

Dr. 6 - Bk. 24

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

COUNTY ROAD "D"

From Labore Rd. To East Co. Line Rd.

Road Acc't. No. 24

Date Filed 12-29-38

File

PLAN SURVEY

CO. RD "D"

from

LoBor Rd to E County Line





Alignment

Sta	Point	ΔL	ΔE
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15	182.66	P.O.T.	
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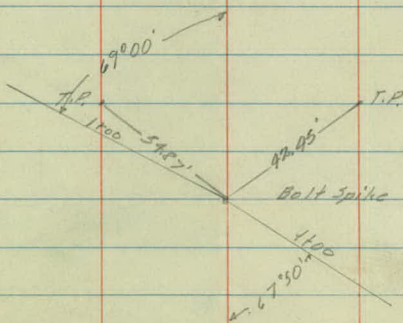
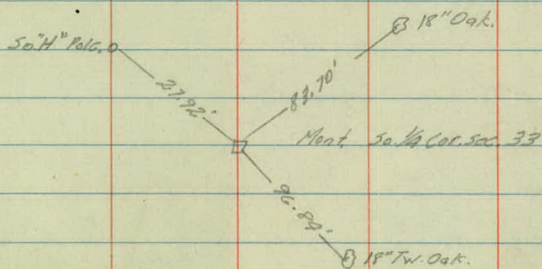
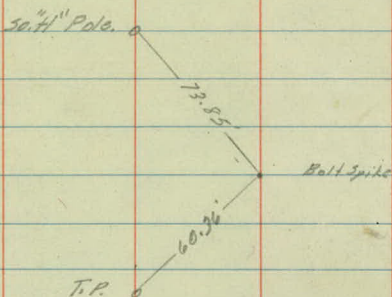
6	159.06	✓ P.I.	
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$0^{\circ}13'30''$

0	100	= E. La Bore Rd.	
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7/16/38
K.R.
L.G.
R.P.
M.d.G.

2



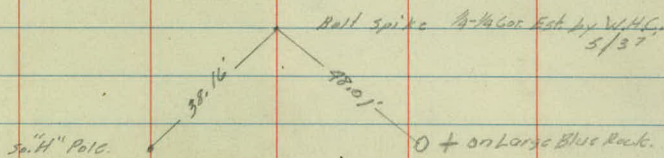
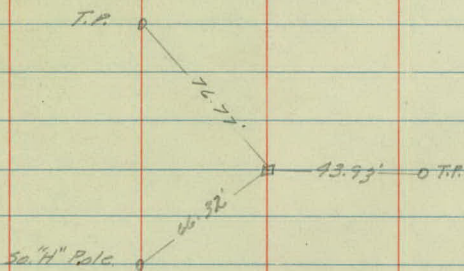
Sta.	Point	ΔLt	ΔRt
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$\left. \begin{array}{l} 33+11.7 \\ 33+11.03 \end{array} \right\} \text{Equal}$

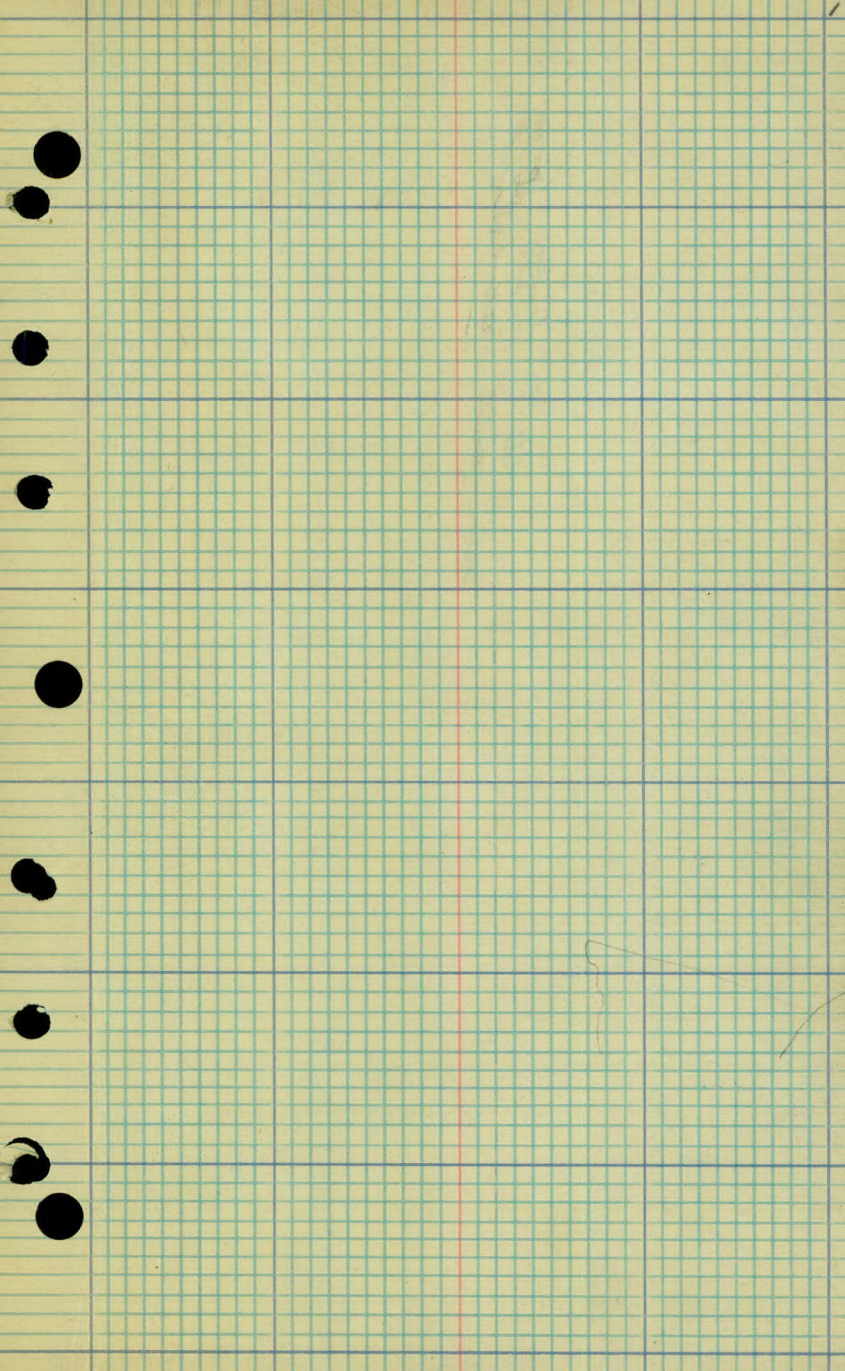
P.I.

$0^{\circ} 06''$

19 + 84.85 P.O.T.



26 57.97
1326.



Station Point Lt. ^{Angle} Rt.

59+56.39 P.I.
Mon. 5°-31'
± Backsht(So.)

57+75.5 P.I. 14°-59'

56+58.5 P.I. 9°-07'

38+78.0 P.O.T.

33+11.9 Mon.

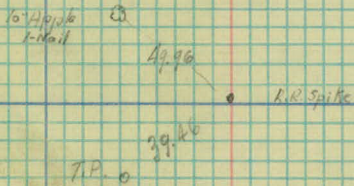
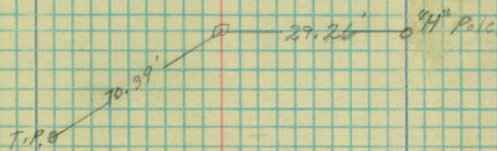
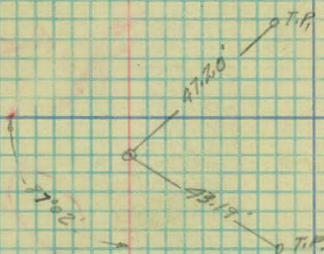
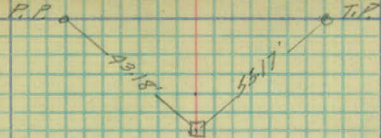
Station	Point	Angle	
		Lt	Rt

112+35.62	Mort.		
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106+57.35	P.O.T.	= White Bear Ave.	
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85+96.78	Mort.	0°-01'	
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71+35.57	P.O.T.		
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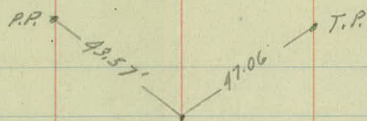


Sta Point Alt. A.Rt.

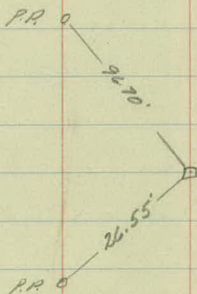
191 +48.45 Brass Plug in Riv.

165 +09.39 P.O.T.

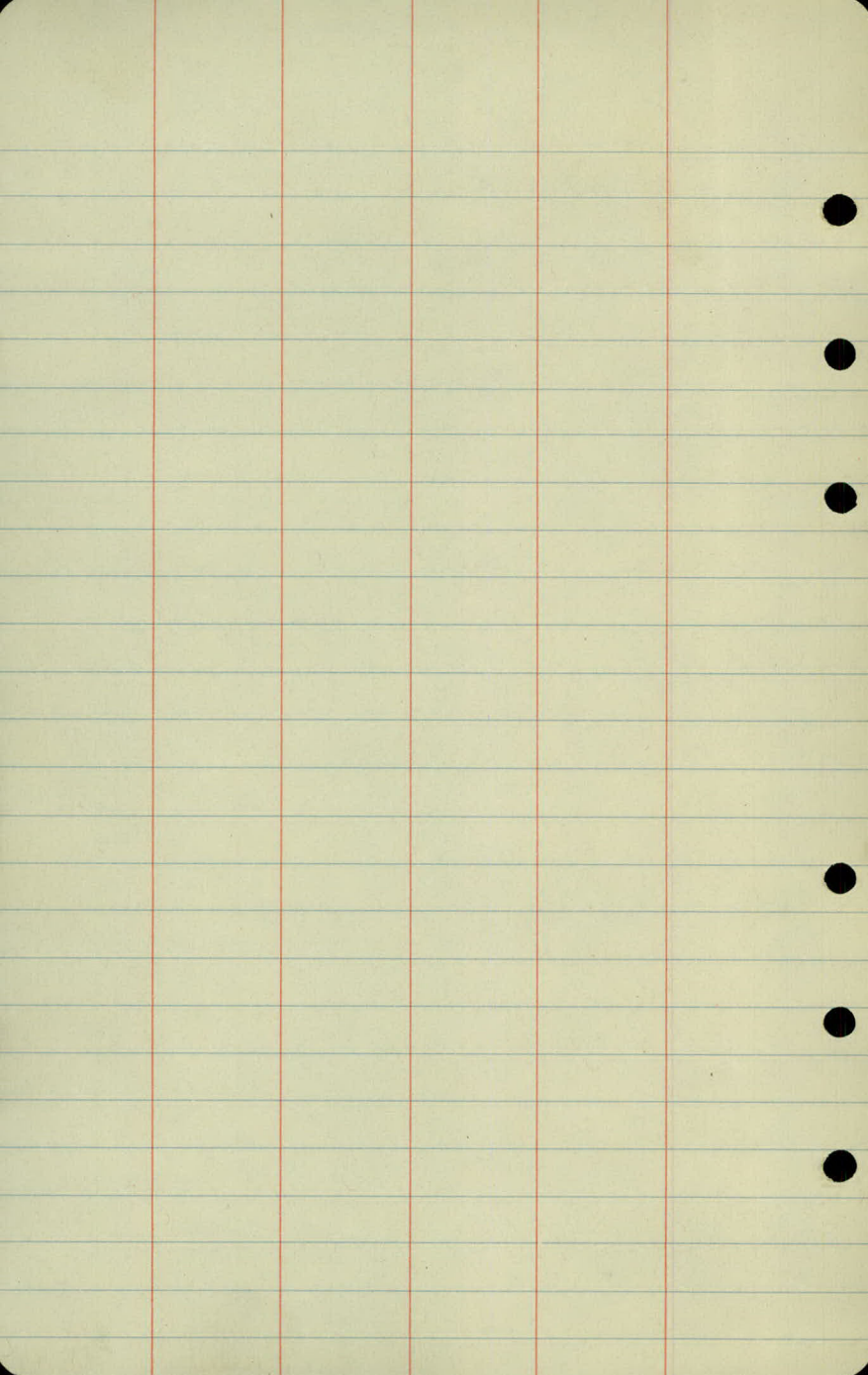
198 +22.76 P.O.T.



5/4 Cor Sec 36



5/4 Cor Sec 36-20-22



7/22/38
K.B.
L.C.
R.P.
M.J.G.

Topography

5

8'

8'

4

1974 29" x 56' C.M.

8'

10'

27'

39'

3

8'

5'
9'

2

8'

10'

1

9'

11'

150

9'

13'

0+100

+150-T.P.-20'

+76-BogFc.-25'

+18-T.P.-19'

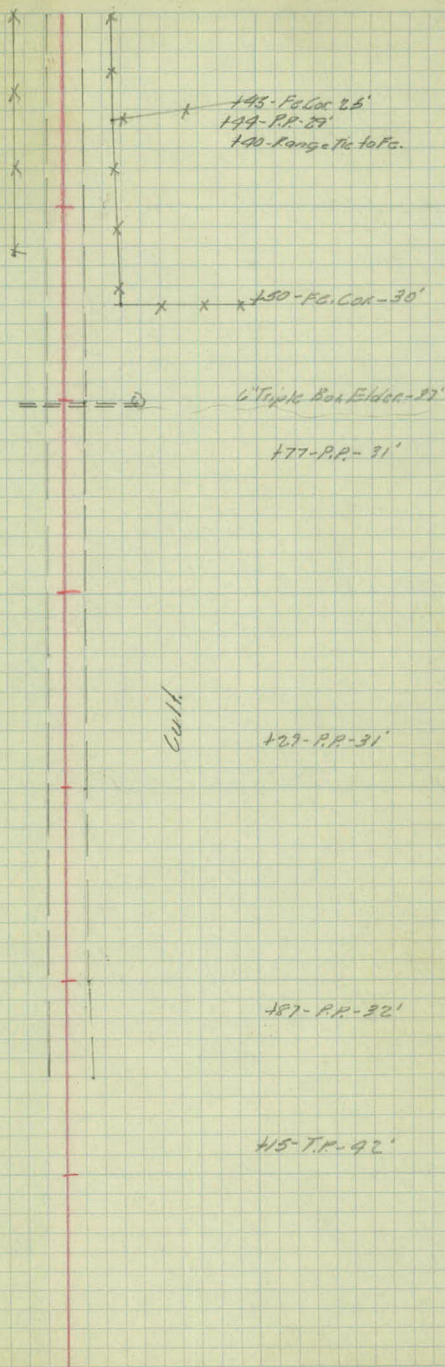
+88-T.P.-19'

+62-T.P.-19'
Trans. Pole.

+59-T.P.-19'

+67-T.P.-17'

+38-T.P.-39'



12

8'

8'

11

8'

8'

10

10 P. 2. 12" 130' C. M.

23'

8'

27'

9'

9

9'

9'

8

8'

9'

7

9'

8'

6

8'

9'

113-T.H.P. - 20'-21'

FC. - 25'

181-T.P. - 21'

Cult.

145-T.P. - 21'

FC - 29'

114-T.P. - 21'

FC - 26'

181-T.H.P. - 16'-23'

FC. 26'



Cult.

100-98' Cult. - 30'

110-End. 15' K26' N. - 17'

192-15' O. - 35'

181-12' Ben. E. 100 - 31'

150-End. Ben. Tra. - 29'

5 Tr. 65.

104-Beg. Row. 12' Tra. 31'

125-Lillie's Hays - 31'

118-End.

105-FC. Cor. - 25'

T.P. - 29'

19

8'

5'

18

9'

8'

17

9'

8'

16

8'

9'

15

9'

8'

14

9'

8'

13

9'

8'

153- T.H. P. - 25' - 30'

FC - 31'

129- T.H. - 26'

T.S.P. 400,
102- Monhale - 10'

187- T.R. - 25'

157- F.C. Cor. - 26' - 29'
End Cont.

113- T.R. - 24'

150- T.R. - 24'

FC - 26'

117- T.R. - 23'

185- F.C. Cor. - 55'
End Woods.

Tr. Line 57'

Tr. Line 93'

Tr. Line - 22'
170- Ent. 15" x 20 C. R. - 14'

181- Beg. Woods - 28'

Cont.

26

10'

7'

25

9'

7'

24

10'

7'

+ 81-812" 156' G.M.T.

25'

25'

23

10'

8'

22

10'

8'

21

8'

9'

20

8'

8'

+10 P.R. - 26' Fe. - 30'

+16 Enk. - 15" Red G. 17-19'

+39 T.P. - 26'

+34 End Trees - 35

Tr. Line - 35

+85 Enk.

+50 T.P. - 26'

End Fe. - 28'

Tr. Line - 35'

+12 T.P. - 26'

+13 - 800 Oak Tr. 37'

Fe. - 27'

+10 T.P. - 27'

Fe. - 28'

Fe. - 28'

+87 T.P. - 25'

+72 End - 12" Red G. 12-16'

+69 Brush - 15'

+76 - 15' Oak - 31'

+51 - 15' Oak - 30'

+29 - 15' Oak - 29'

+20 - 12" Tr. Oak - 30'

+20 P.R. - 26'

+06 - 15' Oak - 34'

+91 - 15' Oak - 34'

+79 - 15' Oak - 29'

+51 - 15' Oak - 29'

+12 - 8' Oak - 26' - 12' Q. - 30'

+03 - 8' Oak - 27'

+55 Group 5 - 12' Oaks - 26'

+42 - 12' Oak - 26'

+78 Fe. Cor. - 31'

+70 Range Dis to Fe.

End Row Trees

Fe. - 25 Tr. - 29'

+18 - 12" Red G. 12-16'

Fe. - 27'

Meadow

Pasture

33

10'

8'

32

10'

7'

31

8'

7'

30

9'

8'

29

9'

8'

28

9'

8'

40-41246 L.M.

28'

28'

27

9'

9'

+83-T.P.-20'

+38-W. End-15" Cuts-20'
+27-R.P.-27'
+06-T.P.-95'

+98-T. 1/4" P.-23'-20'

+78-R.P.-27'
+63-Ent.

+35-Ent.
+15-T.P.-26'

Cut

+72-18" Cuts-27'

+15-R.P.-26'

+89-T.P.-26'

+63-End Row Trees-28'

+06-R.P. Row 15" Cuts-33'

+65-T.P.-27'
+59-Ent.

+08-R.P.-26'
+50-End Branch-R'-95'

+54-T.P.-27'

Brush-23'-60'

+45-R.P.-27'
100-End Row Trees
Row Trees-35'
Brush Cuts-18'

38

#59 R 121185 G.M.

24'

22'

4' X 6' X 3' Deep Rubble
Spillway Rth.

37

7'

10'

36

9'

8'

35

11'

6'

34

11'

6'

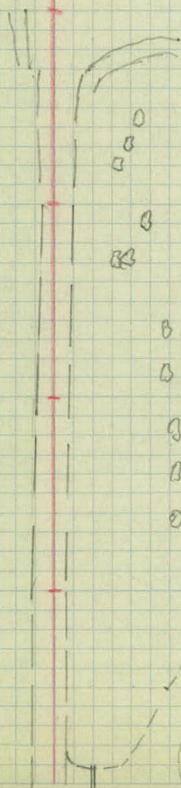
Bur. 17-15'

170-Bur. 14'

122-T.P. 27'

129-T.P. 27'

T.P. 26'



185-Bur. 6.5'
170-Bur. 18'

149-6" Oak-42'
131-8" Oak-39'
121-8" Oak-36'

192-8" Oak-41-49'

171-12" Oak-39'

171-6" Oak-34'

172-6" Elm-31'

193-NE. Loc. ORCHARD-48'

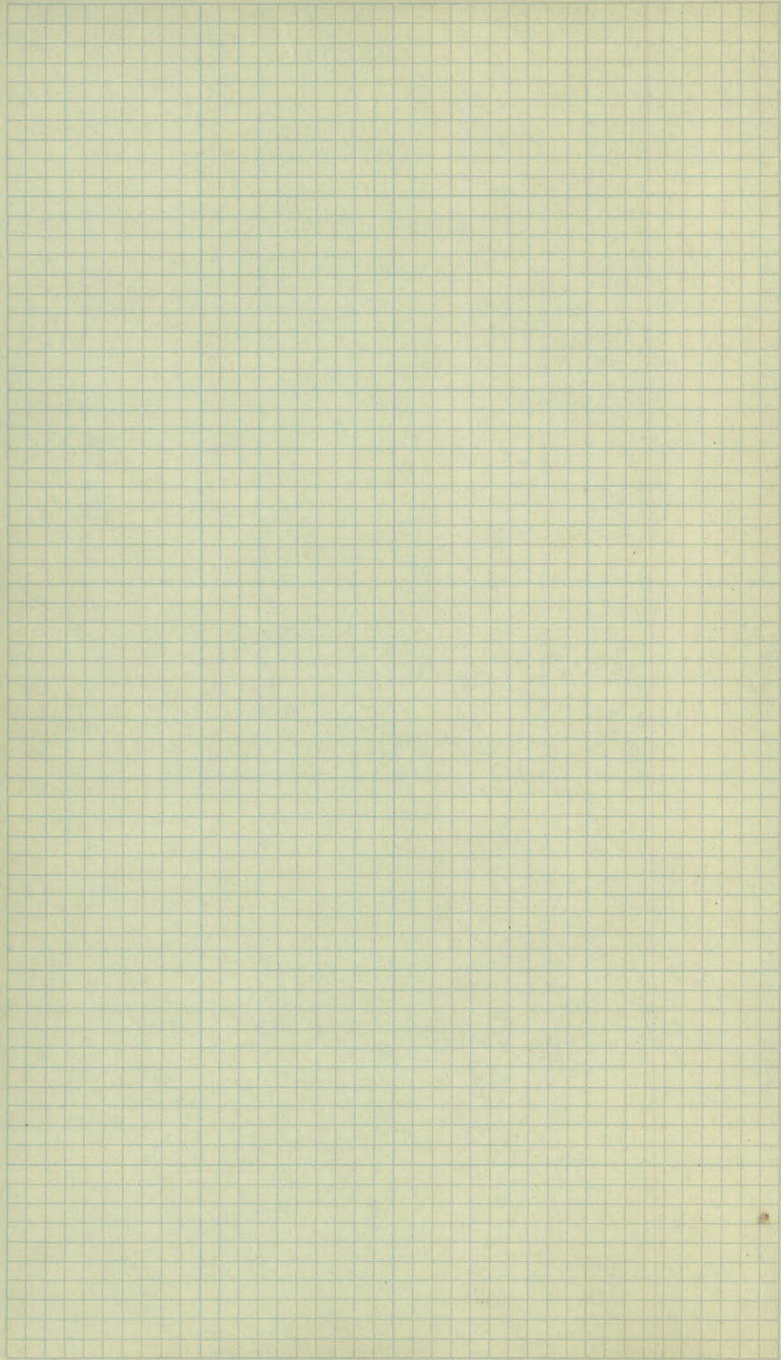
124-P.P. 26'

197-12" Oak-36'

197-N.W. Cor. Apple
Orchard-61'

125-P.P. 35'

108.5-End-156-P.P. 20'



Topography

36x50'-C.M.

41

13' 10'

40

11'

39

+78- 2 T.H. No 61

38

37

181-9.P. 28'
177-7.P. 27'

175-E. Cu. 24'

183-F.P. 27'

175-Rin Ditch. 70

100-Berm 15'

180-S.W. Berm 29'-41'

71-S.W. 57

65-S.W. Berm 57

See 800'

14-E. End Cu 1.
23'

132-F.P. 20'

162-9.P. 23'

192-Beg. Fe. - 28'

+28-
+18-13-22

150-S.W. Berm 25-35

51-S.W. Berm 60
192-Edge Ru.

E.T.H. No. 61 705+706

13-91

710- 15"X.44 { 24+* → 20
48 { H.W. 115"

47

13 10

46

12 9'

45

13 10

44

13-10

43

13 10

42

F-24

F-29

6

F-29

#17-F-26'
#17-T.R. 26

#12-Fence 36'

#25-F. Cor. 29

F-26

#12-T.P.

#48-Ent.

#54-T.P.

#32-T.P.

F-27

#69-T.P.

#10-Box F. 26

X X

Dr. 1/2 h

#53-T.P.

F-24

#30-T.P.

#46-T.P.

F-27

#15-T.P.

#10-Ent.

#12-T.P. 21

#17-F.C. 25

cliff

meadow

55

12 10

54

13-10

53

13 - 10

52

13 10

51

12 - 10

50

13 9

49

199-T.P. 27'

A-43'
198-T.P. 26'

7

F-27'

103-T.P. 25'

F-43'

169-T.P.

197-T.P. 25'
197-T.P. 25'

141-T.P.

177-T.P.

103-T.P.

F-25'

175-T.P. 25'

148-T.P.

- 1000 - Ditch 20' x 2'

Posture

uncult

Meadow

141-F Cor. 29'
145-T.P. 25'
132-Ent. 15' x 30' x 20'
120-F Cor 29'

118-T.P.

12-12

62

13-11

61

15-10

60

12-11

+197- 12" x 40' C.M.

20-20

+156. ²³/₂ Book St. (South)

12'

59

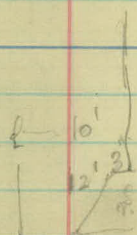
14-10

58

8'-10

57

10-10



+58-10-12

56

FC 50'
+92-T.P.

+11-Ent. $\frac{3}{19}$

+113-T.P.

+56-T.P. 30'

+50-T.P. 26'

+35-T.P. 32'

+60-Bog F. 39'
+62-Ent.
+56-T.P. 39'

+45-F Cor. 25'

+92-E.W. W. 19'
+91-Bog F. 17'
+75-11' Bog 10'

+45-Abut 10'

+33-T.P. 42'
+34-E Fence 20'
+34-End Wing Wall 23'

+91-F Cor. 27-37'
+83-T.P. 32'

+64-Ent

+70'

+46

+32-T.P. 24'

+70-T.P. 18'

+38-Ent

+33-F Cor. 32'

+69-T.P. 12'

+81-E.W. W. 24'
+77-Bog F. 18'
+75-10' Abut

+45-Abut 10'

+36-End Fence 20'
+35-End R/W 11' 28'

+07-R.R. Tel. Line

+91-F Cor. 24-36
+89-T.P. 22'

Wing Walls
2' Thick

Walls 4' Thick

69

11-17

68

11-12¹

67

11-12

66

12-11

65

11-11

64

11-12

172

12'x48'CM (25-23')

63

48840
+90-H-Pole
34-78'

+51-T.P.

+60-10"E/m 41'

+24-T.P.

+63-En + 12"x32" C.M.
15'

+90-T.P. 30'
+89-10" Tr. Apple 19'
+60-E. Fen. 30'

+62-T.P. 30'

FC, 30

+77-T.P.

+42-T.P.

+08-T.P.

+86-T.P.

+60-T.P.

+78-T.P.

+25-T.P.

Cult

Cult

76

11 11'

75

12 11

74

11' 11

198-2 Farm Ent

73

11' - 11

x

72

12 - 11

71

11 - 11'

70

+73-T.P.

+76-T.P. 31'

+83-T.P.

cult

+87-T.P. -

+68-T.P. 31'

+91-T.P. 40

+21-H. D. 10
29-35'

+47-T.P.

cult

+10-Cor. orchard 34'

0 0 0
0 0 0
0 0 0

cult

+96-T.P. 31'

+65-Cor. Orchard 34'

+34-Raw Plum 34'

+47-Ent.

+19-Row Apple 34'

+10-T.P.

L.A. 24

0 0 0
0 0 0
0 0 0

+50-Dr. 1003

+66-T.P.

+87-T.P.

83

11 - 11

82

11 11

81

11 12

80

10 12

79

10 - 12

78

10 12

77

491-T.P. 41
27-32

452-T.P.

469-T.P.

431-T.P. 32'

436-T.P. 30'

waste land

496-T.P. ✓

406-T.P.

470-T.P.

430-Ent

481-T.P.

cult

cult

435-T.P.

451-T.P.

410-T.P.

12-11

90

12-11

156- 3" X 5 1/2 m. 27-24'

89

12 11

88

87

11 10

86

12-10

85

11-11

84

463-T.P.

~~463-T.P.~~

465-T.P.

437-T.P.

Ditch

Posture

464-Range to EXCEL

Ditch

459-F. Cor. 31

433-T.P.

457-F. Cor. 29

407-T.P. 29

446-T.P. 31

410-F. Cor. 29

old
2011000
D.P.

436-T.P.

475-T.P.

435-6" B&E 132
433-10" B&E 33
424-6" B&E 31
417-8" B&E 30

412-Ent.

496-F. cor. 32

400-Fen Cor. 33

499-H. 10/0
74-35'

403-T.P.

cut

479-12" Pnc. 43

462-Ent.

486-T.P. 32

424-12" B&E 134

cut

11-12

97

11-11

96

12-12

95

11-11

94

11-11

93

11-11

92

12-11

91

F-39'

196-T.P. 179

F-50

+86-H-Pole
27-21

+134-T.P.
+32-F. Cor. 50

+30-F. 41'

+28-H-Pole
31-26'

+66-T.P. 25
+66-Lin F. 75

+12-T.P. 32'
Fence 32'

+41-T.P.

+88-T.P.

+16-T.P. 27'
Fence 27'

+42-F. Cor. 27'
+36-Range

+64-T.P.

+86-T.P.

+32-T.P.

10-11

104

10 12

103

10 12

102

11-12

101- 12" 40'-CM, 20'-20'

101

10 12

100

11 13

99

10 10

98

+67-T.P.-25'

+62-T.P.

F-25

+67-T.P.

+34-T.P. 25'

+54-T.P.

F-23'

F-33

+45-T.P.-33'

+11-T.P. 24'

F-24'

+85-T.P.

F-21'

+84-T.P.

Wasteland.

+76-T.P.

F-22'

+48-T.P. 24'

+66-T.P.-33'

F-24'

F-33

+17-T.P.

+53-T.P.

F-40

cult.

110

109

108

107

107 $\ominus$ x $\ominus$ 230

106

11 - 12

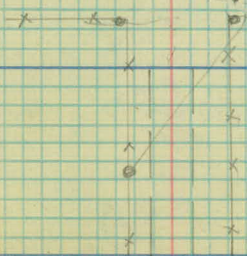
105

+ 67.5- E. P. 0
+ 57.5- 4

+ 47.3- E. P. 0
+ 26- R. R. 28
+ 24- R. Cor. 76

+ 81- 9. P. 28

+ 45- T. P. 28

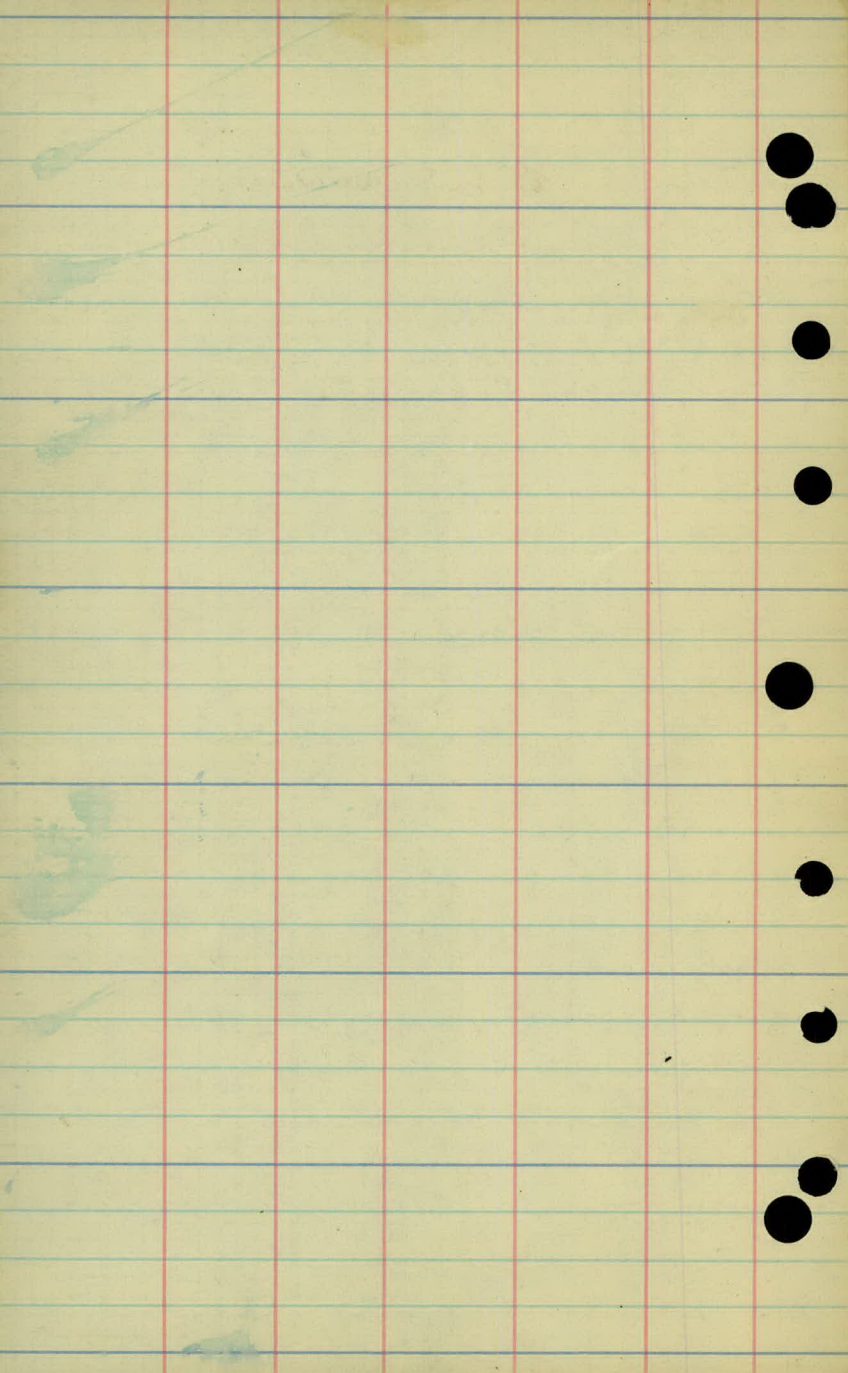


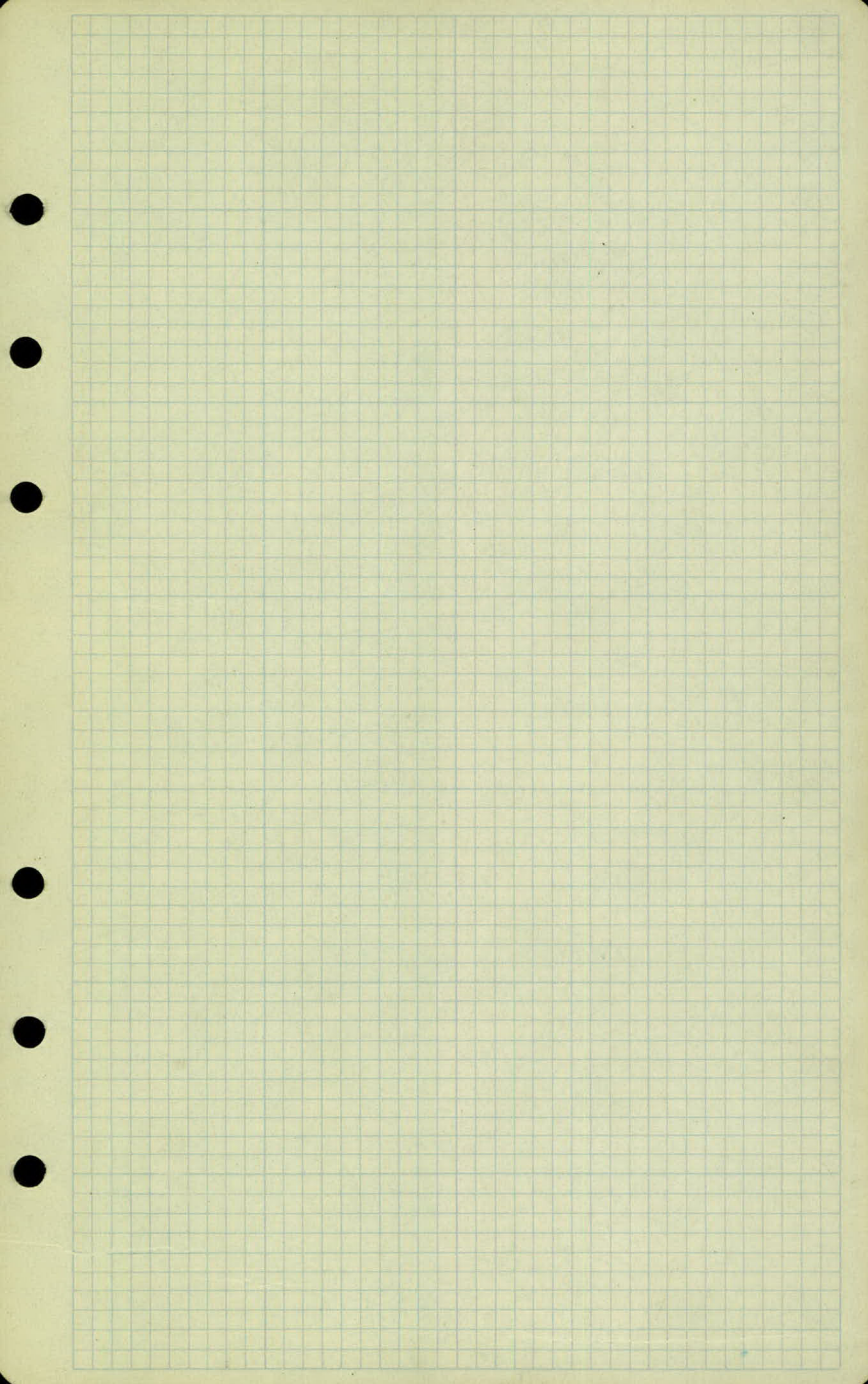
+ 76- E. End. Gang. Cor. 32
24 x 40 P. 3
+ 36- W. End. Gang. Cor. 32
+ 35- Co. Rd. Sp. 76
+ 27- R. Cor. 21
+ 26- T. P. 31



+ 73- 9. P. 33

+ 8- T. P. 32





112

9'

9'

111

10'

9'

110

9'

8'

109

9'

10'

108

10'

9'

107

9'

11'

181-T.P.-21'
170-P.P.-26'

135-Fe Cor.-27'

171-P.P.-26'

170-P.P.-26'

Fe.-26'

156-P.P.-25'

Fe.-27'

112-P.P.-26'

174-P.P.-26'

189-P.P.-27'

189-T.P. Fe Cor.-23'

155 G.M.-26'-T.P.-31'

188-Bes. Cult.

117-Cor. Orchard-38'

139-T.P.-31'

138-N.W. Cor Orchard-38'

160-Ent.-12" 120 G.M.-26'

151-12" 120 G.M.-35'

115-N.W. Cor. No. 77

102-T.P.-32'

197-12" 120 G.M.-39'

188-Apple-47'-60'

166-Ent. Cult.-28'

192-T.P.-31'

183-Bes. Cult.-31'

189-T.P.-31'

184-T.P.-43'

119

11'

2'

118

11'

8'

117

8'

8'

116

10'

7'

115

10'

9'

114

10

10

113

10'

10'

115' 1 1/2 S.F.
2 34'

+90-NW Cor No. 68'

+71-P.P.-26'

+92-NE Cor Nursery - 33'
+88-Ent 12" A.P.C.M. - 13'
T.P. - 28'
2" Elms
+91-NW Cor Nursery 25'

+67-P.P.-25'

+69-Ent

+69-P.P.-26'

+72-T.P.-28'

Cut 1/2

+68-P.P.-26'

+68-T.P.-30'

+71-P.P.-26'

+77-T.P.-29'
+62-Fg Cor - 33'

+91-Ent

+22-T.P.-30'
+06-Fg Cor - 35'

+65-P.P.-26'

+78-Ent

+96-5" Trip Tap - 21'
+23-R. 2 1/2" Stone Stem - 19'
+19-NW Cor Ho. - 62'
+99-T.P.-31'
+87-Cor. Rav. Fr. - 42'

+71-P.P.-27'

+19-Ent
Ho. - 90'

+27-Beg. Row. Mountain
Fsh. 91'

126

11'

7'

125

11'

6'

124

12'

7'

123

12'

6'

122

11'

7'

121

12'

7'

120

11'

7'

145-R.P.-26'

Cult.



157-T.P.-25'

Cult.

145-R.P.-26'
151-Row Tr. 27'

00000

156-P.C. Cor.-27'

131-T.P.-26'

171-R.P.-26'

107-T.P.-27'

167-R.P.-26'

183-T.P.-27'

169-R.P.-26'

Cult.

120-T.P.-27'

170-R.P.-26'

153-T.P.-26'

Cult.

169-R.P.-26'

129-G.P. 17-T.P.-27'

133

10'

9'

132

11'

9'

131

7'

8'

130

9'

9'

129

10'

8'

128

10'

8'

127

11'

6'

+68-P.R.-26'

+66-S.E. Cor Orchard-35'
Fe.-25'

+68-P.R.-26'

+66-P.R.-26'

+36-S.W. Cor Orchard-35'

+22-Fe. Cor.-27'-P.R.-26'

+12-Fe.-12" K&O G.M.-20'

+05-Fe.-29'

+65-P.R.-25'

+66-P.R.-25'

+68-P.R.-26'

+67-P.R.-26'

+67-P.R.-25'

+68-Ent.

Cult.

Cult.

Cult.

Cult.

+95-Top-22' Fe.-22'

+69-Ent.

+62-Fe. Cor.-22'
+59-T.P.-22'

+29-10" Apple-35'
+19-6" Apple-35'

+67-7" Apple-35'
+50-12" Apple-35'
+95-Best Low Apple Tr.-36'
+37-7.5"-28'
+25-Plum Tr.-23-38'

Fe.-23'

+55-Mum Tr.-24-35'

+65-6" Apple Tr.-26'

+40-Bas. Fe.-24'
+38-T.P.-24'

31'
30' 16'-5-Ft. H6-N.E. Cor Ho.-13'
+76-Mum Cor Ho.-15'

+61-Ent.
+58-6" Elm.-33'
+50-T.P.-29'-Fe. Cor.-26'
+90-30" Oak-27'

+18'-15" Oak-37'

+18-T.P.-29-G.R.-39'
+67-Fe. Cor.-26'

Fe.-26'

190

8

6

199

9

6

+60 Reg. Scarified B. Top.

138

11'

8'

137

11'

8'

136

+13-6 18" X 4 1/2" C.M.

10

23'

8'

9'

135

10'

9'

134

11'

8'

+67-P.P.-26'

+72-T.P.-20

+65-P.P.-26'

+98-Ent.

+40-T.P.-20'

+72-Fc Cor.-26'
+69-P.P.-26'

+90-L.Rd.

+72-Fc Cor.-21'

+08-T.P.-21'

Fc-27'

Fc-21'

+69-P.P.-26'

+77-T.P.-20'

Fc 26'

Fc-23'

+65-P.P.-26'

+52-H.P.-19'-25'
+90-Ent.

+66-P.P.-26'

+53-T.P.-22'

+65-Fc Cor.-28'

+17-T.P.-21'
Fc-23'

147

8'

7'

146

8'

7'

145

8'

8'

144

8'

7'

143

8'

7'

142

8'

7'

141

Bas Hedge 26'

+75-T.P.-20'

+13-T.P.-21'

+62-G.P.-26'

+93-Ent.

+65-P.P.-27'

Cut

+78-T.P.-20'

+53-P.P.-29'
+92-Ent.

+68-P.P.-26'

+50-H.T.P.-18'-23'

+63-P.P.-26'

+21-T.P.-20'

+66-P.P.-26'

+82-G.P. Elder-26'
+75-Ent.
+69-Cor Hedge-26'

+57-N.W. Cor. Ho.-72'

+83 Hedge-26'
+95-T.P.-20'

+66-P.P.-26'

+86-Cor Hedge-29'
+34-T.P.-20'

+85 Hedge-29'
+35-Ho.-72'

154

8'

7

153

8'

8

152

8

7

151

8'

8'

150

9'

8

149

8

7'

148

8

7

+32-T.P.-20

+93-H.T.P.-17'-23'

Cult.

+26-T.P.-20'

+91-Fc.-20'

+75-A.R.d.

+95-T.P.-20

+81-Ent

+65-T.P.-20'

+25-R.H.Q.-80'

+46-T.P.-20'

+34-R.H.Q.-80'

+01-Ent

161

10'

7

160

10'

8

159

9'

8'

158

8'

8'

157

8

8

156

8

7'

155

8'

8

+99-T.P.-20'

+64-11" T.P.-17'-22'

Cult.

+72-T.P.-20'

+83-T.P.-20'

+93-T.P.-20'

+02-T.P.-20'

Cult.

+11-T.P.-20'

+22-T.P.-20'

168

9'

6'

167

10

4'

166

10

4

165

109-R Bellairs Ave

164

10'

4'

163

9'

6'

162

8'

6

+68-T.P.-21'

+75- $\frac{7}{8}$ " T.P.-18'-23'
F.C. Cor. 18'

F.C.-21'

+88-T.P.-20

+90-Swamp-40'

+05-Ent.

Swamp-48'

+95-T.P.-20'

Water

+90-F.C. Cor.-21'

+86-T.P.-19'

+00-T.P.-20'

+20-T.P.-20'

+41-T.P.-20'

Culch

175 109-18" X 36' C.M.

7' 15' 21' 9'

174

10'

7'

173

10'

7'

172

10'

7'

171

10'

8'

170

11'

8'

169

11'

6'

+58- Fc Cor- 26'
+59- Range Tie
+61- Range Tie
+55- Fc Cor- 26'
+40- Swamp 100'

Fc- 26'

Fc- 25'

Fc- 26'
+91- End Swamp 50'

Beg. Fc- 27' Swamp 50-120'

+65- Swamp- 31'

1/4-S-F +78-T.P.-22'
44'
+62-Fc Cor- 32'
NW Cor. Ho- 74'

+63-E. End 12' G.M.-23'
+90-41-T.P.-19-25'
+89-W. End 12' G.M.-24'

+50-Swamp 80'

T.P.- 22 Fc- 17'
Δ in Swamp- 29'

+12-P.P.- 22'
Swamp- 26- Fc- 18'

+22-T.P.- 21'

Swamp- 28- Fc- 19'

+39-T.P.- 21'

Swamp- 50- Fc- 21'

+43-T.P.- 21'

+56-T.P.- 20'

Fc- 21'

182

8'

10'

+ 60 - 18" x 84" C.M.

181

9'

10'

180

9'

9'

179

9'

10'

178

8'

10'

177

8'

11'

176

9'

11'

+98-H.T.P.-17-25'
End Swamp

Swamp- FG-26'

+70-T.P.-22'

+46-E.End Culm 29'

+416-90' FG-26'

+32-T.P.-22'

FG-31'

+50-FG-44

+12-T.P.-22'
FG-31'

+31-FG Cor-28'

+54-T.P.-22'

FG Cor-28' +91-80' with 35
+85-End

+67-T.P.-22'

+09-End
+04-FG Cor 32'

+87-Culm-23'

+89-FG Cor-29'

+63-Rangitic

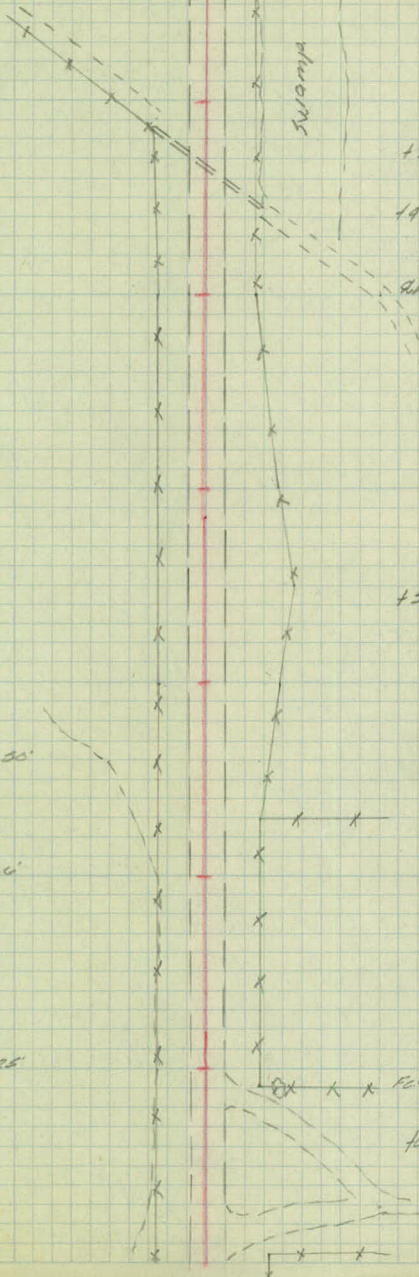
+10-End
FG-25'

FG-24'

+79-End
+60-End Swamp-20'

Swamp-22-FG-26'

Swamp-19-FG-26'



189

10'

8'

188

8'

9'

187

10'

9'

186

8'

10'

185

8'

10'

184

8'

10'

183

8'

10'

+31-T.P.-23'

+06-T.P.-22'
Fc-27'

Pothole-20-100'

Fc-27'

+80-T.P.-23'

+20-Pothole-18'

+68-Ent.

+47-T.P.-22'

+68-Fc.Cac.-20'

+21-T.P.-22'

Fc-26'

+38.35 = Edge Riv.
100' 45'

191

33'

11'

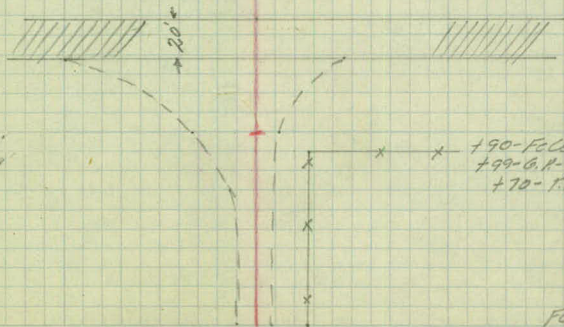
+70- 12'

190

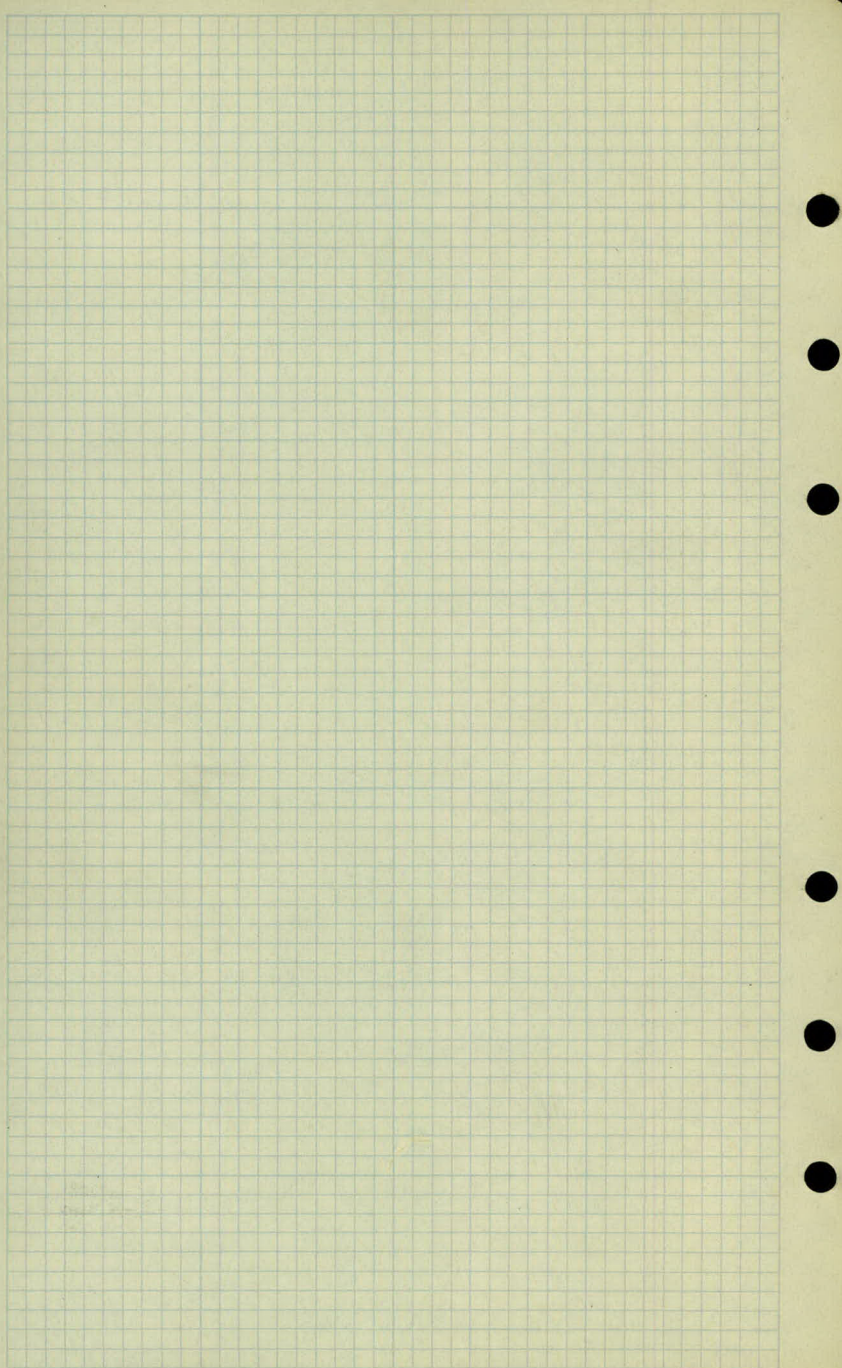
10'

8'

+88-T.P.-57'
+82-G.P.-53'



+90-F.C.-27'
+99-G.P.-33'
+70-T.P.-24'



16
Cross-Sections

Sta.	+	-	Elev.
B.M.	0.11	892.09	891.98
5.21	885.67	11.63	880.46
7.77	884.95	8.49	877.18
13.23	897.59	0.61	884.34
7.07	904.45	0.19	897.38

BM		2.04	902.41	
12.82	908.97	8.30	896.15	
13.58	922.33	0.22	908.75	
11.80	933.71	0.42	921.91	
		0.16	933.65	B.M
4.87	934.21	4.37	929.34	
4.08	938.00	0.29	933.92	
		9.76	928.24	B.M
0.78	925.82	12.96	925.04	
13.68	934.89	4.61	921.21	
9.94	944.33	0.50	934.39	
		2.48	941.85	
12.50	949.13	7.70	936.63	
		2.27	946.86	
BM				

Lt. 2 Rt.

R.R. Spike in T.P. #7 1/2 Lt. Sta.

on S.E. Cor. Foundation N.P.R.B.

H. Pole 74t

Mont.

" Pole Lt 90+85

Station + π - Elev.

Cross sections.

Sta.	T	T	-	Elev.
B.M.	0.02			891.98

38+64

38+78 E

38+92

39+20

485

40+0

27.

2

127.

R.R. spike in T.P. # 7 1/2

$\begin{array}{r} 3.30 \\ - \end{array}$

$\frac{58}{24}$

$\frac{46}{45}$

$\frac{55}{83}$

$\frac{50}{84}$

$\frac{5.3}{96}$

Born

3.0	3.3	3.8	5.5	49	5.2
<u>20</u>		<u>18</u>	61	62 Barn	73

29 35 49 53 49 50
30 Pau. 31 52 53 - Barn 62

	$\frac{29}{43}$	$\frac{38}{16}$	$\frac{44}{-}$	$\frac{5.4}{22}$	$\frac{6.0}{36}$	$\frac{5.4}{37}$	$\frac{5.4}{47}$	$\frac{6.3}{62}$
PAU						Bern		

$\frac{41}{56}$ $\frac{49}{44}$ Berm $\frac{60}{23}$ $\frac{66}{22}$ $\frac{65}{10}$ $\frac{65}{-}$ $\frac{73}{13}$ $\frac{69}{14}$ Berm $\frac{72}{24}$ $\frac{76}{25}$ $\frac{77}{50}$

(end)

$$\begin{array}{r} 85 \\ 73 \end{array} \quad \begin{array}{r} 79 \\ 48 \end{array} \quad \begin{array}{r} 67 \\ 23 \end{array} \quad \begin{array}{r} 69 \\ 12 \end{array} \quad \begin{array}{r} 75 \\ 12 \end{array} \quad \begin{array}{r} 8.0 \\ 16 \end{array} \quad \begin{array}{r} 80 \\ 41 \end{array} \quad \begin{array}{r} 78 \\ 50 \end{array}$$

Station

+

A

-

Elev

Lt.

Z

Rt.

Sta.

+

A

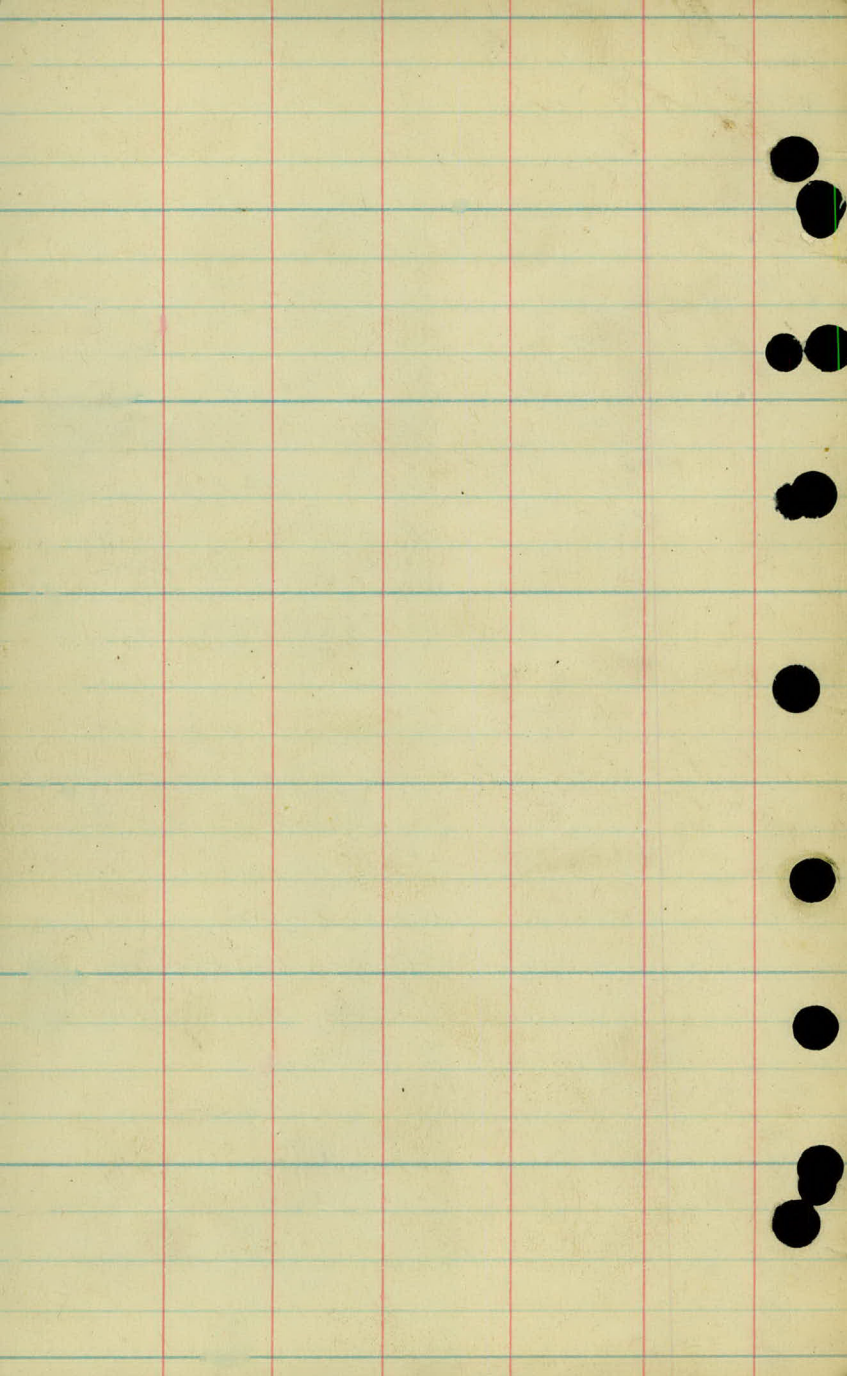
-

Elev.

H.

d

H.



Co. Rd. "D"

Bench Levels.

	+	x	-	Elev.	
B.M.	11.19	903.77	✓		891.98
T.P.	8.46	911.74	0.99	903.28	✓
T.P.	13.39	917.27	7.86	903.88	✓
B.M.			6.78	910.29	✓
T.P.	13.39	930.16	0.30	916.77	✓
T.P.	13.62	943.46	0.32	929.89	✓
B.M.	3.21	945.37	1.30	942.16	✓
T.P.	0.24	933.65	11.96	933.41	✓
				925.99	✓
B.M.	0.35	926.00	8.00	925.65	✓
			0.46	925.54	✓
				925.88	✓

Lapic Bench Elev. 0.94

925.88
54
39

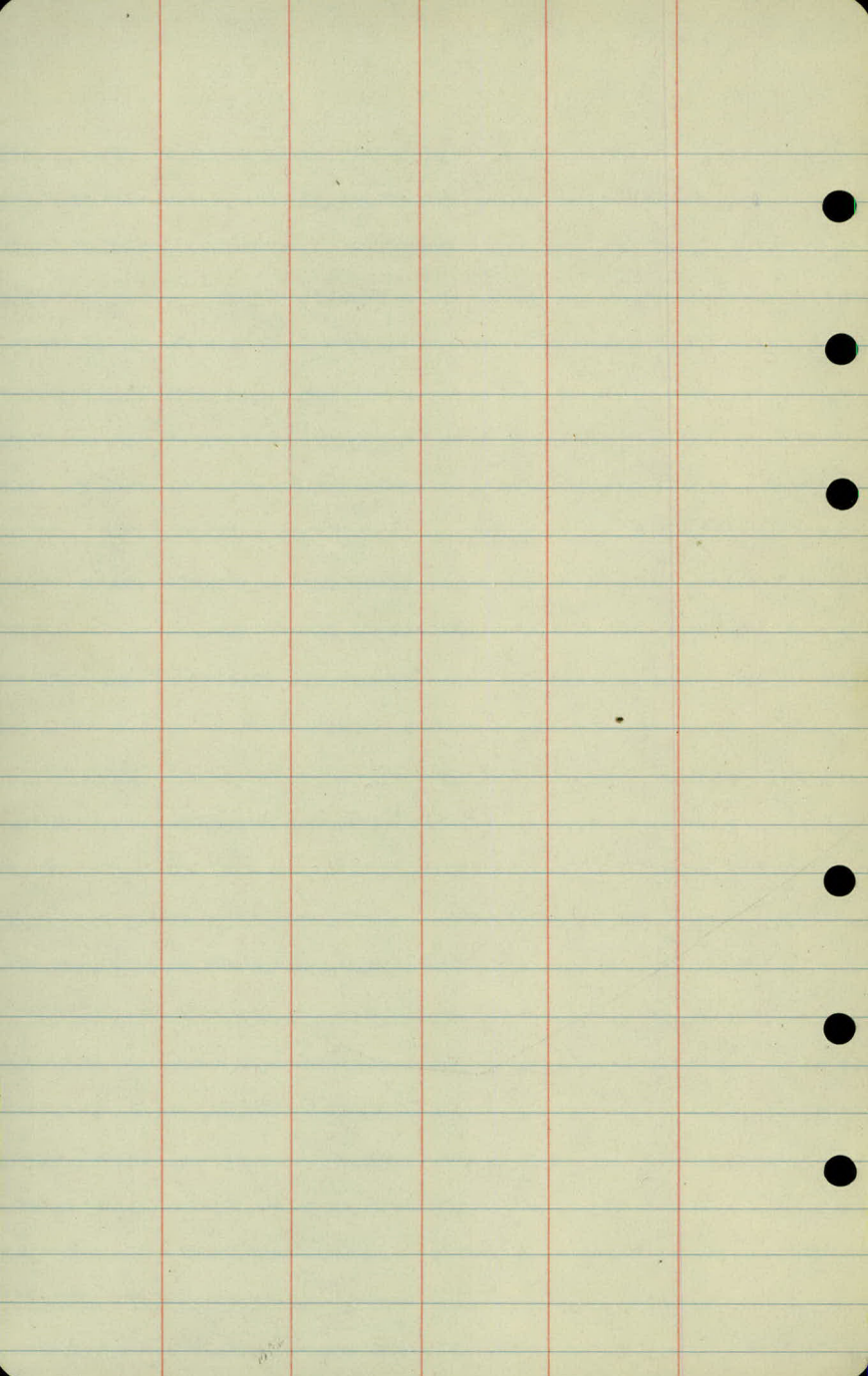
Spl in RR $\frac{27}{2}$ 271156 37122

Spike in 15th Oak - 34' Rt 26104

Top Belt Spike 4. 1818266

Top Mant 613906

$$\begin{array}{r} 16 \\ 34 \\ \hline 50 \end{array}$$



Xsections

Sta

+

K

-

Elev

B.M.

1.52

727.90

725.88

0 + 00

to top board

735.0

+50

24.9

1

24.0

+50

23.4

2

22.9

+50

22.1

3

21.2

+35

20.8

+70

20.5

4

20.5

+50

21.4

Lt

d

Rt.

Spt. 12, Gully Pole S.W. Cor. 29600 - 1/2"

$\frac{22}{100}$	$\frac{23}{50}$	$\frac{24}{50}$	$\frac{23}{50}$	$\frac{20}{100}$
------------------	-----------------	-----------------	-----------------	------------------

$\frac{23}{50}$	$\frac{27}{16}$	$\frac{32}{15}$	$\frac{29}{10}$	$\frac{25}{10}$	$\frac{31}{19}$	$\frac{32}{18}$	$\frac{22}{20}$	$\frac{21}{39}$	$\frac{27}{39}$	$\frac{20}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{30}{50}$	$\frac{31}{15}$	$\frac{37}{12}$	$\frac{37}{8}$	$\frac{39}{12}$	$\frac{39}{16}$	$\frac{43}{18}$	$\frac{40}{18}$	$\frac{44}{34}$	$\frac{53}{38}$	$\frac{57}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{34}{50}$	$\frac{39}{17}$	$\frac{45}{13}$	$\frac{43}{8}$	$\frac{40}{11}$	$\frac{46}{14}$	$\frac{48}{29}$	$\frac{53}{38}$	$\frac{78}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{31}{50}$	$\frac{45}{21}$	$\frac{60}{17}$	$\frac{49}{9}$	$\frac{48}{9}$	$\frac{49}{14}$	$\frac{54}{20}$	$\frac{70}{34}$	$\frac{76}{39}$	$\frac{75}{39}$	$\frac{85}{39}$	$\frac{90}{50}$
-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{34}{50}$	$\frac{42}{29}$	$\frac{50}{20}$	$\frac{57}{17}$	$\frac{55}{8}$	$\frac{53}{11}$	$\frac{56}{9}$	$\frac{58}{12}$	$\frac{85}{23}$	$\frac{89}{37}$	$\frac{93}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{81}{23}$	$\frac{87}{15}$	$\frac{66}{9}$	$\frac{64}{7}$	$\frac{62}{7}$	$\frac{65}{9}$	$\frac{69}{14}$	$\frac{93}{19}$	$\frac{111}{39}$	$\frac{113}{50}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	----------------	-----------------	-----------------	------------------	------------------

$\frac{100}{50}$	$\frac{105}{24}$	$\frac{111}{26}$	$\frac{112}{17}$	$\frac{71}{11}$	$\frac{68}{7}$	$\frac{66}{11}$	$\frac{68}{9}$	$\frac{71}{12}$	$\frac{129}{24}$	$\frac{134}{32}$	$\frac{126}{40}$	$\frac{127}{50}$
------------------	------------------	------------------	------------------	-----------------	----------------	-----------------	----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{106}{50}$	$\frac{114}{28}$	$\frac{116}{17}$	$\frac{75}{10}$	$\frac{71}{7}$	$\frac{69}{11}$	$\frac{73}{9}$	$\frac{76}{13}$	$\frac{149}{26}$	$\frac{143}{39}$	$\frac{139}{50}$
------------------	------------------	------------------	-----------------	----------------	-----------------	----------------	-----------------	------------------	------------------	------------------

1282
Gully

1512
Gully

$\frac{100}{50}$	$\frac{108}{37}$	$\frac{115}{19}$	$\frac{75}{11}$	$\frac{72}{8}$	$\frac{69}{11}$	$\frac{72}{9}$	$\frac{76}{12}$	$\frac{139}{25}$	$\frac{130}{35}$	$\frac{128}{50}$
------------------	------------------	------------------	-----------------	----------------	-----------------	----------------	-----------------	------------------	------------------	------------------

$\frac{89}{50}$	$\frac{99}{24}$	$\frac{109}{18}$	$\frac{66}{12}$	$\frac{62}{7}$	$\frac{60}{11}$	$\frac{64}{8}$	$\frac{67}{13}$	$\frac{144}{27}$	$\frac{146}{50}$
-----------------	-----------------	------------------	-----------------	----------------	-----------------	----------------	-----------------	------------------	------------------

Sta	+	π	-	Elev.
		922.40		
5				922.6
T.P.	12.64	935.49 ✓	4.55	922.85 ✓
+50				28.8
6				24.9
+50				25.8
B.M.			950	925.99 ✓
7				26.4
+14				26.5
+50				26.5
8				26.3
+50				26.2
T.P.	4.67	930.52 ✓	964	925.85 ✓
9				25.8
+30				25.4

925.99

Lt

R

Rt

$\frac{70}{50}$	$\frac{80}{25}$	$\frac{95}{18}$	$\frac{53}{11}$	$\frac{99}{7}$	$\frac{48}{-}$	$\frac{52}{8}$	$\frac{57}{13}$	$\frac{19.7}{28}$	$\frac{128}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-------------------	------------------

Top Cor Fe Post Rt Lt

$\frac{119}{50}$	$\frac{132}{24}$	$\frac{146}{16}$	$\frac{123}{11}$	$\frac{119}{7}$	$\frac{117}{-}$	$\frac{119}{8}$	$\frac{124}{13}$	$\frac{170}{21}$	$\frac{200}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{65}{50}$	$\frac{86}{31}$	$\frac{74}{27}$	$\frac{87}{17}$	$\frac{114}{14}$	$\frac{109}{7}$	$\frac{106}{-}$	$\frac{108}{8}$	$\frac{111}{12}$	$\frac{105}{17}$	$\frac{110}{24}$	$\frac{150}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{20}{50}$	$\frac{83}{31}$	$\frac{25}{27}$	$\frac{104}{17}$	$\frac{100}{8}$	$\frac{97}{-}$	$\frac{100}{8}$	$\frac{107}{15}$	$\frac{42}{21}$	$\frac{71}{27}$	$\frac{84}{50}$
-----------------	-----------------	-----------------	------------------	-----------------	----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{18}{50}$	$\frac{28}{28}$	$\frac{97}{18}$	$\frac{94}{8}$	$\frac{91}{-}$	$\frac{93}{8}$	$\frac{96}{16}$	$\frac{68}{20}$	$\frac{74}{28}$	$\frac{82}{50}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{27}{50}$	$\frac{40}{28}$	$\frac{95}{19}$	$\frac{92}{8}$	$\frac{90}{-}$	$\frac{92}{10}$	$\frac{94}{25}$	$\frac{97}{50}$
-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{46}{50}$	$\frac{53}{25}$	$\frac{96}{18}$	$\frac{92}{8}$	$\frac{90}{-}$	$\frac{93}{8}$	$\frac{98}{15}$	$\frac{94}{16}$	$\frac{92}{33}$	$\frac{94}{50}$
-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{54}{50}$	$\frac{57}{30}$	$\frac{57}{20}$	$\frac{98}{15}$	$\frac{95}{8}$	$\frac{92}{-}$	$\frac{95}{9}$	$\frac{98}{15}$	$\frac{92}{17}$	$\frac{91}{34}$	$\frac{97}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{72}{50}$	$\frac{75}{28}$	$\frac{86}{16}$	$\frac{99}{14}$	$\frac{95}{8}$	$\frac{93}{-}$	$\frac{96}{8}$	$\frac{100}{14}$	$\frac{112}{16}$	$\frac{119}{28}$	$\frac{136}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	------------------	------------------	------------------	------------------

$\frac{56}{50}$	$\frac{67}{25}$	$\frac{72}{17}$	$\frac{52}{13}$	$\frac{49}{8}$	$\frac{47}{-}$	$\frac{80}{10}$	$\frac{56}{13}$	$\frac{83}{17}$	$\frac{86}{25}$	$\frac{97}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{68}{50}$	$\frac{77}{27}$	$\frac{83}{23}$	$\frac{83}{18}$	$\frac{55}{13}$	$\frac{52}{8}$	$\frac{49}{-}$	$\frac{52}{9}$	$\frac{56}{13}$	$\frac{103}{22}$	$\frac{116}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	------------------	------------------

Sta	+	π	-	Elev
		930.52		
10				925.3
	+70			25.8
11				26.3
T.P.	11.81	940.54 ✓	1.79	928.73 ✓
	+90			26.9
	+70			27.8
12				28.7
	+35			29.4
	+70			30.4
13				30.9
	+93			31.9
	+75			32.5

Lt

K

Rt

$$\frac{8.2}{50} \quad \frac{9.2}{30} \quad \frac{9.8}{20} \quad \frac{5.6}{12} \quad \frac{5.4}{8} \quad \frac{5.2}{5} \quad \frac{5.6}{9} \quad \frac{6.5}{16} \quad \frac{11.8}{25} \quad \frac{11.6}{50}$$

$$\frac{9.1}{50} \quad \frac{10.0}{30} \quad \frac{9.7}{20} \quad \frac{5.5}{13} \quad \frac{4.9}{8} \quad \frac{4.7}{5} \quad \frac{5.0}{8} \quad \frac{5.9}{16} \quad \frac{9.2}{21} \quad \frac{9.0}{27} \quad \frac{8.2}{30} \quad \frac{8.3}{50}$$

$$\frac{5.4}{50} \quad \frac{5.4}{30} \quad \frac{5.5}{22} \quad \frac{5.9}{17} \quad \frac{9.6}{11} \quad \frac{9.4}{7} \quad \frac{4.2}{8} \quad \frac{4.4}{8} \quad \frac{4.9}{14} \quad \frac{6.6}{18} \quad \frac{6.5}{30} \quad \frac{6.5}{50}$$

$$\frac{10.8}{50} \quad \frac{10.6}{26} \quad \frac{12.0}{20} \quad \frac{14.0}{15} \quad \frac{13.8}{7} \quad \frac{18.6}{5} \quad \frac{14.0}{9} \quad \frac{14.7}{18} \quad \frac{9.5}{25} \quad \frac{11.6}{31} \quad \frac{13.0}{14} \quad \frac{12.8}{50}$$

$$\frac{5.8}{50} \quad \frac{5.7}{30} \quad \frac{12.5}{19} \quad \frac{12.0}{14} \quad \frac{12.8}{8} \quad \frac{12.7}{5} \quad \frac{13.0}{9} \quad \frac{13.3}{12} \quad \frac{14.1}{18} \quad \frac{5.1}{29} \quad \frac{9.3}{50}$$

$$\frac{5.5}{50} \quad \frac{5.8}{32} \quad \frac{12.2}{16} \quad \frac{12.1}{8} \quad \frac{11.8}{5} \quad \frac{12.2}{9} \quad \frac{12.3}{14} \quad \frac{12.6}{19} \quad \frac{3.5}{29} \quad \frac{6.2}{50}$$

$$\frac{15.6}{50} \quad \frac{6.7}{30} \quad \frac{10.3}{24} \quad \frac{10.3}{19} \quad \frac{11.3}{15} \quad \frac{11.2}{8} \quad \frac{10.9}{5} \quad \frac{11.1}{9} \quad \frac{11.4}{17} \quad \frac{3.3}{27} \quad \frac{6.0}{50}$$

$$\frac{11.1}{50} \quad \frac{8.2}{27} \quad \frac{7.5}{20} \quad \frac{10.5}{14} \quad \frac{10.3}{9} \quad \frac{10.1}{5} \quad \frac{10.6}{8} \quad \frac{10.7}{16} \quad \frac{9.6}{25} \quad \frac{7.1}{50}$$

$$\frac{14.3}{50} \quad \frac{12.0}{28} \quad \frac{10.0}{20} \quad \frac{10.1}{13} \quad \frac{9.7}{8} \quad \frac{9.6}{5} \quad \frac{9.8}{9} \quad \frac{10.0}{14} \quad \frac{6.7}{21} \quad \frac{8.4}{50}$$

$$\frac{15.5}{50} \quad \frac{15.4}{29} \quad \frac{14.7}{25} \quad \frac{13.0}{20} \quad \frac{9.2}{12} \quad \frac{8.8}{8} \quad \frac{8.6}{5} \quad \frac{5.8}{8} \quad \frac{8.1}{15} \quad \frac{8.7}{25} \quad \frac{10.0}{50}$$

$$\frac{14.1}{50} \quad \frac{14.0}{29} \quad \frac{11.3}{18} \quad \frac{8.4}{12} \quad \frac{8.2}{7} \quad \frac{8.0}{5} \quad \frac{8.1}{8} \quad \frac{8.9}{17} \quad \frac{8.6}{19} \quad \frac{11.1}{50}$$

Sta.	+	π	-	Elev.
		940.59		
14				933.0
	+ 92			33.9
	+ 75			34.7
15				35.3
	+ 35			36.3
	+ 66			37.0
T.P.	10.20	948.25 ✓	2.99	938.05 ✓
16				38.0
	+ 96			39.7
17				41.2
	+ 29			41.6
	+ 75			42.5
T.P.	9.67	953.58	4.34	943.91

Lt

K

Rt

$$\frac{12.3}{50} \quad \frac{11.6}{2.8} \quad \frac{10.4}{19} \quad \frac{9.8}{15} \quad \frac{8.3}{13} \quad \frac{7.7}{8} \quad \frac{7.5}{8} \quad \frac{7.7}{8} \quad \frac{7.9}{17} \quad \frac{10.0}{23} \quad \frac{12.0}{50}$$

$$\frac{5.3}{50} \quad \frac{6.5}{29} \quad \frac{6.1}{27} \quad \frac{7.6}{17} \quad \frac{7.1}{14} \quad \frac{6.9}{8} \quad \frac{6.6}{8} \quad \frac{6.9}{8} \quad \frac{7.2}{12} \quad \frac{8.6}{15} \quad \frac{9.4}{18} \quad \frac{11.0}{24} \quad \frac{13.0}{50}$$

$$\frac{2.3}{50} \quad \frac{3.6}{36} \quad \frac{4.8}{20} \quad \frac{6.3}{15} \quad \frac{6.0}{8} \quad \frac{5.8}{8} \quad \frac{6.1}{8} \quad \frac{6.6}{13} \quad \frac{8.8}{21} \quad \frac{12.1}{50}$$

$$\frac{2.1}{50} \quad \frac{4.9}{29} \quad \frac{5.2}{26} \quad \frac{6.0}{18} \quad \frac{5.5}{12} \quad \frac{5.3}{8} \quad \frac{5.2}{8} \quad \frac{5.5}{8} \quad \frac{5.7}{11} \quad \frac{9.8}{20} \quad \frac{11.0}{37} \quad \frac{11.9}{50}$$

$$\frac{5.9}{50} \quad \frac{7.6}{29} \quad \frac{7.8}{17} \quad \frac{4.7}{13} \quad \frac{4.3}{8} \quad \frac{4.2}{8} \quad \frac{4.6}{8} \quad \frac{4.8}{11} \quad \frac{9.9}{20} \quad \frac{11.4}{29} \quad \frac{13.3}{50}$$

$$\frac{5.6}{50} \quad \frac{6.2}{32} \quad \frac{6.5}{19} \quad \frac{4.2}{10} \quad \frac{3.6}{8} \quad \frac{3.5}{8} \quad \frac{2.7}{8} \quad \frac{4.9}{14} \quad \frac{8.5}{20} \quad \frac{10.1}{24} \quad \frac{11.2}{50}$$

T.R. Lt 15 + 70

$$\frac{5.9}{50} \quad \frac{10.5}{31} \quad \frac{11.0}{18} \quad \frac{10.3}{15} \quad \frac{10.9}{13} \quad \frac{10.5}{8} \quad \frac{10.3}{8} \quad \frac{10.5}{8} \quad \frac{10.6}{11} \quad \frac{11.1}{16} \quad \frac{11.6}{26} \quad \frac{12.0}{50}$$

$$\frac{6.8}{50} \quad \frac{7.2}{30} \quad \frac{6.9}{18} \quad \frac{9.0}{13} \quad \frac{8.6}{8} \quad \frac{8.6}{8} \quad \frac{8.7}{8} \quad \frac{9.0}{13} \quad \frac{5.7}{19} \quad \frac{6.3}{25} \quad \frac{5.7}{50}$$

$$\frac{12.4}{50} \quad \frac{11.4}{28} \quad \frac{9.0}{21} \quad \frac{7.7}{12} \quad \frac{7.5}{9} \quad \frac{7.1}{8} \quad \frac{6.9}{7} \quad \frac{6.8}{12} \quad \frac{7.5}{15} \quad \frac{6.2}{21} \quad \frac{4.9}{50} \quad \frac{13.4}{50}$$

$$\frac{12.4}{50} \quad \frac{11.2}{32} \quad \frac{9.7}{25} \quad \frac{7.8}{19} \quad \frac{7.4}{12} \quad \frac{7.1}{8} \quad \frac{6.7}{8} \quad \frac{6.8}{8} \quad \frac{7.0}{11} \quad \frac{7.4}{14} \quad \frac{5.0}{23} \quad \frac{4.0}{50}$$

$$\frac{+2.4}{50} \quad \frac{+2.7}{32} \quad \frac{+4.3}{24} \quad \frac{6.6}{16} \quad \frac{5.9}{8} \quad \frac{5.8}{8} \quad \frac{6.1}{8} \quad \frac{5.9}{23} \quad \frac{+6.3}{36} \quad \frac{+8.5}{50} \quad \frac{+4.3}{75}$$

Sta + K - Elev.

753.58 ✓

18

943.1

+30

43.3

B.M.

7.59

752.09 ✓

10.99

942.59 ✓

942.50 ✓

19

42.0

+35

40.7

+20

39.2

20

37.6 ✓

T.P.

1.85

740.25 ✓

13.69

938.90 ✓

+65

34.6

21

32.9

+22

31.3

+68

29.6

T.P.

2.23

730.16 ✓

12.32

927.93 ✓

22

28.1

14

2

24

$\frac{66}{50} \frac{5.3}{32} \frac{3.5}{24} \frac{10.9}{17} \frac{10.6}{9} \frac{10.5}{8} \frac{10.8}{6} \frac{11.4}{15} \frac{10.2}{19} \frac{9.8}{26} \frac{+4.2}{72} \frac{+4.5}{75} \frac{+4.0}{100}$

$\frac{7.8}{50} \frac{7.2}{37} \frac{5.2}{22} \frac{11.0}{17} \frac{10.5}{8} \frac{10.3}{8} \frac{10.5}{8} \frac{10.7}{12} \frac{12.4}{18} \frac{11.3}{28} \frac{+7.3}{52} \frac{+10.2}{75} \frac{+10.2}{100}$

Top Bolt 18482

$\frac{9.1}{50} \frac{7.8}{30} \frac{6.1}{22} \frac{10.8}{15} \frac{10.5}{8} \frac{10.1}{8} \frac{10.3}{8} \frac{10.2}{19} \frac{6.8}{52} \frac{+12.8}{56.0} \frac{+14.5}{75} \frac{+15.3}{100}$

$\frac{8.3}{50} \frac{7.4}{35} \frac{5.4}{25} \frac{10.0}{18} \frac{11.7}{7} \frac{11.4}{8} \frac{11.5}{8} \frac{11.7}{13} \frac{10.7}{15} \frac{6.0}{83} \frac{+15.0}{56} \frac{+16.5}{75} \frac{+17.8}{100}$

$\frac{6.6}{50} \frac{4.8}{36} \frac{3.7}{27} \frac{12.1}{17} \frac{13.2}{8} \frac{12.7}{7} \frac{13.2}{13} \frac{13.4}{25} \frac{12.0}{25} \frac{+14.6}{35} \frac{+16.5}{66} \frac{+18.1}{80} \frac{+19.3}{100}$

$\frac{7.3}{50} \frac{5.5}{29} \frac{14.1}{21} \frac{14.6}{8} \frac{14.5}{8} \frac{14.9}{8} \frac{15.3}{13} \frac{13.8}{17} \frac{11.8}{27} \frac{+7.4}{52} \frac{+12.4}{75} \frac{+12.1}{100}$

$\frac{3.7}{50} \frac{2.6}{28} \frac{6.2}{11} \frac{5.8}{7} \frac{5.7}{8} \frac{6.1}{13} \frac{6.4}{20} \frac{5.1}{29} \frac{+1.3}{50} \frac{+1.7}{50} \frac{+6.6}{75}$

$\frac{4.4}{50} \frac{9.8}{36} \frac{3.5}{21} \frac{8.0}{15} \frac{7.6}{7} \frac{7.4}{8} \frac{7.7}{13} \frac{8.0}{22} \frac{2.0}{30} \frac{1.6}{30} \frac{0.9}{50}$

$\frac{7.6}{50} \frac{5.8}{29} \frac{6.4}{21} \frac{9.3}{14} \frac{9.2}{7} \frac{9.0}{8} \frac{9.3}{13} \frac{2.6}{21} \frac{3.7}{21} \frac{2.6}{40} \frac{3.7}{50}$

$\frac{14.7}{50} \frac{12.4}{24} \frac{11.5}{18} \frac{10.8}{7} \frac{10.7}{8} \frac{11.1}{8} \frac{11.3}{17} \frac{11.3}{50}$

$\frac{8.3}{50} \frac{7.2}{31} \frac{6.0}{16} \frac{3.0}{14} \frac{2.3}{9} \frac{2.1}{8} \frac{2.5}{16} \frac{3.2}{19} \frac{3.8}{23} \frac{5.4}{30} \frac{5.1}{30}$

Sta.

+

π

-

Elev.

920.16

22 +30

925.7

23

23.4

T.P.

2.00

922.06 ✓

10.10

920.06 ✓

+70

20.4

24

19.3

+29

18.1

+59

16.8

+73

16.1

25

14.9

+50

12.6 ✓

T.P.

1.26

912.89 ✓

10.93

911.63 ✓

26

10.3

+26

09.2

B.M.

2.29

910.60 ✓

(910.63)

Lt.

A

Rt.

$$\frac{101}{50} \quad \frac{116}{35} \quad \frac{120}{23} \quad \frac{52}{14} \quad \frac{17}{9} \quad \frac{45}{9} \quad \frac{47}{16} \quad \frac{53}{12} \quad \frac{128}{27} \quad \frac{131}{50}$$

$$\frac{98}{50} \quad \frac{120}{35} \quad \frac{130}{25} \quad \frac{72}{13} \quad \frac{69}{9} \quad \frac{48}{8} \quad \frac{72}{8} \quad \frac{83}{16} \quad \frac{147}{28} \quad \frac{149}{50}$$

$$\frac{123}{50} \quad \frac{117}{29} \quad \frac{27}{14} \quad \frac{19}{9} \quad \frac{17}{8} \quad \frac{20}{17} \quad \frac{31}{17} \quad \frac{76}{26} \quad \frac{79}{32} \quad \frac{67}{50}$$

$$\frac{141}{50} \quad \frac{145}{33} \quad \frac{113}{24} \quad \frac{40}{14} \quad \frac{30}{9} \quad \frac{28}{80} \quad \frac{31}{7} \quad \frac{41}{18} \quad \frac{60}{23} \quad \frac{56}{30} \quad \frac{50}{50}$$

$$\frac{173}{50} \quad \frac{160}{36} \quad \frac{123}{26} \quad \frac{50}{14} \quad \frac{12}{8} \quad \frac{40}{8} \quad \frac{43}{7} \quad \frac{47}{16} \quad \frac{58}{20} \quad \frac{40}{32} \quad \frac{29}{50}$$

$$\frac{157}{50} \quad \frac{137}{27} \quad \frac{53}{13} \quad \frac{55}{9} \quad \frac{53}{6} \quad \frac{56}{19} \quad \frac{60}{34} \quad \frac{32}{34} \quad \frac{22}{50}$$

$$\frac{113}{50} \quad \frac{93}{43} \quad \frac{63}{10} \quad \frac{60}{6} \quad \frac{64}{6} \quad \frac{67}{10} \quad \frac{57}{18} \quad \frac{25}{23} \quad \frac{17}{50}$$

$$\frac{124}{50} \quad \frac{106}{40} \quad \frac{93}{18} \quad \frac{77}{15} \quad \frac{73}{8} \quad \frac{72}{6} \quad \frac{75}{6} \quad \frac{77}{10} \quad \frac{60}{16} \quad \frac{35}{25} \quad \frac{25}{37} \quad \frac{17}{50}$$

$$\frac{74}{50} \quad \frac{87}{36} \quad \frac{102}{26} \quad \frac{115}{22} \quad \frac{115}{25} \quad \frac{97}{15} \quad \frac{96}{8} \quad \frac{95}{6} \quad \frac{97}{9} \quad \frac{101}{18} \quad \frac{104}{33} \quad \frac{71}{33} \quad \frac{70}{50}$$

$$\frac{33}{50} \quad \frac{33}{24} \quad \frac{47}{22} \quad \frac{47}{20} \quad \frac{28}{16} \quad \frac{28}{8} \quad \frac{26}{7} \quad \frac{28}{7} \quad \frac{29}{13} \quad \frac{46}{20} \quad \frac{47}{25} \quad \frac{39}{50}$$

$$\frac{38}{50} \quad \frac{36}{31} \quad \frac{53}{21} \quad \frac{43}{15} \quad \frac{39}{7} \quad \frac{37}{7} \quad \frac{40}{9} \quad \frac{91}{13} \quad \frac{43}{20} \quad \frac{57}{33} \quad \frac{50}{33} \quad \frac{49}{50}$$

Sta	+	π	-	Elev.
		912.29		
26	+62			907.7 ✓
T.P.	2.83	908.20 ✓	692	905.97 ✓
27				06.0
	+59			03.7
28				03.3
	+37			03.3
	+70			03.6
29				04.0 ✓
T.P.	11.50	716.08 ✓	422	904.58 ✓
	+35			04.8
	+75			05.5
30				05.8
	+62			06.3

Lt.

R.

Rt.

$\frac{75}{50}$	$\frac{90}{46}$	$\frac{113}{87}$	$\frac{103}{23}$	$\frac{59}{14}$	$\frac{55}{8}$	$\frac{52}{-}$	$\frac{54}{7}$	$\frac{63}{15}$	$\frac{73}{20}$	$\frac{85}{28}$	$\frac{97}{45}$	$\frac{98}{50}$
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Totalled to 27100

$\frac{120}{50}$	$\frac{112}{32}$	$\frac{108}{25}$	$\frac{36}{14}$	$\frac{31}{8}$	$\frac{28}{-}$	$\frac{30}{7}$	$\frac{34}{12}$	$\frac{91}{23}$	$\frac{89}{39}$	$\frac{89}{50}$
------------------	------------------	------------------	-----------------	----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{134}{50}$	$\frac{131}{32}$	$\frac{121}{23}$	$\frac{59}{19}$	$\frac{55}{8}$	$\frac{51}{-}$	$\frac{54}{7}$	$\frac{55}{13}$	$\frac{121}{29}$	$\frac{120}{50}$
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$\frac{117}{50}$	$\frac{126}{28}$	$\frac{122}{22}$	$\frac{61}{18}$	$\frac{58}{8}$	$\frac{55}{-}$	$\frac{57}{7}$	$\frac{60}{14}$	$\frac{117}{25}$	$\frac{123}{50}$
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$\frac{86}{50}$	$\frac{104}{32}$	$\frac{102}{22}$	$\frac{62}{19}$	$\frac{57}{8}$	$\frac{55}{-}$	$\frac{59}{7}$	$\frac{60}{19}$	$\frac{123}{24}$	$\frac{125}{50}$
-----------------	------------------	------------------	-----------------	----------------	----------------	----------------	-----------------	------------------	------------------

$\frac{69}{50}$	$\frac{87}{26}$	$\frac{90}{24}$	$\frac{90}{17}$	$\frac{56}{13}$	$\frac{54}{8}$	$\frac{52}{-}$	$\frac{54}{7}$	$\frac{58}{12}$	$\frac{117}{23}$	$\frac{120}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	------------------	------------------

$\frac{72}{50}$	$\frac{76}{37}$	$\frac{82}{22}$	$\frac{82}{17}$	$\frac{53}{12}$	$\frac{52}{9}$	$\frac{48}{-}$	$\frac{49}{6}$	$\frac{52}{12}$	$\frac{108}{22}$	$\frac{114}{27}$	$\frac{107}{36}$	$\frac{104}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{132}{50}$	$\frac{138}{29}$	$\frac{142}{17}$	$\frac{143}{17}$	$\frac{120}{12}$	$\frac{117}{8}$	$\frac{113}{-}$	$\frac{117}{7}$	$\frac{120}{12}$	$\frac{153}{18}$	$\frac{156}{29}$	$\frac{89}{33}$	$\frac{92}{40}$	$\frac{87}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------

$\frac{81}{50}$	$\frac{80}{27}$	$\frac{87}{23}$	$\frac{117}{19}$	$\frac{117}{16}$	$\frac{111}{13}$	$\frac{103}{9}$	$\frac{146}{-}$	$\frac{108}{6}$	$\frac{111}{11}$	$\frac{116}{16}$	$\frac{103}{22}$	$\frac{102}{30}$	$\frac{92}{33}$	$\frac{87}{50}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	-----------------	-----------------

$\frac{59}{50}$	$\frac{55}{40}$	$\frac{62}{28}$	$\frac{114}{18}$	$\frac{114}{16}$	$\frac{107}{13}$	$\frac{107}{9}$	$\frac{143}{-}$	$\frac{103}{10}$	$\frac{108}{14}$	$\frac{83}{19}$	$\frac{85}{31}$	$\frac{63}{34}$	$\frac{61}{50}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------

$\frac{44}{50}$	$\frac{48}{26}$	$\frac{108}{20}$	$\frac{108}{16}$	$\frac{102}{12}$	$\frac{100}{8}$	$\frac{98}{-}$	$\frac{97}{6}$	$\frac{101}{11}$	$\frac{104}{17}$	$\frac{90}{19}$	$\frac{92}{25}$	$\frac{81}{33}$	$\frac{14}{50}$
-----------------	-----------------	------------------	------------------	------------------	-----------------	----------------	----------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------

Sta	+	π	-	Elev
		716.08		
31				906.8
	+17			07.1
	+24			07.1
	+47			07.5
	+56			07.6
32				07.2
	+50			06.7
33				06.5
	+35			06.4
	+43			06.4
34				06.3

Lt

K

Rt

$$\frac{43}{50} \frac{45}{26} \frac{101}{18} \frac{102}{16} \frac{96}{19} \frac{94}{8} \frac{93}{5} \frac{94}{5}$$

$$\frac{97}{15} \frac{24}{27} \frac{17}{34} \frac{13}{50}$$

$$\frac{41}{50} \frac{47}{35} \frac{42}{27} \frac{96}{19} \frac{91}{8} \frac{90}{7} \frac{93}{19} \frac{97}{19} \frac{40}{27} \frac{18}{50}$$

$$\frac{79}{50} \frac{88}{22} \frac{90}{7} \frac{90}{6} \frac{91}{8} \frac{92}{19} \frac{96}{19} \frac{40}{25} \frac{22}{49} \frac{16}{50}$$

$$\frac{82}{50} \frac{81}{32} \frac{89}{21} \frac{88}{7} \frac{86}{6} \frac{84}{16} \frac{87}{25} \frac{49}{37} \frac{37}{37} \frac{24}{50}$$

$$\frac{88}{50} \frac{91}{31} \frac{87}{29} \frac{87}{20} \frac{92}{19} \frac{89}{8} \frac{85}{5} \frac{85}{6} \frac{76}{21} \frac{69}{33} \frac{98}{50}$$

$$\frac{105}{50} \frac{105}{29} \frac{99}{25} \frac{96}{19} \frac{100}{16} \frac{98}{13} \frac{93}{8} \frac{89}{6} \frac{90}{12} \frac{90}{12} \frac{94}{22} \frac{71}{28} \frac{62}{50}$$

$$\frac{100}{50} \frac{103}{31} \frac{103}{19} \frac{106}{17} \frac{105}{14} \frac{99}{13} \frac{96}{9} \frac{94}{5} \frac{95}{16} \frac{95}{16} \frac{103}{19} \frac{103}{22} \frac{85}{29} \frac{76}{50}$$

$$\frac{108}{50} \frac{110}{24} \frac{108}{16} \frac{103}{14} \frac{100}{9} \frac{96}{7} \frac{96}{16} \frac{99}{16} \frac{108}{19} \frac{108}{22} \frac{92}{24} \frac{75}{50}$$

$$\frac{124}{50} \frac{120}{33} \frac{109}{17} \frac{103}{15} \frac{100}{12} \frac{97}{8} \frac{97}{8} \frac{96}{16} \frac{109}{19} \frac{109}{22} \frac{1421}{205} \frac{87}{26} \frac{73}{50}$$

$$\frac{97}{7} \frac{96}{7} \frac{91}{16} \frac{85}{28} \frac{75}{50}$$

$$\frac{98}{5} \frac{99}{12} \frac{97}{26} \frac{74}{38} \frac{63}{50}$$

Sta	+	π	-	Elev
		916.28		
34	+08			906.2 ✓
T.P.	1.49	910.54 ✓	703	909.05 ✓
	+50			05.6
35				04.4
	+35			03.3
	+60			02.3
36				900.5
	+35			898.8 ✓
T.P.			13.65	896.89 ✓
T.P.	12.01	921.06 ✓		909.05
34	+50			05.6
35				04.4 ✓
T.P.	6.02	924.32 ✓	276	918.30 ✓
	+35			03.3

LH

R

RH

$\frac{12.5}{50}$ $\frac{11.5}{29}$ $\frac{10.6}{20}$ $\frac{10.2}{10}$

$\frac{99}{5}$ $\frac{99}{15}$ $\frac{101}{19}$ $\frac{120}{22.5}$ $\frac{121}{22}$ $\frac{122}{27}$ $\frac{72}{30}$ $\frac{59}{30}$ $\frac{45}{50}$

Top G.R. Post Rt

$\frac{6.3}{50}$ $\frac{5.2}{30}$ $\frac{4.8}{29}$ $\frac{5.3}{22}$ $\frac{5.9}{19}$ $\frac{5.4}{11}$ $\frac{4.9}{5}$ $\frac{4.9}{15}$ $\frac{5.1}{18}$ $\frac{7.0}{22}$ $\frac{7.0}{22}$

$\frac{5.9}{50}$ $\frac{3.9}{34}$ $\frac{2.0}{25}$ $\frac{1.8}{30}$ $\frac{1.4}{24}$ $\frac{7.0}{15}$ $\frac{6.7}{11}$ $\frac{4.1}{5}$ $\frac{6.2}{14}$ $\frac{6.3}{14}$ $\frac{7.4}{18}$ $\frac{7.4}{22}$

$\frac{5.5}{50}$ $\frac{5.5}{40}$ $\frac{2.0}{38}$ $\frac{2.0}{36}$ $\frac{2.1}{27}$ $\frac{8.8}{17}$ $\frac{7.7}{10}$ $\frac{7.2}{7}$ $\frac{7.4}{14}$ $\frac{7.4}{14}$ $\frac{8.1}{14}$ $\frac{8.0}{22}$

$\frac{6.9}{50}$ $\frac{3.4}{36}$ $\frac{3.4}{34}$ $\frac{9.1}{27}$ $\frac{9.8}{17}$ $\frac{8.6}{10}$ $\frac{8.2}{7}$ $\frac{8.4}{11}$ $\frac{8.1}{18}$ $\frac{8.2}{22}$ $\frac{8.4}{28}$ $\frac{9.3}{28}$ $\frac{0.0}{33}$

$\frac{12.0}{30}$ $\frac{11.0}{40}$ $\frac{8.9}{34}$ $\frac{11.3}{28}$ $\frac{11.3}{21}$ $\frac{10.8}{18}$ $\frac{10.2}{9}$ $\frac{10.0}{8}$ $\frac{10.3}{15}$ $\frac{10.5}{17}$ $\frac{9.8}{20}$ $\frac{9.5}{25}$ $\frac{7.6}{25}$ $\frac{0.5}{82}$ $\frac{11.0}{50}$ $\frac{12.5}{75}$

$\frac{17.8}{50}$ $\frac{14.9}{32}$ $\frac{13.5}{23}$ $\frac{13.0}{16}$ $\frac{12.4}{13}$ $\frac{12.1}{9}$ $\frac{11.7}{9}$ $\frac{12.0}{9}$ $\frac{12.2}{15}$ $\frac{11.9}{19}$ $\frac{8.3}{23}$ $\frac{4.6}{50}$

Tap stone

Top G.R. Post Rt

$\frac{15.5}{33}$ $\frac{9.2}{30}$ $\frac{7.9}{31}$ $\frac{8.5}{51}$ $\frac{7.3}{57}$ $\frac{6.2}{68}$ $\frac{5.3}{80}$ $\frac{4.4}{87}$ $\frac{3.7}{88}$ $\frac{3.0}{100}$

Roadway

Roadway

$\frac{16.7}{33}$ $\frac{4.6}{37}$ $\frac{3.7}{50}$ $\frac{3.2}{68}$ $\frac{2.5}{73}$ $\frac{2.5}{84}$ $\frac{2.8}{100}$

$\frac{21.0}{40}$ $\frac{5.1}{48}$ $\frac{5.1}{58}$ $\frac{4.1}{88}$ $\frac{4.6}{88}$ $\frac{4.9}{100}$

Sta.	+	π	-	Elev.
		929.32		
35	+60			902.3
T.P.	1.71	912.93 ✓	13.30	911.02 ✓
T.P.	1.07	900.46 ✓	13.59	899.37 ✓
B.M.			2.98	891.98 ✓ (891.98)
36	+70			97.2 ✓
37				95.7 ✓
	+40			93.7 ✓
	+57			92.8 ✓
	+73			92.1 ✓
38				91.0 ✓
T.P.	0.61	891.54 ✓	9.53	890.93 ✓
	+35			89.4 ✓
	+64			88.5 ✓
	+91			85.5 ✓

LL

R

RL

22.0 $\frac{58}{40}$ $\frac{60}{49}$ $\frac{52}{56}$ $\frac{59}{78}$ $\frac{57}{100}$

Sept. 10 AM 4 7 1/2 27.61 37+22

$\frac{98}{50}$ $\frac{100}{27}$ $\frac{55}{19}$ $\frac{40}{19}$ $\frac{37}{8}$ $\frac{33}{9}$ $\frac{36}{11}$ $\frac{35}{21}$ $\frac{42}{26}$ $\frac{35}{50}$ $\frac{00}{50}$

$\frac{103}{50}$ $\frac{111}{25}$ $\frac{64}{16}$ $\frac{5.3}{12}$ $\frac{5.1}{7}$ $\frac{48}{10}$ $\frac{50}{16}$ $\frac{56}{19}$ $\frac{7.2}{28}$ $\frac{7.5}{39}$ $\frac{6.5}{50}$ $\frac{49}{50}$

$\frac{9.3}{50}$ $\frac{115}{28}$ $\frac{102}{22}$ $\frac{77}{16}$ $\frac{6.9}{8}$ $\frac{48}{9}$ $\frac{7.2}{15}$ $\frac{7.7}{25}$ $\frac{12.1}{32}$ $\frac{12.5}{50}$ $\frac{10.1}{50}$

$\frac{90}{50}$ $\frac{95}{39}$ $\frac{108}{34}$ $\frac{114}{27}$ $\frac{81}{17}$ $\frac{7.9}{7}$ $\frac{7.7}{7}$ $\frac{8.1}{13}$ $\frac{8.5}{19}$ $\frac{11.5}{23}$ $\frac{19.49}{23}$ $\frac{159}{29}$ $\frac{16.3}{50}$

Curv

$\frac{8.5}{50}$ $\frac{8.5}{48}$ $\frac{11.0}{38}$ $\frac{11.7}{31}$ $\frac{8.2}{23}$ $\frac{8.3}{19}$ $\frac{8.9}{19}$ $\frac{8.6}{8}$ $\frac{8.9}{50}$ $\frac{8.9}{10}$ $\frac{10.0}{17}$ $\frac{10.9}{29}$ $\frac{10.2}{30}$ $\frac{12.0}{50}$

$\frac{9.7}{50}$ $\frac{9.7}{43}$ $\frac{11.1}{37}$ $\frac{11.9}{32}$ $\frac{9.9}{23}$ $\frac{9.4}{19}$ $\frac{9.9}{15}$ $\frac{10.3}{13}$ $\frac{9.8}{8}$ $\frac{9.5}{11}$ $\frac{10.0}{31}$ $\frac{12.3}{31}$ $\frac{13.1}{30}$

$\frac{1.5}{50}$ $\frac{1.7}{46}$ $\frac{2.9}{39}$ $\frac{1.9}{36}$ $\frac{1.6}{29}$ $\frac{2.3}{8}$ $\frac{2.1}{50}$ $\frac{4.1}{50}$

$\frac{1.2}{50}$ $\frac{2.2}{41}$ $\frac{2.5}{19}$ $\frac{3.0}{24}$ $\frac{3.3}{42}$ $\frac{4.0}{50}$ $\frac{4.3}{50}$

Sta.

t

T

871.59

39

888.2[✓]

t30

86.5[✓]

t78

85.7[✓]

40

85.1[✓]

t20

84.4[✓]

t95

83.5[✓]

T.P.

3.67

883.41[✓]

980

881.74[✓]

41

81.7[✓]

t25

81.2[✓]

t44

80.9[✓]

42

80.4[✓]

t25

80.5[✓]

Lt

K

Rt

$\frac{21}{50} \frac{22}{40} \frac{28}{14} \frac{33}{-} \frac{47}{28} \frac{52}{50}$

$\frac{32}{50} \frac{49}{13} \frac{48}{11} \frac{50}{-} \frac{56}{7} \frac{61}{10} \frac{61}{21} \frac{58}{23} \frac{60}{32} \frac{66}{36} \frac{69}{50}$

$\frac{35}{50} \frac{47}{32} \frac{57}{29} \frac{57}{10} \frac{58}{-} \frac{62}{7} \frac{69}{11} \frac{63}{15} \frac{69}{22} \frac{70}{31} \frac{70}{50}$

$\frac{86}{50} \frac{64}{20} \frac{63}{15} \frac{64}{10} \frac{64}{-} \frac{68}{7} \frac{76}{14} \frac{75}{38} \frac{79}{50}$

$\frac{134}{50} \frac{108}{23} \frac{73}{15} \frac{71}{9} \frac{71}{-} \frac{74}{7} \frac{79}{15} \frac{80}{90} \frac{79}{50}$

$\frac{155}{50} \frac{138}{26} \frac{83}{18} \frac{82}{9} \frac{80}{-} \frac{84}{7} \frac{90}{12} \frac{115}{17} \frac{111}{23} \frac{96}{29} \frac{89}{33} \frac{86}{50}$

$\frac{66}{58} \frac{136}{45} \frac{134}{93} \frac{95}{36} \frac{90}{24} \frac{93}{16} \frac{38}{9} \frac{37}{-} \frac{40}{6} \frac{46}{10} \frac{83}{16} \frac{90}{21} \frac{86}{24} \frac{80}{30} \frac{57}{50}$

$\frac{61}{50} \frac{68}{39} \frac{85}{34} \frac{137}{29} \frac{137}{26} \frac{86}{25} \frac{53}{15} \frac{49}{9} \frac{48}{-} \frac{45}{7} \frac{53}{12} \frac{94}{19} \frac{98}{22} \frac{87}{26} \frac{78}{36} \frac{74}{41} \frac{60}{50}$

$\frac{55}{50} \frac{73}{38} \frac{81}{23} \frac{51}{15} \frac{46}{10} \frac{45}{-} \frac{49}{6} \frac{59}{12} \frac{111}{20} \frac{148}{24} \frac{153}{26} \frac{131}{30} \frac{128}{36} \frac{121}{38} \frac{52}{52}$

$\frac{19}{50} \frac{32}{39} \frac{57}{30} \frac{43}{23} \frac{52}{14} \frac{50}{8} \frac{50}{-} \frac{53}{7} \frac{56}{10} \frac{95}{18} \frac{100}{21} \frac{121}{28} \frac{156}{38} \frac{156}{43} \frac{100}{53}$

$\frac{06}{50} \frac{20}{32} \frac{51}{21} \frac{50}{8} \frac{49}{-} \frac{51}{7} \frac{55}{11} \frac{96}{21} \frac{101}{25} \frac{91}{30} \frac{97}{42} \frac{117}{50} \frac{156}{57}$

Sta + T - E/cv.

883.41

43 ✓
T.P. 8.16 889.42 4.15 881.2 ✓
+90 81.2 ✓

44 ✓
+50 81.1 ✓
80.8 ✓

45 ✓
+50 80.6 ✓
80.5 ✓

46 ✓
+62 80.0 ✓
79.1 ✓

T.P. 4.04 882.17 11.29 878.13 ✓
47 78.4 ✓

+73 77.9 ✓

Lt

L

Rt

$$\frac{108}{50} \quad \frac{112}{36} \quad \frac{108}{31} \quad \frac{40}{22} \quad \frac{44}{15} \quad \frac{42}{7} \quad \frac{42}{8} \quad \frac{44}{19} \quad \frac{55}{26} \quad \frac{44}{50} \quad \frac{57}{50}$$

$$\frac{36}{50} \quad \frac{34}{37} \quad \frac{74}{27} \quad \frac{79}{22} \quad \frac{81}{10} \quad \frac{82}{6} \quad \frac{85}{16} \quad \frac{92}{21} \quad \frac{89}{27} \quad \frac{50}{50} \quad \frac{42}{50}$$

$$\frac{25}{58} \quad \frac{34}{36} \quad \frac{80}{27} \quad \frac{90}{19} \quad \frac{87}{14} \quad \frac{85}{8} \quad \frac{83}{7} \quad \frac{86}{12} \quad \frac{88}{18} \quad \frac{92}{27} \quad \frac{57}{50} \quad \frac{51}{50}$$

$$\frac{20}{50} \quad \frac{27}{35} \quad \frac{73}{28} \quad \frac{88}{22} \quad \frac{86}{9} \quad \frac{86}{6} \quad \frac{89}{19} \quad \frac{96}{19} \quad \frac{87}{28} \quad \frac{52}{50} \quad \frac{45}{50}$$

$$\frac{28}{58} \quad \frac{35}{36} \quad \frac{81}{27} \quad \frac{93}{21} \quad \frac{88}{9} \quad \frac{88}{7} \quad \frac{91}{13} \quad \frac{95}{20} \quad \frac{80}{23} \quad \frac{54}{28} \quad \frac{47}{50} \quad \frac{65}{50}$$

$$\frac{75}{50} \quad \frac{76}{36} \quad \frac{79}{24} \quad \frac{77}{20} \quad \frac{93}{15} \quad \frac{70}{9} \quad \frac{89}{6} \quad \frac{91}{14} \quad \frac{93}{16} \quad \frac{102}{22} \quad \frac{92}{50} \quad \frac{94}{50}$$

$$\frac{112}{50} \quad \frac{115}{31} \quad \frac{112}{22} \quad \frac{98}{15} \quad \frac{96}{8} \quad \frac{94}{6} \quad \frac{97}{10} \quad \frac{99}{18} \quad \frac{111}{28} \quad \frac{114}{50} \quad \frac{120}{50}$$

$$\frac{137}{50} \quad \frac{138}{24} \quad \frac{120}{20} \quad \frac{108}{14} \quad \frac{103}{10} \quad \frac{108}{18} \quad \frac{146}{29} \quad \frac{153}{50} \quad \frac{158}{50}$$

$$\frac{70}{50} \quad \frac{71}{31} \quad \frac{72}{24} \quad \frac{51}{20} \quad \frac{41}{14} \quad \frac{38}{10} \quad \frac{43}{10} \quad \frac{86}{17} \quad \frac{91}{29} \quad \frac{95}{50}$$

$$\frac{78}{50} \quad \frac{74}{39} \quad \frac{78}{23} \quad \frac{52}{16} \quad \frac{47}{11} \quad \frac{43}{6} \quad \frac{46}{10} \quad \frac{48}{18} \quad \frac{90}{31} \quad \frac{89}{42} \quad \frac{101}{67} \quad \frac{109}{70} \quad \frac{125}{70}$$

Sta + A - Elev

882.17

48 +10

877.5 ✓

+60

77.4 ✓

49

77.1 ✓

+50

77.2 ✓

50

77.4 ✓

+50

77.5 ✓

51

77.7 ✓

+50

78.8 ✓

T.P.

12.93

872.85 ✓

2.25

879.22 ✓

52

80.0 ✓

+50

81.2 ✓

53

82.7 ✓

L.

K

Rt

$\frac{85}{50}$ $\frac{95}{35}$ $\frac{113}{30}$ $\frac{118}{29}$ $\frac{118}{24}$ $\frac{86}{24}$ $\frac{57}{17}$ $\frac{51}{12}$ $\frac{47}{5}$ $\frac{49}{5}$ $\frac{52}{8}$ $\frac{92}{17}$ $\frac{95}{20}$ $\frac{86}{22}$ $\frac{128}{29}$ $\frac{105}{33}$ $\frac{107}{50}$

$\frac{84}{50}$ $\frac{88}{23}$ $\frac{58}{16}$ $\frac{52}{11}$ $\frac{48}{6}$ $\frac{51}{11}$ $\frac{55}{19}$ $\frac{88}{29}$ $\frac{91}{50}$

$\frac{85}{50}$ $\frac{86}{22}$ $\frac{57}{15}$ $\frac{59}{11}$ $\frac{51}{6}$ $\frac{52}{9}$ $\frac{54}{16}$ $\frac{82}{29}$ $\frac{83}{50}$

$\frac{107}{50}$ $\frac{80}{22}$ $\frac{78}{28}$ $\frac{59}{18}$ $\frac{53}{11}$ $\frac{50}{6}$ $\frac{52}{11}$ $\frac{54}{17}$ $\frac{76}{30}$ $\frac{76}{50}$

$\frac{78}{50}$ $\frac{76}{22}$ $\frac{50}{16}$ $\frac{48}{11}$ $\frac{48}{9}$ $\frac{49}{11}$ $\frac{53}{16}$ $\frac{66}{29}$ $\frac{70}{50}$

$\frac{72}{50}$ $\frac{63}{19}$ $\frac{54}{16}$ $\frac{49}{10}$ $\frac{47}{13}$ $\frac{51}{15}$ $\frac{58}{30}$ $\frac{53}{50}$

$\frac{69}{50}$ $\frac{62}{21}$ $\frac{50}{16}$ $\frac{45}{13}$ $\frac{46}{19}$ $\frac{55}{30}$ $\frac{49}{50}$

$\frac{80}{50}$ $\frac{56}{29}$ $\frac{53}{19}$ $\frac{47}{15}$ $\frac{38}{13}$ $\frac{36}{18}$ $\frac{39}{19}$ $\frac{45}{21}$ $\frac{32}{34}$ $\frac{30}{50}$

$\frac{159}{50}$ $\frac{153}{42}$ $\frac{149}{19}$ $\frac{133}{14}$ $\frac{129}{11}$ $\frac{131}{17}$ $\frac{141}{19}$ $\frac{131}{21}$ $\frac{126}{36}$ $\frac{122}{50}$

$\frac{145}{50}$ $\frac{142}{19}$ $\frac{125}{14}$ $\frac{121}{10}$ $\frac{117}{5}$ $\frac{118}{18}$ $\frac{121}{21}$ $\frac{119}{36}$ $\frac{116}{50}$

$\frac{137}{50}$ $\frac{133}{39}$ $\frac{130}{21}$ $\frac{110}{15}$ $\frac{105}{11}$ $\frac{102}{6}$ $\frac{103}{13}$ $\frac{100}{28}$ $\frac{104}{22}$ $\frac{109}{37}$ $\frac{92}{50}$

Sta + X - Elev

892.85

53 +50

884.9 ✓

54

87.3 ✓

+50

89.2 ✓

55

90.9 ✓

+90

92.5 ✓

T.P.

10.26

903.11 ✓

0.00

892.85 ✓

56

94.4 ✓

+58.5

96.1 ✓

57

92.7 ✓

+28

99.1 ✓

+95

899.8 ✓

+75.5

900.1 ✓

B.M.

0.69

902.42 ✓

(902.41)

Lt

L

Rt

$\frac{14.1}{50}$ $\frac{127}{50}$ $\frac{120}{28}$ $\frac{110}{21}$ $\frac{91}{15}$ $\frac{86}{4}$ $\frac{80}{1}$ $\frac{8.1}{6}$ $\frac{83}{19}$ $\frac{8.1}{23}$ $\frac{66}{37}$ $\frac{65}{50}$

$\frac{110}{50}$ $\frac{107}{43}$ $\frac{95}{26}$ $\frac{66}{15}$ $\frac{58}{9}$ $\frac{56}{5}$ $\frac{5.8}{12}$ $\frac{6.1}{12}$ $\frac{49}{19}$ $\frac{37}{39}$ $\frac{21}{50}$

$\frac{8.7}{50}$ $\frac{60}{26}$ $\frac{49}{20}$ $\frac{45}{15}$ $\frac{40}{10}$ $\frac{37}{6}$ $\frac{3.7}{6}$ $\frac{4.3}{12}$

$\frac{13.9}{50}$ $\frac{64}{40}$ $\frac{49}{39}$ $\frac{27}{26}$ $\frac{0.7}{19}$ $\frac{2.7}{16}$ $\frac{22}{9}$ $\frac{20}{1}$ $\frac{2.1}{6}$ $\frac{2.5}{13}$

$\frac{56}{50}$ $\frac{4.3}{40}$ $\frac{0.1}{20}$ $\frac{+2.3}{20}$ $\frac{+1.0}{20}$ $\frac{11}{16}$ $\frac{0.7}{9}$ $\frac{0.4}{1}$ $\frac{0.6}{6}$ $\frac{0.8}{14}$

T.P. #13 Lt.

$\frac{11.3}{50}$ $\frac{67}{31}$ $\frac{45}{24}$ $\frac{71}{16}$ $\frac{8.8}{9}$ $\frac{8.7}{1}$ $\frac{2.9}{7}$ $\frac{9.1}{14}$

$\frac{9.3}{50}$ $\frac{56}{35}$ $\frac{38}{25}$ $\frac{74}{15}$ $\frac{71}{7}$ $\frac{70}{10}$ $\frac{7.3}{14}$ $\frac{7.1}{14}$

$\frac{6.1}{50}$ $\frac{1.3}{35}$ $\frac{15}{32}$ $\frac{19.8}{29}$ $\frac{56}{18}$ $\frac{56}{8}$ $\frac{54}{8}$ $\frac{5.5}{8}$ $\frac{56}{10}$

$\frac{4.1}{8}$ $\frac{4.2}{6}$ $\frac{40}{1}$ $\frac{40}{7}$

$\frac{0.63}{10.3}$ $\frac{0.63}{10}$ $\frac{3.5}{7}$ $\frac{3.5}{7}$ $\frac{3.5}{7}$ $\frac{0.67}{7.2}$ $\frac{0.67}{7.2}$

$\frac{0.65}{10.3}$ $\frac{0.65}{10}$ $\frac{3.1}{8}$ $\frac{3.0}{5}$ $\frac{3.0}{5}$ $\frac{2.8}{8}$ $\frac{0.68}{9.6}$ $\frac{0.68}{10.2}$

X Faint S.E. Cor. Faint

Sta.	+	X	-	Elev.
T.P.	13.29	906.19 ✓		892.88
54	+50			889.2 ✓
T.P.	13.41	917.33 ✓	2.24	903.90
55				90.9
	+40			92.5
56				94.4
	+38.5			96.1
57				97.7
	+28			99.1 ✓
T.P.	9.38	920.91 ✓	4.80	912.53
	+45			99.8
151	Top W. Rail			918.65 ✓
+70	Top E. Rail			918.67 ✓
+15.5				900.1
B.M.		17.52		902.27 902.91
				902.39 ✓

"D"

Slope stakes from Back St.
to White Bear Ave. as per
plan dated 9/13/38.

9/38.

20' Crown

23' to Back Slope

2 to 1 Slopes

Hold to 33' except

at Easements.

Sta.	+	π	-	Grade
B.M.	3.65	906.06		902.41

59156 ³⁹				96.6
---------------------	--	--	--	------

+70				96.8
-----	--	--	--	------

+80				96.8
-----	--	--	--	------

60				96.9
----	--	--	--	------

+50				97.2
-----	--	--	--	------

61				97.4
----	--	--	--	------

+50				97.7
-----	--	--	--	------

62				97.9
----	--	--	--	------

Lt.

E

Rt

21

"X" Top of S.E. Cor. Foundation of Bridge.

$$\begin{array}{r} 9.5 \\ 11.5 \end{array}$$

$$\begin{array}{r} 14.0 \\ F.4.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 100 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ 11.3 \end{array}$$

X

$$\begin{array}{r} 9.3 \\ 11.3 \end{array}$$

$$\begin{array}{r} 14.4 \\ F.5.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 10.2 \\ F.0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 13.6 \\ F.4.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 9.2 \\ 11.2 \end{array}$$

$$\begin{array}{r} 14.2 \\ F.5.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 10.5 \\ F.1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 14.8 \\ F.5.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 8.9 \\ 10.9 \end{array}$$

$$\begin{array}{r} 12.9 \\ F.4.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 10.5 \\ F.1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 14.2 \\ F.5.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 8.7 \\ 10.7 \end{array}$$

$$\begin{array}{r} 11.5 \\ F.2.8 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 10.0 \\ F.1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 14.2 \\ F.5.5 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ 10.4 \end{array}$$

$$\begin{array}{r} 11.7 \\ F.3.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 9.6 \\ F.1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 11.4 \\ F.3.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 8.2 \\ 10.2 \end{array}$$

$$\begin{array}{r} 13.8 \\ F.5.0 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 9.5 \\ F.1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 10.0 \\ D.C. 0.2 \\ \hline 23.4 \end{array}$$

Sta.	+	π	-	Grade
		906.06		

62+50				98.3
-------	--	--	--	------

63				99.1
----	--	--	--	------

+50				00.2
-----	--	--	--	------

64				01.6
----	--	--	--	------

+50				03.3
-----	--	--	--	------

65				05.4
----	--	--	--	------

T.P.	2.23	911.76	1.53	904.53
------	------	--------	------	--------

+50				07.8
-----	--	--	--	------

66				10.5
----	--	--	--	------

↑
Easement on Rt.
↓

4.

2

24

3

7.8
9.8

12.9
F.5.1
25.2

8.8
F.1.0

8.4
D.C.1.4
25.8

7.0
9.0

12.7
F.5.7
26.4

7.9
F.0.9

9.0
D.C.0.0
23.4

5.9
7.9

12.6
F.7.7
30.4

7.2
1.3
F.

11.9
F.6.0
27.0

4.5
6.5

12.6
F.8.1
31.2

6.0
1.5
F.

13.0
F.8.5
37.0

2.8
4.8

9.9
F.7.1
29.2

4.2
1.4
F.

13.2
F.10.4
35.8

0.7
2.7

7.8
F.7.1
29.2

1.1
F.0.4

12.4
F.11.7
38.4

4.0

8.4
F.4.4
23.8

3.8
6.02

14.9
F.10.9
36.8

1.3

3.3
F.2.0
14.0

1.2
C.0.0

9.1
F.7.8
30.6

Sta. + π - Grade

66+50

67

+47

68

+50

69

+50

70

+50



ft.

Elevation on

LT.

E

et.

4

6.1
8.1

6.3
DC 1.8
26.4

8.1
DC 0.0
23.1

3.5
8.5

40.2
DC 5.7
33.0

3.7
DC 1.8
26.8

10.3
12.3

2.9
9.4
DC 33.0

6.0
DC 6.3
31.6

11.7
13.7

2.7
DC 11.0
33.0

2.9
DC 10.8
44.6

12.4
14.4

4.2
DC 10.2
33.0

3.3
DC 11.1
45.2

10.6
14.6

3.6
DC 7.0
33.0

2.8
DC 9.8
42.6

8.6
10.6

1.2
7.4
DC 33.0

2.0
DC 8.6
40.2

10.9
14.9

4.2
8.2
DC 33.0

5.5
DC 7.4
37.8

9.6
11.6

4.1
DC 7.5
33.0

3.8
DC 7.8
38.6

Sta. + π - Grade

71

+62

72

+50

73

+50

B.M. 8.67 936.91 928.24

74 29.3

+37 29.4

75 29.5

4.

2

21.

5

8.6
10.8

4.7
D.C. 6.1
33.0

4.3
D.C. 6.5
36.0

8.6
10.6

4.6
D.C. 6.0
33.0

6.1
D.C. 4.5
32.0

4.7
6.7

1.2
D.C. 1.5
33.0

2.0
D.C. 4.2
32.4

5.1
7.1

4.9
D.C. 2.2
27.4

3.9
D.C. 3.2
29.4

5.2
7.2

6.1
D.C. 1.1
25.2

6.8
D.C. 0.3
23.6

5.2
7.2

5.1
D.C. 2.1
23.2

7.2
D.C. 0.0
23.0

Top of Mon. St. 85 + 96.78

7.6
9.6

9.3
D.C. 0.3
23.6

7.6
C.00

7.7
D.C. 1.9
26.8

7.5
9.5

11.7
F.4.2
23.4

7.6
F.0.1

8.1
D.C. 1.4
26.8

7.4
9.4

12.3
F.4.9
24.8

7.8
F.0.4

13.4
F.6.0
27.0

Sta.	+	π	-	Grade
------	---	-------	---	-------

936.91

75+50				29.6
-------	--	--	--	------

76				29.7
----	--	--	--	------

+50				29.8
-----	--	--	--	------

77				30.0
----	--	--	--	------

+50				30.3
-----	--	--	--	------

78				30.6
----	--	--	--	------

+50				31.0
-----	--	--	--	------

79				31.5
----	--	--	--	------

4.

2

4.

6

7.3
9.3

11.1
F3.8
22.6

7.9
F0.6

12.7
F5.4
25.8

7.2
7.4

10.5
F3.3
21.6

7.8
F0.6

10.2
F2.0
21.0

7.1
9.1

10.4
F3.3
21.6

8.1
F1.0

10.0
F2.9
20.8

6.9
8.9

10.4
F2.5
22.0

8.2
F1.3

11.1
F4.2
23.4

6.6
8.6

9.6
F3.0
21.0

7.9
F1.3

10.0
F2.4
21.8

6.3
8.3

8.4
F2.1
19.2

7.2
F0.9

8.3
F2.0
19.0

5.9
7.9

6.6
D.C.1.3
25.6

6.4
F0.1

7.3
D.C.0.6
24.2

5.4
7.4

4.7
D.C.2.2
28.4

5.6
F0.2

5.8
D.C.1.6
24.2

Sta. + π - Grade.

936.91

794.50

37.0

80

37.5

+50

81

+50

82

+28

+50

83

+50

Lt.

E

Rt.

7

$$\begin{array}{r} 4.9 \\ 6.9 \end{array}$$

$$\begin{array}{r} 3.7 \\ DC3.2 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ \hline K.O.1 \end{array}$$

$$\begin{array}{r} 4.8 \\ DC2.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 4.4 \\ 6.4 \end{array}$$

$$\begin{array}{r} 2.6 \\ DC3.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline C.O.O \end{array}$$

$$\begin{array}{r} 4.5 \\ DC1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 10.5 \\ 12.1 \end{array}$$

$$\begin{array}{r} 8.3 \\ DC4.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 10.0 \\ DC2.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ 11.8 \end{array}$$

$$\begin{array}{r} 8.0 \\ DC3.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 8.3 \\ DC3.5 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ 11.8 \end{array}$$

$$\begin{array}{r} 8.4 \\ DC3.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 8.7 \\ DC3.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 9.9 \\ 11.9 \end{array}$$

$$\begin{array}{r} 10.7 \\ DC1.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 11.4 \\ DC0.5 \\ \hline 24.0 \end{array}$$

X

$$\begin{array}{r} 9.8 \\ 11.8 \end{array}$$

$$\begin{array}{r} 10.2 \\ DC1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 11.7 \\ DC0.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 9.9 \\ 11.9 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC6.5 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 2.9 \\ DC4.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 10.1 \\ 12.1 \end{array}$$

$$\begin{array}{r} 8.4 \\ DC3.1 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC6.6 \\ \hline 33.0 \end{array}$$

Sta.	+	x	-	Grade
------	---	---	---	-------

84				
----	--	--	--	--

+50				
-----	--	--	--	--

85				
----	--	--	--	--

+50				
-----	--	--	--	--

86				
----	--	--	--	--

+40				
-----	--	--	--	--

B.M.	2.57	930.81		928.24
------	------	--------	--	--------

87				25.3
----	--	--	--	------

+30				24.4
-----	--	--	--	------

+42				24.1
-----	--	--	--	------

Lt.

E

Rt

8

10.7
12.7
$$\begin{array}{r} 6.8 \\ 1.9 \\ \hline DC. 5.33 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC. 6.3 \\ \hline 33.0 \end{array}$$
11.8
13.8
$$\begin{array}{r} 11.7 \\ DC. 2.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 10.0 \\ DC. 3.8 \\ \hline 30.6 \end{array}$$
12.7
14.7
$$\begin{array}{r} 12.7 \\ DC. 2.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 11.7 \\ DC. 2.0 \\ \hline 29.0 \end{array}$$
5.6
7.6
$$\begin{array}{r} 6.6 \\ DC. 1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 2.6 \\ DC. 5.0 \\ \hline 33.0 \end{array}$$
7.2
9.2
$$\begin{array}{r} 8.4 \\ F. 2.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 3.8 \\ DC. 5.4 \\ \hline 33.0 \end{array}$$
8.6
10.6
$$\begin{array}{r} 13.3 \\ F. 4.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ DC. 3.2 \\ \hline 29.4 \end{array}$$

Top of Mon.

85 + 56.78

5.5
7.5
$$\begin{array}{r} 7.5 \\ PL. 0.0 \\ \hline 14.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ F. 0.1 \\ \hline 5.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC. 3.2 \\ \hline 29.4 \end{array}$$
6.4
8.4
$$\begin{array}{r} 8.4 \\ DC. 0.0 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 6.4 \\ F. 0.0 \\ \hline 5.0 \end{array}$$
6.7
8.7
$$\begin{array}{r} 8.7 \\ PL. 0.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 6.7 \\ F. 0.0 \\ \hline 5.0 \end{array}$$

$$\begin{array}{r} 6.7 \\ DC. 2.6 \\ \hline 28.2 \end{array}$$

Sta. + π - Grade

930.81

88 22.8

+23 22.3

+60 21.7

T.P. 2.86 923.64 10.03 920.78

89 21.2

+50 20.8

90 20.6

+50 20.6

91 20.8

+50 21.4

LT.

E

RT.

9

8.0
10.0

9.5
DCO.1
24.0

8.0
F.00

8.6
DCO.4
25.8

8.5
10.5

6.8
DCO.37
30.4

9.1
11.1

10.7
DCO.4
23.8

9.7
F0.6

12.4
F.3.3
21.6

2.4

8.3
F5.9
26.8

3.6
F.1.7

8.5
F6.1
27.2

2.8

9.1
F6.3
27.6

4.3
F.1.5

10.4
F7.6
30.2

3.0

9.2
F6.2
27.4

4.4
F.1.4

8.8
F7.9
26.8

3.0

9.1
F6.1
27.2

4.5
F.1.5

8.8
F.1.8
26.6

2.8

9.2
F6.2
27.8

4.5
F.1.7

9.9
F7.1
29.2

2.2

9.7
F7.2
30.0

4.2
F.2.0

10.0
F.7.8
30.6

at off Elev. 51.00

Sta.	+	π	-	Grade
		923.64		

92				22.1
T.P.	9.17	922.20	5.61	918.03

+50				23.1
-----	--	--	--	------

93				24.3
----	--	--	--	------

+50				25.8
-----	--	--	--	------

94				27.4
T.P.	7.28	934.29	0.19	927.01

+50				28.9
-----	--	--	--	------

95

T.P.	11.18	943.06	2.41	931.88
------	-------	--------	------	--------

+50

T.P.	12.50	945.22	0.34	942.72
------	-------	--------	------	--------

96				33.7
----	--	--	--	------

↑ +75
Elevation 27

✓ +50

↑ +50

LT.

E

RT

10

1.5

$$\begin{array}{r} 102 \\ \overline{F8.7} \\ 324 \end{array}$$

$$\begin{array}{r} 3.2 \\ \overline{F1.7} \end{array}$$

$$\begin{array}{r} 9.8 \\ \overline{F8.3} \\ 316 \end{array}$$

4.1

$$\begin{array}{r} 116 \\ \overline{F2.5} \\ 30.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ \overline{F1.2} \end{array}$$

$$\begin{array}{r} 41 \\ \overline{F.90} \\ 33.0 \end{array}$$

7.9

$$\begin{array}{r} 118 \\ \overline{F8.9} \\ 37.8 \end{array}$$

$$\begin{array}{r} 34 \\ \overline{F0.5} \end{array}$$

$$\begin{array}{r} 12.9 \\ \overline{F10.0} \\ 31.0 \end{array}$$

1.4

$$\begin{array}{r} 114 \\ \overline{F10.0} \\ 33.0 \end{array}$$

$$\begin{array}{r} 1.8 \\ \overline{F0.4} \end{array}$$

$$\begin{array}{r} 126 \\ \overline{F11.2} \\ 37.4 \end{array}$$

10.7

$$\begin{array}{r} 97 \\ \overline{F9.9} \\ 33 \end{array}$$

$$\begin{array}{r} 10.2 \\ \overline{F0.0} \end{array}$$

$$\begin{array}{r} 111 \\ \overline{F11.3} \\ 37.6 \end{array}$$

17

$$\begin{array}{r} 133 \\ \overline{F8.1} \\ 31.2 \end{array}$$

$$\begin{array}{r} 129 \\ \overline{F7.7} \\ 30.4 \end{array}$$

36

$$\begin{array}{r} 56 \\ \overline{00.D6.} \\ 20.6 \end{array}$$

$$\begin{array}{r} 44 \\ \overline{00.1.2} \\ 25.4 \end{array}$$

11.0
13.0
12.5

$$\begin{array}{r} 86 \\ \overline{00.39} \\ 33.0 \end{array}$$

$$\begin{array}{r} 91 \\ \overline{00.34} \\ 27.8 \end{array}$$

21.5
23.5
23.0

$$\begin{array}{r} 114 \\ \overline{00.11.4} \\ 33.0 \end{array}$$

$$\begin{array}{r} 110 \\ \overline{00.12.5} \\ 41.8 \end{array}$$

Sta.	+	π	-	Grade
		955.22		

96+50				35.4
T.P.	7.30	964.36	0.16	955.06

97				36.9
T.P.	12.78	964.05	13.09	949.27

+32				37.7	180
-----	--	--	--	------	-----

+65				38.5	200
-----	--	--	--	------	-----

98				39.2	46
T.P.	2.17	951.19	13.03	949.02	

+50				39.5	35
-----	--	--	--	------	----

B.M.					944.85
T.P.	3.69	942.72	12.16	939.03	

99				39.0	33
----	--	--	--	------	----

+50				38.7	
-----	--	--	--	------	--

100				38.0	
-----	--	--	--	------	--

Easement on Rt. Special Section

5.26 1200

76+50

13.72

20.46

20.7

22.7

DC 17.9

49.8

97

12.15

18.85

19.1

21.1

DC 16.7

48.0

+32

11.20

17.94

18.2

20.2

DC 15.7

46.5

+65

10.30

17.04

17.3

19.3

DC 15.2

45.8

98

9.7

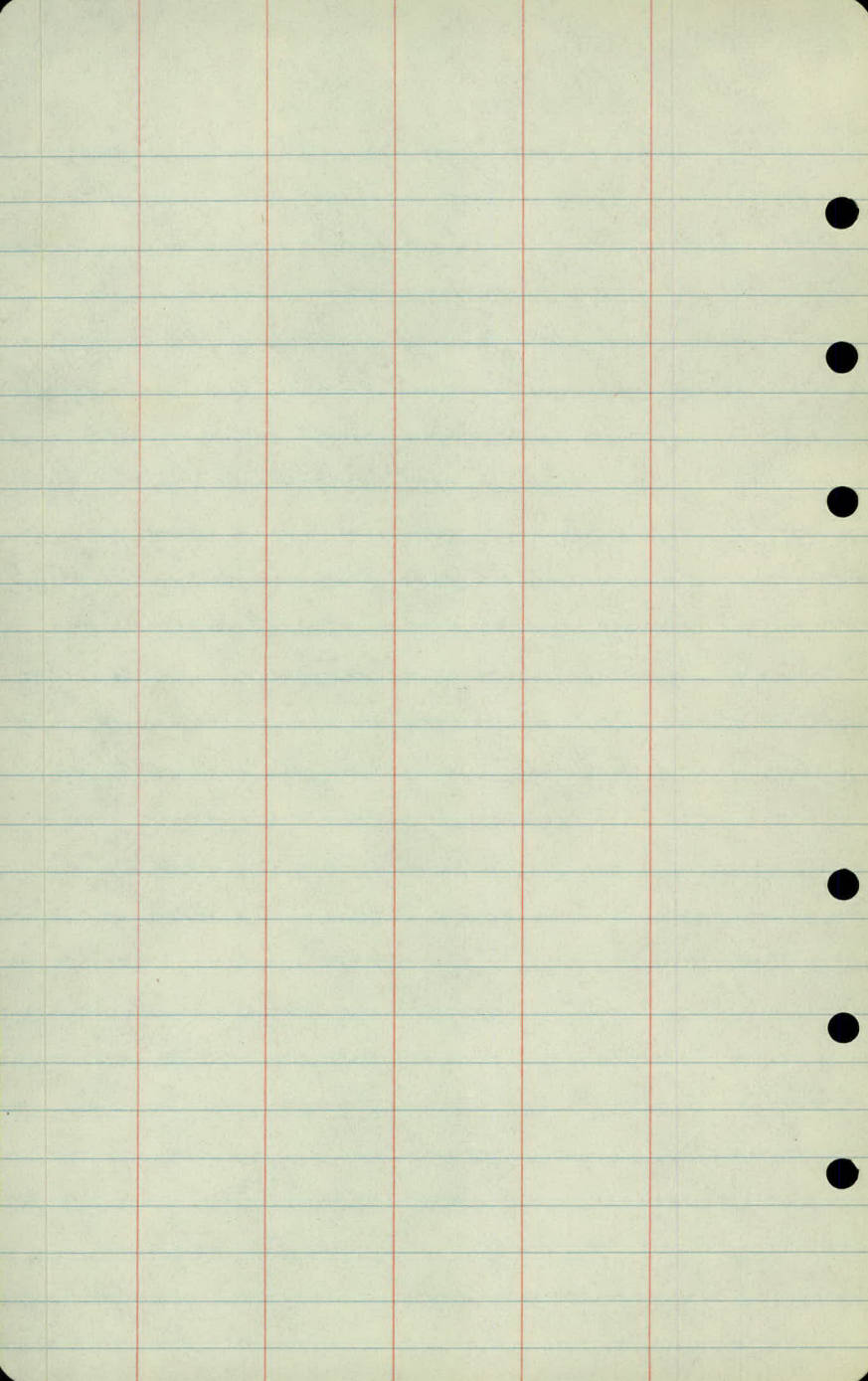
16.44

16.7

18.7

DC 14.6

44.9



Lt.

Rt

Rt

11

19.8
21.8
21.3

DC 16.2
21
33

25.5
27.0

11.8
DC 15.2
33.0

Grade
396 129

24.3
26.3 Rt
25.8 Lt

11.6
DC 14.2
33.0

Grade
154

23.5
25.5
25.0

12.8
DC 12.8
33

Grade
142

22.8
24.8 Rt
24.3 Lt

11.2
DC 13.1
33

Grade
49

15
11.7
13.7 Rt
13.7 Lt

5.3
DC 7.3
33

6.4
DC 7.3
37.6

Grade in R.P. Gone

3.7
5.7 Rt
5.7 Lt

3.5
DC 1.7
33

3.7
DC 0.0
0.00

3.7
DC 2.0
27.0

4.0
5.0
5.5

5.5
DC 0.0
23.5

5.3
DC 0.7
24.8

4.7

4.7
DC 0.0
25.0

5.3
DC 0.7
24.8

Sto + K - Grade

942.72

100+50

101

+50

102

+50

35.9

103

35.8

+50

36.4

T.P.

11.84

942.85

6.71

936.01

104

37.7

+50

39.6

4.

2

2.

$$\frac{5.6}{1}$$

$$\frac{10.8}{F.5.2} = 21.4$$

$$\frac{10.2}{F.4.6} = 24.2$$

$$\frac{6.0}{1}$$

$$\frac{11.8}{F.1.8} = 26.6$$

$$\frac{11.1}{F.1.1} = 25.2$$

$$\frac{6.5}{1}$$

$$\frac{11.8}{F.1.3} = 25.6$$

$$\frac{11.6}{F.1.1} = 25.2$$

$$\frac{6.8}{1}$$

$$\frac{11.0}{F.4.2} = 23.4$$

$$\frac{10.8}{F.4.0} = 23.0$$

$$\frac{6.8}{1}$$

$$\frac{9.7}{F.2.9} = 20.8$$

$$\frac{6.8}{F.0.0}$$

$$\frac{9.0}{F.2.2} = 19.4$$

$$\frac{6.9}{1}$$

$$\frac{10.0}{F.3.1} = 21.2$$

$$\frac{2.0}{F.0.1}$$

$$\frac{9.6}{F.2.7} = 20.4$$

$$\frac{6.3}{1}$$

$$\frac{10.2}{F.3.9} = 22.8$$

$$\frac{6.5}{F.0.2}$$

$$\frac{9.3}{F.3.4} = 21.8$$

$$10.2$$

$$\frac{16.2}{F.6.0} = 27.0$$

$$\frac{10.9}{F.0.7}$$

$$\frac{15.8}{F.1.6} = 26.2$$

$$8.3$$

$$\frac{16.3}{F.8.0} = 31.0$$

$$\frac{10.1}{F.1.8}$$

$$\frac{15.3}{F.2.0} = 25.0$$

Sta.	+	π	-	Grade
------	---	-------	---	-------

947.85

105				41.9
-----	--	--	--	------

+50				44.1
-----	--	--	--	------

106				45.8
-----	--	--	--	------

137				46.3
-----	--	--	--	------

+42				46.3
-----	--	--	--	------

B.M.			1.14	946.71
------	--	--	------	--------

946.74

4.

2

24

13

6.0

$$\begin{array}{r} 15.2 \\ \hline F. 9.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ \hline F. 3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 13.5 \\ \hline F. 7.5 \\ \hline 30.8 \end{array}$$

3.8

$$\begin{array}{r} 12.6 \\ \hline F. 8.8 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline F. 3.3 \\ \hline \end{array}$$

$$\begin{array}{r} 11.5 \\ \hline F. 7.7 \\ \hline 30.4 \end{array}$$

2.1

$$\begin{array}{r} 7.3 \\ \hline F. 5.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline F. 2.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.1 \\ \hline F. 6.0 \\ \hline 27.0 \end{array}$$

1.6

$$\begin{array}{r} 1.9 \\ \hline F. 0.3 \\ \hline \end{array}$$

2 Pr. 512. 106 + 57.35

Sta.

+

π

-

Grade

"D"

White Bear Road To Bellaire

572 + π - Grade

106+57³⁵

+73

+79

+84

107

+50

+77

108

+50

+70

109

+50

+70

4.

5

2.

11.7
13.7

11.1
0.6.2.1
27.7

11.7
0.6.2.0
27.0

9.6
11.6

8.0
0.6.3.6
30.7

8.9
0.6.2.7
28.4

X

7.4
9.4

5.2
0.6.4.2
31.4

6.6
0.6.2.8
28.6

5.7
7.7

6.1
0.6.1.6
26.7

4.6
0.6.3.1
29.7

4.5
6.5

5.2
0.6.1.3
21.6

2.6
0.6.3.9
30.8

3.2
5.2

5
0.6.2.7
28.4

1.4
0.6.3.8
30.6

Sta. + π - Grade.

110

+60

111

+50

112

+50
~~+28~~

+72

113

LH.

E

RT.

54
7.4

46
DC 28
28.6

37
DC 35
30.0

49
6.9

53
DC 16
26.2

42
DC 27
28.4

24
6.4

63
DC 81
23.2

67
FR 3
18.6

39
5.9

57
DC 2
23.4

89
FR 0
25.0

28
4.8

33
DC 15
26.0

62
FR 4
21.8

104
17.4

103
DC 21
27.2

140
FR 6
22.2

X

98
11.8

85
DC 33
29.6

127
FR 9
20.8

Sta. + π - Grade

113+27

+38

+78

114 9.4 969.7 60.0 ^{5.0} 960.3 60.3

+58

59.3

+70

59.2

115

58.8 ^{58.7} 58.1

1.90

60.7

958.80

Sta. 115

+18

58.6



Lt.

2

Rt.

X

9.5
11.5

41
DC 7.4
33.0

80
DC 3.5
30

9.4
11.4

12
DC 10.2
33.0

49
DC 6.5
33.0

9.6
11.6

28
DC 8.8
33.0

40
DC 7.6
33.0

44.
10.4
12.4

5.7
DC 6.7
33.0

10.2

50
DC 7.4
33.0

10.5
12.5

X

10.9
12.9

72
DC 5.7
33.0

10.9
10.0

10.3
DC 2.6
28.2

2.1
4.1

2.4
DC 1.7
26.4

2.3
10.1

6.4
4.3
21.5

Sta.	+	π	-	Grade.	
		60.7			
115+47		Bt.		58.3	
+65		slope on		58.0	
116		Visc 1 1/2 ft		57.6	F09
+42				57.1	
117		↓		56.4	F09
+62				55.6	
118				55.2	F01
+50				54.6	

LH.

E

RT

X

2.7

$$\begin{array}{r} 76 \\ F.4.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 33 \\ \hline F.0.6 \end{array}$$

$$\begin{array}{r} 12.4 \\ F.8.7 \\ \hline 25.1 \end{array}$$

3.1

$$\begin{array}{r} 82 \\ F.0.1 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 40 \\ \hline F.0.9 \end{array}$$

$$\begin{array}{r} 16.4 \\ F.13.3 \\ \hline 43.0 \end{array}$$

3.6

$$\begin{array}{r} 88 \\ F.12 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 42 \\ \hline F.1.1 \end{array}$$

$$\begin{array}{r} 17.9 \\ F.14.3 \\ \hline 33.0 \end{array}$$

4.3

$$\begin{array}{r} 95 \\ F.5.2 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 52 \\ \hline F.0.9 \end{array}$$

$$\begin{array}{r} 16.3 \\ F.12.0 \\ \hline 33.0 \end{array}$$

5.1

$$\begin{array}{r} 90 \\ F.3.9 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 55 \\ \hline F.0.4 \end{array}$$

$$\begin{array}{r} 83 \\ F.3.2 \\ \hline 21.4 \end{array}$$

5.5

$$\begin{array}{r} 84 \\ F.2.9 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 56 \\ \hline F.0.1 \end{array}$$

$$\begin{array}{r} 25 \\ F.2.1 \\ \hline 19.2 \end{array}$$

6.1

8.1

$$\begin{array}{r} 49 \\ O.C.3.2 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 64 \\ \hline F.0.0 \end{array}$$

$$\begin{array}{r} 43 \\ O.C.3.8 \\ \hline 30.6 \end{array}$$

Sta.	+	π	-	Grade
		60.7		

118+75				54.3
--------	--	--	--	------

119				54.0	C. 13
<u>119</u>	8.9	63.7		54.3	Sta. 119

+38				53.5
-----	--	--	--	------

+65				53.7
-----	--	--	--	------

120				54.8	C. 01
-----	--	--	--	------	-------

+30				57.4
-----	--	--	--	------

+60				57.1
-----	--	--	--	------

1.8	54.9	57.9	Sta 120
-----	------	------	---------

121				51.7	C. 09
-----	--	--	--	------	-------

L4.

L

R1.

X

$$\begin{array}{r} 6.7 \\ 8.7 \end{array}$$

$$\begin{array}{r} 15 \\ 16.72 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 64 \\ \hline 60.3 \end{array}$$

$$\begin{array}{r} 34 \\ 20.53 \\ \hline 33.0 \end{array}$$

X

$$\begin{array}{r} 10.0 \\ 14.2 \end{array}$$

$$\begin{array}{r} 19 \\ 20.71 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 99 \\ \hline 60.1 \end{array}$$

$$\begin{array}{r} 26 \\ 20.44 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 10.4 \\ 14.4 \end{array}$$

$$\begin{array}{r} 27 \\ 20.47 \\ \hline 32.4 \end{array}$$

$$\begin{array}{r} 103 \\ \hline 60.1 \end{array}$$

$$\begin{array}{r} 54 \\ 20.70 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.8 \\ 14.8 \end{array}$$

$$\begin{array}{r} 101 \\ 20.22 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 110 \\ \hline 60.2 \end{array}$$

$$\begin{array}{r} 52 \\ 20.76 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.1 \\ 13.1 \end{array}$$

$$\begin{array}{r} 131 \\ 20.00 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 117 \\ \hline 60.6 \end{array}$$

$$\begin{array}{r} 54 \\ 20.37 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 30 \\ 6.0 \end{array}$$

$$\begin{array}{r} 21 \\ 24.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 9 \\ 31 \\ \hline 60.9 \end{array}$$

$$\begin{array}{r} 55 \\ 12.5 \\ \hline 20.0 \end{array}$$

Sta.	+	π	-	Grade
		54.7		

121+27

51.6

+72

51.6

122

51.7

52.0

+36

51.0

+73

51.3

123
≡

51.7

51.7

12.1

65.7

53.6

52.124

+47

53.6

+75

54.7

Lt.

E

Rt.

X

3.1

$$\begin{array}{r} 11.4 \\ F.8.3 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 4.9 \\ F.1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 11.8 \\ F.8.8 \\ \hline 32.6 \end{array}$$

3.0

$$\begin{array}{r} 12.9 \\ F.9.9 \\ \hline F.1.33.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ F.2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 13.0 \\ F.10.0 \\ \hline 33.0 \end{array}$$

2.7

X

2.4

$$\begin{array}{r} 10.2 \\ F.7.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 4.1 \\ F.1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 9.1 \\ F.6.7 \\ \hline 28.4 \end{array}$$

2.0

$$\begin{array}{r} 8.1 \\ F.6.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 3.6 \\ F.1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ F.3.3 \\ \hline 21.6 \end{array}$$

12.1

14.1

$$\begin{array}{r} 14.6 \\ F.2.5 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 13.6 \\ F.1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 6.7 \\ D.C. 7.4 \\ \hline 33.0 \end{array}$$

11.5

Sta. + π - Grade
65.7

124 54.8 15.2

+55 56.0

125 57.0 15.3

+34

+67

126

+50

127

+50
+45

Lt.

E

Rt

$$\begin{array}{r} 10.9 \\ 17.9 \end{array}$$

$$\begin{array}{r} 8.7 \\ DC.42 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 12.1 \\ 1.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC.67 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ 11.7 \end{array}$$

$$\begin{array}{r} 8.9 \\ DC.28 \\ \hline 28. \end{array}$$

$$\begin{array}{r} 10.7 \\ F.1.0 \end{array}$$

$$\begin{array}{r} 6.3 \\ DC.54 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.7 \\ 10.7 \end{array}$$

$$\begin{array}{r} 6.2 \\ DC.45 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ F.0.3 \end{array}$$

$$\begin{array}{r} 1.6 \\ DC.91 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.6 \\ 13.6 \end{array}$$

$$\begin{array}{r} 11.3 \\ DC.23 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 24 \\ DC.11.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.7 \\ 14.7 \end{array}$$

$$\begin{array}{r} 12.7 \\ DC.00 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC.84 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.6 \\ 11.6 \end{array}$$

$$\begin{array}{r} 11.6 \\ DC.00 \\ \hline 20.3 \end{array}$$

$$\begin{array}{r} 3.9 \\ DC.7.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 7.6 \\ 9.6 \end{array}$$

$$\begin{array}{r} 9.4 \\ DC.02 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 2.2 \\ DC.54 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 10.9 \\ 12.9 \end{array}$$

$$\begin{array}{r} 11.0 \\ DC.19 \\ \hline 26. \end{array}$$

$$\begin{array}{r} 5.0 \\ DC.7.9 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.4 \\ 11.4 \end{array}$$

$$\begin{array}{r} 9.0 \\ DC.24 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC.7.3 \\ \hline 33.0 \end{array}$$

Site. + π - Grand

128

+50

129

+50

130

+50

131

+50

132

LH.

E

RH.

$$\begin{array}{r} 8.0 \\ 10.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ D.C. 1.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ D.C. 4.3 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 7.1 \\ 9.1 \end{array}$$

$$\begin{array}{r} 6.7 \\ D.C. 2.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 3.7 \\ D.C. 5.4 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ 8.2 \end{array}$$

$$\begin{array}{r} 8.2 \\ D.C. 2.0 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 2.4 \\ D.C. 1.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ 7.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ D.C. 0.0 \\ \hline 19.7 \end{array}$$

$$\begin{array}{r} 1.2 \\ D.C. 6.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ 7.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ 7.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ D.C. 1.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 3.3 \\ D.C. 4.0 \\ \hline 31.9 \end{array}$$

$$\begin{array}{r} 5.6 \\ 7.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ D.C. 0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.7 \\ D.C. 1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ 7.0 \end{array}$$

$$\begin{array}{r} 7.0 \\ D.C. 0.0 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 5.7 \\ D.C. 1.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 4.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 7.2 \\ D.C. 1.9 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 4.4 \\ D.C. 1.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 3.6 \\ 5.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ D.C. 1.2 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ D.C. 1.4 \\ \hline 25.8 \end{array}$$

Sta + π - Grade

132+50

17.1 84.9

72.8 Sta 133 97.8
71.5 80.3

133

+27

72.9

+75

73.5

134

73.8

74.0

80.2

+58

74.6

135

11.00 85.2

75.1 F.O.9

74.2 Sta 135

+50

75.7

L+

E

R+

$$\begin{array}{r} 3.2 \\ 5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ R2.3 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 3.5 \\ DC1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 17.4 \\ 14.4 \\ \hline \end{array}$$

$$\begin{array}{r} 13.5 \\ DC0.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 12.1 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 10.2 \\ DC4.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 12.0 \\ 14.0 \\ \hline \end{array}$$

$$\begin{array}{r} 13.3 \\ DC0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 11.6 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ DC5.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.4 \\ 13.4 \\ \hline \end{array}$$

$$\begin{array}{r} 12.0 \\ DC1.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 11.2 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ DC1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 11.1 \\ 13.1 \\ \hline \end{array}$$

$$\begin{array}{r} 9.8 \\ DC3.3 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 10.9 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ DC3.6 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 10.3 \\ 12.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.5 \\ DC3.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ F0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 1.0 \\ DC11.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ 11.8 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ 2.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 10.7 \\ F0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ DC5.8 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ 11.5 \\ \hline \end{array}$$

$$\begin{array}{r} 16.7 \\ F7.2 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 10.8 \\ F1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 12.1 \\ F7.6 \\ \hline 20.2 \end{array}$$

5/8 + π - Grade
85.7

136 76.4 F.V. 1

+22 76.7

+50 77.0

137 77.7 F.V. 1

+33 78.1

138 79.0 F.V. 6

+46 79.6

+72 79.9

LT

2

PL

8.8

$$\begin{array}{r} 16.4 \\ \times 1.76 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 10.9 \\ \times 1.21 \\ \hline \end{array}$$

$$\begin{array}{r} 15.8 \\ \times 1.20 \\ \hline 29.0 \end{array}$$

8.5

X

$$\begin{array}{r} 12.7 \\ \times 1.12 \\ \hline 25.4 \end{array}$$

8.2

$$\begin{array}{r} 14.1 \\ \times 1.59 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 10.5 \\ \times 1.23 \\ \hline \end{array}$$

$$\begin{array}{r} 16.4 \\ \times 1.82 \\ \hline 31.4 \end{array}$$

7.5

$$\begin{array}{r} 11.9 \\ \times 1.44 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 9.6 \\ \times 1.21 \\ \hline \end{array}$$

$$\begin{array}{r} 12.7 \\ \times 1.52 \\ \hline 25.4 \end{array}$$

7.1
9.1

$$\begin{array}{r} 9.9 \\ \times 1.28 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 8.9 \\ \times 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ \times 1.33 \\ \hline 21.6 \end{array}$$

6.2
8.2

$$\begin{array}{r} 12.6 \\ \times 1.68 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 7.8 \\ \times 1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ \times 1.22 \\ \hline 25.4 \end{array}$$

5.6
7.6

$$\begin{array}{r} 11.0 \\ \times 1.54 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 6.6 \\ \times 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ \times 1.41 \\ \hline 31.4 \end{array}$$

5.3
7.3

$$\begin{array}{r} 8.1 \\ \times 1.26 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ \times 1.06 \\ \hline \end{array}$$

$$\begin{array}{r} 3.1 \\ \times 1.42 \\ \hline 31.4 \end{array}$$

513. + π - Grade
85.7

139 80.3 80.3

+50 80.9

+75 81.3

140 81.6 81.6

+22

+70

141

+38

+69

LX

Z

CH

4.9
6.9

8.4
F3.5
22.0

5.2
F0.3

5.5
D.C. 1.4
25.8

4.3
6.3

6.8
F1.5
20.0

4.3
F0.0

6.9
F.26
20.2

3.9
5.9

X

3.9
F.00

5.9
F.20
19.0

3.6
5.6

5.4
D.C. 0.2
23.4

3.5
C.0.1

X

13.9
15.9

10.9
D.C. 0.0
23.0

4.0
D.C. 4.9
32.8

12.9
14.8

12.6
D.C. 2.2
27.4

5.9
D.C. 4.9
32.8

12.0
14.0

11.3
D.C. 2.2
28.4

9.0
D.C. 1.0
33.0

10.9
12.9

9.8
D.C. 3.1
25.1

5.0
D.C. 7.9
33.0

10.1
12.1

8.0
D.C. 4.1
25.1

3.8
D.C. 8.3
33.0

572. + π - Grade

147

+50

143

+40

+75

144

+60

145

LH

E

R+

9.5
11.5

6.5
DC 5.0
33.0

4.8
DC 6.7
33.0

8.9
10.9

6.9
DC 4.0
31.0

8.2
DC 2.7
28.4

8.4
10.4

7.1
DC 3.3
28.6

9.1
DC 1.3
25.6

9.2
11.2

8.0
DC 3.2
29.4

10.0
DC 1.2
25.4

8.7
10.7

5.6
DC 5.1
33.0

8.4
DC 2.3
27.6

8.6
10.6

5.1
DC 5.5
33.0

8.6
DC 3.0
27.0

8.3
10.3

5.7
DC 4.6
32.4

12.7
F 4.4
23.8

8.0
10.0

6.6
DC 3.4
29.8

10.2
F 2.2
19.4

Sta. + π - Grade

145+55

5.4

96.0

90.6

Sta. 146

146

90.4

0.02

+35

90.5

+80

90.7

147

90.8

91.1
0.03

+40

91.0

+94

91.2

148

91.2

0.04

L+

E

R+

$$\begin{array}{r} 7.5 \\ 9.5 \end{array}$$

$$\begin{array}{r} 51 \\ DC44 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 88 \\ DC07 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ 7.6 \end{array}$$

$$\begin{array}{r} 38 \\ DC38 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 54 \\ C0.1 \end{array}$$

$$\begin{array}{r} 73 \\ DC03 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ 7.5 \end{array}$$

$$\begin{array}{r} 42 \\ DC33 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 51 \\ C0.4 \end{array}$$

$$\begin{array}{r} 59 \\ DC16 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ 7.3 \end{array}$$

$$\begin{array}{r} 48 \\ DC25 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 49 \\ C0.4 \end{array}$$

$$\begin{array}{r} 42 \\ DC31 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ 7.2 \end{array}$$

$$\begin{array}{r} 54 \\ DC19 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 49 \\ C0.3 \end{array}$$

$$\begin{array}{r} 45 \\ DC27 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ 7.0 \end{array}$$

$$\begin{array}{r} 70 \\ DC00 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 52 \\ F0.1 \end{array}$$

$$\begin{array}{r} 56 \\ DC14 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.8 \end{array}$$

+

$$\begin{array}{r} 52 \\ F0.4 \end{array}$$

$$\begin{array}{r} 34 \\ DC34 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.8 \end{array}$$

$$\begin{array}{r} 66 \\ DC22 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 52 \\ F0.4 \end{array}$$

+

Sta + K - Grade
96.0

148+46 91.4

+57 91.4

149 91.6 F.O.D

+55 91.8

150 91.0 F.O.D

9.7 901.1 91.4 Sta 150

+25 91.2

+73 91.5

151 92.7 P.I.T

LT

E

RT

4.6
6.6

60
D.C. 0.6
24.2

51
F.O. 5

81
F. 3.5
22.0

4.6
6.6

X

4.4
6.4

43
D.C. 2
27.2

51
F.O. 7

94
F.F.O
25.0

4.2
6.2

30
D.C. 3.2
29.4

49
F.O. 7

62
D.C. 0.0
22.2

4.0
6.0

21
D.C. 3.9
30.8

46
F.O. 6

57
D.C. 0.3
23.6

8.9
10.9

78
D.C. 3.9
24.2

98
F.O. 9

110
F. 2.1
19.2

8.6
10.6

106
F. 2.0
19.0

99
F. 1.3

142
F. 5.6
26.2

8.4
10.4

104
F. 2.0
19.0

99
F. 1.1

153
F. 6.9
28.8

$5\frac{1}{2}$	+	π	-	Grade
151+53		901.1		93.2

+62				93.3
-----	--	--	--	------

+84				93.5
-----	--	--	--	------

152				93.8	E. 1.0
-----	--	--	--	------	--------

+50				94.4
-----	--	--	--	------

153				95.0	E. 0.3
-----	--	--	--	------	--------

+50				95.7
-----	--	--	--	------

154				96.3	E. 0.4
-----	--	--	--	------	--------

+50				
-----	--	--	--	--

Lt.

E

Rt.

$$\begin{array}{r} 7.9 \\ 9.9 \end{array}$$

$$\begin{array}{r} 104 \\ F.2.5 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ F.1.6 \end{array}$$

$$\begin{array}{r} 14.0 \\ F.6.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 7.8 \\ 9.8 \end{array}$$

X

$$\begin{array}{r} 7.6 \\ 9.6 \end{array}$$

X

$$\begin{array}{r} 7.3 \\ 9.3 \end{array}$$

$$\begin{array}{r} 25 \\ F.2.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 83 \\ F.1.0 \end{array}$$

$$\begin{array}{r} 93 \\ D.C.00 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 6.7 \\ 8.7 \end{array}$$

$$\begin{array}{r} 24 \\ D.C.1.3 \\ \hline 25.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ F.0.3 \end{array}$$

$$\begin{array}{r} 5.7 \\ D.C.3.0 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 6.1 \\ 8.1 \end{array}$$

$$\begin{array}{r} 4.5 \\ D.C.2.6 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 5.8 \\ C.0.3 \end{array}$$

$$\begin{array}{r} 6.6 \\ D.C.1.5 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ 7.4 \end{array}$$

$$\begin{array}{r} 2.13 \\ D.C.1.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ C.0.3 \end{array}$$

$$\begin{array}{r} 5.4 \\ D.C.2.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.8 \end{array}$$

$$\begin{array}{r} 3.4 \\ D.C.3.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ C.0.3 \end{array}$$

$$\begin{array}{r} 6.3 \\ D.C.0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ 6.3 \end{array}$$

$$\begin{array}{r} 3.2 \\ D.C.3.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 6.3 \\ D.C.0.0 \\ \hline 24.7 \end{array}$$

Sta + K - Grade

"D"

Slope stakes.

9/38

30' Top

23' to Back slope

2' Ditch

2 to 1 Slopes

Sta.	+	π	-	Elev.
B.M.				1024.40

155

+50

+50

156

+50

157

+50

158

+50

Use at below present Grade of Road

Lt.

E

Rt.

Top of Mon. Bellaire & D.

$$\begin{array}{r} 116 \\ 136 \end{array}$$

$$\begin{array}{r} 103 \\ \text{D.C. } 33 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 145 \\ \text{F29} \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 112 \\ 132 \end{array}$$

$$\begin{array}{r} 100 \\ \text{D.C. } 32 \\ \hline 29.4 \end{array}$$

$$\begin{array}{r} 136 \\ \text{F24} \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 105 \\ 125 \end{array}$$

$$\begin{array}{r} 99 \\ \text{D.C. } 26 \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 129 \\ \text{F24} \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 95 \\ 115 \end{array}$$

$$\begin{array}{r} 92 \\ \text{D.C. } 23 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 121 \\ \text{F26} \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 84 \\ 104 \end{array}$$

$$\begin{array}{r} 82 \\ \text{D.C. } 17 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 107 \\ \text{F23} \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 68 \\ 88 \end{array}$$

$$\begin{array}{r} 77 \\ \text{D.C. } 11 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 93 \\ \text{F25} \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 53 \\ 73 \end{array}$$

$$\begin{array}{r} 61 \\ \text{D.C. } 12 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 61 \\ \text{D.C. } 12 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 39 \\ 59 \end{array}$$

$$\begin{array}{r} 38 \\ \text{D.C. } 21 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 32 \\ \text{D.C. } 27 \\ \hline 28.4 \end{array}$$

2 1/2 + π - Grade

159

+50

160

+50

161

+65

164

+30

4.

2

21

13.3
15.3

12.8
DC25
28.0

12.8
DC25
28.0

11.3
13.3

10.6
DC27
28.4

11.3
DC27
27.0

9.2
11.2

8.9
DC23
27.6

8.7
DC25
28.0

7.3
9.3

7.1
DC21
27.2

5.6
DC37
30.4

5.2
7.2

4.2
DC3.0
29.0

2.5
DC4.7
32.4

14.0
16.0

10.4
DC4.6
33.0

13.3
DC27
28.4

13.0
15.0

9.0
DC6.0
33.0

13.3
DC18
26.6

X

Sta + π - Grade

162+65

163

+37

+62

164

+42

+84

+97

LT.

£

RT.

112
132

96
DC34
30.4

100
DC32
29.4

102
122

103
DC19
26.8

60
DC62
33.0

93
11.3

103
DC1.0
25.0

3.2
DC.81
33.0

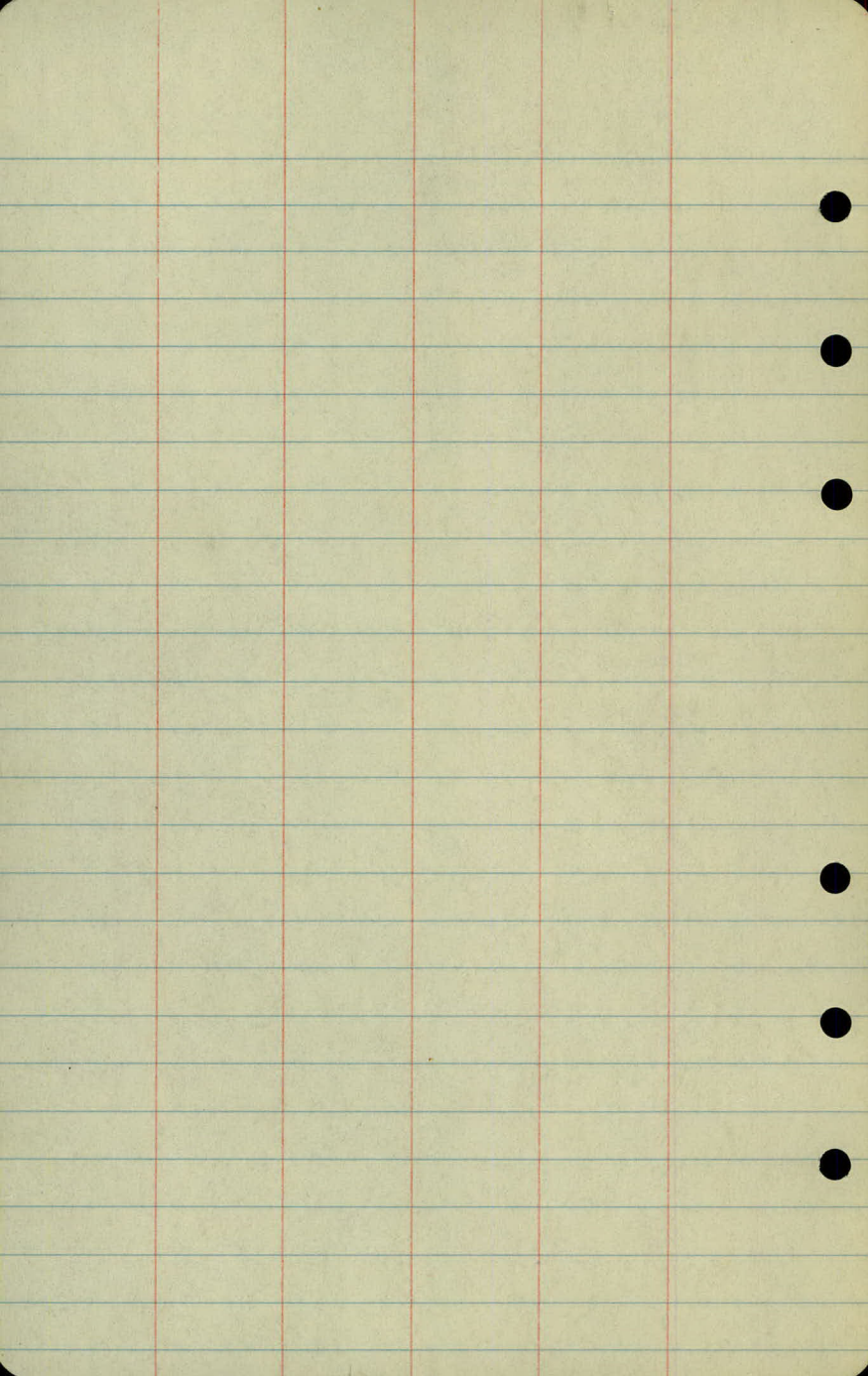
90
11.0

20
DC40
31.0

85
10.5

105
DC00
23.0

86
DC05
24.8



30' Crown

2 to 1 Slopes

2' Pitch

23' to Back slope

"D"

Slope stakes from Bellaire
to East Co. Line.

165+095⁸

Sta. + K - Grade

B.M.

1024.40

165+22

50
+38

166

+50

167

+50

475

+92

168+11

Lt.

E

Rt.

Top of Mon. @ Bellaire & "D"

6.0
8.0
$$\begin{array}{r} 54 \\ DC26 \\ \hline 382 \end{array}$$
4.7
4.7
$$\begin{array}{r} 42 \\ DC25 \\ \hline 280 \end{array}$$

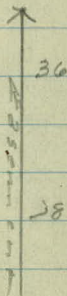
$$\begin{array}{r} 150 \\ F103 \\ \hline 330 \end{array}$$
3.6
5.6
$$\begin{array}{r} 0.9 \\ DC47 \\ \hline 324 \end{array}$$

$$\begin{array}{r} 23 \\ F37 \\ \hline 224 \end{array}$$
12.3
14.3
$$\begin{array}{r} 97 \\ DC46 \\ \hline 322 \end{array}$$

$$\begin{array}{r} 126 \\ DC17 \\ \hline 204 \end{array}$$
12.1
14.1
$$\begin{array}{r} 117 \\ DC24 \\ \hline 278 \end{array}$$

$$\begin{array}{r} 98 \\ DC43 \\ \hline 316 \end{array}$$
1
12.4
14.4
$$\begin{array}{r} 111 \\ DC33 \\ \hline 296 \end{array}$$

$$\begin{array}{r} 79 \\ DC65 \\ \hline 360 \end{array}$$
12.1
14.1
$$\begin{array}{r} 80 \\ DC65 \\ \hline 380 \end{array}$$

$$\begin{array}{r} 70 \\ DC75 \\ \hline 380 \end{array}$$


Sta + π - Grade

168+38

+81

169

+40

+65

170

+31

+68

47.

27

12+

13.0
15.0

86
64
D.C. 330

$$\begin{array}{r} 5.9 \\ \times 9 \\ \hline 53.1 \end{array}$$

144
16.1

$$\begin{array}{r} 15.9 \\ 0.602 \\ \hline 23.4 \end{array}$$

42
D.C. 119
468

14.7
16.7

$$\begin{array}{r} 10^3 \\ \hline 64 \\ \hline 33. \end{array}$$
$$\begin{array}{r} 5.7 \\ 0.5110 \\ \hline 45.0 \end{array}$$

✓ 5-4
7.4

$$\begin{array}{r} 74 \\ 0 \overline{) 5180} \\ \underline{518} \\ 0 \end{array}$$
$$\begin{array}{r} 24 \\ 17.600 \\ \hline 230 \end{array}$$

✓
✓
✓

9.2
PL 100/21

$$\begin{array}{r} 10.3 \\ \times 4.1 \\ \hline 23.2 \end{array}$$

7.5
9.1

$$\begin{array}{r} 7 \\ 14 \overline{) 98} \\ \underline{98} \\ 0 \end{array}$$
$$\begin{array}{r} 114 \\ \times 39 \\ \hline 228 \\ 3420 \\ \hline \end{array}$$

8 ✓

$$\begin{array}{r} 164 \\ \times 80 \\ \hline 13120 \end{array}$$
$$\begin{array}{r} 12^{\circ} \\ \times 38 \\ \hline 96 \\ 240 \\ \hline 456 \end{array}$$

✓
m.

12⁴ / 49 / 30

$$\begin{array}{r} 87 \\ \times 55 \\ \hline 435 \\ 870 \\ \hline 4785 \end{array}$$

42
43
44
45
46
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48
49
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80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100

Sta. + TC - Grade

171

+50

B.M. 8.40 1037.80 12.40 1024.40
3.17 1023.57 1020.40

172

18.0

+50

17.5

173

17.1

+50

16.8

T.P. 9.67 1026.46 6.68 1016.84

174

16.7 14.7

+50

16.8 14.6

Lt.

Q

Rt.

3.9

$$\begin{array}{r} 129 \\ \times 90 \\ \hline 11610 \\ 11610 \\ \hline 11610 \end{array}$$

$$\begin{array}{r} 108 \\ \times 69 \\ \hline 972 \\ 648 \\ \hline 7452 \end{array}$$

5.2

$$\begin{array}{r} 116 \\ \times 64 \\ \hline 464 \\ 1280 \\ \hline 7424 \end{array}$$

$$\begin{array}{r} 135 \\ \times 83 \\ \hline 405 \\ 1080 \\ \hline 11115 \end{array}$$

5.5

$$\begin{array}{r} 109 \\ \times 14 \\ \hline 1526 \\ 1090 \\ \hline 15134 \end{array}$$

$$\begin{array}{r} 51 \\ \times 4 \\ \hline 204 \end{array}$$

$$\begin{array}{r} 132 \\ \times 27 \\ \hline 906 \\ 2640 \\ \hline 3564 \end{array}$$

6.0

$$\begin{array}{r} 91 \\ \times 31 \\ \hline 2731 \\ 2731 \\ \hline 28411 \end{array}$$

$$\begin{array}{r} 58 \\ \times 1 \\ \hline 58 \end{array}$$

$$\begin{array}{r} 126 \\ \times 66 \\ \hline 756 \\ 7560 \\ \hline 8316 \end{array}$$

6.4

$$\begin{array}{r} 117 \\ \times 35 \\ \hline 595 \\ 3500 \\ \hline 4095 \end{array}$$

$$\begin{array}{r} 140 \\ \times 0 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 128 \\ \times 64 \\ \hline 512 \\ 8192 \\ \hline 8216 \end{array}$$

6.7

$$\begin{array}{r} 18 \\ \times 69 \\ \hline 1242 \\ 1620 \\ \hline 12420 \end{array}$$

$$\begin{array}{r} 67 \\ \times 0 \\ \hline 0 \end{array}$$

$$\begin{array}{r} 126 \\ \times 19 \\ \hline 1134 \\ 2352 \\ \hline 2352 \end{array}$$

9.8

11.8

$$\begin{array}{r} 27 \\ \times 91 \\ \hline 243 \\ 2430 \\ \hline 2430 \end{array}$$

$$\begin{array}{r} 97 \\ \times 1 \\ \hline 97 \end{array}$$

$$\begin{array}{r} 151 \\ \times 53 \\ \hline 453 \\ 7560 \\ \hline 7560 \end{array}$$

9.7

11.7

$$\begin{array}{r} 80 \\ \times 37 \\ \hline 560 \\ 2560 \\ \hline 2560 \end{array}$$

$$\begin{array}{r} 96 \\ \times 1 \\ \hline 96 \end{array}$$

$$\begin{array}{r} 117 \\ \times 00 \\ \hline 0 \end{array}$$

Special Ditch

Sta + N - Grade

1026.46

175 17.0 14.5

T.P. 11.90 1028.44 9.92 1016.34

+50 17.2

176 17.5

+50 17.7

177 18.0

+50 18.2

178 18.5

+23 18.6

Special Pitch

4.

£

Rt.

9.5 12.0
11.1
1/2 T.P.P.

130
F.3.5
22.0

96
F.0.1

102
DC.1.3
25.6

11.2
13.2

16.0
F.4.8
24.4

12.1
F.0.9

126
DC.0.6
24.2

10.9
12.7

15.8
F.4.8
24.8

12.8
F.1.9

135
F.2.6
20.2

10.7
12.7

16.1
F.1.4
25.8

13.0
F.2.3

140
F.3.3
21.6

10.4
12.4

16.3
F.1.9
26.8

126
F.2.2

138
F.3.4
21.8

10.2
12.2

16.8
F.1.8
26.6

11.7
F.1.1

138
F.3.6
22.2

9.9
11.9

15.9
F.6.0
27.0

10.1
F.0.2

86
DC.3.3
29.6

9.8
11.8

15.4
F.5.6
26.2

94
F.0.4

88
DC.6.0
35.0

35

Sta.	+	T	-	Grade
------	---	---	---	-------

178+46				18.7
T.P.	7.75	1035.63	0.56	1027.88

179				19.0
-----	--	--	--	------

T.P.	6.87	1039.78	2.72	1034.91
------	------	---------	------	---------

+54				19.2
-----	--	--	--	------

+85				19.4
-----	--	--	--	------

180				19.5
-----	--	--	--	------

+30				19.6
-----	--	--	--	------

T.P.	3.02	1030.13	12.67	1022.11
------	------	---------	-------	---------

+65				19.8
-----	--	--	--	------

181				20.0
-----	--	--	--	------

CH

E

RT.

9.7
11.7

11.7
DC 0.0
22.5

8.8
C.O.9

3.0
DC 8.7
40.4

41

16.6
18.6

16.8
DC 1.8
26.6

14.8
C.1.8

3.3
DC 15.3
53.6

54

20.6
22.6

15.5
DC 7.1
37.2

C.2.3

1.9
DC 20.7
64.4

64

43

20.4
22.4

12.2
DC 10.2
43.4

18.2
C.2.2

7.7
DC 14.7
52.4

53

44

20.3
22.3

11.6
DC 10.7
44.4

18.3
C.2.0

10.7
DC 11.6
46.2

Document

43

20.2
22.2

11.5
DC 10.7
44.4

18.3
C.1.9

15.6
DC 6.6
36.2

37

35

✓ 10.3
11.3

6.4
DC 1.9
34.8

8.7
C.1.6

8.8
DC 3.5
30

10.1
11.1

11.3
DC 0.8
24.6

9.4
C.O.

12.9
P.2.8
20.6

Sta	+	π	-	Grade
T.P.	344	1030.13	10.57	1019.56
181+40				20.2

182				20.5
-----	--	--	--	------

+50				20.7
-----	--	--	--	------

183				21.0
-----	--	--	--	------

+40				21.2
-----	--	--	--	------

T.P.	14.74	1031.55	4.17	1018.83
------	-------	---------	------	---------

+70				21.3
-----	--	--	--	------

184				21.6
-----	--	--	--	------

+80				22.0
-----	--	--	--	------

Lt.

E

Rt.

2.8
4.8
BM 1015.72

8.9
F6.1
27.2

3.4
F0.6

10.8
F8.0
31

2.5
4

11.1
F8.6
32.2

4.5
F2.0

10.7
F8.2
31.4

2.3

10.9
F8.6
32.2

4.8
F2.5

10.7
F8.4
31.8

2.0

10.5
F8.5
32.0

4.8
F2.8

10.2
F8.2
31.4

1.8

7.6
F5.8
26.6

4.4
F2.6

9.1
F7.3
29.6

10.3

X

10.0
14.0

12.6
F2.6
20.2

12.2
F2.2

13.2
F3.2
21.4

F. 2.2

9.6
11.6

11.2
9.6
23.8

11.1
F1.1

11.2
9.6
23.8

Sta. + π - Grade

1031.55

185

22.6

+50

23.3

186

24.3

~~~~~

~~~~~  
off 4

+30

24.8

+65

25.6

187

+52

188

Lt.

E

Rt.

$$\begin{array}{r} 9.0 \\ 11.0 \end{array}$$

$$\begin{array}{r} 8.6 \\ DC2.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 9.5 \\ F0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ DC1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 8.3 \\ 10.3 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC.48 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 8.0 \\ F0.0 \\ \hline 60.3 \end{array}$$

$$\begin{array}{r} 7.5 \\ DC2.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ 9.3 \end{array}$$

$$\begin{array}{r} 9.3 \\ DC.00 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ DC0.6 \\ \hline 24.2 \end{array} \quad C0.4$$

$$\begin{array}{r} 6.6 \\ 8.6 \end{array}$$

$$\begin{array}{r} 10.8 \\ F4.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 8.6 \\ DC.00 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 6.0 \\ 8.0 \end{array}$$

$$\begin{array}{r} 10.9 \\ F4.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 7.4 \\ DC0.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ 7.2 \end{array}$$

$$\begin{array}{r} 10.8 \\ F5.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 6.5 \\ DC0.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 3.6 \\ 5.6 \end{array}$$

$$\begin{array}{r} 8.2 \\ F4.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ DC.00 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 1.8 \\ 3.8 \end{array}$$

$$\begin{array}{r} 5.3 \\ F2.5 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 1.5 \\ DC2.3 \\ \hline 22.6 \end{array}$$

Sto. + π - Grade

188450

189

+50

190

+58

+82✓

+90

191

+23

B.M.

1035.02

LH

Q

RT

15.0
17.0

11.2
DC 1.8
26.6

10.1
DC 6.9
33.0

13.6 35
15.6

9.8
DC 5.8
34.6

8.1
DC 25.5
33.0

12.2
14.2

39

6.1
DC 7.7
38.4

10.3
DC 3.9
30.8

11.5
13.5

41

4.8
DC 8.7
40.4

6.8
DC 0.0 4.8
23.0 6.8

11.3
13.3

41

4.6
DC 8.7
40.4

10.1
F. 6 4.5
26.2 6.5

11.2
13.2

5.0
DC 8.7
39.4

7.7
F. 3.2 4.5
21.4

X

Top of Brass plug in Perament

9 3/4
7 3/4

6 1/4
4 1/4

Lt

R

Rt

T.P. # 13.4t

$$\begin{array}{r} \downarrow \\ (14.9) \quad \frac{14.2}{17} \quad \frac{10.2}{25} \quad \frac{9.1}{30} \quad \frac{6.9}{50} \end{array}$$

$$\begin{array}{r} \downarrow \\ (26.1) \quad \frac{11.1}{38} \quad \frac{10.0}{42} \quad \frac{9.5}{50} \quad \frac{7.3}{75} \quad \frac{6.3}{100} \end{array}$$

$$\begin{array}{r} \downarrow \\ (31.8) \quad \frac{8.0}{38} \quad \frac{6.4}{45} \quad \frac{5.8}{50} \quad \frac{3.5}{73} \quad \frac{2.7}{100} \end{array}$$

$$\begin{array}{r} \downarrow \\ (22.9) \quad \frac{7.5}{40} \quad \frac{6.8}{47} \quad \frac{6.2}{50} \quad \frac{3.4}{73} \quad \frac{1.2}{100} \end{array}$$

$$\begin{array}{r} \downarrow \\ (21.2) \quad \frac{7.3}{37} \quad \frac{5.5}{47} \quad \frac{3.0}{82} \quad \frac{1.5}{100} \end{array}$$

$$\begin{array}{r} \downarrow \\ (19.6) \quad \frac{8.9}{21} \quad \frac{8.6}{42} \quad \frac{5.2}{70} \quad \frac{2.0}{100} \end{array}$$

$$\begin{array}{r} \downarrow \\ \frac{7.2}{30} \quad \frac{7.2}{49} \quad \frac{8.5}{28} \quad \frac{10.3}{18} \quad (18.2) \quad \frac{9.3}{22} \quad \frac{9.0}{50} \quad \frac{8.9}{61} \quad \frac{6.9}{75} \end{array}$$

$$\begin{array}{r} \downarrow \\ (22.1) \quad \frac{4.9}{30} \quad \frac{5.0}{15.1} \quad \frac{4.22}{15.1} \quad \frac{4.28}{13.1} \quad \frac{6.65}{13.1} \quad \frac{6.81}{11.3} \quad \frac{4.78}{17.3} \quad \frac{6.86}{11.0} \quad \frac{6.69}{12.7} \quad \frac{4.33}{12.7} \quad \frac{4.83}{19.7} \quad \frac{4.8}{14.7} \quad \frac{4.9}{50} \end{array}$$

$$\frac{3.31}{50}$$

$$\frac{3.26}{50}$$

$$\frac{3.92}{50}$$

$$\frac{3.29}{50}$$

$$\frac{3.24}{50}$$

$$\frac{3.43}{50}$$

$$\begin{array}{r} \downarrow \\ \frac{4.8}{30} \quad \frac{4.7}{15} \quad \frac{4.32}{150} \quad \frac{4.23}{150} \quad \frac{6.68}{13} \quad \frac{6.81}{11.3} \quad (21.8) \quad \frac{6.88}{11.2} \quad \frac{6.21}{130} \quad \frac{4.35}{130} \quad \frac{4.32}{150} \quad \frac{4.8}{15} \quad \frac{4.9}{50} \end{array}$$

X Top S.E. Cor. Found.

Sta	+	-	Elev
B.M.	066	903.07	902.41

58			899.9 ✓
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+40			98.7 ✓
-----	--	--	--------

59			97.0 ✓
----	--	--	--------

+36			96.7 ✓
-----	--	--	--------

+41			96.6 ✓
-----	--	--	--------

		2 Book 54	96.3 ✓
--	--	-----------	--------

+70			96.0 ✓
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+80			95.9 ✓
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60			95.6 ✓
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+50			95.6 ✓
-----	--	--	--------

61			96.1 ✓
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Lt

R

Rt

X Test S.E. Cor. Found

$$\begin{array}{cccccccccccc} 19.5 & 16.5 & 13.3 & 9.9 & 3.4 & 3.2 & 3.9 & 3.4 & 10.3 & 11.7 & 11.5 \\ 50 & 28 & 17 & 7 & 5 & & 7 & 10 & 19 & 29 & 50 \end{array}$$

$$\begin{array}{cccccccccc} 7.0 & 6.4 & 4.4 & 4.7 & 9.5 & 4.4 & 4.8 & 5.0 & 6.8 & 8.9 \\ 50 & 33 & 21 & 14 & 8 & & 8 & 21 & 30 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 10.7 & 8.9 & 8.4 & 7.6 & 6.4 & 6.1 & 6.1 & 6.4 & 6.7 & 5.9 & 5.9 & 5.8 & 7.5 & 9.1 & 10.5 \\ 50 & 38 & 33 & 21 & 15 & 10 & & 7 & 19 & 16 & 19 & 24 & 29 & 34 & 50 \end{array}$$

$$\begin{array}{cccccccccc} 11.0 & 10.0 & 9.0 & 9.0 & 8.7 & 7.2 & 6.8 & 6.4 & 6.5 & 7.6 & 8.6 & 8.8 \\ 50 & 37 & 35 & 31 & 23 & 17 & 8 & & 7 & 23 & 36 & 50 \end{array}$$

$$\begin{array}{cccc} 6.5 & 6.6 & 6.7 & 7.4 & 7.6 \\ & 6 & 13 & 29 & 30 \end{array}$$

$$\begin{array}{ccc} 6.8 & 6.8 & 7.0 \\ & 8 & 30 \end{array}$$

$$\begin{array}{ccc} 7.1 & & 7.1 & & 7.6 & 7.6 \\ & & 10 & & 28 & 30 \end{array}$$

$$\begin{array}{cccccccccc} 11.0 & 11.2 & 11.2 & 11.7 & 8.0 & 7.6 & 7.2 & 7.3 & 8.1 & 10.8 & 11.7 \\ 50 & 35 & 31 & 22 & 14 & 8 & & 7 & 15 & 21 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 10.2 & 10.5 & 11.1 & 12.59 & 11.3 & 8.2 & 7.8 & 7.5 & 7.7 & 8.2 & 12.49 & 11.7 & 11.7 & 11.8 \\ 50 & 33 & 29 & \text{Culy} & 20 & 13 & 8 & & 6 & 12 & \text{Culy} & 20 & 27 & 50 \end{array}$$

$$\begin{array}{cccccccccccccccc} 9.5 & 8.7 & 9.5 & 10.2 & 10.2 & 7.9 & 7.7 & 7.5 & 7.8 & 8.2 & 12.0 & 14.0 & 11.2 & 11.2 & 12.5 & 12.0 \\ 50 & 33 & 29 & 21 & 18 & 12 & 9 & & 8 & 11 & 18 & 23 & 25 & 29 & 31 & 50 \end{array}$$

$$\begin{array}{cccccccccccc} 8.9 & 8.9 & 8.0 & 8.7 & 8.9 & 7.5 & 7.1 & 7.0 & 7.3 & 7.8 & 8.9 & 11.1 & 11.6 & 12.0 \\ 50 & 34 & 33 & 29 & 18 & 14 & 8 & & 7 & 10 & 14 & 19 & 32 & 50 \end{array}$$

Sta	+	π	-	Elev.
		✓ 903.07		
61	+50			96.5 ✓
62				96.5 ✓
T.P.	9.37	✓ 906.03	6.91	896.66
	+50			97.2 ✓
63				98.2 ✓
	+50			98.9 ✓
64				900.0 ✓
	+50			01.9 ✓
65				05.0 ✓
	+50			(08.0) ✓
T.P.	12.50	✓ 919.06	0.47	905.56 ✓
65	+50			08.0 ✓
66				10.6 ✓

Lt.

A.

Rt.

$$\frac{116}{50} \quad \frac{107}{39} \quad \frac{95}{33} \quad \frac{86}{19} \quad \frac{79}{15} \quad \frac{69}{8} \quad \frac{66}{-} \quad \frac{67}{6} \quad \frac{69}{10} \quad \frac{74}{15} \quad \frac{89}{19} \quad \frac{89}{21} \quad \frac{89}{22} \quad \frac{88}{32} \quad \frac{97}{35} \quad \frac{109}{50}$$

$$\frac{124}{50} \quad \frac{118}{37} \quad \frac{105}{30} \quad \frac{104}{19} \quad \frac{78}{19} \quad \frac{72}{11} \quad \frac{68}{7} \quad \frac{66}{-} \quad \frac{66}{7} \quad \frac{70}{15} \quad \frac{93}{18} \quad \frac{93}{20} \quad \frac{73}{29} \quad \frac{73}{39} \quad \frac{72}{50}$$

$$\frac{147}{50} \quad \frac{134}{37} \quad \frac{130}{38} \quad \frac{122}{18} \quad \frac{96}{13} \quad \frac{92}{8} \quad \frac{88}{-} \quad \frac{90}{8} \quad \frac{96}{16} \quad \frac{110}{20} \quad \frac{89}{29} \quad \frac{84}{26} \quad \frac{91}{28} \quad \frac{88}{39} \quad \frac{86}{50}$$

$$\frac{142}{50} \quad \frac{127}{38} \quad \frac{125}{29} \quad \frac{128}{31} \quad \frac{120}{18} \quad \frac{87}{13} \quad \frac{82}{8} \quad \frac{78}{-} \quad \frac{81}{7} \quad \frac{87}{16} \quad \frac{104}{21} \quad \frac{83}{25} \quad \frac{71}{50}$$

$$\frac{141}{50} \quad \frac{137}{31} \quad \frac{130}{21} \quad \frac{80}{12} \quad \frac{75}{8} \quad \frac{71}{-} \quad \frac{73}{8} \quad \frac{81}{14} \quad \frac{129}{22} \quad \frac{115}{32} \quad \frac{106}{50}$$

$$\frac{123}{50} \quad \frac{126}{36} \quad \frac{120}{25} \quad \frac{100}{18} \quad \frac{68}{11} \quad \frac{69}{8} \quad \frac{60}{-} \quad \frac{65}{7} \quad \frac{70}{14} \quad \frac{132}{23} \quad \frac{130}{35} \quad \frac{127}{50}$$

$$\frac{99}{50} \quad \frac{109}{34} \quad \frac{96}{27} \quad \frac{88}{21} \quad \frac{50}{19} \quad \frac{46}{8} \quad \frac{41}{-} \quad \frac{44}{6} \quad \frac{50}{12} \quad \frac{122}{25} \quad \frac{130}{33} \quad \frac{129}{50}$$

$$\frac{77}{50} \quad \frac{78}{33} \quad \frac{75}{21} \quad \frac{17}{12} \quad \frac{13}{8} \quad \frac{10}{-} \quad \frac{10}{7} \quad \frac{12}{11} \quad \frac{67}{20} \quad \frac{123}{35} \quad \frac{128}{50}$$

$$\frac{40}{50} \quad \frac{43}{34} \quad \frac{30}{33} \quad \frac{33}{26} \quad \frac{19}{19} \quad \frac{20}{-} \quad \frac{36}{19} \quad \frac{75}{31} \quad \frac{95}{41} \quad \frac{106}{50}$$

$$\frac{115}{13} \quad \frac{113}{7} \quad \frac{111}{-} \quad \frac{113}{6} \quad \frac{117}{11}$$

$$\frac{121}{50} \quad \frac{132}{35} \quad \frac{112}{29} \quad \frac{108}{18} \quad \frac{92}{13} \quad \frac{88}{8} \quad \frac{84}{-} \quad \frac{86}{7} \quad \frac{90}{13} \quad \frac{141}{26} \quad \frac{176}{30}$$

Sta.	+	π	-	Elev.
		919.06		
66	+50			913.2 ✓
67				15.9 ✓
T.P.	12.71	931.17 ✓	1.60	917.46 ✓
	+47			17.8 ✓
68				19.8 ✓
T.P.	13.47	935.34 ✓	2.30	921.81 ✓
	+50			21.8
69				23.7
	+50			25.6
70				27.5
	+50			28.7
T.P.	11.5	934.16 ✓	2.03	923.31 ✓
71				29.4
	+62			29.8

Lt

R

Rt

$$\frac{6.9}{50} \quad \frac{7.7}{39} \quad \frac{6.8}{27} \quad \frac{6.0}{23} \quad \frac{6.1}{7} \quad \frac{5.8}{50} \quad \frac{6.1}{6} \quad \frac{6.7}{18} \quad \frac{13.0}{33} \quad \frac{13.0}{50}$$

$$\frac{0.5}{50} \quad \frac{0.5}{21} \quad \frac{3.5}{14} \quad \frac{3.5}{8} \quad \frac{3.2}{7} \quad \frac{3.3}{7} \quad \frac{3.7}{15} \quad \frac{3.4}{30} \quad \frac{6.6}{50}$$

$$\frac{6.1}{50} \quad \frac{6.3}{27} \quad \frac{13.7}{13} \quad \frac{13.7}{7} \quad \frac{13.4}{7} \quad \frac{13.5}{6} \quad \frac{13.7}{14} \quad \frac{11.2}{20} \quad \frac{11.0}{25} \quad \frac{8.4}{29} \quad \frac{9.5}{95} \quad \frac{9.4}{50}$$

$$\frac{2.7}{50} \quad \frac{2.2}{30} \quad \frac{2.3}{22} \quad \frac{11.7}{10} \quad \frac{11.4}{7} \quad \frac{11.1}{13} \quad \frac{12.0}{21} \quad \frac{7.7}{24} \quad \frac{6.4}{31} \quad \frac{2.0}{30} \quad \frac{3.5}{50}$$

$$\frac{6.2}{50} \quad \frac{5.0}{32} \quad \frac{5.6}{29} \quad \frac{14.2}{12} \quad \frac{13.7}{7} \quad \frac{13.5}{7} \quad \frac{13.7}{8} \quad \frac{14.1}{14} \quad \frac{3.7}{29} \quad \frac{9.5}{49} \quad \frac{5.0}{50}$$

$$\frac{4.8}{50} \quad \frac{5.2}{36} \quad \frac{4.5}{29} \quad \frac{12.1}{11} \quad \frac{11.8}{7} \quad \frac{11.6}{8} \quad \frac{11.8}{13} \quad \frac{12.3}{29} \quad \frac{3.7}{30} \quad \frac{4.4}{30}$$

$$\frac{2.5}{50} \quad \frac{2.3}{37} \quad \frac{2.5}{27} \quad \frac{4.5}{22} \quad \frac{6.4}{20} \quad \frac{10.9}{12} \quad \frac{9.9}{7} \quad \frac{9.7}{8} \quad \frac{9.9}{14} \quad \frac{10.9}{22} \quad \frac{6.9}{28} \quad \frac{3.0}{50} \quad \frac{3.9}{50}$$

$$\frac{1.9}{50} \quad \frac{2.1}{38} \quad \frac{1.5}{25} \quad \frac{2.6}{25} \quad \frac{5.0}{20} \quad \frac{6.1}{17} \quad \frac{8.2}{12} \quad \frac{7.9}{7} \quad \frac{7.8}{8} \quad \frac{8.1}{14} \quad \frac{2.9}{24} \quad \frac{2.4}{24} \quad \frac{3.0}{50}$$

$$\frac{1.0}{50} \quad \frac{1.8}{32} \quad \frac{0.5}{27} \quad \frac{1.0}{23} \quad \frac{6.9}{12} \quad \frac{6.6}{7} \quad \frac{6.6}{7} \quad \frac{6.8}{7} \quad \frac{6.9}{15} \quad \frac{8.6}{24} \quad \frac{1.4}{50}$$

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$$\frac{1.6}{50} \quad \frac{1.9}{29} \quad \frac{2.5}{19} \quad \frac{5.1}{13} \quad \frac{5.0}{7} \quad \frac{4.9}{7} \quad \frac{5.0}{7} \quad \frac{5.3}{15} \quad \frac{0.7}{21} \quad \frac{0.6}{31} \quad \frac{0.9}{50}$$

$$\frac{0.5}{50} \quad \frac{0.8}{30} \quad \frac{3.7}{29} \quad \frac{9.6}{12} \quad \frac{4.6}{7} \quad \frac{4.7}{7} \quad \frac{4.9}{7} \quad \frac{5.5}{15} \quad \frac{2.4}{21} \quad \frac{2.3}{37} \quad \frac{2.3}{50}$$

Sta.	+	π	-	Elev.
		734.96		729.6
72				29.3
+50				29.2
73				29.2
+50				29.4
74				29.3
+37				
I.P.	556	739.66 ✓	5.36	729.10 ✓
75				29.1
+50				29.1
76				29.1
+50				28.8
77				28.7

Lt

K

Rt

$\frac{0.5}{50}$ $\frac{1.0}{37}$ $\frac{3.3}{26}$ $\frac{8.7}{15}$ $\frac{5.1}{14}$ $\frac{4.8}{6}$ $\frac{4.9}{8}$ $\frac{5.0}{14}$ $\frac{5.6}{22}$ $\frac{6.1}{31}$ $\frac{2.0}{39}$ $\frac{2.7}{50}$

$\frac{4.8}{50}$ $\frac{5.3}{24}$ $\frac{5.5}{13}$ $\frac{5.3}{7}$ $\frac{5.2}{7}$ $\frac{5.3}{15}$ $\frac{5.9}{19}$ $\frac{4.1}{27}$ $\frac{4.4}{30}$ $\frac{5.0}{50}$

$\frac{5.7}{50}$ $\frac{6.2}{19}$ $\frac{6.0}{16}$ $\frac{5.5}{7}$ $\frac{5.3}{6}$ $\frac{5.4}{17}$ $\frac{4.1}{26}$ $\frac{7.4}{50}$

$\frac{5.0}{50}$ $\frac{5.9}{24}$ $\frac{5.7}{17}$ $\frac{5.4}{7}$ $\frac{5.3}{7}$ $\frac{5.4}{14}$ $\frac{6.1}{19}$ $\frac{7.4}{36}$ $\frac{8.2}{50}$

$\frac{8.4}{50}$ $\frac{6.7}{21}$ $\frac{5.8}{14}$ $\frac{5.2}{7}$ $\frac{5.1}{7}$ $\frac{5.2}{27}$ $\frac{5.3}{42}$ $\frac{5.5}{50}$

$\frac{8.9}{50}$ $\frac{8.9}{44}$ $\frac{8.1}{19}$ $\frac{5.9}{13}$ $\frac{5.5}{7}$ $\frac{5.2}{00}$ $\frac{5.2}{7}$ $\frac{5.8}{25}$ $\frac{6.4}{20}$ $\frac{6.0}{50}$

$\frac{9.1}{50}$ $\frac{9.8}{34}$ $\frac{9.7}{20}$ $\frac{6.4}{14}$ $\frac{5.8}{7}$ $\frac{5.6}{7}$ $\frac{5.8}{14}$ $\frac{6.4}{22}$ $\frac{10.9}{38}$ $\frac{11.2}{50}$

$\frac{8.0}{50}$ $\frac{8.5}{37}$ $\frac{8.5}{20}$ $\frac{6.5}{15}$ $\frac{5.8}{8}$ $\frac{5.4}{7}$ $\frac{5.8}{14}$ $\frac{6.6}{20}$ $\frac{9.8}{31}$ $\frac{11.1}{50}$

$\frac{8.3}{50}$ $\frac{8.4}{34}$ $\frac{8.3}{20}$ $\frac{6.2}{12}$ $\frac{5.8}{8}$ $\frac{5.6}{8}$ $\frac{5.8}{15}$ $\frac{6.5}{20}$ $\frac{7.9}{31}$ $\frac{8.4}{50}$

$\frac{8.0}{50}$ $\frac{8.5}{36}$ $\frac{8.0}{19}$ $\frac{6.3}{12}$ $\frac{6.0}{8}$ $\frac{5.9}{8}$ $\frac{6.2}{13}$ $\frac{6.5}{19}$ $\frac{7.7}{33}$ $\frac{8.1}{50}$

$\frac{8.8}{50}$ $\frac{8.2}{35}$ $\frac{8.0}{18}$ $\frac{6.5}{12}$ $\frac{6.2}{7}$ $\frac{6.0}{8}$ $\frac{6.2}{14}$ $\frac{6.8}{18}$ $\frac{8.1}{35}$ $\frac{9.2}{50}$

Sta	+	X	-	Elev.
		✓		
		934.6		
77	+50			929.1 .
78				29.8 .
	+50			30.5 .
79				31.3 .
	+50			31.9 .
80				32.6 .
T.P.	11.03	943.59 ✓	210	932.36 ✓
	+50			33.6 .
81				34.2 .
	+50			34.3 .
82				34.2 .
	+28			34.2 .

Lt

A

Rt

$$\frac{73}{50} \frac{74}{36} \frac{72}{19} \frac{65}{15} \frac{58}{7} \frac{36}{7} \frac{58}{7} \frac{66}{16} \frac{75}{20} \frac{80}{33} \frac{82}{50}$$

$$\frac{57}{50} \frac{61}{27} \frac{61}{19} \frac{53}{11} \frac{51}{6} \frac{49}{8} \frac{51}{17} \frac{59}{17} \frac{63}{33} \frac{68}{50}$$

$$\frac{35}{50} \frac{41}{36} \frac{40}{18} \frac{46}{11} \frac{44}{7} \frac{42}{7} \frac{49}{7} \frac{48}{15} \frac{52}{33} \frac{56}{50}$$

$$\frac{20}{50} \frac{25}{30} \frac{27}{18} \frac{36}{13} \frac{35}{6} \frac{34}{8} \frac{36}{13} \frac{37}{18} \frac{31}{25} \frac{35}{30} \frac{39}{50}$$

$$\frac{19}{30} \frac{18}{29} \frac{18}{18} \frac{33}{14} \frac{30}{7} \frac{28}{7} \frac{30}{15} \frac{33}{18} \frac{20}{35} \frac{30}{50} \frac{31}{50}$$

$$\frac{10}{50} \frac{05}{19} \frac{25}{19} \frac{23}{8} \frac{21}{7} \frac{29}{7} \frac{27}{18} \frac{19}{18} \frac{19}{21} \frac{20}{22} \frac{30}{50}$$

$$\frac{85}{50} \frac{80}{29} \frac{77}{19} \frac{106}{19} \frac{101}{8} \frac{100}{7} \frac{102}{18} \frac{107}{18} \frac{96}{18} \frac{91}{19} \frac{97}{26} \frac{99}{37} \frac{103}{50}$$

$$\frac{83}{50} \frac{80}{30} \frac{78}{26} \frac{71}{20} \frac{100}{15} \frac{98}{8} \frac{94}{8} \frac{96}{14} \frac{98}{14} \frac{80}{18} \frac{80}{21} \frac{81}{14} \frac{85}{30}$$

$$\frac{90}{50} \frac{83}{33} \frac{81}{17} \frac{101}{14} \frac{77}{8} \frac{94}{8} \frac{95}{8} \frac{98}{15} \frac{85}{19} \frac{89}{22} \frac{79}{28} \frac{80}{50}$$

$$\frac{73}{50} \frac{107}{31} \frac{109}{15} \frac{139}{12} \frac{77}{19} \frac{94}{7} \frac{97}{13} \frac{101}{18} \frac{112}{38} \frac{106}{38} \frac{103}{50}$$

$$\frac{111}{50} \frac{117}{31} \frac{118}{16} \frac{103}{13} \frac{98}{9} \frac{94}{7} \frac{97}{7} \frac{100}{12} \frac{116}{20} \frac{118}{31} \frac{117}{50}$$

Sta.	+	π	-	Elev
		948.59		
83				934.5.
+50				34.0.
84				33.4.
+50				32.3.
85				31.3.
T.P.	3.00	✓ 934.28	12.31	✓ 931.28
+50				29.9.
B.M.	6.02	✓ 939.26	6.02	✓ 928.26 (928.29)
86				28.3.
+90				26.9.
87				25.2.
+30				24.5.
+92				24.2.
T.P.	2.98	✓ 926.63	10.61	✓ 923.65

Lt

L

Rt

$$\frac{53}{50} \frac{51}{26} \frac{90}{22} \frac{100}{15} \frac{97}{10} \frac{99}{7} \frac{96}{7} \frac{101}{14} \frac{67}{20} \frac{79}{24} \frac{90}{50}$$

$$\frac{31}{50} \frac{2.7}{91} \frac{86}{20} \frac{108}{18} \frac{99}{10} \frac{96}{8} \frac{98}{13} \frac{101}{23} \frac{47}{34} \frac{52}{34} \frac{67}{50}$$

$$\frac{37}{50} \frac{36}{38} \frac{118}{53} \frac{89}{25} \frac{102}{18} \frac{105}{14} \frac{105}{8} \frac{102}{8} \frac{104}{14} \frac{108}{23} \frac{54}{23} \frac{60}{25} \frac{7.5}{50}$$

$$\frac{78}{50} \frac{73}{35} \frac{112}{29} \frac{112}{19} \frac{115}{14} \frac{115}{9} \frac{113}{8} \frac{115}{8} \frac{118}{14} \frac{86}{20} \frac{95}{25} \frac{113}{50}$$

$$\frac{142}{50} \frac{12.7}{27} \frac{116}{19} \frac{128}{15} \frac{12.6}{9} \frac{12.3}{9} \frac{12.5}{8} \frac{120}{15} \frac{11.5}{23} \frac{12.5}{50}$$

$$\frac{100}{50} \frac{20}{31} \frac{47}{17} \frac{53}{14} \frac{47}{10} \frac{44}{9} \frac{46}{9} \frac{50}{15} \frac{18}{21} \frac{1.5}{50}$$

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$$\frac{151}{50} \frac{116}{33} \frac{9.2}{26} \frac{8.9}{21} \frac{70}{14} \frac{64}{9} \frac{60}{8} \frac{60}{8} \frac{69}{14} \frac{43}{19} \frac{2.8}{36} \frac{2.0}{50}$$

$$\frac{134}{50} \frac{161}{40} \frac{131}{29} \frac{120}{23} \frac{83}{14} \frac{77}{8} \frac{79}{8} \frac{76}{8} \frac{8.2}{16} \frac{7.7}{17} \frac{59}{33} \frac{49}{50}$$

$$\frac{127}{50} \frac{123}{33} \frac{109}{18} \frac{9.8}{13} \frac{9.5}{5} \frac{91}{7} \frac{9.2}{15} \frac{9.7}{19} \frac{8.3}{19} \frac{7.7}{42} \frac{7.7}{50}$$

$$\frac{86}{50} \frac{91}{27} \frac{107}{19} \frac{102}{9} \frac{98}{9} \frac{100}{9} \frac{101}{12} \frac{106}{16} \frac{86}{18} \frac{86}{39} \frac{88}{50}$$

$$\frac{179}{50} \frac{167}{36} \frac{134}{30} \frac{125}{24} \frac{110}{20} \frac{109}{8} \frac{101}{8} \frac{103}{8} \frac{108}{15} \frac{8.8}{18} \frac{8.0}{50}$$

Sta	+	π	-	Elev.
		926.63		
88				932.7
	+23			22.1
	+60			31.1
89				20.0
T.P.	986	924.79	6.70	919.99
	+50			19.4
	x Akk			
90				19.2
	+50			19.1
91				19.2
	+50			19.5
92				20.5

Lt

R

Rt

$$\frac{11.0}{50} \quad \frac{10.9}{40} \quad \frac{5.8}{27} \quad \frac{4.8}{17} \quad \frac{4.1}{7} \quad \frac{3.9}{9} \quad \frac{4.1}{15} \quad \frac{4.7}{22} \quad \frac{1.4}{31} \quad \frac{1.6}{50}$$

$$\frac{3.1}{50} \quad \frac{3.0}{50} \quad \frac{3.8}{20} \quad \frac{5.2}{16} \quad \frac{4.8}{7} \quad \frac{4.5}{8} \quad \frac{4.7}{14} \quad \frac{5.4}{17} \quad \frac{3.5}{17} \quad \frac{3.6}{50}$$

$$\frac{6.5}{50} \quad \frac{4.2}{32} \quad \frac{7.1}{30} \quad \frac{7.2}{26} \quad \frac{5.8}{19} \quad \frac{6.4}{16} \quad \frac{5.8}{8} \quad \frac{5.5}{8} \quad \frac{5.8}{12} \quad \frac{6.1}{17} \quad \frac{7.0}{17} \quad \frac{8.6}{24} \quad \frac{8.1}{32} \quad \frac{8.5}{50}$$

$$\frac{11.6}{50} \quad \frac{11.4}{27} \quad \frac{11.2}{19} \quad \frac{7.0}{12} \quad \frac{6.8}{7} \quad \frac{6.6}{7} \quad \frac{4.8}{7} \quad \frac{7.2}{12} \quad \frac{11.0}{19} \quad \frac{11.5}{23} \quad \frac{11.8}{50}$$

$$\frac{11.8}{50} \quad \frac{11.5}{43} \quad \frac{10.3}{21} \quad \frac{5.9}{13} \quad \frac{5.7}{8} \quad \frac{5.9}{7} \quad \frac{5.7}{10} \quad \frac{5.9}{13} \quad \frac{6.5}{21} \quad \frac{9.9}{35} \quad \frac{10.5}{35} \quad \frac{10.7}{50}$$

$$\frac{13.1}{100} \quad \frac{12.7}{50} \quad \frac{13.55}{50} \quad \frac{13.5}{50} \quad \frac{12.9}{50} \quad \frac{12.9}{100}$$

$$\frac{11.1}{50} \quad \frac{10.8}{31} \quad \frac{10.1}{27} \quad \frac{6.3}{14} \quad \frac{5.8}{8} \quad \frac{5.4}{7} \quad \frac{5.8}{12} \quad \frac{6.0}{20} \quad \frac{9.5}{32} \quad \frac{10.3}{32} \quad \frac{11.2}{50}$$

$$\frac{9.3}{50} \quad \frac{10.2}{28} \quad \frac{9.1}{20} \quad \frac{6.4}{13} \quad \frac{6.0}{7} \quad \frac{5.7}{7} \quad \frac{5.9}{8} \quad \frac{6.2}{12} \quad \frac{9.8}{22} \quad \frac{10.5}{34} \quad \frac{10.9}{50}$$

$$\frac{9.0}{50} \quad \frac{10.3}{22} \quad \frac{9.5}{20} \quad \frac{6.2}{12} \quad \frac{5.8}{8} \quad \frac{5.6}{7} \quad \frac{6.0}{7} \quad \frac{6.5}{12} \quad \frac{10.6}{22} \quad \frac{11.1}{32} \quad \frac{11.2}{50}$$

$$\frac{10.4}{50} \quad \frac{10.6}{33} \quad \frac{11.1}{22} \quad \frac{5.9}{13} \quad \frac{5.8}{8} \quad \frac{5.9}{7} \quad \frac{5.6}{6} \quad \frac{6.3}{13} \quad \frac{11.1}{24} \quad \frac{11.1}{33} \quad \frac{11.3}{50}$$

$$\frac{10.9}{50} \quad \frac{11.3}{32} \quad \frac{11.2}{24} \quad \frac{5.1}{13} \quad \frac{4.6}{9} \quad \frac{4.3}{7} \quad \frac{4.6}{7} \quad \frac{5.2}{13} \quad \frac{10.3}{23} \quad \frac{11.0}{32} \quad \frac{11.2}{50}$$

1.

Sta. + X - E/cv.

724.79

92 +50

922.0 .

93

23.8 .

+50

(25.5) ✓

94

(27.4) ✓

T.P.

12.38

736.96 ✓

0.21

924.35 ✓

93 +50

25.5 .

94

27.4 .

+50

29.1 .

95

30.7 .

+50

32.2 .

96

33.7 .

+50

35.4 .

14

2

124

$$\frac{88}{50} \quad \frac{91}{38} \quad \frac{85}{22} \quad \frac{33}{13} \quad \frac{29}{8} \quad \frac{28}{8} \quad \frac{31}{8} \quad \frac{38}{13} \quad \frac{77}{25} \quad \frac{107}{33} \quad \frac{109}{50}$$

$$\frac{10.9}{50} \quad \frac{96}{40} \quad \frac{86}{27} \quad \frac{16}{12} \quad \frac{11}{7} \quad \frac{10}{8} \quad \frac{13}{12} \quad \frac{17}{12} \quad \frac{8.2}{24} \quad \frac{104}{35} \quad \frac{106}{50}$$

$$\frac{91}{50} \quad \frac{90}{41} \quad \frac{83}{26}$$

$$+0.1$$

$$\frac{84}{27} \quad \frac{100}{35} \quad \frac{105}{50}$$

$$\frac{80}{50} \quad \frac{64}{27}$$

$$+0.2$$

$$\frac{67}{29} \quad \frac{81}{35} \quad \frac{95}{50}$$

$$\frac{121}{12} \quad \frac{118}{8} \quad \frac{115}{8} \quad \frac{118}{8} \quad \frac{129}{13}$$

$$\frac{103}{13} \quad \frac{97}{8} \quad \frac{96}{7} \quad \frac{97}{7} \quad \frac{101}{13}$$

$$\frac{178}{50} \quad \frac{161}{32} \quad \frac{145}{23} \quad \frac{88}{12} \quad \frac{83}{8} \quad \frac{79}{7} \quad \frac{81}{14} \quad \frac{149}{25} \quad \frac{163}{35} \quad \frac{171}{50}$$

$$\frac{150}{50} \quad \frac{106}{26} \quad \frac{74}{18} \quad \frac{66}{8} \quad \frac{63}{7} \quad \frac{65}{7} \quad \frac{66}{22} \quad \frac{105}{34} \quad \frac{116}{50}$$

$$\frac{37}{50} \quad \frac{28}{36} \quad \frac{19}{23} \quad \frac{53}{12} \quad \frac{50}{6} \quad \frac{48}{5} \quad \frac{50}{13} \quad \frac{53}{30} \quad \frac{90}{50} \quad \frac{10}{50}$$

$$\frac{37}{13} \quad \frac{35}{6} \quad \frac{33}{8} \quad \frac{35}{8} \quad \frac{39}{16}$$

$$\frac{19}{13} \quad \frac{18}{7} \quad \frac{16}{7} \quad \frac{17}{7} \quad \frac{28}{16}$$

Sta	+	Σ	-	Elev.
		936.91		
97				736.9
I.P.	11.83	948.55 ✓	0.24	936.72 ✓
96				(33.7)
I.P.	12.49	960.37 ✓	0.67	947.88 ✓
+50				(35.4)
97				(36.9)
+32				(37.7) ✓
+65				(38.5) ✓
98				(39.2) ✓
I.P.	10.7	950.23 ✓	11.21	949.16 ✓
I.P.			13.50	936.73 ✓
B.M.	5.65	947.80 ✓	8.38	944.85 ✓
97	+32			37.7
+65				38.5
98				39.2

936.72

944.85

lt. R Rt.

$$\frac{0.5}{12} \quad \frac{0.3}{6} \quad \frac{0.1}{7} \quad \frac{0.3}{7} \quad \frac{0.5}{16}$$

TR #4.

$$\frac{7.9}{100} \quad \frac{6.9}{75} \quad \frac{5.9}{50} \quad \frac{5.1}{30} \quad \textcircled{14.9} \quad \frac{3.5}{36} \quad \frac{2.5}{50} \quad \frac{5.2}{75} \quad \frac{6.2}{100}$$

$$\frac{8.0}{100} \quad \frac{8.0}{75} \quad \frac{7.6}{50} \quad \frac{7.4}{40} \quad \textcircled{25.0} \quad \frac{8.4}{42} \quad \frac{7.9}{65} \quad \frac{11.9}{100}$$

$$\frac{3.9}{100} \quad \frac{2.8}{75} \quad \frac{1.5}{50} \quad \textcircled{22.5} \quad \frac{3.1}{48} \quad \frac{3.6}{75} \quad \frac{5.8}{100}$$

$$\frac{2.6}{100} \quad \frac{2.7}{75} \quad \frac{1.8}{50} \quad \textcircled{22.7} \quad \frac{1.6}{48} \quad \frac{2.3}{75} \quad \frac{3.7}{100}$$

$$\frac{4.2}{100} \quad \frac{4.5}{75} \quad \frac{4.0}{49} \quad \textcircled{21.9} \quad \frac{3.0}{49} \quad \frac{4.5}{50} \quad \frac{5.3}{55} \quad \frac{5.8}{75} \quad \frac{5.8}{100}$$

$$\frac{7.8}{100} \quad \frac{8.3}{75} \quad \frac{8.1}{50} \quad \frac{7.5}{37} \quad \textcircled{21.2} \quad \frac{6.8}{39} \quad \frac{9.9}{50} \quad \frac{10.2}{75} \quad \frac{9.2}{100}$$

From TR #A.

Spk in PP

$$\frac{10.0}{75} \quad \frac{9.9}{6} \quad \frac{9.8}{6} \quad \frac{10.0}{6} \quad \frac{10.1}{72}$$

$$\frac{9.3}{12} \quad \frac{9.2}{6} \quad \frac{9.0}{6} \quad \frac{9.1}{6} \quad \frac{9.2}{12}$$

$$\frac{8.5}{13} \quad \frac{8.5}{6} \quad \frac{8.3}{6} \quad \frac{8.9}{6} \quad \frac{8.6}{11}$$

549

+

A

-

Flow

947.50

98 +50

939.5.

99

39.0 .

+50

38.7 .

100

38.0 .

T.P.

2.73

940.77 ✓

9.46

938.09 ✓

+50

37.3 .

101

36.8 .

+50

36.4 .

102

36.1 .

+50

35.9 .

103

35.8 .

+50

36.2 .

14

14

14

$$\frac{2.2}{50} \quad \frac{2.3}{42} \quad \frac{11}{31} \quad \frac{8.2}{14} \quad \frac{8.3}{7} \quad \frac{8.0}{6} \quad \frac{8.2}{12} \quad \frac{8.3}{26} \quad \frac{17}{38} \quad \frac{25}{50}$$

$$\frac{7.6}{50} \quad \frac{8.2}{35} \quad \frac{6.9}{25} \quad \frac{27}{18} \quad \frac{8.7}{13} \quad \frac{8.5}{6} \quad \frac{8.5}{6} \quad \frac{8.7}{12} \quad \frac{8.9}{14} \quad \frac{11}{33} \quad \frac{8.2}{50} \quad \frac{9.5}{50}$$

$$\frac{11.6}{50} \quad \frac{11.7}{35} \quad \frac{11.2}{27} \quad \frac{9.8}{21} \quad \frac{8.9}{7} \quad \frac{8.8}{7} \quad \frac{8.0}{7} \quad \frac{9.2}{21} \quad \frac{12.0}{27} \quad \frac{12.0}{36} \quad \frac{12.5}{50}$$

$$\frac{14.4}{50} \quad \frac{14.7}{36} \quad \frac{14.9}{24} \quad \frac{10.5}{15} \quad \frac{9.6}{7} \quad \frac{9.5}{7} \quad \frac{9.7}{16} \quad \frac{10.3}{16} \quad \frac{13.7}{23} \quad \frac{14.6}{32} \quad \frac{14.0}{38} \quad \frac{14.1}{50}$$

41 sks 100k

$$\frac{8.8}{50} \quad \frac{8.8}{23} \quad \frac{9.1}{13} \quad \frac{3.7}{8} \quad \frac{3.5}{7} \quad \frac{3.6}{7} \quad \frac{4.7}{16} \quad \frac{8.3}{23} \quad \frac{9.1}{33} \quad \frac{9.0}{50}$$

✓
$$\frac{10.1}{50} \quad \frac{10.1}{35} \quad \frac{9.4}{22} \quad \frac{4.9}{13} \quad \frac{4.3}{8} \quad \frac{4.0}{7} \quad \frac{4.2}{8} \quad \frac{4.8}{19} \quad \frac{8.5}{21} \quad \frac{10.0}{35} \quad \frac{10.7}{36} \quad \frac{11.3}{43} \quad \frac{11.8}{50}$$

✓
$$\frac{10.1}{50} \quad \frac{10.1}{35} \quad \frac{9.2}{20} \quad \frac{5.1}{12} \quad \frac{4.7}{9} \quad \frac{4.4}{7} \quad \frac{4.7}{8} \quad \frac{5.3}{14} \quad \frac{9.2}{23} \quad \frac{9.8}{34} \quad \frac{10.8}{37} \quad \frac{11.1}{46} \quad \frac{10.1}{50}$$

✓
$$\frac{9.7}{50} \quad \frac{9.4}{26} \quad \frac{8.0}{19} \quad \frac{5.2}{12} \quad \frac{4.9}{8} \quad \frac{4.7}{9} \quad \frac{5.1}{14} \quad \frac{5.8}{18} \quad \frac{8.1}{34} \quad \frac{9.3}{38} \quad \frac{9.9}{50}$$

✓
$$\frac{8.1}{50} \quad \frac{8.1}{37} \quad \frac{7.6}{19} \quad \frac{5.7}{13} \quad \frac{5.3}{9} \quad \frac{4.9}{7} \quad \frac{5.1}{9} \quad \frac{5.8}{13} \quad \frac{7.2}{20} \quad \frac{7.3}{28} \quad \frac{8.4}{33} \quad \frac{7.7}{50}$$

✓
$$\frac{6.7}{50} \quad \frac{6.5}{39} \quad \frac{7.3}{28} \quad \frac{8.2}{23} \quad \frac{8.0}{16} \quad \frac{5.5}{12} \quad \frac{5.3}{8} \quad \frac{5.0}{7} \quad \frac{5.2}{9} \quad \frac{5.7}{13} \quad \frac{7.5}{18} \quad \frac{7.6}{33} \quad \frac{6.1}{50}$$

✓
$$\frac{7.7}{50} \quad \frac{8.0}{26} \quad \frac{8.0}{18} \quad \frac{5.4}{12} \quad \frac{4.8}{7} \quad \frac{4.6}{7} \quad \frac{4.8}{8} \quad \frac{5.0}{12} \quad \frac{7.7}{20} \quad \frac{8.0}{36} \quad \frac{8.8}{37} \quad \frac{8.9}{38} \quad \frac{1.2}{43} \quad \frac{7.6}{50}$$

Sta. + π - Elev

740.77

104

937.1.

+50

37.8.

105

389.

T.P.

12.93

751.84 ✓

1.86

938.71 ✓

+50

40.7.

106

430.

+37

459.

+42

463.

+

W. Edge Pavement

466.4.

to Pav.

467.4.

B.M.

5.10

751.84 ✓

5.10

746.74 ✓

746.76

E. Edge Pav.

467.3.

+73

46.9.

Lt

L

Lt

$$\begin{array}{r} 93 \\ 50 \end{array} \quad \begin{array}{r} 91 \\ 26 \end{array} \quad \begin{array}{r} 87 \\ 20 \end{array} \quad \begin{array}{r} 43 \\ 11 \end{array} \quad \begin{array}{r} 90 \\ 8 \end{array} \quad \begin{array}{r} 37 \\ 9 \end{array} \quad \begin{array}{r} 39 \\ 13 \end{array} \quad \begin{array}{r} 43 \\ 21 \end{array} \quad \begin{array}{r} 52 \\ 32 \end{array} \quad \begin{array}{r} 85 \\ 35 \end{array} \quad \begin{array}{r} 92 \\ 41 \end{array} \quad \begin{array}{r} 83 \\ 43 \end{array} \quad \begin{array}{r} 86 \\ 50 \end{array}$$

$$\begin{array}{r} 74 \\ 50 \end{array} \quad \begin{array}{r} 91 \\ 28 \end{array} \quad \begin{array}{r} 85 \\ 22 \end{array} \quad \begin{array}{r} 37 \\ 12 \end{array} \quad \begin{array}{r} 53 \\ 8 \end{array} \quad \begin{array}{r} 30 \\ 9 \end{array} \quad \begin{array}{r} 32 \\ 7 \end{array} \quad \begin{array}{r} 36 \\ 13 \end{array} \quad \begin{array}{r} 77 \\ 21 \end{array} \quad \begin{array}{r} 82 \\ 28 \end{array} \quad \begin{array}{r} 82 \\ 36 \end{array} \quad \begin{array}{r} 75 \\ 40 \end{array} \quad \begin{array}{r} 87 \\ 50 \end{array}$$

$$\begin{array}{r} 89 \\ 50 \end{array} \quad \begin{array}{r} 79 \\ 27 \end{array} \quad \begin{array}{r} 67 \\ 22 \end{array} \quad \begin{array}{r} 54 \\ 14 \end{array} \quad \begin{array}{r} 26 \\ 12 \end{array} \quad \begin{array}{r} 22 \\ 9 \end{array} \quad \begin{array}{r} 19 \\ 8 \end{array} \quad \begin{array}{r} 19 \\ 12 \end{array} \quad \begin{array}{r} 22 \\ 20 \end{array} \quad \begin{array}{r} 49 \\ 26 \end{array} \quad \begin{array}{r} 63 \\ 25 \end{array} \quad \begin{array}{r} 67 \\ 50 \end{array}$$

$$\begin{array}{r} 15.7 \\ 50 \end{array} \quad \begin{array}{r} 16.1 \\ 27 \end{array} \quad \begin{array}{r} 15.0 \\ 19 \end{array} \quad \begin{array}{r} 11.8 \\ 12 \end{array} \quad \begin{array}{r} 11.3 \\ 8 \end{array} \quad \begin{array}{r} 11.1 \\ 8 \end{array} \quad \begin{array}{r} 11.3 \\ 13 \end{array} \quad \begin{array}{r} 11.8 \\ 20 \end{array} \quad \begin{array}{r} 14.5 \\ 25 \end{array} \quad \begin{array}{r} 15.2 \\ 33 \end{array} \quad \begin{array}{r} 15.3 \\ 50 \end{array} \quad \begin{array}{r} 16.2 \\ 50 \end{array}$$

$$\begin{array}{r} 10.7 \\ 50 \end{array} \quad \begin{array}{r} 11.1 \\ 26 \end{array} \quad \begin{array}{r} 11.2 \\ 17 \end{array} \quad \begin{array}{r} 7.9 \\ 12 \end{array} \quad \begin{array}{r} 9.1 \\ 7 \end{array} \quad \begin{array}{r} 8.8 \\ 9 \end{array} \quad \begin{array}{r} 8.9 \\ 12 \end{array} \quad \begin{array}{r} 7.1 \\ 17 \end{array} \quad \begin{array}{r} 10.3 \\ 22 \end{array} \quad \begin{array}{r} 11.8 \\ 26 \end{array} \quad \begin{array}{r} 12.4 \\ 31 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 76 \\ 50 \end{array} \quad \begin{array}{r} 65 \\ 25 \end{array} \quad \begin{array}{r} 63 \\ 18 \end{array} \quad \begin{array}{r} 62 \\ 10 \end{array} \quad \begin{array}{r} 59 \\ 10 \end{array}$$

$$\begin{array}{r} 60 \\ 13 \end{array} \quad \begin{array}{r} 61 \\ 21 \end{array} \quad \begin{array}{r} 74 \\ 28 \end{array} \quad \begin{array}{r} 77 \\ 50 \end{array}$$

$$\begin{array}{r} 56 \\ 50 \end{array} \quad \begin{array}{r} 56 \\ 28 \end{array} \quad \begin{array}{r} 55 \\ 10 \end{array}$$

$$\begin{array}{r} 55 \\ 50 \end{array} \quad \begin{array}{r} 55 \\ 11 \end{array} \quad \begin{array}{r} 51 \\ 31 \end{array} \quad \begin{array}{r} 49 \\ 50 \end{array}$$

$$\begin{array}{r} 5.51 \\ 50 \end{array}$$

$$\begin{array}{r} 5.20 \\ 50 \end{array}$$

$$\begin{array}{r} 4.72 \\ 50 \end{array}$$

$$\begin{array}{r} 5.41 \\ 50 \end{array}$$

$$\begin{array}{r} 5.10 \\ 50 \end{array}$$

$$\begin{array}{r} 4.60 \\ 50 \end{array}$$

$$\begin{array}{r} 5.48 \\ 50 \end{array}$$

$$\begin{array}{r} 5.13 \\ 50 \end{array}$$

$$\begin{array}{r} 4.64 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array}$$

$$\begin{array}{r} 5.6 \\ 28 \end{array}$$

$$\begin{array}{r} 5.0 \\ 27 \end{array} \quad \begin{array}{r} 5.1 \\ 27 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array}$$

Sta.	+	Σ	-	Elev.
		951.86		
+79				946.9.
+84				47.0.
107				47.4.
+150				49.0.
B.M.	12.32	959.08 ✓		946.76
+77				50.1.
108				51.1.
+70				53.3.
109				54.1.
+70				55.9.
110				56.2.
+50				56.7.
T.P.	6.85	969.12 ✓	1.81	957.27 ✓

Plotted
✓

lt.

L

Rt.

 $\frac{7.2}{50}$ $\frac{6.6}{30}$ $\frac{5.4}{15}$ $\frac{3.0}{50}$ $\frac{5.3}{23}$ $\frac{6.0}{28}$ $\frac{8.4}{32}$ $\frac{7.4}{50}$
 $\frac{6.6}{50}$ $\frac{6.5}{28}$ $\frac{5.5}{16}$ $\frac{4.9}{50}$ $\frac{5.2}{17}$ $\frac{5.6}{27}$ $\frac{5.9}{50}$
 $\frac{4.7}{50}$ $\frac{4.5}{28}$ $\frac{5.1}{24}$ $\frac{3.3}{16}$ $\frac{4.8}{10}$ $\frac{4.5}{50}$ $\frac{4.8}{17}$ $\frac{5.2}{21}$ $\frac{4.8}{30}$ $\frac{5.3}{50}$
 $\frac{1.1}{50}$ $\frac{1.4}{26}$ $\frac{2.9}{16}$ $\frac{3.4}{12}$ $\frac{3.2}{9}$ $\frac{2.9}{50}$ $\frac{3.2}{9}$ $\frac{3.6}{13}$ $\frac{3.0}{17}$ $\frac{2.5}{34}$ $\frac{2.7}{50}$
 $\frac{6.5}{50}$ $\frac{6.4}{28}$ $\frac{6.6}{15}$ $\frac{7.6}{11}$ $\frac{8.3}{9}$ $\frac{8.0}{50}$ $\frac{9.2}{10}$ $\frac{9.7}{13}$ $\frac{8.9}{18}$ $\frac{8.2}{50}$
 $\frac{6.6}{50}$ $\frac{5.5}{21}$ $\frac{7.8}{14}$ $\frac{8.4}{13}$ $\frac{8.2}{9}$ $\frac{8.0}{50}$ $\frac{8.2}{9}$ $\frac{8.7}{13}$ $\frac{8.0}{17}$ $\frac{7.0}{36}$ $\frac{6.6}{50}$
 $\frac{9.8}{50}$ $\frac{8.4}{34}$ $\frac{5.5}{21}$ $\frac{6.0}{15}$ $\frac{6.4}{13}$ $\frac{6.1}{8}$ $\frac{5.5}{50}$ $\frac{6.0}{9}$ $\frac{6.3}{13}$ $\frac{5.4}{17}$ $\frac{4.4}{33}$ $\frac{3.8}{50}$
 $\frac{7.7}{50}$ $\frac{5.9}{29}$ $\frac{5.8}{29}$ $\frac{4.5}{21}$ $\frac{9.2}{17}$ $\frac{8.6}{12}$ $\frac{5.5}{8}$ $\frac{5.0}{50}$ $\frac{5.3}{10}$ $\frac{5.5}{18}$ $\frac{4.1}{21}$ $\frac{3.3}{50}$
 $\frac{3.3}{50}$ $\frac{1.9}{28}$ $\frac{2.1}{16}$ $\frac{3.7}{12}$ $\frac{3.6}{9}$ $\frac{3.2}{50}$ $\frac{3.4}{10}$ $\frac{3.6}{16}$ $\frac{1.6}{20}$ $\frac{2.2}{38}$ $\frac{2.2}{50}$
 $\frac{2.8}{50}$ $\frac{1.5}{27}$ $\frac{1.8}{17}$ $\frac{3.3}{13}$ $\frac{3.1}{9}$ $\frac{2.9}{50}$ $\frac{3.0}{9}$ $\frac{3.2}{15}$ $\frac{1.7}{18}$ $\frac{1.6}{31}$ $\frac{2.3}{50}$
 $\frac{3.8}{50}$ $\frac{2.9}{29}$ $\frac{2.9}{18}$ $\frac{3.4}{15}$ $\frac{2.6}{9}$ $\frac{2.4}{50}$ $\frac{2.6}{9}$ $\frac{2.9}{19}$ $\frac{1.8}{17}$ $\frac{1.8}{32}$ $\frac{2.6}{50}$

Sta. + - Elev.

969.12

111

957.2 .

+50

57.8 .

112

58.1 .

+28

59.2 .

+72

59.7 .

113

60.0 .

+27

60.3 .

T.P.

9.82

970.21 ✓

3.73

240.39 ✓

+38

60.4 .

+78

60.4 .

114

60.3 .

+58

59.4 .

Lt.

A.

Rt.

$$\frac{83}{50} \quad \frac{90}{32} \quad \frac{88}{16} \quad \frac{74}{12} \quad \frac{72}{9} \quad \frac{69}{9} \quad \frac{71}{9} \quad \frac{79}{13} \quad \frac{92}{16} \quad \frac{97}{34} \quad \frac{100}{50}$$

$$\frac{66}{50} \quad \frac{76}{28} \quad \frac{83}{26} \quad \frac{85}{15} \quad \frac{68}{12} \quad \frac{66}{9} \quad \frac{63}{9} \quad \frac{68}{10} \quad \frac{71}{12} \quad \frac{113}{21} \quad \frac{121}{36} \quad \frac{129}{50}$$

$$\frac{58}{50} \quad \frac{61}{27} \quad \frac{62}{17} \quad \frac{56}{13} \quad \frac{55}{9} \quad \frac{53}{9} \quad \frac{56}{10} \quad \frac{64}{14} \quad \frac{86}{20} \quad \frac{94}{33} \quad \frac{109}{50}$$

$$\frac{56}{50} \quad \frac{53}{26} \quad \frac{50}{9} \quad \frac{49}{9} \quad \frac{53}{9} \quad \frac{56}{10} \quad \frac{64}{14} \quad \frac{86}{20} \quad \frac{94}{33} \quad \frac{109}{50}$$

$$\frac{31}{50} \quad \frac{30}{43} \quad \frac{46}{24} \quad \frac{45}{9} \quad \frac{44}{9} \quad \frac{48}{13} \quad \frac{53}{19} \quad \frac{82}{19} \quad \frac{95}{36} \quad \frac{107}{50}$$

$$\frac{47}{50} \quad \frac{30}{31} \quad \frac{41}{15} \quad \frac{43}{9} \quad \frac{41}{10} \quad \frac{45}{10} \quad \frac{47}{14} \quad \frac{65}{18} \quad \frac{81}{34} \quad \frac{98}{50}$$

$$\frac{11}{50} \quad \frac{32}{26} \quad \frac{41}{16} \quad \frac{38}{10} \quad \frac{40}{10} \quad \frac{47}{18} \quad \frac{40}{22} \quad \frac{46}{33} \quad \frac{69}{50}$$

$$\frac{35}{50} \quad \frac{49}{28} \quad \frac{100}{14} \quad \frac{100}{9} \quad \frac{98}{9} \quad \frac{100}{10} \quad \frac{109}{18} \quad \frac{87}{27} \quad \frac{90}{34} \quad \frac{100}{44} \quad \frac{117}{50}$$

$$\frac{07}{50} \quad \frac{20}{32} \quad \frac{100}{14} \quad \frac{99}{9} \quad \frac{98}{9} \quad \frac{100}{9} \quad \frac{102}{15} \quad \frac{53}{27} \quad \frac{63}{45} \quad \frac{72}{50}$$

$$\frac{26}{50} \quad \frac{36}{29} \quad \frac{84}{21} \quad \frac{100}{14} \quad \frac{101}{9} \quad \frac{99}{9} \quad \frac{102}{10} \quad \frac{103}{15} \quad \frac{46}{30} \quad \frac{46}{50}$$

$$\frac{49}{50} \quad \frac{59}{34} \quad \frac{73}{26} \quad \frac{104}{18} \quad \frac{108}{10} \quad \frac{108}{8} \quad \frac{110}{13} \quad \frac{46}{50} \quad \frac{52}{50}$$

Sta	+	π	-	Elev
		970.21		
114	+70			959.2 .
115				587 .
T.P.	3.41	961.12 ✓	12.50	957.71 ✓
+18				584 .
+42				578 .
+65				573 .
116				567 .
+42				561 .
117				555 .
+67				552 .
118				551 .
+50				547 .

44

4

P4

$\frac{50}{50}$	$\frac{59}{36}$	$\frac{71}{26}$	$\frac{106}{19}$	$\frac{110}{10}$	$\frac{110}{10}$	$\frac{111}{8}$	$\frac{99}{29}$	$\frac{80}{50}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	-----------------	-----------------

$\frac{104}{50}$	$\frac{76}{31}$	$\frac{83}{26}$	$\frac{117}{18}$	$\frac{117}{10}$	$\frac{115}{10}$	$\frac{117}{8}$	$\frac{116}{12}$	$\frac{108}{38}$	$\frac{95}{50}$
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(T.V # A)

$\frac{08}{50}$	$\frac{10}{33}$	$\frac{22}{25}$	$\frac{29}{11}$	$\frac{17}{10}$	$\frac{30}{7}$	$\frac{31}{13}$	$\frac{72}{23}$	$\frac{78}{34}$	$\frac{80}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{47}{50}$	$\frac{48}{36}$	$\frac{52}{21}$	$\frac{34}{15}$	$\frac{34}{10}$	$\frac{33}{10}$	$\frac{36}{7}$	$\frac{39}{12}$	$\frac{109}{29}$	$\frac{113}{34}$	$\frac{113}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	------------------	------------------	------------------

$\frac{69}{50}$	$\frac{77}{34}$	$\frac{89}{21}$	$\frac{41}{14}$	$\frac{39}{11}$	$\frac{38}{10}$	$\frac{41}{7}$	$\frac{46}{12}$	$\frac{123}{25}$	$\frac{130}{31}$	$\frac{130}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	------------------	------------------	------------------

$\frac{79}{50}$	$\frac{82}{34}$	$\frac{90}{21}$	$\frac{48}{19}$	$\frac{95}{8}$	$\frac{44}{10}$	$\frac{47}{8}$	$\frac{50}{12}$	$\frac{170}{28}$	$\frac{183}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	------------------	------------------

$\frac{89}{50}$	$\frac{89}{27}$	$\frac{95}{20}$	$\frac{56}{13}$	$\frac{53}{9}$	$\frac{50}{10}$	$\frac{53}{8}$	$\frac{56}{12}$	$\frac{17.7}{29}$	$\frac{20.7}{50}$	$\frac{21.0}{75}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-------------------	-------------------	-------------------

$\frac{89}{50}$	$\frac{92}{27}$	$\frac{97}{19}$	$\frac{63}{13}$	$\frac{58}{8}$	$\frac{56}{10}$	$\frac{58}{8}$	$\frac{62}{12}$	$\frac{16.3}{28}$	$\frac{17.4}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-------------------	-------------------

$\frac{93}{50}$	$\frac{93}{27}$	$\frac{94}{19}$	$\frac{65}{15}$	$\frac{61}{10}$	$\frac{59}{10}$	$\frac{62}{8}$	$\frac{69}{12}$	$\frac{86}{18}$	$\frac{12.6}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-------------------

$\frac{88}{50}$	$\frac{90}{35}$	$\frac{89}{19}$	$\frac{66}{13}$	$\frac{63}{9}$	$\frac{60}{10}$	$\frac{63}{7}$	$\frac{66}{12}$	$\frac{73}{15}$	$\frac{9.7}{31}$	$\frac{12.1}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-----------------	------------------	-------------------

$\frac{63}{50}$	$\frac{63}{28}$	$\frac{41}{21}$	$\frac{69}{16}$	$\frac{66}{10}$	$\frac{69}{7}$	$\frac{67}{16}$	$\frac{68}{21}$	$\frac{32}{31}$	$\frac{73}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

Sta	L	A	-	Elev.
		961.12		
118	+75			954.5'
119				54.3.
	+38			53.6.
T.P.	9.48	963.74 ✓	6.86	959.26 ✓
	+65			53.3.
120				52.9.
	+30			52.2.
	+60			51.5.
T.P.	4.33	955.09 ✓	12.98	950.76 ✓
121				50.8.
	+27			50.3.
	+72			49.8.
122				49.7.

Lt

L

Rt.

$\frac{43}{30}$	$\frac{31}{32}$	$\frac{32}{23}$	$\frac{69}{15}$	$\frac{69}{11}$	$\frac{66}{-}$	$\frac{69}{8}$	$\frac{72}{15}$	$\frac{25}{22}$	$\frac{23}{28}$	$\frac{4.8}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	------------------

$\frac{24}{30}$	$\frac{17}{40}$	$\frac{28}{23}$	$\frac{71}{16}$	$\frac{71}{11}$	$\frac{68}{-}$	$\frac{71}{8}$	$\frac{73}{17}$	$\frac{4.3}{22}$	$\frac{4.2}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	------------------	------------------

$\frac{12}{50}$	$\frac{0.6}{34}$	$\frac{2.0}{23}$	$\frac{7.7}{15}$	$\frac{7.6}{8}$	$\frac{75}{8}$	$\frac{75}{19}$	$\frac{7.6}{22}$	$\frac{6.5}{40}$	$\frac{5.8}{50}$
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Top W End End Culv.

$\frac{50}{50}$	$\frac{45}{29}$	$\frac{53}{23}$	$\frac{107}{17}$	$\frac{106}{10}$	$\frac{109}{-}$	$\frac{106}{7}$	$\frac{10.7}{17}$	$\frac{87}{23}$	$\frac{7.3}{43}$	$\frac{7.3}{50}$
-----------------	-----------------	-----------------	------------------	------------------	-----------------	-----------------	-------------------	-----------------	------------------	------------------

$\frac{90}{50}$	$\frac{79}{35}$	$\frac{6.7}{23}$	$\frac{11.3}{15}$	$\frac{11.1}{11}$	$\frac{108}{-}$	$\frac{109}{7}$	$\frac{11.1}{13}$	$\frac{6.1}{23}$	$\frac{5.4}{50}$
-----------------	-----------------	------------------	-------------------	-------------------	-----------------	-----------------	-------------------	------------------	------------------

$\frac{131}{50}$	$\frac{11.7}{35}$	$\frac{94}{27}$	$\frac{86}{22}$	$\frac{120}{16}$	$\frac{11.9}{11}$	$\frac{115}{7}$	$\frac{11.7}{12}$	$\frac{11.8}{28}$	$\frac{54}{41}$	$\frac{6.1}{50}$
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$\frac{152}{50}$	$\frac{146}{35}$	$\frac{138}{20}$	$\frac{126}{17}$	$\frac{126}{12}$	$\frac{122}{-}$	$\frac{125}{7}$	$\frac{129}{12}$	$\frac{98}{17}$	$\frac{96}{29}$	$\frac{105}{55}$	$\frac{106}{50}$
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$\frac{72}{50}$	$\frac{68}{27}$	$\frac{74}{25}$	$\frac{74}{21}$	$\frac{50}{16}$	$\frac{46}{12}$	$\frac{43}{7}$	$\frac{46}{11}$	$\frac{48}{15}$	$\frac{58}{30}$	$\frac{60}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{77}{32}$	$\frac{67}{24}$	$\frac{74}{22}$	$\frac{74}{20}$	$\frac{54}{15}$	$\frac{51}{11}$	$\frac{48}{7}$	$\frac{49}{12}$	$\frac{52}{15}$	$\frac{65}{28}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{112}{50}$	$\frac{124}{38}$	$\frac{123}{28}$	$\frac{60}{15}$	$\frac{52}{12}$	$\frac{53}{-}$	$\frac{56}{7}$	$\frac{58}{7}$	$\frac{12.2}{21}$	$\frac{124}{34}$	$\frac{11.9}{50}$
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$\frac{129}{50}$	$\frac{136}{38}$	$\frac{129}{29}$	$\frac{59}{15}$	$\frac{5.7}{12}$	$\frac{54}{7}$	$\frac{5.7}{11}$	$\frac{61}{21}$	$\frac{128}{39}$	$\frac{138}{59}$	$\frac{136}{50}$
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342

t

 π

-

Elev

955.09

122 +36

950.0 .

+73

50.6 ;

123

51.0 .

T.P.

12.89

965.53 ✓

2.45

932.64 ✓

+97

52.1 .

+75

52.9 .

124

53.6 .

+55

55.0 .

125

56.7 .

+34

57.8 .

+67

58.7 .

126

59.7 .

T.P.

11.89

971.64 ✓

5.78

939.75 ✓

Lt

R

Rt

 $\frac{128}{50} \frac{135}{59} \frac{131}{27} \frac{57}{15} \frac{54}{11} \frac{31}{11} \frac{59}{7} \frac{56}{10} \frac{127}{22} \frac{127}{36} \frac{130}{50}$
 $\frac{111}{50} \frac{113}{25} \frac{105}{23} \frac{54}{14} \frac{50}{11} \frac{45}{11} \frac{47}{8} \frac{50}{11} \frac{91}{18} \frac{101}{23} \frac{110}{39} \frac{108}{50}$
 $\frac{110}{50} \frac{87}{28} \frac{82}{21} \frac{49}{14} \frac{45}{11} \frac{41}{11} \frac{42}{7} \frac{94}{12} \frac{58}{18} \frac{58}{29} \frac{64}{35} \frac{52}{50}$
 $\frac{82}{50} \frac{160}{32} \frac{159}{23} \frac{145}{20} \frac{139}{11} \frac{139}{11} \frac{136}{7} \frac{138}{17} \frac{66}{27} \frac{69}{39} \frac{62}{50}$
 $\frac{135}{50} \frac{100}{26} \frac{134}{19} \frac{129}{11} \frac{126}{11} \frac{128}{7} \frac{132}{18} \frac{46}{29} \frac{40}{50}$
 $\frac{113}{50} \frac{81}{27} \frac{129}{20} \frac{121}{12} \frac{119}{11} \frac{132}{7} \frac{129}{19} \frac{67}{28} \frac{59}{39} \frac{48}{50}$
 $\frac{106}{50} \frac{94}{32} \frac{86}{21} \frac{109}{17} \frac{106}{11} \frac{105}{11} \frac{107}{6} \frac{105}{13} \frac{90}{20} \frac{61}{32} \frac{52}{50}$
 $\frac{79}{50} \frac{53}{30} \frac{47}{23} \frac{93}{17} \frac{92}{12} \frac{88}{11} \frac{90}{7} \frac{93}{17} \frac{19}{26} \frac{89}{30} \frac{19}{40} \frac{12}{50}$
 $\frac{119}{50} \frac{65}{26} \frac{55}{20} \frac{82}{16} \frac{80}{11} \frac{77}{11} \frac{79}{7} \frac{80}{17} \frac{412}{26} \frac{120}{30}$
 $\frac{159}{50} \frac{127}{36} \frac{75}{15} \frac{71}{11} \frac{68}{11} \frac{71}{7} \frac{68}{16} \frac{20}{23} \frac{08}{33} \frac{10}{50}$
 $\frac{129}{50} \frac{104}{28} \frac{81}{22} \frac{64}{15} \frac{61}{11} \frac{58}{11} \frac{59}{8} \frac{61}{16} \frac{3721}{25} \frac{11}{27} \frac{11}{50}$

Sta	+	x	-	Elev
		971.69		
126	+50			961.7
B.M.	10.00	971.61	1000	961.69 (961.61)
127				63.5
	+45			64.9
128				66.5
	+50			67.4
T.P.	5.78	974.08	3.31	968.30
129				68.4
	+50			69.0
130				69.4
	+50			69.6
131				70.1
	+50			70.9

Lt.

R.

Rt.

14.0	12.9	11.3	10.3	9.7	10.1	10.7	5.0	4.3
50	28	21	10		7	16	26	50

Spt in R.H. 669 Lt. 126 Lt. 5

7.4	8.6	7.6	8.6	8.3	8.1	8.2	8.7	3.2	1.2
50	41	21	13	10		7	17	25	50

7.5	6.8	6.0	8.3	7.1	6.9	6.7	6.7	7.9	2.5	1.5	1.3
50	36	24	21	13	10		7	16	25	30	50

7.0	5.9	7.2	6.9	5.5	5.5	5.1	5.3	5.7	2.9	2.1	3.1	2.9
50	24	20	14	12	10		8	15	20	26	40	50

5.3	3.8	6.7	6.7	5.0	4.7	4.2	4.1	4.1	1.1	1.5	1.2
50	26	21	18	14	10		8	15	19	35	50

5.3	4.6	8.4	8.4	7.2	6.1	5.9	5.7	5.8	5.8	2.7	2.1	1.7
50	32	25	21	15	12	10		8	15	20	36	50

5.1	4.2	7.7	7.7	5.6	5.2	5.1	5.1	5.3	2.2	1.4	1.5
50	31	26	21	14	10		8	15	19	33	50

6.7	5.5	6.5	6.5	5.3	5.2	4.7	4.7	5.2	3.1	2.7	3.1
50	24	22	17	12	9		7	15	20	33	50

7.5	7.0	7.4	4.9	4.7	4.5	4.5	4.9	5.0	4.1
50	32	23	13	9		7	13	28	50

7.2	7.0	6.3	4.9	4.1	4.0	4.2	4.3	4.9	4.4	4.5
50	40	22	14	8		9	12	21	32	50

7.1	6.7	6.0	6.2	3.7	3.5	3.2	3.3	3.5	4.1	3.5	2.5
50	43	24	18	13	8		9	13	18	26	50

Sta.	+	π	-	Elev.
		979.18		
132				971.6 .
T.P.	13.52	984.93 ✓	2.65	971.43 ✓
+50				72.0 .
133				72.8 .
+27				73.2 .
+75				73.7 .
134				74.0 .
+58				74.2 .
135				74.3 .
T.P.	283	782.12 ✓	10.66	774.29 ✓
+50				74.4 .
136				74.3 .
+22				74.4 .

Lt

L

Rt

$\frac{55}{50}$ $\frac{47}{55}$ $\frac{44}{25}$ $\frac{53}{23}$ $\frac{53}{23}$ $\frac{28}{12}$ $\frac{26}{9}$ $\frac{25}{9}$ $\frac{28}{9}$ $\frac{39}{21}$ $\frac{31}{29}$ $\frac{39}{27}$ $\frac{39}{30}$ $\frac{38}{42}$ $\frac{34}{50}$

$\frac{156}{50}$ $\frac{159}{27}$ $\frac{156}{19}$ $\frac{13.5}{19}$ $\frac{13.2}{9}$ $\frac{13.0}{9}$ $\frac{13.1}{15}$ $\frac{13.9}{31}$ $\frac{13.1}{30}$ $\frac{12.7}{50}$

$\frac{150}{50}$ $\frac{140}{25}$ $\frac{139}{19}$ $\frac{12.7}{14}$ $\frac{12.5}{10}$ $\frac{12.2}{9}$ $\frac{12.4}{9}$ $\frac{12.0}{12}$ $\frac{11.5}{15}$ $\frac{10.2}{24}$ $\frac{10.4}{50}$

$\frac{14.5}{50}$ $\frac{13.1}{27}$ $\frac{13.5}{23}$ $\frac{13.5}{19}$ $\frac{12.0}{15}$ $\frac{12.2}{12}$ $\frac{12.2}{10}$ $\frac{11.8}{9}$ $\frac{11.8}{9}$ $\frac{11.9}{12}$ $\frac{10.3}{14}$ $\frac{9.1}{23}$ $\frac{9.1}{33}$ $\frac{8.6}{50}$

$\frac{11.8}{50}$ $\frac{11.8}{27}$ $\frac{12.0}{23}$ $\frac{12.2}{20}$ $\frac{11.0}{15}$ $\frac{11.6}{14}$ $\frac{11.5}{10}$ $\frac{11.3}{9}$ $\frac{11.5}{8}$ $\frac{11.6}{11}$ $\frac{11.7}{21}$ $\frac{11.5}{22}$ $\frac{11.4}{34}$ $\frac{11.3}{50}$

$\frac{10.5}{50}$ $\frac{10.0}{28}$ $\frac{10.5}{15}$ $\frac{11.4}{13}$ $\frac{11.3}{10}$ $\frac{11.0}{9}$ $\frac{11.3}{8}$ $\frac{11.9}{13}$ $\frac{10.9}{12}$ $\frac{9.3}{33}$ $\frac{9.3}{50}$

$\frac{9.1}{50}$ $\frac{8.8}{26}$ $\frac{9.2}{16}$ $\frac{11.3}{13}$ $\frac{11.3}{10}$ $\frac{10.8}{9}$ $\frac{10.8}{8}$ $\frac{10.8}{11}$ $\frac{12}{24}$ $\frac{0.9}{50}$

$\frac{8.7}{50}$ $\frac{8.8}{26}$ $\frac{10.7}{17}$ $\frac{11.4}{15}$ $\frac{11.3}{10}$ $\frac{10.8}{9}$ $\frac{10.9}{8}$ $\frac{11.1}{12}$ $\frac{10.8}{17}$ $\frac{6.4}{27}$ $\frac{6.3}{50}$

$\frac{12.3}{50}$ $\frac{13.8}{25}$ $\frac{8.5}{12}$ $\frac{8.4}{10}$ $\frac{7.7}{9}$ $\frac{7.8}{8}$ $\frac{8.1}{14}$ $\frac{9.2}{17}$ $\frac{8.0}{34}$ $\frac{6.6}{50}$

$\frac{13.8}{50}$ $\frac{13.8}{25}$ $\frac{12.5}{19}$ $\frac{8.3}{11}$

$\frac{7.8}{8}$ $\frac{7.9}{5}$ $\frac{8.0}{11}$ $\frac{13.1}{22}$ $\frac{13.1}{26}$ $\frac{12.2}{30}$ $\frac{13.1}{40}$ $\frac{11.6}{50}$

$\frac{13.7}{50}$ $\frac{13.6}{24}$ $\frac{11.7}{17}$ $\frac{8.4}{12}$ $\frac{8.1}{10}$ $\frac{7.7}{9}$

$\frac{7.9}{9}$ $\frac{8.2}{11}$ $\frac{10.3}{19}$ $\frac{14.2}{37}$ $\frac{13.5}{50}$

Sta + π - Elev.

982.17₀

136 +50

974.7 .

137

757.6 .

+33

76.3 .

138

77.4 .

+46

78.5 .

+72

79.2 .

B.M.

1826

992.03 ✓

3.33

878.79 ✓

978.77

139

80.0 .

150

80.9 .

+75

81.2 .

140

81.7 .

+22

82.2 .

Lt.

L

Rt.

 $\frac{10.9}{50} \quad \frac{11.2}{26} \quad \frac{11.1}{17} \quad \frac{7.9}{12} \quad \frac{7.8}{10} \quad \frac{7.9}{8} \quad \frac{7.6}{8} \quad \frac{7.8}{11} \quad \frac{12.8}{20} \quad \frac{13.5}{34} \quad \frac{12.7}{50}$
 $\frac{7.8}{50} \quad \frac{7.4}{28} \quad \frac{9.1}{24} \quad \frac{9.1}{18} \quad \frac{6.9}{13} \quad \frac{6.7}{10} \quad \frac{6.5}{-} \quad \frac{6.8}{P} \quad \frac{7.1}{11} \quad \frac{9.2}{15} \quad \frac{9.4}{28} \quad \frac{9.6}{50}$
 $\frac{6.1}{50} \quad \frac{5.7}{29} \quad \frac{7.1}{20} \quad \frac{7.1}{17} \quad \frac{6.2}{18} \quad \frac{6.1}{10} \quad \frac{5.8}{8} \quad \frac{6.1}{8} \quad \frac{6.8}{15} \quad \frac{7.4}{19} \quad \frac{7.6}{30} \quad \frac{7.6}{50}$
 $\frac{9.6}{50} \quad \frac{9.8}{25} \quad \frac{9.2}{18} \quad \frac{5.6}{13} \quad \frac{5.9}{10} \quad \frac{4.7}{-} \quad \frac{4.8}{8} \quad \frac{5.0}{19} \quad \frac{4.5}{15} \quad \frac{4.0}{29} \quad \frac{1.9}{50}$
 $\frac{9.5}{30} \quad \frac{8.2}{29} \quad \frac{7.1}{19} \quad \frac{4.4}{13} \quad \frac{4.0}{10} \quad \frac{3.6}{8} \quad \frac{3.8}{14} \quad \frac{3.8}{25} \quad \frac{0.9}{50} \quad +1.0$
 $\frac{8.4}{50} \quad \frac{6.5}{31} \quad \frac{4.8}{17} \quad \frac{3.3}{13} \quad \frac{3.0}{10} \quad \frac{2.9}{12} \quad \frac{3.0}{12} \quad \frac{0.9}{25} \quad \frac{1.1}{50}$

Spk 110 P.P. #281 LL 5/2 138472

 $\frac{11.6}{50} \quad \frac{10.6}{28} \quad \frac{13.8}{27} \quad \frac{14.7}{18} \quad \frac{12.8}{14} \quad \frac{12.4}{9} \quad \frac{12.0}{8} \quad \frac{13.2}{8} \quad \frac{7.9}{50}$
 $\frac{16.9}{50} \quad \frac{14.2}{28} \quad \frac{12.9}{27} \quad \frac{13.6}{19} \quad \frac{11.8}{14} \quad \frac{11.4}{9} \quad \frac{11.1}{8} \quad \frac{11.5}{12} \quad \frac{11.8}{19} \quad \frac{13.8}{27} \quad \frac{13.8}{27} \quad \frac{8.4}{50}$
 $\frac{11.4}{50} \quad \frac{13.5}{30} \quad \frac{12.8}{28} \quad \frac{12.8}{18} \quad \frac{11.3}{14} \quad \frac{11.0}{9} \quad \frac{10.8}{7} \quad \frac{11.0}{14} \quad \frac{11.3}{20} \quad \frac{12.7}{20} \quad \frac{13.0}{25} \quad \frac{11.9}{50}$
 $\frac{15.8}{50} \quad \frac{14.2}{30} \quad \frac{12.9}{27} \quad \frac{11.6}{18} \quad \frac{10.8}{15} \quad \frac{10.6}{10} \quad \frac{10.3}{7} \quad \frac{10.4}{9} \quad \frac{10.5}{9} \quad \frac{10.0}{30} \quad \frac{10.2}{50}$
 $\frac{15.4}{50} \quad \frac{13.9}{30} \quad \frac{12.6}{27} \quad \frac{10.3}{15} \quad \frac{10.1}{10} \quad \frac{9.8}{-} \quad \frac{9.9}{6} \quad \frac{9.9}{11} \quad \frac{7.3}{16} \quad \frac{7.3}{16} \quad \frac{9.6}{50}$

Sta	+	X	-	Elev
		992.03		
140	+70			983.4
141				84.2
	+38			85.3
	+69			86.1
142				86.6
	+50			87.2
T.P.	8.30	995.88	4.45	997.58
143				87.8
	+90			88.5
	+75			89.0
144				89.3
	+60			89.4

11

4

21

$\frac{120}{50}$ $\frac{103}{30}$ $\frac{85}{27}$ $\frac{80}{19}$ $\frac{82}{15}$ $\frac{89}{9}$ $\frac{86}{6}$ $\frac{89}{6}$ $\frac{90}{10}$ $\frac{59}{12}$ $\frac{60}{41}$ $\frac{75}{49}$ $\frac{81}{50}$

$\frac{102}{50}$ $\frac{82}{30}$ $\frac{73}{29}$ $\frac{74}{21}$ $\frac{83}{16}$ $\frac{81}{9}$ $\frac{78}{-}$ $\frac{82}{6}$ $\frac{83}{12}$ $\frac{52}{18}$ $\frac{52}{50}$

$\frac{77}{50}$ $\frac{60}{30}$ $\frac{49}{28}$ $\frac{41}{22}$ $\frac{73}{16}$ $\frac{69}{9}$ $\frac{61}{-}$ $\frac{70}{6}$ $\frac{73}{12}$ $\frac{18}{24}$ $\frac{13}{50}$

$\frac{57}{50}$ $\frac{41}{30}$ $\frac{30}{29}$ $\frac{29}{22}$ $\frac{64}{15}$ $\frac{61}{9}$ $\frac{59}{-}$ $\frac{62}{6}$ $\frac{64}{13}$ $\frac{06}{24}$ $\frac{402}{36}$ $\frac{401}{50}$

$\frac{28}{50}$ $\frac{27}{30}$ $\frac{20}{28}$ $\frac{23}{21}$ $\frac{58}{16}$ $\frac{55}{8}$ $\frac{54}{-}$ $\frac{57}{7}$ $\frac{59}{12}$ $\frac{11}{23}$ $\frac{11}{50}$

$\frac{28}{50}$ $\frac{28}{28}$ $\frac{36}{19}$ $\frac{49}{16}$ $\frac{48}{8}$ $\frac{48}{-}$ $\frac{50}{6}$ $\frac{52}{10}$ $\frac{48}{14}$ $\frac{42}{27}$ $\frac{42}{50}$

$\frac{67}{50}$ $\frac{69}{28}$ $\frac{76}{19}$ $\frac{83}{16}$ $\frac{81}{7}$ $\frac{81}{-}$ $\frac{83}{9}$ $\frac{89}{16}$ $\frac{91}{26}$ $\frac{81}{50}$

$\frac{65}{50}$ $\frac{65}{27}$ $\frac{71}{20}$ $\frac{78}{16}$ $\frac{76}{8}$ $\frac{74}{-}$ $\frac{77}{7}$ $\frac{82}{15}$ $\frac{83}{30}$ $\frac{77}{50}$

$\frac{44}{50}$ $\frac{40}{26}$ $\frac{72}{17}$ $\frac{70}{9}$ $\frac{69}{-}$ $\frac{75}{8}$ $\frac{75}{16}$ $\frac{63}{19}$ $\frac{65}{23}$ $\frac{65}{50}$

$\frac{82}{50}$ $\frac{87}{28}$ $\frac{56}{20}$ $\frac{67}{9}$ $\frac{66}{-}$ $\frac{72}{8}$ $\frac{75}{12}$ $\frac{64}{18}$ $\frac{75}{22}$ $\frac{88}{50}$

$\frac{28}{50}$ $\frac{43}{28}$ $\frac{65}{21}$ $\frac{63}{9}$ $\frac{68}{-}$ $\frac{69}{8}$ $\frac{72}{12}$ $\frac{106}{19}$ $\frac{108}{27}$ $\frac{116}{50}$

Sta.	+	π	-	Elev
		995.88		
145				989.7 .
	+55			90.2 .
146				90.6 .
	+35			90.9 .
	+80			91.2 .
147				91.1 .
	+40			90.8 .
	+99			90.8 .
148				90.8 .
	+46			90.9 .
	+57			90.9 .

Lt.

K

Rt.

$$\frac{42}{50} \frac{52}{26} \frac{59}{21} \frac{61}{15} \frac{61}{7} \frac{62}{5} \frac{65}{8} \frac{69}{12} \frac{94}{23} \frac{105}{40} \frac{108}{50}$$

$$\frac{30}{50} \frac{38}{25} \frac{56}{18} \frac{56}{9} \frac{57}{9}$$

$$\frac{60}{60} \frac{65}{16} \frac{74}{28} \frac{90}{50}$$

$$\frac{35}{50} \frac{41}{28}$$

$$\frac{52}{9}$$

$$\frac{53}{7} \frac{57}{7} \frac{61}{11} \frac{67}{19} \frac{76}{26} \frac{91}{50}$$

$$\frac{41}{50} \frac{40}{32} \frac{48}{20} \frac{49}{9} \frac{50}{9} \frac{59}{6} \frac{57}{11} \frac{53}{18} \frac{62}{28} \frac{74}{50}$$

$$\frac{62}{50} \frac{48}{29} \frac{47}{17} \frac{51}{13} \frac{49}{8} \frac{47}{7} \frac{50}{13} \frac{39}{19} \frac{38}{25} \frac{69}{50}$$

$$\frac{73}{50} \frac{52}{22} \frac{52}{14} \frac{50}{8} \frac{48}{9} \frac{50}{8} \frac{50}{15} \frac{46}{20} \frac{53}{34} \frac{73}{50}$$

$$\frac{78}{50} \frac{73}{30} \frac{71}{22} \frac{58}{15} \frac{53}{9} \frac{51}{6} \frac{59}{14} \frac{58}{21} \frac{52}{36} \frac{63}{50}$$

$$\frac{61}{50} \frac{49}{23} \frac{56}{14} \frac{53}{8} \frac{51}{9} \frac{52}{6} \frac{53}{14} \frac{43}{20} \frac{38}{23} \frac{21}{50}$$

$$\frac{60}{50} \frac{69}{24} \frac{56}{15} \frac{53}{9} \frac{51}{5} \frac{52}{17} \frac{51}{50}$$

$$\frac{48}{50} \frac{52}{30} \frac{62}{22} \frac{56}{14} \frac{52}{8} \frac{50}{9}$$

$$\frac{51}{5} \frac{50}{13} \frac{82}{23} \frac{54}{31} \frac{53}{50}$$

$$\frac{47}{50} \frac{55}{29} \frac{62}{24} \frac{55}{14} \frac{52}{8} \frac{50}{6} \frac{52}{13} \frac{56}{20} \frac{29}{33} \frac{90}{50} \frac{87}{50}$$

Sta + X - Elev

995.88

149 990.9 .

+55 91.1 .

150 91.4 .

T.P. 8.79 1000.25 ✓ 4.42 991.46 ✓

+25 91.5 .

+73 91.3 .

151 91.2 .

+53 91.7 .

+62 91.9 .

+89 92.4 .

152 92.8 .

+50 94.2 .

LH

K

RH

$$\frac{21}{50} \quad \frac{42}{27} \quad \frac{53}{15} \quad \frac{51}{8} \quad \frac{50}{50}$$

$$\frac{52}{6}$$

$$\frac{56}{13} \quad \frac{90}{21} \quad \frac{94}{30} \quad \frac{102}{50}$$

$$\frac{21}{50} \quad \frac{31}{28} \quad \frac{50}{18} \quad \frac{99}{7}$$

$$\frac{48}{7} \quad \frac{50}{16} \quad \frac{52}{21} \quad \frac{57}{27} \quad \frac{64}{50} \quad \frac{71}{50}$$

$$\frac{08}{50} \quad \frac{21}{29} \quad \frac{47}{16} \quad \frac{46}{8} \quad \frac{46}{50}$$

$$\frac{48}{6} \quad \frac{48}{18} \quad \frac{57}{27} \quad \frac{68}{50}$$

$$\frac{54}{30} \quad \frac{73}{27} \quad \frac{92}{15} \quad \frac{90}{7} \quad \frac{88}{6} \quad \frac{92}{14} \quad \frac{94}{25} \quad \frac{111}{25} \quad \frac{120}{50}$$

$$\frac{98}{50} \quad \frac{104}{40} \quad \frac{105}{21} \quad \frac{93}{14} \quad \frac{92}{7} \quad \frac{90}{6} \quad \frac{92}{12} \quad \frac{97}{12} \quad \frac{126}{19} \quad \frac{136}{38} \quad \frac{143}{50}$$

$$\frac{120}{56} \quad \frac{120}{37} \quad \frac{112}{23} \quad \frac{94}{14} \quad \frac{92}{8} \quad \frac{91}{6} \quad \frac{93}{6} \quad \frac{96}{11} \quad \frac{140}{21} \quad \frac{150}{50}$$

$$\frac{122}{50} \quad \frac{121}{41} \quad \frac{114}{25} \quad \frac{89}{15} \quad \frac{87}{8} \quad \frac{86}{6} \quad \frac{88}{11} \quad \frac{91}{23} \quad \frac{125}{23} \quad \frac{129}{50}$$

$$\frac{120}{50} \quad \frac{110}{24} \quad \frac{87}{18} \quad \frac{86}{9} \quad \frac{84}{50}$$

$$\frac{86}{6} \quad \frac{89}{11} \quad \frac{102}{22} \quad \frac{114}{50}$$

$$\frac{115}{50} \quad \frac{117}{40} \quad \frac{110}{27} \quad \frac{83}{14} \quad \frac{82}{9} \quad \frac{79}{6} \quad \frac{80}{12} \quad \frac{84}{21} \quad \frac{93}{21} \quad \frac{97}{34} \quad \frac{103}{50}$$

$$\frac{110}{50} \quad \frac{103}{27} \quad \frac{78}{15} \quad \frac{78}{9} \quad \frac{75}{6} \quad \frac{76}{15} \quad \frac{80}{25} \quad \frac{88}{25} \quad \frac{84}{50}$$

$$\frac{79}{50} \quad \frac{72}{34} \quad \frac{69}{14} \quad \frac{64}{9} \quad \frac{61}{6} \quad \frac{64}{11} \quad \frac{66}{20} \quad \frac{49}{32} \quad \frac{49}{32} \quad \frac{40}{50}$$

Sta.	+	π	-	Elev.
		1000.25		
153				95.3
B.M.	3.94	✓ 1000.28	3.94	996.31 (996.34)
+50				96.1
154				96.7
+50				92.1
T.P.	12.17	✓ 1009.66	2.79	✓ 997.49
155				92.5
+50				98.0
156				98.7
+50				99.7
157				1000.8
+50				02.4
158				03.1

Lt

Rt

Rt

$\frac{44}{50}$	$\frac{36}{52}$	$\frac{52}{21}$	$\frac{51}{16}$	$\frac{52}{9}$	$\frac{50}{50}$	$\frac{52}{6}$	$\frac{56}{25}$	$\frac{55}{25}$	$\frac{39}{50}$
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Spk. in N. "H" Pole Rt. 153413

$\frac{14}{50}$	$\frac{0.9}{34}$	$\frac{2.9}{26}$	$\frac{4.3}{18}$	$\frac{4.3}{8}$	$\frac{42}{7}$	$\frac{44}{11}$	$\frac{47}{11}$	$\frac{55}{16}$	$\frac{45}{26}$	$\frac{50}{50}$
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$\frac{22}{50}$	$\frac{26}{30}$	$\frac{38}{20}$	$\frac{3.7}{8}$
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$\frac{36}{6}$	$\frac{2.9}{6}$	$\frac{40}{16}$	$\frac{6.1}{26}$	$\frac{7.1}{50}$
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$\frac{38}{50}$	$\frac{2.3}{30}$	$\frac{3.3}{19}$	$\frac{3.4}{8}$	$\frac{32}{7}$	$\frac{3.4}{15}$	$\frac{35}{25}$	$\frac{6.3}{25}$	$\frac{7.3}{50}$
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$\frac{118}{50}$	$\frac{11.3}{31}$	$\frac{11.8}{14}$	$\frac{12.5}{12}$	$\frac{12.3}{8}$	$\frac{12.2}{6}$	$\frac{12.4}{14}$	$\frac{13.1}{14}$	$\frac{13.5}{24}$	$\frac{16.2}{50}$
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$\frac{11.9}{50}$	$\frac{10.7}{29}$	$\frac{11.6}{18}$	$\frac{11.2}{12}$	$\frac{11.8}{8}$	$\frac{11.7}{7}$	$\frac{12.0}{14}$	$\frac{12.6}{14}$	$\frac{15.0}{25}$	$\frac{15.5}{50}$
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$\frac{10.6}{50}$	$\frac{11.1}{35}$	$\frac{10.7}{17}$	$\frac{11.2}{13}$	$\frac{11.2}{9}$	$\frac{11.0}{7}$	$\frac{11.4}{14}$	$\frac{11.9}{14}$	$\frac{13.8}{19}$	$\frac{14.8}{50}$
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$\frac{10.3}{50}$	$\frac{10.3}{37}$	$\frac{10.0}{28}$	$\frac{10.6}{20}$	$\frac{10.3}{10}$	$\frac{10.0}{6}$	$\frac{10.4}{12}$	$\frac{10.7}{12}$	$\frac{12.4}{18}$	$\frac{13.1}{27}$	$\frac{13.7}{50}$
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$\frac{9.3}{50}$	$\frac{9.5}{24}$	$\frac{10.0}{20}$	$\frac{9.4}{15}$	$\frac{9.1}{10}$	$\frac{8.9}{6}$	$\frac{9.2}{12}$	$\frac{9.4}{12}$	$\frac{11.3}{14}$	$\frac{11.9}{27}$	$\frac{12.6}{50}$
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$\frac{7.9}{50}$	$\frac{8.2}{37}$	$\frac{8.0}{29}$	$\frac{8.2}{20}$	$\frac{7.5}{13}$	$\frac{7.4}{9}$	$\frac{7.3}{6}$	$\frac{7.6}{12}$	$\frac{8.1}{12}$	$\frac{10.1}{20}$	$\frac{10.1}{29}$	$\frac{11.0}{50}$
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$\frac{6.6}{50}$	$\frac{7.0}{36}$	$\frac{6.8}{20}$	$\frac{6.1}{17}$	$\frac{5.9}{9}$	$\frac{5.9}{6}$	$\frac{5.9}{14}$	$\frac{6.8}{25}$	$\frac{6.7}{25}$	$\frac{8.5}{50}$
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Sta	+	π	-	Elev.
		1009.66		
158	+50			05.2 .
T.P.	11.84	✓ 1018.73	2.77	✓ 1006.89
159				06.8 .
	+50			08.8 .
160				10.9 .
	+50			12.9 .
T.P.	11.77	✓ 1026.70	3.80	✓ 1014.93
161				14.9 .
	+65			17.1 .
162				18.1 .
	+30			19.3 .
	+65			20.2 .
163				21.1 .

Lt

x

Lt

$$\frac{4.7}{50} \frac{5.3}{38} \frac{9.5}{28} \frac{4.7}{21} \frac{4.5}{10} 4.5 \frac{4.7}{6} \frac{5.1}{11} \frac{3.7}{19} \frac{3.9}{30} \frac{4.4}{30}$$

$$\frac{11.8}{50} \frac{12.1}{37} \frac{11.6}{28} \frac{11.8}{10} \frac{11.9}{6} \frac{12.3}{6} \frac{12.4}{11} \frac{12.2}{22} \frac{12.0}{50}$$

$$\frac{9.5}{58} \frac{9.6}{38} \frac{9.5}{14} \frac{10.3}{16} \frac{9.7}{10} \frac{9.9}{6} \frac{10.2}{15} \frac{10.1}{25} \frac{9.9}{25} \frac{11.2}{50}$$

$$\frac{8.1}{50} \frac{8.2}{39} \frac{7.5}{25} \frac{8.0}{16} \frac{7.7}{9} \frac{7.8}{6} \frac{8.1}{13} \frac{7.3}{24} \frac{7.3}{24} \frac{9.9}{50}$$

$$\frac{6.6}{50} \frac{6.2}{37} \frac{5.4}{26} \frac{6.2}{16} \frac{6.0}{10} \frac{5.8}{6} \frac{6.1}{6} \frac{6.5}{11} \frac{4.0}{15} \frac{4.1}{25} \frac{5.3}{50}$$

$$\frac{11.8}{50} \frac{11.5}{35} \frac{10.6}{26} \frac{12.0}{18} \frac{11.9}{10} \frac{11.8}{6} \frac{12.0}{5} \frac{12.5}{12} \frac{9.2}{15} \frac{9.1}{24} \frac{9.5}{50}$$

$$\frac{5.8}{50} \frac{5.9}{37} \frac{5.2}{29} \frac{9.8}{16} \frac{9.7}{10} \frac{9.6}{5} \frac{9.8}{10} \frac{9.9}{15} \frac{8.6}{23} \frac{10.3}{50}$$

$$\frac{4.8}{50} \frac{4.2}{27} \frac{4.1}{22} \frac{8.6}{16} \frac{8.5}{11} \frac{8.6}{5} \frac{8.6}{10} \frac{9.0}{14} \frac{8.2}{22} \frac{8.8}{22} \frac{10.8}{50}$$

$$\frac{4.9}{50} \frac{4.2}{25} \frac{5.2}{20} \frac{7.8}{15} \frac{7.6}{10} \frac{7.4}{5} \frac{7.6}{10} \frac{7.8}{10} \frac{7.4}{19} \frac{9.8}{50}$$

$$\frac{6.3}{50} \frac{5.9}{37} \frac{5.2}{29} \frac{5.4}{20} \frac{6.7}{15} \frac{6.6}{9} \frac{6.5}{5} \frac{6.8}{4} \frac{6.8}{10} \frac{7.1}{12} \frac{4.9}{16} \frac{4.9}{24} \frac{7.4}{50}$$

$$\frac{7.5}{50} \frac{6.5}{31} \frac{5.4}{21} \frac{5.9}{16} \frac{5.6}{10} \frac{5.6}{4} \frac{5.8}{4} \frac{6.2}{9} \frac{1.4}{18} \frac{1.1}{25} \frac{3.0}{50}$$

Sta	+	π	-	Elev.
		✓ 1026.70		
163	+37			1022.0
	+62			22.3
T.P.	7.50	✓ 1030.41	2.19	✓ 1022.91
164				22.9
	+42			23.7
	184			24.4
	+97			24.6
165	+22			24.9
	+38			25.2
166				26.7
	+50			27.9
167				28.5
T.P.	7.52	✓ 1036.02	1.91	✓ 1028.50
B.M.	11.60	✓ 1036.00	11.60	✓ 1024.42
				1024.40

Lt

L

Rt.

$\frac{8.3}{30}$	$\frac{6.9}{31}$	$\frac{6.2}{25}$	$\frac{5.2}{16}$	$\frac{5.0}{11}$	$\frac{4.7}{5}$	$\frac{4.8}{8}$	$\frac{4.9}{14}$	$\frac{3.9}{20}$	$\frac{4.6}{22}$	$\frac{4.0.3}{42}$	$\frac{0.7}{50}$
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$\frac{8.8}{50}$	$\frac{6.4}{29}$	$\frac{5.1}{17}$	$\frac{4.6}{10}$	$\frac{4.4}{11}$	$\frac{4.5}{8}$	$\frac{3.9}{12}$	$\frac{1.9}{34}$	$\frac{2.9}{50}$
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L 164

$\frac{12.3}{50}$	$\frac{11.1}{25}$	$\frac{8.3}{17}$	$\frac{7.8}{11}$	$\frac{7.6}{5}$	$\frac{7.6}{9}$	$\frac{7.1}{14}$	$\frac{10.4}{36}$	$\frac{16.5}{50}$
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$\frac{11.0}{50}$	$\frac{9.1}{26}$	$\frac{7.2}{16}$	$\frac{6.9}{11}$	$\frac{6.7}{5}$	$\frac{6.9}{11}$	$\frac{7.6}{28}$	$\frac{13.8}{50}$
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$\frac{9.3}{30}$	$\frac{8.8}{45}$	$\frac{6.5}{30}$	$\frac{6.0}{11}$	$\frac{6.0}{6}$	$\frac{6.4}{15}$	$\frac{7.2}{24}$	$\frac{10.5}{50}$	$\frac{17.3}{50}$
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$\frac{6.8}{30}$	$\frac{5.8}{11}$	$\frac{5.8}{7}$	$\frac{6.2}{30}$	$\frac{8.4}{50}$	$\frac{10.1}{50}$
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$\frac{6.5}{50}$	$\frac{5.5}{11}$	$\frac{5.5}{7}$	$\frac{7.8}{22}$	$\frac{9.5}{50}$
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$\frac{6.4}{30}$	$\frac{5.3}{39}$	$\frac{6.7}{39}$	$\frac{5.8}{29}$	$\frac{5.4}{14}$	$\frac{5.2}{13}$	$\frac{6.4}{17}$	$\frac{6.9}{39}$	$\frac{16.2}{50}$	$\frac{17.7}{50}$
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$\frac{4.7}{50}$	$\frac{3.2}{36}$	$\frac{3.2}{28}$	$\frac{3.8}{22}$	$\frac{3.6}{11}$	$\frac{3.7}{6}$	$\frac{4.2}{13}$	$\frac{4.1}{21}$	$\frac{9.3}{48}$	$\frac{15.3}{70}$	$\frac{17.3}{70}$
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$\frac{18}{50}$	$\frac{9.5}{33}$	$\frac{2.7}{16}$	$\frac{2.6}{11}$	$\frac{2.5}{5}$	$\frac{2.8}{12}$	$\frac{2.8}{18}$	$\frac{3.5}{22}$	$\frac{6.4}{32}$	$\frac{9.8}{50}$	$\frac{17.8}{50}$	$\frac{19}{65}$
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(water)

$\frac{13.1}{50}$	$\frac{13.5}{42}$	$\frac{10.8}{36}$	$\frac{10.3}{31}$	$\frac{1.1}{20}$	$\frac{2.3}{14}$	$\frac{2.1}{10}$	$\frac{1.9}{4}$	$\frac{2.1}{11}$	$\frac{2.2}{20}$	$\frac{1.8}{30}$	$\frac{3.1}{50}$	$\frac{10.0}{50}$
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Sta	+	Σ	-	Elev.
		1036.00		
167	+50			28.7
	+92			28.4
168	+11			28.3
	+38			27.8
	+81	2,		26.7
169				26.2
T.P.	0.99	1026.66	7.83	1026.17
	+90			25.0
	+63			24.2
170				22.9
	+31			22.0
	+68			21.1
T.P.	2.34	1022.74	6.26	1020.40

L1

R

Rt.

63	110	47	81	79	113	115	73	75	76	37	56	97
100	62	50	42	31	23	12		5	11	20	34	50

162	161	57	73	74	76	79	80	26	48	63
100	70	60	17	9		5	13	27	44	50

124	1120	28	64	74	77	77	80	80	66	31	25	44
100	53	37	20	18	11		6	15	23	31	40	50

161	1118	1128	57	84	82	85	85	11	10	25
100	74	53	30	12		7	17	32	41	50

166	134	80	116	110	99	75	93	95	96	26	104	104
93	68	34	32	19	14	10		7	17	28	40	50

42	32	106	101	98	100	100	32	16	15
50	35	26	16		8	17	27	42	50

45	42	29	18	17	21	23	18	34	37	10
50	24	17	11		8	12	13	20	27	50

68	71	63	50	27	25	29	37	62	71	56
50	38	26	16	11		9	13	19	32	50

113	114	48	41	38	41	43	70	79	71	44
50	32	19	11		8	12	18	22	26	50

131	130	56	50	47	49	52	88	75	60
50	32	16	11		8	12	22	33	50

173	144	66	60	56	57	62	112	107	113
50	30	14	10		8	12	25	34	50

Sta.	+	$\bar{x}$	-	Elev.
		1022.74		
171				20.4
	+50			19.3
172				18.4
	+50			17.6
173				17.1
	+50			16.8
174				16.8
T.P.	3.71	1020.68	5.71	1016.97
	+50			17.0
175				16.9
	+50			16.3
176				15.6

Lt

R

Rt

 $\frac{11.7}{50} \quad \frac{11.6}{31} \quad \frac{10.6}{25} \quad \frac{2.8}{12} \quad \frac{2.6}{10} \quad \frac{2.3}{-} \quad \frac{2.6}{8} \quad \frac{3.0}{13} \quad \frac{8.2}{22} \quad \frac{9.5}{32} \quad \frac{11}{50}$
 $\frac{12.0}{50} \quad \frac{1.5}{30} \quad \frac{8.9}{23} \quad \frac{3.8}{13} \quad \frac{3.6}{11} \quad \frac{3.4}{-} \quad \frac{3.7}{5} \quad \frac{4.5}{11} \quad \frac{11.1}{24} \quad \frac{12.4}{35} \quad \frac{12.8}{50}$
 $\frac{10.6}{50} \quad \frac{10.6}{35} \quad \frac{9.5}{22} \quad \frac{5.3}{12} \quad \frac{4.5}{10} \quad \frac{4.3}{-} \quad \frac{4.6}{6} \quad \frac{5.2}{11} \quad \frac{10.6}{20} \quad \frac{12.5}{31} \quad \frac{12.6}{50}$
 $\frac{5.1}{50} \quad \frac{6.9}{36} \quad \frac{7.0}{27} \quad \frac{8.3}{23} \quad \frac{8.2}{19} \quad \frac{5.9}{13} \quad \frac{5.6}{11} \quad \frac{5.1}{-} \quad \frac{5.2}{6} \quad \frac{5.6}{10} \quad \frac{11.9}{22} \quad \frac{11.8}{50}$
 $\frac{0.9}{50} \quad \frac{4.8}{27} \quad \frac{5.7}{22} \quad \frac{6.9}{19} \quad \frac{7.2}{16} \quad \frac{6.1}{13} \quad \frac{5.9}{9} \quad \frac{5.6}{-} \quad \frac{5.9}{7} \quad \frac{6.8}{11} \quad \frac{11.5}{19} \quad \frac{12.1}{8.50}$
 $\frac{10.2}{50} \quad \frac{1.9}{37} \quad \frac{1.6}{27} \quad \frac{2.9}{22} \quad \frac{6.2}{16} \quad \frac{6.3}{12} \quad \frac{5.9}{-} \quad \frac{6.1}{6} \quad \frac{6.6}{12} \quad \frac{11.3}{22} \quad \frac{12.0}{50}$
 $\frac{1.8}{50} \quad \frac{0.8}{40} \quad \frac{0.8}{27} \quad \frac{2.3}{21} \quad \frac{6.0}{14} \quad \frac{6.0}{8} \quad \frac{5.9}{-} \quad \frac{6.1}{7} \quad \frac{6.5}{12} \quad \frac{9.3}{18} \quad \frac{11.4}{29} \quad \frac{12.0}{36}$
 $\frac{4.8}{50} \quad \frac{2.2}{28} \quad \frac{4.0}{16} \quad \frac{3.8}{8} \quad \frac{3.1}{-} \quad \frac{4.2}{9} \quad \frac{4.5}{16} \quad \frac{4.9}{26} \quad \frac{8.9}{29} \quad \frac{8.9}{25} \quad \frac{5.8}{29} \quad \frac{6.8}{50}$
 $\frac{8.0}{50} \quad \frac{7.6}{30} \quad \frac{6.6}{19} \quad \frac{4.7}{12} \quad \frac{4.1}{7} \quad \frac{3.8}{-} \quad \frac{4.0}{10} \quad \frac{4.4}{12} \quad \frac{4.5}{30} \quad \frac{5.1}{50}$
 $\frac{8.5}{50} \quad \frac{8.5}{22} \quad \frac{8.2}{17} \quad \frac{5.5}{11} \quad \frac{5.0}{8} \quad \frac{4.4}{-} \quad \frac{4.4}{10} \quad \frac{5.9}{18} \quad \frac{4.5}{31} \quad \frac{3.0}{50}$
 $\frac{8.5}{50} \quad \frac{8.3}{17} \quad \frac{5.6}{11} \quad \frac{5.4}{8} \quad \frac{5.1}{-} \quad \frac{5.3}{10} \quad \frac{5.8}{22} \quad \frac{5.8}{33} \quad \frac{4.4}{50}$

Sta	+	π	-	Elev
		1020.68		
176	+50			15.4
177				15.8
	+50			16.7
T.P.	7.71	1025.41	2.98	1017.70
178				18.3
	+23			19.0
	+96			19.6
179				20.8
T.P.	5.73	1031.14	0.00	1025.41
	SEE NEXT Page for XSection at 177+40			21.5
	+54			21.6
	+85			21.6
180				21.5
	+30			21.5

Lt

L

Rt

$$\begin{array}{r} 850 \\ 50 \end{array} \quad \begin{array}{r} 89 \\ 28 \end{array} \quad \begin{array}{r} 80 \\ 17 \end{array} \quad \begin{array}{r} 58 \\ 11 \end{array} \quad \begin{array}{r} 55 \\ 8 \end{array} \quad \begin{array}{r} 53 \\ 11 \end{array} \quad \begin{array}{r} 56 \\ 17 \end{array} \quad \begin{array}{r} 63 \\ 31 \end{array} \quad \begin{array}{r} 61 \\ 50 \end{array} \quad \begin{array}{r} 58 \\ 50 \end{array}$$

$$\begin{array}{r} 85 \\ 50 \end{array} \quad \begin{array}{r} 85 \\ 21 \end{array} \quad \begin{array}{r} 80 \\ 18 \end{array} \quad \begin{array}{r} 54 \\ 11 \end{array} \quad \begin{array}{r} 52 \\ 8 \end{array} \quad \begin{array}{r} 49 \\ 11 \end{array} \quad \begin{array}{r} 49 \\ 24 \end{array} \quad \begin{array}{r} 62 \\ 50 \end{array} \quad \begin{array}{r} 55 \\ 50 \end{array}$$

$$\begin{array}{r} 85 \\ 50 \end{array} \quad \begin{array}{r} 82 \\ 28 \end{array} \quad \begin{array}{r} 80 \\ 20 \end{array} \quad \begin{array}{r} 96 \\ 12 \end{array} \quad \begin{array}{r} 41 \\ 8 \end{array} \quad \begin{array}{r} 40 \\ 11 \end{array} \quad \begin{array}{r} 43 \\ 18 \end{array} \quad \begin{array}{r} 50 \\ 23 \end{array} \quad \begin{array}{r} 61 \\ 27 \end{array} \quad \begin{array}{r} 52 \\ 34 \end{array} \quad \begin{array}{r} 45 \\ 50 \end{array} \quad \begin{array}{r} 13 \\ 50 \end{array}$$

Nail in T.R.R. 177190

$$\begin{array}{r} 129 \\ 50 \end{array} \quad \begin{array}{r} 129 \\ 27 \end{array} \quad \begin{array}{r} 122 \\ 20 \end{array} \quad \begin{array}{r} 81 \\ 11 \end{array} \quad \begin{array}{r} 77 \\ 7 \end{array} \quad \begin{array}{r} 71 \\ 10 \end{array} \quad \begin{array}{r} 72 \\ 19 \end{array} \quad \begin{array}{r} 76 \\ 21 \end{array} \quad \begin{array}{r} 71 \\ 32 \end{array} \quad \begin{array}{r} 53 \\ 50 \end{array} \quad \begin{array}{r} 13 \\ 50 \end{array}$$

$$\begin{array}{r} 127 \\ 50 \end{array} \quad \begin{array}{r} 126 \\ 30 \end{array} \quad \begin{array}{r} 120 \\ 24 \end{array} \quad \begin{array}{r} 74 \\ 12 \end{array} \quad \begin{array}{r} 69 \\ 8 \end{array} \quad \begin{array}{r} 64 \\ 10 \end{array} \quad \begin{array}{r} 67 \\ 20 \end{array} \quad \begin{array}{r} 65 \\ 27 \end{array} \quad \begin{array}{r} 37 \\ 41 \end{array} \quad \begin{array}{r} 26 \\ 50 \end{array} \quad \begin{array}{r} 20 \\ 50 \end{array}$$

$$\begin{array}{r} 12.5 \\ 50 \end{array} \quad \begin{array}{r} 11.7 \\ 29 \end{array} \quad \begin{array}{r} 86 \\ 23 \end{array} \quad \begin{array}{r} 69 \\ 15 \end{array} \quad \begin{array}{r} 62 \\ 9 \end{array} \quad \begin{array}{r} 58 \\ 10 \end{array} \quad \begin{array}{r} 61 \\ 22 \end{array} \quad \begin{array}{r} 58 \\ 28 \end{array} \quad \begin{array}{r} 14.04 \\ 31 \end{array} \quad \begin{array}{r} 04 \\ 50 \end{array} \quad \begin{array}{r} + 06 \\ 50 \end{array}$$

$$\begin{array}{r} 88 \\ 50 \end{array} \quad \begin{array}{r} 73 \\ 27 \end{array} \quad \begin{array}{r} 60 \\ 19 \end{array} \quad \begin{array}{r} 49 \\ 9 \end{array}$$

$$\begin{array}{r} 46 \\ 11 \end{array} \quad \begin{array}{r} 47 \\ 18 \end{array} \quad \begin{array}{r} 46 \\ 18 \end{array}$$

Nail in P.R. 43 Rt. 179215

$$\begin{array}{r} 88 \\ 50 \end{array} \quad \begin{array}{r} 59 \\ 29 \end{array} \quad \begin{array}{r} 9.2 \\ 22 \end{array} \quad \begin{array}{r} 10.1 \\ 12 \end{array} \quad \begin{array}{r} 100 \\ 9 \end{array} \quad \begin{array}{r} 96 \\ 9 \end{array} \quad \begin{array}{r} 97 \\ 13 \end{array} \quad \begin{array}{r} 97 \\ 21 \end{array} \quad \begin{array}{r} 63 \\ 21 \end{array}$$

$$\begin{array}{r} 59 \\ 50 \end{array} \quad \begin{array}{r} 18 \\ 50 \end{array} \quad \begin{array}{r} 80 \\ 18 \end{array} \quad \begin{array}{r} 96 \\ 13 \end{array} \quad \begin{array}{r} 98 \\ 9 \end{array}$$

$$\begin{array}{r} 95 \\ 9 \end{array} \quad \begin{array}{r} 96 \\ 12 \end{array} \quad \begin{array}{r} 97 \\ 21 \end{array} \quad \begin{array}{r} 96 \\ 21 \end{array}$$

$$\begin{array}{r} 42 \\ 50 \end{array} \quad \begin{array}{r} 14 \\ 35 \end{array}$$

$$\begin{array}{r} 67 \\ 24 \end{array} \quad \begin{array}{r} 99 \\ 13 \end{array} \quad \begin{array}{r} 98 \\ 9 \end{array} \quad \begin{array}{r} 96 \\ 9 \end{array} \quad \begin{array}{r} 96 \\ 9 \end{array} \quad \begin{array}{r} 98 \\ 12 \end{array} \quad \begin{array}{r} 78 \\ 21 \end{array}$$

$$\begin{array}{r} 41 \\ 50 \end{array} \quad \begin{array}{r} 18 \\ 32 \end{array} \quad \begin{array}{r} 76 \\ 23 \end{array} \quad \begin{array}{r} 97 \\ 15 \end{array} \quad \begin{array}{r} 98 \\ 9 \end{array} \quad \begin{array}{r} 96 \\ 9 \end{array} \quad \begin{array}{r} 98 \\ 12 \end{array} \quad \begin{array}{r} 100 \\ 17 \end{array} \quad \begin{array}{r} 92 \\ 28 \end{array} \quad \begin{array}{r} 35 \\ 33 \end{array} \quad \begin{array}{r} 59 \\ 33 \end{array} \quad \begin{array}{r} 98 \\ 50 \end{array}$$

Cont. on next page.

Sta	+	X	-	Elev
		1021.14		
180	+65			21.3
T.P.			10.42	1020.72
T.P.	13.34	1028.75		(1028.91)
179				20.8
	+40			21.5
	+54			21.5
	+85			21.6
180				21.5
T.P.	1.06	1025.80	11.01	1022.79
T.P.	2.46	1023.16	8.10	1020.70 (1020.72)
181				20.7
	+90			19.6

This section along top ditch. Culv $\frac{3}{8}$ Full dirt.

182 18.5

Lt.

K

Rt.

$\frac{60}{50}$	$\frac{74}{36}$	$\frac{63}{28}$	$\frac{93}{24}$	$\frac{105}{16}$	$\frac{100}{9}$	$\frac{98}{9}$	$\frac{102}{9}$	$\frac{103}{13}$	$\frac{99}{20}$	$\frac{86}{23}$	$\frac{124}{33}$	$\frac{137}{50}$
-----------------	-----------------	-----------------	-----------------	------------------	-----------------	----------------	-----------------	------------------	-----------------	-----------------	------------------	------------------

Sta 181

Na. 110 T.P. Rt. 179+15

(18.0)

$\frac{101}{31}$	$\frac{78}{33}$	$\frac{66}{30}$	$\frac{60}{75}$
------------------	-----------------	-----------------	-----------------

(17.3)

$\frac{174}{9}$	$\frac{175}{13}$	$\frac{170}{16}$	$\frac{43}{36}$	$\frac{00}{40}$	$\frac{02}{51}$	$\frac{18}{75}$
-----------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------

(17.3)

$\frac{25}{38}$	$\frac{41}{41}$	$\frac{12}{59}$	$\frac{90}{75}$
-----------------	-----------------	-----------------	-----------------

(17.4)

$\frac{64}{34}$	$\frac{32}{36}$	$\frac{44}{41}$	$\frac{73}{36}$	$\frac{11.1}{75}$
-----------------	-----------------	-----------------	-----------------	-------------------

(17.3)

$\frac{94}{30}$	$\frac{61}{33}$	$\frac{85}{39}$	$\frac{107}{50}$
-----------------	-----------------	-----------------	------------------

Sta 181

$\frac{52}{50}$	$\frac{56}{33}$	$\frac{49}{26}$	$\frac{30}{14}$	$\frac{27}{9}$	$\frac{25}{10}$	$\frac{27}{14}$	$\frac{31}{22}$	$\frac{62}{32}$	$\frac{70}{30}$	$\frac{79}{30}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{84}{50}$	$\frac{91}{36}$	$\frac{91}{27}$	$\frac{83}{17}$	$\frac{42}{12}$	$\frac{38}{8}$	$\frac{36}{10}$	$\frac{28}{13}$	$\frac{44}{25}$	$\frac{106}{50}$	$\frac{110}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{119}{100}$	$\frac{116}{50}$	$\frac{1371}{\text{Culv}}$	($\frac{100}{\text{Culv}}$)	$\frac{1265}{\text{Culv}}$	$\frac{116}{50}$	$\frac{116}{100}$
-------------------	------------------	----------------------------	-------------------------------	----------------------------	------------------	-------------------

$\frac{110}{50}$	$\frac{109}{23}$	$\frac{51}{16}$	$\frac{48}{8}$	$\frac{47}{10}$	$\frac{51}{14}$	$\frac{55}{22}$	$\frac{101}{50}$	$\frac{102}{50}$
------------------	------------------	-----------------	----------------	-----------------	-----------------	-----------------	------------------	------------------

Sta	+	π	-	Elev	
		1023.16			
182	+50			18.2	
183				18.2	
	+40			18.6	
B.M.	11.72	1027.42	7.46	1015.70	1015.72
	+20			19.0	
184				19.4	
	+50			20.5	
185				22.1	
T.P.	9.92	1022.00	5.34	1022.08	
	+50			23.6	
186				24.7	
	+30			25.1	
	+65			25.8	

Lt.

K

Rt.

$$\frac{109}{50} \frac{109}{24} \frac{54}{13} \frac{51}{8} \frac{50}{7} \frac{54}{13} \frac{59}{21} \frac{102}{21} \frac{106}{50}$$

$$\frac{105}{50} \frac{107}{24} \frac{53}{13} \frac{51}{8} \frac{50}{10} \frac{55}{13} \frac{59}{20} \frac{99}{20} \frac{100}{50}$$

$$\frac{70}{50} \frac{76}{53} \frac{85}{21} \frac{84}{13} \frac{49}{8} \frac{46}{10} \frac{50}{13} \frac{88}{22} \frac{89}{34} \frac{82}{50}$$

Jpk in N. H. Calc Rt 182498

$$\frac{56}{30} \frac{82}{27} \frac{98}{16} \frac{106}{14} \frac{91}{13} \frac{81}{8} \frac{84}{10} \frac{88}{15} \frac{92}{18} \frac{112}{21} \frac{106}{21} \frac{107}{50}$$

$$\frac{95}{30} \frac{65}{35} \frac{70}{27} \frac{83}{29} \frac{84}{17} \frac{96}{19} \frac{83}{11} \frac{82}{7} \frac{80}{10} \frac{81}{15} \frac{83}{18} \frac{98}{21} \frac{91}{21} \frac{89}{50}$$

$$\frac{51}{30} \frac{62}{29} \frac{75}{17} \frac{73}{13} \frac{72}{9} \frac{69}{10} \frac{71}{10} \frac{73}{13} \frac{82}{18} \frac{73}{22} \frac{71}{25} \frac{65}{50}$$

$$\frac{67}{30} \frac{44}{26} \frac{58}{17} \frac{75}{14} \frac{59}{12} \frac{56}{8} \frac{53}{7} \frac{57}{10} \frac{59}{17} \frac{65}{19} \frac{53}{22} \frac{52}{33} \frac{43}{36} \frac{43}{50}$$

$$\frac{55}{30} \frac{59}{27} \frac{72}{18} \frac{97}{12} \frac{70}{11} \frac{89}{7} \frac{84}{10} \frac{86}{14} \frac{89}{17} \frac{91}{21} \frac{81}{28} \frac{80}{37} \frac{74}{37} \frac{76}{50}$$

$$\frac{87}{30} \frac{88}{27} \frac{98}{24} \frac{99}{22} \frac{110}{15} \frac{74}{12} \frac{74}{8} \frac{73}{10} \frac{78}{14} \frac{81}{20} \frac{89}{28} \frac{87}{28} \frac{96}{50}$$

$$\frac{108}{50} \frac{111}{20} \frac{78}{14} \frac{71}{8} \frac{69}{10} \frac{71}{10} \frac{76}{17} \frac{76}{22} \frac{98}{28} \frac{99}{37} \frac{86}{50}$$

$$\frac{115}{50} \frac{115}{23} \frac{71}{15} \frac{66}{9} \frac{62}{10} \frac{65}{18} \frac{70}{20} \frac{85}{23} \frac{85}{23} \frac{75}{27} \frac{64}{37} \frac{79}{50}$$

Sta.	+	π	-	Elev.
		1032.00		
187				26.6
	+52			28.1
188				30.0
T.P.	12.53	1043.34	4.19	1090.58
	+50			31.7
189				33.2
	+50			34.6
190				35.2
T.P.	5.27	1040.52	8.09	1035.25
	+58			35.5
	+90			35.5
191				35.6
	+23			35.3

Lt

K

Rt.

$$\frac{11.3}{50} \quad \frac{11.3}{25} \quad \frac{6.9}{15} \quad \frac{5.7}{9} \quad \frac{5.9}{9} \quad \frac{5.7}{9} \quad \frac{6.5}{17} \quad \frac{7.9}{20} \quad \frac{7.1}{23} \quad \frac{6.4}{37} \quad \frac{7.6}{50}$$

$$\frac{9.9}{50} \quad \frac{9.2}{31} \quad \frac{8.0}{22} \quad \frac{4.9}{17} \quad \frac{4.3}{10} \quad \frac{3.9}{10} \quad \frac{4.2}{10} \quad \frac{4.4}{17} \quad \frac{7.4}{22} \quad \frac{7.8}{29} \quad \frac{6.4}{38} \quad \frac{6.1}{50}$$

$$\frac{7.3}{50} \quad \frac{7.2}{30} \quad \frac{5.7}{22} \quad \frac{2.7}{14} \quad \frac{2.5}{10} \quad \frac{2.0}{8} \quad \frac{2.3}{8} \quad \frac{2.5}{17} \quad \frac{3.3}{19} \quad \frac{2.5}{23} \quad \frac{0.9}{36} \quad \frac{1.1}{50}$$

Napil in T. A. Rt. 185+05

$$\frac{13.4}{50} \quad \frac{12.4}{31} \quad \frac{11.4}{26} \quad \frac{11.9}{22} \quad \frac{12.2}{12} \quad \frac{11.8}{10} \quad \frac{11.6}{8} \quad \frac{12.0}{8} \quad \frac{12.4}{12} \quad \frac{12.0}{19} \quad \frac{7.9}{25} \quad \frac{6.7}{36} \quad \frac{7.6}{50}$$

$$\frac{7.1}{50} \quad \frac{6.6}{28} \quad \frac{7.4}{23} \quad \frac{10.5}{20} \quad \frac{10.6}{14} \quad \frac{10.5}{11} \quad \frac{10.1}{8} \quad \frac{10.5}{8} \quad \frac{11.2}{12} \quad \frac{10.7}{15} \quad \frac{9.7}{19} \quad \frac{5.1}{25} \quad \frac{4.9}{33} \quad \frac{6.2}{50}$$

$$\frac{3.0}{50} \quad \frac{3.8}{28} \quad \frac{7.7}{22} \quad \frac{8.7}{17} \quad \frac{8.9}{10} \quad \frac{8.7}{8} \quad \frac{9.1}{8} \quad \frac{9.7}{14} \quad \frac{5.4}{21} \quad \frac{7.2}{30} \quad \frac{8.7}{50}$$

$$\frac{1.0}{50} \quad \frac{2.0}{25} \quad \frac{7.5}{20} \quad \frac{8.0}{15} \quad \frac{8.0}{10} \quad \frac{8.1}{7} \quad \frac{8.5}{7} \quad \frac{8.8}{12} \quad \frac{8.0}{16} \quad \frac{12.2}{29} \quad \frac{14.4}{50}$$

$$\frac{+2.0}{50} \quad \frac{+1.2}{37} \quad \frac{+0.4}{25} \quad \frac{5.2}{17} \quad \frac{5.0}{11} \quad \frac{5.0}{8} \quad \frac{5.3}{8} \quad \frac{5.9}{13} \quad \frac{13.0}{33} \quad \frac{12.9}{50}$$

$$\frac{+1.5}{50} \quad \frac{5.7}{37} \quad \frac{5.3}{27}$$

$$\frac{5.0}{10} \quad \frac{5.4}{10} \quad \frac{6.0}{15} \quad \frac{9.7}{27} \quad \frac{12.0}{34} \quad \frac{13.2}{50}$$

$$\frac{5.3}{50} \quad \frac{5.3}{32} \quad \frac{4.9}{10} \quad \frac{5.4}{10} \quad \frac{6.1}{16} \quad \frac{5.7}{29} \quad \frac{10.1}{43} \quad \frac{9.3}{50}$$

$$\frac{5.2}{62} \quad \frac{5.2}{28} \quad \frac{6.1}{28} \quad \frac{7.0}{37} \quad \frac{8.4}{50}$$

sta + A - Elev

1040.52

191+32

35.1

+38.5

34.9

+48.5 E. Co Line

35.0

5.53

1034.99

1035.02

Lt

C

Rt

$$\frac{5.1}{50}$$

$$\frac{5.4}{50}$$

$$\frac{6.3}{50}$$

$$\frac{5.1}{50}$$

$$\frac{5.6}{50}$$

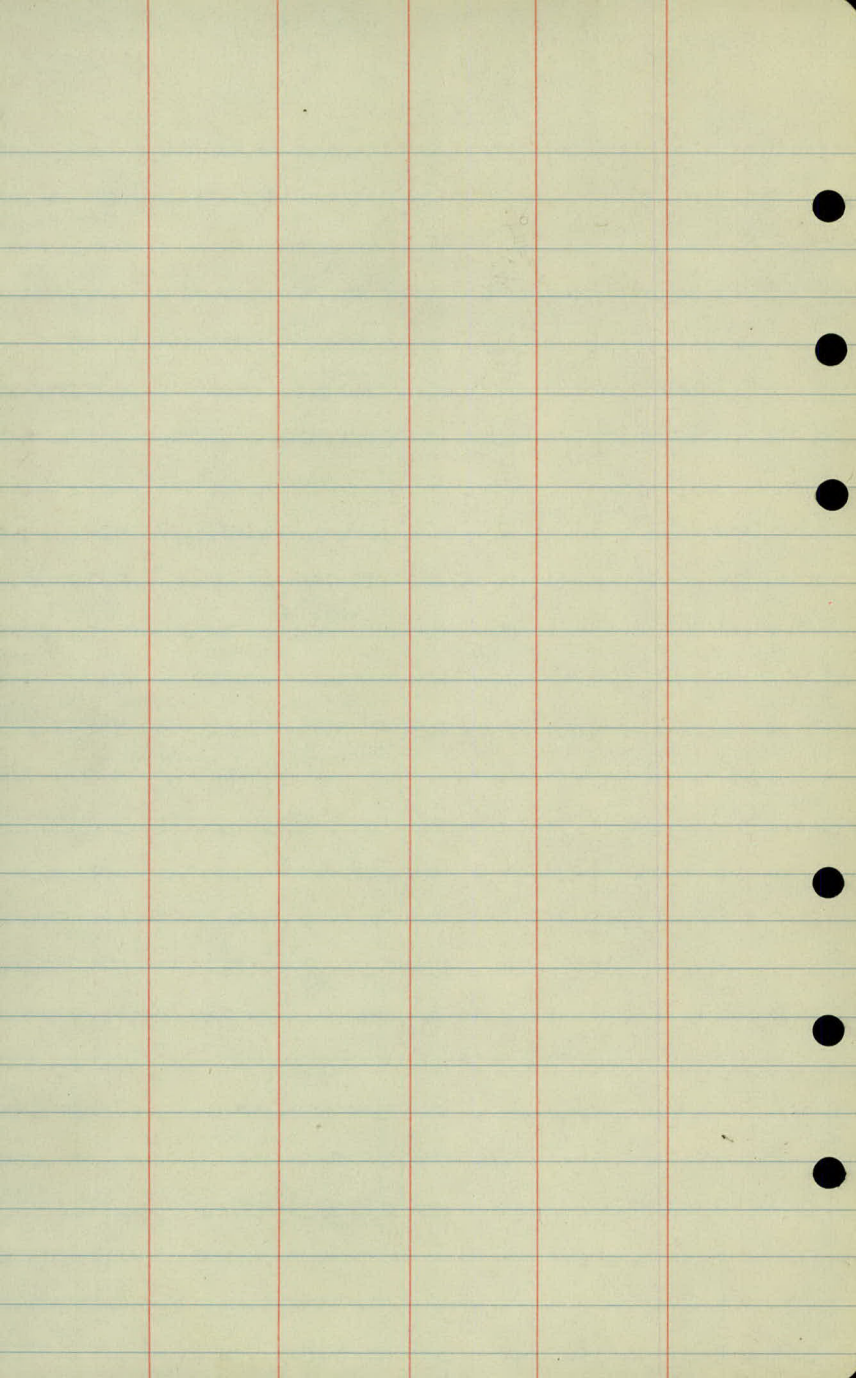
$$\frac{6.4}{50}$$

$$\frac{5.0}{50}$$

$$\frac{5.5}{50}$$

$$\frac{6.4}{50}$$

Brass Plug in Pavement "D" & E. Co. Line



Bench Levels.

Sta.	δ	π	-	Elev.	
B.M.	2.65	949.50			(941.85)
T.P.	3.72	940.74	2.55	936.95	
T.P.	13.53	959.29	0.09	940.70	
B.M.			2.97	946.76	
T.P.	9.18	962.82	0.59	953.64	
T.P.	2.50	962.27	3.05	959.77	
T.P.	2.91	957.99	7.69	959.58	
T.P.	13.18	965.25	5.42	952.07	
B.M.	12.83	974.44	3.64	961.61	
T.P.	6.37	978.64	1.17	973.27	
B.M.	10.27	989.04	0.87	978.77	
T.P.	7.51	996.03	0.52	988.52	
	6.09	997.02	5.10	996.93	
B.M.	8.46	1004.80	0.68	996.34	
T.P.	13.50	1017.89	0.41	1004.39	
T.P.	12.05	1029.36	0.58	1017.31	
B.M.			4.96	1024.40	(1024.35)
T.P.	0.75	1028.62	1.49	1027.57	
T.P.	3.50	1020.61	11.51	1017.11	
T.P.	5.33	1025.02	0.92	1019.69	
B.M.	13.60	1027.32	9.30	1015.72	
T.P.	11.41	1040.04	0.69	1028.63	
B.M.			5.02	1035.02	

Description

Spt in S.H. Pole Lt 90485

Top Hole to the White Bear Ave & Co Rd. "D"

Spt in PP #667 Lt 126465

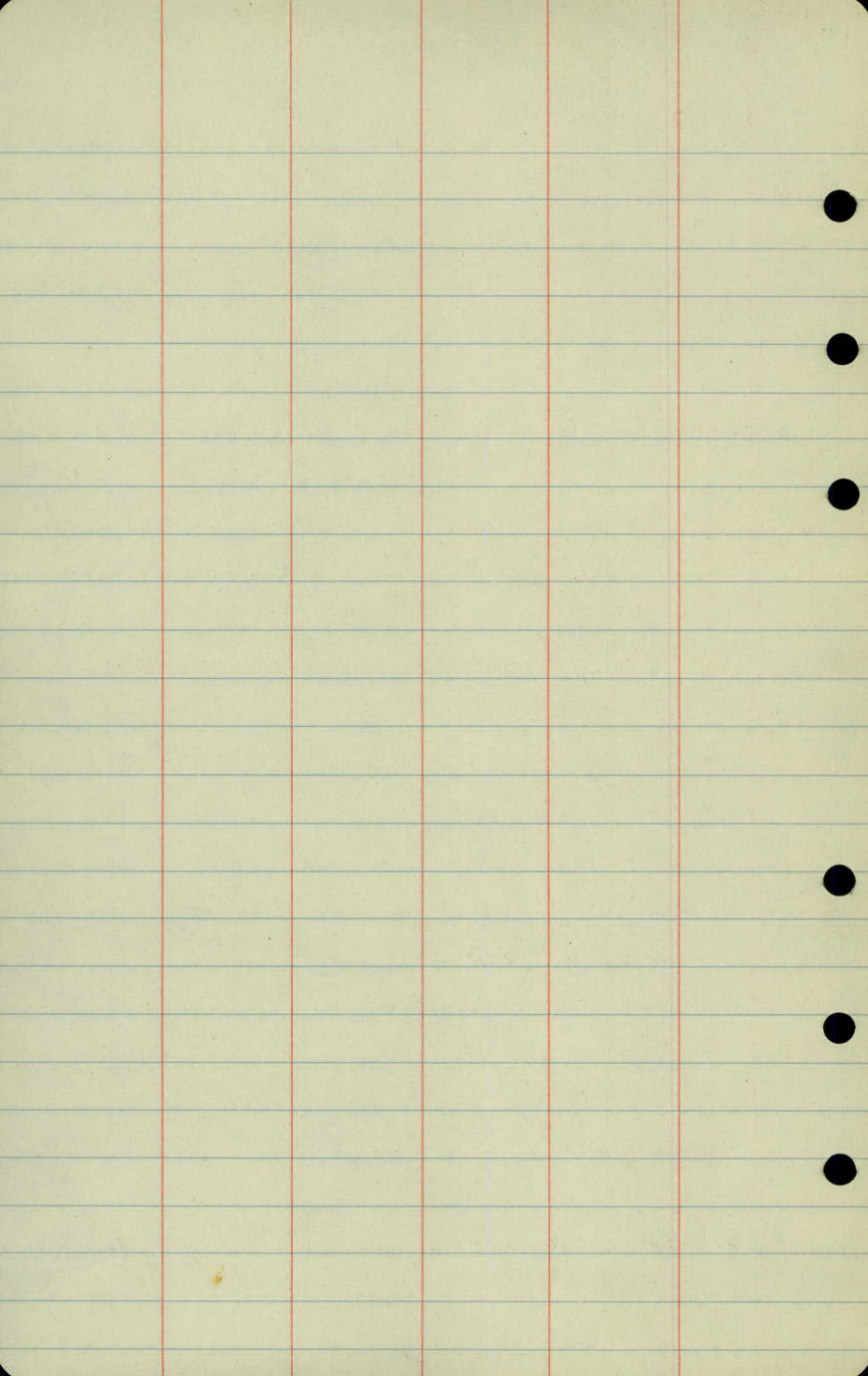
Spt in PP #681 Lt 138472

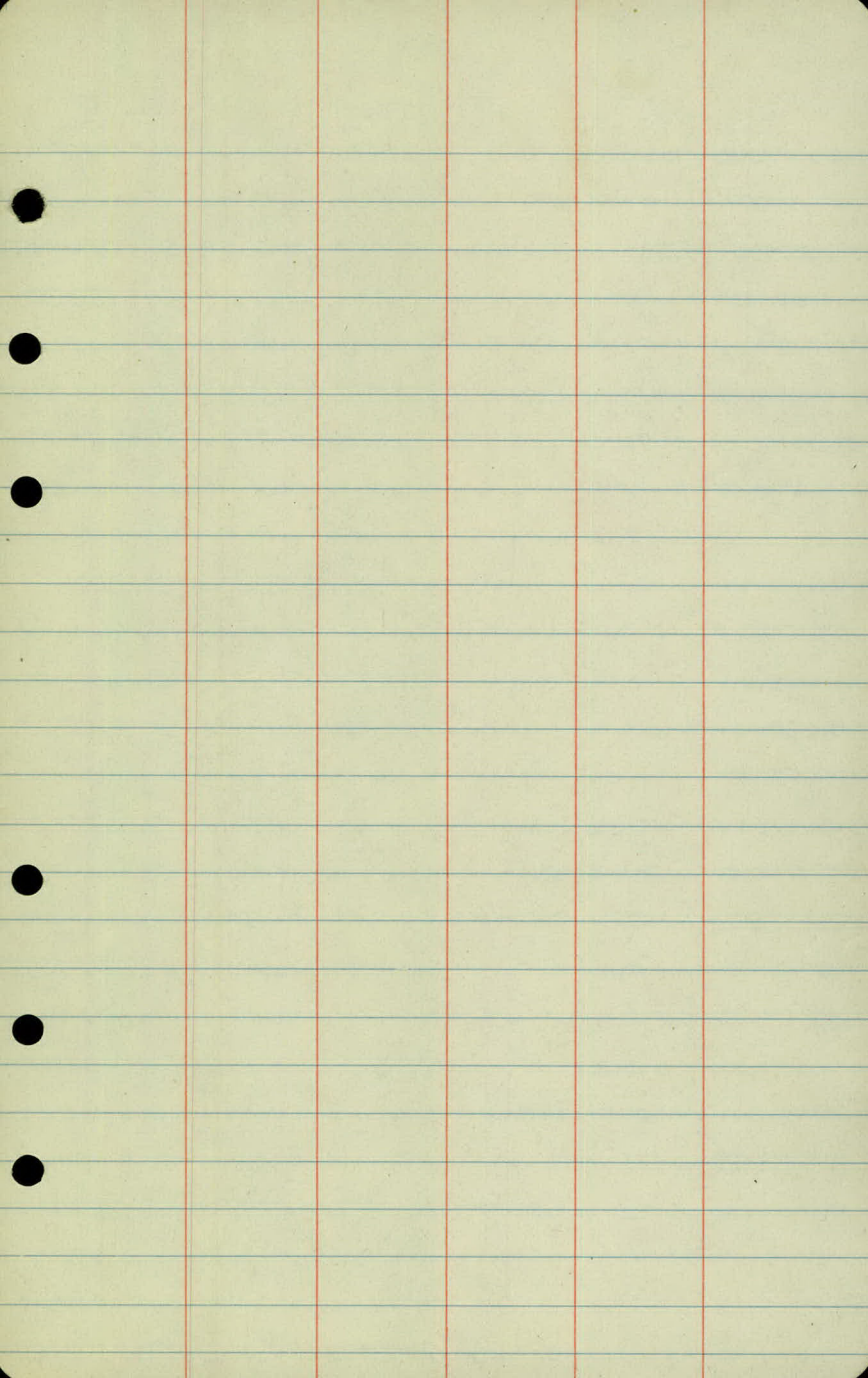
Spt in N.H. Pole Lt 153493

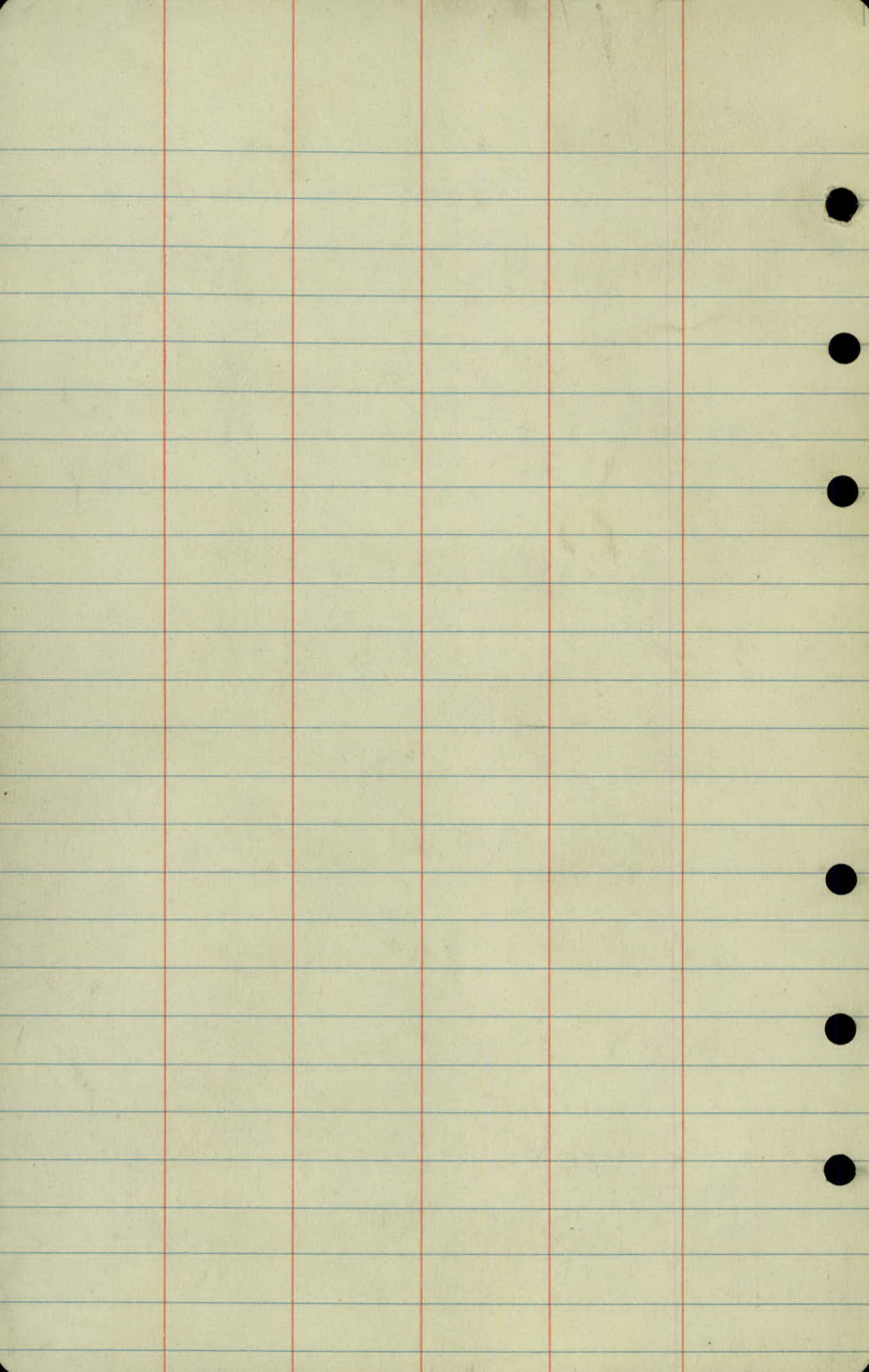
Top Mont. Bellaire & Co Rd. "D"

Spt in N.H. Pole Lt 182498

Top Brass Plus E Coling & Co Rd. "D"







30 Crown 1
2 to 1 Slopes
2' Ditch
23'

"D"

Slope stakes from Labore Rd
St 0+00 to Back St. 59+

Special Section 35 to 36+70 Rt.

" " 54 to 57 Rt

Sta.	+	x	-	Grade.
B.M.	278	928.66		925.88

0

+50

1

+50

23.1

2

22.8

+50

22.5

3

22.3

+35

22.3

Lt.

E

Rt.

21

Spike in Guy Pole S.W. Cor. Loberc & D.

4.0
6.0
$$\begin{array}{r} 38 \\ DC21.7 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 32 \\ DC2.8 \\ \hline 28.6 \end{array}$$
4.9
6.9
$$\begin{array}{r} 42 \\ DC27 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC15 \\ \hline 26.0 \end{array}$$
5.6
7.6
$$\begin{array}{r} 4.9 \\ DC27 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline 60.3 \end{array}$$

$$\begin{array}{r} 2.0 \\ DC0.6 \\ \hline 24.2 \end{array}$$
5.9
7.9
$$\begin{array}{r} 5.5 \\ DC24 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 8.8 \\ \hline 60.1 \end{array}$$

$$\begin{array}{r} 2.9 \\ DC0.0 \\ \hline 21.5 \end{array}$$
6.2
8.2
$$\begin{array}{r} 5.4 \\ DC28 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline 130.4 \end{array}$$

$$\begin{array}{r} 9.4 \\ F32 \\ \hline 21.4 \end{array}$$
6.4
8.4
$$\begin{array}{r} 9.2 \\ F.2 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 7.4 \\ \hline F1.0 \end{array}$$

$$\begin{array}{r} 11.0 \\ F46 \\ \hline 24.2 \end{array}$$
6.4
8.4
$$\begin{array}{r} 11.5 \\ F.1 \\ \hline 21.5 \end{array}$$

$$\begin{array}{r} 7.9 \\ \hline F1.5 \end{array}$$

$$\begin{array}{r} 14.8 \\ F.84 \\ \hline 31. \end{array}$$

Sta.	+	π	-	Grade
		998.66		
3+70				22.3
4				22.4
T.P.	10.27	931.18	7.75	920.91
+50				22.7
5				23.2
+50				23.9
6				24.6
T.P.	8.96	934.51	5.63	925.55
+50				
7				26.1
+14				26.1

4.

2

2.

3

X

6.3

$$\begin{array}{r} 124 \\ \text{F61} \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 8.2 \\ \text{F} \\ \hline 1.9 \end{array}$$

$$\begin{array}{r} 141 \\ \text{F28} \\ \hline 30.6 \end{array}$$

8.5

$$\begin{array}{r} 135 \\ \text{F50} \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ \text{F1.7} \\ \hline \end{array}$$

$$\begin{array}{r} 188 \\ \text{F103} \\ \hline 33.0 \end{array}$$

8.0

$$\begin{array}{r} 124 \\ \text{F44} \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 8.6 \\ \text{F0.6} \\ \hline \end{array}$$

$$\begin{array}{r} 184 \\ \text{F114} \\ \hline 33.0 \end{array}$$

7.3
9.3

$$\begin{array}{r} 88 \\ \text{D60.5} \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ \text{F0.1} \\ \hline \end{array}$$

$$\begin{array}{r} 13.3 \\ \text{F6.0} \\ \hline 27.0 \end{array}$$

6.6
8.6

$$\begin{array}{r} 44 \\ \text{D64.2} \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 6.6 \\ \text{F0.0} \\ \hline \end{array}$$

$$\begin{array}{r} 20 \\ \text{DC16} \\ \hline 26.2 \end{array}$$

8.9
10.9

$$\begin{array}{r} 18 \\ \text{DC9.1} \\ \hline 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ \text{DC46} \\ \hline 32.2 \end{array}$$

8.4
10.4

$$\begin{array}{r} 8 \\ \text{DC6.0} \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.4 \\ \text{F0.0} \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ \text{DC3.8} \\ \hline 30.6 \end{array}$$

8.4
10.4

$$\begin{array}{r} 8.3 \\ \text{DC2.1} \\ \hline 32.2 \end{array}$$

Sta.	+	-	Grade
------	---	---	-------

		934.61	
--	--	--------	--

7+50			26.7
------	--	--	------

8			26.3
---	--	--	------

+50			26.4
-----	--	--	------

T.P.	4.56	930.68	8.39	926.12
------	------	--------	------	--------

9			26.5
---	--	--	------

+30			26.6
-----	--	--	------

10			26.8
----	--	--	------

+70			27.2
-----	--	--	------

11			27.5
----	--	--	------

T.P.	13.46	940.13	4.01	926.67
------	-------	--------	------	--------

+30			27.9
-----	--	--	------

4.

8

84

4

8.3
10.3

4.1
DC 6.2
33.0

8.3
F.00

8.2
DC 2.1
27.2

8.2
10.2

4.6
DC 5.6
33.0

8.2
F.00

8.2
DC 2.3
27.6

8.1
10.1

6.8
DC 3.3
29.6

8.4
F.0.3

10.1
F.2.0
19.0

4.2
6.2

7.2
F.3.0
21.0

4.8
F.0.6

8.4
F.4.2
23.4

4.1

8.2
F.4.1
23.2

5.1
F.1.0

11.1
F.2.0
29.0

3.9

9.6
F.5.7
26.4

5.4
F.1.5

12.1
F.8.2
31.4

3.5

8.7
F.5.2
25.4

4.7
F.1.2

8.8
F.5.3
25.4

3.2

6.9
F.2.8
20.8

4.4
F.1.2

6.6
F.3.4
21.8

12.2
14.2

9.5
DC 4.7
32.4

13.2
F.1.0

11.0
DC 3.2
29.4

Sta.	+	π	-	Grade
------	---	-------	---	-------

940.13

11470

28.5

12

28.9

+35

29.8

+70

13

30.7

+43

+75

14

+42

LT.

E

RT.

5

$$\begin{array}{r} 11.6 \\ 13.6 \\ \hline 49 \\ 8.7 \\ \hline PC. 33.0 \end{array}$$

$$\begin{array}{r} 12.4 \\ \hline F.08 \end{array}$$

$$\begin{array}{r} 61 \\ \hline PC. 95 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.2 \\ 13.2 \end{array}$$

$$\begin{array}{r} 52 \\ \hline PC. 80 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 11.4 \\ \hline F.02 \end{array}$$

$$\begin{array}{r} 42 \\ \hline PC. 90 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 10.3 \\ 12.3 \end{array}$$

$$\begin{array}{r} 63 \\ \hline PC. 69 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 105 \\ \hline F.02 \end{array}$$

$$\begin{array}{r} 44 \\ \hline PC. 79 \\ \hline 33.0 \end{array}$$

X

$$\begin{array}{r} 94 \\ 11.4 \end{array}$$

$$\begin{array}{r} 11.3 \\ \hline PC. 01 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 94 \\ \hline \end{array}$$

$$\begin{array}{r} 73 \\ \hline PC. 41 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 84 \\ \hline 10.4 \end{array}$$

$$\begin{array}{r} 150 \\ \hline F. 66 \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 86 \\ \hline PC. 18 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 78 \\ 98 \end{array}$$

$$\begin{array}{r} 129 \\ \hline F. 11 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 89 \\ \hline PC. 09 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 73 \\ 9.3 \end{array}$$

$$\begin{array}{r} 103 \\ \hline F. 30 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 93 \\ \hline PC. 00 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 65 \\ \hline 8.5 \end{array}$$

$$\begin{array}{r} 61 \\ \hline PC. 24 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 106 \\ \hline F. 41 \\ \hline 23.2 \end{array}$$

Sta. + π - Grade.

14+75

15

+35

+66

16

+45

17

+24

+75

4.

2

6

5.7
7.7

x Δ

3.4
D.C. 4.3
31.6

5.1
7.1

4.8
D.C. 2.3
27.6

10.1
F. 5.0
25.0

10.2
12.2

13.6
F. 3.4
21.8

17.2
F. 7.0
29.0

9.1
11.1

12.2
F. 2.2
20.4

15.1
F. 5.6
26.2

8.6
10.6

8.7
D.C. 1.9
26.8

9.8
D.C. 0.8
24.6

6.8
8.8

5.4
D.C. 3.4
29.8

4.2
D.C. 4.6
32.2

5.4
7.4

2.4
D.C. 0.0
22.1

3.9
D.C. 3.5
30.0

12.9
14.9

14.9
D.C. 0.0
21.6

10.7
D.C. 4.2
31.4

12.00
14.00

8.6
9.6
5.4
33.0

2.4
D.C. 11.6
33.0

Sta.	+	-	Grade
------	---	---	-------

18			
----	--	--	--

B.M.			
------	--	--	--

			944.50
--	--	--	--------

+50			
-----	--	--	--

19			
----	--	--	--

+35			
-----	--	--	--

+70			
-----	--	--	--

20			
----	--	--	--

+65 50			
-----------	--	--	--

21			
----	--	--	--

+32			
-----	--	--	--

Lt.

E

Et. 7

11.4
13.4

5.7
7.7
D.C. 7.33

5.2
D.C. 8.2
33.0

Top of boat spike 18 + 84.66

11.2
13.2

7.3
5.9
D.C. 5.33

11.6
D.C. 1.6
26.2

12.4
14.4

9.9
D.C. 4.5
37.0

7.7
D.C. 6.7
33.0

13.7
15.7

9.1
6.6
D.C. 6.33

7.1
D.C. 8.6
33.0

10.9
12.9

1.8
11.9
D.C. 11.9
33.0

2.2
D.C. 10.7
33.0

12.5
14.5

3.7
10.8
D.C. 10.8
33.0

4.4
D.C. 10.1
33.0

14.9
16.9

11.1
9.8
D.C. 9.8
33.0

6.6
D.C. 10.3
33.0

8.6
10.6

5.4
D.C. 5.4
33.0

2.1
D.C. 8.5
33.0

10.3
12.3

6.7
5.6
D.C. 5.6
33.0

4.1
D.C. 8.1
33.0

Sta. + - - Grade.

21468

22

+50

23

+110

+50

± 124 2.85 524.15 919.30

24 19.0

+29 17.8

+59 16.6

+73 16.1

4.

E

8

4.3
6.3

5.3
DC 1.0
25.0

5.6
DC 0.7
24.4

1.8

10.2
F 4.4
23.8

6.8
F 1.1
17.2

2.3

9.6
F 7.3
29.6

10.7
F 8.4
31.8

4.7

10.8
F 6.7
27.4

12.7
F 8.0
31.0

6.9

16.5
F 9.6
33.0

13.3
F 6.4
27.8

3.7

14.3
F 11.1
33.0

4.0
F 0.8
16.6

4.4
6.4

15.6
F 11.2
33.0

4.1
C.O. 3

5.2
DC 1.2
25.4

5.6
7.6

13.0
F 7.4
29.8

5.4
C.O. 2

3.9
DC 3.7
30.4

6.1

X

5/2 + π - Grade.

92215

25

15.0

+50

13.0

T.P.

3.50

913.95

11.70

910.45

26

11.0

+26

10.0

+62

8.5

27

7.0

+59

5.1

T.P.

5.78

909.16

10.57

903.38

28

4.3

+37

4.5

Lt.

E

Rt. 9

7.2
9.2
$$\begin{array}{r} 95 \\ 123 \\ \hline 196 \end{array}$$

$$\begin{array}{r} 73 \\ \hline F.O. \end{array}$$

$$\begin{array}{r} 33 \\ DC.59 \\ \hline 33.0 \end{array}$$
5.2
11.2
$$\begin{array}{r} 114 \\ 122 \\ \hline 194 \end{array}$$

$$\begin{array}{r} 95 \\ \hline F.O.3 \end{array}$$

$$\begin{array}{r} 88 \\ DC.23 \\ \hline 27.6 \end{array}$$
2.9
4.9
$$\begin{array}{r} 42 \\ DC.07 \\ \hline 244 \end{array}$$

$$\begin{array}{r} 36 \\ \hline F.O.7 \end{array}$$

$$\begin{array}{r} 50 \\ F.27 \\ \hline 20.4 \end{array}$$

3.9

$$\begin{array}{r} 72 \\ F.33 \\ \hline 216 \end{array}$$

$$\begin{array}{r} 47 \\ \hline F.O.8 \end{array}$$

$$\begin{array}{r} 67 \\ F.28 \\ \hline 20.6 \end{array}$$
5.4
15
$$\begin{array}{r} 120 \\ F.66 \\ \hline 28.2 \end{array}$$

$$\begin{array}{r} 62 \\ \hline F.O.8 \end{array}$$

$$\begin{array}{r} 80 \\ F.36 \\ \hline 22.2 \end{array}$$
6.9
16
$$\begin{array}{r} 164 \\ F.95 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 79 \\ \hline F.I.0 \end{array}$$

$$\begin{array}{r} 140 \\ F.21 \\ \hline 29.2 \end{array}$$

8.8

$$\begin{array}{r} 181 \\ F.93 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 100 \\ \hline F.I.2 \end{array}$$

$$\begin{array}{r} 170 \\ F.82 \\ \hline 31.0 \end{array}$$

4.9

$$\begin{array}{r} 129 \\ F.80 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 59 \\ \hline F.I.0 \end{array}$$

$$\begin{array}{r} 125 \\ F.16 \\ \hline 30.2 \end{array}$$

5.2

$$\begin{array}{r} 110 \\ F.18 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 58 \\ \hline F.O.6 \end{array}$$

$$\begin{array}{r} 127 \\ F.25 \\ \hline 30.0 \end{array}$$

Sta. + π - Grade.

909.16

28+70

4.0

29

4.2

+35

4.6

+75

5.1

30

5.4

+62
50

31

06.6

+17

+24

LT.

Z

RT.

10

5.2

X

5.0

$$\begin{array}{r} 8.5 \\ F.35 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 5.1 \\ F.01 \\ \hline \end{array}$$

$$\begin{array}{r} 11.3 \\ F.63 \\ \hline 27.6 \end{array}$$

4.6

$$\begin{array}{r} 7.2 \\ F.26 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 4.4 \\ C.02 \\ \hline \end{array}$$

$$\begin{array}{r} 8.4 \\ F.38 \\ \hline 22.6 \end{array}$$

4.1
6.1

$$\begin{array}{r} 1.0 \\ DC.51 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.6 \\ C.05 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ DC.32 \\ \hline 29.4 \end{array}$$

3.8
5.4

$$\begin{array}{r} +1.3 \\ DC.71 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ C.05 \\ \hline \end{array}$$

$$\begin{array}{r} +1.2 \\ DC.70 \\ \hline 33.0 \end{array}$$

10.7
17.7

$$\begin{array}{r} 2.5 \\ DC.72 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ DC.43 \\ \hline 33.0 \end{array}$$

10.0
17.0

$$\begin{array}{r} 5.2 \\ DC.68 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 2.2 \\ DC.94 \\ \hline 33.0 \end{array}$$

X

$$\begin{array}{r} 9.8 \\ \hline 11.8 \end{array}$$

$$\begin{array}{r} 3.1 \\ DC.24 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 3.6 \\ DC.44 \\ \hline 33.0 \end{array}$$

Sta. + x - Grade

31+47

+56

32

+50

33

+38

+43

34

x08

+25

+08

24.

2

24. 11

9.4
11.4

9.3
DC $\frac{24}{27.}$

4.7
DC 6.7
33

X

7.8
9.8

8.7
DC 11.
25.2

5.1
DC 4.7
32.4

8.3
10.

8.8
DC 1.5
26.0

6.8
DC 3.4
29.8

8.5
10.5

8.7
DC 0.8
24.6

7.4
DC 3.1
29.2

8.6
10.6

10.2
DC 0.4
23.8

7.3
DC 3.3
29.6

X

8.7
10.7

9.9
DC $\frac{9.8}{24.6}$

X

8.9
10.9

4.4
DC 6.5
33.0

Sta. + K - Grade

34+50

35

+35

+50
~~+60~~

36

+35

+70

37

B.M.

891.88

+40

LT.

E

RT.

12

9.3
11.3

9.2
DC 2.1
27.2

D.C. $\frac{28}{8.5}$
33.0

10.6
17.6

Take Manned when
resetting T.P.
4.4
DC 4.2
33.0
D.C. 4.8
32.6

B.T.
12.6
19.0

X

6.4
8.4

6.7
DC 1.7
26.4

6.0
DC 2.4

8.6
10.6

9.7
DC 0.9
24.8

B.T. 19.0
2.2
C.3.4

OOT 33
Slate outy

10.4
17.4

12.1
DC 0.3
23.6

6.5
DC 5.9
30.0

9.9
2.9

3.9
P. 6.8
29.7

3.7
D.C. 2.2
23.4

5.3

11.3
P. 6.0
27.0

7.6
P. 2.3
19.6

Spike in R.D. $\pi 7\frac{1}{2}$ LT. 37+22

Sta.	+	π	-	Grade
------	---	-------	---	-------

37+57				
-------	--	--	--	--

+73				
-----	--	--	--	--

38				
----	--	--	--	--

+35				
-----	--	--	--	--

+64				
-----	--	--	--	--

	4.03	889.13		
--	------	--------	--	--

			885.10	
--	--	--	--------	--

39				
----	--	--	--	--

			88.0	
--	--	--	------	--

+50				
-----	--	--	--	--

			86.9	
--	--	--	------	--

+78				
-----	--	--	--	--

			86.3	
--	--	--	------	--

40				
----	--	--	--	--

			85.8	
--	--	--	------	--

Lt.

E

Rt. 13

$$\begin{array}{r} 82 \\ 102 \\ \hline \end{array}$$

$$\begin{array}{r} 102 \\ D.C.00 \\ \hline 224 \end{array}$$

$$\begin{array}{r} 82 \\ F.C.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 2.2 \\ 4.7 \\ \hline \end{array}$$

$$\begin{array}{r} 2.7 \\ F.O.5 \\ \hline \end{array}$$

$$\begin{array}{r} 3.6 \\ D.C.06 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 2.8 \\ 4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ D.C.14 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 3.4 \\ F.O.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.1 \\ D.C.07 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 3.3 \\ 5.9 \\ \hline \end{array}$$

$$\begin{array}{r} 4.4 \\ D.C.09 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 4.0 \\ F.O.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ D.C.00 \\ \hline 23 \end{array}$$

Sta. + K - Grade

889.13

40+20

85.4

+45

84.8

41

83.6

+25

83.1

+44

82.8

42

81.9

+25

81.6

+70

81.3

43

81.1

+40

81.0

Lt.

E

Rt.

14

3.7
5.7
$$\begin{array}{r} 91 \\ F.5.4 \\ 25.8 \end{array}$$

$$\begin{array}{r} 47 \\ F.1.0 \end{array}$$

$$\begin{array}{r} 57 \\ D.C.00 \\ 23.0 \end{array}$$
4.3
6.3
$$\begin{array}{r} 116 \\ F.7.3 \\ 29.6 \end{array}$$

$$\begin{array}{r} 56 \\ F.1.3 \end{array}$$

$$\begin{array}{r} 88 \\ F.4.5 \\ 24.0 \end{array}$$
5.5
7.5
$$\begin{array}{r} 129 \\ F.7.4 \\ 29.8 \end{array}$$

$$\begin{array}{r} 75 \\ F.2.0 \end{array}$$

$$\begin{array}{r} 118 \\ F.6.3 \\ 27.6 \end{array}$$

6.0

X

6.3

$$\begin{array}{r} 117 \\ F.5.4 \\ 25.8 \end{array}$$

$$\begin{array}{r} 87 \\ F.1.9 \end{array}$$

$$\begin{array}{r} 16.6 \\ F.10.3 \\ 33.0 \end{array}$$

7.2

$$\begin{array}{r} 96 \\ F.8.4 \\ 19.8 \end{array}$$

$$\begin{array}{r} 87 \\ F.1.5 \end{array}$$

$$\begin{array}{r} 172 \\ F.10.0 \\ 33.0 \end{array}$$
7.5
9.5
$$\begin{array}{r} 78 \\ D.C.1.7 \\ 26.4 \end{array}$$

$$\begin{array}{r} 87 \\ F.1.7 \end{array}$$

$$\begin{array}{r} 139 \\ F.6.4 \\ 27.8 \end{array}$$
7.8
9.8
$$\begin{array}{r} 33 \\ D.C.6.3 \\ 26.0 \end{array}$$

$$\begin{array}{r} 81 \\ F.0.3 \end{array}$$

$$\begin{array}{r} 93 \\ D.C.05 \\ 24.0 \end{array}$$
8.0
10.0
$$\begin{array}{r} 31 \\ D.C.6.4 \\ 26.0 \end{array}$$

$$\begin{array}{r} 80 \\ F.0.0 \end{array}$$

$$\begin{array}{r} 80 \\ D.C.2.0 \\ 27.0 \end{array}$$
8.1
10.1
$$\begin{array}{r} 39 \\ D.C.6.2 \\ 26.0 \end{array}$$

$$\begin{array}{r} 91 \\ F.0.0 \end{array}$$

$$\begin{array}{r} 42 \\ D.C.1.9 \\ 23.0 \end{array}$$

Sta.	+	Σ	-	Grade
T.P.	4.27	889.13	4.60	884.53
44		888.80		80.8

+50				80.7
-----	--	--	--	------

45				80.5
----	--	--	--	------

+50				80.3
-----	--	--	--	------

46				80.2
----	--	--	--	------

+62				80.0
-----	--	--	--	------

47				79.9
----	--	--	--	------

+50				79.8
+73				

Lt.

E

Rt.

15

Nail in T.P. Lt.

$$\begin{array}{r} 8.0 \\ 10.0 \end{array}$$

$$\begin{array}{r} 40 \\ DC. 6.0 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 47 \\ DC. 5.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.1 \\ 10.1 \end{array}$$

$$\begin{array}{r} 29 \\ DC. 7.7 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 49 \\ DC. 5.2 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.3 \\ 10.3 \end{array}$$

$$\begin{array}{r} 40 \\ DC. 6.3 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 47 \\ DC. 5.6 \\ \hline 33.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ 10.5 \end{array}$$

$$\begin{array}{r} 65 \\ DC. 4.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 82 \\ DC. 2.3 \\ \hline 27.6 \end{array}$$

$$\begin{array}{r} 8.6 \\ 10.6 \end{array}$$

$$\begin{array}{r} 106 \\ DC. 0.0 \\ \hline 21.8 \end{array}$$

$$\frac{98}{\hline}$$

$$\begin{array}{r} 106 \\ F. 2.0 \\ \hline 19.0 \end{array}$$

$$\begin{array}{r} 8.8 \\ 10.8 \end{array}$$

$$\begin{array}{r} 130 \\ F. 4.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 97 \\ F. 0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 88 \\ F. 5.9 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 8.9 \\ 10.9 \end{array}$$

$$\begin{array}{r} 137 \\ F. 4.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 104 \\ F. 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 158 \\ F. 6.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 9.0 \\ 11.0 \end{array}$$

$$\begin{array}{r} 137 \\ F. 4.2 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 108 \\ F. 1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 160 \\ F. 7.0 \\ \hline 29.0 \end{array}$$

Sta.	+	X	-	Grade.
		888.80		

48+ ⁰⁰ 40				79.6
----------------------	--	--	--	------

+60				79.4
-----	--	--	--	------

49				79.3
----	--	--	--	------

+50				79.1
-----	--	--	--	------

50				79.0
----	--	--	--	------

+50				79.0
-----	--	--	--	------

51				79.3
----	--	--	--	------

+50				79.9
-----	--	--	--	------

52				80.9
----	--	--	--	------

47.

8

24.

16

9.2

$$\begin{array}{r} 138 \\ F4.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 11.3 \\ F2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 12.6 \\ F8.4 \\ \hline 31.8 \end{array}$$

9.4

$$\begin{array}{r} 155 \\ F6.1 \\ \hline 27.2 \end{array}$$

$$\begin{array}{r} 11.4 \\ F2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 155 \\ F6.1 \\ \hline 27.2 \end{array}$$

9.5

$$\begin{array}{r} 153 \\ F5.8 \\ \hline 26.6 \end{array}$$

$$\begin{array}{r} 11.6 \\ F2.1 \\ \hline \end{array}$$

$$\begin{array}{r} 151 \\ F5.6 \\ \hline 26.2 \end{array}$$

9.7

$$\begin{array}{r} 143 \\ F4.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 11.7 \\ F2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 141 \\ F4.4 \\ \hline 23.8 \end{array}$$

9.8

$$\begin{array}{r} 139 \\ F4.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 11.4 \\ F1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 131 \\ F3.3 \\ \hline 21.6 \end{array}$$

9.8

$$\begin{array}{r} 132 \\ F3.4 \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 11.4 \\ F1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 12.6 \\ F2.8 \\ \hline 20.6 \end{array}$$

9.5

$$\begin{array}{r} 127 \\ F3.2 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 11.1 \\ F1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 11.9 \\ F2.4 \\ \hline 19.8 \end{array}$$

8.9
10.9

$$\begin{array}{r} 11.6 \\ F2.1 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 10.0 \\ F1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 9.5 \\ 00.14 \\ \hline 21.8 \end{array}$$

7.9
9.4

$$\begin{array}{r} 10.7 \\ F2.8 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 8.9 \\ F0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 8.9 \\ 0.01.0 \\ \hline 25.0 \end{array}$$

Sta.	+	π	-	Grade
		888.80		
52+50				82.1
53				83.7
+50				85.4
54				82.1
+50				
55				
+40				
56				
+58.5				

24.

2

24.

17

$$\begin{array}{r} 6.7 \\ 8.9 \end{array}$$

$$\begin{array}{r} 10.0 \\ F3.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 76 \\ F0.9 \end{array}$$

$$\begin{array}{r} 80 \\ DC.07 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ 7.7 \end{array}$$

$$\begin{array}{r} 89 \\ F3.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 61 \\ F1.0 \end{array}$$

$$\begin{array}{r} 71 \\ DC.00 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ 5.4 \end{array}$$

$$\begin{array}{r} 71 \\ F3.3 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 39 \\ F0.5 \end{array}$$

$$\begin{array}{r} 39 \\ DC.15 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 1.7 \\ 3.7 \end{array}$$

$$\begin{array}{r} 49 \\ F3.1 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 1.7 \\ F0.0 \end{array}$$

$$\begin{array}{r} 00 \\ DC.37 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 14.2 \\ 16.2 \end{array}$$

$$\begin{array}{r} 16.2 \\ DC.00 \\ \hline 27 \end{array}$$

$$\begin{array}{r} 12.6 \\ 14.6 \end{array}$$

$$\begin{array}{r} 14.6 \\ DC.00 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 11.0 \\ 13.0 \end{array}$$

$$\begin{array}{r} 13.0 \\ DC.00 \\ \hline 34.7 \end{array}$$

$$\begin{array}{r} 9.00 \\ 11.00 \end{array}$$

$$\begin{array}{r} 11.00 \\ DC.00 \\ \hline 46.0 \\ 93 \\ DC.00 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} 7.3 \\ 9.3 \end{array}$$

Sta. + π - Grade

57

+28

+45

+25.5

58

+40

59

+36

+41

4.

5

6.

18

9.1
11.1

11'
DC: 00/13.0

Sta.	+	-	Grade
B.M.	9.94	911.35	902.41

54+50			89.0
-------	--	--	------

55			90.7
----	--	--	------

+40			91.3
-----	--	--	------

56			94.2
----	--	--	------

+58.5			95.9
-------	--	--	------

57			97.5
----	--	--	------

Lt.

C

Rt.

12

X in top S.E. Cor. Pk. of Bridge

$$\begin{array}{r} 23.4 \\ 25.4 \end{array}$$

$$\begin{array}{r} 14.7 \\ \text{D.C. } 10.7 \\ \hline 39.1 \end{array}$$

$$\begin{array}{r} 21.7 \\ 23.7 \end{array}$$

$$\begin{array}{r} 4.6 \\ \text{D.C. } 19.1 \\ \hline 51.6 \end{array}$$

$$\begin{array}{r} 20.1 \\ 22.1 \end{array}$$

$$\begin{array}{r} 0.5 \\ \text{D.C. } 21.6 \\ \hline 55.4 \end{array}$$

$$\begin{array}{r} 18.7 \\ 20.7 \end{array}$$

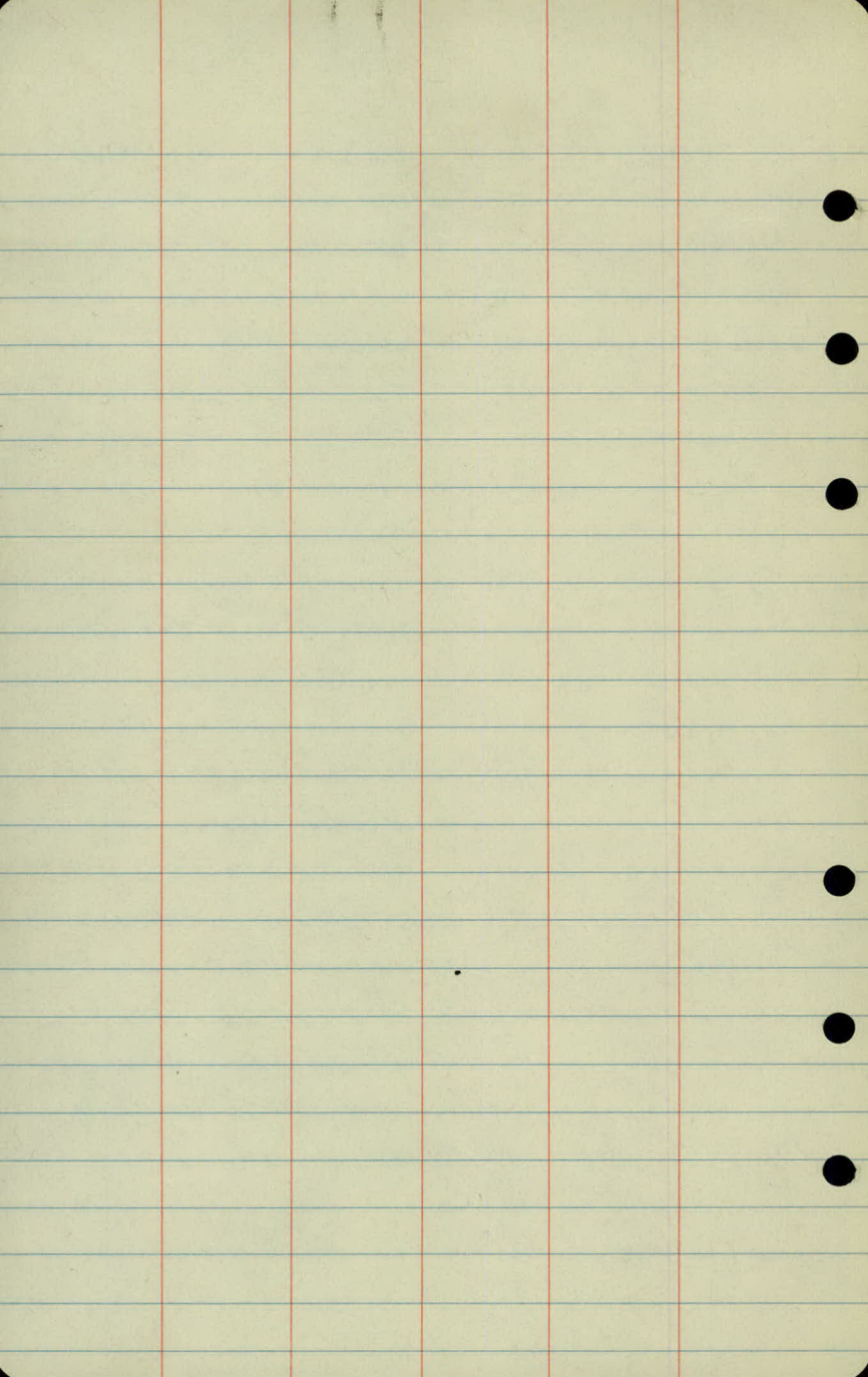
$$\begin{array}{r} 0.8 \\ \text{D.C. } 19.4 \\ \hline 57.1 \end{array}$$

$$\begin{array}{r} 16.5 \\ 18.5 \end{array}$$

$$\begin{array}{r} 0.4 \\ \text{D.C. } 18.1 \\ \hline 50.1 \end{array}$$

$$\begin{array}{r} 14.9 \\ 16.9 \end{array}$$

$$\begin{array}{r} 3.5 \\ \text{D.C. } 13.4 \\ \hline 43.1 \end{array}$$



FK
BW

May 15, 1974

1

Ditch 18 at
Co. Rd. "D"

Co. Rd. "D" Hazelwood to
White Bear Ave

Sta	+	-	Elev.
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± Co Rd D			921.0 [±]
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Culvert Under 694			911.2
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9.46
395

TBM	13.41	924.61	911.2
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Top Pipe N. side	6.65 3.95 10.60	914.01	911.5 _{inv}
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± "D"	3.87	920.74	
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Top Pipe S. side	10.14	914.97	912.0 _{inv}
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BM	1.91	925.17	1.35 923.26
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Top Pipe S End	10.68	914.49	912.0
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Top Pipe N End	11.05		
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S End	912.0	13.17	9.17 C 4.00
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		13.27	4.27 C-9.0
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±		13.37	4.27 C-9.1
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L	911.7	13.47	4.47 C-9.0
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	911.6	13.57	8.50 C-5.0
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May 13, 1974

2

I went to Maplewood Engineering Department and talked with William Cass, assistant engineer, as Maplewood is now the only city concerned in the drainage. Mr Cass stated a legal action was initiated S. End Culvert under 694

by the owners on the south to have the ditch cleaned by the State and City of White Bear Lake. This action would now include Maplewood. The owners wanted the Water level lowered to its old level. I so staked the new Top Hyd S.W. of Culvert

Culvert to the same elevation as the one that is in place.

JK

