

Boo K-14-Dr. 6

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

P.W.A. PLAN Survey

WHITE BEAR ROAD.

From Keller St. To White Bear Ave

Road Acc'l. No. 39

Date Filed 1933

File 146

Alignment

Rd 9C #39

33-39

Sta. Point A-Lt. A-Rt.

4+67.86 P.T. ✓	2° 17'
+50	2° 06' A-4° 34'
4	1° 36' D-2° R
3+53.75 P.I.	4° 34' T-114.22 ✓
+50	1° 06' L-228.33 ✓
3	0° 36' R-2864.93 ✓
+50	0° 06'
2+39.53 P.C. ✓	0° 00'

1+76.94 P.T. ✓	4° 39'
+50	3° 51' A-9° 18'
1	2° 21' D-6° R
0+99.65 P.I.	9° 18' T-77.71 ✓
+50	0° 51' L-155.0 ✓
0+21.94 P.C. ✓	0° 00' R-955.37 ✓

0+00

Spk. — 33.23 — 15" Oak
 — 64.50 — 8" Poplar

N 33° 59' E

G.R. Post — 14.22 —

G.R. Post — 14.55 —

N 24° 41' E

Spk — 60.32 — P.P.
 Iron Rd. Sq. — 53.45 —

Sta. Point A-Lt. A-Rt.

~~13+30.91~~

~~✓ 16°53'~~

~~A-33046 ✓~~

13

12°52'

~~D-26°L~~

12+68.5 P.I.

33°46'

T-67.46 ✓

+50

6°22'

L-129.87 ✓

12+01.04 P.C.

✓ 0°00'

~~R-222.27 ✓~~

See change in sign
for Bank Widen. P. 13

7+35.45 P.O.T.

7+34.9

7+25.40 P.T.

✓ 3°28'

7

3°05'

A-6°56'

+50

2°20'

D-3°L

4+10.0 P.I.

6°56'

T-115.71 ✓

6

1°35'

L-231.11 ✓

+50

0°50'

R-1910.08

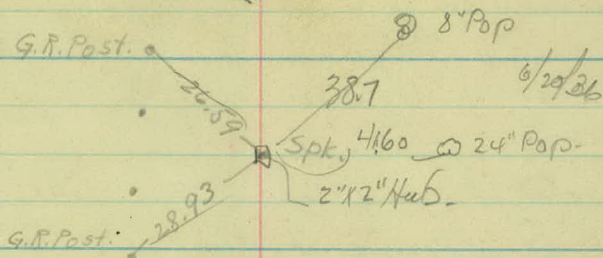
5

0°05'

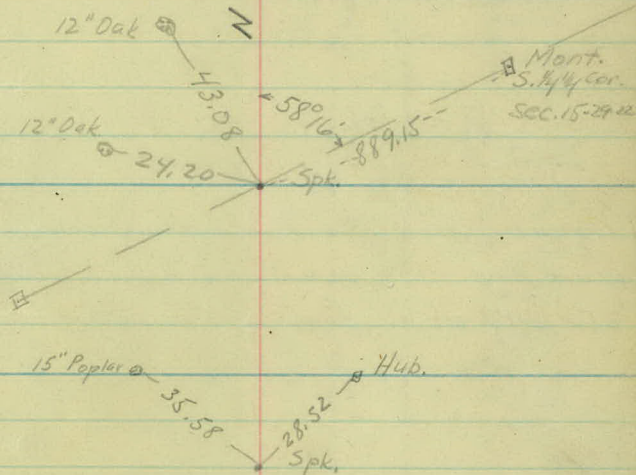
4+94.29 P.C.

✓ 0°00'

N 2-09 W



N 31°-37' E



N 38°-33' E

Sta. Point A-Lt. A-Rt.

22+50.54 P.T. ✓ 3° 04'

22 2° 49'

+50 2° 34'

21 2° 19'

+50 2° 04'

20 1° 49'

+50 1° 34'

19+44.15 P.I. 6° 08'

19 1° 19'

+50 1° 04'

18 0° 49'

+50 0° 34'

17 0° 19'

+50 0° 04'

16+37.21 P.C. ✓ 0° 00'

see change of Align P. 43

A-6° 08'

D-1° L

T-306.94 ✓

L-613.33 ✓

✓ R-5729.65 ✓

15+38.55 P.I. 1° 40'

N 9° 57' W

15" Stump

49.78

Spt.

38.00

near edge of mark

x Iron
F.D.

34.20 x

15" Oak

32.48

N 3° 49' W

15" Tw. Oak

34.13

Spt.

Pop.

25.46

70.36

OPop

15" Oak

58.03

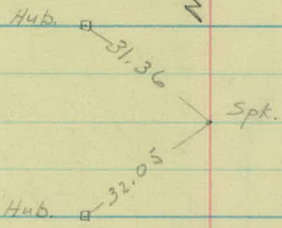
N 2° 09' W

Sta.	Point	$\Delta-L$	$\Delta-R$
43+13.91	P.T. ✓		4° 22'
43			4° 09'
+50			3° 24' $\Delta-8° 44'$
42			2° 39' $D-3° R$
41+68.65	P.I.		8° 44' $T-145.85$ ✓
+50			1° 54' $L-291.11$ ✓
41			1° 09' $R-1910.08$ ✓
+50			0° 24'
40+22.80	P.C. ✓		0° 00'

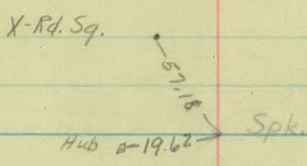
39+89.78	P.T. ✓		17° 55' $\Delta-35° 50'$
+50			13° 56' $D-20° R$
39+03.70	P.I.		35° 50' $T-93.09$ ✓
39			8° 56' $L-179.17$ ✓
+50			3° 56' $R-287.94$ ✓
38+10.61	P.C. ✓		0° 00'

34+61.65	P.I.		1° 04'
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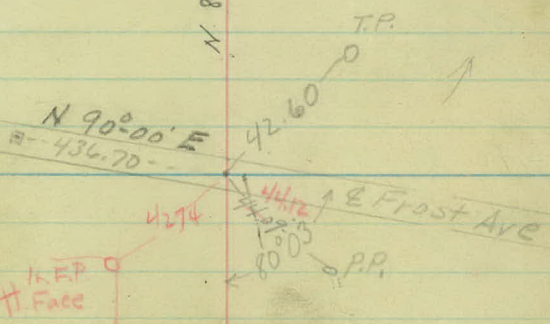
N. 35°-41' E



N. 26°-57' E



N. 8°-53' W



Sta. Point A-Lt. A-Rt.

72+65.28 P.T. ✓

3° 11'

+50

3° 04'

72

2° 41⁵'

+50

2° 19' A-6° 22'

71

1° 56⁵' D-1° 30' R

70+53.30 P.I.

6° 22' T-212.46 ✓

+50

1° 34' L-424.44 ✓

70

1° 11⁵' R-3819.83 ✓

+50

0° 49'

69

0° 26⁵'

+50

0° 04'

68+40.84 P.C. ✓

0° 00'

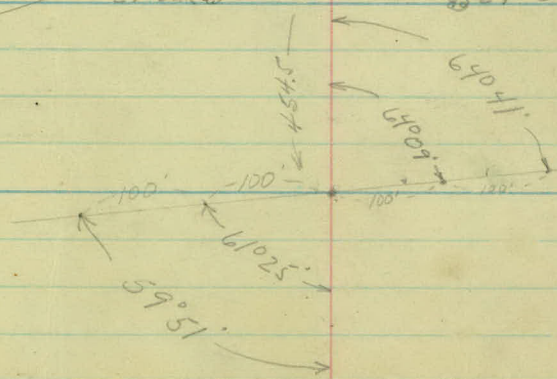
65+87.35 P.O.T. @ Co. Rd. "B"

52+14.0 P.O.T. @ Soo Line R.R.

N. 42° 03' E

Spt. 24.12 Hub
X-Rd. Sq. 59.27

54° 04' Mont.
740.35
39.65
24" Oak
76.67
E Co. Rd. "B" 2
24" Oak



Sta. Point A-Lt. A-Rt.

79+81.70 P.I.

0°36'

78+21.01 PT ✓

2°59'

78

2°46'

+50

2°16' A-5°58'

77

1°46' D-2°R

76+72.0 P.I.

5°58' T-149.32 ✓

+50

1°16' L-298.33 ✓

76

0°46' R-2864.93 ✓

+50

0°16'

75+22.48 P.C. ✓

0°00'

T.P. 0-31.38

N. 48° 37' E

61.55

218" Oak.

48° 52'

± W. B. Ave Pavement

3.6' I.P.I.

48° 13'

68.23'

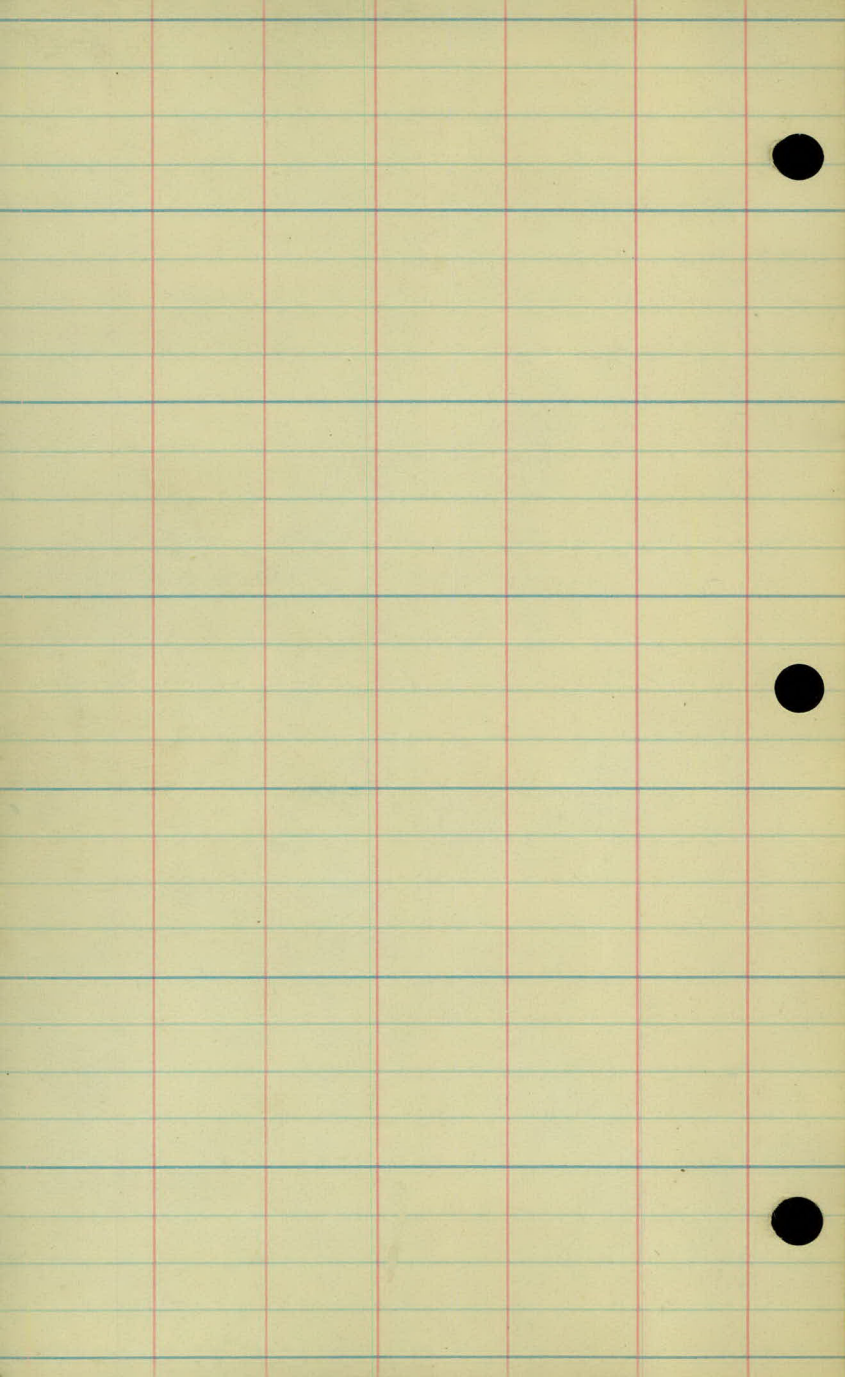
N 48° 01' E

T.P. 0

22.40

42.06

T.P.



Topog.

Rd. $\frac{9}{c}$ #39

5

4

3

2

1

0+00

+77-T.33'
 +66-T.33'
 +53-T.33'
 +48-T.27'
 +38-T.28'
 +30-T.31'
 +14-T.29'
 +09-T.25'

+95-T.18'

+61-T.22'
 +57-T.28'
 +40-T.29'

+10-Rd. Sq. 17'
 +00-End. Hedge 27'

+75-T.29'

+88-Hedge 24'
 +78-End Dr.

+51-End G.R. 13'

G.R. 14'

+22-T.P. 22'

G.R. 13'

G.R. 11'

0-13-Beg. G.R. 14'

Pasture

Cult.

Yard

Yard

+05-T.26'

+92-T.25'
 +82-Stu. 22'
 +80-T.18'
 +69-T.19'
 +55-T.22'
 +41-End Dr.

+68-P.P. 21'

+68-P.P. 20'

Cult.

Cult.

W.B. Rd.

Prosperity Ave

Keller St.

Hazelwood

+58-T.P. 26'
 +52-P.P. 15'
 +50-Rd. Sq. 16'
 +47-Rd. Sq. 19'

12

11

10

9

8

7

6

+91-T.37'

+50-G.R.7'

+05-Rd. Sq. 9'
F. 36-G.R. 8'{ +94-7'X4'X62.5' Stone
Masonry Arch Culv.

+79-T.25'

+23-T.35'

+11-T.37'

+03-T.40'

F. 28'

+99-Beg. G.R. 11'

+03-T.35'

F. 29'

+78-T.37'

F. 30'

F. 32'

+85-T.22'

+77-T.22'

+74-T.22'

+60-T.23'

+52-T.23'

+40-T.24'

+70-T.29'

+20-F. Cor. 33'

+12-T.27'

+00-T.28'

+79-T.36'

+62-T.36'

+59-T.33'

+56-T.26'

+42-T.32'

+34-T.22'

+29-T.27'

+10-T.33'

+50-G.R. 15'

+27-Rd. Sq. 18'

+02-T.29'

G.R. 14'

+94-T.30'

+80-T.28'

+78-T.34'

+70-T.23+30'

+49-T.35'

+23-T.30'

+16-T.22'

+13-Rd. Sq. 13'

+04-T.22'

F. 35' +25 End

+99-Beg. G.R. 12'

+95-T.26'

+74-T.29'

+69-T.30'

+49-T.22'

+34-T.22'

+26-T.31'

+21-T.29'

F. 35'

+90-T.19'

+87-T.27+31'

+60-T.30'

+44-T.21'

+09-T.21'

F. 35'

+99-T.29'

+85-T.28'

+78-T.25'

+72-T.23+31'

+61-T.31'

+55-T.31'

+48-Rd. Sq. 17'

+47-T.23'

+05-T.27'

+00-T.28'

+91-T.28'

+70-T.32'

+60-F. Cor. 36'

Pasture

Pasture

19

18

17

16

15

14

13

+34-T.21'
 +31-T.20'
 +16-T.36'
 +14-T.36'
 F.31'

F.36'

+08-T.24'
 F.31'

F.33'

F.30'

F.34'

+14-Stu.22'
 +03-Stu.21'
 F.32'
 +94-Stu.25'
 +87-Stu.23'
 +76-T.24'
 +70-Rd.59.18'
 +60-T.32'
 +54-T.31'

F.32'

+10-T.26'
 F.33

F.31'

+63-End G.R.11'

+72-T.26'
 +55-Beg. F.32'

G.R.12'-F.35'

G.R.14'

+14-T.22'
 +07-End G.R.7'

Pasture

Cult.

26

25

24

23

22

21

20

+86-T.31'

F.33'

F.32'

+33-12"X40'C.M.

F.32'

+38-2T.26'
+26-T.26'

F.33'

+77-Stu.26'

+28-T.22'

F.36'

+99-T.23'

+81-T.29'

F.34'

+91-T.26'

F.31'

+31-T.31'

F.32'

F.33'

F.33'

F.32'

+61-T.30'
+57-T.28'

+47-T.29'

F.32'

+65-T.28'

+48-T.26'

+27-2T.30'

F.32'

F.34'

Pasture

Cult.

11' 21'

33

32

31

30

29

28

27

+39-12"x40'C.M.

F.31'

F.32'

+86-F.E.

F.32'

F.32'

F.32'

F.33'

+41-T.31'

+10-T.29'
F.33'

19' 21'

F.34'

+40-T.29'

F.35'

+86-T.24'

F.35'

+64-Rd.Sq.19'

F.33'

F.33'

+12-F.Int.33'
+06-30"x61'C.M.
+06-F.Int.33'

+44-F.E.

F.32'

Pasture

Cult

25'

40

39

38

37

36

35

34

+54-Rd.Sg.15'

Hay Field

Old Trail

+42-T.30'

Hay Field

Hay Field

+31-Rd.Sg.17'

I.C.C. Pavement

+79-T.P.40'

+62-Frost Ave. Pave.

+41-Rd.Sg.21'

+33-F.C.31'

+29-Rd.Sg.17'

F.29

+26-P.P.28'

+26-Rd.Sg.16'

+21-F.C.38'

+11-T.36'

F.27'

47

46

45

44

43

42

41

Hay Field

Hay Field

#43-12" X 34' C.M.

17' 17'
C.M.

54

53

52

51

50

49

48

+00-End Hedge 32'

+92-End T. 35'

+53-Walk 32'

+96-Beg Hedge 32'

+85-1/2 Dr.

+66-End F. 28'

+53-Beg. Small T. 35'

F. 33'

+50-F. Int. 38'

+22-R.R. Battery Box 22'

+22-R.R. Signal Block 17'

+14-1/2 500 Line R.R.

+06-Beg. F. 36'

+89-End F. 27'

+43-F. Int. 32'

+40-F.E.

F. 32'

+92-Str. 29'

+85-Str. 29'

+77-Str. 29'

+45-Str. 26'

+63-T. 32'

+51-T. 31'

+39-T. 31'

+25-T. 31'

+21-T. 30'

F. 30'

+32-F.C. 26'

+33-Great Lakes Pipe Line 4'

+16-Air Vent 25'

+99-F.C. 24'

+97-End T. 26'

F. 24'

+33-Beg. Small T. 30'
F. 24'

+85-F. Int. 33'

+37-Beg. F. 25'

+19-End F. 31'

+82-F. Int. 46'

+42-R.R. Sq.

+27-F.E.

+12-T. 28'

F. 30' Str. 27'

+63-T. 35'

+37-T. 34'

+74-F.C. 38'

+38-2 Rd. Sq. 21'

Yard

Yard

Cult.

Pasture

Pasture

61

60

59

58

57

56

55

+67-End.

+35-T.31'

+27-Sta. 30'

+25-Rd. Sq. 16'

+10-T.30'

+96-T.31'

+63-T.P. 24'

+32-T.P. 24'

+13-F.E.
15" X 20" C.M. 24'

+97-T.P. 25'

+59-End T. 37'

+21-T.33'

+67-T.P. 25'

+94-F.E.

+85-2 Rd. Sq. 21'

+44-Beg. Small T. 35'

+39-T.P. 26'

+28-T.38'

+07-T.26'

+75-T.22'

+20-End.

Hay Field

Cult.

68

67

66

65

64

63

62

+28-Rd.Sg.18'

Cult.

+51-T.29'

+36-F.C.30'
+13-T.31'
F.31'

+85-T.35'

+43-F.C.31'
+34-T.32'
+21-T.32'
+08-T.31'

+68-18"X50'C.M.13'

+37-Rd.Sg.27'
+18-T.38'
+04-T.37'

+89-T.36'
+64-T.37'
+60-T.P.21'
+53-T.36'
+40-T.37'
+21-T.36'
+08-T.36'

+91-4 Dr.
12"X20'C.M.18'

+30-T.P.22'

+00-T.P.24'

Cult.

+03-18"X40'C.M.23'

+65-T.33'
+56-T.33'
+49-T.32'
+10-T.34'
+00-T.35'

+72-T.32'
+63-T.33'
+54-T.33'
+45-T.36'
+20-T.37'
+05-T.36'

+57-T.34'
+54-Rd.Sg.17'
+50-T.38'
+30-T.34'
+17-T.34'
+00-T.32'

+91-T.32'
+62-T.34'
+51-T.34'

Cult.

Yard

Rd.

Co.

"B"

75

74

73

72

71

70

69

+81-Rd. Sq. 19'

Cult.

Cult.

+94-Rd. Sq. 16'

80

79

78

77

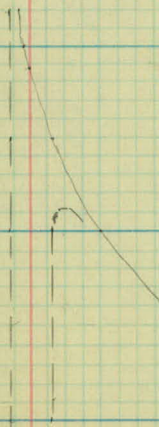
76

+88-Edge Pavement E

+64-G.P. 28'

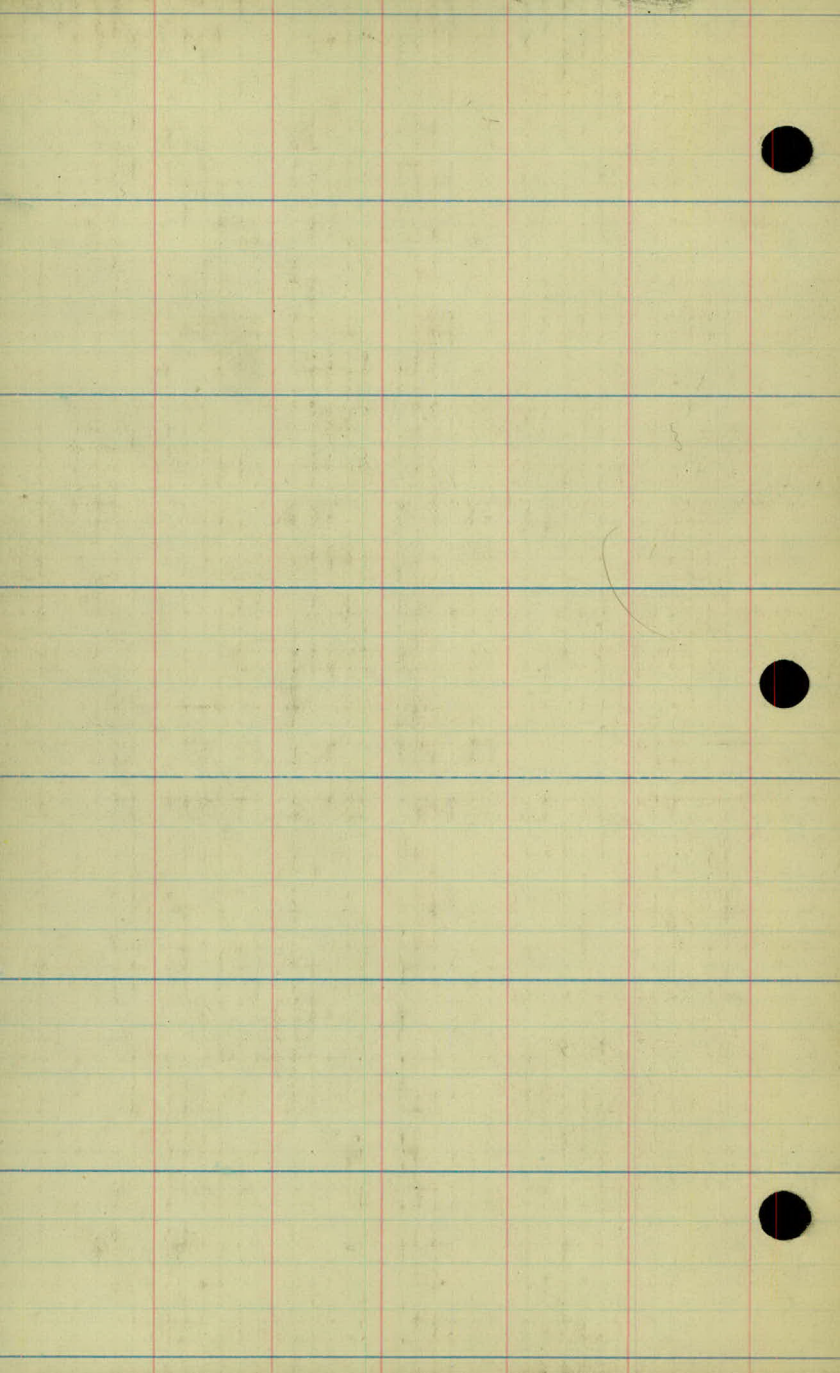
+58-2 T.P. 27' & 34'

+54-Rd. Sq. 15'



+84-Rd. Sq. 21'

+58-T. P. 36'



X-Sections

Rd. $\frac{a}{c}$ #39

B.M. #1 4.19 933.52 ✓ 929.33

0-100 30.9

0-50 30.9

0-30 4 Keller St. Lt. 31.0

0-11 31.1

0+00 31.1

+25 30.6

+60 29.0

1 27.8

+50 27.1

2 26.1

+55 25.3

+67 25.3

+84 25.2

T.P. 5.46 933.22 ✓ 5.76 927.76

Spk. in 16" Dak-S.E. Cor. N.B.R. + Hazelwood Ave

2.6

2.6

$\frac{8.4}{50}$	$\frac{4.6}{20}$	$\frac{2.6}{7}$	2.5	$\frac{3.4}{11}$	$\frac{3.8}{13}$	$\frac{5.2}{15}$	$\frac{5.6}{34}$	$\frac{5.0}{50}$
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$\frac{10.4}{50}$	$\frac{9.0}{30}$	$\frac{6.7}{19}$	$\frac{3.0}{13}$	2.4	$\frac{3.4}{14}$	$\frac{4.8}{17}$	$\frac{5.7}{25}$	$\frac{5.0}{50}$
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$\frac{10.4}{50}$	$\frac{8.4}{22}$	$\frac{2.8}{11}$	2.4	$\frac{3.0}{20}$	$\frac{4.6}{25}$	$\frac{5.4}{38}$	$\frac{4.8}{50}$
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$\frac{10.7}{50}$	$\frac{10.1}{35}$	$\frac{7.4}{19}$	$\frac{3.7}{13}$	2.9	$\frac{2.7}{10}$	$\frac{2.0}{21}$	$\frac{6.9}{25}$	$\frac{2.2}{40}$	$\frac{4.1}{48}$	$\frac{4.1}{55}$
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$\frac{11.3}{50}$	$\frac{11.0}{27}$	$\frac{9.1}{23}$	$\frac{7.7}{17}$	$\frac{5.5}{14}$	$\frac{4.9}{11}$	4.5	$\frac{5.0}{11}$	$\frac{6.3}{14}$	$\frac{6.0}{22}$	$\frac{4.6}{25}$	$\frac{3.8}{28}$	$\frac{3.2}{30}$	$\frac{1.4}{50}$
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$\frac{12.0}{50}$	$\frac{11.0}{32}$	$\frac{11.3}{24}$	$\frac{9.5}{22}$	$\frac{9.0}{18}$	$\frac{6.5}{13}$	$\frac{6.0}{10}$	5.7	$\frac{6.0}{10}$	$\frac{6.2}{14}$	$\frac{7.2}{14}$	$\frac{7.2}{25}$	$\frac{3.6}{28}$	$\frac{2.6}{31}$	$\frac{3.4}{32}$	$\frac{2.7}{50}$
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$\frac{11.2}{50}$	$\frac{10.2}{29}$	$\frac{10.2}{23}$	$\frac{7.2}{16}$	$\frac{4.6}{10}$	6.4	$\frac{6.7}{10}$	$\frac{7.1}{13}$	$\frac{8.1}{14}$	$\frac{7.4}{27}$	$\frac{4.6}{30}$	$\frac{3.2}{33}$	$\frac{3.0}{50}$
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$\frac{11.5}{50}$	$\frac{11.5}{25}$	$\frac{11.0}{21}$	$\frac{8.2}{17}$	$\frac{7.5}{11}$	7.4	$\frac{7.8}{10}$	$\frac{6.2}{14}$	$\frac{9.0}{21}$	$\frac{8.2}{25}$	$\frac{4.5}{29}$	$\frac{3.3}{33}$	$\frac{2.3}{50}$
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$\frac{11.6}{50}$	$\frac{11.2}{33}$	$\frac{11.2}{18}$	$\frac{8.8}{14}$	$\frac{8.2}{10}$	8.2	$\frac{8.6}{10}$	$\frac{9.6}{14}$	$\frac{9.2}{22}$	$\frac{7.2}{24}$	$\frac{5.0}{29}$	$\frac{4.0}{33}$	$\frac{3.0}{50}$
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$\frac{7.0}{50}$	$\frac{8.2}{21}$	$\frac{8.2}{9}$	8.2	$\frac{8.7}{10}$	$\frac{9.0}{12}$	$\frac{9.6}{15}$	$\frac{9.2}{24}$	$\frac{8.2}{27}$	$\frac{5.8}{29}$	$\frac{4.8}{32}$	$\frac{3.2}{50}$
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$\frac{7.5}{50}$	$\frac{7.8}{31}$	$\frac{8.2}{10}$	8.3	$\frac{8.6}{9}$	$\frac{8.8}{13}$	$\frac{9.5}{15}$	$\frac{9.8}{24}$	$\frac{8.6}{27}$	$\frac{6.2}{30}$	$\frac{4.7}{34}$	$\frac{3.7}{50}$
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933.22

2+90

25.2

3

25.2

+50

25.6

+90

25.9

4

25.9

+12

26.0

+32

26.0

+70

25.9

5

25.6

T.P.

11.98

942.34

2.86

930.36

4+12

26.0

+32

26.0

+70

25.9

5

25.6

$$\frac{5.0}{50} \quad \frac{5.5}{24} \quad \frac{7.7}{19} \quad \frac{8.0}{10} \quad 8.0 \quad \frac{8.3}{9} \quad \frac{8.5}{11} \quad \frac{8.6}{13} \quad \frac{9.5}{16} \quad \frac{9.6}{22} \quad \frac{8.6}{27} \quad \frac{6.0}{29} \quad \frac{4.6}{34} \quad \frac{3.4}{50}$$

$$\frac{4.9}{50} \quad \frac{5.5}{24} \quad \frac{7.8}{21} \quad \frac{8.1}{10} \quad 8.0 \quad \frac{8.2}{9} \quad \frac{8.5}{12} \quad \frac{9.3}{16} \quad \frac{8.8}{27} \quad \frac{6.5}{29} \quad \frac{5.5}{34} \quad \frac{4.0}{50}$$

$$\frac{4.4}{50} \quad \frac{5.0}{25} \quad \frac{7.8}{20} \quad \frac{8.0}{10} \quad 7.6 \quad \frac{7.8}{9} \quad \frac{8.0}{20} \quad \frac{6.6}{22} \quad \frac{6.2}{39} \quad \frac{5.0}{45} \quad H_0$$

$$\frac{4.1}{50} \quad \frac{4.6}{26} \quad \frac{7.5}{21} \quad \frac{7.6}{10} \quad 7.3 \quad \frac{7.5}{10} \quad \frac{8.0}{11} \quad \frac{8.1}{16} \quad \frac{7.0}{19} \quad \frac{4.8}{32} \quad \frac{1.8}{50}$$

$$\frac{1.5}{50} \quad \frac{1.8}{33} \quad \frac{4.6}{29} \quad \frac{4.8}{26} \quad \frac{7.6}{21} \quad \frac{7.6}{14} \quad 7.3 \quad \frac{7.5}{10} \quad \frac{7.8}{11} \quad \frac{8.3}{15} \quad \frac{7.0}{17} \quad \frac{4.7}{29} \quad \frac{1.0}{50}$$

$$\frac{7.5}{25} \quad \frac{8.5}{16} \quad \frac{8.1}{14} \quad \frac{7.5}{11} \quad 7.2 \quad \frac{7.5}{10} \quad \frac{7.8}{11} \quad \frac{8.2}{15} \quad \frac{7.0}{17} \quad \frac{6.2}{19} \quad \frac{3.7}{31} \quad \frac{0.4}{50}$$

$$\frac{4.4}{29} \quad \frac{6.6}{25} \quad \frac{9.5}{18} \quad \frac{9.5}{15} \quad \frac{8.2}{14} \quad \frac{7.7}{12} \quad 7.2 \quad \frac{7.6}{19} \quad \frac{7.8}{11} \quad \frac{8.3}{15} \quad \frac{7.3}{16} \quad \frac{3.8}{32} \quad \frac{0.4}{50}$$

$$\frac{4.0}{21} \quad \frac{8.5}{16} \quad \frac{8.0}{13} \quad 7.3 \quad \frac{7.8}{10} \quad \frac{8.4}{12} \quad \frac{8.6}{15} \quad \frac{9.3}{18} \quad \frac{9.0}{20} \quad \frac{8.5}{21} \quad \frac{8.0}{26} \quad \frac{4.6}{50}$$

$$\frac{5.4}{20} \quad \frac{8.4}{16} \quad 7.6 \quad \frac{8.1}{10} \quad \frac{8.4}{12} \quad \frac{9.0}{20} \quad \frac{9.5}{23} \quad \frac{9.6}{28} \quad \frac{7.5}{50}$$

$$\frac{7.8}{50} \quad \frac{8.2}{41} \quad 16.3$$

$$\frac{7.8}{50} \quad \frac{9.7}{41} \quad \frac{12.0}{33} \quad 16.3$$

$$\frac{7.0}{50} \quad \frac{7.5}{39} \quad \frac{8.0}{36} \quad \frac{8.5}{31} \quad \frac{10.2}{25} \quad 16.4$$

$$\frac{6.1}{50} \quad \frac{6.8}{33} \quad \frac{7.8}{27} \quad 16.7$$

942.34

5+50

25.0

T.P.

6.78

945.67

3.45

938.89

6

24.1

+50

23.4

T.P.

2.96

941.88

6.75

938.92

+93

22.5

7

22.4

+50

21.2

T.P.

1.40

930.06

13.22

928.66

5+50

25.0

6

24.1

+50

23.4

+93

22.5

7

22.4

+50

21.2

T.P.

5.50

925.19

10.37

919.69

8

19.6

$$\frac{3.0}{50} \quad \frac{4.0}{37} \quad \frac{5.8}{31} \quad \frac{11.7}{24} \quad 17.3$$

$$\frac{4.0}{50} \quad \frac{5.4}{39} \quad \frac{6.4}{37} \quad 21.6$$

$$\frac{4.0}{50} \quad \frac{7.3}{34} \quad 22.3$$

$$\frac{1.8}{50} \quad \frac{5.6}{34} \quad 19.4$$

$$\frac{2.0}{50} \quad \frac{7.0}{29} \quad 19.5$$

$$\frac{7.0}{50} \quad \frac{10.5}{34} \quad \frac{12.7}{25} \quad 20.7$$

$$\frac{4.6}{18} \quad \frac{5.7}{15} \quad 5.1 \quad \frac{6.0}{12} \quad \frac{6.3}{13} \quad \frac{6.5}{17} \quad \frac{5.6}{19} \quad \frac{5.5}{22} \quad \frac{2.8}{29} \quad \frac{8.7}{34} \quad \frac{8.6}{50}$$

$$\frac{1.4}{24} \quad \frac{6.4}{18} \quad \frac{7.0}{15} \quad \frac{6.0}{8} \quad 6.0 \quad \frac{6.5}{11} \quad \frac{6.4}{17} \quad \frac{5.5}{24} \quad \frac{10.1}{33} \quad \frac{10.8}{37} \quad \frac{11.7}{39} \quad \frac{12.7}{40} \quad \frac{13.8}{50}$$

$$\frac{1.2}{23} \quad \frac{7.8}{15} \quad \frac{7.1}{10} \quad 6.7 \quad \frac{7.1}{10} \quad \frac{7.5}{13} \quad \frac{7.7}{18} \quad \frac{7.1}{22} \quad \frac{13.3}{32} \quad \frac{15.8}{40}$$

$$\frac{1.4}{26} \quad \frac{6.6}{19} \quad \frac{8.2}{15} \quad \frac{7.7}{9} \quad 7.6 \quad \frac{8.1}{11} \quad \frac{9.0}{19} \quad \frac{9.4}{24} \quad \frac{13.8}{27}$$

$$\frac{3.5}{22} \quad \frac{7.0}{18} \quad \frac{8.2}{14} \quad \frac{8.0}{10} \quad 7.7 \quad \frac{8.2}{11} \quad \frac{8.5}{12} \quad \frac{9.0}{19} \quad \frac{10.0}{22} \quad \frac{13.8}{27}$$

$$\frac{9.0}{16} \quad \frac{9.6}{13} \quad \frac{9.2}{10} \quad 8.9 \quad \frac{9.4}{12} \quad \frac{9.7}{13} \quad \frac{10.8}{18} \quad \frac{13.8}{24}$$

$$\frac{+0.8}{50} \quad \frac{1.4}{29} \quad \frac{6.8}{20} \quad \frac{7.0}{15} \quad \frac{5.7}{9} \quad 5.6 \quad \frac{6.1}{11} \quad \frac{6.5}{13} \quad \frac{7.3}{16} \quad \frac{12.3}{23}$$

925.19

8+50

18.4

9

17.4

+50

16.5

10

15.9

+33

15.7

+75

15.4

B.M. #2

3.92

921.27

921.27

11

15.2

T.P.

1.21

913.35

13.05

912.14

6+50

23.4

+93

22.5

7

22.4

+50

21.2

8

19.6

+50

18.4

T.P.

4.53

910.88

7.00

906.35

$$\begin{array}{r} 3.0 \ 4.4 \ 5.2 \ 8.2 \ 8.2 \ 7.2 \ 7.3 \ 8.2 \ 13.7 \\ 50 \ 31 \ 29 \ 24 \ 19 \ 11 \ 6.8 \ 11 \ 14 \ 23 \end{array}$$

$$\begin{array}{r} 4.0 \ 5.0 \ 5.3 \ 8.7 \ 9.1 \ 8.5 \ 8.2 \ 8.4 \ 9.1 \ 12.4 \\ 50 \ 42 \ 28 \ 24 \ 21 \ 17 \ 13 \ 7.8 \ 10 \ 13 \ 19 \end{array}$$

$$\begin{array}{r} 4.6 \ 7.2 \ 8.8 \ 9.0 \ 10.8 \ 10.8 \ 9.7 \ 9.0 \ 9.7 \ 12.4 \\ 50 \ 34 \ 32 \ 28 \ 24 \ 17 \ 15 \ 10 \ 8.7 \ 12 \ 16 \end{array}$$

$$\begin{array}{r} 5.6 \ 9.6 \ 10.0 \ 11.2 \ 11.4 \ 10.2 \ 9.8 \ 10.1 \ 13.0 \\ 50 \ 31 \ 28 \ 24 \ 19 \ 15 \ 11 \ 9.3 \ 12 \ 17 \end{array}$$

$$\begin{array}{r} 4.0 \ 6.5 \ 7.1 \ 12.0 \ 12.2 \ 10.5 \ 10.0 \ 9.8 \ 10.2 \ 12.0 \\ 50 \ 31 \ 27 \ 22 \ 18 \ 14 \ 11 \ 9.5 \ 8 \ 12 \ 16 \end{array}$$

$$\begin{array}{r} 4.0 \ 4.5 \ 8.0 \ 10.7 \ 11.0 \ 11.8 \ 12.2 \ 10.4 \ 10.0 \ 10.4 \ 10.0 \ 10.6 \ 12.4 \\ 50 \ 44 \ 38 \ 33 \ 29 \ 27 \ 22 \ 18 \ 15 \ 13 \ 9.8 \ 10 \ 17 \ 23 \end{array}$$

Spk. in 18" Dak 60' Lt. 10+15

$$\begin{array}{r} 2.0 \ 2.3 \ 8.0 \ 12.7 \ 13.6 \ 12.6 \ 10.0 \ 10.0 \ 10.5 \ 10.2 \ 10.2 \ 10.7 \ 13.5 \\ 49 \ 40 \ 32 \ 26 \ 22 \ 18 \ 14 \ 13 \ 10 \ 10.0 \ 10 \ 14 \ 20 \end{array}$$

$$\begin{array}{r} 1.5 \ 2.5 \\ +10.0 \ 42 \ 50 \end{array}$$

$$\begin{array}{r} 5.6 \ 6.8 \\ +9.1 \ 44 \ 50 \end{array}$$

$$\begin{array}{r} 7.2 \\ +9.0 \ 50 \end{array}$$

$$\begin{array}{r} 3.5 \ 8.5 \\ +7.8 \ 35 \ 50 \end{array}$$

$$\begin{array}{r} 1.0 \ 8.0 \\ +6.2 \ 26 \ 50 \end{array}$$

$$\begin{array}{r} 3.2 \ 8.5 \\ +5.0 \ 27 \ 50 \end{array}$$

910.88

9

17.4

+50

16.5

10

15.9

+33

15.7

+75

15.4

11

15.2

+50

14.7

+70

14.6

12

14.5

T.P.

7.28

916.69

1.47

909.41

11+50

14.7

+70

14.6

12

14.5

+22

14.6

$$+6.5 \quad \frac{3.0}{35} \quad \frac{5.5}{50}$$

$$+5.6 \quad \frac{0.0}{19} \quad \frac{4.5}{35} \quad \frac{7.5}{50}$$

$$+5.0 \quad \frac{2.1}{28} \quad \frac{3.3}{35} \quad \frac{6.5}{50}$$

$$+4.8 \quad \frac{0.6}{27} \quad \frac{2.2}{26} \quad \frac{4.8}{50}$$

$$+4.5 \quad \frac{0.0}{35} \quad \frac{4.0}{50}$$

$$+4.3 \quad \frac{2.0}{31} \quad \frac{3.0}{37} \quad \frac{6.0}{50}$$

$$+3.8 \quad \frac{3.5}{22} \quad \frac{10.5}{31} \quad \frac{13.0}{42} \quad \frac{13.5}{50}$$

$$+3.7 \quad \frac{11.0}{29} \quad \frac{13.4}{38} \quad \frac{14.2}{46} \quad \frac{13.5}{50}$$

$$+3.6 \quad \frac{3.5}{29} \quad \frac{4.8}{35} \quad \frac{11.5}{39} \quad \frac{11.5}{43} \quad \frac{9.0}{50}$$

$$\frac{+1.0}{50} \quad \frac{+0.8}{48} \quad \frac{+1.2}{47} \quad \frac{+6.0}{39} \quad \frac{+10.0}{34} \quad \frac{+10.5}{27} \quad \frac{+9.0}{24} \quad \frac{+4.4}{19} \quad \frac{+2.6}{12} \quad \frac{+2.1}{8} \quad \frac{+2.4}{20} \quad \frac{+3.6}{12} \quad \frac{+14}{14}$$

$$\frac{+6.0}{50} \quad \frac{+13.0}{37} \quad \frac{+13.5}{28} \quad \frac{+3.0}{13} \quad \frac{+2.3}{8} \quad \frac{+2.1}{2.1} \quad \frac{+2.2}{10} \quad \frac{+3.2}{15} \quad \frac{+4.2}{17}$$

$$\frac{+18.8}{50} \quad \frac{+20.2}{39} \quad \frac{+14.8}{27} \quad \frac{+3.2}{9} \quad \frac{+2.4}{7} \quad \frac{+2.2}{2.2} \quad \frac{+2.8}{12} \quad \frac{+4.4}{18} \quad \frac{+23}{23}$$

$$\frac{+21.7}{50} \quad \frac{+21.0}{33} \quad \frac{+16.7}{25} \quad \frac{+3.4}{9} \quad \frac{+2.4}{6} \quad \frac{+2.1}{2.1} \quad \frac{+2.0}{11} \quad \frac{+2.6}{19} \quad \frac{+5.1}{25} \quad \frac{+6.0}{32} \quad \frac{+11.7}{37} \quad \frac{+12.2}{44} \quad \frac{+9.8}{50}$$

916.69

12+50

14.8

13

14.8

T.P. 3.41 909.23 10.87 905.82

+25

14.8

+50

14.8

+80

14.9

14

15.0

+50

15.3

15

15.6

T.P. 11.06 919.73 0.56 908.67

+50

15.9

16

16.2

T.P. 13.64 930.91 2.46 917.27

13+25

14.8

+50

14.8

+80

14.9

$$\frac{21.0}{50} \frac{19.8}{55} \frac{18.7}{72} \frac{18.0}{28} \frac{2.6}{9} \frac{2.1}{7} \quad 1.9 \quad \frac{1.9}{12} \frac{2.5}{14} \frac{5.8}{25} \frac{5.6}{41} \frac{2.0}{50}$$

$$\frac{21.0}{50} \frac{17.4}{38} \frac{2.4}{15} \frac{2.0}{11} \quad 1.9 \quad \frac{2.0}{7} \frac{4.6}{12} \frac{4.4}{23} \frac{0.0}{38}$$

$$\frac{16.2}{63} \frac{16.5}{56} \frac{13.8}{50} \frac{3.5}{31} + 5.6$$

$$\frac{16.5}{61} \frac{15.2}{55} \frac{9.4}{45} \frac{5.2}{35} + 5.6$$

$$\frac{14.4}{59} \frac{12.8}{52} \frac{8.2}{43} \frac{4.0}{33} + 5.7$$

$$\frac{14.5}{64} \frac{10.3}{50} \frac{4.0}{32} + 5.8$$

$$\frac{7.8}{50} \frac{2.6}{30} + 6.1$$

$$\frac{5.4}{50} \frac{0.0}{27} + 6.4$$

$$\frac{12.7}{50} \frac{6.8}{21} \frac{5.1}{16} \frac{4.1}{9} \quad 3.8 \quad \frac{4.0}{10} \frac{4.0}{16} \frac{3.3}{21}$$

$$\frac{11.0}{50} \frac{9.0}{31} \frac{6.4}{17} \frac{4.6}{13} \frac{3.8}{10} \quad 3.5 \quad \frac{3.7}{10} \frac{3.8}{15} \frac{4.2}{20} \frac{3.6}{28}$$

$$16.1 \quad \frac{14.2}{25} \frac{4.0}{36} \frac{2.0}{45} \frac{1.3}{50}$$

$$16.1 \quad \frac{8.5}{32} \frac{6.0}{32} \frac{3.0}{43} \frac{2.0}{50}$$

$$16.0 \quad \frac{6.2}{43} \frac{3.6}{43} \frac{2.5}{50}$$

930.91

14 15.0

+50 15.3

15 15.6

T.P. 3.50 920.77 13.44 917.27

13+25 14.8

+50 14.8

+80 14.9

14 15.0

+50 15.3

15 15.6

T.P. 9.59 926.59 3.77 917.00

+50 15.9

16 16.2

+50 16.9

17 17.2

$$15.9 \quad \frac{7.6}{39} \quad \frac{4.6}{39} \quad \frac{2.8}{50}$$

$$15.6 \quad \frac{8.8}{31} \quad \frac{6.6}{36} \quad \frac{4.8}{50}$$

$$15.3 \quad \frac{11.4}{29} \quad \frac{9.0}{30} \quad \frac{7.4}{34} \quad \frac{5.2}{50}$$

$$\frac{7.0}{17} \quad \frac{6.2}{12} \quad 6.0 \quad \frac{6.3}{2} \quad \frac{7.0}{19} \quad \frac{7.8}{12} \quad \frac{7.5}{20}$$

$$\frac{6.8}{16} \quad \frac{6.2}{11} \quad 6.0 \quad \frac{6.2}{7} \quad \frac{6.2}{14} \quad \frac{4.4}{23}$$

$$\frac{6.8}{15} \quad \frac{6.2}{11} \quad 5.9 \quad \frac{6.2}{9} \quad \frac{5.8}{12} \quad \frac{3.7}{31}$$

$$\frac{6.6}{13} \quad \frac{6.0}{19} \quad 5.8 \quad \frac{6.0}{9} \quad \frac{6.2}{13} \quad \frac{4.4}{26} \quad \frac{2.0}{31}$$

$$\frac{6.4}{12} \quad \frac{5.8}{10} \quad 5.5 \quad \frac{5.7}{10} \quad \frac{5.6}{15} \quad \frac{4.8}{21}$$

$$\frac{6.5}{14} \quad \frac{5.5}{10} \quad 5.2 \quad \frac{5.5}{9} \quad \frac{5.5}{15} \quad \frac{4.4}{20} \quad \frac{1.8}{27}$$

$$10.7 \quad \frac{3.8}{30} \quad \frac{2.0}{34} \quad \frac{0.5}{50}$$

$$10.4 \quad \frac{7.7}{31} \quad \frac{6.0}{28} \quad \frac{4.1}{50}$$

$$\frac{14.2}{50} \quad \frac{13.7}{30} \quad \frac{13.0}{17} \quad \frac{10.5}{11} \quad 9.7 \quad \frac{10.0}{12} \quad \frac{10.3}{14} \quad \frac{10.8}{19} \quad \frac{10.4}{30} \quad \frac{8.8}{32} \quad \frac{7.3}{35} \quad \frac{6.0}{50}$$

$$\frac{11.8}{50} \quad \frac{12.0}{30} \quad \frac{12.0}{17} \quad \frac{10.0}{11} \quad 9.7 \quad 9.4 \quad \frac{9.6}{11} \quad \frac{10.0}{15} \quad \frac{10.4}{19} \quad \frac{10.4}{29} \quad \frac{8.4}{32} \quad \frac{6.7}{35} \quad \frac{5.6}{50}$$

926.59

17+50

17.5

T.P. 10.66 927.19[✓] 10.06 916.53

+72

17.8

18

18.2

+50

18.7

T.P. 11.67 930.90[✓] 7.96 919.23

19

19.2

+45

19.2

20

18.9

+50

18.0

T.P. 2.94 920.23[✓] 13.61 917.29

21

16.7

+25

16.1

+50

15.6

22

14.2

+50

12.7

201

13.8	13.8	12.7	9.7		9.3	9.5	9.4	8.2	7.8	6.0
50	30	16	10	9.1	11	15	30	34	37	50

16.0	15.0	13.5	10.7	9.8		9.5	10.0	9.7	9.0	8.0	8.3	7.4
50	30	17	12	8	9.4	10	15	29	31	37	42	50

14.2	14.0	12.0	10.1	9.6		9.3	10.0	10.6	9.6	8.7	5.2	5.7
50	30	19	14	8	9.0	12	18	24	27	32	37	50

12.4	10.1	8.4	8.0	9.6	8.8		9.0	9.6	8.2	5.5	3.5	3.8
50	30	22	18	12	7	8.5	13	21	27	31	32	50

15.5	13.4	11.7	11.0	12.8	12.1		12.0	13.0	11.2	6.0	5.0	4.4
50	30	20	18	14	8	11.7	14	22	30	35	38	50

10.0	11.4	12.0	13.0	12.0		12.0	12.2	10.6	6.6	4.5	3.0	2.6
50	31	19	15	7	11.7	13	21	29	35	37	40	50

6.7	7.2	6.8	9.5	13.0	12.8	12.4		12.1	12.4	11.1	7.7	5.5	4.8	4.5
50	33	30	28	19	12	9	12.0	10	13	27	34	36	38	50

14.2	14.2	12.6	13.5	13.1		13.1	13.4	12.6	10.0	8.2	7.0	5.2
50	32	25	14	10	12.9	9	13	25	30	32	38	50

8.1	6.8	6.7	6.0	4.5	3.7		4.0	4.6	5.8	6.0	8.0	8.2	6.0
50	44	33	17	13	10	3.5	12	14	16	25	31	37	50

13.4	11.0	8.5	7.1	5.6	4.4		4.4	4.8	7.1	9.6	10.2	10.5	10.2
50	42	33	28	21	10	4.1	12	12	16	25	31	44	50

17.8	14.0	11.0	5.7	4.6		4.8	5.8	6.1	6.0	5.0	6.2	8.0
50	36	31	16	10	4.6	10	14	16	20	23	34	50

23.0	19.3	15.3	6.6	6.1		6.2	6.7	4.4	1.0	+4.0	+5.2	+5.2
50	35	26	12	10	6.0	9	15	22	27	31	34	50

16.0	13.2	10.5	8.5	8.0		7.7	8.2	5.8	0.0	+1.7	+2.4
50	34	19	14	10	7.5	8	13	24	31	35	50

920.23

23 11.0

T.P. 2.76 913.96 9.03 911.20

+50 9.8

24 9.1

+33 12" X 40' C.M. 8.6

25 8.0

+50 7.7

26 7.0

+50 6.6

27 6.0

T.P. 1.74 907.43 8.27 905.69

+50 5.6

+75 5.6

28 5.8

+06 30" X 61' C.M.

$\frac{10.7}{50}$ $\frac{11.0}{25}$ $\frac{12.0}{23}$ $\frac{11.6}{17}$ $\frac{10.1}{12}$ $\frac{9.7}{11}$ 9.2 $\frac{9.5}{10}$ $\frac{10.0}{12}$ $\frac{11.2}{15}$ $\frac{11.0}{23}$ $\frac{9.2}{27}$ $\frac{6.4}{34}$ $\frac{5.4}{45}$ $\frac{4.2}{50}$

$\frac{4.8}{50}$ $\frac{4.8}{38}$ $\frac{5.8}{23}$ $\frac{7.0}{21}$ $\frac{6.6}{16}$ $\frac{4.8}{12}$ $\frac{4.3}{10}$ 4.2 $\frac{4.6}{10}$ $\frac{5.2}{13}$ $\frac{8.4}{20}$ $\frac{8.7}{33}$ $\frac{8.2}{36}$ $\frac{8.2}{50}$

$\frac{11.4}{50}$ $\frac{11.4}{26}$ $\frac{11.0}{24}$ $\frac{9.7}{19}$ $\frac{5.6}{13}$ $\frac{5.1}{10}$ 4.9 $\frac{5.2}{10}$ $\frac{6.0}{12}$ $\frac{11.7}{25}$ $\frac{11.2}{39}$ $\frac{11.4}{50}$

Invert $\downarrow$ $\frac{13.7}{50}$ $\frac{13.5}{34}$ $\frac{12.4}{19}$ $\frac{6.0}{12}$ $\frac{5.6}{10}$ 5.4 $\frac{5.8}{10}$ $\frac{6.4}{12}$ $\frac{8.4}{17}$ $\frac{11.7}{21}$ $\frac{11.7}{32}$ $\frac{11.7}{50}$ $\nwarrow$ Inlet

$\frac{7.2}{50}$ $\frac{6.3}{34}$ $\frac{6.4}{26}$ $\frac{8.0}{23}$ $\frac{8.0}{16}$ $\frac{6.6}{13}$ $\frac{6.2}{10}$ 6.0 $\frac{6.5}{10}$ $\frac{7.1}{14}$ $\frac{8.8}{18}$ $\frac{9.0}{28}$ $\frac{7.1}{31}$ $\frac{6.5}{34}$ $\frac{7.3}{50}$

$\frac{5.5}{50}$ $\frac{4.8}{27}$ $\frac{5.6}{27}$ $\frac{7.3}{22}$ $\frac{7.6}{16}$ $\frac{7.0}{14}$ $\frac{6.5}{10}$ 6.3 $\frac{6.6}{9}$ $\frac{7.4}{17}$ $\frac{8.0}{19}$ $\frac{8.4}{22}$ $\frac{7.0}{28}$ $\frac{4.4}{32}$ $\frac{3.7}{34}$ $\frac{4.3}{50}$

$\frac{6.6}{50}$ $\frac{6.2}{25}$ $\frac{8.0}{23}$ $\frac{8.5}{17}$ $\frac{7.5}{13}$ $\frac{7.2}{10}$ 7.0 $\frac{7.2}{9}$ $\frac{7.6}{13}$ $\frac{8.4}{19}$ $\frac{7.8}{25}$ $\frac{5.2}{30}$ $\frac{4.2}{32}$ $\frac{3.5}{34}$ $\frac{3.5}{50}$

$\frac{7.7}{50}$ $\frac{6.7}{34}$ $\frac{7.0}{27}$ $\frac{8.7}{23}$ $\frac{9.1}{21}$ $\frac{9.1}{17}$ $\frac{8.2}{13}$ $\frac{7.8}{11}$ 7.4 $\frac{7.8}{9}$ $\frac{8.2}{13}$ $\frac{8.5}{16}$ $\frac{9.2}{18}$ $\frac{9.2}{23}$ $\frac{8.0}{28}$ $\frac{5.2}{31}$ $\frac{4.2}{34}$ $\frac{4.2}{50}$

$\frac{12.1}{50}$ $\frac{10.4}{24}$ $\frac{11.1}{23}$ $\frac{10.8}{18}$ $\frac{9.2}{14}$ $\frac{8.6}{11}$ 8.0 $\frac{8.3}{10}$ $\frac{9.0}{15}$ $\frac{10.1}{18}$ $\frac{10.0}{26}$ $\frac{6.3}{32}$ $\frac{5.4}{36}$ $\frac{5.4}{50}$

$\frac{9.4}{50}$ $\frac{8.0}{33}$ $\frac{7.0}{21}$ $\frac{2.5}{13}$ $\frac{2.0}{10}$ 1.8 $\frac{2.2}{10}$ $\frac{2.5}{12}$ $\frac{4.7}{17}$ $\frac{4.2}{32}$ $\frac{3.1}{35}$ $\frac{4.0}{39}$ $\frac{3.4}{50}$

$\frac{10.4}{50}$ $\frac{12.8}{46}$ $\frac{12.4}{39}$ $\frac{9.8}{33}$ $\frac{8.2}{20}$ $\frac{2.4}{12}$ $\frac{2.1}{10}$ 1.8 $\frac{2.2}{10}$ $\frac{3.1}{14}$ $\frac{7.0}{21}$ $\frac{6.4}{33}$ $\frac{5.5}{35}$ $\frac{5.9}{41}$ $\frac{5.0}{45}$ $\frac{5.0}{50}$

$\frac{8.7}{50}$ $\frac{8.8}{33}$ $\frac{7.0}{29}$ $\frac{6.2}{18}$ $\frac{2.0}{10}$ 1.4 $\frac{2.1}{10}$ $\frac{2.4}{13}$ $\frac{7.0}{20}$ $\frac{7.8}{24}$ $\frac{8.2}{33}$ $\frac{7.2}{41}$ $\frac{6.8}{50}$

$\frac{13.4}{29}$ $\frac{13.1}{32}$

907.43

28+50

6.4

29

7.3

T.P. 13.39 920.50 0.32 907.11

+50

8.2

30

8.7

+50

9.1

31

9.2

+50

9.1

32

8.0

+50

7.1

T.P. 4.14 911.25 1339 907.11

+50

7.1

33

6.3

+39 12" X 40' C.M.

6.2

34

6.9

$\frac{6.5}{50}$	$\frac{5.4}{31}$	$\frac{3.7}{17}$	$\frac{1.5}{12}$	$\frac{1.2}{9}$	1.0	$\frac{13}{10}$	$\frac{2.0}{13}$	$\frac{8.5}{25}$	$\frac{8.8}{32}$	$\frac{9.5}{50}$
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$\frac{6.1}{50}$	$\frac{5.4}{34}$	$\frac{4.6}{31}$	$\frac{3.0}{17}$	$\frac{1.0}{13}$	$\frac{0.5}{11}$	0.1	$\frac{0.5}{10}$	$\frac{1.2}{13}$	$\frac{5.4}{29}$	$\frac{6.0}{33}$	$\frac{5.8}{35}$	$\frac{6.8}{50}$
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$\frac{13.6}{50}$	$\frac{12.0}{31}$	$\frac{13.4}{29}$	$\frac{15.1}{25}$	$\frac{15.1}{21}$	$\frac{13.2}{15}$	$\frac{12.7}{7}$	12.5	$\frac{12.6}{10}$	$\frac{13.1}{16}$	$\frac{14.5}{19}$	$\frac{13.3}{22}$	$\frac{14.7}{33}$	$\frac{14.5}{34}$	$\frac{15.4}{50}$
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$\frac{13.6}{50}$	$\frac{11.0}{33}$	$\frac{10.6}{31}$	$\frac{12.6}{28}$	$\frac{13.3}{23}$	$\frac{12.8}{14}$	$\frac{12.1}{10}$	11.8	$\frac{12.0}{10}$	$\frac{12.3}{13}$	$\frac{12.7}{16}$	$\frac{12.5}{22}$	$\frac{9.5}{30}$	$\frac{6.2}{34}$	$\frac{5.5}{36}$	$\frac{6.4}{50}$
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$\frac{14.9}{50}$	$\frac{12.2}{34}$	$\frac{11.5}{31}$	$\frac{12.5}{29}$	$\frac{12.8}{26}$	$\frac{12.5}{14}$	$\frac{11.8}{10}$	11.4	$\frac{11.5}{9}$	$\frac{11.8}{14}$	$\frac{11.7}{20}$	$\frac{9.1}{28}$	$\frac{4.8}{34}$	$\frac{1.8}{35}$	$\frac{1.8}{50}$
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$\frac{16.0}{50}$	$\frac{12.5}{31}$	$\frac{12.2}{26}$	$\frac{13.4}{21}$	$\frac{13.4}{18}$	$\frac{13.0}{17}$	$\frac{11.8}{11}$	11.3	$\frac{11.4}{9}$	$\frac{11.4}{14}$	$\frac{8.2}{24}$	$\frac{2.2}{34}$	$\frac{1.5}{38}$	$\frac{1.7}{50}$
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$\frac{17.3}{50}$	$\frac{15.2}{30}$	$\frac{14.0}{31}$	$\frac{14.7}{30}$	$\frac{14.0}{18}$	$\frac{12.6}{17}$	$\frac{11.9}{10}$	11.4	$\frac{11.6}{10}$	$\frac{12.0}{15}$	$\frac{10.6}{24}$	$\frac{6.9}{29}$	$\frac{4.4}{31}$	$\frac{3.1}{37}$	$\frac{2.6}{50}$
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$\frac{19.0}{50}$	$\frac{16.2}{31}$	$\frac{14.2}{19}$	$\frac{13.4}{13}$	$\frac{12.8}{9}$	12.5	$\frac{12.6}{11}$	$\frac{13.0}{15}$	$\frac{12.3}{20}$	$\frac{10.0}{26}$	$\frac{5.0}{32}$	$\frac{3.6}{37}$	$\frac{2.4}{50}$
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$\frac{13.5}{134}$	$\frac{14.0}{12}$	$\frac{14.6}{15}$	$\frac{14.0}{18}$	$\frac{9.5}{22}$	$\frac{7.5}{28}$	$\frac{5.8}{37}$	$\frac{5.8}{50}$
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$\frac{11.2}{50}$	$\frac{9.4}{29}$	$\frac{7.3}{16}$	$\frac{5.3}{11}$	$\frac{4.6}{9}$	4.2
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$\frac{14.0}{50}$	$\frac{13.6}{30}$	$\frac{7.5}{19}$	$\frac{6.5}{10}$	$\frac{5.5}{8}$	5.0	$\frac{5.0}{9}$	$\frac{5.5}{13}$	$\frac{9.5}{21}$	$\frac{10.0}{29}$	$\frac{9.2}{35}$	$\frac{7.3}{50}$
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$\frac{14.4}{50}$	$\frac{13.4}{30}$	$\frac{12.2}{19}$	$\frac{5.8}{9}$	$\frac{5.5}{7}$	5.1	$\frac{5.4}{12}$	$\frac{6.0}{15}$	$\frac{11.1}{21}$	$\frac{11.2}{36}$	$\frac{11.3}{50}$
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$\frac{8.2}{50}$	$\frac{8.2}{38}$	$\frac{9.0}{33}$	$\frac{9.7}{29}$	$\frac{9.5}{21}$	$\frac{4.8}{10}$	$\frac{4.5}{7}$	4.4	$\frac{4.7}{13}$	$\frac{5.0}{15}$	$\frac{8.4}{22}$	$\frac{8.2}{30}$	$\frac{6.2}{34}$	$\frac{6.0}{38}$	$\frac{6.2}{50}$
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9/1/25

34722

7.0

+33

7.0

+43

6.9

B.M. 4.04 9/1/26 4.04 907.21 907.22

+62. 4 Frost Ave

7.0

T.P. 7.77 915.59 3.44 907.82

+80

6.9

35

7.1

+30

7.6

36

7.2

+50

8.8

37

9.6

+50

10.8

38

12.1

T.P. 11.51 924.98 2.12

913.47

+50

13.4

$\frac{4.2}{50}$ $\frac{4.4}{36}$ $\frac{7.1}{29}$ $\frac{8.6}{27}$ $\frac{8.0}{20}$ $\frac{4.7}{10}$ $\frac{4.5}{8}$ 4.3 $\frac{4.6}{15}$ $\frac{6.8}{20}$ $\frac{7.4}{25}$ $\frac{7.2}{29}$ $\frac{5.2}{35}$ $\frac{4.2}{36}$ $\frac{4.7}{50}$

$\frac{2.5}{50}$ $\frac{3.0}{34}$ $\frac{7.3}{26}$ $\frac{7.0}{22}$ $\frac{6.0}{14}$ $\frac{5.0}{11}$ 4.3 $\frac{4.4}{13}$ $\frac{4.8}{18}$ $\frac{6.0}{21}$ $\frac{7.0}{34}$ $\frac{7.2}{50}$

$\frac{8.6}{50}$ $\frac{7.6}{31}$ $\frac{6.6}{22}$ $\frac{5.6}{17}$ $\frac{4.6}{9}$ 4.4 $\frac{4.3}{29}$ $\frac{4.0}{50}$

Spk. in 18" Oak S.E. Cor. "A2" & W.B. Rd.

$\frac{5.4}{50}$ 4.3 $\frac{3.9}{50}$

$\frac{10.1}{50}$ $\frac{9.0}{16}$ 8.7 $\frac{8.8}{19}$ $\frac{9.8}{24}$ $\frac{10.2}{37}$ $\frac{10.8}{50}$

$\frac{12.4}{50}$ $\frac{12.0}{37}$ $\frac{10.6}{30}$ $\frac{9.6}{19}$ 8.5 $\frac{8.8}{14}$ $\frac{9.8}{18}$ $\frac{10.1}{24}$ $\frac{8.7}{29}$ $\frac{4.7}{34}$ $\frac{6.6}{50}$

$\frac{11.6}{50}$ $\frac{12.4}{25}$ $\frac{11.6}{16}$ $\frac{8.6}{10}$ 8.0 $\frac{8.3}{14}$ $\frac{9.0}{17}$ $\frac{9.2}{19}$ $\frac{9.6}{22}$ $\frac{8.2}{28}$ $\frac{9.2}{37}$ $\frac{5.8}{50}$

$\frac{8.8}{50}$ $\frac{7.6}{38}$ $\frac{10.6}{33}$ $\frac{10.2}{18}$ $\frac{8.7}{12}$ $\frac{7.6}{10}$ 7.4 $\frac{7.8}{12}$ $\frac{7.7}{15}$ $\frac{8.7}{18}$ $\frac{8.7}{22}$ $\frac{8.0}{27}$ $\frac{5.4}{34}$ $\frac{3.0}{38}$ $\frac{2.4}{50}$

$\frac{7.3}{50}$ $\frac{7.8}{39}$ $\frac{9.8}{36}$ $\frac{9.0}{24}$ $\frac{8.6}{15}$ $\frac{7.3}{12}$ 6.8 $\frac{7.3}{12}$ $\frac{7.6}{14}$ $\frac{8.8}{18}$ $\frac{8.0}{24}$ $\frac{6.2}{30}$ $\frac{5.0}{37}$ $\frac{4.2}{50}$

$\frac{12.0}{50}$ $\frac{11.0}{27}$ $\frac{7.0}{20}$ $\frac{7.0}{17}$ $\frac{7.1}{15}$ $\frac{6.4}{13}$ 6.0 $\frac{6.5}{12}$ $\frac{7.0}{16}$ $\frac{9.0}{24}$ $\frac{8.4}{26}$ $\frac{7.5}{50}$

$\frac{10.4}{50}$ $\frac{10.8}{32}$ $\frac{8.8}{24}$ $\frac{6.4}{18}$ $\frac{5.3}{15}$ 4.8 $\frac{5.3}{12}$ $\frac{5.8}{14}$ $\frac{7.7}{19}$ $\frac{6.7}{31}$ $\frac{4.4}{38}$ $\frac{4.0}{50}$

$\frac{2.5}{50}$ $\frac{7.4}{30}$ $\frac{4.4}{17}$ $\frac{3.7}{12}$ 3.5 $\frac{4.1}{13}$ $\frac{4.4}{16}$ $\frac{5.2}{18}$ $\frac{5.0}{26}$ $\frac{4.0}{30}$ $\frac{1.6}{32}$ $\frac{0.4}{36}$ $\frac{0.4}{50}$

$\frac{12.7}{50}$ $\frac{11.4}{31}$ $\frac{11.0}{22}$ $\frac{11.8}{19}$ $\frac{11.6}{12}$ 11.6 $\frac{12.6}{14}$ $\frac{13.1}{21}$ $\frac{12.2}{26}$ $\frac{10.7}{29}$ $\frac{10.0}{37}$ $\frac{9.6}{50}$

92498

39

14.0

+50

13.6

40

13.0

T.P. 3.95 916.38' 12.55

912.43

+50

12.4

41

12.2

+50

11.8

42

11.7

+43. 12" X 34' C.M.

+50

11.6

43

11.6

+50

11.4

44

11.3

+50

11.2

Sta. 39 to 50
Reduce & and 10' Rtglt Sta. 39 to 50

~~913-10~~
~~914.0 913-10~~
916.4 915-14
~~914.2 913-10~~

192

192

192

29.2	22.4	16.6	14.8	13.6	14.2	14.0	12.9	13.4	13.9	15.4	14.5	15.2	33
148	216	84	102	114	108	100	121	116	111	96	105	98	
50	45	39	35	23	12	100	13	16	22	24	37	50	
20.3	20.5	18.0	12.9	12.6	13.6	13.6	12.7	12.2	12.2	18.6	15.0	14.6	
47	45	30	121	124	114	114	123	128	114	100	94	104	10.9
50	38	33	21	17	11	114	13	20	26	29	32	39	50
9.0	10.0	11.8	12.9	13.2	12.3	13.0	12.8	13.6	13.2	14.2	16.0		
50	28	26	23	10	12	120	12	21	28	35	50		
12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	12.1	
314	314	411	511	413	413	1214	417	62	62	515	515		
50	29	23	14	12	40	13	18	30	31	50			
60	5.8	6.3	6.0	4.5	4.2	4.2	4.8	50	6.5	7.7	7.0	7.0	
50	33	17	15	12	12	12	10	13	15	24	27	50	
6.6	6.6	7.3	4.8	4.8	4.8	4.8	5.3	6.8	7.0	7.6			
50	38	17	12	12	12	12	12	15	29	50			
6.3	6.7	8.0	7.1	5.0	4.7	4.7	5.3	9.7	10.0	10.7			
50	33	31	16	12	12	12	13	22	38	50			
7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	7.2	
17	17	17	17	17	17	17	17	17	17	17	17	17	
44	51	61	7.7	8.5	7.3	5.1	5.2	10.5	12.2	12.5			
50	42	38	35	26	17	12	13	23	36	50			
2.6	3.5	6.8	7.3	5.1	4.8	4.8	5.2	5.3	7.3	10.3	12.4		
50	33	27	16	11	11	11	12	15	18	24	50		
6.4	6.4	8.4	8.2	5.5	5.0	5.0	5.3	5.7	7.2	6.2	5.5	7.0	
50	25	23	16	11	11	11	12	16	23	29	36	50	
114	102	8.2	5.7	5.7	5.7	5.7	5.4	5.6	7.1	7.0	6.1	5.4	3.5
50	30	16	11	11	11	11	14	17	23	29	30	33	37
10.8	9.8	8.2	6.7	5.7	5.2	5.2	5.4	5.6	7.0	7.7	6.0	5.4	4.4
50	34	21	14	11	11	11	13	16	19	24	30	33	35

916.38

45

11.1

+50

10.8

+75

10.7

46

5.6

10.8

+50

10.2

T.P.

4.28

913.96

6.70

909.68

47

9.7

+50

9.2

48

9.1

+50

9.1

49

9.3

+50

9.3

50

9.3

B.M.#4

5.40

914.91

4.47

909.49

909.51

+50

9.5

914.91

51 9.6

+50 9.7

+75 9.5

52 9.5

+11 So. Rail 9.49

+17 No. Rail 9.76

+50 10.0

+70 10.2

53 10.4

+50 11.2

54 12.1

T.P. 4.35 916.78 2.48 912.43

+50 12.4

55 12.5

$$\begin{array}{ccccccccc} \frac{5.5}{50} & \frac{5.5}{30} & \frac{8.2}{25} & \frac{7.4}{17} & \frac{5.7}{13} & 5.3 & \frac{5.7}{10} & \frac{5.8}{12} & \frac{7.8}{15} & \frac{8.2}{18} & \frac{8.7}{21} & \frac{8.9}{24} & \frac{7.4}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{9.4}{50} & \frac{7.8}{30} & \frac{8.7}{28} & \frac{8.8}{25} & \frac{7.7}{19} & \frac{5.4}{12} & 5.2 & \frac{5.4}{9} & \frac{9.4}{19} & \frac{10.5}{24} & \frac{11.0}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{8.2}{50} & \frac{9.5}{46} & \frac{9.2}{27} & \frac{8.2}{19} & \frac{5.7}{13} & 5.4 & \frac{5.6}{10} & \frac{9.7}{15} & \frac{10.7}{19} & \frac{12.2}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{6.5}{50} & \frac{6.0}{31} & \frac{5.5}{13} & 5.4 & \frac{5.6}{9} & \frac{6.2}{10} & \frac{10.5}{12} & \frac{12.0}{31} & \frac{12.4}{50} \end{array}$$

5.42

5.15

$$\begin{array}{ccccccccc} \frac{7.0}{50} & \frac{7.4}{33} & \frac{8.1}{30} & \frac{6.4}{26} & \frac{6.8}{22} & \frac{6.5}{19} & \frac{5.7}{16} & \frac{5.2}{13} & 4.9 & \frac{5.4}{9} & \frac{6.5}{12} & \frac{6.2}{24} & \frac{6.2}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{5.4}{50} & \frac{5.3}{37} & \frac{6.0}{31} & \frac{6.7}{27} & \frac{6.2}{17} & \frac{5.0}{13} & 4.7 & \frac{5.2}{10} & \frac{6.4}{13} & \frac{7.1}{22} & \frac{8.2}{25} & \frac{10.2}{31} & \frac{10.2}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{3.5}{50} & \frac{4.6}{33} & \frac{5.0}{31} & \frac{5.8}{23} & \frac{5.1}{15} & \frac{4.8}{13} & 4.5 & \frac{5.0}{10} & \frac{5.8}{12} & \frac{7.0}{16} & \frac{7.4}{25} & \frac{6.6}{30} & \frac{6.3}{23} & \frac{7.0}{26} & \frac{7.5}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{2.0}{50} & \frac{3.0}{29} & \frac{4.0}{23} & \frac{4.4}{15} & \frac{4.0}{13} & 3.7 & \frac{4.2}{11} & \frac{4.4}{12} & \frac{5.6}{17} & \frac{6.1}{20} & \frac{5.6}{25} & \frac{4.7}{34} & \frac{4.7}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{1.5}{50} & \frac{2.2}{27} & \frac{3.1}{21} & \frac{3.1}{13} & 2.8 & \frac{3.2}{8} & \frac{3.6}{13} & \frac{4.1}{15} & \frac{4.4}{19} & \frac{3.7}{24} & \frac{3.0}{27} & \frac{2.6}{35} & \frac{2.6}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{3.1}{50} & \frac{4.0}{21} & \frac{4.9}{19} & \frac{4.7}{13} & 4.4 & \frac{4.7}{12} & \frac{5.1}{18} & \frac{4.7}{23} & \frac{4.0}{50} \end{array}$$

$$\begin{array}{ccccccccc} \frac{3.8}{50} & \frac{4.1}{31} & \frac{4.9}{23} & \frac{5.0}{15} & \frac{4.7}{13} & 4.3 & \frac{4.5}{10} & \frac{4.6}{17} & \frac{4.2}{27} & \frac{3.0}{50} \end{array}$$

916.78[✓]

55 +50

12.1

56

12.2

+50

12.2

57

12.2

+50

12.6

T.P. 8.36 921.59[✓] 3.55

913.23

58

13.2

+50

13.8

59

14.4

+50

15.0

60

15.2

+50

16.4

61

17.1

+50

17.8

$$\begin{array}{cccccccc} \frac{7.3}{50} & \frac{6.5}{39} & \frac{7.0}{29} & \frac{7.4}{27} & \frac{6.7}{18} & \frac{5.3}{14} & \frac{4.9}{12} & \frac{4.9}{10} \end{array}$$

$$\frac{5.2}{13} \quad \frac{5.2}{33} \quad \frac{4.2}{50}$$

$$\begin{array}{cccccccc} \frac{9.1}{50} & \frac{8.6}{34} & \frac{8.7}{26} & \frac{8.2}{21} & \frac{5.2}{14} & \frac{5.0}{10} & \frac{6.6}{14} & \frac{7.4}{24} \end{array}$$

$$\frac{7.4}{50}$$

$$\begin{array}{cccccccc} \frac{9.0}{50} & \frac{8.5}{33} & \frac{8.5}{24} & \frac{7.7}{18} & \frac{5.2}{14} & \frac{4.9}{10} & \frac{5.4}{12} & \frac{7.0}{16} \end{array}$$

$$\frac{7.5}{20} \quad \frac{7.2}{22} \quad \frac{7.8}{50}$$

$$\begin{array}{cccccccc} \frac{7.7}{50} & \frac{7.7}{34} & \frac{8.0}{25} & \frac{7.0}{17} & \frac{5.0}{13} & \frac{5.0}{10} & \frac{6.0}{13} & \frac{8.0}{17} \end{array}$$

$$\frac{7.8}{27} \quad \frac{7.6}{50}$$

$$\begin{array}{cccccccc} \frac{5.7}{50} & \frac{6.0}{34} & \frac{7.2}{30} & \frac{7.5}{24} & \frac{7.0}{17} & \frac{4.8}{15} & \frac{4.6}{11} & \frac{7.5}{17} \end{array}$$

$$\frac{7.8}{26} \quad \frac{6.4}{39} \quad \frac{6.4}{50}$$

$$\begin{array}{cccccccc} \frac{10.4}{50} & \frac{10.2}{38} & \frac{11.2}{30} & \frac{10.7}{19} & \frac{9.2}{15} & \frac{8.8}{14} & \frac{8.8}{11} & \frac{12.4}{16} \end{array}$$

$$\frac{11.8}{30} \quad \frac{10.4}{42} \quad \frac{10.5}{50}$$

$$\begin{array}{cccccccc} \frac{9.1}{50} & \frac{9.7}{27} & \frac{10.4}{24} & \frac{10.0}{20} & \frac{8.2}{16} & \frac{8.0}{13} & \frac{8.2}{11} & \frac{10.7}{17} \end{array}$$

$$\frac{11.4}{28} \quad \frac{10.0}{42} \quad \frac{10.0}{50}$$

$$\begin{array}{cccccccc} \frac{8.6}{50} & \frac{9.1}{27} & \frac{9.9}{25} & \frac{9.6}{17} & \frac{8.2}{14} & \frac{7.6}{11} & \frac{7.7}{12} & \frac{11.0}{17} \end{array}$$

$$\frac{11.1}{28} \quad \frac{9.6}{41} \quad \frac{9.6}{50}$$

$$\begin{array}{cccccccc} \frac{7.2}{50} & \frac{7.2}{38} & \frac{8.2}{24} & \frac{9.1}{21} & \frac{8.8}{17} & \frac{7.2}{13} & \frac{7.1}{11} & \frac{9.1}{15} \end{array}$$

$$\frac{9.7}{19} \quad \frac{9.8}{30} \quad \frac{9.0}{39} \quad \frac{9.0}{50}$$

$$\begin{array}{cccccccc} \frac{4.8}{50} & \frac{4.9}{39} & \frac{6.6}{25} & \frac{7.6}{21} & \frac{8.2}{18} & \frac{7.6}{16} & \frac{6.5}{13} & \frac{6.7}{12} \end{array}$$

$$\frac{8.0}{15} \quad \frac{8.4}{29} \quad \frac{9.0}{50}$$

$$\begin{array}{cccccccc} \frac{3.5}{50} & \frac{3.0}{37} & \frac{4.1}{20} & \frac{7.1}{24} & \frac{7.2}{19} & \frac{6.6}{16} & \frac{5.6}{13} & \frac{5.7}{11} \end{array}$$

$$\frac{7.0}{14} \quad \frac{8.0}{50}$$

$$\begin{array}{cccccccc} \frac{3.1}{50} & \frac{3.1}{41} & \frac{4.1}{31} & \frac{6.4}{25} & \frac{5.7}{15} & \frac{4.9}{13} & \frac{4.9}{11} & \frac{6.3}{15} \end{array}$$

$$\frac{6.8}{20} \quad \frac{6.0}{24} \quad \frac{6.1}{50}$$

$$\begin{array}{cccccccc} \frac{3.2}{50} & \frac{3.1}{35} & \frac{3.8}{29} & \frac{5.6}{21} & \frac{4.5}{15} & \frac{4.1}{13} & \frac{4.1}{11} & \frac{4.5}{14} \end{array}$$

$$\frac{5.1}{16} \quad \frac{5.2}{16} \quad \frac{4.9}{20} \quad \frac{5.5}{23} \quad \frac{5.5}{50}$$

921.59

62 18.5

+50 19.0

T.P. 6.00 925.57 2.02 919.57

63 19.6

+50 20.1

64 20.6

+50 21.1

65 21.6

+40 22.2

+50 22.3

+80 22.7

+88 $\frac{1}{2}$ Co. Rd. "B" 22.7

66 22.7

B.M.#5 3.00 925.55 3.00 922.57 922.55

+15 22.7

$\frac{2.9}{50}$ $\frac{2.9}{36}$ $\frac{3.5}{23}$ $\frac{4.9}{20}$ $\frac{3.8}{15}$ $\frac{3.4}{13}$ 3.1 $\frac{3.3}{11}$ $\frac{4.2}{14}$ $\frac{4.0}{29}$ $\frac{4.5}{50}$

$\frac{2.7}{50}$ $\frac{4.0}{25}$ $\frac{4.7}{20}$ $\frac{4.6}{16}$ $\frac{2.8}{13}$ 2.6 $\frac{3.0}{12}$ $\frac{4.0}{16}$ $\frac{4.0}{23}$ $\frac{4.5}{50}$

$\frac{6.4}{50}$ $\frac{7.4}{31}$ $\frac{8.6}{21}$ $\frac{8.4}{16}$ $\frac{6.4}{12}$ 6.0 $\frac{6.6}{13}$ $\frac{7.4}{15}$ $\frac{8.2}{21}$ $\frac{7.2}{25}$ $\frac{7.2}{34}$ $\frac{7.7}{50}$

$\frac{6.7}{50}$ $\frac{7.4}{24}$ $\frac{8.0}{21}$ $\frac{8.4}{17}$ $\frac{6.0}{12}$ 5.5 $\frac{5.8}{14}$ $\frac{6.4}{14}$ $\frac{7.2}{17}$ $\frac{7.4}{23}$ $\frac{6.4}{27}$ $\frac{6.8}{50}$

$\frac{5.6}{50}$ $\frac{6.4}{30}$ $\frac{7.8}{24}$ $\frac{7.8}{17}$ $\frac{5.3}{12}$ 5.0 $\frac{5.3}{12}$ $\frac{6.4}{16}$ $\frac{6.4}{25}$ $\frac{5.6}{22}$ $\frac{6.1}{50}$

$\frac{5.3}{50}$ $\frac{6.1}{30}$ $\frac{7.0}{27}$ $\frac{7.5}{22}$ $\frac{6.8}{16}$ $\frac{4.9}{12}$ 4.5 $\frac{4.7}{11}$ $\frac{5.4}{14}$ $\frac{5.8}{16}$ $\frac{5.5}{25}$ $\frac{4.9}{27}$ $\frac{4.0}{38}$ $\frac{4.4}{50}$

$\frac{5.0}{50}$ $\frac{4.8}{36}$ $\frac{5.2}{30}$ $\frac{6.2}{26}$ $\frac{6.4}{17}$ $\frac{4.4}{13}$ 4.0 $\frac{4.3}{12}$ $\frac{5.1}{15}$ $\frac{5.2}{22}$ $\frac{4.8}{24}$ $\frac{7.6}{26}$ $\frac{2.7}{40}$ $\frac{3.1}{50}$

$\frac{3.9}{50}$ $\frac{3.8}{40}$ $\frac{4.4}{31}$ $\frac{4.1}{26}$ $\frac{5.5}{23}$ $\frac{5.5}{20}$ $\frac{4.0}{17}$ $\frac{3.7}{13}$ 3.4 $\frac{3.6}{10}$ $\frac{3.8}{13}$ $\frac{4.4}{16}$ $\frac{4.4}{24}$ $\frac{3.3}{22}$ $\frac{2.4}{39}$ $\frac{2.6}{50}$

$\text{E Co. Rd. } 8^{\circ} \rightarrow \frac{3.6}{50}$ $\frac{3.6}{28}$ $\frac{3.6}{14}$ 3.3 $\frac{3.4}{9}$ $\frac{3.4}{12}$ $\frac{4.0}{15}$ $\frac{4.6}{20}$ $\frac{4.2}{24}$ $\frac{3.4}{26}$ $\frac{2.1}{38}$ $\frac{2.6}{50}$

$\frac{3.4}{50}$ $\frac{3.4}{45}$ $\frac{3.0}{35}$ $\frac{2.2}{29}$ $\frac{3.2}{17}$ 2.9 $\frac{3.0}{19}$ $\frac{4.4}{22}$ $\frac{4.1}{24}$ $\frac{4.1}{33}$ $\frac{3.3}{34}$ $\frac{3.7}{50}$

2.9

$\frac{3.6}{50}$ $\frac{3.6}{36}$ $\frac{4.2}{28}$ $\frac{4.7}{23}$ $\frac{4.2}{19}$ $\frac{3.2}{16}$ 2.9 $\frac{2.6}{15}$ $\frac{2.1}{43}$ $\frac{3.2}{50}$

Spk. in 20" Cottonwood 31 Lt 66 + 08

$\frac{3.4}{50}$ $\frac{3.8}{32}$ $\frac{4.4}{26}$ $\frac{4.4}{21}$ $\frac{2.6}{16}$ $\frac{3.1}{12}$ 2.9 $\frac{2.8}{13}$ $\frac{2.1}{29}$ $\frac{1.8}{50}$

925.55

66+30

22.8

67

23.7

B.M. #5 4.90 929.45 3.00 922.55

+50

24.3

68

24.7

+50

25.1

69

25.8

+50

26.3

70

26.7

T.P. 5.81 932.59' 2.67 926.78

+50

26.9

71

26.7

+50

26.3

72

25.6

+50

24.8

$$\begin{array}{cccccc} 2.8 & 3.4 & 4.0 & 4.3 & 3.3 & \\ 50 & 32 & 26 & 20 & 15 & \end{array} \quad \begin{array}{cccccc} 2.8 & 2.9 & 3.7 & 4.1 & 2.0 & 1.7 & 1.5 \\ 10 & 14 & 18 & 27 & 35 & 42 & 50 \end{array} \text{Card B''}$$

$$\begin{array}{cccccc} 40.6 & 1.0 & 2.5 & 2.8 & 2.3 & \\ 50 & 30 & 25 & 16 & 15 & \end{array} \quad \begin{array}{cccccc} 1.9 & 2.2 & 3.2 & 3.1 & 2.4 & \\ 10 & 14 & 18 & 31 & 50 & \end{array}$$

$$\begin{array}{cccccc} 4.0 & 5.0 & 5.2 & 6.1 & 5.6 & \\ 50 & 28 & 24 & 18 & 13 & \end{array} \quad \begin{array}{cccccc} 5.4 & 6.1 & 7.0 & 6.8 & 6.8 & \\ 12 & 15 & 19 & 32 & 50 & \end{array}$$

$$\begin{array}{cccccc} 3.8 & 4.9 & 5.2 & 5.7 & 5.1 & \\ 50 & 29 & 17 & 15 & 12 & \end{array} \quad \begin{array}{cccccc} 5.1 & 5.4 & 6.3 & 6.3 & & \\ 13 & 15 & 18 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 4.2 & 3.9 & 4.9 & 5.1 & 4.7 & \\ 50 & 31 & 19 & 15 & 12 & \end{array} \quad \begin{array}{cccccc} 4.6 & 4.8 & 5.6 & 5.7 & 5.3 & \\ 13 & 16 & 18 & 33 & 50 & \end{array}$$

$$\begin{array}{cccccc} 3.3 & 4.2 & 4.1 & & & \\ 50 & 15 & 11 & & & \end{array} \quad \begin{array}{cccccc} 4.1 & 4.2 & 4.8 & 4.9 & 4.4 & \\ 13 & 16 & 18 & 26 & 50 & \end{array}$$

$$\begin{array}{cccccc} 1.8 & 2.8 & 3.7 & 3.5 & & \\ 50 & 24 & 15 & 11 & & \end{array} \quad \begin{array}{cccccc} 3.4 & 4.0 & 4.2 & & & \\ 13 & 18 & 50 & & & \end{array}$$

$$\begin{array}{cccccc} 40.3 & 1.0 & 2.8 & 3.0 & & \\ 50 & 29 & 14 & 11 & & \end{array} \quad \begin{array}{cccccc} 3.1 & 2.7 & 3.0 & 3.2 & & \\ 13 & 15 & 30 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 2.0 & 3.4 & 5.6 & 6.1 & 6.0 & \\ 50 & 28 & 15 & 14 & 12 & \end{array} \quad \begin{array}{cccccc} 6.0 & 6.3 & 6.1 & 5.5 & & \\ 13 & 16 & 20 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 3.8 & 6.5 & 6.7 & 6.1 & & \\ 50 & 20 & 13 & 12 & & \end{array} \quad \begin{array}{cccccc} 6.2 & 6.4 & 6.8 & 6.5 & 5.8 & \\ 13 & 17 & 19 & 22 & 50 & \end{array}$$

$$\begin{array}{cccccc} 4.0 & 5.0 & 6.5 & 7.0 & 7.3 & 6.7 & \\ 50 & 31 & 20 & 18 & 14 & 12 & \end{array} \quad \begin{array}{cccccc} 6.8 & 7.5 & 8.4 & 7.6 & & \\ 12 & 16 & 36 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 5.7 & 5.5 & 7.5 & 7.1 & & \\ 50 & 33 & 14 & 12 & & \end{array} \quad \begin{array}{cccccc} 7.3 & 7.8 & 8.7 & 9.4 & & \\ 13 & 15 & 28 & 50 & & \end{array}$$

$$\begin{array}{cccccc} 7.3 & 8.3 & 8.6 & 8.2 & & \\ 50 & 27 & 14 & 12 & & \end{array} \quad \begin{array}{cccccc} 8.1 & 8.3 & 8.8 & 8.5 & & \\ 13 & 19 & 28 & 50 & & \end{array}$$

932.59

73 4.37 928.10 8.86 24.1
 T.P. ← 923.73
 +50 23.9

74 23.8

+50 23.6

75 23.4

+50 23.5

76 23.6

+50 23.4

77 23.3

+50 23.8

+88 Edge of Pavement & 24.1

78 24.0

79 23.85

B.M. #6 6.11 921.99 922.00

$\frac{7.6}{50}$	$\frac{9.3}{30}$	$\frac{9.6}{14}$	$\frac{8.8}{12}$	8.5	$\frac{9.0}{14}$	$\frac{9.6}{16}$	$\frac{10.0}{28}$	$\frac{9.0}{50}$
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$\frac{1.7}{50}$	$\frac{5.0}{27}$	$\frac{5.3}{14}$	$\frac{4.7}{12}$	4.2	$\frac{4.6}{13}$	$\frac{5.0}{15}$	$\frac{5.4}{17}$	$\frac{6.1}{40}$	$\frac{6.7}{50}$
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$\frac{2.6}{50}$	$\frac{4.5}{34}$	$\frac{5.6}{26}$	$\frac{5.7}{14}$	$\frac{5.1}{13}$	$\frac{4.9}{12}$	4.3	$\frac{4.8}{13}$	$\frac{5.3}{15}$	$\frac{5.5}{17}$	$\frac{6.2}{27}$	$\frac{6.6}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{3.1}{50}$	$\frac{4.7}{26}$	$\frac{5.8}{22}$	$\frac{6.1}{15}$	$\frac{5.1}{11}$	4.5	$\frac{4.9}{13}$	$\frac{5.4}{15}$	$\frac{6.0}{17}$	$\frac{6.5}{33}$	$\frac{6.7}{50}$
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$\frac{5.0}{50}$	$\frac{5.7}{33}$	$\frac{6.0}{14}$	$\frac{5.1}{12}$	4.7	$\frac{5.1}{13}$	$\frac{5.8}{15}$	$\frac{7.0}{18}$	$\frac{7.1}{32}$	$\frac{6.2}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{6.2}{50}$	$\frac{6.4}{30}$	$\frac{6.4}{14}$	$\frac{5.2}{12}$	4.6	$\frac{5.0}{13}$	$\frac{5.5}{15}$	$\frac{6.8}{19}$	$\frac{7.0}{31}$	$\frac{4.6}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{6.1}{50}$	$\frac{6.7}{31}$	$\frac{6.5}{15}$	$\frac{5.0}{11}$	4.5	$\frac{5.2}{13}$	$\frac{5.5}{14}$	$\frac{6.2}{17}$	$\frac{7.0}{18}$	$\frac{6.4}{28}$	$\frac{4.1}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{2.7}{50}$	$\frac{6.2}{27}$	$\frac{6.8}{17}$	$\frac{5.6}{14}$	$\frac{5.0}{12}$	4.7	$\frac{5.4}{13}$	$\frac{6.4}{15}$	$\frac{6.7}{24}$	$\frac{5.5}{50}$
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$\frac{4.8}{50}$	$\frac{6.6}{29}$	$\frac{7.0}{17}$	$\frac{5.8}{14}$	$\frac{5.3}{11}$	4.8	$\frac{5.0}{15}$	$\frac{5.2}{22}$	$\frac{5.7}{25}$	$\frac{5.6}{31}$	$\frac{4.5}{35}$	$\frac{4.4}{40}$	$\frac{4.9}{50}$
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Edge Pave

$\frac{7.0}{50}$	$\frac{6.8}{38}$	$\frac{7.5}{38}$	$\frac{7.4}{20}$	$\frac{6.7}{16}$	$\frac{4.8}{12}$	4.3	$\frac{4.2}{13}$	$\frac{5.6}{39}$
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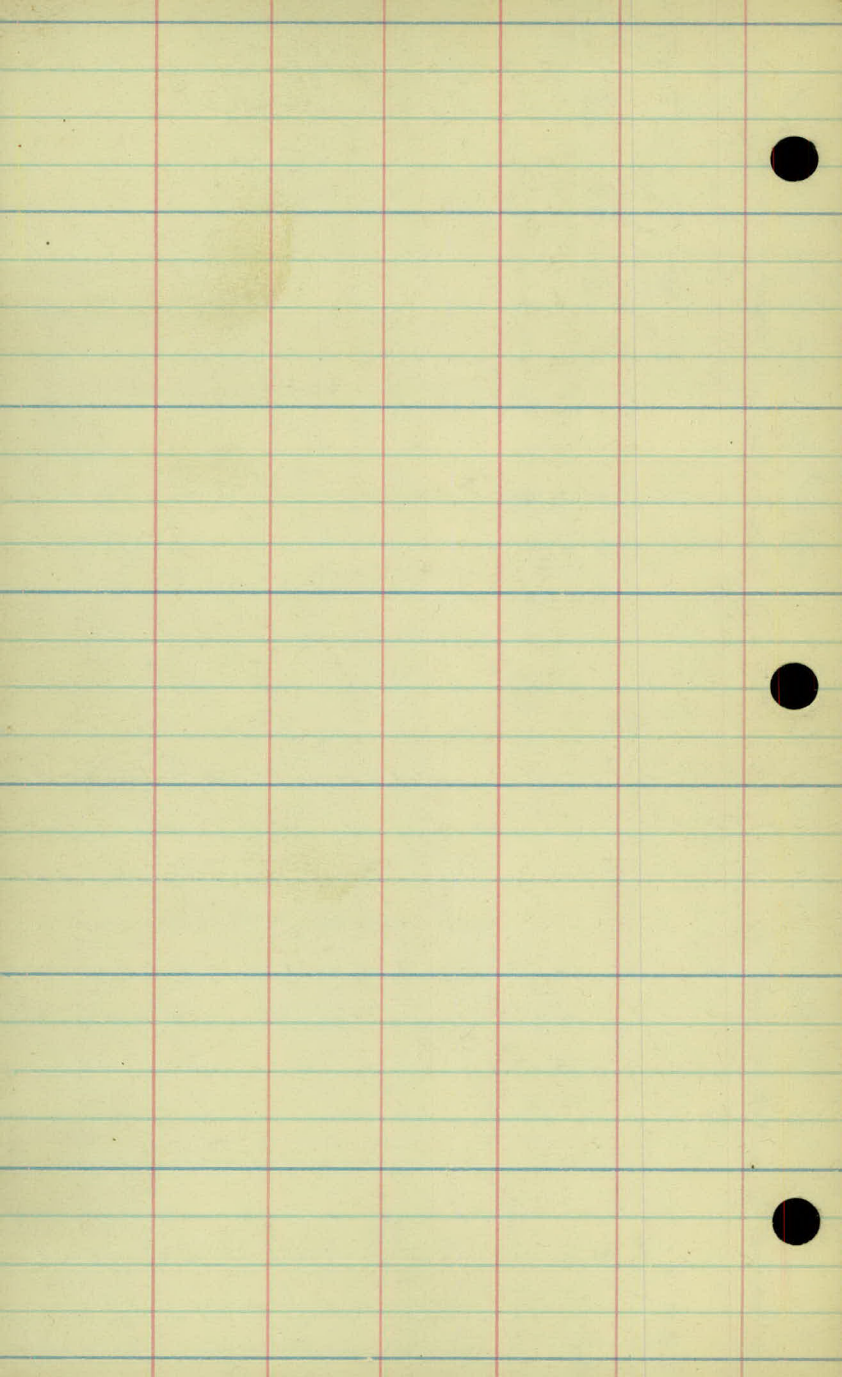
E.P.

$\frac{8.2}{50}$	$\frac{8.4}{25}$	$\frac{7.0}{19}$	$\frac{6.6}{17}$	$\frac{4.7}{12}$	$\frac{4.1}{10}$	4.0	$\frac{5.4}{24}$
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4.1

4.25

Spt. in 18" Oak N.E. Cor. W.B. Ave + W.B. Rd.



Check Levels

Rd. $\frac{2}{c}$ #39

B.M.#0	13.35	908.86		895.51	
B.M.#3			1.64	907.22	
T.P.	1.83	910.50	0.19	908.67	
"	12.58	920.86	2.22	908.28	
"	1.94	919.71	3.09	917.77	
"	6.68	921.61	4.78	914.93	
B.M.#2			0.34	921.27	
T.P.	9.50	930.57	0.54	921.07	
"	7.12	935.00	2.49	927.88	
B.M.#1	4.31	933.64	5.67	929.33	
T.P.	0.28	926.21	7.71	925.93	
"	5.32	921.43	10.10	916.11	
B.M.#2			0.17	921.26	921.27
T.P.	6.06	920.89	6.60	914.83	
"	0.92	919.95	1.86	919.03	
"	2.44	910.70	11.69	908.26	
"	2.24	911.38	1.56	909.14	
B.M.#3	5.15	912.37	4.18	907.20	907.22
T.P.	5.37	917.22	0.52	911.85	
"	2.78	914.05	5.95	911.27	
"	5.38	914.96	4.47	909.58	
B.M.#4			5.45	909.51	
T.P.	8.38	920.50	2.84	912.12	
"	7.71	928.07	0.14	920.36	
B.M.#5			5.52	922.55	
T.P.	2.70	929.32	1.45	926.62	
"	5.61	929.03	5.90	923.42	
B.M.#6			7.03	922.00	

41
Spk. in P.P.-S.E. Cor. "A²" & Bock St.
Spk. in 18" Oak S.E. Cor. "A²" & W.B. Rd.

Spk. in 18" Oak 60' Lt. 10+15

Spk. in 15" Oak S.E. Cor. W.B. Rd. & Hazelwood Ave

Spk. in 12" Oak 60' Rt. 50+90

Spk. in 20" Cottonwood 31' Lt. 66+08 N.W. Cor. "B" & W.B. Rd.

Spk. in 18" Oak N.E. Cor. W.B. Rd. + W.B. Ave

B.M. #6	6.83	928.83		922.00	
T.P.	7.46	931.35	4.94	923.89	
B.M. #5	1.17	923.72	8.80	922.55	922.55
T.P.	2.85	917.29	9.28	914.44	
"	4.41	913.99	7.71	909.58	
B.M. #4			4.47	909.52	909.51
T.P.	5.91	916.85	3.05	910.94	
"	0.39	912.54	3.70	913.15	
B.M. #3	1.54	908.76	6.29	907.25	907.22
B.M. #0			13.24	895.52	895.51

White Bear Rd.
Plans in hand.

8/28/33
Vair
Carley
Beafore

- ✓ 3+50 4+50 Cl. 5 Gr. 7 Rt
- ✓ 4+50 8+00 Cl. 35 Gr. 35 Lt
- ✓ 8+00 12+00 Cl. 39 Gr. 10 Rt
- ✓ Check G.R. Rt. Starts at 11+00
- ✓ 11+50 12+50 Cl. 3 Lt
- ✓ Cable guard rail Rem & Rep
- ✓ 11+94 Ext
- ✓ 13+00 15+50 Cl. 3 Gr. 5 Rt
- ✓ 15+00 16+50 Cl. 4 Gr. 8 Lt
- ✓ 17+65 Rt Pl. 15" X 20' C.M.
- ✓ 18+00 20+00 Cl. 3 Gr. 3 Lt
- ✓ 20+50 23+50 Cl. 6 Gr. 5 Lt
- ✓ 21+00 23+00 Cl. 7 Gr. 4 Rt
- ✓ 27+44 Rt Pl. 15" X 20' C.M.
- ✓ 32+00 33+00 Cl. 2 Gr. 2 Rt
- ✓ 33+ See Xculv. 39-4
- ✓ First Are No. culv. 5 req
- ✓ 42+43 Pl. 18" P3 X
- ✓ 50+00 51+00 Cl. 5 Gr. 9 Lt
- ✓ 50+00 51+00 Cl. 2 Gr. 3 Rt
- ✓ 51+27 Rt Pl. 15" X 20' C.M.
- ✓ 55+20 Rt Rep. 12" C.M.
- ✓ 55+94 Lt No. culv 1 req

✓ 63+91 Lt. Reitt & Rep,
Check drainage at
end of Proj.

White Bear Rd.

Lorpenleur Ave to

Bank Widening
and Line Changes.

Sta. Point Lt 4 Rt

21+47.3 P.T. 3° 03'

21 2° 41.7'

+50 2° 19.2'

P.I. 19+44.15

20 1° 56.7'

Δ 6° 06' Lt.

+50 1° 34.2'

Δ -1° 30'

19 1° 11.7'

T. 203.52

+50 0° 49.2'

L.C. 406.67

18 0° 26.7'

R. 3819.83

17+40.63 P.C. 0° 00'

15+38.55 P.I. 1° 40'

13+60.45 }
13+59.1 } P.T. 16° 53'

+25 13° 48.9'

P.I. 12+68.5

13 11° 33.9'

Δ 33° 46'

+75 9° 12.9'

Δ -18°

+50 7° 03.9'

T. 97.00

+25 4° 48.9'

L.C. 187.60

12 2° 33.9'

R. 319.62

11+71.5 P.C. 0° 00'

W.H.C.

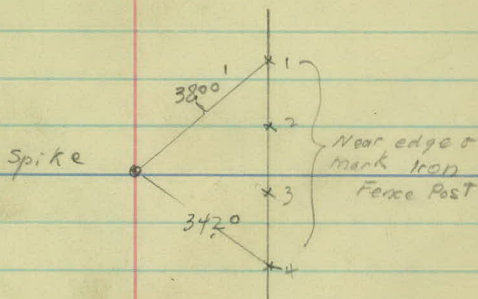
45

K.A.

L.B.H.

A.M.

June, 22, 1938



⊙ Pop.

25.46

• spike

70.36

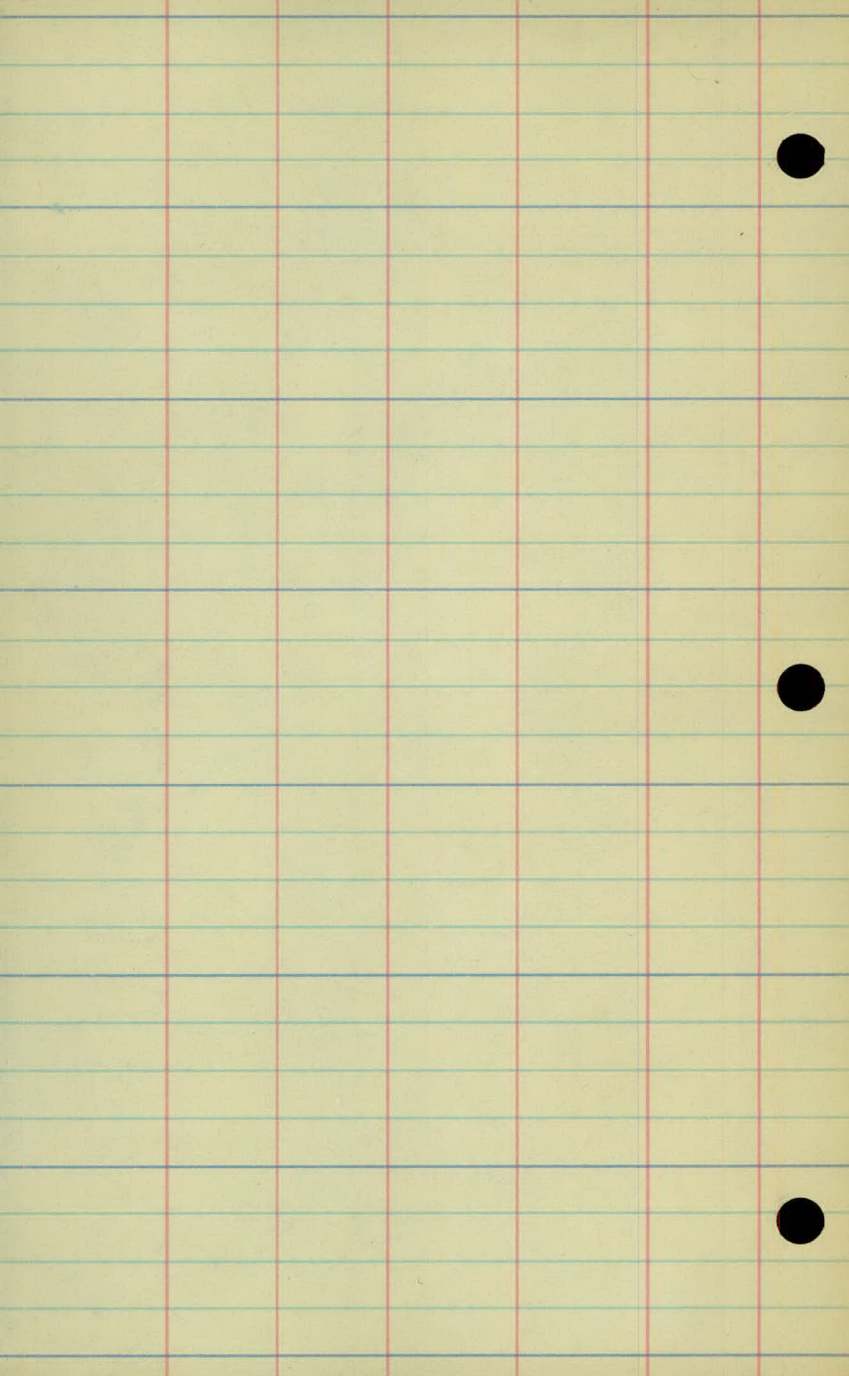
⊙ Pop.

⊙ 8" Pop.

30.7

2x2 4x6.

41.60 — ⊙ 24' Pop



White Bear Road-

Blue Tops & Slope Stakes Widening.

June 22, 1936

0.16 921.79

921.63

8+15

+50

9+0

9+50

10+00

10+50

11+0

T.P. 3.73 918.96 6.56 915.23

+50 4.2 14.8

+71.5 4.3 14.7

12 4.4 14.6

+25 4.4 14.6

+50 4.2 14.8

+75 4.0 15.0

13+0 4.0 15.0

+25 4.1 14.9

13+59.1 } 4.1 14.9

13+60.45 } 4.1 14.9

14+0 3.9 15.1

B/G-Top
✱

$$\begin{array}{r} 2.5 \\ \hline \end{array} \quad \begin{array}{r} 2.8 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 13.2 \\ 35.4 \\ \hline \end{array} \quad \text{Van slope}$$

$$\begin{array}{r} 3.3 \\ \hline \end{array} \quad \begin{array}{r} 7.6 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} -9.6 \\ -55.1 \\ \hline \end{array} \quad \text{Van slope}$$

$$\begin{array}{r} 4.8 \\ \hline \end{array} \quad \begin{array}{r} 4.6 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 12.6 \\ -9.0 \\ \hline \end{array} \quad / 35 \text{ Van}$$

$$\begin{array}{r} 5.2 \\ \hline \end{array} \quad \begin{array}{r} 5.5 \\ 18 \\ \hline \end{array} \quad \begin{array}{r} 15.4 \\ -10.0 \\ \hline \end{array} \quad 353 \text{ Van}$$

$$\begin{array}{r} 5.8 \\ \hline \end{array} \quad \begin{array}{r} 6.1 \\ 17 \\ \hline \end{array} \quad \begin{array}{r} 13.7 \\ -7.6 \\ \hline \end{array} \quad / 32.2 \quad 2.1$$

$$\begin{array}{r} 6.1 \\ \hline \end{array} \quad \begin{array}{r} 6.4 \\ 16 \\ \hline \end{array} \quad \begin{array}{r} 2.0 \\ -2.0 \\ \hline \end{array} \quad / 21.2 \quad 2.1$$

$$\begin{array}{r} 6.6 \\ \hline \end{array} \quad \begin{array}{r} 6.9 \\ 15 \\ \hline \end{array} \quad \begin{array}{r} 9.9 \\ -3.0 \\ \hline \end{array} \quad / 21.0 \quad 2.1$$

918.96

x.07

907.51

1352

905.44

11+71.5

907.

145

12

143

+75

143

+50

145

+75

147

T.P.

5.60

920.83

915.23

12+50

12+75

13+0

+75

13+59.1 }

13+60.45 }

120

$$\begin{array}{r} -11.2 \\ 394 \\ \hline \end{array}$$

6.8

$$\begin{array}{r} -15.6 \\ 482 \\ \hline \end{array}$$

6.8

$$\begin{array}{r} -190 \\ 55 \\ \hline \end{array}$$

70

$$\begin{array}{r} -20 \\ 57 \\ \hline \end{array}$$

72

Bluetops.

$$\begin{array}{r} 6.6 \\ 18 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ 18 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ 18 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ 18 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ 18 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \end{array}$$

920.83

1440

+50

15

+38.55

16

+50

17

+40.63 P.C. 1°40

18

T.R

1.62

BlueTaps

1

$$\frac{60}{18}$$

$$\frac{57}{18}$$

$$42 \mid \frac{178}{-120}$$

$$\frac{58}{18}$$

$$\frac{55}{18}$$

$$34.0 \mid \frac{13.4}{-80}$$

$$\frac{54}{18}$$

$$\frac{51}{18}$$

$$280 \mid \frac{10.1}{-50}$$

$$\frac{5.1}{18}$$

$$\frac{48}{18}$$

$$270 \mid \frac{93}{-45}$$

$$\frac{48}{18}$$

$$\frac{44.5}{18}$$

$$24.8 \mid \frac{7.6}{-34}$$

$$\frac{4.2}{18}$$

$$\frac{39}{18}$$

$$23.2 \mid \frac{6.4}{-30}$$

$$\frac{3.8}{18}$$

$$\frac{35}{18}$$

$$26.0 \mid \frac{7.6}{-40}$$

$$\frac{3.6}{18}$$

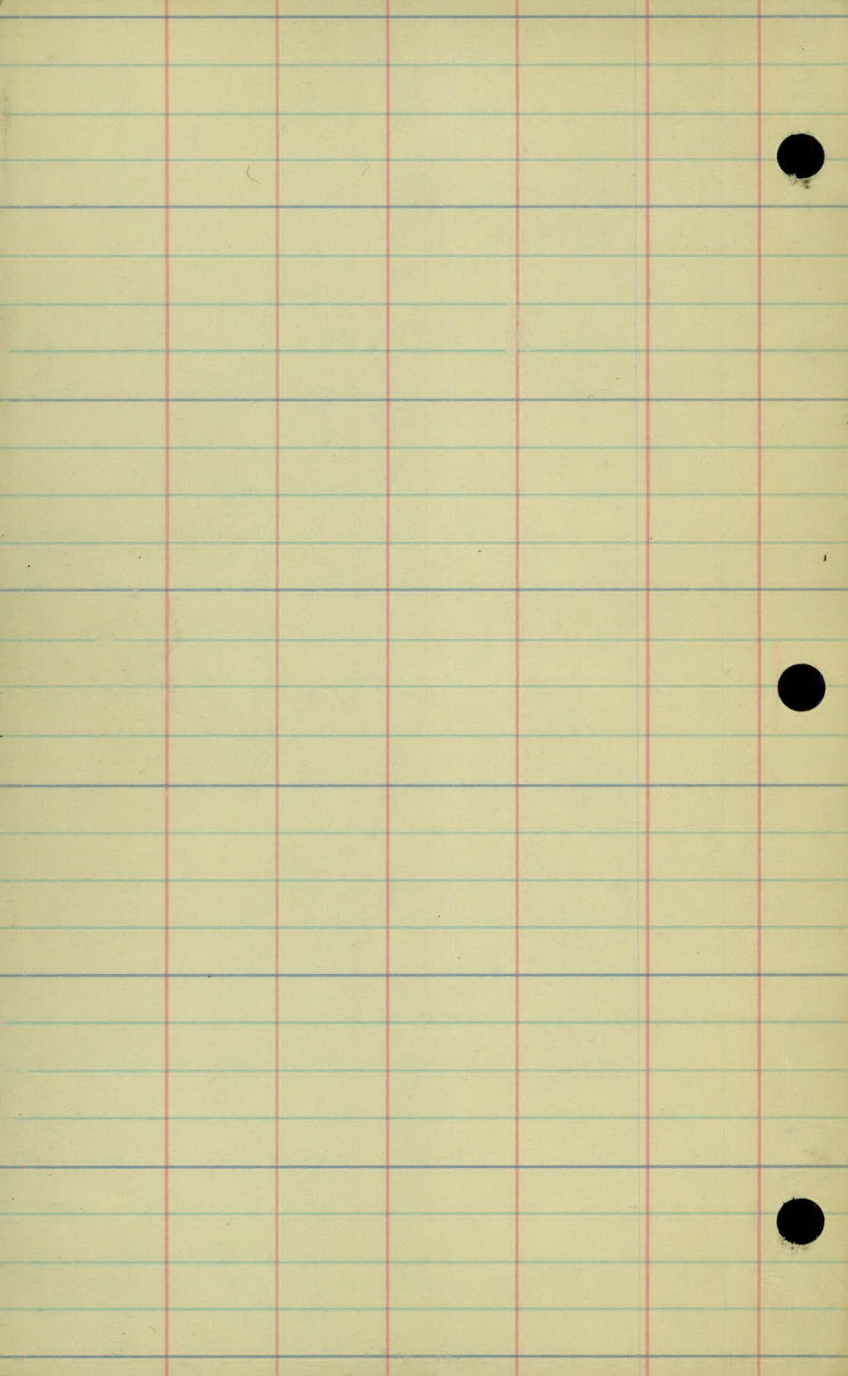
$$\frac{33}{18}$$

$$24.4 \mid \frac{6.1}{-32}$$

$$\frac{2.9}{18}$$

$$\frac{26}{18}$$

Top Spike P.I. 19+44.15



1

WHITE BEAR ROAD

Carpenter to Frost.

Slope Stakes

23.5 to back slope

3.1 slopes

11' - 20' Crown

Sta.	+	π	-	Grade.
B.M.	4.19	911.41 ✓		907.22 ✓

29				06.6
----	--	--	--	------

+50				07.3
-----	--	--	--	------

30				08.0
----	--	--	--	------

+50				08.5
-----	--	--	--	------

31				08.6
----	--	--	--	------

+50				08.4
-----	--	--	--	------

32				07.8
----	--	--	--	------

+50 T.P.	3.64	910.86 ✓	4.19	07.1 ✓ 907.22 ✓
-------------	------	----------	------	--------------------

Lt.

E

Rt

2

Spike in 18" Oak - S.E. Cor. 17th & W. Bond Rd.
¹⁵
 4.8
 6.3

⁸⁰
 F.32
 24.6

¹⁰²
 F.54
 31.2

✓

¹⁵
 4.1
 5.6

³⁰
 0026
 31.3

32

⁴⁷
 0.009
 26.2

✓

¹⁵
 3.4
 4.9

¹⁹
 0030
 32.5

27

✓

¹⁵
 2.9
 4.4

³⁶
 0008
 25.9

25

✓

¹⁵
 2.8
 4.3

³¹
 0012
 27.1

21

✓

¹⁵
 3.0
 4.5

⁵⁵
 F.25
 22.5

23

✓

¹⁵
 3.6
 5.1

⁶¹
 F.25
 22.5

33

✓

¹⁵
 4.3
 5.8

⁹⁴
 F.51
 30.3

42

X

Sta. + π - Grade.

910.86

33

06.7

+35

06.4

34

06.5

+ π
+35

06.6

T.P. #1

13.24

910.86
921.89

2.11

908.75

30+00

08.0

+50

08.5

31+00

08.6

+50

08.4

Lt.

£

Rt.

3

$$\begin{array}{r} 15 \\ 4.2 \\ 5.7 \end{array}$$

$$\begin{array}{r} 13.6 \\ F.9.4 \\ \hline 43.2 \end{array}$$

45

$$\begin{array}{r} 92 \\ F.50 \\ \hline 300 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 4.5 \\ 6.0 \end{array}$$

$$\begin{array}{r} 13.8 \\ F.9.3 \\ \hline 42.1 \end{array}$$

47

$$\begin{array}{r} 10.6 \\ F.61 \\ \hline 33.3 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 4.4 \\ 5.9 \end{array}$$

$$\begin{array}{r} 9.1 \\ F.4.7 \\ \hline 29.1 \end{array}$$

39

$$\begin{array}{r} 59 \\ D.C.00 \\ \hline 22.1 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 4.3 \\ 5.8 \end{array}$$

$$\begin{array}{r} 7.3 \\ F.30 \\ \hline 24.0 \end{array}$$

38

$$\begin{array}{r} 5.8 \\ D.C.00 \\ \hline 24.0 \end{array}$$

✓

Red Stk. 30

$$\begin{array}{r} 14.0 \\ 15.5 \end{array}$$

$$\begin{array}{r} 5.3 \\ D.C.7.2 \\ \hline 40.1 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 13.5 \\ 15.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ D.C.11.0 \\ \hline 56.5 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 13.4 \\ 14.9 \end{array}$$

$$\begin{array}{r} 3.0 \\ D.C.11.9 \\ \hline 59.2 \end{array}$$

✓

$$\begin{array}{r} 15 \\ 13.6 \\ 15.1 \end{array}$$

$$\begin{array}{r} 3.3 \\ D.C.11.8 \\ \hline 58.9 \end{array}$$

✓

Sta.	+	π	-	Grade
------	---	-------	---	-------

921.99[✓]

32				07.8
----	--	--	--	------

+50				07.1
-----	--	--	--	------

B.M.		14.80	907.19 [✓]	907.22
------	--	-------	---------------------	--------

<u>See #1</u>				
T.P.K	3.25	914.00 [✓]		908.75

25				07.6
----	--	--	--	------

+50				07.1
-----	--	--	--	------

26				06.6
----	--	--	--	------

+50				06.1
-----	--	--	--	------

27				05.6
----	--	--	--	------

Lt.

£

Rt.

4

15
14.2 ✓
15.7

2.2
DC 13.5 ✓
64.0

15
14.9 ✓
16.4

2.3
DC 91 ✓
50.8

15
4.4 ✓
5.9

4.3
DC 1.6 ✓
38.3

2.3
DC 2.9 ✓
23.7

15
4.9 ✓
6.4

2.9
DC 3.5 ✓
34.0

4.4

2.0
DC 4.4 ✓
36.7

15
5.4 ✓
6.9

4.2 ✓
DC 2.7 ✓
31.6

5.0

1.9
DC 5.0 ✓
38.5

15
5.9 ✓
7.4

3.0
DC 2.4 ✓
30.7

2.0
DC 4.8 ✓
37.9

15
6.4 ✓
7.9

3.8
DC 2.4 ✓
22.2

3.6
DC 4.3 ✓
36.4

Sta.	+	π ✓	-	Grade
------	---	---------	---	-------

27+50

05.4

+75

05.4

28

05.5

+50

05.9

T.P. #4

5.89

906.11 ✓

Lt.

E

Rt.

5

¹⁵
 6.6.
 8.1

^{12.6}
 $\frac{F6.0}{33.0}$

6.3

^{9.1}
 $\frac{F2.5}{22.5}$ ✓

¹⁵
 6.6.
 8.1

X

¹⁵
 6.5.
 8.0

^{13.5}
 $\frac{F7.0}{36.0}$

6.1

^{12.7}
 $\frac{F6.2}{33.6}$ ✓

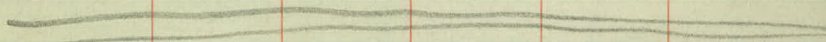
¹⁵
 6.1.
 7.6

^{9.5}
 $\frac{F3.4}{25.2}$ ✓

5.5

^{13.1}
 $\frac{F7.0}{36.0}$ ✓

Rod Sta 27+00



St. + K - Grade.

B.M. 3.55 924.82 ✓ 921.27

T.P. #5 7.85 925.17 ✓ 7.50 917.32 ✓

17

16.6

+50

17.3

+72

17.7

18

18.1

+50

18.7

T.P. 11.55 930.79 ✓ 5.93 919.24 ✓

19

18.9

+45

18.8

Lt.

E

Rt.

6.4

Spike in 18" Oak 60' Lt. Sta. 10+15

Red. Sta 17+00

$$\begin{array}{r} 15 \\ 8.6 \\ 10.1 \end{array}$$

$$\begin{array}{r} 10.0 \\ DC 0.0 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC 3.7 \\ \hline 34.6 \end{array}$$

$$\begin{array}{r} 15 \\ 7.9 \\ 9.4 \end{array}$$

$$\begin{array}{r} 11.9 \\ F 4.0 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ DC 1.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 15 \\ 7.5 \\ 9.0 \end{array}$$

$$\begin{array}{r} 12.7 \\ F 5.2 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 7.6 \\ DC 1.4 \\ \hline 27.7 \end{array}$$

$$\begin{array}{r} 15 \\ 7.1 \\ 8.6 \end{array}$$

$$\begin{array}{r} 10.0 \\ F 2.9 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 3.3 \\ DC 5.3 \\ \hline 39.4 \end{array}$$

$$\begin{array}{r} 15 \\ 6.5 \\ 8.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ DC 1.1 \\ \hline 26.3 \end{array}$$

$$\begin{array}{r} 1.6 \\ DC 6.4 \\ \hline 42.7 \end{array}$$

Red Sta. 19

$$\begin{array}{r} 15 \\ 11.9 \\ 13.4 \end{array}$$

$$\begin{array}{r} 12.3 \\ DC 1.4 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC 9.1 \\ \hline 50.8 \end{array}$$

$$\begin{array}{r} 12.0 \\ 13.5 \end{array}$$

$$\begin{array}{r} 11.2 \\ DC 2.3 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 1.3 \\ DC 12.2 \\ \hline 60.1 \end{array}$$

Sta. + Σ - Grade
930.79

20 18.4

+50 17.5

T.P. 348 921.53 12.74 918.05
20+80 16.5

21 16.4

+25 15.7

T.P. #3 13.70 921.53 13.70 907.83

+50 15.1

T.P. #2 14.83 927.18 7.18 914.35

22 13.8

+50 12.5

23
T.P. 1.70 915.55 14.83 914.35

23 11.2

Lt.

E

Rt.

7

$$\begin{array}{r} 12.4 \\ 13.9 \end{array}$$

$$\begin{array}{r} 6.7 \\ DC.72 \\ \hline 45.1 \end{array}$$

$$\begin{array}{r} 4.1 \\ DC.9.8 \\ \hline 52.9 \end{array}$$

$$\begin{array}{r} 13.3 \\ 14.8 \end{array}$$

$$\begin{array}{r} 13.1 \\ DC.1.7 \\ \hline 28.6 \\ 20 + 50 \end{array}$$

$$\begin{array}{r} 3.3 \\ DC.11.5 \\ \hline 58.0 \end{array}$$

Red sts 20 + 50

20 + 50

$$\begin{array}{r} 4.5 \\ 6.2 \\ 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 8.0 \\ F.2.9 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 5.6 \\ DC.0.6 \\ \hline 21.3 \\ 5.8 \\ F.1.7 \\ \hline 20.1 \end{array}$$

$$\begin{array}{r} 5.8 \\ 7.3 \end{array}$$

$$\begin{array}{r} 7.3 \\ DC.0.0 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 11.3 \\ F.5.5 \\ \hline 31.5 \end{array}$$

$$\begin{array}{r} 6.4 \\ 7.9 \end{array}$$

$$\begin{array}{r} 2.0 \\ DC.0.9 \\ \hline 26.2 \end{array}$$

Red sts. 22

$$\begin{array}{r} 13.4 \\ 14.9 \end{array}$$

$$\begin{array}{r} 2.9 \\ DC.12.0 \\ \hline 59.5 \end{array}$$

$$\begin{array}{r} 14.7 \\ 16.2 \end{array}$$

$$\begin{array}{r} 2.5 \\ DC.13.7 \\ \hline 64.6 \end{array}$$

$$\begin{array}{r} 16.0 \\ 17.5 \end{array}$$

$$\begin{array}{r} 13.3 \\ DC.4.2 \\ \hline 36.1 \end{array}$$

$$\begin{array}{r} 4.4 \\ 5.9 \end{array}$$

$$\begin{array}{r} 5.9 \\ DC.0.0 \\ \hline 25.3 \end{array}$$

Sta. + π - Grade

915.55[✓]

23+50

9.9
~~10.9~~

24

09.0

+33

08.5

T.P. #4

9.42

906.13[✓]

906.11

Lt.

£

Rt.

8

$$\begin{array}{r} 1.5 \\ 5.7 \\ 7.2 \end{array}$$

$$\begin{array}{r} 7.2 \\ 00.0 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 10.4 \\ F.4.7 \\ \hline 29.1 \end{array}$$

$$\begin{array}{r} 1.5 \\ 6.6 \\ 8.1 \end{array}$$

$$\begin{array}{r} 13.2 \\ F.6.6 \\ \hline 34.8 \end{array}$$

$$\begin{array}{r} 13.3 \\ F.6.7 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} 1.5 \\ 7.1 \\ 8.6 \end{array}$$

$$\begin{array}{r} 15.4 \\ F.8.3 \\ \hline 39.9 \end{array}$$

$$\begin{array}{r} 13.2 \\ F.6.1 \\ \hline 33.3 \end{array}$$

check O.K - See T.R. #4 Sta. 27+00

Sta.	+	π	-	Grade
✓ see T.P. #3	0.16	907.99 ✓		907.83

21+50				15.1
-------	--	--	--	------

22				13.8
----	--	--	--	------

+50				12.5
-----	--	--	--	------

T.P.	12.80	916.94 ✓	38.5	904.14 ✓
------	-------	----------	------	----------

T.P.			261	914.33 ✓
------	--	--	-----	----------

Lt.

L

Rt

9

+ 7.1 .

$$\begin{array}{r} 6.2 \\ F.13.3 \\ \hline 54.9 \end{array}$$

+ 5.8 .

$$\begin{array}{r} 15.5 \\ F.21.3 \\ \hline 78.9 \end{array}$$

+ 4.5 .

$$\begin{array}{r} 2.1 \\ F.6.6 \\ \hline 54.8 \end{array}$$

= T.P.R. ✓

914.35

Red Sta. 22 ✓

Sta.	+	K	-	Grade.
B.M.	0.17	921.39		921.27
T.P.	1.31	909.54	13.16	908.73
+50				20.9

8+00	19.9
+20	19.7

+50	18.9
-----	------

9	17.9
---	------

+50	16.9
-----	------

10	16.0
----	------

+33	15.6
-----	------

+75	14.9
-----	------

Lt.

L

Rt.

10

Spike in 18" Oak 60' Lt. Sta. 10+15

+11.4 .

+10.4
+10.2 .

+9.4 .

+8.4 .

+7.4 .

+6.5 .

+6.1 .

+5.4 .

$$\begin{array}{r} 3.5 \\ F. 13.7 \\ \hline 16.1 \end{array}$$

$$\begin{array}{r} 6.9 \\ F. 16.3 \\ \hline 23.9 \end{array}$$

$$\begin{array}{r} 8.4 \\ F. 16.8 \\ \hline 25.4 \end{array}$$

$$\begin{array}{r} 11.7 \\ F. 19.1 \\ \hline 32.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ F. 11.5 \\ \hline 16.5 \end{array}$$

$$\begin{array}{r} 1.2 \\ F. 7.3 \\ \hline 36.9 \end{array}$$

$$\begin{array}{r} +3.9 \\ F. 1.5 \\ \hline 19.5 \end{array}$$

Sto. + K - Grade.

909.54 ✓

11 14.8

+50 14.3

+70 14.3

12 14.2

T.P. 12.07 920.04 ✓ 1.57 907.57 ✓

+22 14.2

+50 14.2

T.P. 12.76 931.54 ✓ 1.28 918.76 ✓

T.P. 10.65 938.17 ✓ 4.00 927.52 ✓

13 14.3

+25 14.3

Lt.

Lt.

Rt.

X 11

+5.3.

$$\begin{array}{r} F.6.6 \\ \hline 34.8 \end{array}$$

+4.8.

$$\begin{array}{r} 12.4 \\ \hline F.17.2 \\ \hline 66.6 \end{array}$$

+4.8.

$$\begin{array}{r} 927.52 \\ 10.65 \\ \hline 938.17 \end{array}$$

$$\begin{array}{r} 8.7 \\ \hline F.13.5 \\ \hline 55.5 \end{array}$$

+4.7.

$$\begin{array}{r} 38.2 \\ 14.3 \\ \hline 23.9 \end{array}$$

$$\begin{array}{r} 2.5 \\ \hline F.12.2 \\ \hline 51.6 \end{array}$$

$$\begin{array}{r} 15 \\ 5.8 \\ \hline 7.3 \end{array}$$

$$\begin{array}{r} 2.3 \\ \hline D.C.0.0 \\ \hline 31.4 \end{array}$$

12+80

$$\begin{array}{r} 6.7 \\ \hline D.C.18.7 \\ \hline 796 \end{array}$$

$$\begin{array}{r} 15 \\ 5.8 \\ \hline 7.3 \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline D.C.0.0 \\ \hline 29.9 \end{array}$$

$$\begin{array}{r} 15 \\ 23.9 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 4.1 \\ \hline D.C.21.3 \\ \hline 87.4 \end{array}$$

$$\begin{array}{r} 23.9 \\ 25.4 \end{array}$$

Sta. + π - Grade.

938.17

13+50

14.4

+80

14.5

14

14.5

+50

14.6

T.P.

0.37

929.60

8.94

929.23

15

14.8

+50

15.0

16

15.4

+50

15.9

T.P.

17.28

917.32

O.K.
(917.32)

Lt.

E

Rt.

12

1.5
23.8.
25.3

1.9
D.C. 23.4
93.7

23.7.
25.2

X

1.5
23.7.
25.2

2.7
D.C. 23.0
97.5

1.5
23.6.
25.1

6.9
D.C. 18.2
78.1

Rock

1.5
14.8.
16.3

0.1
D.C. 16.2
22.1

1.5
14.6.
16.1

2.6
D.C. 14.5
67.0

1.5
14.2.
15.7

7.4
D.C. 8.3
48.4

1.5
13.7.
15.2

10.3
D.C. 4.9
38.2

Sta.	+	π	-	Elev.
B.M.	5.66	946.93		921.27
+10				20.9
8				19.9
+20				19.7
+50				18.9
9				17.9
+50				16.9
10				16.0
+33				15.6

Lt.

E

Rt.

13

Spike in 18" Oak 60' Lt. 5/5 10+15

$$\begin{array}{r} 1.5 \\ 6.0 \\ 7.5 \end{array}$$

$$\begin{array}{r} 1.5 \\ 7.0 \\ 8.5 \end{array}$$

$$\begin{array}{r} 8.5 \\ 11.5 \\ \hline 19.5 \end{array}$$

$$\begin{array}{r} 1.5 \\ 7.2 \\ 8.7 \end{array}$$

$$\begin{array}{r} 1.5 \\ 8.0 \\ 9.5 \end{array}$$

$$\begin{array}{r} 2.8 \\ 26.2 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 1.5 \\ 9.0 \\ 10.5 \end{array}$$

$$\begin{array}{r} 6.9 \\ 27.4 \\ \hline 34.3 \end{array}$$

$$\begin{array}{r} 1.5 \\ 10.0 \\ 11.5 \end{array}$$

$$\begin{array}{r} 11.5 \\ 16.0 \\ \hline 27.1 \end{array}$$

$$\begin{array}{r} 1.5 \\ 10.9 \\ 12.4 \end{array}$$

$$\begin{array}{r} 12.4 \\ 13.6 \\ \hline 26.0 \end{array}$$

$$\begin{array}{r} 1.5 \\ 11.3 \\ 12.8 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33.1 \\ \hline 40.3 \end{array}$$

Sta. + K - Grade.

10+75 976.93 14.9

11 14.8

T.P. 1.41 916.09 12.75 914.68

+50 1.0 14.3

+70 1.15 14.3

12 2.0 14.2

T.P. 0.48 903.57 13.00 903.09

+22 2.5 14.2

+50 3.0 14.2

13 2.0 14.3

T.P. 1.15 904.78 0.48 903.09

+25 1.1 14.3

LY.

E

Rt.

14

17.0.
13.5

4.
DC9.4
51.7

17.1.
13.6

38
DC9.8
52.9

1.8.
3.3

3.3
DC0.0
41.7

1.8.
3.3

3.3
DC0.0
47.6

1.9.

12.9
F11.0
50.0

+ 10.6.

4.6
F11.2
63.1

+ 10.6.

6.3
F16.9
68.7

+ 10.7.

8.0
F18.7
73.1

Sta. + π - Grade.

904.78

13+50

1.0

14.4

+80

0.5

14.5

14

14.5

+50

14.6

15

14.8

T.P.

11.92

915.90

0.30

903.98

+50

15.0

16

15.4

+50

T.P.

6.14

921.37

0.67

915.73

T.P.

4.04

917.33

OK.

917.32

4

E

B.

15

+10.1.

$$\begin{array}{r} 10.5 \\ \hline F. 20.6 \\ \hline 77.8 \end{array}$$

+10.2.

X

+10.2.

$$\begin{array}{r} 9.9 \\ \hline F. 20.1 \\ \hline 75.3 \end{array}$$

+10.3.

$$\begin{array}{r} 6.0 \\ \hline F. 16.3 \\ \hline 63.9 \end{array}$$

+10.5.

$$\begin{array}{r} 10.1 \\ \hline F. 10.4 \\ \hline 46.2 \end{array}$$

0.9.

$$\begin{array}{r} 4.5 \\ \hline F. 3.8 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} F. 3.6 \\ \hline 25.8 \end{array}$$

0.5.

$$\begin{array}{r} 3.5 \\ \hline F. 3.0 \\ \hline 24.0 \end{array}$$

0.0.

X - Cut out ^{Shoulder} slope too wide

Sto.

+

π

-

Grado.

11+94.4 4'X7' Stone Arch Culv.

Ext. 30' Lt. + 40' Rt.

White Bear Road.

Preliminary cross-sections
between Sta 8+50 and 16 to be
used in conjunction with road
plan and slope stake notes.

12/37

Sta.	+	Σ	-	Elev.
B.M.	4.19	925.46.		921.27
10				16.0
+33				15.7
+75				15.5
11				15.2
T.P. #1	4.03	919.93.	9.56	915.90.
+50				14.6
+70				14.6
12				14.2
+22				14.0
+60				14.3
13				14.7
+25				14.8

Lt.

E

Rt.

21

$$\frac{10.0}{28} \quad \frac{11.4}{24} \quad \frac{11.6}{20} \quad \frac{10.8}{15} \quad \frac{10.0}{12} \quad \frac{9.5}{11} \quad \frac{9.8}{16}$$

$$\frac{7.4}{29} \quad \frac{11.0}{25} \quad \frac{12.0}{22} \quad \frac{12.1}{18} \quad \frac{10.6}{15} \quad \frac{10.1}{11} \quad \frac{9.8}{16} \quad \frac{10.1}{16}$$

$$\frac{3.7}{43} \quad \frac{27}{39} \quad \frac{10.9}{30} \quad \frac{11.9}{27} \quad \frac{12.1}{23} \quad \frac{10.8}{20} \quad \frac{10.5}{17} \quad \frac{10.3}{11} \quad \frac{10.0}{15} \quad \frac{10.2}{15} \quad \frac{11.6}{20}$$

$$\frac{2.6}{49} \quad \frac{9.0}{40} \quad \frac{9.5}{31} \quad \frac{12.5}{26} \quad \frac{12.5}{24} \quad \frac{10.6}{21} \quad \frac{10.3}{17} \quad \frac{10.2}{11} \quad \frac{10.7}{15} \quad \frac{13.5}{28}$$

$$\frac{7.2}{41.7} \quad \frac{10.2}{36} \quad \frac{11.2}{34} \quad \frac{8.7}{31} \quad \frac{7.9}{30} \quad \frac{5.5}{24} \quad \frac{5.3}{24} \quad \frac{5.6}{14}$$

$$\frac{7.0}{47.6} \quad \frac{13.4}{39} \quad \frac{10.5}{35} \quad \frac{5.4}{22} \quad \frac{5.3}{22} \quad \frac{5.6}{14}$$

$$\frac{5.9}{24} \quad \frac{5.7}{21} \quad \frac{5.3}{18} \quad \frac{6.7}{27}$$

$$\frac{6.3}{27} \quad \frac{5.9}{29} \quad \frac{5.2}{22} \quad \frac{5.8}{27} \quad \frac{7.2}{31.4}$$

$$\frac{6.3}{25} \quad \frac{5.6}{24} \quad \frac{5.2}{24} \quad \frac{7.1}{30} \quad \frac{8.5}{34} \quad \frac{9.0}{49}$$

$$\frac{6.4}{32} \quad \frac{5.2}{17} \quad \frac{5.3}{17} \quad \frac{7.7}{22} \quad \frac{7.5}{33}$$

$$\frac{6.2}{34} \quad \frac{5.1}{14} \quad \frac{5.4}{14} \quad \frac{6.3}{18} \quad \frac{6.1}{27}$$

Sta.	+	K	-	Elev.
13+50		919.93		14.7

+80				14.9
-----	--	--	--	------

14				15.0
----	--	--	--	------

+50				15.2
-----	--	--	--	------

15				15.6
----	--	--	--	------

+50				15.9
-----	--	--	--	------

16				16.3
----	--	--	--	------

T.P.			3.55	916.38
------	--	--	------	--------

T.P.	0.22	909.60	13.55	909.38
------	------	--------	-------	--------

12				14.2
----	--	--	--	------

+22				14.0
-----	--	--	--	------

+50				14.3
-----	--	--	--	------

13				14.7
----	--	--	--	------

+50				14.7
-----	--	--	--	------

Lt.

L

Rt.

3

$$\begin{array}{r} 6.4 \\ 34 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 5.4 \\ 14 \end{array} \quad \begin{array}{r} 3.5 \\ 26 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 2.7 \\ 31 \end{array}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 4.9 \\ 13 \end{array} \quad \begin{array}{r} 5.1 \\ 13 \end{array} \quad \begin{array}{r} 3.5 \\ 27 \end{array}$$

$$\begin{array}{r} 6.0 \\ 31 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 22 \end{array}$$

$$\begin{array}{r} 5.0 \\ 23 \end{array} \quad \begin{array}{r} 4.3 \\ 12 \end{array} \quad \begin{array}{r} 4.7 \\ 12 \end{array} \quad \begin{array}{r} 3.8 \\ 19 \end{array} \quad \begin{array}{r} 1.9 \\ 26 \end{array}$$

$$\begin{array}{r} 4.5 \\ 23 \end{array} \quad \begin{array}{r} 4.0 \\ 11 \end{array} \quad \begin{array}{r} 4.1 \\ 11 \end{array} \quad \begin{array}{r} 3.5 \\ 22 \end{array}$$

$$\begin{array}{r} 7.4 \\ 24 \end{array} \quad \begin{array}{r} 4.2 \\ 17 \end{array} \quad \begin{array}{r} 3.6 \\ 14 \end{array} \quad \begin{array}{r} 3.8 \\ 14 \end{array} \quad \begin{array}{r} 4.4 \\ 20 \end{array} \quad \begin{array}{r} 3.8 \\ 28 \end{array}$$

Red. Sta. 16+00

$$\begin{array}{r} 3.4 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 47 \end{array} \quad \begin{array}{r} 4.8 \\ 44 \end{array}$$

$$\begin{array}{r} 7.4 \\ 63.1 \end{array} \quad \begin{array}{r} 6.7 \\ 47 \end{array}$$

$$\begin{array}{r} 9.3 \\ 68.7 \end{array} \quad \begin{array}{r} 9.5 \\ 55 \end{array}$$

$$\begin{array}{r} 10.8 \\ 73.1 \end{array} \quad \begin{array}{r} 10.2 \\ 62 \end{array}$$

$$\begin{array}{r} 12.8 \\ 77.8 \end{array} \quad \begin{array}{r} 11.3 \\ 64 \end{array}$$

Sta.	+	π	-	Elev.
14		909.60		15.0

+50

15.2

15

15.6

T.P.

13.75

930.13

916.38

16

16.3

15+50

15.9

15

15.6

14+50

15.2

T.P.

11.12

939.06

927.94

14

15.0

13+50

14.7

13

14.7

12+80

Lt.

E

Rt.

4

$$\frac{12.1}{25.3}$$

$$\frac{10.2}{58}$$

$$\frac{8.2}{63.9}$$

$$\frac{5.6}{47}$$

$$\frac{2.0}{46.2}$$

$$\frac{0.2}{38}$$

Red. Sta. 16+00

$$\frac{9.4}{35} \quad \frac{7.9}{48.4}$$

$$\frac{8.7}{59} \quad \frac{2.1}{67}$$

$$\frac{6.6}{35} \quad \frac{0.6}{22.1}$$

$$\frac{6.3}{36} \quad \frac{2.7}{58}$$

$$\frac{11.3}{47} \quad \frac{8.5}{63} \quad \frac{3.0}{92.5}$$

$$\frac{11.7}{44} \quad \frac{8.7}{63} \quad \frac{2.7}{92.7}$$

$$\frac{10.7}{55} \quad \frac{9.3}{59} \quad \frac{4.9}{87.4}$$

$$\frac{8.5}{69} \quad \frac{7.5}{79.6}$$

Sta.	+	K	-	Elev.
T.P.#1	1.90	917.80		915.90
T.P.	1.36	910.81	8.35	908.45
8+50				

9

+50

10

16.0

+33

15.7

11

15.2

+50

14.6

+70

14.6

12

14.2

Lt.

E

Rt.

5

$$\begin{array}{r} 8.2 \\ 63.9 \end{array} \quad \begin{array}{r} 74 \\ 31 \end{array} \quad \begin{array}{r} 2.7 \\ 34 \end{array} \quad \begin{array}{r} \text{Shoulder} \\ 7.1 \end{array}$$

$$\begin{array}{r} 9.5 \\ 65.4 \end{array} \quad \begin{array}{r} 5.4 \\ 40 \end{array} \quad \begin{array}{r} 3.1 \\ 35 \end{array} \quad \begin{array}{r} 17.0 \end{array}$$

$$\begin{array}{r} 12.9 \\ 72.4 \end{array} \quad \begin{array}{r} 11.1 \\ 61 \end{array} \quad \begin{array}{r} 8.9 \\ 54 \end{array} \quad \begin{array}{r} 4.5 \\ 35 \end{array} \quad \begin{array}{r} 17.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ 49.5 \end{array} \quad \begin{array}{r} 2.6 \\ 32 \end{array}$$

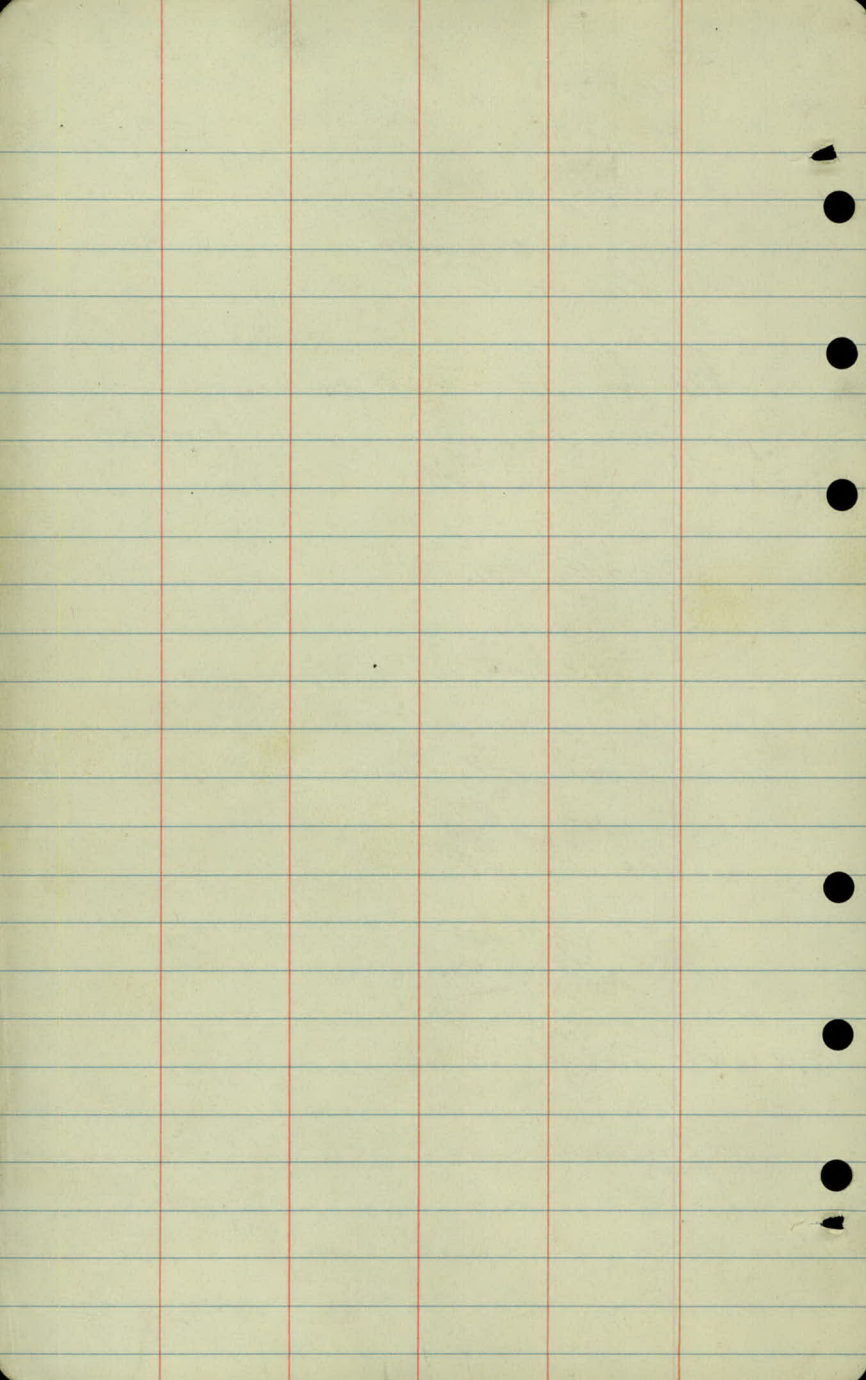
$$\begin{array}{r} 2.3 \\ 36.9 \end{array} \quad \begin{array}{r} 0.0 \\ 25 \end{array}$$

$$\begin{array}{r} 2.5 \\ 34.8 \end{array} \quad \begin{array}{r} 1.2 \\ 27 \end{array}$$

$$\begin{array}{r} 13.6 \\ 66.6 \end{array} \quad \begin{array}{r} 13.8 \\ 52 \end{array} \quad \begin{array}{r} 12.6 \\ 39 \end{array} \quad 3.8$$

$$\begin{array}{r} 9.9 \\ 55.5 \end{array} \quad \begin{array}{r} 13.2 \\ 44 \end{array} \quad \begin{array}{r} 13.6 \\ 34 \end{array} \quad 3.8$$

$$\begin{array}{r} 8.8 \\ 51.6 \end{array} \quad \begin{array}{r} 9.8 \\ 48 \end{array} \quad \begin{array}{r} 9.3 \\ 44 \end{array} \quad \begin{array}{r} 4.0 \\ 40 \end{array} \quad \begin{array}{r} 2.9 \\ 34 \end{array}$$



Profile of
Prosperity Ave
from
Frost Ave North
to RR Tracks

Sta	+	π	-	Elev	
34+50	8.78	108.78		100.00	Assumed
36+00			7.3	101.5	
36+50			6.7	102.0	
37			6.1	102.7	
+50			5.1	103.7	
38			3.5	105.3	
+50			2.5	106.3	
39			2.3	106.5	
TP,	3.30	108.93	3.15	105.63	
39+50			2.5	106.4	106.3
40			3.5	105.4	✓
+50			4.1	104.8	
41			4.4	104.5	
+50			4.7	104.2	104.3
42			4.7	104.2	104.0
+50			5.1	103.8	✓
43			5.3	103.6	103.8
+50			5.2	103.7	
44			5.1	103.8	

RG
KP
JS

May 18, 1959
P. C. L., Cool

2

£ Frost & Prosperity Aves.

Rock

Sta	+	π	-	Elev	
		108.93			
44+50			4.9	104.0	
TP ₂	3.49	107.21	5.21	103.72	
45+00			3.4	103.8	
+50			3.8	103.4	
46			4.2	103.0	
+50			4.5	102.7	
47			4.7	102.5	102.3
+50			5.3	101.9	
48			5.2	102.0	
+50			5.0	102.2	
49			4.6	102.6	102.3
+50			4.6	102.6	102.4
50			4.7	102.5	102.48
+50			4.6	102.6	102.55
51			4.4	102.8	102.5
+50			4.6	102.6	102.4
52+00	Approx		4.75	102.46	102.3
TP ₃	506	109.15	3.12	104.09	

Rock

RR Tracks (S. rail.)

MH $\pm$ Pros. Sta 44+50

Sta	+	π	-	E/cv
-----	---	-------	---	------

		109.15		
--	--	--------	--	--

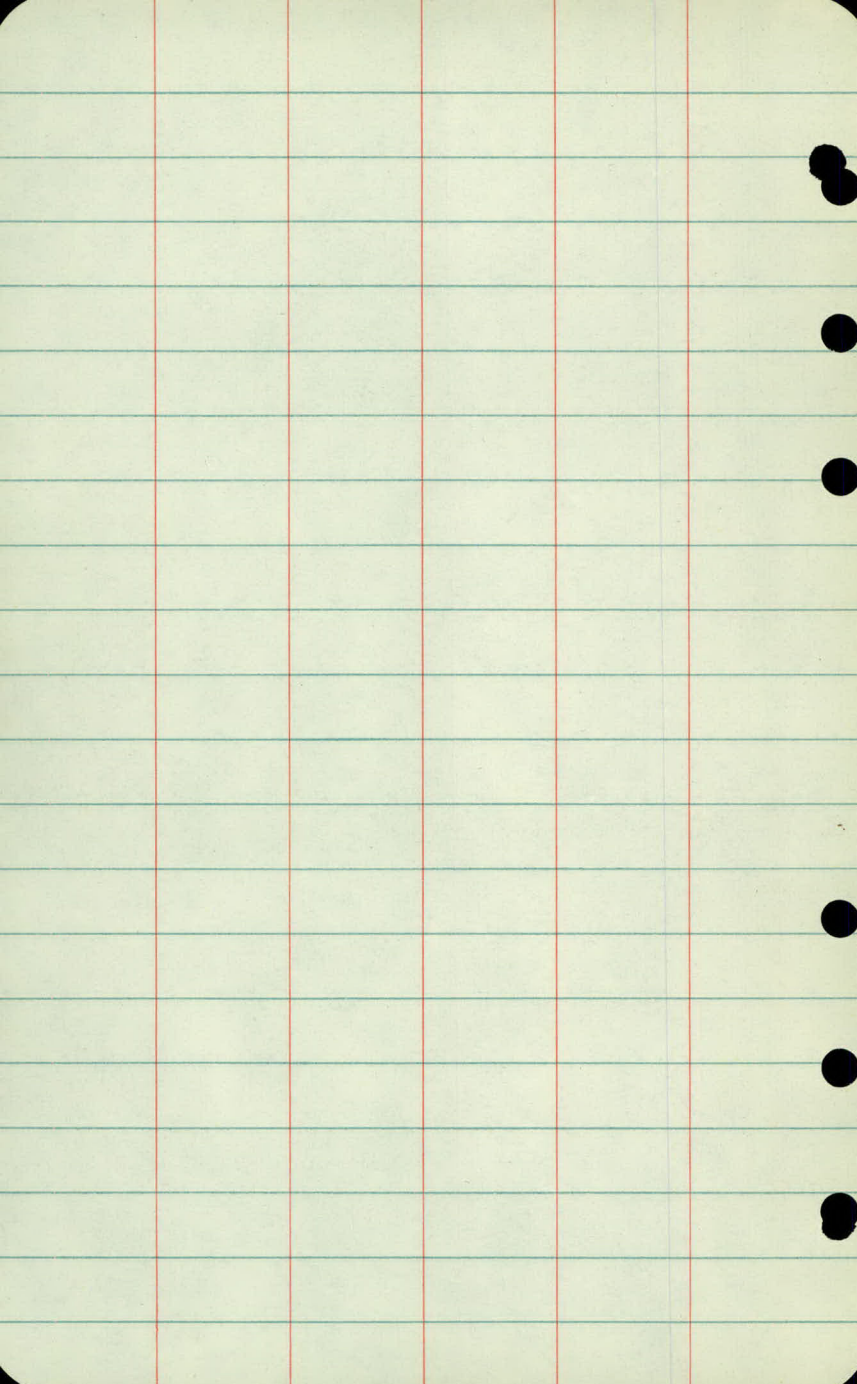
TP 4	1.97	109.10	3.02	107.13
------	------	--------	------	--------

34+50			8.09	100.01
-------	--	--	------	--------

100.00

ROCK

4 Frost & Prosperity Aves.



PROSPERITY ROAD
Frost Ave to Co RD 8.
STAKING

Sta	+	π	-	Elev
BM	7.82	107.82		100.00
	P6	P6R		
35+50	01.0	6.7		
36	01.5	6.3		
+50	02.0	5.8		
37	02.7	5.1		
+50	03.7	4.1		
38	05.3	2.5		
+50	06.3	1.5		
39	06.5	1.3		
TP ₁	3.42	109.94	1.30	106.52

MAY 18, 1959

2.

Lf

±

Rf

± Frost & Prosperity

15'
(6.7
BT)

15'
(6.7
BT)

(6.3
BT)

(6.3
BT)

(5.8
BT)

✓

(5.1
BT)

(5.1
BT)

(4.1
BT)

(4.1
BT)

(2.5
BT)

(2.5
BT)

(1.5
BT)

(1.5
BT)

(1.3
BT)

(1.3
BT)

rock

Sta		T		
		109.94		
	P6	P6R	ELEV	
39	06.5	3.4		
+50	06.3	3.6		
40	05.4	4.5		
+50	04.8	5.1		
41	04.5	5.4		
+50	04.3	5.6		
42	04.0	5.9		
+50	03.8	6.1		
TP ₂	4.82	108.66	6.10	103.84

MAY 18. 1959

Lt

£

Rt

3.

15'

15'

3.4 ✓

(3.6
BT)

(3.6
BT)

(4.5
BT)

(4.5
BT)

✓

(5.1
BT)

(5.4
BT)

(5.4
BT)

(5.6
BT)

✓

(5.9
BT)

(5.9
BT)

(6.1
BT)

(6.1
BT)

Stake

Sta		π	ELEV
		108.66	
40+00	05.4	3.26	
43	03.6	5.1	
+50	03.7	5.0	
44	03.8	4.9	
+50	04.0	4.7	
45	03.8	4.9	
TP ₃	3.32	106.78	5.20 / 103.46
45+00	03.8	03.0	
+50	03.4	3.4	

MAY 18, 1959

Lt.

L

Rt

4.

15'

✓

3.26

15'

(5.1
BT)

(5.1
BT)

(5.0
BT)

(5.0
BT)

(4.9
BT)

(4.9
BT)

(4.7
BT)

(4.7
BT)

(4.9
BT)

(4.9
BT)

Top 12" CM (North End) ^{Sta} 45+00

✓

3.01

Sta	T		Elev.
		106.78	
46	03.0	3.8	
+50	02.7	4.1	
47	02.5	4.3	
+50	01.9	4.9	
48	02.0	4.8	
+50	02.2	4.6	
49	02.6	4.2	
+50	02.6	4.2	
50	02.5	4.3	
+50	02.6	4.2	

Lt

E

Rt

5.

15'

15'

(3.8)
BT

(4.1)
BT

(4.3)
BT

(4.9)
BT

(4.8)
BT

(4.6)
BT

(4.2)
BT

(4.2)
BT

(4.3)
BT

(4.2)
BT

Sta

π

Elev

106.78

51

02.5

4.3

+50

02.4

4.4

52

02.3

4.5

TP

4.25

102.53

102.46

18 MAY 1959

Lt

~~E~~

Rt

15'

15'

(9.4
BT)

LS. RR track

Sta	+	T	-	Elev	
BM	4.51	106.97			(102.46)
TP3			3.58	103.39	(103.46)
45	03.8	3.2			
+50	03.8	3.2			
46	03.0	4.0			
+50	02.7	4.3			
47	02.5	4.5			
+50	01.9	5.4			
48	02.0	5.0			
+50	02.2	4.8			
49	02.6	4.4			

RG
KP
US

Lt

E

MAY 19, 1959

Rt

S. track

N. end 12" CM Sta 45+00

(3.2
BT)

(3.2
BT)

(4.3
BT)

(4.5
BT)

(5.1
BT)

(5.0
BT)

(9.8
BT)

Sta + A - Elev

106.97

49+50 02.6 4.4

50 02.5 4.5

+50 02.6 4.4

51 02.5 4.5

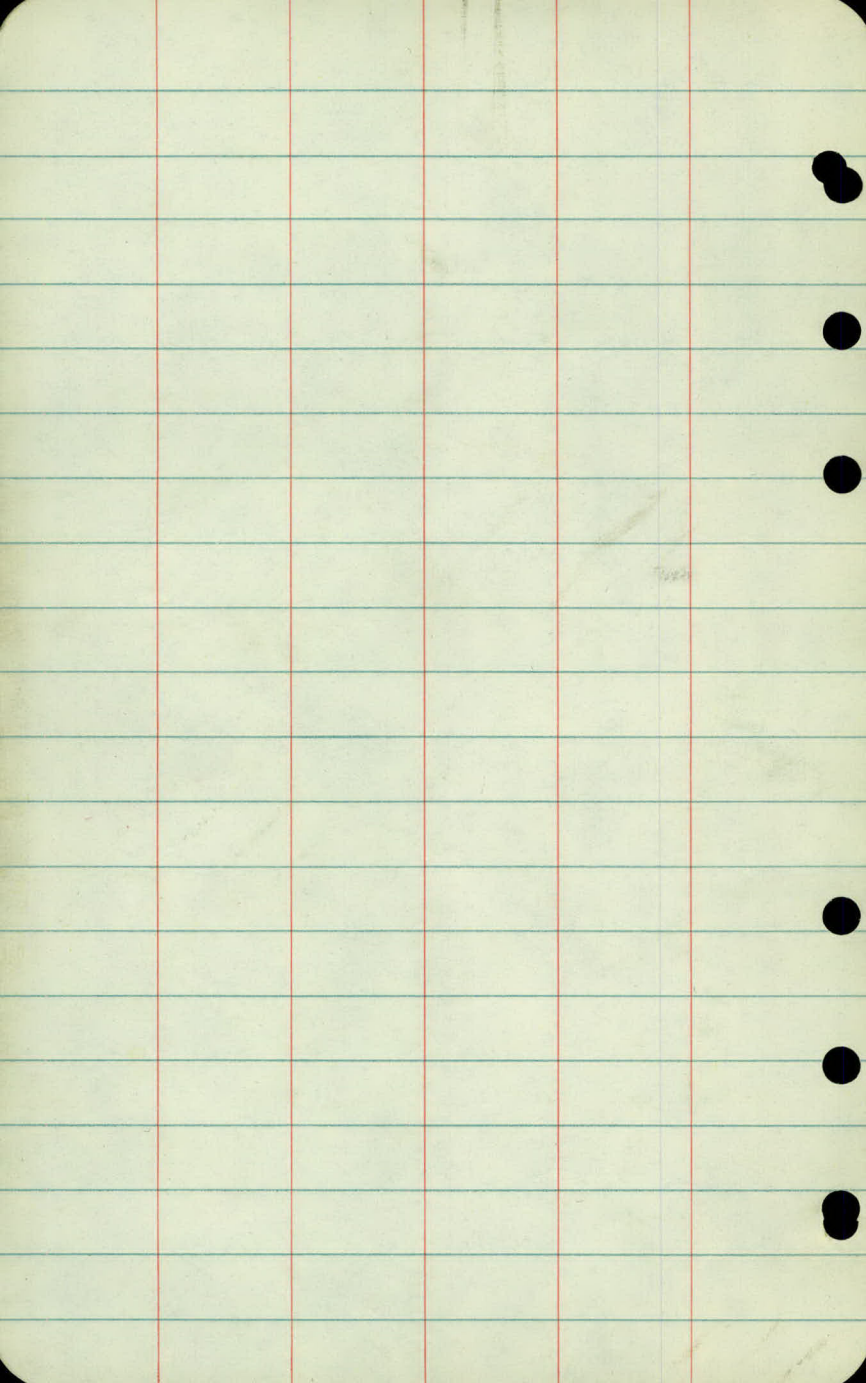
+50 02.4 4.6

52 02.3 4.7

Lt

£

Rt



RG
JL
FS

April 5, 1961

1

Ditch Profile

vicinity Ho #2026 Prosperity Ave. (East side)

0+00 = 16' south of South 12 R Track

4 pages

Sta + π - Elev

0+00 Top So. end 18" cm

+51

+51 Top No. end 15" cm

+77 Top So. end 15" cm

1+00

+50

2+00 Top No. end 18" cm

+40 Top So. end 18" cm

+77 Top No. end 15" cm

3+08 Top So. end 15" cm

2
104.5
4.25

00.15
4.10

99.80
4.45

99.83
4.42

99.75
4.50

99.82
4.43

99.92
4.33

99.83
4.42

99.72
4.53

SH/L Top am
99.5 Ditch Ditch ②
(FL 7.00)
4.8 5.50 97.25 97.2 2.1

99.4
4.9 (FL 6.70) 97.55 97.9
5.45 6.4

99.4
4.9 (FL 6.30) 97.95 98.3
5.05 6.0

99.2
5.1 98.2
6.1

99.3
5.0 98.3
6.0

99.5
4.8 (FL 6.02) 98.23 99.2
4.52 5.1

99.9
4.4 (FL 5.79) 98.46 99.2
4.29 5.1

99.8
4.5 (FL 6.15) 98.10 98.7
4.90 5.6

99.6
4.7 (FL 6.39) 97.88 98.6
5.12 5.7

Sta + π - Elev

3+50

+81 Top No. end 15" cm

Driveway for House
2026 Prosperity Ave

4+00 Top So. end 15" cm

+50

+77 Top No. end 15" cm

5+06 Top So. end 15" cm

+50

6+00

7+00

F

5.1/2

TOPCM
Ditch

Ditch (3)

99.66

9.59

99.2

5.1

98.3

6.0

99.55

4.70

99.2

5.1

(FL 6.12)

4.87

6.1

98.2

99.49

4.76

99.2

5.1

(FL 6.28)

5.03

6.2

98.1

99.66

4.59

99.3

5.0

98.4

5.9

99.92

4.33

99.7

4.6

(FL 6.20)

4.95

5.8

98.5

99.95

4.30

99.7

4.6

(FL 6.04)

4.79

5.3

99.0

100.11

4.14

99.6

4.7

98.7

5.6

100.25

4.00

99.8

4.5

99.2

5.1

101.15

3.10

3.6

00.0

4.3

Sta	+	π	-	Elev
-----	---	-------	---	------

7+50				water runs south from here
------	--	--	--	----------------------------

8+50				
------	--	--	--	--

8

SH/d

Ditch

(4)

101.27
2.98

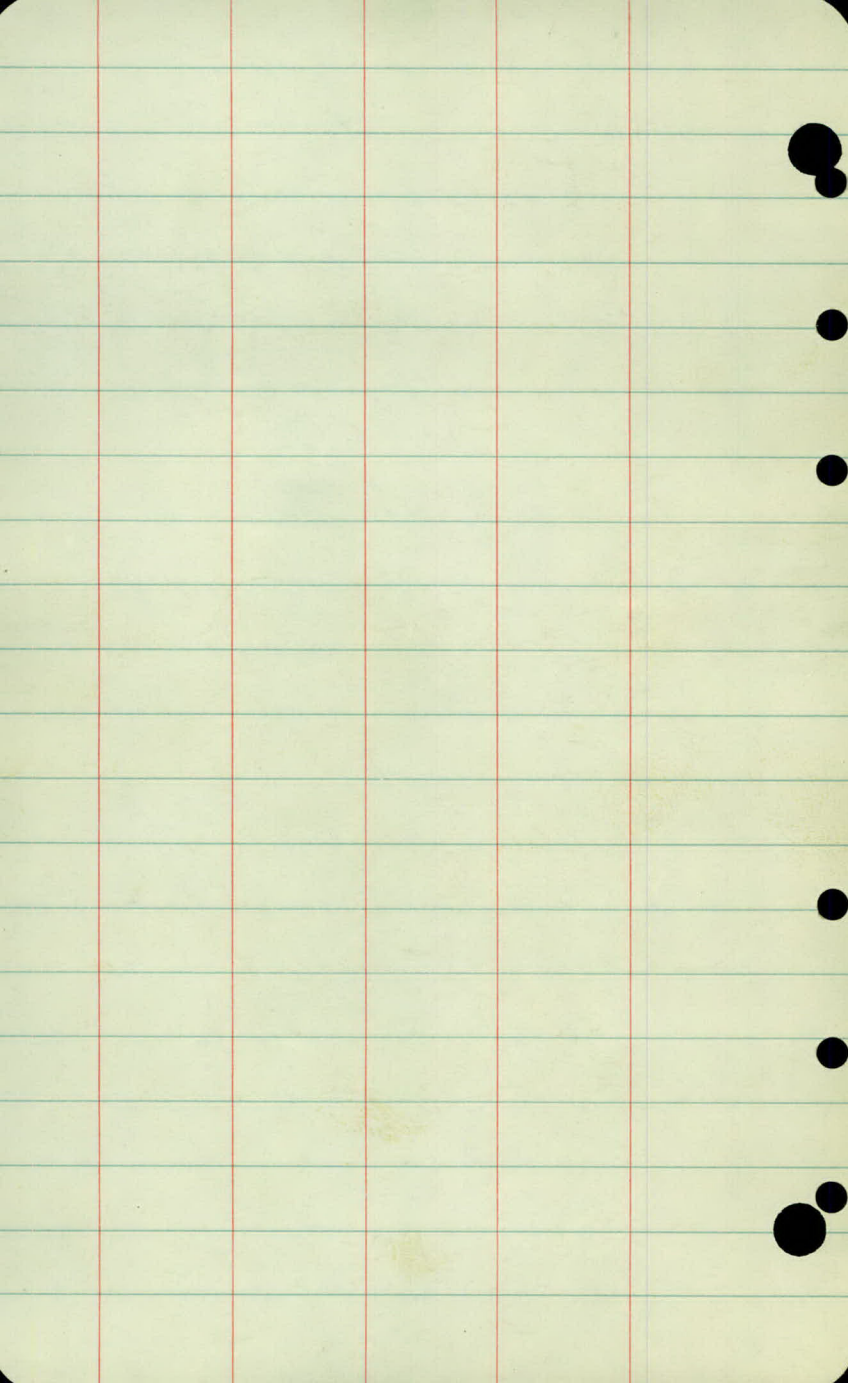
100.9
3.4

100.1
4.2

101.00
3.25

100.5
3.8

99.8
4.5



31 MAY 1961

KP
JS
FS
RB
EKDJR.

PROSPERITY ROAD
SOO LINE TRACKS TO FROST

DRAINAGE

0+00 = 390.3' S. OF SOO LINE TRACKS

STA	+	π	-	ELEV.
-----	---	-------	---	-------

BM	4.51	104.51		100.00
----	------	--------	--	--------

+00

+50

+77 FL S. END 15" CM

+97 FL N. END 15" CM

+100

+50

26.0

E

RT

E PROSPERITY ROAD AT STA. 0+00

100.0

4.5

5.8

99.8

4.7

98.3

6.2

99.7

4.8

97.98

6.53

FL 15"

99.7

4.8

97.82

6.69

FL 15"

99.7

4.8

98.5

6.0

99.3

5.2

97.9

6.6

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		104.51		
--	--	--------	--	--

1+74		FL SEND 15" CM		
------	--	----------------	--	--

+94		FL N. END 15" CM		
-----	--	------------------	--	--

2+00				
------	--	--	--	--

+50				
-----	--	--	--	--

+66		FL 15" CM S. END		
-----	--	------------------	--	--

+96		FL N. END 15" CM		
-----	--	------------------	--	--

31 MAY 1961

LT

£

RT

99.2

5.3

99.3

5.2

99.3

5.2

99.4

5.1

99.4

5.1

99.5

5.0

97.68

6.83

24.0

FL 15"

97.83

6.68

24.0

FL 15"

97.9

6.6

98.2

6.3

97.61

6.90

23.0

FL 15"

97.95

6.56

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		104.51		
--	--	--------	--	--

3+00				
------	--	--	--	--

+33	FL S. END 15" CM			
-----	------------------	--	--	--

+54	= $\cancel{E}$			
-----	----------------	--	--	--

+72	FL N. END 15" CM			
-----	------------------	--	--	--

4+00				
------	--	--	--	--

+50				
-----	--	--	--	--

+96	FL S. END 12" CM			
-----	------------------	--	--	--

31 MAY 1961

LT

±

RT

99.6

98.3

4.9

6.2

99.7

98.40

4.8

6.11

99.7

22.0

FL 15"

4.8

98.22

4.9

6.29

22.0

FL 15"

99.5

97.9

5.0

6.6

99.6

98.0

4.9

6.5

99.6

97.95

4.9

6.56

22.0

FL 12"

STA	+	T	-	ELEV.
-----	---	---	---	-------

		104.51		
--	--	--------	--	--

5+00				
------	--	--	--	--

+20	FL N. END 12" CM			
-----	------------------	--	--	--

+50				
-----	--	--	--	--

+60	FL 18" CM (UNDER ROAD)			
-----	------------------------	--	--	--

+83	FL 18" CM (UNDER ROAD)			
-----	------------------------	--	--	--

+90.3	± RR TRACKS			
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BM		4.53	99.98	
----	--	------	-------	--

				100.00
--	--	--	--	--------

31 MAY 1961

LT

£

RT

99.7

4.8

99.7

4.8

99.7

4.8

99.8

4.7

4.6

97.42

7.09

22.0

FL 12"

97.3

7.2

97.02

7.49

25
FL 18"

96.78

7.73

23.5

FL 18"

TOP ROAD & STA 0+00

