

D-6-8K.115

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ PORTLAND AVE. _____

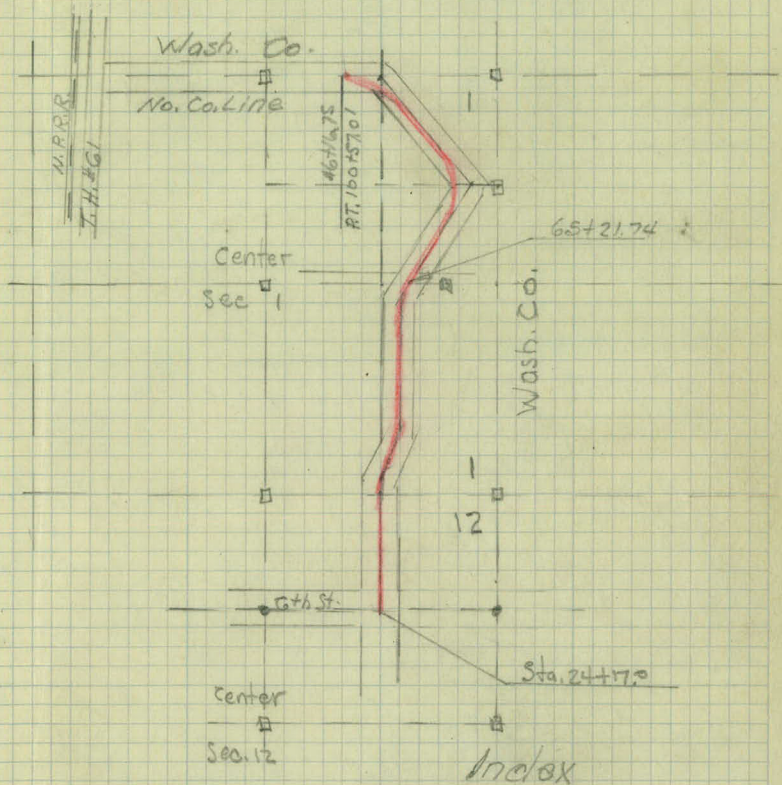
From 6th ST. _____ To NO. CO. LINE.

Road Acc't. No. 19 _____

Date Filed _____

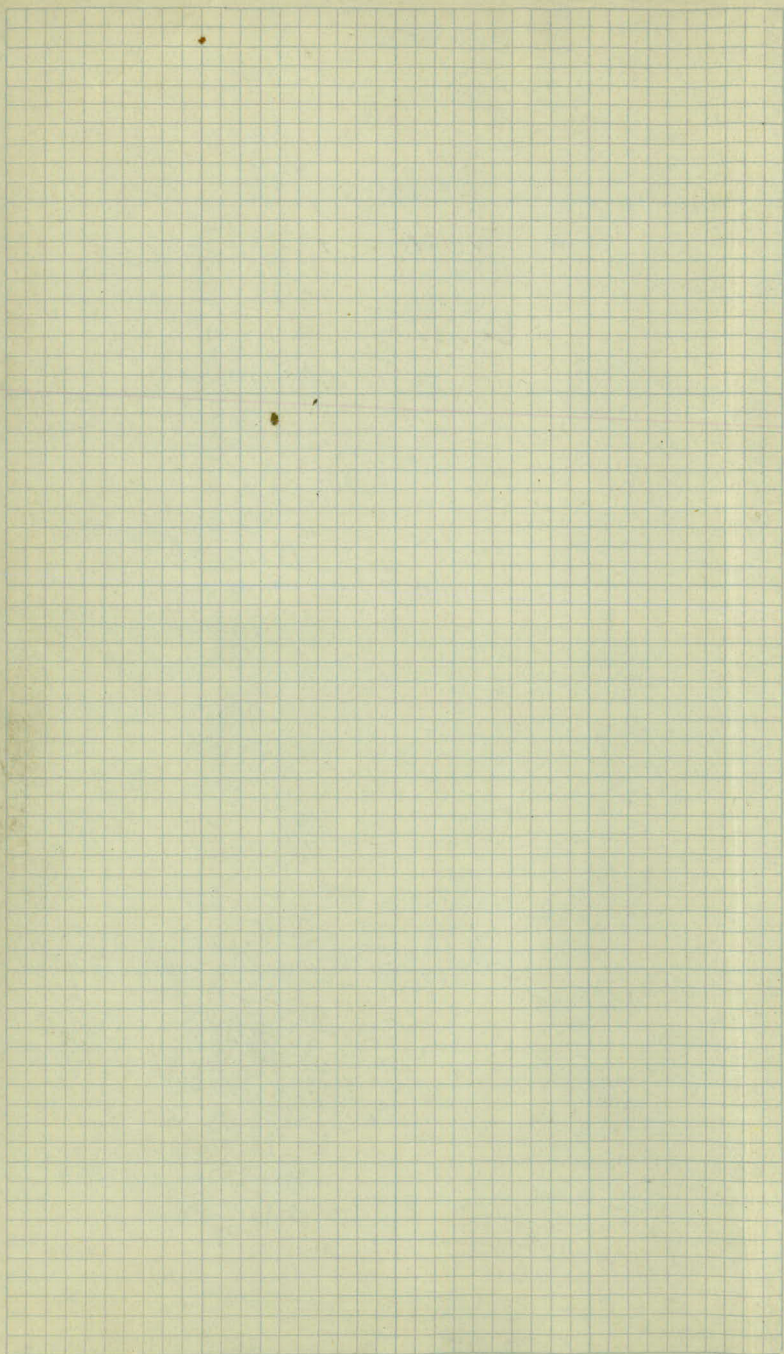
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Plan Survey Portland Ave. 6th St. to No. Co. Line.



align	P. 1-5
Topog.	P. 6-18
Traverse oldrs.	P. 19-24
X-Sections	P. 25-43
Re Corn-	P. 44
Bench Levels	P. 45-49

W. H. Carlson
March 1937



Alignment

Portland Ave.

Station	Point	Angle	
		Lt	Rt
39+71.87	P.T.	12°-30'	P.I. 38+49.05
+50		11°-24.4'	Δ 25°-00'
39+00	P.O.S.T.	8°-54.4'	D- 10°-00'
(37+91.05 E.W. Sec. 4.00)			
38+50		6°-24.4'	T. 127.18.
38+00		3°-54.4'	L. 230.00✓
+50		1°-24.4'	R. 573.69.
37+21.87	P.C.	0°-00'	

33+00.00 P.O.T.

N-0°-00'E.

24+17.00 ± 6th St

Stone

S.E. cor.

Sec. 1

Stone

1317.15

A

R.R. spike

16.92

R.P.

1317.15

Sec 12

N.E. cor.

15.F.

68.68

800

137

12" oak

26°-00'

58°-00'

Ramsey Co.
Wash Co.

Iron Mon.

Meas. 76 39.86

Rec. Holz. 76 32.56
76 38.77

29720 R.P.

6 EG to st.

Fixed
Nail

R.R. spike

T.R.

67.92

90°-30'

W.H. Carlson

K. Anker

L.B. Hendrix

A. Mooschler

Mar. 1, 1937

angle

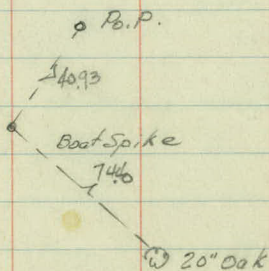
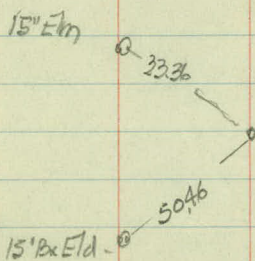
Station	Point	Lt	Rt	
61+1693	P.T.		5°13'1/2'	
61			4-58.3	
+50			4-13.3	P.I. 57+43.30
60			3-28.3	Δ 10°27' Rt.
+50			2-43.3	3°-C.
59			1-58.3	T. 174.70
+50			1-13.3	L. 248.33
58			0°28.3	R=
57+68.60	P.C.		0°00	

N-9°27'-E.

49+29.82	P.T.	13°00'		
49		11°48.4'		P.I. 47+70.3
+50		9°48.4'		Δ 26°00' Lt
48		7°48.4'		O-8°
+50		5°48.4'		T. 165.48
47		3°48.4'		L. 325.00
+50		1°48.4'		R. 716.78
46+04.82	P.C.	0°00		

N-1°00'-W.

N-25°00'-E.



Station	Point	angle	
		Lt	Rt

65+40.54

65+21.74 Ice Line

65+18.94 P.T.

6°-06'

65

5-42.7'

P.I. 63+67.04

4-42.7

A 12°-12'

64

3-42.7

D-4°

2-42.7

153.10
T. 152.59

63

1-42.7

L. 305.0

+50

0°-42.7

62+13.94 P.C.

0°-00'

N. 21° 39' E

center
[] Stone Mon.
sec. 1

$\frac{1342.28}{\text{Rec.} = 2000.00}$

Boat Spike

Nail

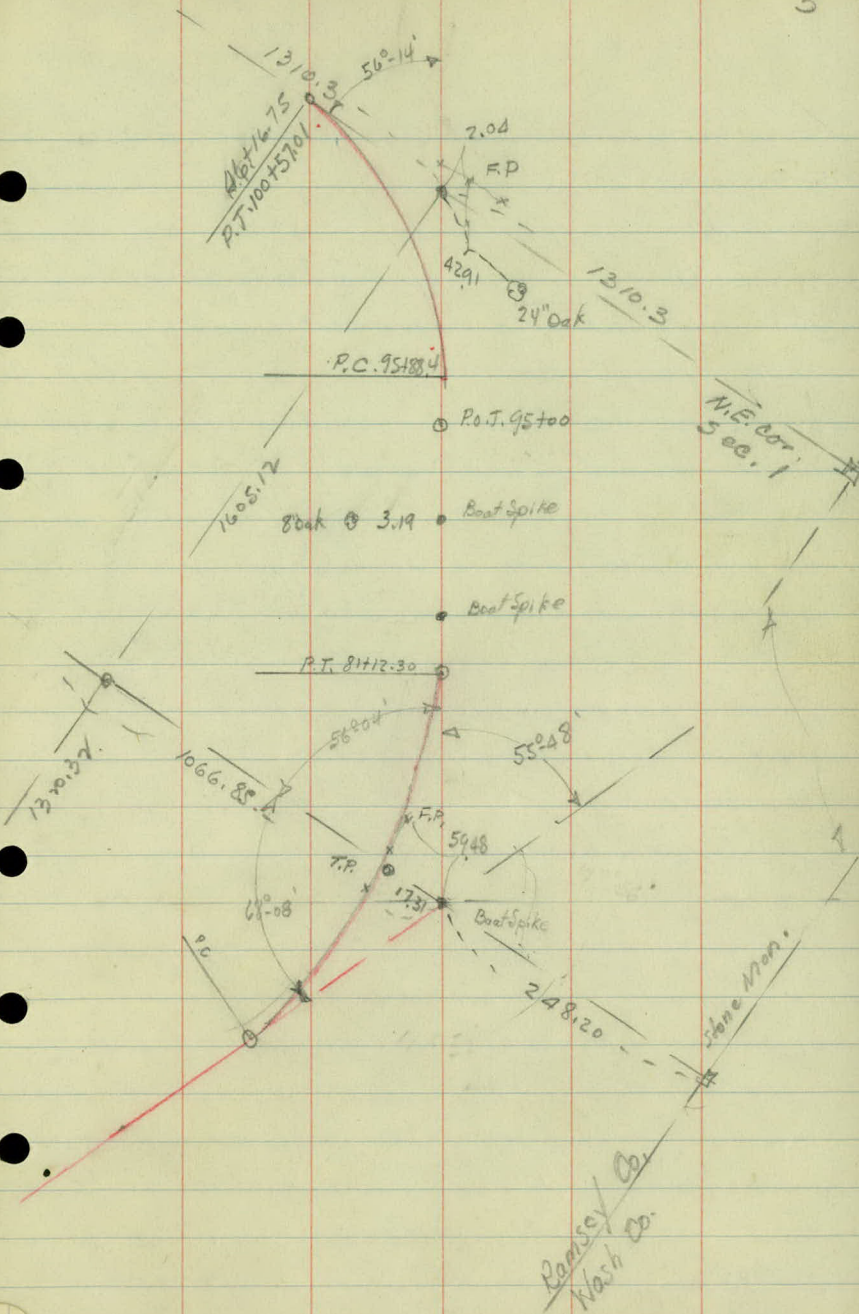
68'-00" 158.69 Stone M.C. 632.18 ft

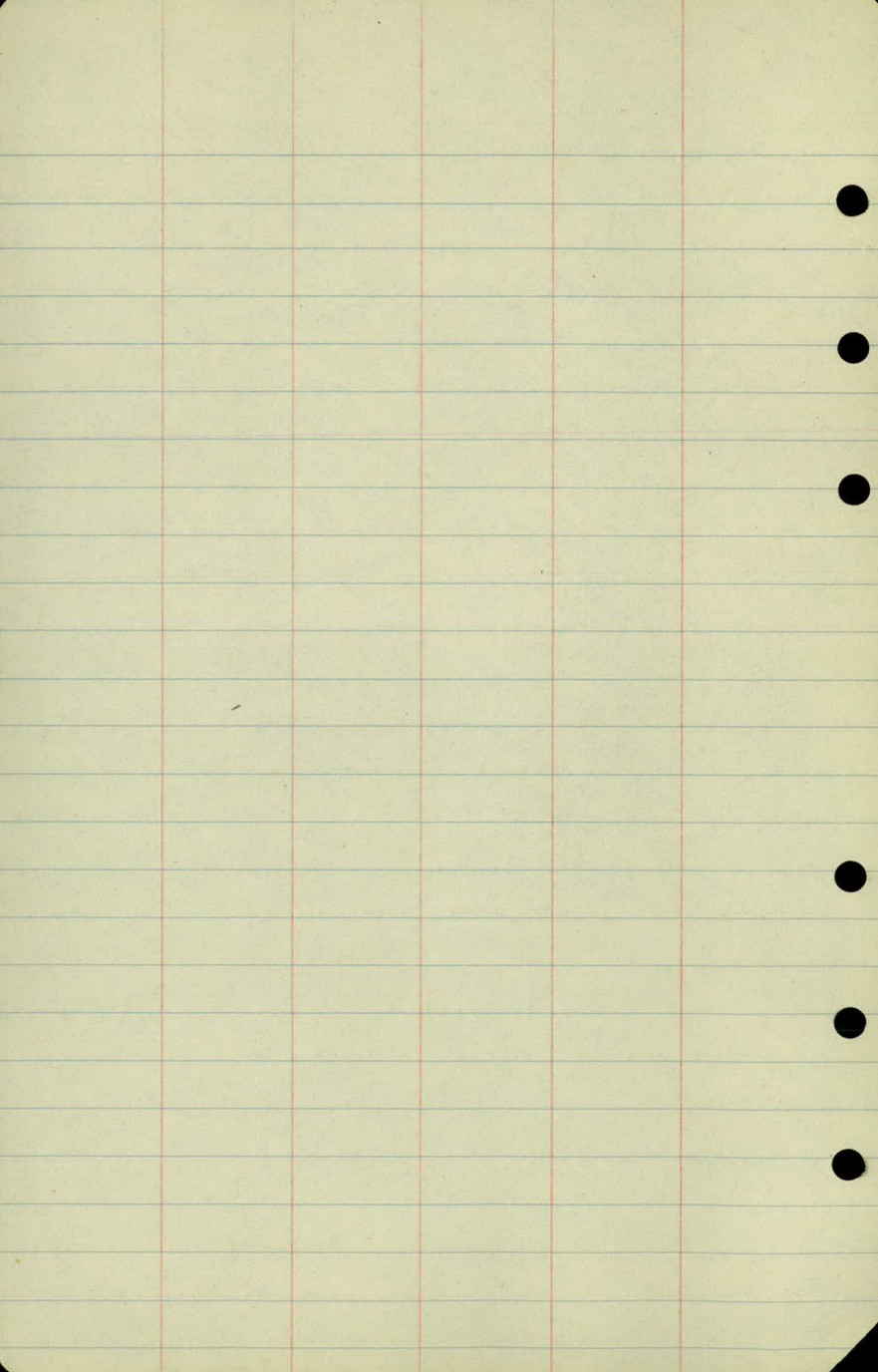
158.69

Ramsey Co.
Wash Co

Sta.	Point	ct	rt
EQ 46+16.75 1100+57.01	P.T.	28°-07'	
100		24°-41.8'	P.A. 98+44.0
		21°-41.8'	
99		18°-41.8'	A 56°14' L.
		15°-41.8'	
98		12°-41.8'	D- 12°
		9°-41.8'	
97		6°-41.8'	T. 255.60
		3°-41.8'	
96		0°-41.8'	L. 468.61
95+88.4	P.C.	0°-00'	R= 478.34
86+83.65	P.O.T.		
82+93.12	P.O.T.		
81+12.30	P.T.	27°-54'	
81		26°-58.7'	
		23°-13.7'	P.A. 79+43.12
80		19°-28.7'	A 55°48' L.
		15°-43.7'	D- 15°
79		11°-58.7'	T. 202.82
		8°-13.7'	L. 372.00
78		4°-28.7'	R= 383.26
77+50		0°-43.7'	
77+40.3	P.C.	0°-00'	

N. 34°-00' W





Topography.

14 10

27

14 10

26

13 13

25

11 14

+17 - 26th - West

24

13 17

+80 10 - 29

Oiled Surface Road

23

4 19

22

+81-T.P. 32'

+49-P.P. 26
65-Cedar 3'-8"

Cult.

+83-24' Oak 42'

+101-Bog (Box) Cedars 27'

+82-Ent.

+66-15' Box Elm 26
2 Cor. 36'

+85-T.P. 31'

+106-2" Cedar 25'

+94-12" Box E 27

+74-E 3 Wall 22

+86-N.W. Cor. 25.5'

+60-S.W. Cor. 10'

+85-24' Box Elm - End Road

+90-P.P. 28'

+44-End Four Tree 35'

+21-N.E. Cor. N.E. 80'



+98-T.P. 28'

+94-S.E. Cor. N.E. 80'

+43-P.P. 60'

+40-End 10" C.M. 17

6 Wires

Ent

+76-Bog (Box) 12' Box Elm 27

+54-Bog (Box) 12' Trees 25'

+34-Ent

+24-P.P. 29'

+92-End 10" E. 17

+78-Cult. 7' H.W. 10.3

+53-T.P. 24'

Ditch

Ditch

+79-Cult. 199
7-Head Wall
7.3 W. Wall 15

G' Wide - A' H.W.

5' x 6' Conc. Box

140 - App. 2 Taylor Ave.

34

19' 5

33

19' 5

32

18' 4

31

18' 7

30

17' 8

29

16' 10

28

+96-T.P. 36'

Cult.

34
15. F. 16

+92-F. Cor. 17
+78-20' Oak 38'
+71-S.W. Cor. 62'
+64-Beg F. 16'
+53-Ent.

+56-F. Cor. 37'

+40-F. Cor. 17'
+40-P. R. 19'

+95-End Oaks 33'

+60-T.P. 35'
+58-F. Cor. 37'

+59-18' Oak 2 1/2'

F-34'

+22-Beg F. 17'
+07-Ent.

+91-5" Oak 36

+72-P. R. 19'

+17-T.P. 35'

F-36

Small 100 ft S.
East. Large Oaks

24

+39-10" Oak 21'
+37-12" Oak 14'
+27-12" Oak 23'
+10-12" Oak 24'
+10-N.W. Cor. 45.5

+34.5-W. Cor. 15.5 F
46.5

Yard.

F-35

+22-Ent.
+01-P. R. 23'

+76-T.P. 35'

F-33

+96-6" Tree 21'

+22-T.P. 34'

Cult.

+22-P. R. 26

F-34

+07-End (End) Code 24.

+44-F. Cor. -24'

+33-Ent.

+05-Beg Oaks
40

Small Oaks

①
②

2-24'

41

1-26

40

1-22

250 0-22'

39

4-17'

950 12 9'

38

17-4'

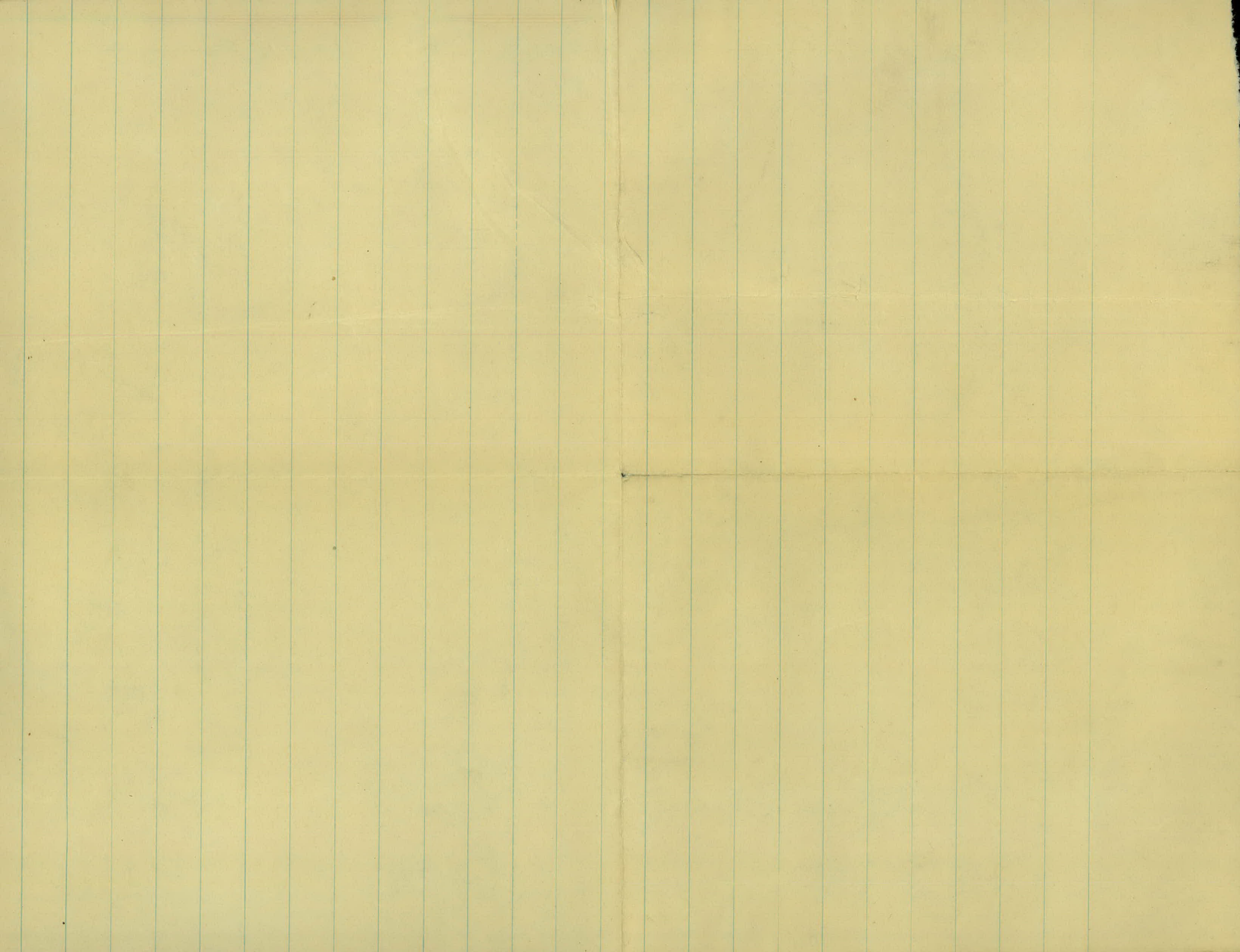
37

24 0

36

24 0

35



177-Rang Tied E.W. Fence

164-T.P. 19

158-P.R. 38

E 40'

105-T.P. 19

F-W 1'

163-P.R. 39
F-W 0

F-87

178-T.P. 24

150-29'

1-Wire Fence Cor. To 13/10

Pasture

Cult.

3791-P.O. St. F. Cor. 375
184-P.R. 42
162-T.P. 37

18x24'-E.W.
173-S.W. Cor. 63
170-12' Oak-18'
163-12' Oak-12'
18-T.P. 13

147-10' Oak-12
175-12' Oak-12
106-Ent.

197-F. Cor. 15

101-Beg F 375

182-Hedge 37
170-Ent.

Small Oaks

180 S-oaks

179-T.P. 28
127-N.E. Cor. 2-S.F-87
20 long
107-S.E. Cor. 2-S.F 89

176-P.R. 16

112-12' Oak-10
F-14'

174-End-F. 29'

163-12' Oak-15'

176 18' Oak-15

Scattered Oaks

13 7'

48

6 16

3 - 17'

47

4 - 17

494 - 12" X 32' D.P.

(7-20')

450 4 - 18

46

4-19

45

3 - 20

44

2 - 21

43

0 22

42

164-T.P. 21'

~~100-T.P.~~

111-T.P. 16'

176-T.P. 21'

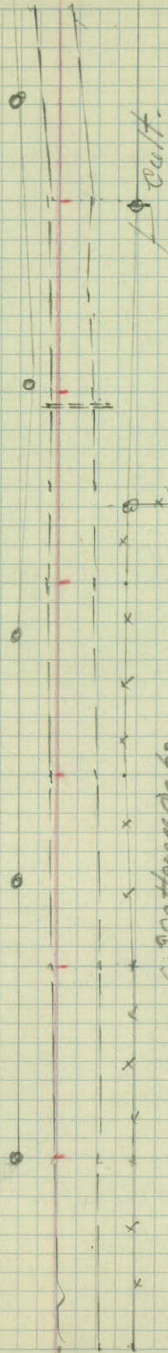
145-T.P. 21'

100-T.P. 20'

1-Wire Fence Bet. 75/100

Cut

Cut



Cut

1-Wire Fence
Bet Pa.P.

199-P.P. 38'

183-P.P. 25'

141-15" Oak-F cor
34 (B.M.)
F-35

195-12" Oak 29'

149-12" Oak 28'

147-12" Oak 30'

120-15" Oak 34'

115-P.P. 25'

F-36

Scattered de ds.
Pasture

152-8" Oak-32'

F-38

146-P.P. 37'

F-39

18-10

55

17 - 2

54

16 - 3

53

15 5

52

13 5

51

50

14 5

100
no oil

49

+69-RR 21

+63-T.P. 25

+71-RR 22

+69-T.P. 25

+64-T.P. 24

+67-RR 23

+10-T.P. 24

+69-RR 25

1-Wire dot. To Poles

6-To/Wires 7

2-Outer Wires

1-Wire dot. To Poles

Cut

Cut

Fence

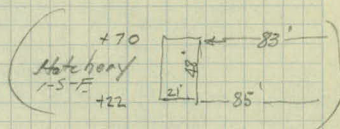
63

8-12'

+50 9-12'

62

13-9'



61

17-3

60

22-2

23'-3

59

23'-2

20-1

58

20-0

57

20' 0

56

+57-15' Ex. 21/24

+50-F 20

+35-T.P. 19'

F-24'

+97-14" Ex. Eld-26'

+70 N.E. cor. Ketcher -

+22-S. Cor. Ketcher - 25

+03- Bag Rows Trees 20'

F-27

+85-T.P. 26'

+84-12" Ex. 34 18-Bag F-28

+73-Ent.

+04 10' Elm 26'

+86-F. Cor. 33'

F-33'

+92-14" Ex. F-170'

+61-F. Cor. 34'

+80-Ent.

+42-T.P. 31

F-33'

+91-8" Tw. Birch- 40'

+73-F. Cor. 32

+81-T.P. 27'

+73-F. Cor. 28'

+10-T.P. 26'

+75-P.P. 34

Cult.

+Wire Bet To Pole

+84-P.P. 24'

+73-Ent. R

+48-6" Tw. Oak- 13'

+42-P.P. 14

Cult.

+67-P.P. 19'

+Wire Bet To Pole

Cult.

68

35-19

67

39'-21'

66

33'-16

65

21'-2'

+50 15 41

64

10-8

+50-8-12

63

62

F-8

179-6" Oak 2'
Last Tree

13

+21-Cor. Orch. 50

+03-T.P. 42

+04-15" Oak 7'

F-12

+82-Orchard. 45'

+60-ENT

+20-12-S.F. 120'

+05-10" Oak 55

F-14

+94-ENT

+58-T.P. 8'

+53-Tri. Oak 7'

+04-F. 45

+36-ENT

F-9

+97-20" Oak 0'

+75-15" Oak 1'

+34-15" Oak 2'

+08-F. Cor. 38

+03-T.P. 25

+50-F. 27'

F. 22'

+66-T.P. 21'

+50-F. 20

Cult.

Orchard

ENT.

Yard

ENT.

Cult.

+35-ENT

Cult.

Scattered oak

Pasture
Scattered
Oak.

+89-R.P. 0'

+24-R.P. 3'

E.W.

+22-F. Cor. 2'

+77-R.P. 23'

1-W/10 Bet 19/10/5

27-49

75

42-62

74

36-56'

73

20-40

72

0-22

71

16 5'

+80± 12" x 30' c.m. On Rt.

+52
0

70

27-6

69

$$\begin{array}{r}
 1607.35 \\
 5426.82 \\
 \hline
 2134.17
 \end{array}$$

$$\begin{array}{r}
 7740.3 \\
 9.97 \\
 \hline
 7730.33
 \end{array}$$

$$\begin{array}{r}
 1590.3 \\
 5426.82 \\
 \hline
 2117.12
 \end{array}$$

$$\begin{array}{r}
 98.2 \\
 234.9 \\
 814.0
 \end{array}$$

$$\begin{array}{r}
 860 \\
 15 \\
 \hline
 875
 \end{array}$$

$$\begin{array}{r}
 2.6 \\
 4.3 \\
 \hline
 6.9
 \end{array}$$

Sec. 1 - T 30-22

Stone Man. 90° 12' 81° 18' 1310 30 7620.6' Rec 7620.6' Rec 1590.30-PL 1607.35 90° 28' 90° 28' 90° 28'

1605.12 1600'

2925.45

2924.65

1316.8 1315.05 10683-R 10679.9 10664.85 2485 2482.0 164.4 164.4 197.4

1320.32 1316.1

2925

1818.74

Stone Man.

8131'

1315.6 1315.04 2000.0 Rec 7630.8 R 6148 2000.97

Mc 620.8 Stone Man.

1317.54 90° 16'

2925.45 2924.65 2925.45 2924.65 2925.45 2924.65

2000.97 2000.97 2000.97 2000.97 2000.97

2635.73

1317.54

R.R. 605.46 90° 11'

7635.6- Hdb. 7634.30-M 7633.7-R R.R. 1692

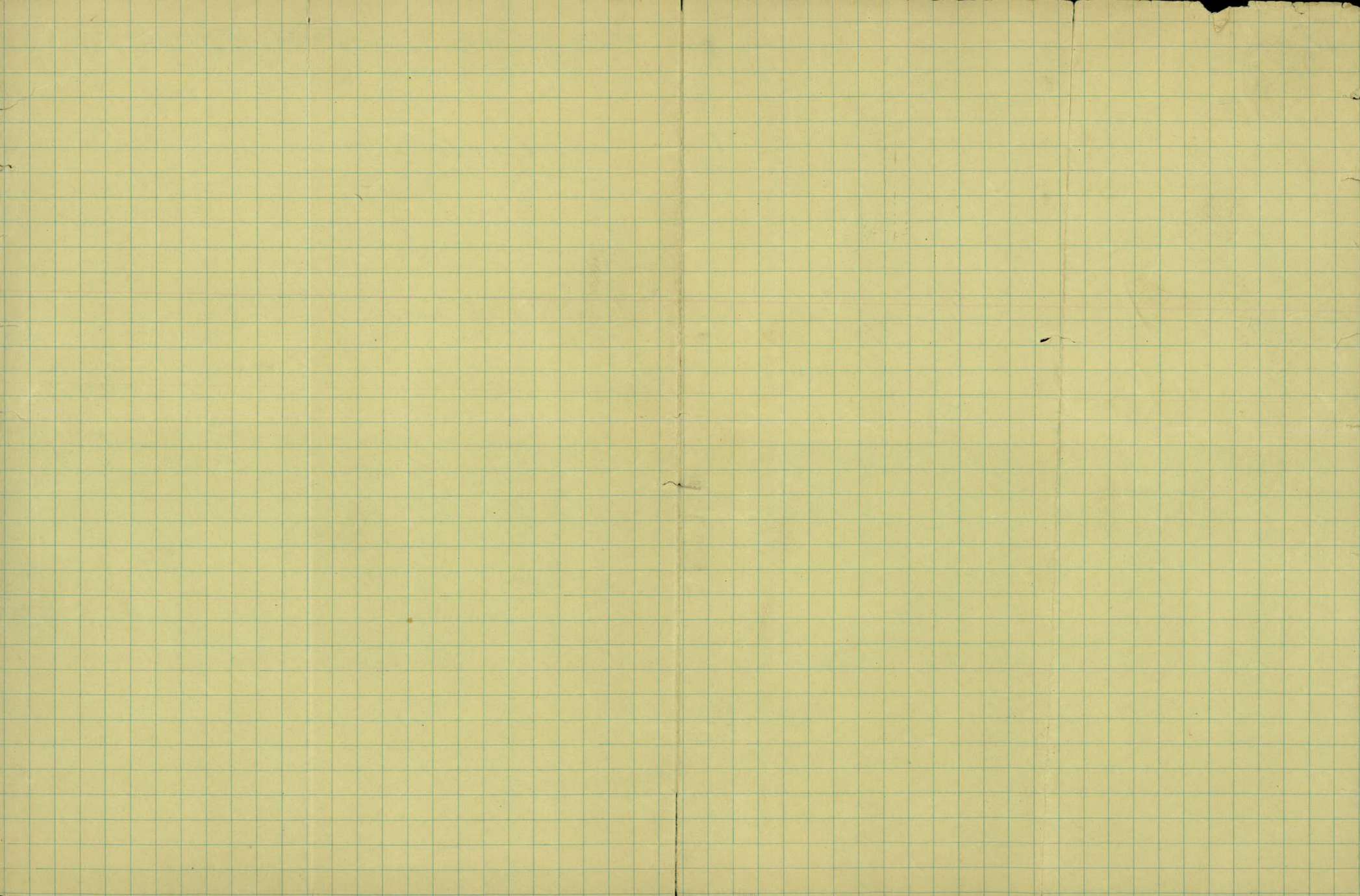
1317.15

1317.15

12" Oak 645.9 68.66 15.5'

68.66

15.5'



+13-T.O. 71'
F-69
+95-T.R. 32

+10-T.P. 21'
F-62
+98-P.P. 70

Cult.

F-47'

+13-T.P. 3'

F-27
+96-P.P. 39'

+16-T.P. 19'

F-10

+80
24

+79
5

Pasture

Cult.

F-1'

+60-T.P. 38'

+92-P.P. 10

82

81

80

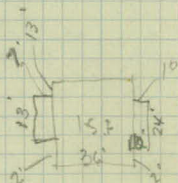
79

0-20

~~150~~ 6-15'

78

2-19'



77

11-20

76

+24-1" F. Cor. 2' -
2" F. on Line 2" W.
2' - 4'

Pasture.

F-12'

+80-F-11'

F-1

See Traverse
of Road P. 20

+70-F-5'

+50-2'

+30-F. Cor. 8'

F-13'

+35-T.P. 33'

F-24'

Ex. 10.

Chicken
Yard.

F-24'

+44-F. Cor. 17'

+13-ENT

+03-F. Cor. 25'

+00-24" Elm 19'
+52-6" H. 12'
+83-2" Spruce 20'

Road

+85-2" Rd. One East
+78-T.P. 54' Last P.
+67-P.P. 36

+71-14" E. Cor. Porch 47'
+47-6" Elm 10'
+45-5" E. Porch 47'
+37-24" Bx. El. 33'
+23-2" Spruce 12'
+17-Hedge
Cor.

774403

+92-15" Elm. 17'

+68-T.P. 45'

+57-8" Bx. El. 3'

Cult.

+03-18" Bx. El. 12'
+02-P.P. 60

89

88

87

86

85

84

83

F-3

16

+65-Δ in F. 3'

+53-Δ in F. 32

F-35

+63-Δ in F. 4'

F-2'

+75-10" oak 7'

F-2

+84-8" oak 4'
+66-8" oak 3'
+62-6" oak 4'
+47-12" oak 10'
+38-6" oak 12'

+4-6" oak 6'

F-1

+65-10" sp 2'

+33-70" sp 1'

Pasture -

Scattered oak Stps. west of Fence

Pasture -

Marsh

+83-24" oak 1'

F-2

F-3

40' - 22'

450 - 41 - 23'

96

36' - 16

95

9-9'

94

24 - 43

93

92

91

90

F-53'

F-16'

17

+52-T.P. 13
+50-F. 54

+50-7'

F-47'

F-21'

+57-Δ Fence 2'

+42-12' Oaks
129-T.P. 28

F-17'

F-24'

+21-Δ in Fence 0'

F-0

F-52'

Pasture.

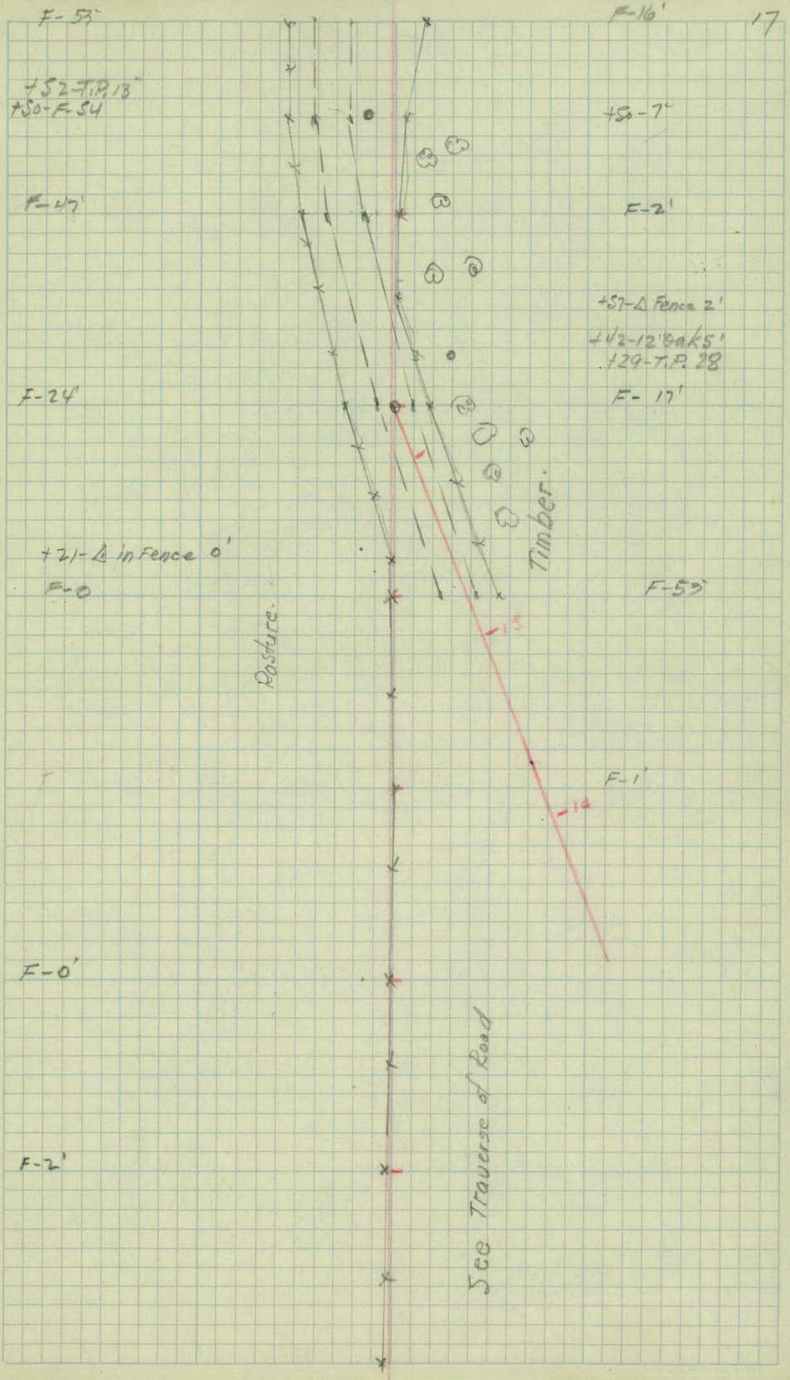
Timber.

F-1'

F-0'

F-2'

See Traverse of Road



$$\frac{46 + 16.75}{100 + 57.01}$$

157-5-14

100

4-15

+50 0-17

99

2-19

+50 5-5

98

18-2

+20 -31-14

97

W.H. Carlson

K. Anker.

L.B. Hendrix

A. Moeschler

Feb. 5, 1937

Ramsey Co

Wash Co

Cult.

Cult

+75-T.P. 23'

K4-F. Cor. 44'

+55-F. Cor 21'

+12-T.P. 76'

+55-End Fug

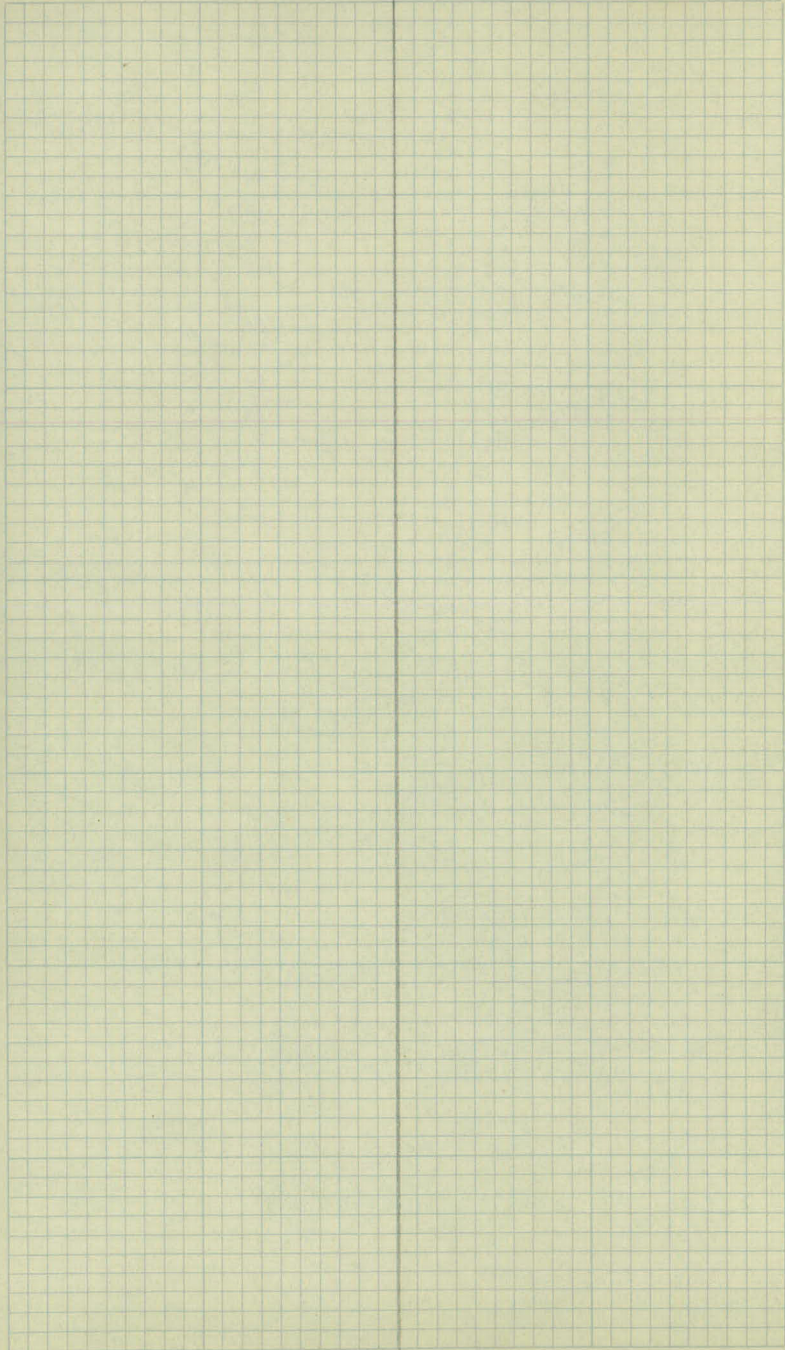
+45-Box Fug

timber

Ten on to 1 1/2 Cor.

K-7

F-21'



Traverse
of — Road

Sta. P.I. 79+43.12 to Sta. 95+00

Station	Point	angle.	
		Lt.	Rt.

15+79.6 = { Orig Line 95+00 P.O.T. }		20°-12'	
---	--	---------	--

14+00	P.I.	9°-48'	
-------	------	--------	--

10+00	P.I.	15°-00'	
-------	------	---------	--

3+00	P.I.	14°-30' d.	
------	------	------------	--

N-15°-09' W.

0+00 = (79+43.12 P.I.)		19°-00'	
------------------------	--	---------	--

W.H.C.

K.A. Mar. 5, 1927

L.B.H.

A.M.

P.C. 95+88.4

P.O.T. 95+00

N 90° 40' W

N 44° 39' W

N 29° 39' W

N 34° 09' W

19° 00'

N 50° 09' W

P.I. Sta. 79+43.12

Sta

+

T

-

Elev

Traverse of Road.

20-0

5

20-2

4

18-0

3

20-4

2

3 15

15 3 15

1

10 6

0

17.5 F
8.2

22
+91-S.W. Cr. Ho. 50'
+62-ET 76' Br. 33 1/4'
+52-P. Co. 8'

510

F-10'

440

F-8'

340

F-5'

+90- P.R. 10'

240

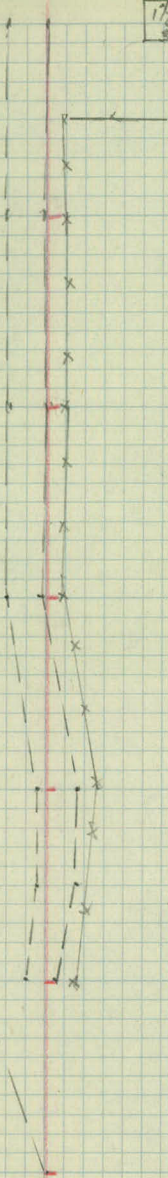
F-19'

P.T. 81+12.3

140

F-14'

at 00 = (79+43.12)



12

2-18

9-9

12

12 6'

13-68

11

12 9

10

9 10

150 0-20

9

0-20

8

9-9

7

14-2

6

F-16'

23

F-13'

Timber.

F-15'

+047. R. 18'

F-17

F-20'

+55 - F. Cor. 75'

+43 - T. R. 45'

+32 - P. R. 20'

429.6

16

15

10-10

14

2-17

2-20

13



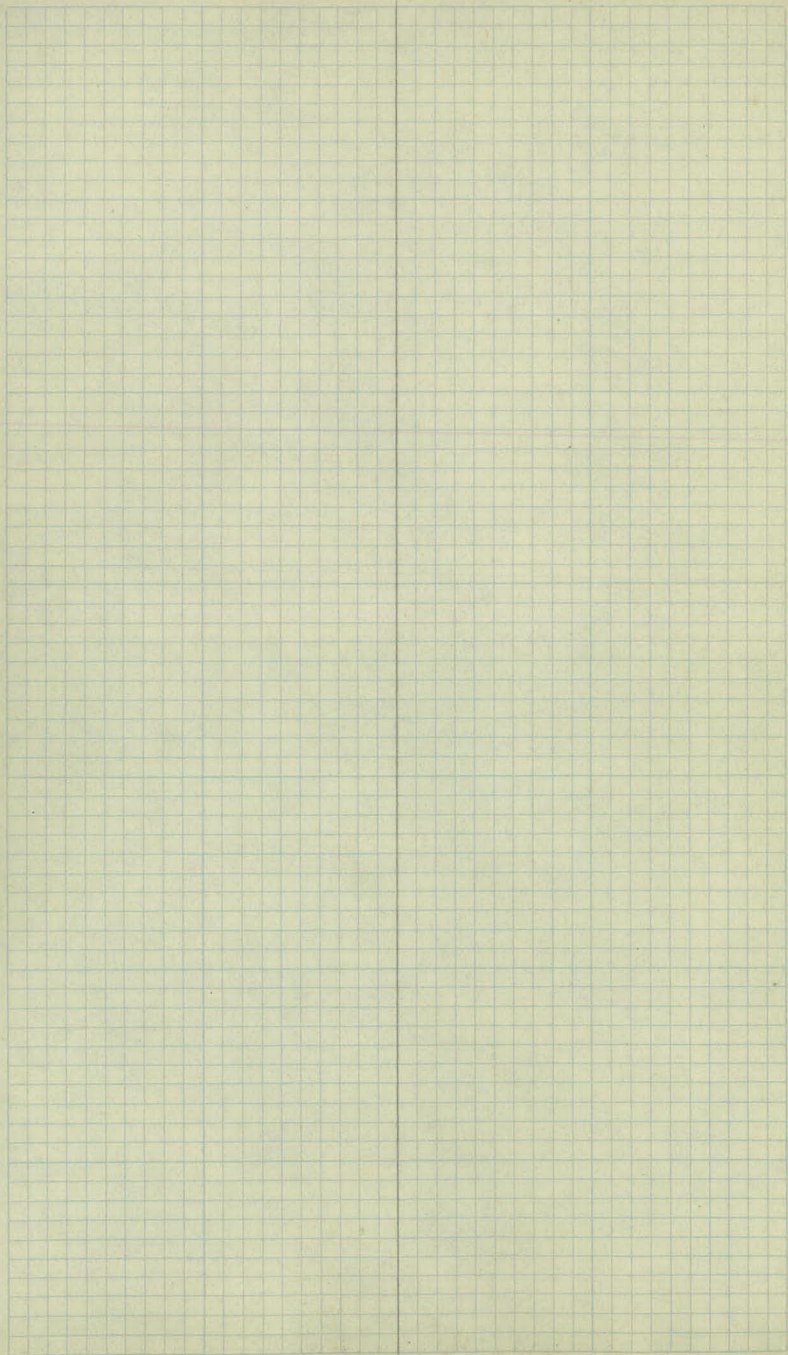
0

$F=19'$

$F=75'$

$F=70'$





Portland Ave.

Cross Section

{ Bratöger
Wilke
Gillen

Sta.	+	T	-	Elev.
B.M.	0.39	922.13		922.74
B.M.			11.55	921.58
	5.31	926.89		
22+00				923.7
+50				22.7
23				21.9
B.M.	6.31	922.89		921.58
23+50				21.8
+70				21.9
+78				21.9
+86				21.9
+96				22.2
24				22.3
+17	6.54	47		22.6

Lt.

E

Rt.

Spike in 14" Oak 60' Lt. Sta. 28+15
 { Top of E.E. Cor. of Headwall of 6' Conc. Box Cul.
 Sta. 22+75 @ Portland Ave. & 6th St.

$\frac{5^0}{50}$ $\frac{4^7}{48}$ $\frac{4^5}{16}$ $\frac{4^1}{11}$ $\frac{3^3}{6}$ $\frac{3^2}{/}$ $\frac{3^1}{8}$ $\frac{3^3}{12}$ $\frac{3^1}{31}$ $\frac{3^0}{37}$ $\frac{1^3}{45}$ $\frac{1^3}{50}$

$\frac{8^5}{50}$ $\frac{7^7}{23}$ $\frac{6^7}{13}$ $\frac{4^9}{7}$ $\frac{4^2}{/}$ $\frac{4^1}{9}$ $\frac{4^4}{22}$ $\frac{4^5}{28}$ $\frac{4^6}{39}$ $\frac{2^9}{50}$

$\frac{8^9}{50}$ $\frac{8^2}{19}$ $\frac{7^6}{12}$ $\frac{5^3}{5}$ $\frac{5^0}{/}$ $\frac{4^9}{6}$ $\frac{5^3}{21}$ $\frac{5^7}{29}$ $\frac{6^4}{37}$ $\frac{6^3}{50}$

$\frac{14^7}{60}$ $\frac{9^1}{38}$ $\frac{8^1}{16}$ $\frac{6^9}{9}$ $\frac{6^1}{/}$ $\frac{6^1}{8}$ $\frac{6^6}{21}$ $\frac{7^6}{26}$ $\frac{9^2}{29}$ $\frac{9^4}{50}$

$\frac{10^0}{60}$ $\frac{10^0}{50}$ $\frac{15^0}{38}$ $\frac{15^0}{30}$ $\frac{10^0}{16}$ $\frac{6^8}{10}$ $\frac{6^0}{/}$ $\frac{6^0}{7}$ $\frac{6^8}{20}$ $\frac{9^0}{26}$ $\frac{11^1}{38}$ $\frac{8^1}{43}$ $\frac{8^5}{50}$

$\frac{6^3}{50}$ $\frac{9^0}{42}$ $\frac{14^0}{22}$ $\frac{14^0}{10}$ $\frac{6^3}{10}$ $\frac{6^0}{/}$ $\frac{6^3}{21}$ $\frac{15^2}{21}$ $\frac{15^2}{50}$ 6' Conc.
Box
Cul.

$\frac{5^9}{50}$ $\frac{6^4}{29}$ $\frac{12^4}{22}$ $\frac{12^4}{20}$ $\frac{6^8}{11}$ $\frac{6^0}{/}$ $\frac{6^3}{21}$ $\frac{15^2}{21}$ $\frac{15^2}{50}$

$\frac{7^5}{50}$ $\frac{6^6}{23}$ $\frac{6^2}{14}$ $\frac{5^7}{/}$ $\frac{6^5}{20}$ $\frac{6^8}{26}$ $\frac{7^4}{50}$

$\frac{5^9}{50}$ $\frac{6^1}{44}$ $\frac{6^0}{17}$ $\frac{5^6}{/}$ $\frac{6^0}{19}$ $\frac{5^8}{45}$ $\frac{6^8}{50}$

$\frac{5^1}{100}$ $\frac{5^1}{50}$ $\frac{5^3}{/}$ $\frac{5^6}{17}$ $\frac{5^7}{27}$ $\frac{7^3}{50}$

Sta	+	7	-	Elev.
		927.89		
24+41				23.1
+50				23.1
25				23.9
T.P.			3.91	923.98 ✓
	10.28	934.26		
+50				25.0
26				26.2
+50				27.4
27				28.5
+50				29.5
28				30.9
B.M.	1.52	934.26	1.52	932.74 932.74
+50				32.4
T.P.			0.67	933.89 ✓
	9.14	944.73		

LT £ Rt

$\frac{5.3}{50}$ $\frac{5.4}{21}$ $\frac{4.8}{19}$ $\frac{5.2}{19}$ $\frac{5.6}{28}$ $\frac{6.2}{50}$

$\frac{1.2}{10}$ $\frac{1.3}{31}$ $\frac{5.1}{22}$ $\frac{5.3}{14}$ $\frac{4.8}{19}$ $\frac{5.0}{19}$ $\frac{5.1}{32}$ $\frac{4.5}{50}$

$\frac{0.4}{50}$ $\frac{0.9}{32}$ $\frac{4.2}{24}$ $\frac{4.7}{18}$ $\frac{4.1}{13}$ $\frac{4.0}{16}$ $\frac{4.2}{16}$ $\frac{3.3}{26}$ $\frac{2.5}{10}$

$\frac{7.0}{50}$ $\frac{7.2}{35}$ $\frac{9.7}{29}$ $\frac{9.6}{18}$ $\frac{9.5}{13}$ $\frac{9.3}{14}$ $\frac{9.7}{14}$ $\frac{9.1}{18}$ $\frac{8.1}{24}$ $\frac{7.5}{35}$ $\frac{6.0}{10}$

$\frac{9.1}{50}$ $\frac{8.4}{42}$ $\frac{8.1}{33}$ $\frac{9.0}{29}$ $\frac{8.7}{23}$ $\frac{8.0}{18}$ $\frac{8.4}{12}$ $\frac{8.1}{14}$ $\frac{8.5}{14}$ $\frac{6.6}{20}$ $\frac{6.0}{26}$ $\frac{5.1}{50}$

$\frac{7.5}{50}$ $\frac{6.4}{38}$ $\frac{6.8}{26}$ $\frac{7.4}{20}$ $\frac{7.3}{14}$ $\frac{7.4}{13}$ $\frac{5.6}{18}$ $\frac{5.3}{28}$ $\frac{4.7}{50}$

$\frac{8.5}{50}$ $\frac{8.3}{39}$ $\frac{7.3}{28}$ $\frac{6.6}{21}$ $\frac{6.1}{12}$ $\frac{5.8}{10}$ $\frac{6.1}{10}$ $\frac{5.9}{16}$ $\frac{5.3}{23}$ $\frac{5.7}{50}$

$\frac{7.6}{50}$ $\frac{7.2}{32}$ $\frac{6.5}{27}$ $\frac{5.4}{23}$ $\frac{5.2}{14}$ $\frac{5.0}{10}$ $\frac{5.8}{16}$ $\frac{6.6}{24}$ $\frac{5.6}{33}$ $\frac{5.4}{50}$

$\frac{4.5}{50}$ $\frac{4.7}{42}$ $\frac{5.1}{30}$ $\frac{4.2}{22}$ $\frac{3.9}{15}$ $\frac{3.4}{12}$ $\frac{3.8}{12}$ $\frac{6.2}{21}$ $\frac{6.2}{27}$ $\frac{5.2}{33}$ $\frac{4.7}{50}$

Spk. 60' Lt 28+15 14" Oak

$\frac{1.4}{50}$ $\frac{8.5}{38}$ $\frac{2.7}{33}$ $\frac{2.1}{21}$ $\frac{2.2}{14}$ $\frac{1.9}{14}$ $\frac{2.6}{14}$ $\frac{3.8}{20}$ $\frac{3.8}{27}$ $\frac{3.8}{10}$

Sta	+	π	-	Elev
29		948.73		33.8
+50				35.2
30				36.9
+50				38.3
T.P.			2.38	940.35
	11.31	951.66		
31				40.0
<u>225</u>	<u>Driveway</u>	<u>Rt.</u>		
+50				41.7
32				43.1
+50				44.8
33			Drive Rt	45.9
+50				46.6
34				46.7

$\frac{7.1}{50}$ $\frac{7.6}{36}$ $\frac{9.2}{27}$ $\frac{8.9}{20}$ $\frac{9.4}{16}$ $\frac{8.7}{6}$ $\frac{8.9}{8}$ $\frac{9.0}{13}$ $\frac{10.0}{20}$ $\frac{11.0}{29}$ $\frac{13.2}{10}$

$\frac{8.5}{50}$ $\frac{8.5}{43}$ $\frac{8.1}{34}$ $\frac{7.9}{26}$ $\frac{7.4}{20}$ $\frac{7.9}{17}$ $\frac{7.2}{8}$ $\frac{7.5}{10}$ $\frac{7.8}{10}$ $\frac{8.3}{13}$ $\frac{8.5}{17}$ $\frac{9.8}{24}$ $\frac{11.1}{36}$ $\frac{12.1}{10}$

$\frac{5.9}{50}$ $\frac{6.4}{41}$ $\frac{7.0}{32}$ $\frac{5.8}{25}$ $\frac{5.9}{21}$ $\frac{6.3}{17}$ $\frac{5.6}{7}$ $\frac{5.8}{11}$ $\frac{6.2}{11}$ $\frac{6.5}{15}$ $\frac{8.4}{21}$ $\frac{8.7}{30}$ $\frac{9.0}{50}$

$\frac{3.0}{50}$ $\frac{2.9}{36}$ $\frac{3.3}{26}$ $\frac{3.6}{22}$ $\frac{4.7}{18}$ $\frac{4.1}{7}$ $\frac{4.4}{7}$ $\frac{4.6}{7}$ $\frac{4.4}{11}$ $\frac{4.4}{18}$ $\frac{4.3}{22}$ $\frac{3.5}{50}$

$\frac{9.2}{50}$ $\frac{8.7}{41}$ $\frac{8.0}{29}$ $\frac{11.3}{22}$ $\frac{11.7}{17}$ $\frac{11.3}{8}$ $\frac{11.7}{7}$ $\frac{11.8}{7}$ $\frac{11.8}{11}$ $\frac{11.2}{11}$ $\frac{9.1}{19}$ $\frac{8.6}{22}$ $\frac{7.3}{25}$ $\frac{8.1}{50}$

941.0 941.0 941.0

$\frac{10.7}{10}$ $\frac{10.7}{10}$ $\frac{10.7}{100}$

$\frac{4.5}{50}$ $\frac{4.1}{35}$ $\frac{3.5}{24}$ $\frac{10.3}{20}$ $\frac{9.8}{8}$ $\frac{10.0}{6}$ $\frac{10.2}{6}$ $\frac{9.2}{9}$ $\frac{4.2}{20}$ $\frac{5.4}{50}$

$\frac{3.1}{50}$ $\frac{3.1}{33}$ $\frac{7.4}{26}$ $\frac{8.7}{19}$ $\frac{8.4}{9}$ $\frac{8.6}{5}$ $\frac{8.7}{5}$ $\frac{7.8}{9}$ $\frac{4.8}{11}$ $\frac{4.2}{26}$ $\frac{3.5}{46}$

$\frac{2.6}{50}$ $\frac{2.6}{32}$ $\frac{6.4}{23}$ $\frac{2.1}{19}$ $\frac{6.6}{10}$ $\frac{6.9}{10}$ $\frac{2.1}{10}$ $\frac{3.9}{17}$ $\frac{5.9}{50}$

$\frac{2.6}{50}$ $\frac{2.6}{35}$ $\frac{3.0}{28}$ $\frac{4.8}{25}$ $\frac{6.0}{19}$ $\frac{5.7}{13}$ $\frac{5.8}{6}$ $\frac{5.9}{6}$ $\frac{4.8}{12}$ $\frac{5.5}{26}$ $\frac{6.6}{50}$

$\frac{3.4}{50}$ $\frac{3.4}{38}$ $\frac{3.7}{29}$ $\frac{4.4}{25}$ $\frac{5.3}{20}$ $\frac{5.0}{13}$ $\frac{5.1}{6}$ $\frac{5.3}{6}$ $\frac{4.9}{10}$ $\frac{5.6}{18}$ $\frac{5.7}{35}$ $\frac{5.8}{50}$

$\frac{5.4}{50}$ $\frac{5.4}{39}$ $\frac{5.4}{29}$ $\frac{4.9}{23}$ $\frac{4.5}{11}$ $\frac{5.0}{6}$ $\frac{5.2}{6}$ $\frac{5.1}{10}$ $\frac{5.1}{13}$ $\frac{5.2}{17}$ $\frac{5.4}{50}$

Sta. + π - Elev.

951.66

34+36

Taylor Ave Lt. 946.76

+50

DRIVE Rt 946.96

T.P.

447

951.54

4.59

947.07

35

946.5

B.M.

419

951.75

3.98

947.56

+50

46.1

36

45.8

+50

45.0

+90

Driveway Lt.

45.0

37

44.3

+10

Driveway Rt.

44.3

+50

43.6

T.P. #1

8.66

942.09

981

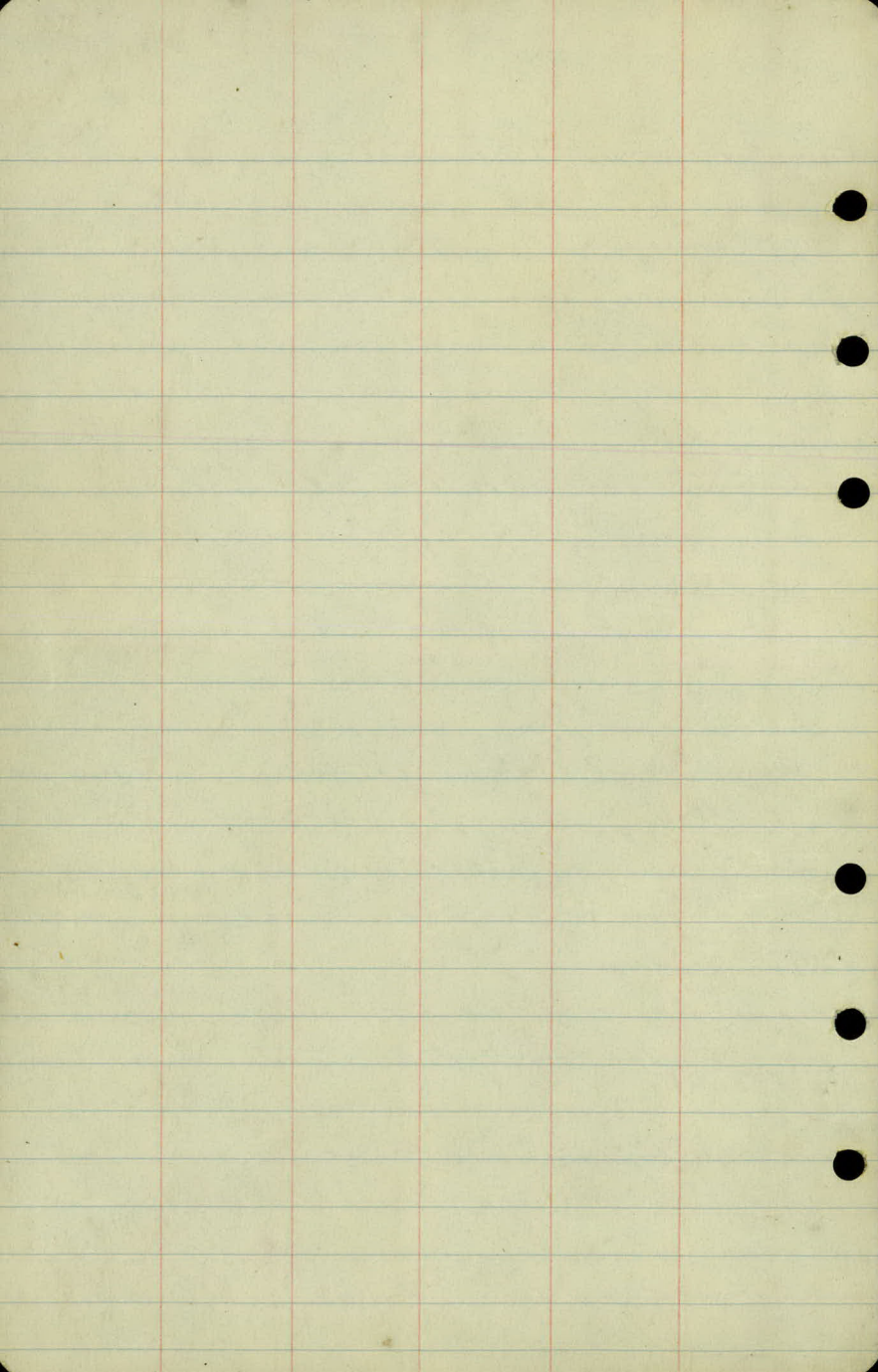
951.90

Spike in 14" Oak 60' Lt. Sta. 28+15

Spike in 14" Oak
Portland & Sea

~~Lt Sta~~

No. West Cor



lt L Rt

$$\frac{5.0}{100} \quad \frac{5.3}{50} \quad \frac{5.2}{38} \quad \frac{4.6}{70} \quad 4.9$$

$$\frac{5.3}{50} \quad \frac{5.3}{39} \quad \frac{5.0}{23} \quad \frac{4.6}{11} \quad 4.7 \quad \frac{4.4}{9} \quad \frac{5.2}{50}$$

$$\frac{4.0}{50} \quad \frac{4.0}{40} \quad \frac{5.0}{27} \quad \frac{5.0}{21} \quad \frac{4.5}{12} \quad 5.0 \quad \frac{4.6}{7} \quad \frac{4.3}{13} \quad \frac{4.8}{19} \quad \frac{5.2}{50}$$

$\frac{5.1}{57}$

Spike in 12" Oak 50' Rt. Stk. 36+90

$$\frac{4.4}{50} \quad \frac{4.2}{40} \quad \frac{4.4}{30} \quad \frac{5.4}{23} \quad \frac{5.1}{14} \quad 5.7 \quad \frac{5.4}{8} \quad \frac{5.4}{12} \quad \frac{5.3}{29} \quad \frac{5.2}{50}$$

$\frac{3.2}{57}$

$$\frac{5.0}{50} \quad \frac{5.2}{35} \quad \frac{5.8}{24} \quad \frac{6.5}{11} \quad 6.0 \quad \frac{5.4}{6} \quad \frac{5.2}{11} \quad \frac{5.2}{18} \quad \frac{5.4}{25} \quad \frac{5.8}{50}$$

$$\frac{6.3}{50} \quad \frac{6.2}{38} \quad \frac{6.0}{30} \quad \frac{6.5}{24} \quad \frac{5.9}{14} \quad 6.8 \quad \frac{5.8}{6} \quad \frac{5.4}{11} \quad \frac{5.0}{16} \quad \frac{5.7}{31} \quad \frac{6.3}{50}$$

$$\frac{6.3}{50}$$

$$\frac{6.8}{50}$$

$$\frac{8.2}{50} \quad \frac{7.8}{34} \quad \frac{7.4}{28} \quad \frac{7.4}{23} \quad \frac{6.8}{14} \quad 7.5 \quad \frac{7.2}{14} \quad \frac{7.2}{21} \quad \frac{8.1}{50}$$

$$\frac{7.5}{50}$$

$$\frac{8.1}{50}$$

$$\frac{8.5}{50} \quad \frac{8.5}{37} \quad \frac{8.0}{29} \quad \frac{8.5}{27} \quad \frac{8.2}{23} \quad \frac{7.5}{12} \quad 8.2 \quad \frac{8.2}{6} \quad \frac{6.4}{24} \quad \frac{8.9}{50}$$

Sta.	+	T	-	Elev.
38		952.90		43.1

+50				42.9
-----	--	--	--	------

39				41.7
----	--	--	--	------

+50				40.5
-----	--	--	--	------

T.P. #1	0.92	944.01		943.09	39.2
40+00					

+50				38.2
-----	--	--	--	------

41				37.0
----	--	--	--	------

+50				36.2
-----	--	--	--	------

42				36.1
----	--	--	--	------

+50				36.1
-----	--	--	--	------

43				36.0
----	--	--	--	------

+50				36.8
-----	--	--	--	------

T.P	4.98	942.15	6.84	937.17
-----	------	--------	------	--------

$\frac{12.4}{50}$ $\frac{10.3}{35}$ $\frac{9.6}{26}$ $\frac{9.6}{19}$ $\frac{9.2}{10}$ $\frac{9.8}{10}$ $\frac{9.3}{3}$ $\frac{8.2}{9}$ $\frac{6.8}{14}$ $\frac{6.6}{31}$ $\frac{6.2}{50}$

$\frac{10.1}{50}$ $\frac{7.4}{30}$ $\frac{8.0}{21}$ $\frac{10.3}{15}$ $\frac{10.0}{10}$ $\frac{10.5}{10}$ $\frac{6.9}{21}$ $\frac{5.8}{22}$ $\frac{4.8}{28}$ $\frac{4.9}{50}$

$\frac{7.5}{50}$ $\frac{8.0}{20}$ $\frac{8.0}{15}$ $\frac{9.8}{10}$ $\frac{11.4}{5}$ $\frac{11.2}{10}$ $\frac{11.0}{9}$ $\frac{11.6}{18}$ $\frac{10.9}{23}$ $\frac{7.2}{31}$ $\frac{5.5}{37}$ $\frac{5.5}{50}$

$\frac{13.5}{50}$ $\frac{11.5}{18}$ $\frac{11.1}{9}$ $\frac{11.5}{4}$ $\frac{12.4}{10}$ $\frac{12.0}{11}$ $\frac{12.5}{23}$ $\frac{11.5}{29}$ $\frac{10.2}{31}$ $\frac{8.4}{50}$

$\frac{6.2}{50}$ $\frac{4.6}{17}$ $\frac{4.6}{8}$ $\frac{4.6}{4}$ $\frac{4.6}{48}$ $\frac{4.0}{12}$ $\frac{4.4}{24}$ $\frac{4.0}{28}$ $\frac{3.4}{34}$ $\frac{2.2}{42}$ $\frac{2.2}{50}$

$\frac{9.3}{50}$ $\frac{8.8}{28}$ $\frac{8.0}{14}$ $\frac{6.8}{5}$ $\frac{6.0}{2}$ $\frac{5.8}{58}$ $\frac{5.2}{14}$ $\frac{5.4}{25}$ $\frac{6.2}{32}$ $\frac{6.2}{42}$ $\frac{6.0}{50}$

$\frac{11.7}{50}$ $\frac{11.4}{33}$ $\frac{10.4}{18}$ $\frac{9.3}{12}$ $\frac{7.0}{13}$ $\frac{6.1}{27}$ $\frac{6.7}{23}$ $\frac{7.4}{33}$ $\frac{9.0}{36}$ $\frac{9.4}{41}$ $\frac{10.2}{50}$

$\frac{12.2}{50}$ $\frac{12.3}{28}$ $\frac{12.4}{17}$ $\frac{11.6}{11}$ $\frac{7.8}{13}$ $\frac{6.7}{29}$ $\frac{7.0}{31}$ $\frac{8.0}{37}$ $\frac{8.2}{37}$ $\frac{9.2}{43}$ $\frac{8.7}{50}$

$\frac{12.8}{50}$ $\frac{12.8}{37}$ $\frac{12.5}{24}$ $\frac{12.3}{15}$ $\frac{12.0}{10}$ $\frac{7.9}{13}$ $\frac{7.4}{25}$ $\frac{8.0}{30}$ $\frac{8.4}{37}$ $\frac{8.8}{43}$ $\frac{8.6}{50}$

$\frac{11.8}{50}$ $\frac{10.5}{24}$ $\frac{10.4}{14}$ $\frac{9.7}{9}$ $\frac{8.3}{3}$ $\frac{7.9}{11}$ $\frac{7.6}{22}$ $\frac{9.0}{28}$ $\frac{9.4}{33}$ $\frac{9.3}{39}$ $\frac{9.4}{50}$

$\frac{12.4}{50}$ $\frac{11.7}{31}$ $\frac{10.7}{21}$ $\frac{10.3}{15}$ $\frac{9.3}{7}$ $\frac{8.0}{2}$ $\frac{7.3}{11}$ $\frac{7.8}{24}$ $\frac{7.9}{29}$ $\frac{8.1}{36}$ $\frac{8.0}{45}$ $\frac{7.5}{50}$

$\frac{10.7}{50}$ $\frac{9.6}{33}$ $\frac{8.7}{20}$ $\frac{8.3}{11}$ $\frac{7.6}{4}$ $\frac{7.2}{12}$ $\frac{6.8}{23}$ $\frac{7.1}{28}$ $\frac{7.0}{35}$ $\frac{6.3}{35}$ $\frac{4.8}{50}$

Sta	+	π	-	Elev
-----	---	-------	---	------

942.15

44				36.9
----	--	--	--	------

+50				36.9
-----	--	--	--	------

45				36.7
----	--	--	--	------

+50				36.7
-----	--	--	--	------

46				36.8
----	--	--	--	------

+50				37.1
-----	--	--	--	------

B.M.			4.01	938.14
------	--	--	------	--------

8.39 946.53

47				36.8
----	--	--	--	------

+50				37.7
-----	--	--	--	------

48				38.5
----	--	--	--	------

+50				39.4
-----	--	--	--	------

49				40.4
----	--	--	--	------

Lt

L

Rt

$$\frac{8.3}{50} \quad \frac{6.4}{20} \quad \frac{5.5}{15} \quad \frac{5.4}{9} \quad \frac{5.3}{5} \quad \frac{5.3}{5} \quad \frac{4.9}{10} \quad \frac{5.2}{21} \quad \frac{4.7}{20} \quad \frac{3.5}{34} \quad \frac{2.1}{37} \quad \frac{1.2}{50}$$

$$\frac{7.0}{50} \quad \frac{5.6}{17} \quad \frac{5.5}{11} \quad \frac{5.3}{6} \quad \frac{5.4}{3} \quad \frac{5.3}{5} \quad \frac{5.0}{11} \quad \frac{5.3}{21} \quad \frac{4.9}{25} \quad \frac{4.2}{28} \quad \frac{1.9}{50}$$

$$\frac{6.3}{50} \quad \frac{5.6}{25} \quad \frac{5.9}{19} \quad \frac{6.0}{11} \quad \frac{5.8}{6} \quad \frac{5.5}{5} \quad \frac{5.4}{8} \quad \frac{5.8}{20} \quad \frac{6.1}{25} \quad \frac{5.4}{29} \quad \frac{5.0}{41} \quad \frac{4.2}{50}$$

$$\frac{6.0}{50} \quad \frac{6.2}{22} \quad \frac{6.2}{15} \quad \frac{6.0}{10} \quad \frac{5.5}{5} \quad \frac{5.5}{5} \quad \frac{5.4}{9} \quad \frac{5.7}{21} \quad \frac{6.0}{25} \quad \frac{5.7}{50}$$

$$\frac{6.0}{50} \quad \frac{5.4}{21} \quad \frac{6.1}{18} \quad \frac{6.1}{13} \quad \frac{5.6}{7} \quad \frac{5.4}{5} \quad \frac{5.2}{8} \quad \frac{5.3}{20} \quad \frac{5.5}{24} \quad \frac{5.4}{30} \quad \frac{5.6}{33} \quad \frac{5.8}{50}$$

$$\frac{7.0}{50} \quad \frac{6.4}{22} \quad \frac{6.0}{15} \quad \frac{5.5}{9} \quad \frac{5.1}{5} \quad \frac{5.0}{7} \quad \frac{5.2}{19} \quad \frac{6.1}{27} \quad \frac{6.1}{33} \quad \frac{6.3}{50}$$

Spike in 18" Oak 34' Rt 510, 46 + 41

$$\frac{13.6}{50} \quad \frac{11.6}{16} \quad \frac{10.8}{14} \quad \frac{10.0}{3} \quad \frac{9.7}{5} \quad \frac{9.1}{9} \quad \frac{9.1}{18} \quad \frac{10.4}{20} \quad \frac{11.6}{50}$$

$$\frac{13.7}{30} \quad \frac{10.8}{19} \quad \frac{10.2}{14} \quad \frac{9.7}{10} \quad \frac{9.1}{4} \quad \frac{8.8}{5} \quad \frac{8.4}{10} \quad \frac{8.6}{20} \quad \frac{10.0}{23} \quad \frac{11.1}{33} \quad \frac{11.2}{50}$$

$$\frac{11.0}{50} \quad \frac{9.7}{20} \quad \frac{8.6}{16} \quad \frac{8.5}{10} \quad \frac{8.3}{6} \quad \frac{8.0}{5} \quad \frac{7.9}{8} \quad \frac{7.9}{16} \quad \frac{8.2}{23} \quad \frac{8.9}{33} \quad \frac{8.7}{50}$$

$$\frac{8.1}{50} \quad \frac{7.1}{31} \quad \frac{6.4}{21} \quad \frac{7.9}{16} \quad \frac{7.3}{9} \quad \frac{7.1}{5} \quad \frac{6.9}{11} \quad \frac{6.1}{15} \quad \frac{5.7}{21} \quad \frac{6.2}{26} \quad \frac{6.1}{50}$$

$$\frac{6.1}{50} \quad \frac{5.0}{29} \quad \frac{5.5}{21} \quad \frac{5.7}{17} \quad \frac{6.3}{14} \quad \frac{6.1}{5} \quad \frac{6.1}{8} \quad \frac{5.3}{10} \quad \frac{4.7}{14} \quad \frac{4.7}{16} \quad \frac{4.1}{38} \quad \frac{3.7}{50}$$

Sta	+	π	-	Elev
		946.53		
T.P.	9.22	951.64	4.11	942.42
49+50				41.5
50				42.4
+50				43.1
51				44.0
+50				44.8
52				45.4
+50				46.4
53				47.7
T.P.	9.03	958.17	2.50	949.14
+50				48.8
54				49.6
+50				50.3

wt

Rt

Rt

$$\frac{10.5}{50} \quad \frac{8.8}{30} \quad \frac{9.0}{23} \quad \frac{10.1}{18} \quad \frac{10.4}{15} \quad \frac{10.1}{6} \quad \frac{10.1}{1} \quad \frac{10.0}{8} \quad \frac{9.5}{10} \quad \frac{8.6}{14} \quad \frac{8.0}{19} \quad \frac{7.2}{25} \quad \frac{6.3}{50}$$

$$\frac{9.8}{50} \quad \frac{7.7}{27} \quad \frac{8.0}{21} \quad \frac{9.0}{17} \quad \frac{9.5}{14} \quad \frac{9.2}{1} \quad \frac{9.4}{8} \quad \frac{7.7}{15} \quad \frac{6.8}{25} \quad \frac{4.8}{29} \quad \frac{3.5}{50}$$

$$\frac{8.5}{50} \quad \frac{6.5}{31} \quad \frac{5.4}{25} \quad \frac{7.2}{21} \quad \frac{8.5}{16} \quad \frac{8.6}{14} \quad \frac{8.2}{6} \quad \frac{8.5}{1} \quad \frac{8.7}{9} \quad \frac{8.0}{10} \quad \frac{6.9}{15} \quad \frac{6.0}{21} \quad \frac{4.4}{29} \quad \frac{2.9}{32} \quad \frac{2.0}{50}$$

$$\frac{6.7}{50} \quad \frac{3.6}{25} \quad \frac{5.4}{21} \quad \frac{7.4}{18} \quad \frac{7.5}{15} \quad \frac{7.4}{5} \quad \frac{7.6}{1} \quad \frac{7.6}{8} \quad \frac{7.0}{10} \quad \frac{5.4}{17} \quad \frac{4.1}{27} \quad \frac{2.1}{32} \quad \frac{0.9}{50}$$

$$\frac{6.3}{50} \quad \frac{4.0}{29} \quad \frac{3.9}{24} \quad \frac{6.4}{17} \quad \frac{6.8}{15} \quad \frac{6.7}{6} \quad \frac{6.8}{1} \quad \frac{6.6}{7} \quad \frac{5.3}{9} \quad \frac{3.8}{17} \quad \frac{3.8}{21} \quad \frac{1.2}{28} \quad \frac{0.2}{50}$$

$$\frac{5.1}{50} \quad \frac{3.6}{26} \quad \frac{4.5}{20} \quad \frac{6.0}{15} \quad \frac{6.2}{1} \quad \frac{6.2}{6} \quad \frac{5.3}{8} \quad \frac{2.7}{20} \quad \frac{1.2}{50}$$

$$\frac{5.2}{50} \quad \frac{4.0}{29} \quad \frac{3.7}{21} \quad \frac{5.2}{18} \quad \frac{5.0}{16} \quad \frac{4.8}{7} \quad \frac{5.2}{1} \quad \frac{5.4}{6} \quad \frac{3.3}{9} \quad \frac{2.8}{19} \quad \frac{2.7}{26} \quad \frac{2.3}{50}$$

$$\frac{6.0}{50} \quad \frac{4.8}{29} \quad \frac{4.2}{21} \quad \frac{4.0}{16} \quad \frac{3.9}{7} \quad \frac{3.9}{1} \quad \frac{3.9}{5} \quad \frac{2.8}{8} \quad \frac{2.5}{15} \quad \frac{2.4}{50}$$

$$\frac{12.6}{50} \quad \frac{10.8}{26} \quad \frac{10.3}{20} \quad \frac{9.9}{17} \quad \frac{9.4}{8} \quad \frac{9.4}{1} \quad \frac{9.3}{5} \quad \frac{8.7}{7} \quad \frac{8.7}{14} \quad \frac{8.6}{24} \quad \frac{8.2}{50}$$

$$\frac{11.7}{50} \quad \frac{9.7}{21} \quad \frac{9.3}{17} \quad \frac{8.7}{8} \quad \frac{8.6}{1} \quad \frac{8.4}{5} \quad \frac{7.7}{8} \quad \frac{7.7}{15} \quad \frac{7.6}{34} \quad \frac{7.1}{50}$$

$$\frac{11.4}{50} \quad \frac{10.0}{27} \quad \frac{8.8}{21} \quad \frac{8.6}{17} \quad \frac{8.0}{9} \quad \frac{7.9}{1} \quad \frac{7.9}{3} \quad \frac{7.1}{6} \quad \frac{7.0}{16} \quad \frac{6.3}{50}$$

Sta.	+	π	-	Elev.
		958.17		
55				51.0
+50				52.0
56				53.0
T.P.	13.55	968.09	3.63	954.54
+50				54.3
57				55.5
T.P.	4.90	970.67	2.37	965.77
B.M.	8.65	970.67	8.65	962.02
+50				57.2
58				58.5
+50				59.5
59				61.2

Lt.

L.

Rt.

$$\frac{11.0}{50} \quad \frac{8.7}{26} \quad \frac{8.1}{20} \quad \frac{7.5}{11} \quad \frac{7.2}{4} \quad \frac{7.2}{7} \quad \frac{6.4}{14} \quad \frac{6.4}{14} \quad \frac{6.2}{22} \quad \frac{5.4}{50}$$

$$\frac{10.1}{50} \quad \frac{7.2}{29} \quad \frac{6.7}{21} \quad \frac{6.1}{10} \quad \frac{6.2}{4} \quad \frac{6.2}{4} \quad \frac{5.2}{6} \quad \frac{4.7}{14} \quad \frac{4.6}{21} \quad \frac{4.3}{50}$$

$$\frac{8.8}{50} \quad \frac{6.0}{28} \quad \frac{5.5}{23} \quad \frac{5.6}{19} \quad \frac{4.9}{9} \quad \frac{5.2}{3} \quad \frac{5.2}{3} \quad \frac{3.6}{9} \quad \frac{3.5}{11} \quad \frac{3.0}{21} \quad \frac{1.9}{50}$$

$$\frac{3.3}{37}$$

$$\frac{17.0}{50} \quad \frac{14.5}{29} \quad \frac{14.0}{23} \quad \frac{14.0}{19} \quad \frac{13.5}{9} \quad \frac{13.8}{4} \quad \frac{12.5}{4} \quad \frac{11.6}{10} \quad \frac{10.8}{20} \quad \frac{9.1}{50}$$

$$\frac{15.0}{50} \quad \frac{12.5}{32} \quad \frac{12.0}{25} \quad \frac{12.5}{21} \quad \frac{12.1}{10} \quad \frac{12.6}{4} \quad \frac{11.4}{8} \quad \frac{10.2}{14} \quad \frac{9.6}{14} \quad \frac{9.3}{25} \quad \frac{7.9}{50}$$

Not in Tol. Pk. Rt. Sta. 59+50

Top of N.E. Bolt on 925 pump Sta. 60+95 Lt. 45'

$$\frac{14.0}{50} \quad \frac{13.4}{30} \quad \frac{13.4}{23} \quad \frac{13.6}{20} \quad \frac{13.3}{8} \quad \frac{13.5}{3} \quad \frac{13.1}{6} \quad \frac{11.8}{6} \quad \frac{11.3}{13} \quad \frac{11.0}{22} \quad \frac{9.6}{50}$$

$$\frac{12.7}{50} \quad \frac{11.3}{31} \quad \frac{11.5}{29} \quad \frac{11.8}{23} \quad \frac{11.2}{19} \quad \frac{11.9}{9} \quad \frac{11.2}{4} \quad \frac{11.5}{4} \quad \frac{10.6}{6} \quad \frac{10.1}{14} \quad \frac{9.9}{20} \quad \frac{8.2}{50}$$

$$\frac{11.2}{50} \quad \frac{10.2}{33} \quad \frac{9.8}{29} \quad \frac{10.2}{25} \quad \frac{11.0}{21} \quad \frac{10.8}{11} \quad \frac{11.2}{3} \quad \frac{8.9}{9} \quad \frac{8.5}{9} \quad \frac{7.6}{17} \quad \frac{5.9}{50}$$

$$\frac{11.1}{50} \quad \frac{9.7}{35} \quad \frac{9.7}{28} \quad \frac{10.5}{24} \quad \frac{10.0}{13} \quad \frac{10.0}{1} \quad \frac{9.5}{4} \quad \frac{8.4}{4} \quad \frac{7.7}{9} \quad \frac{7.0}{17} \quad \frac{4.8}{50}$$

Sta	+	↑	-	Elev
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970.67

59+50

60.8

60

60.7

+50

60.3

+70

Driveway Lt.

60.1

61

59.1

+50

57.8

T.P.

3.93

965.95

8.65

967.07

62

56.1

+50

54.5

63

52.3

T.P.

3.91

958.09

11.77

954.18

+50

50.0

Lt.

L

Rt.

$$\frac{10.1}{50} \quad \frac{10.0}{29} \quad \frac{9.8}{24} \quad \frac{9.5}{13} \quad \frac{9.8}{7} \quad \frac{9.9}{1} \quad \frac{8.4}{3} \quad \frac{6.5}{9} \quad \frac{6.0}{15} \quad \frac{5.5}{17} \quad \frac{4.0}{50}$$

$$\frac{9.0}{50} \quad \frac{10.1}{27} \quad \frac{9.5}{24} \quad \frac{9.5}{17} \quad \frac{10.0}{5} \quad \frac{8.6}{8} \quad \frac{6.1}{11} \quad \frac{6.4}{19} \quad \frac{5.0}{50}$$

$$\frac{8.5}{50} \quad \frac{8.2}{32} \quad \frac{9.4}{29} \quad \frac{10.3}{20} \quad \frac{10.0}{10} \quad \frac{10.4}{1} \quad \frac{10.4}{5} \quad \frac{9.6}{8} \quad \frac{8.2}{12} \quad \frac{7.2}{23} \quad \frac{6.2}{50}$$

$$\frac{9.3}{10} \quad \frac{9.8}{21} \quad \frac{10.6}{1}$$

$$\frac{9.1}{50} \quad \frac{9.6}{26} \quad \frac{11.8}{21} \quad \frac{11.6}{17} \quad \frac{11.3}{7} \quad \frac{11.6}{1} \quad \frac{11.8}{4} \quad \frac{10.7}{10} \quad \frac{9.4}{14} \quad \frac{7.8}{23} \quad \frac{7.1}{50}$$

$$\frac{10.9}{50} \quad \frac{10.2}{48} \quad \frac{9.6}{25} \quad \frac{12.5}{21} \quad \frac{13.3}{17} \quad \frac{12.9}{7} \quad \frac{12.9}{1} \quad \frac{12.9}{6} \quad \frac{13.3}{10} \quad \frac{10.4}{16} \quad \frac{7.8}{28} \quad \frac{6.9}{31} \quad \frac{7.4}{50}$$

$$\frac{7.1}{50} \quad \frac{6.0}{31} \quad \frac{5.5}{22} \quad \frac{9.4}{18} \quad \frac{10.4}{12} \quad \frac{9.9}{5} \quad \frac{9.9}{1} \quad \frac{10.4}{8} \quad \frac{10.8}{12} \quad \frac{9.8}{15} \quad \frac{7.2}{19} \quad \frac{5.0}{26} \quad \frac{3.3}{32} \quad \frac{4.1}{50}$$

$$\frac{8.3}{50} \quad \frac{7.8}{20} \quad \frac{12.4}{13} \quad \frac{11.9}{10} \quad \frac{11.5}{1} \quad \frac{12.1}{12} \quad \frac{12.6}{16} \quad \frac{10.6}{20} \quad \frac{8.9}{26} \quad \frac{7.7}{31} \quad \frac{6.8}{32} \quad \frac{7.8}{50}$$

$$\frac{9.7}{50} \quad \frac{9.3}{20} \quad \frac{12.8}{14} \quad \frac{14.0}{9} \quad \frac{13.7}{1} \quad \frac{14.1}{14} \quad \frac{14.4}{16} \quad \frac{13.5}{23} \quad \frac{11.7}{32} \quad \frac{10.1}{35} \quad \frac{11.2}{50}$$

$$\frac{3.4}{50} \quad \frac{2.4}{23} \quad \frac{4.2}{20} \quad \frac{8.6}{11} \quad \frac{8.3}{9} \quad \frac{8.1}{1} \quad \frac{8.6}{14} \quad \frac{8.6}{16} \quad \frac{8.6}{20} \quad \frac{8.4}{24} \quad \frac{6.7}{32} \quad \frac{5.3}{31} \quad \frac{6.5}{50}$$

Sta.	+	π	-	Elev.
		958.09		
64				48.0
+50				45.8
T.P.	2.10	951.03	9.16	948.93.
B.M.	11.17	951.03	11.17	939.86
65				43.3
+22		Lane Lt.		
+50				41.4
66				39.1
T.P.	3.63	943.49	11.17	939.86
+50				35.1
67				
67		Drive Lt		33.6

Lt

E

Rt

$$\frac{5.8}{50} \quad \frac{5.6}{24} \quad \frac{6.8}{21} \quad \frac{10.7}{15} \quad \frac{10.2}{11} \quad \frac{10.1}{11} \quad \frac{10.5}{11} \quad \frac{10.0}{13} \quad \frac{9.2}{17} \quad \frac{8.7}{23} \quad \frac{9.0}{32} \quad \frac{10.4}{50}$$

$$\frac{9.8}{50} \quad \frac{9.4}{40} \quad \frac{9.9}{26} \quad \frac{12.5}{19} \quad \frac{12.6}{16} \quad \frac{12.1}{7} \quad \frac{12.3}{7} \quad \frac{12.6}{7} \quad \frac{12.5}{12} \quad \frac{12.2}{20} \quad \frac{12.5}{26} \quad \frac{14.5}{50}$$

Spoke in 12" Oak 65' Rt. 512. 65 + 22

$$\frac{5.8}{50} \quad \frac{6.8}{33} \quad \frac{7.7}{27} \quad \frac{7.3}{22} \quad \frac{7.1}{14} \quad \frac{7.7}{3} \quad \frac{7.7}{4} \quad \frac{7.5}{8} \quad \frac{6.4}{13} \quad \frac{6.1}{13} \quad \frac{10.0}{50}$$

$$\frac{6.5}{50} \quad \frac{7.1}{25} \quad \frac{7.8}{25}$$

$$\frac{8.8}{50} \quad \frac{8.8}{27} \quad \frac{9.0}{30} \quad \frac{8.7}{19} \quad \frac{8.9}{14} \quad \frac{9.3}{7} \quad \frac{9.6}{9} \quad \frac{10.1}{17} \quad \frac{11.8}{50}$$

$$\frac{10.0}{50} \quad \frac{10.7}{41} \quad \frac{10.7}{34} \quad \frac{10.5}{26} \quad \frac{10.9}{16} \quad \frac{11.0}{13} \quad \frac{11.3}{9} \quad \frac{11.9}{24} \quad \frac{13.2}{24} \quad \frac{14.7}{20}$$

$$\frac{4.4}{50} \quad \frac{5.1}{43} \quad \frac{5.2}{38} \quad \frac{4.7}{29} \quad \frac{4.9}{20} \quad \frac{5.1}{18} \quad \frac{5.3}{15} \quad \frac{7.1}{11} \quad \frac{8.4}{21} \quad \frac{9.8}{21} \quad \frac{11.5}{50}$$

$$\frac{3.5}{100} \quad \frac{6.3}{50} \quad \frac{6.6}{29} \quad \frac{7.0}{21} \quad \frac{7.1}{18} \quad \frac{9.3}{15} \quad \frac{9.7}{9} \quad \frac{9.9}{9.9} \quad \frac{11.6}{29} \quad \frac{12.8}{50}$$

Sta + π - Elev.

943.49

67+50

Drive L+32.6

T.P.

68

30.7

T.P. 4.28 936.20 11.57 931.92✓

+50

28.6

69

26.9

T.P. 4.40 931.31 9.29 926.91.

+50

25.6

70

24.3

+50

25.5

+80 Cdr. Drains East (Buried in Ice) Corr. L.P.

71

25.6

+50

25.4

72

25.4

Lt

L

Rt

 $\frac{6.4}{100}$
 $\frac{8.0}{50} \frac{8.3}{39} \frac{8.4}{29} \frac{8.8}{20} \frac{9.1}{17} \frac{9.9}{14} \frac{10.6}{10} 10.9 \frac{12.5}{33} \frac{13.3}{50}$
 $\frac{10.1}{50} \frac{9.9}{42} \frac{10.6}{39} \frac{10.6}{36} \frac{10.2}{29} \frac{10.5}{18} \frac{11.0}{14} \frac{11.9}{8} \frac{12.8}{37} \frac{14.7}{50} \frac{15.7}{50}$
 $\frac{5.9}{50} \frac{5.8}{47} \frac{5.3}{41} \frac{5.1}{38} \frac{4.8}{25} \frac{5.0}{14} \frac{5.7}{12} \frac{6.7}{9} 7.6 \frac{9.9}{26} \frac{12.4}{50}$
 $\frac{7.6}{50} \frac{7.4}{43} \frac{7.1}{39} \frac{6.6}{36} \frac{6.1}{21} \frac{6.6}{11} \frac{8.0}{8} 9.3 \frac{12.6}{25} \frac{15.3}{50}$
 $\frac{4.3}{50} \frac{4.1}{44} \frac{3.8}{38} \frac{3.2}{30} \frac{2.7}{19} \frac{2.3}{9} \frac{4.3}{7} \frac{5.0}{5} \frac{6.7}{5} \frac{10.2}{25} \frac{10.6}{50}$
 $\frac{2.6}{50} \frac{5.4}{35} \frac{4.2}{30} \frac{4.0}{15} \frac{4.8}{4} \frac{2.0}{1} \frac{7.0}{1} \frac{10.4}{30} \frac{11.1}{50}$
 $\frac{6.6}{50} \frac{6.2}{34} \frac{5.7}{26} \frac{5.0}{14} \frac{5.8}{3} \frac{7.5}{10} \frac{9.4}{43} \frac{10.9}{43} \frac{11.0}{50}$
 $\frac{6.7}{50} \frac{6.9}{41} \frac{6.9}{25} \frac{5.8}{19} \frac{5.7}{19} \frac{6.3}{7} \frac{8.2}{11} \frac{9.4}{15} \frac{10.8}{50}$
 $\frac{6.1}{50} \frac{6.4}{36} \frac{6.5}{17} \frac{6.1}{14} \frac{6.9}{15} \frac{6.4}{15} \frac{8.1}{17} \frac{9.1}{21} \frac{10.5}{41} \frac{10.8}{50}$
 $\frac{5.4}{50} \frac{6.1}{21} \frac{6.1}{11} \frac{5.9}{12} \frac{5.7}{12} \frac{6.4}{24} \frac{8.3}{27} \frac{10.0}{35} \frac{10.5}{50}$

Sta	+	π	-	Elev.
		931.31		
72+50				25.3
73				25.5
+50				25.9
74				27.0
T.P.	11.90	938.50	4.71	926.60
+50				28.1
75				29.2
+50				30.2
76				31.3
B.M.	3.78	941.03	1.25	937.25
B.M.	1.60	941.03	1.60	939.43
+50				32.7

Lt R

$\frac{4.5}{50}$	$\frac{5.7}{24}$	$\frac{6.1}{8}$	$\frac{6.0}{8}$	$\frac{5.8}{5}$	$\frac{5.6}{9}$	$\frac{5.7}{20}$	$\frac{6.3}{34}$	$\frac{8.0}{37}$	$\frac{9.2}{50}$
$\frac{4.1}{50}$	$\frac{5.2}{25}$		$\frac{5.8}{8}$	$\frac{5.9}{7}$	$\frac{5.8}{12}$	$\frac{5.5}{18}$	$\frac{5.4}{30}$	$\frac{6.0}{42}$	$\frac{7.6}{47}$
$\frac{3.7}{50}$	$\frac{4.6}{28}$	$\frac{5.2}{9}$	$\frac{5.4}{8}$	$\frac{5.5}{12}$	$\frac{5.3}{18}$	$\frac{5.3}{23}$	$\frac{5.3}{26}$	$\frac{5.2}{38}$	$\frac{5.7}{50}$
$\frac{2.3}{50}$	$\frac{3.4}{24}$		$\frac{4.3}{8}$	$\frac{4.5}{13}$	$\frac{4.7}{21}$	$\frac{4.7}{27}$	$\frac{5.0}{34}$	$\frac{4.7}{41}$	$\frac{5.1}{55}$

$\frac{7.9}{50}$	$\frac{9.8}{110}$	$\frac{10.4}{8}$	$\frac{10.8}{16}$	$\frac{10.9}{24}$	$\frac{11.1}{31}$	$\frac{11.6}{39}$	$\frac{11.5}{50}$	$\frac{13.2}{61}$	$\frac{14.0}{64}$
$\frac{6.8}{50}$	$\frac{8.6}{21}$	$\frac{9.3}{8}$	$\frac{9.8}{18}$	$\frac{10.3}{29}$	$\frac{10.1}{35}$	$\frac{10.8}{41}$	$\frac{10.4}{50}$	$\frac{11.1}{63}$	$\frac{12.1}{68}$
$\frac{6.0}{50}$	$\frac{7.7}{16}$	$\frac{8.3}{8}$	$\frac{8.6}{16}$	$\frac{8.8}{23}$	$\frac{9.0}{29}$	$\frac{9.6}{34}$	$\frac{9.4}{47}$	$\frac{9.6}{60}$	$\frac{9.5}{65}$
$\frac{4.5}{50}$	$\frac{6.5}{14}$	$\frac{7.2}{8}$	$\frac{6.3}{7}$	$\frac{6.9}{17}$	$\frac{8.6}{23}$	$\frac{9.4}{27}$	$\frac{8.8}{39}$	$\frac{8.8}{50}$	$\frac{8.3}{52}$

Spikes in 24" Elev. Lt. 5th.

N.E. Cor of Porch - Water table 30' Lt. 5th. 77+71

$\frac{7.4}{50}$	$\frac{8.2}{20}$	$\frac{8.3}{8}$	$\frac{8.7}{8}$	$\frac{8.8}{11}$	$\frac{10.6}{15}$	$\frac{10.8}{18}$	$\frac{10.5}{29}$	$\frac{10.7}{40}$	$\frac{10.0}{44}$
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Sta	+	π	-	Elev
		941.03		
77				34.0
+25				33.4
+50				31.9
78	Road Ct.			32.2
+10	Drive Ct.			32.7
+50				32.8
79				32.9
+50				34.2
80				35.8
+50				37.0
T.P.	2.16	945.32	2.87	928.16
81				39.7

LT

L

RT

$$\frac{58}{50} \quad \frac{68}{31} \quad \frac{70}{6} \quad \frac{70}{\cancel{1}} \quad \frac{82}{5} \quad \frac{104}{9} \quad \frac{100}{21} \quad \frac{100}{21} \quad \frac{92}{37} \quad \frac{81}{45} \quad \frac{77}{50}$$

$$\frac{41}{43} \quad \frac{60}{4} \quad \frac{76}{\cancel{1}} \quad \frac{96}{6} \quad \frac{97}{16} \quad \frac{99}{27} \quad \frac{92}{30} \quad \frac{90}{35} \quad \frac{84}{46} \quad \frac{84}{50}$$

At Dwellings

$$\frac{37}{50} \quad \frac{57}{9} \quad \frac{91}{\cancel{1}} \quad \frac{94}{14} \quad \frac{95}{22} \quad \frac{90}{25} \quad \frac{90}{36} \quad \frac{96}{50}$$

$$\frac{34}{50} \quad \frac{39}{29} \quad \frac{53}{15} \quad \frac{53}{7} \quad \frac{88}{\cancel{1}} \quad \frac{84}{17} \quad \frac{83}{50} \quad \frac{83}{100}$$

$$\frac{39}{100} \quad \frac{51}{40} \quad \frac{73}{15} \quad \frac{83}{\cancel{1}}$$

$$\frac{47}{50} \quad \frac{54}{26} \quad \frac{73}{12} \quad \frac{82}{8} \quad \frac{82}{\cancel{1}} \quad \frac{80}{7} \quad \frac{83}{16} \quad \frac{78}{17} \quad \frac{79}{25} \quad \frac{72}{50}$$

$$\frac{67}{50} \quad \frac{73}{15} \quad \frac{72}{12} \quad \frac{85}{5} \quad \frac{81}{\cancel{1}} \quad \frac{77}{11} \quad \frac{81}{23} \quad \frac{88}{27} \quad \frac{90}{50}$$

$$\frac{51}{50} \quad \frac{57}{36} \quad \frac{66}{9} \quad \frac{68}{\cancel{1}} \quad \frac{73}{5} \quad \frac{82}{10} \quad \frac{76}{21} \quad \frac{81}{32} \quad \frac{89}{36} \quad \frac{107}{50}$$

$$\frac{30}{50} \quad \frac{46}{23} \quad \frac{57}{\cancel{1}} \quad \frac{56}{7} \quad \frac{66}{10} \quad \frac{85}{18} \quad \frac{78}{24} \quad \frac{73}{36} \quad \frac{79}{49} \quad \frac{95}{53}$$

$$\frac{15}{50} \quad \frac{30}{24} \quad \frac{34}{7} \quad \frac{40}{\cancel{1}} \quad \frac{49}{16} \quad \frac{50}{31} \quad \frac{61}{25} \quad \frac{66}{40} \quad \frac{76}{45} \quad \frac{70}{50} \quad \frac{70}{65}$$

$$\frac{29}{50} \quad \frac{41}{30} \quad \frac{51}{14} \quad \frac{56}{\cancel{1}} \quad \frac{67}{16} \quad \frac{80}{40} \quad \frac{83}{50}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

945.32

81+50

39.8

+75

39.1

82

39.7

T.P.

10.40

945.21

✓ 0.51

944.81

✓

+75

82

+25

41.5

+50

45.6

+78

49.4

83+00

49.3

+50

46.5

84

45.6

LT

K

RT

$$\frac{1.0}{50} \quad \frac{3.0}{35} \quad \frac{3.4}{21} \quad \frac{3.9}{9} \quad \frac{5.5}{5} \quad \frac{6.5}{10} \quad \frac{8.1}{27} \quad \frac{8.5}{50}$$

$$\frac{6.2}{11} \quad \frac{7.2}{26} \quad \frac{8.3}{50}$$

$$\frac{5.6}{24} \quad \frac{7.9}{24} \quad \frac{9.3}{50}$$

$$\frac{9.2}{50} \quad \frac{13.2}{24} \quad \frac{15.6}{8} \quad (16.1)$$

$$\frac{6.1}{50} \quad \frac{10.8}{30} \quad \frac{14.1}{15} \quad (15.5)$$

$$\frac{4.3}{50} \quad \frac{6.5}{38} \quad \frac{10.8}{19} \quad \frac{13.2}{5} \quad \frac{13.7}{20} \quad \frac{15.9}{20} \quad \frac{18.7}{50}$$

$$\frac{3.3}{50} \quad \frac{4.3}{42} \quad \frac{6.8}{21} \quad \frac{9.3}{4} \quad \frac{9.6}{6} \quad \frac{11.3}{6} \quad \frac{13.6}{22} \quad \frac{17.0}{50}$$

$$\frac{2.7}{50} \quad \frac{4.3}{24} \quad 5.8 \quad \frac{6.0}{4} \quad \frac{7.0}{6} \quad \frac{9.9}{24} \quad \frac{14.4}{50}$$

$$\frac{2.3}{50} \quad \frac{3.5}{32} \quad \frac{4.8}{12} \quad 5.9 \quad \frac{5.9}{4} \quad \frac{6.9}{6} \quad \frac{9.3}{25} \quad \frac{11.2}{36} \quad \frac{13.4}{50}$$

$$\frac{3.4}{55} \quad \frac{4.8}{36} \quad \frac{6.5}{15} \quad 8.7 \quad \frac{9.1}{4} \quad \frac{9.5}{7} \quad \frac{10.9}{20} \quad \frac{12.9}{10}$$

$$\frac{7.7}{50} \quad \frac{8.0}{25} \quad 9.6 \quad \frac{10.2}{6} \quad \frac{11.1}{10} \quad \frac{12.4}{31} \quad \frac{13.3}{50}$$

Sta	+	T	-	Elev
		955.21		
84+50				43.6
85				38.9
+30				37.7
+60				39.5
86				40.1
+50				45.0
87				46.2
T.P.	1.63	949.70	7.64	947.57 v
+50				43.1
88				35.4
T.P.	3.53	940.24	17.49	936.71
+50				30.1

Lt

L

Rt

$$\frac{9.7}{50} \quad \frac{10.8}{39} \quad \frac{11.7}{20} \quad \frac{11.6}{7} \quad \frac{11.3}{10} \quad \frac{11.8}{26} \quad \frac{13.5}{50} \quad \frac{14.5}{50}$$

$$\frac{10.9}{50} \quad \frac{14.0}{29} \quad \frac{16.0}{13} \quad \frac{16.3}{20} \quad \frac{17.4}{20} \quad \frac{18.0}{34} \quad \frac{17.3}{50}$$

$$\frac{13.0}{50} \quad \frac{15.5}{29} \quad \frac{13.0}{13} \quad \frac{17.5}{14} \quad \frac{17.3}{34} \quad \frac{17.1}{34} \quad \frac{16.6}{50}$$

$$\frac{15.5}{50} \quad \frac{17.0}{21} \quad \frac{15.7}{24} \quad \frac{16.0}{24} \quad \frac{16.3}{50}$$

$$\frac{17.0}{50} \quad \frac{15.1}{21} \quad \frac{15.1}{21} \quad \frac{16.1}{29} \quad \frac{16.1}{50}$$

$$\frac{11.4}{50} \quad \frac{10.6}{29} \quad \frac{10.7}{19} \quad \frac{11.8}{19} \quad \frac{13.7}{38} \quad \frac{14.1}{50}$$

$$\frac{9.0}{50} \quad \frac{8.1}{25} \quad \frac{9.0}{15} \quad \frac{10.7}{15} \quad \frac{12.6}{39} \quad \frac{13.0}{50}$$

$$\frac{4.9}{50} \quad \frac{5.2}{29} \quad \frac{5.8}{8} \quad \frac{6.1}{6} \quad \frac{5.9}{6} \quad \frac{6.1}{17} \quad \frac{6.5}{35} \quad \frac{7.0}{50}$$

$$\frac{11.5}{50} \quad \frac{13.1}{37} \quad \frac{13.6}{8} \quad \frac{13.8}{10} \quad \frac{13.7}{10} \quad \frac{12.8}{26} \quad \frac{12.1}{41} \quad \frac{12.1}{50}$$

$$\frac{6.8}{50} \quad \frac{7.4}{46} \quad \frac{8.1}{28} \quad \frac{10.1}{13} \quad \frac{10.1}{23} \quad \frac{10.4}{23} \quad \frac{11.7}{50}$$

Sta.	+	π	-	Elev.
		940.24		
89				27.8
+50				28.2
90				32.1
+50				33.3
91				34.7
+40				35.8
T.P.	5.10	938.81	- 6.53	933.71 ✓
92 ✓				27.8
+50				25.6
93				25.8
+50				27.9
94				35.2

Lt.

Q

Rt.

$$\frac{10.6}{50}$$

$$\frac{11.7}{22}$$

$$\frac{12.4}{50}$$

$$\frac{12.6}{28}$$

$$\frac{12.5}{50}$$

$$\frac{10.7}{50}$$

$$\frac{11.1}{34}$$

$$\frac{11.8}{11}$$

$$\frac{17.0}{50}$$

$$\frac{12.1}{21}$$

$$\frac{11.4}{50}$$

$$\frac{7.4}{50}$$

$$\frac{2.0}{26}$$

$$\frac{8.1}{50}$$

$$\frac{9.8}{13}$$

$$\frac{10.5}{25}$$

$$\frac{10.5}{39}$$

$$\frac{9.6}{50}$$

$$\frac{3.8}{50}$$

$$\frac{4.3}{24}$$

$$\frac{6.2}{9}$$

$$\frac{6.9}{50}$$

$$\frac{9.0}{14}$$

$$\frac{10.6}{25}$$

$$\frac{9.8}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.2}{25}$$

$$\frac{5.5}{50}$$

$$\frac{7.6}{20}$$

$$\frac{8.3}{36}$$

$$\frac{8.7}{50}$$

$$\frac{4.0}{50}$$

$$\frac{3.6}{46}$$

$$\frac{3.9}{16}$$

$$\frac{4.4}{50}$$

$$\frac{5.5}{18}$$

$$\frac{7.6}{50}$$

$$\frac{7.2}{50}$$

$$\frac{8.3}{39}$$

$$\frac{10.3}{18}$$

$$\frac{11.0}{50}$$

$$\frac{11.5}{11}$$

$$\frac{11.9}{29}$$

$$\frac{11.9}{50}$$

$$\frac{13.2}{50}$$

$$\frac{13.4}{25}$$

$$\frac{13.2}{50}$$

$$\frac{12.8}{35}$$

$$\frac{12.8}{40}$$

$$\frac{12.4}{50}$$

$$\frac{14.0}{50}$$

$$\frac{14.0}{25}$$

$$\frac{13.0}{50}$$

$$\frac{12.5}{25}$$

$$\frac{11.5}{50}$$

$$\frac{12.8}{50}$$

$$\frac{11.6}{19}$$

$$\frac{10.9}{50}$$

$$\frac{8.9}{30}$$

$$\frac{8.3}{37}$$

$$\frac{6.7}{44}$$

$$\frac{5.4}{54}$$

$$\frac{6.1}{64}$$

$$\frac{7.9}{50}$$

$$\frac{6.2}{29}$$

$$\frac{3.6}{50}$$

$$\frac{2.9}{14}$$

$$\frac{4.7}{15}$$

$$\frac{5.3}{19}$$

$$\frac{4.8}{24}$$

$$\frac{4.4}{34}$$

$$\frac{4.9}{45}$$

$$\frac{13.13}{58}$$

Sta	+	Δ	-	Elev.
		938.81		
T.P.	7.90	944.12	2.59	936.22 ✓
94+23				38.3
135				34.7
+55				35.8
95				36.4
+40				36.8
+50				39.6
96				40.00
+50				38.8
97				38.6
+50				38.2
98				38.6

ht k ht.

$$\frac{8.9}{50} \quad \frac{7.7}{24} \quad \frac{6.3}{9} \quad \frac{5.8}{4} \quad \frac{8.4}{8} \quad \frac{10.0}{13} \quad \frac{9.6}{17} \quad \frac{9.7}{25} \quad \frac{9.4}{40} \quad \frac{10.0}{46} \quad \frac{6.1}{50}$$

$$\frac{6.8}{50} \quad \frac{5.9}{30} \quad \frac{5.0}{6} \quad \frac{7.1}{3} \quad \frac{9.4}{6} \quad \frac{8.2}{10} \quad \frac{9.3}{21} \quad \frac{8.0}{33} \quad \frac{9.7}{40} \quad \frac{6.5}{50}$$

$$\frac{5.0}{50} \quad \frac{4.6}{36} \quad \frac{6.2}{11} \quad \frac{7.5}{8} \quad \frac{8.3}{4} \quad \frac{8.6}{15} \quad \frac{8.6}{28} \quad \frac{9.2}{32} \quad \frac{5.6}{40} \quad \frac{5.6}{50}$$

$$\frac{5.5}{50} \quad \frac{5.5}{24} \quad \frac{7.0}{20} \quad \frac{8.0}{16} \quad \frac{7.4}{10} \quad \frac{7.7}{11} \quad \frac{8.5}{16} \quad \frac{5.7}{50}$$

$$\frac{4.5}{50} \quad \frac{4.3}{36} \quad \frac{5.2}{34} \quad \frac{7.5}{28} \quad \frac{6.8}{23} \quad \frac{6.6}{13} \quad \frac{7.3}{8} \quad \frac{4.8}{25} \quad \frac{5.3}{50}$$

$$\frac{4.6}{50} \quad \frac{4.6}{38} \quad \frac{6.2}{35} \quad \frac{6.7}{30} \quad \frac{6.4}{26} \quad \frac{6.2}{18} \quad \frac{7.2}{5} \quad \frac{4.5}{14} \quad \frac{4.7}{14} \quad \frac{6.5}{50}$$

$$\frac{4.5}{50} \quad \frac{4.3}{46} \quad \frac{6.2}{43} \quad \frac{5.5}{38} \quad \frac{6.4}{26} \quad \frac{6.3}{14} \quad \frac{3.8}{10} \quad \frac{4.1}{26} \quad \frac{4.5}{26} \quad \frac{5.0}{50}$$

$$\frac{4.2}{55} \quad \frac{5.0}{50} \quad \frac{5.4}{43} \quad \frac{5.2}{33} \quad \frac{5.9}{21} \quad \frac{5.1}{20} \quad \frac{4.8}{11} \quad \frac{5.3}{30} \quad \frac{6.0}{30} \quad \frac{5.9}{50}$$

$$\frac{5.9}{50} \quad \frac{5.4}{43} \quad \frac{5.4}{34} \quad \frac{5.7}{22} \quad \frac{5.4}{21} \quad \frac{5.5}{23} \quad \frac{7.0}{50}$$

$$\frac{5.0}{50} \quad \frac{5.2}{37} \quad \frac{5.5}{24} \quad \frac{5.8}{15} \quad \frac{5.6}{13} \quad \frac{5.9}{19} \quad \frac{6.2}{19} \quad \frac{6.2}{50}$$

$$\frac{4.4}{50} \quad \frac{3.5}{31} \quad \frac{5.5}{26} \quad \frac{5.4}{19} \quad \frac{5.2}{10} \quad \frac{5.5}{8} \quad \frac{4.1}{8} \quad \frac{4.7}{14} \quad \frac{5.8}{50}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

944.12

98+50				38.7
-------	--	--	--	------

99				38.6
----	--	--	--	------

+50				37.9
-----	--	--	--	------

100				37.6
-----	--	--	--	------

100+57.01				37.3
-----------	--	--	--	------

=
46+16.25 N. Co. Line Road

B.M.		4.82	939.60	
------	--	------	--------	--

939.53

Lt

E

Rt

$$\frac{5.5}{50} \quad \frac{5.1}{21} \quad \frac{4.4}{13} \quad \frac{5.5}{7} \quad \frac{5.4}{50} \quad \frac{5.4}{14} \quad \frac{5.0}{18} \quad \frac{4.9}{24} \quad \frac{5.4}{50}$$

(X)

$$\frac{6.1}{50} \quad \frac{6.6}{30} \quad \frac{5.6}{9}$$

$$\frac{5.5}{50} \quad \frac{5.3}{10} \quad \frac{5.4}{21} \quad \frac{6.9}{25} \quad \frac{7.0}{29} \quad \frac{5.6}{32} \quad \frac{5.7}{50}$$

$$\frac{7.5}{50} \quad \frac{7.5}{31} \quad \frac{6.2}{8} \quad \frac{6.2}{10} \quad \frac{5.6}{21} \quad \frac{5.8}{25} \quad \frac{7.1}{31} \quad \frac{6.4}{36} \quad \frac{5.7}{50}$$

$$\frac{8.3}{50} \quad \frac{8.3}{31} \quad \frac{7.0}{10} \quad \frac{7.1}{6} \quad \frac{6.6}{4} \quad \frac{6.5}{5} \quad \frac{6.7}{23} \quad \frac{8.8}{27} \quad \frac{6.8}{50}$$

(X)

$$\frac{8.4}{50} \quad \frac{8.4}{22} \quad \frac{7.6}{10} \quad \frac{7.2}{6} \quad \frac{6.8}{17} \quad \frac{7.0}{17} \quad \frac{7.5}{50}$$

Spike in 20" Oak intersection of No. 60 line
Road & Portland Ave.

Sta	+	T	-	Elev
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Recommendations.

Sta.

24+17 Pl. 15" Culv. @ 6th St Left

24+34 Pl. 15" " Right

Sta. 24-38 - Ditch 15 deep Back Slopes @ 30' or less

34+40 - Taylor Ave. no culv road (make Summit)

41+ Pl. 24" Culv. Drains Left

47+ Pl. 30" " " "

60+73 Ent. Lt. & Rt. (make Summit)

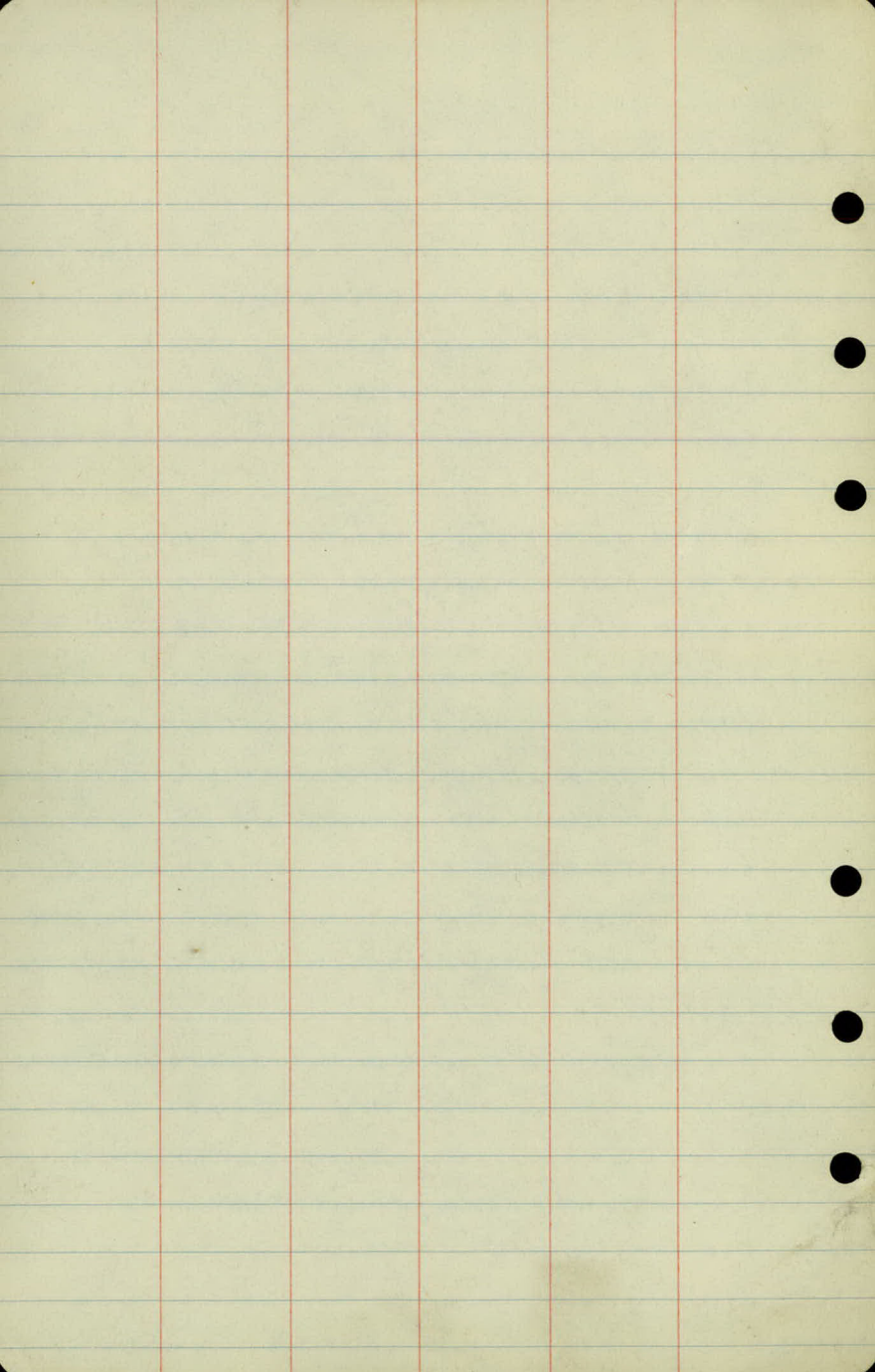
71+0 Pl. 30" Culv. Drains Right

80+0 Pl. 24" Culv. Drain St. to Divert water
from farm Ho. Sta. 72+078-80 make shallow ditch on left and
narrow grading section to save yard.

89+0 Pl. 24" Drains St.

92+75 Pl. 24" Equal.

100+57 Pl. 24" Culv. Drain South, then Ditch Grade
to Sta 95+±W. L. Carlson
March 5, 1937



45

Bench Levels
Portland Ave.

{ Bretager
{ Eillen

These bench levels are run from Top of
East Head Wall of culvert (given Elev.
(924.00) about 400' south of Bald Eagle
Junction on S. Tr. Hy. #61 to Bench placed
in Oak tree at intersection of
Portland Ave. and Second St.

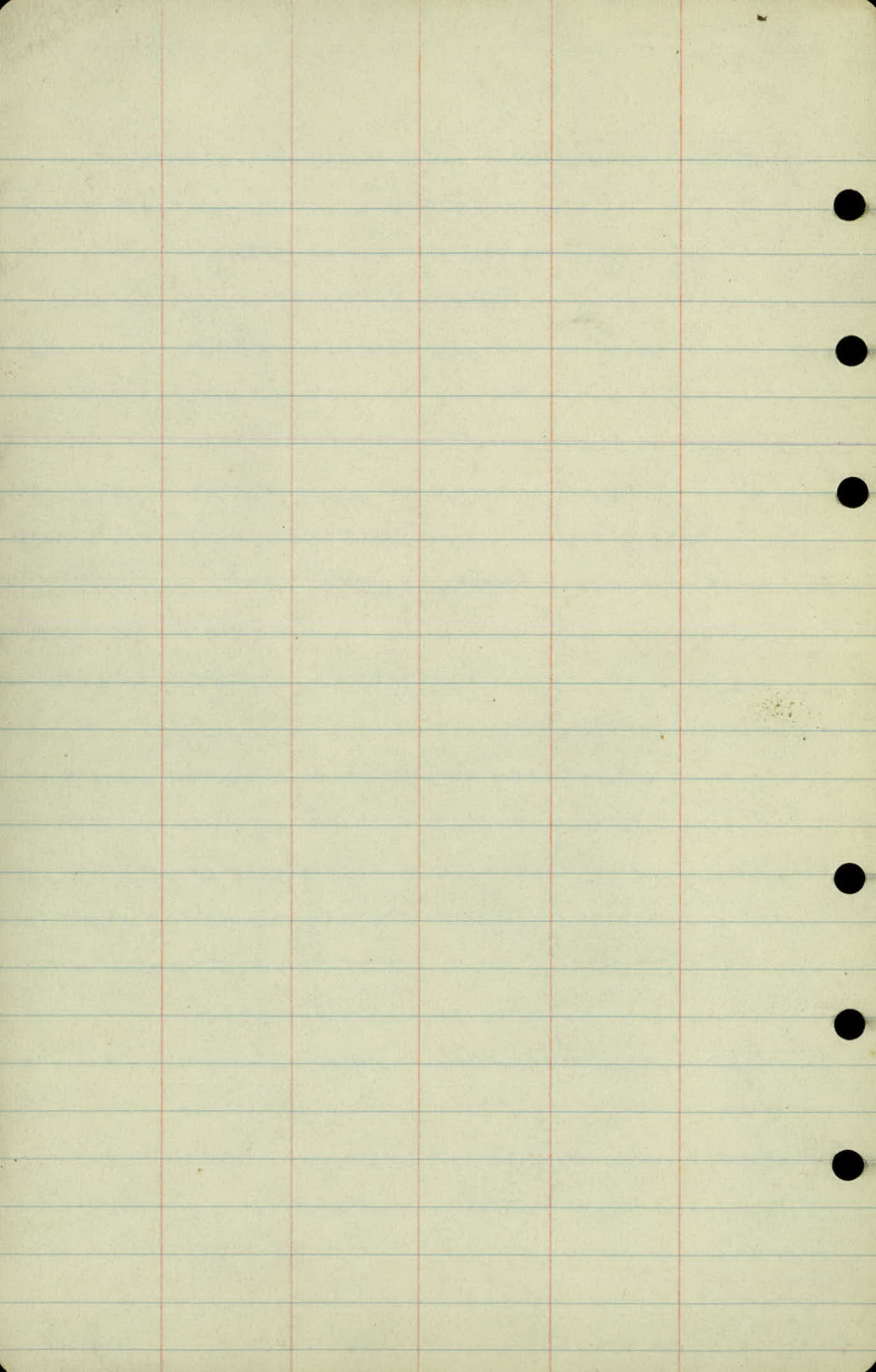
	+	-	Flor.	
B.M				924.00
T.P.	11.25	935.25		
T.P.		4.67	930.58	
	4.07	934.65		
T.P.		3.82	930.83	
	5.40	936.23		
T.P.		2.37	933.86	
	7.48	941.34		
T.P.		3.73	938.11	928.11
	3.73	941.34		
T.P.		6.49	934.85	
	2.80	944.65		
T.P.		4.45	940.20	
	3.37	942.57		
B.M.		6.39		937.18
	6.39	943.57		
T.P.		3.96	939.61	
	0.89	940.50		
T.P.		4.53	935.97	
	1.80	937.77		
T.P.		6.14	931.63	
	2.82	934.45		
T.P.		4.18	930.27	
	5.02	935.29		
T.P.		11.25	924.04	924.00

400' South Bald Eagle Tct.
Top of East. Head Wall T.H. #61
Near Sooline Xing.

Spike in 20" Box Elder

Spike in 15" Oak 4th St. Portland Arc.
and Second St.

W/1
15
37



Bench Levels (Portland Ave.)

From

(No. Co. Line Road to 2nd St.)

Bratton
Wike
Gillon

$\frac{2}{27}$
 $\frac{1}{37}$

Sta	+	π	-	Elev.
B.M.	4.56	944.09		939.53
T.P.			8.52	936.57.
	1.73	937.30		
T.P.			3.42	934.08.
	8.98	942.06		
T.P.			7.98	925.08.
	3.02	938.10		
B.M.			0.85	927.45
	0.85	938.10		
T.P.			8.25	929.85
	1.50	931.35		
T.P.			3.46	927.89
	12.82	940.71		
B.M.			0.85	929.86.
	14.15	954.01		
T.P.			1.09	950.92
	13.29	964.21		
T.P.			2.48	956.73
	0.69	957.42		
T.P.			11.31	946.11
	0.70	946.81		
B.M.			8.67	938.14
	4.30	942.44		
T.P.			2.29	940.06

Spike in 20" Oak @ intersection of No. 6.
Line road + Portland Ave.

Nail in Tel. Pole. Rt.

^{no sta. as yet.}
Spike in 24" Elm Lt.

Spike in 12" Oak 65' Rt. Sta. 65 + 2 ✓

Spike in 12" Oak Rt. 35' - 46 + 41

Sta.	+	Σ	-	Elev.
				940.05
	9.62	949.67		
T.P.			3.31	946.36
	0.74	947.10		
T.P.			14.48	934.62
	1.48	936.10		
B.M.			3.36	932.74
	3.36	936.10		
T.P.			13.40	922.70
	11.22	933.92		
T.P.			1.27	932.65
	9.15	941.80		
B.M.			4.52	937.28 937.18