

Dr. G - BK. 112

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN _____ Survey

_____ BEAVER LAKE RD. _____

From Stillwater Rd To Kerwin St.

Road Acc't. No. _____

Date Filed 3-24-37

File _____

PROPOSED PARKWAY

BEAVER LAKE

INDEX

ALIGNMENT. PAGE 1 TO 10

Dr. G - BK. 112

STA. PT. Δ LT. Δ RT.

14+88.43 P.T. 14°-50'

1783.31

N-00°-00'E

+50 13°-41'

14 12°-11'

+50 10°-41'

13 9°-11'

+50 7°-41'

6° C

12+47.00 P.I. 29°-40'

Δ 29°-40' LT.

12 6°-11'

T 253.01

+50 4°-41'

L. 494.44

11 3°-11'

R

+50 1°-41'

10 0°-11'

9+93.99 P.C.

N-29°-40'E

2+49.85 INT. E. & W. 1/4 LINE

1247.00

0+00

153°-00'

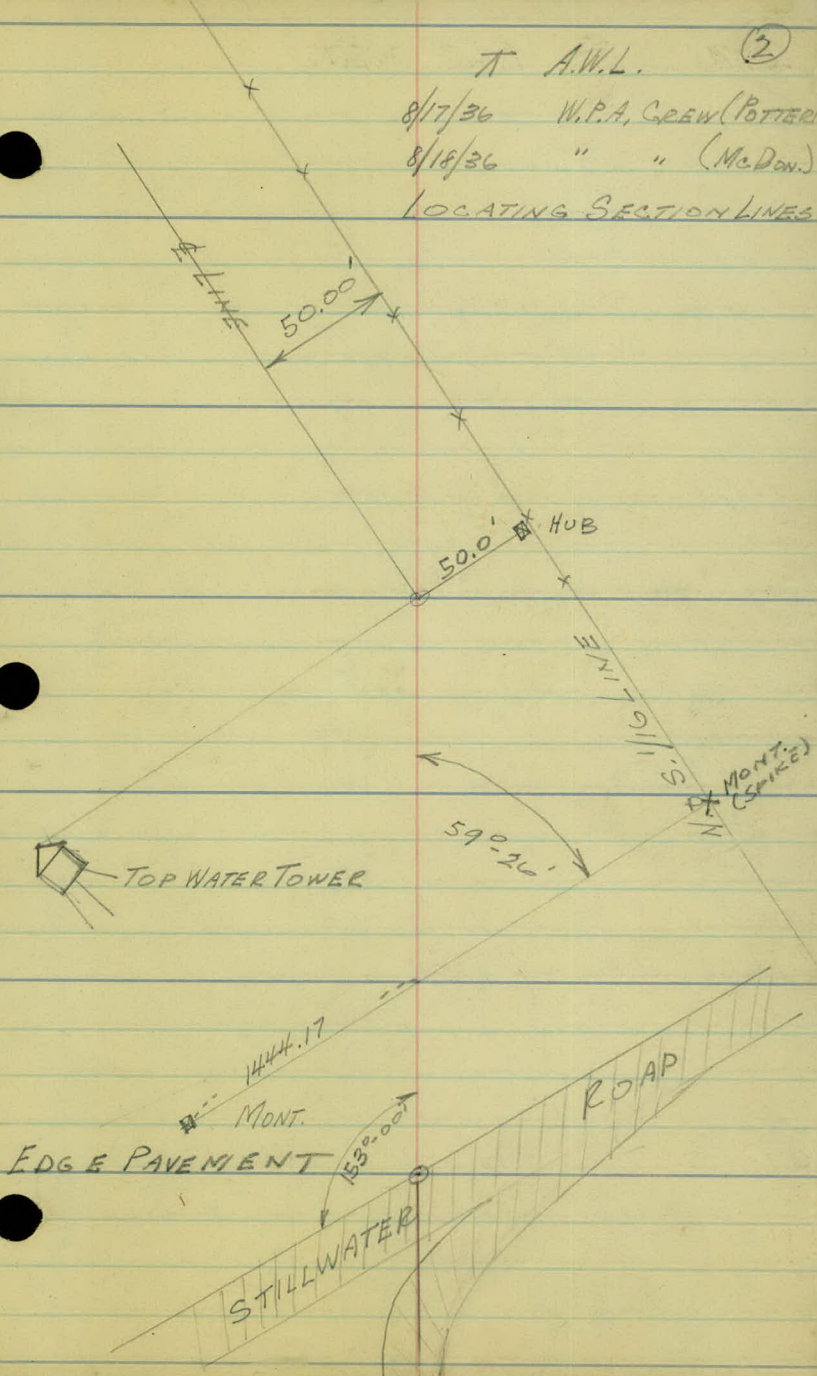
T A.W.L.

(2)

8/17/36 W.P.A. CREW (POTTER)

8/18/36 " " (McDON.)

LOCATING SECTION LINES



STA. P.T. Δ LT. Δ RT.

24+36.08 P.O.T.

395.09

N-21°-16'W

REVISED - SEE - P. 11

23+10.12 P.T.

10°-38'

23

10°-23'

+50

9°-08'

5° C

22+00

7°-53'

Δ 21°-16' L

+50

6°-38'

T - 215.21

21

5°-23'

L 425.33

21+00.00 P.T. 21°-16'

R

+50

4°-08'

20

3°-53'

+50

1°-38'

19

0°-23'

18+84.79 P.C.

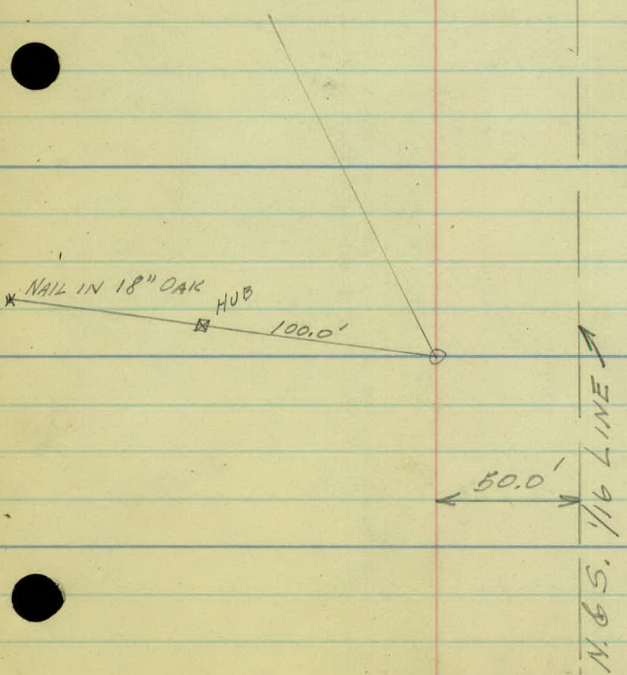
16+69.53 P.O.T.

51.0

T.A.W.L.

(3)

8/19/36 W.P.A. (McDONOUGH)



51.60 HUB

59.20 HUB

STA. PT. Δ LT. Δ RT

350.80
N 15°-16' W

29+34.30 P.T.

15°-30'

29

15°-47'

+50

11°-17'

28

8°-47'

10° C

27+83.40 P.T.

31°-00'

Δ 31°-00' RT

+50

6°-17'

T-159.10

27+00

3°-47'

L-310.00

+50

1°-17'

R.

26+24.30 P.C.

297.76

N 46°-16' W

26+12.82 P.T.

12°-30'

26

11°-52'

10° C

+50

9°-22'

Δ 25°-00' LT.

25

6°-52'

T 127.18'

24+90.00 P.I. 25°-00'

L 250.00'

+50

4°-22'

R

24

1°-52'

23+62.82 P.C.

REVISED - SEE P-11

4

WATER TOWER



HUB

50.0'



WATER TOWER

50.0'

HUB

STA. PT. Δ LT. Δ RT.

2501.90

N 11° 48' S

45+53.75 MONT

REVISED. SEE P. 11

32+49.19 P.T.	37°-46'-30'	
32	31°-37'-	
+50	25°-22'-	25°C
31+26.0 P.I. 75°-33		Δ 75°-33'
31	19°-07'-	T 179.03
+50	12°-52'-	L 302.22
30	6°-37'-	R 231.01
+50	0°-22'-30	
29+46.97 P.C.		

T A.W.L.

(5)

8/20/36 W.P.A. CREW (McD)

49.50

MONT. KNOCKED OVER
SEC. LINE T.P. 59.42

N.W. COR. SEC. 25

90°-56'

MARYLAND ST.

P.T.

BEAVER L. RD.

18.48'

160.55'

P.I.

50.00'

107°11'01"

STA PT. Δ LT. Δ RT.

55+72.06 P.I. $81^{\circ}45'$

+50

55 P.O.C. $23^{\circ}00'$ ✓

+50

54 $20^{\circ}30'$ ✓

+50

53 $18^{\circ}00'$ ✓

+50

52 $15^{\circ}30'$ ✓

+50

51 $13^{\circ}00'$ ✓ $5^{\circ}C$ $\Delta 81^{\circ}45'LT$

+50

T 992.06

50 $10^{\circ}30'$ ✓ L 1635.00'

+50

R.

49 $8^{\circ}00'$ ✓

+50

48 $5^{\circ}30'$ ✓

+50

47+17.42 P.O.T.

47 $3^{\circ}00'$ ✓

+50

46 $0^{\circ}30'$ ✓

45+80.00 P.C.

6

HUB

100.0'

FLAGPOLE
WHITE SCHOOL HO.

GABLE WHITE HOUSE

50.0'

HUB

STA. PT. Δ LT. Δ RT.

2082.51

S-7°-36'W

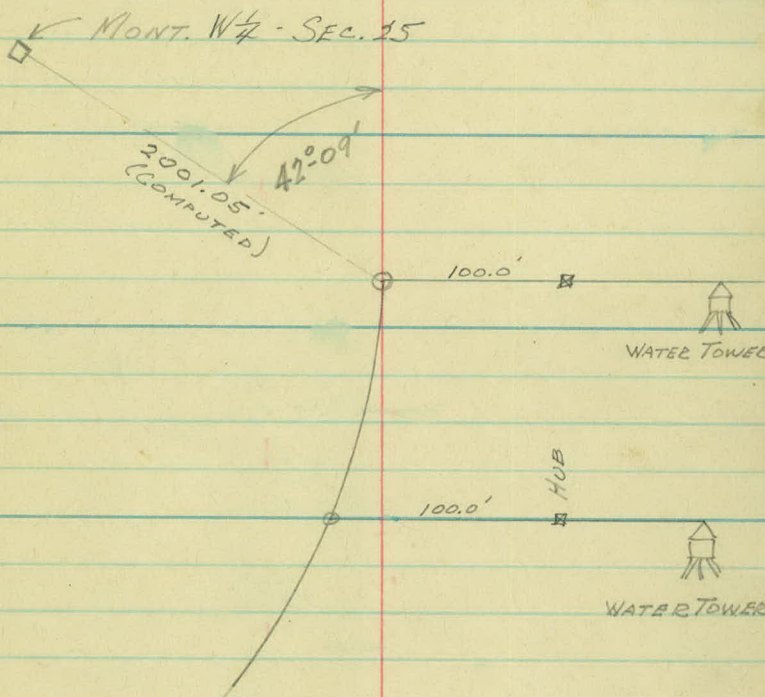
62+15.00	P.T.	40°-52'-30"
62		40°-30'
+50		
61		38°-00'
+50		
60	P.O.C.	35°-30'
+50		
59		33°-00' ✓
+50		
58		30°-30' ✓
+50		
57		28°-00' ✓
+50		
56+00		25°-30' ✓

RAIN

A.W.L.

(7)

8/31/36 W.P.A. (McDONOUGH)



STA. PT. $\Delta L.T.$ $\Delta R.T.$

566.23

S. 20°-49' E

75+82.00 P.T.

14°-07'-30" ✓

+50

13°-19' ✓

75

12°-04' ✓

+50

10°-49' ✓

74

9°-34' ✓ 5°-0

+50

8°-19' ✓ Δ -28°-15' L.T.

73+05.45 P.I. 28°-15'

T-288.45

73

7°-04' ✓ L=565.00

+50

5°-49' ✓

72

4°-34' ✓

+50

3°-19' ✓

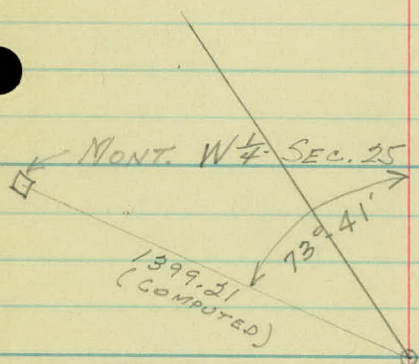
71

2°-04' ✓

+50

0°-49'-30" ✓

70+17.00 P.C.



STA PT. $\Delta L.T.$ $\Delta R.T.$

REVISED

W.L.

81+37.28 P.T. $11^{\circ}38'30''$

81 $10^{\circ}43'$

+50 $9^{\circ}28'$

80 $8^{\circ}13'$

+50 $6^{\circ}58'$

79+07.78 P.I. $23^{\circ}17'$

79 $5^{\circ}43'$

+50 $4^{\circ}28'$

78 $3^{\circ}13'$

+50 $1^{\circ}58'$

77 $0^{\circ}43'$

76+71.61 P.C.

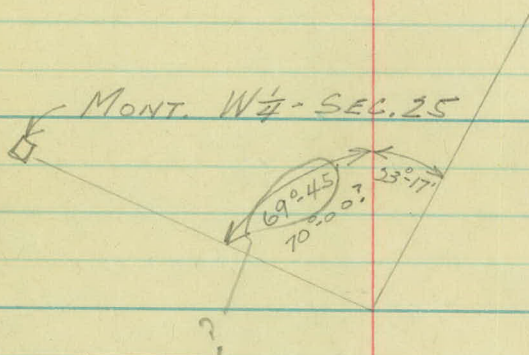
$5^{\circ}-C$

$\Delta-23^{\circ}17'$ R.T.

T-236.17

L-465.67

R-



STA. PT. ALT. DRT.

82+88.30 END N. EDGE PAVEMENT

80+66.69 P.T.

+50

80

+50

79

78+59.78 P.I.

+50

78

+50

77

+50

76+48.02 P.C.

10°-28'

10°-03'

8°-48'

7°-33'

6°-18'

20°-56'

5°-03'

3°-48'

2°-33'

1°-18'

0°-03'

433.37

5°-00'

Δ 20°-56' RT

T- 311.76

L- 418.67

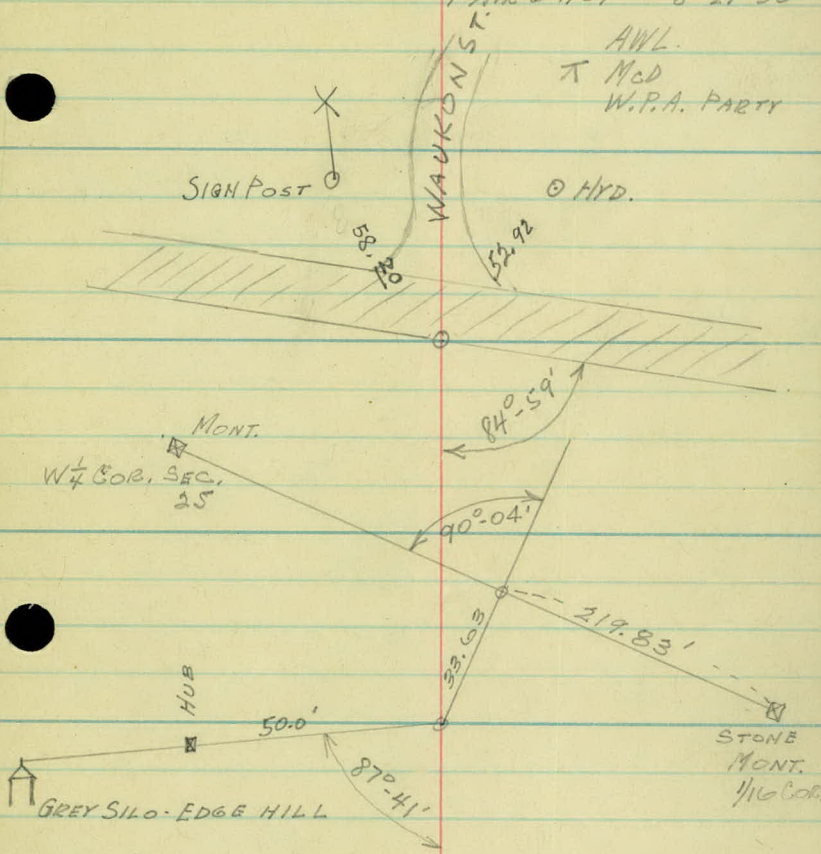
R.

5-0°-07'W

FAIR & HOT - 8-24-36

AWL.

T McD
W.P.A. PARTY



STA. PT. Δ LT. Δ RT
 "B" LINE

2952.77

33+62.23	P.T.	45°-25'	=	32+31.93	"A"
+50		44°-50' ✓			
33		42°-27' ✓			
+50		40°-05' ✓			
32		37°-42' ✓			
+50		35°-20' ✓		9°-30' C	
31		32°-57' ✓		Δ 90°-50' L	
+50		30°-35' ✓		T 612.64	
30+18.73	P.T.	90°-50'		L 950.88	
30		28°-12' ✓		R 603.80	
+50		25°-50' ✓			
29	P.O.C.	23°-27' ✓			
+50		21°-05' ✓			
28		18°-42' ✓			
+50		16°-20' ✓			
27		13°-57' ✓			
+50		11°-35' ✓			
26		9°-12' ✓			
+50		6°-50' ✓			
25		4°-27' ✓			
+50		2°-05' ✓			
24+06.09	P.C.				
21+00.00	P.O.T.				

9-1-36

A.W.L.
BELL
GILLEN

BEAVER L. RD. 1.22'

MARYLAND ST.
SECTION LINE

90°-50'

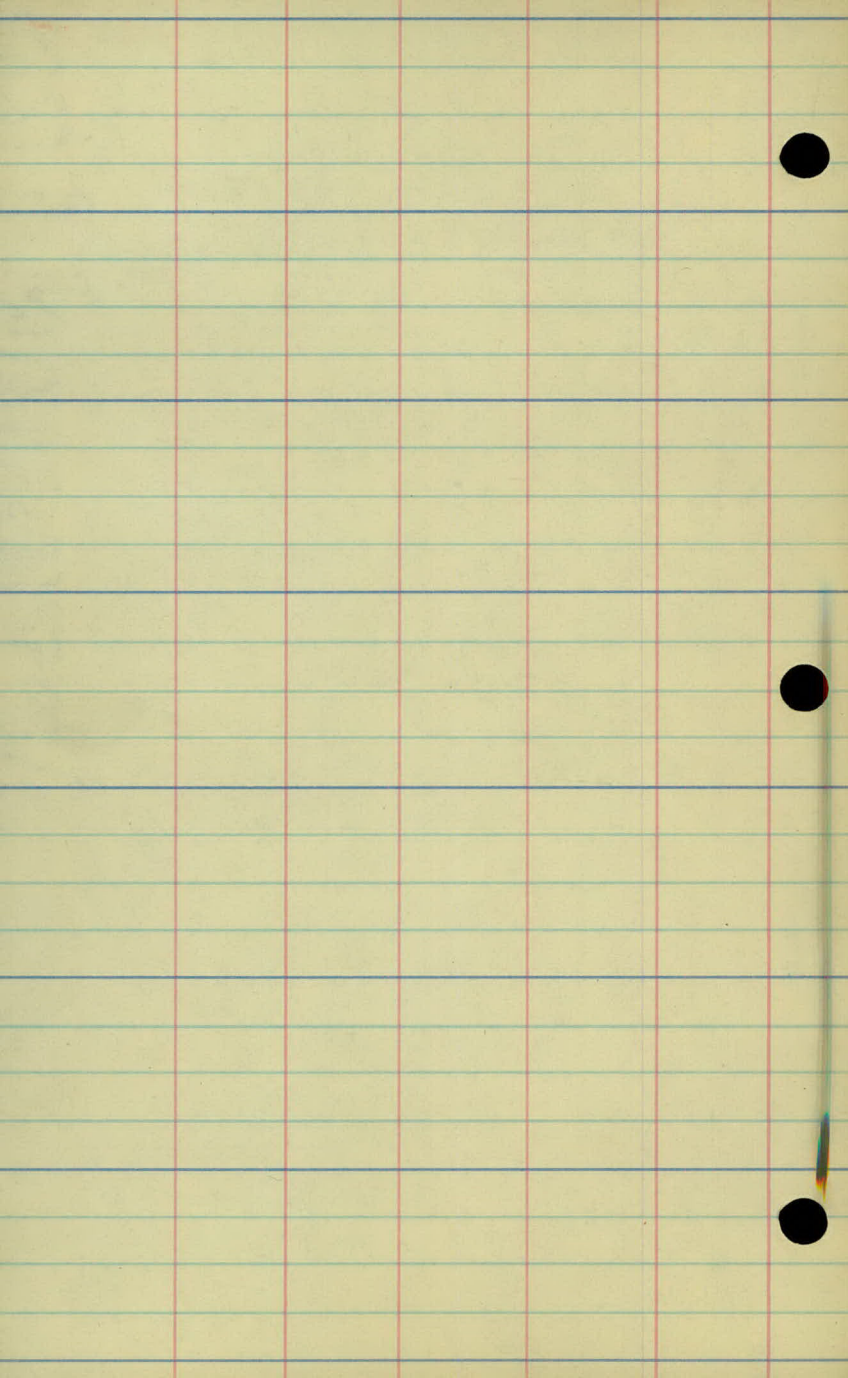
1ST NAT. BANK TOWER

100.00'

STAKE

100.00'

RED IN WILLOW



BEAVER L. PARK

÷ LEVELS ÷

STA.	+	H.I.	—	ROD	ELEV.
B.M.	8.91	984.07			975.16
T.P.	13.07	997.12	0.02		984.05
T.P.	9.95	1006.45	0.62		996.50
T.B.M.				0.24	1006.21
T.P.	1.63	1003.42	4.66		1001.79
T.P.	5.77	997.17	12.02		991.40
				11.24	<u>986.96</u>
T.P.	0.45	987.44	10.18		<u>986.99</u>
T.P.	1.15	977.43	11.16		976.28
				10.24	<u>964.46</u>
T.P.	9.34	973.86	12.91		964.52
T.P.	2.85	967.67	9.04		964.82
T.P.	0.95	955.72	12.90		954.77
T.B.M.				3.62	952.10
T.P.	5.97	955.96	5.73		949.99
T.P.	12.29	967.44	0.81		955.15
T.P.	12.34	978.61	1.17		966.27
				6.25	<u>972.22</u>
T.B.M.					972.22
T.P.			0.57		978.04

8-25-36

13 (2)

CORRECTED BY A.W.L.

SPIKE P.P. COR. EAST AVE. & S. BEAVER L.R.P.

TOP WOOD POST - LT. STA. 3+00

TOP STAKE - P.I. 12+47.00

TOP STUMP - 16+15

TOP FENCE POST. 200' LT. OF STA. 21+00

TOP E. END 36" C.M.

RED LT. 34+50
END TILE IN FOUND. WALL N.E. COR. GARAGE

STA.	+	H.I.	-	ROD	ELEV.
T.P.	10.99	989.03	-		978.04
T.P.	0.38	981.09	8.32		980.71-
B.M.				1.67	979.42-
T.P.	0.83	975.97	5.95		975.14-
T.P.	11.86	975.98	11.85		964.12-
OLD B.M.				0.25	975.58
T.P.	6.06	981.81	0.23		975.75-
T.P.	3.96	981.71	4.06		977.75
T.P.	0.52	977.00	5.23		976.48 ✓
T.B.M.				10.82	966.03
T.P.	1.32	977.80	-		976.48
T.P.	12.35	989.19	0.96		976.84-
T.P.	1.80	986.06	4.93		984.26-
T.B.M.	1.97	983.89	4.14		981.92-
T.P.	0.97	972.13	12.73		971.16-
B.M.				10.56	961.42
			3.96		968.17-

NAIL INT.P. LT. 38+00

TOP CONC. STEPS TO HO. LT. OF 40+00

(975.58) ^{2.2}/₁₅
SPIKE IN P.P. 80' N. OF MONT. N.W COR. SEC. 25

300' LT. STA. 55+00
TOP GRANITE ROCK- FOOT LARGE COTTONWOOD

25'
TOP COLLAR-WATER P. RT. 65+40

NAIL TOP STUMP- 300' LT. STA. 71+00

STA. + H.I. - ROD FLEV.

T.P. 8.12 976.29 - 968.17

T.P. 6.73 977.92' 5.10 977.19 -

B.M. 5.83 ~~977.93~~
~~972.99~~

T.P. 2.91 975.79' 5.04 972.88 -

B.M. 1.56 965.62' 11.73. 963.90

T.P. 6.73 959.77' 12.58 ~~952.88~~
~~953.24~~

T.P. 9.83 964.40' 5.20 954.57 -

T.P. 13.07 976.67' 0.80 963.60 -

T.P. 6.35 981.48' 1.54 975.13 -

B.M. 6.15 975.16
~~975.25~~

15 (4)
8-25-36 FAIRBARM

A.W.L

T J.S.

W.P.A. CREW

P.T. 75+82

TOP $\frac{1}{16}$ MONT. COR.

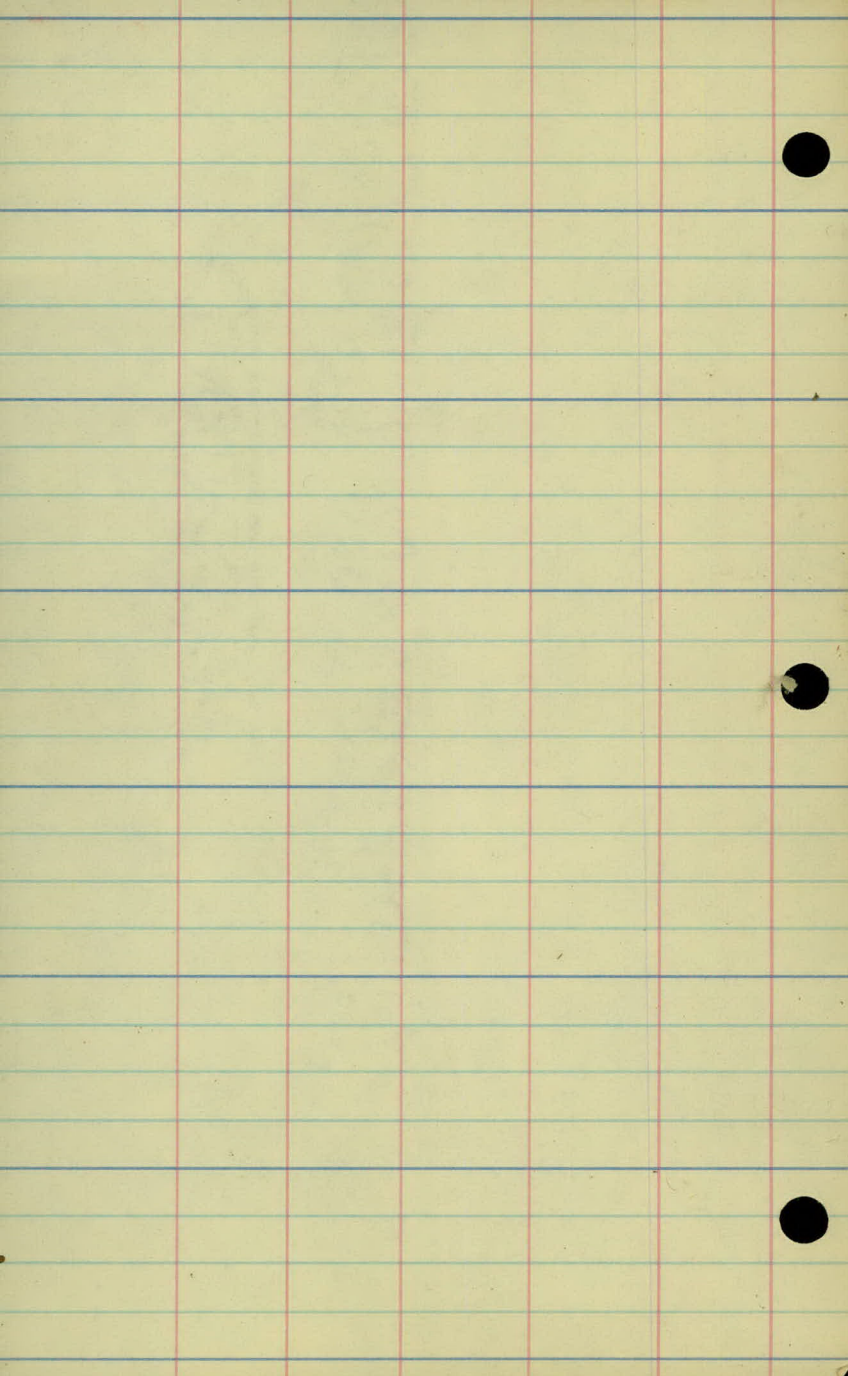
STAKE 80+50

TOP HYD. WAUKON & STILLWATER RD.

N.W. COR, CONC. HEADWALL - N. SIDE R.D.

(975.16)

B.M. P.P. EAST AVE. & S. BEAVER L. RD.



BEAVER L. PARK RD.
X- SECTIONS

STA.	+	H.I.	-	ROD	ELEV.
B.M.	12.52	1018.73			1006.21
0+00					1015.0
+05					-15.0
+50					-11.9
1+00					-13.5
2+00					-12.7
3+00					-10.7
	10.57	1016.78	-		1006.21
4+00					-08.8
5+00					05.8
+50					04.3
6+00					03.9
+50	E GULLEY				96.6
+65	"				96.6
7+00					07.5
8+00					08.3

L.H.

175

17

KT

9-2-36
T.A.W.L.
M.G.
J.B.

(6)
17

B.M. Top of Wood Post-Lt. Sta 3+00

EDGE PAVE.

$$\frac{4.3}{100}$$

$$\frac{3.7}{100}$$

EDGE PAVE.

$$\frac{3.7}{100}$$

$$\frac{3.7}{100}$$

$$\frac{10.3}{100}$$

$$\frac{8.3}{50}$$

$$\frac{8.0}{29}$$

$$\frac{6.8}{100}$$

TO PAVE

$$\frac{9.7}{100}$$

$$\frac{7.0}{68}$$

$$\frac{5.4}{28}$$

$$\frac{5.2}{100}$$

$$\frac{6.0}{14}$$

$$\frac{6.4}{30}$$

$$\frac{7.3}{35}$$

$$\frac{7.3}{42}$$

$$\frac{4.1}{50}$$

PAVE

$$\frac{3.7}{61}$$

$$\frac{12.7}{100}$$

$$\frac{8.2}{50}$$

$$\frac{6.8}{33}$$

$$\frac{6.0}{100}$$

$$\frac{7.0}{35}$$

$$\frac{6.7}{78}$$

$$\frac{6.0}{100}$$

$$\frac{18.7}{100}$$

$$\frac{10.1}{50}$$

$$\frac{8.8}{28}$$

$$\frac{8.0}{100}$$

$$\frac{6.9}{24}$$

$$\frac{6.3}{50}$$

$$\frac{5.5}{100}$$

SAME SLOPE

$$\frac{17.0}{76}$$

$$\frac{11.8}{50}$$

$$\frac{8.2}{78}$$

$$\frac{8.0}{100}$$

$$\frac{5.0}{50}$$

$$\frac{4.0}{100}$$

$$\frac{11.0}{24}$$

$$\frac{7.5}{24}$$

$$\frac{5.5}{30}$$

$$\frac{5.1}{50}$$

$$\frac{4.0}{100}$$

$$\frac{12.5}{100}$$

$$\frac{12.9}{100}$$

$$\frac{5.8}{50}$$

$$\frac{5.0}{61}$$

$$\frac{3.3}{67}$$

$$\frac{4.0}{78}$$

$$\frac{3.6}{100}$$

$$\frac{04.00}{100}$$

$$\frac{20.2}{100}$$

$$\frac{12.8}{50}$$

$$\frac{07.9}{100}$$

$$\frac{20.2}{100}$$

$$\frac{8.9}{80}$$

SAME SLOPE

$$\frac{18.0}{80}$$

$$\frac{13.0}{42}$$

$$\frac{9.3}{100}$$

$$\frac{4.6}{50}$$

$$\frac{2.5}{100}$$

$$\left\{ \begin{array}{l} 1012.3 \\ \text{GULLEY} \\ 4.4 \\ 155 \end{array} \right.$$

$$\frac{18.5}{90}$$

$$\frac{12.3}{50}$$

$$\frac{8.5}{100}$$

$$\frac{6.6}{27}$$

$$\frac{4.4}{50}$$

$$\frac{2.4}{100}$$

STA	+	H.I	-	ROD	ELEV.
9+00	↓				06.0
T.P.	0.40	1004.19	12.99		1003.79
5+00	↓				05.8
6+00	↓				03.9
+25	↓				99.8
+42	↓				96.6 ✓
+60	↓				01.2
+71	↓				04.2
T.P.	12.32	1016.11	0.40		1003.79
9+35	↓				04.1
+75	✓				99.3
10+00	✓				96.1
11+00	✓				80.8
T.P.	0.66	1003.64	13.13		1002.98
9+35	✓				04.1
+75	✓				99.3
10+00	↓				96.1

L.T.

E

R.T.

18 (7)

$$\frac{10.8}{14} \quad \frac{10.0}{14} \quad \frac{5.6}{50} \quad \frac{2.6}{80} \quad \frac{2.1}{100}$$

SAME SLOPE

$$\frac{11.5}{67} \quad \frac{6.7}{50} \quad \frac{03.6}{23} \quad (11.6)$$

$$\frac{23.0}{100} \quad \frac{15.6}{70} \quad \frac{11.4}{50} \quad (0.3)$$

E GOL. E GULLY

$$\frac{23.0}{90} \quad \frac{13.7}{40} \quad \frac{4.4}{10}$$

$$981.2 \quad 940.5$$

$$\frac{7.6}{10}$$

$$\frac{3.0}{10}$$

$$0.0$$

$$\frac{12.0}{25} \quad \frac{9.0}{25} \quad \frac{5.0}{50} \quad \frac{2.6}{70} \quad \frac{1.5}{100}$$

$$\frac{16.8}{50} \quad \frac{6.1}{50} \quad \frac{1.5}{100}$$

$$(20.0) \quad \frac{7.1}{50} \quad \frac{3.7}{75} \quad \frac{2.0}{100}$$

$$(35.3) \quad \frac{16.5}{50} \quad \frac{5.0}{100}$$

SAME SLOPE

$$\frac{12.7}{72} \quad \frac{5.1}{40} \quad (10.5)$$

$$5.5 \quad \frac{19.0}{60} \quad \frac{16.7}{50} \quad (4.3)$$

$$\frac{7.5}{10}$$

1003.64

STA	+	H.I.	-	ROD	ELEV.
10+50				✓	87.34
11+75				✓	74.4
12				✓	75.2
+30				✓	76.7
T.P.	1.23	991.78	13.09		990.55
B.M.				4.84	986.96
10+00	✓			✓	96.1
11+00				✓	80.8
+50				✓	76.2
12+00				✓	75.2
+30				✓	76.7
+50				✓	76.8
13+00				✓	74.4
+50				✓	71.1
14+00				✓	69.2

16.3

(29.8)

$\frac{15.3}{50}$

$\frac{1.1}{100}$

(28.4)

$\frac{13.8}{50}$

$\frac{3.3}{100}$

(26.9)

$\frac{15.9}{33}$

$\frac{13.5}{50}$

$\frac{4.0}{100}$

TOP P.I. STAKE 12+47

$\frac{11.7}{50}$

(+4.3)

11.0

15.6

16.6

15.1

15.0

17.4

$\frac{5.4}{50}$

$\frac{0.0}{79}$

$\frac{+2.0'}{100}$

(20.7)

$\frac{8.3}{50}$

(22.6)

$\frac{8.9}{50}$

$\frac{0.0}{100}$

STA	+	H.I.	-	ROD	ELEV.
T.P.	0.06	978.56	13.28		978.50
10+00	✓			✓	96.1
11+00				✓	80.8
+75				✓	74.4
12				✓	75.2
+30				✓	76.7
13				✓	74.4
+50				✓	71.1
14				✓	69.2
+50				✓	70.0
15				✓	71.1
+50				✓	74.0
16				✓	75.6
T.P.	13.15	989.36	2.35		976.21

$$\checkmark \frac{10.2}{100}$$

$$+17.5$$

10.2

$$\checkmark \frac{18.0}{100}$$

$$\frac{13.2}{60}$$

$$+2.2$$

$$\frac{22.0}{100}$$

$$\frac{15.7}{50}$$

$$\frac{4.2}{100}$$

$$\frac{22.0}{100}$$

$$\frac{16.0}{50}$$

$$3.4$$

$$\frac{21.0}{100}$$

$$\frac{15.9}{50}$$

$$1.9$$

$$\frac{20.0}{100}$$

$$\frac{16.2}{50}$$

$$\frac{10.7}{17}$$

$$4.2$$

$$\frac{16.2}{50}$$

$$\frac{7.5}{100}$$

$$\frac{19.0}{100}$$

$$\frac{15.8}{50}$$

$$\frac{14.6}{28}$$

$$\frac{9.4}{100}$$

$$\frac{16.0}{50}$$

$$\frac{14.2}{24}$$

$$\frac{8.6}{100}$$

$$\frac{0.0}{38}$$

$$\frac{22.0}{100}$$

$$\frac{15.6}{50}$$

$$\frac{7.5}{100}$$

$$\frac{19.3}{100}$$

$$\frac{12.7}{41}$$

$$\frac{4.6}{100}$$

$$\frac{29.0}{100}$$

$$\frac{28.0}{85}$$

$$\frac{15.8}{60}$$

$$\frac{8.0}{34}$$

$$\frac{3.0}{100}$$

(976.38)

STA	+	H.I.	-	ROD	ELEV.
15+00		989.36		✓	71.1
+50				✓	74.0
16				✓	75.6
+70				✓	74.4
17				✓	73.0
18				✓	71.0
+60				✓	70.3
19				✓	70.5
T.P.	0.00	976.17	- 13.19		976.17
16+70				✓	74.4
17+00				✓	73.0
+50				✓	70.9
18+00				✓	71.0
+35				✓	69.7
+60				✓	70.3

L.T.

K.T.

9-5-36
A.W.L.
J.B.
M.G.(10)
21

78.7

(18.3)

 $\frac{10.7}{50}$ $\frac{0.0}{100}$

80.8

(15.4)

 $\frac{8.6}{50}$ $\frac{0.0}{100}$

82.5

(13.8)

 $\frac{6.9}{50}$ $\frac{4.5}{55}$ $\frac{+1.0}{100}$ 15.0 $\frac{7.5}{50}$ $\frac{+2.0}{100}$ 16.4 $\frac{9.2}{50}$ $\frac{0.2}{100}$

84.4

(18.4)

 $\frac{15.0}{50}$ $\frac{7.9}{100}$

76.2

(19.1)

 $\frac{13.2}{50}$ $\frac{8.5}{100}$

71.8

(18.9)

 $\frac{17.6}{15}$ $\frac{13.2}{35}$ $\frac{13.0}{50}$ $\frac{9.3}{100}$

63.1

 $\frac{20.5}{100}$ $\frac{13.1}{50}$

(1.8)

63.5

 $\frac{20.5}{100}$ $\frac{12.7}{50}$

(3.2)

5.3 $\frac{17.3}{100}$ $\frac{11.7}{50}$ 6.2 $\frac{17.0}{100}$ $\frac{11.4}{50}$ 6.5 $\frac{1.2}{50}$ $\frac{21.0}{100}$ $\frac{20.5}{50}$ $\frac{13.1}{26}$ $\frac{7.0}{10}$ 5.9

STA.	+	H.I.	—	ROD	FLEV.
19+00		976.17		✓	70.5
+50				✓	66.2
+82				✓	61.1
E. GULLEY FROM EAST					
T.P.	12.59	976.07	12.69		963.48 -
20				✓	67.0
+30				✓	68.3
21				✓	68.6
+50				✓	68.7
+70				✓	66.7
22				✓	66.9
+35				✓	67.7
T.P.	8.49	972.31	12.25		963.82 -
+80				✓	63.6
23				✓	61.3
+10				✓	58.3
E. DRAW					
+30				✓	59.8

L.T

R.T

71
22

$$\frac{21.0}{100} \quad \frac{19.9}{46} \quad \frac{7.5}{14} \quad \frac{5.7}{1}$$

$$\frac{20.6}{102} \quad \frac{19.5}{63} \quad \frac{10.9}{19} \quad \frac{10.0}{1} \quad \frac{7.7}{10} \quad \frac{6.0}{20} \quad \frac{6.1}{43} \quad \frac{0.0}{98}$$

$$\frac{20.0}{100} \quad \frac{19.0}{50} \quad \frac{17.1}{5} \quad \frac{15.1}{1} \quad \frac{7.8}{9} \quad \frac{5.3}{50} \quad \frac{0.2}{80} \quad \frac{+4.0}{100}$$

$$\frac{19.5}{100} \quad \frac{18.4}{50} \quad \frac{17.5}{21} \quad \frac{14.3}{16} \quad \frac{13.6}{5} \quad \frac{9.1}{1} \quad \frac{7.9}{3} \quad \frac{6.0}{42} \quad \frac{+2.0}{100}$$

$$\frac{18.8}{100} \quad \frac{18.3}{50} \quad \frac{13.1}{34} \quad \frac{11.7}{14} \quad \frac{8.7}{7} \quad \frac{7.8}{1} \quad \frac{6.2}{43} \quad \frac{0.2}{83} \quad \frac{+2.0}{100}$$

$$\frac{17.3}{100} \quad \frac{15.2}{50} \quad \frac{12.2}{32} \quad \frac{9.1}{33} \quad \frac{7.5}{1} \quad \frac{3.0}{50} \quad \frac{0.2}{80} \quad \frac{+2.0}{100}$$

$$\frac{16.5}{100} \quad \frac{14.1}{50} \quad \frac{12.9}{41} \quad \frac{10.4}{34} \quad \frac{9.0}{14} \quad \frac{7.4}{1} \quad \frac{3.5}{50} \quad \frac{+1.0}{100}$$

$$\uparrow \text{ SAME } \frac{14.0}{50} \quad \frac{13.2}{38} \quad \frac{11.1}{32} \quad \frac{9.4}{1} \quad \frac{4.9}{50} \quad \frac{0.0}{100}$$

4 Cr.

$$\frac{17.4}{100} \quad \frac{17.7}{70} \quad \frac{14.7}{50} \quad \frac{13.7}{38} \quad \frac{11.8}{34} \quad \frac{10.2}{11} \quad \frac{9.2}{1} \quad \frac{6.0}{24} \quad \frac{4.4}{50} \quad \frac{1.1}{100}$$

4 Cr.

$$\frac{14.6}{100} \quad \frac{16.4}{70} \quad \frac{17.7}{60} \quad \frac{14.7}{36} \quad \frac{11.8}{19} \quad \frac{8.4}{1} \quad \frac{5.4}{22} \quad \frac{4.1}{50} \quad \frac{1.8}{100}$$

$$\frac{5.3}{100} \quad \frac{11.5}{84} \quad \frac{14.3}{65} \quad \frac{12.7}{56} \quad \frac{12.4}{33} \quad \frac{9.5}{16} \quad \frac{8.7}{1} \quad \frac{7.5}{40} \quad \frac{9.0}{75} \quad \frac{8.3}{100}$$

$$\frac{11.0}{1}$$

$$\frac{14.0}{1}$$

$$\frac{+5.0}{100} \quad \frac{0.0}{92} \quad \frac{13.1}{55} \quad \frac{12.6}{29} \quad \frac{12.5}{1} \quad \frac{12.1}{10} \quad \frac{13.5}{15} \quad \frac{13.6}{50} \quad \frac{13.1}{100}$$

STA.	+	H.I.	-	ROD	ELEV.
		972.31			
23	+55				60.8
24	+06				75.9
	+50				76.8
	+65				75.6
25	+00				72.6
	+50				70.1
T.P.		12.83	983.93	1.21	971.10
24					75.1
	+06				75.9
	+50				76.8
	+65				75.6
25					72.6
	+50				70.1
	+75	DRAW FROM WEST			69.8

$$\begin{array}{r} +9.0 \\ 100 \end{array} \quad \begin{array}{r} +8.7 \\ 86 \end{array} \quad \begin{array}{r} 0.0 \\ 68 \end{array} \quad \begin{array}{r} 8.3 \\ 50 \end{array} \quad \begin{array}{r} 11.0 \\ 32 \end{array} \quad \begin{array}{r} 11.5 \\ 26 \end{array} \quad \begin{array}{r} 11.2 \\ 32 \end{array} \quad \begin{array}{r} 12.2 \\ 86 \end{array} \quad \begin{array}{r} 11.6 \\ 90 \end{array} \quad \begin{array}{r} 13.1 \\ 96 \end{array}$$

$$67.0$$

$$+3.6$$

$$\begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 9.2 \\ 66 \end{array} \quad \begin{array}{r} 11.0 \\ 80 \end{array} \quad \begin{array}{r} 11.2 \\ 100 \end{array}$$

$$69.8$$

$$+4.5$$

$$\begin{array}{r} 2.5 \\ 32 \end{array} \quad \begin{array}{r} 10.9 \\ 59 \end{array} \quad \begin{array}{r} 11.2 \\ 71 \end{array} \quad \begin{array}{r} 13.0 \\ 76 \end{array} \quad \begin{array}{r} 10.7 \\ 81 \end{array} \quad \begin{array}{r} 10.9 \\ 100 \end{array}$$

$$64.5$$

$$+3.3$$

$$\begin{array}{r} 7.8 \\ 25 \end{array} \quad \begin{array}{r} 10.4 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 73 \end{array} \quad \begin{array}{r} 12.2 \\ 76 \end{array} \quad \begin{array}{r} 10.6 \\ 81 \end{array} \quad \begin{array}{r} 9.6 \\ 100 \end{array}$$

$$62.7$$

$$+0.3$$

$$\begin{array}{r} 9.6 \\ 25 \end{array} \quad \begin{array}{r} 10.5 \\ 43 \end{array} \quad \begin{array}{r} 12.2 \\ 50 \end{array} \quad \begin{array}{r} 10.6 \\ 60 \end{array} \quad \begin{array}{r} 10.6 \\ 74 \end{array} \quad \begin{array}{r} 8.7 \\ 100 \end{array}$$

$$70.2$$

$$2.2$$

$$\begin{array}{r} 2.1 \\ 10 \end{array} \quad \begin{array}{r} 5.6 \\ 16 \end{array} \quad \begin{array}{r} 8.0 \\ 25 \end{array} \quad \begin{array}{r} 9.0 \\ 38 \end{array} \quad \begin{array}{r} 11.6 \\ 46 \end{array} \quad \begin{array}{r} 10.2 \\ 50 \end{array} \quad \begin{array}{r} 8.7 \\ 100 \end{array}$$

$$8.8$$

$$\begin{array}{r} 0.0 \\ 100 \end{array} \quad \begin{array}{r} 1.9 \\ 66 \end{array} \quad \begin{array}{r} 1.6 \\ 53 \end{array} \quad \begin{array}{r} 3.2 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 27 \end{array}$$

$$\begin{array}{r} 1.0 \\ 100 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 36 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 8 \end{array} \quad \begin{array}{r} 7.7 \\ 8 \end{array}$$

$$\begin{array}{r} 2.3 \\ 100 \end{array} \quad \begin{array}{r} 5.3 \\ 42 \end{array} \quad \begin{array}{r} 4.7 \\ 31 \end{array} \quad \begin{array}{r} 6.2 \\ 27 \end{array} \quad \begin{array}{r} 8.3 \\ 27 \end{array}$$

$$\begin{array}{r} 4.6 \\ 100 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 9.2 \\ 25 \end{array} \quad \begin{array}{r} 8.8 \\ 14 \end{array} \quad \begin{array}{r} 10.5 \\ 12 \end{array} \quad \begin{array}{r} 11.3 \\ 12 \end{array}$$

$$\begin{array}{r} 7.3 \\ 100 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.9 \\ 100 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array} \quad \begin{array}{r} 17.5 \\ 24 \end{array} \quad \begin{array}{r} 17.2 \\ 50 \end{array} \quad \begin{array}{r} 17.7 \\ 100 \end{array}$$

982.93

STA	+	H.I.	-	ROD	ELEV.
26					70.2
	+50				73.5
27					75.4
	+50				76.7
T.P.	8.62	991.70	0.85		983.08 -
28					79.2 -
	+50				85.1
	+90				89.5
29					89.0
	+25				86.9
	+50				78.6
T.P.	1.07	980.21	12.56		979.14 -
	+65				77.4
30+00					65.8
T.P.	1.00	967.75	13.46		966.75 -
	+50				57.8
31+00					54.0

L.T.

E

K.T.

24

15

$$\frac{8.2}{100} \quad \frac{9.0}{50} \quad \frac{13.7}{50} \quad \frac{13.3}{27} \quad \frac{15.7}{32} \quad \frac{15.7}{50} \quad \frac{14.8}{100}$$

$$\frac{10.3}{50} \quad \frac{10.4}{50} \quad \frac{9.6}{37} \quad \frac{10.7}{42} \quad \frac{10.7}{50}$$

$$\frac{8.5}{100} \quad \frac{9.1}{31} \quad \frac{8.5}{50} \quad \frac{7.0}{50} \quad \frac{7.5}{55} \quad \frac{7.3}{100}$$

$$\frac{7.2}{50}$$

$$\frac{12.4}{100} \quad \frac{12.6}{50} \quad \frac{12.5}{50} \quad \frac{11.9}{34} \quad \frac{7.0}{100}$$

$$\frac{8.0}{100} \quad \frac{6.4}{50} \quad \frac{6.6}{50} \quad \frac{7.6}{50} \quad \frac{6.4}{100}$$

$$\frac{6.3}{100} \quad \frac{2.0}{38} \quad \frac{2.2}{50} \quad \frac{3.2}{50} \quad \frac{2.4}{100}$$

$$\frac{2.7}{50}$$

$$\frac{9.8}{100} \quad \frac{7.6}{50} \quad \frac{4.8}{50} \quad \frac{5.0}{50} \quad \frac{6.2}{100}$$

$$\frac{16.3}{100} \quad \frac{14.7}{50} \quad \frac{12.5}{29} \quad \frac{13.3}{11} \quad \frac{13.1}{50} \quad \frac{12.7}{6} \quad \frac{8.9}{50} \quad \frac{12.1}{100}$$

$$\frac{6.7}{100} \quad \frac{6.0}{50} \quad \frac{2.8}{50} \quad \frac{1.5}{50} \quad \frac{2.9}{100}$$

$$\frac{17.5}{100} \quad \frac{16.0}{50} \quad \frac{14.4}{50} \quad \frac{10.3}{50} \quad \frac{7.0}{84} \quad \frac{7.2}{100}$$

$$\frac{13.8}{100} \quad \frac{12.8}{50} \quad \frac{9.9}{50} \quad \frac{5.8}{50} \quad \frac{1.00}{100}$$

$$\frac{15.4}{100} \quad \frac{15.4}{50} \quad \frac{13.7}{50} \quad \frac{10.6}{50} \quad \frac{5.7}{100}$$

967.75

STA.	+	H.I.	-	ROD	ELEV.
+50					52.9

32+00					52.7
-------	--	--	--	--	------

32+50					52.9
-------	--	--	--	--	------

33					53.1
----	--	--	--	--	------

+50	± RD. N. & S.				56.3
-----	---------------	--	--	--	------

EQUATION $\left\{ \begin{array}{l} 33+62.23 \\ 32+31.93 \end{array} \right.$

32+50					56.5
-------	--	--	--	--	------

33+00					61.0
-------	--	--	--	--	------

T.P.	8.68	974.74	- 1.69		966.06 -
------	------	--------	--------	--	----------

+60					65.9 -
-----	--	--	--	--	--------

34					69.5
----	--	--	--	--	------

+40					73.4
-----	--	--	--	--	------

+70					75.0
-----	--	--	--	--	------

T.P.	13.64	987.19	- 1.19		973.55 -
------	-------	--------	--------	--	----------

B.M.				CORRECTED 15.03	972.22 972.16
------	--	--	--	--------------------	------------------

+70					75.0
-----	--	--	--	--	------

35					75.6
----	--	--	--	--	------

L.T.

4

R.T.

77.7
25

14.8

$$\frac{16.3}{100} \quad \frac{15.7}{50} \quad \frac{15.0}{50} \quad \frac{14.0}{50} \quad \frac{12.8}{100}$$

$$\frac{16.9}{100} \quad \frac{15.9}{50} \quad \frac{14.8}{50} \quad \frac{14.0}{50} \quad \frac{13.3}{100}$$

$$\frac{16.4}{100} \quad \frac{16.3}{50} \quad \frac{14.6}{50} \quad \frac{13.1}{50} \quad \frac{12.6}{100}$$

$$\frac{15.7}{100} \quad \frac{14.1}{50} \quad \frac{11.4}{50} \quad \frac{10.0}{50} \quad \frac{9.8}{100}$$

$$\frac{16.1}{100} \quad \frac{14.4}{50} \quad \frac{11.2}{50} \quad \frac{9.2}{21} \quad \frac{8.1}{50} \quad \frac{7.5}{100}$$

13'R

$$\frac{15.6}{100} \quad \frac{11.8}{50} \quad \frac{8.7}{6} \quad \frac{6.7}{50} \quad \frac{7.1}{19} \quad \frac{4.2}{31} \quad \frac{3.2}{50} \quad \frac{2.4}{100} \quad \frac{0.6}{\text{PORCH}}$$

$$\frac{25.0}{100} \quad \frac{18.6}{50} \quad \frac{12.9}{22} \quad \frac{9.4}{3} \quad \frac{8.8}{50} \quad \frac{8.7}{21} \quad \frac{7.0}{35} \quad \frac{6.7}{50} \quad \frac{10.0}{100}$$

8'R

$$\frac{14.8}{50} \quad \frac{8.2}{24} \quad \frac{5.3}{4} \quad \frac{5.2}{50} \quad \frac{5.7}{22} \quad \frac{4.6}{26} \quad \frac{5.7}{50}$$

$$\frac{22.0}{100} \quad \frac{11.3}{50} \quad \frac{5.5}{29} \quad \frac{3.5}{12} \quad \frac{1.3}{50} \quad \frac{1.4}{22} \quad \frac{+0.5}{26} \quad \frac{+0.3}{50} \quad \frac{2.1}{100}$$

$$\frac{18.3}{100} \quad \frac{9.1}{42} \quad \frac{5.2}{32} \quad \frac{2.2}{7} \quad \frac{+0.3}{3} \quad \frac{+0.3}{50}$$

(972.36)

END TILE IN FOUND. WALL GARAGE

75.4 LT. 35+00

$$\frac{(12.2)}{20} \quad \frac{11.8}{23} \quad \frac{10.2}{31} \quad \frac{10.1}{50} \quad \frac{8.0}{50} \quad \frac{6.2}{100}$$

$$\frac{30.0}{100} \quad \frac{20.2}{50} \quad \frac{14.3}{7} \quad \frac{11.6}{50} \quad \frac{10.9}{21} \quad \frac{10.4}{30} \quad \frac{9.5}{43} \quad \frac{2.8}{100}$$

8'R

STA.	+	H.I.	-	ROD	ELEV.
		987.19			
+55	YARD				78.9
+67					79.8
T.P.	7.34	992.92	-1.61		985.58
36+00					82.8
+50					85.6
37+00					84.3
T.P.	6.29	986.49	-12.72		980.20
38+00					78.4
+50					76.5
T.P.	3.22	978.79	-10.92		975.57
39+00					75.5
+55					76.1
40+00					76.0
+50					75.1
41+00					74.3
+70					70.2
T.P.	12.99	986.51	-5.27	973.52	-

L.T.

4

R.T.

15
26

$\frac{13.6}{100}$	$\frac{11.6}{50}$	$\frac{10.0}{14}$	$\frac{8.3}{2}$	$\frac{8.3}{10}$	$\frac{8.0}{10}$	$\frac{7.0}{31}$	$\frac{7.1}{50}$	$\frac{0.0}{100}$
--------------------	-------------------	-------------------	-----------------	------------------	------------------	------------------	------------------	-------------------

$\frac{16.0}{100}$	$\frac{7.7}{50}$	$\frac{3.5}{14}$	$\frac{7.2}{5}$	$\frac{7.4}{20}$	$\frac{7.0}{20}$	$\frac{5.0}{27}$	$\frac{7.2}{44}$	$\frac{5.7}{62}$	$\frac{3.0}{100}$
--------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	-------------------

7'R

$\frac{19.8}{100}$	$\frac{9.3}{50}$	$\frac{4.3}{27}$	$\frac{3.9}{11}$	$\frac{9.9}{4}$	$\frac{10.1}{24}$	$\frac{9.8}{24}$	$\frac{6.4}{29}$	$\frac{13.1}{66}$	$\frac{11.5}{100}$
--------------------	------------------	------------------	------------------	-----------------	-------------------	------------------	------------------	-------------------	--------------------

4'R

$\frac{24.0}{100}$	$\frac{8.8}{50}$	$\frac{4.3}{32}$	$\frac{2.7}{12}$	$\frac{7.3}{6}$	$\frac{7.3}{14}$	$\frac{7.5}{14}$	$\frac{4.4}{18}$	$\frac{6.0}{37}$	$\frac{13.8}{80}$	$\frac{14.0}{100}$
--------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	-------------------	--------------------

1'R

$\frac{22.5}{100}$	$\frac{8.1}{50}$	$\frac{5.5}{14}$	$\frac{8.5}{10}$	$\frac{8.6}{12}$	$\frac{8.7}{12}$	$\frac{7.9}{15}$	$\frac{13.4}{42}$	$\frac{16.6}{70}$	$\frac{15.8}{100}$
--------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------	-------------------	--------------------

2'L

$\frac{11.3}{100}$	$\frac{5.0}{50}$	$\frac{6.1}{17}$	$\frac{8.3}{14}$	$\frac{8.1}{10}$	$\frac{8.3}{10}$	$\frac{10.4}{14}$	$\frac{11.4}{31}$	$\frac{10.6}{45}$	$\frac{2.6}{110}$
--------------------	------------------	------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{12.4}{100}$	$\frac{6.2}{50}$	$\frac{7.3}{17}$	$\frac{9.4}{14}$	$\frac{10.0}{10}$	$\frac{9.6}{10}$	$\frac{13.4}{23}$	$\frac{10.6}{50}$	$\frac{5.6}{100}$
--------------------	------------------	------------------	------------------	-------------------	------------------	-------------------	-------------------	-------------------

3'L

$\frac{13.1}{100}$	$\frac{7.9}{50}$	$\frac{6.5}{18}$	$\frac{3.5}{11}$	$\frac{3.3}{9}$	$\frac{3.5}{9}$	$\frac{8.2}{17}$	$\frac{9.0}{50}$	$\frac{6.8}{100}$
--------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	-------------------

$\frac{9.8}{100}$	$\frac{4.9}{72}$	$\frac{2.5}{50}$	$\frac{1.6}{17}$	$\frac{2.8}{14}$	$\frac{2.7}{11}$	$\frac{2.9}{11}$	$\frac{6.3}{50}$	$\frac{9.2}{100}$
-------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------

3'L

$\frac{13.0}{100}$	$\frac{3.4}{72}$	$\frac{1.7}{50}$	$\frac{0.8}{18}$	$\frac{3.0}{11}$	$\frac{2.8}{11}$	$\frac{2.8}{11}$	$\frac{2.1}{13}$	$\frac{7.0}{50}$	$\frac{10.4}{75}$	$\frac{10.8}{100}$
--------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	-------------------	--------------------

$\frac{3.3}{17}$	$\frac{3.7}{10}$	$\frac{3.9}{9}$	$\frac{10.2}{50}$	$\frac{12.3}{67}$	$\frac{11.5}{90}$	$\frac{10.0}{100}$
------------------	------------------	-----------------	-------------------	-------------------	-------------------	--------------------

$\frac{4.5}{15}$	$\frac{4.5}{11}$	$\frac{5.2}{8}$	$\frac{4.4}{11}$	$\frac{12.7}{50}$	$\frac{12.6}{75}$	$\frac{10.7}{100}$
------------------	------------------	-----------------	------------------	-------------------	-------------------	--------------------

$\frac{7.7}{20}$	$\frac{8.6}{10}$	$\frac{8.5}{10}$	$\frac{15.1}{55}$	$\frac{14.5}{100}$
------------------	------------------	------------------	-------------------	--------------------

		986.5		
STA.	+	H.I.	-	ROD ELEV.
40+50				75.1
41				74.3
+70				70.2
42				68.1
T.P.	6.89	980.41	12.99	973.52 -
B.M.			4.91	975.50 - }
B.M.	0.85	976.43		975.58 }
42+00				68.1
+50				65.3
43				63.8
+63		12" C.M. X COLV.		63.7
44				63.8
+70				65.0
45				66.2
+57				71.4
+70		± EAST AVE.		72.6

L.T.

4

P.T.

(16)

27

$$\begin{array}{r} 13.8 \\ 100 \end{array} \quad \begin{array}{r} 10.4 \\ 90 \end{array} \quad \begin{array}{r} 10.4 \\ 75 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 79.1 \\ 7.4 \\ 20 \end{array} \quad (11.4)$$

$$\begin{array}{r} 13.8 \\ 100 \end{array} \quad \begin{array}{r} 6.5 \\ 70 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 30 \end{array} \quad \begin{array}{r} 76.7 \\ 9.8 \\ 21 \end{array} \quad (12.2)$$

$$\begin{array}{r} 7.4 \\ 100 \end{array} \quad \begin{array}{r} 3.2 \\ 75 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 28 \end{array} \quad \begin{array}{r} 74.8 \\ 11.7 \\ 26 \end{array} \quad (16.3)$$

$$\begin{array}{r} 6.2 \\ 100 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array} \quad \begin{array}{r} 14.3 \\ 20 \end{array} \quad (18.4)$$

9-4-36
T.A.W.L.
J.B.
M.G.

(975.58) SPIKE P.P. 80' N. OF 45+50

$$\begin{array}{r} 8.1 \\ 19 \end{array} \quad \begin{array}{r} 8.3 \\ 3 \end{array} \quad \begin{array}{r} 8.7 \\ 7 \end{array} \quad \begin{array}{r} 10.2 \\ 50 \end{array} \quad \begin{array}{r} 13.5 \\ 100 \end{array} \quad \begin{array}{r} 13.7 \\ 100 \end{array}$$

$$\begin{array}{r} 1.2 \\ 100 \end{array} \quad \begin{array}{r} 2.4 \\ 77 \end{array} \quad \begin{array}{r} 4.4 \\ 70 \end{array} \quad \begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 12.3 \\ 35 \end{array} \quad \begin{array}{r} 12.3 \\ 21 \end{array} \quad \begin{array}{r} 11.1 \\ 18 \end{array} \quad \begin{array}{r} 11.1 \\ 2 \end{array} \quad \begin{array}{r} 13.5 \\ 6 \end{array} \quad \begin{array}{r} 14.6 \\ 50 \end{array} \quad \begin{array}{r} 14.4 \\ 100 \end{array}$$

$$\begin{array}{r} 4.3 \\ 100 \end{array} \quad \begin{array}{r} 9.3 \\ 85 \end{array} \quad \begin{array}{r} 12.8 \\ 68 \end{array} \quad \begin{array}{r} 14.4 \\ 50 \end{array} \quad \begin{array}{r} 14.4 \\ 21 \end{array} \quad \begin{array}{r} 12.3 \\ 17 \end{array} \quad \begin{array}{r} 12.6 \\ 2 \end{array} \quad \begin{array}{r} 12.6 \\ 6 \end{array} \quad \begin{array}{r} 14.5 \\ 50 \end{array} \quad \begin{array}{r} 14.8 \\ 50 \end{array} \quad \begin{array}{r} 14.8 \\ 100 \end{array}$$

$$\begin{array}{r} 60.4 \\ \text{F.L. COLV.} \\ 16.0 \\ 30 \end{array} \quad \begin{array}{r} 12.7 \\ 12 \end{array} \quad \begin{array}{r} 60.8 \\ \text{F.L. COLV.} \\ 15.6 \\ 12 \end{array}$$

$$\begin{array}{r} 14.7 \\ 100 \end{array} \quad \begin{array}{r} 15.5 \\ 50 \end{array} \quad \begin{array}{r} 15.0 \\ 15 \end{array} \quad \begin{array}{r} 13.1 \\ 12 \end{array} \quad \begin{array}{r} 12.6 \\ 5 \end{array} \quad \begin{array}{r} 13.1 \\ 8 \end{array} \quad \begin{array}{r} 14.7 \\ 50 \end{array} \quad \begin{array}{r} 14.4 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 100 \end{array}$$

$$\begin{array}{r} 14.6 \\ 100 \end{array} \quad \begin{array}{r} 14.9 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 23 \end{array} \quad \begin{array}{r} 12.0 \\ 10 \end{array} \quad \begin{array}{r} 11.4 \\ 7 \end{array} \quad \begin{array}{r} 11.6 \\ 14 \end{array} \quad \begin{array}{r} 13.9 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ 100 \end{array} \quad \begin{array}{r} 10.2 \\ 100 \end{array}$$

$$\begin{array}{r} 14.2 \\ 100 \end{array} \quad \begin{array}{r} 13.4 \\ 50 \end{array} \quad \begin{array}{r} 11.5 \\ 17 \end{array} \quad \begin{array}{r} 10.2 \\ 11 \end{array} \quad \begin{array}{r} 10.2 \\ 7 \end{array} \quad \begin{array}{r} 10.0 \\ 10 \end{array} \quad \begin{array}{r} 11.0 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 75 \end{array} \quad \begin{array}{r} 10.4 \\ 75 \end{array} \quad \begin{array}{r} 8.1 \\ 100 \end{array}$$

$$\begin{array}{r} 12.2 \\ 100 \end{array} \quad \begin{array}{r} 10.6 \\ 60 \end{array} \quad \begin{array}{r} 6.9 \\ 30 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad \begin{array}{r} 5.0 \\ 19 \end{array} \quad \begin{array}{r} 4.5 \\ 29 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 100 \end{array} \quad \begin{array}{r} 0.3 \\ 100 \end{array}$$

$$\begin{array}{r} 3.8 \\ 50 \end{array} \quad \begin{array}{r} 2.3 \\ 100 \end{array} \quad \begin{array}{r} 0.0 \\ 100 \end{array}$$

STA.	+	H.I.	-	ROD	ELEV.
		976.43			
45+80					73.1
46					75.0
+40					77.1
T.P.	10.92	986.68	0.07		976.36
45+80					73.3
46+40					77.1
47					79.2
+50					78.3
48+00		3 E.G. SWAMP			73.1
T.P.	8.11	981.91	12.88		973.80
+50					70.2
INLET	20" VIT. CULV.			10.0	71.9
49+00					70.4
+50					69.4
50+00					76.8
+30					80.3

$$\frac{12.6}{100} \quad \frac{12.0}{83} \quad \frac{8.5}{50} \quad \frac{5.4}{25} \quad \frac{3.3}{}$$

$$\frac{1.4}{}$$

$$\frac{11.9}{100} \quad \frac{11.0}{75} \quad \frac{68.7}{50} \quad (40.8)$$

$$\frac{13.4}{5} \quad \frac{13.2}{5} \quad \frac{11.8}{10} \quad \frac{9.9}{50} \quad \frac{7.3}{100}$$

$$\frac{9.6}{18} \quad \frac{8.2}{18} \quad \frac{7.2}{22} \quad \frac{5.11}{50} \quad \frac{2.2}{100}$$

$$\frac{16.0}{100} \quad \frac{16.1}{77} \quad \frac{9.8}{27} \quad \frac{7.5}{39} \quad \frac{4.9}{39} \quad \frac{2.5}{67} \quad \frac{3.7}{100}$$

$$\frac{13.8}{100} \quad \frac{11.4}{76} \quad \frac{10.5}{50} \quad \frac{8.4}{50} \quad \frac{8.0}{50} \quad \frac{9.7}{100}$$

$$\frac{11.5}{100} \quad \frac{11.0}{50} \quad \frac{11.8}{18} \quad \frac{13.6}{18} \quad \frac{13.9}{18} \quad \frac{10.5}{54} \quad \frac{9.4}{66} \quad \frac{11.2}{100}$$

$$\frac{8.5}{100} \quad \frac{11.1}{50} \quad \frac{11.7}{35} \quad \frac{9.4}{35} \quad \frac{6.6}{44} \quad \frac{5.7}{60} \quad \frac{4.5}{66} \quad \frac{6.1}{100}$$

$$\frac{8.6}{100} \quad \frac{8.8}{90} \quad \frac{12.1}{50} \quad \frac{12.6}{20} \quad \frac{11.5}{20} \quad \frac{10.3}{20} \quad \frac{6.7}{38} \quad \frac{5.8}{81} \quad \frac{7.2}{100}$$

$$\frac{7.7}{100} \quad \frac{7.4}{74} \quad \frac{9.7}{50} \quad \frac{11.2}{24} \quad \frac{10.5}{17} \quad \frac{8.4}{17} \quad \frac{6.7}{28} \quad \frac{5.1}{50} \quad \frac{7.8}{81} \quad \frac{7.8}{100}$$

$$\frac{6.9}{100} \quad \frac{6.0}{50} \quad \frac{5.0}{36} \quad \frac{6.0}{23} \quad \frac{5.1}{31} \quad \frac{3.7}{31} \quad \frac{5.2}{50} \quad \frac{7.1}{100}$$

$$\frac{3.6}{100} \quad \frac{2.9}{50} \quad \frac{2.4}{11} \quad \frac{1.6}{33} \quad \frac{1.4}{33} \quad \frac{0.8}{35} \quad \frac{4.1}{100}$$

STA.	+	H.I.	-	ROD	ELEV.
		981.91			
51+00					77.5
+50					77.9
52+00					78.2
+50					76.5
53+00					73.4
+50					73.8
54+00					74.1
T.P.	13.90	989.71	6.10		975.81
51+00					77.5
+50					77.9
52+00					78.2
+50					76.5
53					73.4
+50					73.8

L.T.

F

R.T.

78
29

$$\frac{3.6}{100} \quad \frac{4.8}{50} \quad \frac{4.4}{15} \quad \frac{4.0}{15} \quad \frac{0.4}{47}$$

$$\frac{4.6}{100} \quad \frac{4.2}{71} \quad \frac{6.1}{42} \quad \frac{6.2}{78} \quad \frac{4.0}{15}$$

$$\frac{8.8}{100} \quad \frac{7.6}{77} \quad \frac{9.7}{50} \quad \frac{9.7}{36} \quad \frac{3.7}{15}$$

$$\frac{13.7}{100} \quad \frac{13.7}{50} \quad \frac{11.2}{25} \quad \frac{5.4}{15}$$

$$\frac{14.4}{100} \quad \frac{13.7}{50} \quad \frac{13.1}{38} \quad \frac{8.5}{15} \quad \frac{4.8}{29}$$

$$\frac{12.0}{100} \quad \frac{11.0}{50} \quad \frac{8.1}{15} \quad \frac{5.4}{50}$$

$$\frac{10.5}{100} \quad \frac{9.7}{50} \quad \frac{7.8}{15} \quad \frac{4.9}{50} \quad \frac{0.0}{100}$$

$$\frac{83.6}{100}$$

$$(12.2) \quad \frac{6.1}{68} \quad \frac{6.9}{100}$$

$$\frac{87.8}{100}$$

$$(11.8) \quad \frac{1.9}{50} \quad \frac{1.3}{66} \quad \frac{4.0}{100}$$

$$\frac{88.3}{100}$$

$$(11.5) \quad \frac{1.4}{50} \quad \frac{1.8}{66} \quad \frac{8.2}{100}$$

$$\frac{85.0}{100}$$

$$(13.2) \quad \frac{4.7}{50} \quad \frac{9.4}{100}$$

$$\frac{77.6}{100}$$

$$(16.3) \quad \frac{12.1}{50} \quad \frac{9.7}{100}$$

$$(15.9) \quad \frac{77.7}{12.0} \quad \frac{100}{100}$$

STA.	+	H.I.	-	ROD	ELEV.
		989.71			
54+40					75.6
+80					79.7
55+00					79.7
+50					76.4
56+00	/				74.6
+50					73.7
57+00					75.4
+50					80.3
58					85.0
T.P.	4.96	992.58	2.09		987.62
59+00					88.4
+50					89.5
60+00					89.1
61+00					87.2

L.T.

E

R.T.

49
30

87.8

$$\begin{array}{r} 14.0 \\ 100 \end{array} \quad \begin{array}{r} 13.6 \\ 50 \end{array} \quad \begin{array}{r} 14.5 \\ 24 \end{array} \quad \begin{array}{r} 14.1 \\ \hline \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 1.9 \\ 100 \end{array}$$

$$\begin{array}{r} 14.2 \\ 100 \end{array} \quad \begin{array}{r} 11.4 \\ 50 \end{array} \quad \begin{array}{r} 10.0 \\ \hline \end{array} \quad \begin{array}{r} 8.8 \\ 24 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array} \quad \begin{array}{r} 1.0 \\ 100 \end{array}$$

10.0

$$\begin{array}{r} 20.3 \\ 100 \end{array} \quad \begin{array}{r} 16.3 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ \hline \end{array} \quad \begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 100 \end{array}$$

$$\begin{array}{r} 21.5 \\ 100 \end{array} \quad \begin{array}{r} 18.4 \\ 50 \end{array} \quad \begin{array}{r} 15.1 \\ \hline \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 9.6 \\ 100 \end{array}$$

$$\begin{array}{r} 21.4 \\ 100 \end{array} \quad \begin{array}{r} 18.0 \\ 50 \end{array} \quad \begin{array}{r} 16.0 \\ \hline \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 8.6 \\ 100 \end{array}$$

$$\begin{array}{r} 19.5 \\ 100 \end{array} \quad \begin{array}{r} 15.9 \\ 50 \end{array} \quad \begin{array}{r} 14.3 \\ \hline \end{array} \quad \begin{array}{r} 10.7 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 100 \end{array}$$

$$\begin{array}{r} 16.3 \\ 100 \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array} \quad \begin{array}{r} 2.8 \\ 100 \end{array}$$

$$\begin{array}{r} 12.0 \\ 100 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ \hline \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 0.5 \\ 100 \end{array}$$

$$\begin{array}{r} 6.2 \\ 100 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ \hline \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 2.3 \\ 100 \end{array}$$

$$\begin{array}{r} 2.2 \\ 100 \end{array} \quad \begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 3.1 \\ \hline \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 3.2 \\ 100 \end{array}$$

$$\begin{array}{r} 2.4 \\ 100 \end{array} \quad \begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ \hline \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 3.4 \\ 100 \end{array}$$

$$\begin{array}{r} 4.5 \\ 100 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 100 \end{array}$$

STA.	+	H.I.	-	ROD	ELEV.
62+00					85.5
63+00					81.7
64+00					80.7
65+00					80.8
B.M.	0.51	982.30	10.79		981.79
66+00					79.9
67+00					79.4
68+00	/				78.8
69+00					77.3
70+00					75.7
71+00					73.3
+50					72.2
72+00					72.9
+50					74.4
73+00					74.1

$$\begin{array}{r} 9.9 \\ 100 \end{array} \quad \begin{array}{r} 8.1 \\ 50 \end{array} \quad \begin{array}{r} 8.3 \\ 39 \end{array} \quad \begin{array}{r} 7.1 \\ \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 100 \end{array}$$

$$\begin{array}{r} 14.0 \\ 100 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 50 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 100 \end{array}$$

$$\begin{array}{r} 14.6 \\ 100 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 10.6 \\ 100 \end{array}$$

$$\begin{array}{r} 14.6 \\ 100 \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 50 \end{array} \quad \begin{array}{r} 11.3 \\ 100 \end{array}$$

(981.77)

$$\begin{array}{r} 4.8 \\ 100 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 1.8 \\ 50 \end{array} \quad \begin{array}{r} 1.4 \\ 100 \end{array}$$

$$\begin{array}{r} 5.8 \\ 100 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array} \quad \begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 2.1 \\ 100 \end{array}$$

$$\begin{array}{r} 7.8 \\ 100 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 50 \end{array} \quad \begin{array}{r} 2.9 \\ 50 \end{array} \quad \begin{array}{r} 3.0 \\ 100 \end{array}$$

$$\begin{array}{r} 12.7 \\ 100 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 4.1 \\ 100 \end{array}$$

$$\begin{array}{r} 14.8 \\ 100 \end{array} \quad \begin{array}{r} 10.4 \\ 50 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 5.9 \\ 100 \end{array}$$

$$\begin{array}{r} 12.4 \\ 100 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 9.0 \\ 38 \end{array} \quad \begin{array}{r} 8.2 \\ 38 \end{array} \quad \begin{array}{r} 6.8 \\ 100 \end{array}$$

$$\begin{array}{r} 12.9 \\ 100 \end{array} \quad \begin{array}{r} 8.7 \\ 44 \end{array} \quad \begin{array}{r} 9.8 \\ 15 \end{array} \quad \begin{array}{r} 10.1 \\ 40 \end{array} \quad \begin{array}{r} 8.9 \\ 40 \end{array} \quad \begin{array}{r} 7.2 \\ 100 \end{array}$$

$$\begin{array}{r} 12.0 \\ 100 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 30 \end{array} \quad \begin{array}{r} 9.4 \\ 16 \end{array} \quad \begin{array}{r} 10.0 \\ 50 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array} \quad \begin{array}{r} 8.00 \\ 100 \end{array}$$

$$\begin{array}{r} 11.3 \\ 100 \end{array} \quad \begin{array}{r} 9.2 \\ 50 \end{array} \quad \begin{array}{r} 7.9 \\ 37 \end{array} \quad \begin{array}{r} 9.6 \\ 37 \end{array} \quad \begin{array}{r} 10.4 \\ 100 \end{array}$$

$$\begin{array}{r} 11.1 \\ 100 \end{array} \quad \begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 8.2 \\ 35 \end{array} \quad \begin{array}{r} 8.0 \\ 35 \end{array} \quad \begin{array}{r} 11.3 \\ 100 \end{array}$$

STA.	+	H.I.	-	ROD	ELEV.
		982.30			
74+00					73.0
T.P.	3.26	977.09	8.47		973.83
+50					71.8
75+00					69.0
+35	DRAW TO LAKE				68.2
+50					68.7
76+00					70.9
+50					70.5
77+00					70.7
T.P.	3.04	975.88	4.25		972.84
+50					72.1
78					71.4
+50	✓				70.5
79					70.2
+50					70.5

L.T.

4

R.T.

9-5-36

A.W.L.

J.B.

M.G.

32

$$\frac{11.5}{100} \quad \frac{10.2}{50} \quad \frac{9.3}{50} \quad \frac{8.9}{50} \quad \frac{8.5}{100}$$

$$\frac{7.1}{100} \quad \frac{6.0}{50} \quad \frac{5.3}{50} \quad \frac{4.6}{50} \quad \frac{4.3}{100}$$

$$\frac{11.6}{100} \quad \frac{8.3}{50} \quad \frac{8.1}{50} \quad \frac{7.4}{50} \quad \frac{6.5}{100}$$

$$\frac{12.8}{100} \quad \frac{10.7}{50} \quad \frac{8.9}{50} \quad \frac{8.8}{50} \quad \frac{8.8}{100}$$

$$\frac{8.4}{50}$$

$$\frac{13.5}{100} \quad \frac{9.8}{50} \quad \frac{6.2}{50} \quad \frac{5.4}{50} \quad \frac{5.9}{100}$$

$$\frac{15.1}{100} \quad \frac{11.9}{50} \quad \frac{6.6}{43} \quad \frac{4.5}{43} \quad \frac{5.0}{100}$$

$$\frac{16.5}{100} \quad \frac{13.2}{50} \quad \frac{6.4}{50} \quad \frac{3.8}{50} \quad \frac{3.8}{100}$$

$$\frac{16.1}{100} \quad \frac{11.8}{50} \quad \frac{4.8}{10} \quad \frac{3.8}{22} \quad \frac{2.6}{22} \quad \frac{2.6}{50} \quad \frac{3.0}{100}$$

$$\frac{17.1}{100} \quad \frac{13.2}{50} \quad \frac{6.3}{11} \quad \frac{4.5}{19} \quad \frac{3.1}{19} \quad \frac{2.9}{50} \quad \frac{2.5}{100}$$

$$\frac{19.3}{100} \quad \frac{17.2}{77} \quad \frac{13.7}{50} \quad \frac{5.4}{18} \quad \frac{4.0}{18} \quad \frac{2.8}{50} \quad \frac{2.0}{100}$$

$$\frac{18.7}{100} \quad \frac{17.0}{82} \quad \frac{13.2}{50} \quad \frac{7.7}{16} \quad \frac{5.7}{21} \quad \frac{4.1}{21} \quad \frac{3.1}{50} \quad \frac{2.2}{70} \quad \frac{2.9}{100}$$

$$\frac{17.6}{100} \quad \frac{17.0}{88} \quad \frac{12.4}{50} \quad \frac{9.3}{28} \quad \frac{5.4}{12} \quad \frac{4.2}{12} \quad \frac{3.2}{50} \quad \frac{3.4}{100}$$

STA	+	H.I.	-	ROD	ELEV.
		975.88			
79+90					69.7
80					69.7
+50					72.1
+73					72.3
81					72.5
+50					73.4
82					71.3
T.P.	1.41	973.10	4.19		971.69
+40					68.3
+64					67.6
B.M.	0.98	964.92		9.16	963.94
+82		GUTTER			59.2
+88		EDGE PAVE.			59.57

$$\frac{14.2}{100} \quad \frac{10.5}{50} \quad \frac{7.6}{19} \quad \frac{6.2}{19} \quad \frac{5.3}{19} \quad \frac{5.1}{50} \quad \frac{4.0}{100}$$

$$\frac{6.2}{19}$$

$$\frac{10.3}{100} \quad \frac{5.6}{50} \quad \frac{4.0}{33} \quad \frac{3.8}{12} \quad \frac{3.8}{12} \quad \frac{6.2}{50} \quad \frac{7.2}{100}$$

$$\frac{9.9}{100} \quad \frac{7.7}{76} \quad \frac{4.1}{50} \quad \frac{2.6}{37} \quad \frac{3.8}{17} \quad \frac{3.6}{30} \quad \frac{4.2}{30} \quad \frac{5.4}{50} \quad \frac{7.3}{100}$$

$$\frac{8.5}{100} \quad \frac{4.2}{67} \quad \frac{2.6}{43} \quad \frac{2.3}{21} \quad \frac{3.4}{23} \quad \frac{4.4}{23} \quad \frac{5.5}{50} \quad \frac{7.3}{100}$$

$$\frac{7.8}{100} \quad \frac{2.7}{40} \quad \frac{2.5}{40} \quad \frac{2.9}{50} \quad \frac{3.8}{100}$$

$$\frac{9.8}{100} \quad \frac{5.3}{50} \quad \frac{4.5}{24} \quad \frac{5.1}{16} \quad \frac{4.6}{50} \quad \frac{3.7}{50} \quad \frac{3.2}{100}$$

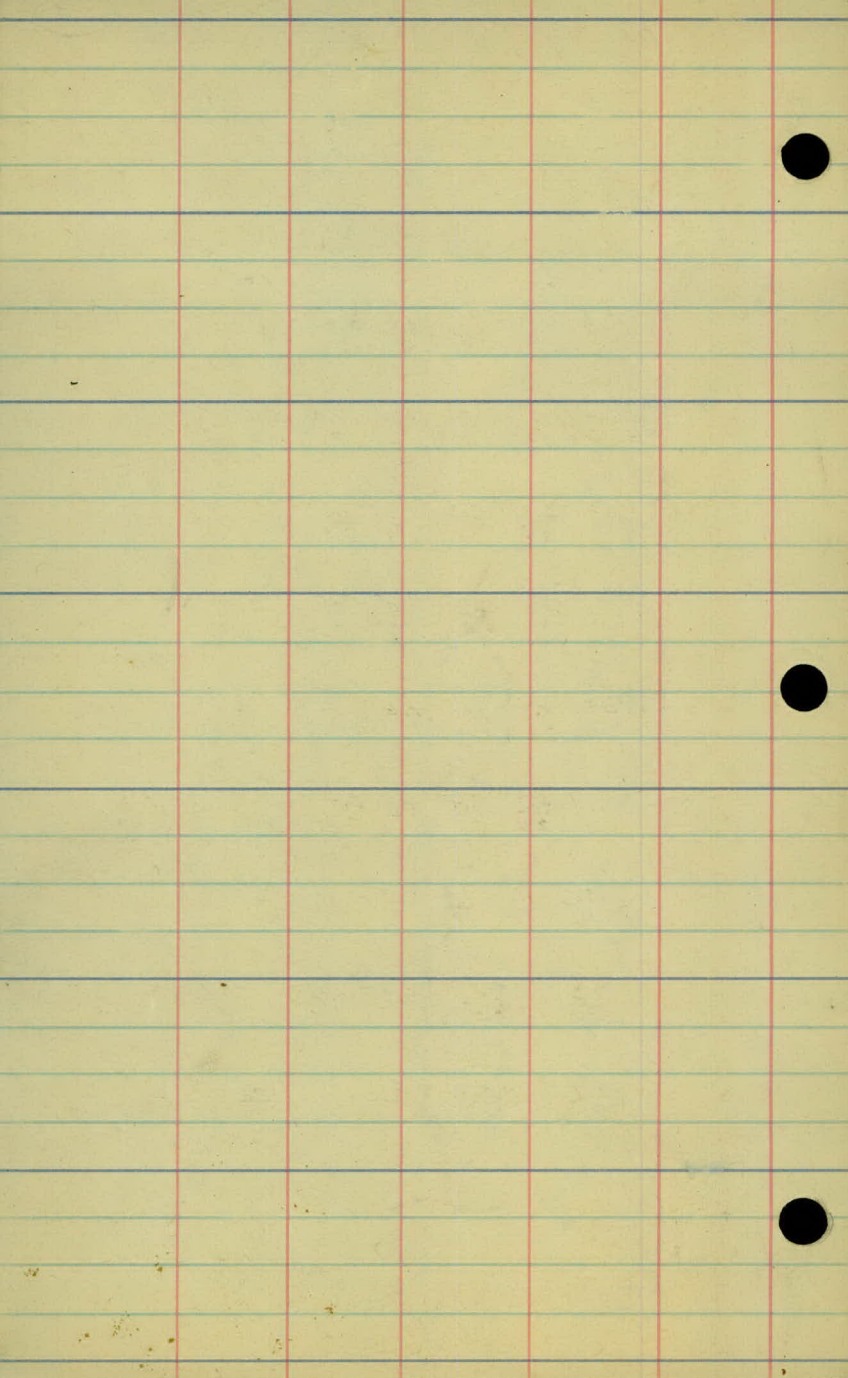
$$\frac{10.0}{100} \quad \frac{7.7}{50} \quad \frac{6.2}{29} \quad \frac{5.4}{22} \quad \frac{4.8}{30} \quad \frac{3.4}{30} \quad \frac{2.0}{50} \quad \frac{1.2}{70} \quad \frac{1.2}{100}$$

$$\frac{12.0}{100} \quad \frac{9.7}{50} \quad \frac{7.5}{18} \quad \frac{5.5}{50} \quad \frac{1.9}{50} \quad \frac{1.5}{100}$$

(963.90) ✓

$$\frac{9.2}{100} \quad \frac{7.6}{50} \quad \frac{5.7}{50} \quad \frac{4.3}{50} \quad \frac{2.6}{100}$$

$$\frac{8.7}{100} \quad \frac{7.0}{50} \quad \frac{5.85}{50} \quad \frac{3.6}{50} \quad \frac{2.0}{100}$$



NEW CANADA TOWNSHIP

2645.70

NATLAND

1322.85

1323.85

661.42

BEAVER L. RD.

25

EAST AVE

