

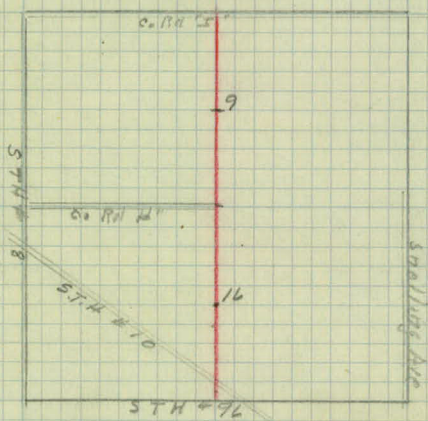
OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN._____ **PLAN** _____ Survey_____ **MOUNDS VIEW RD.** _____From **S.T.H. N^o 96** To **CO. RD. "1"**Road Acc't. No. **35** _____

Date Filed _____

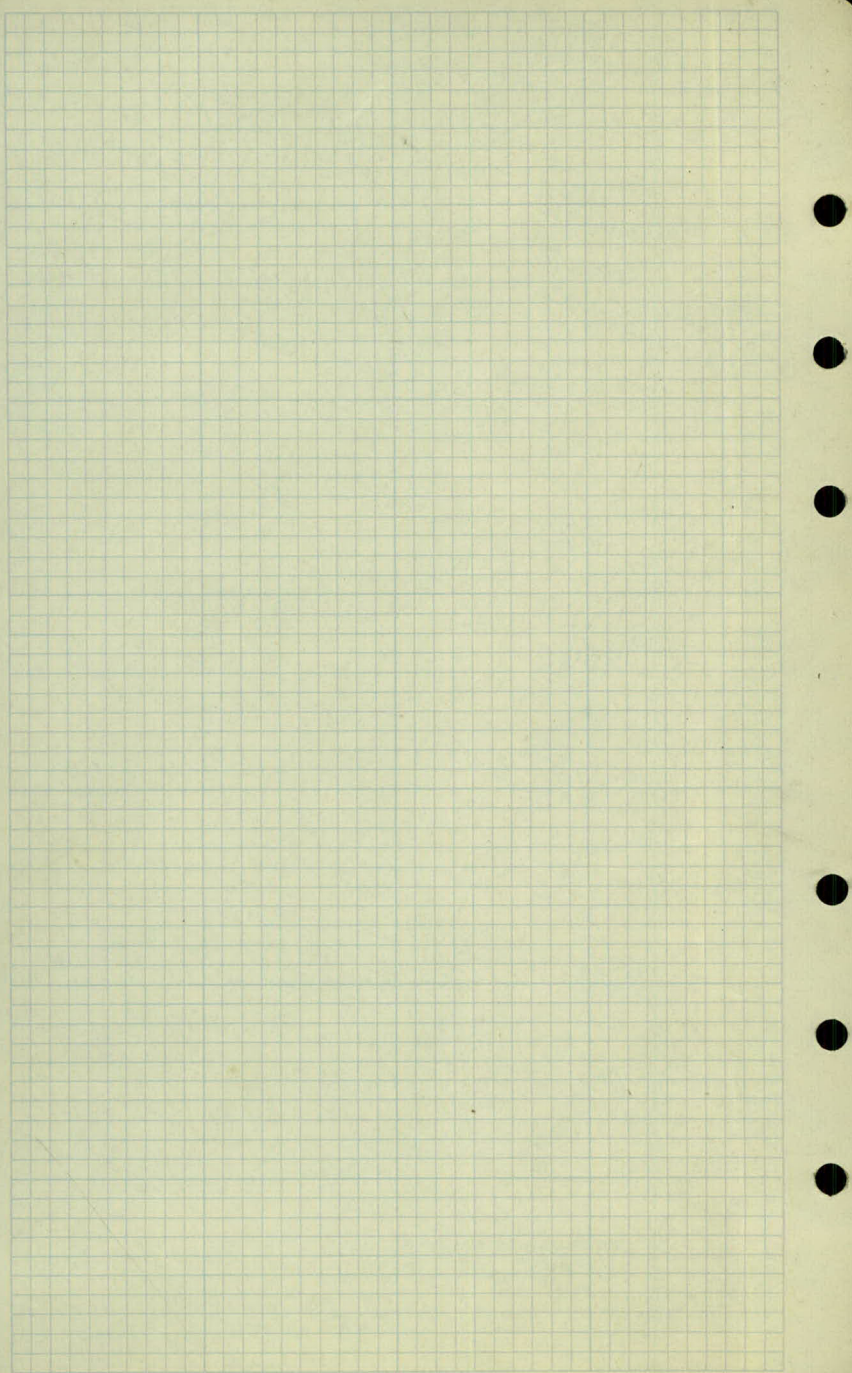
File _____

PLAN SURVEY MOUNDS VIEW RD.

From
S.T.H #96
To
Co. Rd. "I"



Index	Pages 1
Alignment	2-4
Topog	5-21
Cross Sections	22-37
CK. Levels	38-39
Recommendations	40-41



Mounds View Road.

Alignment Co. Rd. "E."
to "I"

4/37

Sta

Angle

Lt.

Rt.

52+80⁰⁸ ^{Stone} Mon. $\Delta 0^{\circ}5'$

41+00 P.O.T.

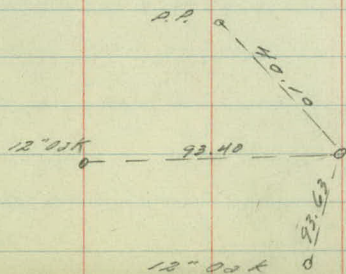
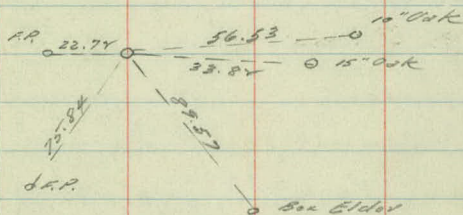
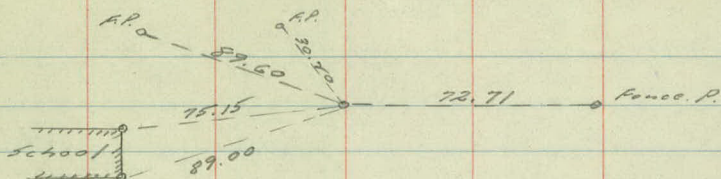
26+39⁴⁵ ^{Stone} Mon. P.O.T.

23+00 P.O.T.

10+27⁵⁵ P.O.T.

0+00 ^{Stone} Mon. Co. Rd. 6 & Mounds View Rd.

Reference Points



Sta.

Angle

Lt.

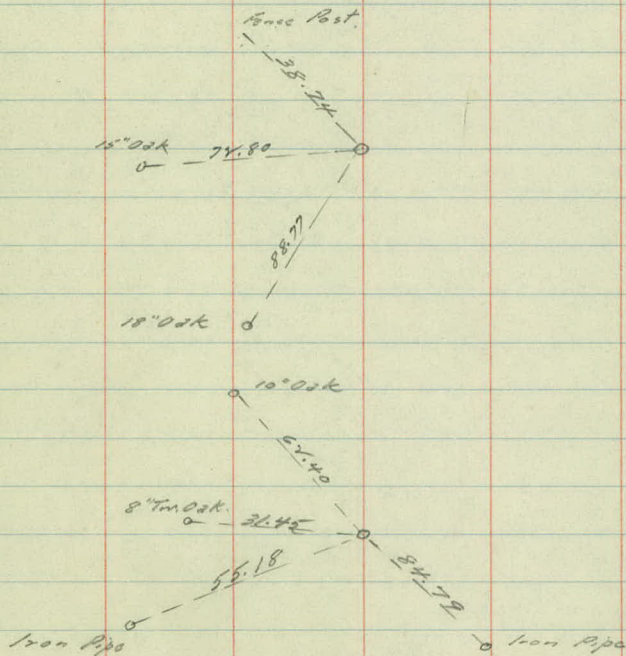
Rt.

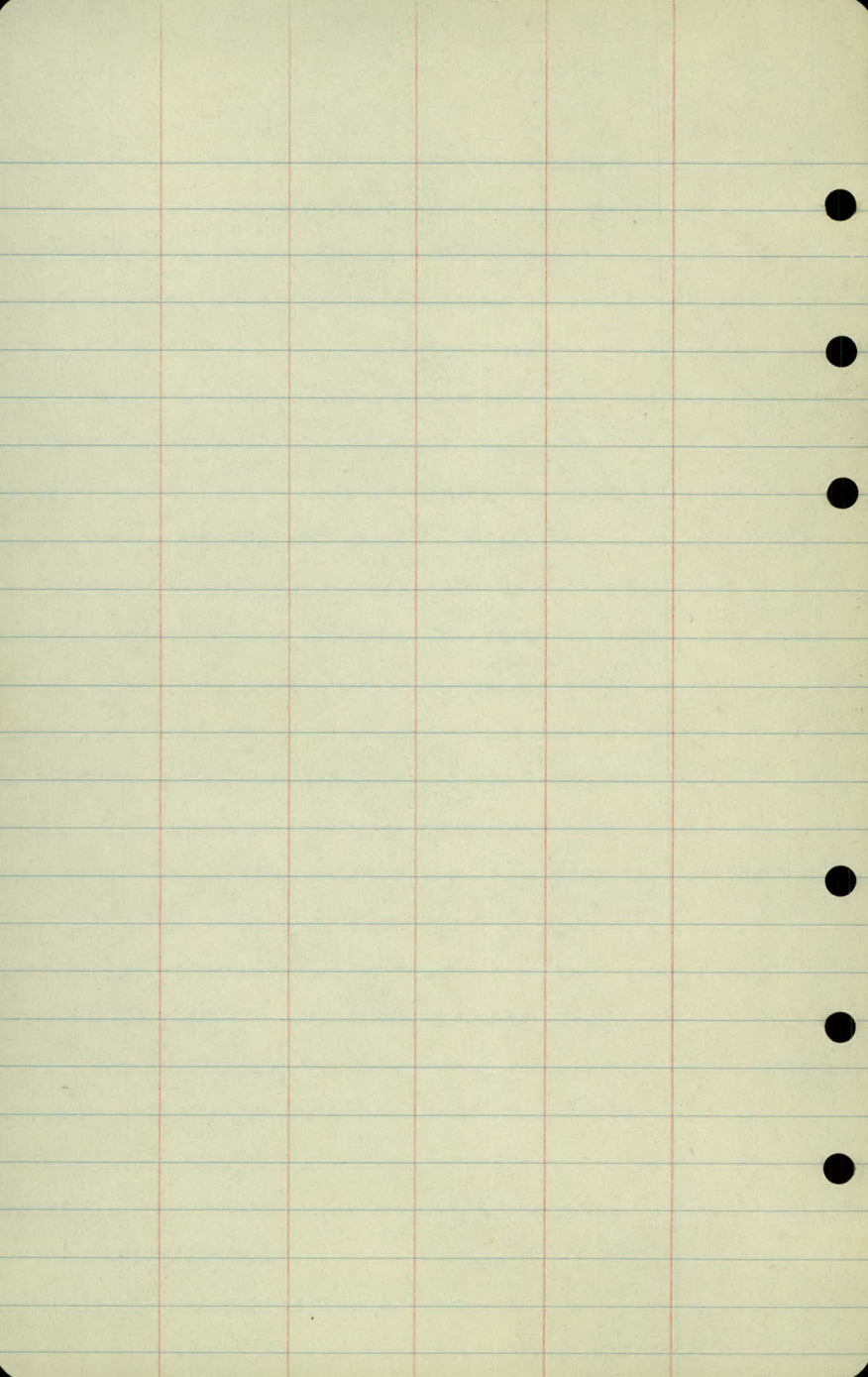
105+61 ^{Stone} ~~to~~ Mon.

79+16 ^{Stone} ~~Mon.~~ P.O.T.

67+00 P.O.T.

Reference Points





3/22/37 5

TOPOGRAPHY
MOUNDS VIEW ROAD
S.T.H. #96 to CO. RD. "I"

4/37

Gonfrida
Wilke
Goldberg
Larson

+67 End 24' Conc +91 PP

$$\begin{array}{r} 16 \\ +52 \text{ Shoulder} \\ \hline 30 \end{array}$$

$$\begin{array}{r} 27 \\ +78 \text{ Rd Sn} \\ \hline 21 \\ +74 \text{ Stop Sn} \\ \hline 19 \end{array}$$

$$\begin{array}{r} +68 \text{ Rd} \\ \hline 11-9 \end{array}$$

$$\begin{array}{r} +18 \text{ Shoulder} \\ \hline 9 \end{array}$$

$$\begin{array}{r} +05 \text{ Shoulder} \\ \hline 9 \end{array}$$

$$\begin{array}{r} +87 \text{ Tr} \\ \hline 25 \end{array}$$

$$\begin{array}{r} +25 \text{ FC} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +28 \text{ Tr} \\ \hline 30 \end{array}$$

$$\begin{array}{r} +17 \text{ End Cul} \\ \hline 21 \end{array}$$

$$\begin{array}{r} \text{Spillway} \\ \hline 15 \end{array}$$

$$\begin{array}{r} +71 \text{ Edge Fare} \\ \hline 0 \end{array}$$

$$\begin{array}{r} +27 \\ +56 \text{ FC} - \text{PP} \\ \hline 24 \quad 26 \end{array}$$

$$\begin{array}{r} +33 \text{ Rd} \\ \hline 35 \end{array}$$

$$\begin{array}{r} +13 \text{ End Cul} - \text{Stop Sn} \\ \hline 21 \quad 18 \end{array}$$

$$\begin{array}{r} +18 \text{ Rd} \\ \hline 9-12 \\ \hline 21 \\ \hline 9-8 \end{array}$$

$$\begin{array}{r} \text{Edge Fare} \\ \hline 62 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 23 \end{array}$$

$$\begin{array}{r} +06 \text{ PP} \\ \hline 26 \end{array}$$

$$\begin{array}{r} \text{Fc} \\ \hline 22 \end{array}$$

$$\begin{array}{r} \text{Rd} \\ \hline 11-8 \end{array}$$

$$\begin{array}{r} +57 \text{ PP} \\ \hline 26 \end{array}$$

$$\begin{array}{r} +85-12' \times 40 \text{ CM} \\ \hline 21-19 \end{array}$$

$$\begin{array}{r} +31 \text{ PP} \quad +32 \text{ FC} \\ \hline 25 \quad 18 \end{array}$$

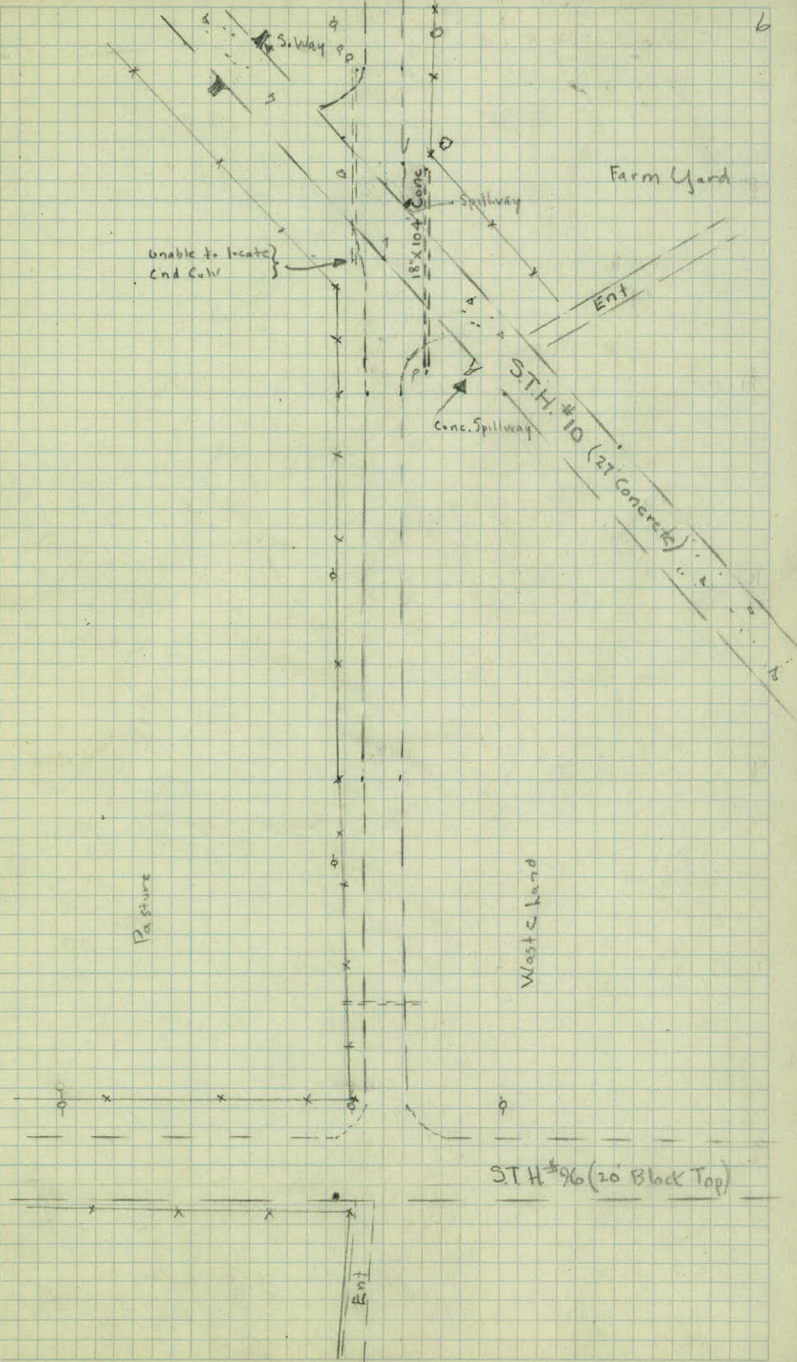
$$\begin{array}{r} +32 \text{ Rd} \\ \hline 8-12 \\ +16 \text{ Shoulder} \\ \hline 25-34 \end{array}$$

$$\begin{array}{r} +31 \text{ PP} \\ \hline 60 \end{array}$$

$$\begin{array}{r} +84 \text{ Guy Po} \\ \hline 25 \end{array}$$

$$\begin{array}{r} +77 \text{ FC} \\ \hline 17 \end{array}$$

$$+84 \text{ Shoulder}$$



12

$$\frac{Fc}{28}$$

$$\frac{Rd}{9-10}$$

$$\frac{Fc}{27}$$

$$\frac{+88 PP}{28}$$

11

$$\frac{+39 PP}{29}$$

10

$$\frac{Fc}{28}$$

$$\frac{Rd}{7-12}$$

$$\frac{Fc}{31}$$

9

$$\frac{+89 PP}{27}$$

$$\frac{+85 Fc}{27}$$

8

$$\frac{Fc}{26}$$

$$\frac{Rd}{10-10}$$

$$\frac{Fc}{26}$$

$$\frac{+40 PP}{27}$$

7

$$\frac{+60 Fc}{26}$$

+72 Ent

$$\frac{+58 Fc}{92}$$

$$\frac{+30 Ent (9' \times 20' CM)}{22}$$

6

$$\frac{Rd}{10-9}$$

$$\frac{Fc}{27}$$

Cultivated

Cultivated

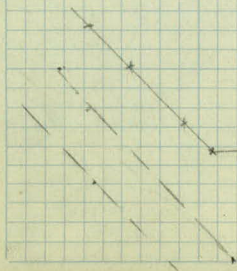
Pot Hole

Pot Hole

Pot Hole

Ent

Ent



19

$$+51 \text{ Ent} \quad \frac{+60 \text{ EC} + 43}{24} \quad \frac{+65 \text{ PP}}{29}$$

$$\frac{+22 \text{ Guy Po}}{25}$$

18

$$\frac{F_2}{28}$$

$$\frac{Rd}{10-9}$$

$$\frac{F_2}{25}$$

$$\frac{+28 \text{ PP}}{28}$$

17

$$\frac{+55 \text{ EC}}{25}$$

$$+40 \text{ Ent} \left(\frac{12' \times 20' \text{ CM}}{16} \right)$$

16

$$\frac{F_2}{28}$$

$$\frac{Rd}{10-9}$$

$$\frac{F_2}{25}$$

$$\frac{+43 \text{ PP}}{28}$$

15

$$\frac{+58 \text{ PP}}{28}$$

14

$$\frac{F_2}{28}$$

$$\frac{Rd}{10-10}$$

$$\frac{F_2}{26}$$

$$\frac{+23 \text{ PP}}{28}$$

13

Pot Hole

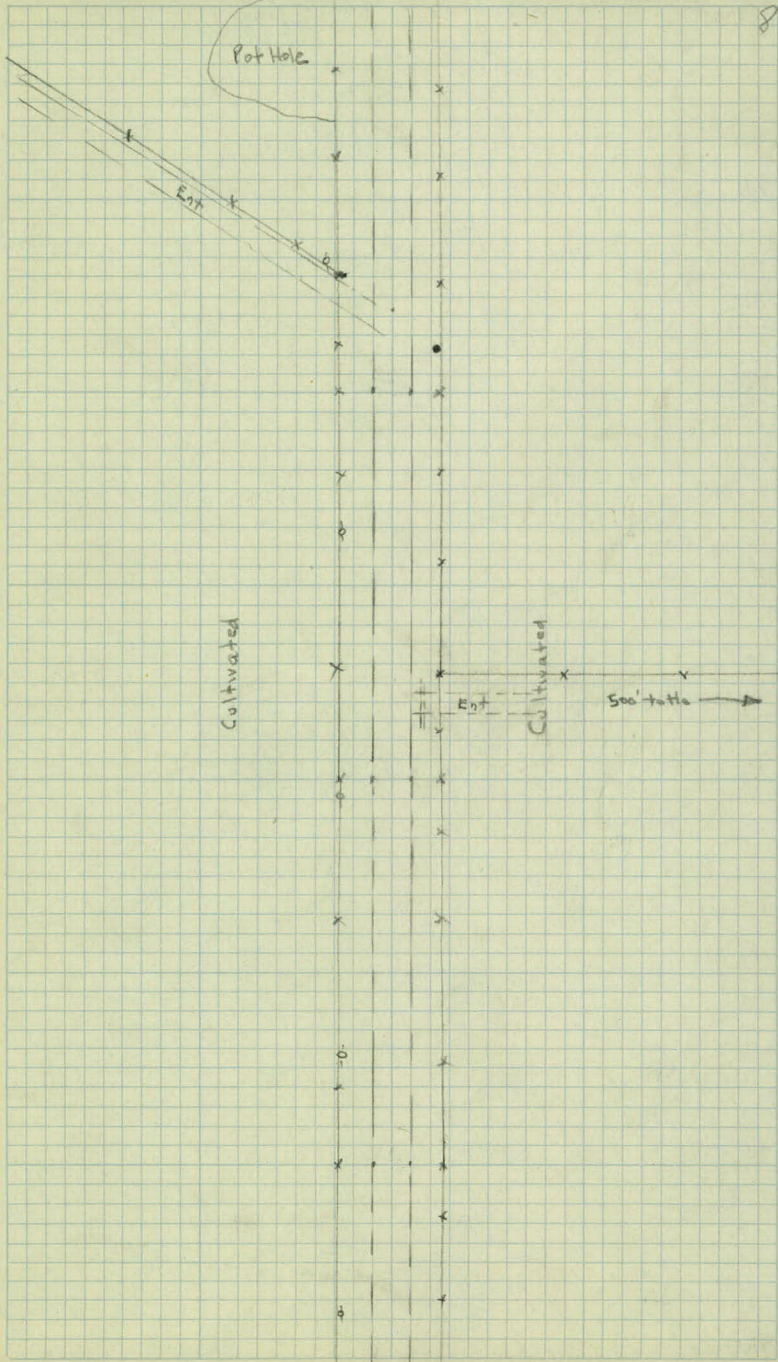
Ent

Cultivated

Cultivated

Ent

Sooty-tail



$$\frac{+64 \text{ S.F. Con House}}{200}$$

$$\frac{+36 \text{ FC.}}{22}$$

$$\frac{+37 \text{ FC.}}{21}$$

$$\frac{+24 \text{ FC.}}{21}$$

$$\frac{+31 \text{ Two DR.}}{32}$$

26

$$\frac{\text{FC}}{24}$$

$$\frac{\text{RD}}{11-9}$$

$$\frac{+96 \text{ Cor Gar}}{24}$$

$$+83 \text{ Ent}$$

$$\frac{+34 \text{ PP}}{29}$$

25

$$\frac{+87 \text{ Cor Ho}}{182}$$

$$+84 \text{ Ent}$$

$$\frac{+53 \text{ PP}}{30}$$

24

$$\frac{\text{FC}}{28}$$

$$\frac{\text{RD}}{12-8}$$

$$\frac{\text{FC}}{22}$$

23

$$\frac{+15 \text{ PP.}}{30}$$

22

$$\frac{\text{FC}}{31}$$

$$\frac{\text{RD}}{12-8}$$

$$\frac{\text{FC}}{22}$$

$$\frac{+43 \text{ PP}}{30}$$

21

$$\frac{+14 \text{ PP}}{29}$$

20

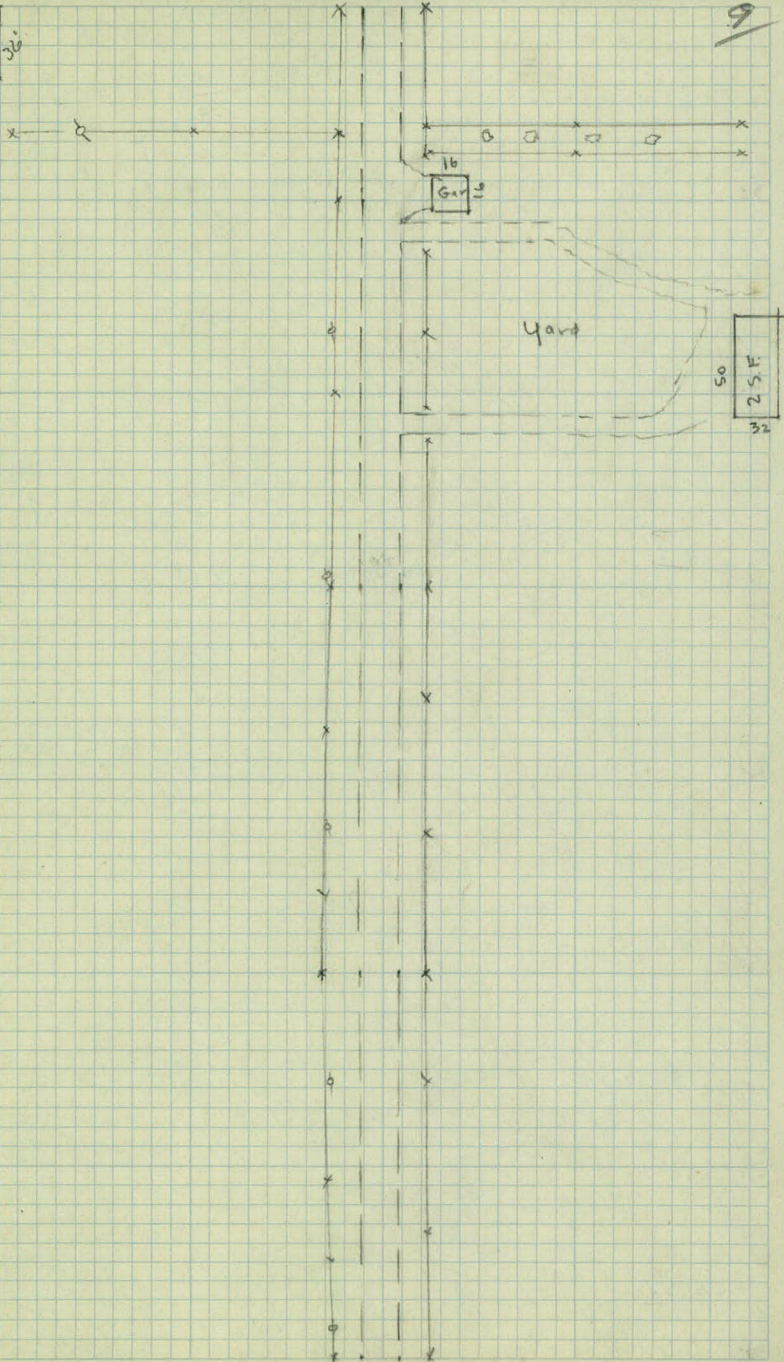
$$\frac{\text{FC}}{26}$$

$$\frac{\text{RD}}{10-9}$$

$$\frac{\text{FC}}{24}$$

25
5' 10" 30'
20'

9



$$\frac{+55-10 \times 34 \text{ cM.}}{18-16}$$

33

$$\frac{Fc.}{18}$$

$$\frac{Rd.}{9-9}$$

$$\frac{Fc.}{18} \quad \frac{Fc.}{33}$$

$$\frac{+51 \times Fc. Cor.}{18}$$

$$\frac{+43 \text{ Ent.}}{}$$

31

$$\frac{+03-12 \times 36 \text{ cM.}}{18-18}$$

$$\frac{+22 \times Fc. Cor.}{33}$$

$$\frac{+23 \text{ Ent.}}{}$$

$$\frac{Fc.}{16}$$

$$\frac{Rd.}{10-10}$$

$$\frac{Fc.}{19}$$

29

$$\frac{Fc.}{15}$$

$$\frac{Rd.}{10-9}$$

$$\frac{Fc.}{20}$$

$$\frac{+53 \times Fc. Cor.}{15}$$

$$\frac{+36 \text{ Ent.}}{}$$

27

$$\frac{+24 \times Fc. Cor.}{21}$$

Pasture

Cultivated

Pot
Hole

Cultivated

Cultivated

+90 tree 21 197 Fc, Cor 15

+85 Non Tree 19-22-33

+57 S. F. Corn House 142

+34 Ent

+48 Begin orchard 29

+46 Fc, Cor 17

Fc 29

40

Rd 11-8

Fc 16

Fc 31

+81 Plum tree 25

+46-15 tree 24-33-37

+41 X Fc 20

39

38

Rd 9-9

Fc 16

Fc 30

37

+21-9x26 CM. Plogged 12-14'

+58 Ent.

36

Rd 10-8

Fc 16

Fc 32

35

+46 Fc, Cor 18

34

Fc 17

Rd 11-9

Fc 17

Fc 32

18
F
House
24

26

Cultivated

Cultivated

Cultivated

47

46

$$\frac{Rd.}{12-7}$$

45

$$\frac{End. Fc.}{19}$$

$$\frac{+ 32 Rd. Sgn.}{17}$$

$$\frac{+ 16 \times Fc.}{21}$$

44

$$\frac{Fc.}{19}$$

$$\frac{Rd.}{7-8}$$

$$\frac{Fc.}{20}$$

43

$$+ 00 Ent.$$

$$\frac{+ 46 Fc. Cor}{20}$$

$$\frac{+ 44 SW. Cor Barn}{88}$$

$$\frac{+ 09 tree}{24}$$

$$\frac{+ 04 Fc. Cor}{20}$$

42

$$\frac{Fc.}{13}$$

$$\frac{Rd}{9-11}$$

$$\frac{+ 56-30 tree}{25}$$

$$+ 32 Ent.$$

$$\frac{+ 13-20 tree}{35}$$

$$\frac{+ 00 tree}{34}$$

$$\frac{+ 84-8 tree}{34}$$

$$\frac{+ 50-24 tree}{30}$$

$$\frac{+ 48-9 tree CM.}{15-16}$$

$$\frac{+ 41 SW. Cor House}{77}$$

41

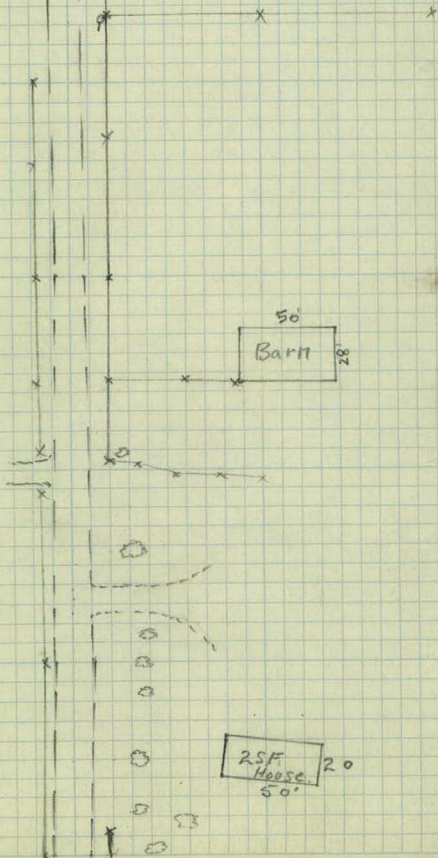
$$\frac{+ 12 Fc. Cor}{18}$$

$$\frac{+ 24 End Orchard}{29}$$

Cultivated

Cultivated

Cultivated



54

$$\frac{Fc}{20}$$

$$\frac{Rd}{10-10}$$

53

$$\frac{+09 Fc}{20}$$

$$\frac{+14 Rd}{11-9}$$

$$\frac{+12 S.19.2}{32}$$

$$\frac{+59 Pump}{48}$$

$$\frac{+71 Cor School}{68}$$

$$\begin{array}{r} +91 Shoulder \\ 42 \\ +71 Shoulder \\ 38-9 \\ +43 Rd \\ 11-9 \end{array}$$

$$\frac{+81 Fc}{14}$$

52

$$\frac{Rd}{11-9}$$

$$\frac{Fc}{14}$$

$$\frac{+76-9 \times 38 CM}{18-20}$$

51

50

$$\frac{Rd}{12-6}$$

$$\frac{Fc}{13}$$

49

48

$$\frac{Rd}{13-6}$$

$$\frac{Fc}{14}$$

Cultivate

Cultivated

CO. RD. "H" Gravel

24
15 F
School
40'

School
Yard

Cultivated

Cultivated

$$\begin{array}{r} +88 \text{ 9" x 28" } \\ 16-12 \end{array}$$

$$\begin{array}{r} +37 \text{ Fold/Ent } \\ 87-12 \text{ x } 22 \text{ ' RIT } \end{array}$$

61

60

$$\begin{array}{r} Fc \\ 23 \end{array}$$

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} +59 \text{ Prop. Iron } \\ 33 \end{array}$$

$$\begin{array}{r} +41 \text{ Prop. Iron } \\ 33 \end{array}$$

59

$$\begin{array}{r} +51 \text{ Caution Sch } \\ 16 \end{array}$$

$$\begin{array}{r} +42 \text{ Sch. Zone } \\ 14 \end{array}$$

$$\begin{array}{r} +41 \text{ Ditch } \\ 100 \end{array}$$

58

$$\begin{array}{r} Fc \\ 23 \end{array}$$

$$\begin{array}{r} Rd \\ 11-11 \end{array}$$

$$\begin{array}{r} +42 \text{ Ditch } \\ 26 \end{array}$$

57

$$\begin{array}{r} +70-24 \text{ x } 40 \text{ ' CM } \\ 17-23 \end{array}$$

56

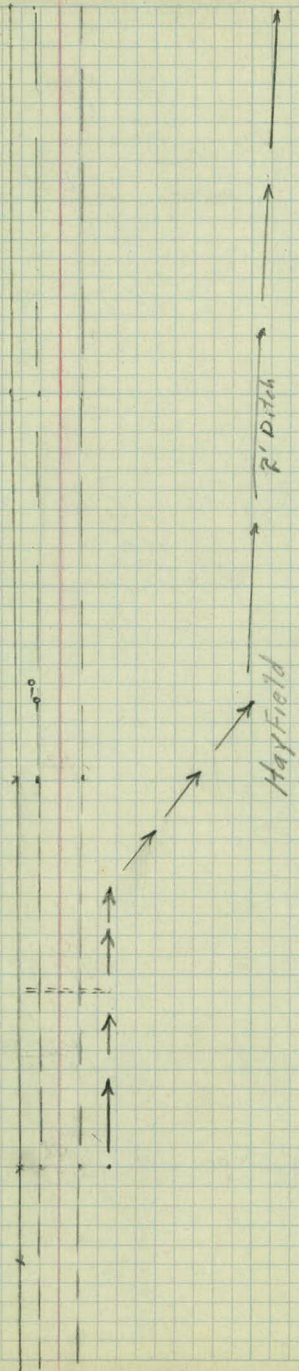
$$\begin{array}{r} Fc \\ 20 \end{array}$$

$$\begin{array}{r} Rd \\ 10-10 \end{array}$$

$$\begin{array}{r} \text{Req 2' Bnd Ditch } \\ 26 \end{array}$$

55

Cultivated



68

+02 4" Drain Tile
Heat Buried
Fence 23'

$$\begin{array}{r} +03 \times 12' \times 32' \\ 21' - 11' \\ \hline Rd \\ 15' - 8' \end{array}$$

67

66

Fence 24'

$$\begin{array}{r} Rd \\ 15' - 7' \end{array}$$

+34 Prop Iron
33'

+88 Field Ent

+67 Prop Iron
33'

65

64

Fe 24'

$$\begin{array}{r} Rd \\ 14' - 8' \end{array}$$

118' Ditch

$$\begin{array}{r} +54 \times \text{Drain } 12' \times 30' \\ 18' - 12' \end{array}$$

63

+74 Prop Iron
23'

+44 Fe Cor
24'

+30 Field Ent

+21 Fe Cor
40'

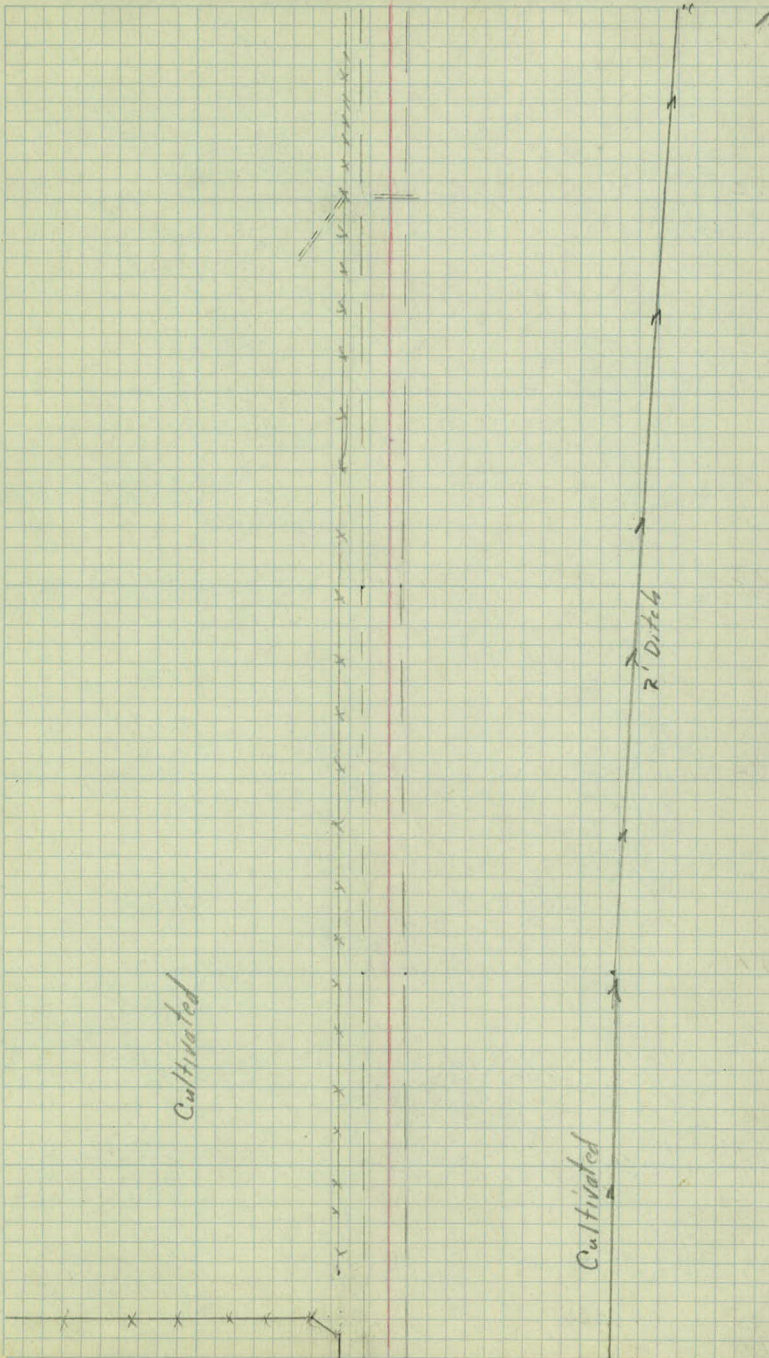
+13 Fe Cor
25'

Fe. 24'

+54 Prop Iron
33'

62

$$\begin{array}{r} Rd \\ 13' - 9' \end{array}$$



+33 Prop Iron
33'

+40 Field Ent

+37 Prop Iron
33'

75

+35 4 Ditch Lt
100'

74

Fence 20

1/2 X Ditch 30" X 52' Vt

22' - 30'

Rd
11' - 10'

18' X 10' Conc Hd Wall

+40 Ditch Lt
150'

73

+36 Prop Iron
33'

72

Fence 21'

Rd
18' - 10'

+36 Prop Iron
33'

Ditch 150

71

70

Fence 22'

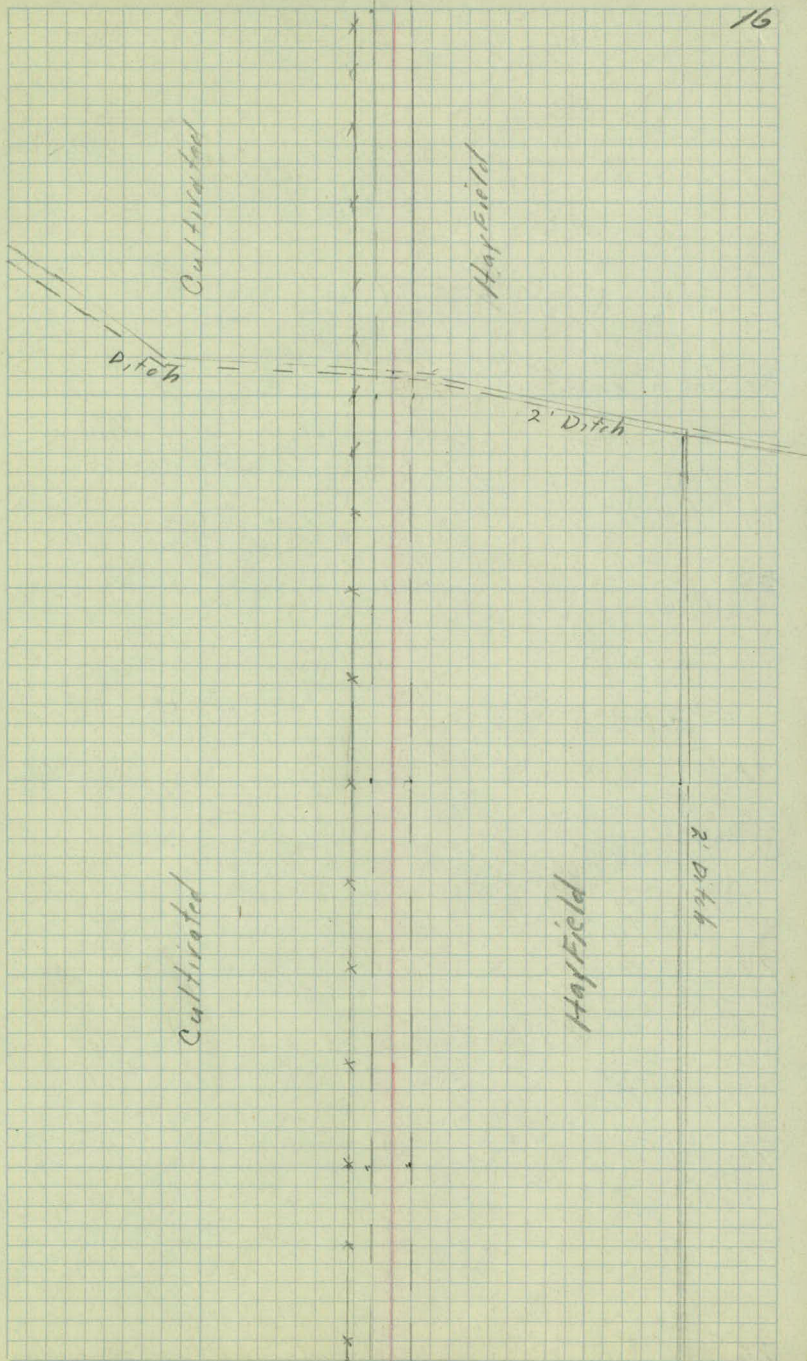
Rd
13' - 9'

Ditch 148'

69

+19 Prop Iron
33'

+35 Prop Iron
33'



52

Rel
10-10'

+53 Beg Row 10" Traps

81 $\frac{16}{18}$ 12 Oak

+66 Fence Cor

+54 $\frac{12}{18}$ Oak80 $\frac{10}{18}$ 12 Oak
Fence 18'Rel
10-10'+76 $\frac{10}{18}$ Oak + 91 $\frac{10}{18}$ Oak+35 $\frac{12}{22}$ Twin Oak+23 $\frac{12}{31}$ Twin Oak+20 $\frac{12}{24}$ Fence Cor

+27 Field Ent

79

+71 $\frac{12}{33}$ Prop Front+65 $\frac{12}{24}$ Fence Cor+39 $\frac{12}{23}$ Prop Front

78 Fence 24'

Rel
12-10'

77

76 Fence 22'

Rel
11-9

yard

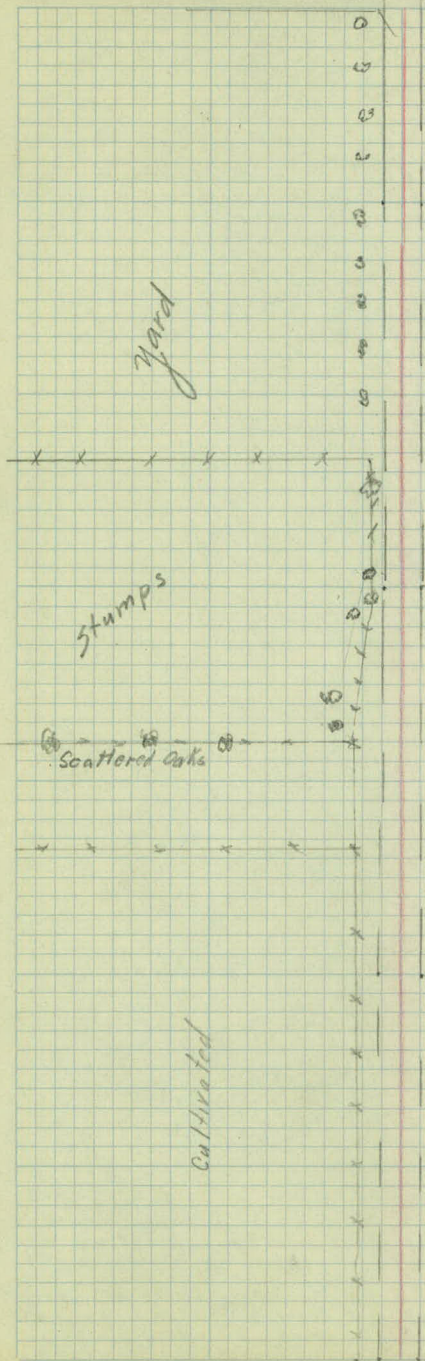
Cultivated

stumps

Scattered Oaks

Cultivated

Hay Field



+30 End Brush

89

88

Fence 20'

$\frac{Rd}{9-11'}$

87

86

Fence 20'

$\frac{Rd}{7-11'}$

85

End yard

+72 Fence
22'

+40 End Yard

+62 Drive

84

$\frac{Rd}{8-10'}$

+117 S.W. Corner house

+98 $\frac{4000}{35}$ oak

+80 Bay yard

83

+19 End Row Trees
78' 42'

+06 Field End

Cultivated

Cultivated

Scrub Brush

2 Shrub
Frame
24' 17'

Cultivated



97 Begin Timber

96 Fence 23' $\frac{Rd}{12-8'}$

+ 40 Fence
20

95 Stamps 20'

94 Fence 19' $\frac{Rd}{10-10}$

+ 50 Begin Trees
+ Brush 100'

93

+ 55 Fence
20

+ 35 Field Ery
+ 28 Field Ery

92 Fence 20' $\frac{Rd}{9-11'}$

91

90 Fence 20 $\frac{Rd}{9-11'}$

Stumps & Brush

Small Trees & Brush

Pasture

Cultivated

Cultivated

103

+56 Rd sign
15'

102 Fence 23'

Rd
12'-8'

101

100 Fence 20'

Rd
12'-9'

99

98 Fence 22'

Rd
12'-7'

97 Begin Timber 23'

Sea Hered Oaks
Brush

Stumps

Stumps

Cultivated

105+61 ⁴⁰ Co Rd I'

+34 Rd Sign
35'

+31 PP
76'

+20 Fe. Out
37'

105

+76 4 Fence
25'

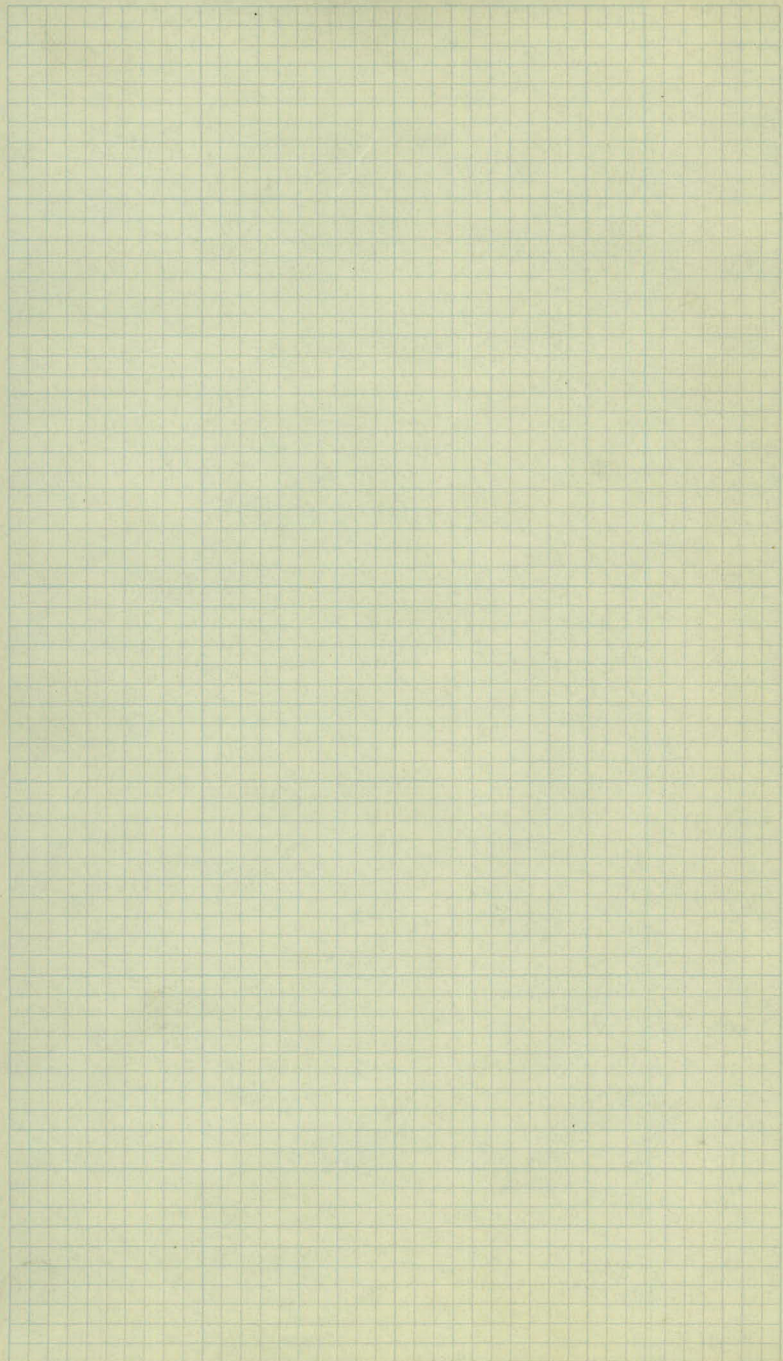
104

Fence 24'

Rd.
10'+9'

Co. Rd "I"

Scattered Oaks
Brush + Stumps



Mounds View Road
Cross Sections from
Co. Rd. "G" to "I"

4/37

Bratogan
Wilke
Goldberg
Gillen
Larson

Sta.	+	Δ	-	Elev.
B.M.	0.55	916.39		915.84
0+00				04.6
+15				04.1
+20				04.3
+45				03.8
+85 = 17" C.M.				
1+00				04.0
+50				04.4
2				04.9
+50				05.7
3				06.7
+50				07.9
4				09.7

Culvert on Rt. under Tr. Hg. 2/10

T.P. 7.67 920.91 3.15 913.24

Lt.

E

Rt

Spike in 30" Maple N.E. Cor. Mounds
View Road + St. Tr. Hy. #10.

$$\begin{array}{r}
 15.0 \\
 \hline
 100 \\
 15.4 \\
 \hline
 100
 \end{array}
 \quad
 \begin{array}{r}
 11.8 \\
 \hline
 17.3
 \end{array}
 \quad
 \begin{array}{r}
 7.8 \\
 \hline
 100 \\
 5.3 \\
 \hline
 100
 \end{array}$$

$$\begin{array}{r}
 18.7 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 16.6 \\
 \hline
 24
 \end{array}
 \quad
 \begin{array}{r}
 13.5 \\
 \hline
 18
 \end{array}
 \quad
 \begin{array}{r}
 12.1 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 11.8 \\
 \hline
 24
 \end{array}
 \quad
 \begin{array}{r}
 16.5 \\
 \hline
 47
 \end{array}
 \quad
 \begin{array}{r}
 16.4 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 17.5 \\
 \hline
 50
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 \quad
 \begin{array}{r}
 18.4 \\
 \hline
 25
 \end{array}
 \quad
 \begin{array}{r}
 17.7 \\
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 19
 \end{array}
 \quad
 \begin{array}{r}
 13.3 \\
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 12
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 \begin{array}{r}
 12.6 \\
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 17
 \end{array}
 \quad
 \begin{array}{r}
 12.8 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 17.0 \\
 \hline
 26
 \end{array}
 \quad
 \begin{array}{r}
 16.6 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 18.0 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 18.3 \\
 \hline
 40
 \end{array}
 \quad
 \begin{array}{r}
 18.0 \\
 \hline
 24
 \end{array}
 \quad
 \begin{array}{r}
 13.4 \\
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 14
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 \begin{array}{r}
 12.4 \\
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 17
 \end{array}
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 12.6 \\
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 13
 \end{array}
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 \begin{array}{r}
 17.4 \\
 \hline
 24
 \end{array}
 \quad
 \begin{array}{r}
 17.4 \\
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 50
 \end{array}$$

$$\begin{array}{r}
 16.4 \\
 \hline
 50
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 \quad
 \begin{array}{r}
 17.4 \\
 \hline
 21
 \end{array}
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 \begin{array}{r}
 12.7 \\
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 13
 \end{array}
 \quad
 \begin{array}{r}
 12.0 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 12.6 \\
 \hline
 15
 \end{array}
 \quad
 \begin{array}{r}
 15.9 \\
 \hline
 22
 \end{array}
 \quad
 \begin{array}{r}
 15.6 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 15.7 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 16.7 \\
 \hline
 20
 \end{array}
 \quad
 \begin{array}{r}
 12.3 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 11.5 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 11.9 \\
 \hline
 13
 \end{array}
 \quad
 \begin{array}{r}
 14.8 \\
 \hline
 20
 \end{array}
 \quad
 \begin{array}{r}
 13.6 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 14.5 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 14.0 \\
 \hline
 29
 \end{array}
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 13.2 \\
 \hline
 19
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 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 10.7 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 11.3 \\
 \hline
 13
 \end{array}
 \quad
 \begin{array}{r}
 13.6 \\
 \hline
 19
 \end{array}
 \quad
 \begin{array}{r}
 13.7 \\
 \hline
 27
 \end{array}
 \quad
 \begin{array}{r}
 12.2 \\
 \hline
 32
 \end{array}
 \quad
 \begin{array}{r}
 12.0 \\
 \hline
 44
 \end{array}
 \quad
 \begin{array}{r}
 10.7 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 10.8 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 10.8 \\
 \hline
 39
 \end{array}
 \quad
 \begin{array}{r}
 12.5 \\
 \hline
 26
 \end{array}
 \quad
 \begin{array}{r}
 11.6 \\
 \hline
 20
 \end{array}
 \quad
 \begin{array}{r}
 10.1 \\
 \hline
 15
 \end{array}
 \quad
 \begin{array}{r}
 9.7 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 10.0 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 12.2 \\
 \hline
 18
 \end{array}
 \quad
 \begin{array}{r}
 11.4 \\
 \hline
 26
 \end{array}
 \quad
 \begin{array}{r}
 10.1 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 9.7 \\
 \hline
 44
 \end{array}
 \quad
 \begin{array}{r}
 8.4 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 6.0 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 2.0 \\
 \hline
 41
 \end{array}
 \quad
 \begin{array}{r}
 10.6 \\
 \hline
 19
 \end{array}
 \quad
 \begin{array}{r}
 9.0 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 8.5 \\
 \hline
 17
 \end{array}
 \quad
 \begin{array}{r}
 9.0 \\
 \hline
 14
 \end{array}
 \quad
 \begin{array}{r}
 10.3 \\
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 18
 \end{array}
 \quad
 \begin{array}{r}
 9.2 \\
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 25
 \end{array}
 \quad
 \begin{array}{r}
 8.2 \\
 \hline
 28
 \end{array}
 \quad
 \begin{array}{r}
 7.8 \\
 \hline
 43
 \end{array}
 \quad
 \begin{array}{r}
 6.4 \\
 \hline
 50
 \end{array}$$

$$\begin{array}{r}
 4.5 \\
 \hline
 50
 \end{array}
 \quad
 \begin{array}{r}
 5.1 \\
 \hline
 21
 \end{array}
 \quad
 \begin{array}{r}
 7.6 \\
 \hline
 16
 \end{array}
 \quad
 \begin{array}{r}
 7.0 \\
 \hline
 13
 \end{array}
 \quad
 \begin{array}{r}
 6.7 \\
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 17
 \end{array}
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 \begin{array}{r}
 6.8 \\
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 15
 \end{array}
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 \begin{array}{r}
 7.4 \\
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 17
 \end{array}
 \quad
 \begin{array}{r}
 7.6 \\
 \hline
 25
 \end{array}
 \quad
 \begin{array}{r}
 5.1 \\
 \hline
 29
 \end{array}
 \quad
 \begin{array}{r}
 4.8 \\
 \hline
 42
 \end{array}
 \quad
 \begin{array}{r}
 2.0 \\
 \hline
 53
 \end{array}$$

7.40
No. End.

24" Conc

8.70
So. End

Sta.	+	π	-	Elev.
		970.91		
4+35				11.4
+58				13.0
+93				13.2
Culvert on lt. under Tr. Hy. #10				
5+15				13.0
Tr. Hy. #10				
+65				13.8
+70				13.9
+85				14.4
6+00				14.8
+50				15.9
7				17.2

4.

2

24

$$\frac{29}{50} \quad \frac{22}{22} \quad \frac{113}{11} \quad \frac{104}{13} \quad \frac{95}{13} \quad \frac{96}{13} \quad \frac{88}{19} \quad \frac{70}{34} \quad \frac{66}{20}$$

$$\frac{54}{50} \quad \frac{52}{35} \quad \frac{44}{29} \quad \frac{47}{26} \quad \frac{116}{11} \quad \frac{146}{13} \quad \frac{90}{12} \quad \frac{79}{10} \quad \frac{76}{32} \quad \frac{72}{50}$$

$$\frac{45}{53} \quad \frac{100}{44} \quad \frac{100}{38} \quad \frac{79}{27} \quad \frac{79}{20} \quad \frac{77}{19} \quad \frac{78}{26} \quad \frac{75}{35} \quad \frac{97}{37} \quad \frac{90}{42} \quad \frac{83}{50} \quad \frac{79}{50}$$

14.5
30 End.

24 Conc

11.75
No. End

$$\frac{104}{54} \quad \frac{104}{49} \quad \frac{81}{40} \quad \frac{80}{32} \quad \frac{79}{18} \quad \frac{79}{15} \quad \frac{78}{20} \quad \frac{78}{22} \quad \frac{80}{30} \quad \frac{87}{10}$$

$$\frac{810}{100}$$

$$\frac{618}{100}$$

$$\frac{82}{50} \quad \frac{82}{44} \quad \frac{81}{29} \quad \frac{87}{23} \quad \frac{73}{14} \quad \frac{71}{16} \quad \frac{77}{20} \quad \frac{86}{23} \quad \frac{68}{34} \quad \frac{80}{34} \quad \frac{87}{50}$$

$$\frac{82}{50} \quad \frac{78}{40} \quad \frac{102}{31} \quad \frac{105}{23} \quad \frac{96}{17} \quad \frac{74}{13} \quad \frac{70}{17} \quad \frac{76}{20} \quad \frac{83}{24} \quad \frac{70}{33} \quad \frac{73}{50}$$

$$\frac{98}{50} \quad \frac{51}{34} \quad \frac{56}{21} \quad \frac{78}{16} \quad \frac{67}{13} \quad \frac{65}{9} \quad \frac{70}{20} \quad \frac{72}{22} \quad \frac{85}{22} \quad \frac{63}{25} \quad \frac{72}{50}$$

$$\frac{81}{50} \quad \frac{56}{44} \quad \frac{53}{20} \quad \frac{73}{16} \quad \frac{65}{12} \quad \frac{61}{18} \quad \frac{90}{21} \quad \frac{90}{23} \quad \frac{53}{27} \quad \frac{56}{34} \quad \frac{65}{50}$$

$$\frac{66}{50} \quad \frac{53}{11} \quad \frac{50}{17} \quad \frac{49}{20} \quad \frac{85}{22} \quad \frac{85}{27} \quad \frac{40}{27} \quad \frac{39}{50}$$

$$\frac{73}{50} \quad \frac{68}{18} \quad \frac{47}{13} \quad \frac{37}{11} \quad \frac{40}{20} \quad \frac{78}{22} \quad \frac{78}{23} \quad \frac{73}{23} \quad \frac{72}{50}$$

Sta.	+	π	-	Elev.
		920.91		

+50				18.6
-----	--	--	--	------

8				20.2
---	--	--	--	------

T.P.	11.12	931.09	0.84	919.97
------	-------	--------	------	--------

+35				21.4
-----	--	--	--	------

9				23.3
---	--	--	--	------

+40				24.7
-----	--	--	--	------

T.P.	7.23	934.93	3.39	927.70
------	------	--------	------	--------

10				26.7
----	--	--	--	------

+50				27.9
-----	--	--	--	------

11				28.5
----	--	--	--	------

+38				29.2
-----	--	--	--	------

12				29.4
----	--	--	--	------

+45				29.7
-----	--	--	--	------

+70				29.8
-----	--	--	--	------

Lt.

E

Rt

25

Pot Hole	$\frac{9^2}{50}$	$\frac{8^8}{22}$	$\frac{2^9}{11}$	$\frac{2^3}{1}$	$\frac{3^2}{16}$	$\frac{7^9}{24}$	$\frac{8^7}{27}$	$\frac{9^0}{50}$	Pot Hole
-------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	-------------

$\frac{5^5}{50}$	$\frac{5^8}{34}$	$\frac{6^2}{21}$	$\frac{1^4}{12}$	$\frac{0^7}{1}$	$\frac{1^3}{16}$	$\frac{7^8}{27}$	$\frac{7^8}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{13^2}{50}$	$\frac{14^1}{21}$	$\frac{13^0}{16}$	$\frac{10^3}{11}$	$\frac{9^7}{1}$	$\frac{10^5}{16}$	$\frac{14^9}{25}$	$\frac{15^0}{50}$
-------------------	-------------------	-------------------	-------------------	-----------------	-------------------	-------------------	-------------------

$\frac{8^1}{50}$	$\frac{8^0}{27}$	$\frac{7^5}{20}$	$\frac{8^3}{10}$	$\frac{7^8}{1}$	$\frac{8^2}{16}$	$\frac{8^9}{20}$	$\frac{7^7}{22}$	$\frac{6^7}{28}$	$\frac{7^3}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{1^8}{50}$	$\frac{1^8}{28}$	$\frac{1^6}{19}$	$\frac{6^9}{9}$	$\frac{6^4}{1}$	$\frac{7^0}{18}$	$\frac{1^6}{28}$	$\frac{2^6}{50}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{3^1}{50}$	$\frac{1^2}{23}$	$\frac{6^3}{16}$	$\frac{8^6}{9}$	$\frac{8^2}{1}$	$\frac{8^7}{17}$	$\frac{2^5}{27}$	$\frac{3^9}{50}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{2^9}{50}$	$\frac{1^9}{30}$	$\frac{0^5}{25}$	$\frac{6^8}{14}$	$\frac{7^6}{9}$	$\frac{7^0}{1}$	$\frac{7^4}{17}$	$\frac{6^6}{22}$	$\frac{1^7}{30}$	$\frac{3^2}{50}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{5^3}{50}$	$\frac{4^0}{29}$	$\frac{2^5}{24}$	$\frac{6^9}{17}$	$\frac{6^4}{1}$	$\frac{6^9}{17}$	$\frac{5^9}{21}$	$\frac{3^5}{24}$	$\frac{6^6}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

$\frac{7^1}{50}$	$\frac{6^3}{30}$	$\frac{5^2}{25}$	$\frac{2^0}{19}$	$\frac{6^3}{12}$	$\frac{5^7}{1}$	$\frac{6^3}{15}$	$\frac{7^7}{18}$	$\frac{8^7}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{10^2}{50}$	$\frac{8^8}{27}$	$\frac{8^2}{18}$	$\frac{6^2}{13}$	$\frac{5^5}{1}$	$\frac{6^4}{15}$	$\frac{9^8}{20}$	$\frac{11^2}{50}$	Pot Hole
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$\frac{8^7}{50}$	$\frac{7^8}{20}$	$\frac{6^1}{15}$	$\frac{5^2}{1}$	$\frac{6^0}{14}$	$\frac{9^2}{20}$	$\frac{9^2}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{6^4}{50}$	$\frac{6^3}{27}$	$\frac{2^5}{22}$	$\frac{2^5}{20}$	$\frac{5^7}{14}$	$\frac{5^1}{1}$	$\frac{5^7}{15}$	$\frac{7^3}{19}$	$\frac{8^0}{34}$	$\frac{7^7}{38}$	$\frac{7^8}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

$5\frac{1}{2}$	+	π	-	Elev.
		934.93		
13100				30.1
T.P.	14.21	944.38	4.76	930.17
+ 50				30.6
14				31.2
+ 50				32.0
15				32.5
+ 45				32.8
16				33.1
+ 40	Field Entrance 12+			
+ 50				33.8
17				34.6
+ 50				35.2
18				35.7

Lt.

L

Rt.

$$\frac{41}{50} \quad \frac{52}{27} \quad \frac{74}{22} \quad \frac{74}{18} \quad \frac{56}{13} \quad \frac{48}{16} \quad \frac{54}{20} \quad \frac{72}{24} \quad \frac{58}{29} \quad \frac{50}{50}$$

$$\frac{149}{50} \quad \frac{135}{26} \quad \frac{134}{17} \quad \frac{123}{14} \quad \frac{118}{16} \quad \frac{123}{18} \quad \frac{135}{27} \quad \frac{108}{50}$$

$$\frac{153}{50} \quad \frac{135}{28} \quad \frac{140}{17} \quad \frac{119}{13} \quad \frac{112}{16} \quad \frac{115}{18} \quad \frac{131}{22} \quad \frac{131}{27} \quad \frac{118}{50}$$

$$\frac{146}{50} \quad \frac{127}{25} \quad \frac{136}{18} \quad \frac{113}{14} \quad \frac{104}{16} \quad \frac{112}{18} \quad \frac{123}{20} \quad \frac{123}{27} \quad \frac{114}{50}$$

$$\frac{141}{50} \quad \frac{123}{28} \quad \frac{123}{18} \quad \frac{107}{14} \quad \frac{99}{16} \quad \frac{103}{18} \quad \frac{115}{20} \quad \frac{115}{25} \quad \frac{106}{50}$$

$$\frac{149}{50} \quad \frac{117}{27} \quad \frac{121}{18} \quad \frac{102}{13} \quad \frac{96}{15} \quad \frac{102}{17} \quad \frac{111}{19} \quad \frac{111}{27} \quad \frac{104}{50}$$

$$\frac{161}{50} \quad \frac{140}{28} \quad \frac{135}{18} \quad \frac{97}{14} \quad \frac{93}{13} \quad \frac{96}{16} \quad \frac{101}{18} \quad \frac{101}{22} \quad \frac{97}{50}$$

$$\frac{21}{100}$$

$$\frac{137}{50} \quad \frac{115}{27} \quad \frac{110}{17} \quad \frac{91}{13} \quad \frac{86}{16} \quad \frac{86}{20} \quad \frac{86}{50}$$

$$\frac{124}{50} \quad \frac{90}{25} \quad \frac{90}{15} \quad \frac{82}{12} \quad \frac{78}{11} \quad \frac{82}{24} \quad \frac{83}{50}$$

$$\frac{121}{50} \quad \frac{91}{27} \quad \frac{89}{19} \quad \frac{75}{12} \quad \frac{72}{16} \quad \frac{74}{12} \quad \frac{56}{26} \quad \frac{58}{50}$$

$$\frac{91}{50} \quad \frac{63}{25} \quad \frac{66}{19} \quad \frac{73}{16} \quad \frac{68}{13} \quad \frac{67}{14} \quad \frac{68}{24} \quad \frac{37}{28} \quad \frac{18}{50}$$

Sta.	+	Σ	-	Elev.
		947.38		
18+33				36.0
+40	Field Entrance Lt.			
+63				35.9
19				35.9
+40				35.9
+85				35.7
20+36				36.3
+65				36.8
21				37.3
T.P.	9.78	947.24	4.97	937.46
+50				38.2
22				39.0
+70				39.8
23				39.9

L+

E

R+

$$\frac{4.1}{50} \quad \frac{4.0}{50} \quad \frac{4.1}{20} \quad \frac{6.5}{16} \quad \frac{6.4}{\cancel{16}} \quad \frac{6.6}{12} \quad \frac{5.2}{13} \quad \frac{2.2}{29} \quad \frac{2.2}{10}$$

$$\frac{5.7}{100}$$

$$\frac{4.7}{50} \quad \frac{4.6}{21} \quad \frac{6.5}{17} \quad \frac{6.5}{\cancel{17}} \quad \frac{6.9}{11} \quad \frac{5.6}{13} \quad \frac{2.6}{27} \quad \frac{2.6}{50}$$

$$\frac{8.4}{50} \quad \frac{8.4}{24} \quad \frac{8.3}{18} \quad \frac{7.2}{15} \quad \frac{6.5}{\cancel{15}} \quad \frac{6.7}{12} \quad \frac{5.9}{15} \quad \frac{3.6}{28} \quad \frac{3.9}{50}$$

$$\frac{12.3}{50} \quad \frac{14.3}{33} \quad \frac{13.5}{25} \quad \frac{7.9}{16} \quad \frac{6.5}{\cancel{16}} \quad \frac{7.0}{13} \quad \frac{8.5}{16} \quad \frac{8.5}{18} \quad \frac{2.7}{24} \quad \frac{7.0}{50}$$

$$\text{Pat Hole} \quad \frac{15.2}{50} \quad \frac{16.0}{32} \quad \frac{15.2}{26} \quad \frac{7.2}{13} \quad \frac{6.7}{\cancel{13}} \quad \frac{7.1}{14} \quad \frac{8.1}{17} \quad \frac{9.1}{19} \quad \frac{8.4}{25} \quad \frac{8.1}{50}$$

$$\frac{8.7}{50} \quad \frac{8.9}{30} \quad \frac{9.7}{25} \quad \frac{9.7}{20} \quad \frac{7.2}{16} \quad \frac{6.1}{\cancel{16}} \quad \frac{6.4}{13} \quad \frac{7.9}{17} \quad \frac{7.9}{22} \quad \frac{7.0}{25} \quad \frac{7.1}{39} \quad \frac{6.0}{50}$$

$$\frac{7.2}{50} \quad \frac{7.2}{22} \quad \frac{7.6}{20} \quad \frac{7.6}{18} \quad \frac{6.3}{15} \quad \frac{5.6}{\cancel{15}} \quad \frac{5.9}{12} \quad \frac{6.5}{16} \quad \frac{6.5}{18} \quad \frac{5.5}{24} \quad \frac{5.7}{32} \quad \frac{4.6}{50}$$

$$\frac{4.9}{50} \quad \frac{4.1}{40} \quad \frac{3.2}{23} \quad \frac{6.1}{18} \quad \frac{6.1}{17} \quad \frac{5.6}{14} \quad \frac{5.1}{\cancel{14}} \quad \frac{5.5}{12} \quad \frac{5.1}{16} \quad \frac{3.5}{25} \quad \frac{3.7}{50}$$

$$\frac{6.3}{50} \quad \frac{4.7}{28} \quad \frac{10.2}{19} \quad \frac{10.2}{17} \quad \frac{9.5}{14} \quad \frac{9.0}{\cancel{14}} \quad \frac{9.5}{12} \quad \frac{8.2}{17} \quad \frac{6.7}{24} \quad \frac{7.7}{50}$$

$$\frac{3.8}{50} \quad \frac{3.0}{30} \quad \frac{9.6}{22} \quad \frac{9.6}{18} \quad \frac{8.7}{14} \quad \frac{8.2}{\cancel{14}} \quad \frac{8.4}{12} \quad \frac{7.4}{14} \quad \frac{7.0}{18} \quad \frac{5.7}{24} \quad \frac{7.7}{50}$$

$$\frac{4.0}{50} \quad \frac{3.4}{28} \quad \frac{9.1}{21} \quad \frac{9.1}{18} \quad \frac{8.0}{14} \quad \frac{7.4}{\cancel{14}} \quad \frac{7.9}{12} \quad \frac{7.7}{16} \quad \frac{8.2}{27} \quad \frac{9.1}{39} \quad \frac{9.1}{50}$$

$$\frac{4.8}{50} \quad \frac{4.4}{29} \quad \frac{3.7}{28} \quad \frac{8.7}{22} \quad \frac{8.7}{18} \quad \frac{7.8}{13} \quad \frac{7.3}{\cancel{13}} \quad \frac{7.7}{12} \quad \frac{7.2}{23} \quad \frac{7.9}{50}$$

Sta.	+	-	Elev.
		947.24	

23+53			40.1
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24			40.2
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+50			40.3
-----	--	--	------

+85	Ents. Rt.		
-----	-----------	--	--

25			39.7
----	--	--	------

+50			38.8
-----	--	--	------

B.M.	4.8V	947.24	4.8V	944.4V
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+82	Ents. Rt.		
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26			37.5
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	1.81	939.00	10.05	937.19
--	------	--------	-------	--------

+39			36.6
-----	--	--	------

27			35.1
----	--	--	------

+39	Ents. Lt.		34.2
-----	-----------	--	------

28			32.8
----	--	--	------

Lt.

E

Rt.

 $\frac{54}{50}$ $\frac{62}{31}$ $\frac{70}{24}$ $\frac{80}{20}$ $\frac{90}{18}$ $\frac{26}{14}$ $\frac{71}{10}$ $\frac{76}{10}$ $\frac{64}{17}$ $\frac{51}{25}$ $\frac{48}{37}$ $\frac{35}{50}$
 $\frac{65}{50}$ $\frac{67}{38}$ $\frac{22}{28}$ $\frac{80}{19}$ $\frac{80}{15}$ $\frac{73}{13}$ $\frac{70}{13}$ $\frac{73}{13}$ $\frac{50}{18}$ $\frac{16}{33}$ $\frac{11}{50}$
 $\frac{77}{50}$ $\frac{35}{24}$ $\frac{73}{19}$ $\frac{25}{14}$ $\frac{69}{14}$ $\frac{72}{17}$ $\frac{67}{19}$ $\frac{54}{37}$ $\frac{31}{50}$ $\frac{25}{50}$
 $\frac{51}{50}$ $\frac{32}{100}$
 $\frac{11.0}{50}$ $\frac{52}{22}$ $\frac{73}{16}$ $\frac{79}{13}$ $\frac{75}{13}$ $\frac{80}{8}$ $\frac{76}{16}$ $\frac{48}{22}$ $\frac{38}{40}$ $\frac{41}{50}$
 $\frac{13.5}{50}$ $\frac{86}{20}$ $\frac{91}{16}$ $\frac{51}{14}$ $\frac{86}{17}$ $\frac{84}{9}$ $\frac{91}{17}$ $\frac{88}{21}$ $\frac{67}{27}$ $\frac{70}{46}$ $\frac{66}{50}$

Spike in R.P. 100" Rt. Stg. 25+30

 $\frac{75}{50}$ $\frac{67}{100}$
 $\frac{162}{50}$ $\frac{128}{22}$ $\frac{103}{14}$ $\frac{97}{14}$ $\frac{102}{9}$ $\frac{9.9}{17}$ $\frac{84}{20}$ $\frac{77}{50}$
 $\frac{85}{50}$ $\frac{58}{18}$ $\frac{31}{14}$ $\frac{24}{14}$ $\frac{28}{9}$ $\frac{24}{20}$ $\frac{31}{24}$ $\frac{11}{50}$
 $\frac{83}{50}$ $\frac{59}{17}$ $\frac{46}{14}$ $\frac{39}{10}$ $\frac{43}{10}$ $\frac{41}{15}$ $\frac{42}{23}$ $\frac{24}{50}$
 $\frac{122}{100}$ $\frac{90}{50}$ $\frac{52}{11}$ $\frac{48}{11}$ $\frac{52}{16}$ $\frac{48}{19}$ $\frac{33}{50}$
 $\frac{93}{50}$ $\frac{83}{17}$ $\frac{67}{11}$ $\frac{62}{13}$ $\frac{60}{13}$ $\frac{70}{17}$ $\frac{64}{23}$ $\frac{57}{34}$ $\frac{56}{50}$

Sta.	+	K	-	Elev.
		939.00		
28+50				31.7
29				30.7
+50				29.6
T.P.	1.42	930.77	9.65	929.35
30				28.7
31+02	12" C.M.			27.7
32				26.8
33				25.7
+65	Culr. 9" C.M.			25.1
34				25.0
35				25.6
36				25.8
T.P.	4.56	931.49	3.84	946.93

Lt.

C

Rt.

$$\frac{105}{50} \quad \frac{9.3}{16} \quad \frac{7.9}{12}$$

$$\frac{73}{14} \quad \frac{28}{14} \quad \frac{8.7}{24} \quad \frac{8.1}{50}$$

$$\frac{11.3}{50} \quad \frac{10.1}{18} \quad \frac{8.7}{13}$$

$$\frac{8.3}{17} \quad \frac{9.0}{17} \quad \frac{9.7}{19} \quad \frac{9.6}{50}$$

$$\frac{13.7}{50} \quad \frac{12.7}{17} \quad \frac{10.0}{13}$$

$$\frac{9.4}{15} \quad \frac{9.8}{15} \quad \frac{10.8}{19} \quad \frac{12.3}{50}$$

$$\frac{5.9}{50} \quad \frac{5.1}{16} \quad \frac{2.9}{13}$$

$$\frac{2.1}{14} \quad \frac{2.7}{17} \quad \frac{4.8}{25} \quad \frac{4.1}{50} \quad \frac{3.7}{50}$$

$$\frac{2.1}{50} \quad \frac{6.0}{18} \quad \frac{3.7}{13}$$

$$\frac{3.1}{14} \quad \frac{3.5}{17} \quad \frac{5.9}{17} \quad \frac{5.0}{22} \quad \frac{4.6}{50}$$

$$\frac{6.8}{50} \quad \frac{7.4}{19} \quad \frac{4.6}{14}$$

$$\frac{4.0}{12} \quad \frac{4.3}{18} \quad \frac{4.5}{34} \quad \frac{3.5}{50} \quad \frac{4.2}{50}$$

$$\frac{7.6}{50} \quad \frac{8.2}{18} \quad \frac{6.0}{14}$$

$$\frac{5.1}{12} \quad \frac{5.8}{18} \quad \frac{6.8}{33} \quad \frac{5.8}{50} \quad \frac{6.6}{50}$$

$$\frac{9.2}{50} \quad \frac{9.1}{18} \quad \frac{6.3}{14}$$

$$\frac{5.7}{13} \quad \frac{6.1}{17} \quad \frac{8.4}{17} \quad \frac{8.0}{50}$$

$$\frac{8.9}{50} \quad \frac{8.2}{18} \quad \frac{6.3}{14}$$

$$\frac{5.8}{12} \quad \frac{6.1}{18} \quad \frac{7.8}{50} \quad \frac{7.9}{50}$$

$$\frac{6.9}{50} \quad \frac{6.4}{20} \quad \frac{5.6}{15}$$

$$\frac{5.2}{11} \quad \frac{5.4}{16} \quad \frac{6.1}{16} \quad \frac{7.1}{50}$$

$$\frac{4.7}{50} \quad \frac{4.7}{15}$$

$$\frac{5.4}{11}$$

$$\frac{5.0}{9}$$

$$\frac{5.4}{11}$$

$$\frac{4.7}{15}$$

$$\frac{4.4}{15}$$

$$\frac{5.2}{30}$$

$$\frac{7.0}{50}$$

Nail in F.P. Rt. 36+00

Sta	+	π	-	Elev.
		931.49		

37				25.9
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+21	- 9" C.M.			25.9
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38				26.9
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39				26.9
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40				26.9
----	--	--	--	------

+33	Entr. Lt.			
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41				25.3
----	--	--	--	------

+49	9" C.M.			29.5
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B.M.	4.06	931.49	4.06	927.43
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B.M.	1.66	925.80	7.35	924.14
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42				24.1
----	--	--	--	------

+33	Entr. Rt.			
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43				22.3
----	--	--	--	------

Lt.

2

Rt.

$$\frac{6.3}{50} \quad \frac{5.8}{19} \quad \frac{6.0}{11} \quad \frac{5.6}{10} \quad \frac{5.7}{10} \quad \frac{6.6}{17} \quad \frac{7.2}{32} \quad \frac{7.4}{50}$$

$$\frac{7.1}{50} \quad \frac{7.0}{19} \quad \frac{7.8}{13} \quad \frac{6.0}{14} \quad \frac{5.6}{11} \quad \frac{5.9}{11} \quad \frac{8.1}{13} \quad \frac{8.5}{50} \quad \text{Orain Rt.}$$

$$\frac{5.6}{50} \quad \frac{5.1}{25} \quad \frac{5.4}{11} \quad \frac{5.1}{14} \quad \frac{5.3}{14} \quad \frac{5.1}{29} \quad \frac{6.6}{50}$$

$$\frac{5.2}{50} \quad \frac{4.1}{32} \quad \frac{4.0}{21} \quad \frac{5.1}{12} \quad \frac{4.6}{11} \quad \frac{5.1}{9} \quad \frac{5.1}{14} \quad \frac{4.5}{14} \quad \frac{3.4}{30} \quad \frac{4.8}{50}$$

$$\frac{6.1}{50} \quad \frac{5.8}{22} \quad \frac{5.9}{17} \quad \frac{5.9}{15} \quad \frac{5.4}{13} \quad \frac{5.1}{11} \quad \frac{5.6}{14} \quad \frac{4.9}{16} \quad \frac{4.4}{30} \quad \frac{5.4}{50}$$

$$\frac{7.7}{100} \quad \frac{6.5}{50}$$

$$\frac{8.7}{50} \quad \frac{8.4}{30} \quad \frac{8.4}{21} \quad \frac{7.7}{16} \quad \frac{6.6}{13} \quad \frac{6.2}{11} \quad \frac{6.5}{13} \quad \frac{7.2}{16} \quad \frac{7.0}{50}$$

$$\frac{10.9}{50} \quad \frac{9.1}{21} \quad \frac{9.4}{15} \quad \frac{7.5}{13} \quad \frac{7.0}{11} \quad \frac{7.1}{14} \quad \frac{8.4}{16} \quad \frac{7.2}{23} \quad \frac{6.2}{50}$$

S.W. Cor. of Bench 75' Rt. Sta. 41+50

U.S.G.S. Bench - Sta. # W. 1 - 25' Rt. Sta. 42+95

$$\frac{5.1}{50} \quad \frac{2.5}{16} \quad \frac{2.6}{14} \quad \frac{2.2}{11} \quad \frac{1.7}{11} \quad \frac{2.0}{19} \quad \frac{1.4}{23} \quad \frac{1.0}{30} \quad \frac{1.1}{50}$$

$$\frac{2.1}{30} \quad \frac{1.8}{50} \quad \frac{1.0}{75}$$

$$\frac{5.4}{50} \quad \frac{3.7}{17} \quad \frac{4.2}{14} \quad \frac{3.5}{11} \quad \frac{3.9}{14} \quad \frac{2.1}{21} \quad \frac{2.3}{50}$$

Sta.	+	K	-	Elev.
		925.80		
44				20.0
45				16.7
T.P.	0.88	916.37	10.31	915.49
46				13.7
47				10.8
48				07.4
T.P.	1.98	906.61	11.74	904.63
49				03.8
50				00.9
+60				899.6
51				98.9
+75 = 9" C.M.				97.8
52				97.7
B.M.	2.11	900.89	8.23	898.38
+80				97.0
				Co. Rd. H. on Lt.

Lt.

E

Rt.

$$\frac{9.0}{50} \quad \frac{6.9}{22}$$

$$\frac{5.8}{50} \quad \frac{6.3}{13} \quad \frac{7.0}{14} \quad \frac{7.0}{16} \quad \frac{4.9}{19} \quad \frac{4.1}{50}$$

$$\frac{13.5}{50} \quad \frac{11.0}{20} \quad \frac{11.0}{18} \quad \frac{9.7}{15} \quad \frac{9.1}{12} \quad \frac{9.4}{14} \quad \frac{9.9}{14} \quad \frac{9.9}{15} \quad \frac{8.3}{19} \quad \frac{7.4}{50}$$

$$\frac{2.6}{50} \quad \frac{5.2}{21} \quad \frac{3.5}{17} \quad \frac{2.7}{17} \quad \frac{3.3}{8} \quad \frac{2.8}{14} \quad \frac{3.2}{14} \quad \frac{1.4}{50}$$

$$\frac{9.4}{50} \quad \frac{2.6}{22} \quad \frac{6.3}{19}$$

$$\frac{5.6}{50} \quad \frac{6.0}{13} \quad \frac{7.2}{19} \quad \frac{6.8}{21} \quad \frac{4.0}{33} \quad \frac{2.5}{50}$$

$$\frac{11.6}{50} \quad \frac{10.8}{25} \quad \frac{9.8}{18} \quad \frac{9.0}{15} \quad \frac{9.5}{15} \quad \frac{10.5}{18} \quad \frac{10.6}{22} \quad \frac{8.0}{35} \quad \frac{7.3}{50}$$

$$\frac{5.7}{50} \quad \frac{4.7}{26} \quad \frac{3.4}{19} \quad \frac{2.8}{17} \quad \frac{3.2}{14} \quad \frac{5.2}{18} \quad \frac{5.1}{21} \quad \frac{4.4}{27} \quad \frac{2.0}{42} \quad \frac{1.4}{50}$$

$$\frac{8.2}{50} \quad \frac{2.7}{25} \quad \frac{2.4}{18} \quad \frac{6.4}{14} \quad \frac{5.7}{13} \quad \frac{5.9}{13} \quad \frac{7.8}{17} \quad \frac{7.0}{25} \quad \frac{6.0}{50}$$

$$\frac{10.5}{50} \quad \frac{9.9}{19} \quad \frac{7.8}{11} \quad \frac{7.0}{17} \quad \frac{7.4}{13} \quad \frac{8.7}{17} \quad \frac{9.1}{30} \quad \frac{8.2}{35} \quad \frac{7.7}{50}$$

$$\frac{9.4}{50} \quad \frac{9.2}{28} \quad \frac{11.0}{23} \quad \frac{11.0}{20} \quad \frac{8.4}{14} \quad \frac{7.7}{13} \quad \frac{8.2}{13} \quad \frac{9.7}{18} \quad \frac{9.9}{29} \quad \frac{9.0}{31} \quad \frac{9.0}{10}$$

School yard

Lx.

$$\frac{9.1}{50} \quad \frac{9.4}{27} \quad \frac{10.9}{22} \quad \frac{12.1}{18} \quad \frac{9.4}{14} \quad \frac{8.8}{13} \quad \frac{9.1}{13} \quad \frac{11.1}{21} \quad \frac{11.1}{50}$$

$$\frac{9.1}{50} \quad \frac{9.1}{27} \quad \frac{9.6}{18} \quad \frac{8.9}{15} \quad \frac{9.4}{15} \quad \frac{11.0}{19} \quad \frac{11.0}{26} \quad \frac{11.2}{50}$$

NE Cor. Bottom Step of School House 75' Lt. Sts.

52 + 38

$$\frac{3.9}{50} \quad \frac{3.0}{50} \quad \frac{2.4}{100}$$

Sta.	+	π	-	Elev.
53		900.89		96.7
54				99.9
55				93.1
56				91.6
56+70	24" C.M.			91.2
57				91.0
+45				90.8
T.P.	4.15	895.42	10.04	890.87
58				90.8
59				90.7
60				90.4
61				89.8
188	9" C.M.			89.2
62+30	Field Ent Lt.			89.2

Lr.

2

Rt.

$$\frac{2^2}{50} \quad \frac{3^2}{42} \quad \frac{4^3}{22} \quad \frac{4^2}{\cancel{12}} \quad \frac{4^5}{12} \quad \frac{6^0}{17} \quad \frac{6^0}{19} \quad \frac{1^0}{23} \quad \frac{5^5}{50}$$

$$\frac{4^4}{50} \quad \frac{5^4}{36} \quad \frac{6^4}{27} \quad \frac{6^4}{17} \quad \frac{6^0}{\cancel{16}} \quad \frac{6^4}{16} \quad \frac{7^6}{19} \quad \frac{7^6}{21} \quad \frac{6^7}{23} \quad \frac{7^7}{50}$$

$$\frac{7^7}{50} \quad \frac{8^4}{34} \quad \frac{9^2}{25} \quad \frac{8^7}{18} \quad \frac{8^4}{13} \quad \frac{7^8}{\cancel{14}} \quad \frac{8^5}{14} \quad \frac{9^3}{16} \quad \frac{10^0}{26} \quad \frac{10^5}{50}$$

$$\frac{12^1}{50} \quad \frac{12^2}{27} \quad \frac{11^6}{16} \quad \frac{10^0}{13} \quad \frac{9^3}{\cancel{12}} \quad \frac{9^6}{12} \quad \frac{12^4}{26} \quad \frac{12^0}{28} \quad \frac{12^3}{34} \quad \frac{12^0}{50}$$

$$\frac{13^3}{50} \quad \frac{13^6}{27} \quad \frac{12^1}{\cancel{18}} \quad \frac{13^7}{18} \quad \frac{10^7}{15} \quad \frac{9^7}{\cancel{15}} \quad \frac{10^3}{15} \quad \frac{12^1}{\cancel{23}} \quad \frac{13^5}{23} \quad \frac{13^9}{25} \quad \frac{11^7}{29} \quad \frac{12^3}{\cancel{50}}$$

$$\frac{12^4}{50} \quad \frac{12^4}{17} \quad \frac{10^7}{14} \quad \frac{9^9}{\cancel{14}} \quad \frac{10^4}{14} \quad \frac{12^6}{22} \quad \frac{13^9}{23} \quad \frac{13^9}{25} \quad \frac{12^2}{27} \quad \frac{12^5}{37} \quad \frac{12^3}{50}$$

$$\frac{11^5}{50} \quad \frac{11^7}{20} \quad \frac{10^0}{17} \quad \frac{10^1}{\cancel{12}} \quad \frac{10^5}{12} \quad \frac{12^3}{23} \quad \frac{14^3}{26} \quad \frac{14^3}{28} \quad \frac{12^4}{31} \quad \frac{12^6}{50}$$

Ditch L Rt

$$\frac{5^0}{50} \quad \frac{4^9}{40} \quad \frac{5^7}{20} \quad \frac{5^1}{12} \quad \frac{4^6}{\cancel{12}} \quad \frac{5^0}{13} \quad \frac{6^5}{24} \quad \frac{6^9}{29} \quad \frac{7^6}{47} \quad \frac{7^9}{43} \quad \frac{8^6}{66} \quad \frac{7^8}{68} \quad \frac{7^8}{69} \quad \frac{8^4}{94}$$

$$\frac{5^7}{50} \quad \frac{2^9}{33} \quad \frac{4^0}{21} \quad \frac{5^0}{11} \quad \frac{4^7}{\cancel{14}} \quad \frac{5^3}{14} \quad \frac{6^2}{21} \quad \frac{8^1}{50}$$

$$\frac{2^3}{50} \quad \frac{2^5}{31} \quad \frac{3^0}{28} \quad \frac{4^3}{18} \quad \frac{5^0}{14} \quad \frac{5^3}{11} \quad \frac{5^0}{\cancel{12}} \quad \frac{5^5}{11} \quad \frac{6^4}{26} \quad \frac{8^0}{50}$$

$$\frac{2^4}{50} \quad \frac{3^0}{34} \quad \frac{5^0}{22} \quad \frac{5^0}{17} \quad \frac{6^2}{14} \quad \frac{5^6}{\cancel{14}} \quad \frac{6^0}{11} \quad \frac{6^6}{16} \quad \frac{8^3}{50}$$

$$\frac{4^6}{50} \quad \frac{5^8}{26} \quad \frac{6^3}{21} \quad \frac{7^3}{16} \quad \frac{6^6}{11} \quad \frac{6^2}{\cancel{12}} \quad \frac{6^6}{10} \quad \frac{8^2}{12} \quad \frac{9^4}{50}$$

$$\frac{3^5}{100} \quad \frac{5^6}{50} \quad \frac{6^4}{12} \quad \frac{6^2}{\cancel{12}} \quad \frac{6^7}{9} \quad \frac{8^2}{14} \quad \frac{9^1}{20} \quad \frac{9^7}{50}$$

Sta.	+	π	-	Elev.
		895.42		
63				88.6
+54	12" C.M.			88.6
64				88.9
65				88.4
B.M.	8.95	895.42	8.95	886.47
T.P.	2.96	891.12	7.26	888.16
65+88	Field Ent. Rt.			
66				88.1
67				87.7
68+03	12" C.M.			86.3
69				86.1
70				86.5
71				86.2
72				86.1

Lt.

E

Rt.

$$\begin{array}{ccccccc}
 \frac{72}{50} & \frac{77}{29} & \frac{73}{17} & \frac{68}{\cancel{17}} & \frac{72}{9} & \frac{70}{14} & \frac{96}{19} & \frac{100}{50} \\
 & & \text{Inv.} & & & & \text{Inv.} & \\
 \frac{74}{50} & \frac{77}{27} & \frac{86}{19} & \frac{74}{16} & \frac{68}{\cancel{17}} & \frac{73}{8} & \frac{87}{12} & \frac{103}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{74}{50} & \frac{73}{27} & \frac{72}{11} & \frac{70}{\cancel{17}} & & \frac{75}{9} & \frac{93}{11} & \frac{102}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{61}{50} & \frac{69}{24} & \frac{76}{15} & \frac{70}{\cancel{17}} & \frac{74}{9} & \frac{89}{16} & \frac{95}{42} & \frac{96}{50}
 \end{array}$$

Sp. No. in NW. Cor. of Barn 300' Rt. 66 + 21

$$\begin{array}{ccccccc}
 \frac{15}{50} & \frac{16}{45} & \frac{29}{33} & \frac{31}{24} & \frac{32}{17} & \frac{30}{\cancel{17}} & \frac{36}{9} & \frac{44}{18} & \frac{40}{25} & \frac{46}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{44}{50} & \frac{52}{32} & \frac{46}{21} & \frac{39}{16} & \frac{34}{\cancel{17}} & \frac{39}{11} & \frac{50}{16} & \frac{50}{18} & \frac{42}{26} & \frac{48}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{56}{50} & \frac{65}{36} & \frac{66}{25} & \frac{76}{21} & \frac{53}{17} & \frac{48}{\cancel{17}} & \frac{54}{9} & \frac{82}{12} & \frac{83}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{52}{50} & \frac{64}{32} & \frac{62}{19} & \frac{56}{18} & \frac{50}{\cancel{17}} & \frac{57}{9} & \frac{79}{15} & \frac{87}{38} & \frac{86}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{38}{50} & \frac{50}{33} & \frac{53}{26} & \frac{48}{18} & \frac{46}{\cancel{17}} & & \frac{53}{10} & \frac{70}{18} & \frac{82}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{41}{50} & \frac{47}{27} & \frac{53}{21} & \frac{50}{17} & \frac{49}{\cancel{17}} & \frac{57}{10} & \frac{74}{16} & \frac{87}{44} & \frac{88}{50}
 \end{array}$$

$$\begin{array}{ccccccc}
 \frac{48}{50} & \frac{50}{23} & \frac{62}{14} & \frac{50}{\cancel{17}} & \frac{57}{9} & \frac{78}{16} & \frac{89}{50}
 \end{array}$$

Sts.	+	π	-	Elev.
		891.12		

73				86.5
----	--	--	--	------

74				86.4
----	--	--	--	------

+ 12	24" Vit. Tile Pipe, 54' Long			
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74+50				87.0
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T.P.	9.20	896.21	4.11	887.01
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75				87.4
----	--	--	--	------

76				88.6
----	--	--	--	------

77				90.0
----	--	--	--	------

+ 50				90.6
------	--	--	--	------

78				91.2
----	--	--	--	------

79				92.3
----	--	--	--	------

+ 27	Field Entry Rt.			
------	-----------------	--	--	--

80				92.5
----	--	--	--	------

Lt.

E

Rt.

$$\frac{3.9}{50}$$

$$\frac{4.7}{22}$$

$$\frac{5.3}{19}$$

$$\frac{4.6}{50}$$

$$\frac{5.1}{11}$$

$$\frac{6.9}{18}$$

$$\frac{8.6}{50}$$

$$\frac{5.5}{50}$$

$$\frac{5.6}{23}$$

$$\frac{6.3}{18}$$

$$\frac{5.2}{14}$$

$$\frac{4.7}{50}$$

$$\frac{5.3}{10}$$

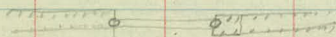
$$\frac{8.2}{19}$$

$$\frac{8.4}{28}$$

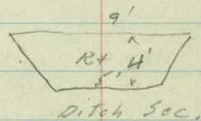
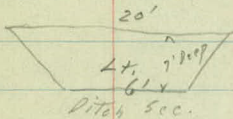
$$\frac{7.9}{34}$$

$$\frac{8.4}{50}$$

$$\frac{14.1}{12.8}$$



$$\frac{14.1}{12.3}$$



$$\frac{5.1}{50}$$

$$\frac{6.2}{27}$$

$$\frac{5.5}{20}$$

$$\frac{4.6}{15}$$

$$\frac{4.1}{50}$$

$$\frac{4.7}{12}$$

$$\frac{6.7}{21}$$

$$\frac{7.1}{41}$$

$$\frac{7.6}{50}$$

$$\frac{9.4}{50}$$

$$\frac{9.2}{29}$$

$$\frac{10.1}{21}$$

$$\frac{9.6}{17}$$

$$\frac{9.8}{16}$$

$$\frac{9.8}{13}$$

$$\frac{9.4}{11}$$

$$\frac{8.8}{50}$$

$$\frac{9.3}{11}$$

$$\frac{10.5}{16}$$

$$\frac{11.2}{50}$$

$$\frac{6.7}{50}$$

$$\frac{7.2}{26}$$

$$\frac{7.0}{18}$$

$$\frac{8.3}{14}$$

$$\frac{8.1}{11}$$

$$\frac{7.6}{50}$$

$$\frac{8.0}{11}$$

$$\frac{9.0}{17}$$

$$\frac{9.9}{50}$$

$$\frac{4.4}{50}$$

$$\frac{2.7}{25}$$

$$\frac{3.4}{22}$$

$$\frac{7.0}{17}$$

$$\frac{6.6}{11}$$

$$\frac{6.2}{50}$$

$$\frac{6.6}{50}$$

$$\frac{6.6}{18}$$

$$\frac{6.9}{50}$$

$$\frac{3.6}{50}$$

$$\frac{2.4}{21}$$

$$\frac{6.7}{17}$$

$$\frac{6.1}{11}$$

$$\frac{5.6}{50}$$

$$\frac{6.0}{11}$$

$$\frac{5.2}{18}$$

$$\frac{5.0}{50}$$

$$\frac{3.0}{50}$$

$$\frac{3.1}{36}$$

$$\frac{1.8}{23}$$

$$\frac{6.0}{17}$$

$$\frac{5.7}{12}$$

$$\frac{5.0}{50}$$

$$\frac{5.4}{12}$$

$$\frac{5.0}{16}$$

$$\frac{5.2}{50}$$

$$\frac{3.0}{50}$$

$$\frac{3.1}{39}$$

$$\frac{2.4}{24}$$

$$\frac{5.5}{18}$$

$$\frac{5.0}{12}$$

$$\frac{3.9}{50}$$

$$\frac{4.1}{10}$$

$$\frac{4.7}{16}$$

$$\frac{4.0}{19}$$

$$\frac{5.3}{27}$$

$$\frac{5.4}{50}$$

↑ as above

$$\frac{3.5}{50}$$

$$\frac{3.5}{16}$$

$$\frac{4.6}{14}$$

$$\frac{4.2}{11}$$

$$\frac{3.7}{50}$$

$$\frac{4.4}{14}$$

$$\frac{4.1}{17}$$

$$\frac{4.1}{50}$$

Sta.	+	Σ	-	Elev.
		896.21		
81				92.1
+ T.P.	3.58	896.73	3.06	893.15
82				91.9
+80				91.6
83			Drive L	+ 91.7
84				92.0
B.M.	0.01	896.73	0.01	896.72
+60			Drive R	+ 92.2
85				92.6
86				92.2
87				92.9
88				93.2
T.P.	5.10	898.34	3.49	893.24
89				93.1
90				93.6
+50				93.7

Lt.

±

Rt.

$$\frac{5.5}{50} \quad \frac{5.1}{45} \quad \frac{4.4}{17} \quad \frac{4.6}{10} \quad \frac{4.1}{\cancel{10}} \quad \frac{4.6}{14} \quad \frac{3.6}{22} \quad \frac{2.9}{50}$$

Nail in oak 20' Lt 81+10

$$\frac{5.0}{50} \quad \frac{4.8}{24} \quad \frac{4.7}{19} \quad \frac{5.9}{14} \quad \frac{5.5}{10} \quad 4.8 \quad \frac{5.3}{13} \quad \frac{4.9}{27} \quad \frac{4.8}{50}$$

$$\frac{5.7}{50} \quad \frac{6.7}{32} \quad \frac{6.5}{20} \quad \frac{7.1}{22} \quad \frac{7.2}{16} \quad \frac{5.4}{11} \quad 5.1 \quad \frac{5.7}{16} \quad \frac{8.0}{21} \quad \frac{7.2}{27} \quad \frac{8.9}{35} \quad \frac{7.8}{50}$$

$$\frac{4.2}{100} \quad \frac{5.6}{50} \quad \frac{6.1}{32} \quad \frac{5.2}{11} \quad 5.0 \quad \frac{5.8}{14} \quad \frac{8.0}{28} \quad \frac{6.7}{42} \quad \frac{6.5}{50}$$

$$\frac{2.2}{50} \quad \frac{2.2}{27} \quad \frac{1.7}{21} \quad \frac{4.9}{11} \quad 4.7 \quad \frac{5.6}{17} \quad \frac{3.4}{26} \quad \frac{2.5}{50}$$

Top Comp. Pier WRT 84+30

$$\frac{3.8}{50} \quad \frac{4.1}{34} \quad \frac{4.2}{28} \quad \frac{3.6}{24} \quad \frac{4.1}{12} \quad \frac{4.8}{8} \quad \pm \quad \frac{4.5}{12} \quad \frac{4.9}{50} \quad \frac{3.9}{50} \quad \frac{2.6}{100}$$

$$\frac{5.0}{50} \quad \frac{5.4}{34} \quad \frac{4.9}{26} \quad \frac{4.2}{15} \quad \frac{3.2}{13} \quad \frac{4.7}{8} \quad 4.1 \quad \frac{5.0}{12} \quad \frac{6.0}{26} \quad \frac{6.1}{45} \quad \frac{5.7}{50}$$

$$\frac{5.2}{50} \quad \frac{5.0}{29} \quad \frac{4.1}{23} \quad \frac{4.1}{14} \quad \frac{4.7}{8} \quad 4.5 \quad \frac{4.6}{11} \quad \frac{4.3}{14} \quad \frac{5.1}{22} \quad \frac{4.7}{28} \quad \frac{4.4}{50}$$

$$\frac{4.4}{50} \quad \frac{3.9}{32} \quad \frac{2.0}{18} \quad \frac{2.7}{11} \quad \frac{4.0}{8} \quad 3.8 \quad \frac{4.2}{12} \quad \frac{3.5}{16} \quad \frac{3.3}{25} \quad \frac{2.2}{28} \quad \frac{2.5}{50}$$

$$\frac{5.2}{50} \quad \frac{3.8}{24} \quad \frac{3.7}{16} \quad 3.5 \quad \frac{3.9}{12} \quad \frac{4.0}{22} \quad \frac{3.5}{25} \quad \frac{3.2}{50}$$

$$\frac{6.4}{50} \quad \frac{6.2}{21} \quad \frac{6.7}{18} \quad \frac{5.8}{11} \quad 5.2 \quad \frac{5.7}{14} \quad \frac{5.5}{16} \quad \frac{6.7}{24} \quad \frac{5.5}{29} \quad \frac{4.5}{50}$$

$$\frac{4.3}{50} \quad \frac{3.0}{20} \quad \frac{5.3}{13} \quad 4.7 \quad \frac{5.0}{15} \quad \frac{4.3}{50}$$

$$\frac{3.6}{50} \quad \frac{2.9}{28} \quad \frac{1.7}{20} \quad \frac{5.0}{12} \quad 4.6 \quad \frac{5.1}{15} \quad \frac{4.9}{50}$$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		898.34		
--	--	--------	--	--

91				93.5
----	--	--	--	------

92				93.3
----	--	--	--	------

+39		Drive Rt		93.6
-----	--	----------	--	------

93				93.4
----	--	--	--	------

94				93.6
----	--	--	--	------

95				94.8
----	--	--	--	------

+50				95.5
-----	--	--	--	------

96				96.3
----	--	--	--	------

T.P	8.24	905.04	1.54	896.80
-----	------	--------	------	--------

97				97.4
----	--	--	--	------

98				99.0
----	--	--	--	------

+50				99.7
-----	--	--	--	------

99				900.2
----	--	--	--	-------

Lt.

E

Rt

$$\frac{3.6}{50} \quad \frac{3.2}{27} \quad \frac{2.1}{20} \quad \frac{4.9}{13} \quad 48 \quad \frac{5.2}{12} \quad \frac{5.7}{30}$$

$$\frac{5.0}{30} \quad \frac{4.5}{24} \quad \frac{5.5}{13} \quad 50 \quad \frac{5.1}{11} \quad \frac{5.9}{14} \quad \frac{5.9}{30}$$

$$\frac{4.8}{50} \quad \frac{4.7}{26} \quad \frac{5.7}{14} \quad 47 \quad \frac{4.9}{13} \quad \frac{4.7}{30} \quad \frac{5.1}{100}$$

$$\frac{5.3}{30} \quad \frac{5.8}{30} \quad \frac{5.5}{16} \quad 49 \quad \frac{5.4}{13} \quad \frac{5.2}{15} \quad \frac{6.4}{28} \quad \frac{6.2}{39} \quad \frac{7.1}{46} \quad \frac{6.6}{50}$$

$$\frac{7.8}{30} \quad \frac{7.5}{19} \quad \frac{5.2}{14} \quad 4.7 \quad \frac{5.3}{13} \quad \frac{6.3}{19} \quad \frac{7.0}{30}$$

$$\frac{6.0}{30} \quad \frac{5.7}{19} \quad \frac{4.2}{14} \quad 3.5 \quad \frac{4.1}{13} \quad \frac{4.7}{16} \quad \frac{5.8}{30}$$

$$\frac{2.8}{50} \quad \frac{2.5}{17} \quad \frac{3.2}{13} \quad 28 \quad \frac{3.0}{10} \quad \frac{2.3}{13} \quad \frac{4.5}{47} \quad \frac{4.4}{30}$$

$$\frac{1.7}{50} \quad \frac{1.8}{20} \quad \frac{2.8}{16} \quad 20 \quad \frac{1.7}{13} \quad \frac{3.6}{50}$$

$$\frac{6.5}{50} \quad \frac{7.1}{19} \quad \frac{8.4}{16} \quad 7.6 \quad \frac{7.8}{9} \quad \frac{7.2}{13} \quad \frac{7.7}{17} \quad \frac{9.1}{50}$$

$$\frac{4.0}{50} \quad \frac{4.2}{21} \quad \frac{6.7}{15} \quad 6.0 \quad \frac{6.4}{8} \quad \frac{5.5}{15} \quad \frac{6.0}{30}$$

$$\frac{3.9}{50} \quad \frac{4.1}{20} \quad \frac{6.2}{15} \quad 53 \quad \frac{5.6}{8} \quad \frac{4.8}{13} \quad \frac{4.2}{36} \quad \frac{4.6}{50}$$

$$\frac{3.6}{50} \quad \frac{3.5}{20} \quad \frac{5.7}{15} \quad 48 \quad \frac{5.2}{8} \quad \frac{4.4}{12} \quad \frac{3.3}{36} \quad \frac{3.5}{50}$$

Sta.	+	Σ	-	Elev.
		905.04		
100				00.3
101				99.9
102				99.9
+65				99.5
103				99.5
104				99.7
T.P	5.59	905.33	5.30	899.74
105				00.0
+29				00.1
+35				00.2
+47				00.2
+61.40				00.5
B.M			3.76	901.57
				(901.61)

Lt.

E

Rt.

$$\frac{4.5}{50} \quad \frac{4.4}{19} \frac{5.6}{16} \quad 4.7 \quad \frac{4.5}{12} \quad \frac{4.0}{38} \quad \frac{4.5}{50}$$

$$\frac{4.2}{50} \quad \frac{5.1}{20} \frac{5.7}{16} \quad 5.1 \quad \frac{5.6}{13} \quad \frac{5.9}{50}$$

$$\frac{6.6}{50} \frac{5.8}{15} \quad 5.1 \quad \frac{5.8}{13} \frac{6.8}{15} \quad \frac{7.0}{40} \quad \frac{7.1}{50}$$

$$\frac{9.3}{30} \quad \frac{9.5}{24} \frac{8.8}{18} \quad \frac{6.0}{13} \quad 5.5 \quad \frac{6.2}{12} \quad \frac{7.7}{15} \quad \frac{7.3}{32} \quad \frac{7.5}{50}$$

$$\frac{9.1}{50} \frac{8.5}{17} \quad \frac{6.5}{13} \quad 5.5 \quad \frac{6.2}{13} \quad \frac{7.6}{18} \quad \frac{7.3}{14} \quad \frac{7.5}{50}$$

$$\frac{7.0}{50} \quad \frac{7.0}{26} \quad \frac{6.2}{13} \quad 5.3 \quad \frac{5.9}{13} \quad \frac{7.0}{20} \quad \frac{7.4}{50}$$

$$\frac{6.1}{50} \quad \frac{6.1}{31} \quad \frac{6.1}{15} \frac{5.7}{12} \quad 5.3 \quad \frac{5.4}{16} \quad \frac{6.0}{19} \quad \frac{6.6}{36} \quad \frac{7.4}{50}$$

$$\frac{5.5}{50} \quad \frac{5.9}{31} \quad \frac{5.6}{15} \quad 5.2 \quad \frac{5.5}{10} \quad \frac{5.2}{14} \quad \frac{6.8}{38} \quad \frac{6.5}{50}$$

$$\frac{6.9}{50} \quad \frac{6.7}{42} \quad \frac{5.7}{33} \quad \frac{5.5}{20} \quad 5.1 \quad \frac{5.5}{17} \quad \frac{7.2}{21} \quad \frac{7.1}{50}$$

$$\frac{5.2}{50} \quad \frac{5.3}{50} \quad 5.1 \quad \frac{5.0}{50}$$

$$\frac{4.9}{200} \quad \frac{4.8}{50} \quad 4.8 \quad \frac{4.6}{50} \quad \frac{4.4}{100}$$

Spk in 18" Oak 33' Lt Sta 105+20

Sto.

+

π

-

Elev.

Bench Levels

Mounds View Rd.

Co Rd "G" To Co Rd I

3/25/37

Wilke π

Gillert Road

	+	A	-	How	
	5.68	921.52			915.84

	11.78	932.74	0.56	920.96	
--	-------	--------	------	--------	--

	8.74	940.03	1.45	931.29	
--	------	--------	------	--------	--

	4.78	944.04	0.77	939.26	
--	------	--------	------	--------	--

B.M	1.62	944.04	1.62	942.42	
-----	------	--------	------	--------	--

	0.85	931.74	13.15	931.89	
--	------	--------	-------	--------	--

	6.10	931.85	5.99	925.75	
--	------	--------	------	--------	--

B.M	4.42	931.85	4.42	927.43	
-----	------	--------	------	--------	--

	0.14	921.28	10.71	921.14	
--	------	--------	-------	--------	--

	0.65	910.21	11.72	909.56	
--	------	--------	-------	--------	--

B.M	1.57	899.95	11.83	898.38	898.53
-----	------	--------	-------	--------	--------

	2.88	894.11	8.72	891.23	
--	------	--------	------	--------	--

B.M	7.64	894.11	7.64	886.47	
-----	------	--------	------	--------	--

	3.17	891.27	6.01	888.10	
--	------	--------	------	--------	--

	7.88	894.39	4.76	886.51	
--	------	--------	------	--------	--

	4.58	896.90	2.07	892.32	
--	------	--------	------	--------	--

B.M	0.18	896.90	0.18	896.72	
-----	------	--------	------	--------	--

	5.52	898.55	3.87	893.03	
--	------	--------	------	--------	--

	8.55	904.78	2.32	896.23	
--	------	--------	------	--------	--

	5.15	905.30	4.63	900.13	
--	------	--------	------	--------	--

B.M			3.73	901.57	901.61
-----	--	--	------	--------	--------

↑
wrong

Description

SpK in 30" Maple N.E Cor M.V. Rd. + STA #10

SpK in P.P. 100' Rt Sta 25+30

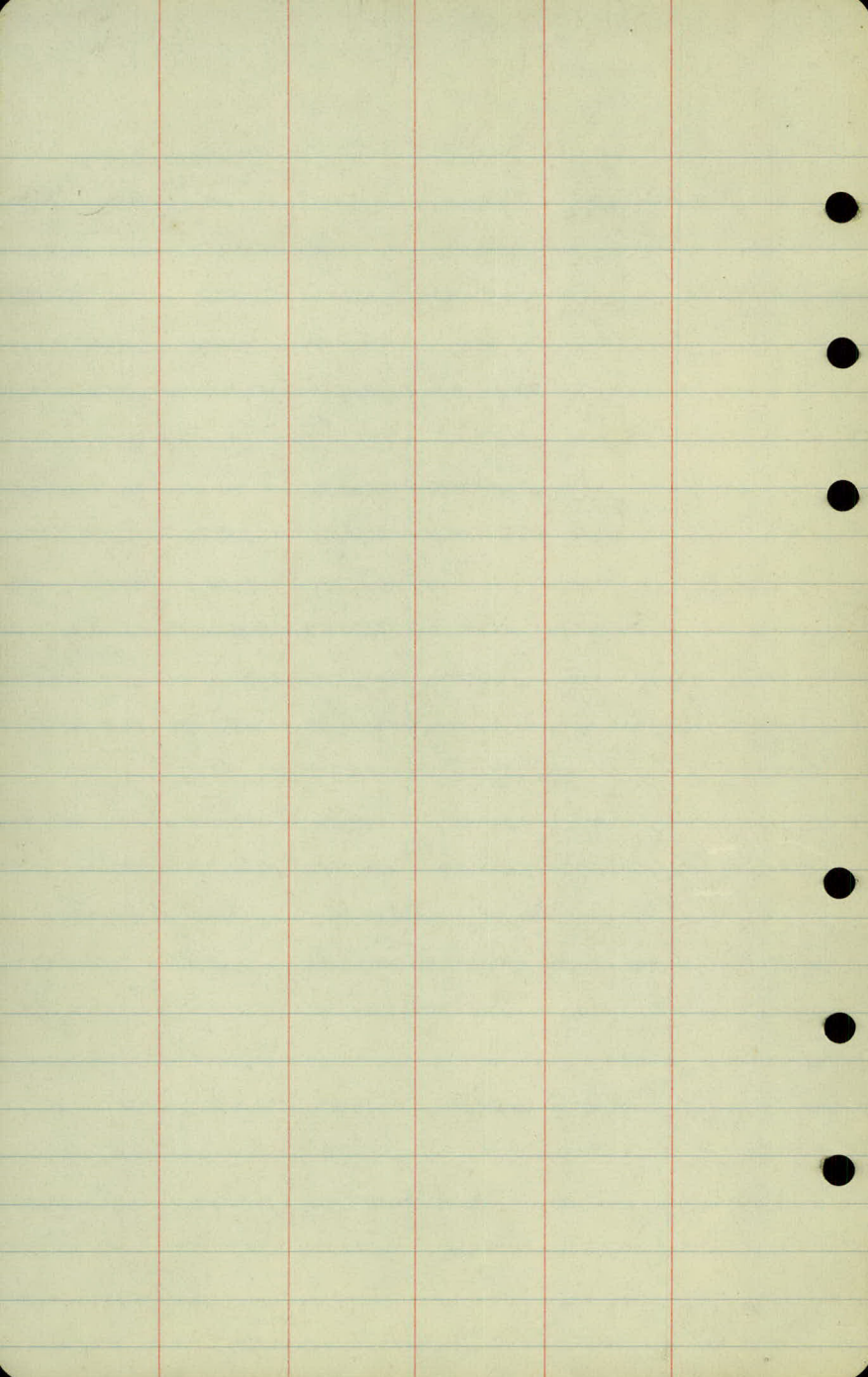
S.W. Cor Porch 100' Rt Sta 41+50

N.E Cor bottom step sch House, S.W. Cor M.V. Rd + "H"

SpK in N.W Cor, Barn.

Top S.W. Cor. Conc Step. Pier, Bottom

SpK in Tree 18" O.K. 33' Lt Sta 105+20





St. Paul Corrugating Co.

ST. PAUL, MINN.

Sheet Metal Products

IF YOU NEED THESE
YOU NEED US

Culverts

"Gohi" (C. B. Pure Iron)

"USS" Pure Iron

"USS" Copper Steel

"K.C.B." Copper Steel

Corrugated Cattle Passes

Corrugated Well Curbing

Anti-Washout Strip

Ridge Roll

Hip Shingles

Metal Valleys

Eaves Trough

Conductor Pipe

Fittings

Gutters

Building Corners

Metal Lath

Corner Beads

Metal Roofings (All Styles)

Metal Sidings

"Gohi" C. B. Pure Iron
Sheets

"Copper Alloy" Steel Sheets

Galvanized Sheets

Black Sheets

Skylights

Ventilators

Steel Ceilings

Galvanizing (Hot Dip)

Steel Roof Decking

Lux-Right Metal Areawalls

1843.89
157.03
633.30
2634.22

159.09
3
155.3

HARRY C. NORD

Sales Representative

PHONES: RIVERVIEW 3703, 8704, 3705, and NESTOR 2255

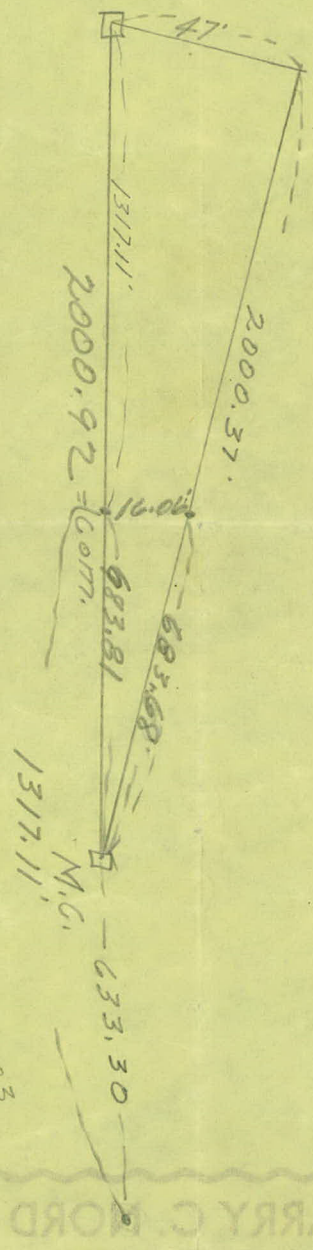
22+11
612+52
794312

St. Paul Corrugating Co.
ST. PAUL, MINN.
Sheet Metal Products



IF YOU NEED THESE
YOU NEED US

Culverts
"Gohi" (C. & B. type iron)
"USS" Pure Iron
"USS" Corrugated Steel
"K.C.E." Corrugated Steel
Corrugated Cable Pipes
Corrugated Wire Corrugating
Anti-Washout Pipe
Ridge Roll
Hip Roll
Metal Valves
Cover Trough
Conductor Pipe
Fittings
Gutters
Building Corrugating
Metal Lath
Corner Beads
Metal Roofing (All Sizes)
Metal Siding
"Gohi" C. & B. type iron
Steel
Copper Alloy Sheet
Galvanized Sheet
Blot Sheet
Stylites
Ventilators
Steel Ceiling
Galvanizing (Dip)
Steel Roof Decking
Lux Right Metal Awnings



2634.22
790.35
1843.89

157.03
633.30
790.33

HARRY C. NORD
Sales Representative

PHONES: RIVERVIEW 3708, 3709 and WESTBOR 5246

Recommendations

Mounds View Road. for
building up of plans.

At Sta. 0+85 replace present 12" C.M. with a 24" C.M. X

At Sta. 7+50 is a pot hole, ditch on Rt. & left to meet culverts at St. Tr. Hy. #10 or place a 24" C.M. and ditch on Rt. to meet St. Tr. Hy. #10 culvert on Rt. X

At Sta. 12+00, pot hole on Rt., drain if possible, a culvert at this point would throw water on the land on the left side which might not be desirable.

At Sta. 16+40 on the Rt. is entrance to farm replace present 12" C.M. side culvert with a 15" x 20' C.M. X

At Sta. 19+85, pot hole on Lt., cannot be drained X

At Sta. 24+85 & 25+88 ^{Rt.} determine which entrance is desired & provide drainage either by side ditch or side culvert 15" C.M.

At Sta. 31+07 replace 12" C.M. culvert with
15" or larger.

At Sta. 33+55 replace 9" C.M. with 15" C.M.

At Sta. 37+21 replace 9" C.M. with 15" C.M.

At Sta. 40+33 on Lt. place 15" x 20' C.M.

At Sta. 41+49 replace 9" C.M. culvert with 15"
V

At Sta. 51+75 replace 9" C.M. culvert with 15"

At Sta. 54x, school house on Lt. grounds
being filled, provide by ditch or
culvert for entrance.

At Sta. 56+70 = 24" C.M. extend if necessary
to planned roadway section and
reconstruct ditch on Rt. where at
present too close in. 80' to point
where ditch angles out. See X-SECS.

At 61+88 & 63+54 are 9" x 12" C.M. culverts
eliminate one by side ditch and increase
size to 15" & provide drainage for side entr.

At 65+88 on Rt. field entrance to hay barn
on Rt. ditch north or place 15" x 20' C.M.

At 68+03 = 12" C.M. replace with 15" C.M. X

At Sta. 74+14 = 24" x 54' V.T.R. replace with 36" X
concrete or C.M. pipe

At Sta. 79+27, field entrance on Rt. provide drainage
if to be used. X

At 83+05 Ent. Lt. provide drainage by side
ditches if possible

At 84+60 Rt., Ent. provide for drainage by side
ditch or pipe 15" x 20'

At 94+27 Rt., Ent. provide for drainage by side
ditch or 15" x 20' C.M.

At 94+40, low spot, place culvert 15" C.M. or equalizer
or take care of by side ditches

At 105+ Provide drainage for intersection Mounds
View 4 "I"

Rt Sta. 48+95 is located H.S.G.S.
Bench which is only 25' Rt of $\angle$.