

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

____ PLAN ____ Survey

____ LARPENTEUR AVE. ____

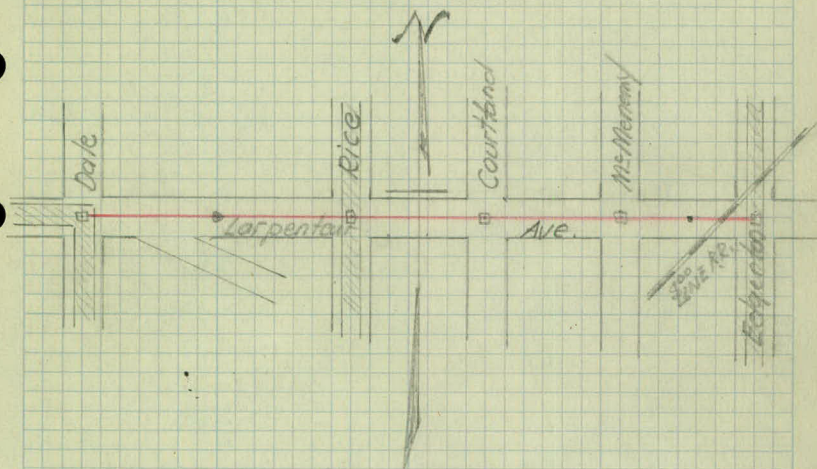
From DALE ST. To EDGERTON ST.

Road Acc't. No. 50

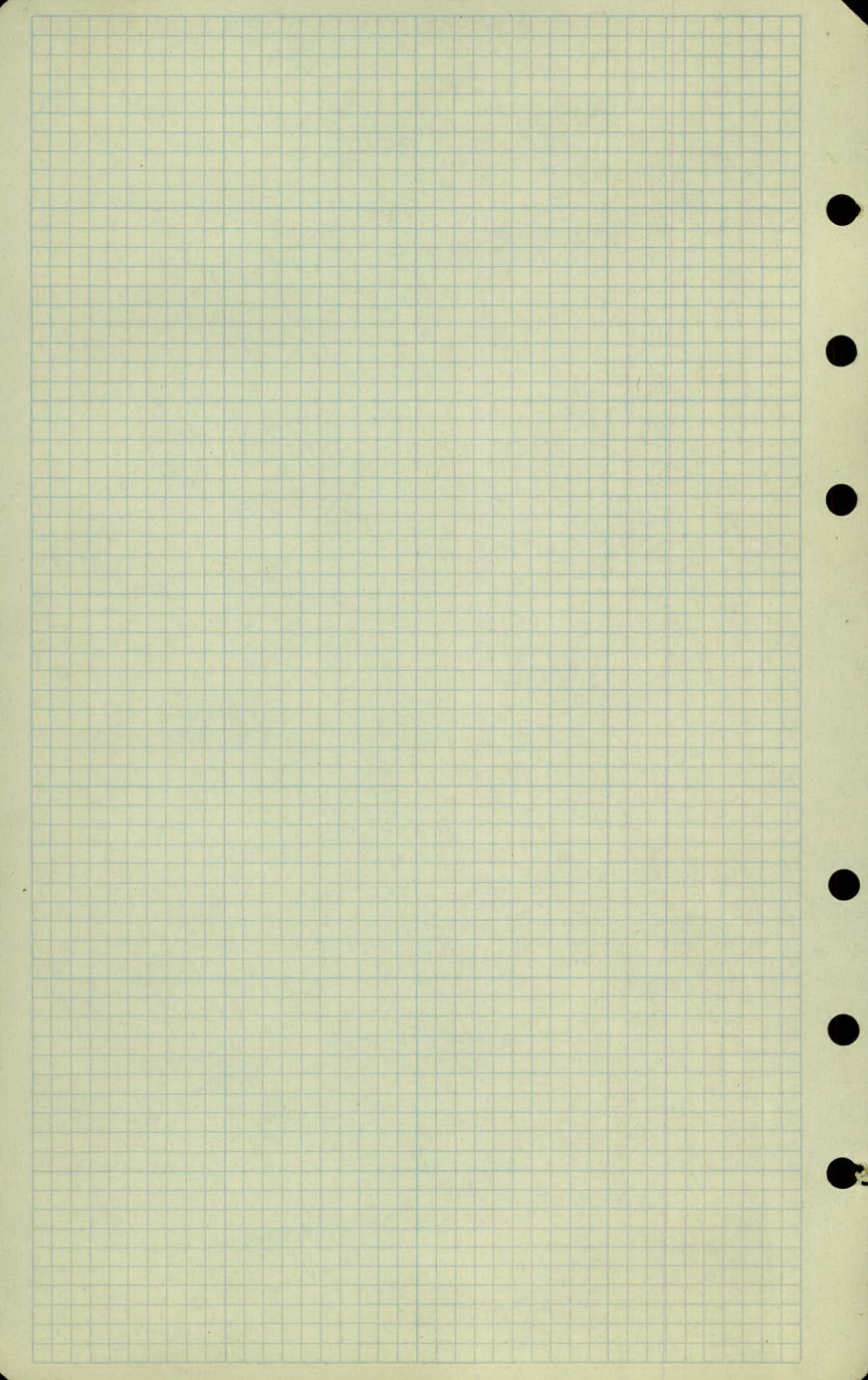
Date Filed. _____

File. _____

Plan Survey
Larpenteur Ave.
Dale St. to Edgerton.



Index



1
alignment

Larpenteur Ave.

Dale St. to Edgerton.

Station	Point	Angle Lt Rt.
249+53.2	P.O.T.	

229+00	P.O.T.	
	Approx P.I. of Rd. Rt.	

220+49.66	P.O.T.	
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210+75.75	R.I. Mop. 2 Dale	1°-08'
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2'x2" Hub



Approx

14°35'

Nail



Boat Spike.



W. H. Carlson

K. Anker.

L. B. Hendrix

A. Moschter

Nov. 17, 1936

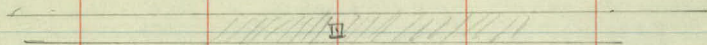
Station	Point	angle	
		Lt.	Rt.

263+10.45	P.I. Map E Rice St.		
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260+53.65	P.O.T.		
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257+26.33	P.O.T.		
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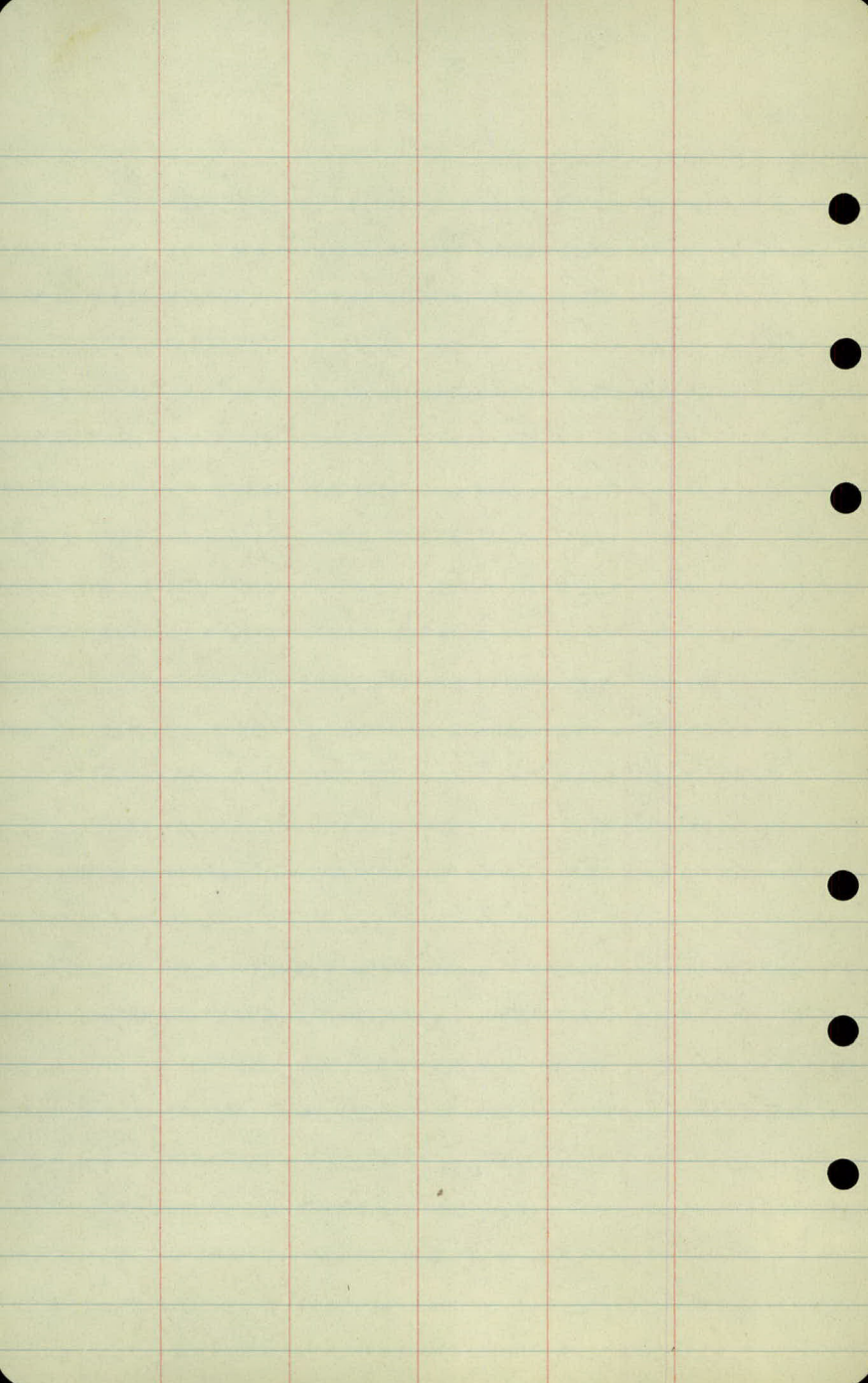
254+32.83	P.O.T.		
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□ 1"x2" Hub.

□ 1"x2" Hub.

□ 1"x2" Hub.



Topography.

Larpenteur Ave.

Dale St. to Edgerton.

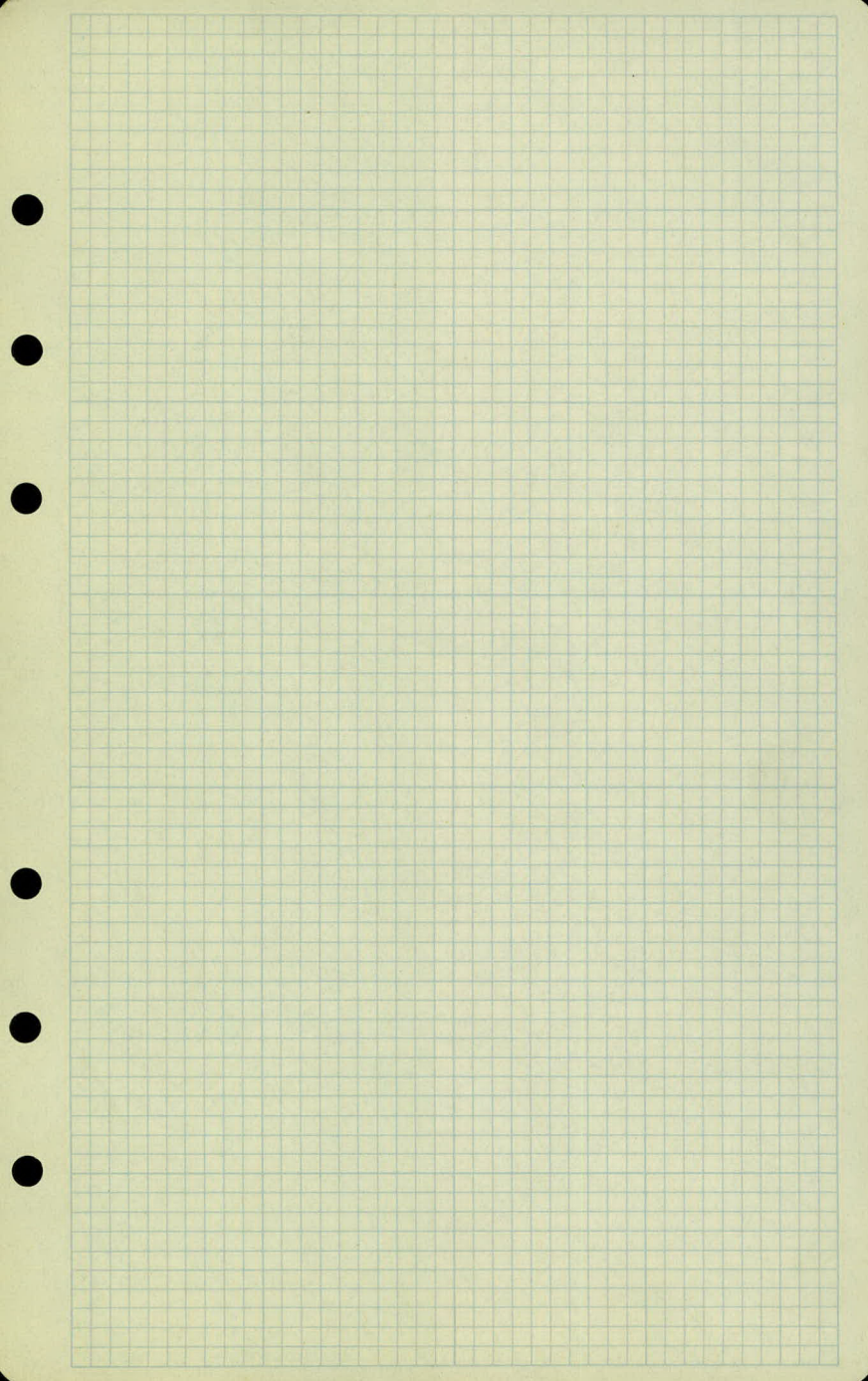
214

213

212

211

210



221

220

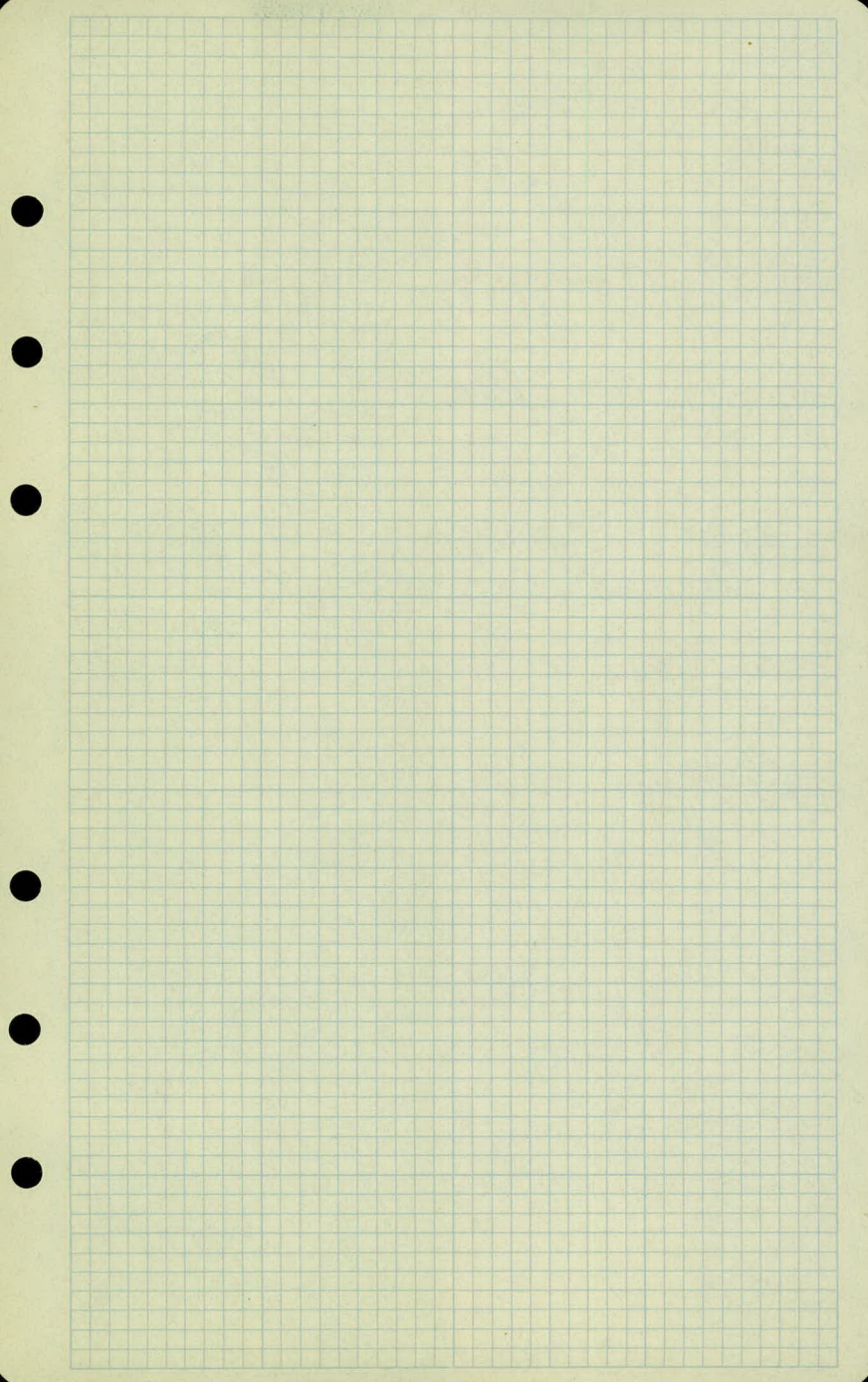
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215



228

227

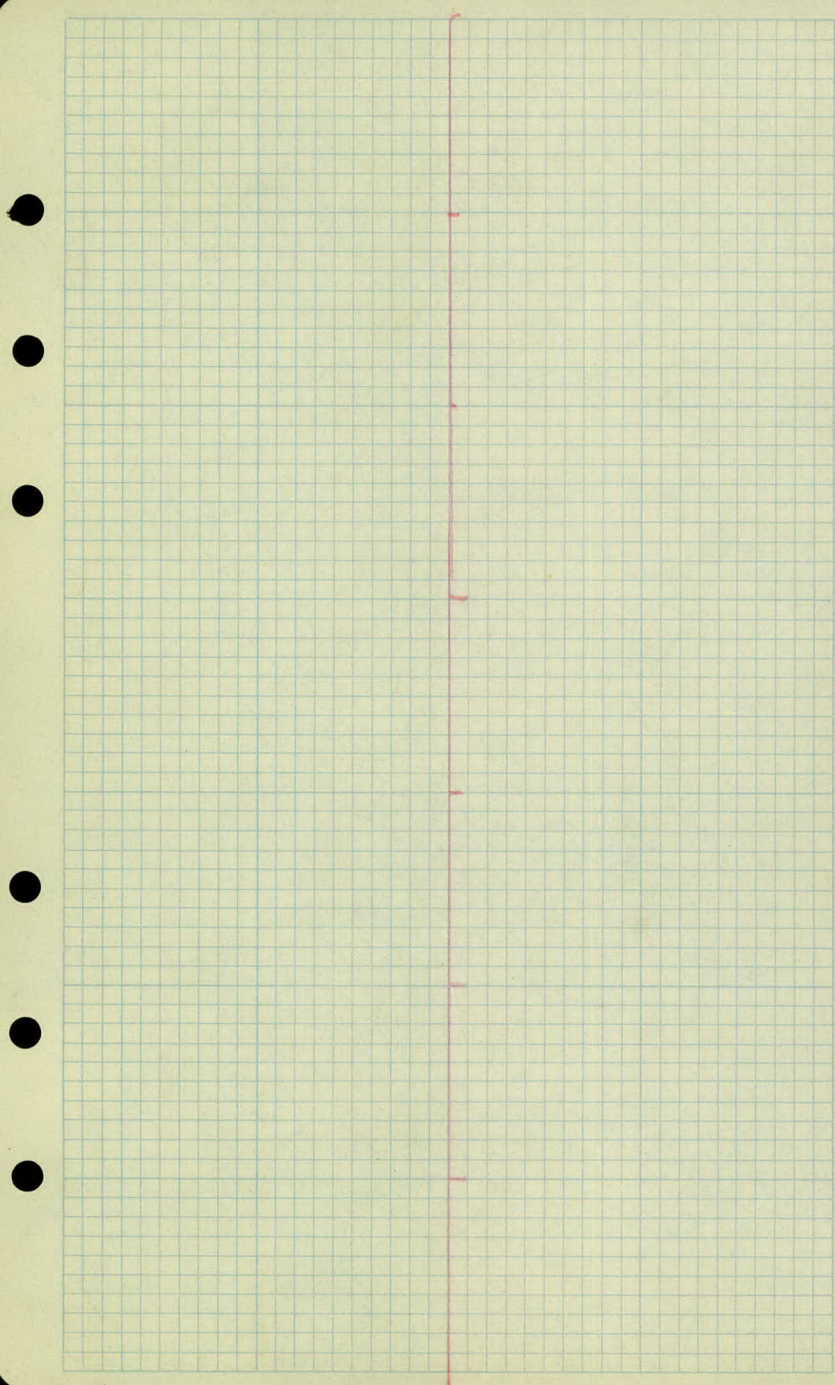
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223

222



235

234

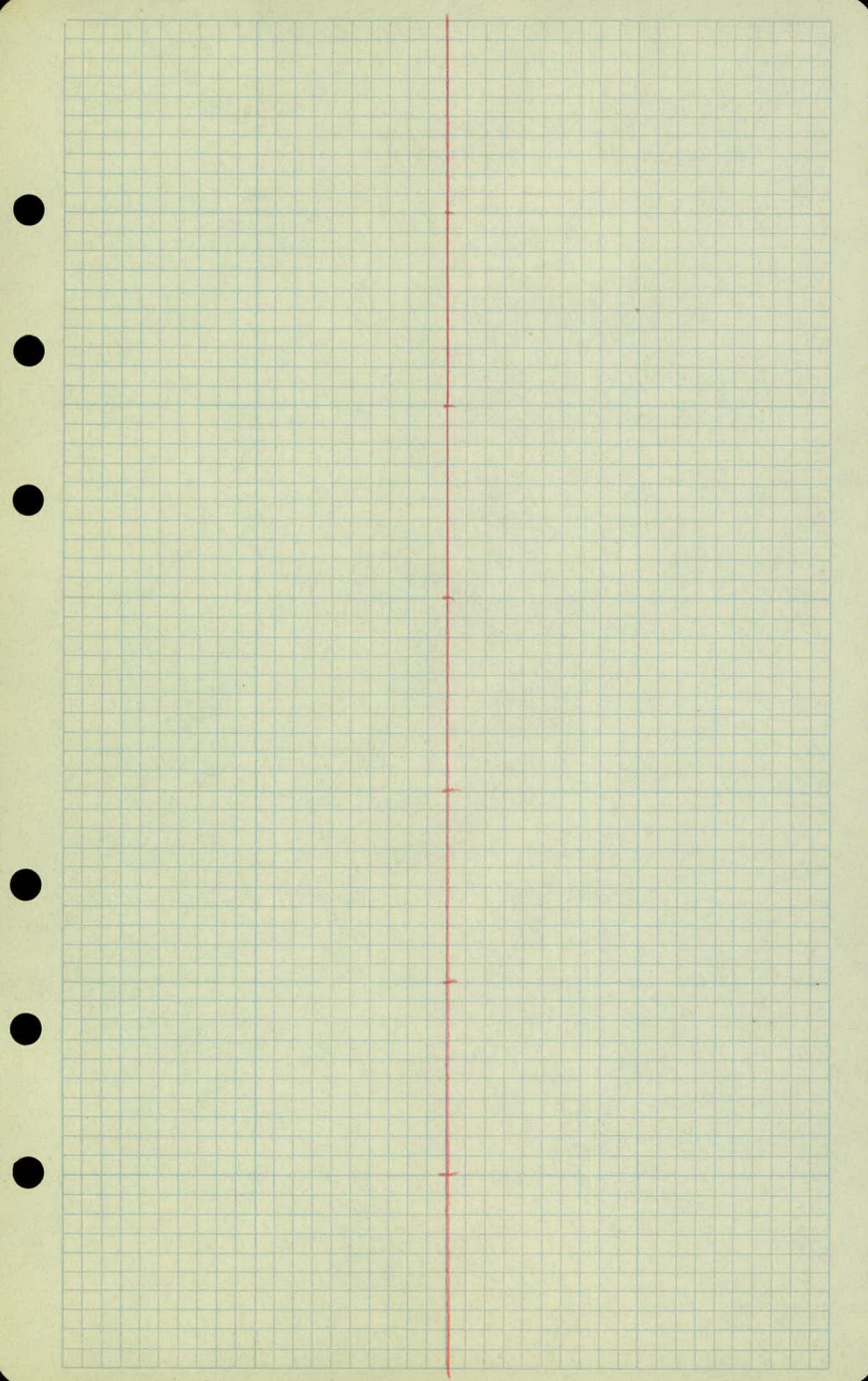
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230

229



242

241

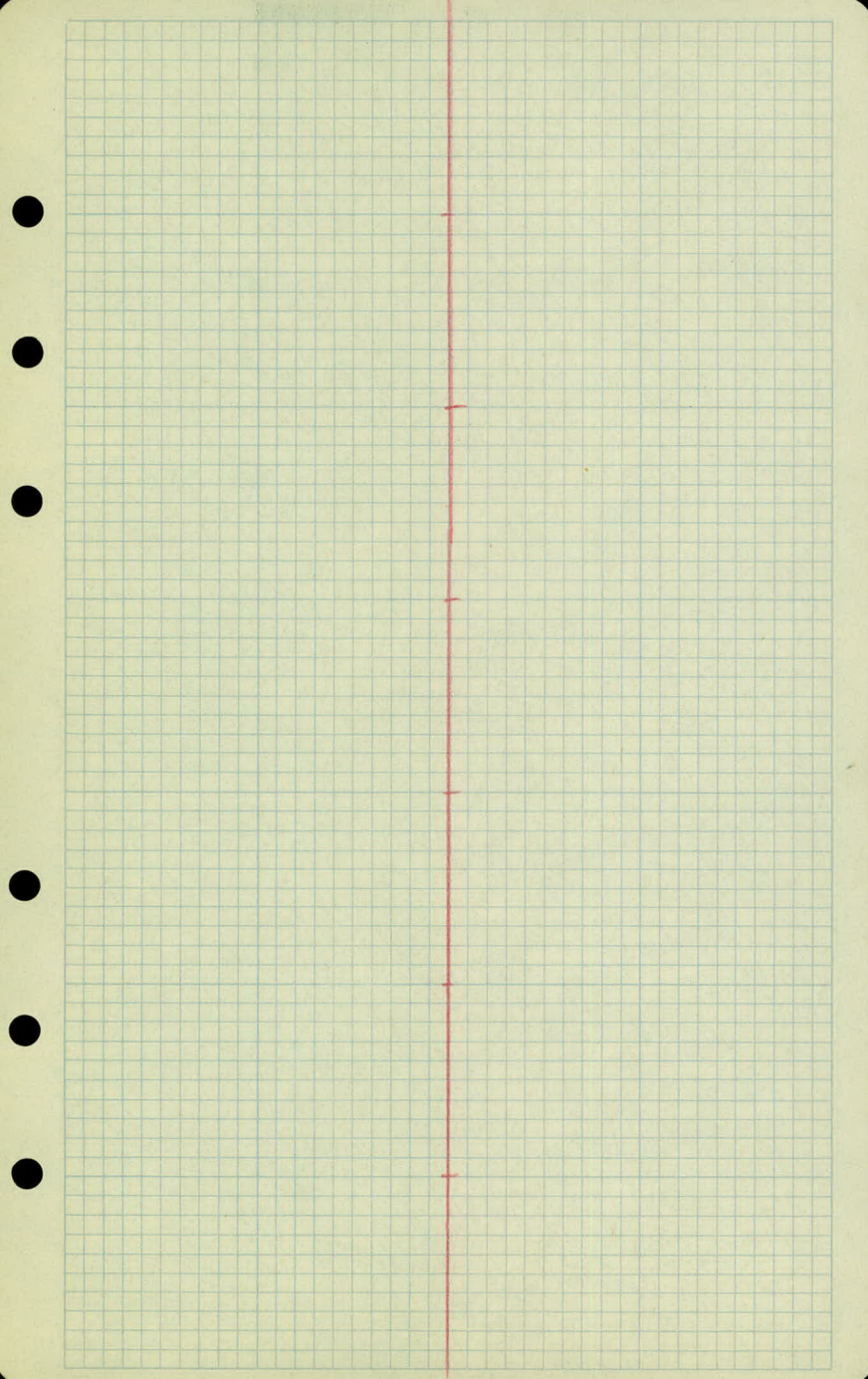
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249

248

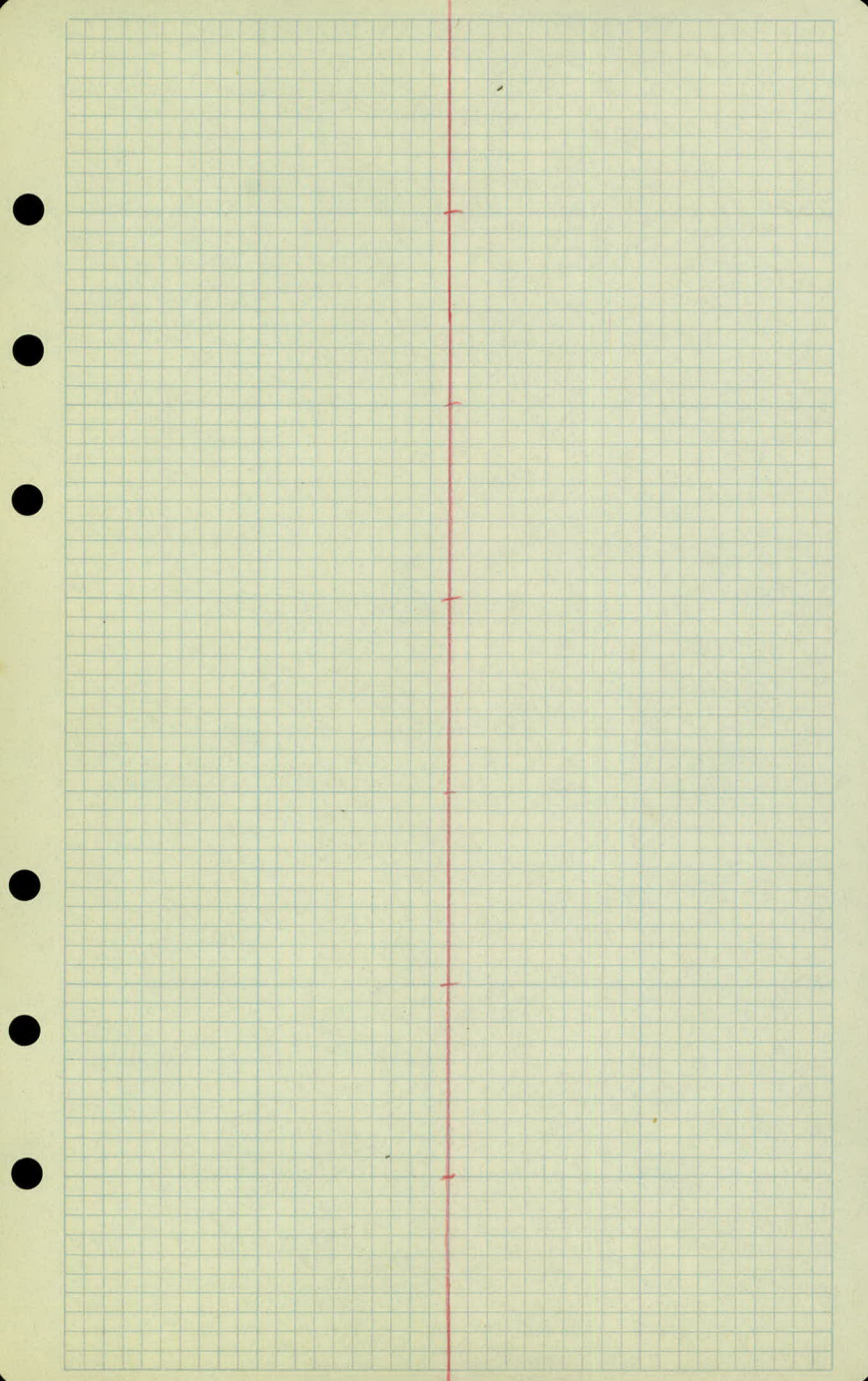
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246

245

244

243



256

255

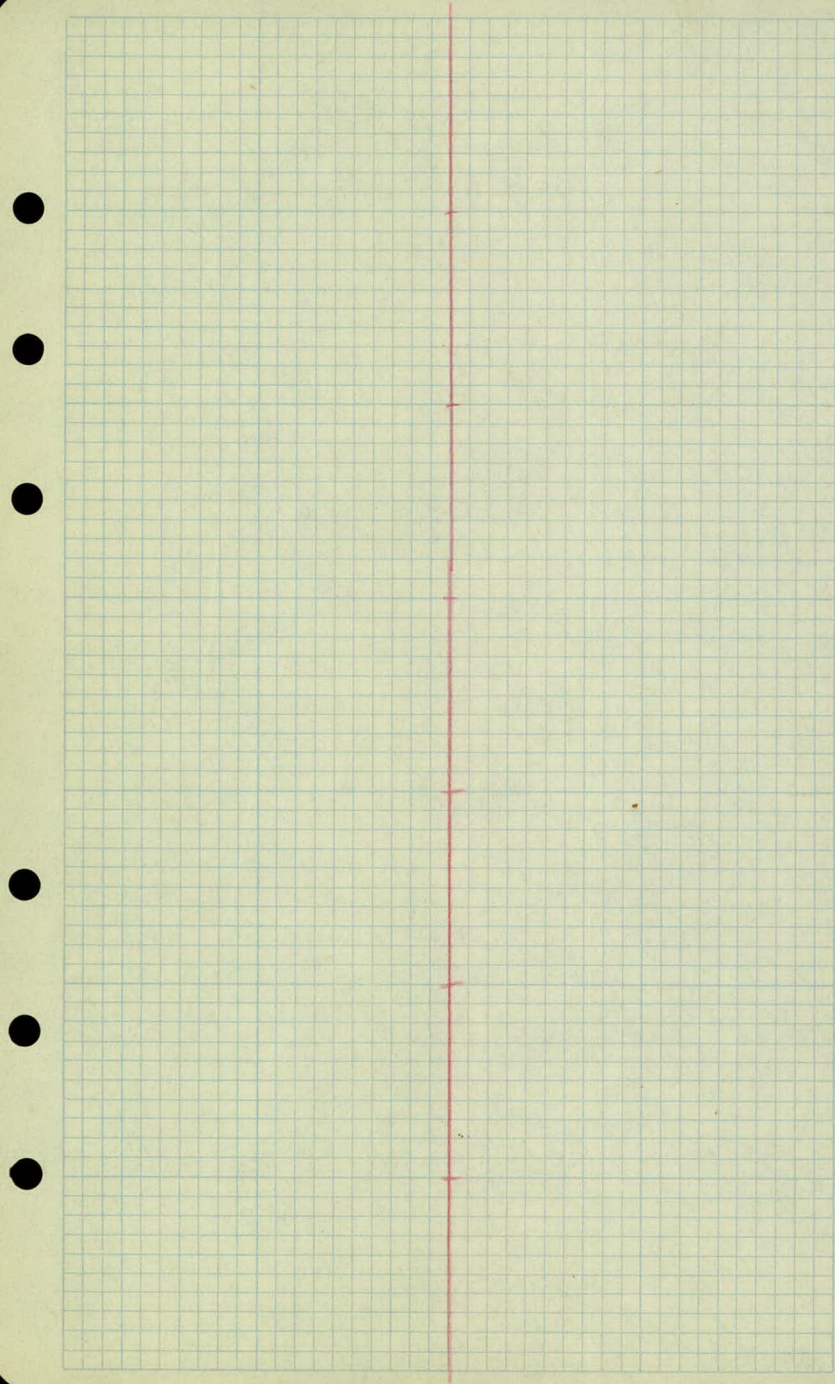
254

253

252

251

250



+10.45 = Mon E Rce St.

263

262

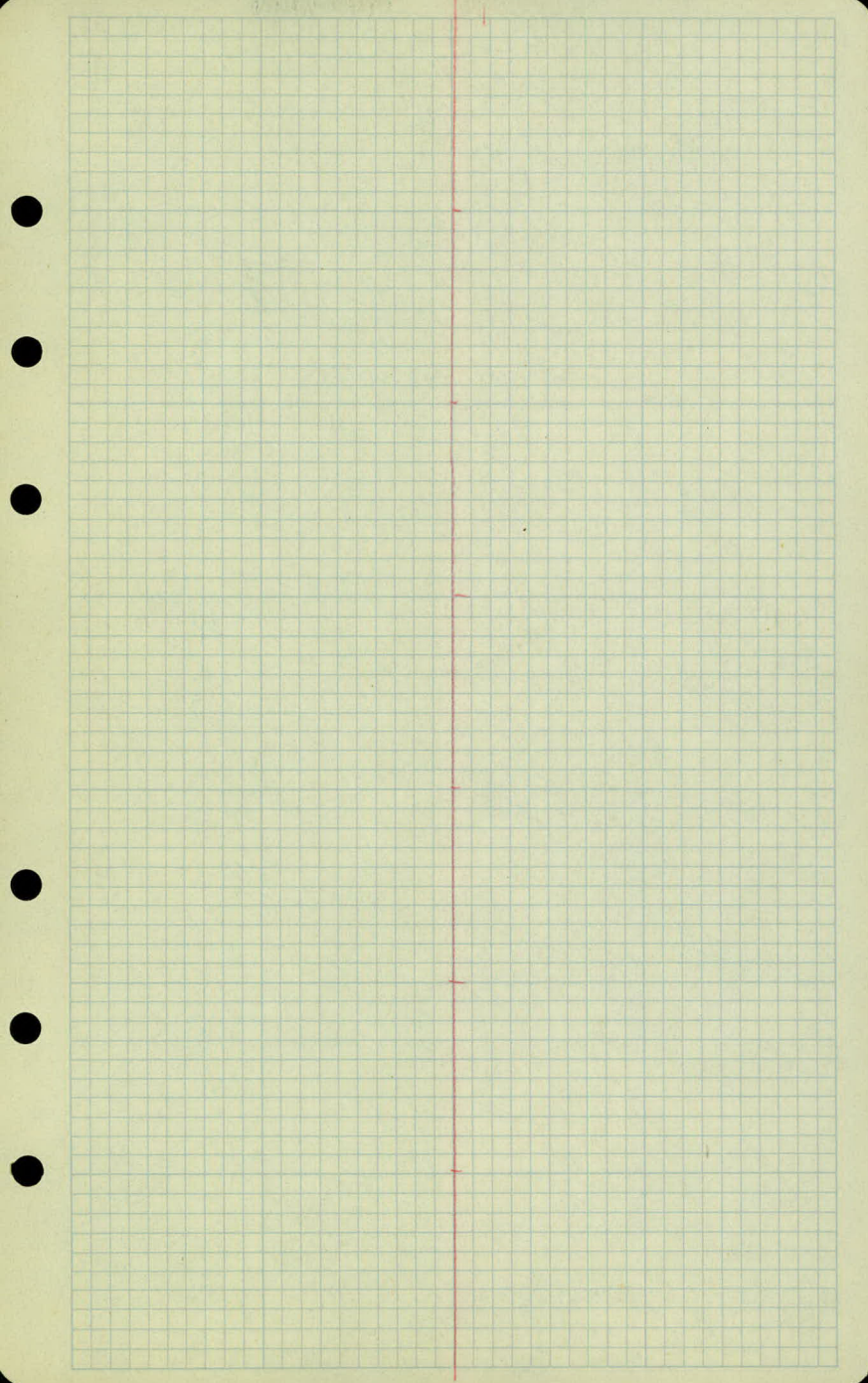
261

260

259

258

257



266

265

264

1

Cross Sections

Larpeur
Dale to Edgerton.

Sta	+	X	-	Elev.
B.M.	5.51	924.44		918.93
210+75				18.9
211				19.2
+50				19.6
212				19.6
+47				
+47				19.4
213				19.3
+50				19.5
214				19.5
+50				19.6
215				19.6
+50				19.5
216				19.6

18" Corrug Pipe

Bratager
Wilko
Gillon

11/17/30

LT

2

RT

Top Mon. Dalg & Larp. 210475.75

$\frac{70}{53} \frac{48}{47} \frac{5.2}{41} \quad 5.5 \quad \frac{5.6}{50} \quad \frac{5.6}{100}$

$\frac{66}{50} \frac{6.1}{37} \frac{6.0}{34} \frac{5.2}{26} \frac{5.3}{15} \quad 5.2 \quad \frac{5.4}{12} \frac{5.4}{18} \frac{6.0}{21} \frac{6.0}{24} \frac{5.4}{28} \frac{5.4}{50}$

$\frac{80}{50} \frac{7.5}{39} \frac{5.2}{26} \frac{5.2}{12} \quad 48 \quad \frac{5.4}{9} \frac{5.5}{16} \frac{7.0}{21} \frac{7.1}{25} \frac{6.1}{29} \frac{6.2}{50}$

$\frac{74}{50} \frac{5.0}{28} \frac{5.2}{12} \quad 48 \quad \frac{5.4}{10} \frac{5.4}{14} \frac{7.6}{19} \frac{8.0}{22} \frac{7.3}{28} \frac{7.5}{50}$

$\frac{8.3}{Inv} 16.14$

$\frac{7.3}{Inv} 15.14$

$\frac{8.1}{50} \frac{8.4}{43} \frac{6.4}{38} \frac{5.3}{27} \frac{5.4}{12} \quad 50 \quad \frac{5.4}{11} \frac{5.4}{15} \frac{8.7}{20} \frac{8.5}{31} \frac{7.7}{36} \frac{7.6}{50}$

$\frac{78}{50} \frac{7.6}{39} \frac{5.3}{28} \frac{5.4}{12} \quad 5.1 \quad \frac{5.5}{10} \frac{5.4}{15} \frac{8.7}{22} \frac{8.7}{25} \frac{7.7}{34} \frac{7.7}{50}$

$\frac{66}{50} \frac{6.6}{35} \frac{5.0}{29} \frac{5.4}{12} \quad 49 \quad \frac{5.4}{11} \frac{5.4}{16} \frac{8.7}{21} \frac{8.7}{27} \frac{8.1}{30} \frac{7.7}{50}$

$\frac{47}{50} \frac{5.2}{36} \frac{5.6}{27} \frac{7.3}{24} \frac{5.1}{20} \frac{5.3}{12} \quad 49 \quad \frac{5.4}{12} \frac{6.4}{20} \frac{7.9}{22} \frac{7.9}{27} \frac{7.1}{28} \frac{7.4}{50}$

$\frac{40}{50} \frac{4.4}{28} \frac{6.7}{24} \frac{5.2}{21} \frac{5.2}{12} \quad 48 \quad \frac{5.3}{12} \frac{5.3}{14} \frac{6.9}{20} \frac{6.8}{23} \frac{5.4}{28} \frac{5.3}{50}$

$\frac{3.3}{50} \frac{3.7}{29} \frac{5.7}{25} \frac{6.4}{18} \frac{5.1}{14} \frac{5.2}{11} \quad 48 \quad \frac{5.2}{12} \frac{5.2}{13} \frac{6.8}{18} \frac{6.7}{23} \frac{5.5}{27} \frac{5.6}{50} \frac{3.0}{151} \text{Floor}$

$\frac{2.7}{50} \frac{1.8}{30} \frac{6.7}{24} \frac{6.8}{19} \frac{5.4}{15} \frac{5.3}{12} \quad 49 \quad \frac{5.2}{12} \frac{5.6}{16} \frac{6.5}{20} \frac{6.3}{23} \frac{4.6}{26} \frac{3.9}{37} \frac{4.3}{50}$

$\frac{3.3}{50} \frac{3.3}{29} \frac{6.4}{24} \frac{6.3}{19} \frac{5.0}{14} \frac{5.1}{11} \quad 48 \quad \frac{5.3}{12} \frac{5.3}{14} \frac{6.6}{19} \frac{6.4}{23} \frac{4.9}{27} \frac{4.7}{40} \frac{4.7}{50}$

Sta	+	π	-	Elev
		924.44		
216+50				20.0
217				20.2
+50				20.3
TP #1	3.42	923.64	4.22	920.22
218				20.6
+50				20.6
219				20.2
+45				19.8
220				19.1
+50				18.3
221				17.1
+50				15.5
222				12.5
T.P	0.36	913.17	10.83	912.81

LT * RT

$\frac{41}{50}$ $\frac{41}{29}$ $\frac{6.2}{25}$ $\frac{5.9}{17}$ $\frac{4.7}{14}$ 4.4 $\frac{4.8}{11}$ $\frac{4.9}{14}$ $\frac{6.6}{19}$ $\frac{6.5}{23}$ $\frac{4.9}{28}$ $\frac{4.5}{40}$ $\frac{4.5}{50}$

$\frac{3.4}{50}$ $\frac{3.3}{30}$ $\frac{6.4}{24}$ $\frac{6.9}{20}$ $\frac{4.7}{15}$ $\frac{4.6}{12}$ 4.2 $\frac{4.6}{12}$ $\frac{4.9}{15}$ $\frac{6.3}{20}$ $\frac{6.2}{26}$ $\frac{4.6}{28}$ $\frac{4.6}{50}$

$\frac{1.2}{50}$ $\frac{1.5}{32}$ $\frac{6.0}{24}$ $\frac{6.2}{20}$ $\frac{4.8}{16}$ $\frac{4.4}{12}$ 4.1 $\frac{4.6}{12}$ $\frac{4.7}{15}$ $\frac{6.1}{21}$ $\frac{6.1}{25}$ $\frac{3.6}{30}$ $\frac{3.6}{41}$ $\frac{3.6}{50}$

Cont'd $\frac{4.2}{26}$ $\frac{4.7}{19}$ $\frac{3.5}{16}$ 3.0 $\frac{3.3}{15}$ $\frac{4.9}{21}$ $\frac{4.9}{26}$ Cont'd

11 $\frac{3.9}{29}$ $\frac{4.7}{24}$ $\frac{4.7}{19}$ $\frac{3.6}{15}$ 3.0 $\frac{3.4}{15}$ $\frac{4.5}{22}$ $\frac{4.4}{26}$

11 $\frac{3.3}{28}$ $\frac{4.5}{23}$ $\frac{4.7}{21}$ $\frac{4.1}{17}$ $\frac{3.8}{12}$ 3.4 $\frac{3.8}{12}$ $\frac{4.2}{16}$ $\frac{4.8}{20}$ $\frac{4.8}{23}$ $\frac{4.8}{27}$

11 $\frac{4.7}{25}$ $\frac{5.1}{20}$ $\frac{4.6}{16}$ $\frac{4.2}{12}$ 3.8 $\frac{4.3}{12}$ $\frac{4.6}{16}$ $\frac{5.3}{19}$ $\frac{5.7}{22}$ $\frac{5.2}{24}$

11 $\frac{5.8}{23}$ $\frac{6.0}{17}$ $\frac{5.0}{14}$ 4.5 $\frac{5.0}{12}$ $\frac{5.2}{15}$ $\frac{6.3}{18}$ $\frac{6.4}{21}$ $\frac{5.5}{24}$

11 $\frac{4.9}{27}$ $\frac{6.4}{22}$ $\frac{6.9}{18}$ $\frac{5.8}{14}$ 5.3 $\frac{5.8}{12}$ $\frac{5.8}{14}$ $\frac{7.2}{18}$ $\frac{7.2}{22}$

11 $\frac{6.6}{25}$ $\frac{7.8}{19}$ $\frac{7.0}{14}$ 6.5 $\frac{7.0}{15}$ $\frac{8.5}{19}$ $\frac{8.2}{22}$

$\frac{9.4}{24}$ $\frac{9.9}{20}$ $\frac{8.7}{15}$ 8.1 $\frac{9.7}{14}$ $\frac{10.1}{18}$ $\frac{9.9}{22}$

$\frac{10.7}{26}$ $\frac{12.0}{20}$ $\frac{11.9}{18}$ $\frac{10.8}{14}$ 10.1 $\frac{10.5}{15}$ $\frac{12.4}{20}$ $\frac{10.7}{26}$

Sta	+	π	-	Elev
		913.17		
222+50				11.2
223+15				07.6
+45				06.1
+70				04.7
224				03.0
+20				01.7
T.P.	0.44	900.08	13.53	899.64
+35				00.6
+50				99.7
225				96.6
+20				95.4
+50				93.4
+80				91.1

4 L PT

$$\frac{2.8}{24} \frac{3.5}{22} \frac{3.0}{16} \frac{2.6}{13} 2.0 \frac{2.3}{15} \frac{4.1}{20} \frac{3.0}{27}$$

$$\frac{4.7}{26} \frac{7.2}{20} \frac{7.2}{16} \frac{6.0}{13} 5.6 \frac{6.1}{17} \frac{7.5}{19} \frac{7.3}{23} \frac{3.1}{32}$$

$$\frac{5.8}{24} \frac{8.7}{18} \frac{8.8}{16} \frac{7.6}{12} 7.1 \frac{7.2}{15} \frac{8.6}{19} \frac{8.0}{39} \frac{5.7}{50} \frac{4.4}{90}$$

$$\frac{6.5}{25} \frac{9.6}{18} \frac{9.7}{17} \frac{9.0}{12} 8.5 \frac{8.6}{17} \frac{10.7}{26} \frac{8.7}{50} \frac{6.3}{100}$$

$$\frac{7.3}{27} \frac{11.3}{18} \frac{11.5}{15} \frac{10.7}{12} 10.2 \frac{10.2}{11} \frac{10.0}{33} \frac{8.4}{50} \frac{4.9}{100}$$

$$\frac{10.5}{24} \frac{13.0}{20} \frac{13.1}{15} \frac{12.0}{13} 11.5 \frac{12.6}{18} \frac{13.8}{24} \frac{13.3}{33} \frac{9.0}{40} \frac{9.0}{50} \frac{4.2}{100}$$

$$\frac{0.0}{22} \frac{1.4}{18} \frac{1.4}{15} \frac{0.0}{12} + 0.5 \frac{+0.4}{17} \frac{1.7}{21} \frac{1.3}{27}$$

$$\frac{0.4}{25} \frac{1.3}{21} \frac{2.2}{20} \frac{2.3}{15} \frac{1.0}{11} 0.4 \frac{0.9}{17} \frac{2.9}{20} \frac{2.6}{24} \frac{0.3}{29}$$

$$\frac{2.2}{28} \frac{5.4}{20} \frac{5.6}{16} \frac{4.3}{14} 3.5 \frac{4.1}{15} \frac{6.3}{19} \frac{6.1}{24} \frac{4.9}{26} \frac{2.7}{31}$$

$$\frac{4.4}{25} \frac{6.1}{20} \frac{7.0}{19} \frac{7.0}{15} \frac{5.3}{13} 4.7 \frac{5.3}{16} \frac{7.2}{20} \frac{6.9}{24} \frac{4.7}{30}$$

$$\frac{5.4}{38} \frac{6.8}{23} \frac{7.5}{21} \frac{7.6}{13} 6.7 \frac{7.4}{15} \frac{7.0}{19} \frac{8.9}{25} \frac{6.3}{29} \frac{3.2}{37} \frac{1.7}{50} \frac{1.4}{75}$$

+0.6 Floor Room

$$\frac{5.6}{73} \frac{7.0}{50} \frac{7.6}{16} 9.0 \frac{9.9}{14} \frac{9.9}{27} \frac{8.3}{31} \frac{3.7}{38} \frac{2.9}{50} \frac{2.7}{75}$$

Sta + π - Elev

900.08

225+93

89.9

B.M

10.35

889.73

T.P #1

10.80

931.02

920.22

218

+50

219

+45

220

+50

221

+50

222

+50

14 2 14

$\frac{7.1}{100}$ $\frac{5.9}{69}$ $\frac{7.6}{50}$ $\frac{10.7}{12}$ 10.2 $\frac{10.9}{14}$ $\frac{10.4}{43}$ $\frac{9.4}{100}$

889.73

Top Cess pool 70' R+ Stg. 226+30 N.E. Corr

Cont.
 $\frac{6.0}{75}$ $\frac{6.7}{50}$ $\frac{6.7}{36}$ $\frac{8.7}{31}$ $\frac{8.3}{50}$ $\frac{9.0}{75}$ ✓

$\frac{5.2}{75}$ $\frac{5.8}{50}$ $\frac{5.9}{37}$ $\frac{5.8}{34}$ $\frac{6.5}{50}$ $\frac{7.0}{75}$ ✓

$\frac{5.1}{75}$ $\frac{5.4}{50}$ $\frac{5.1}{38}$ $\frac{6.7}{33}$ $\frac{7.7}{50}$ $\frac{7.6}{75}$ ✓

$\frac{6.1}{75}$ $\frac{6.4}{50}$ $\frac{6.2}{38}$ $\frac{7.4}{31}$ $\frac{8.9}{50}$ $\frac{9.0}{75}$ ✓

$\frac{5.2}{100}$ $\frac{5.5}{75}$ $\frac{5.9}{56}$ $\frac{5.4}{36}$ HA $\frac{6.8}{33}$ $\frac{8.4}{50}$ $\frac{9.9}{100}$

$\frac{9.5}{100}$ $\frac{4.8}{75}$ $\frac{4.5}{39}$ $\frac{6.7}{34}$ $\frac{8.4}{50}$ $\frac{10.0}{100}$

$\frac{5.9}{100}$ $\frac{5.2}{75}$ $\frac{4.5}{41}$ $\frac{6.7}{37}$ $\frac{7.7}{50}$ $\frac{9.5}{100}$ ✓

$\frac{9.2}{100}$ $\frac{8.0}{75}$ $\frac{5.6}{41}$ $\frac{5.6}{41}$ $\frac{6.1}{50}$ $\frac{7.8}{100}$ ✓

$\frac{7.3}{100}$ $\frac{8.7}{75}$ $\frac{8.7}{40}$ $\frac{4.4}{45}$ $\frac{5.1}{50}$ $\frac{6.2}{100}$ ✓

$\frac{5.6}{100}$ $\frac{7.1}{75}$ $\frac{6.4}{48}$ $\frac{6.7}{45}$ $\frac{7.1}{50}$ $\frac{8.7}{100}$ ✓

Sta + π - Elev

931.02

223 + 15

+ 45

+ 70

224

+ 20

T.P. 2.56 919.85 13.73 917.29

+ 35

+ 50

225

+ 20

T.P. 0.46 908.46 11.85 908.00

225 + 20

+ 50

T.P. 0.96 896.44 12.78 895.48

B.M. 6.72 889.72

Sections lost - see following page for
re-cross sections

Sta.	+	-	Elev.
B.M.	13.48	903.21	889.73
T.P.		0.36	902.85
	11.46	914.31	
T.P.		0.30	914.01
	13.02	927.03	
T.P.		1.64	925.39
	8.42	933.81	

223+15

+45

+70

224

+20

T.P. 8.42 925.39

1.20 926.59

+35

+50

T.P. 12.41 914.18

0.01 914.19

225

Lt.

E

Rt.

See Bench Levels.
 Cont. cesspool - N.E. cor. 70' Rt. Sta. 226+30

$\frac{10.3}{100}$	$\frac{9.7}{75}$	$\frac{6.7}{52}$ ^{26.2}	$\frac{8.9}{53}$	$\frac{10.0}{67}$	$\frac{11.2}{100}$
--------------------	------------------	----------------------------------	------------------	-------------------	--------------------

$\frac{8.6}{100}$	$\frac{7.6}{75}$	$\frac{5.6}{52}$
-------------------	------------------	------------------

$\frac{7.2}{100}$	$\frac{5.9}{75}$	$\frac{4.7}{55}$
-------------------	------------------	------------------

$\frac{8.8}{100}$	$\frac{8.2}{75}$	$\frac{7.6}{56}$
-------------------	------------------	------------------

$\frac{14.2}{100}$	$\frac{12.5}{75}$	$\frac{11.0}{51}$
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$\frac{10.3}{100}$	$\frac{8.9}{75}$	$\frac{9.2}{50}$	$\frac{12.9}{72}$	$\frac{11.5}{100}$
--------------------	------------------	------------------	-------------------	--------------------

$\frac{12.6}{100}$	$\frac{11.4}{75}$	$\frac{10.9}{47}$	$\frac{15.0}{60}$	$\frac{12.3}{100}$
--------------------	-------------------	-------------------	-------------------	--------------------

$\frac{5.4}{100}$	$\frac{6.6}{43}$ ^{17.6}	$\frac{8.5}{41}$	$\frac{10.2}{100}$
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House Floor
4.5

Sta.	+	T.	-	Elev.
		914.19		
225+20				
+50				
T.P.			11.33	902.86
	0.54	903.40		
B.M.			13.67	889.73
B.M.	1.50	891.23		889.73
226			89.4	
+17			87.9	
+50			85.0	
T.P. #1			13.05	878.18
227			80.4	
T.P.			13.12	878.11
	0.51	878.61		
+50			76.3	
228			71.7	
+50			67.5	

4.

2

10.

8

$$\frac{7.3}{100}$$

$$\frac{7.3}{50}$$

$$\frac{8.7}{42}$$

$$\frac{12.4}{38}$$

$$\frac{12.1}{50}$$

$$\frac{11.3}{100}$$

$$\frac{8.9}{100}$$

$$\frac{10.5}{52}$$

(889.73) Bench Levels

$$\frac{2.3}{100} \frac{1.0}{75} \frac{2.0}{60} \frac{0.5}{34} \frac{1.4}{28} \frac{2.0}{13} \frac{1.8}{18} \frac{1.5}{50} \frac{0.4}{87}$$

$$\frac{6.6}{100} \frac{6.7}{50} \frac{5.9}{25} \frac{3.4}{19} \frac{3.4}{14} \frac{3.6}{13} \frac{3.3}{14} \frac{3.8}{14} \frac{2.8}{16} \frac{5.7}{28} \frac{1.1}{63} \frac{0.0}{100}$$

$$\frac{17.0}{100} \frac{15.3}{54} \frac{14.0}{29} \frac{6.2}{16} \frac{6.2}{14} \frac{6.5}{13} \frac{6.2}{13} \frac{6.8}{13} \frac{6.4}{14} \frac{6.4}{17} \frac{13.4}{29} \frac{13.0}{80} \frac{11.6}{100}$$

For later use only

$$\frac{10.7}{17} \frac{10.7}{15} \frac{11.1}{13} \frac{10.8}{13} \frac{11.4}{14} \frac{11.2}{18} \frac{11.7}{20}$$

$$\frac{2.3}{13} \frac{2.3}{13} \frac{2.5}{14} \frac{2.3}{14} \frac{3.1}{16} \frac{2.6}{17} \frac{2.6}{21}$$

$$\frac{7.0}{14} \frac{7.0}{11} \frac{7.1}{10} \frac{6.9}{18} \frac{7.7}{20} \frac{7.4}{20} \frac{7.4}{23}$$

$$\frac{11.1}{7} \frac{11.3}{8} \frac{11.1}{9} \frac{11.1}{9} \frac{12.0}{22} \frac{11.6}{24}$$

Sta.	+	π	-	Elev.
		878.62		
T.P.#3			13.38	865.24
229	0.14	865.38		63.8
+15				63.1
+75				51.6
T.P.#4			8.34	857.04
	2.27	859.31		
230				50.1
+46 = 30" Corr. Metal Culvert.				
+50				45.3
231				46.0
+50				44.8
232				46.3
+50				47.1
233				48.3

47.21219

$$\frac{1.4}{3}$$

$$\frac{1.6}{1}$$

$$\frac{1.4}{13}$$

$$\frac{2.3}{27}$$

$$\frac{1.9}{28}$$

$$\frac{2.3}{1}$$

$$\frac{2.4}{18}$$

$$\frac{2.4}{37}$$

$$\frac{3.8}{33}$$

$$\frac{3.4}{33}$$

$$\frac{13.8}{11}$$

$$\frac{5.7}{13}$$

$$\frac{6.0}{27}$$

$$\frac{6.0}{43}$$

$$\frac{7.6}{44}$$

$$\frac{7.3}{44}$$

$$\frac{13.8}{100}$$

$$\frac{13.1}{50}$$

$$\frac{13.4}{34}$$

$$\frac{12.0}{20}$$

$$\frac{14.2}{16}$$

$$\frac{10.1}{10}$$

$$\frac{9.2}{5}$$

$$\frac{8.8}{16}$$

$$\frac{12}{17}$$

$$\frac{13}{30}$$

$$\frac{12}{45}$$

$$\frac{23}{47}$$

$$\frac{2.1}{51}$$

$$\frac{5.2}{67}$$

$$\frac{16.7}{100}$$

$$\frac{15.7}{15.4}$$

$$\frac{10.4}{70}$$

$$\frac{11.0}{78}$$

$$\frac{15.3}{83}$$

$$\frac{12.2}{89}$$

$$\frac{13.6}{100}$$

$$\frac{14.9}{100}$$

$$\frac{15.3}{100}$$

$$\frac{14.4}{50}$$

$$\frac{14.0}{7}$$

$$\frac{13.0}{27}$$

$$\frac{3.6}{28}$$

$$\frac{4.1}{43}$$

$$\frac{3.4}{43}$$

$$\frac{4.3}{26}$$

$$\frac{4.0}{87}$$

$$\frac{8.7}{67}$$

$$\frac{11.3}{80}$$

$$\frac{15.0}{100}$$

$$\frac{15.1}{50}$$

$$\frac{14.3}{17}$$

$$\frac{13.3}{22}$$

$$\frac{5.4}{37}$$

$$\frac{5.7}{38}$$

$$\frac{5.2}{50}$$

$$\frac{6.3}{68}$$

$$\frac{6.6}{70}$$

$$\frac{12.6}{88}$$

$$\frac{15.1}{100}$$

$$\frac{14.9}{50}$$

$$\frac{15.0}{16}$$

$$\frac{14.5}{15}$$

$$\frac{14.0}{31}$$

$$\frac{14.5}{37}$$

$$\frac{13.5}{53}$$

$$\frac{6.1}{55}$$

$$\frac{6.2}{67}$$

$$\frac{5.9}{83}$$

$$\frac{6.6}{88}$$

$$\frac{7.0}{100}$$

$$\frac{14.1}{100}$$

$$\frac{14.6}{50}$$

$$\frac{13.8}{16}$$

$$\frac{13.0}{15}$$

$$\frac{12.6}{50}$$

$$\frac{12.3}{88}$$

$$\frac{6.0}{25}$$

$$\frac{6.1}{67}$$

$$\frac{5.4}{81}$$

$$\frac{6.4}{76}$$

$$\frac{11.1}{106}$$

$$\frac{11.1}{110}$$

$$\frac{13.5}{100}$$

$$\frac{13.7}{50}$$

$$\frac{13.1}{16}$$

$$\frac{12.2}{30}$$

$$\frac{11.5}{50}$$

$$\frac{12.0}{71}$$

$$\frac{10.1}{81}$$

$$\frac{4.4}{87}$$

$$\frac{4.6}{94}$$

$$\frac{4.0}{110}$$

$$\frac{4.4}{120}$$

$$\frac{8.2}{120}$$

$$\frac{13.4}{100}$$

$$\frac{12.3}{50}$$

$$\frac{11.0}{15}$$

$$\frac{11.0}{28}$$

$$\frac{10.4}{50}$$

$$\frac{9.9}{80}$$

$$\frac{9.2}{80}$$

$$\frac{3.0}{90}$$

$$\frac{3.5}{91}$$

$$\frac{2.3}{100}$$

$$\frac{2.8}{120}$$

$$\frac{6.7}{128}$$

Sta.	+	Σ	-	Elev.
233+50		859.31		49.2
234				51.1
T.P.			7.63	851.68
	4.82	856.50		
B.M.			10.66	845.84
T.P.#1	0.19	878.37		878.18
T.P.			13.11	865.26
	0.52	865.78		
227				
+50				
T.P.			12.75	853.03
228	5.22	858.25		
+50				
229				
+15				
+75				
T.P.			11.80	846.45

Lt.ERt.10

$\frac{12.5}{100}$	$\frac{11.5}{65}$	$\frac{11.1}{50}$	$\frac{10.7}{15}$	$\frac{10.1}{50}$	$\frac{9.0}{50}$	$\frac{7.3}{90}$	$\frac{2.0}{100}$	$\frac{0.4}{105}$	$\frac{0.7}{106}$	20	120	$\frac{0.6}{133}$	$\frac{4.6}{142}$
--------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------	-------------------	-------------------	-------------------	----	-----	-------------------	-------------------

$\frac{12.4}{100}$	$\frac{10.3}{50}$	$\frac{9.1}{14}$	$\frac{8.2}{50}$	$\frac{7.8}{50}$	$\frac{5.9}{62}$	$\frac{9.9}{79}$	$\frac{8.4}{100}$	$\frac{+0.7}{117}$
--------------------	-------------------	------------------	------------------	------------------	------------------	------------------	-------------------	--------------------

845.88 See Bench Levels. 80' Lt. Sta. 236+ 97.85

14.6

Note: Ditch takes off at
end of frame spillway
see topog notes.

$\frac{4.0}{47}$	$\frac{4.5}{66}$	$\frac{2.8}{100}$
------------------	------------------	-------------------

$\frac{6.8}{48}$	$\frac{9.4}{58}$	$\frac{16.1}{68}$	$\frac{16.1}{70}$	$\frac{14.0}{73}$	$\frac{16.4}{100}$
------------------	------------------	-------------------	-------------------	-------------------	--------------------

12
21
3613.4

$\frac{5.4}{50}$	$\frac{7.5}{64}$	$\frac{12.0}{70}$	$\frac{12.0}{72}$	$\frac{9.9}{74}$	$\frac{11.0}{100}$
------------------	------------------	-------------------	-------------------	------------------	--------------------

$\frac{7.8}{50}$	$\frac{9.2}{68}$	$\frac{12.0}{74}$	$\frac{13.0}{76}$	$\frac{10.4}{78}$	$\frac{11.9}{100}$
------------------	------------------	-------------------	-------------------	-------------------	--------------------

5.5

$\frac{8.3}{50}$	$\frac{9.2}{72}$	$\frac{13.2}{76}$	$\frac{13.2}{78}$	$\frac{11.2}{82}$	$\frac{11.8}{87}$	$\frac{12.5}{100}$
------------------	------------------	-------------------	-------------------	-------------------	-------------------	--------------------

$\frac{8.0}{51}$	$\frac{9.0}{69}$	$\frac{13.4}{76}$	$\frac{13.4}{78}$	$\frac{10.8}{84}$	$\frac{11.4}{87}$	$\frac{12.6}{100}$
------------------	------------------	-------------------	-------------------	-------------------	-------------------	--------------------

$\frac{7.5}{54}$	$\frac{9.9}{73}$	$\frac{13.6}{80}$	$\frac{13.6}{82}$	$\frac{11.3}{86}$	$\frac{12.6}{100}$
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846.41

Top of C.M. culvert Rt. end. Sta. 230+46

Sta. + K - Elev.

T.P.#3 2.94 868.16 865.24

227

+50

T.P. 13.44 854.77

4.56 859.28

228

+50

229

+15

+25

T.P.#4 2.26 857.02

Lt.

L

Rt.

11

$$\frac{8.7}{100}$$

$$\frac{6.2}{46}$$

(12.2)

$$\frac{12.7}{100} \quad \frac{16.1}{67} \quad \frac{14.9}{63} \quad \frac{16.5}{61} \quad \frac{16.5}{57} \quad \frac{13.0}{51} \quad \frac{11.4}{44}$$

$$\frac{11.2}{100} \quad \frac{10.2}{67} \quad \frac{8.2}{63} \quad \frac{11.0}{60} \quad \frac{11.0}{56} \quad \frac{6.7}{50} \quad \frac{4.8}{39}$$

(12.4)

$$\frac{12}{21} \\ \hline 36$$

$$\frac{12.1}{100} \quad \frac{10.4}{58} \quad \frac{12.3}{55} \quad \frac{12.3}{51} \quad \frac{9.2}{45} \quad \frac{6.2}{34}$$

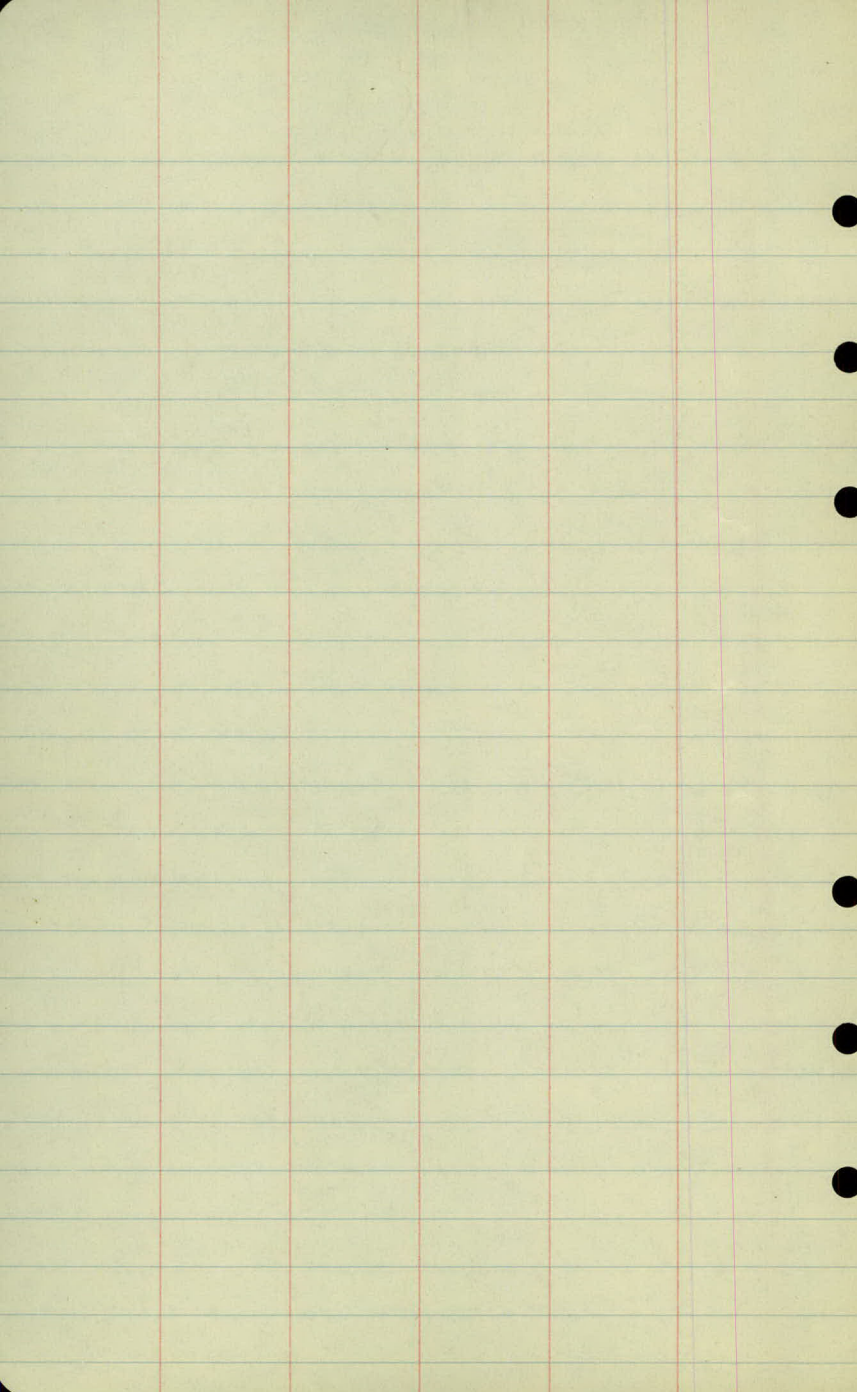
$$\frac{12.5}{100} \quad \frac{11.8}{53} \quad \frac{13.5}{48} \quad \frac{13.5}{45} \quad \frac{10.5}{37} \quad \frac{9.5}{28}$$

(4.5)

$$\frac{12.8}{100} \quad \frac{12.4}{50} \quad \frac{14.5}{46} \quad \frac{14.5}{41} \quad \frac{11.3}{37} \quad \frac{9.5}{32}$$

$$\frac{14.0}{100} \quad \frac{12.0}{50} \quad \frac{7.6}{29} \quad \frac{14.1}{26} \quad \frac{14.1}{23} \quad \frac{10.4}{17} \quad \frac{9.3}{3}$$

857.04



Carpenter Ave.

(Dale St. to Edgerton St.)

Bench Levels.

Sta.	+	K	-	Elev.
B.M.	5.14	924.07		918.93
T.P.	5.52	924.77	4.82	919.25
B.M.	0.35	919.46	5.66	919.11
T.P.	1.11	907.17	13.40	906.06
T.P.	0.73	894.99	12.91	894.26
B.M.	5.26	894.99	5.26	889.73
T.P.	0.61	882.49	12.11	882.88
T.P.	0.38	872.00	11.87	871.62
T.P.	0.07	863.05	9.02	862.98
T.P.	4.02	857.19	9.88	852.17
B.M.	7.38	852.26	11.31	845.88
T.P.	2.29	849.24	6.31	846.95
✓	10.84	856.91	3.17	846.07
B.M.	4.19	856.91	4.19	852.72
T.P.	14.54	868.28	1.17	855.74
T.P.	12.94	880.87	0.35	867.93
✓	12.46	894.98	0.35	880.52
B.M.	9.22	894.98	9.22	882.76
T.P.	1.65	884.35	14.28	880.70
T.P.	4.63	871.59	13.39	868.96
B.M.	6.82	871.59	6.82	864.77 O.K.
B.M.			6.63	864.96

Very Windy Day.

10/28/36
46.

2

Lerpentour Ave.

Top of Monument 210 + 75.75
x Dale & W. Lerpentour

Spike in T.P. Lt. of Sta.

Conc. Cesspool - N.E. Cor. 70' Rt. Sta. 226 + 30

Bratager } 10/31/56
Gillon }

Spike in Fence Post 80' Lt. Sta. 236 + 97.85

150' Rt. Sta.

Belt - Bridge ditch Xing 40' Lt. Sta.

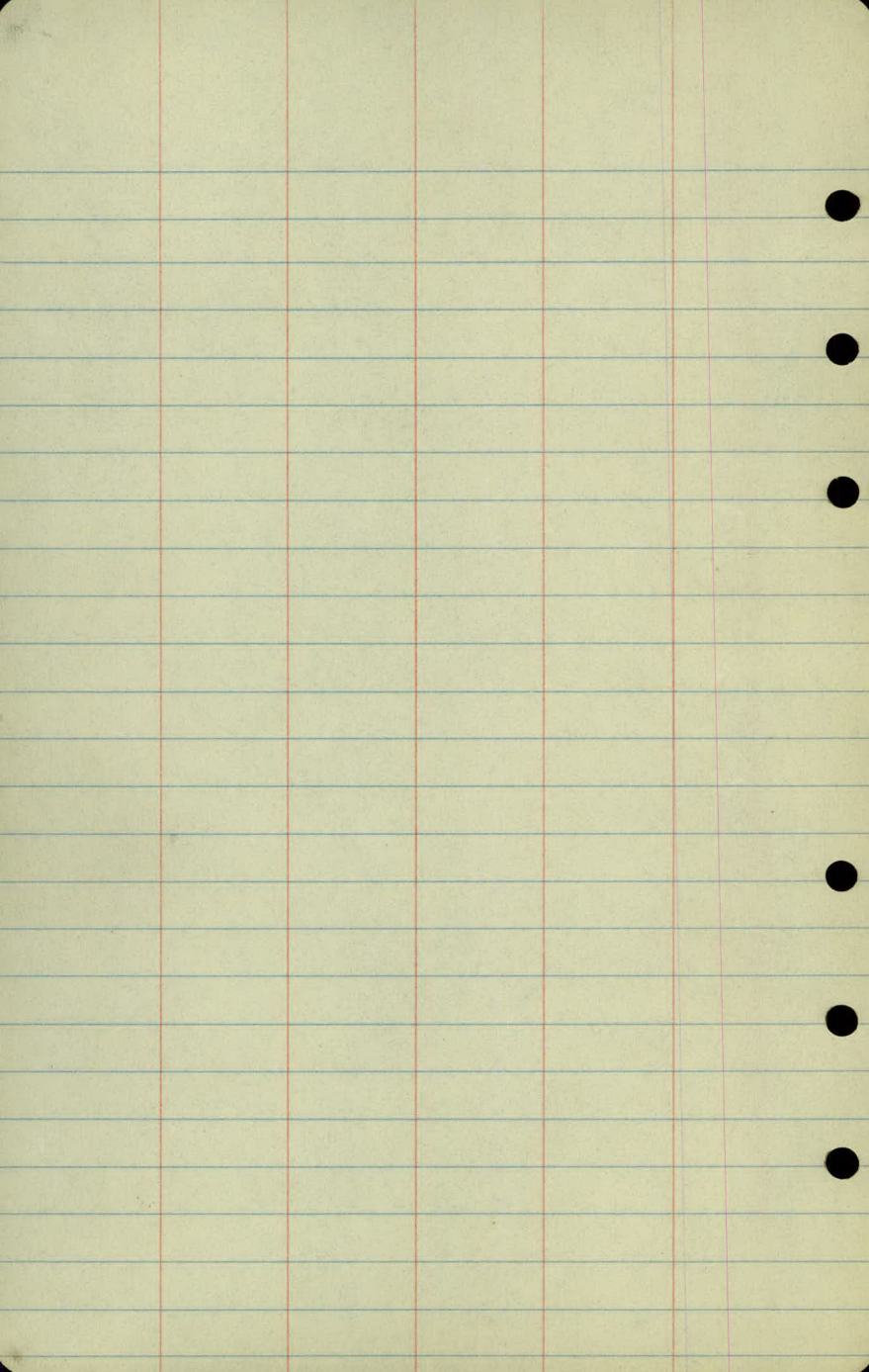
Nail in fence post 175' Lt. Sta.

Boulder 35' Rt. Sta.

Spike in Fence post 100' Lt. Sta.

R.R. spike in power pole N.W. cor. Lerpentour
+ Rice Sts.

Top monument Rice & Lerpentour Aves.



Corporateur X-Sec.
(Date to Edger ton.)

Sts.	+	K	-	Elev.
B.M 226	1.50	891.23		889.73

+17

+50

(T.P. #1)

(13.05)

(878.18)

227

T.P. #2	0.51	878.62	13.12	878.11
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+50

228

150

T.P. #3	0.14	865.38	13.34	865.24
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229

+15

229 + 75

T.P. #4	2.27	859.31	8.34	857.04
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LT.ERT

2

$$\frac{2.3}{100} \quad \frac{1.0}{75} \quad \frac{2.0}{60} \quad \frac{0.5}{32} \quad \frac{1.4}{28} \quad \frac{2.0}{13} \quad \frac{1.8}{10} \quad \frac{1.5}{50} \quad \frac{0.4}{87}$$

$$\frac{6.6}{100} \quad \frac{6.7}{50} \quad \frac{5.9}{25} \quad \frac{3.7}{19} \quad \frac{3.7}{14} \quad \frac{3.6}{13} \quad \frac{3.3}{10} \quad \frac{3.8}{12} \quad \frac{2.8}{16} \quad \frac{5.7}{28} \quad \frac{1.1}{63} \quad \frac{0.0}{100}$$

$$\frac{17.0}{100} \quad \frac{15.3}{54} \quad \frac{14.0}{29} \quad \frac{6.2}{16} \quad \frac{6.2}{14} \quad \frac{6.5}{13} \quad \frac{6.2}{10} \quad \frac{6.8}{13} \quad \frac{6.4}{14} \quad \frac{6.4}{17} \quad \frac{13.4}{29} \quad \frac{13.0}{50} \quad \frac{11.6}{100}$$

$$\frac{10.7}{17} \quad \frac{10.7}{15} \quad \frac{11.1}{13} \quad \frac{10.8}{10} \quad \frac{11.4}{14} \quad \frac{11.7}{15} \quad \frac{11.7}{20}$$

$$\frac{2.3}{11} \quad \frac{2.3}{13} \quad \frac{2.5}{12} \quad \frac{2.3}{10} \quad \frac{3.1}{16} \quad \frac{2.6}{17} \quad \frac{2.6}{21}$$

$$\frac{7.0}{12} \quad \frac{7.0}{11} \quad \frac{7.1}{10} \quad \frac{6.9}{9} \quad \frac{7.7}{18} \quad \frac{7.4}{20} \quad \frac{7.4}{23}$$

$$\frac{11.1}{7} \quad \frac{11.3}{5} \quad \frac{11.1}{4} \quad \frac{11.1}{9} \quad \frac{12.0}{22} \quad \frac{11.6}{24}$$

$$\frac{1.4}{3} \quad \frac{1.6}{1} \quad \frac{1.4}{13} \quad \frac{2.3}{27} \quad \frac{1.9}{28}$$

$$\frac{2.2}{1} \quad \frac{2.4}{1} \quad \frac{2.4}{18} \quad \frac{3.8}{31} \quad \frac{3.4}{33}$$

$$\frac{13.8}{11} \quad \frac{5.7}{11} \quad \frac{6.0}{13} \quad \frac{6.0}{27} \quad \frac{7.6}{43} \quad \frac{7.3}{44}$$

Sta.	+	T	-	Elev.
230		859.31		50.1
+46 Culvert	15.7	2nd Lt.	15.4	1st Lt.
+50				14.9
				16.2
				100' Lt.

231				46.0
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+50

232				46.3
-----	--	--	--	------

+50

233				48.3
-----	--	--	--	------

+50

234				51.1
-----	--	--	--	------

I.P.	4.82	816.50	7.63	811.18
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B.M.			10.66	845.84
------	--	--	-------	--------

4.

2

124

3

$$\frac{13.8}{100} \quad \frac{13.1}{50} \quad \frac{13.7}{34} \quad \frac{13.0}{20} \quad \frac{14.2}{16} \quad \frac{10.1}{10} \quad 9.2$$

$$\left\{ \begin{array}{l} \frac{8.8}{5} \quad \frac{1.7}{16} \quad \frac{1.3}{17} \quad \frac{1.2}{30} \quad \frac{2.3}{45} \quad \frac{2.1}{47} \quad \frac{2.7}{51} \quad \frac{6.0}{62} \\ \frac{10.4}{70} \quad \frac{11.0}{78} \quad \frac{11.3}{83} \quad \frac{12.2}{89} \quad \frac{13.6}{100} \end{array} \right.$$

$$\frac{15.3}{100}$$

$$\frac{14.4}{50}$$

$$\frac{14.0}{10}$$

$$\frac{13.0}{7}$$

$$\frac{3.6}{27}$$

$$\frac{4.1}{28}$$

$$\frac{3.4}{43}$$

$$\frac{4.3}{16}$$

$$\frac{9.0}{57}$$

$$\frac{8.7}{67}$$

$$\frac{11.3}{10}$$

$$\frac{15.5}{86}$$

$$\frac{12.0}{93}$$

$$\frac{12.1}{100}$$

$$\frac{15.0}{100}$$

$$\frac{15.1}{50}$$

$$\frac{14.3}{17}$$

$$\frac{13.3}{10}$$

$$\left\{ \begin{array}{l} \frac{12.4}{22} \quad \frac{5.4}{37} \quad \frac{5.7}{38} \quad \frac{5.2}{50} \quad \frac{6.3}{68} \quad \frac{6.6}{70} \quad \frac{12.6}{88} \end{array} \right.$$

$$\frac{14.9}{93}$$

$$\frac{12.8}{99}$$

$$\frac{12.8}{100}$$

$$\frac{15.1}{100}$$

$$\frac{14.9}{50}$$

$$\frac{15.0}{16}$$

$$\frac{14.5}{10}$$

$$\frac{14.0}{11}$$

$$\frac{14.5}{31}$$

$$\frac{13.5}{37}$$

$$\frac{6.1}{73}$$

$$\frac{6.2}{55}$$

$$\frac{5.9}{67}$$

$$\frac{6.6}{83}$$

$$\frac{2.0}{85}$$

$$\frac{12.1}{94}$$

$$\frac{12.5}{100}$$

$$\frac{14.6}{106}$$

$$\frac{14.1}{100}$$

$$\frac{14.6}{50}$$

$$\frac{13.8}{15}$$

$$\frac{13.0}{10}$$

$$\left\{ \begin{array}{l} \frac{12.6}{50} \quad \frac{12.3}{55} \quad \frac{6.0}{61} \quad \frac{6.1}{67} \quad \frac{5.4}{81} \quad \frac{6.4}{96} \quad \frac{11.1}{106} \end{array} \right.$$

$$\frac{11.1}{110}$$

$$\frac{13.5}{100}$$

$$\frac{13.7}{50}$$

$$\frac{12.1}{16}$$

$$\frac{12.2}{10}$$

$$\left\{ \begin{array}{l} \frac{11.1}{30} \quad \frac{12.0}{50} \quad \frac{10.1}{71} \quad \frac{4.4}{81} \quad \frac{4.6}{86} \quad \frac{4.0}{94} \quad \frac{7.4}{110} \end{array} \right.$$

$$\frac{11.1}{110}$$

$$\frac{13.4}{100}$$

$$\frac{12.3}{50}$$

$$\frac{11.0}{11}$$

$$\frac{11.0}{10}$$

$$\left\{ \begin{array}{l} \frac{10.4}{26} \quad \frac{9.9}{50} \quad \frac{9.7}{80} \quad \frac{3.0}{90} \quad \frac{3.5}{91} \quad \frac{2.3}{100} \end{array} \right.$$

$$\frac{2.8}{120}$$

$$\frac{6.7}{128}$$

$$\frac{12.5}{100}$$

$$\frac{11.5}{50}$$

$$\frac{11.1}{30}$$

$$\frac{10.2}{15}$$

$$\frac{10.1}{10}$$

$$\left\{ \begin{array}{l} \frac{9.0}{80} \quad \frac{7.3}{90} \quad \frac{2.0}{100} \quad \frac{0.4}{105} \quad \frac{0.7}{106} \quad \frac{0.0}{110} \quad \frac{0.6}{133} \end{array} \right.$$

$$\frac{4.6}{142}$$

$$\frac{12.4}{100}$$

$$\frac{10.3}{50}$$

$$\frac{9.1}{14}$$

$$\frac{8.2}{10}$$

$$\frac{7.8}{50}$$

$$\frac{8.9}{67}$$

$$\frac{9.9}{49}$$

$$\frac{8.4}{100}$$

$$\frac{10.7}{117}$$

841.88

Sta.	+	-	Elev.
T.P. #1	0.19	878.37	878.18
T.P.	0.52	865.78	865.26
227			

+50			
T.P.	5.22	858.75	853.03
228			

+50

229

+15

+75

T.P.	20p. Culvert	11.80
------	--------------	-------

546.45	OK
546.41	

41.

E

Rt.

Date begins at
end of flower
see topog

$$\frac{4.0}{47} \quad \frac{4.5}{66} \quad \frac{2.8}{100}$$

$$\frac{6.8}{48} \quad \frac{9.4}{58} \quad \frac{16.1}{68} \quad \frac{16.1}{70} \quad \frac{14.0}{73} \quad \frac{16.4}{100}$$

$$\frac{5.4}{50} \quad \frac{7.5}{64} \quad \frac{12.0}{70} \quad \frac{12.0}{72} \quad \frac{8.9}{74} \quad \frac{11.0}{100}$$

$$\frac{7.8}{50} \quad \frac{9.2}{68} \quad \frac{13.0}{74} \quad \frac{13.8}{76} \quad \frac{10.4}{78} \quad \frac{11.9}{100}$$

$$\frac{8.3}{50} \quad \frac{9.7}{72} \quad \frac{13.2}{76} \quad \frac{13.2}{78} \quad \frac{11.2}{82} \quad \frac{11.8}{87} \quad \frac{12.5}{100}$$

$$\frac{8.0}{51} \quad \frac{9.0}{69} \quad \frac{13.4}{76} \quad \frac{13.4}{78} \quad \frac{10.8}{84} \quad \frac{11.9}{87} \quad \frac{12.5}{100}$$

$$\frac{7.5}{54} \quad \frac{9.9}{73} \quad \frac{13.0}{80} \quad \frac{13.6}{82} \quad \frac{11.3}{86} \quad \frac{12.6}{100}$$

Sta.	+	$\times$	-	Elev.
T.P. #3	2.92	868.16		865.24

227

+50

T.P.	4.56	859.28	13.44	854.72
------	------	--------	-------	--------

228

+50

229

+15

+75

T.P. #4

2.26

857.02
 (857.04)

1/4 234 = last section

4.

2

et.

5

$$\frac{27}{100}$$

$$\frac{6.2}{46}$$

$$\frac{17.7}{100}$$

$$\frac{16.1}{67}$$

$$\frac{14.9}{63}$$

$$\frac{12.7}{61}$$

$$\frac{16.5}{59}$$

$$\frac{13.0}{57}$$

$$\frac{11.4}{44}$$

$$\frac{11.7}{100}$$

$$\frac{10.7}{67}$$

$$\frac{9.7}{63}$$

$$\frac{11.0}{60}$$

$$\frac{11.0}{56}$$

$$\frac{6.7}{50}$$

$$\frac{4.8}{29}$$

$$\frac{12.1}{100}$$

$$\frac{10.4}{58}$$

$$\frac{12.3}{55}$$

$$\frac{12.3}{51}$$

$$\frac{9.7}{45}$$

$$\frac{6.7}{34}$$

$$\frac{12.5}{100}$$

$$\frac{11.9}{53}$$

$$\frac{13.5}{48}$$

$$\frac{13.5}{45}$$

$$\frac{10.5}{37}$$

$$\frac{9.5}{28}$$

$$\frac{12.8}{100}$$

$$\frac{12.4}{50}$$

$$\frac{14.1}{46}$$

$$\frac{14.1}{41}$$

$$\frac{11.3}{37}$$

$$\frac{9.5}{27}$$

$$\frac{14.0}{100}$$

$$\frac{13.0}{50}$$

$$\frac{7.6}{29}$$

$$\frac{14.1}{26}$$

$$\frac{14.1}{23}$$

$$\frac{10.4}{17}$$

$$\frac{9.3}{3}$$

