

Dr.6-BK.125

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN.....Survey

Long Lake Road.....

From S.T.H. #10..... To No. Co. Line.....

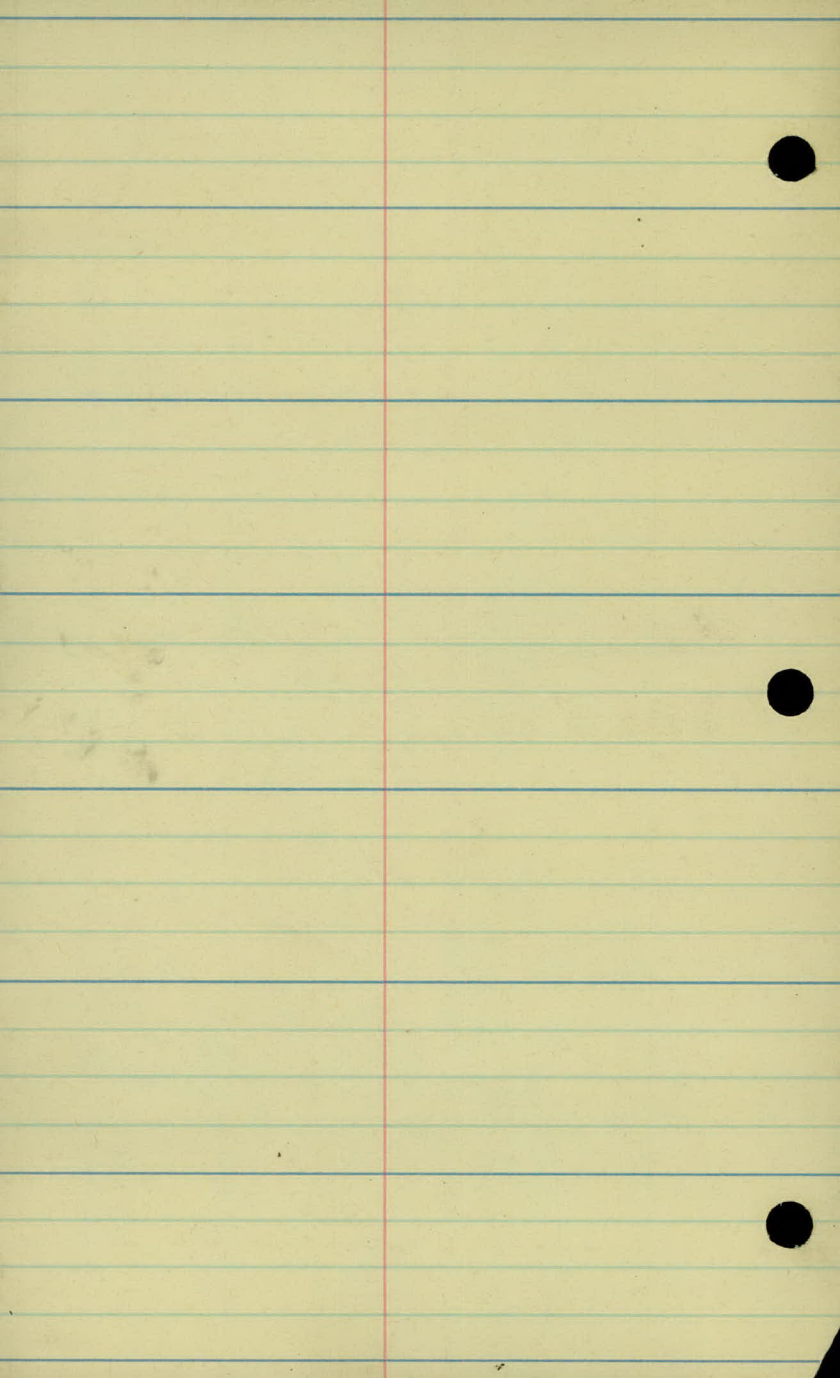
Road Acc't. No.

Date Filed 1937.....

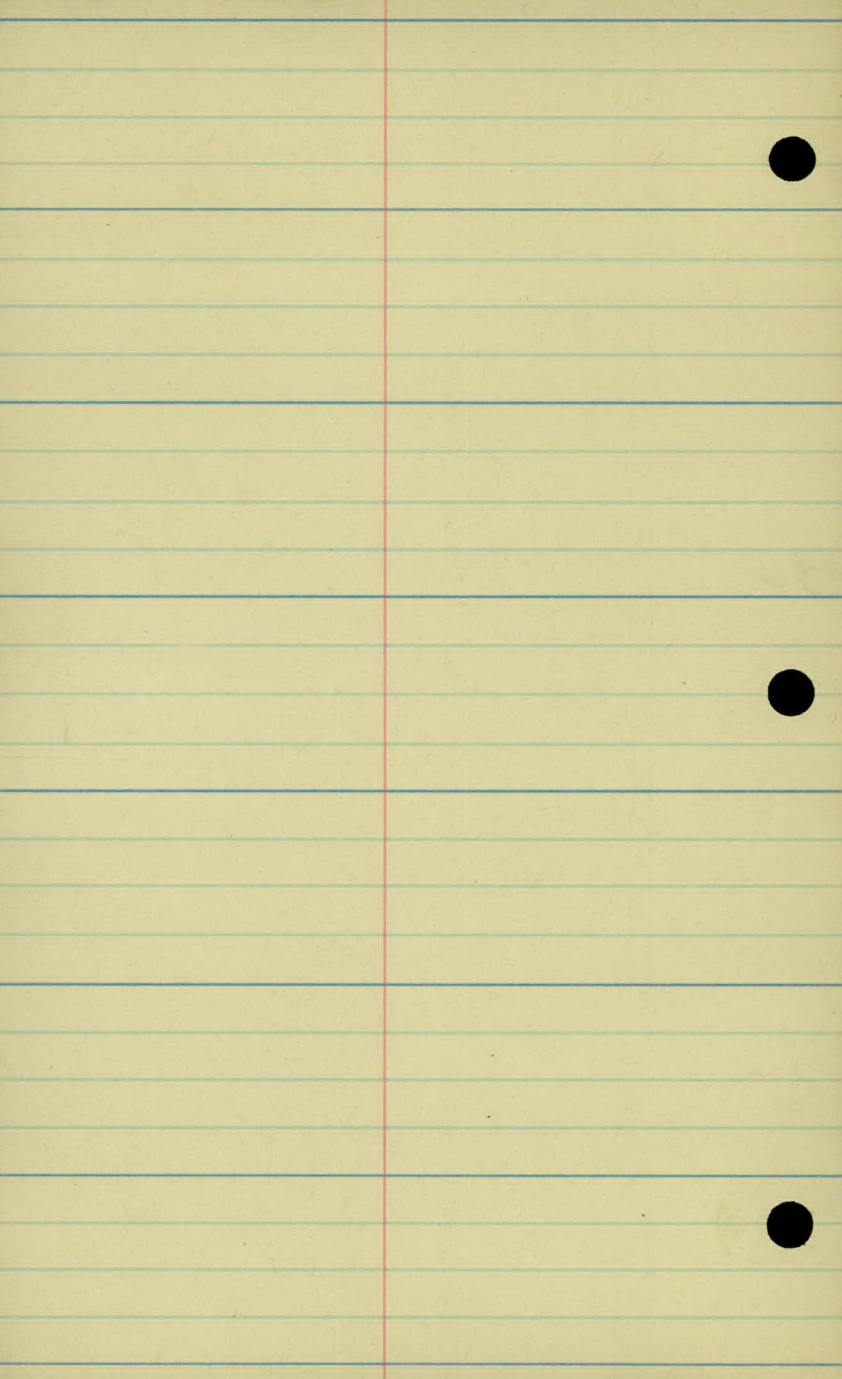
File

Page 3

Object	Asimuth	Stadia	Vertical	Red
30 Shoulder Rd W.	181° 55'	440		7.1
31 toe fill edge swamp	182° 45'	440		10.1
32 grey pole - Rd sign	182° 00'	438		7.1
33 P.P.	306° 00'	500		7.8
34 W. end X chain flow line	182° 00'	525		11.2
35 E end " "	178° 23'	530		11.5
36 P.P. edge swamp S.	303° 50'	315		10.6
37 Shoulder Rd W.	181° 25'	560		7.6
38 toe fill edge swamp	182° 00'	565		10.0
39 Shoulder Rd W. over culv.	306° 25'	290		7.4
40 toe fill flow line culv edge swamp	304° 45'	290		11.6
41 fence line	302° 45'	290		10.4
42 Shoulder Rd W.	181° 15'	680		8.2
43 toe fill edge swamp	181° 25'	680		10.0
44 Shoulder Rd W.	306° 30'	190		7.0
45 toe shoulder edge swamp	305° 25'	190		9.4
46 P.P.	300° 45'	195		9.7



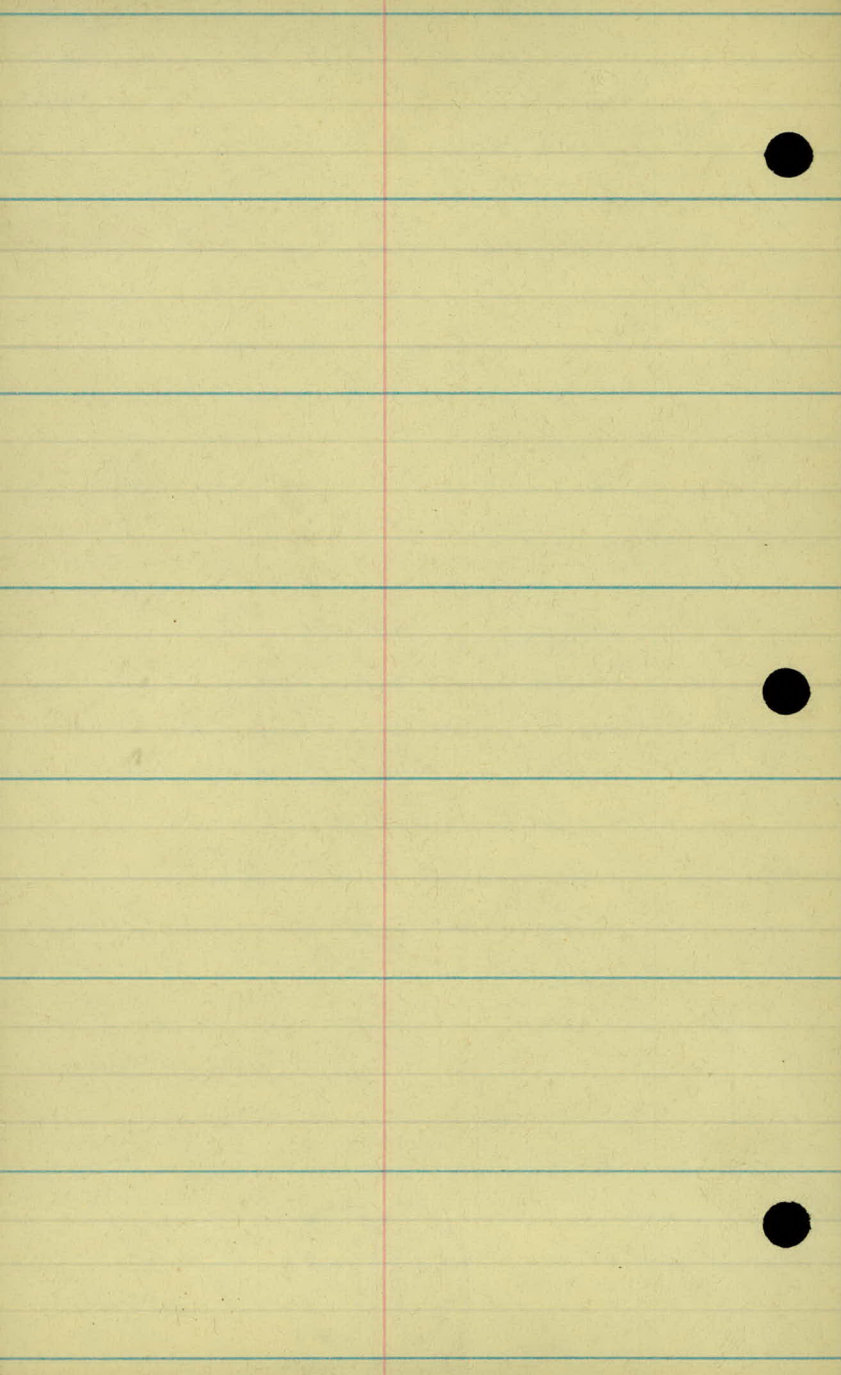
	Asimuth	Stadia	Vert	Red
40 P.P. to ^{swamp} shoulder edge	285°00'	70		8.4
41 X pt fence ^{at junction} - ^{pl. where}	271°10'	57		6.6
42 Shoulder Rd N.W.	275°15'	49		5.8
43 to slope knoll ^{SE cor brush} edge swamp	265°00'	88		9.0
44 W slope knoll	242°10'	93		7.7
45 E ditch	298°25'	310		12.0
46 Edge swamp E	239°25'	145		10.0
47 E. dge brush S.W. Cor' elev	294°15'	275		9.7
48 W. slope knoll	230°10'	130		7.7
49 Edge brush W Cor' elev	287°40'	342		9.6
50 E dge swamp E.	221°20'	210		9.7
51 W. slope knoll	216°55'	160		7.1
52 Edge brush N.W. Cor' elev	272°00'	360		9.5
53 " " N. edge needs	270°40'	300		9.5
54 15" tree on N. slope knoll	190°00'	180		6.1
55 Edge brush NE Cor' elev	270°20'	216		9.4
56 Edge " E	284°15'	170		9.2



Object

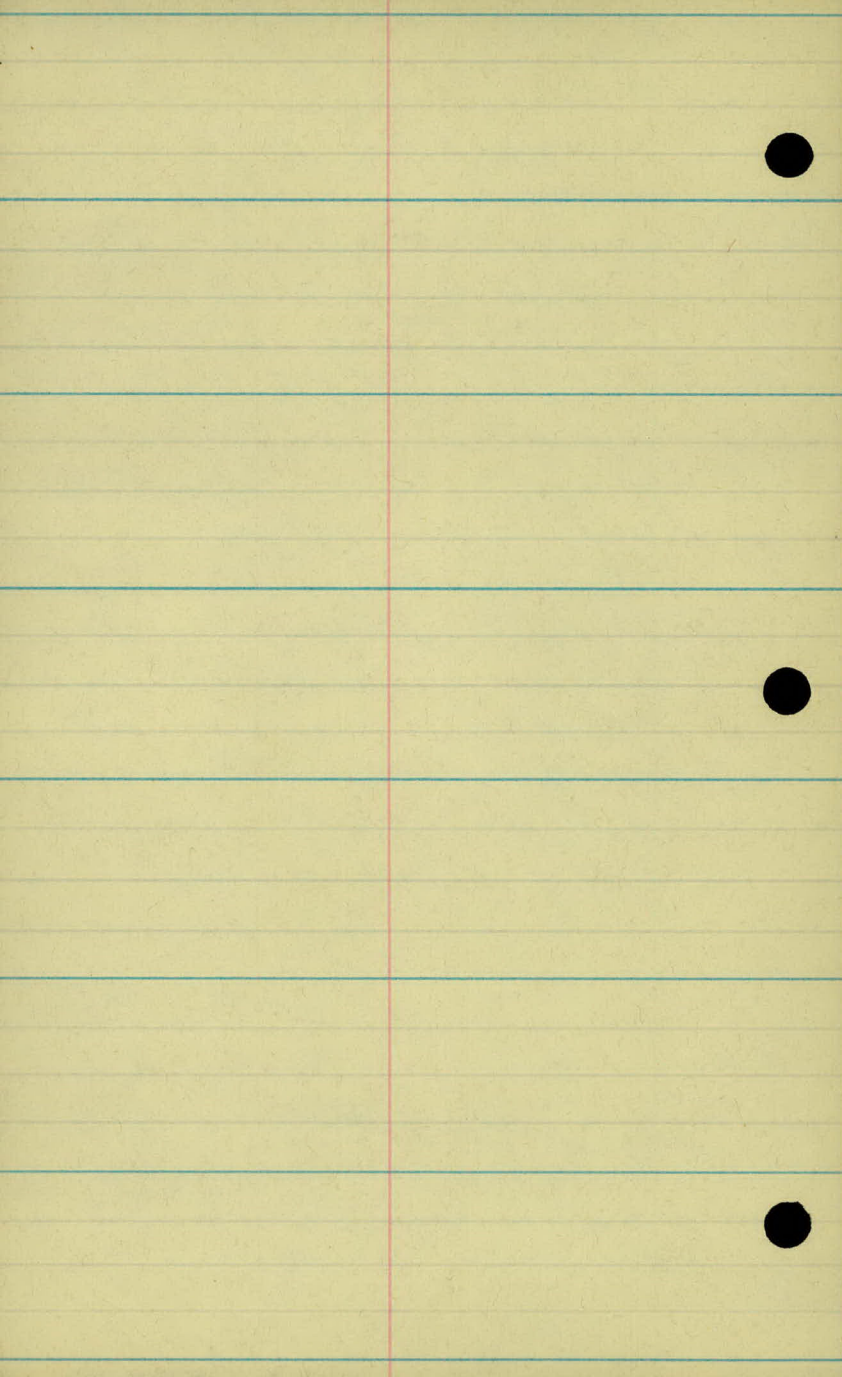
Object	Azimuth	Stadia	Vert.	Red
44 12" tree on N. slope	199°	178	+2°0'	12.9
45 Edge swamp E.	251°20'	100		9.7
46 8" tree on N. slope	204°15'	180		6.7
47 8" " " W.	206°30'	148		4.6
48 8" " " W.	210°45'	132		4.9
49 6" tree " " "	221°30'	144		6.2
50 pot hole in swamp low point	244°35'	170		11.2
51 pot hole in swamp " "	233°55'	200		12.0
52 Edge woods So.	260°45'	190		9.5
53 " " "	247°20'	220		10.5
To O. I. A.	240°16'	287		6.54

#

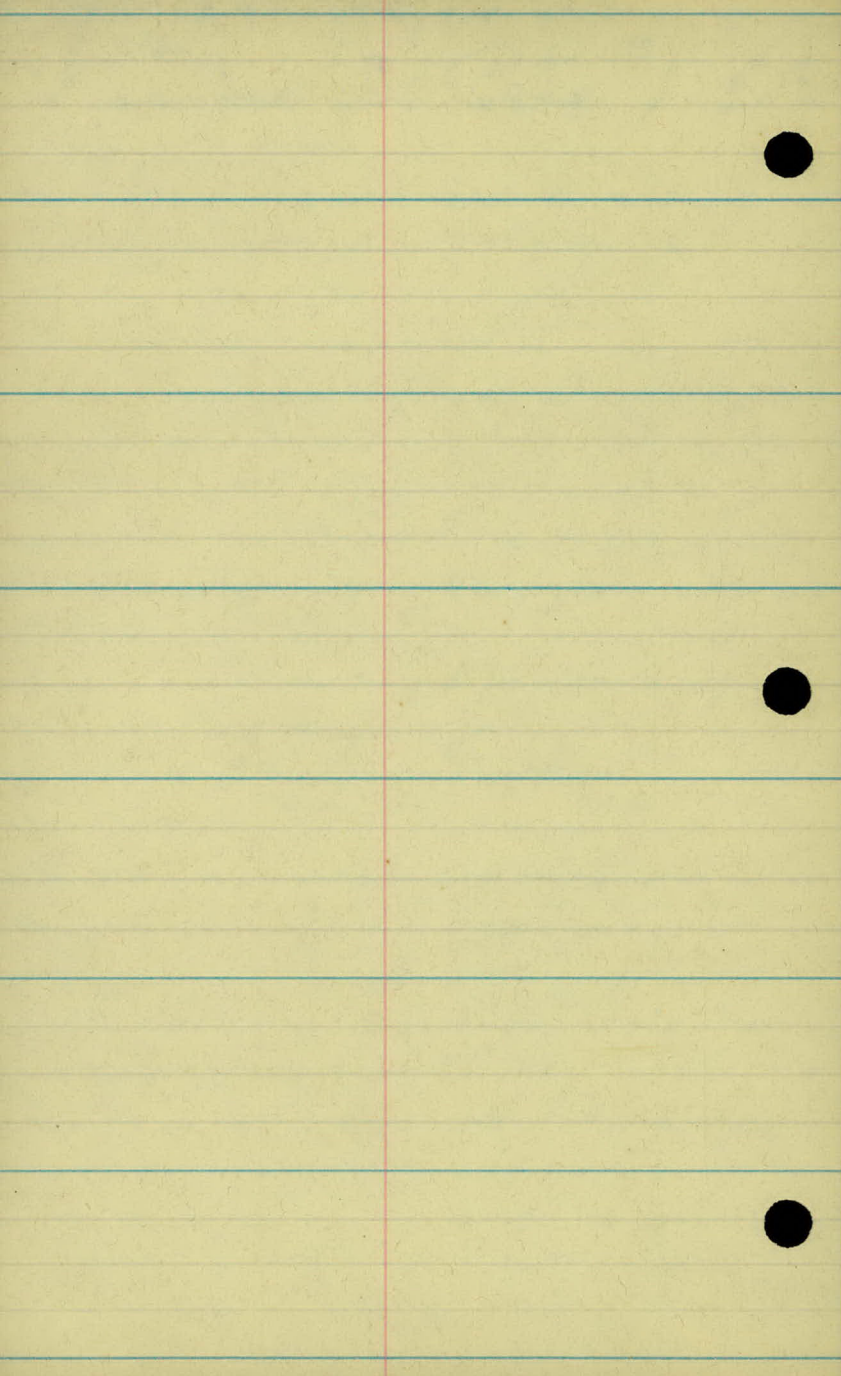


Object	Azimuth	Stadia	Vert	Red
A + O 1 A				
to O 1		287		
Elev				
H.I. = 5.25				
1 Toe slope Knoll E.	125° 15'	82		8.7
2 " " 5 E.	63° 15'	52		8.7
3 " " N.E.	160° 50'	96		8.6
4 " " 5 E.	25° 40'	51		8.7
5 " " 5 E.	35° 45'	81		8.8
6 Toe slope Knoll N.	195° 00'	120		8.5
7 " " 5.	350° 35'	100		8.4
8 " " N.	232° 35'	130		8.8
9 " " 5	321° 05'	115		9.3
10 " " 5 N.	314° 56'	153		9.2
11 " " N.W.	253° 35'	170		9.0
12 Elev on 5. slope Knoll	351° 15'	14		6.7

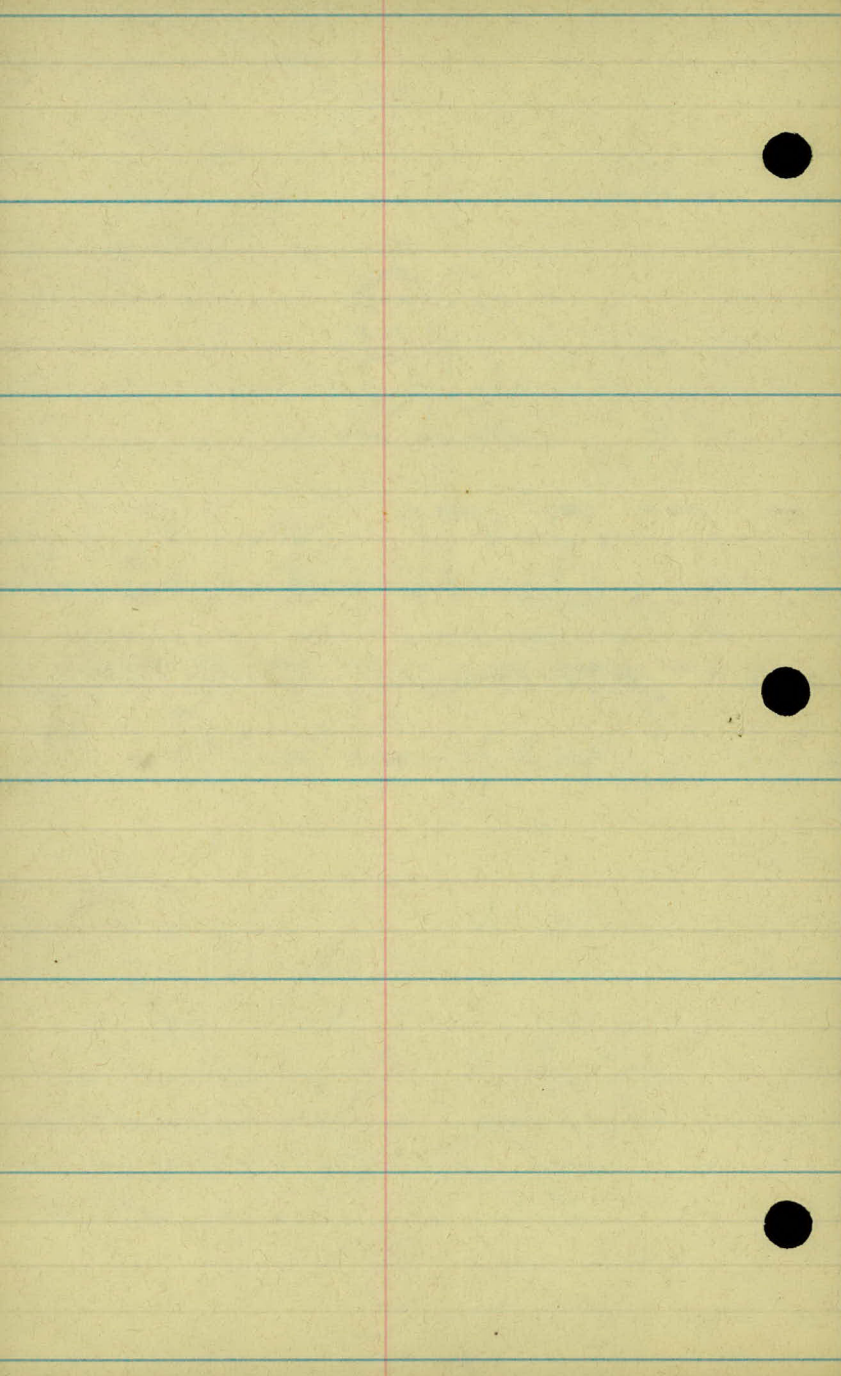
Knoll covered by these shots is quite heavily wooded



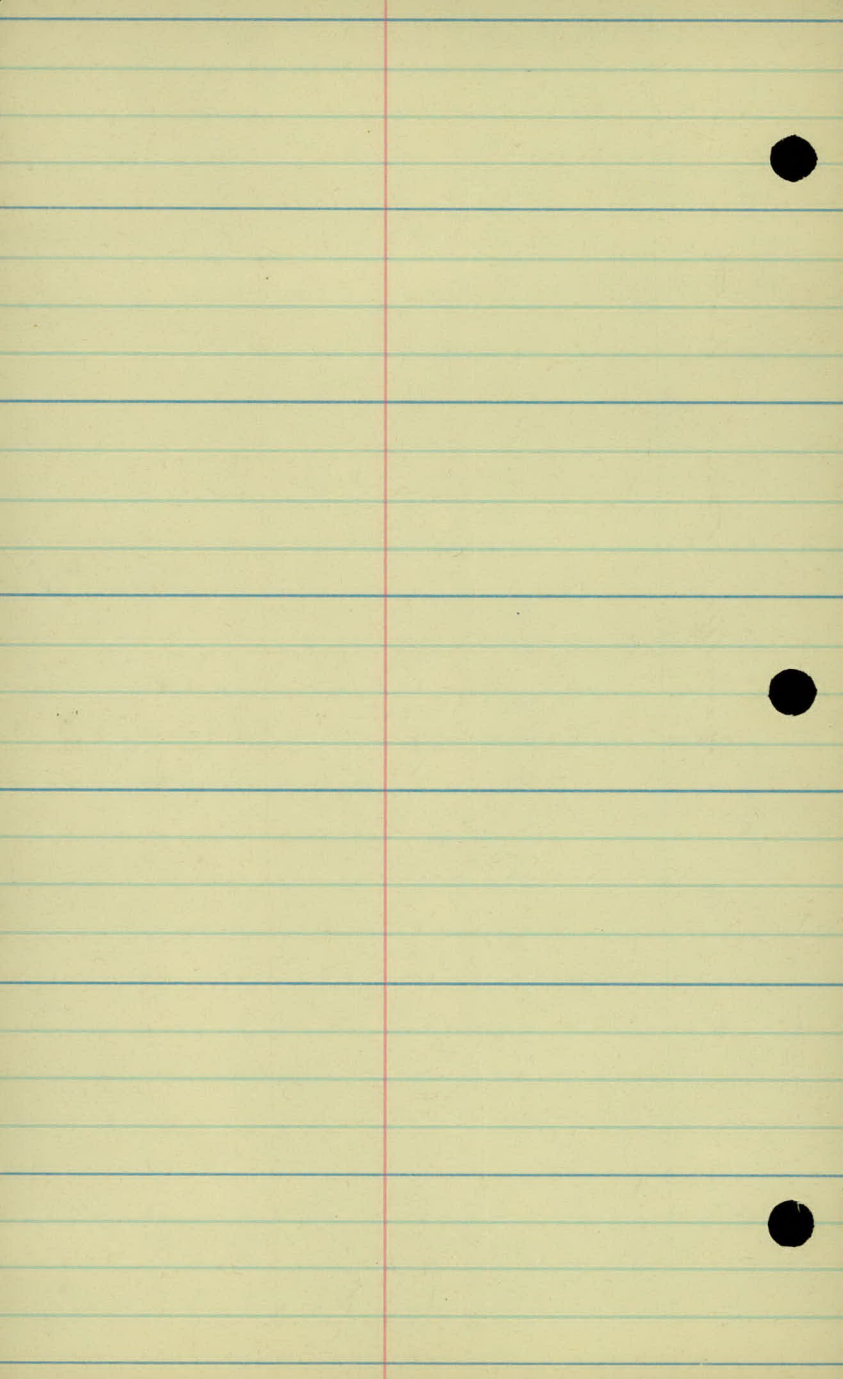
13 Cont'd	At 01 A		Azimuth	Stadia	Red
14 Elev on slope	Knoll	SE	93°20'	35	7.2
15 "	"	E	154°50'	45	7.7
16 Top	Knoll		241°30'	40	2.4
17 Elev on slope	Knoll	N.E.	189°15'	72	2.2
18 Top	Knoll		268°00'	63	3.1
19 Elev on slope	Knoll	N.	215°00'	81	6.7
20 "	"	N.	244°50'	90	7.1
21 Top	Knoll		281°40'	102	4.5
22 Elev on slope	Knoll	N.W.	267°20'	120	7.1
23 "	"	S.W.	302°45'	104	7.5
24 "	"	S	314°45'	50	7.3
25 "	"	S E	205°15'	9	4.6



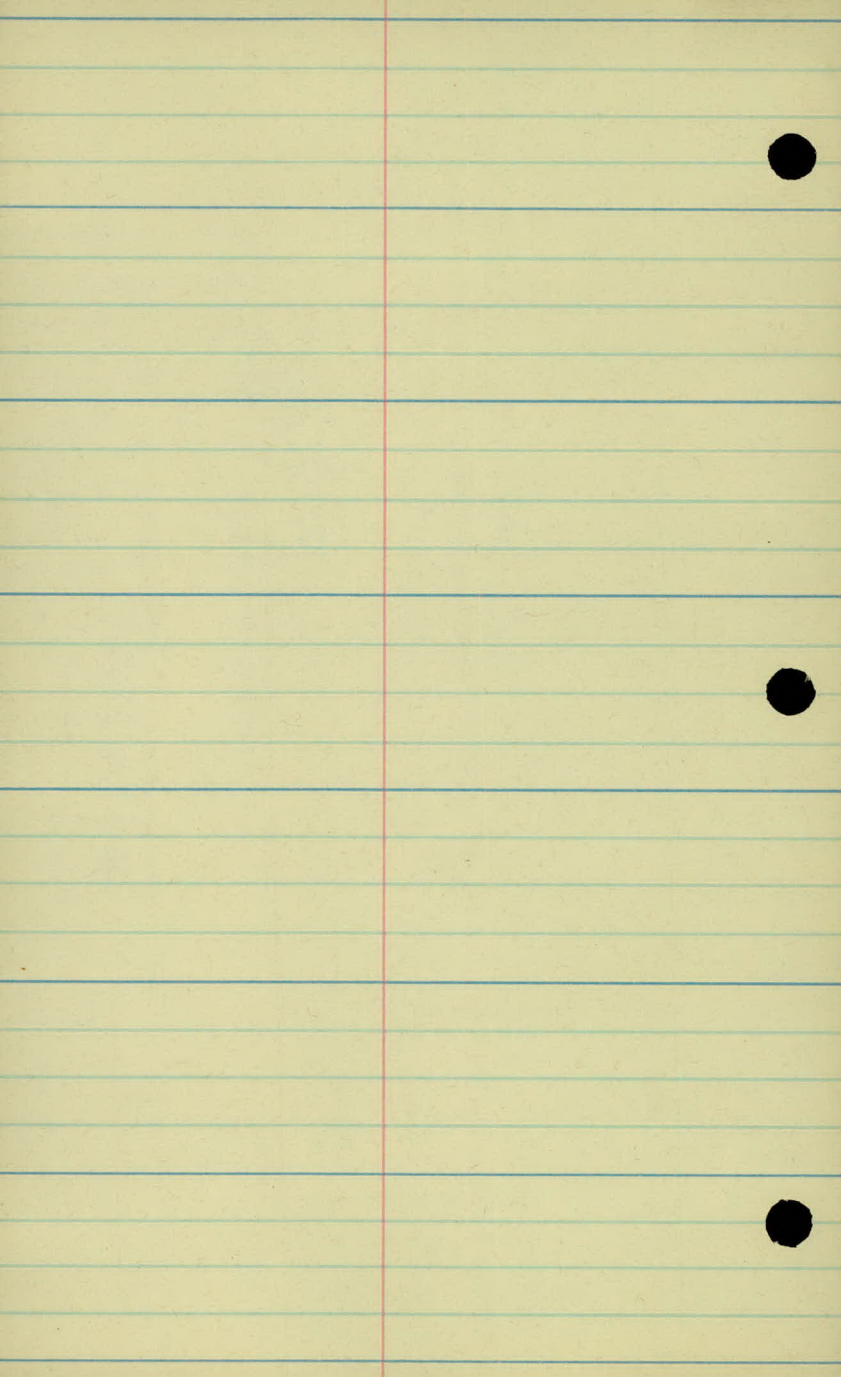
	Azimuth	Stadia	Vert	Red
A+02				
to 01		846		
to 03	169°26'	552		4.10
Elev =				
H.I. = 5.0				
Shoulder line E. Auto cut	0°55'	165		3.0
to shoulder in ditch	40°15'	162		5.2
top cut on knoll	70°00'	168		0.8
Shoulder line E side cut on	1°30'	106		4.1
to shoulder fill	6°-15'	110		6.3
Fence line	18°00'	110		7.1
Fence Cor,	8°-05'	242	+1°-15'	2.2
"	13°-15'	265	+1°-15'	2.3
Elev on NW slope	28°-10'	115		6.6
" " NW "	28°-15'	192	+1°-00'	2.0
" " NW "	32°-15'	142		6.0
top knoll on fence	36°-50'	225	+3°-45'	5.1



Can'ted @ 0 2	Azimuth	Stadia	Vert	Pod
Elev on N slope knoll	80°-30'	190		6.3
P.P. in ditch heading	37°-25'	230	+3°-10'	5.2
Elev on N. slope knoll	88°-40'	240		7.0
Shoulder R/W heading	32°-50'	235	+3°-45'	5.2
Top slope knoll edge swamp	95°-15'	232		10.2
Top knoll	60°-00'	240	+4°-15'	5.2
Top slope-knoll edge swamp	92°-15'	190		10.3
Top knoll fence line	60°-10'	230	+4°-15'	5.1
Top slope knoll edge swamp	83°-05'	145		10.4
Elev on N.W. slope knoll	55°-20'	186	+3°-30	5.0
Top slope edge swamp	60°-25'	113		10.2
Elev on N. slope knoll	70°-40'	200	+3°-15'	5.0
Top slope knoll edge swamp	39°-00'	98		10.3
Top fill edge swamp	14°-25'	66		9.8
Shoulder cut off	2°-15'	63		4.4
Gen'l in swamp	113°-15'	81		11.0
" "	112°-40'	203		10.8

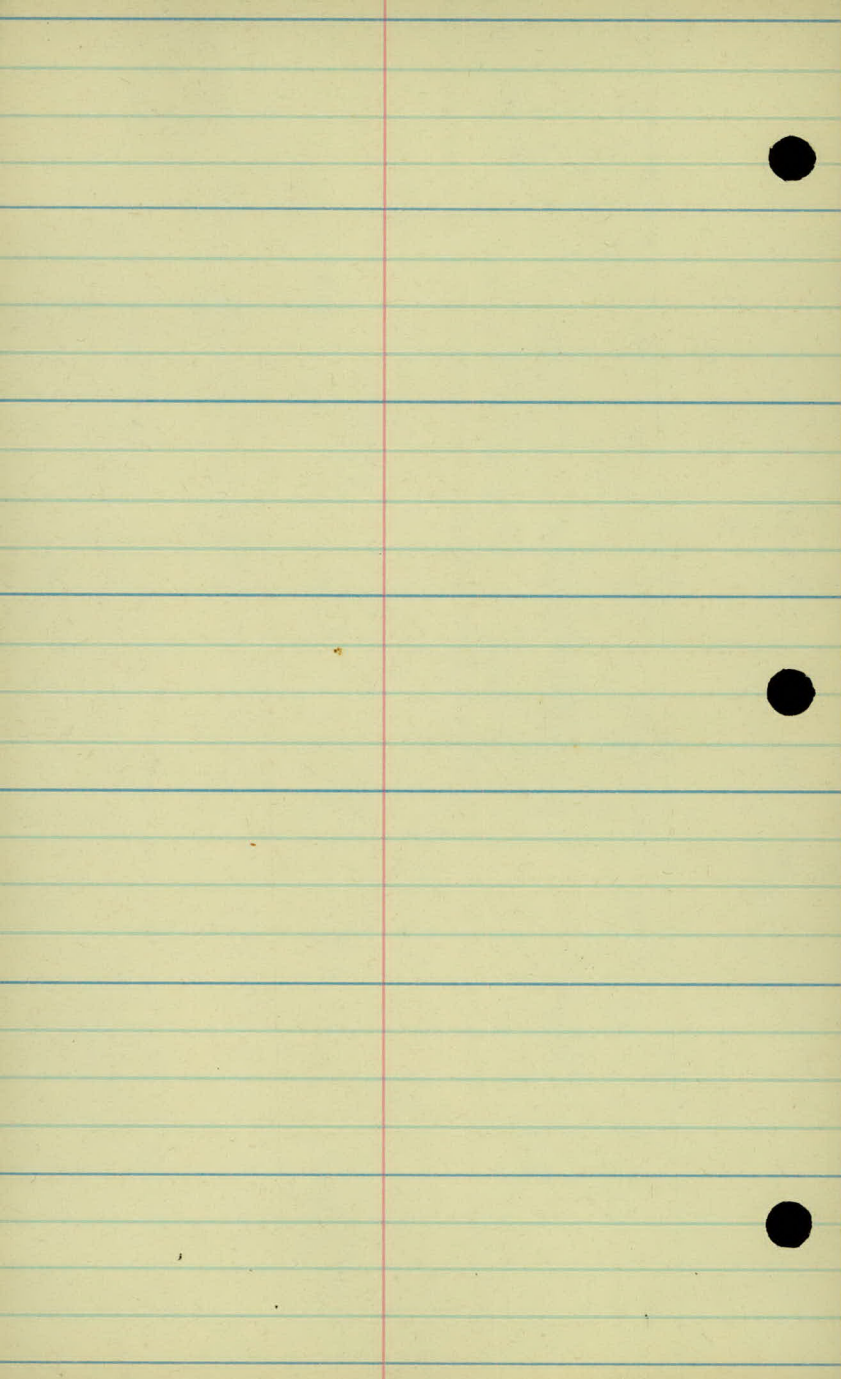


Cont'd @ 2	Azimuth	Stadia	Vert	Red
Shoulder cut off	167°-45'	17		5.4
Toe shoulder edge swamp	144-15	28		10.1
Gen'l in swamp	113°-00'	332		10.9
Shoulder cut-off	178°-45'	160		5.2
& ditch	120°-50'	480		12.6
Toe fill edge swamp	174°-40'	160		10.5
Fence line	167°-05'	155		10.8
Post hole in swamp	130°-40'	480		12.6
Gen'l in swamp	142°-30'	194		10.8
Toe Knoll S.W.	132°-00'	500		11.4
Gen'l in swamp	126°-30'	270		10.6
" "	135°-30'	375		10.9
Post hole in swamp	139°-00'	504		13.3
Gen'l in swamp	158°-45'	346		10.9
" "	163°-45'	332		11.0
Fence line edge swamp	173°-30'	325		10.9
Post hole in swamp	142°-45'	562		13.1

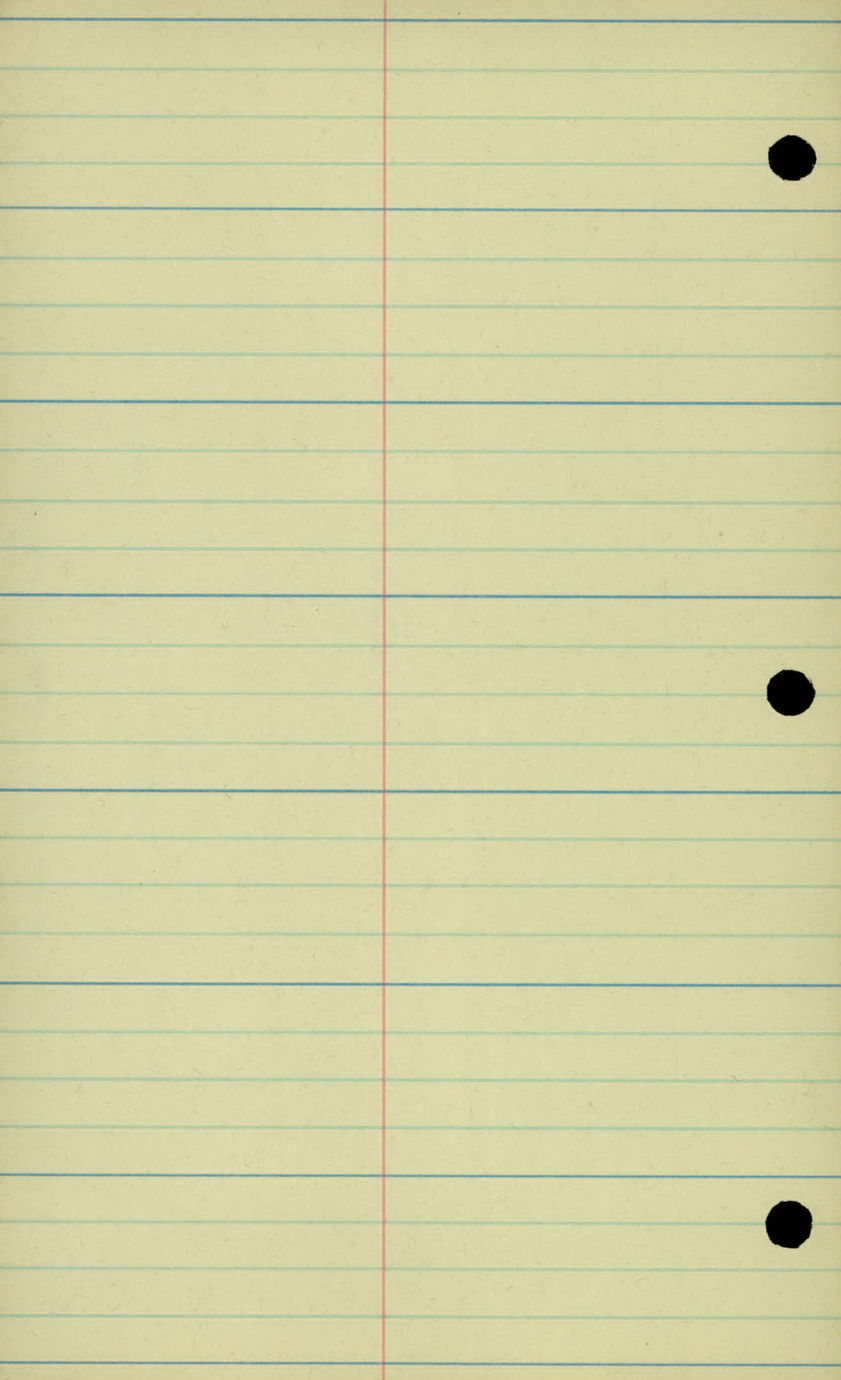


Cont'd at 0 2	Azimuth	Stadia	Vert	Red
too fill	176°-45'	316		9.6
Shoulder line cut-off	179°-30'	318		5.0
Pat hole in swamp	147°-30'	570		13.0
S.E. cor bridge	179°-50'	380		4.3
S.W. cor bridge	185°-04'	380		4.0
Gentl in swamp	150°-00'	515		10.7
N.E. cor bridge	179°-50'	402		3.6
N.W. cor	184°-48'	402		3.5
Gentl in swamp	140°-30'	430		11.0
Elev on 50 slope Knoll	177°-15'	432		3.8
" " S.E. "	173°-00'	461		3.4
2 ditch	157°-00'	360		13.0
Elev on E. slope Knoll	170°-00'	532		2.2
too Knoll edge swamp	171°-30'	400		10.3
E. end culv	147°-43'	37		
" "	237°-50'	57		

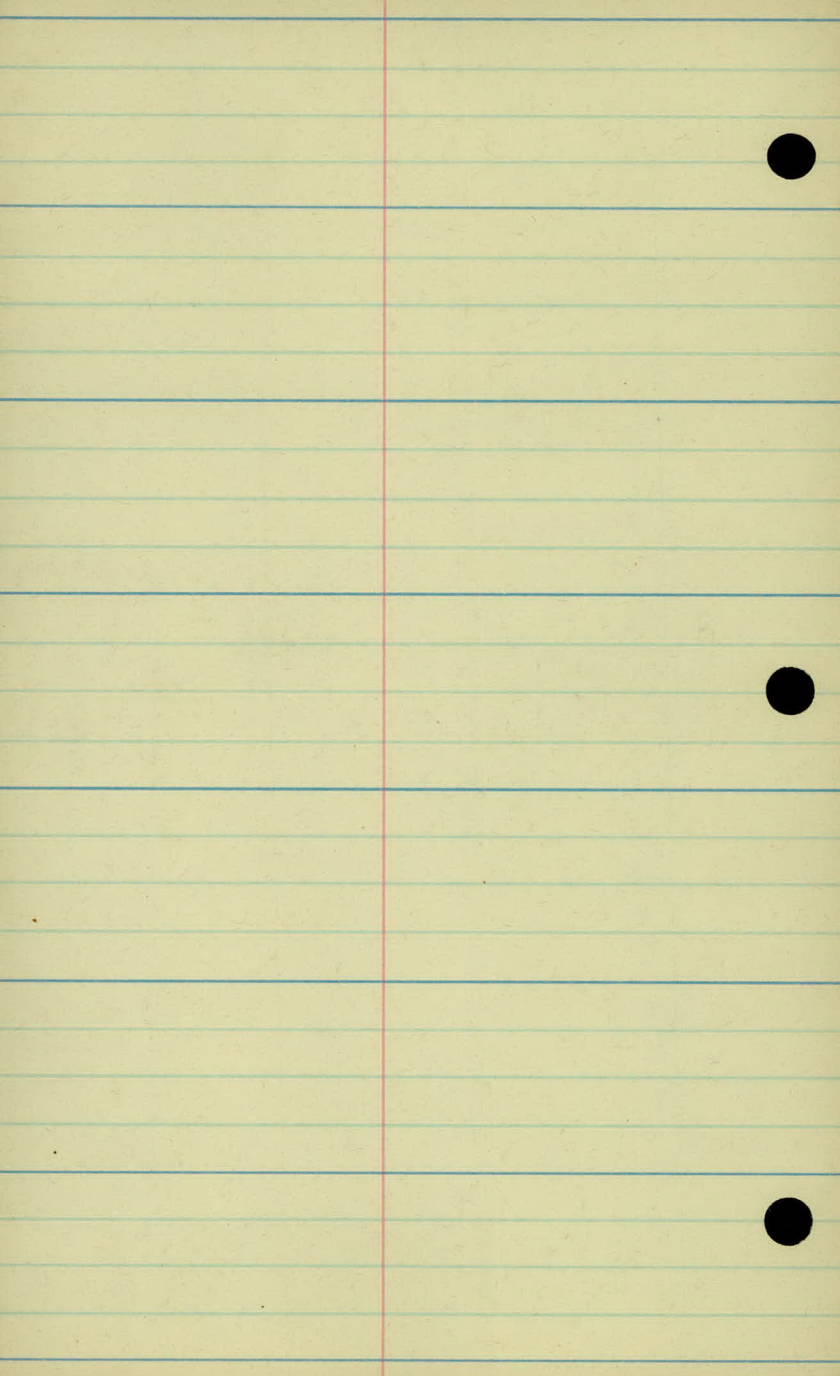
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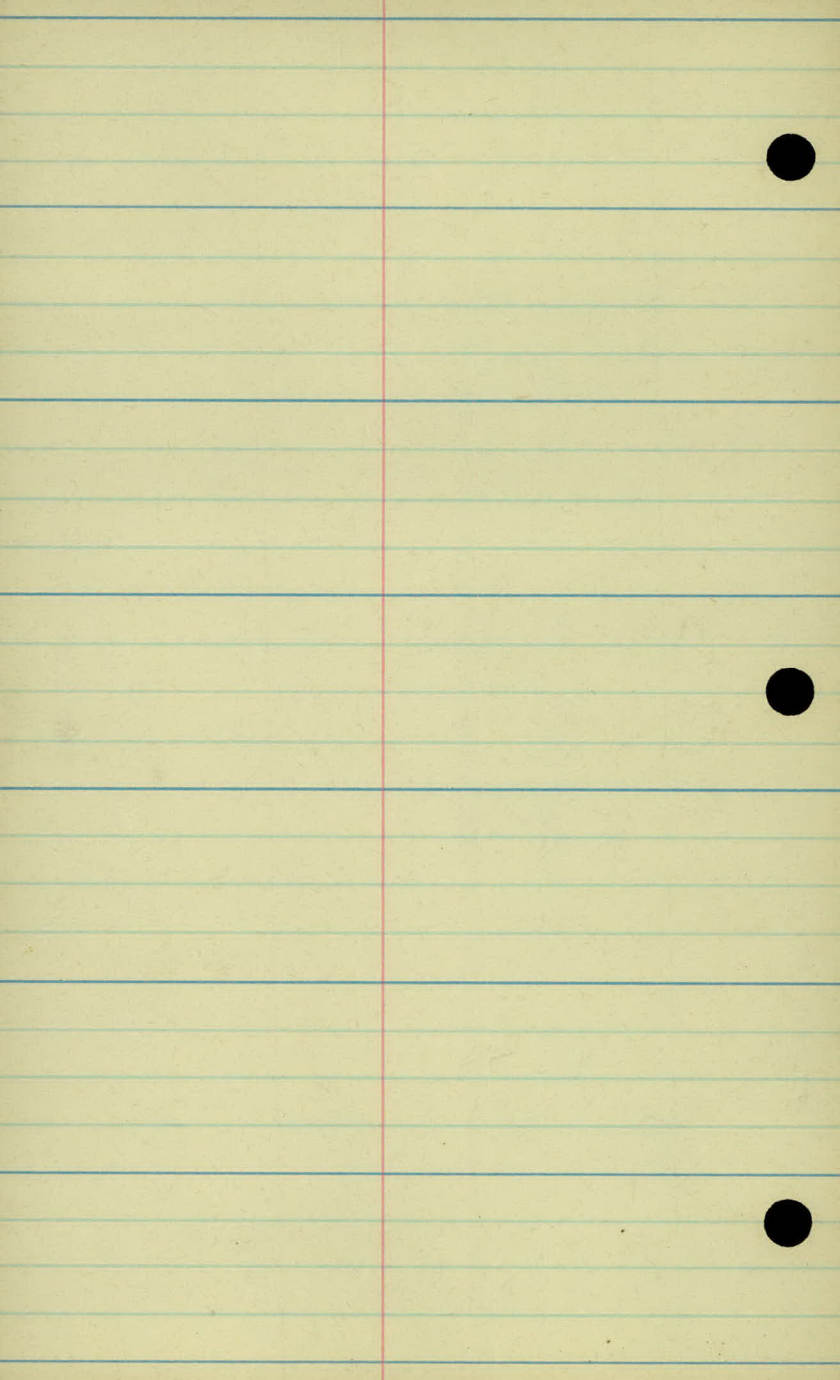
		Azimuth	Stadia	Vert	Red
41	0 3		553		8.45-
to	0 2				
to	0 4				
Elev					
H.I. =	4.95		123°-23'	416	
to c slope knoll	3. E. swamp	25°-00'		76	11.3
Elev on SE slope knoll	"	3°-30'		56	9.2
" " "	"	19°-50'		88	2.6
" " E.	"	91°-40'		15	8.4
" " SE	"	1°-10'		27	2.2
Edge swamp to c slope E	"	94°-10'		51	11.0
Elev on E. slope knoll	"	226°-20'		19	2.7
Edge swamp E to c slope	"	137°-20'		95	11.2
Fence on N slope knoll	"	220 00		103	1.8
Elev on E slope knoll	"	123°15'		45	7.6
Elev on E slope	"	203°40'		107	7.1
Edge swamp	"	187°10'		130	10.9



Cont'd @ 0.3	43'	570	Vert	Foot
Edge on E. slope	196° 15'	163		8.0
Edge swamp W	184° 05'	199		11.4
Fence line top slope	202° 30'	175		4.2
Edge swamp N.W.	182° 25'	290		10.9
Fence line top slope	194° 40'	265		2.4
On E slope	188° 15'	255		8.0
" "	186° 40'	315		8.2
Fence line on slope E	191° 20'	340		2.5
10' tree on slope SE	181° 30'	340		8.8
24" " " "	187° 15'	348		4.5
Edge swamp N.	175° 25'	330		11.0
ON S.E. slope	184° 30'	372		4.6
" " "	176° 15'	373		7.0
Edge swamp	166° 00'	275		11.7
ON S.W. slope	166° 45'	330		8.4
12' tree on S.W. slope	161° 20'	292		9.2
ON W slope	157° 10'	296		7.8

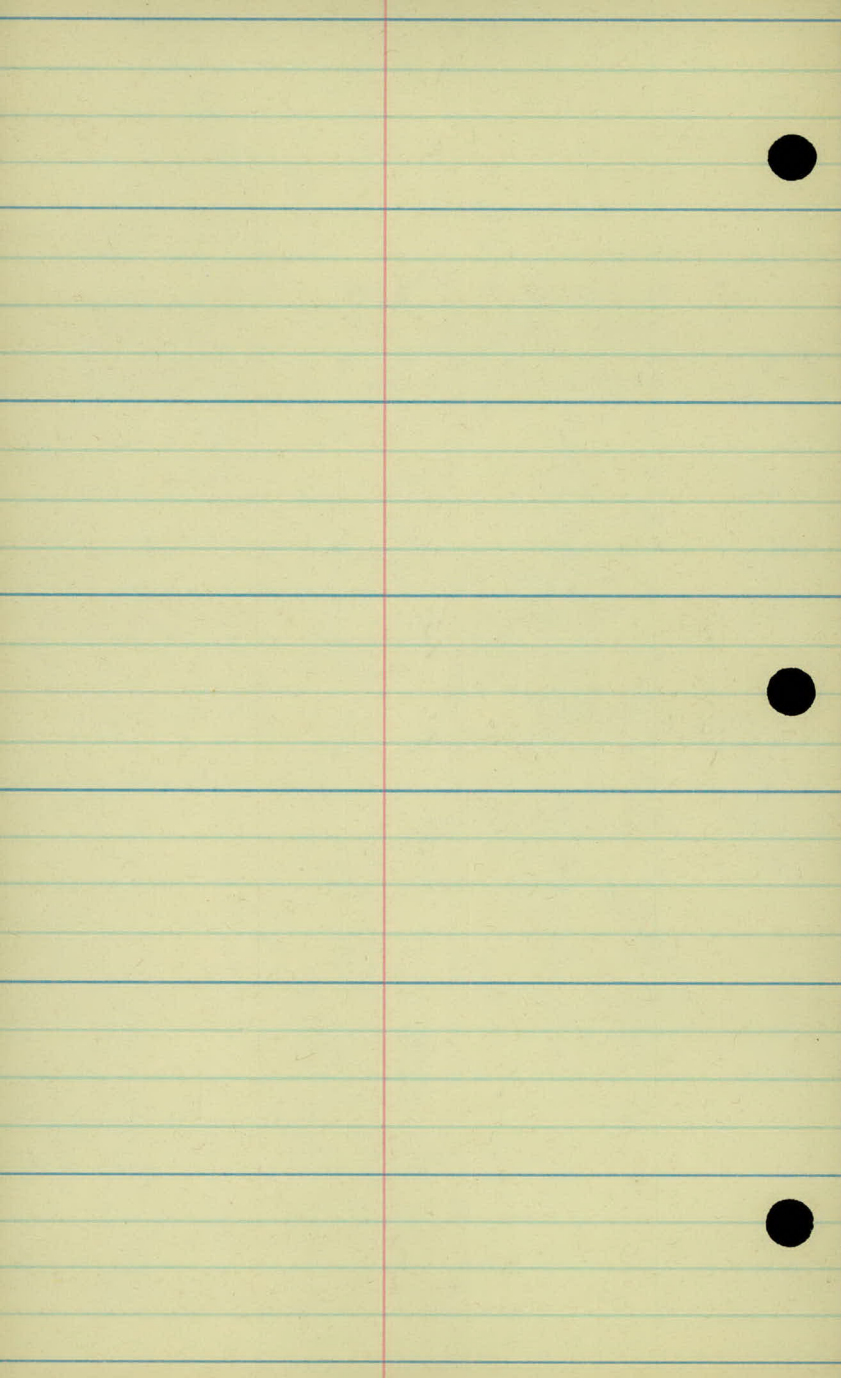


Cont'd at 0.3	Azimuth	Stake	Ver	Red
Set stake in swamp	156° 10'	196		13.0
24" tree on W slope	151° 00'	300		2.5-
on W slope	157° 00'	277		8.1
Edge swamp - edge brush	140° 45'	238		11.8
on W slope S.W.	141° 30'	266		9.9
"	135° 00'	306		8.9
Edge brush in swamp	124° 45'	237		12.3
W edge brush in pot hole	131° 55'	170		13.4
E. " " "	108° 00'	148		12.3
N.W. " " and edge potato	131° 30'	124		12.8
S.W. " " "	95° 00'	100		11.8
Fence on E. slope from cut-off	189° 20'	410	+ 10.00'	5.1
top ridge	179° 00'	448		1.2
" " "	168° 10'	372		5.9
" " "	157° 20'	330		4.7
" " "	147° 00'	320		0.5-
" " "	138° 00'	365	+ 10.0	4.8



12

Cont'd at 03	Azimuth	Stadia	Vert	Red
top knoll or ridge	132°-05'	415	+ 1.0'	5.0
Edge swamp edge brush	135°-00'	290		10.2
///				
At 04				
To 03		416		5.8
To 05	166°-15'	572		
Elev =				
HI = 5.10				
Edge swamp	283°-00'	124		8.0
Elev on 5. slope knoll	272°-50'	120		4.6
" " "	271°-15'	42		4.8
Edge swamp	319°-00'	51		8.0
On S.E. slope knoll	219°-40'	10		3.8
Edge swamp	25°-00'	54		8.6
" " "	76°-00'	60		8.6
On E. slope knoll	181°-35'	63		3.3



Edge swamp
ON E. slope
Edge swamp
ON E. slope
Edge swamp
ON E. slope
Edge swamp
ON N.E. 5/10 p.
" E 5/10 p.
In swamp

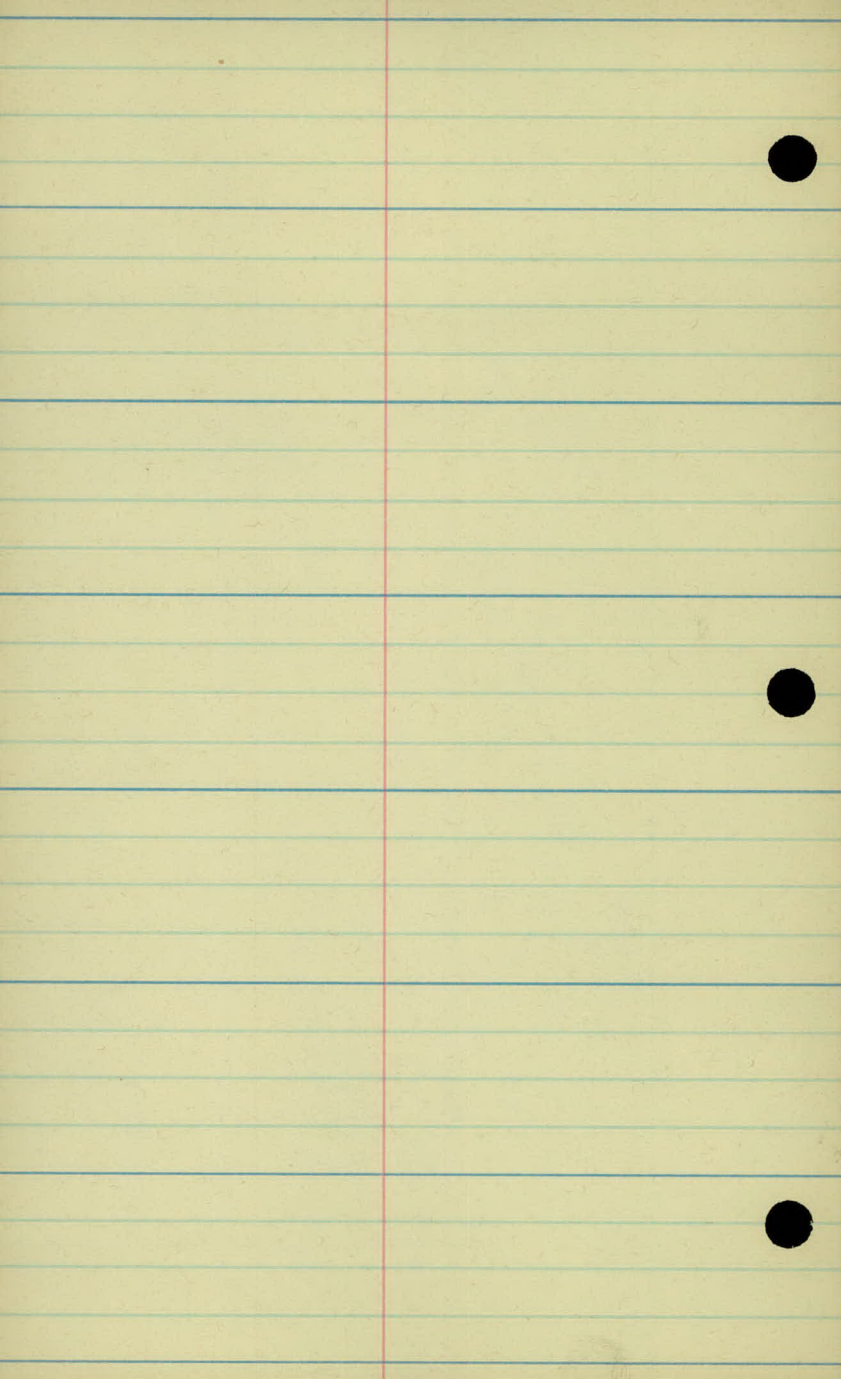
Azimuth
127-35
166-30
154-00
177-30
160-15
169-15
162-15
175-25
168-45
172-00

Stadia

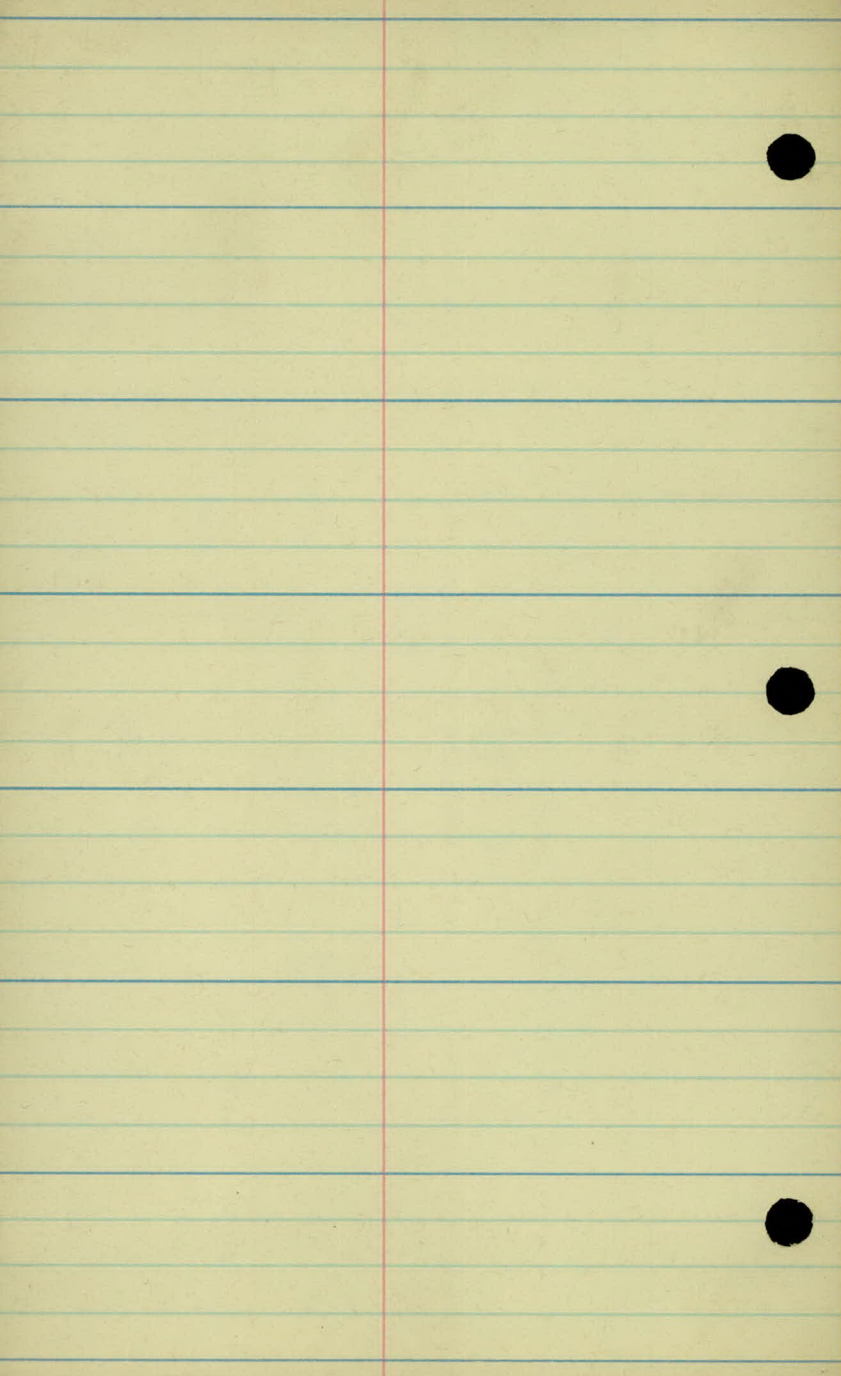
Vert

Red
8.4
2.3
8.1
14.9
5.2
2.3
8.5
3.8
18.6

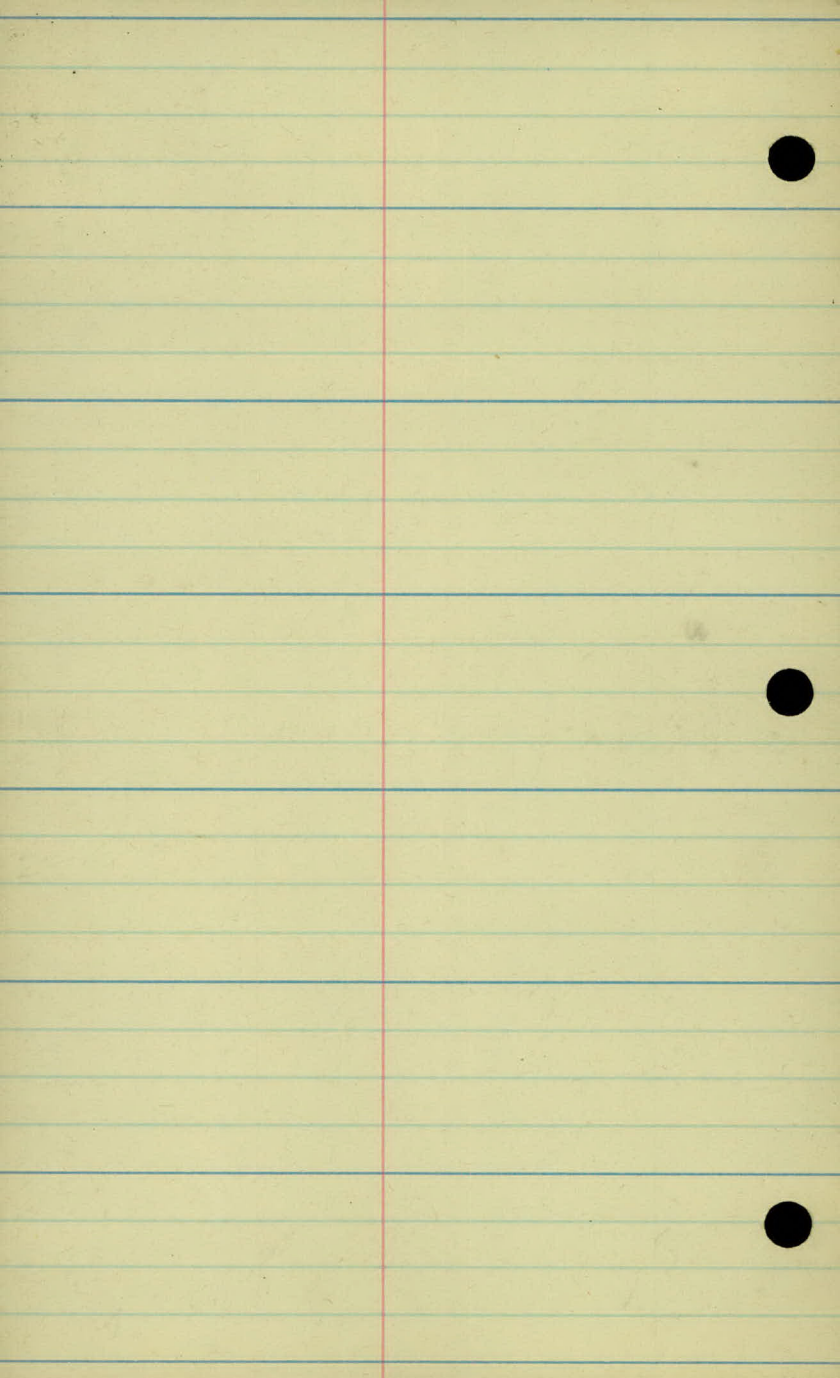
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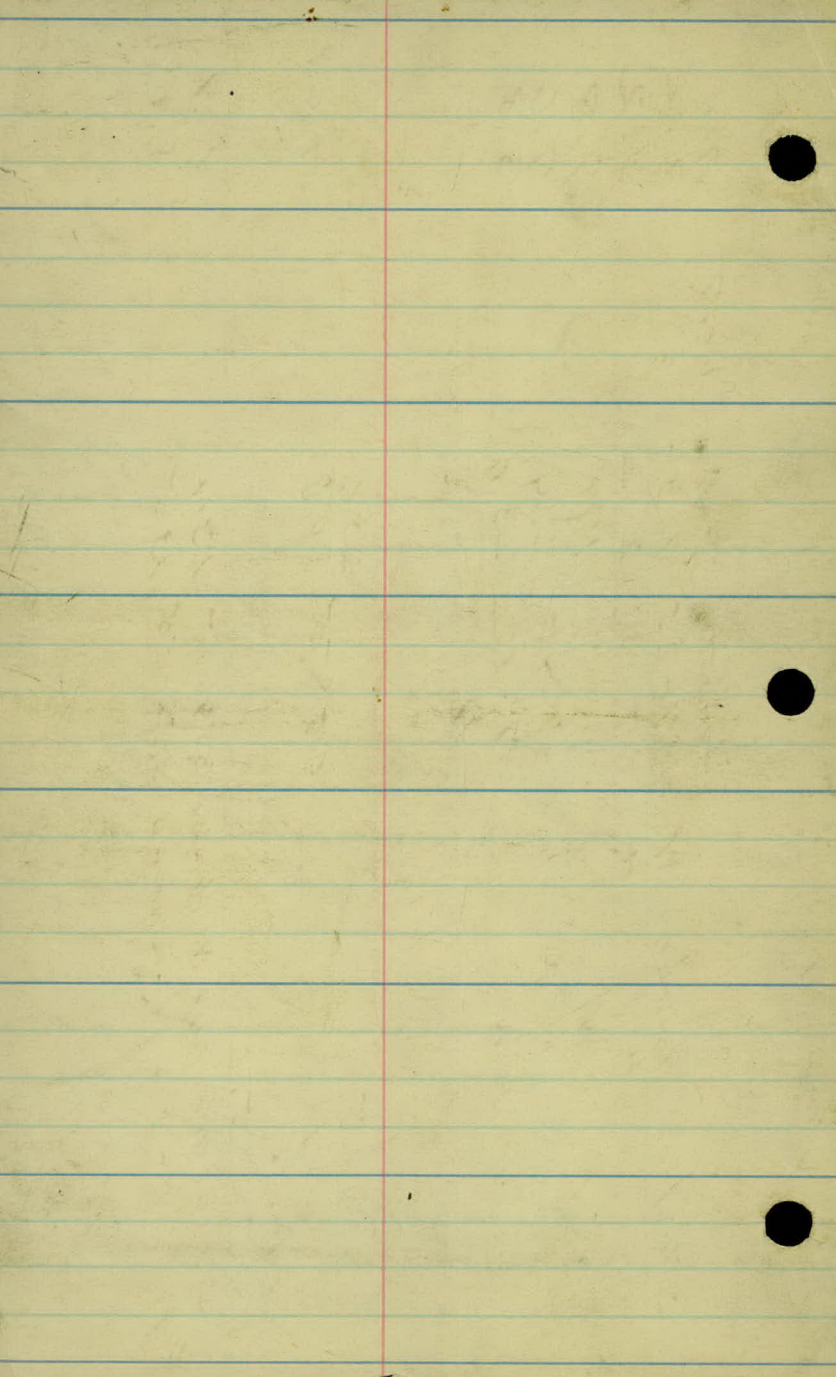
At 05'	04'	06'	Elev =	HI = 5.10	Azimuth Station Vert Rod		
ON NE	"	"	"	Slope Knoll	335°-00'	330	4.6
"	"	"	"	"	319°-30'	26.5'	5.9
"	"	"	"	"	322°-15'	25.4'	6.8
Edge swamp					322°-15'	230	7.3
ON NE	"	"	"	Slope Knoll	302°-00'	232	3.1
"	"	"	"	"	304°-10'	211	6.1
"	"	"	"	"	288°-30'	235'	3.2
Edge swamp					292°-30'	180	2.8
ON N.E. slope					270°-00'	270'	2.2
In draw					280°-00'	214	6.4
"					271°-30'	235'	6.0
ON S.				Slope	283°-30'	130	6.0
ON S.W.				Slope Knoll	264°-20'	198	4.5



Edge swamp	Azimuth	Stadia	
ON S.W. slope	294-40	131	2.8
Edge swamp	268-45	151	3.0
ON S. slope	311-40	78	2.3
" " "	269-40	64	3.4
" " "	292-15	65	5.4
" " "	190-20	18	3.4
" " "	170-30	68	6.3
Edge swamp	140-15	36	2.4
ON S. slope	197-30	86	3.4
Edge swamp	26-10	88	2.5
ON S. slope	91-10	85	6.2
Edge swamp	79-15	135	2.6
ON S. slope	91-15	148	6.4
Fence line on S. slope	102-45	170	2.3
Top Pill Hamlin swamp	88-15	177	5.9
" " "	102-45	180	3.3
Star/Star Hamline W.	102-50	190	1.2



	Asimuth	Stadia	Vert	Red
Shoulder Horn line W	87°-25'	183		2.2
" "	67°-00'	202		3.2
Toe Fill W. edge swamp	" "	190		7.8
Toe " " edge swamp	57°-15'	224		7.6
Shoulder Rd W	51°-10'	239		3.8
At 0 6-				
To 0 5-		236		
To 0 1	00°-35'	868		4.08
Elev =				
H.I. = 5.0				
Shoulder line W. Hornline	35°-10'	134		6.9
Toe Fill - fence - swamp	35°-55'	135		8.8



Long Lake Rd.

Alignment

New Brighton Road

from

STH. #10 to No. Co. Line

9/37

71+06.28

✓

E County Road "J"

61+68.44

POT. ✓

37+78.70

PI

Δ 0° 00' ^{1' Rt.} ~~30'~~

11+31.00

PI. ✓

Δ 0° 02' Rt. ✓

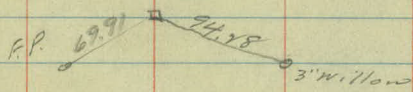
0+00

✓

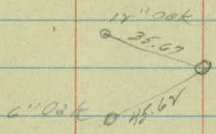
E S.T.H. #10 ✓

No
↑

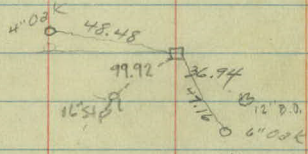
Stone
Mont



Boat Spk

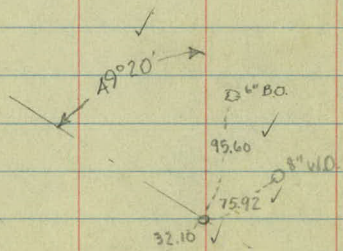
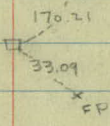


Mont.



Cor Ho

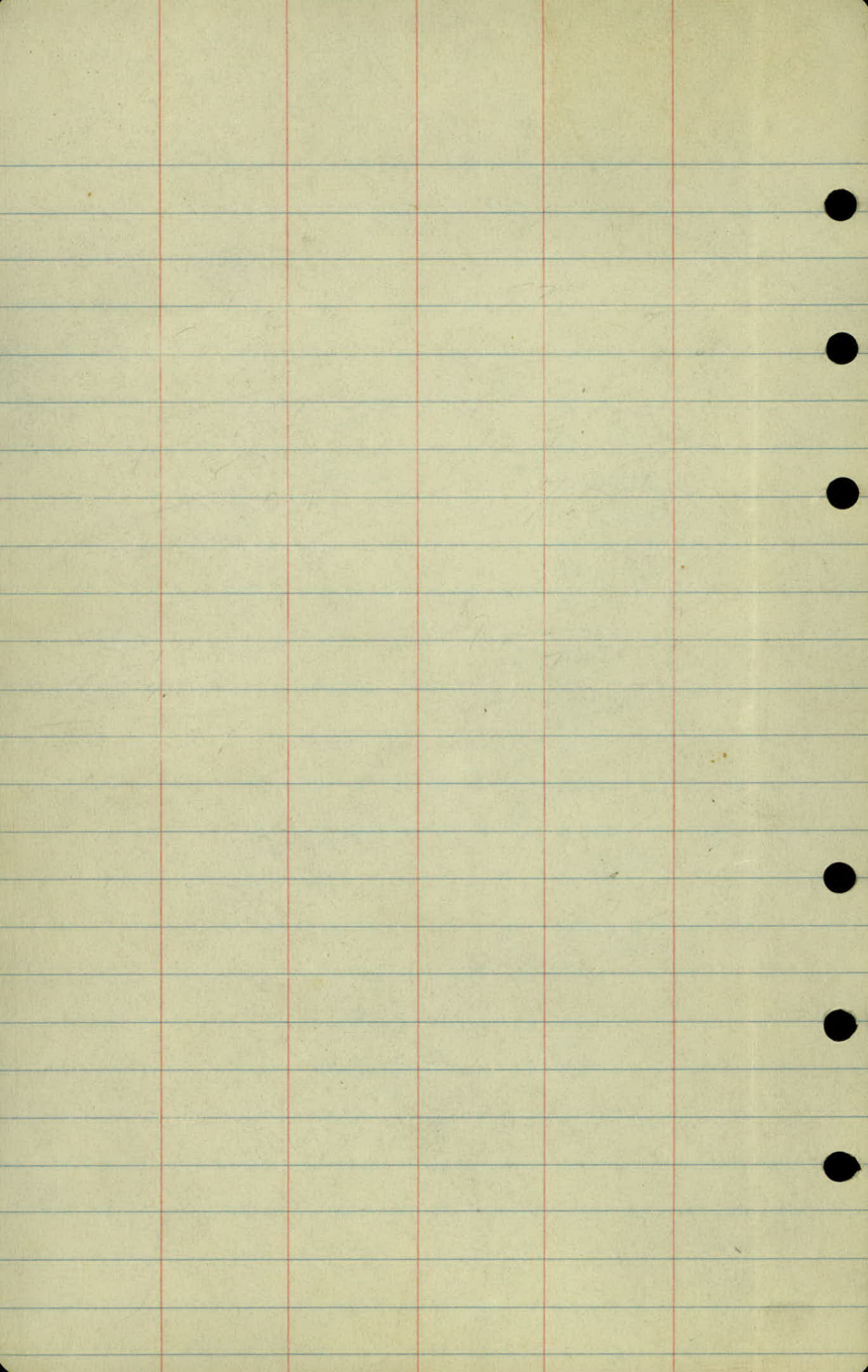
Mont.



Hole in Pave.

Van 12.57

EST. H # 107



Bench Levels

Long Lake Road from
S.T. Hy. #10 to No Co. Line Rd. J.

8/37

Bratager
Gillen

Sta.	+	Σ	-	Elev.
B.M.				907.97

T.P.	2.56	910.53	4.65	905.88
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T.P.	4.68	910.56	3.87	906.74
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B.M.	4.53	911.27	2.19	909.08
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T.P.	2.19	911.27	4.53	906.74
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T.P.	4.19	910.93	2.16	908.77
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B.M.	6.37	915.09	5.63	909.46
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T.P.	5.63	915.09	7.58	907.51
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T.P.	3.97	911.43	4.77	907.21
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B.M.	8.66	915.87	4.96	910.91
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T.P.	4.96	915.87	3.71	914.16
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T.P.	2.74	914.90	6.68	908.77
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T.P.	5.88	914.10	4.73	909.37
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B.M.	6.94	916.31	3.39	914.97
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T.P.	8.37	921.24	6.91	914.33
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B.M.	4.09	918.47	4.46	913.96
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Description

R.R. spike in 12" Oak 33' Rt. Sta.
73+50 on N. Co. line Rd. "I" Refer
to "I" improvement plans.

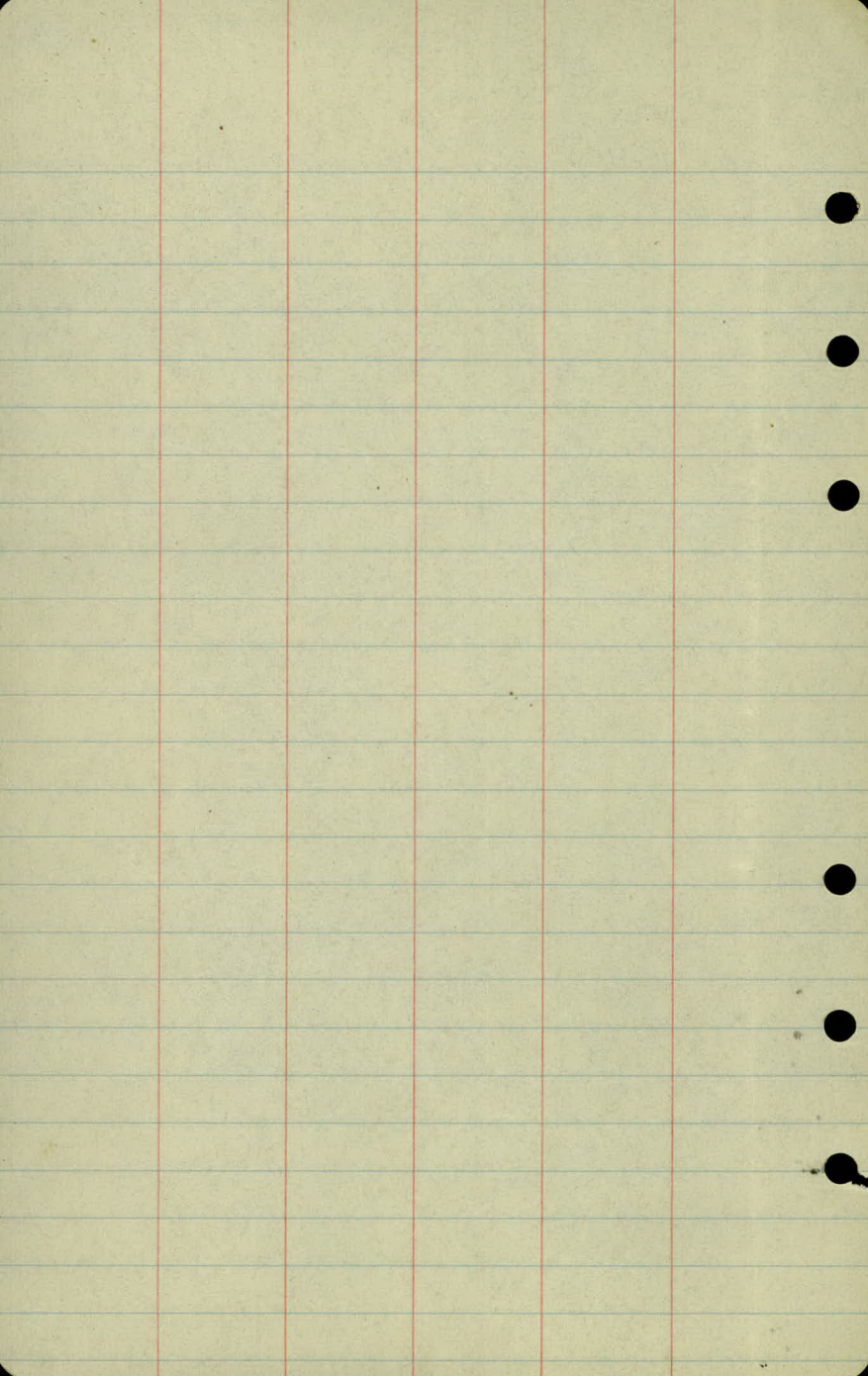
Spike in 14" Stump 100' Rt. Sta. 64±

Spike in 12" Stump 50' Rt. Sta. 57+50

Spike in 14" Oak 100' Rt. Sta. 36+

Spike in stump used as fence post 100' Rt.
Sta. 11+00

Top of Conc. Paving, (Drilled Hole) intersection
S.T. Hy. #10 & Long Lake Road.



5

Preliminary Cross-Sections
of Long Lake Road from Sta.
0+00 intersection with S.T. Hy. #10
to Sta. 71+06.28 intersection with
No. Co. Line Road J.

9/37

{ Bratager
Wilke
Goldberg
Gillen
Larsen

Sta.	+	K	-	Elev.
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B.M.	401	917.97		913.96
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0+00	Along & #10			14.0
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+18				14.0
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+63				13.9
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+71				13.8
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+85				13.7
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1				13.5
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+50				13.4
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2				13.3
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(Sta. 3+ Haca culvert drain East)

+50	(Large Pot Hole)			13.4
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3				13.4
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+50				13.7
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Lt.

E

Rt.

6

Top of concrete paving (Drill Hole)
intersection S.Tr. Hg. #10 & Long Lake Rd.

$\frac{3.5}{100}$ $\frac{36}{50}$ $\frac{40}{/}$ $\frac{46}{50}$ $\frac{5.3}{100}$

$\frac{2.7}{50}$ $\frac{40}{/}$ $\frac{46}{21}$ $\frac{4.7}{36}$ $\frac{4.2}{50}$

$\frac{2.9}{50}$ $\frac{40}{22}$ $\frac{41}{/}$ $\frac{4.7}{8}$ $\frac{4.1}{14}$ $\frac{2.7}{30}$ $\frac{2.6}{50}$

$\frac{4.1}{50}$ $\frac{4.1}{47}$ $\frac{4.8}{44}$ $\frac{4.9}{23}$ $\frac{4.1}{16}$ $\frac{4.2}{/}$ $\frac{4.7}{9}$ $\frac{3.4}{16}$ $\frac{2.7}{24}$ $\frac{2.7}{50}$

$\frac{4.5}{50}$ $\frac{2.7}{27}$ $\frac{2.9}{26}$ $\frac{5.1}{19}$ $\frac{5.3}{17}$ $\frac{4.2}{15}$ $\frac{4.3}{/}$ $\frac{4.6}{14}$ $\frac{2.6}{17}$ $\frac{3.0}{50}$

$\frac{2.8}{50}$ $\frac{2.8}{24}$ $\frac{5.3}{19}$ $\frac{5.3}{18}$ $\frac{4.5}{16}$ $\frac{4.6}{14}$ $\frac{4.5}{/}$ $\frac{4.9}{9}$ $\frac{5.1}{14}$ $\frac{3.2}{16}$ $\frac{3.5}{50}$

$\frac{2.7}{50}$ $\frac{2.9}{21}$ $\frac{5.5}{18}$ $\frac{5.5}{17}$ $\frac{5.0}{15}$ $\frac{4.6}{/}$ $\frac{5.0}{10}$ $\frac{5.9}{14}$ $\frac{5.8}{16}$ $\frac{4.8}{19}$ $\frac{5.2}{30}$ $\frac{5.5}{50}$

$\frac{6.1}{50}$ $\frac{5.7}{24}$ $\frac{6.2}{20}$ $\frac{5.0}{15}$ $\frac{4.7}{/}$ $\frac{5.2}{8}$ $\frac{5.4}{11}$ $\frac{6.7}{20}$ $\frac{7.1}{50}$

$\frac{7.1}{50}$ $\frac{6.7}{36}$ $\frac{7.2}{26}$ $\frac{6.7}{18}$ $\frac{5.0}{14}$ $\frac{4.6}{/}$ $\frac{5.3}{9}$ $\frac{7.1}{13}$ $\frac{8.0}{50}$

$\frac{7.0}{50}$ $\frac{7.0}{42}$ $\frac{6.7}{19}$ $\frac{5.0}{14}$ $\frac{4.6}{/}$ $\frac{5.4}{9}$ $\frac{7.0}{14}$ $\frac{8.6}{50}$

$\frac{6.0}{50}$ $\frac{6.0}{44}$ $\frac{6.2}{24}$ $\frac{5.8}{18}$ $\frac{4.6}{14}$ $\frac{4.3}{/}$ $\frac{4.9}{11}$ $\frac{6.5}{14}$ $\frac{7.4}{22}$ $\frac{9.2}{45}$ $\frac{10.0}{50}$

Sta. + π - Elev.

917.97

4 13.8

+50 13.8

5 13.9

T.P. 4.90 918.97 3.90 914.07

+50 14.2

6 14.5

+50 14.6

7 14.6

+50 15.1

8 15.8

+50 16.3

T.P. 4.55 910.83 2.69 916.48

9 16.2

Lt.

E

Rt.

7

 $\frac{53}{50}$ $\frac{54}{39}$ $\frac{53}{18}$ $\frac{45}{14}$ $\frac{42}{10}$ $\frac{50}{10}$ $\frac{72}{15}$ $\frac{79}{22}$ $\frac{109}{60}$
 $\frac{63}{50}$ $\frac{57}{34}$ $\frac{62}{19}$ $\frac{46}{15}$ $\frac{42}{9}$ $\frac{48}{9}$ $\frac{80}{15}$ $\frac{86}{21}$ $\frac{111}{80}$
 $\frac{53}{50}$ $\frac{55}{34}$ $\frac{62}{17}$ $\frac{45}{13}$ $\frac{41}{11}$ $\frac{48}{11}$ $\frac{71}{15}$ $\frac{75}{22}$ $\frac{107}{80}$
 $\frac{51}{50}$ $\frac{55}{17}$ $\frac{54}{16}$ $\frac{51}{10}$ $\frac{48}{11}$ $\frac{54}{11}$ $\frac{72}{15}$ $\frac{72}{17}$ $\frac{64}{19}$ $\frac{91}{80}$
 $\frac{42}{50}$ $\frac{44}{21}$ $\frac{50}{17}$ $\frac{50}{12}$ $\frac{45}{11}$ $\frac{51}{11}$ $\frac{60}{13}$ $\frac{60}{14}$ $\frac{45}{17}$ $\frac{55}{40}$ $\frac{67}{50}$
 $\frac{36}{50}$ $\frac{36}{30}$ $\frac{42}{19}$ $\frac{48}{18}$ $\frac{52}{16}$ $\frac{48}{15}$ $\frac{44}{11}$ $\frac{47}{8}$ $\frac{50}{14}$ $\frac{40}{17}$ $\frac{45}{46}$ $\frac{48}{50}$
 $\frac{43}{50}$ $\frac{42}{30}$ $\frac{46}{27}$ $\frac{49}{15}$ $\frac{46}{14}$ $\frac{44}{11}$ $\frac{49}{10}$ $\frac{54}{12}$ $\frac{55}{15}$ $\frac{48}{18}$ $\frac{50}{50}$
 $\frac{42}{50}$ $\frac{41}{32}$ $\frac{46}{14}$ $\frac{41}{12}$ $\frac{39}{11}$ $\frac{44}{11}$ $\frac{51}{14}$ $\frac{51}{16}$ $\frac{47}{18}$ $\frac{42}{50}$
 $\frac{28}{50}$ $\frac{23}{25}$ $\frac{32}{19}$ $\frac{41}{17}$ $\frac{41}{15}$ $\frac{36}{13}$ $\frac{32}{11}$ $\frac{37}{15}$ $\frac{29}{10}$ $\frac{22}{50}$
 $\frac{19}{50}$ $\frac{11}{33}$ $\frac{15}{21}$ $\frac{32}{18}$ $\frac{27}{11}$ $\frac{33}{11}$ $\frac{17}{15}$ $\frac{15}{50}$
 $\frac{42}{50}$ $\frac{42}{21}$ $\frac{56}{18}$ $\frac{56}{11}$ $\frac{52}{13}$ $\frac{46}{11}$ $\frac{50}{11}$ $\frac{54}{14}$ $\frac{54}{16}$ $\frac{39}{18}$ $\frac{37}{50}$

Sta. + X - Elev.

920.83

9+50 15.3

10 14.6

B.M. 5.14 918.06 7.91 914.92

+50 13.8

11 13.0

+31 12.3

+50 12.0

12 11.4

+50 10.7

13 10.0

T.P. 3.80 913.78 8.08 909.78

+50 09.4

14 08.6

Lt.

E

Rt.

8/

$\frac{52}{50}$	$\frac{52}{44}$	$\frac{48}{20}$	$\frac{63}{12}$	$\frac{65}{14}$	$\frac{59}{14}$	$\frac{55}{8}$	$\frac{59}{8}$	$\frac{62}{18}$	$\frac{51}{23}$	$\frac{48}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{66}{50}$	$\frac{65}{19}$	$\frac{62}{18}$	$\frac{68}{18}$	$\frac{58}{50}$
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Spike in stump used as fence post 100' Rt.

Sta. 11+00

$\frac{61}{50}$	$\frac{58}{28}$	$\frac{60}{18}$	$\frac{48}{11}$	$\frac{43}{14}$	$\frac{47}{10}$	$\frac{54}{15}$	$\frac{57}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{79}{50}$	$\frac{74}{30}$	$\frac{71}{18}$	$\frac{57}{11}$	$\frac{51}{14}$	$\frac{56}{14}$	$\frac{67}{12}$	$\frac{62}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{89}{50}$	$\frac{88}{26}$	$\frac{75}{14}$	$\frac{62}{9}$	$\frac{58}{14}$	$\frac{60}{14}$	$\frac{69}{11}$	$\frac{76}{50}$
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Drain Low
Dig Pot Hole
if possible by
ditches

$\frac{73}{50}$	$\frac{69}{24}$	$\frac{67}{11}$	$\frac{61}{14}$	$\frac{61}{11}$	$\frac{63}{20}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{76}{50}$	$\frac{69}{10}$	$\frac{67}{9}$	$\frac{66}{9}$	$\frac{61}{19}$	$\frac{61}{50}$
-----------------	-----------------	----------------	----------------	-----------------	-----------------

$\frac{69}{50}$	$\frac{55}{20}$	$\frac{76}{15}$	$\frac{74}{9}$	$\frac{74}{11}$	$\frac{74}{15}$	$\frac{52}{19}$	$\frac{51}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{58}{50}$	$\frac{59}{38}$	$\frac{62}{20}$	$\frac{83}{14}$	$\frac{78}{8}$	$\frac{81}{14}$	$\frac{78}{8}$	$\frac{81}{14}$	$\frac{62}{20}$	$\frac{68}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-----------------	-----------------

$\frac{40}{50}$	$\frac{40}{44}$	$\frac{39}{20}$	$\frac{40}{15}$	$\frac{46}{14}$	$\frac{41}{6}$	$\frac{44}{14}$	$\frac{42}{11}$	$\frac{45}{27}$	$\frac{43}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{62}{50}$	$\frac{62}{17}$	$\frac{52}{11}$	$\frac{48}{4}$	$\frac{52}{14}$	$\frac{49}{9}$	$\frac{62}{18}$	$\frac{65}{35}$	$\frac{66}{50}$
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Place pipe
Drain
west

907.6

Sta.	+	π	-	Elev.
		913.78		
14+50				08.5
15				08.3
+50				08.4
16				08.1
+50				07.8
17				07.9
+50				08.1
18				08.2
+50				08.4
T.P.	10.03	918.66	5.15	908.63
19				08.5
+50				08.3
20				08.7

14.

2

Rt.

9

$$\frac{6.8}{50} \quad \frac{6.5}{17} \quad \frac{5.0}{11} \quad \frac{4.7}{4} \quad \frac{5.3}{5} \quad \frac{4.7}{6} \quad \frac{5.0}{10} \quad \frac{6.3}{17} \quad \frac{6.0}{28} \quad \frac{6.6}{50}$$

$$\frac{6.4}{50} \quad \frac{6.0}{17} \quad \frac{5.3}{11} \quad \frac{5.0}{3} \quad \frac{5.5}{5} \quad \frac{4.9}{7} \quad \frac{5.2}{16} \quad \frac{5.5}{17} \quad \frac{4.9}{23} \quad \frac{4.9}{27} \quad \frac{5.5}{31} \quad \frac{5.4}{50}$$

$$\frac{6.0}{50} \quad \frac{5.4}{25} \quad \frac{5.0}{3} \quad \frac{5.4}{5} \quad \frac{5.0}{7} \quad \frac{4.9}{9} \quad \frac{5.3}{11} \quad \frac{4.3}{14} \quad \frac{4.2}{23} \quad \frac{3.8}{25} \quad \frac{4.2}{31} \quad \frac{4.6}{50}$$

$$\frac{5.5}{50} \quad \frac{4.7}{20} \quad \frac{5.6}{16} \quad \frac{4.8}{8} \quad \frac{5.7}{2} \quad \frac{5.7}{5} \quad \frac{5.0}{6} \quad \frac{5.1}{8} \quad \frac{5.6}{10} \quad \frac{3.9}{16} \quad \frac{2.1}{25} \quad \frac{4.0}{50}$$

$$\frac{5.3}{50} \quad \frac{4.6}{21} \quad \frac{5.7}{17} \quad \frac{5.0}{7} \quad \frac{6.0}{2} \quad \frac{6.0}{4} \quad \frac{5.3}{7} \quad \frac{5.5}{11} \quad \frac{3.8}{16} \quad \frac{3.7}{27} \quad \frac{4.1}{50}$$

$$\frac{6.0}{50} \quad \frac{5.5}{20} \quad \frac{6.0}{18} \quad \frac{5.5}{2} \quad \frac{5.9}{1} \quad \frac{5.9}{5} \quad \frac{5.4}{10} \quad \frac{5.1}{13} \quad \frac{4.5}{25} \quad \frac{4.8}{50}$$

$$\frac{6.7}{50} \quad \frac{6.2}{18} \quad \frac{5.5}{12} \quad \frac{5.3}{3} \quad \frac{5.7}{2} \quad \frac{5.7}{5} \quad \frac{5.6}{5} \quad \frac{5.3}{6} \quad \frac{4.5}{28} \quad \frac{5.2}{50}$$

907.1

$$\frac{6.4}{50} \quad \frac{6.8}{17} \quad \frac{5.4}{9} \quad \frac{5.4}{6} \quad \frac{5.8}{4} \quad \frac{5.6}{5} \quad \frac{5.5}{2} \quad \frac{5.1}{3} \quad \frac{6.2}{11} \quad \frac{5.4}{27} \quad \frac{5.7}{50}$$

$$\frac{7.0}{50} \quad \frac{6.7}{18} \quad \frac{5.9}{14} \quad \frac{5.1}{5} \quad \frac{5.4}{4} \quad \frac{5.4}{5} \quad \frac{5.3}{3} \quad \frac{5.0}{5} \quad \frac{6.3}{13} \quad \frac{6.3}{23} \quad \frac{5.5}{26} \quad \frac{5.7}{50}$$

$$\frac{11.2}{50} \quad \frac{11.0}{17} \quad \frac{10.1}{10} \quad \frac{9.8}{5} \quad \frac{10.2}{4} \quad \frac{10.2}{5} \quad \frac{10.2}{3} \quad \frac{9.8}{4} \quad \frac{10.2}{9} \quad \frac{10.8}{23} \quad \frac{10.3}{27} \quad \frac{10.4}{50}$$

$$\frac{10.8}{50} \quad \frac{10.8}{18} \quad \frac{10.0}{9} \quad \frac{10.1}{4} \quad \frac{10.5}{3} \quad \frac{10.4}{5} \quad \frac{10.4}{3} \quad \frac{9.8}{5} \quad \frac{10.8}{14} \quad \frac{10.8}{24} \quad \frac{10.2}{27} \quad \frac{10.6}{50}$$

$$\frac{9.9}{50} \quad \frac{9.9}{25} \quad \frac{9.5}{3} \quad \frac{10.0}{5} \quad \frac{9.5}{6} \quad \frac{9.9}{23} \quad \frac{9.6}{27} \quad \frac{10.2}{50}$$

Sta. + π - Elev.

918.66

20+50 08.9

21 09.5

+50 09.3

22 10.2

+50 09.4

23 09.4

T.P. 131 918.32 ✓ 7.65 911.01

+50 09.2

24 08.4

+50 07.7

25 07.0

+65 Culvert. 06.8

Lt.

L

Rt.

10

$$\frac{8.3}{50} \quad \frac{8.1}{18} \quad \frac{9.5}{14} \quad \frac{9.0}{4} \quad \frac{9.8}{1} \quad \frac{9.0}{7} \quad \frac{9.1}{16} \quad \frac{8.0}{19} \quad \frac{7.7}{30} \quad \frac{8.1}{50}$$

$$\frac{6.5}{50} \quad \frac{6.4}{20} \quad \frac{8.6}{15} \quad \frac{8.6}{7} \quad \frac{9.2}{1} \quad \frac{8.3}{2} \quad \frac{8.6}{15} \quad \frac{6.3}{20} \quad \frac{7.0}{50}$$

$$\frac{5.2}{50} \quad \frac{5.2}{19} \quad \frac{8.1}{14} \quad \frac{9.2}{6} \quad \frac{9.4}{1} \quad \frac{8.2}{5} \quad \frac{7.9}{14} \quad \frac{5.5}{21} \quad \frac{6.0}{50}$$

$$\frac{5.2}{20} \quad \frac{5.2}{22} \quad \frac{7.6}{18} \quad \frac{8.0}{7} \quad \frac{8.5}{1} \quad \frac{7.5}{5} \quad \frac{7.5}{15} \quad \frac{5.4}{20} \quad \frac{5.8}{30}$$

$$\frac{5.9}{50} \quad \frac{6.0}{20} \quad \frac{8.0}{17} \quad \frac{8.2}{6} \quad \frac{9.0}{4} \quad \frac{9.3}{1} \quad \frac{9.0}{3} \quad \frac{8.1}{8} \quad \frac{7.7}{17} \quad \frac{6.0}{20} \quad \frac{6.4}{50}$$

$$\frac{8.6}{50} \quad \frac{8.3}{20} \quad \frac{9.0}{17} \quad \frac{8.9}{3} \quad \frac{9.3}{1} \quad \frac{8.7}{8} \quad \frac{9.3}{12} \quad \frac{9.1}{21} \quad \frac{8.2}{24} \quad \frac{8.2}{50}$$

$$\frac{4.4}{50} \quad \frac{4.2}{16} \quad \frac{3.5}{10} \quad \frac{3.0}{3} \quad \frac{3.1}{1} \quad \frac{3.0}{4} \quad \frac{4.2}{14} \quad \frac{4.3}{24} \quad \frac{4.1}{50}$$

$$\frac{5.9}{50} \quad \frac{5.3}{17} \quad \frac{4.0}{6} \quad \frac{3.9}{1} \quad \frac{3.7}{8} \quad \frac{5.0}{17} \quad \frac{5.2}{18} \quad \frac{5.2}{50}$$

$$\frac{6.6}{50} \quad \frac{6.3}{16} \quad \frac{4.6}{7} \quad \frac{4.6}{1} \quad \frac{4.5}{8} \quad \frac{6.1}{19} \quad \frac{6.3}{28} \quad \frac{5.9}{31} \quad \frac{6.4}{50}$$

$$\frac{7.3}{50} \quad \frac{6.9}{18} \quad \frac{5.2}{8} \quad \frac{5.3}{1} \quad \frac{5.3}{10} \quad \frac{6.7}{17} \quad \frac{7.0}{50}$$

$$\frac{7.7}{50} \quad \frac{7.2}{26} \quad \frac{7.1}{17} \quad \frac{5.6}{5} \quad \frac{5.5}{1} \quad \frac{5.4}{5} \quad \frac{7.3}{17} \quad \frac{7.6}{50}$$

$$\frac{5.0}{1 \text{ hr.}} \quad (04.3)$$

$$\frac{7.85}{1 \text{ hr.}} \quad (04.5)$$

Sta. + π - Elev.

914.32

26 07.2

+50 07.5

27 07.9

+50 08.3 ✓

28 08.6

+50 09.1

29 09.7

T.P. 6.83 916.54 2.61 909.71

+50 10.2

30 10.7

+50 10.8

31 11.4

Lt.

Q

Rt.

11

$$\frac{7.5}{50} \quad \frac{7.6}{27} \quad \frac{7.7}{19} \quad \frac{5.8}{10} \quad \frac{5.1}{8} \quad \frac{5.2}{17} \quad \frac{7.4}{28} \quad \frac{7.3}{50}$$

$$\frac{7.4}{50} \quad \frac{7.7}{17} \quad \frac{4.8}{8} \quad \frac{4.8}{9} \quad \frac{4.8}{16} \quad \frac{6.3}{23} \quad \frac{6.9}{50}$$

$$\frac{6.8}{50} \quad \frac{6.7}{19} \quad \frac{4.4}{10} \quad \frac{4.4}{9} \quad \frac{4.5}{13} \quad \frac{6.2}{16} \quad \frac{6.5}{29} \quad \frac{6.0}{33} \quad \frac{6.4}{50}$$

$$\frac{6.6}{50} \quad \frac{6.8}{29} \quad \frac{5.7}{17} \quad \frac{4.0}{10} \quad \frac{4.0}{9} \quad \frac{4.1}{16} \quad \frac{5.9}{23} \quad \frac{5.4}{50}$$

$$\frac{5.6}{50} \quad \frac{5.4}{30} \quad \frac{5.7}{18} \quad \frac{4.3}{14} \quad \frac{2.6}{9} \quad \frac{3.7}{7} \quad \frac{3.6}{15} \quad \frac{4.3}{50}$$

$$\frac{4.2}{50} \quad \frac{3.9}{16} \quad \frac{3.0}{10} \quad \frac{3.7}{9} \quad \frac{2.7}{17} \quad \frac{3.3}{24} \quad \frac{2.6}{50}$$

$$\frac{2.1}{50} \quad \frac{2.0}{29} \quad \frac{3.2}{19} \quad \frac{3.7}{18} \quad \frac{2.8}{10} \quad \frac{2.6}{23} \quad \frac{2.2}{50}$$

$$\frac{5.4}{50} \quad \frac{5.2}{28} \quad \frac{5.4}{19} \quad \frac{6.6}{15} \quad \frac{6.3}{6} \quad \frac{6.0}{50}$$

$$\frac{4.7}{50} \quad \frac{4.9}{29} \quad \frac{4.9}{21} \quad \frac{6.5}{17} \quad \frac{5.8}{27} \quad \frac{5.2}{50}$$

$$\frac{4.7}{50} \quad \frac{4.0}{29} \quad \frac{4.4}{20} \quad \frac{5.9}{16} \quad \frac{5.7}{3} \quad \frac{5.2}{31} \quad \frac{4.5}{50}$$

$$\frac{4.3}{50} \quad \frac{3.5}{28} \quad \frac{4.1}{20} \quad \frac{5.5}{16} \quad \frac{5.1}{11} \quad \frac{4.7}{19} \quad \frac{4.4}{50}$$

Sta.	+	π	-	Elev.
		916.54		
31+50				11.7
T.P.	4.34	916.27	4.59	911.95
32				12.0
+50				11.7
33				11.2
+50				11.4
34				11.2
+50				11.7
35				11.5
T.P.	5.50	916.54	5.25	911.04
+50				11.4
36				11.5
B.M.	3.98	914.89	5.61	910.91

Lt.

E

Rt.

12

$$\frac{40}{50} \quad \frac{38}{30} \quad \frac{34}{23} \quad \frac{40}{18} \quad \frac{53}{15} \quad \frac{48}{14} \quad \frac{47}{14} \quad \frac{48}{50}$$

$$\frac{39}{50} \quad \frac{41}{30} \quad \frac{43}{18} \quad \frac{47}{15} \quad \frac{43}{15} \quad \frac{46}{15} \quad \frac{49}{50}$$

$$\frac{44}{50} \quad \frac{44}{30} \quad \frac{46}{17} \quad \frac{52}{16} \quad \frac{50}{14} \quad \frac{46}{10} \quad \frac{46}{8} \quad \frac{44}{5} \quad \frac{51}{25} \quad \frac{49}{50}$$

$$\frac{51}{50} \quad \frac{51}{30} \quad \frac{51}{12} \quad \frac{47}{7} \quad \frac{51}{6} \quad \frac{47}{6} \quad \frac{55}{13} \quad \frac{47}{16} \quad \frac{44}{50}$$

$$\frac{59}{50} \quad \frac{54}{18} \quad \frac{56}{14} \quad \frac{48}{6} \quad \frac{49}{3} \quad \frac{46}{3} \quad \frac{55}{11} \quad \frac{47}{14} \quad \frac{46}{50}$$

$$\frac{60}{50} \quad \frac{56}{30} \quad \frac{56}{13} \quad \frac{47}{6} \quad \frac{46}{12} \quad \frac{55}{12} \quad \frac{47}{14} \quad \frac{44}{50}$$

$$\frac{64}{50} \quad \frac{54}{30} \quad \frac{51}{16} \quad \frac{48}{8} \quad \frac{46}{11} \quad \frac{52}{11} \quad \frac{48}{13} \quad \frac{45}{50}$$

$$\frac{46}{50} \quad \frac{48}{30} \quad \frac{48}{17} \quad \frac{52}{13} \quad \frac{49}{10} \quad \frac{48}{13} \quad \frac{51}{13} \quad \frac{51}{50}$$

$$\frac{42}{50} \quad \frac{49}{16} \quad \frac{56}{14} \quad \frac{50}{8} \quad \frac{51}{8} \quad \frac{52}{50}$$

$$\frac{46}{50} \quad \frac{49}{18} \quad \frac{58}{15} \quad \frac{51}{9} \quad \frac{50}{9} \quad \frac{51}{34} \quad \frac{51}{50}$$

Spike in 14" Oak 100' Rt. 512, 36 + 65

Sta. + π - Elev.

914.89

36+50 11.5.

37 10.9.

+50 10.3.

38 10.2.

+50 09.9.

39 09.1.

+50 08.2.

T.P. 3.47 910.88 7.48 907.41

40 07.6.

+50 07.3.

41 07.0.

+50 06.5.

42 05.9.

4

7

Rt

13

$\frac{23}{50}$ $\frac{23}{30}$ $\frac{25}{18}$ $\frac{27}{17}$ $\frac{26}{11}$ $\frac{24}{7}$ $\frac{24}{8}$ $\frac{27}{8}$ $\frac{41}{13}$ $\frac{38}{16}$ $\frac{40}{50}$

$\frac{4^1}{30} \quad \frac{4^0}{18} \quad \frac{4^5}{16} \quad \frac{4^5}{14} \quad \frac{4^2}{11} \quad \frac{4^0}{1} \quad \frac{4^4}{12} \quad \frac{4^6}{30}$

$$\frac{4.5}{50} \quad \frac{44}{17} \quad \frac{52}{15} \quad \frac{46}{6} \quad \frac{46}{17} \quad \frac{53}{17} \quad \frac{48}{19} \quad \frac{52}{50}$$

$$\frac{4.0}{50} \quad \frac{4.1}{18} \quad \frac{5.0}{15} \quad \frac{4.6}{5} \quad 4.7 \quad \frac{4.7}{5} \quad \frac{5.3}{14} \quad \frac{4.9}{16} \quad \frac{5.0}{50}$$

$$\frac{36}{50} \quad \frac{40}{19} \quad \frac{55}{15} \quad \frac{47}{4} \quad \frac{50}{2} \quad \frac{52}{6} \quad \frac{57}{13} \quad \frac{49}{16} \quad \frac{50}{50}$$

$\frac{4.9}{50}$	$\frac{4.7}{18}$	$\frac{6.4}{15}$	$\frac{5.8}{7}$	$\frac{5.7}{4}$	$\frac{5.8}{1}$	$\frac{5.7}{1}$	$\frac{6.2}{9}$	$\frac{6.2}{12}$	$\frac{5.4}{16}$	$\frac{6.1}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{6.2}{50}$	$\frac{6.3}{15}$	$\frac{6.4}{3}$	$\frac{6.5}{6}$	$\frac{6.6}{8}$	$\frac{7.1}{17}$	$\frac{8.3}{50}$
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26	28	33	40	33	31	33	34	43	50	50
50	38	37	23	19	3	3	8	13	37	50

$\frac{35}{50}$	$\frac{34}{39}$	$\frac{51}{38}$	$\frac{58}{22}$	$\frac{40}{15}$	$\frac{34}{4}$	$\frac{36}{21}$	$\frac{36}{7}$	$\frac{46}{19}$	$\frac{53}{33}$	$\frac{57}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	----------------	-----------------	-----------------	-----------------

4.6	46	6.0	6.6	48	3.9		40	5.1	5.8
<u>30</u>	<u>38</u>	<u>35</u>	<u>22</u>	<u>16</u>	<u>3</u>	<u>39</u>	<u>7</u>	<u>23</u>	<u>50</u>

$\frac{5.5}{50} \frac{5.5}{38} \frac{6.7}{36} \frac{7.3}{22} \frac{5.3}{16} \frac{4.5}{6} \frac{4.4}{1} \frac{4.5}{8} \frac{5.6}{15} \frac{6.0}{21} \frac{5.8}{50}$

$\frac{64}{50}$	$\frac{64}{39}$	$\frac{72}{37}$	$\frac{72}{22}$	$\frac{54}{13}$	$\frac{50}{2}$	$\frac{50}{10}$	$\frac{63}{19}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------

Sta.	+	π	-	Elev.
		910.88		
42+50				05.9
43				05.6
+45	V.T.P Culvert			05.5
44				05.7
+50				06.2
45				06.5
+20				06.6
+60				06.3
T.P.	6.98	913.22	4.64	906.24
46				06.4
+50				06.5
47				06.4
+50				06.4

Lt.

L

Rt.

14

$$\frac{7.2}{50} \quad \frac{7.0}{18} \quad \frac{5.4}{8} \quad \frac{5.0}{50} \quad \frac{5.2}{11} \quad \frac{7.0}{20} \quad \frac{7.2}{50}$$

$$\frac{7.1}{50} \quad \frac{7.3}{18} \quad \frac{5.5}{10} \quad \frac{5.3}{50} \quad \frac{5.6}{11} \quad \frac{7.2}{20} \quad \frac{7.3}{50}$$

03.3

$$\frac{7.6}{50} \quad \frac{7.0}{21} \quad \frac{7.4}{15} \quad \frac{5.6}{8} \quad \frac{5.4}{50} \quad \frac{6.0}{10} \quad \frac{8.1}{20} \quad \frac{8.1}{41} \quad \frac{7.6}{50} \quad \frac{7.7}{50}$$

$$\frac{6.5}{50} \quad \frac{6.6}{44} \quad \frac{6.8}{17} \quad \frac{5.2}{9} \quad \frac{5.2}{50} \quad \frac{5.5}{10} \quad \frac{6.9}{18} \quad \frac{6.7}{23} \quad \frac{6.7}{50}$$

$$\frac{5.7}{50} \quad \frac{5.8}{14} \quad \frac{5.1}{9} \quad \frac{4.7}{50} \quad \frac{5.2}{12} \quad \frac{6.1}{19} \quad \frac{5.8}{21} \quad \frac{5.6}{50}$$

$$\frac{5.1}{50} \quad \frac{4.8}{20} \quad \frac{5.3}{18} \quad \frac{4.6}{5} \quad \frac{4.4}{50} \quad \frac{4.7}{12} \quad \frac{5.0}{17} \quad \frac{4.6}{19} \quad \frac{4.5}{50}$$

$$\frac{4.1}{50} \quad \frac{4.2}{20} \quad \frac{4.8}{17} \quad \frac{4.4}{11} \quad \frac{4.0}{5} \quad \frac{4.3}{50} \quad \frac{4.3}{9} \quad \frac{4.4}{18} \quad \frac{3.7}{22} \quad \frac{4.0}{50}$$

$$\frac{1.8}{50} \quad \frac{1.4}{21} \quad \frac{4.3}{15} \quad \frac{4.2}{2} \quad \frac{4.6}{1} \quad \frac{4.6}{50} \quad \frac{4.6}{6} \quad \frac{4.2}{7} \quad \frac{4.6}{14} \quad \frac{1.0}{23} \quad \frac{0.7}{50}$$

$$\frac{3.4}{50} \quad \frac{3.2}{22} \quad \frac{6.3}{15} \quad \frac{6.1}{4} \quad \frac{6.8}{2} \quad \frac{6.8}{50} \quad \frac{6.9}{5} \quad \frac{6.0}{8} \quad \frac{6.1}{13} \quad \frac{2.5}{24} \quad \frac{2.3}{50}$$

$$\frac{6.4}{50} \quad \frac{5.7}{18} \quad \frac{6.4}{16} \quad \frac{6.8}{12} \quad \frac{6.7}{50} \quad \frac{6.5}{4} \quad \frac{5.7}{7} \quad \frac{6.2}{14} \quad \frac{4.4}{20} \quad \frac{3.6}{50}$$

$$\frac{7.6}{50} \quad \frac{7.2}{22} \quad \frac{6.7}{8} \quad \frac{6.8}{50} \quad \frac{6.7}{16} \quad \frac{6.4}{23} \quad \frac{5.9}{50}$$

$$\frac{8.8}{50} \quad \frac{8.5}{18} \quad \frac{7.0}{6} \quad \frac{6.8}{50} \quad \frac{7.0}{10} \quad \frac{7.8}{15} \quad \frac{7.8}{30} \quad \frac{7.6}{50}$$

Sta.	+	K	-	Elev.
------	---	---	---	-------

913.72

48				06.4
----	--	--	--	------

+50				06.6
-----	--	--	--	------

49				07.1
----	--	--	--	------

+50				07.4
-----	--	--	--	------

50				07.7
----	--	--	--	------

+50				08.8
-----	--	--	--	------

51				09.7
----	--	--	--	------

+50				10.2
-----	--	--	--	------

52				10.5
----	--	--	--	------

B.M	5.22	914.68	3.76	909.46
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10.5

+50				10.5
-----	--	--	--	------

53				10.0
----	--	--	--	------

+50				09.8
-----	--	--	--	------

Lt.

Q

Rt.

15

$$\frac{7.3}{50} \quad \frac{7.7}{16} \quad \frac{6.7}{7} \quad \frac{6.8}{8} \quad \frac{7.2}{8} \quad \frac{8.4}{14} \quad \frac{9.2}{33} \quad \frac{8.9}{50}$$

$$\frac{6.5}{50} \quad \frac{7.5}{16} \quad \frac{6.6}{8} \quad \frac{6.6}{9} \quad \frac{6.9}{9} \quad \frac{8.1}{18} \quad \frac{9.0}{29} \quad \frac{9.2}{50}$$

$$\frac{7.1}{50} \quad \frac{7.9}{19} \quad \frac{6.4}{10} \quad \frac{6.1}{14} \quad \frac{6.6}{14} \quad \frac{8.7}{28} \quad \frac{9.0}{39} \quad \frac{8.7}{50}$$

$$\frac{6.6}{50} \quad \frac{6.8}{18} \quad \frac{6.0}{7} \quad \frac{5.8}{10} \quad \frac{6.3}{10} \quad \frac{7.1}{19} \quad \frac{7.7}{33} \quad \frac{7.4}{50}$$

$$\frac{4.5}{50} \quad \frac{5.2}{18} \quad \frac{5.8}{15} \quad \frac{5.4}{6} \quad \frac{5.5}{18} \quad \frac{5.9}{18} \quad \frac{5.9}{50}$$

$$\frac{3.3}{50} \quad \frac{3.3}{23} \quad \frac{3.2}{17} \quad \frac{4.7}{10} \quad \frac{4.7}{9} \quad \frac{5.0}{13} \quad \frac{3.7}{17} \quad \frac{3.8}{50}$$

$$\frac{2.2}{50} \quad \frac{2.4}{18} \quad \frac{3.8}{15} \quad \frac{3.5}{8} \quad \frac{3.5}{35} \quad \frac{3.7}{5} \quad \frac{4.1}{13} \quad \frac{2.5}{18} \quad \frac{2.5}{50}$$

$$\frac{1.8}{50} \quad \frac{2.2}{18} \quad \frac{3.7}{14} \quad \frac{3.3}{9} \quad \frac{3.2}{9} \quad \frac{3.5}{14} \quad \frac{2.5}{17} \quad \frac{2.8}{30}$$

$$\frac{1.9}{50} \quad \frac{2.2}{17} \quad \frac{2.8}{13} \quad \frac{2.7}{13} \quad \frac{3.5}{13} \quad \frac{3.8}{25} \quad \frac{3.8}{50}$$

Spk. in 12' stump 50' Rt Sta 52+50

$$\frac{3.4}{50} \quad \frac{3.7}{29} \quad \frac{4.1}{17} \quad \frac{4.4}{15} \quad \frac{4.7}{16} \quad \frac{5.4}{50}$$

$$\frac{4.1}{50} \quad \frac{4.3}{18} \quad \frac{4.8}{15} \quad \frac{4.7}{12} \quad \frac{5.4}{12} \quad \frac{6.7}{50}$$

$$\frac{4.1}{50} \quad \frac{4.3}{25} \quad \frac{5.0}{21} \quad \frac{5.0}{10} \quad \frac{4.9}{15} \quad \frac{5.2}{15} \quad \frac{6.4}{50}$$

Sta. + x - Elev.

914.68

54 09.5

+50 09.5

55 09.5

+50 ~~09.0~~
~~08.9~~

56 08.5

+50 08.0

T.P. 5.26 912.40 7.64 907.04

57 07.0

+50 06.7

58 06.1

+47 V.T.P. Culvert 05.7

59 05.4

+50 06.0

Lt.

£

Rt.

16

$$\frac{3.9}{50} \quad \frac{4.3}{23} \quad \frac{6.7}{19} \quad \frac{5.5}{10} \quad \frac{5.2}{51} \quad \frac{5.8}{13} \quad \frac{4.9}{16} \quad \frac{5.8}{50}$$

$$\frac{4.2}{50} \quad \frac{4.1}{40} \quad \frac{4.6}{24} \quad \frac{6.9}{20} \quad \frac{5.3}{9} \quad \frac{5.2}{52} \quad \frac{6.1}{12} \quad \frac{4.5}{16} \quad \frac{5.1}{50}$$

$$\frac{3.9}{50} \quad \frac{4.6}{23} \quad \frac{6.1}{21} \quad \frac{5.3}{7} \quad \frac{5.2}{51} \quad \frac{6.3}{13} \quad \frac{5.2}{16} \quad \frac{4.6}{50}$$

$$\frac{3.9}{50} \quad \frac{4.7}{23} \quad \frac{6.5}{18} \quad \frac{5.8}{8} \quad \frac{5.7}{51} \quad \frac{6.3}{12} \quad \frac{5.2}{15} \quad \frac{5.4}{50}$$

$$\frac{4.6}{50} \quad \frac{5.5}{18} \quad \frac{6.5}{15} \quad \frac{6.2}{8} \quad \frac{6.2}{62} \quad \frac{7.0}{13} \quad \frac{6.4}{14} \quad \frac{7.1}{50}$$

$$\frac{6.4}{50} \quad \frac{7.1}{21} \quad \frac{6.9}{8} \quad \frac{6.7}{61} \quad \frac{7.0}{11} \quad \frac{8.1}{15} \quad \frac{8.7}{50}$$

$$\frac{6.1}{50} \quad \frac{6.6}{16} \quad \frac{5.2}{10} \quad \frac{5.4}{54} \quad \frac{5.5}{9} \quad \frac{6.8}{18} \quad \frac{7.2}{50}$$

$$\frac{6.9}{50} \quad \frac{7.1}{17} \quad \frac{5.8}{10} \quad \frac{5.7}{57} \quad \frac{6.2}{11} \quad \frac{7.4}{17} \quad \frac{7.9}{50}$$

$$\frac{7.1}{50} \quad \frac{7.5}{16} \quad \frac{6.3}{9} \quad \frac{6.3}{63} \quad \frac{6.4}{11} \quad \frac{8.1}{19} \quad \frac{8.2}{50}$$

$$\text{Flow Line} \quad \frac{7.9}{50} \quad \frac{8.0}{18} \quad \frac{6.6}{11} \quad \frac{6.7}{61} \quad \frac{7.0}{12} \quad \frac{8.2}{18} \quad \frac{8.8}{50}$$

8.4

(04.0)

$$\text{Flow time} \quad \frac{8.9}{50} \quad (03.5)$$

$$\frac{7.8}{50} \quad \frac{8.1}{16} \quad \frac{7.0}{12} \quad \frac{7.0}{70} \quad \frac{7.2}{14} \quad \frac{8.3}{18} \quad \frac{8.6}{50}$$

$$\frac{7.8}{50} \quad \frac{7.9}{17} \quad \frac{6.8}{12} \quad \frac{6.4}{64} \quad \frac{6.6}{12} \quad \frac{8.3}{18} \quad \frac{8.3}{50}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

912.40

60				06.2
----	--	--	--	------

+50				06.2
-----	--	--	--	------

61				06.6
----	--	--	--	------

+50				06.6
-----	--	--	--	------

62				07.0
----	--	--	--	------

+50				06.7
-----	--	--	--	------

63				06.2
----	--	--	--	------

+50				06.4
-----	--	--	--	------

+70				06.3
-----	--	--	--	------

64				06.4
----	--	--	--	------

B.M.	2.70	911.70	3.37	909.08
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+50				06.2
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Lt¢Rt17

$$\frac{7.2}{50} \quad \frac{7.2}{16} \quad \frac{6.5}{11} \quad \frac{6.2}{\cancel{6.1}} \quad \frac{6.3}{10} \quad \frac{7.1}{19} \quad \frac{7.3}{50}$$

$$\frac{6.2}{50} \quad \frac{6.4}{19} \quad \frac{6.2}{7} \quad \frac{6.2}{\cancel{6.1}} \quad \frac{6.3}{14} \quad \frac{7.5}{19} \quad \frac{7.0}{24} \quad \frac{6.5}{27} \quad \frac{6.9}{50}$$

$$\frac{4.8}{50} \quad \frac{5.1}{14} \quad \frac{6.0}{13} \quad \frac{5.8}{4} \quad \frac{5.8}{\cancel{5.7}} \quad \frac{6.0}{9} \quad \frac{6.8}{22} \quad \frac{5.6}{28} \quad \frac{5.8}{50}$$

$$\frac{3.8}{50} \quad \frac{3.7}{15} \quad \frac{6.0}{10} \quad \frac{5.8}{4} \quad \frac{5.8}{\cancel{5.7}} \quad \frac{5.6}{10} \quad \frac{5.7}{24} \quad \frac{4.8}{28} \quad \frac{5.5}{50}$$

$$\frac{3.5}{50} \quad \frac{3.7}{13} \quad \frac{5.7}{10} \quad \frac{5.4}{\cancel{5.3}} \quad \frac{5.6}{8} \quad \frac{6.6}{20} \quad \frac{5.5}{27} \quad \frac{6.2}{50}$$

$$\frac{4.3}{50} \quad \frac{4.4}{30} \quad \frac{4.9}{14} \quad \frac{5.7}{11} \quad \frac{5.8}{4} \quad \frac{5.7}{\cancel{5.6}} \quad \frac{6.0}{13} \quad \frac{6.7}{17} \quad \frac{6.7}{22} \quad \frac{6.1}{26} \quad \frac{6.2}{50}$$

$$\frac{6.4}{50} \quad \frac{6.5}{21} \quad \frac{6.2}{\cancel{6.1}} \quad \frac{6.3}{13} \quad \frac{6.8}{21} \quad \frac{6.4}{22} \quad \frac{6.4}{50}$$

$$\frac{6.7}{50} \quad \frac{6.4}{31} \quad \frac{7.5}{29} \quad \frac{7.5}{19} \quad \frac{6.3}{11} \quad \frac{6.0}{\cancel{5.9}} \quad \frac{6.2}{18} \quad \frac{4.9}{23} \quad \frac{4.7}{50}$$

$$\frac{6.0}{20} \quad \frac{5.8}{32} \quad \frac{6.8}{29} \quad \frac{7.0}{23} \quad \frac{7.4}{19} \quad \frac{6.2}{8} \quad \frac{6.1}{\cancel{6.0}} \quad \frac{6.6}{14} \quad \frac{2.1}{17} \quad \frac{4.7}{18} \quad \frac{4.4}{50}$$

$$\frac{5.1}{50} \quad \frac{5.5}{33} \quad \frac{6.6}{31} \quad \frac{7.2}{21} \quad \frac{6.1}{8} \quad \frac{6.0}{\cancel{5.9}} \quad \frac{6.8}{16} \quad \frac{5.3}{21} \quad \frac{5.0}{50}$$

Spike in 14" stump 100' Rt. Sta 64+00

$$\frac{2.8}{50} \quad \frac{4.0}{41} \quad \frac{6.7}{24} \quad \frac{6.5}{18} \quad \frac{5.2}{9} \quad \frac{5.4}{\cancel{5.3}} \quad \frac{5.5}{3} \quad \frac{5.8}{10} \quad \frac{6.6}{14} \quad \frac{6.2}{50}$$

Sta. + x - Elev.

911.78

65 06.0

+50 06.6

66 07.2

T.P. 3.83 912.91 2.70 909.08

07.7

+50 07.9

67 07.7

+50 06.1

68 05.3

+50 05.4

T.P. 5.55 910.71 2.75 905.16

69 05.4

+50 05.0

70 04.4

4.

E

B4

18

$$\frac{43}{50} \quad \frac{47}{31} \quad \frac{72}{18} \quad \frac{58}{10} \quad \frac{58}{5} \quad \frac{53}{2} \quad \frac{59}{8} \quad \frac{73}{17} \quad \frac{24}{50}$$

$$\frac{22}{50} \quad \frac{72}{41} \quad \frac{39}{35} \quad \frac{39}{21} \quad \frac{50}{13} \quad \frac{50}{6} \quad \frac{52}{5} \quad \frac{53}{6} \quad \frac{60}{11} \quad \frac{71}{15} \quad \frac{73}{50}$$

$$\frac{75}{50} \quad \frac{73}{31} \quad \frac{41}{23} \quad \frac{38}{9} \quad \frac{44}{2} \quad \frac{46}{5} \quad \frac{52}{8} \quad \frac{64}{14} \quad \frac{88}{21} \quad \frac{91}{26} \quad \frac{95}{28} \quad \frac{61}{34} \quad \frac{61}{50}$$

$$\frac{83}{50} \quad \frac{87}{37} \quad \frac{87}{35} \quad \frac{86}{24} \quad \frac{66}{16} \quad \frac{51}{8} \quad \frac{50}{5} \quad \frac{56}{10} \quad \frac{71}{15} \quad \frac{101}{22} \quad \frac{101}{24} \quad \frac{66}{31} \quad \frac{64}{50}$$

$$\frac{74}{50} \quad \frac{77}{37} \quad \frac{87}{29} \quad \frac{85}{21} \quad \frac{61}{15} \quad \frac{63}{9} \quad \frac{52}{5} \quad \frac{49}{6} \quad \frac{50}{16} \quad \frac{72}{25} \quad \frac{76}{40} \quad \frac{77}{50}$$

$$\frac{84}{50} \quad \frac{83}{38} \quad \frac{87}{32} \quad \frac{90}{19} \quad \frac{72}{13} \quad \frac{68}{5} \quad \frac{64}{5} \quad \frac{57}{10} \quad \frac{52}{14} \quad \frac{55}{31} \quad \frac{80}{36} \quad \frac{88}{50}$$

$$\frac{89}{50} \quad \frac{90}{38} \quad \frac{106}{33} \quad \frac{106}{28} \quad \frac{94}{19} \quad \frac{81}{13} \quad \frac{76}{5} \quad \frac{76}{9} \quad \frac{81}{16} \quad \frac{44}{27} \quad \frac{55}{41} \quad \frac{86}{50}$$

$$\frac{91}{50} \quad \frac{94}{35} \quad \frac{107}{28} \quad \frac{96}{21} \quad \frac{80}{13} \quad \frac{75}{8} \quad \frac{75}{11} \quad \frac{75}{13} \quad \frac{89}{20} \quad \frac{89}{26} \quad \frac{55}{35} \quad \frac{50}{39} \quad \frac{52}{50}$$

$$\frac{69}{50} \quad \frac{67}{41} \quad \frac{65}{34} \quad \frac{81}{28} \quad \frac{88}{26} \quad \frac{73}{21} \quad \frac{63}{19} \quad \frac{55}{11} \quad \frac{53}{5} \quad \frac{54}{13} \quad \frac{60}{16} \quad \frac{72}{19} \quad \frac{72}{28} \quad \frac{61}{31} \quad \frac{57}{37} \quad \frac{34}{44} \quad \frac{31}{50}$$

$$\frac{67}{50} \quad \frac{67}{48} \quad \frac{67}{46} \quad \frac{66}{35} \quad \frac{74}{33} \quad \frac{77}{26} \quad \frac{72}{21} \quad \frac{60}{16} \quad \frac{58}{10} \quad \frac{57}{5} \quad \frac{64}{15} \quad \frac{72}{18} \quad \frac{78}{24} \quad \frac{79}{28} \quad \frac{64}{32} \quad \frac{63}{50}$$

$$\frac{64}{50} \quad \frac{66}{36} \quad \frac{75}{34} \quad \frac{78}{28} \quad \frac{73}{21} \quad \frac{63}{16} \quad \frac{59}{11} \quad \frac{59}{13} \quad \frac{63}{5} \quad \frac{69}{6} \quad \frac{63}{11} \quad \frac{65}{15} \quad \frac{74}{19} \quad \frac{79}{25} \quad \frac{78}{29} \quad \frac{67}{31} \quad \frac{65}{50}$$

Sta.

+

K

-

Elev.

910.71

70+65

04.2

+80

05.0

+89

05.3

71+06.28

05.6

B.M.

2.74

907.97

Lt.

Z

Rt.

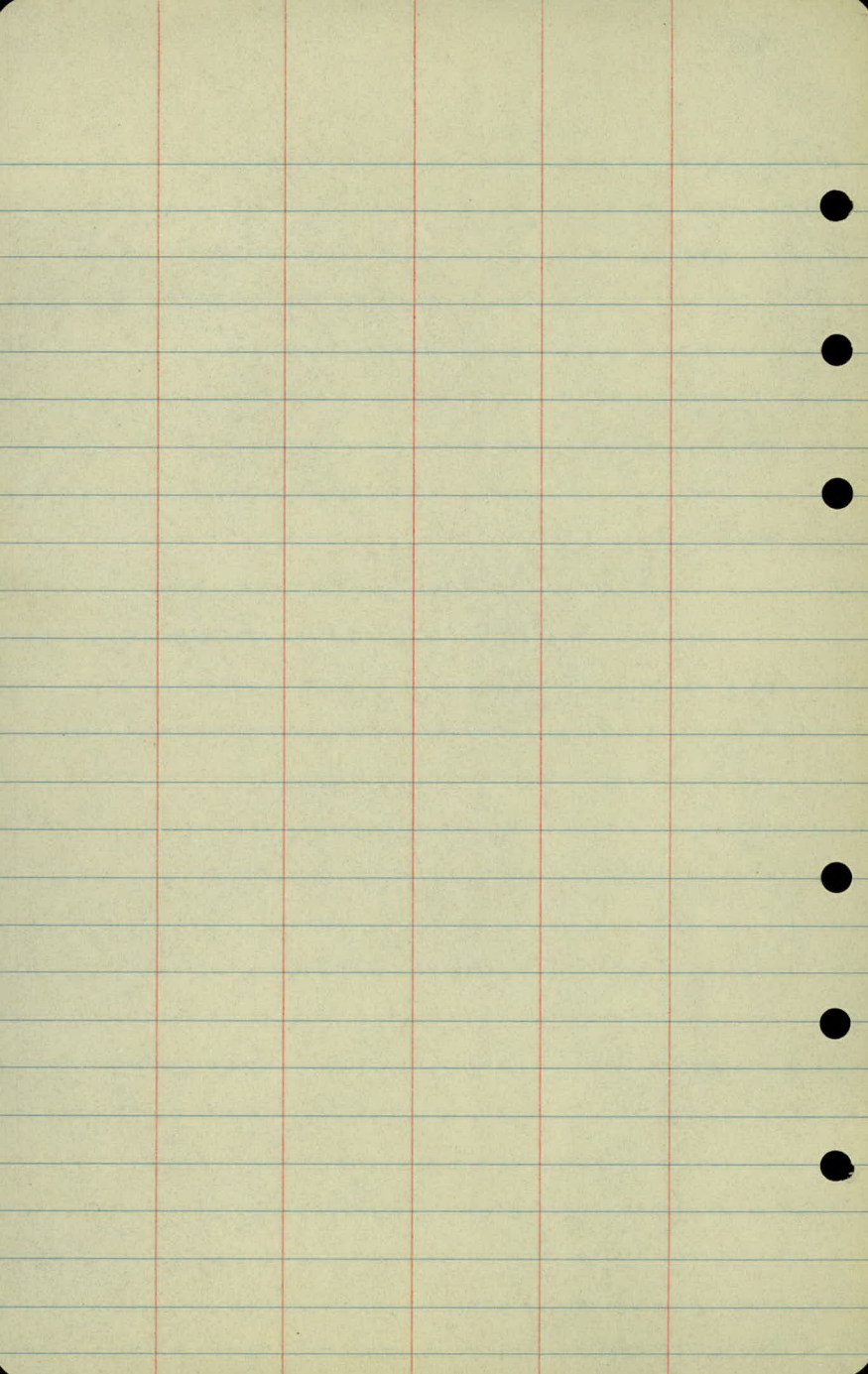
19

 $\frac{75}{50}$ $\frac{74}{34}$ $\frac{86}{31}$ $\frac{76}{21}$ $\frac{65}{18}$ $\frac{65}{9}$ $\frac{65}{5}$ $\frac{64}{5}$ $\frac{78}{17}$ $\frac{71}{31}$ $\frac{76}{50}$
 $\frac{77}{50}$ $\frac{72}{18}$ $\frac{60}{15}$ $\frac{55}{9}$ $\frac{57}{6}$ $\frac{60}{6}$ $\frac{72}{9}$ $\frac{77}{50}$
 $\frac{53}{50}$
 $\frac{54}{50}$
 $\frac{54}{50}$
shoulder
"I"
 $\frac{47}{100}$
 $\frac{50}{50}$
 $\frac{51}{50}$
 $\frac{49}{50}$
 $\frac{49}{100}$

Ch. I.

R.R. Spike in 12" Oak 33' Rt. Sta. 73+50

No. Co Line Rd. "I". Refer to "I" improvement plans.



Topography

Long Lake Rd

From

S.T.H #10 To No. Co. Line

{ Wilke
Goldberg
Larsen 9/37

L1

L2

R1

5 +29 Reg Brush
23'

ER
7'

ER
5'

FC
22'

4

ER
7'

ER
5'

FC
23'

+85 4" Oak
20'

3

ER
8'

ER
4'

FC
22'

+82 6-6" Oak
22'

+62 Group 7 4" Oak
22'

2

+06 End Trees
21'

ER
8'

ER
4'

FC
22'

+42 FC Cor
23'

1

+13 Reg 15 Traces R/W
25'

ER
10'

ER
8'

+10 End Timber
30'

+94 2-6" Oak
17'

+82 Rd Sign
20'

+68 Cor Ho
106'

+61 End Timber
36'

+59 Cor House
95'

0

ER
11'

ER
8'

1

21

[illegible]

2

3 strands 1300000

Cultivated

pasture

5. I. H. #1

27. Conc. Base

47

疾

RT

+96 6" Pop
28'

+82 15" Pop.
34'

+33 24" Pop
32'
+29 12" Pine
52'

+31 Cor Ho
125'

12

Fe 24' ET 5' ET 3' Fe 18'

+70 2" Pipe Line

+52 Ent

+31 End Cult +31 Fe Cor
120 End Brush 25'

+31 End of Grate Beg Trail
ER 6' ER 6' Fe 18' +06 Fe Cor 12'

10

Brush 12' ER 7' ER 6' Fe Cor 20'

9

Brush 21' ER 7' ER 6' Fe 21'

+65 Bog Brush
21'

8

ER 8' ER 6' Fe 20'

+25 End Brush
21'

7

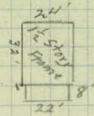
ER 8' ER 5' Fe 21'

6

Brush 21' ER 8' ER 5' Fe 21'

Scattered Oaks
+ Stumps

22



Brush

Gene Condit

ST Paul W.W - R/W

Cultivated

Pasture

55 50 40 30 20 10

+ 25 $\frac{6'' \text{ Pop}}{15'}$

19 $\frac{Fc}{26}$ $\frac{Tr}{5}$ $\frac{Tr}{3}$

+ 40 Clump Pop $\frac{15'}$

18 $\frac{Fc}{26}$ $\frac{Tr}{5}$ $\frac{Tr}{3}$

17 $\frac{Fc}{26}$ $\frac{Tr}{1}$ $\frac{Tr}{7}$

+ 60 End Trees $\frac{15'}$

16 $\frac{Fc}{26}$ $\frac{Tr}{3}$ $\frac{Tr}{5}$

15 $\frac{Fc}{25}$ $\frac{Tr}{3}$ $\frac{Tr}{5}$ $\frac{Fc}{15}$ + 09 Fc Box $\frac{15'}$

+ 61 Beg Row 25 Pop on R $\frac{15'}$

14 $\frac{Fc}{25}$ $\frac{Tr}{4}$ $\frac{Tr}{4}$ $\frac{Fc}{19'}$

+ 60 End Brushy
Beg Hay Meadow

+ 64 End + 72 Fc Box $\frac{24'}$
+ 44 8" Oak $\frac{29'}$ + 70 Row 5 Trees $\frac{34'}$
+ 41 6" Twin Oak $\frac{15'}$

13 $\frac{Fc}{25}$ $\frac{Tr}{8'}$ $\frac{Tr}{0.0}$ $\frac{Fc}{23}$

Meadow

Cult.

Cultivated

Meadow

Pasture

Yard
scattered
trees

28

$$\frac{Fc}{28} \quad \frac{Tf}{5} \quad \frac{Tf}{3}$$

+65' X Drain
Imp. 12" X 34 Vit.

25

$$\frac{Fc}{28'} \quad \frac{Tf}{5} \quad \frac{Tf}{3}$$

24

$$\frac{Fc}{28'} \quad \frac{Tf}{3} \quad \frac{Tf}{5}$$

+61 End Out
Beg Hay Meadow

23 End Brush + Beg Meadow

$$\frac{Fc}{28'} \quad \frac{Tf}{3} \quad \frac{Tf}{5}$$

22

$$\frac{Fc}{28'} \quad \frac{Tf}{2} \quad \frac{Tf}{2}$$

21

$$\frac{Fc}{28'} \quad \frac{Tf}{7} \quad \frac{Tf}{1}$$

+52 6" Pop
10'

20

Beg Brush

$$\frac{Fc}{26} \quad \frac{Tf}{3} \quad \frac{Tf}{3}$$

Meadow

Brush

Meadow

Corn Cultivated

$$+54 \frac{Fe}{73}$$

33

$$\frac{Fe}{29} \quad \frac{Tr}{7} \quad \frac{Tr}{2} \quad \frac{Fe}{27}$$

+85 FeCor 33' +90 Ent
+85 Beg Small Tree
+13 Brush

32

$$\frac{Fe}{29} \quad \frac{Tr}{8} \quad \frac{Tr}{3}$$

31

$$\frac{Fe}{29} \quad \frac{Tr}{8} \quad \frac{Tr}{3}$$

30

$$\frac{Fe}{29} \quad \frac{Tr}{8} \quad \frac{Tr}{3}$$

29

Beg Brush
29'

$$\frac{Fe}{29} \quad \frac{Tr}{8} \quad \frac{Tr}{1}$$

28

$$\frac{Fe}{28} \quad \frac{Tr}{6} \quad \frac{Tr}{2}$$

27

$$\frac{Fe}{28} \quad \frac{Tr}{5} \quad \frac{Tr}{3}$$

Timber + Brush

Cott

Meadow

+90 Ent

+50 End Brushy Bog
Meadow

40 End Heavy Timber $\frac{Fc}{16}$ $\frac{Tr}{1}$ $\frac{Tr}{7}$ $\frac{Fc}{16}$

+80 Ent

+64 12" Oak
10"

39 $\frac{Fc}{19}$ $\frac{Tr}{3}$ $\frac{Tr}{5}$ $\frac{Fc}{15}$

38 $\frac{Fc}{22'}$ $\frac{Tr}{4}$ $\frac{Tr}{4}$ $\frac{Fc}{13'}$

+79 Fc Cor End Brushy Bog
Heavy Timber

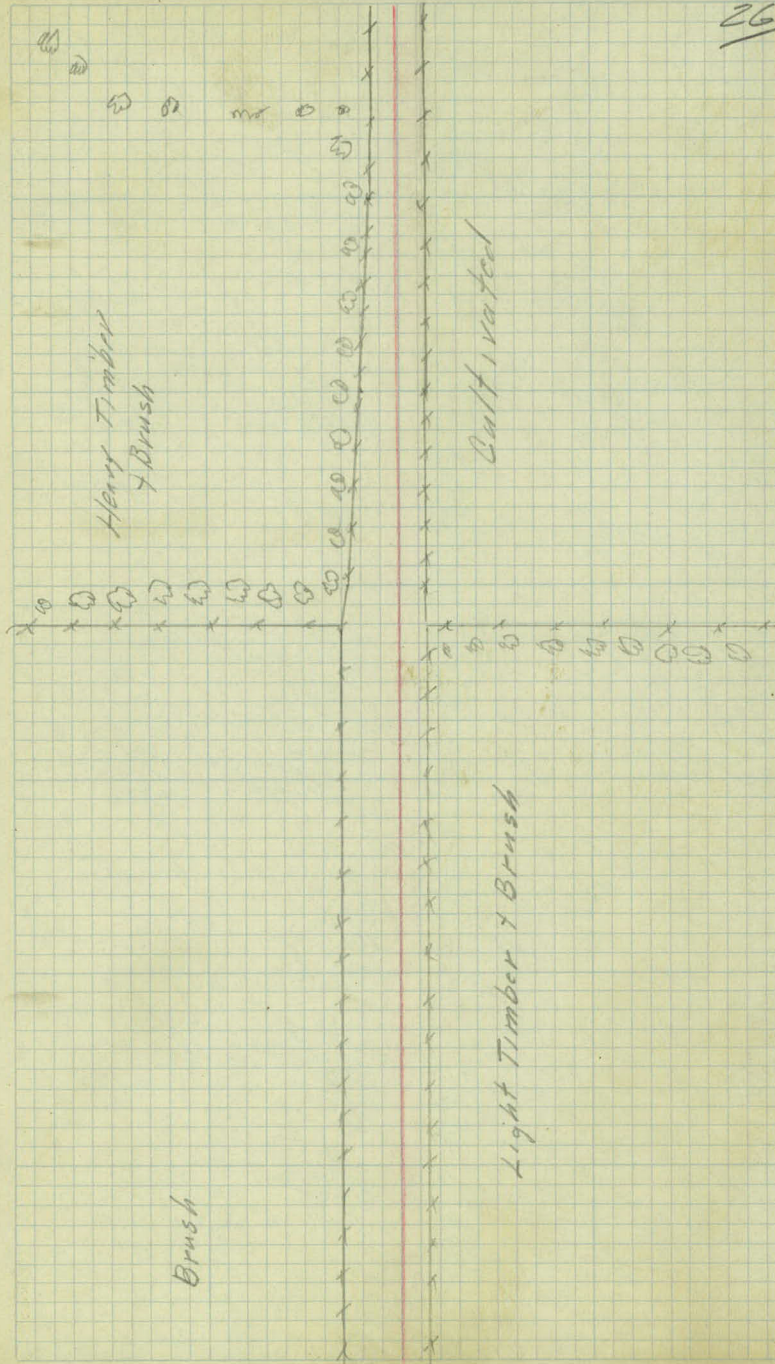
+79 Fc Cor End Brushy
Small Timber
Bog Cor

37 $\frac{Fc}{31'}$ $\frac{Tr}{6}$ $\frac{Tr}{2}$ $\frac{Fc}{15'}$

36 $\frac{Fc}{31'}$ $\frac{Tr}{6}$ $\frac{Tr}{2}$ $\frac{Fc}{14'}$

35 $\frac{Fc}{30}$ $\frac{Tr}{5}$ $\frac{Tr}{3}$ $\frac{Fc}{13}$ Timber
12'

34 $\frac{Fc}{30'}$ $\frac{Tr}{6}$ $\frac{Tr}{2}$ $\frac{Fc}{12}$



$$47 \quad \frac{Fc}{20'} \quad \frac{Tr}{3} \quad \frac{Tr}{5} \quad \frac{Fc}{20'}$$

+30 Bog Heavy Meadow +55 Enl

+40 End Brush + Oaks
22

$$+18 \frac{6'' \text{ Pop}}{16'}$$

$$46 \quad \frac{Fc}{22'} \quad \frac{Tr}{2} \quad \frac{Tr}{6} \quad \frac{Fc}{21}$$

$$+75 \frac{1'' \text{ Pop}}{17'}$$

+15 Bog Brush + Scatter Oak

$$45 \quad \frac{Fc}{20'} \quad \frac{Tr}{2} \quad \frac{Tr}{6} \quad \frac{Fc}{21}$$

+20 End Path hole
50'

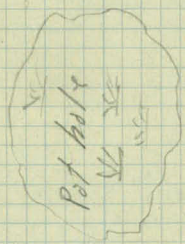
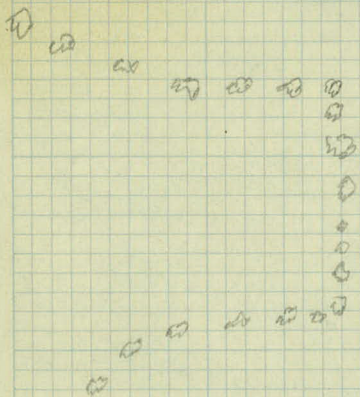
$$44 \quad \frac{Fc}{17'} \quad \frac{Tr}{2} \quad \frac{Tr}{6} \quad \frac{Fc}{20'}$$

+56 X Drain
Imp 12" X 30 Vt

$$43 \quad \text{Bog Path hole} \quad \frac{Fc}{17} \quad \frac{Tr}{3} \quad \frac{Tr}{5} \quad \frac{Fc}{19}$$

$$42 \quad \frac{Fc}{16} \quad \frac{Tr}{4} \quad \frac{Tr}{4} \quad \frac{Fc}{19}$$

$$41 \quad \frac{Fc}{16} \quad \text{Trail} \quad \frac{Trail}{6} \quad \frac{Fc}{18}$$



Meadow



Cultivated

54

Fe	Tr	Tr
24'	8'	1'

 Tree Line
26'

53

Fe	Tr	Tr
19'	8'	1'

 Tree Line
26'

52

Fe	Tr	Tr	:	Tree Line
17'	7'	1'		26'

51

 +38 Fe Car
15

Fe	Tr	Tr	Fe
18'	6'	2'	16'

 Tree Line
26'

 +50 Tree Line
50

50

 Beg Brush + Timber
20'

Fe	Tr	Tr	Fe
16'	5'	3'	17'

 +90 Tree Line
100

+91 Ent

49

 Brush
100'

Fe	Tr	Tr	Fe
19'	3'	5'	18'

48

Fe	Tr	Tr	Fe
20'	3'	5'	17'

to

Meadow

Heavy Timber & Brush

to

Heavy

Timber

Stumps

Meadow

Meadow

$$61 \quad \frac{Fc}{17} \quad \frac{Tr}{3} \quad \frac{Tr}{5}$$

$$60 \quad \frac{Fc}{18} \quad \frac{Tr}{6} \quad \frac{Tr}{2}$$

$$59 \quad \frac{Fc}{19'} \quad \frac{Tr}{3} \quad \frac{Tr}{5}$$

+47 X Drain
Imp 12" X 32'

$$58 \quad \frac{Fc}{19} \quad \frac{Tr}{4} \quad \frac{Tr}{4}$$

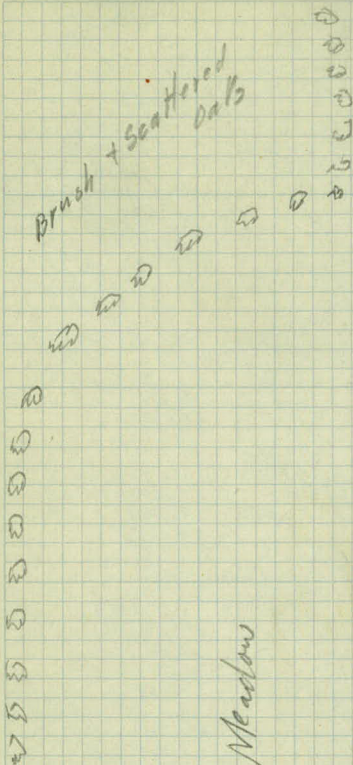
$$57 \quad \frac{Fc}{20} \quad \frac{Tr}{5} \quad \frac{Tr}{3}$$

+60 End Timber
Bay Meadow

$$56 \quad \frac{Fc}{22'} \quad \frac{Tr}{4} \quad \frac{Tr}{4} \quad +10 \text{ End Timber } \frac{26'}{23'}$$

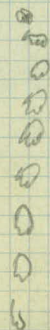
$$55 \quad \frac{Fc}{24'} \quad \frac{Tr}{6} \quad \frac{Tr}{2} \quad \text{The Line } \frac{23'}{23'}$$

Brush + Scattered
oaks

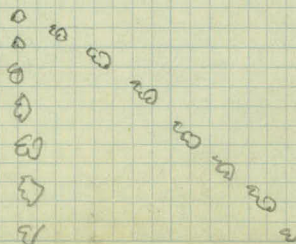


Meadow

Brush +
Timber



Hay Meadow



68

Brush FC IR IR Brush
 1'42' 42' 1' 7' 7'

+50 Beg Brush
 10'4 39'

67

FC IR IR +10 Beg Brush
 39' 3' 5' 10'

66

+05 10" Stamp
 10'

FC IR IR
 37' 2' 6'

+91 End Pop

+86 Stamp Brush
 26'

65

+44 Beg Row Pop 4
 27'

FC IR IR
 29' 7' 1'

64

+10 24" Pop
 50'

FC IR IR
 24' 8' 0'

+78 End Onks
 +50 Beg Scattered Onks
 50'

63

FC IR IR
 21' 6' 2'

62

FC IR IR
 18' 1' 7'

71

+68 End Brush + 68 FeCoT
56'

+68 End Brush

70

Fe Tr
53' 1

Tr
7

Brush
10'

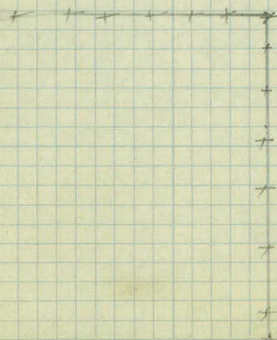
69

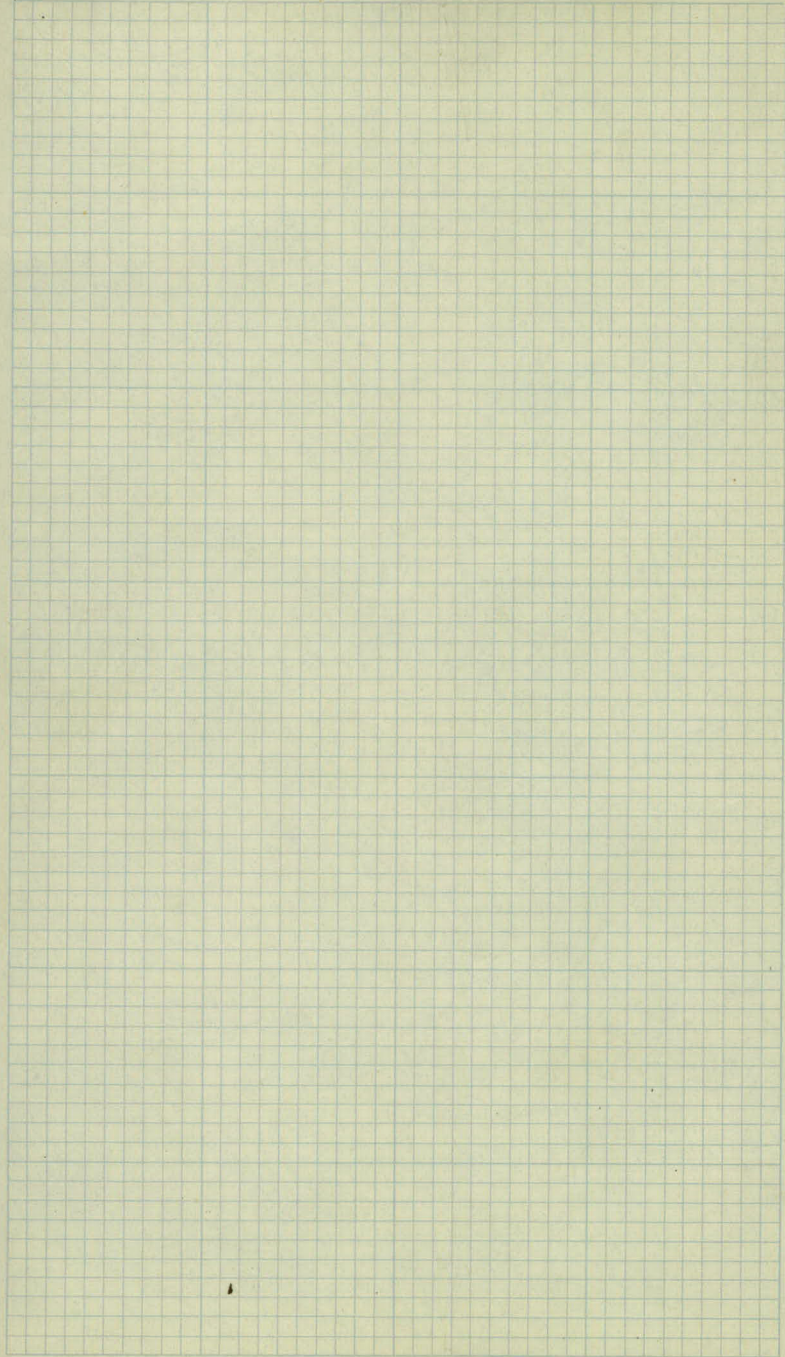
Brush Fe Tr
50' - 4' 50' 1

Tr
7

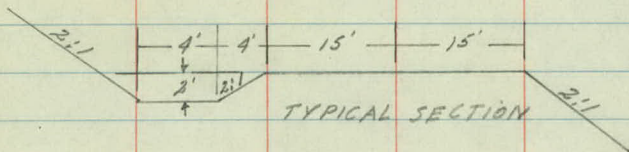
Brush
10

C. Rd "I"





Slope Stakes
Long Lake Rd.



Sta.	+	-	Grade
B.M.	4.12	918.08	713.96
0	+00		914.0
	+6.3		13.7
	+71		13.8
	+85		13.8
1			13.8
	+50		13.9
2			14.0
	+50		14.0
3			14.1
	+50		14.2
4			14.3

Gr Bod Lt R Rt

Top Halc Carr. Pav. S.T.H. #10 & Long Lake Rd.

4.1

14.4

4.3

4.3

4.3

4.2

4.1

4.1

4.0

3.9

3.6

Lt

R

Rt

F0.3

F0.3

C.0.1

C.0.0

F.0.2

F.0.3

F.0.8

F.0.7

F.0.7

F.0.5

F.0.6

C.1.3

$\frac{C.1.3}{29.6}$

$\frac{C.1.7}{30.4}$

$\frac{C.1.2}{29.4}$

$\frac{C.1.2}{29.4}$

$\frac{C.0.2}{27.4}$

$\frac{F.2.7}{20.4}$

$\frac{F.3.5}{22.0}$

$\frac{F.3.6}{22.2}$

$\frac{F.3.5}{22.0}$

$\frac{F.4.5}{24.0}$

$\frac{D.C.2.1}{29.2}$

$\frac{C.1.7}{30.4}$

$\frac{C.1.4}{29.8}$

$\frac{D.C.1.2}{25.4}$

$\frac{F.2.1}{19.2}$

$\frac{F.3.0}{21.0}$

$\frac{F.3.0}{21.0}$

$\frac{F.2.0}{19.0}$

$\frac{D.C.0.0}{23.0}$

Sta	+	X	-	Grade
		918.08		

4	+50			14.4
---	-----	--	--	------

T.P.	5.62	919.53	4.17	913.91
------	------	--------	------	--------

5				14.4
---	--	--	--	------

	+50			14.5
--	-----	--	--	------

6				14.6
---	--	--	--	------

	+50			14.7
--	-----	--	--	------

7				14.8
---	--	--	--	------

	+50			14.8
--	-----	--	--	------

8				14.9
---	--	--	--	------

	+50			14.8
--	-----	--	--	------

9				14.5
---	--	--	--	------

T.P.	6.05	918.97	4.61	912.92
------	------	--------	------	--------

	+50			14.3
--	-----	--	--	------

		4.65		8
--	--	------	--	---

Gr. Mod.

Lt.

R

Lt.

3.7	$\frac{F2.4}{20.2}$	F0.6	$\frac{F5.5}{26.0}$
-----	---------------------	------	---------------------

5.1	$\frac{F2.2}{19.4}$	F0.5	$\frac{F4.4}{23.8}$
-----	---------------------	------	---------------------

5.0	$\frac{F2.0}{19.0}$	F0.4	$\frac{D.C. 1.2}{25.4}$
-----	---------------------	------	-------------------------

4.9	$\frac{C.00}{27.0}$	F.03	$\frac{DC 1.2}{25.4}$
-----	---------------------	------	-----------------------

4.8	$\frac{C.O.6}{28.2}$	F.O.1	$\frac{D.C. 1.8}{26.6}$
-----	----------------------	-------	-------------------------

4.7	$\frac{D.C. 1.5}{26.0}$	F0.2	$\frac{DC. 1.2}{25.4}$
-----	-------------------------	------	------------------------

4.7	$\frac{D.C. 1.7}{26.4}$	C0.2	$\frac{D.C. 1.6}{26.2}$
-----	-------------------------	------	-------------------------

4.6	$\frac{C 1.5}{30.0}$	C0.8	$\frac{C 1.4}{29.8}$
-----	----------------------	------	----------------------

4.7	$\frac{C.2.7}{32.4}$	C 1.4	$\frac{C 2.4}{31.8}$
-----	----------------------	-------	----------------------

5.0	$\frac{C 2.4}{31.8}$	C 1.6	$\frac{C 2.5}{32.0}$
-----	----------------------	-------	----------------------

4.7	$\frac{C 2.1}{31.2}$	C.11	$\frac{C 1.7}{30.4}$
-----	----------------------	------	----------------------

Sta.	+	Σ	-	Grade
		918.97		
10				13.9
	+50			13.3
11				12.7
B.M.				912.92
	+31			12.4
	+50			12.1
12				11.6
	+50			11.1
13				10.7
	+50			10.4
T. P.	4.22	913.44	9.75	909.22
14				10.2
	+50			09.9

Gr. Rod.

Lt.

R.

Rt.

5.9

$$\frac{C 1.7}{30.4}$$

C. 1.6

$$\frac{C 1.1}{25.2}$$

5.7

$$\frac{DC 0.9}{24.8}$$

C 0.5

$$\frac{DC 1.4}{25.8}$$

6.3

$$\frac{DC 0.1}{23.2}$$

C. 0.2

$$\frac{DC 1.1}{25.2}$$

Spk. in stamp 100' Rt. Sta. 11+00

6.6

$$\frac{F 2.1}{19.2}$$

C. 0.0

$$\frac{DC 0.3}{23.6}$$

6.9

$$\frac{DC 1.1}{25.2}$$

F. 0.2

$$\frac{DC 1.8}{26.6}$$

7.4

$$\frac{DC 1.0}{25.0}$$

F. 0.5

$$\frac{C 0.3}{27.6}$$

7.9

$$\frac{C 1.3}{29.6}$$

F. 0.8

$$\frac{C 1.9}{30.8}$$

8.3

$$\frac{C 1.3}{29.6}$$

F. 1.1

$$\frac{C 1.2}{29.4}$$

8.6

$$\frac{DC 1.4}{25.8}$$

F. 1.2

$$\frac{DC 0.8}{24.6}$$

8.2

$$\frac{F 2.9}{20.8}$$

F. 1.6

$$\frac{F 2.9}{20.8}$$

3.5

$$\frac{F 2.6}{20.2}$$

F. 1.4

$$\frac{DC 0.3}{23.6}$$

Sta.	+	π	-	Grade
		913.44		

15				09.7
----	--	--	--	------

	+50			09.5
--	-----	--	--	------

16				09.3
----	--	--	--	------

	+50			09.2
--	-----	--	--	------

17				09.1
----	--	--	--	------

	+50			09.1
--	-----	--	--	------

18				09.1
----	--	--	--	------

T.P.	860	916.68	5.36	908.08
------	-----	--------	------	--------

	+50			09.2
--	-----	--	--	------

19				09.2
----	--	--	--	------

	+50			09.3
--	-----	--	--	------

20				09.3
----	--	--	--	------

Gr. Rod

Lt.

4.

pt.

3.7

$$\begin{array}{r} DC \ 1.6 \\ \hline 26.0 \end{array}$$

F 1.4

$$\begin{array}{r} DC \ 0.0 \\ \hline 23.0 \end{array}$$

3.9

$$\begin{array}{r} DC \ 0.9 \\ \hline 24.8 \end{array}$$

F 1.2

$$\begin{array}{r} C \ 0.3 \\ \hline 27.6 \end{array}$$

4.1

$$\begin{array}{r} DC \ 1.7 \\ \hline 26.4 \end{array}$$

F 1.3

$$\begin{array}{r} C \ 1.1 \\ \hline 29.2 \end{array}$$

4.2

$$\begin{array}{r} DC \ 1.8 \\ \hline 26.6 \end{array}$$

F 1.5

$$\begin{array}{r} C \ 0.9 \\ \hline 28.8 \end{array}$$

4.3

$$\begin{array}{r} DC \ 1.2 \\ \hline 25.4 \end{array}$$

F 1.2

$$\begin{array}{r} C \ 0.0 \\ \hline 27.0 \end{array}$$

4.5

$$\begin{array}{r} D.C. \ 0.4 \\ \hline 23.8 \end{array}$$

F 1.0

$$\begin{array}{r} DC \ 1.9 \\ \hline 26.8 \end{array}$$

4.3

$$\begin{array}{r} F \ 2.1 \\ \hline 19.2 \end{array}$$

F 1.0

$$\begin{array}{r} DC \ 1.2 \\ \hline 25.4 \end{array}$$

7.5

$$\begin{array}{r} F \ 2.2 \\ \hline 19.4 \end{array}$$

F 0.8

$$\begin{array}{r} DC \ 0.9 \\ \hline 24.8 \end{array}$$

7.5

$$\begin{array}{r} DC \ 0.3 \\ \hline 23.6 \end{array}$$

F 0.7

$$\begin{array}{r} DC \ 0.9 \\ \hline 24.8 \end{array}$$

7.4

$$\begin{array}{r} DC \ 0.5 \\ \hline 24.0 \end{array}$$

F 1.2

$$\begin{array}{r} DC \ 0.8 \\ \hline 24.6 \end{array}$$

7.4

$$\begin{array}{r} DC \ 1.4 \\ \hline 25.8 \end{array}$$

F 0.6

$$\begin{array}{r} DC \ 1.6 \\ \hline 26.2 \end{array}$$

Sta.	+	Σ	-	Grade
		916.68		
20	+50			09.4
21				09.4
	+50			09.5
22				09.5
	+50			09.6
23				09.7
	+50			09.7
T.P	4.34	912.76	8.26	908.42
24				09.8
	+50			09.8
25				09.9
	+65			10.0

Gr Rod	Lt	g	rt
7.3	$\frac{C 1.2}{29.4}$	F0.6	$\frac{C 1.5}{30}$
7.3	$\frac{C 3.1}{33}$	F0.0	$\frac{C 2.9}{32.8}$
7.2	$\frac{C 3.7}{33}$	F0.4	$\frac{C 4.2}{33.0}$
7.2	$\frac{C 3.9}{33.0}$	C0.4	$\frac{C 4.2}{33.0}$
7.1	$\frac{C 3.3}{33.0}$	F0.0	$\frac{C 3.3}{33.0}$
7.0	$\frac{C 0.2}{27.4}$	F0.4	$\frac{C 0.8}{28.6}$
7.0	$\frac{DC 0.2}{23.4}$	F0.5	$\frac{DC 0.4}{23.8}$
3.0	$\frac{F 8.0}{21.0}$	F1.6	$\frac{F 2.6}{20.2}$
3.0	$\frac{F 3.2}{22.4}$	F1.9	$\frac{F 3.7}{22.4}$
2.9	$\frac{F 4.5}{24.0}$	F1.8	$\frac{F 4.3}{23.6}$
2.8	$\frac{F 5.1}{25.2}$	F2.0	$\frac{F 5.2}{25.4}$

Sta.	+	π	-	Grade
		912.76		
26				10.0
	+50			10.0
27				10.1
	+50			10.1
28				10.2
	+50			10.3
29				10.3
T.P.	6.16	916.98	1.94	910.82
	+50			10.4
30				10.4
	+50			10.5
31				10.5

Gr Rod

Lt.

L

Rt.

2.8

$$\frac{F5.1}{25.2}$$

F1.8

$$\frac{F4.8}{24.6}$$

2.8

$$\frac{F4.6}{24.2}$$

F2.4

$$\frac{F4.2}{24.2}$$

2.7

$$\frac{F4.4}{23.8}$$

F2.2

$$\frac{F4.1}{23.2}$$

2.7

$$\frac{F3.8}{22.2}$$

F1.9

$$\frac{F3.5}{22.0}$$

2.6

$$\frac{F3.2}{21.4}$$

F1.8

$$\frac{F2.6}{20.2}$$

2.5

$$\frac{DC 0.2}{23.4}$$

F1.3

$$\frac{DC 1.0}{25}$$

2.5

$$\frac{DC 0.0}{27}$$

F0.7

$$\frac{DC 1.8}{26.6}$$

6.6

$$\frac{C 1.0}{29.0}$$

F0.2

$$\frac{C 0.3}{27.6}$$

6.6

$$\frac{C 0.9}{28.8}$$

C 0.4

$$\frac{C 1.2}{29.4}$$

6.5

$$\frac{C 1.6}{30.2}$$

C 0.6

$$\frac{C 1.9}{30.8}$$

6.5

$$\frac{C 2.2}{31.4}$$

C 0.9

$$\frac{C 1.5}{30}$$

Sta.	+	π	-	Grade
		916.98		
31	+50			10.6
32				10.6
	+50			10.7
33				10.7
	+50			10.8
34				10.8
	+50			10.8
T. P.	5.41	916.39	6.00	910.98
35				10.8
	+50			10.7
36				10.6
B.M.	4.29	915.20	5.37	911.02
	+50			10.5
				(910.91)

Gr. Rod

Lt

R

Rt

$$6.4 \quad \begin{array}{r} C 2.0 \\ 31.0 \end{array}$$

$$C 1.2$$

$$\begin{array}{r} C 1.2 \\ 29.4 \end{array}$$

$$6.4 \quad \begin{array}{r} C 1.7 \\ 30.4 \end{array}$$

$$C 1.4$$

$$\begin{array}{r} C 0.8 \\ 28.6 \end{array}$$

$$6.3 \quad \begin{array}{r} 5.1 \\ 29.4 \end{array} \quad \begin{array}{r} C 1.2 \\ \hline \end{array}$$

$$C 0.9$$

$$\begin{array}{r} C 0.03 \\ 27.6 \end{array}$$

$$6.3 \quad \begin{array}{r} 5.8 \\ 28.0 \end{array} \quad \begin{array}{r} C 0.5 \\ \hline \end{array}$$

$$6.4 \\ F 0.1$$

$$\begin{array}{r} 5.3 \\ 29.0 \end{array} \quad \begin{array}{r} C 1.0 \\ \hline \end{array}$$

$$6.2 \quad \begin{array}{r} 6.3 \\ 26.8 \end{array} \quad \begin{array}{r} D C 1.9 \\ \hline \end{array}$$

$$5.9 \\ C 0.3$$

$$\begin{array}{r} 5.2 \\ 29.0 \end{array} \quad \begin{array}{r} C 1.0 \\ \hline \end{array}$$

$$6.2 \quad \begin{array}{r} 6.4 \\ 26.6 \end{array} \quad \begin{array}{r} D C 1.8 \\ \hline \end{array}$$

$$5.7 \\ C 0.5$$

$$\begin{array}{r} 5.3 \\ 28.8 \end{array} \quad \begin{array}{r} C 0.9 \\ \hline \end{array}$$

$$6.2 \quad \begin{array}{r} 6.0 \\ 27.4 \end{array} \quad \begin{array}{r} C 0.2 \\ \hline \end{array}$$

$$5.7 \\ C 0.5$$

$$\begin{array}{r} 5.3 \\ 28.8 \end{array} \quad \begin{array}{r} C 0.9 \\ \hline \end{array}$$

$$5.6 \quad \begin{array}{r} 5.0 \\ 28.2 \end{array} \quad \begin{array}{r} C 0.6 \\ \hline \end{array}$$

$$5.4 \\ C 0.2$$

$$\begin{array}{r} 5.3 \\ 27.6 \end{array} \quad \begin{array}{r} C 0.3 \\ 27.6 \end{array}$$

$$5.7 \quad \begin{array}{r} 5.2 \\ 28.0 \end{array} \quad \begin{array}{r} C 0.5 \\ \hline \end{array}$$

$$5.8 \\ F 0.1$$

$$\begin{array}{r} 4.7 \\ 29.0 \end{array} \quad \begin{array}{r} C 1.0 \\ \hline \end{array}$$

$$5.8 \quad \begin{array}{r} 5.1 \\ 28.4 \end{array} \quad \begin{array}{r} C 0.7 \\ \hline \end{array}$$

$$5.2 \\ C 0.6$$

$$\begin{array}{r} 4.6 \\ 29.4 \end{array} \quad \begin{array}{r} C 1.2 \\ \hline \end{array}$$

Sok. in 14" Oak 100' Rt. Sta. 36+00

$$4.7 \quad \begin{array}{r} 3.5 \\ C 1.2 \\ 29.4 \end{array}$$

$$4.3 \\ C 0.4$$

$$\begin{array}{r} 4.2 \\ C 0.3 \\ 28.0 \end{array}$$

sta.	+	Σ	-	Grade
		915.20		
37				10.3
	1.50			10.1
38				10.0
	1.50			09.8
39				09.6
	1.50			09.4
40				09.3
	1.50			09.1
41				08.9
T.P.	4.23	911.81	7.62	907.58
	1.50			08.8
42				08.6

Gr. Rod.

L.

R.

Rt.

$$4.9 \quad \begin{array}{r} 4.4 \\ C0.2 \\ \hline 28.0 \end{array}$$

$$4.9 \\ C0.0$$

$$\begin{array}{r} 4.9 \\ C0.0 \\ \hline 22.0 \end{array}$$

$$5.1 \quad \begin{array}{r} 4.4 \\ C0.2 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ F0.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ R1.7 \\ \hline 26.4 \end{array}$$

$$5.2 \quad \begin{array}{r} 4.4 \\ C0.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ F0.2 \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.1 \\ \hline 27.2 \end{array}$$

$$5.4 \quad \begin{array}{r} 4.3 \\ C1.1 \\ \hline 29.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ F0.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ C0.4 \\ \hline 29.8 \end{array}$$

$$5.6 \quad \begin{array}{r} 4.9 \\ C0.7 \\ \hline 28.4 \end{array}$$

$$\begin{array}{r} 6.5 \\ F0.9 \end{array}$$

$$\begin{array}{r} 5.8 \\ R1.8 \\ \hline 26.6 \end{array}$$

$$5.8 \quad \begin{array}{r} 6.2 \\ R1.6 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 7.3 \\ F1.5 \end{array}$$

$$\begin{array}{r} 7.8 \\ R0.0 \\ \hline 23.0 \end{array}$$

$$5.9 \quad \begin{array}{r} 8.0 \\ F2.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 7.8 \\ F1.9 \end{array}$$

$$\begin{array}{r} 8.9 \\ F3.0 \\ \hline 21.0 \end{array}$$

$$6.1 \quad \begin{array}{r} 10.2 \\ F4.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 8.2 \\ F2.1 \end{array}$$

$$\begin{array}{r} 9.1 \\ F3.0 \\ \hline 21.0 \end{array}$$

$$6.3 \quad \begin{array}{r} 11.0 \\ F4.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 8.7 \\ F2.4 \end{array}$$

$$\begin{array}{r} 9.2 \\ F2.9 \\ \hline 20.8 \end{array}$$

$$3.0 \quad \begin{array}{r} 8.2 \\ F5.2 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ F2.5 \end{array}$$

$$\begin{array}{r} 6.6 \\ F3.6 \\ \hline 22.2 \end{array}$$

$$3.2 \quad \begin{array}{r} 8.3 \\ F5.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 6.0 \\ F2.8 \end{array}$$

$$\begin{array}{r} 7.3 \\ F4.1 \\ \hline 23.2 \end{array}$$

sta.	+	π	-	Grade
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911.81

42	+50			08.4
----	-----	--	--	------

43				08.3
----	--	--	--	------

	+50			08.1
--	-----	--	--	------

44				07.9
----	--	--	--	------

	+50			07.7
--	-----	--	--	------

45				07.6
----	--	--	--	------

	+20			07.5
--	-----	--	--	------

	+60			07.4
--	-----	--	--	------

46				07.2
----	--	--	--	------

	+50			07.1
--	-----	--	--	------

47				06.9
----	--	--	--	------

Gr Red

Lt

L

Rt

3.4

$$\begin{array}{r} 8.0 \\ F4.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ F2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 8.2 \\ F4.8 \\ \hline 24.6 \end{array}$$

3.5

$$\begin{array}{r} 8.1 \\ F4.7 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 6.5 \\ F3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 8.0 \\ F4.5 \\ \hline 24.0 \end{array}$$

3.7

$$\begin{array}{r} 8.0 \\ F4.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 6.7 \\ F3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 8.9 \\ F5.2 \\ \hline 26.4 \end{array}$$

3.9

$$\begin{array}{r} 7.5 \\ F3.6 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 6.4 \\ F2.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.8 \\ F3.9 \\ \hline 22.8 \end{array}$$

4.1

$$\begin{array}{r} 6.7 \\ F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 6.0 \\ F1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ F2.7 \\ \hline 20.4 \end{array}$$

4.2

$$\begin{array}{r} 5.8 \\ DC0.6 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 5.7 \\ F1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ DC0.6 \\ \hline 24.2 \end{array}$$

4.3

$$\begin{array}{r} 4.9 \\ DC1.4 \\ \hline 25.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ DC1.7 \\ \hline 26.4 \end{array}$$

4.4

$$\begin{array}{r} 2.2 \\ C2.2 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ F1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 1.9 \\ C2.5 \\ \hline 32.0 \end{array}$$

4.6

$$\begin{array}{r} 4.4 \\ C0.2 \\ \hline 27.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 1.3 \\ C3.3 \\ \hline 33.0 \end{array}$$

4.7

$$\begin{array}{r} 4.4 \\ C0.3 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 5.3 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.0 \\ C1.7 \\ \hline 30.4 \end{array}$$

4.9

$$\begin{array}{r} 5.9 \\ DC1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 5.6 \\ F0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ DC1.8 \\ \hline 26.6 \end{array}$$

Sta.	+	Σ	-	Grade
		911.81		
47	+50			06.9
48				06.9
T.P	9.67	915.22	6.26	905.55
	+50			07.0
49				07.2
	+50			07.5
50				07.8
	+50			08.1
51				08.3
	+50			08.5
52				08.7
	+50			08.7
B.M.			5.75	909.47
				909.46

Gr. Rod

Lt

R

Rt

A.9

$$\begin{array}{r} 7.2 \\ W0.7 \\ \hline 79.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ F0.5 \end{array}$$

$$\begin{array}{r} 6.6 \\ W0.3 \\ \hline 23.6 \end{array}$$

4.9

$$\begin{array}{r} 6.2 \\ W0.7 \\ \hline 74.4 \end{array}$$

$$\begin{array}{r} 5.7 \\ F0.8 \end{array}$$

$$\begin{array}{r} 7.5 \\ F2.4 \\ \hline 20.2 \end{array}$$

Fc Root 20' Rt Sta 48+00

8.2

$$\begin{array}{r} 9.2 \\ W1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ F0.3 \end{array}$$

$$\begin{array}{r} 10.2 \\ F2.0 \\ \hline 19.0 \end{array}$$

8.0

$$\begin{array}{r} 9.8 \\ W0.4 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 8.3 \\ F0.3 \end{array}$$

$$\begin{array}{r} 10.0 \\ W0.0 \\ \hline 21.0 \end{array}$$

7.7

$$\begin{array}{r} 8.7 \\ W1.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 7.9 \\ F0.2 \end{array}$$

$$\begin{array}{r} 9.4 \\ W0.3 \\ \hline 23.6 \end{array}$$

7.4

$$\begin{array}{r} 7.0 \\ W0.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 7.4 \\ C0.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ W1.4 \\ \hline 25.8 \end{array}$$

7.1

$$\begin{array}{r} 5.3 \\ C1.8 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 6.7 \\ C0.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ C1.2 \\ \hline 30.0 \end{array}$$

6.9

$$\begin{array}{r} 4.4 \\ C2.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ C1.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ C2.3 \\ \hline 31.6 \end{array}$$

6.7

$$\begin{array}{r} 3.9 \\ C2.8 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ C1.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ C2.3 \\ \hline 31.6 \end{array}$$

6.5

$$\begin{array}{r} 4.0 \\ C2.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ C1.5 \end{array}$$

$$\begin{array}{r} 5.4 \\ C1.1 \\ \hline 29.2 \end{array}$$

6.5

$$\begin{array}{r} 4.0 \\ C2.5 \\ \hline 32.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ C1.9 \end{array}$$

$$\begin{array}{r} 5.3 \\ C1.2 \\ \hline 29.4 \end{array}$$

spl. in 12" stump 50' Rt 52+50

Sta.	+	π	-	Grade
		915.22		

53				08.7
----	--	--	--	------

+50				08.7
-----	--	--	--	------

54				08.6
T.P.	2.79	912.29	5.72	909.50

+50				08.5
-----	--	--	--	------

55				08.4
----	--	--	--	------

+50				08.3
-----	--	--	--	------

56				08.2
----	--	--	--	------

+50				08.1
-----	--	--	--	------

57				08.0
----	--	--	--	------

+50				07.9
-----	--	--	--	------

58				07.8
----	--	--	--	------

Gr. Rod

Lt

R

Rt

L.5

$$\begin{array}{r} 4.9 \\ C1.6 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ C1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ C0.3 \\ \hline 27.6 \end{array}$$

L.5

$$\begin{array}{r} 4.9 \\ C1.6 \\ \hline 30.2 \end{array}$$

$$\begin{array}{r} 5.4 \\ C1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ C0.4 \\ \hline 27.8 \end{array}$$

L.6

$$\begin{array}{r} 4.2 \\ C2.4 \\ \hline 31.8 \end{array}$$

$$\begin{array}{r} 5.7 \\ C0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ C0.8 \\ \hline 28.6 \end{array}$$

3.8

$$\begin{array}{r} 1.7 \\ C2.1 \\ \hline 31.2 \end{array}$$

$$\begin{array}{r} 3.0 \\ C0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ C1.4 \\ \hline 27.8 \end{array}$$

3.9

$$\begin{array}{r} 1.6 \\ C2.3 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 3.3 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 2.3 \\ C1.6 \\ \hline 30.2 \end{array}$$

4.0

$$\begin{array}{r} 2.0 \\ C2.0 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 2.9 \\ C1.1 \\ \hline 29.2 \end{array}$$

4.1

$$\begin{array}{r} 2.7 \\ C1.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 3.8 \\ C0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C0.2 \\ \hline 27.4 \end{array}$$

4.2

$$\begin{array}{r} 4.1 \\ C3.1 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ F0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ C0.3 \\ \hline 23.6 \end{array}$$

4.3

$$\begin{array}{r} 6.4 \\ F2.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ F2.5 \\ \hline 20.0 \end{array}$$

4.4

$$\begin{array}{r} 7.0 \\ F2.6 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 5.6 \\ F1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 7.5 \\ F3.1 \\ \hline 21.2 \end{array}$$

4.5

$$\begin{array}{r} 7.5 \\ F3.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ F1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.0 \\ F3.5 \\ \hline 22.0 \end{array}$$

Sta	+	π	-	Grade
		912.29		

58	+47			07.7
----	-----	--	--	------

59				07.6
----	--	--	--	------

	+50			07.5
--	-----	--	--	------

60				07.4
----	--	--	--	------

	+50			07.3
--	-----	--	--	------

61				07.2
----	--	--	--	------

T.P.	6.36	912.75	5.90	906.39
------	------	--------	------	--------

	+50			07.1
--	-----	--	--	------

62				07.0
----	--	--	--	------

	+50			06.9
--	-----	--	--	------

63				06.8
----	--	--	--	------

	+50			06.7
--	-----	--	--	------

Gr. Rod

Lt

L

Rt

$$\begin{array}{r}
 8.0 \\
 F3.4 \\
 \hline
 21.8
 \end{array}
 \quad
 \begin{array}{r}
 6.6 \\
 F2.0 \\
 \hline
 8.6 \\
 F3.8 \\
 \hline
 22.6
 \end{array}$$

$$\begin{array}{r}
 8.1 \\
 F3.4 \\
 \hline
 21.8
 \end{array}
 \quad
 \begin{array}{r}
 6.9 \\
 F2.2 \\
 \hline
 8.3 \\
 F3.6 \\
 \hline
 22.2
 \end{array}$$

$$\begin{array}{r}
 7.7 \\
 F2.9 \\
 \hline
 20.8
 \end{array}
 \quad
 \begin{array}{r}
 6.5 \\
 F1.7 \\
 \hline
 8.0 \\
 F3.2 \\
 \hline
 21.4
 \end{array}$$

$$\begin{array}{r}
 7.1 \\
 F2.2 \\
 \hline
 19.4
 \end{array}
 \quad
 \begin{array}{r}
 6.3 \\
 F1.4 \\
 \hline
 6.9 \\
 F2.0 \\
 \hline
 19.0
 \end{array}$$

$$\begin{array}{r}
 6.3 \\
 D0.7 \\
 \hline
 24.4
 \end{array}
 \quad
 \begin{array}{r}
 6.2 \\
 F1.2 \\
 \hline
 7.0 \\
 D0.2 \\
 \hline
 23.0
 \end{array}$$

$$\begin{array}{r}
 4.9 \\
 C0.2 \\
 \hline
 27.4
 \end{array}
 \quad
 \begin{array}{r}
 5.9 \\
 F0.8 \\
 \hline
 6.0 \\
 D0.1 \\
 \hline
 25.2
 \end{array}$$

$$\begin{array}{r}
 4.0 \\
 C1.7 \\
 \hline
 30.4
 \end{array}
 \quad
 \begin{array}{r}
 6.4 \\
 F0.7 \\
 \hline
 5.1 \\
 C0.6 \\
 \hline
 28.2
 \end{array}$$

$$\begin{array}{r}
 3.9 \\
 C1.9 \\
 \hline
 30.8
 \end{array}
 \quad
 \begin{array}{r}
 6.2 \\
 F0.4 \\
 \hline
 5.8 \\
 C0.2 \\
 \hline
 29.0
 \end{array}$$

$$\begin{array}{r}
 4.8 \\
 C1.1 \\
 \hline
 29.2
 \end{array}
 \quad
 \begin{array}{r}
 6.0 \\
 F0.1 \\
 \hline
 6.4 \\
 D0.3 \\
 \hline
 26.0
 \end{array}$$

$$\begin{array}{r}
 6.8 \\
 D1.2 \\
 \hline
 25.4
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
 F0.7 \\
 \hline
 6.7 \\
 D0.3 \\
 \hline
 25.6
 \end{array}$$

$$\begin{array}{r}
 7.8 \\
 D0.3 \\
 \hline
 23.6
 \end{array}
 \quad
 \begin{array}{r}
 6.6 \\
 F0.5 \\
 \hline
 5.2 \\
 C0.9 \\
 \hline
 28.8
 \end{array}$$

Sta	+	π	-	Grade	
		912.75			
63	+70			06.6	
64				06.6	
B.M.	341	912.49	3.68	909.07	909.08
	+50			06.5	
65				06.4	
	+50			06.3	
66				06.2	
	+50			06.1	
67				06.0	
	+50			05.9	
68				05.8	
T.P.	5.49	910.41	7.57	904.92	
	+50			05.7	

Gr. Rod.	Lt	E	Rt
L.2	$\begin{array}{r} 7.1 \\ R3.1 \\ \hline 25.2 \end{array}$	$\begin{array}{r} L6 \\ F0.4 \end{array}$	$\begin{array}{r} 5.0 \\ C1.2 \\ \hline 29.4 \end{array}$
L.2	$\begin{array}{r} 7.1 \\ R3.1 \\ \hline 25.2 \end{array}$	$\begin{array}{r} 6.5 \\ F0.3 \end{array}$	$\begin{array}{r} 5.7 \\ C0.5 \\ \hline 28.0 \end{array}$
Sph. in 14" stump 100' Rt sta 64			
L.0	$\begin{array}{r} 7.4 \\ R0.6 \\ \hline 24.2 \end{array}$	$\begin{array}{r} L4 \\ F0.4 \end{array}$	$\begin{array}{r} 7.3 \\ R0.7 \\ \hline 24.4 \end{array}$
L.1	$\begin{array}{r} 7.1 \\ R0.1.0 \\ \hline 25.0 \end{array}$	$\begin{array}{r} 6.7 \\ F0.6 \end{array}$	$\begin{array}{r} 8.1 \\ R0.0 \\ \hline 28.0 \end{array}$
L.2	$\begin{array}{r} 4.7 \\ C1.8 \\ \hline 30.0 \end{array}$	$\begin{array}{r} L0 \\ C0.2 \end{array}$	$\begin{array}{r} 8.0 \\ R0.2 \\ \hline 23.4 \end{array}$
L.3	$\begin{array}{r} L3 \\ C0.0 \\ \hline 27.0 \end{array}$	$\begin{array}{r} 5.7 \\ C0.6 \end{array}$	$\begin{array}{r} 8.3 \\ R0.0 \\ \hline 32.0 \end{array}$
L.4	$\begin{array}{r} 8.4 \\ R0.0 \\ \hline 25.2 \end{array}$	$\begin{array}{r} 4.9 \\ C1.5 \end{array}$	$\begin{array}{r} 8.4 \\ R0.0 \\ \hline 28.2 \end{array}$
L.5	$\begin{array}{r} 8.5 \\ R0.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 5.1 \\ C1.4 \end{array}$	$\begin{array}{r} 6.9 \\ R1.6 \\ \hline 26.2 \end{array}$
L.6	$\begin{array}{r} 8.2 \\ F2.0 \\ \hline 19.0 \end{array}$	$\begin{array}{r} L4 \\ C0.7 \end{array}$	$\begin{array}{r} 5.1 \\ C1.3 \\ \hline 30.0 \end{array}$
L.7	$\begin{array}{r} 9.4 \\ F2.7 \\ \hline 20.4 \end{array}$	$\begin{array}{r} 7.5 \\ F0.8 \end{array}$	$\begin{array}{r} 5.5 \\ C1.4 \\ \hline 24.8 \end{array}$
4.7	$\begin{array}{r} 6.9 \\ F2.2 \\ \hline 19.4 \end{array}$	$\begin{array}{r} 4.9 \\ F0.2 \end{array}$	$\begin{array}{r} 6.7 \\ R0.0 \\ \hline 19.2 \end{array}$

Sta	+	Σ	-	Grade
		910.41		
69				05.6
	+50			05.5
70				05.4
	6.41	910.30	6.52	903.89
	+65			05.2
	+80			05.2
	+89			05.2
71	+05.6			05.6
B.M.			2.30	908.00
				907.97

Gr. Rod.

Lt

2

Rt

4.8	$\begin{array}{r} 6.8 \\ 100.0 \\ \hline 20.4 \end{array}$	$\begin{array}{r} 5.3 \\ 10.5 \end{array}$	$\begin{array}{r} 6.8 \\ 100.0 \\ \hline 19.2 \end{array}$
4.9	$\begin{array}{r} 6.9 \\ 100.0 \\ \hline 20.2 \end{array}$	$\begin{array}{r} 5.3 \\ 10.4 \end{array}$	$\begin{array}{r} 7.2 \\ 10.3 \\ \hline 19.6 \end{array}$
5.0	$\begin{array}{r} 7.0 \\ 100.0 \\ \hline 19.9 \end{array}$	$\begin{array}{r} 5.8 \\ 10.8 \end{array}$	$\begin{array}{r} 7.3 \\ 10.3 \\ \hline 19.6 \end{array}$
5.1	$\begin{array}{r} 6.0 \\ 101.1 \\ \hline 25.2 \end{array}$	$\begin{array}{r} 6.6 \\ 10.5 \end{array}$	$\begin{array}{r} 7.2 \\ 10.1 \\ \hline 19.2 \end{array}$
5.1			

Spk. in 12" Oct. 33 Rt. Sta. 73+50

