elev. 900.4

130-End Brush.

cultivated

Fence 0'

+67-Box Brush 5' Wide-

Hay Meadow.

+66 Fence Cor.

cultivated

Ditch 2

F-3

F-4

~~157~~ ~~Edgerton~~

24

23

22

21

20

+574 Edgerton Stone Men. Paul V. 125' lt.

6' x 5' box x 3' x 5'
conc

19



→ 6' ←

18

+57-2 Ditch - 30'

+72-4 in Ditch 0'

+72-2 6" (11, 12) 0'

2 Ditch - 130'
130'

+64 Ditch
3'

F-0

F-0'

F-0'

Meadow.

Alfalfa.

Ditch 7

E 190m

+88-T.R 0'
+91-100-Fen 0
+91-14" dak-2'

20' One Course Concrete

+24-Fence Con. 2'

Ditch 7

Meadow

Cultivated.

31

30

29

28

27

26

25

F-2'

Ken 11' Ditch-2' 10

3145-A in Ditch 261 North
Ditch then runs 20° N.E.

450-6" (D), 11-1'

F-2'

F9'- Ditch 3'

183-24" Pop 4'

F-3' F. cor.

Ditch-3'

199-F. cor. 11
114-6" (D) 11-3'

F-2'
Ditch-244'
244' (D) 11-3'

165-F. cor. 2'
190-20" Ditch @ 45°

155-20" Pop. 2'

F-2'

112-15" Pop. 4'
Ditch-4'

167-F. cor. 2'
160-E Ditch-158'

5 Pop- 6-10" Pop.

F-5'

Ditch-5'

F-4' Ditch

11-9-12" Pop in Ditch

Ditch-3'

8-4-10" Pop. in Ditch

F-4'

Ditch

Hay Meadow

Ditch

38

37

36

35

34

33

32

F-0'

Ditch-2' Fence-rv 11

+35-End Brush

F-3'

F-2'

Pop in Brush +35

F-1'

F-2'

+15-End Brush

Brush-15'
Fence 1'

Fence 1'
Brush Line 15'



Cult

Hay Meadow

Wetland

+27-F Cor. 14'
+10-12" Pop. 1'
+07-13" Pop. 4'
Fence 7' - Ditch 1'

+94-10" Pop 1'

+52-F. A 21'

+20-6" Pop-2'

F-17' - Ditch 3'
3' wide

+83-10" Elm 7'
2 4"

+36-6" Pop. 5'

Ditch-2' F-11'
+77-3-10" Elm 22'
+78-5-8" Elm -39'
+75-F Cor. 11'

Ditch-3' Fence 10'

+10-18" Pop.
Ditch-3' Fence 4'
+94-10" Pop. 3'

Ditch-2' - Fence 13'

+64-12" Will-3'

+17-2-5" Will-2'

189.2- Stone Man

45

44

43

42

41

40

39

Ditch 5'
+ 30-Ditch 6'
3' Wide

Ditch - 1'

Ditch - 0'
2' Wide

Ditch - 0
Brush - 0.0

+60-Brush-22'

Brush - 20'
+87-Ain Fenc 5'

Fences
Brush 23'

+30-Brush 20

F- 4'

Hay Meadow

Meadow

Thick Oaks

Oaks 4-12" Thick

+16-8" Oak 7 1/2

+89-F Cor 0

+65-F x Timber 9'

+44-Ditch 3' Wide
0

Fence Timber 5

Fen-Timber 9'

Fen-10'-Timber
13ru

Ditch-1'
Fence + Timber 10

+12-24" Pop 0-0

Ditch-2'

+15-F. Cor 18'
+60-18" Pop -0

+18-10" Pop 0

Ditch 2' F- 15'

+86-4" Pop -0'

+76-3" Pop. 0

Refuse

52

51

50

49

48

47

46

cultivated

F-1'

Hay Meadow.

F-0

cultivated

#43 - Shallow Ditch
From North

Ditch 3'

Drainage Ditch

Ditch 5'-3' wide

59

58

57

56

55

54

53

+50-2 4' Ditch 90'
+15-30" Pop. 12'
+20-2 4' Ditch 0'

Waste

Cult

Cult

F-1'
Oaks
+48-F. Cor. 65'
F-1-45'

+07-30" Pop. 2'
+04-F. Cor. 12'
+99-6" Pop. 34'

F-1'

F-1'

+04-8" in oaks
F-0

F-1'

+ Cult

+20-F. Cor. 1'

66

+76.32 - 2 Labore Rd.

65

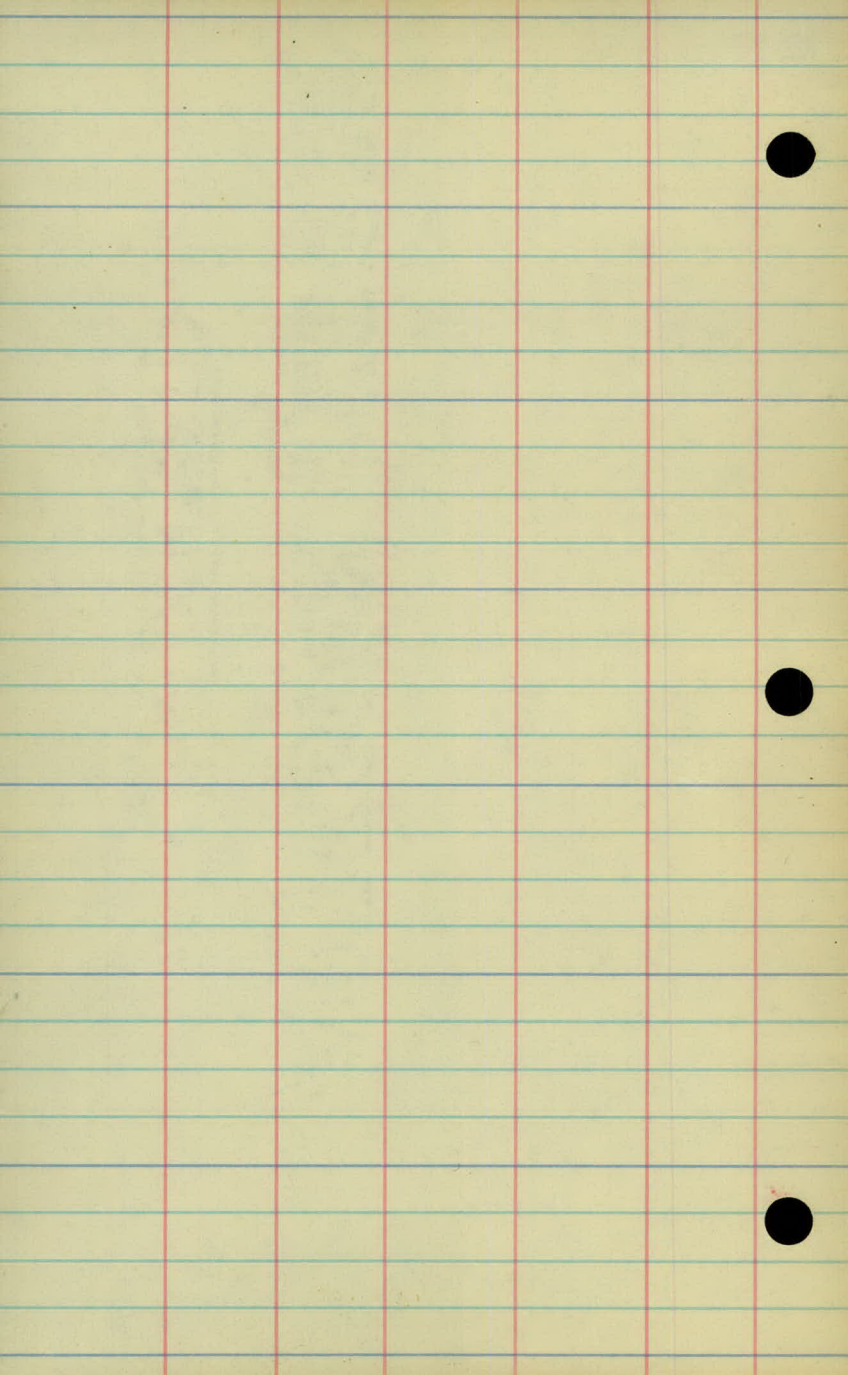
64

63

62

61

60



Bench Levels.

Co. Road "D"

T. H. # 61 - Labore Road.

B.M. 9.60 896.32 ✓ 886.72 ✓

903.55

900.49

B.M. 4.34 891.98 ✓

T.P. 13.01 909.22 ✓ 0.11 896.21 ✓

✓ 7.05 913.44 ✓ 2.83 906.39 ✓

✓ 11.12 924.42 ✓ 0.14 913.30 ✓

✓ 11.92 936.26 ✓ 0.08 924.34 ✓

✓ 9.35 945.08 ✓ 0.13 936.13 ✓

✓ 1.05 932.26 ✓ 13.27 932.21 ✓

B.M. 7.38 925.88 ✓

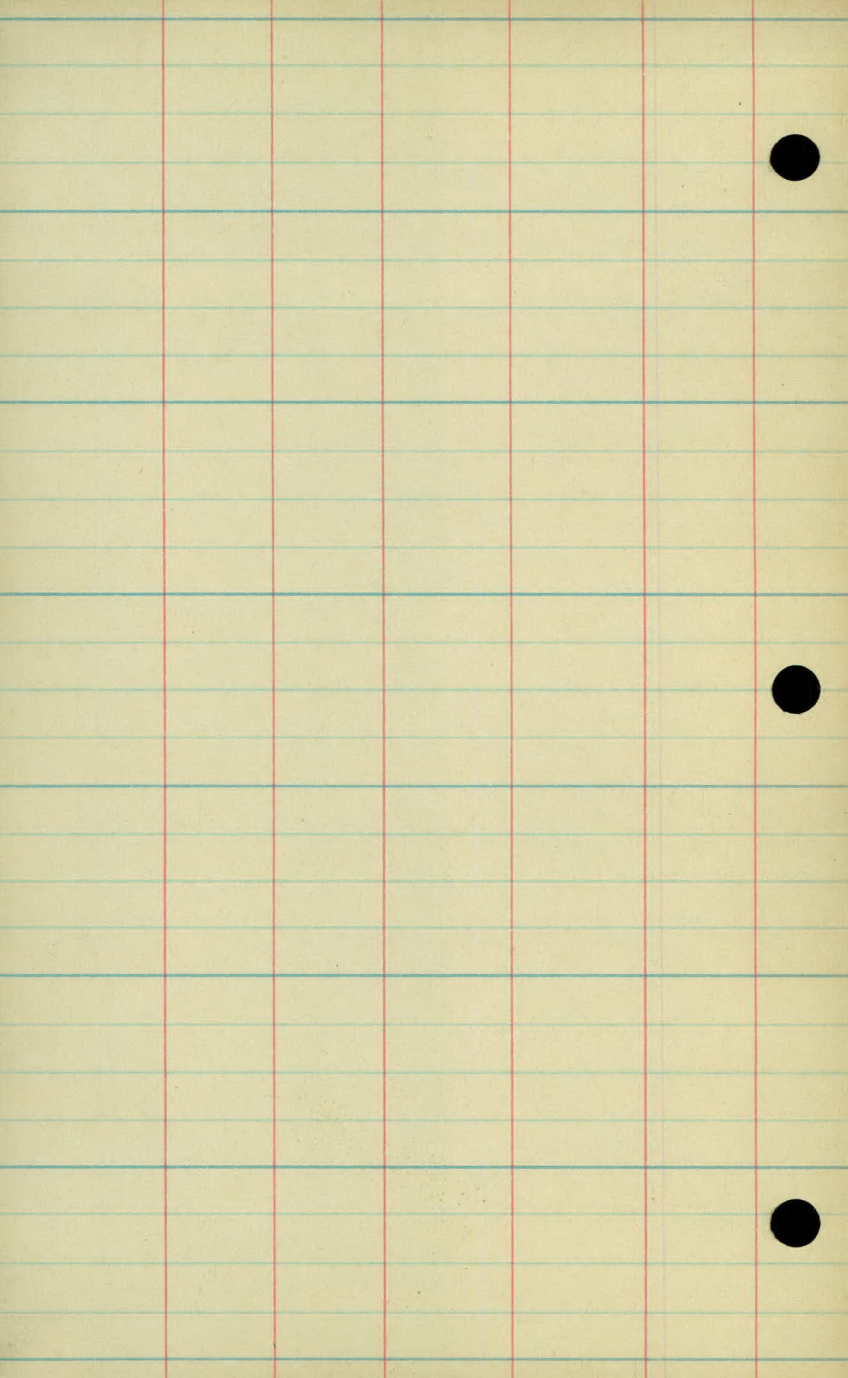
Sp in P.P. 20' Lt. Sta. 179+55 (2D = 181+75.5)

(1. in T.P. 40' Lt. Sta. 193+30)

(Sp. in P.P. 20' Lt. Sta. 174+10)

P.R. spike in T.P. N.W. cor. D" & 61 - T.P. # 7 1/2

Spike in Guy Pole W. Side Labor Road 1 Co. Rd "D"



Cross-sections.

Sta.	+	π	-	Elev.
B.M.	1.70	925.30 ✓		923.60 ✓
T.P.	2.91	921.32 ✓	6.89	918.41 ✓
✓	2.37	915.49 ✓	8.20	913.12 ✓
✓	7.25	910.40 ✓	12.34	903.15 ✓
✓	8.07	918.29 ✓	0.18	910.22 ✓
✓	2.75	916.91 ✓	4.13	914.16 ✓
✓	3.45	914.05 ✓	6.31	910.60 ✓
✓	4.31	916.14 ✓	2.22	911.83 ✓
✓	3.90	914.52 ✓	3.52	912.62 ✓
B.M.	4.34	916.52 ✓	4.34	912.18 ✓
-0+15				912.1 ✓
0+0				12.6 ✓
0+15				12.2 ✓
0+20				11.5 11.1 ✓
0+33				12.4 ✓
0+50				10.7 ✓
1+0				042 ✓
T.P.	0.76	905.90 ✓	11.38	905.14 ✓

R.R. Spike in T.P. N.E. Cor. Co. Rd. "E" & Centerville Rd.

200 Bridge

R.R. Spike in 18" Bx Edd. 20' Lt. Sta. -0 + 141

$$\begin{array}{r} 44 \\ \hline 39 \\ 17-4 \\ \hline 36 \end{array} \quad \begin{array}{r} 44 \\ \hline 5.1 \\ 44 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 5.2 \\ \hline 23 \end{array} \quad \begin{array}{r} 43 \\ \hline 16- \\ \hline 16 \end{array} \quad \begin{array}{r} 39 \\ \hline 17-4 \\ \hline 36 \end{array} \quad \begin{array}{r} 43 \\ \hline 17-4 \\ \hline 36 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 27 \end{array} \quad \begin{array}{r} 44 \\ \hline 31 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 5.2 \\ \hline 50 \end{array} \quad \begin{array}{r} 44 \\ \hline 23- \\ \hline 23 \end{array} \quad \begin{array}{r} 38 \\ \hline 17 \\ \hline 17 \end{array} \quad \begin{array}{r} 43 \\ \hline 0 \\ \hline 0 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 8 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 11 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 44 \\ \hline 45 \end{array} \quad \begin{array}{r} 39 \\ \hline 27 \\ \hline 27 \end{array} \quad \begin{array}{r} 42 \\ \hline 11 \\ \hline 11 \end{array} \quad \begin{array}{r} 50 \\ \hline 50 \end{array} \quad \begin{array}{r} 4.1 \\ \hline 5 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 43 \\ \hline 58- \\ \hline 58 \end{array} \quad \begin{array}{r} 39 \\ \hline 40 \\ \hline 40 \end{array} \quad \begin{array}{r} 42 \\ \hline 21 \\ \hline 21 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 10 \end{array} \quad \begin{array}{r} 4.1 \\ \hline 41 \end{array} \quad \begin{array}{r} 6.6 \\ \hline 27 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 4.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 36 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 58 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 21 \end{array} \quad \begin{array}{r} 10.0 \\ \hline 50 \end{array}$$

← Tarvia →

$$\begin{array}{r} 6.7 \\ \hline 50 \end{array} \quad \begin{array}{r} 8.4 \\ \hline 35 \end{array} \quad \begin{array}{r} 11.0 \\ \hline 12 \end{array} \quad \begin{array}{r} 12.3 \\ \hline 123 \end{array} \quad \begin{array}{r} 14.6 \\ \hline 30 \end{array} \quad \begin{array}{r} 16.2 \\ \hline 50 \end{array}$$

No. 1000 Reg.

Sta.	+	T	-	Elev.
		905.90 ✓		
1+50				899.9 ✓
2+0				98.1 ✓
2+20	Top Bank E			96.6 ✓
2+29	Edge Ditch E			93.4 ✓
2+40	Edge Ditch E			93.4 ✓
2+52	Top Bank E			95.4 ✓
T.P.	7.34	904.31 ✓	8.93	896.97 ✓
3+0				96.5 ✓
4+50				98.9 ✓
4+0				98.3 ✓
5+0				899.6 ✓
6+0				901.6 ✓
T.P.	8.72	910.92 ✓	2.11	902.20 ✓
7+0				903.4 ✓

4. 4. 41.

$\frac{3.0}{5.0}$	$\frac{4.1}{4.0}$	$\frac{5.0}{1.2}$	$\frac{6.0}{1.0}$	$\frac{8.0}{2.5}$	$\frac{8.2}{5.0}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

Elev in Ditch
 266.5. W. of
 2 13.9.2 892.0

$\frac{6.2}{5.0}$	$\frac{7.2}{2.1}$	$\frac{7.8}{1.0}$	$\frac{9.0 \text{ top}}{2.8 \text{ Bank}}$	$\frac{12.5}{3.9}$	$\frac{12.5}{4.4}$	$\frac{11.1 \text{ Top}}{6.6 \text{ Bank}}$
-------------------	-------------------	-------------------	--	--------------------	--------------------	---

$\frac{7.3}{5.0}$	$\frac{7.8}{2.3}$	$\frac{9.3 \text{ Top}}{1.0 \text{ Bank}}$	$\frac{12.6}{1.1}$	$\frac{12.6}{1.8}$	$\frac{12.6}{2.5} = \text{Bank}$	$\frac{10.5}{5.0}$
-------------------	-------------------	--	--------------------	--------------------	----------------------------------	--------------------

$\frac{7.4}{5.0}$	$\frac{7.8}{2.5}$	$\frac{\text{Top } 9.3}{\text{Bank } 1.9}$	$\frac{12.5}{1.0}$	$\frac{12.3}{.9}$	$\frac{10.5 \text{ top}}{1.5 \text{ Bank}}$	$\frac{10.6}{5.0}$
-------------------	-------------------	--	--------------------	-------------------	---	--------------------

$\frac{7.8}{5.0}$	$\frac{\text{Top } 8.9}{\text{Bank } 1.7}$	$\frac{12.2}{.8}$	$\frac{12.5}{1.0}$	$\frac{10.5 \text{ Top}}{.6 \text{ Bank}}$	$\frac{10.2}{5.0}$
-------------------	--	-------------------	--------------------	--	--------------------

(Note Ditch Drains South-West)

$\frac{7.8}{5.0}$	$\frac{\text{Top } 9.2}{\text{Bank } 1.8}$	$\frac{12.4}{1.5}$	$\frac{12.4}{.9}$	$\frac{10.5}{1.0 \text{ Bank}}$	$\frac{10.2}{3.0}$	$\frac{10.0}{5.0}$
-------------------	--	--------------------	-------------------	---------------------------------	--------------------	--------------------

$\frac{\text{Top } 8.5}{\text{Bank } 1.2}$	$\frac{10.6}{4.7}$	$\frac{10.6}{4.1}$	$\frac{8.6 \text{ top}}{3.5 \text{ Bank}}$	$\frac{8.0}{2.4}$	$\frac{7.8}{1.0}$	$\frac{6.6}{5.0}$
--	--------------------	--------------------	--	-------------------	-------------------	-------------------

$\frac{10.1}{7.0}$	$\frac{8.0 \text{ top}}{6.8 \text{ Bank}}$	$\frac{7.5}{5.0}$	$\frac{7.3}{2.1}$	$\frac{6.0}{1.1}$	$\frac{5.4}{1.0}$	$\frac{4.6}{5.0}$
--------------------	--	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{7.6}{5.0}$	$\frac{7.0}{2.5}$	$\frac{6.0}{1.0}$	$\frac{4.7}{5.0}$
-------------------	-------------------	-------------------	-------------------

$\frac{6.0}{5.0}$	$\frac{5.6}{2.8}$	$\frac{4.7}{5.0}$
-------------------	-------------------	-------------------

$\frac{8.3 \text{ top}}{18.6 \text{ Bank}}$	$\frac{8.3}{17.6}$	$\frac{4.4}{1.0}$	$\frac{3.8}{5.0}$	$\frac{2.7}{5.0}$
---	--------------------	-------------------	-------------------	-------------------

$\frac{9.0}{5.0}$	$\frac{8.2}{2.5}$	$\frac{7.5}{1.0}$	$\frac{6.3}{5.0}$
-------------------	-------------------	-------------------	-------------------

Place 48" Cul.

Sta.	+	π	-	Elev.
		910.92 ✓		
7+65				05.8 ✓
8+0				06.7 ✓
+40				06.5 ✓
9+0				05.9 ✓
10+0				05.7 ✓
11+0				06.0 ✓
12+0				07.2 ✓
13+0				06.6 ✓
T.D.	2.56	910.97 ✓	2.51	908.41 ✓
14+0				08.2 ✓
+65				07.5 ✓
15+0				07.5 ✓
16+0				04.4 ✓

Lt.

Z

Ret.

$$\frac{7.6}{50}$$

$$\frac{6.3}{22}$$

$$\frac{5.1}{20}$$

$$\frac{4.2}{20}$$

$$\frac{4.3}{50}$$

$$\frac{6.8}{50}$$

$$\frac{5.3}{26}$$

$$\frac{4.2}{20}$$

$$\frac{3.4}{20}$$

$$\frac{3.5}{50}$$

$$\frac{6.1}{50}$$

$$\frac{4.8}{25}$$

$$\frac{4.4}{15}$$

$$\frac{3.8}{15}$$

$$\frac{4.0}{50}$$

$$\frac{6.8}{50}$$

$$\frac{6.0}{30}$$

$$\frac{5.0}{30}$$

$$\frac{4.7}{30}$$

$$\frac{4.7}{50}$$

89.86

123 9.2 104 9.1 7.6
EDT 197 193 160 100 50

$$\frac{6.0}{25}$$

$$\frac{5.2}{25}$$

$$\frac{5.0}{50}$$

$$\frac{5.6}{50}$$

$$\frac{5.2}{31}$$

$$\frac{4.9}{30}$$

$$\frac{4.6}{30}$$

$$\frac{4.4}{50}$$

FW

$$\frac{5.3}{50}$$

$$\frac{4.6}{30}$$

$$\frac{3.7}{30}$$

$$\frac{2.8}{50}$$

FB

$$\frac{5.0}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.0}{50}$$

$$\frac{3.4}{50}$$

$$\frac{3.2}{35}$$

$$\frac{2.8}{35}$$

$$\frac{3.5}{50}$$

$$\frac{3.8}{50}$$

$$\frac{3.7}{30}$$

$$\frac{3.5}{30}$$

$$\frac{3.8}{50}$$

Krus Ditch.

EDT 195 192

TP 5.7 5.7
PWA 180 100

$$\frac{4.6}{50}$$

$$\frac{4.5}{16}$$

$$\frac{3.5}{30}$$

$$\frac{3.9}{50}$$

400.4

$$\frac{8.0}{50}$$

$$\frac{8.0}{30}$$

$$\frac{4.6}{30}$$

$$\frac{5.4}{30}$$

$$\frac{5.0}{50}$$

Sta	+	π	-	Elev.
		910.97 ✓		
16+35				03.4 ✓
17+0				05.7 ✓
T.P.	5.01	911.86 ✓	4.12	906.85 ✓
+50				06.9 ✓
18				07.2 ✓
19				07.7 ✓
+25				07.0 ✓
+30				03.9 ✓
+36				03.9 ✓
+45				08.9 ✓
+47.4 - Edge Pav.				09.0 ✓
B.M.	2.91	911.86 ✓	2.91	908.95 ✓
+62.4 Edge Pav.				08.85 ✓
+70 - Edge Pav.				08.5 ✓

Lt. R. R1.

1650 Δ in Ditch.
 104 6.3 2.1
 1650 4.2 173 110 100

7.8
 50

7.6

7.5
 14

6.2
 50

Place 24" Culv. Drains N. to Ditch.

5.6
 50

5.2
 25

5.3
 50

5.2
 25

5.2
 50

5.7
 50

5.0
 15

5.0
 50

5.5
 50

5.2
 50

4.7
 50

5.0
 50

5.3
 50

4.2
 50

4.9
 50

5.1
 50

4.9
 50

4.4
 50

2.6
 50

8.0
 50

7.1
 50

} Place 24" Culv. Drains North to Ditch.

7.4
 50

8.0
 50

6.9
 50

3.4
 50

3.0
 50

3.1
 50

3.02
 50

2.90
 50

2.92
 50

Top Stone 2 Edgerton Sta. 19+57.4

3.14
 50

3.01
 50

3.01
 50

3.4
 50

3.4
 50

3.5
 50

Sta.	+	π	-	E/V.
		911.86 ✓		
19+78				905.6 ✓
+82				05.5 ✓
+86				07.6
20+0				07.3 ✓
21+0				07.4 ✓
22+0				07.1 ✓
23+0				07.6 ✓
T.P.	4.55	912.11 ✓	4.30	907.56 ✓
+60				07.4 ✓
+72				07.6 ✓
24+0				07.3 ✓
+72-	Int. of Ditches E			(904.1) ✓
25+0				903.8 ✓

Lt. 2 Rt.

902.1
t-cut 7.8

} Place 24" Culv. Drains North to Ditch.

$\frac{6.6}{50}$ $\frac{43}{50}$ $\frac{6.7}{50}$

$\frac{7.1}{50}$ $\frac{6.4}{50}$ $\frac{7.2}{50}$

$\frac{5.2}{50}$ $\frac{4.3}{50}$ $\frac{4.7}{50}$

$\frac{5.2}{50}$ $\frac{4.6}{50}$ $\frac{4.4}{50}$

$\frac{5.1}{50}$ $\frac{4.5}{50}$ $\frac{4.9}{50}$

$\frac{5.2}{50}$ $\frac{4.8}{50}$ $\frac{4.6}{50}$

$\frac{4.8}{50}$ $\frac{4.3}{50}$ $\frac{5.1}{50}$

$\frac{5.7}{50}$ $\frac{4.7}{50}$ $\frac{4.6}{50}$

$\frac{5.9}{50}$ $\frac{4.5}{50}$ $\frac{6.4}{3}$ $\frac{6.4}{5}$ $\frac{4.7}{7}$ $\frac{4.6}{25}$ $\frac{4.4}{50}$ 8.11 + 7.5 = $\frac{5.2}{100}$
Ditch

Int. 8.5
Ditch 130

$\frac{6.0}{50}$ $\frac{4.8}{50}$ $\frac{6.5}{4}$ $\frac{6.5}{5}$ $\frac{4.8}{8}$ $\frac{5.2}{50}$

904.1 / 8.0

$\frac{5.4}{50}$ $\frac{4.8}{20}$ $\frac{4.0}{10}$ $\frac{4.9}{4}$ $\frac{8.3}{0}$ $\frac{8.3}{2}$ $\frac{5.3}{8}$ $\frac{4.8}{20}$ $\frac{4.8}{50}$

Sta.	+	T	-	Elev.
		912.11 ✓		
26 to				05.4 ✓
27				06.6 ✓
28				07.5 ✓
	4.15	912.92 ✓	3.34	908.77 ✓
29				06.5 ✓
30				06.4 ✓
31				06.9 ✓
31 + 65 A in Ditch, 26.1 North.		8.1		904.8 ✓
32				07.0 ✓
33				08.2 ✓
34				08.0 ✓
35				08.1 ✓
36				08.6 ✓
T.P.	6.13	916.95 ✓	2.10	910.82 ✓

LH.

Z

RT.

$$\frac{5.1}{50} \quad \frac{5.0}{25} \quad \frac{4.0}{4} \quad \frac{4.7}{20} \quad \frac{8.0}{2} \quad \frac{8.0}{3} \quad \frac{4.5}{10} \quad \frac{4.9}{50}$$

$$\frac{5.5}{50} \quad \frac{5.8}{25} \quad \frac{4.6}{5} \quad \frac{5.5}{20} \quad \frac{7.6}{3} \quad \frac{7.6}{5} \quad \frac{4.6}{10} \quad \frac{5.1}{50}$$

$$\frac{4.3}{50} \quad \frac{4.5}{25} \quad \frac{3.5}{3} \quad \frac{4.6}{20} \quad \frac{6.7}{3} \quad \frac{6.7}{4} \quad \frac{3.6}{10} \quad \frac{4.2}{50}$$

$$\frac{5.0}{50} \quad \frac{5.4}{25} \quad \frac{5.2}{3} \quad \frac{6.4}{20} \quad \frac{7.5}{3} \quad \frac{7.5}{5} \quad \frac{5.6}{10} \quad \frac{5.7}{50}$$

$$\frac{5.2}{50} \quad \frac{4.8}{20} \quad \frac{5.7}{3} \quad \frac{6.5}{20} \quad \frac{6.9}{2} \quad \frac{6.9}{4} \quad \frac{5.8}{8} \quad \frac{5.1}{27} \quad \frac{5.1}{50}$$

$$\frac{5.1}{50} \quad \frac{5.2}{25} \quad \frac{4.5}{13} \quad \frac{5.0}{38} \quad \frac{6.0}{20} \quad \frac{6.3}{1} \quad \frac{6.3}{3} \quad \frac{5.2}{8} \quad \frac{5.4}{34} \quad \frac{5.2}{50}$$

$$\frac{5.7}{50} \quad \frac{5.2}{25} \quad \frac{4.7}{15} \quad \frac{5.2}{2} \quad \frac{5.9}{20} \quad \frac{6.1}{2} \quad \frac{5.3}{8} \quad \frac{5.0}{25} \quad \frac{5.2}{50}$$

$$\frac{4.9}{50} \quad \frac{4.9}{25} \quad \frac{4.2}{15} \quad \frac{4.7}{20} \quad \frac{6.0}{3} \quad \frac{5.1}{7} \quad \frac{4.8}{27} \quad \frac{4.8}{50}$$

$$\frac{4.3}{50} \quad \frac{4.2}{30} \quad \frac{3.5}{15} \quad \frac{3.9}{1} \quad \frac{4.9}{20} \quad \frac{5.5}{1} \quad \frac{5.5}{4} \quad \frac{4.4}{8} \quad \frac{3.8}{21} \quad \frac{4.3}{50}$$

$$\frac{4.0}{50} \quad \frac{4.1}{30} \quad \frac{3.6}{15} \quad \frac{4.0}{2} \quad \frac{4.8}{20} \quad \frac{5.2}{3} \quad \frac{4.2}{7} \quad \frac{3.5}{17} \quad \frac{4.0}{50}$$

$$\frac{3.5}{50} \quad \frac{3.3}{30} \quad \frac{2.8}{15} \quad \frac{3.3}{2} \quad \frac{4.3}{20} \quad \frac{4.2}{3} \quad \frac{3.4}{6} \quad \frac{3.1}{20} \quad \frac{3.2}{50}$$

Sta.	T	A	-	Elev.
		916.95 ✓		
37				09.5 ✓
38				10.2 ✓
39				11.5 ✓
40				12.2 ✓
41				13.2 ✓
42				13.0 ✓ 14.0 ✓
T.P.	7.23	923.39 ✓	0.79	916.16 ✓
43				13.9 ✓
44				15.4 ✓
450				15.6 ✓
45				16.1 ✓
485				18.6 ✓
46				18.2 ✓
B.M.	4.97	923.39 ✓	4.97	918.42

4.

2

RT.

T917.0

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 30 \end{array} \quad \begin{array}{r} 6.5 \\ 15 \end{array} \quad \begin{array}{r} 6.8 \\ 1 \end{array} \quad \begin{array}{r} 7.5 \\ 15 \end{array} \quad \begin{array}{r} 7.5 \\ 4 \end{array} \quad \begin{array}{r} 7.0 \\ 7 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array}$$

$$\begin{array}{r} 6.6 \\ 50 \end{array} \quad \begin{array}{r} 6.5 \\ 30 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \end{array} \quad \begin{array}{r} 6.4 \\ 1 \end{array} \quad 6.8 \quad \begin{array}{r} 7.1 \\ 2 \end{array} \quad \begin{array}{r} 6.2 \\ 6 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 30 \end{array} \quad \begin{array}{r} 5.3 \\ 15 \end{array} \quad 5.5 \quad \begin{array}{r} 6.6 \\ 2 \end{array} \quad \begin{array}{r} 5.6 \\ 5 \end{array} \quad \begin{array}{r} 5.2 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 30 \end{array} \quad \begin{array}{r} 4.4 \\ 10 \end{array} \quad 4.8 \quad \begin{array}{r} 5.9 \\ 2 \end{array} \quad \begin{array}{r} 4.9 \\ 4 \end{array} \quad \begin{array}{r} 4.3 \\ 25 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 4.1 \\ 30 \end{array} \quad \begin{array}{r} 3.8 \\ 10 \end{array} \quad 3.8 \quad \begin{array}{r} 4.7 \\ 2 \end{array} \quad \begin{array}{r} 3.9 \\ 5 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ 50 \end{array} \quad \begin{array}{r} 2.6 \\ 10 \end{array} \quad \begin{array}{r} 2.5 \\ 4 \end{array} \quad 4.0 \quad \begin{array}{r} 4.0 \\ 1 \end{array} \quad \begin{array}{r} 2.5 \\ 4 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 7.9 \\ 15 \end{array} \quad \begin{array}{r} 7.9 \\ 3 \end{array} \quad 9.5 \quad \begin{array}{r} 9.5 \\ 1 \end{array} \quad \begin{array}{r} 7.7 \\ 4 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.8 \\ 50 \end{array} \quad \begin{array}{r} 5.6 \\ 30 \end{array} \quad \begin{array}{r} 5.0 \\ 3 \end{array} \quad 8.0 \quad \begin{array}{r} 8.0 \\ 1 \end{array} \quad \begin{array}{r} 5.1 \\ 3 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 30 \end{array} \quad \begin{array}{r} 4.6 \\ 4 \end{array} \quad \begin{array}{r} 7.8 \\ 1 \end{array} \quad 7.8 \quad \begin{array}{r} 3.7 \\ 5 \end{array} \quad \begin{array}{r} 4.6 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 4.9 \\ 5 \end{array} \quad \begin{array}{r} 7.3 \\ 1 \end{array} \quad 7.3 \quad \begin{array}{r} 4.5 \\ 2 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 5.2 \\ 30 \end{array} \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 7.3 \\ 7 \end{array} \quad \begin{array}{r} 7.3 \\ 5 \end{array} \quad \begin{array}{r} 4.8 \\ 2 \end{array} \quad 5.3 \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 6 \end{array} \quad \begin{array}{r} 7.5 \\ 4 \end{array} \quad 5.2 \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

top Stone Man.

Sta.	T	X	-	Elev.
		913.39 ✓		
47				18.3 ✓
T.P	5.30	924.48 ✓	4.21	919.18 ✓
+29				18.4 ✓
+43 - 2 Ditch Ora				18.4 ✓
+57				18.7 ✓
48				19.6 ✓
49				19.6 ✓
50				19.8 ✓
51				20.4 ✓
52				19.9 ✓
53				19.4 ✓
T.P	3.42	922.63 ✓	5.27	919.21 ✓
54				18.9 ✓
55				18.6 ✓

Lt.

E

Rt.

$$\begin{array}{r} 43 \\ 50 \end{array} \quad \begin{array}{r} 47 \\ 15 \end{array} \quad \begin{array}{r} 59 \\ 7 \end{array} \quad \begin{array}{r} 70 \\ 4 \end{array} \quad \begin{array}{r} 70 \\ 2 \end{array} \quad 51$$

$$\begin{array}{r} 52 \\ 20 \end{array} \quad \begin{array}{r} 52 \\ 50 \end{array}$$

$$\begin{array}{r} 60 \\ 50 \end{array} \quad \begin{array}{r} 63 \\ 18 \end{array} \quad \begin{array}{r} 71 \\ 9 \end{array} \quad \begin{array}{r} 86 \\ 5 \end{array} \quad \begin{array}{r} 86 \\ 3 \end{array} \quad 61$$

$$\begin{array}{r} 60 \\ 50 \end{array}$$

$$\begin{array}{r} 81 \\ 50 \end{array} \quad \begin{array}{r} 83 \\ 30 \end{array} \quad \begin{array}{r} 916.1 \\ 80 \\ 5 \end{array} \quad 61$$

$$\begin{array}{r} 57 \\ 50 \end{array}$$

$$\begin{array}{r} 61 \\ 50 \end{array}$$

$$\begin{array}{r} 58 \\ 20 \end{array}$$

$$\begin{array}{r} 58 \\ 10 \end{array}$$

$$\begin{array}{r} 56 \\ 50 \end{array}$$

$$\begin{array}{r} 58 \\ 50 \end{array}$$

$$49$$

$$\begin{array}{r} 57 \\ 5 \end{array}$$

$$\begin{array}{r} 51 \\ 15 \end{array}$$

$$\begin{array}{r} 53 \\ 50 \end{array}$$

$$\begin{array}{r} 51 \\ 50 \end{array}$$

$$49$$

$$\begin{array}{r} 50 \\ 9 \end{array}$$

$$\begin{array}{r} 52 \\ 50 \end{array}$$

$$\begin{array}{r} 51 \\ 50 \end{array}$$

$$47$$

$$\begin{array}{r} 48 \\ 50 \end{array}$$

$$\begin{array}{r} 49 \\ 50 \end{array}$$

$$41$$

$$\begin{array}{r} 47 \\ 50 \end{array}$$

$$\begin{array}{r} 51 \\ 50 \end{array}$$

$$46$$

$$\begin{array}{r} 47 \\ 75 \end{array}$$

$$\begin{array}{r} 54 \\ 50 \end{array}$$

$$\begin{array}{r} 53 \\ 50 \end{array}$$

$$51$$

$$\begin{array}{r} 55 \\ 20 \end{array}$$

$$\begin{array}{r} 60 \\ 50 \end{array}$$

$$\begin{array}{r} 40 \\ 50 \end{array}$$

$$\begin{array}{r} 41 \\ 10 \end{array}$$

$$37$$

$$\begin{array}{r} 41 \\ 50 \end{array}$$

$$\begin{array}{r} 43 \\ 50 \end{array}$$

$$\begin{array}{r} 45 \\ 10 \end{array}$$

$$40$$

$$\begin{array}{r} 45 \\ 50 \end{array}$$

Dec 1944.

Sta.	+	A	-	Elev.
		92263 ✓		
56				18.1 ✓
57				17.9 ✓
+75				17.0 ✓
+93				17.6 ✓
58				15.0 ✓
+07				17.7 ✓
+25				17.0 ✓
59				17.3 ✓
60				19.5 ✓
TIP	8.85	92258 ✓	2.90	919.73 ✓
61				21.0 ✓
62				22.1 ✓
63				23.0 ✓

Lt. 2 Rt.

$\frac{4.6}{50}$

4.5

$\frac{4.5}{50}$

4.8

4.7

$\frac{5.0}{50}$

Drain South

$\frac{4.6}{50}$

$\frac{5.0}{53}$

$\frac{6.2}{3}$

$\frac{5.6}{1}$

$\frac{4.5}{38}$

$\frac{7.9}{48}$

$\frac{7.9}{52}$

$\frac{5.0}{59}$

Ditch

$\frac{5.1}{50}$

$\frac{5.6}{11}$

$\frac{6.7}{3}$

5.0

$\frac{7.8}{10}$
(Ditch)

$\frac{7.8}{14}$

$\frac{5.2}{29}$

$\frac{3.2}{40}$

$\frac{5.0}{50}$

$\frac{5.5}{50}$

$\frac{6.3}{25}$

$\frac{6.5}{16}$

$\frac{7.4}{6}$

$\frac{7.6}{1}$

Ditch

$\frac{7.4}{6}$

$\frac{3.8}{22}$

$\frac{3.8}{35}$

$\frac{5.0}{50}$

$\frac{5.5}{50}$

$\frac{6.1}{20}$

$\frac{7.5}{17}$
(Ditch)

$\frac{7.5}{9}$

4.9

$\frac{5.1}{20}$

$\frac{5.0}{50}$

$\frac{5.4}{55}$

$\frac{7.5}{47}$
(Ditch)

$\frac{7.5}{42}$

$\frac{5.1}{29}$

$\frac{5.6}{1}$

$\frac{5.3}{20}$

$\frac{5.3}{50}$

$\frac{5.0}{50}$

$\frac{5.3}{1}$

$\frac{4.7}{50}$

$\frac{3.1}{50}$

3.1

$\frac{7.6}{50}$

$\frac{8.2}{50}$

7.6

$\frac{7.5}{30}$

$\frac{7.7}{50}$

$\frac{7.3}{50}$

6.5

$\frac{6.8}{50}$

$\frac{6.5}{50}$

5.6

$\frac{5.4}{50}$

P. 30" cu 10

Sol. + A - Elev

92858 ✓

64

24.9 ✓

64+50

25.2 ✓

65+0

24.9 ✓

TIP

4.47

930.07 ✓

2.98

925.60 ✓

+43

24.8 ✓

766

24.77 ✓

+76.72 E. 66000

25.07 ✓

66

25.07 ✓

67

23.7 ✓

B.M.

4.11

92596 ✓

L.

I

Rt.

$$\frac{3.7}{50}$$

$$\frac{3.7}{1}$$

$$\frac{3.0}{1}$$

$$\frac{3.5}{50}$$

$$\frac{3.4}{50}$$

$$\frac{3.4}{1}$$

$$\frac{3.3}{15}$$

$$\frac{3.3}{50}$$

$$\frac{3.9}{50}$$

$$\frac{3.7}{1}$$

$$\frac{3.6}{50}$$

$$\frac{5.7}{50}$$

$$\frac{5.3}{1}$$

$$\frac{5.5}{27}$$

$$\frac{5.15}{50}$$

$$\frac{4.74}{69} = \text{Labore.}$$

$$\frac{6.0}{50}$$

$$\frac{5.6}{21}$$

$$\frac{5.30}{24}$$

$$\frac{4.90}{24}$$

$$\frac{5.30}{50}$$

$$\frac{6.1}{50}$$

$$\frac{5.40}{22}$$

$$\frac{5.00}{27}$$

$$\frac{5.0}{27}$$

$$\frac{5.65}{34}$$

$$\text{E Road} = \frac{4.82}{52}$$

$$\frac{5.2}{32}$$

$$\frac{5.0}{1}$$

$$\frac{5.7}{19}$$

$$6.4$$

* S.W. Cor Labore r D. (spike in guy pole 16' Rt. Sta. 65+50)
 Levels from T.H. #61 and D - this B.M. = 975.88

