

Dr. 6-BK. 113

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

-----PLAN----- Survey

-----HAMLINE AVE-----

From CO. RD. "E" To LEXINGTON AV.

Road Acc't. No. 9-----

Date Filed-----

File-----

146

$$\begin{array}{r} 32 \\ + 20100 \\ \hline \end{array}$$

$$\begin{array}{r} 7-10 \\ \hline 21 \\ \hline \end{array}$$

147

$$\begin{array}{r} 82 \\ + 5900 \\ \hline \end{array}$$

148

$$\begin{array}{r} 9-10 \\ \hline 21 \\ \hline \end{array}$$

149

$$\begin{array}{r} 28 \\ + 1100 \\ \hline \end{array}$$

150

$$\begin{array}{r} 9-10 \\ \hline 21 \\ \hline \end{array}$$

151

$$\begin{array}{r} 28 \\ + 1100 \\ \hline \end{array}$$

152

$$\begin{array}{r} 8-10 \\ \hline 21 \\ \hline \end{array}$$

$$\begin{array}{r} 28 \\ + 2500 \\ \hline \end{array}$$

$$\begin{array}{r} 14 \\ + 29 \text{ Eht-12} \times 26 \text{ (V.P. + P)} \\ \hline \end{array}$$

$$\begin{array}{r} 29 \\ + 53 \text{ Beg on hand} \\ \hline \end{array}$$

$$\begin{array}{r} 112 \\ + 64 \text{ Car Ho} \\ \hline \end{array}$$

Cultivated

arm 800

31

Cultivated

Cultivated

Ent

31
1 1/2 5-5
24

139

$$\begin{array}{r} +14.00 \\ 2.7 \\ \hline \end{array}$$

140

$$\begin{array}{r} 12.0 \\ 8.11 \\ \hline \end{array}$$

141

$$\begin{array}{r} +35.00 \\ 27.127 \\ \hline \end{array}$$

+45 ENT

142

$$\begin{array}{r} 12.0 \\ 9.9 \\ \hline \end{array}$$

143

$$\begin{array}{r} +91.00 \\ 2.7 \\ \hline \end{array}$$

144

$$\begin{array}{r} +41.00 \\ 2.7 \\ \hline \end{array}$$

145

$$\begin{array}{r} +39.60 \text{ Cor Ho} \\ 11.8 \\ \hline +03.00 \text{ ENT} \end{array}$$

Cultivated

80+100

Cultivated

80+100

132

$$\begin{array}{r} 0.8 \\ \times 19 \\ \hline 15.2 \\ + 15.2 \\ \hline 30.4 \end{array}$$

133

Ent

$$\begin{array}{r} 25 \\ + 34.2 \\ \hline 59.2 \end{array}$$

134

$$\begin{array}{r} 11.6 \\ \times 7.1 \\ \hline 81.36 \end{array}$$

$$\begin{array}{r} 28 \\ + 94.2 \\ \hline 122.2 \end{array}$$

135

136

$$\begin{array}{r} 11.6 \\ \times 9.1 \\ \hline 105.56 \end{array}$$

$$\begin{array}{r} 28 \\ + 54.2 \\ \hline 82.2 \end{array}$$

137

138

$$\begin{array}{r} 5.8 \\ \times 2.9 \\ \hline 16.82 \end{array}$$

$$\begin{array}{r} 28 \\ + 14.2 \\ \hline 42.2 \end{array}$$

Cultivated

0

0

0

0

Pasture + Steps

Pot hole

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

125

$$\begin{array}{r} 28 \\ +4500 \\ \hline \end{array}$$

$$\begin{array}{r} 27 \\ +7200 \\ \hline \end{array}$$

126

$$\begin{array}{r} 9-10 \\ R1 \\ \hline \end{array}$$

$$\begin{array}{r} 27 \\ Fc \\ \hline \end{array}$$

127

$$\begin{array}{r} 28 \\ +6800 \\ \hline \end{array}$$

128

$$\begin{array}{r} 9-10 \\ R1 \\ \hline \end{array}$$

$$\begin{array}{r} 28 \\ Fc \\ \hline \end{array}$$

129

$$\begin{array}{r} 28 \\ +5400 \\ \hline \end{array}$$

130

$$\begin{array}{r} 28 \\ +1400 \\ \hline \end{array}$$

$$\begin{array}{r} 8-10 \\ R1 \\ \hline \end{array}$$

$$\begin{array}{r} 23 \\ Fc \\ \hline \end{array}$$

131

$$\begin{array}{r} 28 \\ +7300 \\ \hline \end{array}$$

$$\begin{array}{r} 22 \\ +13000 \\ \hline \end{array}$$

400' Ho (on High ground)

Ent Ent

Hay

Bush

Bush

Cultivated

Ent

Ent

+ 71 PP. f.c.
27-127 - 53

+ 71 Guy. Po

119

+ 48 Ent

+ 26
+ 26 Guy. Brush
f.c.
27

8 - 11
Rd

120

+ 27
+ 27 PP.

121

+ 27
+ 27 PP.

122

7 - 11
Rd

f.c.
24

123

+ 26
End Brush

+ 27
+ 71 PP.

124

+ 18 PP.
27-150

+ 17
+ 21 Guy. Po

8 - 9
Rd

f.c.
26

+ 31 Ent

+ 31 Ent

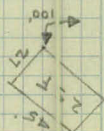
+ 42 IV
23

Coltrane had

Tha y

10/10

Lyons



111

$$\begin{array}{r}
 81 \\
 + 25 \\
 \hline
 106 \\
 + 92.5 \\
 \hline
 198.5 \\
 + 19.5 \\
 \hline
 218 \\
 + 12 \\
 \hline
 230
 \end{array}$$

112

$$\begin{array}{r}
 21 \\
 + 50 \\
 \hline
 71 \\
 + 440 \\
 \hline
 511
 \end{array}$$

113

$$\begin{array}{r}
 27 \\
 + 99 \\
 \hline
 126
 \end{array}$$

114

$$\begin{array}{r}
 27 \\
 + 27 \\
 \hline
 54
 \end{array}$$

$$\begin{array}{r}
 7-11 \\
 + 11 \\
 \hline
 20
 \end{array}$$

$$\begin{array}{r}
 20 \\
 + 20 \\
 \hline
 40
 \end{array}$$

$$\begin{array}{r}
 22 \\
 + 22 \\
 \hline
 44
 \end{array}$$

115

$$\begin{array}{r}
 26 \\
 + 07 \\
 \hline
 33 \\
 + 27.9 \\
 \hline
 60.9 \\
 + 51.7 \\
 \hline
 112.6
 \end{array}$$

$$\begin{array}{r}
 27 \\
 + 22 \\
 \hline
 49
 \end{array}$$

116

$$\begin{array}{r}
 27 \\
 + 27 \\
 \hline
 54
 \end{array}$$

$$\begin{array}{r}
 8-10 \\
 + 10 \\
 \hline
 18
 \end{array}$$

+ 95 Ent. (unable to locate Gully)

117

$$\begin{array}{r}
 27 \\
 + 100 \\
 \hline
 127
 \end{array}$$

$$\begin{array}{r}
 27.1 \\
 + 55 \text{ (or 110)} \\
 \hline
 82.1
 \end{array}$$

$$\begin{array}{r}
 24 \\
 + 24 \\
 \hline
 48
 \end{array}$$

$$\begin{array}{r}
 8 \\
 + 10 \\
 \hline
 18
 \end{array}$$

Cultivated

Posture & Traces

53 0
0 0 0
0 0 0

9 Trees on E/W

105

$$\begin{array}{r}
 40 \\
 +12 FC \\
 \hline
 31 \\
 +78 PP \\
 \hline
 +83 FC - RDSn \\
 26 \\
 \hline
 17 \\
 +90 Rd \\
 \hline
 10 - 12 \\
 \hline
 39 \\
 +82 End Cully \\
 \hline
 29 \\
 +91 FC \\
 \hline
 50 \\
 +75 FC
 \end{array}$$

106

$$\begin{array}{r}
 27 \\
 +24 PP \\
 \hline
 \end{array}$$

107

$$\begin{array}{r}
 27 \\
 +96 - 2TVs \\
 \hline
 \end{array}$$

108

$$\begin{array}{r}
 27 \\
 +81 PP \\
 \hline
 25 \\
 FC \\
 \hline
 8 - 12 \\
 Rd \\
 \hline
 24 - 19 \\
 +80 - 12 \times 43V.P. \\
 \hline
 28 \\
 +91 - 3TVs \\
 \hline
 25 \\
 FC \\
 \hline
 25 \\
 2 - TVs \\
 \hline
 26 \\
 +99 - 2TVs \\
 \hline
 33 \\
 +31 - 4TVs
 \end{array}$$

109

$$\begin{array}{r}
 27 \\
 +33 RDSn \\
 \hline
 27 \\
 +34 PP \\
 \hline
 \end{array}$$

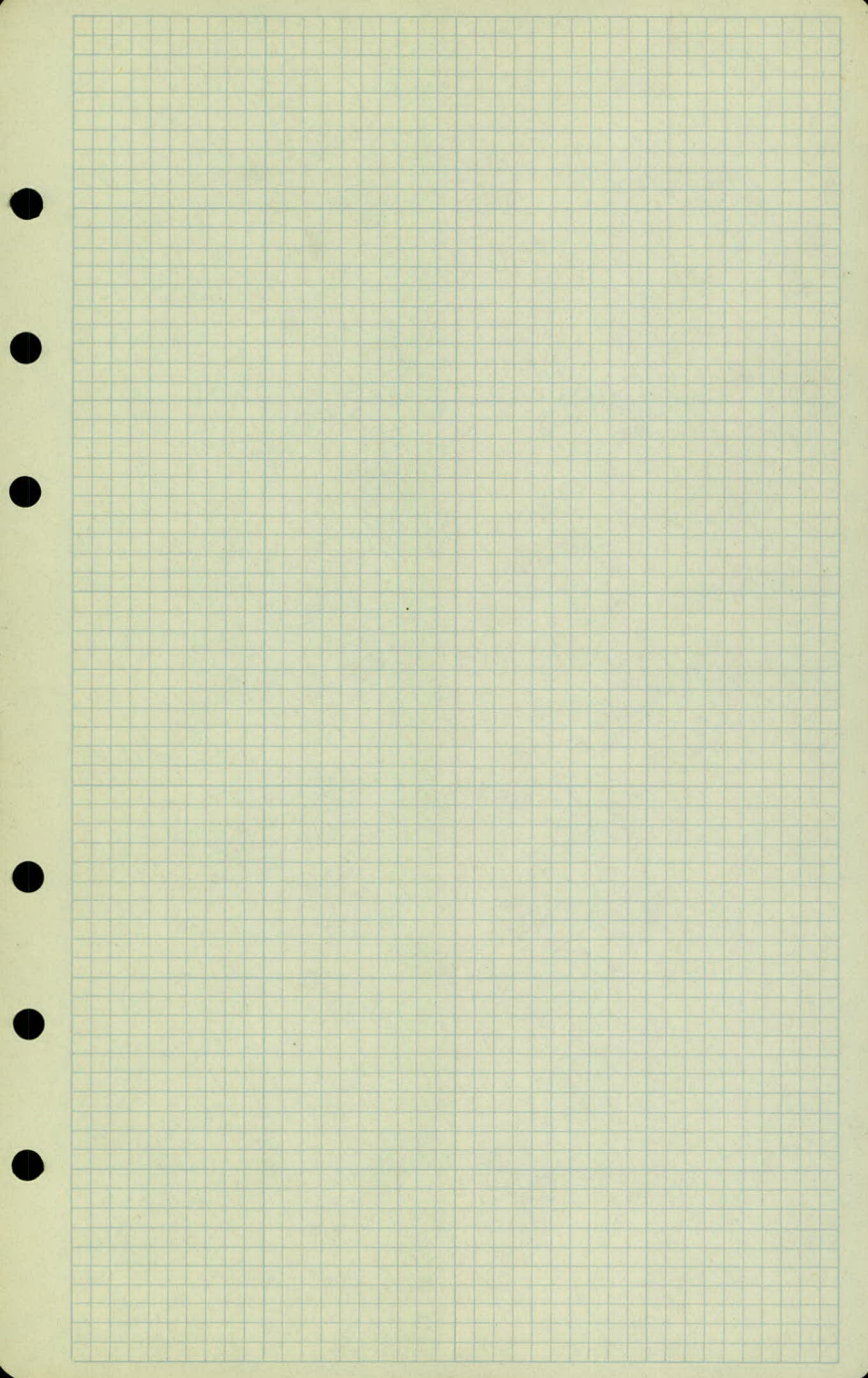
110

$$\begin{array}{r}
 27 \\
 +29 PP \\
 \hline
 26 \\
 FC \\
 \hline
 7 - 9 \\
 Rd \\
 \hline
 32 \\
 FC \\
 \hline
 32 \\
 +33 Grove Trees \\
 \hline
 24 \\
 +46 Grove \\
 \hline
 34 \\
 +59 End Grove
 \end{array}$$

TOPOG
Co Rd "G" to Lex Ave
HAMLINE AVE

3/2/37

Harold Porter
Charles Gottfried
Larry Larsen



Cultivated

18" Black Top

S.T.H. #96

9 9

x

x

x

x

x

x

x

x

102

103

104

$$\frac{21}{FCC}$$

$$\frac{9-11}{21}$$

105

$$\frac{25}{+23 \text{ L.R. RM}} \\ +27 \text{ R.C.}$$

$$\frac{8-11}{+15 \text{ R.}} \\ +35-36 \\ +27 \text{ Shoulder} \\ +40 \text{ Edge Rave} \\ +58 \text{ Edge Rave}$$

$$\frac{24}{+15 \text{ Stop on}} \\ +23 \text{ L.R. RM}$$

106

Cultivated

Cultivated

95

$$\frac{10-12}{Rd}$$

$$\frac{81}{Fce}$$

96

97

$$\frac{9-11}{Rd}$$

$$\frac{19}{Fce}$$

98

99

$$\frac{7-13}{Rd}$$

$$\frac{18}{Fce}$$

100

101

$$\frac{7-13}{Rd}$$

$$\frac{19}{Fce}$$

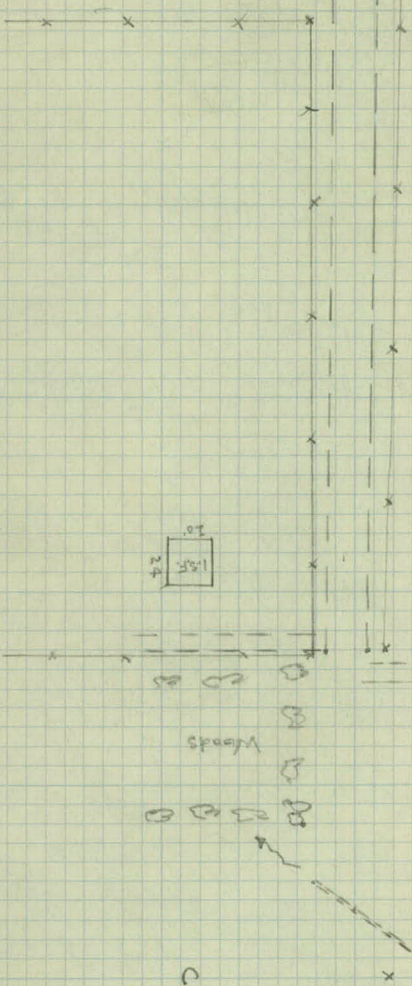
Cult

Cult.

Cult

1.5 ft
2 ft

Woods



88

89

$$\begin{array}{r} +05 \text{ Ec} \\ \hline 22 \end{array}$$

90

$$\begin{array}{r} 12 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 10-12 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 12 \\ \hline 22 \end{array}$$

91

$$\begin{array}{r} +12 \text{ Low Ho.} \\ \hline 15 \end{array}$$

92

$$\begin{array}{r} 17 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 8-14 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 12 \\ \hline 22 \end{array}$$

$$+27 \text{ Ent}$$

$$\begin{array}{r} 17 \\ \hline +34 \text{ Ec} \end{array}$$

$$\begin{array}{r} +36 \text{ Beg Woods} \\ +94 \text{ Low Ec} \\ \hline 23 \end{array}$$

93

$$\begin{array}{r} +21 \text{ End Woods} \\ \hline 24 \end{array}$$

$$\begin{array}{r} +51 \text{ End Coll} \\ \hline 21 \end{array}$$

94

$$\begin{array}{r} 17 \\ \hline 120 \end{array}$$

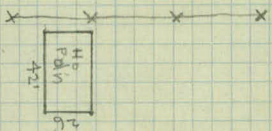
$$\begin{array}{r} 10-12 \\ \hline 24 \end{array}$$

$$+65.12 \times 46 \text{ cm}$$

woods

woods

Cultivated



81

82

$$\frac{Fence}{28}$$

$$\frac{Rd}{139}$$

83

$$\frac{+24 Cor Foundation}{112}$$

84

$$\frac{Fence}{30}$$

$$\frac{Rd}{1210}$$

$$\frac{+16-X5 Fence}{22}$$

$$\frac{+43-15' \times 20' OM}{22}$$

85

$$\frac{+25 Tr}{36}$$

$$\frac{+23 Cor Ht}{105}$$

$$+22 Ent$$

$$\frac{+25 Cor Ht}{77}$$

$$\frac{+25 Tr}{26}$$

$$\frac{+20 Tr}{31}$$

$$+56 Ent$$

86

$$\frac{Fence}{28}$$

$$\frac{Rd}{14-12}$$

$$\frac{+95 Twin Oaks}{20}$$

87

$$\frac{Fence}{35}$$

$$\frac{Rd}{12-12}$$

Meadow

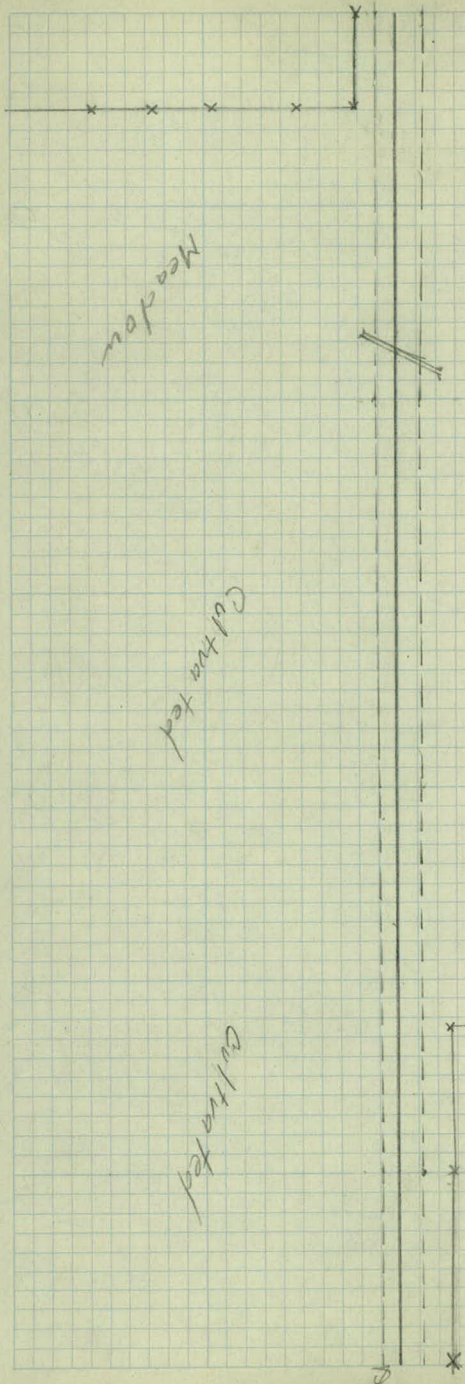
Meadow

Cultivated

Brush

woods

Cultivated



74

75

76

77

78

79

80

$$\begin{array}{r} \text{Rd.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{Fence} \\ 20 \end{array}$$

$$\begin{array}{r} + 49 \text{ End Fence Gap} \\ 21 \end{array}$$

$$\begin{array}{r} \text{Rd.} \\ 11 \end{array}$$

$$\begin{array}{r} + 76 - 18 \text{ C.M. 9 km.} \\ 24 \end{array}$$

$$\begin{array}{r} \text{Rd.} \\ 12 \end{array}$$

$$\begin{array}{r} + 26 \text{ Beg. for Fence} \\ 27 \end{array}$$

$$\begin{array}{r} \text{Rd.} \\ 12 \end{array}$$

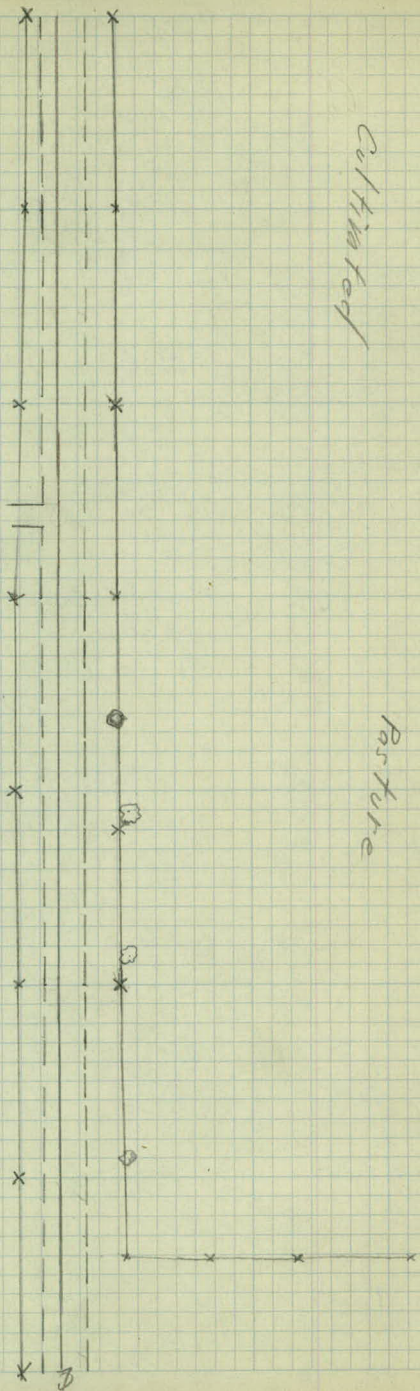
$$\begin{array}{r} \text{Fence} \\ 28 \end{array}$$

Cultivated

Pasture

Cultivated

Cultivated



67

68

Fence
30Rd.
149Fence
17

69

+ 58 ENT 12'

70

Fence
30Rd.
139Fence
22+ 64-18" 3+P
30

71

+ 11-18" OAK
35

72

Fence
31
+ 85-15" OAK
35Rd.
128Fence
21

73

+ 89-15" OAK
34+ 41 Cor (End) Fence
33

Cultivated

Cultivated

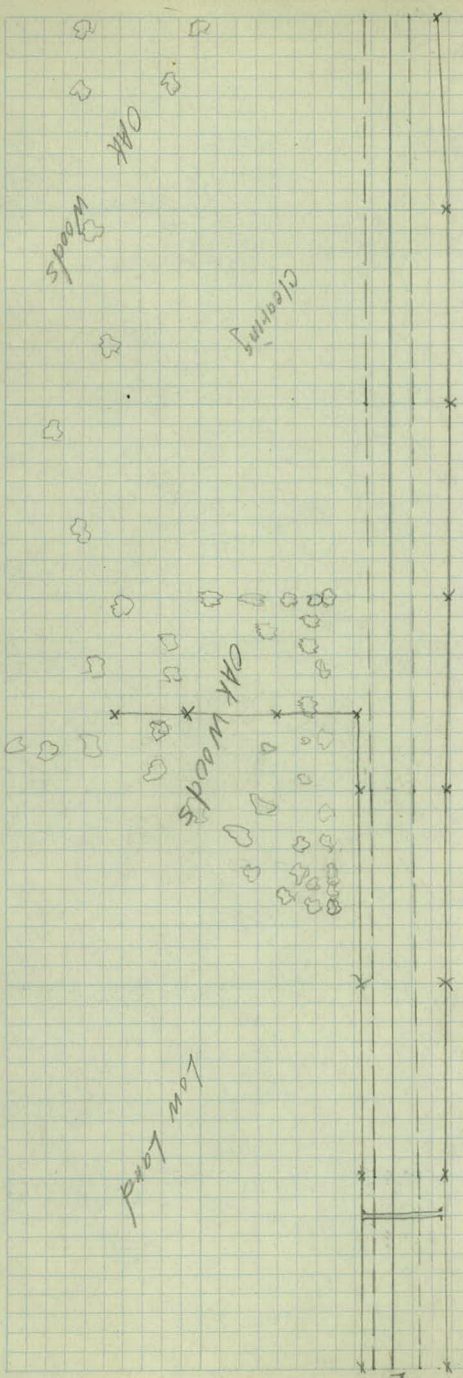
Low Land

Clearing

Oak Woods

Oak Woods

Low Land



61

60 $\frac{\text{Fence}}{28}$

$\frac{\text{Rd.}}{13}$

62

$\frac{\text{Fence}}{30}$

$\frac{\text{Rd.}}{11 \ 13}$

63

$\frac{+ 04 \text{ Begin Woods}}{31}$

$\frac{+ 60 \text{ Fence Gap.}}{18}$

64

$\frac{\text{Fence}}{29}$

$\frac{\text{Rd.}}{11 \ 11}$

$\frac{\text{Fence}}{17}$

$\frac{+ 62 \text{ End of Woods}}{29}$

65

66

$\frac{\text{Fence}}{28}$

$\frac{\text{Rd.}}{12 \ 10}$

$\frac{\text{Fence}}{16}$

$\frac{+ 19.5 \text{ G.M.}}{25 \ 15}$

Cultivated

Yard

28' 28' 28' 28'

20' 20'

Cultivated

Oak Woods

Oak Woods

Oak Woods

59

$$\begin{array}{r} +20 \text{ Fence} \\ 23 \\ \hline \end{array}$$

58

$$\begin{array}{r} \text{Fence} \\ 21 \\ \hline \end{array}$$

$$\begin{array}{r} \text{Rel.} \\ 10 \ 12 \\ \hline \end{array}$$

$$\begin{array}{r} +00 \text{ End of Woods} \\ 29 \\ \hline \end{array}$$

57

$$\begin{array}{r} +22 \text{ Bath} \\ 751 \\ \hline \end{array}$$

56

$$\begin{array}{r} +18 \text{ SE. Corner} \\ 162 \\ \hline \end{array}$$

$$\begin{array}{r} \text{Rel.} \\ 10 \ 12 \\ \hline \end{array}$$

55

$$\begin{array}{r} +708 \text{ DE.} \\ 20 \\ \hline +53 \text{ E.H. +12} \end{array}$$

54

$$\begin{array}{r} \text{Rel.} \\ 11 \ 11 \\ \hline \end{array}$$

$$\begin{array}{r} +41 \text{ Besin Woods} \\ 19 \\ \hline \end{array}$$

53

$$\begin{array}{r} +908 \text{ OAK} \\ 21 \\ \hline \end{array}$$

$$\begin{array}{r} +54-24 \text{ OAK} \\ 50 \\ \hline +45-30 \text{ OAK} \\ 44 \\ \hline \end{array}$$

Cultivated

Cultivated

Cultivated

Co. Rd.

Cultivated

Cultivated

Cultivated

"F"



Q

46

Fence 17
+00

Rd. 9
13

47

Fence 20
+00

48

Fence 23
+00

Rd. 9
13

49

50

Fence 17
+00

Rd. 9
13

51

Fence 14
+00

52

+ 94.57. 59m
21
+ 63 shoulder st.
35
+ 45 Cor Fence
17
+ 21 Fence
14
+00 Fence

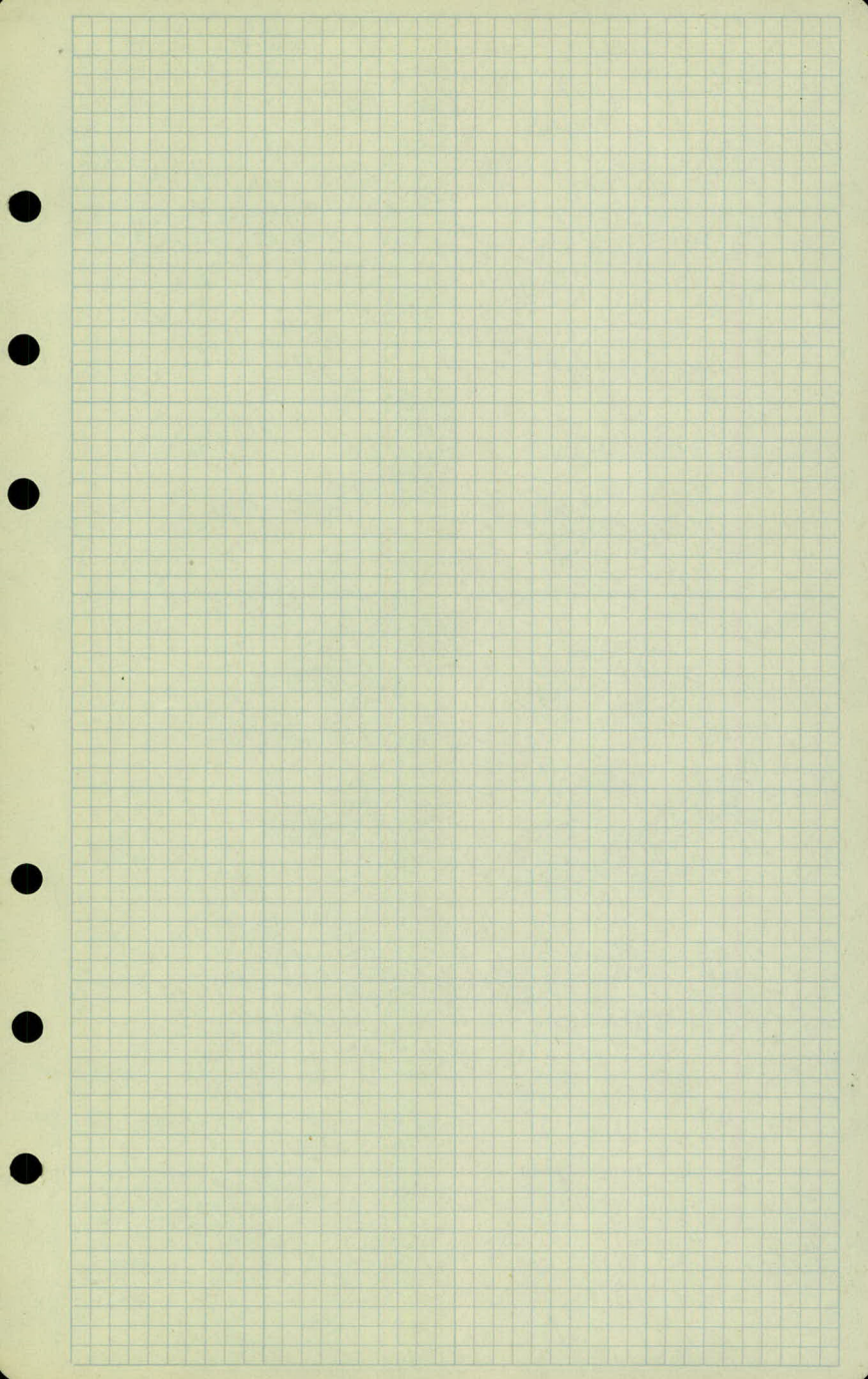
Rd. 9
11

+ 50 12" tree
21
+ 48 10" oak
36

+ 75 In t. corl F-20 wd.

Ⓢ

Topography
No Hammill Ave.
Sta. 45 to



H Tension Lines

+

+

41

$$\left. \begin{array}{r} 15 \times 10 \\ 12.4 \times 10 \\ 17 - 25 \end{array} \right\} + 51$$

$$+ 4.7 \text{ EC} + 7.4$$

42

$$\frac{15}{15}$$

$$\frac{8}{24} - 9$$

43

$$\frac{13}{13}$$

$$+ 2.2 \text{ EC}$$

44

$$\frac{22}{22}$$

$$\frac{9}{24} - 9$$

45

46

47

$$+ 5.6 \text{ steel H/L on lower} + 31$$

Colt

Colt

34

35

36

+ 92 ENT

$$\frac{17}{F_c}$$

$$\frac{8-10}{R_d}$$

37

38

+ 26 - 15" X 52 CM

28 - 24

$$\frac{9-10}{R_d}$$

$$\frac{14}{F_c}$$

+ 22 ENT

39

$$\frac{15}{F_c}$$

+ 75 Fc2

26

40

$$\frac{28}{F_c}$$

$$\frac{8-10}{R_d}$$

+ 63 Fc

20

Cultivated

Cultivated

27

$$\begin{array}{r} 17 \\ + 52 \text{ Fc} \\ \hline \end{array}$$

28

$$\begin{array}{r} 14 \\ \text{Fc} \\ \hline 24 \\ 9 - 72 \end{array}$$

$$\begin{array}{r} 12 \times 56 \text{ Tile} \\ 29 - 27 \\ \hline + 72 \end{array}$$

29

$$\begin{array}{r} 14 \\ \text{Fc} \\ \hline \end{array}$$

$$\begin{array}{r} 18 \\ + 27 \text{ Tr} \\ \hline 24 \\ + 48 \text{ Fc} \end{array}$$

30

$$\begin{array}{r} 25 \\ \text{Fc} \\ \hline \end{array}$$

$$\begin{array}{r} 24 \\ 9 - 13 \end{array}$$

31

$$\begin{array}{r} 24 \\ + 35 \text{ Fc} \\ \hline \end{array}$$

32

$$\begin{array}{r} 19 \\ \text{Fc} \\ \hline \end{array}$$

$$\begin{array}{r} 24 \\ 9 - 12 \end{array}$$

33

$$\begin{array}{r} 17 \\ \text{Fc} \\ \hline \end{array}$$

$$\begin{array}{r} 24 \\ 8 - 13 \end{array}$$

Woods

Piquant Shore

Wood

Cultivated

"F₂" Road

20

$$\frac{31}{+0.21}$$

$$\frac{34}{34}$$

$$\frac{11}{10}$$

$$\frac{27}{27}$$

$$\frac{23}{+4.79}$$

21

22

$$\frac{23}{+3.21}$$

$$\frac{10}{10}$$

$$\frac{25}{25}$$

$$\frac{32}{+9.11}$$

23

$$\frac{30}{+2.11}$$

$$\frac{24}{+8.51}$$

$$\frac{9}{9}$$

$$\frac{26}{26}$$

24

$$\frac{33}{33}$$

25

$$\frac{32}{+3.31}$$

$$\frac{30}{+9.71}$$

26

$$\frac{34}{34}$$

$$\frac{34}{+4.11}$$

$$\frac{9}{9}$$

$$\frac{25}{25}$$

$$\frac{24}{+1.31}$$

+31.51

+50.51

$$\frac{25}{25}$$

Dopant Stone Grounds

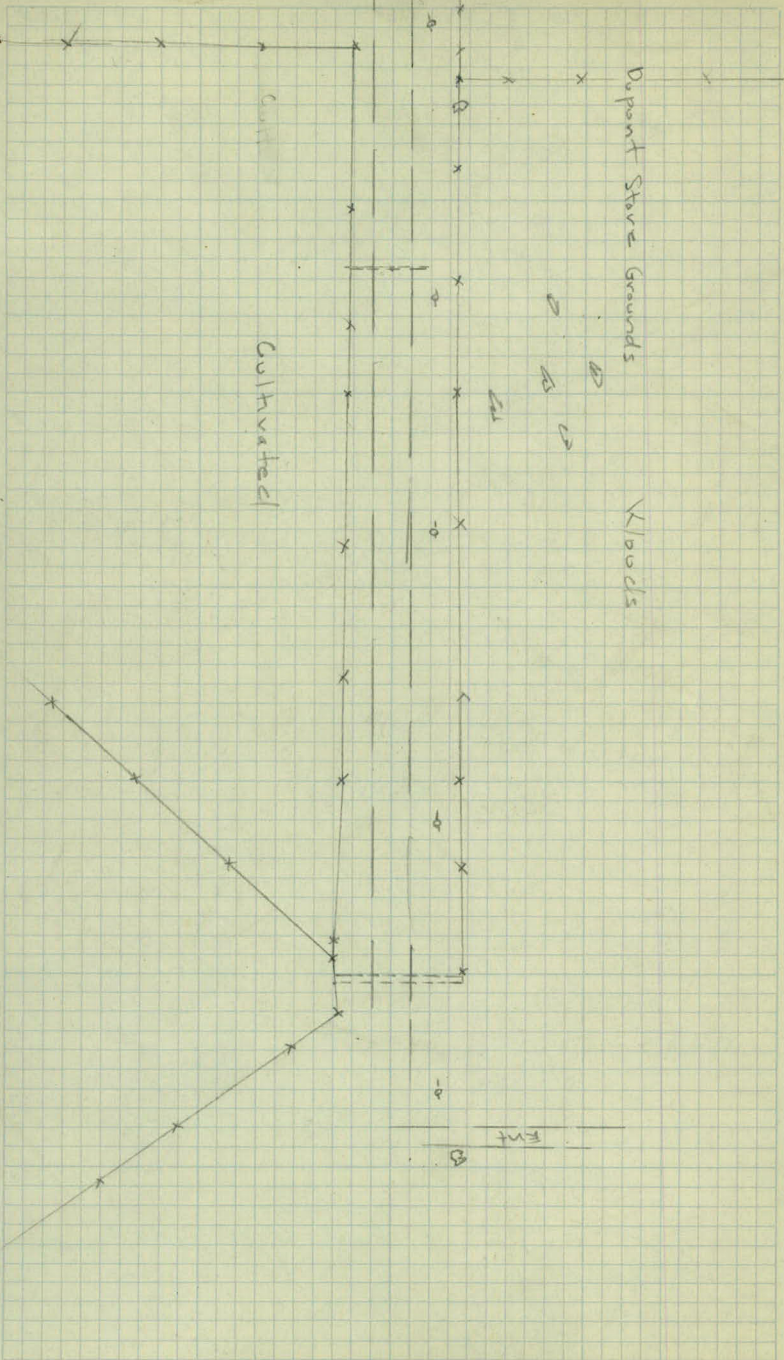
X blocks

Cultivated

ENT

B

1/2



13

$$\begin{array}{r}
 +56.14 \\
 +37.7C \\
 \hline
 93.84 \\
 +08.82 \\
 \hline
 102.66
 \end{array}$$

$$\begin{array}{r}
 120 \pm 19 \\
 \hline
 139
 \end{array}$$

14

$$\begin{array}{r}
 +35.12 \times 400 M \\
 100 - 201 \\
 \hline
 129 \\
 11 - 9 \\
 \hline
 20
 \end{array}$$

unable to locate

$$\begin{array}{r}
 +51.0P \\
 \hline
 92
 \end{array}$$

15

$$\begin{array}{r}
 83 \\
 \hline
 83
 \end{array}$$

$$\begin{array}{r}
 83 \\
 \hline
 83
 \end{array}$$

$$\begin{array}{r}
 +73.0P \\
 \hline
 81
 \end{array}$$

16

$$\begin{array}{r}
 10 - 9 \\
 \hline
 1
 \end{array}$$

17

$$\begin{array}{r}
 34 \\
 \hline
 34
 \end{array}$$

$$\begin{array}{r}
 27 \\
 \hline
 27
 \end{array}$$

$$\begin{array}{r}
 +22.2P \\
 \hline
 22
 \end{array}$$

18

$$\begin{array}{r}
 36 \\
 \hline
 36
 \end{array}$$

$$\begin{array}{r}
 +21.75 + 0.3 \\
 \hline
 106.24 \times 68' CM + 111.29 \\
 \hline
 106.24 \times 68' CM + 111.29 \\
 \hline
 106.24 \times 68' CM + 111.29
 \end{array}$$

(16' CM Rest Tile)

$$\begin{array}{r}
 +94.75 + 19 \\
 \hline
 30
 \end{array}$$

19

$$\begin{array}{r}
 +96.14 \\
 +62.0P \\
 \hline
 158.14 \\
 +85.5M + 12' \times 22' V.P.
 \end{array}$$

$$\begin{array}{r}
 +91.2 Tns \\
 \hline
 32
 \end{array}$$

House



1135' x 1135' P.R. sign

orchard

cultivated

cultivated

cultivated

T.P.O.
x
x
x
x

T.P.O.
x

108' 19'

Gay P.
Palo P.

P.P.O.

R.R. sign

500' Alignment Notes for
Lot R.R. Xing

500' Line

R.R. X 99'

R/W Fee

Garden

Yard



Cult



+76 C-V-Ho
91

+04 En + 10' x 16' CM

24
11-9

+69 Rd 5n
20

+64 x 8 P
20

+81 Fc.
42
+87 Fc.
33

+31 Dug Fence
42
+22 CP
21

+16 Gvp 2
14

+00 R.R. X sign
14' Lt.

see Alignments Notes for L of Xing.

+65 ~~begin R.R. Xing~~

+42 R.P.
22' Lt.

+20 - 15' R.R.
+27 Guy R.
13' Rt.

+23' End of Fence
33' Lt.

12' x 40' CM

+82 ~~15' X Drain~~ (No. 9-65)
X Lt. - 19' Rt.

(see Culu. Location Notes)

+14 I.R.
22'

+80 End of Orchard
36' Lt.

+95 Begin Fence
33' Lt.

(Steel Posts - Topstrand Barbed)
Lower Post 4 "Mechwire"

+79 I.R.
23' Lt.

+45 Row 2 "Apple Trees
40' Lt.

+7 R.R. X sign
11' Rt.
+10 S.E. Cor. House
64' Lt.

S.T. #10

Moist

27' Rav

108

Rd. sign
T.P. 8

Cultivated

108



T.P. 8

Cultivated

108

Cultivated

Cultivated

117 T.P. 8

Cultivated

117 Rd. sign
T.P. 8

Cultivated

126

T.P. 8

8

5

5+51

$$\frac{T.F}{23.74}$$

4

4+26
4+24

$$\frac{T.F * P.R}{23.74}$$

$$\frac{Rd. Sign}{23.74}$$

2

1+76

$$\frac{T.F * P.R}{25.72}$$

1+50

$$\frac{Pop}{29.74}$$

1+32

$$\frac{Pop}{31.74}$$

1

0+50

$$\frac{Rd. Sign}{24.74}$$

0+46 T.F

$$\frac{26.74}{}$$

0+28

$$\frac{X Drain}{15X56.2M.}$$

+00 - Intersection ST. #10 & Co. Rd. #9

Topography Notes
for

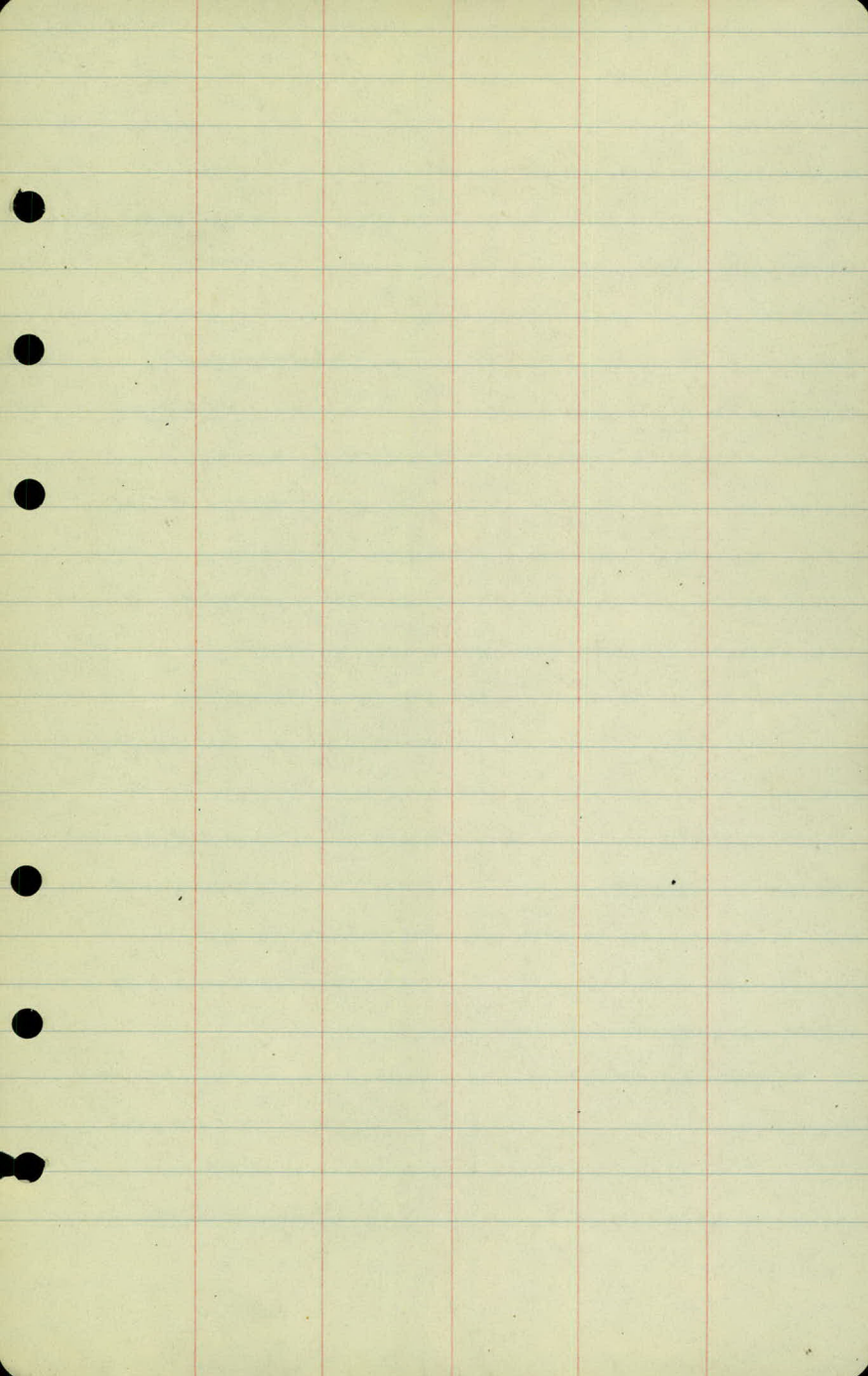
Hornum Ave.

from

St. H. # 10

North to

Lexington Ave.



3. 2

Boat Spite

90.62
58.38
T.P. 0

०००

Nail in
Box Elder

3245 / 12" Boat Spike

42.06

24040

③ Stone Mon.

23

12.06

Nov 14
1899

→ 59°40' → 15" Boot Spike

-соби

12. Boot spike.

24028

Ch. Lybels of
Born.

$\frac{3}{10}$ from pin

R.R. Spike
12" Root Spike. 82.33

K. 2.9046

82.33

189+00 P.O.T.

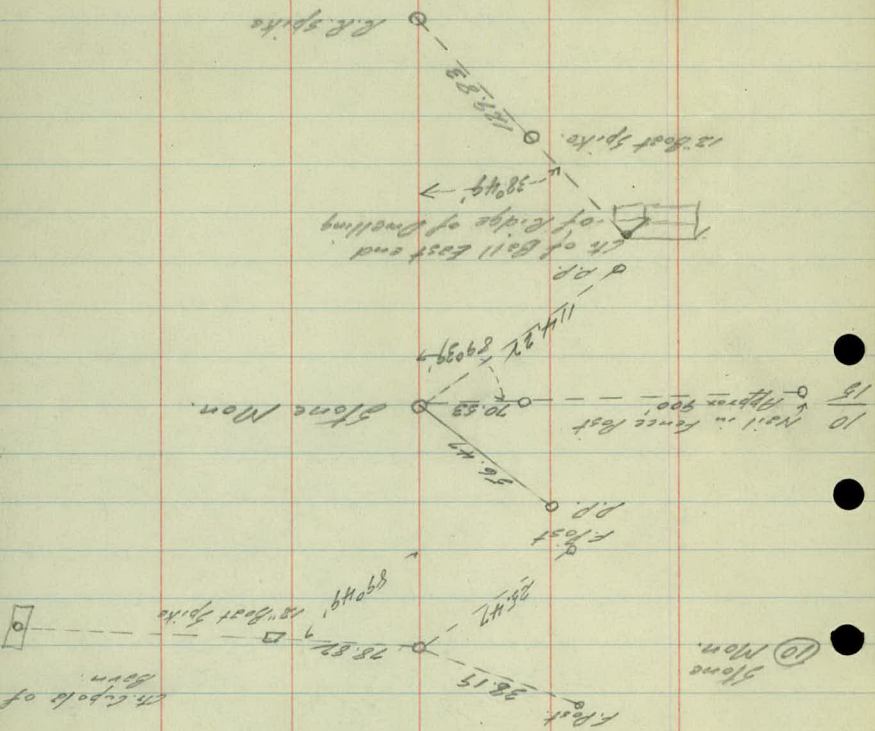
211+04.12 Δ 0° 2' "I"

237+33.28 Δ 0° 2' "I"

250+52.57 Lexington Ave.

Angle
Left Right

Reference Points.



(15) Stone Mon.

(10) Stone Mon.

Angle

Left Right

H₂

1844+59.70

0° 3'

H

0° 9'

1584+18.58

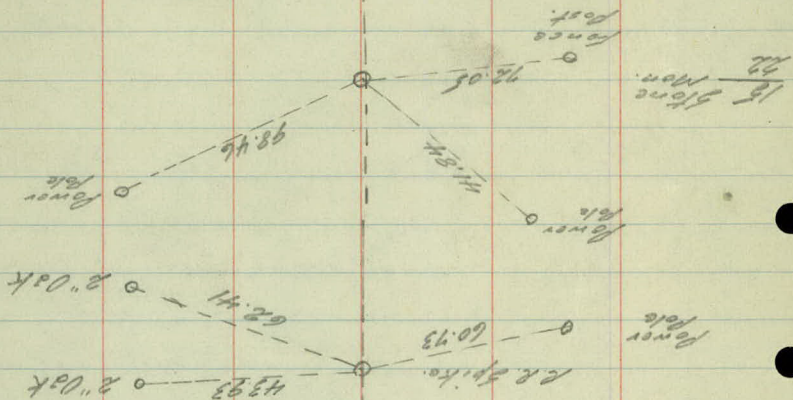
1437+98.10 P.O.T.

1317+82.98 P.O.T.

F₂

Reference Points

N



No ties
Range in if point
is required.

22 Mon. was
not found.
20\" Oak - 82.52
R.R. Spike
47.62
10\" Oak stump

5/2.

Angle
Left Right

120 + 57.85 P.O.T.

105 + 48.64 Δ

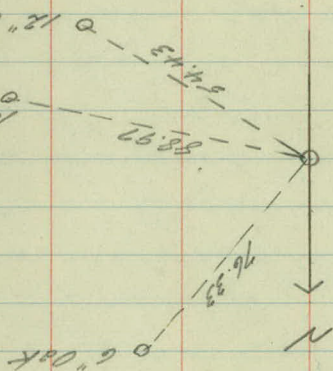
0° 30' " 3"

97 + 07.85 P.O.T.

79 + 19.29 P.O.T.

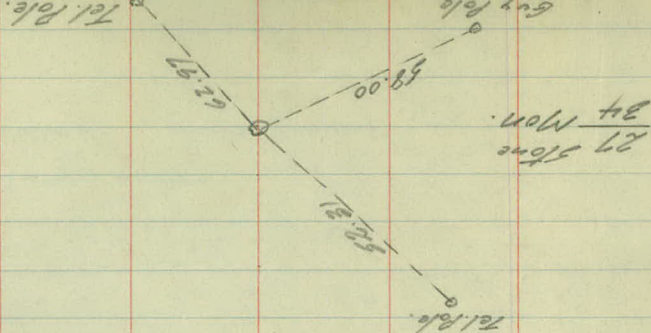
Reference Points.

22 Stone
29 Mon.



Get this from notes
turned in previously

(27) Stone
Mon



0+00

Remark:
The notes were turned
in previously for the
first mile.

F₁

26+40.52 P.O.T.

F₂

52+76.16

△

0° 2'

F

3/3.

Left Right

Angle

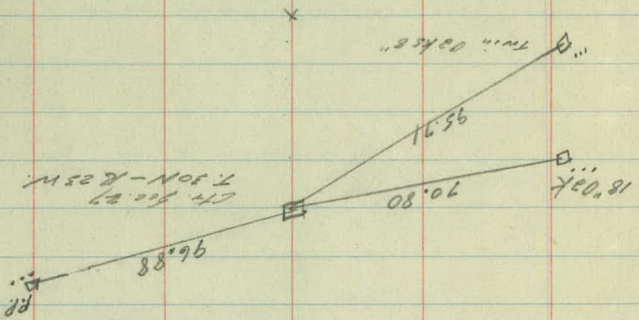
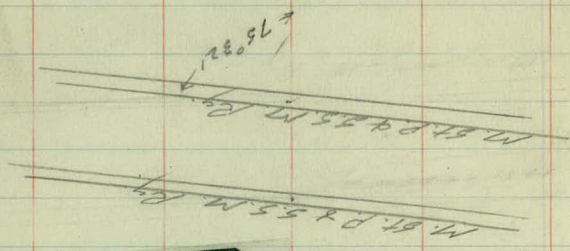
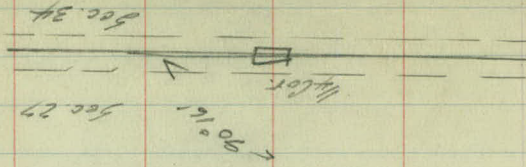
Hamm line Ave

Alignment from County
Road "E" to Lexington Ave.
T-30N - R 33W.

4/37 {
Mike
Goldberg
Gillen
Larson

Sto.

Anglo.



Men. not found, buried (2)
 in garden, ground level point
 from 5 feet. marks. sec
 bounds first book of
 section. Nos.

Sec 27
 Dec 27

4

5th. Angle.

54+74.95 Mon.

26+40.54 Mon. 1/2 C. P.O.T.

11/11/54
↓

24+66.64 P.O.T.

9+80.63 P.O.T.

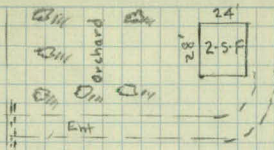
9+65.15 P.O.T.

0+00 Mon. & 5THy. #10.

Alignment Notes.
(Baseline Hrs.)

Cultivated

Cultivated



159

$$\begin{array}{r} + 68 \text{ PP} \\ \hline 28' \end{array}$$

$$\begin{array}{r} + 19-X \text{ Fence} \\ \hline 42 \end{array}$$

$$\begin{array}{r} + 02 \text{ Conc. Cu.} - 18'' \text{ P}_1 \\ \hline 26' 26' \end{array}$$

158

$$\begin{array}{r} R_1 \\ \hline 8-11 \end{array}$$

$$\begin{array}{r} + 08 \text{ PP} \\ \hline 28 \end{array}$$

157

156

$$\begin{array}{r} R_1 \\ \hline 9-10 \end{array}$$

$$\begin{array}{r} + 48 \text{ PP} \\ \hline 27 \end{array}$$

155

154

$$\begin{array}{r} R_1 \\ \hline 9-10 \end{array}$$

$$\begin{array}{r} + 73 \text{ PP} \\ \hline 28 \end{array}$$

$$\begin{array}{r} + 36 \text{ End Orchard} \\ \hline 29 \end{array}$$

153

Cultivated



Meadow



0.11 2.11 2.11

2.11 orchard

0.11

$$\frac{+69 \text{ PP}}{28}$$

166

$$\frac{\text{Rd}}{7 \text{ 11.}}$$

$$\frac{+86 - 142' \times 4" \text{ Hex. Tile Pipe}}{125' \text{ 17'}}$$

$$165 \quad \frac{+08 \text{ PP}}{28}$$

164

$$\frac{\text{Rd}}{7 \text{ 12}}$$

$$\frac{+48 \text{ PP}}{28}$$

163

162

$$\frac{\text{Rd}}{8 \text{ 12}}$$

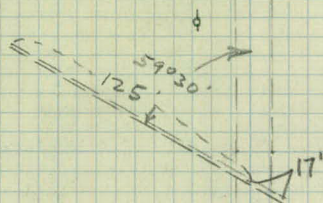
$$\frac{+88 \text{ PP}}{2}$$

161

$$\frac{+28 \text{ PP}}{28}$$

160

$$\frac{\text{Rd}}{9 \text{ 11}}$$



Cultivated

Cultivated

Cultivated

Meadow

173

$$\begin{array}{r} +77 \text{ PP.} \\ \hline 19 \end{array}$$

172

$$\begin{array}{r} \text{Fence} \\ \hline 19 \end{array}$$

$$\begin{array}{r} \text{Rd.} \\ \hline 6 \text{ } 11 \end{array}$$

$$\begin{array}{r} \text{Fence} \\ \hline 19 \end{array}$$

171

$$\begin{array}{r} +38 \text{ Begin Fence Cor.} \\ \hline 20 \end{array}$$

$$\begin{array}{r} +38 \text{ R.P.} \\ \hline 18 \end{array}$$

$$\begin{array}{r} +38 \text{ Fence Cor.} \\ \hline 20 \end{array}$$

+100 Ent

$$\begin{array}{r} +73-2-18 \text{ "Pop."} \\ \hline 27 \end{array}$$

$$\begin{array}{r} +74 \text{ End Orchard} \\ \hline 25 \end{array}$$

170

$$\begin{array}{r} \text{Rd.} \\ \hline 7 \text{ } 11 \end{array}$$

$$\begin{array}{r} +82 \text{ PP.} \\ \hline 18 \end{array}$$

$$\begin{array}{r} +27 \text{ SE. Cor. House} \\ \hline 153 \end{array}$$

$$\begin{array}{r} +08 \text{ Begin Orchard} \\ \hline 27 \end{array}$$

169

$$\begin{array}{r} +28 \text{ PP.} \\ \hline 28 \end{array}$$

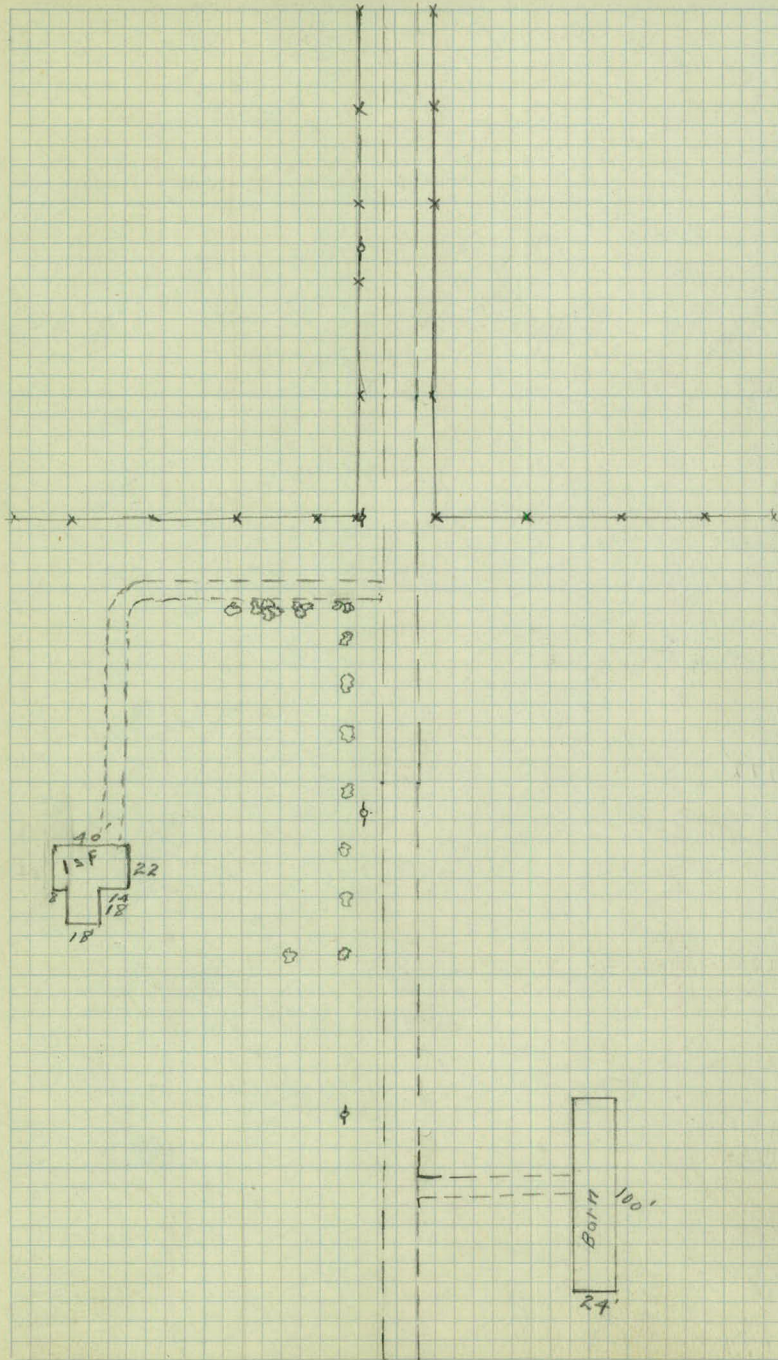
168

$$\begin{array}{r} \text{Rd.} \\ \hline 7 \text{ } 11 \end{array}$$

+90 Ent.

167

$$\begin{array}{r} +35 \text{ S.W. Cor. Barn} \\ \hline 91 \end{array}$$



180

$$\frac{\text{Fence}}{22}$$

$$\frac{\text{Rd}}{8/2}$$

$$\frac{+ 16 \text{ P.P.}}{19}$$

$$\frac{+ 25 \text{ Guy Pole}}{17}$$

179

$$\frac{+ 47 \times \text{Fence}}{27}$$

$$\frac{+ 89 \text{ Ent.}}{21}$$

178

$$\frac{\text{Fence}}{26}$$

$$\frac{\text{Rd}}{7/11}$$

$$\frac{\text{Fence}}{20}$$

$$\frac{+ 52 \text{ P.P.}}{19}$$

177

176

$$\frac{\text{Fence}}{19}$$

$$\frac{\text{Rd}}{7/11}$$

$$\frac{\text{Fence}}{19}$$

$$\frac{+ 59 \text{ P.P.}}{18}$$

175

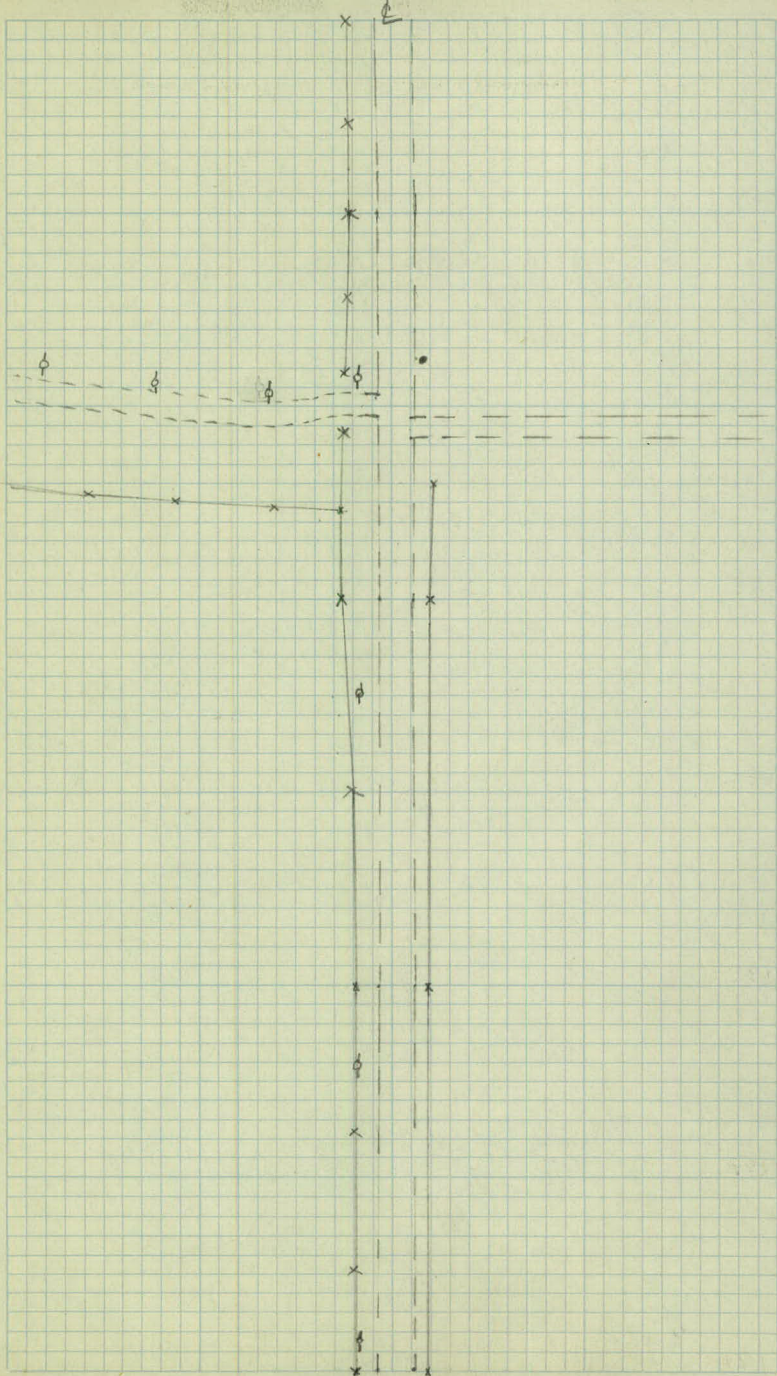
$$\frac{+ 17 \text{ P.P.}}{18}$$

174

$$\frac{\text{Fence}}{19}$$

$$\frac{\text{Rd}}{7/11}$$

$$\frac{\text{Fence}}{19}$$



187

186

$$\frac{Fence}{28}$$

$$\frac{Rd.}{10-11}$$

185

+ 60-3' Bot Ditch

$$\frac{+ 52-X Fence}{24}$$

$$+ 77-18" \times 34"? (Double) CM$$

unable to locate - 19

$$\frac{+ 60 Fence Cor.}{28}$$

184

$$\frac{Fence}{24}$$

$$\frac{Rd.}{7-11}$$

$$\frac{Fence}{28}$$

183

$$\frac{+ 16 Begly Fence}{30}$$

182

$$\frac{Fence}{26}$$

$$\frac{Rd.}{8-10}$$

$$\frac{+ 47 15" Bone Col.}{28-27}$$

$$\frac{+ 10 SE Horse}{500}$$

181

25
8

4500 ft

Cultivated

Cultivated

2' Bot. Ditch

Cultivated

Cultivated

194

$$\frac{Fc}{33}$$

$$\frac{Rd}{7-12}$$

193

192 +ol Ent

$$\frac{Fc}{23}$$

$$\frac{Rd}{6-12}$$

191

190

$$\frac{Fc}{26}$$

$$\frac{Rd}{9-11}$$

$$\frac{+30 Fc}{27}$$

189

$$\frac{+57-24 \times 28' CM. + Long}{20 + 18}$$

188

$$\frac{Fc}{25}$$

$$\frac{Rd}{9-11}$$

Cultivated

Int

Cultivated

x x x



x

x

x

x

x

x

x

x

x

x

x

x

x



201

200

Rd
6-10

199

+14 Cor. Tar paper Duvelling
210+69 Tr
40

198

Rd
5-12+5 Cor Ho. (under Const.)
55+80 FC
41

197

196

Fc
37Rd
5-13

195

Cultivated

Low Water Land

W

15 18

2 4

Cultivated

208

Rd
11-6

207

+24 Rd Sn
16

206

Rd
8-8

205

204

Rd
8-8

+07 Ent

203

+33 Ent

202

Rd
8-8

Cultivated

Low Waite Land

P

Ent

Ent

Rd
16-4

$$\begin{array}{r} +62-30 \times 38 \text{ CM} \\ \hline 22-16 \end{array}$$

$$\begin{array}{r} +20 \text{ Rd Sn} \\ \hline 23 \end{array}$$

215

$$\begin{array}{r} +67-4' \text{ Pot Ditch} \\ \hline 17 \text{ E} \end{array}$$

214

$$\begin{array}{r} R1 \\ \hline 18-1 \end{array}$$

213

212

$$\begin{array}{r} R1 \\ \hline 15-2 \end{array}$$

$$\begin{array}{r} +60 \text{ Rd} \\ \hline 18-4 \end{array}$$

+45 St. P. W. W. Conduit -

134

$$\begin{array}{r} +21 \text{ Shoulder} \\ \hline 55-5 \end{array}$$

$$\begin{array}{r} +15 \text{ End Sn} \\ \hline 15 \end{array}$$

211

$$\begin{array}{r} +88 \text{ Shoulder} \\ \hline 50-4 \end{array}$$

$$\begin{array}{r} +48 R1 \\ \hline 13-5 \end{array}$$

210

$$\begin{array}{r} R1 \\ \hline 11-5 \end{array}$$

209

1' x 9' Masonry Head Wall

Partly Cultivated

Partly Cultivated

1' cut ditch

+452 St. Paul W. W. Conduit

Colv.

unable to measure size
Acct High Water

CO. RD. I (Gravel Surf.)

Cultivated

Waste Land

222

$$\frac{Rd}{7-11}$$

221

$$220 \quad + 20 \text{ Ent.}$$

$$\frac{Rd}{8-10}$$

$$\frac{+ 16-15'' \text{ POP.}}{23}$$

$$\frac{+ 24-15'' \text{ BP}}{24}$$

$$+ 76 \text{ Ent.}$$

$$\frac{+ 63 - \text{Twin Willow} - 8''}{26}$$

219

$$\frac{+ 78 \text{ Brush}}{26}$$

218

$$\frac{Rd}{9-9}$$

217

216

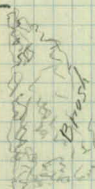
$$\frac{Rd}{10-4}$$

Meadow

Cultivated

Meadow

Meadow



Low land

Meadow

A. B. + D. Rd

229

228

Fence
17

Rd
7-9

227

+ 42 10" V.P. X Drain
15' - 15'

226

Fence
14

Rd
7-11

225

+ 76 End of Grave
30

+ 48 Ent.

+ 23 (Begin) Fence Corn
16

+ 21 Begin Groves of Trees
28

224

Rd
7-11

223

Meadow

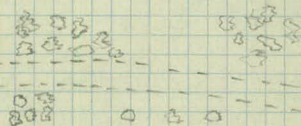
Meadow

Cultivated

cultivated

Cultivated

Cultivated



236

$$\frac{\text{Fence}}{18}$$

$$\frac{\text{Rd}}{8-8}$$

235

234

$$\frac{\text{Fence}}{18}$$

$$\frac{\text{Rd}}{7-9}$$

233

232

$$\frac{\text{Fence}}{18}$$

$$\frac{\text{Rd}}{7-9}$$

231

230

$$\frac{\text{Fence}}{19}$$

$$\frac{\text{Rd}}{6-9}$$

Cultivated

Cultivated

Cultivated

x

x

x

x

x

x

x

x

x

x

x

x

x

Cultivated

Cultivated

Cultivated

243

$$\frac{+0.4 PP}{28}$$

242

$$\frac{Rd}{10-6}$$

$$\frac{+6.4 Tr}{18}$$

$$\frac{Ag}{21}$$

$$\frac{+8.1 Tr}{70}$$

$$\frac{+7.3 Tr}{23}$$

$$\frac{+3.6 PP}{27}$$

$$\frac{+6.8 Tr}{36}$$

$$\frac{+1.3 Shed}{31}$$

$$\frac{+0.2 Tr}{32}$$

241

$$\frac{+6.6 FC}{34}$$

$$+6.0 Ent$$

$$\frac{+9.9 Tr}{30}$$

$$\frac{+6.9 Shed}{51}$$

$$+5.6 Ent$$

240

$$\frac{Fence}{34}$$

$$\frac{Rd}{11-7}$$

$$\frac{+0.8-15' Oak}{26}$$

$$\frac{Fence}{15}$$

$$\frac{+8.5 S.W. Cor House}{124}$$

$$\frac{+8.4-24' Oak}{21}$$

239

$$\frac{+2.8-8' B.F.}{19}$$

$$\frac{+9.7 Triple Willow}{18'}$$

$$\frac{+7.2-18' Willow}{19'}$$

$$\frac{+0.6-12' B.F.}{20'}$$

$$\frac{+3.6-15' Willow}{18'}$$

238

$$\frac{Fence}{33}$$

$$\frac{Rd}{12-7}$$

$$\frac{+0.0 Fence Cor}{18}$$

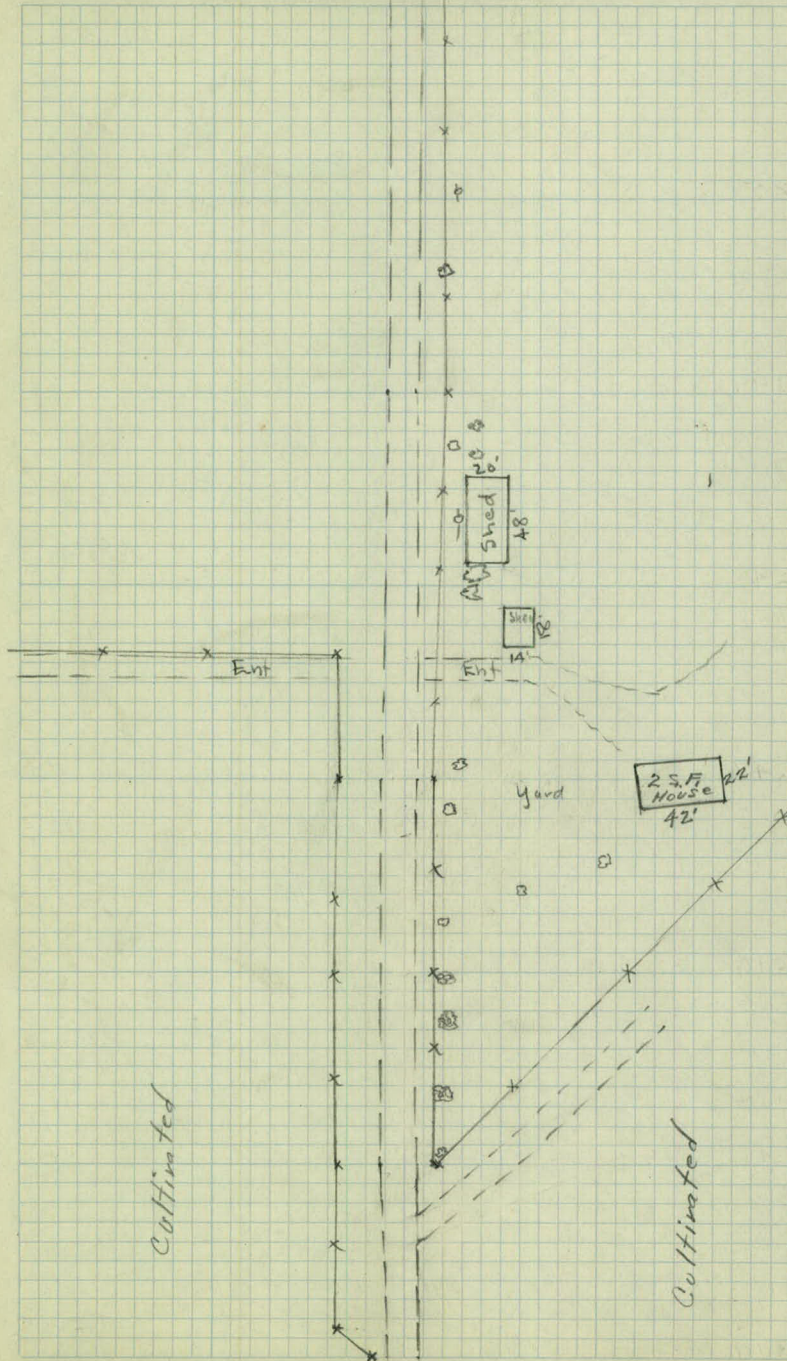
$$\frac{+9.8 Rd Spr.}{16}$$

$$+6.7 Ent$$

237

$$\frac{+1.5 Fence Cor}{33}$$

$$\frac{+0.1 Fence Cor}{16}$$



$$\begin{array}{r} +70 \text{ End Sn} \\ \hline 8 \end{array}$$

+69 Shoulder

$$\begin{array}{r} +36 \text{ Shoulder} \\ 40 - 38 \\ \hline \text{Rd} \\ 16 - 16 \end{array}$$

250

$$\begin{array}{r} +93 \text{ PP} \\ \hline 31 \end{array}$$

249

248

$$\begin{array}{r} \text{Rd} \\ 16 - 15 \end{array}$$

$$\begin{array}{r} +61 \text{ PP} \\ \hline 32 \end{array}$$

247

$$\begin{array}{r} +19 \text{ PP} \\ \hline 33 \end{array}$$

246

$$\begin{array}{r} \text{Rd} \\ 16 - 15 \end{array}$$

$$\begin{array}{r} +75 \text{ Rd in Post} \\ \hline 19 \end{array}$$

+34 Ent

$$\begin{array}{r} +45 \text{ Rd} \\ 16 - 16 \end{array}$$

$$\begin{array}{r} +45 \text{ FC} \\ \hline 19 \end{array}$$

245

$$\begin{array}{r} +41 \text{ Rd} \\ \hline 15 \end{array}$$

$$\begin{array}{r} +32 - 12 \times 34 \text{ VP} \\ 16 - 18 \end{array}$$

$$\begin{array}{r} +54 \text{ PP} \\ \hline 16 \end{array}$$

244

$$\begin{array}{r} \text{Rd} \\ 8 - 8 \end{array}$$

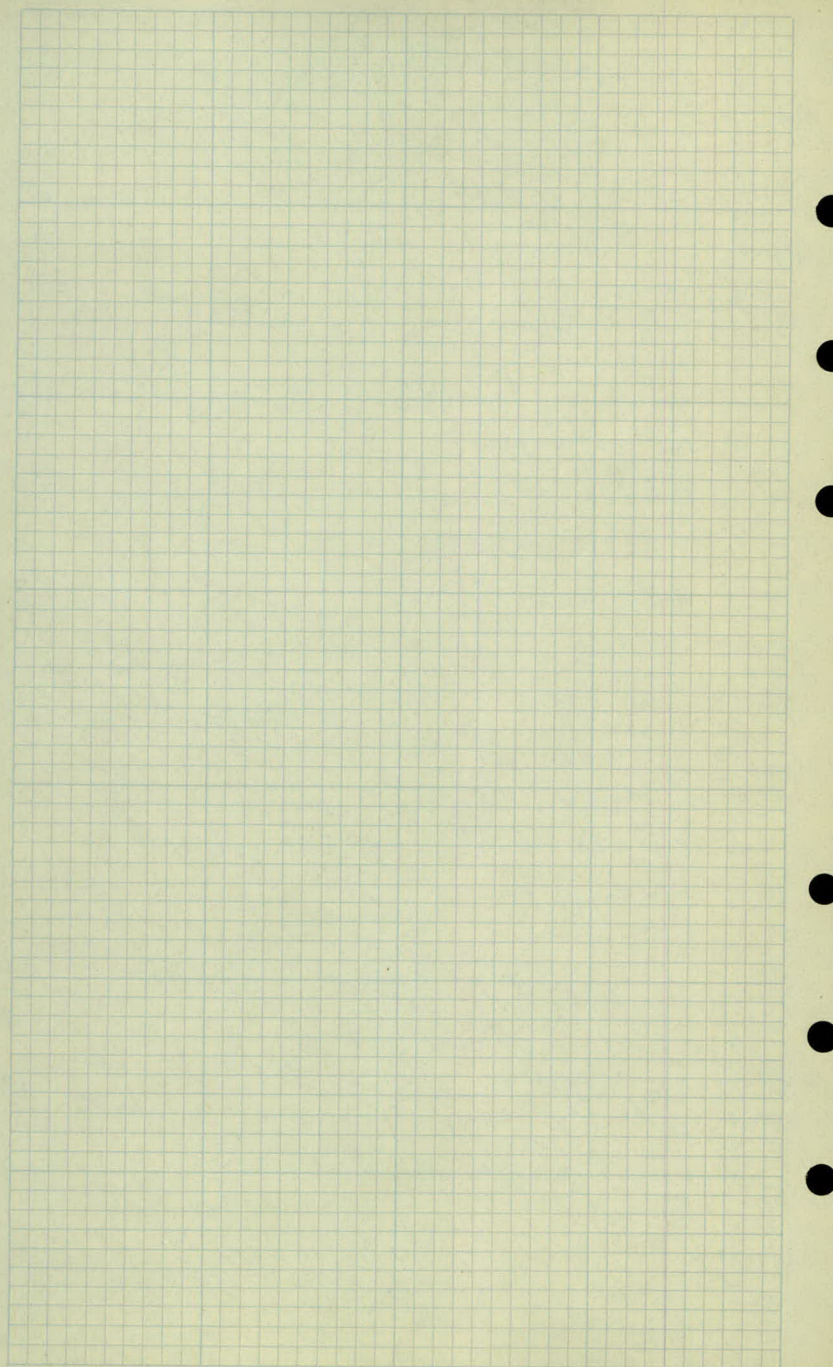
$$\begin{array}{r} \text{FC} \\ \hline 18 \end{array}$$

LEX. AVE (Gravel Sort)

Cultivated

Cultivated

Pot Hole



Bench Levels
Horn Line Ave.

from S.T. Hy. #10 to

Sta.	+	Σ	-	Elev.
B.M.				985.22
T.P.	0.33	985.55	12.79	972.76
T.P.	0.63	973.39	13.56	959.83
B.M.	0.61	960.44	5.81	954.63 X
T.P.	5.81	960.44	13.25	947.19
T.P.	0.15	947.34	8.84	938.50
B.M.	1.12	939.62	3.15	936.47 X
B.M.	6.97	943.44	5.32	938.12
T.P.	5.32	943.44	14.13	931.31
B.M.	3.60	934.91	3.11	931.80 X
B.M.	1.88	933.68		931.80
O	7.22	932.22	8.68	925.00
B.M.			2.45	929.77
O	4.48	934.21	2.41	929.73
B.M.			3.65	930.56

Spike in 8" Oak S.E. Cor. (Hamline & F)

10 F.R.

Spike in Power Pole 48' Rt. Sta. 44+45

Ctr. Mon. Sta. 26+40.54

Spike in P.P. 100' Rt. Sta. 26+65

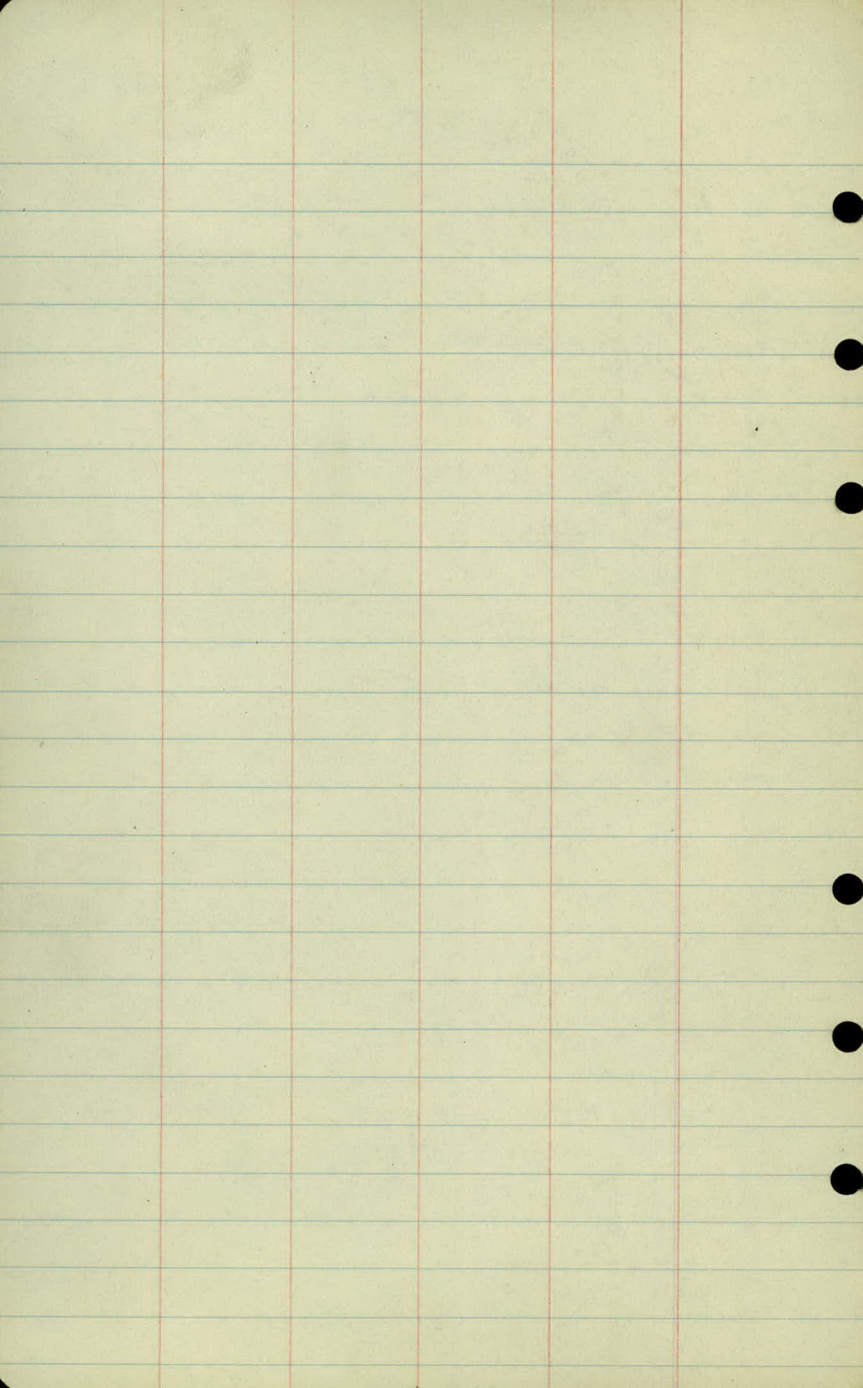
Spike in 24" Oak 100' Lt. Sta. 21+00

" " " " " " " "

12" Oak 60' Rt. Sta. 12+80

Top Rail S_{oo} Line S. Rail of No Trk

Top Mast "E" and Handline



1/25/37

H.T.P

C.G.

L.G.

L.L.

X- Sections

Hamline Avenue

Co Rd E to Lexington

Sta	+	π	-	Elev.
B.M.	3.54	934.10		930.56
0	4 Co. Rd E			30.6
+18				30.9
+25				31.1
+38				31.4
1				31.1
2				30.2
3				29.6
+50				29.5
4				29.3 5+73
5				29.2 7+73
6				28.9 8+73

Top Mont Cor "E" and Hamline

S.S. = Same Slope
L.O. = Level Out

$$\frac{2.9}{50} \quad 3.5 \quad \frac{4.4}{50} \quad \frac{6.2}{100}$$

$$\frac{2.9}{50} \quad 3.2 \quad \frac{4.4}{50} \quad \frac{5.7}{100}$$

$$\frac{4.1}{100} \quad \frac{5.0}{45} \quad \frac{4.0}{31} \quad \frac{3.0}{23} \quad 3.0 \quad \frac{3.6}{15} \quad \frac{6.2}{28} \quad \frac{6.6}{45} \quad \frac{6.8}{50} \quad \frac{5.5}{90}$$

$$\frac{+1.0}{10} \quad \frac{2.7}{45} \quad \frac{3.6}{28} \quad \frac{3.0}{16} \quad 2.7 \quad \frac{3.7}{16} \quad \frac{5.7}{35-50} \quad \frac{3.7}{80} \quad \frac{4.5}{100}$$

$$\frac{0.8}{100} \quad \frac{0.0}{70-40} \quad \frac{2.1}{33} \quad \frac{3.1}{24} \quad \frac{3.2}{16} \quad 3.0 \quad \frac{3.6}{10} \quad \frac{4.1}{13} \quad \frac{6.7}{21} \quad \frac{7.4}{14} \quad \frac{7.1}{15} \quad \frac{5.1}{80} \quad \frac{6.0}{100}$$

$$L.O. \quad \frac{0.8}{60} \quad \frac{1.6}{44} \quad \frac{4.1}{25} \quad \frac{4.4}{20} \quad 3.9 \quad \frac{4.7}{12} \quad \frac{8.5}{22} \quad \frac{10.0}{50} \quad \frac{9.2}{100}$$

$$\frac{5.1}{100} \quad \frac{2.1}{70} \quad \frac{5.1}{50} \quad \frac{5.8}{37} \quad \frac{6.8}{23} \quad \frac{5.1}{18} \quad 4.5 \quad \frac{5.3}{13} \quad \frac{8.8}{25-50} \quad \frac{6.7}{100}$$

$$\frac{2.2}{100} \quad \frac{0.0}{65} \quad \frac{2.2}{50} \quad \frac{4.6}{34} \quad \frac{6.1}{23} \quad \frac{4.7}{17} \quad 4.6 \quad \frac{5.2}{13} \quad \frac{7.1}{24} \quad \frac{6.5}{50} \quad \frac{7.3}{100}$$

$$\frac{0.0}{100} \quad \frac{+2.6}{50} \quad \frac{+2.0}{34} \quad \frac{2.9}{28} \quad \frac{5.6}{21} \quad \frac{5.0}{17} \quad 4.8 \quad \frac{5.3}{13} \quad \frac{8.4}{28} \quad \frac{10.2}{50} \quad \frac{9.8}{100}$$

$$\frac{2.1}{100} \quad 5.0 \quad \frac{3.0}{27} \quad \frac{5.1}{17} \quad 4.9 \quad \frac{5.4}{14} \quad \frac{8.0}{23} \quad \frac{10.0}{50} \quad \frac{10.7}{100}$$

$$5.5 \quad \frac{2.9}{50} \quad \frac{3.2}{34} \quad \frac{6.4}{27} \quad \frac{5.3}{18} \quad 5.2 \quad \frac{5.1}{11} \quad \frac{6.1}{20} \quad \frac{4.9}{22} \quad \frac{6.4}{50} \quad \frac{9.0}{100}$$

Sta	+	Σ	-	Elev.
		934.10		
7				28.5 . 2+73
8				27.9 . 1+73
0	6.43	936.16	4.34	129.76 929.73
9				28.4 . 0+73
+30				28.7 . 0+73
+55				29.6 . 0+18
+65	± East Bound Trk			29.67 . 0+08 +73 = 0+00
+81	± West Bound Trk			29.69 . 0+08
+86				29.6 . 0+13
10				29.2 . 0+27
+24				28.8 . 0+53
11				28.5 . 1+27

$$\frac{3.1}{100} \quad \frac{5.1}{50} \quad \frac{7.6}{29} \quad \frac{6.7}{21} \quad \frac{6.2}{18} \quad 5.6 \quad \frac{6.4}{11} \quad \frac{8.2}{19} \quad \frac{9.5}{50} \quad \frac{10.4}{70} \quad \frac{8.0}{100}$$

$$\frac{4.0}{100} \quad \frac{8.6}{50} \quad \frac{9.0}{43} \quad \frac{9.2}{25} \quad \frac{6.7}{18} \quad 6.2 \quad \frac{7.0}{11} \quad \frac{10.0}{20} \quad \frac{11.0}{50} \quad \frac{9.6}{100}$$

$$\frac{9.6}{100} \quad \frac{12.6}{50} \quad \frac{12.4}{26} \quad \frac{5.5}{16} \quad 7.8 \quad \frac{8.0}{12} \quad \frac{13.2}{22} \quad \frac{14.0}{41} \quad \frac{13.8}{50} \quad \frac{11.3}{100}$$

$$\frac{8.5}{100} \quad \frac{11.6}{50} \quad \frac{10.8}{25} \quad \frac{8.2}{15} \quad 7.5 \quad \frac{7.6}{11} \quad \frac{13.2}{25} \quad \frac{13.1}{50} \quad \frac{7.5}{80} \quad 10$$

$$\frac{7.3}{50} \quad \frac{6.9}{16} \quad \frac{7.0}{12} \quad \frac{2.8}{50}$$

$$\frac{6.84}{50} \quad \frac{7.0}{12} \quad \frac{6.2}{50}$$

$$\frac{6.80}{50} \quad \frac{7.0}{12} \quad \frac{6.24}{50}$$

$$+ 73 = 0 + 0.0$$

$$\frac{7.5}{30} \quad \frac{6.7}{14} \quad 6.6 \quad \frac{6.9}{12} \quad \frac{7.1}{50} \quad \frac{6.7}{50}$$

$$\frac{7.1}{50} \quad \frac{7.2}{16} \quad 7.0 \quad \frac{7.5}{12} \quad \frac{13.4}{27} \quad \frac{13.6}{50} - 10.0$$

$$\frac{11.7}{50} \quad \frac{11.9}{43} \quad \frac{11.3}{21} \quad \frac{8.0}{14} \quad 7.4 \quad \frac{7.8}{13} \quad \frac{13.1}{26} \quad \frac{12.7}{50}$$

$$\frac{12.0}{100} \quad \frac{10.1}{41} \quad \frac{10.3}{27} \quad \frac{7.2}{22} \quad \frac{8.4}{15} \quad 7.7 \quad \frac{8.5}{14} \quad \frac{11.0}{23} \quad \frac{10.5}{50} \quad \frac{7.0}{100}$$

Sta	+	Σ	-	Elev.
		936.16		
12				28.1 . 2+27
	+70			27.7 . 2+97
BM.			6.40	929.76 . 929.77
13				27.4 . 3+27
	+55			26.8 . 3+82
14				26.2 . 4+27
	+37	4 Coly		25.8 . 4+69
15				25.8 . 5+27
T.P.	12.15	937.49 .	10.82	925.34 .
	+20			25.6 .
	+17			25.5 .
16				25.0 25.5

129.71

$$100 - \frac{7.3}{50} \frac{8.0}{14} 8.1 \frac{8.5}{13} \frac{8.0}{21} \frac{6.3}{27} \frac{6.7}{30} \frac{8.7}{100}$$

$$(Yard) \frac{43.0}{50} \frac{41.0}{30} \frac{40}{26} \frac{8.9}{15} 8.5 \frac{9.2}{14} \frac{9.3}{21} \frac{7.8}{28} \frac{7.7}{50}$$

Sp Kin 12' Oak 60' Rt Sta 12+80

$$(Yard) \frac{46.0}{50} \frac{00}{33} \frac{07}{29} \frac{8.9}{20} \frac{9.3}{15} 8.8 \frac{9.2}{13} \frac{8.8}{19} \frac{8.5}{24} \frac{6.9}{50} \frac{8.0}{100}$$

$$\frac{6.2}{100} \frac{9.2}{50} \frac{12.0}{34} \frac{11.3}{20} \frac{9.9}{14} 9.4 \frac{10.0}{12} \frac{12.0}{16} \frac{13.0}{22} \frac{12.6}{50} \frac{9.0}{100}$$

$$\frac{14.0}{100} \frac{14.6}{50} \frac{14.0}{23} \frac{10.7}{14} 10.0 \frac{10.7}{12} \frac{14.0}{19} \frac{14.5}{50} \frac{13.0}{100}$$

$$\frac{13.0}{100} \frac{13.1}{50} \frac{14.9}{32} \frac{14.5}{22} \frac{11.4}{13} 10.4 \frac{11.1}{12} \frac{14.2}{19} \frac{14.9}{100} - \text{ctr Pot Hole}$$

$$\frac{11.0}{100} \frac{14.0}{50} \frac{9.2}{33} \frac{10.8}{24} \frac{11.0}{15} 10.4 \frac{11.0}{13} \frac{12.1}{23} \frac{11.6}{50}$$

nail in PP Lt Sta 15+73

$$\frac{14.0}{100} \frac{11.0}{50} \frac{8.7}{33} \frac{8.2}{28} \frac{12.5}{16} 11.9 \frac{12.4}{11} \frac{10.8}{21} \frac{9.9}{25} \frac{10.9}{50+100}$$

$$\frac{5.5}{100} \frac{15.1}{50} \frac{10.9}{28} \frac{13.5}{22} \frac{12.8}{16} 12.0 \frac{12.4}{11} \frac{11.1}{19} \frac{6.9}{24} \frac{6.7}{50} \frac{7.0}{100}$$

$$100-50 \frac{23.0}{50} \frac{22.2}{33} \frac{17.2}{27} \frac{13.2}{14} 12.5 \frac{12.9}{12} \frac{13.2}{22} \frac{10.6}{25} \frac{9.9}{50} \frac{8.0}{100}$$

Sta	+	π	-	E/cv.
		937.49		24.4
17				
①	1.65	925.91	13.23	924.26
+40				24.2
18				24.4
①	1.66	925.92	1.65	924.26
+62				25.4
①	11.40	935.66	1.66	924.26
19				26.3
20				28.5
21				30.7
B.M.	5.43	937.23	3.84	931.82 931.80
22				33.0
+75				35.3

$\frac{9.6}{100}$ $\frac{11.7}{34}$ $\frac{11.0}{28}$ $\frac{12.8}{26}$ $\frac{13.7}{15}$ 13.1 $\frac{13.7}{12}$ $\frac{11.6}{22}$ $\frac{10.0}{27}$ $\frac{15.0}{50}$ $\frac{55}{100}$

$\frac{+1.5}{100}$ $\frac{1.6}{50}$ $\frac{4.3}{34}$ $\frac{4.5}{19}$ $\frac{2.2}{14}$ 17 $\frac{2.5}{10}$ $\frac{10.3}{28}$ $\frac{13.5}{42}$ $\frac{13.8}{50}$ $\frac{14.1}{100}$

$\frac{19.5}{100}$ $\frac{18.5}{36}$ $\frac{2.3}{14}$ 1.5 $\frac{2.2}{10}$ $\frac{17.5}{36}$ $\frac{15.7}{50}$ $\frac{15.4}{100}$

$\frac{5.5}{100}$ $\frac{6.0}{50}$ $\frac{7.3}{35}$ $\frac{5.9}{27}$ $\frac{9.9}{14}$ 0.5 $\frac{1.3}{12}$ $\frac{10.6}{27}$ $\frac{13.9}{36-100}$

$\frac{25}{100}$ $\frac{11.0}{50}$ $\frac{9.4}{34}$ $\frac{11.0}{29}$ $\frac{11.8}{21}$ $\frac{12.0}{15.0}$ 9.4 $\frac{10.0}{14}$ $\frac{13.1}{27}$ $\frac{18.0}{40}$ $\frac{20.0}{50}$ $\frac{21.0}{100}$

$\frac{5.1}{100}$ $\frac{7.3}{50}$ $\frac{6.3}{34}$ $\frac{7.6}{26}$ $\frac{7.8}{15}$ 7.2 $\frac{7.6}{12}$ $\frac{7.5}{21}$ $\frac{3.1}{27}$ $\frac{4.9}{50}$ $\frac{13.0}{100}$

$\frac{0.0}{100}$ $\frac{7.0}{50}$ $\frac{6.9}{34}$ $\frac{6.4}{21}$ $\frac{5.5}{16}$ 5.0 $\frac{5.4}{12}$ $\frac{5.6}{21}$ $\frac{1.7}{27}$ $\frac{0.0}{37}$ $\frac{+1.5}{50}$ $\frac{14.0}{100}$

Sprk in 24" rails 100' Lt Sta 21+00

$\frac{0.0}{100}$ $\frac{9.0}{50}$ $\frac{8.4}{34}$ $\frac{8.0}{21}$ $\frac{5.1}{13}$ 4.2 $\frac{4.8}{14}$ $\frac{4.1}{22}$ $\frac{3.6}{26}$ $\frac{0.2}{50}$ $\frac{16.0}{100}$

$\frac{+1.0}{100}$ $\frac{3.0}{50}$ $\frac{3.1}{34}$ $\frac{3.2}{24}$ $\frac{2.5}{14}$ 1.9 $\frac{2.3}{13}$ $\frac{+1.0}{24}$ $\frac{+0.7}{26}$ $\frac{2.4}{50}$ $\frac{12.1}{100}$

Sta.	+	Δ	—	Elev.
0	10.54	946.15	1.62	935.61
23				36.2
24				39.4
25				39.9
26				37.6
0 B.M.	1.96	938.47	9.69	936.51 936.47
+24				37.0
+28				36.9
+40				36.6
+52				36.3
+56				36.3

Nov 17 P.P. Lt. Sta. 22+33

$\frac{4.0}{100}$ $\frac{6.5}{50}$ $\frac{8.0}{34}$ $\frac{9.0}{25}$ $\frac{10.5}{15}$ 10.0 $\frac{10.5}{12}$ $\frac{8.6}{21}$ $\frac{8.4}{26}$ $\frac{12.0}{50}$ $\frac{23.0}{100}$

$\frac{10.0}{100}$ $\frac{+1.0}{50}$ $\frac{+1.6}{34}$ $\frac{+1.4}{26}$ $\frac{3.6}{24}$ $\frac{7.4}{15}$ 6.8 $\frac{7.3}{12}$ $\frac{5.6}{21}$ $\frac{5.0}{26}$ $\frac{10.0}{50}$ $\frac{29.0}{100}$

$\frac{+0.5}{50}$ $\frac{0.5}{34}$ $\frac{0.8}{29}$ $\frac{3.5}{22}$ $\frac{6.8}{14}$ 6.3 $\frac{6.6}{13}$ $\frac{2.8}{22}$ $\frac{2.7}{26}$ $\frac{1.5}{50}$ $\frac{1.2}{80}$ $\frac{1.8}{100}$

$\frac{5.5}{50}$ $\frac{7.5}{34}$ $\frac{8.0}{24}$ $\frac{9.1}{14}$ 8.6 $\frac{8.9}{13}$ $\frac{8.0}{21}$ $\frac{8.1}{25}$ $\frac{6.1}{50}$ $\frac{4.0}{75}$ $\frac{11.0}{100}$

Ctr. Mott. Sta. 26+40.52

Bottom of Ditch 1.5 $\frac{1.6}{14}$ $\frac{2.0}{26}$ $\frac{2.8}{50}$ $\frac{3.0}{100}$

Shoulder 1.6 $\frac{1.6}{14}$ $\frac{1.9}{50}$ $\frac{2.0}{100}$

$\frac{+3.0}{100}$ $\frac{+3.5}{50}$ $\frac{+1.7}{34}$ $\frac{.09}{27}$ $\frac{2.4}{12}$ 1.9 $\frac{1.8}{14}$ $\frac{1.7}{50}$ 100

Shoulder 2.2 $\frac{2.3}{14}$ $\frac{2.1}{50}$

Ditch 2.2 $\frac{2.7}{14}$ $\frac{3.1}{50}$

938.47

Sta.	+	π	-	Elev
BM.	2.02	938.49	9.64	936.51
			?	
27				35.5
+35				35.0
28				33.7
29				33.0
+55				33.1
				33.5
30				33.0
31				34.8
0	13.79	948.66	3.62	934.87
32				35.6
33				36.1
+70				36.8

Ctr Mont Sta 26 + 40.52

$\frac{0.0}{100}$ $\frac{+1.0}{50}$ $\frac{0.1}{24}$ $\frac{4.1}{21}$ $\frac{3.3}{12}$ 3.0 $\frac{3.6}{16}$ $\frac{3.9}{25}$ $\frac{0.9}{30}$ $\frac{2.4}{50}$ $\frac{1.2}{100}$

$\frac{5.0}{100}$ $\frac{6.1}{50}$ $\frac{6.9}{37}$ $\frac{6.5}{21}$ $\frac{4.1}{12}$ 3.5 $\frac{4.1}{15}$ $\frac{5.4}{17}$ $\frac{5.3}{50}$ $\frac{4.5}{100}$

$\frac{17.0}{100}$ $\frac{17.2}{50}$ $\frac{16.1}{29}$ $\frac{15.4}{12}$ 4.8 $\frac{5.7}{14}$ $\frac{12.6}{26}$ $\frac{11.2}{50}$ $\frac{15.7}{100}$

$\frac{14.0}{100}$ $\frac{16.0}{50}$ $\frac{15.5}{28}$ $\frac{6.1}{12}$ 5.5 $\frac{6.1}{13}$ $\frac{13.8}{27}$ $\frac{14.5}{50}$ $\frac{8.0}{100}$

$\frac{8.5}{100}$ $\frac{9.7}{50}$ $\frac{9.3}{29}$ $\frac{5.7}{12}$ 5.4 $\frac{5.9}{12}$ $\frac{10.9}{30}$ $\frac{11.9}{50}$ $\frac{11.0}{100}$

$\frac{2.0}{100}$ $\frac{4.5}{50}$ $\frac{3.9}{25}$ $\frac{5.6}{29}$ $\frac{5.5}{13}$ 5.0 $\frac{5.3}{14}$ $\frac{3.6}{26}$ $\frac{0.5}{30}$ $\frac{0.5}{50}$ $\frac{0.0}{79}$ $\frac{+4.5}{100}$

$\frac{0.0}{100}$ $\frac{+1.0}{50}$ $\frac{+0.8}{25}$ $\frac{4.3}{17.13}$ 3.7 $\frac{4.0}{15}$ $\frac{3.9}{24}$ $\frac{+2.0+2.5}{34}$ $\frac{+3.0}{50}$ $\frac{+3.0}{100}$

$\frac{7.8}{100}$ $\frac{10.9}{50}$ $\frac{11.5}{37}$ $\frac{12.1}{20}$ $\frac{13.1}{18}$ $\frac{13.4}{11}$ 13.1 $\frac{13.5}{14}$ $\frac{13.7}{20}$ $\frac{14.2}{40-50}$ $\frac{13.6}{100}$

$\frac{7.0}{100}$ $\frac{6.0}{65}$ $\frac{7.0}{50}$ $\frac{1.4}{23}$ $\frac{12.2}{17}$ $\frac{12.9}{12}$ 12.6 $\frac{13.3}{16}$ $\frac{15.0}{22}$ $\frac{15.4}{50}$ $\frac{14.2}{100}$

$\frac{13.2}{100}$ $\frac{11.1}{50}$ $\frac{11.9}{21-17}$ $\frac{12.2}{10}$ 11.9 $\frac{12.1}{12}$ $\frac{12.4}{21}$ $\frac{12.8}{29}$ $\frac{13.4}{50}$ $\frac{14.0}{100}$

Sta	+	Σ	-	Elev
		948.66		
34				37.3 .
35				38.8 .
+60				39.4 .
36				39.6 .
②	5.57	945.09	9.14	939.52 .
②	7.64	947.11	5.62	939.47 .
37				40.2 .
38				41.3 .
39				43.5
40				46.2 .
①	11.40	957.68	0.89	946.22

11.4

$\frac{13.0}{100}$ $\frac{8.6}{75}$ $\frac{6.6}{50}$ $\frac{4.6}{30}$ $\frac{5.3}{20}$ $\frac{7.3}{19}$ $\frac{10.2}{12}$ 9.9 $\frac{10.1}{14}$ $\frac{5.4}{25}$ $\frac{1.4}{32}$ $\frac{0.6}{50}$ $\frac{+2.5}{100}$

$\frac{9.8}{100}$ $\frac{5.8}{55}$ $\frac{8.9}{30}$ $\frac{9.9}{21}$ $\frac{9.6}{17}$ $\frac{9.8}{12}$ 9.3 $\frac{9.4}{15}$ $\frac{6.4}{24}$ $\frac{3.6}{27}$ $\frac{1.3}{31}$ $\frac{0.9}{50}$ $\frac{+1.0}{100}$

$\frac{11.0}{100}$ $\frac{10.3}{50}$ $\frac{9.5}{11}$ 9.1 $\frac{9.1}{12}$ $\frac{8.3}{20}$ $\frac{6.8}{22}$ $\frac{4.8}{23}$ $\frac{3.8}{50}$ $\frac{1.0}{100}$

Nail in West Post Ent Lt Stg 36+00

$\frac{22.0}{100}$ $\frac{20.0}{50}$ $\frac{18.5}{37}$ $\frac{7.3}{12}$ 6.9 $\frac{7.3}{12}$ $\frac{8.6}{20}$ $\frac{7.5}{33}$ $\frac{6.3}{50}$ $\frac{3.5}{100}$

$\frac{22.0}{100}$ $\frac{21.2}{50}$ $\frac{18.0}{33}$ $\frac{6.4}{12}$ 5.8 $\frac{6.2}{12}$ $\frac{13.0}{24}$ $\frac{13.3}{50}$ $\frac{11.9}{100}$

$\frac{14.0}{100}$ $\frac{10.6}{50}$ $\frac{8.6}{28}$ $\frac{4.0}{12}$ 3.6 $\frac{4.2}{12}$ $\frac{4.3}{22}$ $\frac{3.7}{25}$ $\frac{3.6}{50}$ $\frac{7.5}{100}$

$\frac{4.8}{100}$ $\frac{0.0}{50}$ $\frac{+4.0}{26}$ $\frac{1.3}{12}$ 0.9 $\frac{1.3}{14}$ $\frac{1.7}{24}$ $\frac{+4.9}{32}$ $\frac{+3.0}{50}$ $\frac{8.0}{100}$

Sta	+	Σ	-	Elev	
		957.68			
40 + 65				48.4	
41				49.5	
42				53.1	
B.M.			3.05	954.63	954.63
0	13.58	970.99	0.27	957.41	
43				57.4	
44				62.0	
+ 50				64.0	
45				66.0	
46				69.7	
0	11.97	981.91	1.05	969.94	
47				73.9	
0	9.18	986.84	4.25	977.66	

$\frac{16.1}{100}$ $\frac{14.7}{50}$ $\frac{12.5}{19}$ $\frac{9.8}{13}$ 9.3 $\frac{9.7}{13}$ $\frac{9.5}{26}$ $\frac{8.8}{31}$ $\frac{8.6}{50}$ $\frac{9.5}{100}$

$\frac{17.8}{100}$ $\frac{17.0}{50}$ $\frac{16.7}{54}$ $\frac{8.5}{12}$ 8.2 $\frac{8.8}{13}$ $\frac{13.8}{25}$ $\frac{12.7}{50-100}$

$\frac{15.3}{100}$ $\frac{14.6}{50}$ $\frac{14.4}{27}$ $\frac{5.4}{12}$ 4.6 $\frac{4.9}{15}$ $\frac{11.8}{25}$ $\frac{12.1}{50}$ $\frac{11.0}{100}$

Sprink PP. 48' Sta 42+45

Nail to Road Sta 43+00

$\frac{16.8}{100}$ $\frac{15.8}{50}$ $\frac{15.0}{17}$ $\frac{14.0}{12}$ 13.6 $\frac{13.8}{13}$ $\frac{14.2}{18}$ $\frac{12.5}{24}$ $\frac{12.2}{35}$ $\frac{10.0}{50}$ $\frac{7.0}{100}$

$\frac{7.5}{100}$ $\frac{6.5}{50}$ $\frac{5.5}{21}$ $\frac{9.7}{15}$ $\frac{9.6}{12}$ 9.0 $\frac{9.1}{14}$ $\frac{7.4}{17}$ $\frac{0.0}{31}$ $\frac{+0.2}{100}$

$\frac{0.0}{100}$ $\frac{+1.3}{50}$ $\frac{+1.8}{25}$ $\frac{7.0}{14}$ $\frac{7.5}{12}$ 7.0 $\frac{7.5}{14}$ $\frac{7.2}{18}$ $\frac{+0.5}{25}$ $\frac{+0.5}{100}$

$\frac{0.8}{100}$ $\frac{1.4}{50}$ $\frac{1.8}{42-19}$ $\frac{5.2}{13}$ $\frac{5.6}{10}$ 5.0 $\frac{5.3}{15}$ $\frac{6.1}{18}$ $\frac{2.9}{25}$ $\frac{2.7}{50}$ $\frac{2.0}{100}$

$\frac{0.0}{100}$ $\frac{0.8}{50}$ $\frac{1.1}{28}$ $\frac{1.2}{13}$ $\frac{1.6}{11}$ 1.3 $\frac{1.9}{16}$ $\frac{2.4}{19}$ $\frac{2.2}{23}$ $\frac{1.9}{37}$ $\frac{1.2}{50}$ $\frac{0.3}{100}$

$\frac{4.9}{100}$ $\frac{5.6}{50}$ $\frac{7.2}{26}$ $\frac{7.0}{18}$ $\frac{8.4}{10}$ 8.0 $\frac{8.3}{14}$ $\frac{8.1}{16}$ $\frac{6.6}{24}$ $\frac{7.2}{50}$ $\frac{6.1}{100}$

Sta	+	π	-	Elev	
		986.84			
48				77.6	
49				80.0	
50				81.7	
51				82.2	
52				82.5	
+50				83.1	
+59	So. Shoulder "F"			83.3	
B.M.	5.98	991.20	1.62	985.22	985.22
+87	No Shoulder "F"			83.8	
+91				83.8	
53				83.7	
+70				84.7	

$\frac{4.0}{100}$ $\frac{4.0}{50}$ $\frac{3.2}{24}$ $\frac{9.7}{13}$ $\frac{9.5}{10}$ 9.2 $\frac{9.5}{13}$ $\frac{9.7}{16}$ $\frac{6.8}{25}$ $\frac{8.7}{50}$ $\frac{9.6}{100}$

$\frac{6.0}{100}$ $\frac{4.8}{50}$ $\frac{3.3}{23}$ $\frac{7.9}{13}$ $\frac{7.1}{10}$ 6.8 $\frac{7.0}{14}$ $\frac{7.4}{7}$ $\frac{3.4}{23}$ $\frac{5.7}{50}$ $\frac{7.0}{100}$

$\frac{6.0}{100}$ $\frac{5.8}{50}$ $\frac{4.1}{18}$ $\frac{5.8}{11}$ $\frac{5.4}{8}$ 5.1 $\frac{5.5}{17}$ $\frac{5.6}{21}$ $\frac{6.1}{36}$ $\frac{8.1}{30-100}$

$\frac{4.0}{100}$ $\frac{9.3}{50}$ $\frac{4.0}{32}$ $\frac{5.3}{13}$ $\frac{5.2}{10}$ 4.6 $\frac{5.6}{16}$ $\frac{8.4}{20}$ $\frac{9.8}{26}$ $\frac{9.7}{50}$ $\frac{9.0}{100}$

$\frac{14.5}{100}$ $\frac{13.9}{50}$ $\frac{12.2}{28}$ 14 $\frac{4.9}{12}$ 4.3 $\frac{4.7}{15}$ $\frac{8.4}{22-50}$ $\frac{7.5}{100}$

$\frac{13.9}{45}$ $\frac{11.0}{50}$ $\frac{5.7}{33}$ 37 $\frac{3.7}{12}$ $\frac{3.8}{17}$ $\frac{1.8}{28}$ $\frac{0.8}{50}$ $\frac{0.0}{100}$

$\frac{8.9}{45}$ $\frac{6.5}{50}$ $\frac{4.4}{18}$ 3.5 $\frac{3.4}{17}$ $\frac{3.6}{50-100}$

SpK in 8" Oak 2E. Cor Hamlin & F

$\frac{3.5}{100}$ $\frac{10.1}{43}$ $\frac{7.7}{14}$ 7.4 $\frac{7.3}{34}$ $\frac{6.7}{100}$

$\frac{3.5}{100}$ $\frac{10.5}{50}$ $\frac{10.3}{44}$ $\frac{8.2}{15}$ 7.4 $\frac{7.5}{35}$ $\frac{7.0}{100}$

$\frac{5.5}{100}$ $\frac{2.9}{50}$ $\frac{6.6}{20}$ $\frac{7.5}{12}$ 7.5 $\frac{7.5}{38-50}$ $\frac{+0.5}{74}$ $\frac{0.0}{100}$

$\frac{5.5}{100}$ $\frac{4.4}{50}$ $\frac{3.3}{21}$ $\frac{6.7}{12}$ 6.5 $\frac{6.9}{14}$ $\frac{4.0}{21}$ $\frac{0.0}{38}$ $\frac{+0.5}{50}$ $\frac{0.5}{100}$

Sta	+	Σ	-	Elev
		991.20		
54				85.2
55				86.4
56				85.8
57				84.5
+55				83.5
58				82.5
59				80.5
+50				79.8
○	2.22	981.36	12.06	979.14
B.M.			0.44	880.92
				980.92
60				79.2

SS = Same Slope
or Same Shift

$\frac{5.5}{100}$ $\frac{5.1}{50}$ $\frac{4.0}{21}$ $\frac{6.0}{14}$ 6.0 $\frac{6.3}{12}$ $\frac{1.6}{21}$ $\frac{0.8}{50}$ $\frac{5.8}{100}$

$\frac{2.7}{100}$ $\frac{3.3}{50}$ $\frac{3.4}{20}$ $\frac{5.4}{13}$ 4.8 $\frac{5.1}{16}$ $\frac{3.6}{20}$ $\frac{3.3}{50}$ $\frac{2.8}{100}$

$\frac{4.4}{100}$ 5.0 $\frac{4.9}{16}$ $\frac{5.5}{14}$ 5.4 $\frac{6.1}{17}$ $\frac{5.9}{20}$ $\frac{3.7}{50}$ $\frac{2.0}{100}$

$\frac{5.5}{100}$ $\frac{5.1}{50}$ $\frac{6.6}{28}$ 7.0 $\frac{7.0}{13}$ 6.7 $\frac{8.0}{19}$ $\frac{7.4}{22}$ $\frac{6.5}{38}$ $\frac{4.5}{100}$

$\frac{5.5}{100}$ $\frac{1.8}{47}$ $\frac{3.8}{30}$ $\frac{4.7}{22}$ $\frac{8.0}{14}$ 7.7 $\frac{8.7}{18}$ $\frac{8.2}{22}$ $\frac{8.8}{26}$ $\frac{9.0}{45}$ $\frac{7.5}{100}$

$\frac{5.5}{100}$ $\frac{4.5}{50}$ $\frac{8.5}{20}$ $\frac{8.9}{18}$ $\frac{9.2}{12}$ 8.7 $\frac{9.2}{16}$ $\frac{11.2}{20}$ $\frac{11.6}{25}$ $\frac{11.0}{44}$ $\frac{5.5}{100}$

SS $\frac{7.7}{50}$ $\frac{12.7}{35}$ $\frac{12.9}{20}$ $\frac{11.2}{13}$ 10.7 $\frac{11.4}{17}$ $\frac{13.3}{20}$ $\frac{13.5}{26}$ $\frac{12.0}{50}$ $\frac{5.5}{100}$

$\frac{7.0}{100}$ $\frac{8.2}{50}$ $\frac{11.3}{22}$ $\frac{12.1}{15}$ 11.4 $\frac{12.3}{14}$ $\frac{12.7}{18}$ $\frac{12.2}{22-26}$ $\frac{10.6}{50}$ $\frac{5.5}{100}$

Set SpK in 30' Oak 120' Rt Sta 59+90

$\frac{3.9}{100}$ $\frac{5.5}{50}$ $\frac{3.9}{29}$ $\frac{4.7}{21}$ $\frac{2.6}{12}$ 2.2 $\frac{2.8}{13}$ $\frac{4.8}{19}$ $\frac{5.5}{23}$ $\frac{5.6}{33}$ $\frac{5.3}{50}$ $\frac{4.2}{100}$

Sta	+	π	-	Elev.
		981.36		
61				77.9
62				76.7
63				74.9
64				72.0
65				69.3
66	7.80	975.91	13.25	948.11
66				67.3
67				67.3
68				68.0
69				70.3
70				71.8

$\frac{3.0}{100}$ $\frac{1.0}{40}$ $\frac{1.0}{18}$ $\frac{3.8}{11}$ 3.5 $\frac{3.9}{11}$ $\frac{5.1}{17}$ $\frac{4.3}{22}$ $\frac{3.4}{24}$ $\frac{3.8}{50-100}$

$\frac{3.0}{100}$ $\frac{10.5}{50}$ $\frac{0.0}{28}$ $\frac{5.6}{16}$ $\frac{4.9}{11}$ 4.7 $\frac{5.4}{14}$ $\frac{6.3}{18}$ $\frac{5.0}{24}$ $\frac{6.8}{50-100}$

$\frac{5.5}{100}$ $\frac{3.5}{50}$ $\frac{4.8}{35}$ $\frac{6.7}{29}$ $\frac{6.7}{26}$ $\frac{7.5}{17}$ $\frac{7.2}{13}$ 6.5 $\frac{7.0}{13}$ $\frac{6.6}{18}$ $\frac{4.5}{20}$ $\frac{4.4}{50}$ $\frac{5.0}{100}$

$\frac{5.5}{100}$ $\frac{9.0}{50}$ $\frac{9.7}{37}$ $\frac{9.8}{28}$ $\frac{10.9}{18}$ $\frac{9.8}{14}$ 9.4 $\frac{9.9}{12}$ $\frac{10.8}{14}$ $\frac{11.0}{18}$ $\frac{11.8}{26}$ $\frac{13.0}{50-100}$

$\frac{5.5}{100}$ $\frac{13.9}{50}$ $\frac{14.1}{40}$ $\frac{14.3}{28}$ $\frac{14.0}{22}$ $\frac{12.5}{16}$ 12.1 $\frac{12.8}{11}$ $\frac{15.0}{15}$ $\frac{18.0}{36-100}$

$\frac{12.6}{100}$ $\frac{13.4}{50}$ $\frac{13.3}{34}$ $\frac{13.0}{27}$ $\frac{12.6}{20}$ $\frac{9.2}{15}$ 8.6 $\frac{9.2}{11}$ $\frac{12.3}{15}$ $\frac{13.5}{30}$ $\frac{13.1}{50-100}$

$\frac{12.2}{100}$ $\frac{13.5}{29}$ $\frac{12.7}{22}$ $\frac{9.4}{16}$ 8.6 $\frac{9.0}{10}$ $\frac{10.9}{15}$ $\frac{13.0}{26}$ $\frac{12.3}{50}$ $\frac{11.0}{80}$ $\frac{12.3}{100}$

$\frac{9.5}{100}$ $\frac{12.9}{50}$ $\frac{12.5}{29}$ $\frac{11.9}{23}$ $\frac{8.5}{16}$ 7.9 $\frac{8.2}{10}$ $\frac{11.2}{14}$ $\frac{12.5}{23}$ $\frac{11.5}{50}$ $\frac{8.5}{100}$

$\frac{2.0}{100}$ $\frac{2.8}{50}$ $\frac{3.1}{36}$ $\frac{5.5}{29}$ $\frac{6.4}{22}$ $\frac{5.6}{18}$ 5.6 $\frac{6.3}{12}$ $\frac{7.6}{16}$ $\frac{7.4}{20}$ $\frac{7.7}{25}$ $\frac{2.0}{34}$ $\frac{1.9}{50-100}$

$\frac{5.5}{100}$ $\frac{0.4}{37}$ $\frac{3.4}{31}$ $\frac{4.6}{28}$ $\frac{5.0}{20}$ 4.1 $\frac{4.4}{10-17}$ $\frac{1.4}{22}$ $\frac{0.6}{50-100}$

Sta	+	-	Elev.
		875.91	
71			71.5
72			69.7
73			66.5
0	3.59	966.74	12.76 963.15 ✓
74			63.1
75			60.3
76			59.2
77			59.1
+55			59.6
78			60.4
+73			61.7

$\frac{0.5}{100}$ $\frac{1.8}{28}$ $\frac{2.8}{24}$ $\frac{4.8}{14}$ 4.4 $\frac{4.6}{11}$ $\frac{5.1}{16}$ $\frac{4.2}{22}$ $\frac{2.0}{60}$

$\frac{0.0}{100}$ $\frac{+0.5}{29}$ $\frac{3.4}{23}$ $\frac{6.3}{15}$ 6.2 $\frac{6.8}{12}$ $\frac{6.7}{19}$ $\frac{3.2}{28-50}$ $\frac{5.6}{100}$

$\frac{2.3}{100}$ $\frac{2.3}{50}$ $\frac{2.8}{31}$ $\frac{8.4}{23}$ $\frac{9.9}{15}$ 9.4 $\frac{9.7}{13}$ $\frac{11.0}{16}$ $\frac{10.0}{20}$ $\frac{6.0}{32}$ $\frac{7.2}{50}$ $\frac{5.1}{100}$

Nail to Sta 74+00

$\frac{2.8}{100}$ $\frac{4.9}{50}$ $\frac{6.8}{24}$ $\frac{4.0}{14}$ 3.6 $\frac{4.4}{12}$ $\frac{9.9}{20}$ $\frac{10.9}{28}$ $\frac{11.6}{100}$

$\frac{10.8}{100}$ $\frac{11.1}{50}$ $\frac{11.4}{22}$ $\frac{7.1}{13}$ 6.4 $\frac{7.4}{13}$ $\frac{10.8}{20}$ $\frac{11.3}{50-100}$

ctr ditch

$\frac{10.2}{100}$ $\frac{10.6}{50}$ $\frac{10.8}{36}$ $\frac{11.9}{30}$ $\frac{11.7}{26}$ $\frac{11.1}{20}$ $\frac{8.3}{14}$ 7.5 $\frac{8.2}{13}$ $\frac{10.9}{20}$ $\frac{10.0}{50}$ $\frac{11.0}{80}$ $\frac{7.1}{100}$

$\frac{10.0}{100-75}$ $\frac{7.5}{65-50}$ $\frac{9.9}{42}$ $\frac{10.8}{30}$ $\frac{10.7}{20}$ $\frac{8.2}{13}$ 7.6 $\frac{8.4}{13}$ $\frac{10.7}{19}$ $\frac{10.8}{30}$ $\frac{10.0}{50}$ $\frac{7.0}{100}$

$\frac{7.4}{100}$ $\frac{10.1}{50}$ $\frac{10.8}{35}$ $\frac{10.7}{24}$ $\frac{10.2}{19}$ $\frac{8.0}{14}$ 7.1 $\frac{7.7}{13}$ $\frac{8.7}{19}$ $\frac{8.3}{26}$ $\frac{7.3}{50}$ $\frac{5.8}{100}$

$\frac{3.5}{100-70}$ $\frac{6.0}{50}$ $\frac{6.7}{34}$ $\frac{11.2}{25}$ $\frac{7.8}{20}$ $\frac{6.8}{14}$ 6.3 $\frac{6.8}{14}$ $\frac{6.2}{19}$ $\frac{2.5}{28}$ $\frac{1.0}{50}$ $\frac{5.1}{100}$

$\frac{1.6}{100}$ $\frac{0.6}{50}$ $\frac{1.5}{28}$ $\frac{5.4}{21}$ $\frac{5.5}{15}$ 5.0 $\frac{5.7}{13}$ $\frac{7.3}{20}$ $\frac{6.6}{50}$ $\frac{5.6}{100}$

Sta	+	Σ	-	Elev
		966.74		
79				61.8 .
+65				62.7 .
80				63.7 .
BM.			1.61	965.13 .
⊙	8.82	974.39 .	1.17	965.57 .
81				66.2 .
82				68.3 .
83				69.5 .
84				71.5 .
⊙	9.25	982.91 .	0.73	973.66 .
85				74.2 .
86				76.2 .

$$\frac{4.1}{100} \quad \frac{2.0}{41} \quad \frac{4.5}{28} \quad \frac{5.1}{21} \quad \frac{5.4}{16} \quad 4.9 \quad \frac{5.4}{19} \quad \frac{7.4}{18} \quad \frac{7.2}{30} \quad \frac{6.0}{50} \quad \frac{5.1}{100}$$

$$\frac{2.9}{100} \quad \frac{5.9}{50} \quad \frac{7.8}{38-27} \quad \frac{7.4}{21} \quad \frac{4.4}{15} \quad 4.0 \quad \frac{4.3}{13} \quad \frac{6.4}{18} \quad \frac{6.0}{44} \quad \frac{5.7}{50} \quad \frac{3.7}{100}$$

$$\frac{3.8}{100} \quad \frac{4.7}{50} \quad \frac{3.4}{23} \quad \frac{3.4}{16} \quad 3.0 \quad \frac{3.2}{13} \quad \frac{4.6}{18} \quad \frac{2.3}{50}$$

Set SpK in 24" W. Oak 80' Lt Sta 80+50

Nail on F.P. Lt Sta 80+15

$$\frac{6.3}{100} \quad \frac{6.6}{40} \quad \frac{9.0}{28} \quad \frac{8.1}{21} \quad \frac{8.4}{16} \quad 8.2 \quad \frac{8.3}{10} \quad \frac{7.9}{14} \quad \frac{7.3}{21} \quad \frac{6.8}{29} \quad \frac{5.1}{50} \quad \frac{5.5}{100}$$

$$\frac{4.1}{100} \quad \frac{2.9}{35} \quad \frac{5.5}{29} \quad \frac{8.2}{21} \quad \frac{6.9}{13} \quad 6.1 \quad \frac{6.4}{12} \quad \frac{6.2}{16} \quad \frac{5.3}{23} \quad \frac{4.7}{30} \quad \frac{3.6}{100}$$

$$\frac{8.0}{100} \quad \frac{7.2}{50} \quad \frac{6.2}{29} \quad \frac{6.6}{21} \quad \frac{5.7}{17} \quad 4.9 \quad \frac{5.2}{12} \quad \frac{8.1}{18} \quad \frac{9.5}{50} \quad \frac{10.3}{100}$$

$$\frac{5.5}{100} \quad \frac{4.9}{50} \quad \frac{3.9}{29} \quad \frac{4.1}{21} \quad \frac{3.4}{15} \quad 2.9 \quad \frac{3.2}{14} \quad \frac{4.1}{17} \quad \frac{3.6}{23} \quad \frac{0.6}{50} \quad \frac{5.5}{100}$$

$$\frac{9.4}{100} \quad \frac{8.4}{50} \quad \frac{8.9}{29} \quad \frac{8.0}{19} \quad \frac{9.0}{14} \quad 8.7 \quad \frac{9.1}{12} \quad \frac{7.9}{18} \quad \frac{6.1}{23} \quad \frac{5.2}{50} \quad \frac{5.5}{80} = \text{Ho. Floor.}$$

$$\frac{7.5}{100-80} \quad \frac{6.8}{50} \quad \frac{5.7}{28} \quad \frac{5.4}{18} \quad \frac{6.1}{14} \quad 6.7 \quad \frac{6.9}{12} \quad \frac{7.1}{18} \quad \frac{5.2}{34} \quad \frac{4.3}{50-100}$$

Sta	+	X	-	Elev
-----	---	---	---	------

		982.91		
--	--	--------	--	--

7				78.2
---	--	--	--	------

8				78.8
---	--	--	--	------

9				79.0
---	--	--	--	------

0	7.88	987.09	3.70	979.21
---	------	--------	------	--------

90				80.1
----	--	--	--	------

11				81.2
----	--	--	--	------

+40				81.5
-----	--	--	--	------

2				81.9
---	--	--	--	------

BM.			4.43	982.64
-----	--	--	------	--------

3				82.0
---	--	--	--	------

14				82.2
----	--	--	--	------

$\frac{55}{100}$ $\frac{47}{50}$ $\frac{39}{40}$ $\frac{50}{33}$ $\frac{44}{28}$ $\frac{40}{18}$ $\frac{49}{74}$ 47 $\frac{51}{13}$ $\frac{38}{78}$ $\frac{24}{22}$ $\frac{25}{50}$ 100

$\frac{55}{100}$ $\frac{63}{50}$ $\frac{57}{29}$ $\frac{48}{20}$ $\frac{45}{12}$ 41 $\frac{44}{13}$ $\frac{54}{17}$ $\frac{56}{25}$ $\frac{51}{50}$ $\frac{46}{100}$

$\frac{76}{100}$ $\frac{63}{50}$ $\frac{49}{18}$ $\frac{41}{14}$ 39 $\frac{44}{13}$ $\frac{73}{19}$ $\frac{79}{23}$ $\frac{77}{50}$ 100

Top F. Gir Post, Rt Stg 89+00

$\frac{98}{100}$ $\frac{93}{50}$ $\frac{91}{23}$ $\frac{84}{20}$ $\frac{74}{13}$ 70 $\frac{74}{12}$ $\frac{89}{18}$ $\frac{82}{24}$ $\frac{88}{38}$ $\frac{89}{50}$ $\frac{55}{100}$

$\frac{43}{100}$ $\frac{40}{50}$ $\frac{47}{25}$ $\frac{59}{15}$ $\frac{60}{10}$ 59 $\frac{63}{74}$ $\frac{58}{18}$ $\frac{54}{23-28}$ $\frac{64}{30}$ $\frac{55}{100}$

$\frac{55}{100}$ $\frac{17}{50}$ $\frac{48}{19}$ $14 - \frac{56}{9}$ 56 $\frac{54}{14}$ $\frac{47}{20}$ $\frac{44}{23}$ $\frac{45}{50}$ $\frac{50}{100}$ (4.7 Floor Ho)

$\frac{37}{100}$ $\frac{57}{50}$ $\frac{72}{24}$ $\frac{58}{15}$ $\frac{54}{11}$ 52 $\frac{58}{14}$ $\frac{51}{19}$ $\frac{52}{20}$ $\frac{50}{27}$ $\frac{46}{50}$ $\frac{67}{100}$

Set Spk in 18" Oak 180' Lt Stg 92+00

$\frac{48}{100}$ $\frac{55}{50}$ $\frac{67}{27}$ $\frac{68}{17}$ $\frac{57}{13}$ $\frac{54}{11}$ 51 $\frac{57}{13}$ $\frac{71}{17}$ $\frac{79}{22}$ $\frac{82}{100}$

$\frac{86}{100}$ $\frac{98}{50}$ $\frac{99}{40}$ $\frac{75}{18}$ $\frac{54}{11}$ 49 $\frac{54}{13}$ $\frac{81}{19}$ 50 $\frac{75}{100}$

Sta	+	π	-	Elev
		987.09		
95				82.7
96				83.5
97	5.24	989.04	3.29	983.80
98				83.8
				82.4
+70				80.3
99				79.6
100				76.2
0			7.51	981.41

$\frac{7.4}{100}$ $\frac{6.6}{50}$ $\frac{4.9}{19}$ $\frac{5.4}{15}$ $\frac{4.8}{11}$ 4.4 $\frac{4.9}{13}$ $\frac{5.2}{21}$ $\frac{5.6}{50}$ $\frac{4.6}{100}$

$\frac{5.5}{100}$ $\frac{3.0}{50}$ $\frac{3.6}{28}$ $\frac{3.5}{18}$ $\frac{4.0}{14}$ $\frac{3.7}{10}$ 3.6 $\frac{4.1}{18}$ $\frac{3.4}{16}$ $\frac{2.6}{27}$ $\frac{2.2}{50}$ $\frac{5.5}{100}$

Top R.R. SpK & Sta 96+82.40

$\frac{5.0}{100}$ $\frac{4.1}{50}$ $\frac{3.8}{21}$ $\frac{5.3}{16}$ $\frac{5.4}{11}$ 5.2 $\frac{5.6}{11}$ $\frac{5.8}{15}$ $\frac{2.2}{24}$ $\frac{1.4}{30}$ $\frac{1.0}{100}$

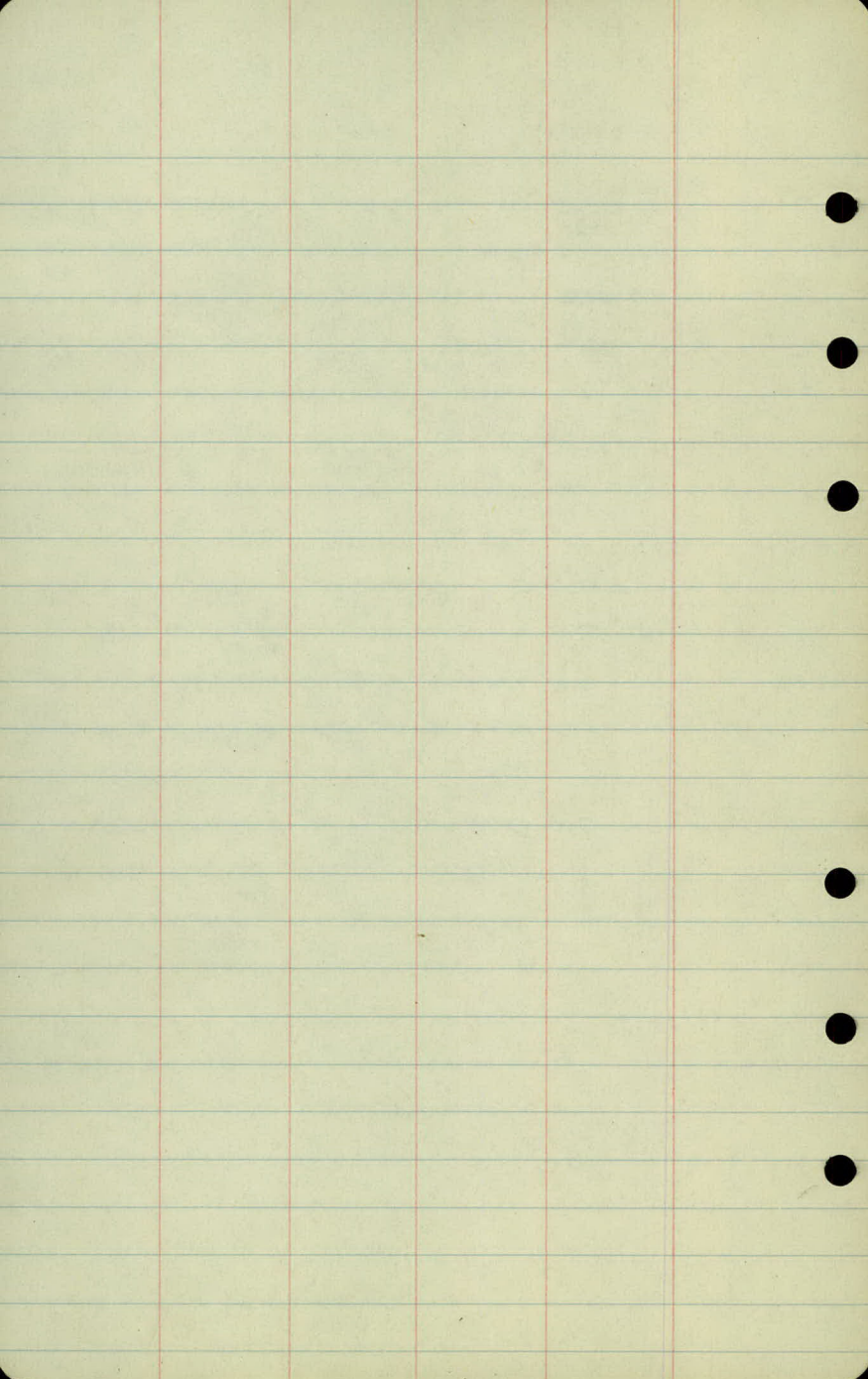
$\frac{5.5}{100}$ $\frac{6.3}{50}$ $\frac{4.7}{20}$ $\frac{6.3}{15}$ $\frac{6.8}{11}$ 6.6 $\frac{7.1}{11}$ $\frac{7.0}{16}$ $\frac{4.6}{24}$ $\frac{5.0}{50}$ $\frac{5.6}{100}$

$\frac{9.5}{100}$ $\frac{10.4}{50}$ $\frac{10.2}{20}$ $\frac{7.5}{16}$ $\frac{7.0}{12}$ 8.7 $\frac{8.8}{11}$ $\frac{8.5}{15}$ $\frac{7.6}{24}$ $\frac{9.0}{50}$ -100

$\frac{9.9}{100}$ $\frac{8.4}{50}$ $\frac{6.8}{21}$ $\frac{10.7}{15}$ $\frac{9.9}{11}$ 9.4 $\frac{9.7}{13}$ $\frac{9.2}{16}$ $\frac{8.1}{25}$ $\frac{9.5}{50}$ -100

$\frac{5.6}{100}$ $\frac{5.8}{50}$ $\frac{8.3}{25}$ $\frac{13.5}{13}$ $\frac{13.1}{10}$ 12.8 $\frac{13.2}{13}$ $\frac{12.7}{18}$ $\frac{7.0}{33}$ $\frac{8.5}{50}$ -100

Top FPost Lt Sta 100+00



Cross Sections
No. Hamline Ave.
Sta. - 101 to

Sta.	+	π	-	Elev.
0	0.18	981.65		981.47

101				71.7
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+45				68.5
-----	--	--	--	------

0	0.41	972.10	9.96	971.69
---	------	--------	------	--------

102				66.5
-----	--	--	--	------

103				61.8
-----	--	--	--	------

0	2.12	963.27	10.95	961.15
---	------	--------	-------	--------

+47				59.8
-----	--	--	--	------

104				57.8
-----	--	--	--	------

105				54.5
-----	--	--	--	------

+26				54.0
-----	--	--	--	------

+33				53.9
-----	--	--	--	------

+48 64				53.4
--------	--	--	--	------

0			10.02	953.25
---	--	--	-------	--------

Top of Fence post sta. 100 + 00 - 18' Left.

$\frac{0.5}{100}$ $\frac{0.4}{50}$ $\frac{0.2}{34}$ $\frac{10.5}{20}$ $\frac{10.1}{13}$ 10.0 $\frac{10.5}{13}$ $\frac{10.6}{20}$ $\frac{3.9}{35}$ $\frac{4.8}{50}$ $\frac{11.0}{100}$

$\frac{5.5}{100}$ $\frac{6.0}{50}$ $\frac{6.7}{43}$ $\frac{6.8}{32}$ $\frac{13.4}{20}$ $\frac{13.3}{12}$ 13.2 $\frac{13.6}{13}$ $\frac{13.6}{18}$ $\frac{12.6}{31}$ $\frac{13.4}{50}$ $\frac{19.0}{100}$

Nail in sta. 101

$\frac{2.0}{100}$ $\frac{0.5}{50}$ $\frac{+0.6}{20}$ $\frac{5.8}{18}$ $\frac{5.6}{12}$ 5.6 $\frac{5.9}{13}$ $\frac{6.1}{20}$ $\frac{7.1}{30}$ $\frac{8.7}{50}$ $\frac{12.4}{100}$

$\frac{+2.9}{100}$ $\frac{0.0}{50}$ $\frac{4.3}{37}$ $\frac{7.1}{27}$ $\frac{10.0}{19}$ $\frac{10.4}{12}$ 10.3 $\frac{10.9}{13}$ $\frac{12.7}{19}$ $\frac{15.9}{25}$ $\frac{19.3}{40}$ $\frac{19.2}{50}$ $\frac{12.0}{100}$

Top of Fence Post sta. 103 + 47 - 21' Left.

$\frac{+0.5}{100}$ $\frac{3.5}{50}$ $\frac{5.6}{21}$ $\frac{4.4}{14}$ $\frac{3.7}{10}$ 3.5 $\frac{4.3}{13}$ $\frac{9.0}{20}$ $\frac{12.7}{34}$ $\frac{12.7}{50}$ $\frac{9.8}{100}$

$\frac{1.3}{100}$ $\frac{5.4}{50}$ $\frac{8.4}{31}$ $\frac{8.5}{22}$ $\frac{7.5}{15}$ $\frac{5.7}{12}$ 5.5 $\frac{6.2}{14}$ $\frac{11.7}{21}$ $\frac{13.8}{37}$ $\frac{14.0}{50}$ $\frac{13.6}{100}$

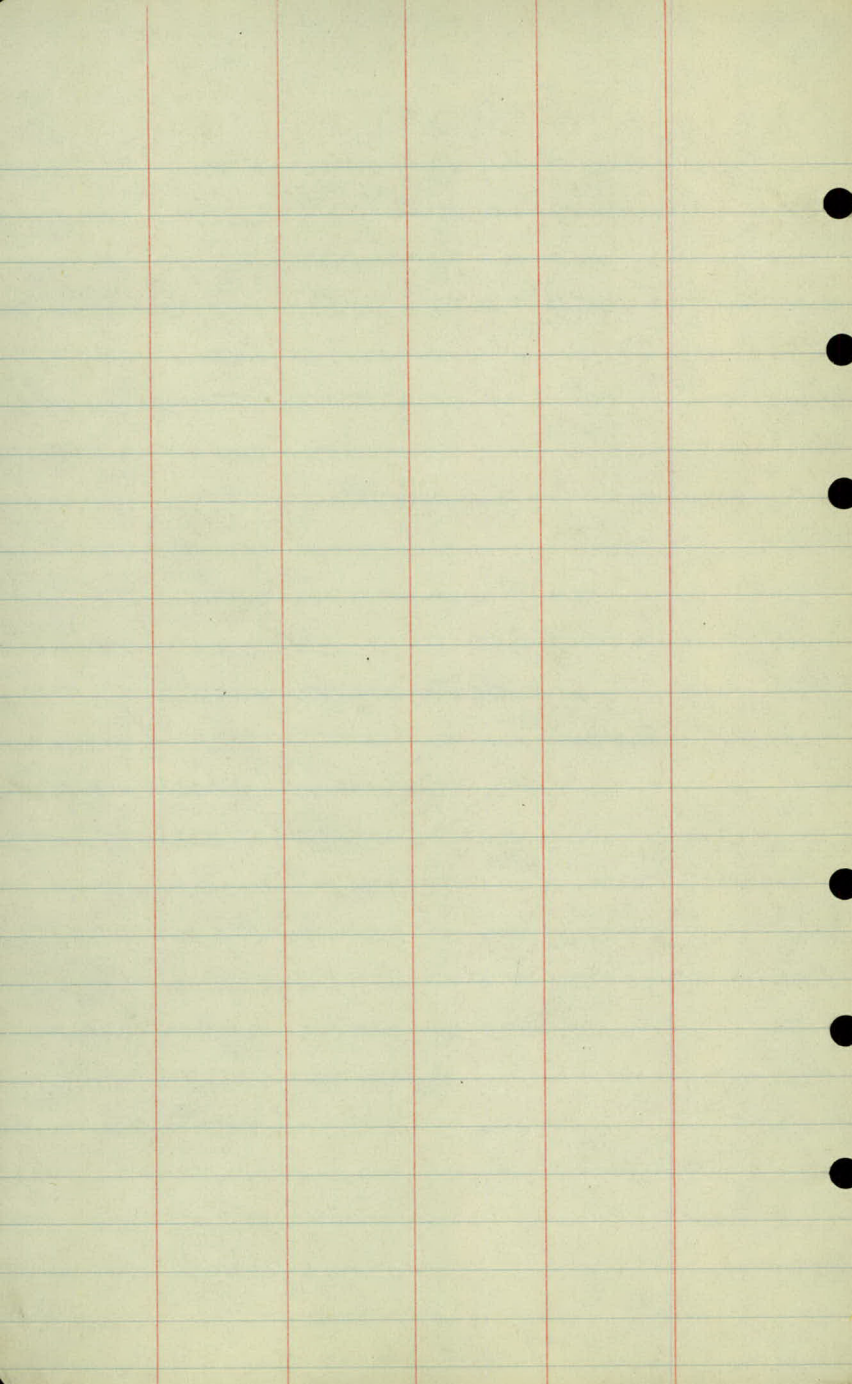
$\frac{7.3}{100}$ $\frac{9.3}{50}$ $\frac{10.2}{33}$ $\frac{10.2}{24}$ $\frac{10.3}{16}$ $\frac{9.3}{12}$ 8.8 $\frac{9.4}{14}$ $\frac{13.7}{20}$ $\frac{13.6}{34}$ $\frac{13.8}{50}$ $\frac{13.5}{100}$

$\frac{9.3}{100}$ $\frac{9.4}{50}$ $\frac{10.7}{35}$ $\frac{9.8}{18}$ $\frac{9.3}{12}$ 9.3 $\frac{9.5}{14}$ $\frac{10.0}{21}$ $\frac{13.2}{50}$ $\frac{12.9}{100}$

$\frac{9.5}{50}$ $\frac{9.6}{25}$ $\frac{9.5}{14}$ 9.4 $\frac{9.5}{14}$ $\frac{9.5}{21}$ $\frac{10.1}{50}$

$\frac{9.1}{100}$ $\frac{9.5}{50}$ 9.9 $\frac{9.8}{50}$ $\frac{9.6}{100}$

ctr of Mont. - Int. S.F.H. #96



Hamline Ave.

Cross Sections.

Bratager } $\frac{3}{37}$
Wilke }
Ellen }

Sta.	+	∞	-	Elev.
B.M.	1.00	954.25		953.25
105+70				52.8
+75				52.7
+85				52.4
106				52.0
+50				51.1
107				50.4
+50				49.9
+81				49.7
Culvert 12" V.T.P.				
108+50				49.7
109				49.5
+50				49.5
110				49.7

Lt.

E

Rt.

Top of monument (atr) at
Hamline Ave. & Co. Rd. "C"

$$\begin{array}{r} \frac{14}{50} \quad \frac{16}{25} \quad \frac{15}{20} \quad \frac{20}{50} \quad \frac{14}{50} \\ \frac{0.5}{50} \quad \frac{2.5}{30} \quad \frac{2.0}{18} \quad \frac{16}{25} \quad \frac{2.0}{25} \quad \frac{1.5}{50} \end{array}$$

$$\frac{16}{50} \quad \frac{43}{29} \quad \frac{36}{19} \quad \frac{27}{16} \quad \frac{19}{20} \quad \frac{27}{26} \quad \frac{48}{38} \quad \frac{63}{50}$$

$$\frac{24}{50} \quad \frac{48}{34} \quad \frac{48}{21} \quad \frac{28}{11} \quad \frac{23}{14} \quad \frac{32}{20} \quad \frac{61}{21} \quad \frac{70}{31} \quad \frac{71}{50}$$

$$\frac{82}{50} \quad \frac{82}{30} \quad \frac{80}{21} \quad \frac{42}{14} \quad \frac{32}{14} \quad \frac{42}{21} \quad \frac{60}{29} \quad \frac{83}{50}$$

$$\frac{94}{50} \quad \frac{86}{24} \quad \frac{52}{15} \quad \frac{41}{6} \quad \frac{39}{11} \quad \frac{47}{20} \quad \frac{86}{20} \quad \frac{95}{50}$$

$$\frac{98}{50} \quad \frac{102}{30} \quad \frac{87}{23} \quad \frac{55}{14} \quad \frac{44}{13} \quad \frac{52}{19} \quad \frac{89}{28} \quad \frac{101}{50}$$

$$\frac{99}{50} \quad \frac{99}{25} \quad \frac{105}{12} \quad \frac{46}{14} \quad \frac{57}{21} \quad \frac{93}{21} \quad \frac{105}{50}$$

$$\frac{85}{50} \quad \frac{86}{40} \quad \frac{90}{27} \quad \frac{100}{25} \quad \frac{68}{20} \quad \frac{50}{12} \quad \frac{46}{14} \quad \frac{58}{19} \quad \frac{97}{27} \quad \frac{101}{30}$$

$$\frac{88}{50} \quad \frac{100}{27} \quad \frac{102}{23} \quad \frac{56}{14} \quad \frac{48}{14} \quad \frac{55}{19} \quad \frac{94}{36} \quad \frac{105}{25} \quad \frac{104}{50}$$

$$\frac{100}{30} \quad \frac{100}{24} \quad \frac{57}{14} \quad \frac{48}{13} \quad \frac{54}{20} \quad \frac{90}{25} \quad \frac{96}{50}$$

$$\frac{98}{50} \quad \frac{102}{27} \quad \frac{110}{23} \quad \frac{54}{13} \quad \frac{46}{14} \quad \frac{55}{19} \quad \frac{82}{34} \quad \frac{27}{50}$$

Sta. + 丕 - Elev.

110+20 954.75 49.6

+50 49.5

+75 49.5

111 49.6

+40 49.6

112 49.8

T.P. 10.65 959.00 5.90 948.35

+50 49.9

113 50.6

+60 51.3

Lt.

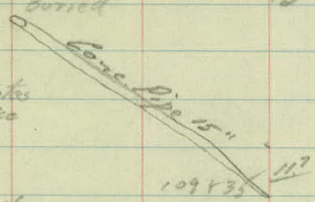
E

Rt.

$\frac{91}{50}$ $\frac{20}{25}$ $\frac{29}{24}$ $\frac{97}{30}$ $\frac{55}{13}$ $\frac{47}{11}$
 110 ± Buried

$\frac{57}{13}$ $\frac{20}{19}$ $\frac{57}{34}$ $\frac{59}{50}$

See Calc notes
 Buried in ice



$\frac{69}{50}$ $\frac{73}{31}$ $\frac{63}{21}$ $\frac{56}{17}$

109 ± 35 $\frac{117}{13}$ $\frac{68}{18}$ $\frac{107}{40}$ $\frac{108}{50}$

$\frac{10}{50}$ $\frac{29}{30}$ $\frac{83}{24}$ $\frac{55}{13}$ $\frac{48}{11}$ $\frac{55}{13}$ $\frac{93}{19}$ $\frac{103}{27}$ $\frac{116}{50}$

$\frac{17}{50}$ $\frac{53}{24}$ $\frac{31}{18}$ $\frac{57}{17}$ $\frac{47}{11}$ $\frac{58}{14}$ $\frac{109}{24}$ $\frac{112}{50}$

Buried in ice

$\frac{108}{110 \pm 64}$

$\frac{113}{111 \pm 00}$

Calc # 9-84
 18" Conc. Pipe

$\frac{58}{50}$ $\frac{69}{34}$ $\frac{68}{16}$ $\frac{57}{17}$ $\frac{47}{11}$

$\frac{55}{13}$ $\frac{110}{21}$ $\frac{116}{50}$

$\frac{68}{50}$ $\frac{20}{17}$ $\frac{50}{17}$ $\frac{45}{13}$ $\frac{57}{18}$ $\frac{98}{18}$ $\frac{115}{50}$

$\frac{79}{50}$ $\frac{87}{31}$ $\frac{87}{21}$ $\frac{107}{17}$ $\frac{94}{13}$ $\frac{91}{14}$ $\frac{98}{14}$ $\frac{129}{18}$ $\frac{126}{23}$ $\frac{144}{40}$ $\frac{148}{50}$

$\frac{67}{50}$ $\frac{69}{23}$ $\frac{86}{21}$ $\frac{91}{17}$ $\frac{88}{10}$ $\frac{84}{15}$ $\frac{90}{19}$ $\frac{99}{25}$ $\frac{100}{25}$ $\frac{107}{50}$

$\frac{98}{50}$ $\frac{85}{21}$ $\frac{100}{18}$ $\frac{87}{17}$ $\frac{77}{15}$ $\frac{81}{15}$ $\frac{84}{19}$ $\frac{63}{26}$ $\frac{51}{30}$ $\frac{81}{31}$ $\frac{14}{50}$

Sta. + X - Elev.

959.00

114

51.7

+50

52.4

T.P.

11.56

964.57

5.99

953.01

115

53.2

+50

53.9

+83

14" Conc. Pipe Culv.

54.9

116 +25

55.7

+75

57.1

117 Entrance Lt.

57.7

+50

58.6

118

59.8

+50

60.8

B.M.

4.66

967.65

1.58

967.99

Lt.

E

Rt.

4

$$\frac{96}{50} \quad \frac{96}{20} \quad \frac{96}{19} \quad \frac{77}{18} \quad \frac{73}{17} \quad \frac{77}{15} \quad \frac{85}{21} \quad \frac{70}{27} \quad \frac{48}{32} \quad \frac{20}{36} \quad \frac{12}{50}$$

$$\frac{59}{50} \quad \frac{66}{19} \quad \frac{76}{16} \quad \frac{69}{13} \quad \frac{66}{14} \quad \frac{70}{28} \quad \frac{55}{33} \quad \frac{40}{36} \quad \frac{15}{50}$$

$$\frac{37}{50} \quad \frac{44}{28} \quad \frac{63}{21} \quad \frac{117}{18} \quad \frac{117}{17} \quad \frac{114}{15} \quad \frac{116}{13} \quad \frac{88}{32} \quad \frac{38}{27} \quad \frac{27}{50}$$

$$\frac{61}{50} \quad \frac{78}{38} \quad \frac{93}{23} \quad \frac{116}{16} \quad \frac{109}{17} \quad \frac{107}{15} \quad \frac{111}{19} \quad \frac{115}{30} \quad \frac{108}{50}$$

$$\frac{102}{50} \quad \frac{108}{18} \quad \frac{114}{14} \quad \frac{101}{12} \quad \frac{97}{16} \quad \frac{105}{19} \quad \frac{126}{25} \quad \frac{137}{50}$$

$$\frac{98}{50} \quad \frac{101}{16} \quad \frac{94}{13} \quad \frac{89}{12} \quad \frac{94}{17} \quad \frac{95}{21} \quad \frac{96}{33} \quad \frac{97}{45} \quad \frac{108}{50}$$

$$\frac{72}{50} \quad \frac{65}{30} \quad \frac{75}{23} \quad \frac{76}{14} \quad \frac{75}{12} \quad \frac{80}{20} \quad \frac{54}{24} \quad \frac{15}{28} \quad \frac{21}{50}$$

$$\frac{59}{50} \quad \frac{69}{18} \quad \frac{69}{14} \quad \frac{74}{23} \quad \frac{11}{31} \quad \frac{23}{50}$$

$$\frac{68}{50} \quad \frac{67}{16} \quad \frac{62}{11} \quad \frac{60}{13} \quad \frac{62}{17} \quad \frac{63}{19} \quad \frac{42}{34} \quad \frac{43}{50}$$

$$\frac{53}{50} \quad \frac{58}{18} \quad \frac{51}{13} \quad \frac{48}{13} \quad \frac{52}{17} \quad \frac{52}{20} \quad \frac{23}{29} \quad \frac{25}{50}$$

$$\frac{29}{50} \quad \frac{31}{29} \quad \frac{40}{11} \quad \frac{38}{14} \quad \frac{39}{21} \quad \frac{17}{27} \quad \frac{23}{50}$$

Spike in Power Pole 125' Lt. 5th. 118 + 70

Sta. + π — Elev.

119 962.65 61.4

+50 61.9

120 62.5

+50 62.4

121 61.9

+50 61.2

122 60.2

+50 59.2

123 58.3

T.R. 3.85 961.58 9.92 957.73

+50 57.4

124 56.6

+33 Enter Lt. 56.3

+66 56.1

Lt.

L

Rt.

5

$$\frac{6.0}{50} \quad \frac{6.3}{36} \quad \frac{6.5}{15} \quad \frac{6.4}{11} \quad \frac{6.3}{1} \quad \frac{6.8}{14} \quad \frac{5.4}{21} \quad \frac{5.9}{30} \quad \frac{5.8}{50}$$

$$\frac{1.8}{50} \quad \frac{4.1}{23} \quad \frac{6.7}{17} \quad \frac{6.1}{14} \quad \frac{5.8}{5} \quad \frac{6.3}{16} \quad \frac{7.1}{23} \quad \frac{7.5}{50}$$

$$\frac{2.4}{50} \quad \frac{1.8}{20} \quad \frac{5.6}{15} \quad \frac{5.2}{5} \quad \frac{5.7}{13} \quad \frac{5.2}{17} \quad \frac{3.8}{19} \quad \frac{3.8}{37} \quad \frac{3.8}{50}$$

$$\frac{6.0}{50} \quad \frac{3.7}{27} \quad \frac{2.5}{21} \quad \frac{5.5}{14} \quad \frac{5.3}{5} \quad \frac{5.7}{13} \quad \frac{4.5}{18} \quad \frac{3.1}{21} \quad \frac{3.0}{42} \quad \frac{3.0}{50}$$

$$\frac{5.9}{50} \quad \frac{4.4}{25} \quad \frac{3.8}{20} \quad \frac{6.3}{15} \quad \frac{5.8}{5} \quad \frac{6.4}{16} \quad \frac{4.7}{20} \quad \frac{5.3}{50}$$

$$\frac{4.8}{50} \quad \frac{4.2}{28} \quad \frac{3.6}{21} \quad \frac{6.8}{16} \quad \frac{6.5}{5} \quad \frac{6.8}{14} \quad \frac{4.5}{19} \quad \frac{5.1}{34} \quad \frac{6.1}{50}$$

$$\frac{10.3}{50} \quad \frac{10.7}{28} \quad \frac{10.2}{19} \quad \frac{8.1}{15} \quad \frac{7.5}{5} \quad \frac{8.0}{14} \quad \frac{8.9}{17} \quad \frac{8.7}{25} \quad \frac{9.6}{50}$$

$$\frac{14.1}{50} \quad \frac{14.5}{34} \quad \frac{13.4}{20} \quad \frac{9.2}{14} \quad \frac{8.5}{5} \quad \frac{9.3}{14} \quad \frac{13.6}{21} \quad \frac{13.8}{39} \quad \frac{12.0}{50}$$

$$\frac{15.3}{50} \quad \frac{14.8}{21} \quad \frac{10.0}{14} \quad \frac{9.4}{5} \quad \frac{10.1}{15} \quad \frac{13.5}{21} \quad \frac{12.2}{39} \quad \frac{11.5}{50}$$

$$\frac{9.4}{50} \quad \frac{8.3}{21} \quad \frac{8.2}{19} \quad \frac{4.8}{13} \quad \frac{4.2}{5} \quad \frac{4.9}{14} \quad \frac{7.0}{20} \quad \frac{2.1}{27} \quad \frac{5.1}{50}$$

$$\frac{8.9}{50} \quad \frac{8.8}{19} \quad \frac{7.6}{15} \quad \frac{5.4}{11} \quad \frac{5.0}{5} \quad \frac{5.6}{14} \quad \frac{8.2}{20} \quad \frac{8.9}{27} \quad \frac{8.7}{50}$$

$$\frac{6.8}{100} \quad \frac{6.7}{50} \quad \frac{6.3}{20} \quad \frac{5.5}{12} \quad \frac{5.3}{5} \quad \frac{5.6}{14} \quad \frac{7.1}{18} \quad \frac{6.9}{50}$$

$$\frac{6.1}{50} \quad \frac{5.4}{23} \quad \frac{5.3}{20} \quad \frac{6.1}{14} \quad \frac{5.7}{11} \quad \frac{5.5}{5} \quad \frac{5.7}{14} \quad \frac{3.5}{19} \quad \frac{2.8}{50}$$

Sta.	+	Σ	-	Elev.
125		961.58		55.7
+50				55.2
126				54.7
+50				54.0
127				52.9
T.P.	3.09	955.89	8.78	952.80
+50				51.4
128				50.5
+50				49.5
129				48.6
+50				47.5
130				46.6
T.P.	3.28	949.31	9.86	946.03
B.M.	3.33	949.31	3.33	945.98

Lt.

E

Rt.

$$\frac{49}{50} \quad \frac{37}{21} \quad \frac{54}{18} \quad \frac{67}{15} \quad \frac{61}{11} \quad \frac{59}{14} \quad \frac{61}{21} \quad \frac{22}{50}$$

$$\frac{40}{50} \quad \frac{37}{20} \quad \frac{70}{14} \quad \frac{67}{12} \quad \frac{64}{14} \quad \frac{66}{18} \quad \frac{61}{22} \quad \frac{28}{50}$$

$$\frac{30}{50} \quad \frac{26}{26} \quad \frac{26}{21} \quad \frac{68}{16} \quad \frac{69}{11} \quad \frac{69}{14} \quad \frac{72}{18} \quad \frac{61}{22} \quad \frac{28}{50}$$

$$\frac{30}{50} \quad \frac{25}{23} \quad \frac{23}{18} \quad \frac{80}{15} \quad \frac{77}{11} \quad \frac{76}{13} \quad \frac{80}{18} \quad \frac{71}{24} \quad \frac{43}{26} \quad \frac{37}{50}$$

$$\frac{61}{50} \quad \frac{66}{28} \quad \frac{60}{21} \quad \frac{95}{16} \quad \frac{87}{18} \quad \frac{81}{22} \quad \frac{70}{50}$$

$$\frac{40}{50} \quad \frac{43}{23} \quad \frac{54}{17} \quad \frac{46}{10} \quad \frac{45}{15} \quad \frac{48}{21} \quad \frac{50}{26} \quad \frac{61}{50}$$

$$\frac{48}{50} \quad \frac{52}{37} \quad \frac{59}{14} \quad \frac{55}{11} \quad \frac{52}{13} \quad \frac{68}{22} \quad \frac{72}{24} \quad \frac{68}{42} \quad \frac{57}{50}$$

$$\frac{37}{50} \quad \frac{47}{32} \quad \frac{61}{20} \quad \frac{61}{12} \quad \frac{64}{15} \quad \frac{68}{18} \quad \frac{51}{29} \quad \frac{43}{50}$$

$$\frac{21}{50} \quad \frac{42}{29} \quad \frac{53}{18} \quad \frac{28}{15} \quad \frac{74}{11} \quad \frac{73}{16} \quad \frac{47}{21} \quad \frac{37}{30} \quad \frac{14}{50}$$

$$\frac{65}{50} \quad \frac{84}{33} \quad \frac{90}{17} \quad \frac{86}{12} \quad \frac{84}{13} \quad \frac{84}{17} \quad \frac{92}{22} \quad \frac{88}{50}$$

$$\frac{128}{50} \quad \frac{118}{25} \quad \frac{110}{16} \quad \frac{98}{12} \quad \frac{93}{13} \quad \frac{98}{20} \quad \frac{124}{37} \quad \frac{126}{50}$$

Spike in stump 100' Rt. Sta. 129+50

Sts.	+	π	-	Elev.
130+50		949.31		45.8
131				45.2
+50				44.8
132+10 = 12" Conc. Pipe Culv.				44.6
+50				44.5
133				44.9
T.R.	7.48	952.88	3.91	945.40
+50				45.4
134				45.7
+50				46.0
135				46.4
+50				46.5
+69 = 12" Conc. Pipe Culv. 34'				
136				47.1

LT.

E

RT.

$$\frac{21}{50} \quad \frac{60}{17} \quad \frac{41}{12} \quad \frac{35}{15} \quad \frac{44}{15} \quad \frac{20}{20} \quad \frac{89}{50}$$

$$\frac{69}{50} \quad \frac{67}{18} \quad \frac{45}{12} \quad \frac{41}{14} \quad \frac{47}{14} \quad \frac{64}{19} \quad \frac{94}{35} \quad \frac{104}{50}$$

$$\frac{74}{50} \quad \frac{68}{29} \quad \frac{21}{17} \quad \frac{50}{13} \quad \frac{45}{14} \quad \frac{53}{14} \quad \frac{82}{20} \quad \frac{103}{50}$$

$$\frac{25}{50} \quad \frac{85}{32} \quad \frac{97}{21} \quad \frac{56}{13} \quad \frac{47}{14} \quad \frac{55}{14} \quad \frac{106}{20} \quad \frac{102}{50}$$

$$\frac{67}{50} \quad \frac{82}{23} \quad \frac{96}{20} \quad \frac{57}{14} \quad \frac{48}{14} \quad \frac{54}{13} \quad \frac{104}{24} \quad \frac{101}{50}$$

$$\frac{23}{50} \quad \frac{38}{30} \quad \frac{48}{21} \quad \frac{48}{12} \quad \frac{44}{15} \quad \frac{50}{15} \quad \frac{57}{19} \quad \frac{54}{28} \quad \frac{48}{50}$$

$$\frac{06}{50} \quad \frac{10}{43} \quad \frac{50}{27} \quad \frac{68}{12} \quad \frac{79}{16} \quad \frac{29}{11} \quad \frac{75}{13} \quad \frac{72}{25} \quad \frac{50}{50}$$

$$\frac{45}{50} \quad \frac{52}{35} \quad \frac{72}{26} \quad \frac{62}{21} \quad \frac{80}{16} \quad \frac{77}{10} \quad \frac{72}{13} \quad \frac{25}{13} \quad \frac{68}{21} \quad \frac{48}{40} \quad \frac{48}{50}$$

$$\frac{118}{50} \quad \frac{89}{21} \quad \frac{25}{13} \quad \frac{69}{13} \quad \frac{72}{13} \quad \frac{64}{18} \quad \frac{51}{25} \quad \frac{123}{50}$$

$$\frac{134}{50} \quad \frac{125}{23} \quad \frac{73}{13} \quad \frac{65}{13} \quad \frac{65}{13} \quad \frac{57}{18} \quad \frac{50}{26} \quad \frac{0.3}{10}$$

$$\frac{134}{50} \quad \frac{125}{31} \quad \frac{119}{21} \quad \frac{21}{12} \quad \frac{64}{14} \quad \frac{67}{14} \quad \frac{73}{16} \quad \frac{62}{32} \quad \frac{20}{50}$$

$$\frac{10.4}{10.4}$$

$$\frac{8.9}{8.9}$$

$$\frac{13.3}{50} \quad \frac{123}{25} \quad \frac{63}{12} \quad \frac{68}{13} \quad \frac{63}{13} \quad \frac{22}{19} \quad \frac{67}{23} \quad \frac{63}{32} \quad \frac{30}{50}$$

Sta.	+	π	-	Elev.
136+50		954.88		47.4
137				47.8
+50				48.3
138				48.8
+50				49.2
139				50.1
+50				50.8
T.P.	10.2V	961.3V	1.78	951.10
140				51.0
+50				51.4
141				51.8
T.P.	5.0V	965.80	10.54	960.78
+50	Road left			52.2
142				51.9

L.

L

R.

$$\frac{127}{50} \quad \frac{107}{22} \quad \frac{95}{19} \quad \frac{62}{14} \quad \frac{55}{1} \quad \frac{59}{16} \quad \frac{57}{33} \quad \frac{47}{50}$$

$$\frac{109}{50} \quad \frac{104}{33} \quad \frac{86}{18} \quad \frac{57}{13} \quad \frac{51}{1} \quad \frac{54}{14} \quad \frac{51}{34} \quad \frac{45}{50}$$

$$\frac{101}{50} \quad \frac{74}{18} \quad \frac{51}{13} \quad \frac{46}{1} \quad \frac{50}{14} \quad \frac{39}{30} \quad \frac{37}{50}$$

$$\frac{81}{50} \quad \frac{57}{16} \quad \frac{46}{14} \quad \frac{41}{1} \quad \frac{46}{12} \quad \frac{43}{22} \quad \frac{42}{29} \quad \frac{43}{50}$$

$$\frac{72}{50} \quad \frac{62}{20} \quad \frac{54}{14} \quad \frac{40}{11} \quad \frac{37}{1} \quad \frac{40}{14} \quad \frac{46}{23} \quad \frac{44}{50}$$

$$\frac{34}{50} \quad \frac{32}{18} \quad \frac{33}{10} \quad \frac{28}{1} \quad \frac{32}{12} \quad \frac{30}{28} \quad \frac{27}{50}$$

$$\frac{+05}{50} \quad \frac{08}{21} \quad \frac{14}{14} \quad \frac{26}{11} \quad \frac{21}{1} \quad \frac{25}{12} \quad \frac{23}{19} \quad \frac{27}{50}$$

$$\frac{42}{50} \quad \frac{52}{35} \quad \frac{85}{18} \quad \frac{105}{10} \quad \frac{103}{1} \quad \frac{104}{14} \quad \frac{96}{20} \quad \frac{109}{50}$$

$$\frac{19}{50} \quad \frac{29}{35} \quad \frac{26}{19} \quad \frac{98}{15} \quad \frac{99}{1} \quad \frac{102}{10} \quad \frac{88}{28} \quad \frac{104}{50}$$

$$\frac{42}{50} \quad \frac{43}{32} \quad \frac{70}{21} \quad \frac{96}{14} \quad \frac{95}{1} \quad \frac{97}{11} \quad \frac{89}{14} \quad \frac{75}{23} \quad \frac{67}{36} \quad \frac{75}{50}$$

$$\frac{29}{50} \quad \frac{39}{11} \quad \frac{36}{1} \quad \frac{38}{12} \quad \frac{18}{25} \quad \frac{11}{50}$$

$$\frac{42}{50} \quad \frac{40}{23} \quad \frac{41}{15} \quad \frac{39}{1} \quad \frac{40}{12} \quad \frac{36}{16} \quad \frac{27}{25} \quad \frac{12}{50}$$

Sta. + π - Elev.

142+50 955.80 51.8

143 51.6

+50 50.9

144 49.7

+50 48.4

145 Ent. Left.

145 47.1

+50 45.9

146 44.3

+50 42.6

T.P. 6.26 949.22 12.84 948.96

147 40.7

+50 38.7

148 36.3

L+

E

R+

9

$$\frac{59}{50} \quad \frac{53}{23} \quad \frac{43}{15} \quad \frac{40}{13} \quad \frac{40}{13} \quad \frac{42}{18} \quad \frac{38}{28} \quad \frac{32}{50}$$

$$\frac{68}{50} \quad \frac{63}{18} \quad \frac{48}{13} \quad \frac{42}{14} \quad \frac{46}{14} \quad \frac{52}{16} \quad \frac{54}{21} \quad \frac{40}{50}$$

$$\frac{68}{50} \quad \frac{66}{17} \quad \frac{55}{14} \quad \frac{49}{15} \quad \frac{54}{15} \quad \frac{73}{19} \quad \frac{75}{32} \quad \frac{74}{50}$$

$$\frac{65}{50} \quad \frac{66}{21} \quad \frac{27}{15} \quad \frac{66}{13} \quad \frac{61}{15} \quad \frac{67}{15} \quad \frac{80}{50} \quad \frac{97}{50}$$

$$\frac{46}{50} \quad \frac{55}{20} \quad \frac{24}{14} \quad \frac{74}{13} \quad \frac{29}{19} \quad \frac{94}{29} \quad \frac{107}{29} \quad \frac{109}{50}$$

$$\frac{23}{50} \quad \frac{21}{19} \quad \frac{87}{50}$$

$$\frac{25}{50} \quad \frac{35}{23} \quad \frac{28}{14} \quad \frac{87}{15} \quad \frac{91}{23} \quad \frac{79}{40} \quad \frac{98}{50} \quad \frac{102}{50}$$

$$\frac{25}{50} \quad \frac{31}{24} \quad \frac{53}{24} \quad \frac{105}{15} \quad \frac{105}{10} \quad \frac{99}{18} \quad \frac{106}{16} \quad \frac{100}{21} \quad \frac{55}{21} \quad \frac{83}{50}$$

$$\frac{33}{50} \quad \frac{25}{25} \quad \frac{62}{23} \quad \frac{98}{18} \quad \frac{116}{13} \quad \frac{115}{14} \quad \frac{117}{17} \quad \frac{119}{23} \quad \frac{69}{26} \quad \frac{50}{26} \quad \frac{72}{50}$$

$$\frac{48}{50} \quad \frac{45}{28} \quad \frac{29}{26} \quad \frac{117}{20} \quad \frac{135}{15} \quad \frac{132}{14} \quad \frac{134}{20} \quad \frac{124}{25} \quad \frac{93}{26} \quad \frac{67}{33} \quad \frac{74}{33} \quad \frac{86}{50}$$

$$\frac{103}{50} \quad \frac{03}{29} \quad \frac{47}{26} \quad \frac{90}{18} \quad \frac{85}{10} \quad \frac{88}{18} \quad \frac{75}{24} \quad \frac{39}{25} \quad \frac{20}{30} \quad \frac{26}{30} \quad \frac{32}{50}$$

$$\frac{20}{50} \quad \frac{33}{40} \quad \frac{29}{30} \quad \frac{44}{25} \quad \frac{100}{20} \quad \frac{106}{16} \quad \frac{105}{14} \quad \frac{110}{21} \quad \frac{74}{23} \quad \frac{53}{33} \quad \frac{66}{33} \quad \frac{80}{50}$$

$$\frac{62}{50} \quad \frac{64}{27} \quad \frac{92}{24} \quad \frac{139}{18} \quad \frac{134}{12} \quad \frac{129}{13} \quad \frac{126}{17} \quad \frac{133}{20} \quad \frac{111}{24} \quad \frac{91}{28} \quad \frac{91}{28} \quad \frac{112}{50}$$

Sta. + π - Elev.

148+50 949.22 34.2

T.P.#1 7.97 945.29 11.90 937.32

149

+50

150

+50

151

+50

152

T.P.#2 13.09 937.20

T.P.#1 0.21 937.53 937.32

149 32.1

2

+50 29.9

150 27.6

Lt.

E

Rt.

10

$$\frac{78}{28} \quad \frac{87}{26} \quad \frac{158}{21} \quad \frac{153}{17} \quad \frac{150}{16} \quad \frac{154}{16} \quad \frac{115}{23} \quad \frac{90}{26} \quad \frac{100}{33} \quad \frac{107}{50}$$

$$\frac{10}{75} \quad \frac{27}{50} \quad \frac{37}{30} \quad \frac{51}{26} \quad 13.2$$

$$\frac{00}{75} \quad \frac{40}{43} \quad \frac{45}{29} \quad 15.4$$

$$\frac{38}{75} \quad \frac{55}{50} \quad \frac{56}{31} \quad 17.7$$

$$\frac{39}{75} \quad \frac{35}{50} \quad \frac{24}{38} \quad \frac{65}{37} \quad 20.2$$

$$\frac{54}{75} \quad \frac{48}{50} \quad \frac{42}{39} \quad \frac{87}{38} \quad 21.9$$

$$\frac{56}{75} \quad \frac{61}{50} \quad \frac{56}{39} \quad 24.7$$

$$\frac{72}{75} \quad \frac{93}{50} \quad \frac{101}{41} \quad \frac{95}{37} \quad \frac{128}{36} \quad 26.8$$

$$\frac{50}{21} \quad \frac{58}{17} \quad \frac{54}{17} \quad \frac{56}{8} \quad \frac{58}{15} \quad \frac{54}{18} \quad \frac{30}{21} \quad \frac{20}{22} \quad \frac{28}{26} \quad \frac{57}{50}$$

$$\frac{27}{20} \quad \frac{54}{16} \quad \frac{81}{12} \quad \frac{76}{12} \quad \frac{80}{14} \quad \frac{70}{18} \quad \frac{42}{21} \quad \frac{54}{23} \quad \frac{67}{34} \quad \frac{102}{50}$$

$$\frac{92}{23} \quad \frac{111}{20} \quad \frac{104}{16} \quad \frac{99}{10} \quad \frac{102}{12} \quad \frac{108}{18} \quad \frac{100}{18} \quad \frac{50}{24} \quad \frac{115}{50}$$

Sta.	+	π	-	Elev.
150+50		937.53		25.1
151				22.7
				23.4
T.P. for Check		5.33		932.20

T.P. 1.89 927.05 13.37 924.16
+50 20.6

152 18.5

+26 Ent. Pt. 16.9

+63 15.7

153 14.2

+26 12.9

+64 11.5

T.P. 0.97 914.80 13.27 913.83

153

B.M. 6.70 914.80 6.70 908.10

Lt.

E

Rt.

11

$$\frac{8.9}{27} \quad \frac{11.6}{23} \quad \frac{13.1}{18} \quad \frac{12.6}{15} \quad \frac{12.4}{8} \quad \frac{12.7}{11} \quad \frac{12.7}{16} \quad \frac{11.0}{19} \quad \frac{6.6}{26} \quad \frac{13.9}{50}$$

$$\frac{11.2}{27} \quad \frac{13.3}{21} \quad \frac{14.6}{16} \quad \frac{14.8}{18} \quad \frac{14.8}{27} \quad \frac{8.4}{39} \quad \frac{12.0}{50}$$

$$\frac{7.3}{19} \quad \frac{7.0}{11} \quad \frac{6.5}{15} \quad \frac{7.2}{17} \quad \frac{7.8}{23} \quad \frac{2.1}{50}$$

$$\frac{9.5}{18} \quad \frac{9.8}{16} \quad \frac{9.0}{13} \quad \frac{8.6}{14} \quad \frac{9.0}{19} \quad \frac{9.8}{22} \quad \frac{6.5}{50}$$

$$\begin{array}{l} +6.6 \\ 25 \end{array} \quad \begin{array}{l} +12.6 \\ 50 \end{array} \quad \frac{0.4}{31} \quad \frac{4.9}{26} \quad \frac{11.1}{18} \quad \frac{10.4}{14} \quad \frac{10.5}{10} \quad \frac{10.2}{14} \quad \frac{10.5}{21} \quad \frac{11.7}{50} \quad \frac{15.4}{100}$$

$$\frac{+4.0}{75} \quad \frac{1.0}{50} \quad \frac{3.4}{36} \quad \frac{5.4}{28} \quad \frac{10.3}{21} \quad \frac{12.0}{15} \quad \frac{11.6}{10} \quad \frac{11.4}{11} \quad \frac{12.0}{13} \quad \frac{13.4}{15} \quad \frac{13.4}{16} \quad \frac{12.9}{50} \quad \frac{17.6}{50}$$

$$\frac{0.0}{75} \quad \frac{4.0}{50} \quad \frac{2.0}{34} \quad \frac{8.4}{23} \quad \frac{12.7}{16} \quad \frac{13.6}{11} \quad \frac{13.7}{7} \quad \frac{12.9}{7}$$

$$\frac{2.5}{75} \quad \frac{6.7}{50} \quad \frac{7.9}{48} \quad \frac{9.2}{34} \quad \frac{10.6}{25} \quad \frac{12.0}{20} \quad \frac{14.7}{10} \quad \frac{14.2}{14.2}$$

$$\frac{6.6}{75} \quad \frac{9.0}{50} \quad \frac{11.7}{30} \quad \frac{16.4}{27} \quad \frac{14.4}{19} \quad \frac{16.0}{13} \quad \frac{16.2}{9} \quad \frac{15.6}{9}$$

$$\frac{.6}{75} \quad \frac{1.5}{74} \quad \frac{6.5}{18} \quad \frac{6.5}{19} \quad \frac{4.9}{19} \quad \frac{7.3}{25} \quad \frac{8.8}{50}$$

Top of concr. step North End of South Entrance
of dwelling 140' Rt. of Sta 152+63

Sta.	+	π	-	Elev.
153 + 26		914.80		
+64				907.7
154				909.7
+42				07.8
T.P.	0.68	907.81	7.67	907.13
155				05.3
+50				03.2
T.P.	1.01	901.67	7.15	900.66
156				00.9
+50				899.1
157				97.6
+50				96.5
158 = 18" Conc. Pipe Culvert				96.1
+50				95.9
159				95.8

89-90

LH

L

RH

12

$$\frac{1.9}{E} \quad \frac{2.7}{14} \quad \frac{7.6}{20} \quad \frac{7.6}{21} \quad \frac{6.7}{21} \quad \frac{8.8}{39} \quad \frac{9.8}{50}$$

$$\frac{3.3}{E} \quad \frac{4.5}{14} \quad \frac{9.7}{23} \quad \frac{14.3}{50}$$

$$\frac{1.6}{50} \quad \frac{4.3}{28} \quad \frac{5.9}{21} \quad \frac{5.4}{13} \quad \frac{5.1}{51} \quad \frac{5.9}{14} \quad \frac{9.9}{21} \quad \frac{13.9}{29} \quad \frac{16.8}{50}$$

$$\frac{10.2}{50} \quad \frac{11.4}{41} \quad \frac{10.9}{20} \quad \frac{7.4}{13} \quad \frac{7.0}{70} \quad \frac{7.9}{14} \quad \frac{16.3}{27} \quad \frac{20.8}{50}$$

$$\frac{9.9}{50} \quad \frac{9.4}{35} \quad \frac{9.0}{25} \quad \frac{6.2}{19} \quad \frac{3.0}{13} \quad \frac{2.5}{25} \quad \frac{3.2}{14} \quad \frac{12.9}{26} \quad \frac{15.6}{40} \quad \frac{16.4}{50}$$

$$\frac{11.8}{50} \quad \frac{11.3}{37} \quad \frac{11.1}{24} \quad \frac{9.8}{20} \quad \frac{4.8}{12} \quad \frac{4.6}{46} \quad \frac{5.6}{14} \quad \frac{11.6}{23} \quad \frac{15.6}{31} \quad \frac{15.1}{50}$$

$$\frac{8.4}{50} \quad \frac{8.3}{25} \quad \frac{6.6}{20} \quad \frac{1.0}{11} \quad \frac{0.8}{0.8} \quad \frac{2.0}{15} \quad \frac{9.8}{24} \quad \frac{12.6}{30} \quad \frac{14.0}{39} \quad \frac{14.9}{50}$$

$$\frac{12.0}{50} \quad \frac{10.7}{30} \quad \frac{9.4}{25} \quad \frac{2.9}{13} \quad \frac{2.6}{26} \quad \frac{3.8}{15} \quad \frac{10.1}{24} \quad \frac{12.6}{30} \quad \frac{14.2}{38} \quad \frac{15.0}{50}$$

$$\frac{13.3}{50} \quad \frac{12.3}{29} \quad \frac{11.3}{24} \quad \frac{4.7}{14} \quad \frac{4.1}{41} \quad \frac{5.1}{15} \quad \frac{10.5}{24} \quad \frac{13.6}{30} \quad \frac{14.9}{50}$$

$$\frac{13.6}{50} \quad \frac{13.5}{28} \quad \frac{10.8}{22} \quad \frac{8.5}{15} \quad \frac{8.2}{82} \quad \frac{8.9}{16} \quad \frac{9.8}{23} \quad \frac{14.3}{30} \quad \frac{15.1}{50}$$

$$\frac{13.4}{50} \quad \frac{13.4}{30} \quad \frac{14.1}{28} \quad \frac{11.0}{20} \quad \frac{6.1}{12} \quad \frac{6.16}{616} \quad \frac{6.7}{18} \quad \frac{11.8}{25} \quad \frac{15.1}{26} \quad \frac{15.3}{50}$$

$$\frac{12.9}{50} \quad \frac{12.7}{31} \quad \frac{11.6}{21} \quad \frac{6.1}{14} \quad \frac{6.8}{68} \quad \frac{6.7}{16} \quad \frac{10.0}{29} \quad \frac{14.0}{35} \quad \frac{15.1}{50}$$

$$\frac{11.2}{50} \quad \frac{10.0}{20} \quad \frac{6.2}{12} \quad \frac{5.9}{59} \quad \frac{6.7}{15} \quad \frac{11.0}{21} \quad \frac{12.7}{30} \quad \frac{13.8}{50}$$

Sta.	+	π	-	Elev.
159+50		901.67		895.9
+80				96.0
160+15				96.2
+50				96.3
161				96.4
T.P.	13.66	909.96	5.37	896.30
+50				896.3
162				96.2
+50				96.4
163				96.8
+50				97.6
164				98.6
+50				99.7
165				901.2

Lt.

Z

Rt.

$\frac{6.7}{50}$ $\frac{7.2}{19}$ $\frac{8.1}{15}$ $\frac{6.3}{12}$ $\frac{5.8}{14}$ $\frac{6.5}{19}$ $\frac{7.1}{26}$ $\frac{9.8}{50}$ $\frac{11.4}{50}$

$\frac{3.9}{50}$ $\frac{6.8}{23}$ $\frac{7.3}{17}$ $\frac{7.6}{16}$ $\frac{6.2}{13}$ $\frac{5.7}{14}$ $\frac{6.6}{19}$ $\frac{8.4}{19}$ $\frac{7.8}{30}$ $\frac{9.8}{43}$ $\frac{10.8}{50}$

$\frac{1.9}{50}$ $\frac{4.8}{28}$ $\frac{6.2}{19}$ $\frac{6.8}{16}$ $\frac{6.0}{13}$ $\frac{5.5}{14}$ $\frac{6.4}{18}$ $\frac{7.1}{18}$ $\frac{5.6}{30}$ $\frac{4.7}{40}$ $\frac{7.4}{50}$

$\frac{1.8}{50}$ $\frac{4.2}{30}$ $\frac{5.8}{19}$ $\frac{6.4}{15}$ $\frac{5.9}{13}$ $\frac{5.4}{15}$ $\frac{6.0}{17}$ $\frac{6.4}{17}$ $\frac{3.5}{38}$ $\frac{1.3}{40}$ $\frac{3.5}{50}$

$\frac{2.7}{50}$ $\frac{4.5}{31}$ $\frac{6.0}{16}$ $\frac{5.6}{12}$ $\frac{5.3}{15}$ $\frac{6.0}{15}$ $\frac{5.9}{20}$ $\frac{1.4}{35}$ $\frac{1.6}{50}$

$\frac{12.3}{50}$ $\frac{13.5}{29}$ $\frac{14.0}{16}$ $\frac{13.8}{13}$ $\frac{13.7}{15}$ $\frac{14.1}{16}$ $\frac{14.3}{21}$ $\frac{13.7}{30}$ $\frac{11.7}{30}$ $\frac{11.4}{50}$

$\frac{13.4}{50}$ $\frac{13.6}{29}$ $\frac{13.6}{13}$ $\frac{13.8}{17}$ $\frac{14.2}{28}$ $\frac{13.6}{28}$ $\frac{13.6}{50}$

$\frac{13.2}{50}$ $\frac{13.4}{20}$ $\frac{13.7}{16}$ $\frac{13.5}{13}$ $\frac{13.6}{15}$ $\frac{14.0}{19}$ $\frac{14.7}{19}$ $\frac{15.4}{50}$

$\frac{12.6}{50}$ $\frac{13.0}{19}$ $\frac{13.3}{17}$ $\frac{13.2}{12}$ $\frac{13.2}{14}$ $\frac{13.9}{14}$ $\frac{14.6}{17}$ $\frac{16.4}{50}$

$\frac{11.9}{50}$ $\frac{12.4}{26}$ $\frac{12.8}{15}$ $\frac{12.4}{13}$ $\frac{12.4}{15}$ $\frac{12.9}{18}$ $\frac{14.3}{29}$ $\frac{14.6}{29}$ $\frac{15.4}{50}$

$\frac{11.0}{50}$ $\frac{11.5}{21}$ $\frac{11.5}{13}$ $\frac{11.4}{14}$ $\frac{12.0}{18}$ $\frac{12.8}{18}$ $\frac{12.9}{25}$ $\frac{13.3}{50}$

$\frac{7.9}{50}$ $\frac{8.3}{25}$ $\frac{10.0}{16}$ $\frac{10.5}{10}$ $\frac{10.3}{17}$ $\frac{10.9}{17}$ $\frac{10.0}{27}$ $\frac{10.3}{50}$

$\frac{5.9}{50}$ $\frac{6.1}{29}$ $\frac{6.8}{19}$ $\frac{8.6}{14}$ $\frac{9.2}{9}$ $\frac{8.8}{14}$ $\frac{9.4}{18}$ $\frac{9.5}{24}$ $\frac{2.0}{24}$ $\frac{10.0}{48}$ $\frac{10.4}{50}$

Sta.	+	∓	-	Elev.
165+50		909.96		02.8.
166				04.7.
+50				07.1.
T.P	11.18	920.54	0.60	909.36.
167				09.2.
+50				10.9.
168				11.9.
+50				12.8.
169				13.8.
+50				15.0.
170				15.3.
+50				15.3.
171 Ent. Lt.				14.8.
BM	0.40	920.00	0.94	919.60. ✓

Lt.

L

Rt.

$\frac{40}{50}$ $\frac{47}{38}$ $\frac{56}{21}$ $\frac{70}{14}$ $\frac{74}{10}$ $\frac{72}{14}$ $\frac{78}{14}$ $\frac{81}{17}$ $\frac{100}{31}$ $\frac{105}{50}$

$\frac{28}{50}$ $\frac{43}{29}$ $\frac{52}{15}$ $\frac{53}{14}$ $\frac{58}{14}$ $\frac{76}{17}$ $\frac{85}{50}$

$\frac{07}{50}$ $\frac{15}{30}$ $\frac{21}{21}$ $\frac{21}{15}$ $\frac{29}{15}$ $\frac{38}{15}$ $\frac{43}{17}$ $\frac{41}{31}$ $\frac{43}{50}$

$\frac{94}{50}$ $\frac{99}{23}$ $\frac{118}{18}$ $\frac{113}{15}$ $\frac{117}{12}$ $\frac{113}{13}$ $\frac{120}{13}$ $\frac{111}{17}$ $\frac{108}{26}$ $\frac{102}{50}$

$\frac{84}{50}$ $\frac{90}{23}$ $\frac{88}{16}$ $\frac{97}{11}$ $\frac{96}{15}$ $\frac{99}{15}$ $\frac{103}{17}$ $\frac{98}{38}$ $\frac{96}{50}$

$\frac{74}{50}$ $\frac{80}{24}$ $\frac{80}{17}$ $\frac{87}{16}$ $\frac{86}{16}$ $\frac{88}{16}$ $\frac{92}{18}$ $\frac{94}{50}$

$\frac{63}{50}$ $\frac{67}{19}$ $\frac{77}{17}$ $\frac{78}{9}$ $\frac{77}{15}$ $\frac{80}{15}$ $\frac{86}{16}$ $\frac{100}{50}$

$\frac{37}{50}$ $\frac{49}{26}$ $\frac{59}{19}$ $\frac{66}{14}$ $\frac{67}{14}$ $\frac{70}{14}$ $\frac{81}{17}$ $\frac{101}{33}$ $\frac{114}{50}$

$\frac{18}{50}$ $\frac{35}{19}$ $\frac{55}{13}$ $\frac{55}{14}$ $\frac{57}{14}$ $\frac{61}{18}$ $\frac{84}{50}$

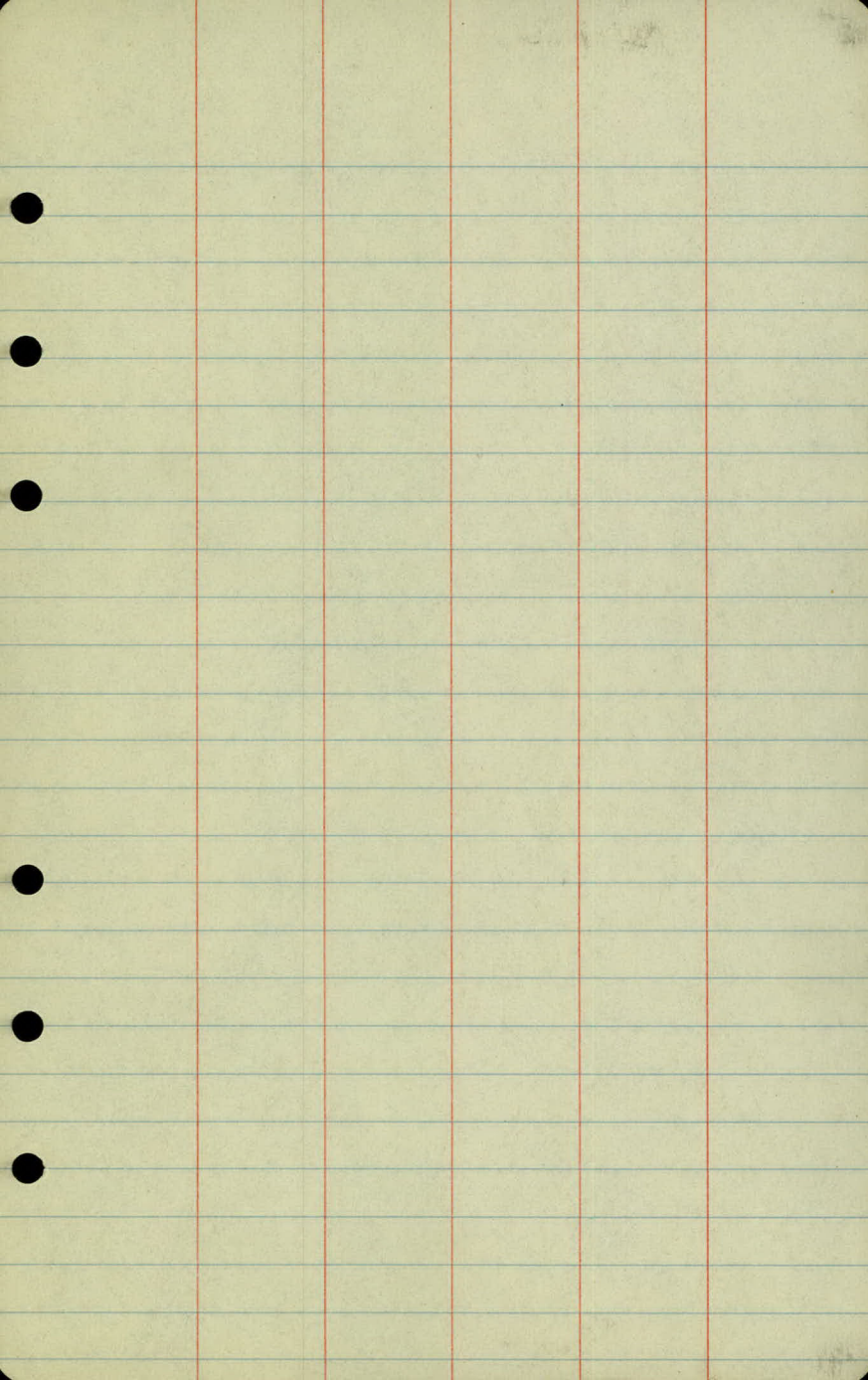
$\frac{25}{50}$ $\frac{27}{20}$ $\frac{52}{18}$ $\frac{52}{14}$ $\frac{51}{14}$ $\frac{59}{36}$ $\frac{70}{50}$

$\frac{10}{50}$ $\frac{25}{21}$ $\frac{50}{15}$ $\frac{52}{14}$ $\frac{52}{14}$ $\frac{62}{35}$ $\frac{75}{50}$

$\frac{90}{100}$ $\frac{19}{50}$ $\frac{42}{17}$ $\frac{56}{14}$ $\frac{67}{15}$ $\frac{64}{15}$ $\frac{85}{25}$ $\frac{108}{50}$

Spike in Root of Cottonwood tree 70' Lt.
of 5/10. 171

Sta.	+	x	-	Elev.
171 + 35 = ^{24" C.M.} Culvert		920.00		914.5.
172				14.1.
+50				13.6.
173				13.8.
+50				13.7.
174				13.7.
+50 = 18" Cor. Pipe Culvert				13.8.
175				14.0.
+50				15.0.
176				16.3.
+50				17.5.
T.P.	17.33	930.06	17.7	917.73 :
177				18.5.



105 + 4864 P.I.

97 + 38.21 P.O.T.

89 + 99.22 P.O.T.

79 + 19.22 P.O.T.

52 + 76.16 P.O.T.

Lt.

L

Rt.

$$\frac{29}{50} \quad \overset{100}{\frac{77}{16}} \quad \frac{50}{16} \quad \frac{56}{10} \quad \frac{55}{16} \quad \overset{40}{\frac{58}{16}} \quad \overset{40}{\frac{91}{24}} \quad \frac{102}{50}$$

$$\frac{37}{50} \quad \frac{46}{24} \quad \frac{54}{13} \quad \frac{62}{14} \quad \frac{69}{15} \quad \frac{64}{15} \quad \frac{79}{23} \quad \frac{101}{50}$$

$$\frac{20}{50} \quad \frac{36}{21} \quad \frac{48}{13} \quad \frac{63}{11} \quad \frac{64}{14} \quad \frac{70}{14} \quad \frac{76}{19} \quad \frac{91}{33} \quad \frac{102}{50}$$

$$\frac{19}{50} \quad \frac{25}{38} \quad \frac{49}{18} \quad \frac{61}{12} \quad \frac{62}{15} \quad \frac{65}{15} \quad \frac{75}{23} \quad \frac{92}{50}$$

$$\frac{09}{50} \quad \frac{23}{23} \quad \frac{60}{12} \quad \frac{62}{13} \quad \frac{63}{15} \quad \frac{66}{15} \quad \frac{76}{20} \quad \frac{86}{50}$$

$$\frac{11}{50} \quad \frac{22}{23} \quad \frac{50}{14} \quad \frac{60}{12} \quad \frac{63}{16} \quad \frac{68}{16} \quad \frac{80}{20} \quad \frac{101}{50}$$

$$\frac{23}{50} \quad \frac{28}{20} \quad \overset{40}{\frac{59}{13}} \quad \overset{40}{\frac{64}{11}} \quad \frac{62}{16} \quad \overset{40}{\frac{69}{16}} \quad \overset{40}{\frac{80}{21}} \quad \frac{95}{50}$$

$$\frac{24}{50} \quad \frac{24}{20} \quad \frac{41}{18} \quad \frac{54}{13} \quad \frac{60}{17} \quad \frac{63}{17} \quad \frac{71}{24} \quad \frac{91}{50}$$

$$\frac{21}{50} \quad \frac{26}{19} \quad \frac{50}{14} \quad \frac{50}{16} \quad \frac{52}{16} \quad \frac{56}{21} \quad \frac{70}{40} \quad \frac{75}{50}$$

$$\frac{07}{50} \quad \frac{16}{20} \quad \frac{36}{14} \quad \frac{42}{10} \quad \frac{37}{17} \quad \frac{43}{17} \quad \frac{49}{21} \quad \frac{59}{50}$$

$$\frac{110}{50} \quad \frac{05}{20} \quad \frac{26}{13} \quad \frac{25}{16} \quad \frac{32}{16} \quad \frac{40}{20} \quad \frac{56}{42} \quad \frac{62}{50}$$

$$\frac{48}{50} \quad \frac{74}{26} \quad \frac{104}{21} \quad \frac{113}{13} \quad \frac{116}{17} \quad \frac{120}{17} \quad \frac{132}{24} \quad \frac{157}{39} \quad \frac{175}{50}$$

Sta.	+	×	-	Elev
177+50		930.06		919.8
178				21.1
+50				22.3
179 Road Lt.				23.5
+50				24.1
180				24.7
+50				25.3
181				26.1
+47 = 12" Cont. Pipe Elev.				27.3
182				28.7
+50				30.1
T.P.	17.83	941.95	0.94	949.12
183				31.7

Lt.

E

Rt.

$$\frac{1^3}{50} \quad \frac{3^5}{28} \quad \frac{8^3}{22} \quad \frac{10^1}{16} \quad \frac{10^3}{17} \quad \frac{10^9}{17} \quad \frac{11^7}{21} \quad \frac{16^0}{50}$$

$$+ \frac{3^0}{50} \quad \frac{0^7}{52} \quad \frac{0^9}{26} \quad \frac{6^1}{21} \quad \frac{9^1}{13} \quad \frac{9^0}{17} \quad \frac{9^4}{17} \quad \frac{10^1}{22} \quad \frac{13^4}{44} \quad \frac{14^2}{50}$$

$$\frac{10^5}{50} \quad \frac{0^5}{28} \quad \frac{5^2}{22} \quad \frac{7^5}{14} \quad \frac{7^8}{16} \quad \frac{8^1}{16} \quad \frac{8^7}{25} \quad \frac{12^1}{50}$$

$$\frac{1^4}{100} \quad \frac{3^6}{50} \quad \frac{5^4}{25} \quad \frac{5^9}{16} \quad \frac{6^6}{15} \quad \frac{7^1}{15} \quad \frac{10^1}{30} \quad \frac{12^2}{50}$$

$$\frac{1^2}{50} \quad \frac{3^4}{21} \quad \frac{5^9}{13} \quad \frac{6^0}{15} \quad \frac{6^3}{15} \quad \frac{8^6}{22} \quad \frac{10^3}{50}$$

$$\frac{0^8}{50} \quad \frac{3^0}{22} \quad \frac{3^9}{17} \quad \frac{5^2}{12} \quad \frac{5^4}{15} \quad \frac{5^9}{15} \quad \frac{9^2}{22} \quad \frac{10^1}{50}$$

$$\frac{4^4}{50} \quad \frac{5^5}{30} \quad \frac{5^6}{18} \quad \frac{4^8}{13} \quad \frac{4^8}{16} \quad \frac{5^4}{16} \quad \frac{10^2}{22} \quad \frac{12^2}{50}$$

$$\frac{6^4}{50} \quad \frac{7^2}{28} \quad \frac{6^3}{21} \quad \frac{4^1}{14} \quad \frac{4^0}{15} \quad \frac{4^6}{15} \quad \frac{12^8}{27} \quad \frac{14^0}{50}$$

Burred this end

$$\frac{6^4}{50} \quad \frac{6^5}{35} \quad \frac{6^9}{22} \quad \frac{3^2}{15} \quad \frac{2^8}{15} \quad \frac{3^5}{15} \quad \frac{11^1}{26} \quad \frac{12^8}{27} \quad \frac{12^8}{50}$$

$$\frac{5^4}{50} \quad \frac{5^4}{27} \quad \frac{4^5}{21} \quad \frac{1^7}{14} \quad \frac{1^4}{14} \quad \frac{1^8}{14} \quad \frac{9^8}{26} \quad \frac{11^4}{43} \quad \frac{11^1}{50}$$

$$\frac{1^8}{50} \quad \frac{2^4}{26} \quad \frac{1^7}{21} \quad \frac{0^0}{16} \quad \frac{0^0}{14} \quad \frac{0^4}{14} \quad \frac{5^4}{23} \quad \frac{2^2}{29} \quad \frac{8^6}{50}$$

$$\frac{2^0}{50} \quad \frac{2^0}{34} \quad \frac{11^2}{28} \quad \frac{10^8}{19} \quad \frac{10^5}{16} \quad \frac{10^3}{14} \quad \frac{11^3}{14} \quad \frac{13^5}{19} \quad \frac{14^0}{27} \quad \frac{15^2}{33} \quad \frac{16^0}{50}$$

Stn.	+	x	-	Elev.
183 + 50		941.95		32.9
184				34.2
B.M.	12.86	941.95	12.86	929.09
T.P.	9.95	945.87	6.08	935.87
184 + 60				35.8
185 - 18" C.M. Double Row				37.1
+ 50				38.4
186				39.9
T.P.	14.76	955.49	2.09	942.73
+ 50				41.7
187				43.0
-				
+ 50				43.6
188				44.0

+ 58 = 24" part conc. part C.M. 43.4

Lt.

E

Rt

$\frac{81}{50}$	$\frac{11}{37}$	$\frac{50}{30}$	$\frac{94}{25}$	$\frac{90}{17}$	$\frac{95}{11}$	$\frac{91}{14}$	$\frac{98}{18}$	$\frac{112}{27}$	$\frac{126}{40}$	$\frac{126}{50}$	$\frac{135}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{+17}{50}$	$\frac{+12}{42}$	$\frac{0.0}{35}$	$\frac{4.2}{30}$	$\frac{6.7}{25}$	$\frac{7.3}{15}$	$\frac{8.0}{13}$	$\frac{7.8}{14}$	$\frac{8.7}{18}$	$\frac{9.3}{22}$	$\frac{9.7}{28}$	$\frac{10.2}{29}$	$\frac{9.8}{40}$	$\frac{9.5}{40}$	$\frac{10.7}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	-------------------

Spike in Fence Post 80' Rt. Sta. 184+60

$\frac{38}{50}$	$\frac{68}{33}$	$\frac{88}{34}$	$\frac{93}{17}$	$\frac{10.4}{13.1}$	$\frac{100}{14}$	$\frac{107}{16}$	$\frac{112}{16}$	$\frac{14.7}{50}$
-----------------	-----------------	-----------------	-----------------	---------------------	------------------	------------------	------------------	-------------------

Running this end

$\frac{64}{50}$	$\frac{77}{24}$	$\frac{84}{14}$	$\frac{8.8}{11}$	$\frac{8.7}{14}$	$\frac{9.6}{14}$	$\frac{11.0}{19}$	$\frac{12.8}{20}$	$\frac{12.8}{22}$	$\frac{15.2}{50}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{2.6}{50}$	$\frac{4.2}{27}$	$\frac{5.2}{19}$	$\frac{7.6}{17}$	$\frac{7.5}{14}$	$\frac{7.4}{15}$	$\frac{8.0}{15}$	$\frac{9.2}{20}$	$\frac{12.9}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{+1.5}{50}$	$\frac{1.2}{27}$	$\frac{2.2}{22}$	$\frac{6.2}{16}$	$\frac{6.5}{12}$	$\frac{5.9}{15}$	$\frac{6.5}{15}$	$\frac{5.8}{22}$	$\frac{11.5}{41}$	$\frac{12.1}{50}$
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$\frac{51}{50}$	$\frac{78}{30}$	$\frac{111}{23}$	$\frac{13.6}{17}$	$\frac{14.2}{13}$	$\frac{13.8}{18}$	$\frac{14.5}{18}$	$\frac{12.0}{22}$	$\frac{22.0}{50}$
-----------------	-----------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{39}{50}$	$\frac{60}{31}$	$\frac{74}{27}$	$\frac{9.9}{23}$	$\frac{12.8}{15}$	$\frac{12.9}{11}$	$\frac{12.5}{14}$	$\frac{13.4}{14}$	$\frac{15.0}{21}$	$\frac{20.4}{50}$
-----------------	-----------------	-----------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{2.2}{50}$	$\frac{4.8}{30}$	$\frac{5.1}{23}$	$\frac{10.9}{21}$	$\frac{12.0}{16}$	$\frac{11.9}{13}$	$\frac{11.9}{16}$	$\frac{12.8}{16}$	$\frac{14.6}{21}$	$\frac{15.6}{50}$
------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{2.6}{50}$	$\frac{4.6}{30}$	$\frac{8.0}{23}$	$\frac{11.6}{18}$	$\frac{11.6}{11}$	$\frac{11.5}{14}$	$\frac{12.1}{14}$	$\frac{14.1}{21}$	$\frac{19.7}{50}$
------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{7.9}{50}$	$\frac{8.6}{30}$	$\frac{12.2}{21}$	$\frac{14.8}{12}$	$\frac{12.4}{12}$	$\frac{12.1}{15}$	$\frac{12.7}{19}$	$\frac{13.6}{19}$	$\frac{18.4}{28}$	$\frac{15.4}{34}$	$\frac{18.0}{50}$
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Sta.	+	Σ	-	Elev.
189		955.49		43.0
+50				42.5
190				41.8
T.P.	8.08	950.16	13.41	944.08
+45				41.3
191				40.9
+50				40.6
192				40.0
T.P. #1	1.37	947.77	9.76	940.90
+50				38.6
193				36.7
+35				35.6
194				33.2
+35				32.0

LT

Q

RT

$$\frac{23}{50} \quad \frac{66}{27} \quad \frac{99}{21} \quad \frac{120}{16} \quad \frac{127}{11} \quad \frac{125}{12} \quad \frac{131}{12} \quad \frac{140}{18} \quad \frac{180}{50}$$

$$\frac{0.5}{50} \quad \frac{29}{34} \quad \frac{63}{30} \quad \frac{98}{25} \quad \frac{124}{18} \quad \frac{133}{13} \quad \frac{130}{14} \quad \frac{136}{14} \quad \frac{132}{20} \quad \frac{147}{33} \quad \frac{171}{50}$$

$$\frac{09}{50} \quad \frac{38}{33} \quad \frac{65}{28} \quad \frac{102}{23} \quad \frac{137}{16} \quad \frac{140}{12} \quad \frac{137}{16} \quad \frac{143}{16} \quad \frac{159}{23} \quad \frac{210}{50}$$

$$\frac{130}{50} \quad \frac{25}{27} \quad \frac{81}{18} \quad \frac{90}{11} \quad \frac{89}{15} \quad \frac{102}{15} \quad \frac{134}{23} \quad \frac{185}{50}$$

$$\frac{17}{50} \quad \frac{68}{28} \quad \frac{27}{23} \quad \frac{92}{13} \quad \frac{93}{18} \quad \frac{105}{18} \quad \frac{147}{25} \quad \frac{187}{50}$$

$$\frac{28}{50} \quad \frac{60}{44} \quad \frac{85}{22} \quad \frac{91}{15} \quad \frac{97}{12} \quad \frac{96}{16} \quad \frac{102}{16} \quad \frac{140}{26} \quad \frac{164}{50}$$

$$\frac{60}{50} \quad \frac{84}{24} \quad \frac{94}{11} \quad \frac{102}{16} \quad \frac{113}{16} \quad \frac{108}{22} \quad \frac{151}{50}$$

$$\frac{27}{14} \quad \frac{38}{10} \quad \frac{37}{11} \quad \frac{47}{11} \quad \frac{34}{20} \quad \frac{47}{29} \quad \frac{96}{60} \quad \frac{178}{100}$$

$$\frac{47}{19} \quad \frac{49}{14} \quad \frac{60}{9} \quad \frac{56}{17} \quad \frac{60}{17} \quad \frac{32}{21} \quad \frac{73}{48} \quad \frac{184}{100}$$

$$\frac{50}{20} \quad \frac{54}{13} \quad \frac{71}{9} \quad \frac{67}{16} \quad \frac{72}{16} \quad \frac{35}{24} \quad \frac{76}{52} \quad \frac{181}{100}$$

$$\frac{70}{21} \quad \frac{88}{13} \quad \frac{93}{10} \quad \frac{91}{19} \quad \frac{96}{19} \quad \frac{48}{29} \quad \frac{89}{59} \quad \frac{148}{100}$$

$$\frac{88}{17} \quad \frac{105}{12} \quad \frac{103}{20} \quad \frac{112}{20} \quad \frac{71}{30} \quad \frac{52}{34} \quad \frac{84}{64} \quad \frac{124}{100}$$

Sta.	+	+	-	Elev.
195		948.27		929.2
+50				25.9
T.P.	8.66	938.49	12.44	929.83
196				24.8
+54				22.6
T.P.	1.18	926.28	13.39	925.10
197				20.8
+45				18.8
+75				17.4
T.P.	1.82	918.70	9.40	916.88
198				16.4
+35				14.2
				14.7
+63				12.5
B.M.			10.99	907.71 ✓

4.

8

24.

$$\frac{11.3}{15} \quad \frac{13.2}{10} \quad \frac{13.1}{11} \quad \frac{13.5}{10} \quad \frac{14.1}{19} \quad \frac{13.2}{24} \quad \frac{3.5}{38} \quad \frac{7.1}{100}$$

$$\frac{8.9}{21} \quad \frac{11.7}{18} \quad \frac{13.1}{14} \quad \frac{16.5}{11} \quad \frac{16.4}{14} \quad \frac{16.7}{19} \quad \frac{16.1}{19} \quad \frac{13.8}{26} \quad \frac{4.3}{43} \quad \frac{6.6}{82} \quad \frac{8.5}{100}$$

$$\frac{11.2}{17} \quad \frac{13.2}{11} \quad \frac{13.7}{13} \quad \frac{14.4}{13} \quad \frac{14.4}{20} \quad \frac{13.2}{24} \quad \frac{1.3}{44} \quad \frac{3.3}{64} \quad \frac{7.3}{75} \quad \frac{13.8}{100}$$

$$\frac{11.4}{19} \quad \frac{13.9}{13} \quad \frac{15.6}{8} \quad \frac{15.9}{14} \quad \frac{16.1}{24} \quad \frac{5.3}{40} \quad \frac{11.0}{64} \quad \frac{18.0}{100}$$

$$\frac{2.7}{17} \quad \frac{4.8}{14} \quad \frac{5.5}{19} \quad \frac{6.1}{19} \quad \frac{6.6}{22} \quad \frac{6.6}{32} \quad \frac{8.0}{42} \quad \frac{5.6}{62} \quad \frac{13.0}{88} \quad \frac{15.0}{100}$$

$$\frac{4.2}{19} \quad \frac{7.3}{8} \quad \frac{7.5}{18} \quad \frac{8.1}{21} \quad \frac{8.7}{28} \quad \frac{8.0}{34} \quad \frac{4.2}{54} \quad \frac{10.5}{54} \quad \frac{19.5}{100}$$

$$\frac{6.1}{19} \quad \frac{8.2}{10} \quad \frac{8.9}{18} \quad \frac{9.4}{23} \quad \frac{10.8}{23} \quad \frac{10.2}{31} \quad \frac{9.0}{37} \quad \frac{13.3}{52} \quad \frac{18.3}{70} \quad \frac{28.3}{100}$$

$$\frac{2.4}{22} \quad \frac{3.0}{11} \quad \frac{2.3}{19} \quad \frac{3.3}{19} \quad \frac{4.9}{22} \quad \frac{6.0}{33} \quad \frac{5.2}{37} \quad \frac{12.7}{63} \quad \frac{22.0}{91} \quad \frac{27.0}{100}$$

$$\frac{4.7}{20} \quad \frac{4.5}{22} \quad \frac{5.7}{22} \quad \frac{8.0}{27} \quad \frac{9.6}{36} \quad \frac{12.4}{51} \quad \frac{19.9}{70} \quad \frac{27.0}{100}$$

$$\frac{2.2}{31} \quad \frac{4.2}{29} \quad \frac{5.3}{20} \quad \frac{6.6}{12} \quad \frac{6.4}{10} \quad \frac{6.2}{10}$$

Top of Granite boulder 75' Rt. Sta. 197+75

Sto.	+	x	-	Elev
------	---	---	---	------

T.P.#1	10.69	951.59		940.90
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192 +50

193

+35

194

+35

195

+50

196

+54

197

+45

T.P.	4.23	944.75	13.07	938.52
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+75

Lt.

E

Rt.

See page 18

$$\frac{17}{100} \quad \frac{62}{50} \quad \frac{84}{25} \quad \underline{13.0} \checkmark$$

$$\frac{10.3}{100} \quad \frac{5.1}{50} \quad \frac{6.3}{27} \quad 14.9 \checkmark$$

$$\frac{10.1}{100} \quad \frac{24}{75} \quad \frac{46}{50} \quad \frac{6.6}{28} \quad 16.0 \checkmark$$

$$\frac{18}{100} \quad \frac{49}{50} \quad \frac{54}{31} \quad 18.4 \checkmark$$

$$\frac{24}{100} \quad \frac{52}{50} \quad \frac{58}{31} \quad 19.6 \checkmark$$

$$\frac{41}{100} \quad \frac{21}{50} \quad \frac{72}{32} \quad 22.4 \checkmark$$

$$\frac{49}{100} \quad \frac{63}{75} \quad \frac{77}{50} \quad \frac{85}{32} \quad 25.7 \checkmark$$

$$\frac{65}{100} \quad \frac{89}{50} \quad \frac{93}{33} \quad 26.8 \checkmark$$

$$\frac{76}{100} \quad \frac{103}{50} \quad \frac{111}{33} \quad 29.0 \checkmark$$

$$\frac{98}{100} \quad \frac{118}{50} \quad \frac{119}{28} \quad 30.8 \checkmark$$

$$\frac{114}{100} \quad \frac{133}{50} \quad \frac{136}{38} \quad 32.8 \checkmark$$

$$\frac{33}{100} \quad \frac{52}{53} \quad 25.4$$

Sta. + K - Elev.

944.75

198

+35

T.P. 1.90 933.22 11.43 931.32

+63

T.P. 0.17 920.76 14.63 920.59

B.M.

13.05 907.71 ✓

13.05 920.76

198+63

199 10.3

+50 07.1

T.P. 1.13 908.84 13.05 907.71

198+63

199

+50

200 04.0

T.P. 0.97 902.47 7.34 901.50

Lt.

E.

Rt.

$$\frac{4.3}{100} \quad \frac{6.6}{25} \quad \frac{12.4}{46} \quad 26.4$$

$$\frac{11.6}{100} \quad \frac{14.2}{50} \quad \frac{16.8}{25} \quad 28.6$$

$$\frac{8.4}{100} \quad \frac{10.1}{75} \quad \frac{13.1}{50} \quad 20.7$$

Top of granite boulder 75' Rt. 56 197 + 75

$$8.3 \quad \frac{8.6}{25}$$

$$\frac{3.0}{75} \quad \frac{6.5}{50} \quad \frac{8.4}{25} \quad \frac{10.6}{18} \quad \frac{12.3}{15} \quad \frac{10.8}{10} \quad \frac{10.5}{19} \quad \frac{11.2}{19} \quad \frac{11.8}{30}$$

$$\frac{7.5}{75} \quad \frac{10.5}{50} \quad \frac{13.3}{31} \quad \frac{14.1}{16} \quad \frac{15.1}{14} \quad \frac{14.1}{13} \quad \frac{13.7}{15} \quad \frac{14.6}{15}$$

$$+ 3.7 \quad \frac{6.1}{43} \quad \frac{11.4}{57} \quad \frac{12.4}{70} \quad \frac{15.8}{100}$$

$$+ 1.5 \quad \frac{4.0}{36} \quad \frac{9.6}{50} \quad \frac{12.4}{57} \quad \frac{15.7}{56} \quad \frac{16.7}{100}$$

$$1.7 \quad \frac{10.2}{25} \quad \frac{14.5}{50} \quad \frac{17.6}{75} \quad \frac{20.5}{100}$$

$$\frac{4.5}{50} \quad \frac{5.4}{43} \quad \frac{5.4}{14} \quad \frac{4.7}{11} \quad \frac{4.8}{14} \quad \frac{5.3}{14} \quad \frac{16.0}{31} \quad \frac{17.8}{50} \quad \frac{20.5}{25} \quad \frac{22.5}{100}$$

Sta.	+	π	-	Elev.
200 + 50		902.47		901.6
201				899.2
+50				96.8
202				94.5
+50				93.0
T.P.	2.49	894.47	10.49	891.98
203				92.0
+50				91.6
204				91.2
+50				90.9
205				90.7
+50				90.4
206				89.9

Lt.

E

Rt.

$$\frac{26}{50} \quad \frac{25}{50} \quad \frac{13}{13} \quad 0.9 \quad \frac{13}{13} \quad \frac{8.4}{24} \quad \frac{10.2}{32} \quad \frac{13.0}{50} \quad \frac{15.9}{75}$$

$$\frac{46}{50} \quad \frac{50}{38} \quad \frac{39}{11} \quad \frac{35}{11} \quad \frac{33}{11} \quad \frac{41}{14} \quad \frac{115}{24} \quad \frac{140}{33} \quad \frac{153}{50} \quad \frac{165}{75}$$

$$\frac{6.7}{50} \quad \frac{6.1}{10} \quad \frac{5.7}{12} \quad \frac{6.6}{12} \quad \frac{12.2}{20} \quad \frac{14.3}{28} \quad \frac{15.8}{50}$$

$$\frac{8.3}{50} \quad \frac{8.9}{34} \quad \frac{8.9}{15} \quad \frac{8.5}{9} \quad \frac{8.0}{12} \quad \frac{8.6}{12} \quad \frac{12.5}{19} \quad \frac{15.0}{28} \quad \frac{16.3}{50}$$

$$\frac{10.5}{50} \quad \frac{10.3}{28} \quad \frac{10.1}{12} \quad \frac{9.5}{11} \quad \frac{10.1}{11} \quad \frac{13.1}{17} \quad \frac{14.3}{21} \quad \frac{16.5}{50}$$

$$\frac{34}{50} \quad \frac{35}{14} \quad \frac{28}{11} \quad \frac{25}{12} \quad \frac{35}{12} \quad \frac{7.2}{19} \quad \frac{8.7}{50}$$

$$\frac{44}{50} \quad \frac{48}{34} \quad \frac{48}{14} \quad \frac{5.3}{11} \quad \frac{2.9}{12} \quad \frac{3.7}{12} \quad \frac{2.6}{18} \quad \frac{9.1}{50}$$

$$\frac{36}{50} \quad \frac{5.0}{30} \quad \frac{5.0}{15} \quad \frac{3.8}{12} \quad \frac{3.3}{11} \quad \frac{4.2}{11} \quad \frac{2.8}{17} \quad \frac{9.0}{50}$$

$$\frac{44}{50} \quad \frac{5.2}{36} \quad \frac{5.6}{16} \quad \frac{4.2}{12} \quad \frac{3.6}{12} \quad \frac{4.2}{12} \quad \frac{2.9}{17} \quad \frac{9.0}{50}$$

$$\frac{5.5}{50} \quad \frac{5.9}{44} \quad \frac{6.2}{31} \quad \frac{6.1}{15} \quad \frac{4.2}{12} \quad \frac{3.8}{11} \quad \frac{4.2}{11} \quad \frac{2.7}{16} \quad \frac{8.4}{33} \quad \frac{8.8}{50}$$

$$\frac{5.7}{50} \quad \frac{6.4}{36} \quad \frac{6.4}{16} \quad \frac{4.8}{12} \quad \frac{4.1}{12} \quad \frac{4.8}{12} \quad \frac{2.9}{15} \quad \frac{8.6}{33} \quad \frac{8.9}{50}$$

$$\frac{6.3}{50} \quad \frac{2.2}{34} \quad \frac{2.2}{16} \quad \frac{5.1}{11} \quad \frac{4.6}{11} \quad \frac{5.2}{11} \quad \frac{8.4}{16} \quad \frac{5.7}{21} \quad \frac{9.0}{50}$$

Sta.	+	Δ	-	Elev.
206+50		894.47		89.7
207				89.5
+50				89.3
208				88.7
+50				87.8
209				87.4
+50				87.5
210				87.8
+50				88.2
+83				88.0
+88				88.0
211+05	Co. Rd. I. Lt.			87.9

L.

E

R.

$$\frac{67}{50} \quad \frac{75}{35} \quad \frac{74}{16} \quad \frac{55}{13} \quad \frac{48}{11} \quad \frac{56}{14} \quad \frac{86}{16} \quad \frac{91}{50}$$

$$\frac{68}{50} \quad \frac{73}{41} \quad \frac{78}{17} \quad \frac{58}{13} \quad \frac{50}{11} \quad \frac{59}{11} \quad \frac{90}{16} \quad \frac{93}{50}$$

$$\frac{72}{50} \quad \frac{79}{17} \quad \frac{59}{13} \quad \frac{52}{11} \quad \frac{60}{11} \quad \frac{90}{15} \quad \frac{92}{31} \quad \frac{93}{50}$$

$$\frac{73}{50} \quad \frac{83}{17} \quad \frac{64}{14} \quad \frac{58}{11} \quad \frac{64}{10} \quad \frac{96}{16} \quad \frac{97}{50}$$

$$\frac{78}{50} \quad \frac{89}{19} \quad \frac{91}{15} \quad \frac{67}{9} \quad \frac{72}{9} \quad \frac{108}{14} \quad \frac{108}{25} \quad \frac{99}{30} \quad \frac{99}{50}$$

$$\frac{82}{50} \quad \frac{94}{20} \quad \frac{76}{16} \quad \frac{71}{11} \quad \frac{76}{11} \quad \frac{104}{14} \quad \frac{107}{27} \quad \frac{100}{27} \quad \frac{99}{50}$$

$$\frac{83}{50} \quad \frac{89}{19} \quad \frac{74}{15} \quad \frac{70}{8} \quad \frac{95}{8} \quad \frac{95}{12} \quad \frac{95}{22} \quad \frac{99}{50}$$

$$\frac{82}{50} \quad \frac{85}{40} \quad \frac{85}{18} \quad \frac{72}{15} \quad \frac{67}{7} \quad \frac{74}{7} \quad \frac{93}{10} \quad \frac{97}{50}$$

$$\frac{82}{50} \quad \frac{86}{21} \quad \frac{66}{17} \quad \frac{63}{7} \quad \frac{68}{7} \quad \frac{88}{12} \quad \frac{91}{27} \quad \frac{92}{50}$$

$$\frac{78}{50} \quad \frac{29}{41} \quad \frac{68}{35} \quad \frac{65}{7} \quad \frac{74}{7} \quad \frac{86}{9} \quad \frac{92}{50}$$

$$\frac{60}{50} \quad \frac{64}{25} \quad \frac{65}{6} \quad \frac{70}{6} \quad \frac{88}{10} \quad \frac{87}{50}$$

$$\frac{44}{100} \quad \frac{56}{50} \quad \frac{61}{21} \quad \frac{64}{7} \quad \frac{70}{7} \quad \frac{81}{11} \quad \frac{87}{50}$$

Sta.	+	Δ	-	Elev.
211+21		894.47		888.0
+26				87.9
+36				87.8
+40				87.9
+50				87.6
+85				87.5
212				87.2
B.M.	0.56	893.15	1.88	894.59 ✓
214+50				86.8
213				87.0

L

E

Rt.

$$\frac{5.8}{50} \quad \frac{6.0}{28} \quad \frac{6.5}{7} \quad \frac{2.0}{7} \quad \frac{8.3}{14} \quad \frac{8.2}{50}$$

$$\frac{7.1}{50} \quad \frac{6.0}{41} \quad \frac{6.3}{14} \quad \frac{6.6}{8} \quad \frac{7.4}{8} \quad \frac{8.1}{14} \quad \frac{8.3}{50}$$

$$\frac{7.3}{50} \quad \frac{7.2}{29} \quad \frac{6.1}{33} \quad \frac{6.2}{18} \quad \frac{6.7}{8} \quad \frac{7.2}{8} \quad \frac{8.2}{14} \quad \frac{8.2}{50}$$

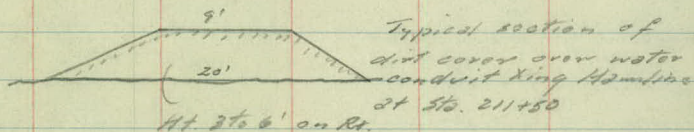
$$\frac{5.2}{50} \quad \frac{7.4}{47} \quad \frac{7.2}{39} \quad \frac{6.3}{36} \quad \frac{6.4}{22} \quad \frac{6.3}{9} \quad \frac{6.6}{10} \quad \frac{8.0}{14} \quad \frac{8.0}{50}$$

$$\frac{5.6}{50} \quad \frac{6.3}{46} \quad \frac{7.9}{45} \quad \frac{2.8}{39} \quad \frac{6.7}{37} \quad \frac{6.6}{13} \quad \frac{6.9}{8} \quad \frac{7.1}{8} \quad \frac{8.3}{14} \quad \frac{9.1}{50}$$

$$\frac{7.1}{50} \quad \frac{2.1}{41} \quad \frac{2.4}{39} \quad \frac{2.1}{35} \quad \frac{7.6}{32} \quad \frac{7.7}{20} \quad \frac{7.0}{6} \quad \frac{7.3}{6} \quad \frac{8.6}{9} \quad \frac{8.0}{11} \quad \frac{9.3}{41} \quad \frac{9.9}{50}$$

$$\frac{8.2}{50} \quad \frac{8.1}{41} \quad \frac{9.8}{39} \quad \frac{9.7}{33} \quad \frac{7.9}{31} \quad \frac{2.8}{17} \quad \frac{7.7}{4} \quad \frac{7.6}{8} \quad \frac{9.5}{8} \quad \frac{10.5}{14} \quad \frac{11.0}{20} \quad \frac{10.9}{50}$$

Top of brick N.W. cor. of brick & concrete
manhole 200' Rt. Sta. 211+50



$$\frac{7.5}{50} \quad \frac{7.5}{37} \quad \frac{8.5}{26} \quad \frac{9.0}{31} \quad \frac{7.6}{30} \quad \frac{7.1}{20} \quad \frac{6.4}{4} \quad \frac{7.1}{8} \quad \frac{8.8}{9} \quad \frac{9.6}{13} \quad \frac{9.3}{50}$$

$$\frac{2.9}{50} \quad \frac{8.1}{35} \quad \frac{9.4}{34} \quad \frac{9.4}{30} \quad \frac{8.9}{29} \quad \frac{8.6}{21} \quad \frac{7.1}{19} \quad \frac{6.2}{4} \quad \frac{7.1}{8} \quad \frac{9.2}{8} \quad \frac{9.3}{29} \quad \frac{9.4}{30} \quad \frac{9.1}{21} \quad \frac{10.5}{74} \quad \frac{10.5}{80} \quad \frac{9.1}{91} \quad \frac{9.1}{90}$$

Sta.	+	K	-	Elev.
213+50		893.15		86.8
214				87.5
+62				88.0
215				88.1
+61	30" C.M. Culvert			87.9
216				87.7
T.P.	12.16	900.57	4.74	888.41
+50				88.2
217				89.0
+50				90.3
218				91.0
+50				91.4
219				92.4
+50				93.0

Lt.

L

Rt

$$\frac{8^1}{36} \frac{8^1}{50}$$

$$\frac{8^4}{35} \frac{8^5}{31} \frac{8^9}{30} \frac{8^5}{27} \frac{7^2}{20} \frac{6^0}{8} \frac{6^4}{5} \frac{7^0}{4} \frac{8^1}{8} \frac{9^2}{29} \frac{8^8}{50} \frac{10^5}{51} \frac{10^5}{60} \frac{8^8}{61} \frac{8^8}{75}$$

$$\frac{8^9}{50} \frac{9^0}{34} \frac{9^5}{33} \frac{9^6}{30} \frac{8^4}{28} \frac{8^1}{27} \frac{6^7}{19} \frac{5^5}{8} \frac{5^7}{5} \frac{6^6}{4} \frac{8^7}{7} \frac{8^5}{35} \frac{10^6}{38} \frac{10^6}{46} \frac{8^0}{45} \frac{7^0}{50}$$

$$\frac{8^6}{34} \frac{9^4}{27} \frac{9^4}{30} \frac{7^9}{29} \frac{7^3}{27} \frac{5^9}{19} \frac{5^2}{12} \frac{5^2}{5} \frac{5^7}{8} \frac{8^2}{7} \frac{8^2}{14} \frac{10^4}{15} \frac{10^4}{21} \frac{8^0}{24} \frac{7^3}{34} \frac{7^3}{50}$$

$$\frac{8^8}{50} \frac{8^7}{34} \frac{9^5}{31} \frac{9^5}{30} \frac{7^8}{29} \frac{7^4}{27} \frac{5^8}{19} \frac{5^0}{10} \frac{5^1}{5} \frac{5^6}{8} \frac{7^3}{8} \frac{7^7}{16} \frac{10^7}{17} \frac{10^7}{24} \frac{8^0}{28} \frac{7^3}{50}$$

$$\frac{8^1}{50} \frac{7^8}{38} \frac{9^9}{33} \frac{9^9}{27} \frac{5^8}{19} \frac{8^3}{5} \frac{5^9}{7} \frac{6^4}{9} \frac{6^4}{15} \frac{10^5}{16} \frac{10^5}{23} \frac{7^8}{24} \frac{7^8}{50}$$

$$\frac{7^6}{50} \frac{8^4}{41} \frac{9^5}{38} \frac{9^5}{31} \frac{5^5}{31} \frac{7^5}{20} \frac{5^9}{17} \frac{5^3}{16} \frac{5^5}{16} \frac{6^2}{6} \frac{7^4}{9} \frac{7^6}{50}$$

$$\frac{15^7}{50} \frac{14^7}{21} \frac{13^0}{16} \frac{12^4}{17} \frac{13^3}{7} \frac{14^3}{16} \frac{14^4}{50}$$

$$\frac{15^2}{50} \frac{14^3}{19} \frac{12^5}{16} \frac{11^6}{7} \frac{11^6}{17} \frac{12^4}{9} \frac{13^9}{12} \frac{13^1}{21} \frac{13^0}{50}$$

$$\frac{14^7}{50} \frac{14^3}{20} \frac{11^2}{13} \frac{10^3}{13} \frac{11^2}{11} \frac{13^2}{15} \frac{13^3}{28} \frac{13^1}{50}$$

$$\frac{14^7}{50} \frac{14^3}{24} \frac{12^1}{18} \frac{10^2}{12} \frac{9^6}{11} \frac{10^4}{11} \frac{12^0}{15} \frac{13^0}{50}$$

$$\frac{13^4}{50} \frac{12^8}{17} \frac{9^9}{12} \frac{9^2}{11} \frac{9^7}{11} \frac{10^8}{14} \frac{11^4}{30} \frac{12^0}{50}$$

$$\frac{11^7}{50} \frac{11^3}{30} \frac{10^2}{15} \frac{9^1}{13} \frac{8^2}{12} \frac{8^7}{12} \frac{9^3}{15} \frac{8^7}{24} \frac{9^7}{50}$$

$$\frac{11^0}{50} \frac{8^8}{16} \frac{8^2}{12} \frac{7^6}{13} \frac{7^9}{13} \frac{8^1}{17} \frac{7^7}{20} \frac{8^0}{50}$$

Sta.	+	K	-	Elev.
220		900.57		93.3
+50				93.6
221				93.6
+50				93.4
T.P.	4.41	897.55	7.43	893.14
222				93.2
+50				92.8
223				92.5
+50				92.2
224				92.1
+50				92.4
225				92.7
+50				92.6
226				92.6

4

2

12+

$$\frac{108}{50} \quad \frac{98}{31} \quad \frac{84}{14} \quad \frac{76}{11} \quad \frac{73}{1} \quad \frac{80}{14} \quad \frac{97}{17} \quad \frac{96}{22} \quad \frac{66}{27} \quad \frac{74}{25} \quad \frac{82}{50}$$

$$\frac{80}{50} \quad \frac{76}{31} \quad \frac{100}{26} \quad \frac{104}{22} \quad \frac{94}{16} \quad \frac{73}{11} \quad \frac{70}{1} \quad \frac{75}{13} \quad \frac{84}{16} \quad \frac{84}{21} \quad \frac{32}{31} \quad \frac{41}{50}$$

$$\frac{77}{50} \quad \frac{51}{37} \quad \frac{93}{29} \quad \frac{108}{24} \quad \frac{106}{19} \quad \frac{73}{20} \quad \frac{70}{1} \quad \frac{73}{14} \quad \frac{77}{19} \quad \frac{20}{29} \quad \frac{03}{34} \quad \frac{20}{50}$$

$$\frac{104}{50} \quad \frac{77}{31} \quad \frac{43}{25} \quad \frac{112}{16} \quad \frac{80}{10} \quad \frac{72}{1} \quad \frac{75}{13} \quad \frac{64}{19} \quad \frac{37}{24} \quad \frac{46}{50}$$

$$\frac{98}{50} \quad \frac{72}{24} \quad \frac{80}{22} \quad \frac{76}{15} \quad \frac{49}{9} \quad \frac{44}{1} \quad \frac{48}{14} \quad \frac{21}{21} \quad \frac{13}{50}$$

$$\frac{99}{50} \quad \frac{87}{32} \quad \frac{71}{15} \quad \frac{53}{10} \quad \frac{48}{1} \quad \frac{50}{14} \quad \frac{22}{21} \quad \frac{05}{50}$$

$$\frac{101}{50} \quad \frac{95}{31} \quad \frac{80}{15} \quad \frac{57}{10} \quad \frac{51}{1} \quad \frac{54}{14} \quad \frac{27}{19} \quad \frac{27}{33} \quad \frac{06}{50}$$

$$\frac{104}{50} \quad \frac{98}{30} \quad \frac{80}{15} \quad \frac{59}{11} \quad \frac{54}{1} \quad \frac{56}{15} \quad \frac{34}{19} \quad \frac{18}{50}$$

$$\frac{98}{50} \quad \frac{97}{28} \quad \frac{78}{14} \quad \frac{60}{11} \quad \frac{55}{1} \quad \frac{58}{14} \quad \frac{46}{16} \quad \frac{44}{31} \quad \frac{28}{50}$$

$$\frac{95}{50} \quad \frac{78}{13} \quad \frac{65}{15} \quad \frac{55}{11} \quad \frac{52}{1} \quad \frac{56}{14} \quad \frac{53}{26} \quad \frac{48}{50}$$

$$\frac{77}{50} \quad \frac{68}{15} \quad \frac{54}{11} \quad \frac{49}{1} \quad \frac{57}{13} \quad \frac{66}{16} \quad \frac{27}{50}$$

$$\frac{69}{50} \quad \frac{65}{32} \quad \frac{69}{14} \quad \frac{54}{11} \quad \frac{50}{1} \quad \frac{58}{13} \quad \frac{76}{16} \quad \frac{81}{50}$$

$$\frac{80}{50} \quad \frac{85}{16} \quad \frac{55}{11} \quad \frac{50}{1} \quad \frac{57}{13} \quad \frac{80}{17} \quad \frac{82}{31} \quad \frac{82}{50}$$

Sta.	+	π	-	Elev.
226+50		897.55		893.1
226+40 = 12" V. T.P. pt				
227				94.2
+50				95.4
228				96.9
+50				
T.P.	10.94	908.23	0.76	897.29
228+50				98.3
229				899.7
+50				901.1
230				02.3
+50				03.0
231				03.2
+50				03.0

44

4

124

$$\frac{86}{50} \quad \frac{7.9}{16} \quad \frac{5.2}{11}$$

$$\frac{4.5}{50} \quad \frac{5.7}{14} \quad \frac{7.8}{17} \quad \frac{7.8}{50}$$

$$\frac{1.28}{8.8}$$

$$\frac{1.28}{8.8}$$

$$\frac{8.7}{50} \quad \frac{8.2}{18} \quad \frac{4.0}{13} \quad \frac{3.4}{13} \quad \frac{4.1}{13} \quad \frac{6.5}{16} \quad \frac{6.8}{27} \quad \frac{6.0}{33} \quad \frac{5.1}{50}$$

$$\frac{8.5}{50} \quad \frac{8.2}{34} \quad \frac{7.7}{20} \quad \frac{6.1}{18} \quad \frac{2.8}{10} \quad \frac{2.2}{13} \quad \frac{2.6}{16} \quad \frac{3.1}{16} \quad \frac{3.4}{39} \quad \frac{2.3}{50}$$

$$\frac{8.0}{50} \quad \frac{5.9}{21} \quad \frac{3.7}{15} \quad \frac{1.4}{11} \quad \frac{0.7}{9} \quad \frac{1.1}{9} \quad \frac{0.1}{15} \quad \frac{0.1}{20} \quad \frac{0.0}{35} \quad \frac{+0.5}{50}$$

$$\frac{6.0}{50} \quad \frac{3.4}{21} \quad \frac{2.0}{22} \quad \frac{0.0}{14} \quad \frac{.7}{50}$$

$$\frac{9.9}{10} \quad \frac{10.1}{10} \quad \frac{7.0}{20} \quad \frac{7.4}{36} \quad \frac{6.4}{50}$$

$$\frac{13.4}{50} \quad \frac{8.2}{22} \quad \frac{7.4}{16} \quad \frac{7.8}{11} \quad \frac{8.6}{8} \quad \frac{8.5}{10} \quad \frac{8.5}{10} \quad \frac{6.9}{16} \quad \frac{3.7}{23} \quad \frac{4.1}{37} \quad \frac{3.7}{50}$$

$$\frac{10.1}{50} \quad \frac{6.3}{24} \quad \frac{5.1}{15} \quad \frac{7.3}{8} \quad \frac{7.1}{10} \quad \frac{2.1}{10} \quad \frac{6.1}{12} \quad \frac{5.1}{18} \quad \frac{1.5}{26} \quad \frac{2.0}{39} \quad \frac{2.1}{50}$$

$$\frac{7.1}{50} \quad \frac{2.0}{20} \quad \frac{4.0}{16} \quad \frac{4.8}{11} \quad \frac{6.0}{8} \quad \frac{5.9}{9} \quad \frac{6.1}{9} \quad \frac{4.4}{16} \quad \frac{1.5}{24} \quad \frac{1.1}{23} \quad \frac{1.7}{38} \quad \frac{2.0}{50}$$

$$\frac{5.5}{50} \quad \frac{4.0}{34} \quad \frac{2.2}{19} \quad \frac{3.4}{14} \quad \frac{5.4}{8} \quad \frac{5.2}{11} \quad \frac{5.4}{11} \quad \frac{3.9}{17} \quad \frac{1.9}{23} \quad \frac{1.7}{23} \quad \frac{2.4}{38} \quad \frac{3.0}{50}$$

$$\frac{6.0}{50} \quad \frac{2.2}{19} \quad \frac{4.2}{11} \quad \frac{5.2}{8} \quad \frac{5.0}{11} \quad \frac{4.9}{11} \quad \frac{2.1}{23} \quad \frac{2.1}{30} \quad \frac{3.3}{40} \quad \frac{4.0}{50}$$

$$\frac{6.8}{50} \quad \frac{3.0}{18} \quad \frac{4.1}{14} \quad \frac{5.4}{9} \quad \frac{5.2}{12} \quad \frac{5.1}{12} \quad \frac{2.8}{20} \quad \frac{3.1}{29} \quad \frac{4.3}{37} \quad \frac{5.3}{50}$$

Sta.	+	π	-	Elev.
232		908.73		903.2
+50				03.2
233				03.1
+50				02.7
234				02.3
+50				01.9
235				02.0
BM. +50	4.08	907.15	5.16	903.07 ✓ 02.5
236				02.9
+50				02.9
237				03.2
+50				03.2

L+

L

R+

$$\frac{7.3}{50} \quad \frac{5.1}{31} \quad \frac{3.3}{18} \quad \frac{4.3}{14} \quad \frac{5.2}{12} \quad \frac{5.0}{50} \quad \frac{5.0}{11} \quad \frac{3.2}{18} \quad \frac{3.9}{26} \quad \frac{4.1}{26} \quad \frac{4.6}{50}$$

$$\frac{6.6}{50} \quad \frac{3.2}{18} \quad \frac{5.4}{11} \quad \frac{5.0}{50} \quad \frac{5.0}{11} \quad \frac{3.3}{16} \quad \frac{3.1}{25} \quad \frac{4.5}{26} \quad \frac{5.4}{50}$$

$$\frac{6.0}{50} \quad \frac{4.5}{25} \quad \frac{3.5}{17} \quad \frac{5.3}{14} \quad \frac{5.1}{50} \quad \frac{5.2}{9} \quad \frac{4.4}{16} \quad \frac{4.4}{23} \quad \frac{5.2}{31} \quad \frac{2.1}{50}$$

$$\frac{5.1}{50} \quad \frac{5.2}{30} \quad \frac{4.8}{15} \quad \frac{5.8}{11} \quad \frac{5.5}{50} \quad \frac{5.5}{14} \quad \frac{6.2}{20} \quad \frac{5.9}{41} \quad \frac{10.5}{50}$$

$$\frac{5.9}{50} \quad \frac{5.6}{17} \quad \frac{6.2}{14} \quad \frac{5.9}{50} \quad \frac{6.2}{13} \quad \frac{10.2}{21} \quad \frac{11.6}{31} \quad \frac{12.9}{50}$$

$$\frac{6.3}{50} \quad \frac{6.8}{44} \quad \frac{6.7}{20} \quad \frac{6.3}{13} \quad \frac{6.3}{50} \quad \frac{6.7}{11} \quad \frac{10.6}{18} \quad \frac{12.3}{29} \quad \frac{12.3}{50}$$

$$\frac{6.3}{50} \quad \frac{7.4}{33} \quad \frac{7.3}{23} \quad \frac{6.2}{13} \quad \frac{6.2}{50} \quad \frac{6.8}{10} \quad \frac{10.4}{15} \quad \frac{10.6}{22} \quad \frac{10.6}{50}$$

Top of monument 50 237+33 28

$$\frac{4.9}{50} \quad \frac{5.2}{45} \quad \frac{5.0}{23} \quad \frac{4.2}{14} \quad \frac{4.8}{12} \quad \frac{4.7}{47} \quad \frac{4.9}{11} \quad \frac{6.2}{26} \quad \frac{7.0}{50}$$

$$\frac{4.2}{50} \quad \frac{4.3}{25} \quad \frac{3.5}{19} \quad \frac{3.4}{14} \quad \frac{4.0}{11} \quad \frac{4.3}{43} \quad \frac{4.5}{7} \quad \frac{3.6}{12} \quad \frac{3.8}{22} \quad \frac{5.8}{50}$$

$$\frac{6.4}{50} \quad \frac{6.8}{38} \quad \frac{5.9}{24} \quad \frac{4.6}{19} \quad \frac{4.3}{12} \quad \frac{4.6}{11} \quad \frac{4.3}{43} \quad \frac{4.3}{7} \quad \frac{3.8}{8} \quad \frac{3.6}{11} \quad \frac{3.7}{20} \quad \frac{6.0}{50}$$

$$\frac{6.2}{50} \quad \frac{6.2}{37} \quad \frac{5.6}{26} \quad \frac{4.4}{18} \quad \frac{4.4}{12} \quad 4.0 \quad \frac{4.0}{8} \quad \frac{3.4}{13} \quad \frac{3.4}{20} \quad \frac{5.3}{48} \quad \frac{5.3}{50}$$

$$\frac{4.3}{50} \quad \frac{3.3}{31} \quad \frac{6.3}{24} \quad \frac{6.0}{17} \quad \frac{4.3}{14} \quad 4.0 \quad \frac{4.0}{12} \quad \frac{3.7}{16} \quad \frac{3.4}{21} \quad \frac{5.3}{50}$$

Sta. + π - Elev.

907.15

238

03.0

+50

02.8

239

02.3

+50

01.7

240

00.9

+50

Ent Rt 00.2

241

899.7

+50

99.4

242

98.8

T.P

6.26

904.53

8.88

898.27

+60

97.9

243

97.4

B.M

4.10

904.53

4.10

900.43

Lt.

E

Rt

$$\frac{3.2}{50} \quad \frac{2.3}{32} \quad \frac{6.3}{25} \quad \frac{6.3}{19} \quad \frac{4.2}{15} \quad 4.2 \quad \frac{4.2}{16} \quad \frac{5.4}{26} \quad \frac{6.7}{50}$$

$$\frac{2.6}{50} \quad \frac{2.0}{32} \quad \frac{6.2}{25} \quad \frac{6.7}{19} \quad \frac{4.7}{15} \quad 4.4 \quad \frac{4.7}{11} \quad \frac{3.6}{16} \quad \frac{4.6}{33} \quad \frac{5.4}{50}$$

$$\frac{2.5}{50} \quad \frac{2.1}{32} \quad \frac{7.0}{25} \quad \frac{7.0}{18} \quad \frac{5.0}{15} \quad 4.9 \quad \frac{5.0}{10} \quad \frac{3.1}{15} \quad \frac{4.4}{50}$$

$$\frac{3.6}{50} \quad \frac{3.0}{32} \quad \frac{7.7}{27} \quad \frac{7.7}{18} \quad \frac{5.7}{15} \quad 5.5 \quad \frac{5.7}{10} \quad \frac{4.7}{15} \quad \frac{5.6}{50}$$

$$\frac{5.7}{50} \quad \frac{5.6}{32} \quad \frac{8.9}{28} \quad \frac{8.9}{20} \quad \frac{6.6}{15} \quad 6.3 \quad \frac{6.5}{13} \quad \frac{7.0}{16} \quad \frac{7.4}{30} \quad \frac{7.1}{50}$$

$$\frac{7.1}{50} \quad \frac{6.8}{33} \quad \frac{9.5}{28} \quad \frac{9.2}{21} \quad \frac{7.7}{14} \quad 7.0 \quad \frac{7.0}{10} \quad \frac{7.3}{50} \quad \frac{6.3}{10}$$

$$\frac{9.9}{50} \quad \frac{8.3}{32} \quad \frac{10.2}{26} \quad \frac{10.1}{21} \quad \frac{7.7}{16} \quad 7.5 \quad \frac{7.9}{10} \quad \frac{5.5}{20} \quad \frac{4.7}{37} \quad \frac{6.5}{50}$$

$$\frac{9.9}{50} \quad \frac{7.9}{32} \quad \frac{10.8}{24} \quad \frac{10.8}{20} \quad \frac{8.4}{15} \quad 7.8 \quad \frac{8.1}{9} \quad \frac{7.3}{15} \quad \frac{3.7}{23} \quad \frac{1.7}{50}$$

$$\frac{10.7}{50} \quad \frac{8.6}{32} \quad \frac{11.4}{24} \quad \frac{11.4}{21} \quad \frac{9.0}{15} \quad 8.4 \quad \frac{8.5}{10} \quad \frac{3.5}{21} \quad \frac{2.7}{34} \quad \frac{1.2}{50}$$

$$\frac{10.8}{50} \quad \frac{9.7}{34} \quad \frac{8.4}{19} \quad \frac{7.2}{14} \quad 6.6 \quad \frac{6.9}{9} \quad \frac{6.3}{19} \quad \frac{5.5}{32} \quad \frac{4.4}{50}$$

$$\frac{14.0}{50} \quad \frac{13.2}{33} \quad \frac{11.6}{20} \quad \frac{7.8}{13} \quad 7.1 \quad \frac{7.5}{12} \quad \frac{10.4}{17} \quad \frac{10.1}{24} \quad \frac{9.9}{36} \quad \frac{8.5}{50}$$

Spk 125' Rt Sta 243 Spk in 18' 0.0 K

Sta.	+	⌒	-	Elev.
		90453		
243+50				96.8
244				96.2
+35		12"	V. +	ADKAIN
+50				95.6
245				95.8
+35				95.9
+50				95.9
246				95.6
+50				95.3
247				95.1
+50				94.9
248				94.5
+50				94.0

Lt.

E

Rt.

$$\frac{15.5}{50} \quad \frac{15.4}{34} \quad \frac{14.5}{27} \quad \frac{12.5}{19} \quad \frac{8.3}{11} \quad \frac{8.4}{7.7} \quad \frac{12.4}{18} \quad \frac{13.6}{26} \quad \frac{13.1}{40} \quad \frac{12.2}{50}$$

$$\frac{15.9}{60} \quad \frac{15.3}{32} \quad \frac{16.3}{30} \quad \frac{16.3}{27} \quad \frac{12.4}{20} \quad \frac{8.9}{13} \quad \frac{8.3}{8.3} \quad \frac{9.0}{11} \quad \frac{12.7}{19} \quad \frac{14.5}{24} \quad \frac{14.4}{39} \quad \frac{14.0}{60}$$

$$\frac{15.30}{111}$$

$$\frac{15.30}{111}$$

$$\frac{15.2}{50} \quad \frac{15.3}{21} \quad \frac{13.5}{22} \quad \frac{9.3}{11} \quad 8.9 \quad \frac{9.4}{11} \quad \frac{13.9}{18} \quad \frac{14.9}{30} \quad \frac{14.9}{50}$$

$$\frac{12.8}{50} \quad \frac{13.5}{25} \quad \frac{13.8}{23} \quad \frac{9.2}{12} \quad 8.7 \quad \frac{9.3}{12} \quad \frac{13.4}{19} \quad \frac{14.5}{32} \quad \frac{14.2}{50}$$

$$\frac{9.4}{50} \quad \frac{10.5}{28} \quad \frac{11.0}{25} \quad \frac{11.0}{19} \quad \frac{9.4}{14} \quad 8.6 \quad \frac{9.3}{15} \quad \frac{12.0}{20} \quad \frac{12.8}{32} \quad \frac{12.2}{50}$$

$$\frac{8.5}{50} \quad \frac{9.6}{29} \quad \frac{11.4}{24} \quad \frac{11.2}{20} \quad \frac{9.0}{14} \quad 8.6 \quad \frac{9.0}{16} \quad \frac{11.1}{21} \quad \frac{11.1}{25} \quad \frac{9.8}{29} \quad \frac{8.6}{50}$$

$$\frac{5.2}{50} \quad \frac{5.2}{33} \quad \frac{11.7}{25} \quad \frac{11.7}{19} \quad \frac{9.2}{16} \quad 8.9 \quad \frac{9.4}{16} \quad \frac{11.0}{20} \quad \frac{11.3}{24} \quad \frac{5.7}{33} \quad \frac{5.8}{50}$$

$$\frac{4.7}{50} \quad \frac{4.5}{33} \quad \frac{11.4}{24} \quad \frac{11.4}{18} \quad \frac{9.4}{16} \quad 9.2 \quad \frac{9.3}{16} \quad \frac{10.8}{21} \quad \frac{10.8}{26} \quad \frac{2.6}{33} \quad \frac{2.7}{50}$$

$$\frac{6.8}{50} \quad \frac{5.1}{33} \quad \frac{11.7}{25} \quad \frac{11.7}{20} \quad \frac{9.6}{16} \quad 9.4 \quad \frac{9.4}{16} \quad \frac{10.7}{20} \quad \frac{10.7}{24} \quad \frac{2.2}{33} \quad \frac{2.4}{50}$$

$$\frac{7.4}{50} \quad \frac{6.5}{33} \quad \frac{13.0}{24} \quad \frac{13.0}{20} \quad \frac{10.2}{16} \quad 9.6 \quad \frac{10.0}{16} \quad \frac{11.1}{20} \quad \frac{11.1}{24} \quad \frac{2.7}{33} \quad \frac{2.8}{50}$$

$$\frac{9.7}{50} \quad \frac{8.1}{32} \quad \frac{11.8}{24} \quad \frac{11.8}{20} \quad \frac{10.6}{16} \quad 10.0 \quad \frac{10.3}{16} \quad \frac{11.4}{18} \quad \frac{11.4}{24} \quad \frac{2.8}{32} \quad \frac{3.3}{50}$$

$$\frac{10.4}{50} \quad \frac{8.8}{32} \quad \frac{11.6}{26} \quad \frac{11.6}{19} \quad \frac{10.8}{16} \quad 10.5 \quad \frac{10.9}{16} \quad \frac{12.9}{19} \quad \frac{12.9}{25} \quad \frac{3.1}{32} \quad \frac{3.4}{50}$$

Sta.	+	K	-	Elev.
------	---	---	---	-------

249		904.53		893.8
-----	--	--------	--	-------

+50				93.5
-----	--	--	--	------

250				93.2
-----	--	--	--	------

+22				93.2
-----	--	--	--	------

+26				93.3
-----	--	--	--	------

+32				93.4
-----	--	--	--	------

+37				93.5
-----	--	--	--	------

+53				93.5
-----	--	--	--	------

B.M.		10.89	893.64	✓
------	--	-------	--------	---

Lt.

C

Rt.

$\frac{10.7}{50}$	$\frac{8.9}{34}$	$\frac{13.1}{25}$	$\frac{13.1}{19}$	$\frac{11.1}{16}$	$\frac{10.7}{16}$	$\frac{11.3}{16}$	$\frac{13.3}{19}$	$\frac{13.3}{25}$	$\frac{3.8}{34}$	$\frac{4.2}{50}$
-------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{11.1}{50}$	$\frac{11.4}{34}$	$\frac{13.7}{26}$	$\frac{13.7}{19}$	$\frac{11.7}{15}$	$\frac{11.0}{15}$	$\frac{11.4}{15}$	$\frac{13.4}{19}$	$\frac{13.4}{25}$	$\frac{5.6}{34}$	$\frac{6.3}{50}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{12.1}{50}$	$\frac{10.8}{33}$	$\frac{13.8}{27}$	$\frac{13.8}{20}$	$\frac{11.7}{16}$	$\frac{11.3}{16}$	$\frac{11.4}{17}$	$\frac{12.1}{20}$	$\frac{13.1}{25}$	$\frac{8.0}{31}$	$\frac{9.0}{50}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{12.1}{50}$	$\frac{11.6}{44}$	$\frac{14.3}{35}$	$\frac{14.3}{29}$	$\frac{12.1}{24}$	$\frac{11.3}{20}$	$\frac{11.4}{20}$	$\frac{12.6}{24}$	$\frac{12.6}{30}$	$\frac{9.4}{39}$	$\frac{9.8}{50}$
-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------	------------------	------------------

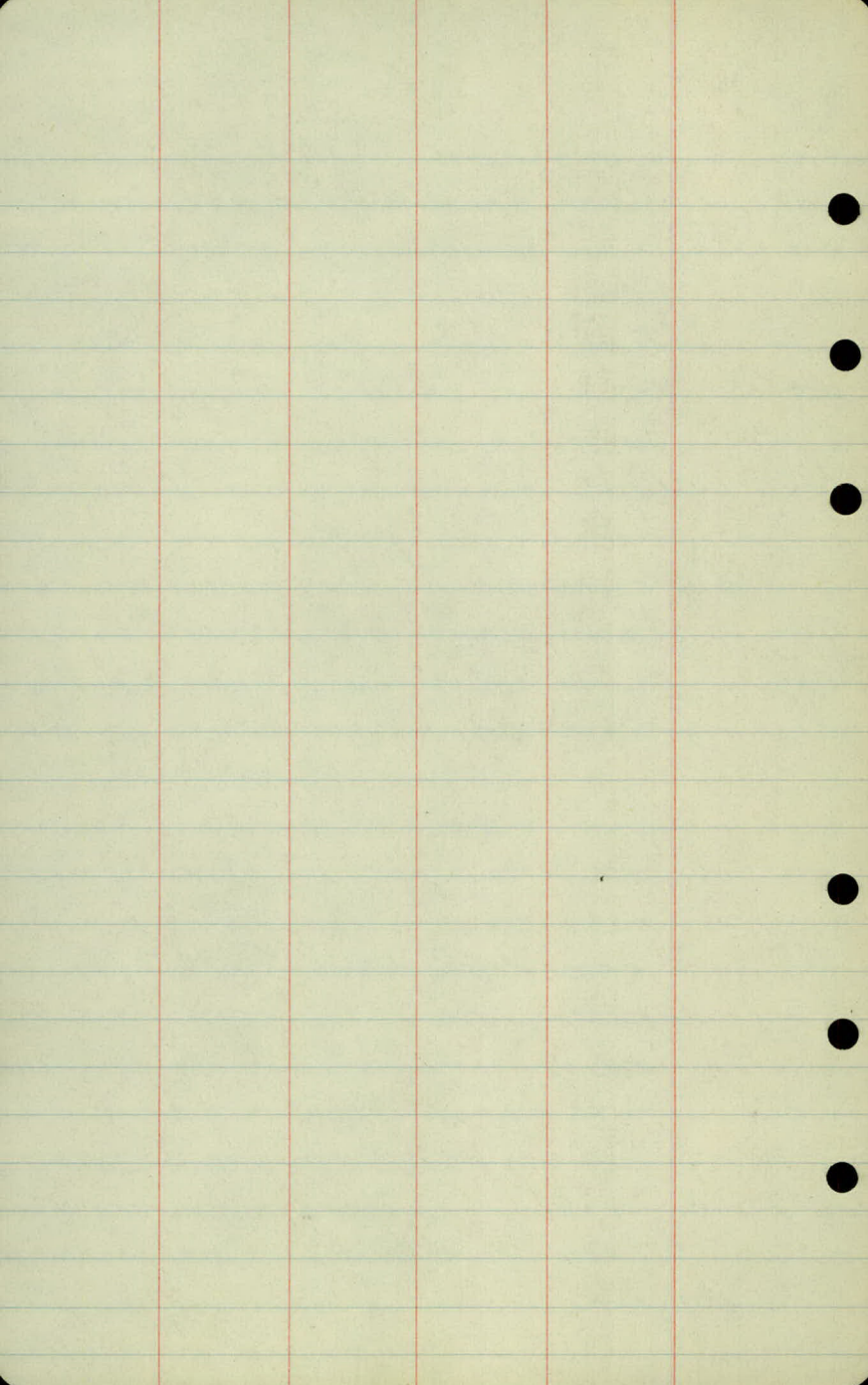
$\frac{14.5}{50}$	$\frac{14.3}{34}$	$\frac{12.3}{28}$		$\frac{11.2}{21}$	$\frac{11.4}{21}$	$\frac{12.5}{26}$	$\frac{13.0}{50}$
-------------------	-------------------	-------------------	--	-------------------	-------------------	-------------------	-------------------

$\frac{14.5}{50}$	$\frac{14.3}{43}$	$\frac{12.4}{34}$	$\frac{11.1}{34}$		$\frac{11.3}{26}$	$\frac{13.0}{36}$	$\frac{12.7}{50}$
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$\frac{12.3}{50}$		$\frac{11.0}{50}$		$\frac{10.6}{50}$
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$\frac{12.8}{50}$	$\frac{12.0}{50}$	$\frac{11.0}{50}$	$\frac{10.3}{50}$	$\frac{8.9}{100}$
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R.R. spike in Power Pole 52' East of
Intersection Lexington & Mainline Aves.



1
Huntline Ave
Bench Levels

Bratager } 3/37
Wilke }
Gillen }

Sta	+	π	-	Elev
B.M	1.22	954.47		953.25
	6.94	956.41	5.00	949.47
	10.26	965.72	0.95	955.46
B.M	2.73	965.72	2.73	962.99
	0.94	961.86	4.80	960.92
	0.15	952.94	9.07	952.79
B.M	6.96	952.94	6.96	945.98
	7.09	951.66	8.37	944.57
T.P.	10.14	957.00	4.80	946.86
	0.62	949.16	8.46	948.54
	0.40	936.81	12.75	936.41
	0.18	924.16	12.83	923.98
	0.00	915.17	8.99	915.17
B.M	7.07	915.17	7.07	908.10
	0.15	903.29	12.03	903.14
	7.10	903.30	7.09	896.20
	13.34	915.87	0.77	902.53
	5.08	920.35	0.60	915.77
B.M	0.75	920.35	0.75	919.60
	12.02	925.91	6.46	913.89
	12.36	937.53	0.74	925.17
B.M	8.44	937.53	8.44	929.09
	11.29	948.23	0.59	936.94
	0.65	942.41	6.47	941.76

2

Description

Top of most (ctr) Hamline rG

Spt in P.P. 125' Lt Sta

Spt in Swamp 100' Rt

Nail in P.P. 25' Sta. 138

Top of Conc Step. N. End of So End of House e Sta

Spt. in Pool of Cottonwood 70' Lt Sta

Spt in F.P. 80' Rt Sta 184 + 60

Sta	-	π	+	Elev
		942.41		
	0.24	929.53	13.12	929.29
	0.48	916.94	13.07	916.46
B.M	9.23	916.94	9.23	907.71 ✓
	0.19	903.73	13.40	903.54
	2.73	893.71	12.75	890.98
B.M	0.33	892.92	1.12	892.59
	7.21	898.21	1.92	891.00
	11.73	904.20	5.74	892.47
	4.19	907.45	0.94	903.26
B.M	4.38	907.45	4.38	903.07
	1.95	903.65	5.75	901.70
B.M	4.09	904.52	3.22	900.43
B.M.			10.88	893.64

2

Description

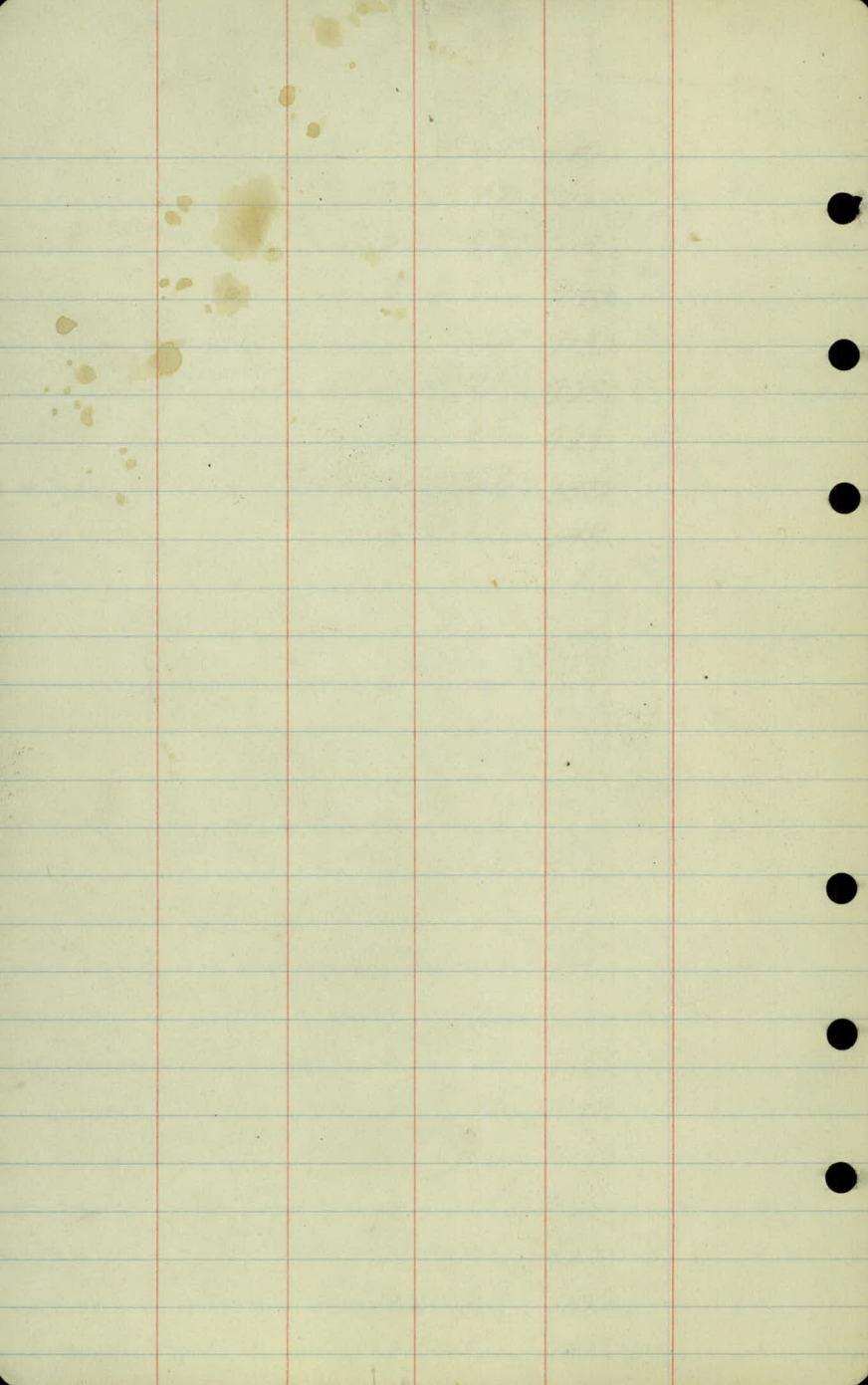
Top of Granite Boulder 75' Rt Sta

Top of Brick NW Cor of Brick & Conc. M.H. 200' Rt
Sta

Top of Mast ~~to~~ Cor

Spk. 17 18" Oak 175' Rt Sta 243

R.R. spike in RR 52' Rt. of N.E. Cor of
Lexington & Hamline Aves.



20' Top

2' Ditch

23' to ditch

27' to grade

3 to 1 fill

2 to 1 cut slope

Limit 33'

Home line

128
38

Sta.	+	π	-	Elev.
B.M.	3.25	985.91		988.66

87				77.4
----	--	--	--	------

+50				78.0
-----	--	--	--	------

88				78.1
----	--	--	--	------

+50				78.4
-----	--	--	--	------

89				78.5
----	--	--	--	------

+50				79.0
-----	--	--	--	------

90				79.5
----	--	--	--	------

+50				80.1
-----	--	--	--	------

4.

E.

B.

8.5

$$\begin{array}{r} 7.6 \\ C.0.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 7.7 \\ C.0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ C.2.7 \\ \hline 32.4 \end{array}$$

7.9
9.9

$$\begin{array}{r} 8.2 \\ DC.1.7 \\ \hline 26.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ C.0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ C.0.8 \\ \hline 28.6 \end{array}$$

9.8
9.8

$$\begin{array}{r} 8.7 \\ DC.1.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 7.1 \\ C.0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ DC.1.1 \\ \hline 25.2 \end{array}$$

7.5
9.5

$$\begin{array}{r} 9.0 \\ DC.0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 6.9 \\ C.0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 10.0 \\ F.2.5 \\ \hline 22.5 \end{array}$$

7.4
9.4

$$\begin{array}{r} 9.2 \\ DC.0.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 6.9 \\ C.0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 11.0 \\ F.3.6 \\ \hline 25.8 \end{array}$$

6.9
8.9

$$\begin{array}{r} 8.9 \\ DC.0.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 6.6 \\ C.0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ F.3.0 \\ \hline 24.0 \end{array}$$

6.4
8.4

$$\begin{array}{r} 8.0 \\ DC.0.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ C.0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ DC.1.2 \\ \hline 25.4 \end{array}$$

5.8
7.8

$$\begin{array}{r} 4.8 \\ C.1.0 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ C.0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ C.0.9 \\ \hline 28.8 \end{array}$$

Sta.	+	π	-	Elev.
		985.91		

91				80.8
----	--	--	--	------

+40		985.91 4.02		81.2
-----	--	----------------	--	------

$$\begin{array}{r} 985.91 \\ - 4.02 \\ \hline 981.89 \\ - 1.95 \\ \hline 987.84 \end{array}$$

92				81.6
----	--	--	--	------

$$\begin{array}{r} 878 \\ 520 \\ \hline 158 \end{array}$$

+50				81.8
-----	--	--	--	------

T.P.	5.95	987.84	4.02	981.89
------	------	--------	------	--------

93				82.0
----	--	--	--	------

+50				82.1
-----	--	--	--	------

94				82.3
----	--	--	--	------

+50				82.5
-----	--	--	--	------

LT.ERT.

5.1

$$\begin{array}{r} 23 \\ 628 \\ \hline 32.6 \end{array}$$

$$\begin{array}{r} 47 \\ 604 \\ \hline \end{array}$$

$$\begin{array}{r} 43 \\ 608 \\ \hline 286 \end{array}$$

4.7

$$\begin{array}{r} 05 \\ 642 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 44 \\ 603 \\ \hline \end{array}$$

$$\begin{array}{r} 30 \\ 17 \\ \hline 30.4 \end{array}$$

4.3

$$\begin{array}{r} 67 \\ 124 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 40 \\ 603 \\ \hline \end{array}$$

$$\begin{array}{r} 37 \\ 06 \\ \hline 28.2 \end{array}$$

4.1
6.1

$$\begin{array}{r} 50 \\ 1011 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 39 \\ 602 \\ \hline \end{array}$$

$$\begin{array}{r} 49 \\ 612 \\ \hline 25.4 \end{array}$$

5.8
7.8

$$\begin{array}{r} 76 \\ 1002 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 58 \\ 600 \\ \hline \end{array}$$

$$\begin{array}{r} 84 \\ 126 \\ \hline 22.8 \end{array}$$

5.7

$$\begin{array}{r} 100 \\ 143 \\ \hline 27.9 \end{array}$$

$$\begin{array}{r} 58 \\ 101 \\ \hline \end{array}$$

$$\begin{array}{r} 105 \\ 48 \\ \hline 29.4 \end{array}$$

5.5

$$\begin{array}{r} 105 \\ 110 \\ \hline 30.0 \end{array}$$

$$\begin{array}{r} 57 \\ 102 \\ \hline \end{array}$$

$$\begin{array}{r} 57 \\ 130 \\ \hline 24.6 \end{array}$$

5.3
7.7

$$\begin{array}{r} 90 \\ 137 \\ \hline 26.1 \end{array}$$

$$\begin{array}{r} 55 \\ 102 \\ \hline \end{array}$$

$$\begin{array}{r} 71 \\ 100 \\ \hline 23.4 \end{array}$$

Sto.	+	π	-	Elev.
------	---	-------	---	-------

		987.84		
--	--	--------	--	--

95				
----	--	--	--	--

				87.6
--	--	--	--	------

+50				
-----	--	--	--	--

				87.8
--	--	--	--	------

96				
----	--	--	--	--

				87.9
--	--	--	--	------

+50				
-----	--	--	--	--

				83.0
--	--	--	--	------

97				
----	--	--	--	--

				83.0
--	--	--	--	------

4.

5

8.

$$\begin{array}{r} 5.2 \\ 7.2 \end{array}$$

$$\begin{array}{r} 6.2 \\ D.C. 1.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 5.2 \\ C.00 \end{array}$$

$$\begin{array}{r} 6.1 \\ D.C. 1.1 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ 7.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ C.0.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ C.0.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ C.0.2 \\ \hline 27.4 \end{array}$$

$$4.9$$

$$\begin{array}{r} 4.4 \\ C.0.5 \\ \hline 28.0 \end{array}$$

$$\begin{array}{r} 4.4 \\ C.0.5 \end{array}$$

$$\begin{array}{r} 3.4 \\ C.1.5 \\ \hline 30.0 \end{array}$$

$$4.8$$

$$\begin{array}{r} 3.4 \\ 1.4 \\ \hline 29.8 \end{array}$$

$$\begin{array}{r} 4.2 \\ C.0.6 \end{array}$$

$$\begin{array}{r} 2.3 \\ 2.5 \\ \hline 32.0 \end{array}$$

$$4.8$$

$$\begin{array}{r} 4.1 \\ C.0.7 \end{array}$$

Sta. B.M.	+	π	-	Elev.
	1.42	966.55		965.13

73

66.3

+50

64.7

74

63.7

+50

62.5

75

61.9

+50

61.0

76

60.7

+50

60.5

77

60.4

LT.ERT

1.9

$$\frac{1.9}{C.00}$$

$$\frac{4.0}{F2.1} \\ 21.3$$

2.9

$$\frac{6.6}{F.37} \\ 26.1$$

$$\frac{3.5}{F.0.6}$$

$$\frac{10.6}{F7.7} \\ 33$$

4.1

$$\frac{10.6}{F.6.5} \\ 33$$

$$\frac{5.0}{F.0.9}$$

$$\frac{10.5}{F6.7} \\ 33$$

4.7

$$\frac{10.4}{F.6.2} \\ 33$$

$$\frac{6.2}{F.1.1}$$

$$\frac{10.7}{F6.0} \\ 33.0$$

5.6

$$\frac{11.3}{F.5.7} \\ 32.1$$

$$\frac{7.0}{F.1.4}$$

$$\frac{11.0}{F.5.4} \\ 31.2$$

5.9

$$\frac{11.2}{F.5.3} \\ 30.9$$

$$\frac{7.4}{F.1.1}$$

$$\frac{10.5}{F.4.6} \\ 28.8$$

6.1

$$\frac{9.9}{F.3.8} \\ 26.4$$

$$\frac{7.5}{F.1.4}$$

$$\frac{10.4}{F.4.3} \\ 27.9$$

6.2

$$\frac{10.3}{F.4.1} \\ 27.3$$

$$\frac{7.5}{F.1.3}$$

$$\frac{10.3}{F.4.1} \\ 27.3$$

Sta.	+	π	-	<u>Elev.</u>
		966.55		

77+55

60.4

78

60.7

+50

61.0

+73

61.5

79

61.8

LT.

E

RT.

4.2

$\begin{array}{r} 10.5 \\ \times 43 \\ \hline 27.9 \end{array}$

$\begin{array}{r} 6.9 \\ \times 0.7 \\ \hline \end{array}$

$\begin{array}{r} 8.5 \\ \times 23 \\ \hline 21.9 \end{array}$

$\begin{array}{r} 5.9 \\ 7.4 \\ \hline 5.6 \end{array}$

$\begin{array}{r} 6.8 \\ \times 1.1 \\ \hline 25.2 \end{array}$

$\begin{array}{r} 6.1 \\ \times 0.2 \\ \hline \end{array}$

$\begin{array}{r} 2.1 \\ \times 38 \\ \hline 33.0 \end{array}$

$\begin{array}{r} 5.1 \\ 7.1 \\ \hline \end{array}$

$\begin{array}{r} 23 \\ \times 23 \\ \hline 529 \end{array}$

$\begin{array}{r} 4.8 \\ \times 0.3 \\ \hline \end{array}$

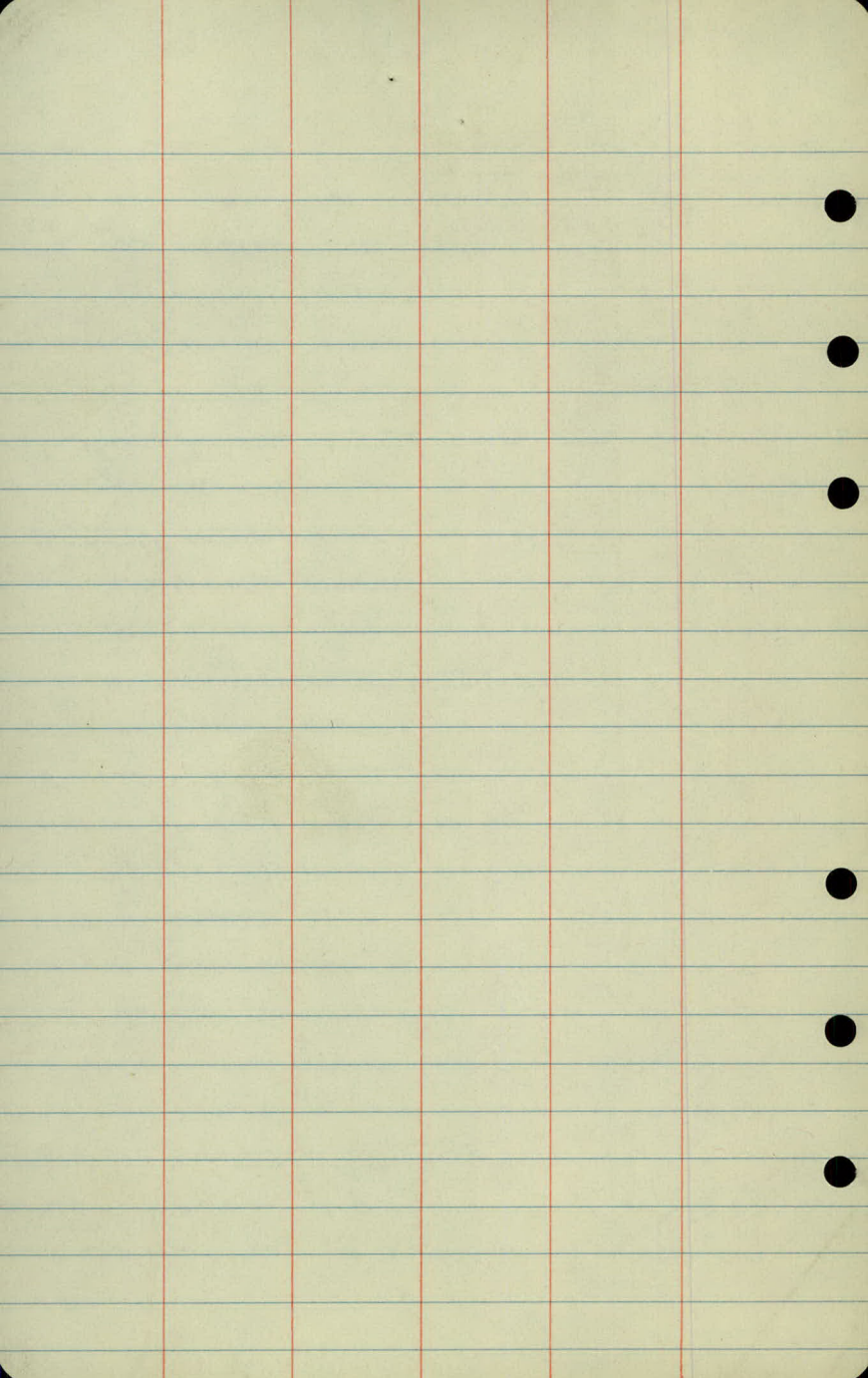
$\begin{array}{r} 4.6 \\ \times 10 \\ \hline 29.0 \end{array}$

$\begin{array}{r} 4.8 \\ 6.8 \\ \hline \end{array}$

$\begin{array}{r} 4.3 \\ \times 0.1 \\ \hline 28.0 \end{array}$

$\begin{array}{r} 4.8 \\ \times 0.0 \\ \hline \end{array}$

$\begin{array}{r} 6.4 \\ \times 0.4 \\ \hline 23.8 \end{array}$



144

Pat.

122

Pat.

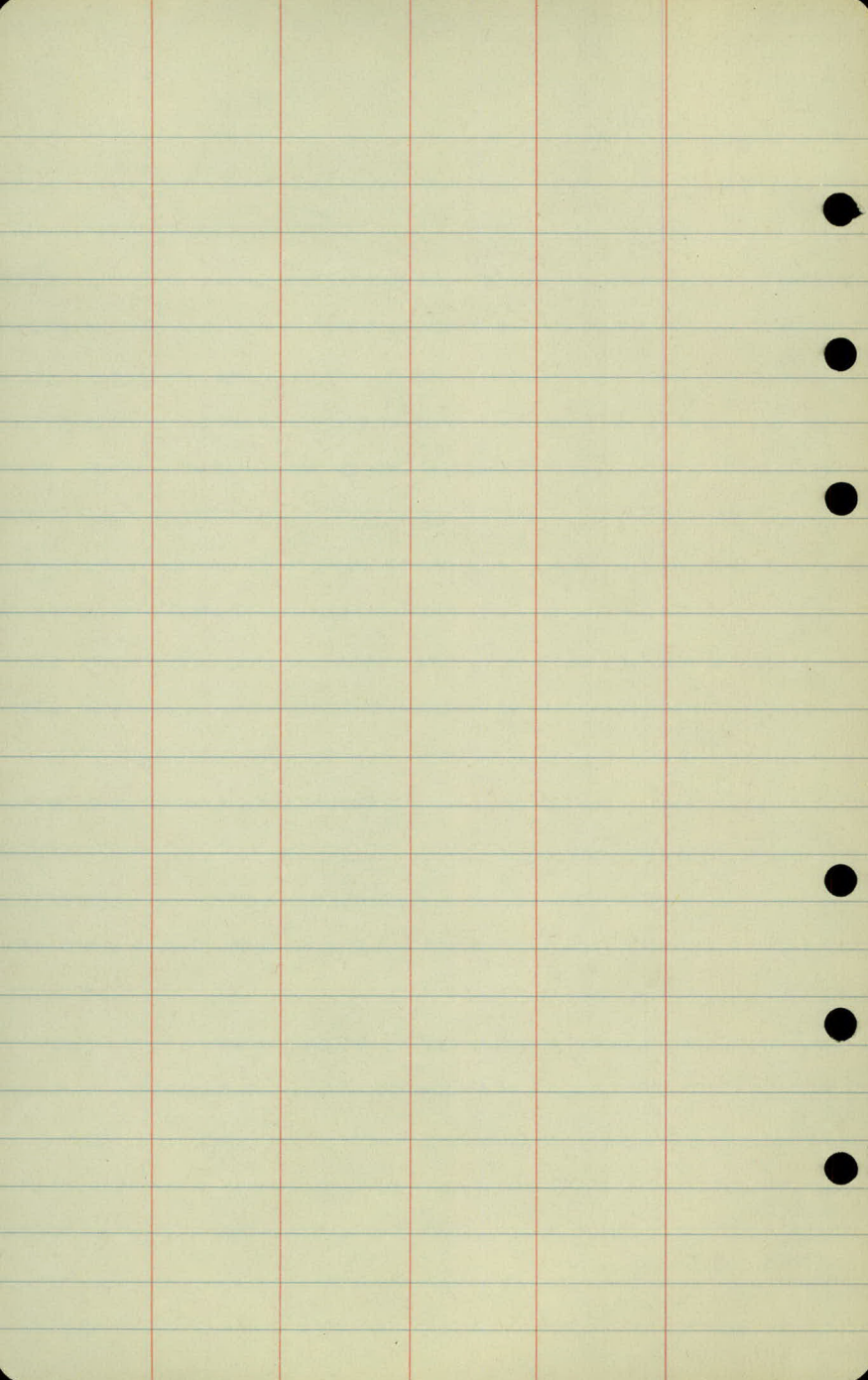
B.M. 718,56 £ stg 152

2

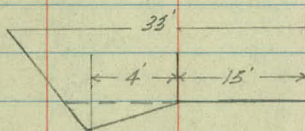
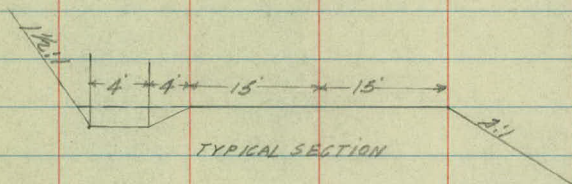
Slope Stakes

Hamling Ave.

Co. Rd "E" to Lexington Ave.



Slope Stakes.
Hamline Ave.



STA. 12+10 to 12+50 L.T.

Sta	+.	X	-	Grade
B.M.	4.74	735.90		930.56

0+00				930.4
------	--	--	--	-------

+50				930.3
-----	--	--	--	-------

1				930.3
---	--	--	--	-------

+50				930.3
-----	--	--	--	-------

2				30.2
---	--	--	--	------

+50				
-----	--	--	--	--

3				30.1
---	--	--	--	------

+50				
-----	--	--	--	--

4				30.0
---	--	--	--	------

I.P.	431	743.62	5.99	722.31
------	-----	--------	------	--------

+50				10.0
-----	--	--	--	------

5				29.9
---	--	--	--	------

PC 00 = 28.
C 00 = 26

Gr. Rod.

Lt

8

Rt

Top Mount Co. Rd. E. & Hamling Ave.

$$5.0 \quad 26.0 / \begin{array}{r} 5.0 \\ +0.0 \end{array} \quad \begin{array}{r} 9.0 \\ +1.0 \end{array}$$

$$5.0 \quad 25.9 / \begin{array}{r} 5.1 \\ 25.19 \end{array} \quad \begin{array}{r} 9.8 \\ +0.8 \end{array} \quad \begin{array}{r} 8.1 \\ +3.1 / 24.2 \end{array}$$

$$5.0 \quad 24.8 / \begin{array}{r} 5.8 \\ 25.12 \end{array} \quad \begin{array}{r} 4.6 \\ +0.9 \end{array} \quad \begin{array}{r} 5.6 \\ -3.0 / 21.9 \end{array}$$

$$5.1 \quad 23.5 / \begin{array}{r} 6.8 \\ 25.03 \end{array} \quad \begin{array}{r} 5.1 \\ 0.0 \end{array} \quad \begin{array}{r} 10.0 \\ -4.9 / 24.8 \end{array}$$

$$5.1 \quad 17.2 / \begin{array}{r} 6.2 \\ -1.1 \end{array} \quad \begin{array}{r} 5.1 \\ -0.6 \end{array} \quad \begin{array}{r} 12.6 \\ -7.5 / 30.0 \end{array}$$

$$5.2 \quad 17.4 / \begin{array}{r} 6.4 \\ -1.2 \end{array} \quad \begin{array}{r} 5.1 \\ -0.5 \end{array} \quad \begin{array}{r} 10.0 \\ -4.8 / 24.6 \end{array}$$

$$5.2 \quad 17.2 / \begin{array}{r} 6.2 \\ -1.1 \end{array} \quad \begin{array}{r} 5.8 \\ -0.6 \end{array} \quad \begin{array}{r} 8.2 \\ 3.1 / 21.2 \end{array}$$

$$5.3 \quad 23.6 / \begin{array}{r} 7.0 \\ 25.03 \end{array} \quad \begin{array}{r} 6.0 \\ -0.7 \end{array} \quad \begin{array}{r} 9.3 \\ -9.0 / 22.0 \end{array}$$

$$5.6 \quad 24.2 / \begin{array}{r} 4.8 \\ 25.08 \end{array} \quad \begin{array}{r} 4.6 \\ -1.0 \end{array} \quad \begin{array}{r} 8.8 \\ -4.9 / 24.8 \end{array}$$

$$5.7 \quad 24.5 / \begin{array}{r} 4.7 \\ 25.10 \end{array} \quad \begin{array}{r} 4.4 \\ -0.7 \end{array} \quad \begin{array}{r} 7.6 \\ -3.9 / 22.8 \end{array}$$

Sta	+	π	-	Grade
		933.62		

5	+50			29.9
---	-----	--	--	------

6				29.8
---	--	--	--	------

	+50			29.8
--	-----	--	--	------

7				29.7
---	--	--	--	------

	+50			
--	-----	--	--	--

8				29.6
---	--	--	--	------

	+50			
--	-----	--	--	--

T.P.	988	933.26	526	988.86
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9				29.5
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	+30			29.5
--	-----	--	--	------

	+50			29.4
--	-----	--	--	------

	+65			29.3
--	-----	--	--	------

Gr. Rod

Lf

S

Rt

$$3.7 \quad 23.9 / \frac{5.1}{20.06}$$

$$\frac{44}{-0.7}$$

$$\frac{53}{R.04} / 23.6$$

$$3.8 \quad 23.0 / \frac{5.8}{20.00}$$

$$\frac{47}{-0.9}$$

$$\frac{5.0}{R.08} / 29.2$$

$$2.8 \quad 18.4 / \frac{5.5}{-1.7}$$

$$\frac{48}{-1.0}$$

$$\frac{6.0}{-2.2} / 19.4$$

$$3.9 \quad 20.0 / \frac{6.4}{-2.5}$$

$$\frac{51}{-1.2}$$

$$\frac{7.8}{-3.9} / 22.8$$

$$3.9 \quad 21.8 / \frac{7.3}{-2.1}$$

$$\frac{56}{-1.7}$$

$$\frac{9.1}{-5.2} / 25.4$$

$$4.0 \quad 25.6 / \frac{9.3}{-5.3}$$

$$\frac{58}{-1.8}$$

$$\frac{10.1}{-6.1} / 27.2$$

$$4.0 \quad 26.6 / \frac{9.8}{-5.8}$$

$$\frac{54}{-1.4}$$

$$\frac{10.6}{-6.6} / 28.2$$

$$3.8 \quad 27.4 / \frac{10.0}{-6.2}$$

$$\frac{49}{-1.1}$$

$$\frac{10.9}{-7.1} / 29.2$$

$$3.8 \quad 27.0 / \frac{9.8}{-6.0}$$

$$\frac{45}{-0.7}$$

$$\frac{10.3}{-6.5} / 28.0$$

$$3.8 \quad 17.0 / \frac{4.9}{-1.0}$$

Sta	+	-	Grade	Ditch Grade	
		933.26		Lt	Rt
9	+81		29.3		
	+86		29.3		
10			29.2		
	+26		29.1		
	+60		29.9		
11			28.6	7.5 25.8	
	+50		28.2	7.0 26.3	
12			27.8	26.8	
B.M.	8.21	757.97	3.49	929.77	929.76
	+10		27.8		
	+50		27.4		
	+70		27.2		
13			27.0		

Gr. Rod

Lt

L

Rt

4.1

41 $\frac{10.9}{-6.8/28.6}$

4.2

 $\frac{25.9}{-5.0}$ $\frac{45}{-0.3}$ $\frac{3.9}{-5.7/26.7}$

4.4

 $\frac{25.2}{-5.1}$ $\frac{47}{-0.3}$ $\frac{9.6}{-5.2/25.7}$

4.7

 $\frac{2.9}{2.0.2}$ $\frac{1.7}{1.9/-2.0}$ $\frac{47}{0.0}$ $\frac{8.0}{-3.3/26.1}$

Dites 2.1 Dosa

5.1

 $\frac{23.2}{20.0}$ $\frac{50}{+0.1}$ $\frac{57}{27.4/25.1}$

5.5

 $\frac{58}{+0.3}$ $\frac{37}{+1.8/28.7}$

Spk in 12" Oak 60' 24 12480

10.2

 $\frac{32.5}{+0.8}$ 100

10.6

 $\frac{32.5}{+0.6}$ $\frac{101}{+0.5}$ $\frac{8.2}{+2.4/27.6}$

10.8

11.0

 $\frac{32.5}{+9.2}$ $\frac{106}{+0.4}$ $\frac{101}{+0.9/27.4}$

Sta.	+	-	Grade
		937.97	
	+40		24.7
13	+55		24.6
B.M.	1.99	931.75	929.76
14			24.2
	+37		25.9
	+70		25.6
15			25.4
	+20		25.2
	+47		25.0
16			24.6
	+50		24.3
17			24.3
T.P.	1.98	926.36	924.38
	+40		24.5

Gr. Rod.

L1

L2

L3

$$16.3 \quad 30.5 / \begin{array}{r} 9.3 \\ +2.0 \end{array}$$

$$\begin{array}{r} 111 \\ +0.2 \end{array}$$

$$\begin{array}{r} 13.3 \\ 12.00 / 23.0 \end{array}$$

$$11.4 \quad 17.8 / \begin{array}{r} 12.8 \\ -1.4 \end{array}$$

$$\begin{array}{r} 112 \\ +0.2 \end{array}$$

$$\begin{array}{r} 147 \\ 23 / 21.6 \end{array}$$

$$5.6 \quad 23.6 / \begin{array}{r} 9.9 \\ -4.3 \end{array}$$

$$\begin{array}{r} 56 \\ 90 \end{array}$$

$$\begin{array}{r} 10.3 \\ -4.9 / 24.8 \end{array}$$

$$5.9 \quad 23.6 / \begin{array}{r} 10.2 \\ -4.3 \end{array}$$

$$\begin{array}{r} 60 \\ -0.1 \end{array}$$

$$\begin{array}{r} 10.9 \\ -5.0 / 25.0 \end{array}$$

$$6.2 \quad 21.0 / \begin{array}{r} 9.2 \\ -3.0 \end{array}$$

$$\begin{array}{r} 60 \\ +0.2 \end{array}$$

$$\begin{array}{r} 9.9 \\ -3.7 / 22.4 \end{array}$$

$$6.4 \quad 27.1 / \begin{array}{r} 5.7 \\ +0.7 \end{array}$$

$$\begin{array}{r} 61 \\ +0.3 \end{array}$$

$$\begin{array}{r} 15 \\ 12.07 / 24.5 \end{array}$$

$$6.6 \quad 31.4 / \begin{array}{r} 2.9 \\ +2.7 \end{array}$$

$$\begin{array}{r} 62 \\ +0.4 \end{array}$$

$$\begin{array}{r} 42 \\ +2.4 \end{array}$$

$$6.8 \quad 28.3 / \begin{array}{r} 5.3 \\ +1.5 \end{array}$$

$$\begin{array}{r} 63 \\ +0.5 \end{array}$$

$$\begin{array}{r} 0.9 \\ 15.7 / 33.0 \end{array}$$

$$7.2 \quad 23.2 / \begin{array}{r} 11.3 \\ -4.1 \end{array}$$

$$\begin{array}{r} 6.9 \\ +0.3 \end{array}$$

$$\begin{array}{r} 5.8 \\ 4.4 / 28.1 \end{array}$$

$$7.5 \quad 23.5 / \begin{array}{r} 9.2 \\ +0.3 \end{array}$$

$$\begin{array}{r} 72 \\ +0.3 \end{array}$$

$$\begin{array}{r} 4.3 \\ 13.2 / 30.8 \end{array}$$

$$7.5 \quad 23.8 / \begin{array}{r} 9.0 \\ +0.5 \end{array}$$

$$\begin{array}{r} 74 \\ +0.1 \end{array}$$

$$\begin{array}{r} 5.1 \\ 12.4 / 22.6 \end{array}$$

$$11.9 \quad 23.0 / \begin{array}{r} 5.9 \\ -4.0 \end{array}$$

$$\begin{array}{r} 22 \\ +0.3 \end{array}$$

$$\begin{array}{r} 14.0 \\ 12.1 / 39.2 \end{array}$$

Sta	+	A	-	Grade
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926.36

24" X 92' C.M.

18		Cur Lt 908.3 76'		Cur Rt 908.9 46'	24.9
	+40				25.2

	+62				25.8
--	-----	--	--	--	------

T.P.	11.16	937.46	0.06	926.50
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19				26.6
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	+50			27.7
--	-----	--	--	------

20				28.7
----	--	--	--	------

	+50			29.8
--	-----	--	--	------

21				30.8
----	--	--	--	------

B.M.				931.80
------	--	--	--	--------

	+50			31.9
--	-----	--	--	------

22				33.3
----	--	--	--	------

	+50			34.4
--	-----	--	--	------

T.P.	13.22	949.59	1.29	936.17
------	-------	--------	------	--------

	+75			35.4
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Gr. Rod

Lt

L

Rt

$$1.5 \quad 436 / \begin{array}{r} 168 \\ -15.3 \end{array} \quad \begin{array}{r} 20 \\ -05 \end{array} \quad \begin{array}{r} 16.8 \\ -14.8 \end{array} / 44.8$$

$$1.2 \quad 400 / \begin{array}{r} 13.7 \\ -12.5 \end{array}$$

$$0.6 \quad 35.0 / \begin{array}{r} 5.4 \\ -5.0 \end{array} \quad \begin{array}{r} 0.9 \\ -0.3 \end{array} \quad \begin{array}{r} 12.8 \\ -12.2 \end{array} / 39.4$$

$$10.9 \quad 20.5 / \begin{array}{r} 13.7 \\ -8.8 \end{array} \quad \begin{array}{r} 11.2 \\ -0.3 \end{array} \quad \begin{array}{r} 14.2 \\ -3.3 \end{array} / 21.6$$

$$9.8 \quad 23.9 / \begin{array}{r} 11.8 \\ 20.0 \end{array} \quad \begin{array}{r} 10.1 \\ +0.3 \end{array} \quad \begin{array}{r} 8.2 \\ 41.6 \end{array} / 28.4$$

$$8.8 \quad 27.5 / \begin{array}{r} 7.8 \\ 4.0 \end{array} \quad \begin{array}{r} 9.0 \\ -0.2 \end{array} \quad \begin{array}{r} 5.0 \\ +3.8 \end{array} / 31.7$$

$$7.7 \quad 24.8 / \begin{array}{r} 8.5 \\ 12.13 \end{array} \quad \begin{array}{r} 7.5 \\ -0.1 \end{array} \quad \begin{array}{r} 4.0 \\ +3.7 \end{array} / 31.6$$

$$6.7 \quad 23.2 / \begin{array}{r} 8.6 \\ 12.01 \end{array} \quad \begin{array}{r} 6.8 \\ -0.1 \end{array} \quad \begin{array}{r} 6.7 \\ 41.2 \end{array} / 32.3$$

5pk in 24" Oak 102 Lt. 21100

$$5.6 \quad 23.0 / \begin{array}{r} 9.6 \\ 4.0 \end{array} \quad \begin{array}{r} 5.8 \\ -0.2 \end{array} \quad \begin{array}{r} 2.8 \\ +2.8 \end{array} / 30.2$$

$$4.2 \quad 23.0 / \begin{array}{r} 8.2 \\ -9.0 \end{array} \quad \begin{array}{r} 4.4 \\ -0.2 \end{array} \quad \begin{array}{r} 2.6 \\ 41.6 \end{array} / 28.4$$

$$3.1 \quad 23.0 / \begin{array}{r} 5.1 \\ 20.0 \end{array} \quad \begin{array}{r} 2.8 \\ +0.3 \end{array} \quad \begin{array}{r} 0.5 \\ +2.8 \end{array} / 30.2$$

Sta	+	1	-	Grade
		949.39		
23				36.1
	+50			37.15
24				38.9
	+50			39.5
25				39.5
	+50			38.7
26				37.9
B.M.		16.85		326.59
	+24			374
	+28			37.3
	+40			37.1
	+52			36.8
B.M.				936.51

936.51

Gr Rod.

11

8

121

$$13.3 \quad 29.0 / \begin{array}{r} 11.3 \\ + 0.0 \end{array}$$

$$\begin{array}{r} 132 \\ + 01 \end{array}$$

$$\begin{array}{r} 116 \\ 417 / 286 \end{array}$$

$$12.3 \quad 35.3 / \begin{array}{r} 0.1 \\ + 0.2 \end{array}$$

$$\begin{array}{r} 119 \\ - 01 \end{array}$$

$$\begin{array}{r} 105 \\ 418 / 287 \end{array}$$

$$10.5 \quad 39.4 / \begin{array}{r} 1.6 \\ + 0.9 \end{array}$$

$$\begin{array}{r} 110 \\ + 05 \end{array}$$

$$\begin{array}{r} 85 \\ 120 / 280 \end{array}$$

$$7.7 \quad 38.9 / \begin{array}{r} 13 \\ + 86 \end{array}$$

$$\begin{array}{r} 93 \\ + 06 \end{array}$$

$$\begin{array}{r} 6.5 \\ 134 / 311 \end{array}$$

$$9.9 \quad 35.0 / \begin{array}{r} 3.9 \\ + 0.0 \end{array}$$

$$\begin{array}{r} 96 \\ + 03 \end{array}$$

$$\begin{array}{r} 5.9 \\ 195 / 32.8 \end{array}$$

$$10.7 \quad 29.8 / \begin{array}{r} 8.2 \\ + 2.5 \end{array}$$

$$\begin{array}{r} 105 \\ + 02 \end{array}$$

$$\begin{array}{r} 6.9 \\ 138 / 31.7 \end{array}$$

$$11.5 \quad 26.3 / \begin{array}{r} 11.3 \\ + 0.2 \end{array}$$

$$\begin{array}{r} 118 \\ - 03 \end{array}$$

$$\begin{array}{r} 11.2 \\ 10.8 / 26.3 \end{array}$$

Top Mount 26+40.52

Sta	+	1	-	Grade
B.M.	3.56	940.07		936.51

26	+56			36.7
----	-----	--	--	------

27				35.9
----	--	--	--	------

	+35			35.2
--	-----	--	--	------

	+50			34.9
--	-----	--	--	------

T.P.	4.40	938.09	6.31	933.69
------	------	--------	------	--------

28				34.2
----	--	--	--	------

	+50			33.7
--	-----	--	--	------

29				33.4
----	--	--	--	------

	+30			33.3
--	-----	--	--	------

30				33.4
----	--	--	--	------

T.P.	7.65	942.56	3.19	934.91
------	------	--------	------	--------

	+30			33.6
--	-----	--	--	------

31				34.1
----	--	--	--	------

Gr Rod

LH

L

RH

Top Mont.

$$3.4 \quad \begin{array}{r} 32.3 \\ +1.1 \\ \hline +9.5 \end{array} \quad \begin{array}{r} 39 \\ -0.5 \end{array} \quad +60 \frac{44}{213} / 25.7$$

$$4.2 \quad \begin{array}{r} 30.1 \\ +1.5 \\ \hline +2.7 \end{array} \quad \begin{array}{r} 45 \\ +0.3 \end{array} \quad \frac{5.9}{21.03} / 23.5$$

$$4.9 \quad \begin{array}{r} 51 \\ -0.2 \end{array} \quad \frac{7.3}{-2.4} / 9.8$$

$$5.2 \quad \begin{array}{r} 28.4 \\ +11.8 \\ \hline -6.7 \end{array} \quad \begin{array}{r} 54 \\ -0.2 \end{array} \quad \frac{90}{-38} / 22.6$$

$$3.9 \quad \begin{array}{r} 40.6 \\ +16.7 \\ \hline -12.8 \end{array} \quad \begin{array}{r} 44 \\ -0.5 \end{array} \quad \frac{12.1}{-8.2} / 31.4$$

$$4.4 \quad \begin{array}{r} 39.8 \\ +16.8 \\ \hline -12.4 \end{array} \quad \begin{array}{r} 49 \\ -0.3 \end{array} \quad \frac{13.5}{9.4} / 32.8$$

$$4.7 \quad \begin{array}{r} 36.2 \\ +15.3 \\ \hline -10.6 \end{array} \quad \begin{array}{r} 51 \\ -0.4 \end{array} \quad \frac{13.7}{-70} / 33.0$$

$$4.8 \quad \begin{array}{r} 24.4 \\ +9.5 \\ \hline -4.7 \end{array} \quad \begin{array}{r} 50 \\ -0.2 \end{array} \quad \frac{10.6}{-5.8} / 26.6$$

$$4.7 \quad \begin{array}{r} 28.4 \\ +9.1 \\ \hline +16 \end{array} \quad \begin{array}{r} 45 \\ +0.2 \end{array} \quad \frac{0.3}{+4.4} / 32.6$$

$$9.0 \quad \begin{array}{r} 34.3 \\ +9.5 \\ \hline +5.5 \end{array} \quad \begin{array}{r} 83 \\ +0.7 \end{array} \quad \frac{1.7}{+73} / 37.0$$

$$8.5 \quad \begin{array}{r} 34.7 \\ +2.7 \\ \hline +5.5 \end{array} \quad \begin{array}{r} 77 \\ +0.8 \end{array} \quad \frac{0.8}{+7.7} / 37.6$$

Sta.	+	π	-	Grade	Lt.	Rt.
		948.56				

31	+50			34.7		32.7
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32				35.2		32.9
----	--	--	--	------	--	------

	+50			35.7		33.1
--	-----	--	--	------	--	------

I.P.	13.54	948.05	8.05	934.51		
------	-------	--------	------	--------	--	--

33				36.3		
----	--	--	--	------	--	--

	+50			36.9		
--	-----	--	--	------	--	--

	+70			37.0		
--	-----	--	--	------	--	--

34				37.4		
----	--	--	--	------	--	--

	+50			38.0		
--	-----	--	--	------	--	--

35				38.5		
----	--	--	--	------	--	--

	+ 50					
--	------	--	--	--	--	--

	+60			39.1		
--	-----	--	--	------	--	--

36				39.6		
----	--	--	--	------	--	--

Gr. Rod

Lt.

¢

Rt.

7.7

$$311 / \frac{4.5}{+3.4}$$

$$\frac{73}{+0.6}$$

$$\frac{38}{+91/32.2}$$

1.3 Deep
C.W. = 2.46
R.O. = 2.86 7.4

$$286 / \frac{57}{+1.7}$$

$$\frac{70}{+0.4}$$

$$\frac{76}{R.21/26.8}$$

Ditch 2.5

2.4 Deep
C.W. = 2.72
R.O. = 2.92 6.9

$$286 / \frac{46}{+2.3}$$

$$\frac{69}{90}$$

$$\frac{90}{R.03/25.0}$$

Ditch 2.6

11.8

$$289 / \frac{98}{+2.0}$$

$$\frac{12.0}{-0.2}$$

$$\frac{140}{R.00/28.4}$$

Ditch 2.2

11.2

$$266 / \frac{108}{+0.4}$$

$$\frac{116}{-0.4}$$

$$\frac{129}{R.03/23.5}$$

11.1

10.7

$$266 / \frac{103}{+0.4}$$

$$\frac{107}{0.0}$$

$$\frac{101}{+0.6/26.9}$$

10.1

$$287 / \frac{50}{+0.1}$$

$$\frac{99}{+0.2}$$

$$\frac{49}{+57/34.6}$$

9.6

$$340 / \frac{43}{+5.3}$$

$$\frac{93}{+0.3}$$

$$\frac{0.2}{+9.4/40.1}$$

9.1

$$255 / \frac{2.8}{+4.8}$$

9.0

$$25.3 / \frac{9.5}{R.1.5}$$

$$\frac{86}{+0.4}$$

$$\frac{0.6}{+8.4/38.6}$$

8.5

$$25.4 / \frac{8.7}{R.1.6}$$

$$\frac{85}{0.0}$$

$$\frac{4.7}{+38/30.7}$$

Sta	L	A	-	Grade
		799.05		

36	+50			40.2
----	-----	--	--	------

T.P.	5.38	945.56	7.80	790.18
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37		940.2		40.7
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	+50			41.25
--	-----	--	--	-------

38				41.9
----	--	--	--	------

	+50			42.8
--	-----	--	--	------

T.P.	10.73	953.91	2.38	793.18
------	-------	--------	------	--------

39				43.7
----	--	--	--	------

	+50			44.7
--	-----	--	--	------

40				46.2
----	--	--	--	------

	+65			48.3
--	-----	--	--	------

41				49.5
----	--	--	--	------

	+50			51.4
--	-----	--	--	------

T.P.	10.78	961.05	3.64	950.27
------	-------	--------	------	--------

Gr. Rod

Lk

F

Rt.

7.9

$$290/70$$

$$-70$$

$$82$$

$$-03$$

$$71$$

$$+08/27.2$$

L sta 97

-05

4.9

$$409/120$$

$$-125$$

$$54$$

$$-05$$

$$61$$

$$128.08/24.2$$

-2.2

4.4

$$496/151$$

$$-173$$

$$98$$

$$-04$$

$$103$$

$$5.9/26.8$$

-1.7

3.7

$$448/132$$

$$-149$$

$$42$$

$$-05$$

$$115$$

$$-78/30.6$$

-2.6

2.8

$$378/88$$

$$114$$

$$31$$

$$-03$$

$$81$$

$$53/25.6$$

9.7

10.2

$$720/142$$

$$-46$$

$$104$$

$$-02$$

$$102$$

$$00/260$$

8.5

9.0

$$280/72$$

$$+73$$

$$91$$

$$+01$$

$$57$$

$$+33/361$$

7.2

7.7

$$311/38$$

$$+34$$

$$77$$

$$0.0$$

$$16$$

$$+61/36.2$$

5.1 7.8

5.6

$$239/71$$

$$1000$$

$$5.5$$

$$+0.7$$

$$5.6$$

$$00/260$$

3.9

4.4

$$362/128$$

$$-109$$

$$44$$

$$00$$

$$102$$

$$-68/26.6$$

2.0

2.5

$$360/125$$

$$-708$$

$$29$$

$$-04$$

$$100$$

$$-75/30.0$$

Sta.	+	π	-	Grade.
		953.39 961.05		
42				53.4
B.M.	8.78 6.44	961.81 961.05	0.36 6.44	953.93 954.63
+50				55.4
43				57.4
+50				59.4
T.P.	13.49 13.56	975.27 974.31	0.05 0.30	961.76 960.75
44				61.4
+50				63.4
45				65.4
+50				67.4
46				69.4
+50				71.4
T.P.	13.18 12.76	987.11 986.67	1.34 0.90	973.93 973.91
47				73.4

Gr. Rod.

Lt.

C

Rt.

$$\begin{array}{r} 0.1 \\ 7.7 \end{array}$$

$$\begin{array}{r} 36.2/10.7 \\ -10.6 \end{array}$$

$$\begin{array}{r} 8.0 \\ -0.3 \end{array}$$

$$\begin{array}{r} 15.5 \\ -18.1/31.6 \end{array}$$

Spt in PP 48 Rt sto 42145

$$\begin{array}{r} 6.4 \\ 5.7 \end{array}$$

$$\begin{array}{r} 28.4/13.2 \\ -6.8 \end{array}$$

$$\begin{array}{r} 5.8 \\ -0.1 \end{array}$$

$$\begin{array}{r} 10.0 \\ -4.3/24.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ 3.7 \end{array}$$

$$\begin{array}{r} 23.9/6.4 \\ -10.0 \end{array}$$

$$\begin{array}{r} 3.6 \\ +0.1 \end{array}$$

$$\begin{array}{r} 2.7 \\ +1.0/27.5 \end{array}$$

$$\begin{array}{r} 2.4 \\ 1.7 \end{array}$$

$$\begin{array}{r} 27.3/1.6 \\ -10.0 \end{array}$$

$$\begin{array}{r} 1.4 \\ +0.3 \end{array}$$

$$\begin{array}{r} 4.7 \\ -1.4/31.1 \end{array}$$

$$\begin{array}{r} 13.9 \\ 12.9 \end{array}$$

$$\begin{array}{r} 31.1/10.5 \\ -13.4 \end{array}$$

$$\begin{array}{r} 12.3 \\ +0.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ +0.5/38.8 \end{array}$$

$$\begin{array}{r} 11.9 \\ 10.9 \end{array}$$

$$\begin{array}{r} 38.3/3.7 \\ +5.2 \end{array}$$

$$\begin{array}{r} 10.3 \\ +0.6 \end{array}$$

$$\begin{array}{r} 3.1 \\ +7.8/37.7 \end{array}$$

$$\begin{array}{r} 9.9 \\ 8.9 \end{array}$$

$$\begin{array}{r} 4.1/4.5 \\ +3.4 \end{array}$$

$$\begin{array}{r} 8.9 \\ +0.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ +2.1/29.2 \end{array}$$

$$\begin{array}{r} 7.9 \\ 6.9 \end{array}$$

$$\begin{array}{r} 28.9/6.4 \\ +1.2 \end{array}$$

$$\begin{array}{r} 6.6 \\ +0.3 \end{array}$$

$$\begin{array}{r} 6.9 \\ +0.0/26.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ 4.7 \end{array}$$

$$\begin{array}{r} 26.6/5.5 \\ +0.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ +0.3 \end{array}$$

$$\begin{array}{r} 5.8 \\ 20.1/24.7 \end{array}$$

$$\begin{array}{r} 3.9 \\ 2.7 \end{array}$$

$$\begin{array}{r} 26.3/3.7 \\ +0.2 \end{array}$$

$$\begin{array}{r} 2.7 \\ +0.2 \end{array}$$

$$\begin{array}{r} 3.3 \\ +0.4/26.6 \end{array}$$

$$\begin{array}{r} 13.7 \\ 13.3 \end{array}$$

$$\begin{array}{r} 31.1/1.9 \\ -1.8 \end{array}$$

$$\begin{array}{r} 12.8 \\ +0.5 \end{array}$$

$$\begin{array}{r} 1.8 \\ +1.5/28.3 \end{array}$$

Sta.	+	π	-	Grade
		986.67		
47	+50			75.3
48				77.0
	+50			78.4
49				79.7
	+50			80.7
50				81.5
	+50			82.1
51				82.6
	+50			82.8
52				83.1
	+50			83.3
B.M.			1.45	985.22
B.M.			0.89	986.22
			0.40	

Co. Rd.

Lt.

E

Rt.

$$\begin{array}{r} 118 \\ 11.4 \end{array}$$

$$\begin{array}{r} 338/46 \\ +5.2 \end{array}$$

$$\begin{array}{r} 108 \\ +0.6 \end{array}$$

$$\begin{array}{r} 94 \\ +20/29.0 \end{array}$$

$$\begin{array}{r} 10.1 \\ 9.7 \end{array}$$

$$\begin{array}{r} 41/34 \\ +2.7 \end{array}$$

$$\begin{array}{r} 90 \\ +0.7 \end{array}$$

$$\begin{array}{r} 7.3 \\ +2.4/29.4 \end{array}$$

$$\begin{array}{r} 8.7 \\ 8.5 \end{array}$$

$$\begin{array}{r} 38/36 \\ +1.1 \end{array}$$

$$\begin{array}{r} 75 \\ +0.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ +3.3/31.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ 7.0 \end{array}$$

$$\begin{array}{r} 32.3/3.3 \\ +1.1 \end{array}$$

$$\begin{array}{r} 66 \\ +0.4 \end{array}$$

$$\begin{array}{r} 4.0 \\ +3.0/30.5 \end{array}$$

$$\begin{array}{r} 6.4 \\ 6.0 \end{array}$$

$$\begin{array}{r} 27.2/4.3 \\ +1.1 \end{array}$$

$$\begin{array}{r} 56 \\ +0.4 \end{array}$$

$$\begin{array}{r} 4.9 \\ +1.1/27.7 \end{array}$$

$$\begin{array}{r} 5.6 \\ 5.2 \end{array}$$

$$\begin{array}{r} 27.5/4.6 \\ +1.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ +0.3 \end{array}$$

$$\begin{array}{r} 5.9 \\ 2.13/25.0 \end{array}$$

$$\begin{array}{r} 5.0 \\ 4.6 \end{array}$$

$$\begin{array}{r} 24.5/6.0 \\ +1.0 \end{array}$$

$$\begin{array}{r} 46 \\ 0.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ -3.4/21.8 \end{array}$$

$$\begin{array}{r} 4.2 \\ 4.2 \end{array}$$

$$\begin{array}{r} 4.5 \\ -0.3 \end{array}$$

$$\begin{array}{r} 9.4 \\ -5.2/25.4 \end{array}$$

$$\begin{array}{r} 4.3 \\ 3.9 \end{array}$$

$$\begin{array}{r} 4.3 \\ -0.4 \end{array}$$

$$\begin{array}{r} 9.5 \\ -5.6/25.2 \end{array}$$

$$\begin{array}{r} 4.0 \\ 3.6 \end{array}$$

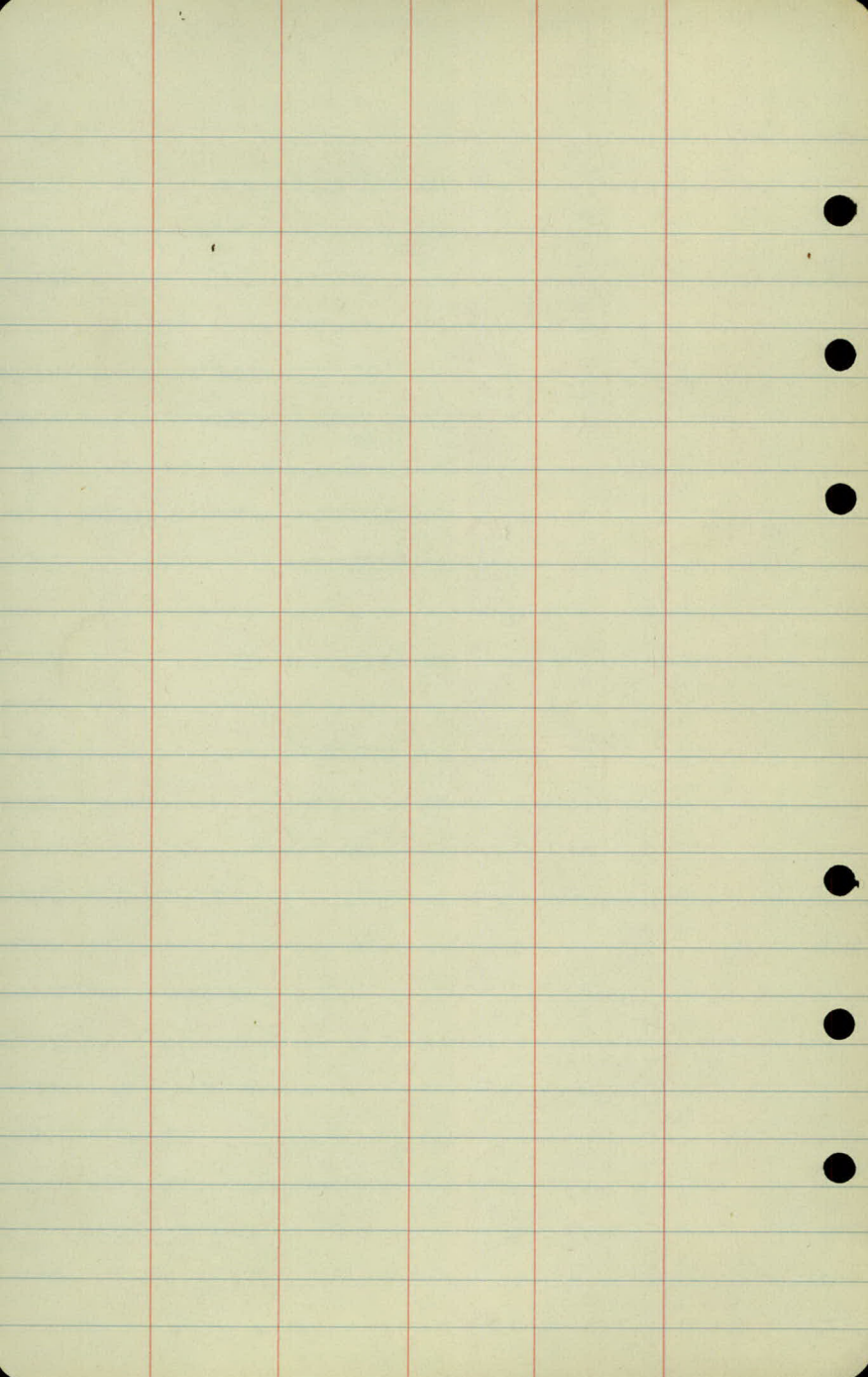
$$\begin{array}{r} 330/130 \\ -90 \end{array}$$

$$\begin{array}{r} 4.1 \\ -0.5 \end{array}$$

$$\begin{array}{r} 8.2 \\ -4.6/24.2 \end{array}$$

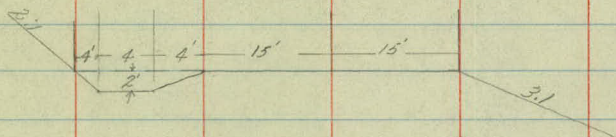
3pk in 8" Oak S.E. Cor. Harding & Co. Rd. F.

" " 30" Oak 100' Rt. 52+



Slope Stakes
Hamline Ave
Co. Rd. "F" to Co. Rd. "H"

TYPICAL SECTION



Sta	+	-	Grade	Pitch Grade
B.M.	2.09	988.33	986.24	986.22

52 + 76.16

T.P.	5.89	991.06	316	985.17
------	------	--------	-----	--------

53				83.6
----	--	--	--	------

+50				841
-----	--	--	--	-----

+70				846
-----	--	--	--	-----

54				850
----	--	--	--	-----

+50				854
-----	--	--	--	-----

55				858
----	--	--	--	-----

+50				858
-----	--	--	--	-----

56				855
----	--	--	--	-----

+50				848
-----	--	--	--	-----

57				841
----	--	--	--	-----

+55				830
-----	--	--	--	-----

T.P.	2.76	986.07	775	983.31
------	------	--------	-----	--------

Gr. Rod

Lt.

%

Rt.

Spk in 30" Oct S.E. Cor Hamline & Co Rd E"

75

$$29.8 / \frac{64}{+11}$$

$$\frac{74}{+91}$$

70

$$330 / \frac{34}{+26}$$

$$\frac{68}{+102}$$

65

61

$$31.0 / \frac{41}{+20}$$

$$\frac{59}{+92}$$

57

$$29.8 / \frac{48}{+19}$$

$$\frac{52}{+93}$$

$$\frac{34}{+23} / 31.6$$

53

$$31.4 / \frac{31}{+2.2}$$

$$\frac{47}{+106}$$

$$\frac{34}{+19} / 30.8$$

53

$$29.6 / \frac{40}{+13}$$

$$\frac{48}{+91}$$

$$\frac{39}{+14} / 29.8$$

56

$$28.8 / \frac{5.0}{+106}$$

$$\frac{53}{+93}$$

$$\frac{51}{+25} / 28.0$$

63

$$26.6 / \frac{6.5}{+20.8}$$

$$\frac{57}{+109}$$

$$\frac{66}{+17} / 26.4$$

70

$$28.0 / \frac{6.5}{+93}$$

$$\frac{66}{+104}$$

$$\frac{70}{+100} / 27.0$$

8.4

$$26.0 / \frac{9.6}{+20.15}$$

$$\frac{78}{+116}$$

$$\frac{78}{+46} / 32.0$$

Sta	+	X	-	Grade
		986.07		
58				82.1
	+50			81.1
59				80.2
	+50			79.4
60				78.7
B.M.	3.68		515	980.92
	+50			78.2
61				77.6
	+50			77.1
62				76.2
	+50			75.5
63				74.3
	+50			73.0

Gr. Rod

Lat

E

RL

4.0

 $\frac{36}{+0.4}$ $\frac{213}{+17/20.4}$

5.0

 $\frac{24.6}{+0.08} \frac{6.2}{20.08}$ $\frac{48}{+0.2}$

5.9

 $\frac{23.0}{+0.0} \frac{7.9}{20.0}$ $\frac{56}{+0.3}$

6.7

 $\frac{22.9}{+1.2} \frac{5.5}{11.2}$ $\frac{63}{+0.4}$ $\frac{6.9}{+0.18/26.6}$

7.4

 $\frac{23.4}{+0.02} \frac{9.2}{20.02}$ $\frac{68}{+0.6}$

6.9

 $\frac{22.8}{+0.07} \frac{7.5}{20.07}$ $\frac{60}{+0.4}$

7.0

 $\frac{31.6}{+0.3} \frac{4.7}{12.3}$ $\frac{68}{+0.2}$ $\frac{66}{+0.16/26.2}$

7.6

 $\frac{33.0}{+0.1} \frac{3.4}{4.1}$ $\frac{73}{+0.2}$ $\frac{80}{+0.13/26.0}$

8.4

 $\frac{33.0}{+0.0} \frac{3.4}{15.0}$ $\frac{80}{+0.4}$ $\frac{86}{+0.2/27.4}$

9.1

 $\frac{33.0}{+0.0} \frac{5.1}{4.0}$ $\frac{88}{+0.3}$ $\frac{8.4}{+0.7/28.4}$

10.3

 $\frac{31.0}{+0.0} \frac{8.3}{12.0}$ $\frac{98}{+0.5}$ $\frac{10.5}{+2.5/32.6}$

11.6

 $\frac{28.8}{+0.9} \frac{10.1}{10.1}$ $\frac{11.1}{+0.5}$ $\frac{10.3}{+1.3/29.6}$

Sph in 20° Oak 120' RL 19820
 7.4
 23.4/20.02
 68/106

Sta.	+	Σ	-	Grade
T.P.	986	975.69		974.83
64				71.8
+50				71.5
65				69.5
+50				68.7
66				68.2
T.P.	761	974.91	8.39	967.30
+50				67.9
67				67.9
+50				68.1
68				68.5
+50				69.2
69				70.2
+50				71.2
T.P.	4.76	976.60	3.07	971.84
70				76.8
+50				71.8

Geo. Red.

kt

E

RL

R 340 68

3.9

$$\frac{210}{1800} \frac{5.9}{1800}$$

$$\frac{3.7}{+0.2}$$

$$\frac{5.9}{1800} \frac{210}{1800}$$

4.2

$$\frac{214}{1800} \frac{7.4}{1800}$$

$$\frac{5.1}{-0.9}$$

$$\frac{10.4}{1800} \frac{214}{1800}$$

4.2

$$\frac{24.9}{1800} \frac{7.9}{1800}$$

$$\frac{6.5}{-0.3}$$

$$\frac{12.6}{1800} \frac{24.9}{1800}$$

7.0

$$\frac{300}{1800} \frac{12.0}{1800}$$

$$\frac{7.7}{-0.7}$$

$$\frac{13.3}{1800} \frac{300}{1800}$$

7.5

$$\frac{30.9}{1800} \frac{12.8}{1800}$$

$$\frac{8.4}{-0.9}$$

$$\frac{13.5}{1800} \frac{30.9}{1800}$$

L 349 66

7.0

$$\frac{31.2}{1800} \frac{12.4}{1800}$$

$$\frac{7.8}{-0.8}$$

$$\frac{12.6}{1800} \frac{31.2}{1800}$$

7.0

$$\frac{30.9}{1800} \frac{12.8}{1800}$$

$$\frac{7.7}{-0.7}$$

$$\frac{11.9}{1800} \frac{30.9}{1800}$$

6.8

$$\frac{29.1}{1800} \frac{11.5}{1800}$$

$$\frac{7.9}{-0.5}$$

$$\frac{11.1}{1800} \frac{29.1}{1800}$$

6.4

$$\frac{30.0}{1800} \frac{11.9}{1800}$$

$$\frac{6.9}{-0.5}$$

$$\frac{11.4}{1800} \frac{30.0}{1800}$$

5.7

$$\frac{23.0}{1800} \frac{7.7}{1800}$$

$$\frac{5.7}{0.0}$$

$$\frac{9.8}{1800} \frac{23.0}{1800}$$

4.7

$$\frac{24.0}{1800} \frac{5.5}{1800}$$

$$\frac{4.6}{+0.1}$$

$$\frac{4.5}{1800} \frac{24.0}{1800}$$

3.7

$$\frac{24.6}{1800} \frac{3.9}{1800}$$

$$\frac{3.8}{-0.1}$$

$$\frac{3.4}{1800} \frac{24.6}{1800}$$

4.8

$$\frac{25.6}{1800} \frac{5.5}{1800}$$

$$\frac{4.6}{+0.2}$$

$$\frac{1.6}{1800} \frac{25.6}{1800}$$

4.8

$$\frac{25.4}{1800} \frac{4.6}{1800}$$

$$\frac{4.8}{0.0}$$

$$\frac{0.9}{1800} \frac{25.4}{1800}$$

Sta	+	π	-	Grade
		976.60		

71				71.5
----	--	--	--	------

+50				70.8
-----	--	--	--	------

72				69.4
----	--	--	--	------

+50				68.0
-----	--	--	--	------

73				66.3
----	--	--	--	------

+50				64.6
-----	--	--	--	------

T.P.			13.46	
------	--	--	-------	--

74				63.7
----	--	--	--	------

+50				62.6
-----	--	--	--	------

75				61.9
----	--	--	--	------

+50				
-----	--	--	--	--

76				
----	--	--	--	--

+50				
-----	--	--	--	--

Gr. Red

Lt

E

Rt

5.1

$$\begin{array}{r} 33.0 / 1.8 \\ + 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 50 \\ + 91 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ + 1.6 \\ \hline 5.0 \end{array} \quad 10.2$$

5.8

$$\begin{array}{r} 33.0 / 0.8 \\ + 5.5 \\ \hline \end{array}$$

$$\begin{array}{r} 58 \\ + 0 \\ \hline \end{array}$$

$$\begin{array}{r} 2.5 \\ + 3.5 \\ \hline 6.0 \end{array} \quad 33.0$$

7.2

$$\begin{array}{r} 33.0 / 0.2 \\ + 7.0 \\ \hline \end{array}$$

$$\begin{array}{r} 68 \\ + 64 \\ \hline \end{array}$$

$$\begin{array}{r} 2.6 \\ + 4.6 \\ \hline 7.2 \end{array} \quad 32.0$$

8.6

$$\begin{array}{r} 33.0 / 2.4 \\ + 6.2 \\ \hline \end{array}$$

$$\begin{array}{r} 84 \\ + 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.3 \\ + 5.3 \\ \hline 8.6 \end{array} \quad 33.0$$

10.3

$$\begin{array}{r} 33.0 / 3.2 \\ + 7.1 \\ \hline \end{array}$$

$$\begin{array}{r} 101 \\ + 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ + 3.8 \\ \hline 8.3 \end{array} \quad 33.0$$

12.3

$$\begin{array}{r} 33.0 / 10.1 \\ + 2.2 \\ \hline \end{array}$$

$$\begin{array}{r} 119 \\ + 0.9 \\ \hline \end{array}$$

Sta	+	T	-	Grade
77				
	+55			
78				
	+			
	+73			
B.M.	5.36	97049		965.13
79				61.8
	+			
	+65			62.8
80				63.5
	+50			64.3
81				65.3
	+50			66.3
T.P.	7.70	97087	2.92	968.17

Gr. Rod

Lt

\$

Rt

Spt in 24' W OAK, 50' LT. 80+30

8.7

$$\frac{87}{00}$$

$$\frac{111}{24} / 22.2$$

7.7

$$\frac{77}{02}$$

$$\frac{101}{24} / 22.2$$

7.0

$$23.0 / \frac{9.0}{20.0}$$

$$\frac{70}{0.0}$$

$$\frac{84}{20.0} / 24.2$$

6.2

$$26.0 / \frac{6.7}{22.15}$$

$$\frac{56}{106}$$

$$\frac{49}{43} / 22.0$$

5.2

$$27.6 / \frac{4.9}{10.3}$$

$$\frac{43}{109}$$

$$\frac{28}{29} / 31.8$$

4.2

$$21.6 / \frac{3.9}{10.3}$$

$$\frac{32}{110}$$

$$\frac{0.6}{13.6} / 32.0$$

Sta	+	π	-	Grade
		975.87		
82				67.4
	+50			68.4
83				69.5
	+50			70.6
84				71.6
	+50			72.7
T.P	8.49	981.35	2.01	972.86
85				73.7
	+50			74.7
86				75.8
	+50			76.7
87				77.4
	+50			77.9

Gr. Rod

Lt

%

Rt

$$8.5 \quad 23.0 / \frac{5.0}{+3.5} \quad \frac{77}{+18} \quad \frac{63}{+22} / 31.9$$

$$7.5 \quad 28.0 / \frac{7.0}{+0.5} \quad \frac{69}{+06} \quad \frac{56}{+09} / 24.8$$

$$6.4 \quad 23.8 / \frac{8.0}{+0.9} \quad \frac{69}{+00} \quad \frac{104}{-99} / 27.0$$

$$5.3 \quad 23.0 / \frac{7.3}{+0.0} \quad \frac{56}{-03} \quad \frac{104}{-5.1} / 30.3$$

$$4.3 \quad 25.4 / \frac{5.6}{+0.7} \quad \frac{44}{+00} \quad \frac{48}{+13} / 26.0$$

$$3.2 \quad 27.2 / \frac{3.1}{+0.1} \quad \frac{30}{+0.2} \quad \frac{44}{+04} / 24.6$$

$$2.1 \quad 28.0 / \frac{7.2}{+0.5} \quad \frac{72}{+05} \quad \frac{45}{+22} / 39.0$$

$$6.7 \quad 29.4 / \frac{5.5}{+1.2} \quad \frac{60}{+07} \quad \frac{29}{+44} / 33.0$$

$$5.6 \quad 29.2 / \frac{4.5}{+1.1} \quad \frac{32}{+04} \quad \frac{36}{+20} / 31.0$$

$$4.7 \quad 28.8 / \frac{3.8}{+0.9} \quad \frac{40}{+07} \quad \frac{25}{+22} / 31.4$$

4.0

Sta	+	π	-	Grade
88				78.05
	+50			78.2
89				78.5
	+50			79.0
90				79.55
	+50			80.2
91				80.8
	+40			
	+			
92				
	+50			
93				

Gr. Rod

lt

g

Rt

Sta + 1 - Grade

93 +50

94

+50

95

+50

96

+50

97

+50

98

+

+70

Gr. Rod.

Lt.

E

Rt.

Sta	+	π	-	Grade
-----	---	-------	---	-------

99

+50

100

+50

101

+

+65

102

150

103

+47

104

Ger. Rod

Lt

E

Rt

Sta.	+	X	-	Grade	Ditch Grade	
					Lt.	Rt.

104	+50					
-----	-----	--	--	--	--	--

105						
-----	--	--	--	--	--	--

	+					
--	---	--	--	--	--	--

+46.64	= Co. Rd "G"			53.1		
--------	--------------	--	--	------	--	--

B.M.	1.51	959.76			953.25	
------	------	--------	--	--	--------	--

+70				52.8		
-----	--	--	--	------	--	--

+85				52.4		
-----	--	--	--	------	--	--

106				52.2		
-----	--	--	--	------	--	--

+50				51.6		
-----	--	--	--	------	--	--

107				51.2		
-----	--	--	--	------	--	--

+50				51.1		
-----	--	--	--	------	--	--

108			$\begin{array}{r} 10.10 \\ 37.0 \\ \hline \end{array}$	51.1	41.5	
-----	--	--	--	------	------	--

+50			$\begin{array}{r} 0.23 \\ 42.9 \\ \hline \end{array}$	51.1	41.5	
-----	--	--	---	------	------	--

Gr. Rod

Lt.

E

Rt.

Top. Mont. Hamilton + TH. # 96

2.5

$$240 \begin{array}{r} / 45 \\ - 3.0 \end{array}$$

$$25 \begin{array}{r} / 103 \end{array}$$

$$72 \begin{array}{r} / 29.1 \\ - 4.7 \end{array}$$

31

$$320 \begin{array}{r} / 24 \\ - 5.2 \end{array}$$

$$27 \begin{array}{r} / 06 \end{array}$$

$$92 \begin{array}{r} / 32.0 \\ - 6.1 \end{array}$$

3.5

$$330 \begin{array}{r} / 100 \\ - 6.5 \end{array}$$

$$44 \begin{array}{r} / 09 \end{array}$$

$$103 \begin{array}{r} / 33.0 \\ - 6.8 \end{array}$$

36

$$330 \begin{array}{r} / 105 \\ - 6.9 \end{array}$$

$$49 \begin{array}{r} / 13 \end{array}$$

$$106 \begin{array}{r} / 33.0 \\ - 7.0 \end{array}$$

36

$$330 \begin{array}{r} / 105 \\ - 6.9 \end{array}$$

$$51 \begin{array}{r} / 15 \end{array}$$

$$111 \begin{array}{r} / 32.0 \\ - 7.5 \end{array}$$

36

$$330 \begin{array}{r} / 92 \\ - 5.6 \end{array}$$

$$61 \begin{array}{r} / 15 \end{array}$$

$$126 \begin{array}{r} / 32.0 \\ - 7.0 \end{array}$$

Sta	+	π	-	Grade	Ditch Grade
		954.76			Lt. Rt.
109			$\frac{23.17}{46.1}$	51.1	41.5
	+50		$\frac{23.02}{36.9}$	51.1	41.5
110			$\frac{27.10}{39.0}$	51.1	41.5
110	+20			51.1	
	+50			51.1	46.5
	+75			51.1	46.6
111				51.1	46.7
T.P.	5.38	955.24	51.0		949.66
				51.1	
	+40			51.1	
	+50				46.8
112				51.1	
	+50			51.1	

Gr. Rod

Lt.

E

Rt.

$$3.6 \quad 33.0 / \begin{array}{r} 98 \\ -6.2 \end{array} \quad 52 \\ -1.5 \quad 110 / 33.0$$

$$3.6 \quad 33.0 / \begin{array}{r} 109 \\ -7.3 \end{array} \quad 52 \\ -1.6 \quad 95 / 33.0$$

$$3.6 \quad 33.0 / \begin{array}{r} 105 \\ -6.9 \end{array} \quad 51 \\ -1.5 \quad 83 / 29.1$$

$$3.6 \quad \quad \quad 51 \\ -1.5 \quad 67 / 24.3$$

$$3.6 \quad 31.3 / \begin{array}{r} 20 \\ 8.2 \end{array} \quad 28.9 / \begin{array}{r} 82 \\ -4.1 \end{array} \quad 52 \\ -1.6 \quad 72 / 53 / 31.8$$

$$3.6 \quad 35.9 / \begin{array}{r} 33 \\ 15.9 \end{array} \quad 26.7 / \begin{array}{r} 72 \\ -3.6 \end{array} \quad 52 \\ -1.6 \quad 114 / 78 / 33.0$$

$$3.6 / \begin{array}{r} 35 \\ 15.6 \end{array} \quad 22.8 / \begin{array}{r} 12 \\ -6.6 \end{array} \quad 52 \\ -1.6 \quad 113 / 77 / 33.0$$

$$3.7 \quad 31.5 / \begin{array}{r} 22 \\ 11.95 \end{array} \quad 26.1 / \begin{array}{r} 26 \\ -3.7 \end{array} \quad 53 \\ -1.4 \quad 12.5 / 36 / 33.0$$

$$3.7 \quad 26.7 / \begin{array}{r} 25 \\ -3.9 \end{array} \quad 53 \\ -1.4 \quad 12.3 / 34 / 33.0$$

$$3.9 \quad 33.0 / \begin{array}{r} 77 \\ -6.0 \end{array} \quad 50 \\ -1.1 \quad 42 / 21.7 / 26.4$$

Sta	+	π	-	Grade	
		953.04			
113				51.1	
I.P.	10.87	963.26	2.65		752.39
+					
B.M.			11.29		951.97
+60				51.3	
114				51.6	
+50				52.2	
115				53.1	
+50				54.1	
+83				54.8	
116					
+25				55.6	
I.P.	12.06	967.35	7.97		955.29
+					
+75				56.6	

Gr. Rod

Lt

Rt

Rt

$$\begin{array}{r}
 28.2 / \begin{array}{l} 3.3 \\ +1.6 \end{array} \\
 3.9
 \end{array}
 \qquad
 \begin{array}{r}
 4.3 \\
 -0.4
 \end{array}
 \qquad
 \begin{array}{r}
 59 \\
 12.00 / 23.0
 \end{array}$$

Spk. in T.P. Lt Sta 114

$$\begin{array}{r}
 23.0 / \begin{array}{l} 14.0 \\ +2.0 \end{array} \\
 10.0
 \end{array}
 \qquad
 \begin{array}{r}
 11.9 \\
 -0.1
 \end{array}
 \qquad
 \begin{array}{r}
 6.2 \\
 15.8 / 32.0
 \end{array}$$

$$\begin{array}{r}
 21.6 / \begin{array}{l} 13.9 \\ -2.2 \end{array} \\
 11.7
 \end{array}
 \qquad
 \begin{array}{r}
 11.6 \\
 +0.1
 \end{array}
 \qquad
 \begin{array}{r}
 7.9 \\
 13.9 / 32.0
 \end{array}$$

$$\begin{array}{r}
 27.6 / \begin{array}{l} 10.8 \\ +0.9 \end{array} \\
 11.1
 \end{array}
 \qquad
 \begin{array}{r}
 10.5 \\
 +0.3
 \end{array}
 \qquad
 \begin{array}{r}
 8.9 \\
 12.2 / 31.4
 \end{array}$$

$$\begin{array}{r}
 33.0 / \begin{array}{l} 3.8 \\ +6.4 \end{array} \\
 10.2
 \end{array}
 \qquad
 \begin{array}{r}
 10.2 \\
 +0.2
 \end{array}
 \qquad
 \begin{array}{r}
 1.9 \\
 15.3 / 32.0
 \end{array}$$

$$\begin{array}{r}
 31.2 / \begin{array}{l} 7.1 \\ +2.1 \end{array} \\
 9.2
 \end{array}
 \qquad
 \begin{array}{r}
 9.3 \\
 -0.1
 \end{array}
 \qquad
 \begin{array}{r}
 10.1 \\
 12.1 / 25.2
 \end{array}$$

$$\begin{array}{r}
 25.6 / \begin{array}{l} 9.2 \\ 12.1 \end{array} \\
 8.3
 \end{array}
 \qquad
 \begin{array}{r}
 8.7 \\
 -0.2
 \end{array}
 \qquad
 \begin{array}{r}
 11.3 \\
 -2.8 / 23.4
 \end{array}$$

$$\begin{array}{r}
 7.7
 \end{array}
 \qquad
 \begin{array}{r}
 7.6 \\
 -0.1
 \end{array}
 \qquad
 \begin{array}{r}
 8.5 \\
 11.2 / 25.4
 \end{array}$$

$$\begin{array}{r}
 30.2 / \begin{array}{l} 9.2 \\ +1.6 \end{array} \\
 10.8
 \end{array}
 \qquad
 \begin{array}{r}
 10.2 \\
 +0.6
 \end{array}
 \qquad
 \begin{array}{r}
 5.2 \\
 15.0 / 33.0
 \end{array}$$

Sta	+	π	-	Grade
		96735		
117				57.1
	+50			58.1
118				59.1
	+50			60.1
119				60.9
	+50			61.5
120				61.7
	+50			61.6
121				61.2
	+50			60.5
122				59.7
	+50			58.8
T.P.	2.94	96132	8.97	958.58

Gr. Rod.

Lt

R

Rt

$$10.3 \quad \frac{29.0}{+1.0} \begin{array}{r} 9.3 \\ 29.0 \end{array} \quad \frac{9.6}{+0.7} \begin{array}{r} 9.6 \\ 10.7 \end{array} \quad \frac{5.2}{+5.1} \begin{array}{r} 5.2 \\ 15.1 \end{array} / 33.0$$

$$9.9 \quad \frac{26.0}{+2.5} \begin{array}{r} 9.8 \\ 26.0 \end{array} \quad \frac{8.7}{+0.6} \begin{array}{r} 8.7 \\ 10.6 \end{array} \quad \frac{7.2}{+2.1} \begin{array}{r} 7.2 \\ 21.1 \end{array} / 31.2$$

$$8.3 \quad \frac{26.4}{+2.1} \begin{array}{r} 8.6 \\ 26.4 \end{array} \quad \frac{7.5}{+0.8} \begin{array}{r} 7.5 \\ 10.8 \end{array} \quad \frac{5.1}{+2.2} \begin{array}{r} 5.1 \\ 22.2 \end{array} / 33.0$$

$$7.3 \quad \frac{30.0}{+1.5} \begin{array}{r} 5.8 \\ 30.0 \end{array} \quad \frac{6.5}{+0.8} \begin{array}{r} 6.5 \\ 10.8 \end{array} \quad \frac{4.8}{+2.5} \begin{array}{r} 4.8 \\ 25.5 \end{array} / 32.0$$

$$6.5 \quad \frac{27.8}{+0.7} \begin{array}{r} 6.1 \\ 27.8 \end{array} \quad \frac{5.9}{+0.6} \begin{array}{r} 5.9 \\ 10.6 \end{array} \quad \frac{5.5}{+1.0} \begin{array}{r} 5.5 \\ 11.0 \end{array} / 29.0$$

$$5.9 \quad \frac{32.8}{+2.9} \begin{array}{r} 3.0 \\ 32.8 \end{array} \quad \frac{5.3}{+0.6} \begin{array}{r} 5.3 \\ 10.6 \end{array} \quad \frac{6.8}{+2.1} \begin{array}{r} 6.8 \\ 21.1 \end{array} / 25.2$$

$$5.7 \quad \frac{33.0}{+3.6} \begin{array}{r} 2.1 \\ 33.0 \end{array} \quad \frac{4.8}{+0.7} \begin{array}{r} 4.8 \\ 10.7 \end{array} \quad \frac{3.1}{+2.6} \begin{array}{r} 3.1 \\ 26.6 \end{array} / 32.2$$

$$5.8 \quad \frac{30.6}{+1.8} \begin{array}{r} 4.0 \\ 30.6 \end{array} \quad \frac{4.8}{+1.0} \begin{array}{r} 4.8 \\ 11.0 \end{array} \quad \frac{2.5}{+3.8} \begin{array}{r} 2.5 \\ 38.3 \end{array} / 33.0$$

$$6.2 \quad \frac{30.8}{+1.8} \begin{array}{r} 4.4 \\ 30.8 \end{array} \quad \frac{5.4}{+0.8} \begin{array}{r} 5.4 \\ 10.8 \end{array} \quad \frac{4.3}{+1.9} \begin{array}{r} 4.3 \\ 19.9 \end{array} / 30.8$$

$$6.9 \quad \frac{33.0}{+3.0} \begin{array}{r} 3.9 \\ 33.0 \end{array} \quad \frac{6.1}{+0.8} \begin{array}{r} 6.1 \\ 10.8 \end{array} \quad \frac{3.7}{+2.2} \begin{array}{r} 3.7 \\ 22.2 \end{array} / 31.4$$

$$7.7 \quad \frac{23.0}{+0.0} \begin{array}{r} 10.0 \\ 23.0 \end{array} \quad \frac{7.6}{+0.6} \begin{array}{r} 7.6 \\ 10.6 \end{array} \quad \frac{8.9}{+2.2} \begin{array}{r} 8.9 \\ 22.2 \end{array} / 24.6$$

$$8.6 \quad \frac{31.5}{+5.5} \begin{array}{r} 14.1 \\ 31.5 \end{array} \quad \frac{8.2}{+0.4} \begin{array}{r} 8.2 \\ 10.4 \end{array} \quad \frac{13.8}{+5.2} \begin{array}{r} 13.8 \\ 5.2 \end{array} / 30.6$$

E sto 123

Sta	+	π	-	Grade	Ditch Gr.
		961.32			Rt. L.
123				58.0	
	+50			57.2	
124				56.4	51.8
	+33			55.9	51.7
	+66			55.6	51.6
125				55.1	51.5
	+50			54.5	51.4
126				53.8	51.3
	+50			53.1	51.2
127				52.3	51.1
T.P.	405	957.00	8.40		952.92
	+50			51.3	
128				50.3	51.5

Gr. Rod

L₁

R

R₁

$$3.3 \quad 31.8 / \begin{array}{r} 8.9 \\ -5.6 \end{array} \quad \begin{array}{r} 3.3 \\ +0.4 \end{array} \quad \begin{array}{r} 6.8 \\ -2.5 \end{array} / 25.5$$

$$4.1 \quad 29.7 / \begin{array}{r} 7.0 \\ -4.7 \end{array} \quad \begin{array}{r} 3.9 \\ +0.2 \end{array} \quad \begin{array}{r} 6.9 \\ -2.8 \end{array} / 23.4$$

$$4.9 \quad 25.8 / \begin{array}{r} 8.5 \\ -3.6 \end{array} \quad \begin{array}{r} 4.8 \\ +0.1 \end{array} \quad \begin{array}{r} 8.5 \\ -3.6 \end{array} / 25.8$$

$$5.9 \quad \begin{array}{r} 45 \\ 3.2 \end{array} \quad \begin{array}{r} 5.0 \\ +0.4 \end{array} \quad \begin{array}{r} 7.0 \\ 10.4 \end{array} / 23.8$$

$$+50 \quad \begin{array}{r} 100.42 \\ 25.8 \end{array}$$

$$5.7 \quad 29.8 / \begin{array}{r} 4.3 \\ -1.4 \end{array} \quad \begin{array}{r} 5.2 \\ +0.5 \end{array} \quad \begin{array}{r} 1.8 \\ 13.9 \end{array} / 23.0$$

$$6.2 \quad 31.8 / \begin{array}{r} 3.8 \\ +2.4 \end{array} \quad \begin{array}{r} 100.60 \\ 2.51 \end{array} \quad \begin{array}{r} 5.5 \\ +0.7 \end{array} \quad \begin{array}{r} 2.2 \\ 19.0 \end{array} / 33.0$$

$$6.5 \quad 33.0 / \begin{array}{r} 3.5 \\ +3.3 \end{array} \quad \begin{array}{r} 100.66 \\ 29.4 \end{array} \quad \begin{array}{r} 6.0 \\ +0.8 \end{array} \quad \begin{array}{r} 2.0 \\ 14.8 \end{array} / 33.0$$

$$7.5 \quad 38.0 / \begin{array}{r} 2.4 \\ +2.1 \end{array} \quad \begin{array}{r} 100.79 \\ 30.5 \end{array} \quad \begin{array}{r} 6.5 \\ +1.0 \end{array} \quad \begin{array}{r} 2.5 \\ 15.0 \end{array} / 33.0$$

$$8.2 \quad 32.0 / \begin{array}{r} 2.8 \\ +2.3 \end{array} \quad \begin{array}{r} 101.77 \\ 27.8 \end{array} \quad \begin{array}{r} 7.3 \\ +0.9 \end{array} \quad \begin{array}{r} 5.3 \\ 17.9 \end{array} / 33.0$$

$$9.0 \quad 31.8 / \begin{array}{r} 6.6 \\ +2.4 \end{array} \quad \begin{array}{r} 104.1 \\ 17.9 \end{array} \quad \begin{array}{r} 8.4 \\ +0.6 \end{array} \quad \begin{array}{r} 7.0 \\ 12.0 \end{array} / 31.0$$

$$5.7 \quad 27.4 / \begin{array}{r} 5.5 \\ +0.2 \end{array} \quad \begin{array}{r} 5.6 \\ +0.1 \end{array} \quad \begin{array}{r} 6.5 \\ 10.9 \end{array} / 29.7$$

$$6.7 \quad 27.8 / \begin{array}{r} 6.3 \\ +0.4 \end{array} \quad \begin{array}{r} 6.4 \\ +0.1 \end{array} \quad \begin{array}{r} 8.7 \\ 10.0 \end{array} / 29.0$$

Sta.	+	x	-	Grade	Lt.
		937.00			
28	+50			49.3	49.4
29				48.4	
	+50			47.8	
T.P.	9.07	950.72	10.35		846.65
30				47.4	
	+50			47.3	
31				47.3	
	+50			47.3	
B.M.	3.35	949.33	4.59		946.13 945.95
32				47.3	
	+50			47.3	
33				47.3	
	+50			47.3	
34				47.3	
T.P.	6.86	952.45	3.74		945.59

Gr. Rod

LH

R

RH

$$7.7 \quad 30.8 / \frac{58}{1.9}$$

$$\frac{76}{199}$$

$$\frac{27}{+30} / 33.0$$

$$8.6 \quad 33.0 / \frac{47}{+37}$$

$$\frac{83}{+0.3}$$

$$\frac{91}{+95} / 33.0$$

$$9.2 \quad 25.8 / \frac{98}{21.4}$$

$$\frac{95}{-0.3}$$

$$\frac{101}{21.1} / 25.2$$

$$3.3 \quad 24.6 / \frac{45}{3.2}$$

$$\frac{41}{-0.8}$$

$$\frac{7.7}{42} / 28.2$$

$$3.4 \quad 28.8 / \frac{79}{-76}$$

$$\frac{49}{-1.5}$$

$$\frac{91}{-5.7} / 32.1$$

$$3.4 \quad 27.6 / \frac{76}{-92}$$

$$\frac{59}{-2.0}$$

$$\frac{103}{-7.1} / 33.0$$

$$3.4 \quad 28.9 / \frac{79}{-45}$$

$$\frac{57}{-2.3}$$

$$\frac{11.4}{-8.0} / 33.0$$

Spt in str 104 Rl. 129+50

$$2.0 \quad 30.0 / \frac{81}{-61}$$

$$\frac{18}{-25}$$

$$\frac{10.1}{-8.1} / 33.0$$

$$2.0 \quad 32.4 / \frac{75}{-58}$$

$$\frac{50}{-30}$$

$$\frac{10.0}{-9.0} / 33.0$$

$$2.0 \quad 27 / \frac{12}{-0.9}$$

$$\frac{15}{-25}$$

$$\frac{55}{-35} / 22.4$$

$$2.0 \quad 328 / \frac{10.9}{+2.9}$$

$$\frac{40}{-2.0}$$

$$\frac{3.5}{21.02} / 22.4$$

$$2.0 \quad 29.0 / \frac{9.0}{21.00}$$

$$\frac{27}{-1.7}$$

$$\frac{28}{21.02} / 25.4$$

Sta	+	X	-	Grade
		952.45		
134	+50			47.3
135				47.3
	+50			47.3
136				47.3
	+50			47.3
137				47.5
	+50			47.8
138				48.3
T.P.	11.85	958.68	5.62	946.83
	+50			49.0
139				49.6
	+50			50.2
140				50.9

Gr. Rod

Lt

R

Rt

$$5.2 \quad 31.2 / \begin{array}{r} 10.6 \\ -5.4 \end{array}$$

$$\begin{array}{r} 65 \\ -13 \end{array}$$

$$\begin{array}{r} 47 \\ +0.5 \end{array} / 28.0$$

$$5.2 \quad 33.0 / \begin{array}{r} 10.6 \\ -7.4 \end{array}$$

$$\begin{array}{r} 61 \\ -0.9 \end{array}$$

$$\begin{array}{r} 43 \\ +0.9 \end{array} / 29.8$$

$$5.2 \quad 33.0 / \begin{array}{r} 10.7 \\ -7.5 \end{array}$$

$$\begin{array}{r} 60 \\ -0.8 \end{array}$$

$$\begin{array}{r} 60 \\ +0.2 \end{array} / 25.4$$

$$5.2 \quad 33.0 / \begin{array}{r} 10.8 \\ -7.6 \end{array}$$

$$\begin{array}{r} 59 \\ -0.2 \end{array}$$

$$\begin{array}{r} 64 \\ +0.8 \end{array} / 24.6$$

$$5.2 \quad 33.0 / \begin{array}{r} 11.8 \\ -6.6 \end{array}$$

$$\begin{array}{r} 51 \\ +0.1 \end{array}$$

$$\begin{array}{r} 55 \\ +0.17 \end{array} / 26.4$$

$$5.0 \quad 27.9 / \begin{array}{r} 7.3 \\ -4.2 \end{array}$$

$$\begin{array}{r} 47 \\ +0.3 \end{array}$$

$$\begin{array}{r} 49 \\ +0.1 \end{array} / 27.2$$

$$4.7 \quad 24.7 / \begin{array}{r} 8.0 \\ -3.3 \end{array}$$

$$\begin{array}{r} 43 \\ +0.5 \end{array}$$

$$\begin{array}{r} 3.8 \\ +0.9 \end{array} / 28.5$$

$$4.2 \quad 19.2 / \begin{array}{r} 5.6 \\ -1.4 \end{array}$$

$$\begin{array}{r} 27 \\ +0.3 \end{array}$$

$$\begin{array}{r} 38 \\ +0.4 \end{array} / 27.8$$

Nail in TP. Lt 138+

$$9.7 \quad 23.1 / \begin{array}{r} 12.4 \\ -2.7 \end{array}$$

$$\begin{array}{r} 96 \\ +0.1 \end{array}$$

$$\begin{array}{r} 105 \\ +0.12 \end{array} / 25.4$$

$$9.1 \quad 25.0 / \begin{array}{r} 10.1 \\ +0.10 \end{array}$$

$$\begin{array}{r} 88 \\ +0.3 \end{array}$$

$$\begin{array}{r} 5.7 \\ +0.2 \end{array} / 27.4$$

$$8.5 \quad 30.8 / \begin{array}{r} 8.5 \\ +1.9 \end{array}$$

$$\begin{array}{r} 81 \\ +0.4 \end{array}$$

$$\begin{array}{r} 84 \\ +0.1 \end{array} / 27.2$$

$$7.8 \quad 33.0 / \begin{array}{r} 2.9 \\ +4.9 \end{array}$$

$$\begin{array}{r} 77 \\ +0.1 \end{array}$$

$$\begin{array}{r} 7.0 \\ +0.7 \end{array} / 28.6$$

Sta	+	Σ	-	Grade
		958.68		
140	+50			51.4
141				51.8
	+50			51.9
142				51.8
	+50			51.6
143				51.1
	+50			50.4
144				49.5
	+50			48.4
T.P.	1.26	952.36	7.58	951.10
145				47.0
	+50			45.5
146				43.7

Gr Rod.

Lt.

F

Rt.

$$7.2 \quad \begin{array}{r} 33.0 \\ + 0.5 \\ \hline 33.5 \end{array} \quad \begin{array}{r} 7.3 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 6.4 \\ + 0.9 \\ \hline 7.3 \end{array} / 25.8$$

$$6.9 \quad \begin{array}{r} 33.0 \\ + 1.4 \\ \hline 34.4 \end{array} \quad \begin{array}{r} 6.9 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 4.2 \\ + 2.7 \\ \hline 6.9 \end{array} / 32.4$$

$$6.8 \quad \begin{array}{r} 28.0 \\ + 0.3 \\ \hline 28.3 \end{array} \quad \begin{array}{r} 6.4 \\ + 0.4 \\ \hline \end{array} \quad \begin{array}{r} 3.7 \\ + 3.1 \\ \hline 6.8 \end{array} / 31.0$$

$$6.9 \quad \begin{array}{r} 27.4 \\ + 0.2 \\ \hline 27.6 \end{array} \quad \begin{array}{r} 6.4 \\ + 0.3 \\ \hline \end{array} \quad \begin{array}{r} 5.2 \\ + 1.7 \\ \hline 6.9 \end{array} / 29.8$$

$$7.1 \quad \begin{array}{r} 24.6 \\ + 8.3 \\ \hline 32.9 \end{array} \quad \begin{array}{r} 6.7 \\ + 0.2 \\ \hline \end{array} \quad \begin{array}{r} 6.7 \\ + 0.9 \\ \hline 7.6 \end{array} / 27.8$$

$$7.6 \quad \begin{array}{r} 23.4 \\ + 9.4 \\ \hline 32.8 \end{array} \quad \begin{array}{r} 7.1 \\ + 0.5 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ + 2.14 \\ \hline 10.44 \end{array} / 25.8$$

$$8.3 \quad \begin{array}{r} 24.2 \\ + 9.7 \\ \hline 33.9 \end{array} \quad \begin{array}{r} 7.7 \\ + 0.6 \\ \hline \end{array} \quad \begin{array}{r} 10.3 \\ + 2.00 \\ \hline 12.3 \end{array} / 23.0$$

$$9.2 \quad \begin{array}{r} 26.4 \\ + 9.5 \\ \hline 35.9 \end{array} \quad \begin{array}{r} 8.9 \\ + 0.3 \\ \hline \end{array} \quad \begin{array}{r} 12.3 \\ + 3.0 \\ \hline 15.3 \end{array} / 24.0$$

$$10.3 \quad \begin{array}{r} 31.8 \\ + 2.9 \\ \hline 34.7 \end{array} \quad \begin{array}{r} 10.1 \\ + 0.2 \\ \hline \end{array} \quad \begin{array}{r} 12.8 \\ + 2.6 \\ \hline 15.4 \end{array} / 22.8$$

Nail in T.P.L.H. + 50

$$5.4 \quad \begin{array}{r} 5.1 \\ + 0.3 \\ \hline \end{array} \quad \begin{array}{r} 5.5 \\ + 0.2 \\ \hline 5.7 \end{array} / 27.4$$

$$6.9 \quad \begin{array}{r} 36.1 \\ + 0.2 \\ \hline 36.3 \end{array} \quad \begin{array}{r} 6.4 \\ + 0.5 \\ \hline \end{array} \quad \begin{array}{r} 2.8 \\ + 3.1 \\ \hline 5.9 \end{array} / 33.0$$

$$8.7 \quad \begin{array}{r} 39.1 \\ + 8.7 \\ \hline 47.8 \end{array} \quad \begin{array}{r} 7.9 \\ + 0.8 \\ \hline \end{array} \quad \begin{array}{r} 2.4 \\ + 4.3 \\ \hline 6.7 \end{array} / 33.0$$

Sta	+	π	-	Grade	
		752.36			
146	+50			41.8	
147				39.9	
	+50			38.0	
T.P.	4.74	743.60	13.50		748.84
148				36.1	
	+50			34.2	
149				32.3	
	(13.14)	(745.12)			(727.95)
	+50			30.2	
T.P.	1.89	731.57	13.62		729.98
150				28.1	
	+50			25.7	
151				23.7	
	+50			21.3	
152				18.9	
T.P.	0.28	718.72	13.43		915.44

Ga. Rod.

Lt

R

Rt

$$10.6 \quad 40.0 / \frac{1.3}{+9.3}$$

$$\frac{9.6}{+1.0}$$

$$\frac{3.5}{+7.1} / 33.0$$

$$12.3 \quad 40.0 / \frac{3.0}{+9.3}$$

$$\frac{11.5}{+9.8}$$

$$\frac{5.9}{+6.4} / 33.0$$

$$14.2 \quad 38.0 / \frac{6.2}{+8.0}$$

$$\frac{13.5}{+6.7}$$

$$\frac{9.5}{+9.7} / 33.0$$

$$7.5 \quad 36.8 / \frac{0.3}{+7.2}$$

$$\frac{7.1}{+0.9}$$

$$\frac{4.1}{+5.4} / 33.0$$

$$9.4 \quad 36.4 / \frac{2.5}{+6.9}$$

$$\frac{9.6}{+0.2}$$

$$\frac{7.1}{+5.3} / 33.0$$

$$11.3 \quad 41.0 / \frac{1.3}{+10.0}$$

$$\frac{11.3}{0.0}$$

$$\frac{9.2}{+2.0} / 31.0$$

$$(14.9) \quad 13.4 \quad (43.0) / \frac{3.6}{+11.9}$$

$$\frac{13.6}{-0.2}$$

$$\frac{12.1}{+1.1} / 29.6$$

$$(17.0) \quad 2.5 \quad (44.0) / \frac{5.0}{+12.0}$$

$$\frac{4.2}{-0.4}$$

$$\frac{1.5}{+3.5} / 32.0$$

$$(19.2) \quad 6.0 \quad (49.9) / \frac{3.3}{+13.9}$$

$$\frac{6.7}{-0.7}$$

$$\frac{3.3}{+2.8} / 32.6$$

$$(21.4) \quad 2.2 \quad (50.2) / \frac{7.6}{+16.8}$$

$$\frac{9.1}{-0.7}$$

$$\frac{4.6}{+9.6} / 33.0$$

$$(23.8) \quad 10.6 \quad (53.3) / \frac{5.6}{+18.2}$$

$$\frac{11.3}{-0.7}$$

$$\frac{9.6}{+9.0} / 31.0$$

$$(26.2) \quad 13.0 \quad (52.3) / \frac{8.7}{+17.5}$$

$$\frac{13.4}{-0.4}$$

$$\frac{12.7}{+9.3} / 28.2$$

Sta	+	π	-	Grade	
		918.72			
152	+36			17.9	
			10.65	908.07	908.19 ←
	2.56	921.12			918.52
	+63			15.9	
B.M.					
153				14.1	
	+26			12.8	
	+69			11.0	
T.P.	3.07	912.79	11.40		909.72
154				09.3	
	+42			07.9	
	+				
T.P.	0.36	905.76	7.37		905.42
155				04.9	
	+50			03.0	
T.P.	0.10	901.35	4.51		901.25
156				901.4	
	+50			899.9	

Gr. Rod

Lt

E

Rt

0.8

 $\frac{1.1}{}$ $\frac{2.0}{2.0} / 28.0$

From sta 52

5.2

 $\frac{38.5}{+53}$

Top Conc. Stop N End So. Ent Ho. 140' Rt 152+63

7.0

 $\frac{35.0}{+6.0}$ $\frac{6.9}{+0.1}$ $\frac{12.0}{-5.0} / 25.8$

P.3

 $\frac{34.0}{+5.3}$ $\frac{8.0}{+0.3}$ $\frac{13.5}{-5.2} / 27.0$

10.1

 $\frac{33.5}{+5.0}$ $\frac{9.7}{+0.4}$ $\frac{19.9}{-9.8} / 44.4$

3.3

 $\frac{28.4}{+1.6}$ $\frac{3.1}{+0.4}$ $\frac{14.5}{-11.0} / 48.0$

5.4

 $\frac{27.0}{-3.7}$ $\frac{4.9}{+0.5}$ $\frac{18.5}{-19.1} / 50.0$

0.9

 $\frac{35.6}{-6.2}$ $\frac{0.7}{+0.3}$ $\frac{14.4}{-12.5} / 50.0$

2.8

 $\frac{35.4}{-6.5}$ $\frac{2.5}{+0.3}$ $\frac{17.3}{-14.5} / 50.0$

0.0

 $\frac{39.0}{-8.0}$ $\frac{0.2}{+0.3}$ $\frac{14.9}{-14.4} / 50.0$

1.5

 $\frac{45.6}{-10.2}$ $\frac{2.1}{+0.6}$ $\frac{14.6}{-13.1} / 50.0$

Sta	+	π	-	Grade
		901.35		
157				98.7
	+50			97.6
158				96.8
B.M.	490	701.12	5.13	896.22
	+50			96.2
159				95.7
	+50			95.5
	+80			95.5
160				95.6
	+15			95.6
	+50			95.6
161				95.7
	+50			95.8

143

14.9

15.0

15.2

5.2

$$\begin{array}{r} 84 \\ 33 \\ \hline 51 \end{array}$$

33

54

$$\begin{array}{r} 309 \\ 48.3 \\ \hline 53.2 \end{array}$$

Gr Red

Lt

R

Rt

2.7

$$\begin{array}{r} 45.0/13.0 \\ -103 \end{array}$$

$$\begin{array}{r} 36 \\ -09 \end{array}$$

$$\begin{array}{r} 14.5/54.0 \\ -11.8 \end{array}$$

3.8

$$\begin{array}{r} 48.5/13.3 \\ -95 \end{array}$$

$$\begin{array}{r} 46 \\ -08 \end{array}$$

$$\begin{array}{r} 14.3/48.0 \\ -11.0 \end{array}$$

4.6

$$\begin{array}{r} 39.7/12.7 \\ -8.9 \end{array}$$

$$\begin{array}{r} 51 \\ -05 \end{array}$$

$$\begin{array}{r} 14.7/45.2 \\ -10.1 \end{array}$$

High Ph on Mant.

4.7

$$\begin{array}{r} 26.4/10.6 \\ -5.7 \end{array}$$

$$\begin{array}{r} 51 \\ -03 \end{array}$$

5.4

$$\begin{array}{r} 21.9/8.6 \\ -3.2 \end{array}$$

$$\begin{array}{r} 52 \\ +02 \end{array}$$

$$\begin{array}{r} 10.1/24.9 \\ -4.7 \end{array}$$

5.6

$$\begin{array}{r} 24.8/6.7 \\ 20.9 \end{array}$$

$$\begin{array}{r} 51 \\ +05 \end{array}$$

5.6

$$\begin{array}{r} 27.0/5.6 \\ +90 \end{array}$$

$$\begin{array}{r} 50 \\ +06 \end{array}$$

$$\begin{array}{r} 7.6/23.0 \\ 20.0 \end{array}$$

5.5

$$\begin{array}{r} 29.7/4.4 \\ +1.1 \end{array}$$

$$\begin{array}{r} 50 \\ +05 \end{array}$$

$$\begin{array}{r} 5.6/26.8 \\ 20.1 \end{array}$$

5.5

$$\begin{array}{r} 32.0/3.0 \\ +2.5 \end{array}$$

$$\begin{array}{r} 48 \\ +07 \end{array}$$

$$\begin{array}{r} 0.8/36.4 \\ +4.7 \end{array}$$

5.5

5.4

$$\begin{array}{r} 29.8/4.0 \\ +1.4 \end{array}$$

$$\begin{array}{r} 47 \\ +07 \end{array}$$

$$\begin{array}{r} 0.5/36.8 \\ +4.9 \end{array}$$

5.3

$$\begin{array}{r} 28.6/4.5 \\ +0.8 \end{array}$$

$$\begin{array}{r} 47 \\ +06 \end{array}$$

$$\begin{array}{r} 2.2/33.2 \\ +3.1 \end{array}$$

Sta	+	Σ	-	Grade
		901.12		
162				96.0
	+50			96.4
163				96.9
T.P.	8.74	907.45	2.41	898.71
	+50			97.7
164				98.6
	+50			899.8
165				901.1
	+50			02.7
166				04.3
T.P.	12.74	917.56	2.63	904.82
	+50			06.9
167				07.6
	+50			07.1

Ditch = 2'
 R₁₀₀ = 23'
 C₁₀₀ = 27'

Fill 2' = 15'

Gr Rod	Lt	E	Rt
5.1	$2.78 / \frac{4.7}{+0.4}$	$\frac{48}{+0.3}$	$\frac{4.7}{+0.4} / 2.78$
4.7	$2.76 / \frac{4.4}{+0.3}$	$\frac{47}{+0.0}$	$\frac{5.7}{+0.10} / 2.50$
4.2	$2.73 / \frac{4.1}{+0.1}$	$\frac{43}{-0.1}$	$\frac{5.6}{+0.06} / 2.42$
3.8	$26.4 / \frac{10.1}{+0.12}$	$\frac{10.0}{-0.2}$	$\frac{11.8}{+0.00} / 2.30$
8.9	$27.0 / \frac{8.9}{+0.0}$	$\frac{8.9}{0.0}$	$\frac{10.9}{+0.05} / 2.40$
7.7	$31.4 / \frac{5.5}{+0.2}$	$\frac{7.7}{+0.0}$	$\frac{7.4}{+0.3} / 2.76$
6.4	$33.0 / \frac{3.4}{+0.0}$	$\frac{6.4}{+0.2}$	$\frac{6.4}{+0.0} / 2.70$
4.2	$31.0 / \frac{2.8}{+0.0}$	$\frac{4.5}{+0.3}$	$\frac{6.7}{+0.1} / 2.32$
3.2	$30.0 / \frac{1.6}{+0.6}$	$\frac{2.6}{+0.6}$	$\frac{5.1}{+0.2} / 2.32$
2 st 166			
11.7	$32.0 / \frac{9.0}{+0.7}$	$\frac{10.4}{+0.3}$	$\frac{11.9}{+0.15} / 2.46$
100	$33.0 / \frac{6.0}{+0.8}$	$\frac{8.3}{+0.7}$	$\frac{7.5}{+0.5} / 32.0$
8.5	$32.8 / \frac{5.0}{+0.9}$	$\frac{6.5}{+0.0}$	$\frac{7.1}{+0.4} / 2.98$

Sta	+	X	-	Grade	
		917.56			
168				10.5	
	+50			11.7	
169				12.6	
	+30			13.4	
T.P.	4.94	920.06	2.44	915.12	
170				14.0	
	+50			14.4	
171				14.6	
B.M.				0	918.60
	+35			14.7	
	+50			14.7	
172				14.8	
T.R	2.26	919.46	2.86	917.20	
	+50			15.0	

$D_{1.25} = 2'$
 $R_{2.0} = 23'$ Fill = 2.1-15'
 $Cut_{00} = 27'$

Gr. Rod

Lt

Rt

Rt

7.1 $31.6 / \begin{smallmatrix} 4.8 \\ +2.3 \end{smallmatrix}$

$\begin{smallmatrix} 5.6 \\ +1.5 \end{smallmatrix}$

$\begin{smallmatrix} 6.3 \\ +0.8 \end{smallmatrix} / 28.6$

5.9 $32.0 / \begin{smallmatrix} 5.4 \\ +2.5 \end{smallmatrix}$

$\begin{smallmatrix} 4.6 \\ +1.5 \end{smallmatrix}$

$\begin{smallmatrix} 6.4 \\ +1.5 \end{smallmatrix} / 26.0$

5.0 $34.9 / \begin{smallmatrix} 1.3 \\ +2.7 \end{smallmatrix}$

$\begin{smallmatrix} 3.5 \\ +1.5 \end{smallmatrix}$

$\begin{smallmatrix} 6.1 \\ +0.9 \end{smallmatrix} / 29.8$

4.2 $36.6 / \begin{smallmatrix} 10.6 \\ +9.8 \end{smallmatrix}$

$\begin{smallmatrix} 2.4 \\ +1.9 \end{smallmatrix}$

$\begin{smallmatrix} 9.0 \\ +0.2 \end{smallmatrix} / 27.4$

6.1 $37.4 / \begin{smallmatrix} 10.9 \\ +5.2 \end{smallmatrix}$

$\begin{smallmatrix} 4.6 \\ +1.5 \end{smallmatrix}$

$\begin{smallmatrix} 5.1 \\ +1.0 \end{smallmatrix} / 29.0$

3.7 $35.8 / \begin{smallmatrix} 1.3 \\ +4.4 \end{smallmatrix}$

$\begin{smallmatrix} 4.7 \\ +1.0 \end{smallmatrix}$

$\begin{smallmatrix} 5.3 \\ +0.4 \end{smallmatrix} / 27.8$

5.5 $33.0 / \begin{smallmatrix} 2.5 \\ +3.0 \end{smallmatrix}$

$\begin{smallmatrix} 5.2 \\ +0.3 \end{smallmatrix}$

$\begin{smallmatrix} 7.5 \\ +0.0 \end{smallmatrix} / 23.0$

5 pk in Root of Coll. 70' Ld 171

5.4

5.4 $30.4 / \begin{smallmatrix} 3.7 \\ +1.7 \end{smallmatrix}$

$\begin{smallmatrix} 5.7 \\ -0.3 \end{smallmatrix}$

$\begin{smallmatrix} 7.4 \\ +0.0 \end{smallmatrix} / 19.5$

4.3 $29.0 / \begin{smallmatrix} 4.3 \\ +1.0 \end{smallmatrix}$

$\begin{smallmatrix} 6.0 \\ -0.7 \end{smallmatrix}$

$\begin{smallmatrix} 7.8 \\ +0.0 \end{smallmatrix} / 20.6$

Nail in PP

4.5 $30.6 / \begin{smallmatrix} 2.7 \\ +1.8 \end{smallmatrix}$

$\begin{smallmatrix} 5.9 \\ -1.4 \end{smallmatrix}$

$\begin{smallmatrix} 7.7 \\ -3.2 \end{smallmatrix} / 21.4$

Sta	+	X	-	Grade
		919.46		

173				15.3
-----	--	--	--	------

+50				15.7
-----	--	--	--	------

124				16.1
-----	--	--	--	------

+50				16.7
-----	--	--	--	------

175				17.2
-----	--	--	--	------

+50				17.9
-----	--	--	--	------

176				18.6
-----	--	--	--	------

T.P.	13.67	930.01	3.12	916.34
------	-------	--------	------	--------

+50				19.3
-----	--	--	--	------

177				20.0
-----	--	--	--	------

+50				20.7
-----	--	--	--	------

178				21.4
-----	--	--	--	------

T.P.	10.43	932.47	7.97	922.04
------	-------	--------	------	--------

2' 1.60 15' Top.
 103.00 = 23'
 104.00 = 27'

Gr. Rod

Lt

R

Rt

$$4.2 \quad 31.2 / \frac{2.1}{+2.1} \quad \frac{57}{1.5} \quad \frac{67}{+2.5 / 20.0}$$

$$3.8 \quad 32.0 / \frac{1.5}{+2.5} \quad \frac{57}{-1.9} \quad \frac{72}{-3.4 / 21.8}$$

$$3.4 \quad 31.6 / \frac{1.1}{+2.3} \quad \frac{57}{-2.3} \quad \frac{79}{-4.5 / 24.0}$$

$$2.8 \quad 28.4 / \frac{2.1}{+0.7} \quad \frac{57}{-3.9} \quad \frac{69}{-4.1 / 23.2}$$

$$2.3 \quad 27.0 / \frac{2.3}{+0.0} \quad \frac{54}{-3.1} \quad \frac{65}{-2.7 / 23.9}$$

$$1.6 \quad 25.8 / \frac{2.2}{+0.14} \quad \frac{44}{-2.8} \quad \frac{53}{-3.7 / 22.4}$$

$$0.9 \quad 26.6 / \frac{1.1}{+0.18} \quad \frac{31}{-2.2} \quad \frac{49}{-3.5 / 22.0}$$

$$10.7 \quad 27.6 / \frac{10.4}{+0.3} \quad \frac{124}{-1.7} \quad \frac{14.5}{-3.8 / 22.6}$$

$$10.0 \quad 33.0 / \frac{6.9}{+3.1} \quad \frac{114}{-1.4} \quad \frac{12.8}{-2.8 / 20.6}$$

$$9.3 \quad 33.0 / \frac{3.5}{+5.8} \quad \frac{10.2}{-0.9} \quad \frac{11.3}{-2.0 / 19.0}$$

$$8.6 \quad 33.0 / \frac{10.0}{-8.4} \quad \frac{89}{-0.3} \quad \frac{10.6}{100.0 / 26.4}$$

Sta	+	π	-	Grade
		832.47		
178	+50			21.1
179				22.8
				^{7.4} +1.5 23.1
	+50			23.5
180				24.4
	+50			25.3
181				26.3
	+47			27.4
182				28.6
	+50			29.8
183				31.2
T.P.	7.76	939.92	0.31	712.16
	+50			32.6

$$\begin{array}{r} 166 \\ 129 \\ \hline 30 \\ \hline 57.0 \end{array}$$

66. Rod

44

2

124

$$11.4 \quad \begin{array}{r} 33.0 \\ \times 2.6 \\ \hline 198 \\ + 660 \\ \hline 85.8 \end{array} \quad \begin{array}{r} 10.2 \\ \times 1.2 \\ \hline 12.24 \end{array} \quad \begin{array}{r} 11.4 \\ \times 27.0 \\ \hline 77.8 \end{array}$$

9.7 $\frac{368}{129}$ $\frac{90}{107}$ $\frac{117}{120/240}$

$$9.6 \quad 33.0 / \begin{array}{r} 4.9 \\ + 2.1 \\ \hline \end{array} \quad \begin{array}{r} 84 \\ + 96 \\ \hline \end{array} \quad \begin{array}{r} 11.0 \\ \hline 100.0 / 23.0 \end{array}$$

81	$\begin{array}{r} 33.0 / 48 \\ + 3.2 \end{array}$	$\begin{array}{r} 78 \\ + 03 \end{array}$	$\begin{array}{r} 10.1 \\ - 2.0 / 19.0 \end{array}$
----	---	---	---

$$22 \quad \begin{array}{r} 259 \overline{) 80} \\ 518 \\ \hline 101 \end{array} \quad \begin{array}{r} 71 \\ 101 \end{array} \quad \begin{array}{r} 131 \\ 59 \overline{) 248} \\ 118 \\ \hline 130 \end{array}$$

6.2	20.8	8.2	63	10.2
		2.00	-0.1	-100/33.0

$$\begin{array}{r} 51 \\ 26,4 \overline{) 108} \\ \underline{-5,7} \end{array} \qquad \begin{array}{r} 5,1 \\ 0,0 \end{array} \qquad \begin{array}{r} 151 \\ -10,0 \overline{) 93,0} \end{array}$$

3.9	$\begin{array}{r} 20.9 / 6.6 \\ - 8.7 \\ \hline \end{array}$	$\begin{array}{r} 57 \\ + 0.2 \\ \hline \end{array}$	$\begin{array}{r} 13.0 \\ - 9.1 / 38.0 \\ \hline \end{array}$
-----	--	--	---

$$\begin{array}{r} 2.1 \\ 30.6 \overline{) 9.7} \\ \underline{61.2} \\ 35.8 \end{array} \qquad \begin{array}{r} 2.1 \\ 10.6 \overline{) 21} \\ \underline{21.2} \\ .2 \end{array} \qquad \begin{array}{r} 9.9 \\ 46 \overline{) 459} \\ \underline{458} \\ 1 \end{array}$$

1.3	$256 / 20$ 12.8	07 106	43 $3.0 / 21.0$
-----	----------------------	---------------	----------------------

23	$\begin{array}{r} 33.0 \\ \times 16.9 \\ \hline \end{array}$	$\begin{array}{r} 70 \\ + 103 \\ \hline \end{array}$	$\begin{array}{r} 95 \\ 1090 \\ \hline \end{array} \quad 20.4$
----	--	--	--

Sta	+	-	Grade
		929.92	
184			34.0
+60			35.7
B.M.	18.76	942.85	10.78
			929.14
185			36.8
+50			38.2
T.P.	12.82	952.73	2.94
			939.91
186			39.6
+50			40.9
187			41.9
+50			42.5
188			43.4
T.P.	7.69	953.68	8.74
			943.99
+50			43.7
189			43.9

Gr. Rod

Lt

L

Rt

5.9

$$33.0 / \begin{matrix} 10.6 \\ +6.5 \end{matrix}$$

$$\begin{matrix} 58 \\ +91 \end{matrix}$$

$$\begin{matrix} 79 \\ 80.4 \end{matrix} / 22.0$$

4.2

$$33.0 / \begin{matrix} 1.0 \\ +3.2 \end{matrix}$$

$$\begin{matrix} 1.0 \\ +9.2 \end{matrix}$$

$$\begin{matrix} 6.2 \\ 10.00 \end{matrix} / 30.4$$

Spt in Fe. Post 80 Rt +60

6.1

$$30.6 / \begin{matrix} 4.3 \\ +1.8 \end{matrix}$$

$$\begin{matrix} 58 \\ +0.3 \end{matrix}$$

$$\begin{matrix} 81 \\ 80.00 \end{matrix} / 20.7$$

4.7

$$33.0 / \begin{matrix} 14 \\ +3.3 \end{matrix}$$

$$\begin{matrix} 44 \\ +9.3 \end{matrix}$$

$$\begin{matrix} 6.7 \\ 80.0 \end{matrix} / 20.8$$

13.1

$$33.0 / \begin{matrix} 86 \\ +4.5 \end{matrix}$$

$$\begin{matrix} 127 \\ +9.7 \end{matrix}$$

$$\begin{matrix} 131 \\ 80.00 \end{matrix} / 19.7$$

11.8

$$52.0 / \begin{matrix} 4.8 \\ +7.0 \end{matrix}$$

$$\begin{matrix} 110 \\ +9.8 \end{matrix}$$

$$\begin{matrix} 138 \\ 100.00 \end{matrix} / 20.9$$

10.8

$$33.0 / \begin{matrix} 2.9 \\ +7.9 \end{matrix}$$

$$\begin{matrix} 97 \\ +1.1 \end{matrix}$$

$$\begin{matrix} 12.8 \\ 80.00 \end{matrix} / 20.6$$

9.9

$$33.0 / \begin{matrix} 1.7 \\ +8.2 \end{matrix}$$

$$\begin{matrix} 90 \\ +9.9 \end{matrix}$$

$$\begin{matrix} 11.9 \\ 80.00 \end{matrix} / 22.0$$

9.3

$$33.0 / \begin{matrix} 1.6 \\ +7.7 \end{matrix}$$

$$\begin{matrix} 87 \\ +0.6 \end{matrix}$$

$$\begin{matrix} 11.3 \\ 100.00 \end{matrix} / 25.1$$

K 5/2188

100

$$\begin{matrix} 100 \\ 00 \end{matrix}$$

$$\begin{matrix} 15.0 \\ 100.00 \end{matrix} / 23.2$$

9.8

$$33.0 / \begin{matrix} 34 \\ +6.4 \end{matrix}$$

$$\begin{matrix} 106 \\ -0.6 \end{matrix}$$

$$\begin{matrix} 11.8 \\ 100.00 \end{matrix} / 19.0$$

2 Blk. Tan

Sta	+	X	-	Grade
		953.68		

189	+50			43.8
-----	-----	--	--	------

190				43.5
-----	--	--	--	------

T.P.	7.51	948.92	12.77	940.91
------	------	--------	-------	--------

+45				43.0
-----	--	--	--	------

191				42.2
-----	--	--	--	------

+50				41.2
-----	--	--	--	------

192				40.0
-----	--	--	--	------

+50				38.5
-----	--	--	--	------

193				36.8
-----	--	--	--	------

+35				35.8
-----	--	--	--	------

T.P.	11.0	937.79	11.74	926.68
------	------	--------	-------	--------

+70				34.2
-----	--	--	--	------

194				33.2
-----	--	--	--	------

Gr. Rod

Lt.

R.

Rt.

9.9

$$33.0 / \begin{array}{r} 1.0 \\ +8.9 \end{array}$$

$$\begin{array}{r} 111 \\ -12 \end{array}$$

$$\begin{array}{r} 11.9 \\ 12.00 / 24.0 \end{array}$$

10.2

$$33.0 / \begin{array}{r} 1.2 \\ +8.3 \end{array}$$

$$\begin{array}{r} 119 \\ -17 \end{array}$$

$$\begin{array}{r} 10.0 \\ -4.0 / 23.0 \end{array}$$

5.4

$$33.0 / \begin{array}{r} 1.0 \\ +6.4 \end{array}$$

$$\begin{array}{r} 71 \\ -17 \end{array}$$

$$\begin{array}{r} 12.8 \\ -7.4 / 29.8 \end{array}$$

6.2

$$33.0 / \begin{array}{r} 4.0 \\ +2.2 \end{array}$$

$$\begin{array}{r} 75 \\ -18 \end{array}$$

$$\begin{array}{r} 141 \\ -7.9 / 30.8 \end{array}$$

7.2

$$33.0 / \begin{array}{r} 5.8 \\ +1.9 \end{array}$$

$$\begin{array}{r} 79 \\ -9.7 \end{array}$$

$$\begin{array}{r} 9.2 \\ 12.00 / 20.2 \end{array}$$

8.4

$$33.0 / \begin{array}{r} 6.3 \\ +2.1 \end{array}$$

$$\begin{array}{r} 83 \\ +91 \end{array}$$

$$\begin{array}{r} 7.4 \\ 12.0 / 25.0 \end{array}$$

9.9

$$33.0 / \begin{array}{r} 4.0 \\ +5.9 \end{array}$$

$$\begin{array}{r} 99 \\ 00 \end{array}$$

$$\begin{array}{r} 10.2 \\ 12.17 / 26.4 \end{array}$$

11.6

$$33.0 / \begin{array}{r} 2.8 \\ +8.8 \end{array}$$

$$\begin{array}{r} 117 \\ -91 \end{array}$$

$$\begin{array}{r} 10.0 \\ 4.6 / 30.2 \end{array}$$

12.9

$$33.0 / \begin{array}{r} 2.6 \\ +10.4 \end{array}$$

$$\begin{array}{r} 129 \\ 00 \end{array}$$

$$\begin{array}{r} 10.7 \\ 12.2 / 31.4 \end{array}$$

3.6

$$33.0 / \begin{array}{r} 11.8 \end{array}$$

$$\begin{array}{r} 35 \\ +91 \end{array}$$

$$\begin{array}{r} 10 \\ 12.6 / 32.2 \end{array}$$

4.6

$$33.0 / \begin{array}{r} 13.1 \end{array}$$

$$\begin{array}{r} 46 \\ 00 \end{array}$$

$$\begin{array}{r} 5.7 \\ 13.9 / 33.0 \end{array}$$

Sta	+	Δ	-	Grade
		987.78		

194	+35			31.9
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	+70			30.6
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195				27.4
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	+50			27.4
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196				25.2
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T.P.	2.61	987.38	1201	989.77
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	+52			22.9
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197				20.7
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	+45			18.5
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T.P.	2.71	980.18	791	917.97
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	+75			17.0
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198				15.8
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	+25			11.9
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Gr. Red.

Lt.

C.

Rt.

$$5.7 \quad 33.0 / \overline{+18.9} \quad \begin{array}{r} 58 \\ 101 \end{array} \quad \begin{array}{r} 20 \\ 139/33.0 \end{array}$$

$$7.2 \quad 33.0 / \overline{+14.3} \quad \begin{array}{r} 74 \\ -02 \end{array} \quad \begin{array}{r} 24 \\ 198/33.0 \end{array}$$

$$8.4 \quad 33.0 / \overline{+15.3} \quad \begin{array}{r} 87 \\ -03 \end{array} \quad \begin{array}{r} 42 \\ 192/33.0 \end{array}$$

$$10.4 \quad 33.0 / \overline{+16.3} \quad \begin{array}{r} 110 \\ -06 \end{array} \quad \begin{array}{r} 76 \\ 128/33.0 \end{array}$$

$$12.6 \quad 33.0 / \overline{+17.2} \quad \begin{array}{r} 131 \\ -06 \end{array} \quad \begin{array}{r} 86 \\ 140/33.0 \end{array}$$

$$1.5 \quad 33.9 / \overline{+17.5} \quad \begin{array}{r} 48 \\ -03 \end{array} \quad \begin{array}{r} 19 \\ 216/20.2 \end{array}$$

$$6.7 \quad 33.0 / \overline{+17.0} \quad \begin{array}{r} 68 \\ -01 \end{array} \quad \begin{array}{r} 71 \\ 209/24.8 \end{array}$$

$$8.9 \quad 33.0 / \overline{+17.8} \quad \begin{array}{r} 86 \\ 103 \end{array} \quad \begin{array}{r} 99 \\ 1010/250 \end{array}$$

Top Blue Tan L.

$$3.2 \quad 33.0 / \overline{+19.1} \quad \begin{array}{r} 29 \\ 103 \end{array} \quad \begin{array}{r} 46 \\ 1206/24.2 \end{array}$$

$$4.4 \quad 33.0 / \overline{+19.2} \quad \begin{array}{r} 40 \\ 104 \end{array} \quad \begin{array}{r} 64 \\ 1200/25.4 \end{array}$$

$$6.3 \quad 33.0 / \overline{+19.7} \quad \begin{array}{r} 62 \\ 101 \end{array} \quad \begin{array}{r} 83 \\ 1200/26.1 \end{array}$$

Sta	+	T	-	Grade
		920.18		
198	+63			12.4
199				10.45
T.P	1.36	908.32	13.02	907.16
	+50			077
200				050
	+50			02.2
T.P	1.21	900.25	9.48	899.04
201				899.7
	+50			97.3
202				95.4
	+50			93.7
203				92.5
	+50			91.4

Gr. Rod.

Lt.

L

Rt

$$7.8 \quad 330 \begin{array}{r} 36 \\ 14.2 \end{array} \quad \begin{array}{r} 78 \\ 90 \end{array} \quad \begin{array}{r} 93 \\ 20.05/33.0 \end{array}$$

$$9.8 \quad 292 \begin{array}{r} 87 \\ 11.1 \end{array} \quad \begin{array}{r} 100 \\ -0.2 \end{array} \quad \begin{array}{r} 118 \\ 20.00/33.0 \end{array}$$

$$0.8 \quad 264 \begin{array}{r} 11 \\ 12.17 \end{array} \quad \begin{array}{r} 17 \\ -0.9 \end{array} \quad \begin{array}{r} 106 \\ -98/33.0 \end{array}$$

$$3.5 \quad 236 \begin{array}{r} 52 \\ 12.03 \end{array} \quad \begin{array}{r} 46 \\ -11 \end{array} \quad \begin{array}{r} 15.3 \\ -11.8/33.0 \end{array}$$

$$6.3 \quad 230 \begin{array}{r} 83 \\ 12.00 \end{array} \quad \begin{array}{r} 71 \\ -0.8 \end{array} \quad \begin{array}{r} 16.0 \\ -9.7/33.0 \end{array}$$

$$0.6 \quad 226 \begin{array}{r} 23 \\ 12.03 \end{array} \quad \begin{array}{r} 12 \\ -0.6 \end{array} \quad \begin{array}{r} 11.3 \\ -10.6/33.0 \end{array}$$

$$3.0 \quad 244 \begin{array}{r} 43 \\ 12.07 \end{array} \quad \begin{array}{r} 36 \\ -0.6 \end{array} \quad \begin{array}{r} 125 \\ -95/33.0 \end{array}$$

$$4.9 \quad 238 \begin{array}{r} 65 \\ 12.04 \end{array} \quad \begin{array}{r} 59 \\ -10 \end{array} \quad \begin{array}{r} 129 \\ -8.6/31.0 \end{array}$$

$$6.6 \quad 249 \begin{array}{r} 81 \\ 12.03 \end{array} \quad \begin{array}{r} 72 \\ -0.8 \end{array} \quad \begin{array}{r} 124 \\ -58/26.6 \end{array}$$

$$7.8 \quad 240 \begin{array}{r} 93 \\ 12.05 \end{array} \quad \begin{array}{r} 82 \\ -0.5 \end{array} \quad \begin{array}{r} 132 \\ -54/25.8 \end{array}$$

$$8.9 \quad 244 \begin{array}{r} 103 \\ 12.07 \end{array} \quad \begin{array}{r} 87 \\ -0.2 \end{array} \quad \begin{array}{r} 135 \\ -46/24.2 \end{array}$$

Sta.	+	π	-	Grade
		900.25		

204				90.8
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	+50			90.3
--	-----	--	--	------

T.P.	3.21	898.83	963	890.62
------	------	--------	-----	--------

205				90.1
-----	--	--	--	------

	+50			89.8
--	-----	--	--	------

206				89.6
-----	--	--	--	------

	+50			89.4
--	-----	--	--	------

207				89.2
-----	--	--	--	------

	+50			89.0
--	-----	--	--	------

208				88.8
-----	--	--	--	------

	+50			88.6
--	-----	--	--	------

209				88.4
-----	--	--	--	------

Gr. Rod

L_tL_cR_t

9.5

$$25.0 / \frac{105}{10.10}$$

$$\frac{92}{+0.3}$$

$$\frac{137}{-42/28.9}$$

10.0

$$35.4 / \frac{108}{10.12}$$

$$\frac{95}{+0.5}$$

$$\frac{135}{-38/22.6}$$

9.7

$$23.6 / \frac{5.4}{10.09}$$

$$\frac{22}{+0.5}$$

$$\frac{7.0}{-23/21.6}$$

9.0

$$23.0 / \frac{6.0}{10.00}$$

$$\frac{36}{+0.4}$$

$$\frac{7.5}{-12/22.0}$$

9.2

$$19.6 / \frac{6.5}{-2.3}$$

$$\frac{40}{+0.2}$$

$$\frac{7.8}{-26/22.2}$$

9.4

$$20.4 / \frac{7.1}{-2.7}$$

$$\frac{43}{+0.1}$$

$$\frac{7.9}{-3.5/22.0}$$

9.6

$$20.2 / \frac{7.2}{-2.6}$$

$$\frac{45}{+0.1}$$

$$\frac{8.4}{-3.8/22.6}$$

9.8

$$20.4 / \frac{7.5}{-2.9}$$

$$\frac{47}{+0.1}$$

$$\frac{8.6}{-3.8/22.6}$$

5.0

$$20.0 / \frac{7.5}{-2.5}$$

$$\frac{52}{-0.2}$$

$$\frac{8.8}{-3.8/22.6}$$

5.2

$$20.4 / \frac{7.9}{-2.7}$$

$$\frac{61}{-0.9}$$

$$\frac{10.4}{-5.2/25.9}$$

5.4

$$20.6 / \frac{8.2}{-2.8}$$

$$\frac{65}{-1.1}$$

$$\frac{10.0}{-4.6/24.2}$$

Sta	+	X	-	Grade	
		892.83			
209	+50			88.2	
210				88.0	
	+50			87.8	
B.M.	-0.06	892.58	1.27	892.56	892.59
211				87.5	
	+50			87.7	
212				87.9	
	+50			88.1	
213				88.3	
	+50			88.5	
214				88.7	
T.P.	5.09	892.53	8.07		
	+62			88.9	

Gr. Rod.

L

R

Rt.

$$5.6 \quad 19.6 / \begin{array}{r} 7.9 \\ -2.3 \end{array}$$

$$\begin{array}{r} 6.9 \\ -0.7 \end{array}$$

$$\begin{array}{r} 8.8 \\ -3.8 \end{array} / 21.4$$

$$5.8 \quad 18.8 / \begin{array}{r} 7.7 \\ -1.9 \end{array}$$

$$\begin{array}{r} 6.0 \\ -0.2 \end{array}$$

$$\begin{array}{r} 8.4 \\ -2.6 \end{array} / 20.2$$

$$6.0 \quad 18.4 / \begin{array}{r} 7.7 \\ -1.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ +0.3 \end{array}$$

$$\begin{array}{r} 8.4 \\ -2.4 \end{array} / 19.8$$

Top Brick N.W. Cor. Brick & Conc. M. H. 200' Rt. 211+50

$$5.0 \quad \begin{array}{r} 4.3 \\ +0.7 \end{array}$$

$$\begin{array}{r} 6.0 \\ -1.0 \end{array} / 17.0$$

$$4.8 \quad \begin{array}{r} 4.7 \\ +0.1 \end{array}$$

$$4.6 \quad 17.4 / \begin{array}{r} 5.8 \\ +1.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ -0.7 \end{array}$$

$$\begin{array}{r} 8.6 \\ -4.0 \end{array} / 23.0$$

$$4.4 \quad 19.4 / \begin{array}{r} 16.4 \\ -2.8 \end{array}$$

$$\begin{array}{r} 5.8 \\ -1.4 \end{array}$$

$$\begin{array}{r} 8.5 \\ -4.1 \end{array} / 23.2$$

$$4.2 \quad 22.6 / \begin{array}{r} 8.0 \\ -3.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ -1.7 \end{array}$$

$$\begin{array}{r} 9.5 \\ -3.3 \end{array} / 25.6$$

$$4.0 \quad 22.6 / \begin{array}{r} 7.6 \\ -3.6 \end{array}$$

$$\begin{array}{r} 5.7 \\ -1.7 \end{array}$$

$$\begin{array}{r} 8.4 \\ -4.4 \end{array} / 23.8$$

$$3.8 \quad 22.2 / \begin{array}{r} 7.4 \\ -3.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ -1.3 \end{array}$$

$$\begin{array}{r} 8.2 \\ -4.4 \end{array} / 23.8$$

$$3.7 \quad 21.2 / \begin{array}{r} 6.8 \\ -3.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ -0.9 \end{array}$$

$$\begin{array}{r} 6.6 \\ -2.9 \end{array}$$

$$\boxed{R. 3.5}$$

Sta	+	X	-	Grade
		892.55		

215				89.1
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+50				89.3
-----	--	--	--	------

216				89.5
-----	--	--	--	------

+50				89.7
-----	--	--	--	------

217				89.9
-----	--	--	--	------

+50				90.1
-----	--	--	--	------

218				90.3
-----	--	--	--	------

T.P.	6.54	897.40	1.69	890.86
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+50				90.5
-----	--	--	--	------

219				90.7
-----	--	--	--	------

+50				90.9
-----	--	--	--	------

220				91.1
-----	--	--	--	------

T.P.	10.00	903.28	4.12	893.28
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92
57
3.5

Gr. Pool

Lt

R

Rt

3.5

$$22.0 / \begin{array}{r} 7.0 \\ -3.5 \end{array}$$

$$\begin{array}{r} 15 \\ -1.0 \end{array}$$

$$\begin{array}{r} 6.1 \\ -2.6 \end{array}$$

12 3.1

2.3

$$22.8 / \begin{array}{r} 7.7 \\ -4.4 \end{array}$$

$$\begin{array}{r} 9.6 \\ -1.3 \end{array}$$

$$\begin{array}{r} 6.8 \\ -3.5 \end{array}$$

102 12 35

2.1

$$22.3 / \begin{array}{r} 6.7 \\ -2.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ -1.7 \end{array}$$

$$\begin{array}{r} 6.6 \\ -3.4 \end{array} / 22.0$$

2.9

$$23.2 / \begin{array}{r} 7.0 \\ -4.1 \end{array}$$

$$\begin{array}{r} 9.8 \\ -1.4 \end{array}$$

$$\begin{array}{r} 6.5 \\ -3.6 \end{array} / 22.2$$

2.7

$$23.0 / \begin{array}{r} 6.7 \\ -4.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ -1.0 \end{array}$$

$$\begin{array}{r} 5.5 \\ -2.8 \end{array} / 20.6$$

2.5

$$22.6 / \begin{array}{r} 6.3 \\ -3.8 \end{array}$$

$$\begin{array}{r} 9.4 \\ +0.1 \end{array}$$

$$\begin{array}{r} 5.0 \\ -2.5 \end{array} / 20.0$$

2.3

$$23.0 / \begin{array}{r} 6.3 \\ -4.0 \end{array}$$

$$\begin{array}{r} 1.7 \\ +0.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ -2.5 \end{array} / 20.0$$

2 218

6.9

$$20.6 / \begin{array}{r} 9.7 \\ -2.8 \end{array}$$

$$\begin{array}{r} 6.1 \\ +0.8 \end{array}$$

$$\begin{array}{r} 8.0 \\ +0.9 \end{array} / 24.8$$

6.7

$$24.4 / \begin{array}{r} 8.0 \\ +0.7 \end{array}$$

$$\begin{array}{r} 5.3 \\ +1.4 \end{array}$$

$$\begin{array}{r} 5.8 \\ +0.9 \end{array} / 28.8$$

6.5

$$25.4 / \begin{array}{r} 7.3 \\ +0.2 \end{array}$$

$$\begin{array}{r} 9.6 \\ +1.9 \end{array}$$

$$\begin{array}{r} 9.7 \\ +1.8 \end{array} / 30.6$$

6.3

$$26.8 / \begin{array}{r} 6.4 \\ +1.9 \end{array}$$

$$\begin{array}{r} 9.1 \\ +2.2 \end{array}$$

$$\begin{array}{r} 3.5 \\ +2.9 \end{array} / 32.6$$

Sta	+	X	-	Grade
		903.28		

220	+50			91.3
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221				91.5
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	+50			91.7
--	-----	--	--	------

222				91.9
-----	--	--	--	------

	+50			92.1
--	-----	--	--	------

223				92.3
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T.P.	6.45	898.75	10.98	898.30
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	+50			92.5
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224				92.7
-----	--	--	--	------

	+50			93.0
--	-----	--	--	------

225				93.4
-----	--	--	--	------

	+50			93.9
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T.P.	9.79	901.02	7.52	891.23
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Gr Rad

Lt

Σ

Rt

$$12.0 \quad 31.6 / \begin{array}{r} 97 \\ +23 \end{array}$$

$$\begin{array}{r} 97 \\ +23 \end{array}$$

$$\begin{array}{r} 57 \\ 163 / 33.0 \end{array}$$

$$11.8 \quad 33.0 / \begin{array}{r} 81 \\ +37 \end{array}$$

$$\begin{array}{r} 98 \\ +20 \end{array}$$

$$\begin{array}{r} 37 \\ 181 / 33.0 \end{array}$$

$$11.6 \quad 29.4 / \begin{array}{r} 104 \\ +12 \end{array}$$

$$\begin{array}{r} 110 \\ +16 \end{array}$$

$$\begin{array}{r} 67 \\ 149 / 33.0 \end{array}$$

$$11.4 \quad 238 / \begin{array}{r} 130 \\ +04 \end{array}$$

$$\begin{array}{r} 102 \\ +12 \end{array}$$

$$\begin{array}{r} 77 \\ +37 / 33.0 \end{array}$$

$$11.2 \quad 204 / \begin{array}{r} 139 \\ -27 \end{array}$$

$$\begin{array}{r} 105 \\ +07 \end{array}$$

$$\begin{array}{r} 78 \\ 184 / 33.0 \end{array}$$

$$11.0 \quad 23.0 / \begin{array}{r} 150 \\ -40 \end{array}$$

$$\begin{array}{r} 110 \\ 00 \end{array}$$

$$\begin{array}{r} 88 \\ 120 / 33.0 \end{array}$$

$$6.3 \quad 24.4 / \begin{array}{r} 110 \\ -27 \end{array}$$

$$\begin{array}{r} 68 \\ -23 \end{array}$$

$$\begin{array}{r} 47 \\ 116 / 30.2 \end{array}$$

$$6.1 \quad 24.2 / \begin{array}{r} 107 \\ -46 \end{array}$$

$$\begin{array}{r} 68 \\ -27 \end{array}$$

$$\begin{array}{r} 58 \\ 103 / 27.6 \end{array}$$

$$5.8 \quad 20.6 / \begin{array}{r} 86 \\ -28 \end{array}$$

$$\begin{array}{r} 65 \\ -27 \end{array}$$

$$\begin{array}{r} 68 \\ 121.0 / 25.0 \end{array}$$

$$5.4 \quad 20.8 / \begin{array}{r} 88 \\ -29 \end{array}$$

$$\begin{array}{r} 63 \\ -27 \end{array}$$

$$\begin{array}{r} 80 \\ -26 / 20.2 \end{array}$$

$$4.9 \quad 19.2 / \begin{array}{r} 80 \\ -21 \end{array}$$

$$\begin{array}{r} 64 \\ -15 \end{array}$$

$$\begin{array}{r} 92 \\ 13 / 23.6 \end{array}$$

Sta	+	π	-	Grade
		901.02		

226				94.4
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+50				95.0
-----	--	--	--	------

227				95.7
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+50				96.5
-----	--	--	--	------

228				97.3
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T.P.	9.57	907.47	3.12	897.90
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+50				98.1
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229				98.9
-----	--	--	--	------

+50				99.7
-----	--	--	--	------

230				100.3
-----	--	--	--	-------

+50				100.9
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231				01.4
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Gr. Rod.

Lt

£

Rt

$$6.6 \quad 25.0 / \begin{array}{r} 11.6 \\ -5.0 \end{array} \quad \begin{array}{r} 55 \\ -19 \end{array} \quad \begin{array}{r} 11.5 \\ -49 \end{array} / 248$$

$$6.0 \quad 26.4 / \begin{array}{r} 11.7 \\ -5.7 \end{array} \quad \begin{array}{r} 80 \\ -20 \end{array} \quad \begin{array}{r} 11.4 \\ -54 \end{array} / 258$$

$$5.3 \quad 28.2 / \begin{array}{r} 11.9 \\ -6.6 \end{array} \quad \begin{array}{r} 71 \\ -18 \end{array} \quad \begin{array}{r} 10.0 \\ -47 \end{array} / 29.4$$

$$4.5 \quad 29.2 / \begin{array}{r} 11.6 \\ -7.1 \end{array} \quad \begin{array}{r} 51 \\ -12 \end{array} \quad \begin{array}{r} 6.3 \\ -20.2 \end{array} / 234$$

$$3.7 \quad 27.8 / \begin{array}{r} 10.1 \\ -6.4 \end{array} \quad \begin{array}{r} 42 \\ -05 \end{array} \quad \begin{array}{r} 34 \\ -10.3 \end{array} / 273$$

$$2.4 \quad 19.4 / \begin{array}{r} 11.6 \\ -2.2 \end{array} \quad \begin{array}{r} 9.0 \\ -04 \end{array} \quad \begin{array}{r} 61 \\ -13.3 \end{array} / 33.0$$

$$8.6 \quad 25.6 / \begin{array}{r} 9.3 \\ -2.3 \end{array} \quad \begin{array}{r} 75 \\ -1.1 \end{array} \quad \begin{array}{r} 28 \\ -15.8 \end{array} / 33.0$$

$$7.8 \quad 29.4 / \begin{array}{r} 6.6 \\ -1.8 \end{array} \quad \begin{array}{r} 62 \\ -16 \end{array} \quad \begin{array}{r} 05 \\ -17.3 \end{array} / 33.0$$

$$7.2 \quad 32.6 / \begin{array}{r} 4.4 \\ -12.8 \end{array} \quad \begin{array}{r} 50 \\ -22 \end{array} \quad \begin{array}{r} 04 \\ -14.8 \end{array} / 33.0$$

$$6.6 \quad 33.0 / \begin{array}{r} 3.8 \\ -13.5 \end{array} \quad \begin{array}{r} 44 \\ -22 \end{array} \quad \begin{array}{r} 0.9 \\ -15.7 \end{array} / 33.0$$

$$6.1 \quad 32.4 / \begin{array}{r} 3.4 \\ -12.7 \end{array} \quad \begin{array}{r} 41 \\ -20 \end{array} \quad \begin{array}{r} 16 \\ -14.5 \end{array} / 33.0$$

Sta	+	X	-	Grade
		907.47		
231	+50			01.8
232				02.1
	+50			02.4
T.P.	2.71	906.84	3.34	904.13
233				02.5
	+50			02.6
234				02.7
	+50			02.8
235				02.9
	+50			03.0
236				03.1
B.M.				903.07
	+50			03.2

Gr. Rod

H

L

Rt

$$5.7 \quad \begin{array}{r} 30.6 / 39 \\ +18 \end{array} \quad \begin{array}{r} 43 \\ +14 \end{array} \quad \begin{array}{r} 27 \\ +50 / 39.0 \end{array}$$

$$5.4 \quad \begin{array}{r} 29.4 / 42 \\ +12 \end{array} \quad \begin{array}{r} 41 \\ +13 \end{array} \quad \begin{array}{r} 27 \\ +27 / 52.4 \end{array}$$

$$5.1 \quad \begin{array}{r} 29.6 / 38 \\ +13 \end{array} \quad \begin{array}{r} 41 \\ +10 \end{array} \quad \begin{array}{r} 2.9 \\ +22 / 21.4 \end{array}$$

$$4.3 \quad \begin{array}{r} 28.8 / 34 \\ +0.9 \end{array} \quad \begin{array}{r} 37 \\ +0.6 \end{array} \quad \begin{array}{r} 37 \\ +0.6 / 28.2 \end{array}$$

$$4.2 \quad \begin{array}{r} 27.0 / 42 \\ +0.0 \end{array} \quad \begin{array}{r} 40 \\ +0.2 \end{array} \quad \begin{array}{r} 6.2 \\ +20.0 / 27.5 \end{array}$$

$$4.1 \quad \begin{array}{r} 25.7 / 49 \\ +12 \end{array} \quad \begin{array}{r} 44 \\ -0.3 \end{array} \quad \begin{array}{r} 9.5 \\ -5.4 / 25.8 \end{array}$$

$$4.0 \quad \begin{array}{r} 23.4 / 58 \\ +0.2 \end{array} \quad \begin{array}{r} 48 \\ -0.8 \end{array} \quad \begin{array}{r} 10.7 \\ -6.7 / 28.7 \end{array}$$

$$3.9 \quad \begin{array}{r} 23.0 / 59 \\ +0.5 \end{array} \quad \begin{array}{r} 46 \\ -0.7 \end{array} \quad \begin{array}{r} 9.2 \\ -5.3 / 25.6 \end{array}$$

$$3.8 \quad \begin{array}{r} 25.2 / 47 \\ +11 \end{array} \quad \begin{array}{r} 43 \\ -0.5 \end{array} \quad \begin{array}{r} 58 \\ +20.0 / 23.0 \end{array}$$

$$3.7 \quad \begin{array}{r} 26.4 / 40 \\ +17 \end{array} \quad \begin{array}{r} 39 \\ -0.2 \end{array} \quad \begin{array}{r} 40 \\ +17 / 26.4 \end{array}$$

Top Mast. 237 + 33.28

$$36 \quad \begin{array}{r} 240 / 56 \\ +0.0 \end{array} \quad \begin{array}{r} 39 \\ -0.3 \end{array} \quad \begin{array}{r} 28 \\ +17 / 26.4 \end{array}$$

Sta	+	Σ	-	Grade	
		906.84			
237				03.1	
B.M.	3.08	906.10	274	903.10	903.07
+50				03.0	
238				02.8	
+50				02.5	
239				02.1	
+50				01.7	
240				01.1	
+50				900.5	
241				899.9	
+50				99.3	
242				98.7	

Gr. Rod

Lt

Rt

Rt

3.7

$$242 / \frac{5.1}{2.06}$$

$$\frac{37}{0.0}$$

$$\frac{39}{4.10} / 26.6$$

Top Mast 237 + 33.28

3.1

$$339 / \frac{2.5}{10.6}$$

$$\frac{29}{102}$$

$$\frac{29}{102} / 27.4$$

3.3

$$320 / \frac{1.9}{12.0}$$

$$\frac{32}{101}$$

$$\frac{49}{10.9} / 24.8$$

3.6

$$320 / \frac{1.0}{12.6}$$

$$\frac{34}{102}$$

$$\frac{33}{10.3} / 27.6$$

4.0

$$330 / \frac{0.6}{13.9}$$

$$\frac{38}{102}$$

$$\frac{25}{11.5} / 30.0$$

4.4

$$330 / \frac{1.9}{12.3}$$

$$\frac{45}{101}$$

$$\frac{40}{10.4} / 27.8$$

5.0

$$330 / \frac{1.6}{10.4}$$

$$\frac{53}{103}$$

$$\frac{63}{12.07} / 24.4$$

6.0

$$330 / \frac{1.1}{12.19}$$

$$\frac{60}{0.0}$$

$$\frac{64}{12.12} / 26.2$$

6.2

$$190 / \frac{8.2}{12.00}$$

$$\frac{66}{10.9}$$

$$\frac{25}{13.7} / 30.0$$

6.8

$$190 / \frac{1.8}{12.0}$$

$$\frac{68}{101}$$

$$\frac{22}{12.6} / 25.0$$

7.4

$$140 / \frac{9.4}{12.0}$$

$$\frac{74}{0.0}$$

$$\frac{19}{15.5} / 30.0$$

Sta	+	π	-	Grade
		906.10		
242	+60			98.1
243				97.7
T.P.	2.86	900.24	8.72	897.38
				900.43
	+50			97.3
244				96.9
	+50			96.5
245				96.2
	+35			96.0
	+50			95.9
246				95.7
T.P.	6.26	906.27	0.23	900.01
	+50			95.4
247				95.1

Gr. Rod.

Lt

E

Rt.

$$8.0 \quad 18.0 / \begin{array}{r} 95 \\ -15 \end{array}$$

$$\frac{88}{-0.3}$$

$$10.6 / \begin{array}{r} 74 \\ 28.2 \end{array}$$

$$8.4 \quad 26.0 / \begin{array}{r} 139 \\ -5.5 \end{array}$$

$$\frac{87}{-0.3}$$

$$12.3 / \begin{array}{r} 2.9 \\ 22.8 \end{array}$$

Spt. in 18' Oak 125' Bl. 243+00

$$2.9 \quad 30.8 / \begin{array}{r} 108 \\ -79 \end{array}$$

$$\frac{26}{-0.7}$$

$$9.2 / \begin{array}{r} 6.3 \\ 27.6 \end{array}$$

$$3.3 \quad 30.8 / \begin{array}{r} 112 \\ -79 \end{array}$$

$$\frac{41}{-0.8}$$

$$10.1 / \begin{array}{r} 6.8 \\ 28.6 \end{array}$$

$$3.7 \quad 29.2 / \begin{array}{r} 108 \\ -18 \end{array}$$

$$\frac{40}{-0.9}$$

$$10.1 / \begin{array}{r} 6.9 \\ 27.8 \end{array}$$

$$4.0 \quad 25.6 / \begin{array}{r} 93 \\ -5.3 \end{array}$$

$$\frac{48}{-0.5}$$

$$10.2 / \begin{array}{r} 6.2 \\ 27.4 \end{array}$$

$$4.2 \quad 23.2 / \begin{array}{r} 61 \\ 20.1 \end{array}$$

$$\frac{44}{-0.2}$$

$$7.9 / \begin{array}{r} 5.7 \\ 22.9 \end{array}$$

$$4.3 \quad 33.0 / \begin{array}{r} 0.9 \\ 7.36 \end{array}$$

$$\frac{44}{-0.1}$$

$$6.3 / \begin{array}{r} 20.00 \\ 20.5 \end{array}$$

$$4.5 \quad 33.0 / \begin{array}{r} 0.9 \\ 7.36 \end{array}$$

$$\frac{46}{-0.1}$$

$$1.0 / \begin{array}{r} 19.5 \\ 33.0 \end{array}$$

$$10.9 \quad 33.0 / \begin{array}{r} 6.0 \\ 14.9 \end{array}$$

$$\frac{109}{6.0}$$

$$41 / \begin{array}{r} 4.9 \\ 33.0 \end{array}$$

$$11.2 \quad 33.0 / \begin{array}{r} 6.6 \\ 14.6 \end{array}$$

$$\frac{111}{10.1}$$

$$38 / \begin{array}{r} 17.4 \\ 33.0 \end{array}$$

Sta	+	X	-	Grade
		906.27		
247	+50			94.9
248				94.7
	+50			94.4
249				94.1
	+50			93.9
250				93.6
B.M.			1266	893.61 893.64

Gr. Rod

Lt.

L

Rt.

$$11.4 \quad \begin{array}{r} 33.0 \\ + 9.1 \\ \hline 42.1 \end{array} \quad \begin{array}{r} 11.4 \\ - 9.0 \\ \hline 2.4 \end{array} \quad \begin{array}{r} 4.3 \\ + 21.7 \\ \hline 26.0 \end{array}$$

$$11.6 \quad \begin{array}{r} 33.0 \\ + 9.7 \\ \hline 42.7 \end{array} \quad \begin{array}{r} 11.9 \\ - 9.3 \\ \hline 2.6 \end{array} \quad \begin{array}{r} 4.5 \\ + 21.1 \\ \hline 25.6 \end{array}$$

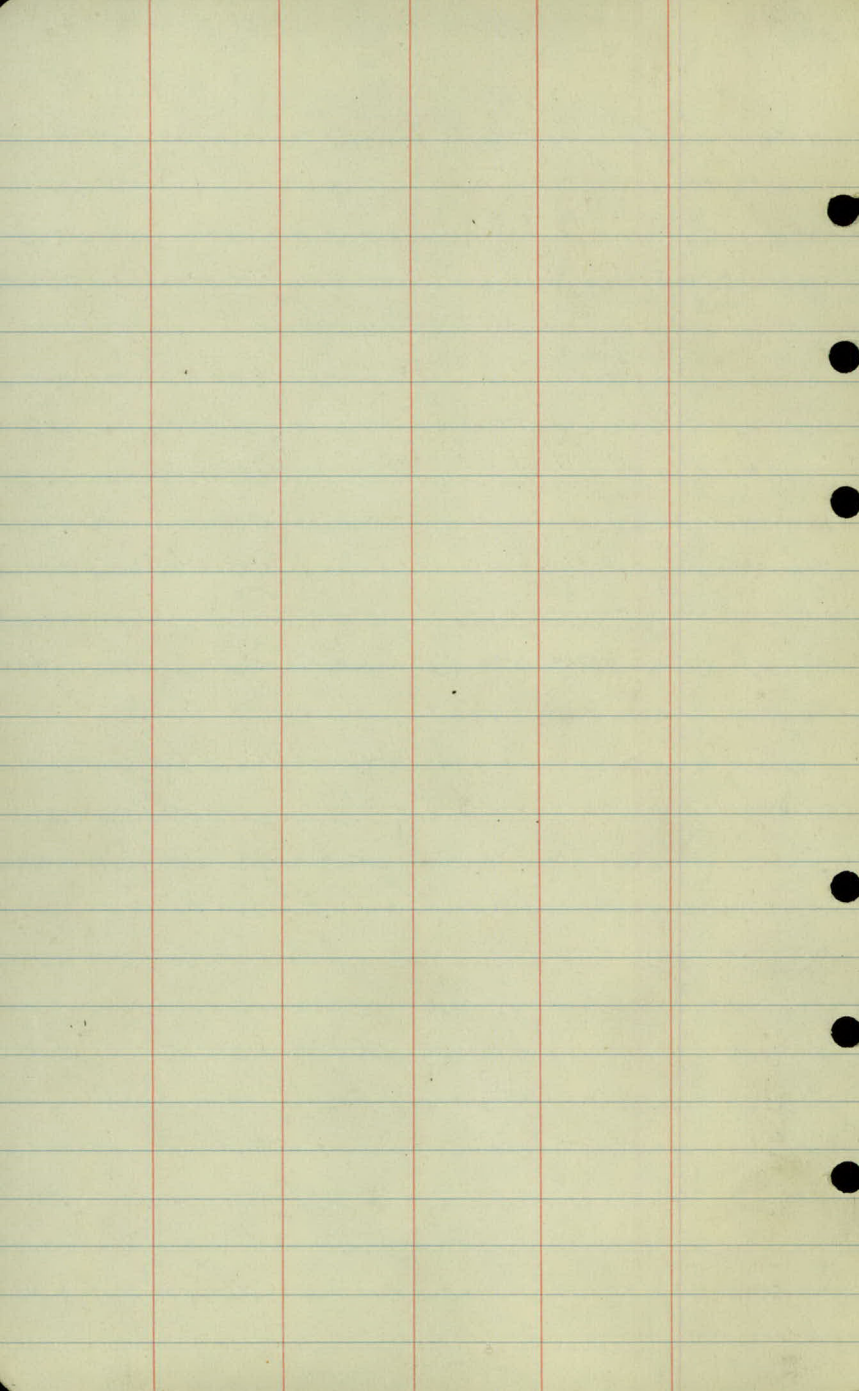
$$11.9 \quad \begin{array}{r} 33.0 \\ + 10.3 \\ \hline 43.3 \end{array} \quad \begin{array}{r} 12.3 \\ - 9.4 \\ \hline 2.9 \end{array} \quad \begin{array}{r} 4.7 \\ + 20.2 \\ \hline 24.9 \end{array}$$

$$12.2 \quad \begin{array}{r} 33.0 \\ + 10.6 \\ \hline 43.6 \end{array} \quad \begin{array}{r} 12.6 \\ - 9.4 \\ \hline 3.2 \end{array} \quad \begin{array}{r} 5.6 \\ + 19.6 \\ \hline 25.2 \end{array}$$

$$12.4 \quad \begin{array}{r} 33.0 \\ + 11.0 \\ \hline 44.0 \end{array} \quad \begin{array}{r} 12.9 \\ - 9.5 \\ \hline 3.4 \end{array} \quad \begin{array}{r} 7.3 \\ + 15.1 \\ \hline 22.4 \end{array}$$

$$12.7 \quad \begin{array}{r} 33.0 \\ + 12.4 \\ \hline 45.4 \end{array} \quad \begin{array}{r} 13.1 \\ - 9.4 \\ \hline 3.7 \end{array} \quad \begin{array}{r} 9.7 \\ + 13.0 \\ \hline 22.7 \end{array}$$

Spt. in P.P. 52' East Harding Lexington

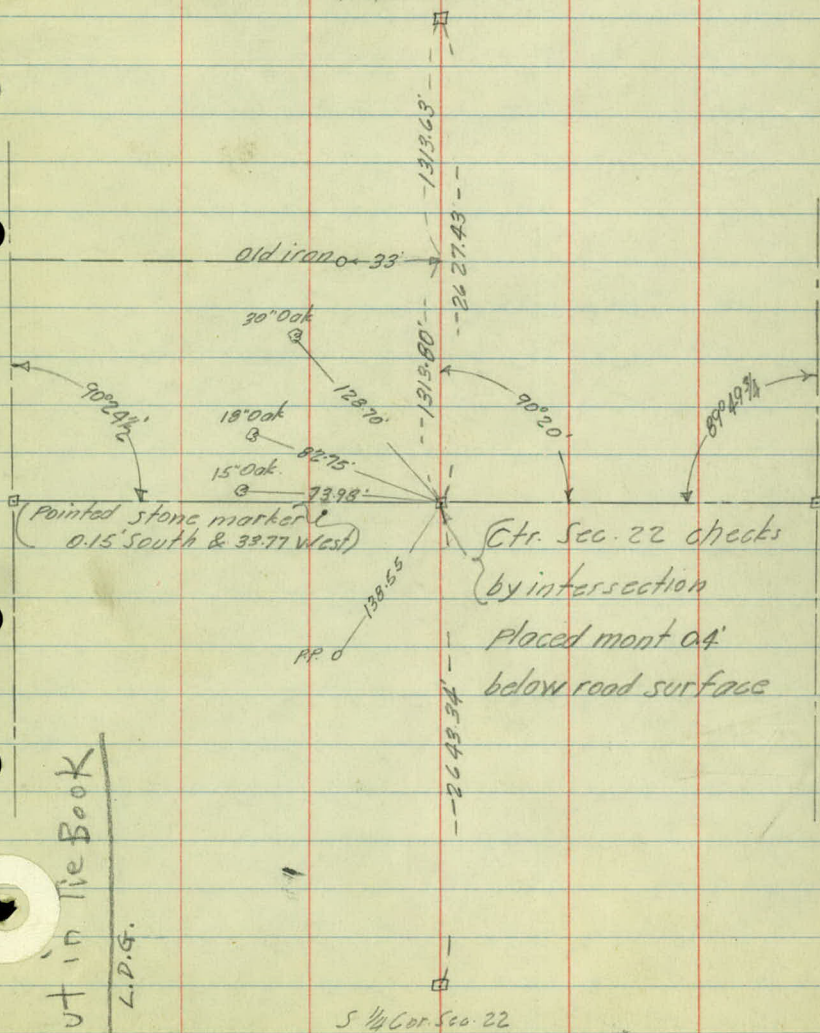


FIELD NOTES - CTR. SEC. 22 T30N R23W

Save: place in Hamline Ave. notes. 6-17-45

K.A.
A.M.
M.B.
C.F.

N $\frac{1}{4}$ Cor. Sec. 22



Put in the Book

