

Dr. G - BK. 104

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey
Also Stadia Survey (1946)
_____ EAST AVE. _____

From Larperneur Co. 1/2 mi. So.
150 X-Sections
Road Acc't. No. 75

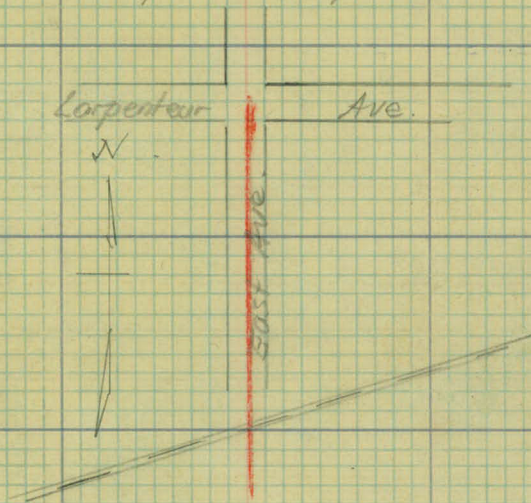
Filed 1936

File D. G. B. 104

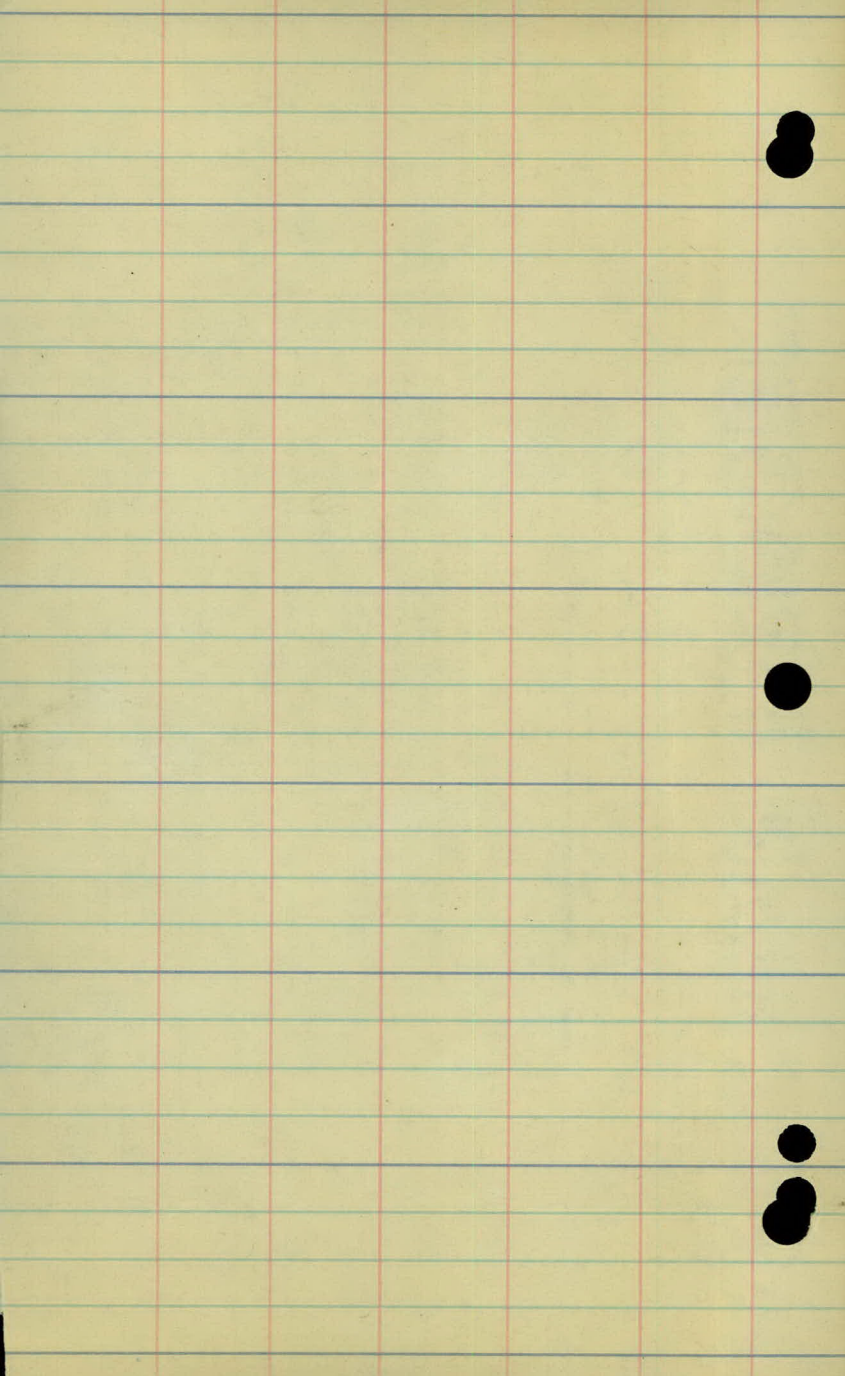
Plan Survey

East Ave

So. of Larp to Larpentour.



W. H. Carlson
Sept. 18, 1936



1
alignment.

Sta. Point

52+72.2 Larpenteur.

39+54.6 P.O.T.
Mon.

36+54.6 P.O.T.

34+00 P.O.T.

28+37.4 P.O.T.

26² - Mon. (26+34.55) tipped

~~26+35.65~~

N



stone Moss

Rock Moss

Boat Spike

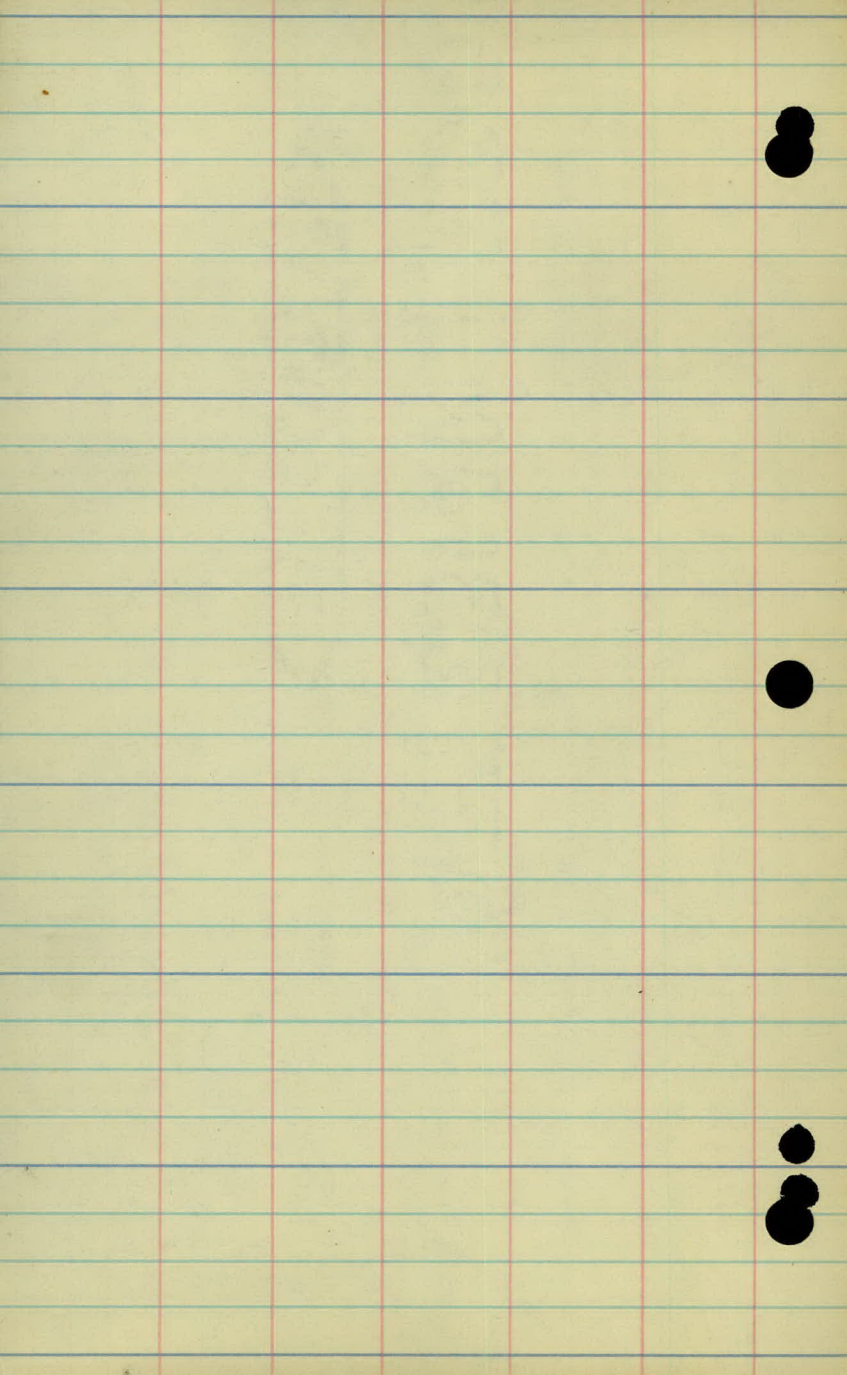
Boat Spike.

Boat spike

Nail in 182"

B.M.
975.58-213400

59.65



Topography.









24

23

22

21

20



24

16'

31

15'

30

9 5'

+ 13. End taruia + imorde

29

28

27

26

25

+87-T.P. 21'

+60- 4" willow 30'

+33- A.P. 23'

+90 Ent

+51-T.P. 22'

+56 end trees 12-22'

12 willows

Reg'n trees

+02-T.P. 21'

+90- Ent

+91- A.P. 22'

+52- 3-4" willows 26'
4-6" " 26'

+23- Ent

+08- 10" oak 20'

pop
20+50

+03- 6" oak 21'

+08- A.P. 20'

+85

+20

+73- Popple Thicket
20 small trees

+45- 12' cotton wood-19'

+36- P.P. 21'

+34 Fence corner
Fence!

9' 10

38

7 11

37

9' 9'

36

11 7

35

14 2

34

17'

33

18'

32

16'

+15-T.P. 22'
201-8" oak 20'

+14-T.P. 21'

+77-Ent.

+03-T.P. 21'
+

+78-12" stump 26'
+70-6" " 28'

+41-R.P. 22'

+00 T.P. - 22'

+08 Fence cor. 26'

+68-Ent.

X Fence 24'

Fence 23' sta - 2 - 10" oaks 23'

+71-8" P.P. 23
+66-T.P. 22

+66-R.P. 21'

+40-Ent

+13-12" stump 26'

+08 Fence 23'

+70-2-8" oaks 28'

+180
- 21.0
+ 550
Stumps
6"

+60-6" oak 31'

+45-10" oak 28'

+39-10" oak 18'

+31-10" stump 19'

+29-8" oak 26'

+13-12" stump 16'

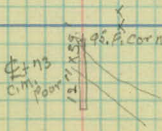
+32-T.P. 22'

+95-R.P. 23'

+80-conc. wall 12'
3' wide

+68-12" oak 31'

+30-shrub - 19'



6' 12

45

6' 12'

44

5' 12'

43

6' 12'

42

8' 11'

41

9' 10'

40

10-9

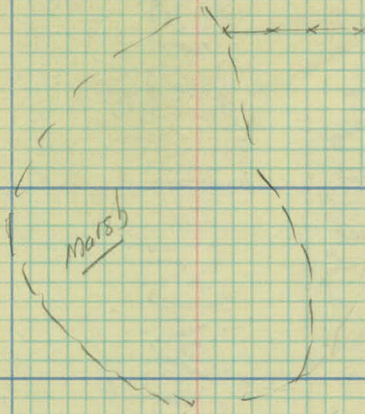
154.6 Stone Mon.

+42 - T.P. 16'

+50 - Ent.
12" X 20' C.M.

+82 - G.P. 16

+85 - R.P. 16
+83 - F. Cor. 16



F-15'

+18 - T.P. 22'

+66 - 8" W. 11' 24'
+02 - R.P. 18'
F-17'

+02 - 8" R.P. 25'

+91 - 12" R.P. 24'
+15 - T.P. 17'

Golf Course

x x x

+62 - R.P. 18'
+56 - F. Cor. 24'
+46 - Ent.

18 - Evergreen 29'
+15 - N.W. Cor. 25' 11' 1/2
+56 - 6" Mount - 28'
to 41' W-E

+90 - Cor. Tee

+62 - Cor. Tee 31'

+46 - 20" R.P. 24'
+42 - 15" R.P. 10
+36 - T.P. 22'

Tee

Gard

+87 - S.W. Cor. 8' 1/2

+79 - 14" Tw. W. 11'
20

+74 - 8" R.P. 22'

+38 - T.P. 22'

x x x

+55 - Fan Line 31'
+53 - T.P. 21'

+31 - Rd. 17'
12" X 20' C.M.

150 2' - 3

52

14' 5"

51

13' 5"

50

12' 8"

49

9' 11"

170 - 2

$\frac{13' 20}{18' \text{ C.M. N.G.}}$

48

6' 12"

47

6' 12"

46

+62 - S. edge Torva.

+65 - Cor. Tee

+58 - Tee 42'
 +57 - T.P. 76
 +50 - Ent.

Tee

+75 - P.P. 13'

+98 - T.P. 27'

Golf Course

+49 - T.P. 27'

Marsh

+05 - T.P. 27'

Marsh

+86 - Tree end - 13

+60 - Tree Line

6-8" Oaks. 17

+39 - P.P. 14'

+64 - 22

+75 - 6" Oak
 18' - 26'

+09 - 10" Oak 23'

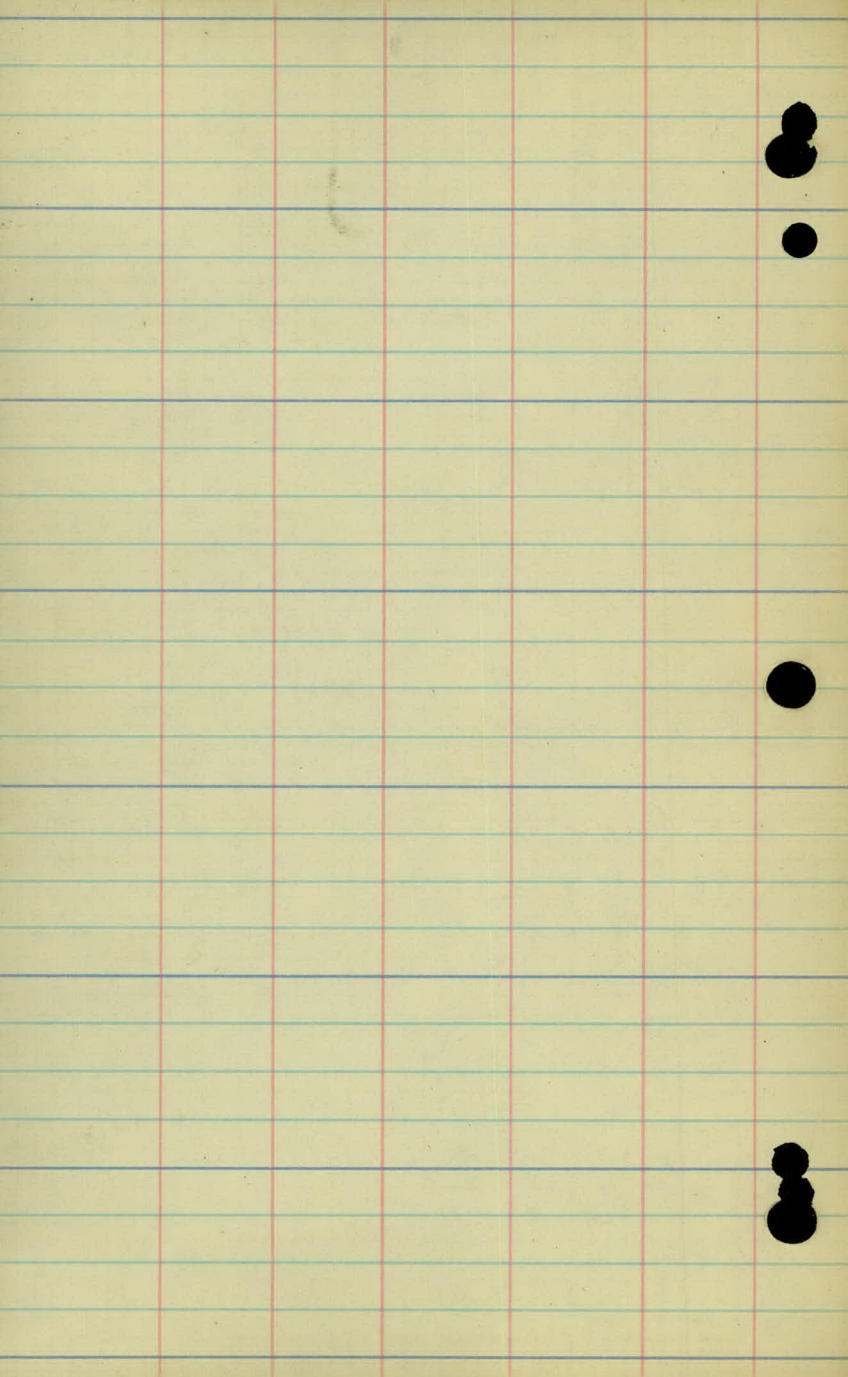
+05 - P.P. - 15'

+70 - P.P. 76'

+70 - Bag 34'

+35 - RR 17'

+01 - 5" Triple 19'



East Ave.

4 Levels.

Sta.	+	π	-	E/100.
B.M	2.02	1025.03		1023.01
"			4.05	1020.99 1020.99

52+72.2 = ^{Top Mon.} ~~Larp~~ 4.05 1021.0

450 4.5 20.5

52 4.9 20.1

51 4.2 20.8

50 3.4 21.6

T.P. 3.25 1024.88 3.40 1021.63

49 4.7 20.2

48+50 5.7 19.2

48 5.5 19.4

47 4.6 20.3

46 5.2 19.7

45 4.7 20.2

44 4.7 20.2

T.P. 8.95 1029.13 4.70 1020.18

43 7.6 21.5

42 4.5 24.6

41 1.6 27.5

T.P. 12.03 1040.54 0.62 1028.51

40 9.6 30.9

39+54.6 Top Mon. 7.08 1033.46

39 4.6 35.9

W.H.C.
L.B.H.
H. Pratt
Mason

Aug. 12, 1936

@ Store.

Top Mon. (1020.74 - East Ave, going north)

S _h	+	π	-	ETU
		1040.54		
38+50			2.4	38.1
38			1.7	38.8
T.P.	8.87	1047.76	1.65	1038.89
37+50			7.9	39.9
B.M.			6.06	1041.70
37			6.1	41.7
36+54			4.7	43.1
B.M	6.11	1047.81		1041.70
36			5.6	42.2
35+50			7.4	40.4
35			9.1	38.7
34+50			9.2	38.6
34			10.0	37.8
33+50			12.1	35.7
T.P.	1.48	137.20	12.09	1035.72
33			5.6	31.6
32+45			10.1	27.1
T.P.	1.27	1025.52	12.95	1024.25
32			3.3	22.2
31+50			7.4	18.1
31			11.2	14.3
T.P.	1.65	1015.68	11.49	1014.03
30+50			4.0	11.7
30			5.8	09.9
29+50			6.8	08.9

Spike in 10' oak 35' Sta. 37+30

Spike in 10' oak 35' Rt Sta 37+30

Sta

+

A

-

E/eo

1015.68

29+00

6.5

09.2

28+50

6.3

09.4

T.P.

4.80

1014.67

5.81

1009.87

T.P.

1011.51

5.19

1009.48

28+00

5.00

06.5

27+50

12.6

98.9

T.P.

2.16

1001.49

12.18

999.33

27.00

4.2

97.3

26+50

6.7

94.8

(mon. + 34.5?) tipped

7.0

94.5

26+00

6.8

94.7

B.A.

5.05

996.44

Spike in P.P. 21' Rt Sta 29+75

Spike in 14" Cottonwood 20' Rt 26+46



X-sections East Ave.

Sta 26+30.1 - 52+72.2

Sta.	+	Δ	-	Elev	B.M.
	4.48	1000.94		996.44	
26+36.1		.92		94.5-	

27+00				97.3-	
T.P.	10.15	1007.95	3.12	997.80	
+50				99.0-	

+75				00.7-	
-----	--	--	--	-------	--

+90				04.3-	
T.P.	11.75	1018.91	0.79	1007.16	
28+00				06.5-	

+25				10.2-	
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+50				09.4-	
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29+00				09.2-	
T.P.	5.79	1014.75	9.95	1008.96	
+50				08.9-	

30+00				10.0-	
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+50				11.8-	
T.P.	12.66	1026.61	0.80	1013.95	

LT

D

RT

$$\frac{4.8}{33} \quad \frac{6.3}{17} \quad \frac{6.4}{7} \quad \frac{6.4}{90} \quad \frac{6.5}{5} \quad \frac{6.0}{22} \quad \frac{6.0}{33}$$

$$\frac{3.7}{33} \quad \frac{3.1}{22} \quad \frac{3.6}{9} \quad \frac{3.6}{90} \quad \frac{3.9}{9} \quad \frac{4.7}{19} \quad \frac{6.1}{33}$$

$$\frac{6.6}{33} \quad \frac{7.5}{15} \quad \frac{8.0}{8} \quad \frac{9.0}{90} \quad \frac{9.2}{7} \quad \frac{10.1}{15} \quad \frac{11.3}{24} \quad \frac{12.8}{33}$$

$$\frac{3.0}{33} \quad \frac{4.1}{23} \quad \frac{4.2}{16} \quad \frac{5.1}{8} \quad \frac{7.3}{9} \quad \frac{7.7}{9} \quad \frac{8.7}{14} \quad \frac{9.2}{25} \quad \frac{11.0}{33}$$

$$\frac{1.0}{33} \quad \frac{1.4}{16} \quad \frac{2.9}{7} \quad \frac{5.7}{9} \quad \frac{5.7}{9} \quad \frac{6.1}{15} \quad \frac{8.5}{25} \quad \frac{9.3}{33}$$

$$\frac{6.4}{33} \quad \frac{9.9}{16} \quad \frac{11.3}{5} \quad \frac{12.4}{9} \quad \frac{13.4}{12} \quad \frac{15.4}{14.5} \quad \frac{14.2}{19} \quad \frac{19.0}{33}$$

$$\frac{1.1}{33} \quad \frac{2.7}{22} \quad \frac{3.1}{17} \quad \frac{4.3}{10} \quad \frac{6.1}{4} \quad \frac{8.7}{9} \quad \frac{10.5}{5} \quad \frac{11.1}{10} \quad \frac{13.3}{14} \quad \frac{14.4}{19} \quad \frac{12.6}{33}$$

$$\frac{4.0}{33} \quad \frac{3.7}{29} \quad \frac{4.7}{24} \quad \frac{7.0}{14} \quad \frac{6.2}{9} \quad \frac{9.5}{11.5} \quad \frac{9.5}{9} \quad \frac{10.2}{9} \quad \frac{12.0}{13} \quad \frac{9.9}{17} \quad \frac{9.9}{33}$$

$$\frac{12.1}{33} \quad \frac{10.7}{22} \quad \frac{9.9}{6} \quad \frac{9.7}{9} \quad \frac{10.0}{11.5} \quad \frac{11.0}{14.5} \quad \frac{9.2}{19} \quad \frac{9.2}{33}$$

$$\frac{9.0}{33} \quad \frac{7.9}{14} \quad \frac{6.2}{8} \quad \frac{5.9}{9} \quad \frac{5.9}{12} \quad \frac{6.1}{18} \quad \frac{6.5}{27} \quad \frac{6.5}{33}$$

$$\frac{7.5}{33} \quad \frac{7.3}{19} \quad \frac{5.2}{12} \quad \frac{4.8}{9} \quad \frac{5.1}{6} \quad \frac{5.0}{15} \quad \frac{5.5}{33}$$

$$\frac{5.2}{33} \quad \frac{4.2}{20} \quad \frac{3.4}{14} \quad \frac{3.0}{9} \quad \frac{3.5}{5} \quad \frac{3.0}{6} \quad \frac{3.2}{8} \quad \frac{2.9}{18} \quad \frac{2.2}{30} \quad \frac{1.6}{33}$$

Sta + π ✓ — E/10 B.M

1026.61

31+00

14.1 -

+50

18.1 -

32+00

22.2 -

T.P.

12.77

1032.32 ✓

2.01

1024.60 ✓

+45

26.3 -

T.P.

5.80

1043.08 ✓

0.09

1037.28 ✓

+60

29.1 -

+95

30.7 -

33+00

31.2 -

+50

35.8 -

34+00

37.8 -

+50

38.7 -

35+00

38.7 -

+50

40.4 -

T.P.

11.86

1052.05 ✓

2.89

1046.19 ✓

LTPRT

$$\begin{array}{r} 14.4 \\ 33 \end{array} \quad \begin{array}{r} 11.9 \\ 18 \end{array} \quad \begin{array}{r} 12.5 \\ 2 \end{array} \quad \begin{array}{r} 12.7 \\ 2 \end{array} \quad \begin{array}{r} 10.6 \\ 8 \end{array} \quad \begin{array}{r} 9.6 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 23 \end{array} \quad \begin{array}{r} 7.8 \\ 33 \end{array}$$

$$\begin{array}{r} 11.2 \\ 33 \end{array} \quad \begin{array}{r} 10.9 \\ 30 \end{array} \quad \begin{array}{r} 9.5 \\ 22 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 8.5 \\ 3 \end{array} \quad \begin{array}{r} 8.7 \\ 3 \end{array} \quad \begin{array}{r} 5.3 \\ 8 \end{array} \quad \begin{array}{r} 4.0 \\ 25 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 28 \end{array} \quad \begin{array}{r} 4.3 \\ 18 \end{array} \quad \begin{array}{r} 4.4 \\ 18 \end{array} \quad \begin{array}{r} 3.1 \\ 5 \end{array} \quad \begin{array}{r} 1.7 \\ 9 \end{array} \quad \begin{array}{r} 1.3 \\ 19 \end{array} \quad \begin{array}{r} 0.3 \\ 28 \end{array} \quad \begin{array}{r} 0.9 \\ 33 \end{array}$$

$$\begin{array}{r} 13.4 \\ 33 \end{array} \quad \begin{array}{r} 12.8 \\ 29 \end{array} \quad \begin{array}{r} 10.8 \\ 24 \end{array} \quad \begin{array}{r} 11.1 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 9 \end{array} \quad \begin{array}{r} 7.2 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 27 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array}$$

Spike in T.P. 33+32 = 22' 44"

$$\begin{array}{r} 17.8 \\ 33 \end{array} \quad \begin{array}{r} 16.8 \\ 26 \end{array} \quad \begin{array}{r} 15.5 \\ 20 \end{array} \quad \begin{array}{r} 15.3 \\ 5 \end{array} \quad \begin{array}{r} 14.0 \\ 13 \end{array} \quad \begin{array}{r} 12.8 \\ 13 \end{array} \quad \begin{array}{r} 10.0 \\ 21 \end{array} \quad \begin{array}{r} 9.7 \\ 27 \end{array} \quad \begin{array}{r} 6.1 \\ 34 \end{array}$$

$$\begin{array}{r} 12.9 \\ 33 \end{array} \quad \begin{array}{r} 12.4 \\ 30 \end{array} \quad \begin{array}{r} 11.2 \\ 22 \end{array} \quad \begin{array}{r} 11.9 \\ 18 \end{array} \quad \begin{array}{r} 12.4 \\ 5 \end{array} \quad \begin{array}{r} 11.1 \\ 5 \end{array} \quad \begin{array}{r} 10.7 \\ 11.5 \end{array} \quad \begin{array}{r} 9.3 \\ 15 \end{array} \quad \begin{array}{r} 8.6 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 32 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 12.8 \\ 33 \end{array} \quad \begin{array}{r} 11.7 \\ 28 \end{array} \quad \begin{array}{r} 10.6 \\ 22 \end{array} \quad \begin{array}{r} 11.4 \\ 18 \end{array} \quad \begin{array}{r} 11.9 \\ 18 \end{array} \quad \begin{array}{r} 7.9 \\ 6 \end{array} \quad \begin{array}{r} 6.4 \\ 9 \end{array} \quad \begin{array}{r} 4.9 \\ 24 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 31 \end{array} \quad \begin{array}{r} 5.5 \\ 22 \end{array} \quad \begin{array}{r} 7.7 \\ 18 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 3.3 \\ 5 \end{array} \quad \begin{array}{r} 2.4 \\ 16 \end{array} \quad \begin{array}{r} 2.0 \\ 24 \end{array} \quad \begin{array}{r} 1.6 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 23 \end{array} \quad \begin{array}{r} 5.6 \\ 20.5 \end{array} \quad \begin{array}{r} 5.3 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 3 \end{array} \quad \begin{array}{r} 3.5 \\ 3 \end{array} \quad \begin{array}{r} 2.7 \\ 23 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 23 \end{array} \quad \begin{array}{r} 5.0 \\ 16 \end{array} \quad \begin{array}{r} 4.4 \\ 16 \end{array} \quad \begin{array}{r} 4.7 \\ 7 \end{array} \quad \begin{array}{r} 4.1 \\ 22 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array}$$

$$\begin{array}{r} 7.1 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 4.9 \\ 14 \end{array} \quad \begin{array}{r} 4.4 \\ 14 \end{array} \quad \begin{array}{r} 6.3 \\ 8 \end{array} \quad \begin{array}{r} 6.4 \\ 18 \end{array} \quad \begin{array}{r} 6.1 \\ 26 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 24 \end{array} \quad \begin{array}{r} 4.4 \\ 18 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad \begin{array}{r} 2.9 \\ 5 \end{array} \quad \begin{array}{r} 2.9 \\ 5 \end{array} \quad \begin{array}{r} 5.0 \\ 11 \end{array} \quad \begin{array}{r} 5.1 \\ 22 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

Sta + $\checkmark$ - Elev B.M

1052.05

36+00

42.2-

+30

43.0-

+80

42.5-

T.P.

3.65

1044.15

11.55

1040.50

Check B.M

2.45

1041.70

1041.70 ✓

$$\frac{5.4}{33} \quad \frac{4.7}{25} \quad \frac{10.1}{155} \quad \frac{10.2}{125} \quad 9.9 \quad \frac{10.1}{8} \quad \frac{9.5}{18.5} \quad \frac{8.2}{23} \quad \frac{8.2}{26} \quad \frac{7.4}{33}$$

49.4

$$\frac{2.7}{33} \quad \frac{2.0}{28} \quad \frac{9.0}{15} \quad \frac{9.6}{11} \quad 9.1 \quad \frac{9.2}{9} \quad \frac{9.5}{15} \quad \frac{0.7}{26} \quad \frac{0.5}{33}$$

51.2

$$\frac{7.6}{33} \quad \frac{6.2}{24} \quad \frac{10.2}{14.5} \quad \frac{9.8}{11} \quad \frac{9.6}{11} \quad \frac{10.2}{8} \quad \frac{9.5}{10} \quad \frac{1.2}{24} \quad \frac{0.8}{33}$$

Sta.	+ 6.06	π 1047.76	-	Elev.
37+0				41.7 ✓
+30				40.6 ✓
+70				39.3 ✓
38+0				38.8 ✓
T.P.	4.02	1042.83 ✓	895	1038.81 ✓
+50				38.0 ✓
39+0				35.9 ✓
+30				34.6 ✓
+54.6	Mon.		9.37	33.4 ✓
B.M.	1.72	1035.18 ✓	9.37	1033.46 ✓
40+0				31.0 ✓
+50				28.9 ✓
41+0				27.6 ✓
	2.89	1029.22 ✓	8.85	1026.33 ✓
+50				26.3 ✓

Lt.

C

Rt.

Spoke in 10' Oak 35' Rt. 56 37+30

76	66	52	6.5		6.5	5.3	0.0	11.5
<u>33</u>	<u>28</u>	<u>19</u>	<u>16</u>	<u>6.1</u>	<u>9</u>	<u>16</u>	<u>76</u>	<u>40</u>

134	12.5	10.9	7.7	7.2	7.5	7.7		7.7
<u>33</u>	<u>24</u>	<u>14</u>	<u>8</u>	<u>7</u>	<u>9</u>	<u>17</u>		<u>33</u>

13.0		11.8	8.8	8.5	9.1	10.2		11.3
<u>33</u>		<u>15</u>	<u>9</u>	<u>9</u>	<u>12</u>	<u>15</u>		<u>33</u>

10.2	9.1	9.8	9.0	9.0	9.6	10.1	8.2	8.2
<u>33</u>	<u>27</u>	<u>13</u>	<u>9</u>	<u>9</u>	<u>13</u>	<u>25</u>	<u>30</u>	<u>33</u>

1.7	1.7	2.5	4.5	4.7	5.1	4.8	5.6	5.2	4.8	1.0	1.0
<u>33</u>	<u>26</u>	<u>21</u>	<u>17</u>	<u>10</u>	<u>9</u>	<u>4</u>	<u>11</u>	<u>13</u>	<u>28</u>	<u>31</u>	<u>33</u>

2.6	3.4	6.8	7.0	7.4	6.9	7.4	7.0	2.8	2.8
<u>33</u>	<u>23</u>	<u>17</u>	<u>10</u>	<u>9</u>	<u>6</u>	<u>11</u>	<u>26</u>	<u>32</u>	<u>33</u>

7.8	3.0	8.5	8.3	7.9	8.2	8.5		8.0
<u>33</u>	<u>27</u>	<u>19</u>	<u>11</u>	<u>9</u>	<u>8</u>	<u>9</u>		<u>33</u>

4.4	4.4	10.2	9.9	9.4	10.0	10.5		11.0
<u>33</u>	<u>26</u>	<u>18</u>	<u>10</u>	<u>9</u>	<u>10</u>	<u>19</u>		<u>33</u>

Top Mon 34 5 46

2.0	2.5	5.0	4.6	4.2	4.9	7.8		8.1
<u>33</u>	<u>26</u>	<u>23</u>	<u>10</u>	<u>4</u>	<u>10</u>	<u>15</u>		<u>33</u>

4.0	4.5	7.2	7.2	6.6	6.3	7.0	8.8	9.2
<u>33</u>	<u>28</u>	<u>18</u>	<u>14</u>	<u>10</u>	<u>6</u>	<u>11</u>	<u>14</u>	<u>33</u>

6.6	8.2	9.0	8.8	7.9	7.6	8.3	9.2	7.7	5.8	= yard
<u>33</u>	<u>27</u>	<u>20</u>	<u>13</u>	<u>10</u>	<u>7</u>	<u>12</u>	<u>18</u>	<u>29</u>	<u>36</u>	

11.4	11.1	2.5	3.4	3.4	2.9	3.2	7.6	2.8
<u>33</u>	<u>27</u>	<u>21</u>	<u>11</u>	<u>9</u>	<u>2</u>	<u>11</u>	<u>24</u>	<u>33</u>

Sta.

+

X

-

1029.22

41+75

25.4 ✓

42+0

24.6 ✓

+40

23.0 ✓

T.P.

3.21

1024.80

7.63

1021.59

+80

22.1 ✓

43+00

21.6 ✓

+50

20.5 ✓

44+00

20.2 ✓

+50

20.0 ✓

+90

20.1 ✓

45+25

20.3 ✓

+60

20.1 ✓

46+00

19.7 ✓

Sta.	+	T	-	Elev.
		1024.80 ✓		
T.P.	5.34	1025.02 ✓	5.12	1019.68 ✓
46+30				19.6 ✓
+65				19.9 ✓
47+00				20.2 ✓
T.P.	5.10	1025.10 ✓	5.02	1020.00 ✓
+45				20.1 ✓
+75				19.7 ✓
48+00				19.3 ✓
+50				19.2 ✓
+90				20.0 ✓
49+00				20.2 ✓
B.m	5.20	1026.19 ✓		1020.99
+25				20.7 ✓
+60				21.2 ✓
50+00				21.7 ✓

$$\begin{array}{r} 10.5 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 26 \end{array} \quad \begin{array}{r} 10.0 \\ 19 \end{array} \quad \begin{array}{r} 9.5 \\ 12 \end{array} \quad \begin{array}{r} 5.9 \\ 8 \end{array} \quad 5.4 \quad \begin{array}{r} 5.9 \\ 13 \end{array} \quad \begin{array}{r} 8.4 \\ 18 \end{array} \quad \begin{array}{r} 8.5 \\ 28 \end{array} \quad \begin{array}{r} 8.2 \\ 30 \end{array} \quad \begin{array}{r} 8.0 \\ 33 \end{array}$$

$$\begin{array}{r} 9.2 \\ 33 \end{array} \quad \begin{array}{r} 8.6 \\ 29 \end{array} \quad \begin{array}{r} 8.1 \\ 18 \end{array} \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} 5.5 \\ 8 \end{array} \quad 5.1 \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 8.8 \\ 20 \end{array} \quad \begin{array}{r} 8.7 \\ 27 \end{array} \quad \begin{array}{r} 5.4 \\ 31 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 7.8 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 29 \end{array} \quad \begin{array}{r} 6.8 \\ 24 \end{array} \quad \begin{array}{r} 6.1 \\ 12 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 9 \end{array} \quad 4.8 \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 8.0 \\ 22 \end{array} \quad \begin{array}{r} 2.7 \\ 30 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array}$$

Spike in AP LT Sta: 47+69

$$\begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 18 \end{array} \quad \begin{array}{r} 8.4 \\ 15 \end{array} \quad \begin{array}{r} 5.4 \\ 9 \end{array} \quad 5.0 \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad \begin{array}{r} 8.1 \\ 18 \end{array} \quad \begin{array}{r} 8.8 \\ 27 \end{array} \quad \begin{array}{r} 8.9 \\ 33 \end{array}$$

$$\begin{array}{r} 10.1 \\ 33 \end{array} \quad \begin{array}{r} 9.9 \\ 24 \end{array} \quad \begin{array}{r} 9.8 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 8 \end{array} \quad 5.4 \quad \begin{array}{r} 6.1 \\ 14 \end{array} \quad \begin{array}{r} 9.4 \\ 20 \end{array} \quad \begin{array}{r} 9.7 \\ 29 \end{array} \quad \begin{array}{r} 9.7 \\ 33 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 21 \end{array} \quad \begin{array}{r} 10.1 \\ 13 \end{array} \quad \begin{array}{r} 6.0 \\ 8 \end{array} \quad 5.8 \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 9.7 \\ 19 \end{array} \quad \begin{array}{r} 10.9 \\ 26 \end{array} \quad \begin{array}{r} 10.2 \\ 33 \end{array}$$

$$\begin{array}{r} 10.8 \\ 33 \end{array} \quad \begin{array}{r} 10.8 \\ 29 \end{array} \quad \begin{array}{r} 10.4 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 8 \end{array} \quad 5.9 \quad \begin{array}{r} 6.3 \\ 12 \end{array} \quad \begin{array}{r} 9.4 \\ 19 \end{array} \quad \begin{array}{r} 10.0 \\ 25 \end{array} \quad \begin{array}{r} 10.7 \\ 33 \end{array}$$

$$\begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 9.2 \\ 27 \end{array} \quad \begin{array}{r} 8.7 \\ 19 \end{array} \quad \begin{array}{r} 8.2 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 9 \end{array} \quad 6.1 \quad \begin{array}{r} 5.5 \\ 13 \end{array} \quad \begin{array}{r} 8.4 \\ 18 \end{array} \quad \begin{array}{r} 9.1 \\ 23 \end{array} \quad \begin{array}{r} 9.4 \\ 33 \end{array}$$

$$\begin{array}{r} 8.6 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 16 \end{array} \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad 4.9 \quad \begin{array}{r} 5.1 \\ 13 \end{array} \quad \begin{array}{r} 7.0 \\ 18 \end{array} \quad \begin{array}{r} 8.0 \\ 22 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array}$$

Stone Monument Sta 52+72.2

$$\begin{array}{r} 6.1 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 28 \end{array} \quad \begin{array}{r} 7.0 \\ 22 \end{array} \quad \begin{array}{r} 6.5 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 9 \end{array} \quad \begin{array}{r} 5.9 \\ 9 \end{array} \quad \begin{array}{r} 6.6 \\ 13 \end{array} \quad \begin{array}{r} 4.1 \\ 19 \end{array} \quad \begin{array}{r} 7.6 \\ 33 \end{array}$$

$$\begin{array}{r} 0.9 \\ 33 \end{array} \quad \begin{array}{r} 1.7 \\ 29 \end{array} \quad \begin{array}{r} 5.9 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 10 \end{array} \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 5.7 \\ 20.5 \end{array} \quad \begin{array}{r} 9.1 \\ 33 \end{array}$$

$$\begin{array}{r} +0.2 \\ 33 \end{array} \quad \begin{array}{r} 0.3 \\ 28 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 5.5 \\ 14 \end{array} \quad \begin{array}{r} 4.5 \\ 00 \end{array} \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 16 \end{array} \quad \begin{array}{r} 6.4 \\ 21 \end{array} \quad \begin{array}{r} 8.4 \\ 33 \end{array}$$

Sta.

+

A



-

Elev

B.M.

1026.19

50+50

21.4 ✓

+1.0

4.91

1026.35³⁷

4.73

1021.44 ✓

+85

21.1 ✓

51+00

20.9 ✓

+50

20.2 ✓

+60

+60

52+00

20.1 ✓

+05

+35

20.3 ✓

+57

20.8 ✓

Shoulder line Carpenter

CK B.M.

5.36

1020.99 ✓

1020.99

1021.01 ✓

$$\begin{array}{r} 0.0 \\ 28 \end{array} \quad \begin{array}{r} 0.7 \\ 28 \end{array} \quad \begin{array}{r} 4.3 \\ 22 \end{array} \quad \begin{array}{r} 5.3 \\ 16 \end{array} \quad \begin{array}{r} 4.8 \\ 00 \end{array} \quad \begin{array}{r} 5.4 \\ 7 \end{array} \quad \begin{array}{r} 6.4 \\ 10 \end{array} \quad \begin{array}{r} 7.5 \\ 24 \end{array} \quad \begin{array}{r} 8.6 \\ 32 \end{array}$$

$$\begin{array}{r} 1.8 \\ 33 \end{array} \quad \begin{array}{r} 2.1 \\ 29 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 14 \end{array} \quad \begin{array}{r} 5.3 \\ 00 \end{array} \quad \begin{array}{r} 5.9 \\ 6 \end{array} \quad \begin{array}{r} 7.2 \\ 10 \end{array} \quad \begin{array}{r} 7.9 \\ 16 \end{array} \quad \begin{array}{r} 8.5 \\ 18 \end{array} \quad \begin{array}{r} 9.2 \\ 25 \end{array} \quad \begin{array}{r} 9.5 \\ 29 \end{array} \quad \begin{array}{r} 9.9 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 3.2 \\ 28 \end{array} \quad \begin{array}{r} 6.0 \\ 21 \end{array} \quad \begin{array}{r} 6.4 \\ 17 \end{array} \quad \begin{array}{r} 5.6 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 00 \end{array} \quad \begin{array}{r} 6.1 \\ 7.5 \end{array} \quad \begin{array}{r} 8.2 \\ 14 \end{array} \quad \begin{array}{r} 8.6 \\ 19 \end{array} \quad \begin{array}{r} 9.4 \\ 23 \end{array} \quad \begin{array}{r} 9.8 \\ 28 \end{array} \quad \begin{array}{r} 10.0 \\ 33 \end{array}$$

$$\begin{array}{r} 5.5 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 31 \end{array} \quad \begin{array}{r} 6.2 \\ 24 \end{array} \quad \begin{array}{r} 6.4 \\ 13 \end{array} \quad \begin{array}{r} 6.2 \\ 00 \end{array} \quad \begin{array}{r} 6.6 \\ 6 \end{array} \quad \begin{array}{r} 8.2 \\ 10.5 \end{array} \quad \begin{array}{r} 9.4 \\ 13 \end{array} \quad \begin{array}{r} 10.2 \\ 17 \end{array} \quad \begin{array}{r} 10.4 \\ 23 \end{array} \quad \begin{array}{r} 11.0 \\ 33 \end{array}$$

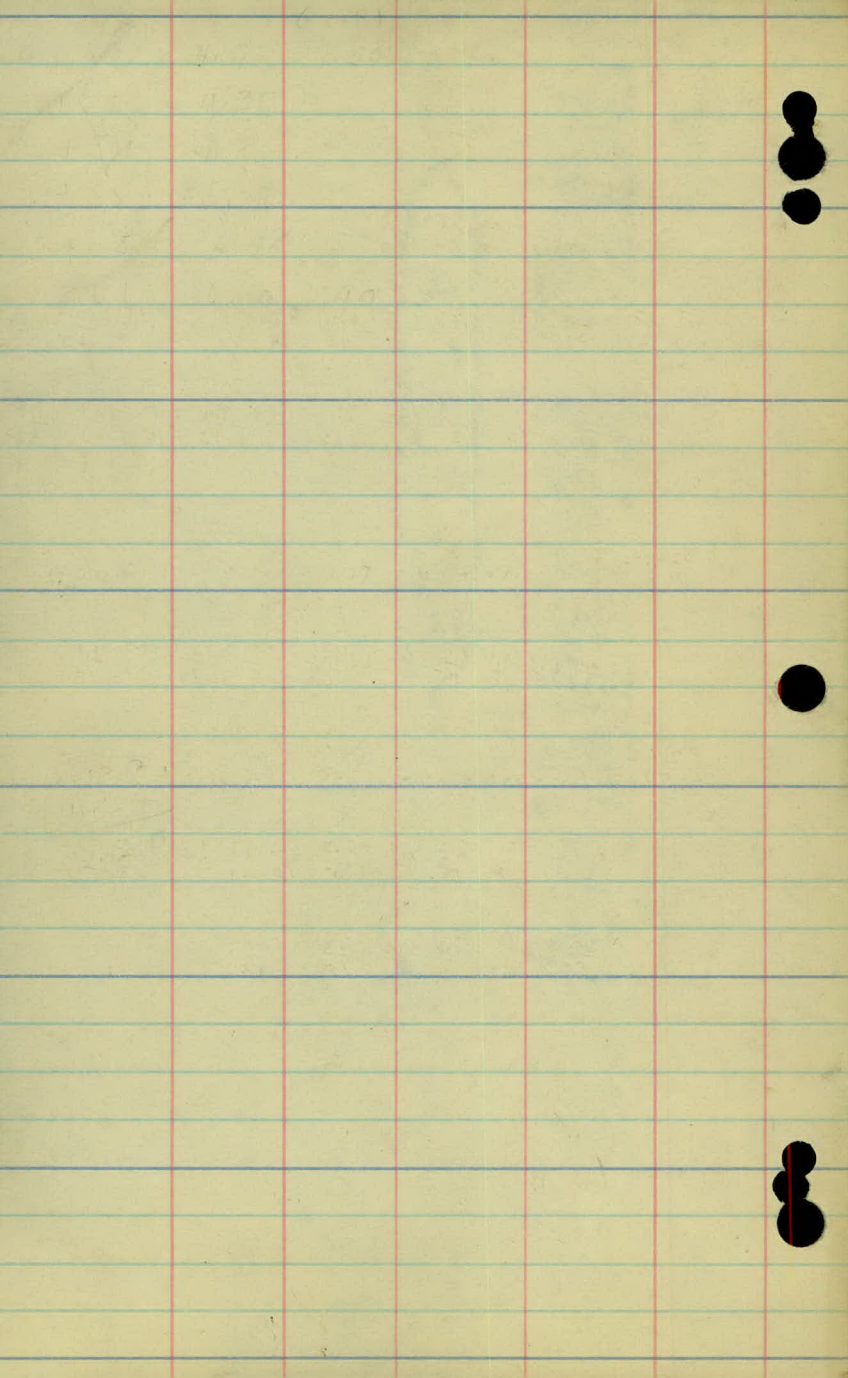
$$\frac{31.0}{42} = \text{Corner of tee on Golf Course}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 29 \end{array} \quad \begin{array}{r} 7.6 \\ 19 \end{array} \quad \begin{array}{r} 6.7 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 00 \end{array} \quad \begin{array}{r} 6.6 \\ 6 \end{array} \quad \begin{array}{r} 8.5 \\ 9 \end{array} \quad \begin{array}{r} 10.1 \\ 14 \end{array} \quad \begin{array}{r} 10.4 \\ 17 \end{array} \quad \begin{array}{r} 11.1 \\ 33 \end{array}$$

$$\frac{21.9}{44} = \text{Corner of tee on Golf Course}$$

$$\begin{array}{r} 3.5 \\ 33 \end{array} \quad \begin{array}{r} 3.7 \\ 31 \end{array} \quad \begin{array}{r} 6.7 \\ 21 \end{array} \quad \begin{array}{r} 6.2 \\ 18 \end{array} \quad \begin{array}{r} 6.1 \\ 00 \end{array} \quad \begin{array}{r} 6.3 \\ 5 \end{array} \quad \begin{array}{r} 8.3 \\ 10 \end{array} \quad \begin{array}{r} 9.1 \\ 14 \end{array} \quad \begin{array}{r} 9.9 \\ 21 \end{array} \quad \begin{array}{r} 10.2 \\ 33 \end{array}$$

$$\begin{array}{r} 5.4 \\ 33 \end{array} \quad \begin{array}{r} 3.7 \\ 29 \end{array} \quad \begin{array}{r} 5.5 \\ 16 \end{array} \quad \begin{array}{r} 5.6 \\ 00 \end{array} \quad \begin{array}{r} 5.7 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array}$$



1
Check of Blue Tops
as set by W. P.A.

East Avenue
South of Larp. to Larpenteur
Sta. 47+00 to Sta. 52+72.2

W. H. Carlson
4/30/37

Sta.	+	+	-	Grade	Elev.
B.M.	5.06	1026.05			1020.99
47+00				1019.7	
45				19.8	
+75				19.9	
48+0				19.9	
+50				20.0	
49				20.1	
+25				20.1	
+60				20.2	
50				20.3	
+50				20.4	
51+0				20.5	

Grade Rod Lt. E Rt.

(Top Mon. Sta. 52+72.2)

6.35

$\frac{6.37}{16}$

$\frac{6.33}{16}$

6.25

$\frac{6.30}{16}$

$\frac{6.25}{16}$

6.15

$\frac{6.17}{16}$

$\frac{6.15}{16}$

6.15

$\frac{6.16}{16.1}$

$\frac{6.10}{16.0}$

6.05

$\frac{6.01}{16.1}$

$\frac{6.05}{16.0}$

5.95

$\frac{5.98}{16.3}$

$\frac{5.98}{16.2}$

5.95

$\frac{5.95}{16.1}$

$\frac{5.92}{16.1}$

5.85

$\frac{5.83}{16.}$

$\frac{5.88}{16.3}$

5.75

$\frac{5.75}{16.2}$

$\frac{5.63}{16.1}$

5.65

$\frac{5.67}{16.3}$

$\frac{5.64}{16.3}$

5.55

$\frac{5.55}{16.0}$

$\frac{5.54}{16.0}$

Rod Readings
and Distances
to Stakes as
set.

Sta.	+	π	-	Grade	Elev.
------	---	-------	---	-------	-------

1026.05

51+50

20.6

52

20.7

+35

20.8

+57

52+72.2 $\pm$ Larp.

5.06

1020.99

Grade Rod

Lt.

L

Rt.

5.45

$$\begin{array}{r} 5.46 \\ 16.1 \end{array}$$

$$\begin{array}{r} 5.44 \\ 16.3 \end{array}$$

5.35

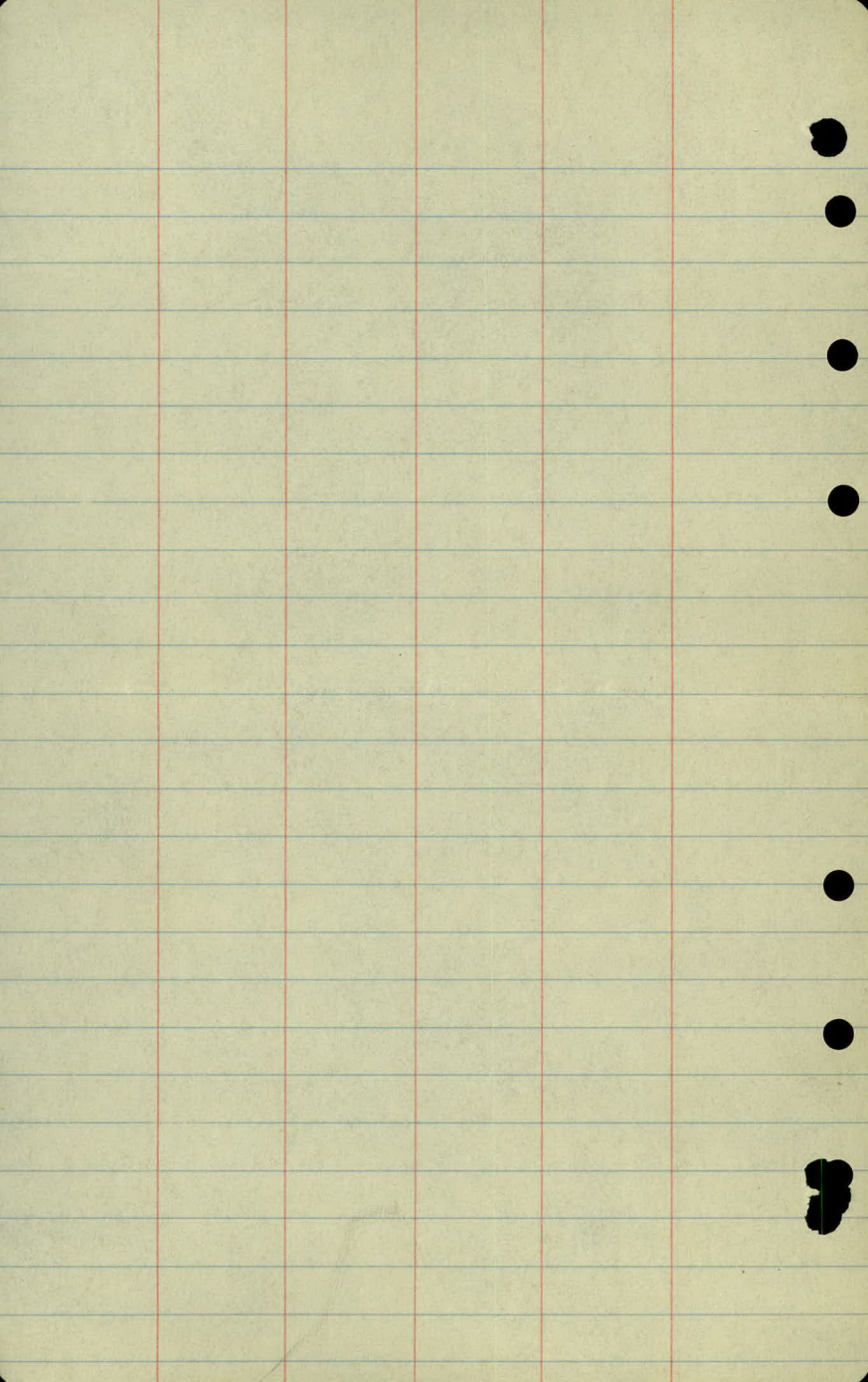
$$\begin{array}{r} 5.33 \\ 16.2 \end{array}$$

$$\begin{array}{r} 5.43 \\ 16.1 \end{array}$$

5.25

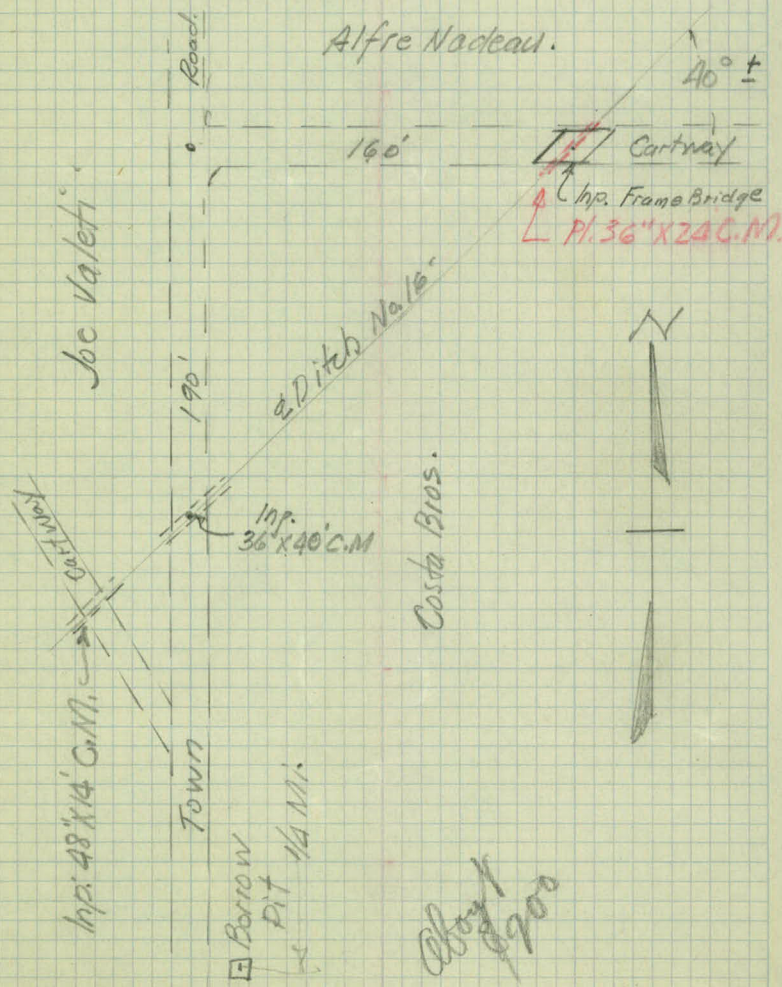
$$\begin{array}{r} 5.22 \\ 16.2 \end{array}$$

$$\begin{array}{r} 5.23 \\ 16.1 \end{array}$$



Proposed.
2 x 2 Wood Box Culvert
East Avenue
Sta. 45+95

Proposed Culvert Ditch #16

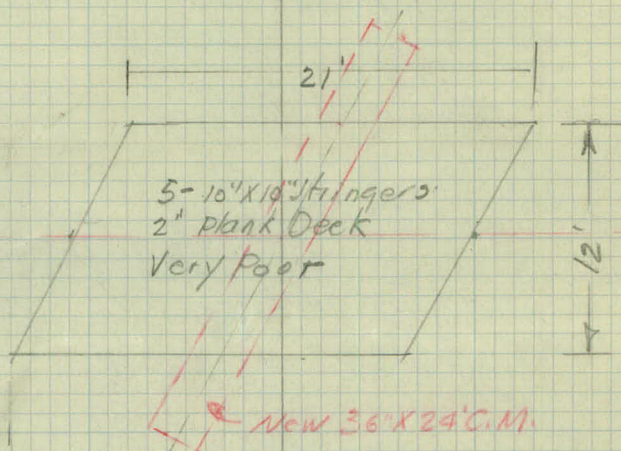


W. H. Carlson
4-2/37

Abey
\$900

over.

Existing Bridge



12' Road Way for Hay Rake

6' Slopes

$\frac{6}{24}$ - total Culvert

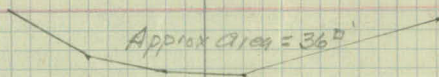
$$\frac{0.0}{20} = \frac{4.0}{20}$$

$$\frac{0.4}{16}$$

$$\frac{7.1}{12}$$

$$\frac{7.4}{8}$$

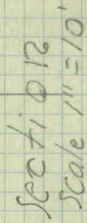
$$\frac{4.0}{0}$$



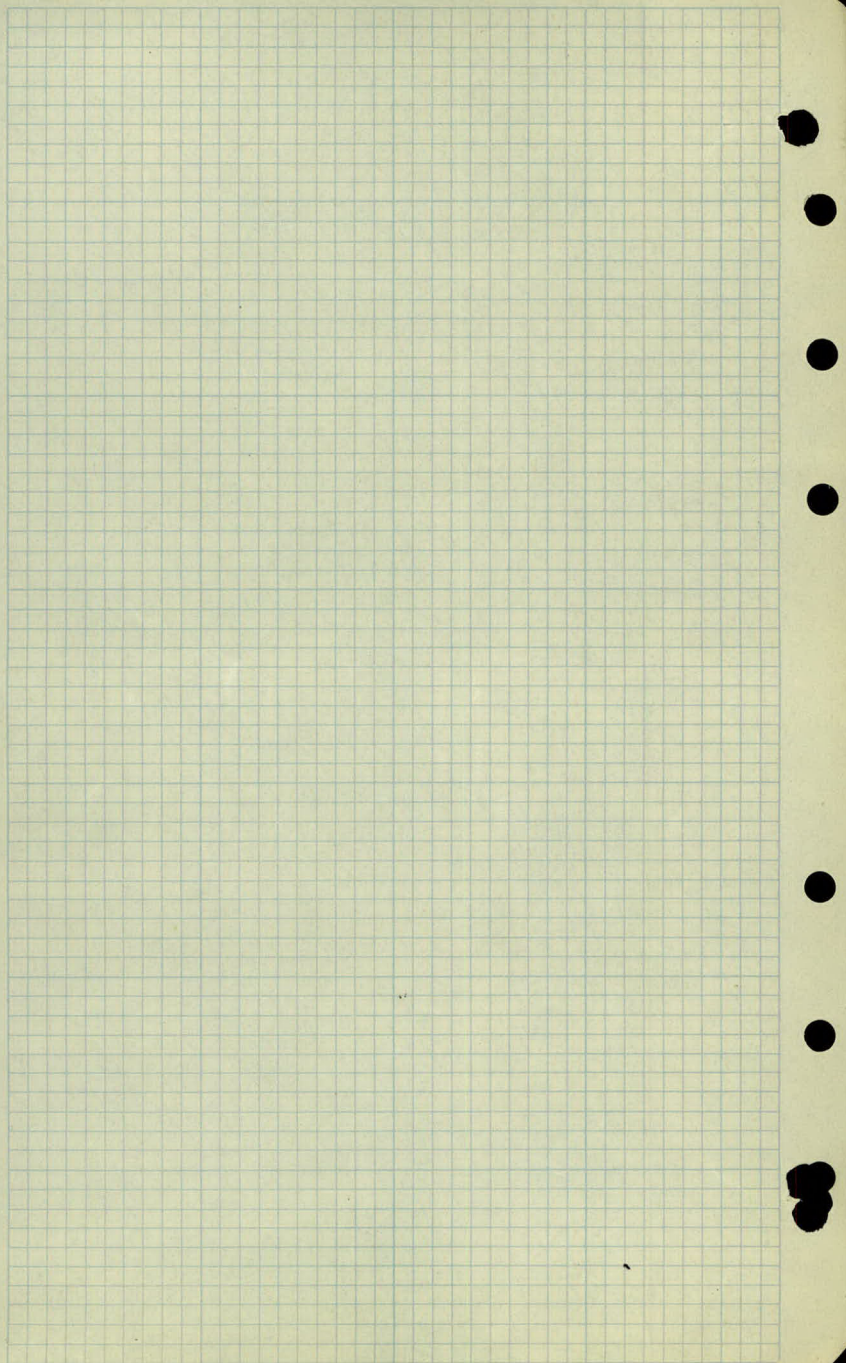
Typical X-sec.

15 Cu. Yds Fill

Haul from 1/4 Mi. South
on Town Road.



W. A. Carlson
May 3, 1937



East Ave.

$\frac{1}{2}$ Mi. So. of Larp to Larp.

Construction Notes.

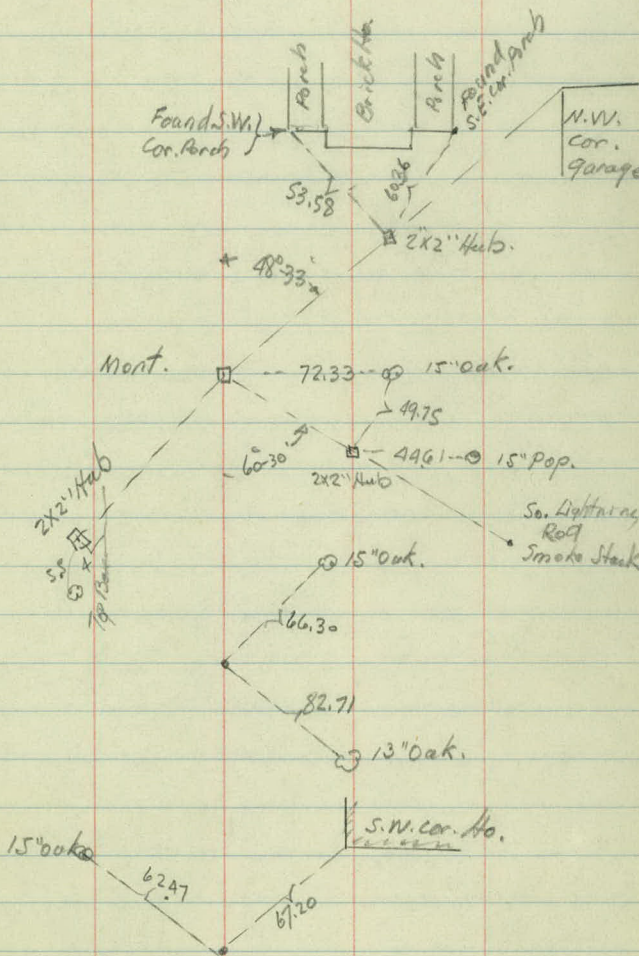
Station Point

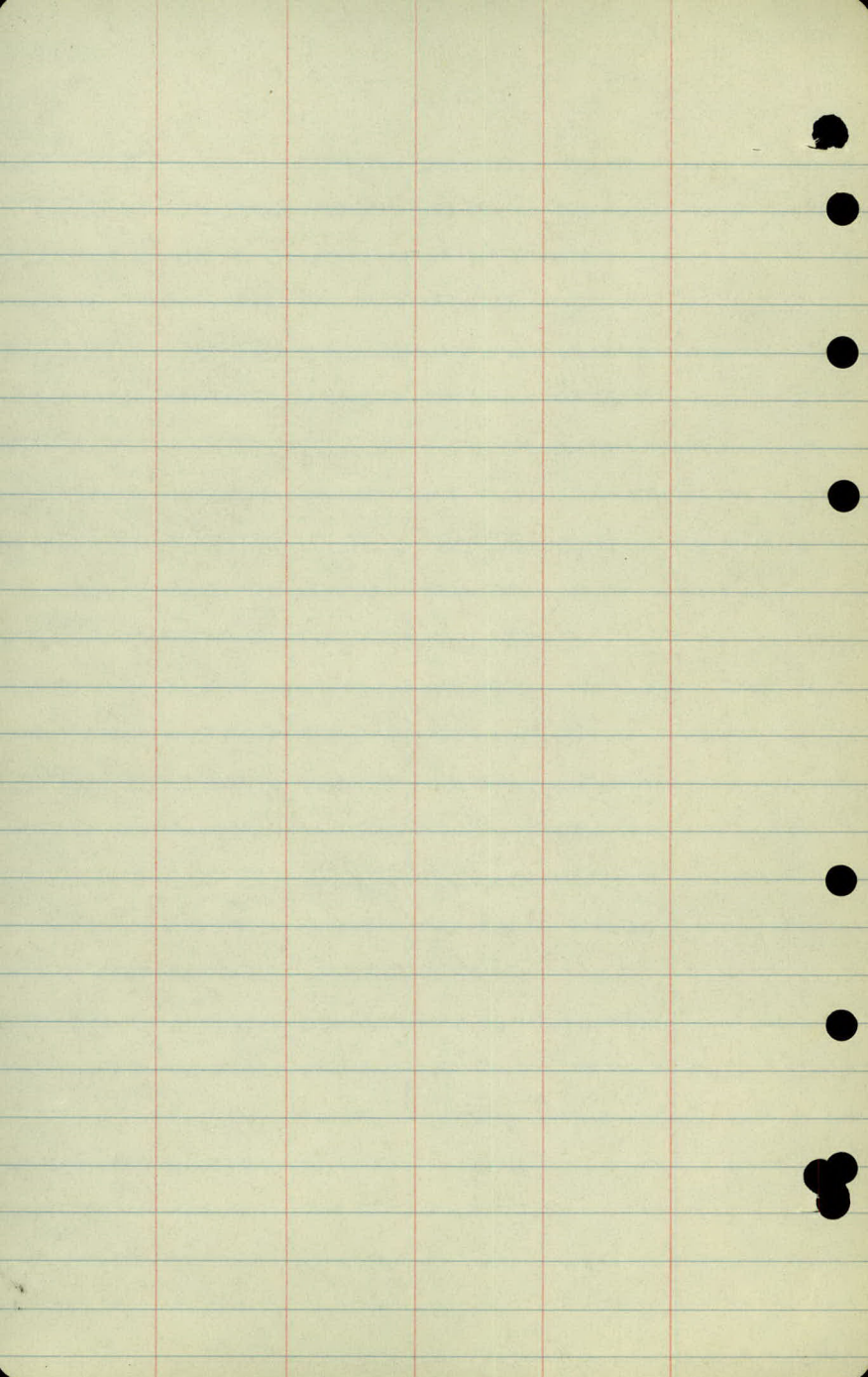
52t £ Larp Mon

34+00 P.O.T.

28+37.34/

4





East Ave

$\frac{1}{2}$ mi. So. of Larp to Larp.

Slope stakes

Sta.	+	-	Elev.	Grade.
B.M.	8.88	1005.32		(996.44)
26 + 36.1				97.8
27				99.8
+50				01.8
+25				02.8
T.P.	13.46	1016.98	1.80	1003.52
28				03.9
+25				04.9
+50				06.0
29				08.3
+50				10.6
30				13.1
+50				15.7
T.P.	13.35	1027.78	2.55	1014.43
31				18.3
+50				21.1
32				23.9
T.P.	12.74	1039.52	1.00	1026.76

998.78

Nail in P.D. Rd. Sta. 26+40

Nov. 13, 1936

W.A.C.

K.A.

L.B.

L.B.H.

A.M.

M.J.

(Moa Tipped) 4 8 24

Spk in 14" Cottonwood 20' Rd 26+46

$$7.5 \quad 33 \overline{) 9.2} \quad \begin{array}{r} 10.8 \\ -3.3 \\ \hline \end{array} \quad \begin{array}{r} 8.0 \\ -1.5 \\ \hline 3.3 \end{array}$$

$$5.5 \quad (7.0) \quad 33 \overline{) 8.3} \quad \begin{array}{r} 8.0 \\ -2.5 \\ \hline \end{array} \quad \begin{array}{r} 10.4 \\ -4.9 \\ \hline 3.3 \end{array}$$

$$3.5 \quad 33 \overline{) 4.0} \quad \begin{array}{r} 5.7 \\ -2.2 \\ \hline \end{array} \quad \begin{array}{r} 9.3 \\ -6.2 \\ \hline 3.3 \end{array}$$

$$2.5 \quad 33 \overline{) 10.8} \quad \begin{array}{r} 4.7 \\ -2.2 \\ \hline \end{array} \quad \begin{array}{r} 6.7 \\ -4.2 \\ \hline 2.5 \end{array}$$

$$13.1 \quad 33 \overline{) 3.1} \quad \begin{array}{r} 10.5 \\ +2.6 \\ \hline \end{array} \quad \begin{array}{r} 13.1 \\ 0.0 \\ \hline 10.5 \end{array} \quad \begin{array}{r} 14.5 \\ 0.0 \\ \hline 13.1 \end{array}$$

$$12.1 \quad 33 \overline{) 10.8} \quad \begin{array}{r} 7.3 \\ +4.8 \\ \hline \end{array} \quad \begin{array}{r} 10.6 \\ +1.5 \\ \hline 3.3 \end{array}$$

$$11.0 \quad 33 \overline{) 1.9} \quad \begin{array}{r} 7.6 \\ +3.1 \\ \hline \end{array} \quad \begin{array}{r} 8.0 \\ +2.0 \\ \hline 3.3 \end{array}$$

$$10.2 \quad 1.5 \quad 33 \overline{) 10.2} \quad \begin{array}{r} 7.8 \\ +2.9 \\ \hline \end{array} \quad \begin{array}{r} 7.3 \\ +1.4 \\ \hline 3.3 \end{array}$$

$$6.4 \quad 30.1 \overline{) 1.1} \quad \begin{array}{r} 8.0 \\ -1.8 \\ \hline \end{array} \quad \begin{array}{r} 26.1 \\ -2.2 \\ \hline 2.9 \end{array} \quad \begin{array}{r} 28.0 \\ 2.0 \\ \hline 3.3 \end{array}$$

$$2.9 \quad 33 \overline{) 10.2} \quad \begin{array}{r} 7.1 \\ -3.2 \\ \hline \end{array} \quad \begin{array}{r} 7.5 \\ -2.6 \\ \hline 2.9 \end{array}$$

$$1.3 \quad 1.8 \quad 33 \overline{) 7.4} \quad \begin{array}{r} 5.3 \\ -4.0 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ -3.1 \\ \hline 1.3 \end{array}$$

$$9.5 \quad 11.0 \quad 33 \overline{) 15.8} \quad \begin{array}{r} 13.5 \\ -4.0 \\ \hline \end{array} \quad \begin{array}{r} 8.7 \\ +0.8 \\ \hline 3.3 \end{array}$$

$$6.7 \quad 33 \overline{) 12.1} \quad \begin{array}{r} 9.8 \\ -3.1 \\ \hline \end{array} \quad \begin{array}{r} 4.0 \\ +2.7 \\ \hline 3.3 \end{array}$$

$$2.9 \quad 33 \overline{) 7.9} \quad \begin{array}{r} 5.5 \\ -1.6 \\ \hline \end{array} \quad \begin{array}{r} 4.0 \\ +2.4 \\ \hline 3.3 \end{array}$$

Sta.	+	X	-	Elev.	grade
------	---	---	---	-------	-------

1039.52

32 +45

26.4

+60

27.3

33

29.5

T.P.

11.89

1048.86

2.55

1036.97

+50

32.3

34

34.9

+50

37.0

35

38.6

+50

39.8

36

40.5

T.P.

11.73

1054.69

5.90

1042.96

+30

40.8

+80

40.8

37

40.6

Lt

C

Rt

$$13.1 \quad \frac{146}{1}$$

$$75.7 \quad \frac{146}{2.0}$$

$$\frac{13.0}{-0.2}$$

$$\frac{6.0}{7.1/33}$$

$$10.0$$

$$33 \quad \frac{9.0}{+1.0}$$

$$\frac{82}{+1.8}$$

$$\frac{0.8}{+9.2/33}$$

$$16.6$$

$$33 \quad \frac{13.1}{+3.5}$$

$$\frac{132}{+3.4}$$

$$\frac{7.6}{+9.0/33}$$

$$14.0$$

$$33 \quad \frac{11.9}{+2.1}$$

$$\frac{11.2}{+2.8}$$

$$\frac{8.3}{+5.7/33}$$

$$11.9$$

$$33 \quad \frac{12.7}{+0.7}$$

$$\frac{10.2}{+1.7}$$

$$\frac{9.8}{+2.1/33}$$

$$10.3$$

$$72 \quad \frac{12.3}{-2.0}$$

$$\frac{10.2}{+0.1}$$

$$\frac{10.2}{+9.6/33} \quad (2.9 \text{ Diff } Rt)$$

$$9.0$$

$$33 \quad \frac{10.0}{+0.8}$$

$$\frac{8.8}{+0.5}$$

$$\frac{11.0}{-2.0/2.0}$$

$$8.3$$

$$33 \quad \frac{12.4}{+4.1}$$

$$\frac{6.8}{+1.5}$$

$$\frac{4.8}{+4.0/33}$$

$$13.9$$

$$33 \quad \frac{5.3}{+8.6}$$

$$\frac{11.7}{+2.2}$$

$$\frac{2.9}{+11.0/33}$$

$$13.9$$

$$33 \quad \frac{10.4}{+3.5}$$

$$\frac{12.3}{+1.6}$$

$$\frac{3.3}{+10.6/33}$$

$$14.1$$

$$33 \quad \frac{14.2}{+0.1}$$

$$\frac{13.1}{+1.0}$$

$$\frac{6.0}{+7.8/33}$$

Sta.	+	π 1054.69	-	Elev.	Grade.
	1.94	1043.64	13.02	1041.67	
37 +30					40.3
+70					39.6
38					38.9
+50					37.3
39					35.5
+54					33.5
T.P.	2.37	1035.81	10.16		1033.48
40					31.9
+50					30.1
41					28.3
+50					26.5
+75					25.6
42					24.8

lt.

8

rt.

3.3

4.8

33 $\frac{9.3}{-6.0}$

$\frac{3.1}{+0.2}$

$\frac{3.3}{+0.0} / 33$

1041.70 - 38' lt. 37+30 10°00k

4.0

30.1 $\frac{8.7}{-4.7}$

$\frac{4.3}{-0.0}$

$\frac{7.0}{-2.0} / 25.0$

4.7

33 $\frac{5.6}{-2.6}$

$\frac{4.8}{-0.1}$

$\frac{4.4}{+0.3} / 33$

6.3

2.7

33 $\frac{2.7}{+3.6}$

$\frac{5.6}{+0.7}$

$\frac{1.7}{+4.6} / 33$

8.1

3.0

33 $\frac{3.6}{+4.8}$

$\frac{2.7}{+0.4}$

$\frac{3.6}{+4.5} / 33$

10.1

11.0

33 $\frac{5.2}{+4.9}$

$\frac{1.2}{-0.1}$

$\frac{11.6}{+0.0} / 33$

Top Mon. High Pt. S.E. Cor. 39+54.6

3.9

33 $\frac{2.7}{+1.2}$

$\frac{4.7}{-1.0}$

$\frac{9.3}{-5.4} / 32.2$

5.7

33 $\frac{4.7}{+1.6}$

$\frac{7.0}{-1.3}$

$\frac{10.2}{-4.5} / 29.5$

7.5

33 $\frac{7.4}{+0.1}$

$\frac{8.3}{-0.8}$

$\frac{9.2}{-1.7} / 21.1$

9.3

33 $\frac{5.9}{+0.4}$

$\frac{9.5}{-0.2}$

$\frac{9.6}{+1.2} / 33$

10.2

33 $\frac{11.1}{+9.1}$

11.0

33 $\frac{4.8}{+0.2}$

$\frac{11.2}{+0.2}$

$\frac{10.6}{+0.4} / 33$

Sta.	+	x	-	Elev.	Grade
		1035.81			
42 +40					23.6
T.P.	1.36	1024.23	1294	1022.87	
+80					22.5
43					22.1
+50					21.1
44					20.3
+50					19.8
15100 44 + 90					19.5
+25					19.4
+60					19.4
46					19.5
+30					19.6
+65					19.7

4.

2

21.

12.2

13.7

$$\begin{array}{r} 33 \\ 10.8 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 12.8 \\ \hline -8.6 \end{array}$$

$$\begin{array}{r} 13.1 \\ 20.3/33 \end{array}$$

1.7

13.7

$$\begin{array}{r} 33 \\ 7.2 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 2.1 \\ \hline -0.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ 2.4/29.2 \end{array}$$

2.1

$$\begin{array}{r} 283 \\ 6.2 \\ \hline -4.1 \end{array}$$

$$\begin{array}{r} 2.7 \\ \hline -8.6 \end{array}$$

$$\begin{array}{r} 7.5 \\ 5.5/32.2 \end{array}$$

3.1

$$\begin{array}{r} 298 \\ 7.7 \\ \hline -4.6 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline -0.7 \end{array}$$

$$\begin{array}{r} 8.1 \\ 5.0/31.0 \end{array}$$

3.9

$$\begin{array}{r} 280 \\ 7.9 \\ \hline -4.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ \hline -0.1 \end{array}$$

$$\begin{array}{r} 8.1 \\ 4.2/28.6 \end{array}$$

4.4

$$\begin{array}{r} 26.8 \\ 8.0 \\ \hline 3.6 \end{array}$$

$$\begin{array}{r} 4.3 \\ \hline 10.1 \end{array}$$

$$\begin{array}{r} 7.8 \\ 3.4/26.2 \end{array}$$

4.7

6.2

$$\begin{array}{r} 33 \\ 5.3 \\ \hline 20.9 \end{array}$$

$$\begin{array}{r} 4.0 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 7.4 \\ 2.7/24.1 \end{array}$$

4.8

$$\begin{array}{r} 33 \\ 1.8 \\ \hline 18.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ \hline 10.8 \end{array}$$

$$\begin{array}{r} 6.9 \\ 2.1/22.3 \end{array}$$

4.8

6.3

$$\begin{array}{r} 33 \\ 5.7 \\ \hline 20.9 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 7.7 \\ 2.4/23.2 \end{array}$$

4.7

$$\begin{array}{r} 30.4 \\ 9.5 \\ \hline 4.8 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 8.5 \\ 2.8/27.4 \end{array}$$

$$\begin{array}{r} 8.1 \\ 0.20/33 \end{array}$$

DTR 8.4

4.6

$$\begin{array}{r} 4.6 \\ \hline 10.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ 3.4/46.2 \end{array}$$

$$\begin{array}{r} 7.4 \\ 0.29/33 \end{array}$$

8.3

4.5

$$\begin{array}{r} 76.5 \\ 18.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 11.4 \\ \hline 10.1 \end{array}$$

$$\begin{array}{r} 8.2 \\ 3.7/21.1 \end{array}$$

$$\begin{array}{r} 4.9 \\ 0.22/33 \end{array}$$

8.2

Sta.	+	π	-	Elev.	grade
------	---	-------	---	-------	-------

1024.23

47					19.7
----	--	--	--	--	------

+45					19.8
-----	--	--	--	--	------

+75					19.9
-----	--	--	--	--	------

48					19.9
----	--	--	--	--	------

+50					20.0
-----	--	--	--	--	------

49					20.1
----	--	--	--	--	------

T.P.	8.04	1028.44	3.83	1020.40	
------	------	---------	------	---------	--

+25					20.1
-----	--	--	--	--	------

+60					20.2
-----	--	--	--	--	------

50					20.3
----	--	--	--	--	------

+50					20.4
-----	--	--	--	--	------

51					20.5
----	--	--	--	--	------

+50					20.6
-----	--	--	--	--	------

LT. E RT.

Dist. Road.

$$\begin{array}{r} 4.5 \\ 187 \overline{) 54} \\ -09 \end{array} \quad \begin{array}{r} 40 \\ 105 \end{array} \quad \begin{array}{r} 17 \\ 20.64 \end{array} \quad 8.1$$

$$\begin{array}{r} 4.4 \\ 229 \overline{) 67} \\ -23 \end{array} \quad \begin{array}{r} 42 \\ 102 \end{array} \quad \begin{array}{r} 80 \\ 76 \overline{) 26.8} \end{array} \quad 8.0$$

$$\begin{array}{r} 4.3 \\ 322 \overline{) 97} \\ -54 \end{array} \quad \begin{array}{r} 50 \\ -07 \end{array} \quad \begin{array}{r} 94 \\ -5.1 \overline{) 31.3} \end{array}$$

$$\begin{array}{r} 4.3 \\ 322 \overline{) 97} \\ -54 \end{array} \quad \begin{array}{r} 50 \\ -07 \end{array} \quad \begin{array}{r} 94 \\ -5.1 \overline{) 31.3} \end{array}$$

$$\begin{array}{r} 4.2 \\ 328 \overline{) 98} \\ -56 \end{array} \quad \begin{array}{r} 51 \\ -09 \end{array} \quad \begin{array}{r} 90 \\ -5.0 \overline{) 31.0} \end{array}$$

$$\begin{array}{r} 4.1 \\ 735 \overline{) 6.6} \\ -26 \end{array} \quad \begin{array}{r} 41 \\ 6 \end{array} \quad \begin{array}{r} 69 \\ 28 \overline{) 24.4} \end{array}$$

$$\begin{array}{r} 9.8 \\ 8.3 \\ 73 \overline{) 84} \\ -21.4 \end{array} \quad \begin{array}{r} 78 \\ 105 \end{array} \quad \begin{array}{r} 9.8 \\ 200 \overline{) 33} \end{array} \quad \text{Day/}$$

$$\begin{array}{r} 9.7 \\ 8.2 \\ 33 \overline{) 3.5} \\ -11.7 \end{array} \quad \begin{array}{r} 74 \\ 108 \end{array} \quad \begin{array}{r} 9.7 \\ 200 \overline{) 27.2} \end{array} \quad \text{D. St.}$$

$$\begin{array}{r} 9.6 \\ 8.1 \\ 73 \overline{) 1.8} \\ -16.3 \end{array} \quad \begin{array}{r} 69 \\ 11.2 \end{array} \quad \begin{array}{r} 9.6 \\ 200 \overline{) 16.2} \end{array} \quad 5.14$$

$$\begin{array}{r} 9.5 \\ 8.0 \\ 26 \overline{) 2.2} \\ -15.8 \end{array} \quad \begin{array}{r} 71 \\ 109 \end{array} \quad \begin{array}{r} 9.5 \\ 200 \overline{) 24.9} \end{array} \quad \text{D. St.}$$

$$\begin{array}{r} 7.9 \\ 53 \overline{) 5.5} \\ -12.4 \end{array} \quad \begin{array}{r} 76 \\ 103 \end{array} \quad \begin{array}{r} 11.9 \\ -40 \overline{) 28.0} \end{array}$$

$$\begin{array}{r} 7.8 \\ 33 \overline{) 7.7} \\ -10.1 \end{array} \quad \begin{array}{r} 83 \\ -05 \end{array} \quad \begin{array}{r} 11.9 \\ -5.1 \overline{) 31.3} \end{array}$$

Sta.	+	-	Elev.	Grade
		1078.44		
5%				20.7
+35				20.8
+57				
B.M.		7.49		1020.99

H.

L

H.

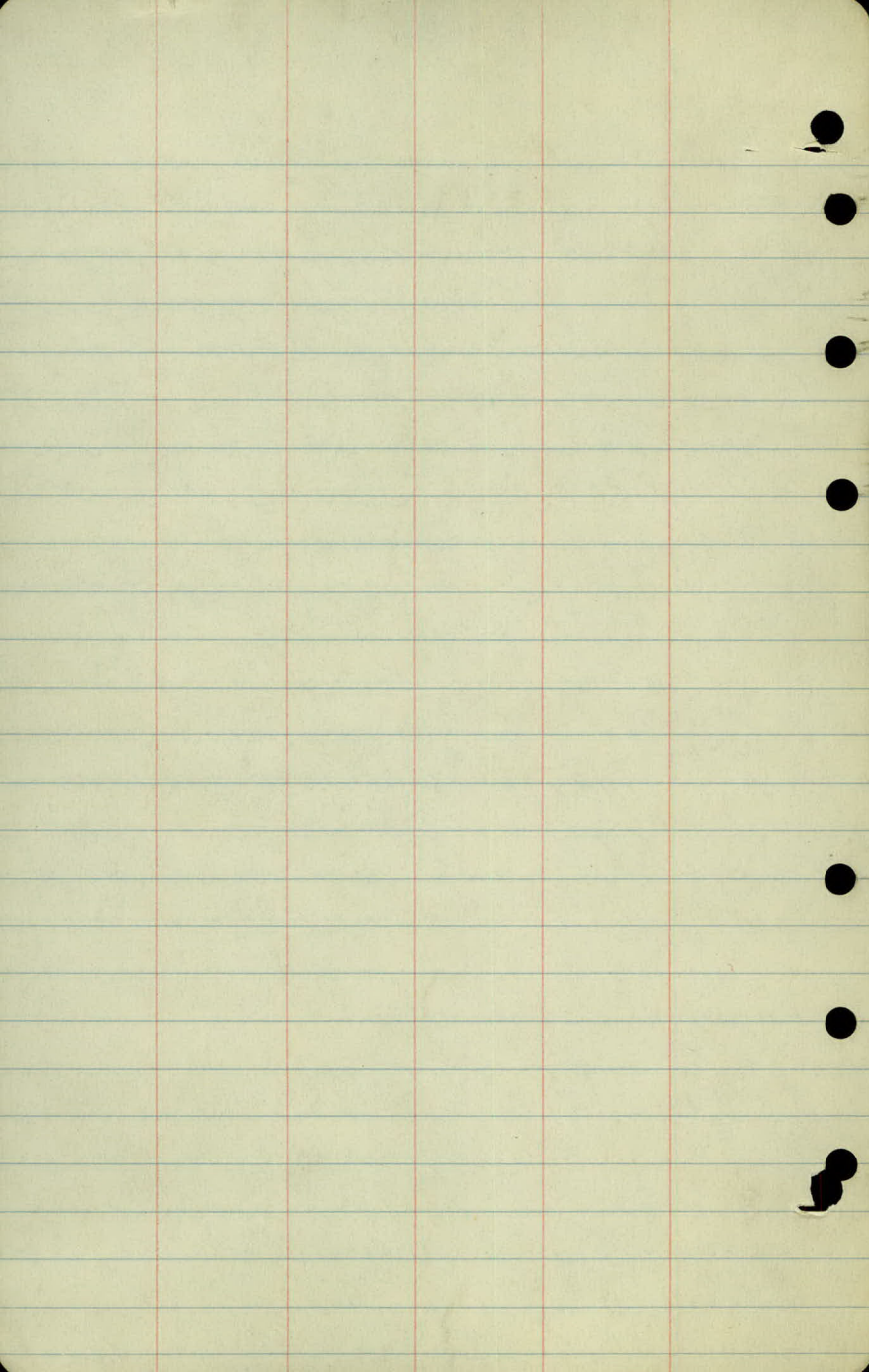
7.7

$$23 \overline{) 8.7} \\ \underline{18.0} \\ 0.7$$

$$\frac{8.4}{-0.7}$$

$$\frac{13.0}{-5.3} / 31.9$$

Top Mont at 52 + 72.2



East Ave

X Sections

Sta 25+50 to 31

Oct 9, 1951

K. Parker

Sta	+	π	-	Elev
B.M.	7.30	1007.42		998.28

25	+50			95.5
----	-----	--	--	------

	+85			95.7
--	-----	--	--	------

	+93			97.4
--	-----	--	--	------

26	+10			97.5
		$\frac{1}{2}$ Omaha Red & Gun Club Rd.		

	+55			98.2
--	-----	--	--	------

27				99.7
----	--	--	--	------

	+50			1002.0
--	-----	--	--	--------

28				1004.3
----	--	--	--	--------

	+25			1005.5
--	-----	--	--	--------

T.P.	13.40	1020.04	0.34	1006.64
------	-------	---------	------	---------

	+50			06.6
--	-----	--	--	------

29				08.8
----	--	--	--	------

Lt.

C

Rt.

Nail in P.P. to Rt. sta 26+26

$\frac{113}{50}$	$\frac{109}{35}$	$\frac{112}{20}$	$\frac{110}{40}$	$\frac{120}{10}$	$\frac{128}{10}$	$\frac{130}{25}$	$\frac{130}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{100}{50}$	$\frac{101}{41}$	$\frac{110}{22}$	$\frac{112}{50}$	$\frac{118}{20}$	$\frac{123}{20}$	$\frac{129}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{134}{50}$	$\frac{129}{42}$	$\frac{100}{29}$	$\frac{110}{22}$	$\frac{102}{14}$	$\frac{101}{28}$	$\frac{99}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------

$\frac{115}{50}$	$\frac{115}{31}$	$\frac{107}{21}$	$\frac{97}{17}$	$\frac{100}{25}$	$\frac{100}{25}$	$\frac{97}{50}$	$\frac{80}{100}$
------------------	------------------	------------------	-----------------	------------------	------------------	-----------------	------------------

$\frac{102}{50}$	$\frac{109}{32}$	$\frac{96}{21}$	$\frac{93}{28}$	$\frac{99}{28}$	$\frac{107}{34}$	$\frac{105}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{105}{50}$	$\frac{100}{23}$	$\frac{82}{23}$	$\frac{78}{24}$	$\frac{85}{24}$	$\frac{120}{24}$	$\frac{12.7}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------

$\frac{55}{50}$	$\frac{57}{34}$	$\frac{67}{30}$	$\frac{66}{22}$	$\frac{59}{18}$	$\frac{55}{20}$	$\frac{63}{20}$	$\frac{114}{31}$	$\frac{122}{41}$	$\frac{122}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{51}{26}$	$\frac{51}{21}$	$\frac{36}{17}$	$\frac{32}{17}$	$\frac{40}{14}$	$\frac{42}{22}$	$\frac{53}{21}$	$\frac{72}{31}$	$\frac{9.7}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{17}{50}$	$\frac{21}{33}$	$\frac{24}{29}$	$\frac{24}{20}$	$\frac{21}{16}$	$\frac{20}{17}$	$\frac{25}{21}$	$\frac{40}{21}$	$\frac{40}{29}$	$\frac{10}{33}$	$\frac{20}{41}$	$\frac{6.7}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{27}{50}$	$\frac{49}{22}$	$\frac{153}{26}$	$\frac{152}{23}$	$\frac{127}{16}$	$\frac{124}{17}$	$\frac{140}{24}$	$\frac{101}{24}$	$\frac{101}{27}$	$\frac{112}{33}$	$\frac{124}{50}$
-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{134}{50}$	$\frac{133}{23}$	$\frac{130}{24}$	$\frac{117}{16}$	$\frac{112}{17}$	$\frac{118}{17}$	$\frac{140}{23}$	$\frac{142}{21}$	$\frac{102}{33}$	$\frac{101}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

Sta	+	π	-	Elev
		1020.04		
28				
29	+50			1010.8
30				13.0
	+50			15.3
31				18.2

Lt.

K

Rt.

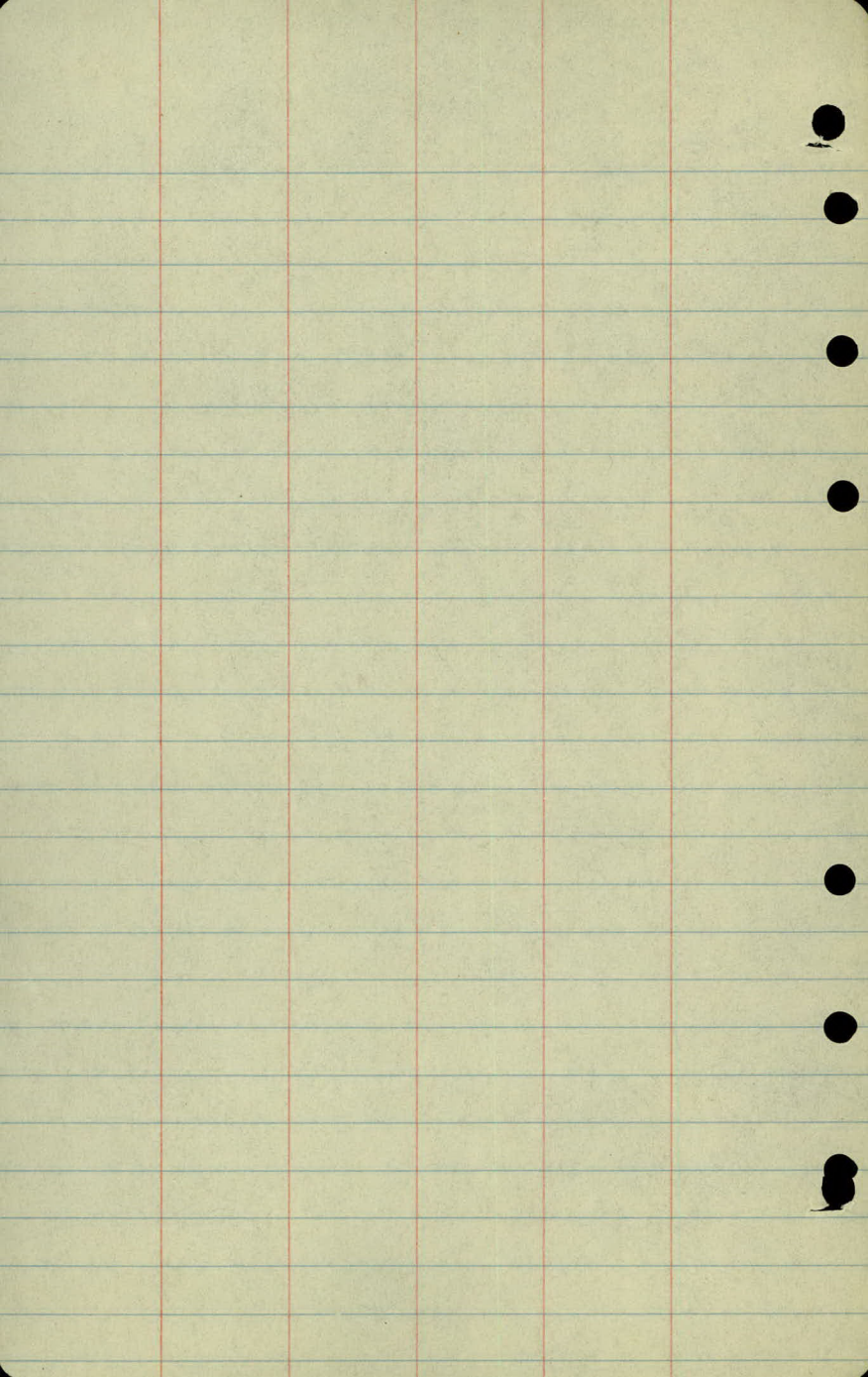
$$\frac{34}{50} \quad \frac{64}{330}$$

$$\frac{143}{50} \quad \frac{140}{32} \quad \frac{96}{17} \quad \frac{92}{16} \quad \frac{97}{16} \quad \frac{114}{22} \quad \frac{116}{59} \quad \frac{116}{50}$$

$$\frac{130}{50} \quad \frac{129}{29} \quad \frac{77}{17} \quad \frac{70}{17} \quad \frac{77}{17} \quad \frac{94}{24} \quad \frac{99}{28} \quad \frac{89}{50}$$

$$\frac{112}{50} \quad \frac{110}{40} \quad \frac{88}{30} \quad \frac{48}{17} \quad \frac{47}{17} \quad \frac{51}{16} \quad \frac{66}{23} \quad \frac{67}{22} \quad \frac{51}{50}$$

$$\frac{80}{50} \quad \frac{71}{31} \quad \frac{22}{17} \quad \frac{18}{17} \quad \frac{23}{18} \quad \frac{35}{22} \quad \frac{35}{29} \quad \frac{08}{14} \quad \frac{00}{50}$$



East Ave. 50.

X Sections
Sta 40 - 52+74.2

Sta.	+	A	-	Elev.
B.M.	2.03	1043.78		1041.70
I.P.	0.88	1032.78	11.78	1031.95
40	+00			32.0
	+50			30.0
41				28.4
	+50			27.0
42				25.2
	+50			23.8
I.P.	2.86	1025.92	10.22	1022.56
43				22.5
	+50			21.6
44				21.1
	+50			20.8
45				20.6

ht.

h

Rt.

5 pt in 10" Oak 35' Rt sta 37+30.

98

38

44

58

$\frac{10}{50}$	$\frac{20}{38}$	$\frac{25}{25}$	$\frac{28}{20}$	$\frac{80}{16}$	$\frac{76}{16}$	$\frac{80}{16}$	$\frac{99}{21}$	$\frac{96}{31}$	$\frac{78}{39}$	$\frac{93}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{20}{50}$	$\frac{89}{38}$	$\frac{112}{26}$	$\frac{102}{20}$	$\frac{96}{16}$	$\frac{90}{16}$	$\frac{95}{16}$	$\frac{102}{21}$	$\frac{116}{33}$	$\frac{123}{50}$
-----------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{68}{50}$	$\frac{70}{39}$	$\frac{69}{26}$	$\frac{33}{16}$	$\frac{29}{16}$	$\frac{33}{16}$	$\frac{62}{24}$	$\frac{81}{23}$	$\frac{81}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{87}{50}$	$\frac{89}{80}$	$\frac{71}{29}$	$\frac{43}{16}$	$\frac{38}{16}$	$\frac{93}{16}$	$\frac{89}{31}$	$\frac{90}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{26}{50}$	$\frac{89}{28}$	$\frac{78}{21}$	$\frac{50}{16}$	$\frac{43}{16}$	$\frac{47}{16}$	$\frac{74}{22}$	$\frac{84}{29}$	$\frac{85}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

L.O.	$\frac{85}{39}$	$\frac{89}{21}$	$\frac{51}{16}$	$\frac{46}{16}$	$\frac{50}{16}$	$\frac{75}{27}$	$\frac{88}{30}$	$\frac{90}{50}$
------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{26}{50}$	$\frac{52}{47}$	$\frac{60}{34}$	$\frac{75}{21}$	$\frac{68}{18}$	$\frac{59}{16}$	$\frac{48}{16}$	$\frac{51}{16}$	$\frac{77}{23}$	$\frac{73}{29}$	$\frac{75}{30}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Sta	+	π	-	Elev.
		1025.92		
45+50				20.4
46				20.3
+50				20.5
T.P	5.81	1025.96	4.77	1020.65
47				20.7
+50				20.7
48				20.7
+50				20.8
49				21.1
+50				21.0
50				21.1
+50				21.3

Lt

E

Rt

61	56	75	74	55	50	53	82	82	74	74	71
50	88	29	21	16		16	22	26	38	31	50

+75 Beg. Water

103	99	87	55	51	57	80	95	95
50	28	24	15		16	22	31	50

102	103	90	86	57	49	54	83	89	83	62	65
50	32	29	23	16		16	26	28	29	34	50

94	94	74	57	53	58	82	82	85	34
50	38	23	16		16	24	28	34	50

102	94	86	60	53	58	91	98	107
50	35	26	16		16	26	33	50

120	125	94	59	53	59	106	110	L.O.
50	29	25	16		16	31	36	

Water Level 96
Elev. 10174

120	105	94	61	52	62	101	102	L.O.
50	30	24	16		16	29	36	

+100 End Water

93	93	81	53	49	56	83	101	105
50	39	26	16		16	25	39	50

35	35	15	71	71	54	50	54	71	72	93	92
50	46	34	27	20	16		16	30	32	38	50

37	18	14	68	68	53	49	54	69	72	93	93
50	39	32	24	20	16		16	21	32	36	50

28	16	71	66	53	47	53	68	77	75
50	32	25	19	16		16	21	36	50

Sta	+	π	-	Elev
		1025.96		
51	+00			21.3
	+50			21.2
52				21.2
	+34			21.4
	+43			21.4
	+58			21.4
	+12.20			21.2 ← ?
B.M.		4.99	1030.97	1030.99

Lt

L

Rt

$\frac{36}{50}$	$\frac{32}{34}$	$\frac{68}{29}$	$\frac{67}{20}$	$\frac{52}{16}$	<u>47</u>	$\frac{54}{16}$	$\frac{86}{27}$	$\frac{100}{39}$	$\frac{10.9}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------	-----------------	-----------------	------------------	-------------------

$\frac{37}{50}$	$\frac{52}{33}$	$\frac{72}{31}$	$\frac{68}{20}$	$\frac{51}{16}$	<u>48</u>	$\frac{55}{6}$	$\frac{90}{28}$	$\frac{109}{35}$	L.O.
-----------------	-----------------	-----------------	-----------------	-----------------	-----------	----------------	-----------------	------------------	------

$\frac{24}{50}$	$\frac{24}{43}$	$\frac{52}{37}$	$\frac{60}{35}$	$\frac{78}{30}$	$\frac{67}{20}$	$\frac{52}{16}$	<u>48</u>	$\frac{52}{16}$	$\frac{99}{29}$	$\frac{104}{37}$	$\frac{10.4}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------	-----------------	-----------------	------------------	-------------------

$\frac{29}{50}$	$\frac{38}{35}$	$\frac{66}{30}$	$\frac{65}{21}$	$\frac{52}{16}$	<u>46</u>	$\frac{52}{16}$	$\frac{80}{27}$	$\frac{97}{37}$	L.O.
-----------------	-----------------	-----------------	-----------------	-----------------	-----------	-----------------	-----------------	-----------------	------

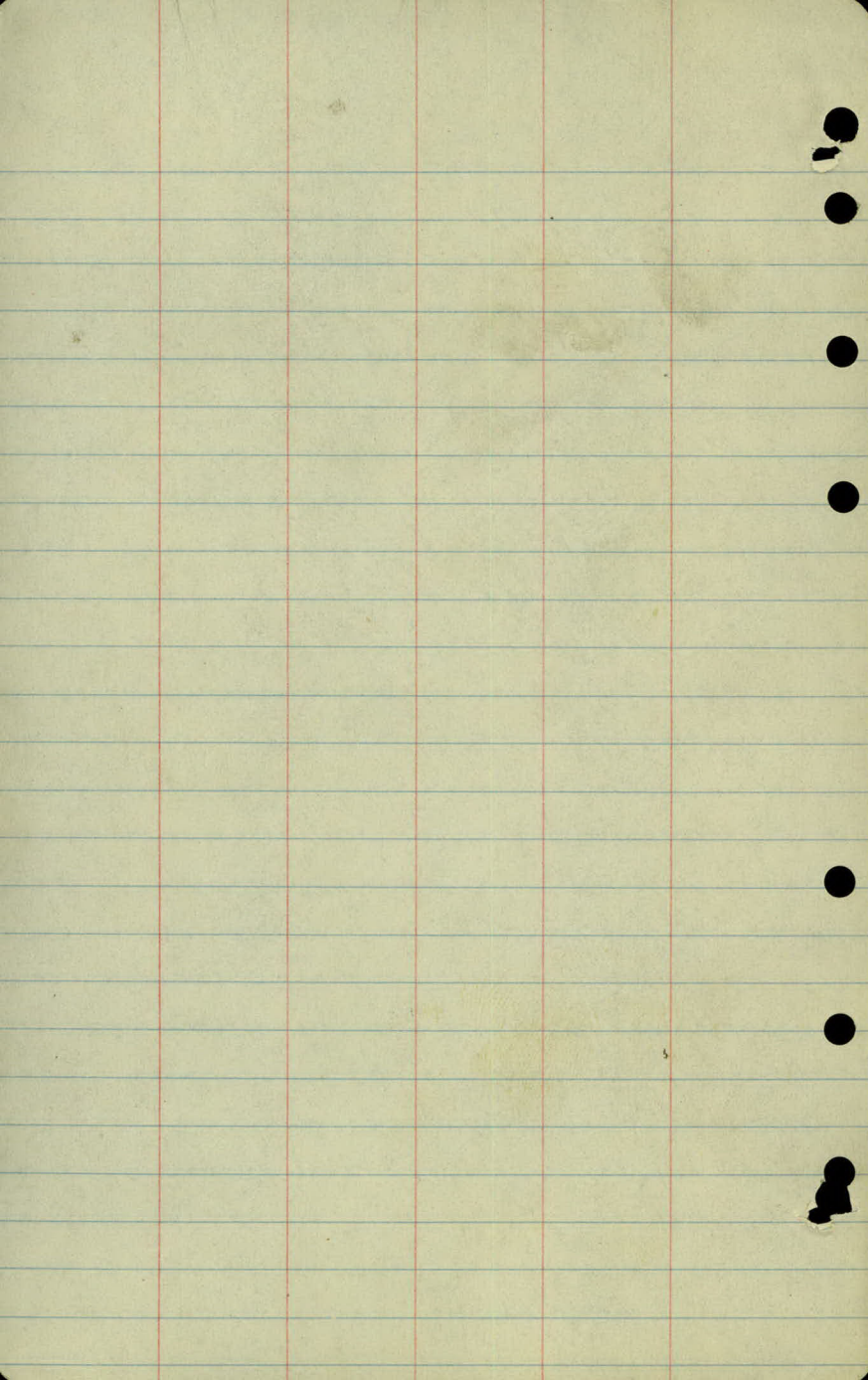
$\frac{62}{50}$	$\frac{69}{35}$	$\frac{69}{21}$	$\frac{51}{16}$	<u>46</u>	$\frac{51}{16}$	$\frac{82}{30}$	$\frac{89}{50}$
-----------------	-----------------	-----------------	-----------------	-----------	-----------------	-----------------	-----------------

$\frac{46}{50}$	$\frac{46}{30}$	<u>46</u>	$\frac{53}{29}$	$\frac{58}{50}$
-----------------	-----------------	-----------	-----------------	-----------------

$\frac{45}{50}$	<u>48</u>	$\frac{53}{50}$
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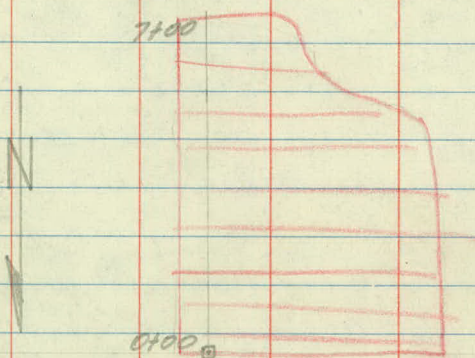
Top Mont Sta 52+72.20

25.46
4.88
20.97 ✓



1
X Sections

East Ave - south of Lapradeur



5 Pages

Sta	+	π	-	Elev.
B.M.	3.53	1026.34		(1022.91)

0 +00				21.1
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+50				21.2
-----	--	--	--	------

1				21.2
---	--	--	--	------

+50				21.2
-----	--	--	--	------

8-7-47

L L E E C

Top S.W. Cor. of Top Step Ent. to Store at Larp. & East Aves.

52 21.1

46	42	32	21
100	200	300	400
21.8	22.1	23.1	24.2

1.0	104	95	63	55	51	54	61	67	76	42	49	71	74	72	76	62	66
33	31	24	11			9	17	19	29	34	60	83	100	127	150	184	197
	15.9	16.8	20.0	20.8	21.2	20.9	20.2	19.6	18.7	22.1	21.4	19.2	18.9	19.1	18.7	20.1	19.7

6.2	7.9	10.0	11.4	10.7	9.0	7.9	7.5
410	385	350	300	250	217	WS	25
20.1	18.4	16.3	14.9	15.6	17.3	18.4	18.5

L.O.	10.4	66	57	51	5.4	5.9	6.9	7.7	31	31	36
	33	24	11		9	16	20	31	42	64	100
	15.9	19.7	20.6	21.2	20.9	20.4	19.4	18.6	23.2	23.2	22.7

19.8	19.3	17.3	16.8		16.4	18.2	21.7
6.5	7.0	9.0	9.5	cannot	9.9	8.1	9.6
425	412	405	390	964	206	180	150

16.5	20.0	20.6
9.8	6.3	5.7
33	25	11

51	53	59	74	76	50	35	42	71	79	70
21.2	21.0	20.4	18.9	18.7	21.3	22.8	22.1	19.2	18.4	19.3
9	16	21	30	33	67	100		150	175	206

425	406	400	385	300	224	210
5.4	6.8	8.3	9.9	11.4	10.9	8.2
20.9	19.5	18.0	16.4	14.9	15.4	18.1

Sta	+	π	-	Elev.
		1026.34		

2				21.3
---	--	--	--	------

t50				21.2
-----	--	--	--	------

B.M.	6.35	1029.16	3.53	1022.81
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3				21.1
---	--	--	--	------

t50				21.1
-----	--	--	--	------

L

E

R

18.1	20.1	20.7	21.3	20.8	20.2	19.0	19.3	24.2	23.3	23.2	19.6	18.1
82	6.2	5.6	50.65	6.1	7.3	7.0	2.1	3.0	3.1	6.7	8.2	
33	24	11	10	18	20	27	34	45	62	92	150	

23.1	21.7	19.5	19.0	18.8	19.1	18.8	18.3
9.2	4.6	6.8	7.3	7.5	7.2	7.5	8.0
425	413	400	394	350	300	250	200

18.6	20.4	20.7	21.2	20.7	20.2	19.3	19.0	24.2	23.0	25.4	25.0	20.7
7.7	5.9	5.6	5.1	5.6	6.1	7.0	7.3	8.1	9.3	9.9	1.3	5.6
33	25	11	10	17	19	24	33	58	65	77	100	

21.8	19.0	18.1	17.9	18.1	18.1	18.3
45	7.3	8.2	8.4	8.2	8.2	8.0
425	400	364	300	250	200	150

17.0	20.6	20.7
12.2	8.6	8.5
33	24	11

21.1	20.7	20.2	19.1	19.3	24.6	22.5	21.4	19.4	18.1	18.1
81	85	9.0	101	99	4.6	6.7	7.8	9.8	11.1	11.1
10	17	21	26	33	58	79	100	150	200	

22.6	20.8	18.7	18.3	17.6	18.0	18.0	18.3
6.6	8.4	10.5	10.9	11.6	11.2	11.2	10.9
425	375	347	320	318	316	300	260

18.3	20.2	20.6
109	90	8.6
33	23	11

21.1	22.6	20.1	20.1	20.1	20.1	20.1
8.4	9.1	10.3	11.0	11.0	11.0	11.0
9	17	20	29	32	47	80

29.8	29.2	26.7	21.2	18.2	17.4	18.0	18.0	18.0	18.0
10.6	9.0	2.5	8.0	11.0	11.8	11.2	11.2	11.2	11.2
425	400	326	300	275	273	271	231	200	

Sta	+	π	-	Elev
-----	---	-------	---	------

102916

4				20.9
---	--	--	--	------

+50				20.7
-----	--	--	--	------

+52 FL18" C.M. X Drain

5				20.7
---	--	--	--	------

L

R

R

16.0
132 90 89
33 20 11

20.9
8.3 89 95 129 149 134 150 141 135 119
9 17 27 40 W.S. 77 109 120 130

32.3
131 100 109 120 122 112 112 125 119 109
317 264 253 250 223 221 178 174 172 150

32.7
+35 +25 +10 +1.3
325 340 392 425

16.4
128 94 90 85
33 21 11

20.0
92 101 127 144 146 152 145 135
10 16 26 33 55 100 123 139

33.0
+38 +46 +35 +82 +30 29 34 101 110
425 374 327 274 258 212 201 187 147

14.8
14.4
30'

14.9
14.3
30'

15.8
134 96 89
33 22 11

20.7
8.5 91 98 135 144 146 141 136 130 111 98
10 16 29 33 59 75 100 133 145 175

30.8
+16
362
28.1
+11
300
31.2
+20
275
33.3
+41
257
34.6
+54
232
33.2
+40
220
25.6
36
188

Edge of 9/1000

Sta	+	π	-	Elev.
		1028.16		

5	+25			
---	-----	--	--	--

5	+50			20.8
---	-----	--	--	------

6				20.6
---	--	--	--	------

	+50			20.3
--	-----	--	--	------

7				20.4
---	--	--	--	------

BM.		634	1022.82	1022.81
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L

E

R

38.8'

19.0
10.2 12.4 9.8 9.0 8.4
33 26 16 11

16.8
19.9
20.2
20.8

29.6
+0.4
200

31.8
+2.6
208

31.8
+2.6
231

28.1
1.1
265

196
143
37

= Edge of green

20.2
9.0 9.8 11.7 13.5 14.4 19.4
10 19 42 65 71 75

19.4
17.5
15.7
14.8

2 Hand ditch
15.5

28.1
11 1.8
30.8 26.4
Edge of green

27.4
2.2
214

27.0
4.4
118

24.8
9.0
167

20.2
9.5
150

19.7
11.7
100

17.5

9.8 12.5 9.4 9.0
33 27 16 11

20.8
19.9
19.5
17.0
15.6
14.9
15.6
15.9
17.0
18.5

8.6 9.3 9.7 12.2 13.6 14.3 13.6 13.3 12.2 10.7
10 16 25 42 64 70 100 132 165

23.1
6.1
250

20.5
8.7
197

16.0
13.2
33

17.0
13.2
25

19.0
10.2
18

19.9
9.3
11

20.3
8.9
10

19.7
9.5
10

19.4
9.8
16

15.0
14.2
27

13.8
15.4
41

14.5
14.7
68

15.8
13.4
14.5

15.4
13.8
100

17.4
11.8
150

21.1
8.1
200

18.3
10.9 12.1 12.1 9.4 9.0 8.8 9.4 9.7 11.5 12.6 13.7 13.0 10.3
33 28 23 14 11 10 16 22 47 77 100 150

17.1
17.1
19.8
20.2
20.4
19.8
19.5
17.7
16.6
15.5
16.2
18.9

Top step

1026.3

52

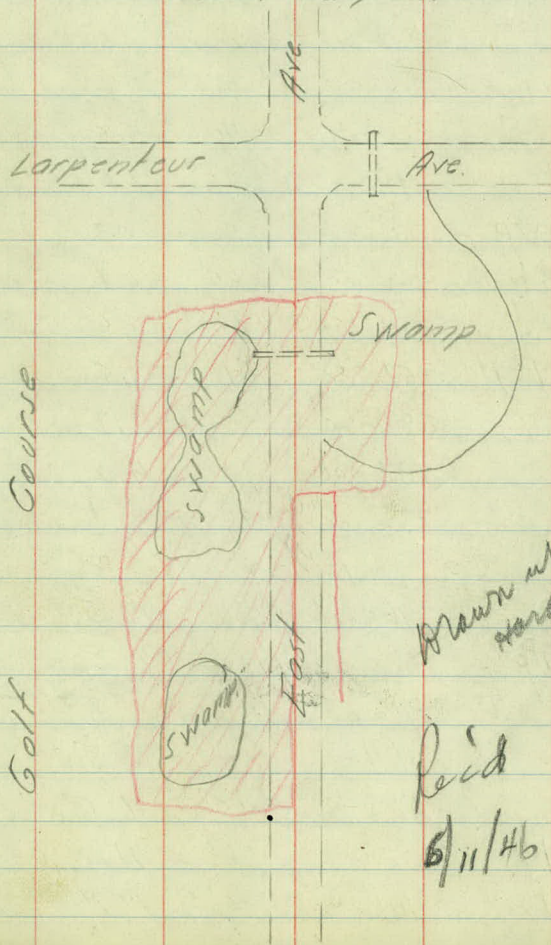
- 1 1

50' = 1"

Stadia Survey

EAST AVE.

South of Larpentour



Brown up on
~~marshland~~
6/4/46

Reid
6/11/46

Object	Azimuth	Dist	Bod	Elev
	+	+	-	
B.M.	3.40	1026.21		1022.81
T.P.	542	1026.03	5.60	1020.61
		H.I. = 1026.03		

π on E East Ave

493' S. of Long Ave	0°00'	= North.		
E EAST AVE	0°00'	246'	4.9	21.1 ✓
SHLDR	3°40'	240'	5.5	20.5 ✓
GRD	9°00'	245'	8.6	17.4 -
EDGE SWP	13°05'	250'	10.3	15.7 -
SWAMP	22°00'	260'	10.8	15.2 -
SHLDR	354°50'	160'	5.6	20.4 -
4' DITCH	357°50'	161'	7.5	18.5 -
GRD	347°20'	180'	2.7	23.3 ✓
"	338°00'	170'	4.2	21.8 -
"	332°00'	174'	6.9	19.1 ✓
"	309°15'	222'	8.2	17.8 ✓
SWAMP	39°00'	161'	10.5	15.5 -
EDGE SWP	16°00'	115'	10.5	15.5 -
SHLDR	7°00'	111'	5.8	20.2 -
RD	0° -	44'	5.5	20.5 ✓
SHLDR	16° -	45'	6.0	20.0 ✓
18" C.M.	35° -	53'	11.3	14.7 ✓
SWP	61° -	78'	10.6	15.4 ✓

2-10-76
 L.P.
 R.M.
 N.B.
 C.H.

Object	Az.	Dist	Pod	Elev.
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H.I. = 1026.03

Top S.W. Cor Top Step Ent. to Store at East Harp Ave.

GRD	180° -	34'	5.4	20.6✓
SHLDR	157° 30'	39'	6.1	19.9✓
EDGE SWP	146° -	42'	8.6	17.4-
" "	137° 30'	55'	9.5	16.5-
SWP	100° -	70'	10.7	15.3-
Top KNOAK	156° 20'	85'	3.6	22.4-
" "	140° -	128'	3.0	23.0✓
EDGE SWP	128° -	114'	9.1	16.9-
SHLDR	190° -	58'	5.9	20.1-
GRD	218° 30'	74'	9.2	16.8-
EDGE SWP	235° 20'	50'	10.7	15.3-
SHLDR	264° -	15'	6.3	19.7-
EDGE	264° -	28'	10.8	15.2✓
18" C.M	326° -	53'	11.15	14.88-
EDGE SWP	344° -	105'	10.5	15.5-
GRD	341° -	132'	9.4	16.6-
EDGE SW	320° -	150'	10.5	15.5-
GRD	320° -	165'	7.6	18.4-
DITCH EDGE	302° -	147'	10.3	15.7-
2' DITCH	301° -	162'	9.8	16.2-
" "	292° 20'	223'	9.1	16.9-

Object	Az	Dist	Pod	Elev
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H.I = 1026.03

EDGE SWP	285° 30'	145'	10.4	15.6 ✓
" "	285° 30'	156'	8.1	17.9 ✓
GRD	285° 30'	192	72	18.8 ✓
"	267° 30'	122	10.2	15.8 ✓
"	267° 30'	142	8.0	18.0 ✓
TOE SLOPE	267° 30'	169	6.8	19.2 ✓
GRD	242° -	124	8.0	18.0 ✓
EDGE SWP	241° 30'	84'	10.4	15.6 ✓
" "	235° -	72'	10.4	15.6 ✓
SWAMP	288° -	65'	11.7	14.3 ✓
W.S			1025	15.78 ✓
SWAMP	310° -	85'	11.9	14.1 ✓
EDGE SWP	226° -	130'	10.3	15.7 ✓
" "	220° -	100'	10.3	15.7 ✓
GRD	244° 20'	179'	6.1	19.9 ✓
"	231° 40'	245'	5.7	20.3 ✓
"	216° 30'	282'	2.9	23.1 ✓
SH LDR	184° -	192'	6.7	19.3 ✓
EDGE SWP	212° -	215'	10.3	15.7 ✓
" "	194° -	120'	10.3	15.7 ✓
" "	183° -	194	10.0	16.0 ✓
" "	201° -	218'	10.3	15.7 ✓
SWP	197° 20'	180'	11.9	14.1 ✓

Object	Az.	Dist	Pod	Elev.
H.I. = 102603				
GRD	208° -	239'	8.9	17.1 -
"	210° -	285'	4.6	21.4 -
"	188° -	240'	4.8	21.2 -
SHLDR	182° 20'	355'	6.2	19.8 ✓
± SWP	200° -	155	12.0	14.0 -
W.S			10.25	15.78 -
± 4' DITCH	185° 20'	235'	8.4	17.6 -
SHDR	183° -	285'	6.6	19.4 -
EDGE GOLF TEE	292° -	352'	3.0	23.0 ✓
" " "	203° -	295'	3.0	23.0 -
" " "	189° 30'	270'	3.0	23.0 -
" " "	196° 20'	315'	3.1	22.9 -
TOE SLOP	184° -	355	8.6	17.4 ✓
± 4' DITCH	185° -	287'	8.7	17.3 -
EDGE SWP	189° 30'	285'	7.6	18.4 -
" " "	194° 40'	325'	7.5	18.5 ✓
W.S			7.6	18.4 ✓
SHLDR	182° -	457'	4.7	21.1 -
EDGE SWP	196° -	378'	7.8	18.2 -
" "	192° 40'	418'	7.9	18.1 -
GRD.	197° -	432	+0.5	26.5 -
GRD	200° -	382'	1.0	25.0 -
"	194° 20'	420'	5.6	20.4 -
TOE SLOPE	183°	382.	8.6	17.4 -

OBJECT	AZ	DIST.	ROD	ELEV.
	H.I. = 1026.03			
± RD	180° -	468'	3.7	22.3 /
EDGE SWP	183° 00	510'	7.0	19.0 ✓
" "	186° 40'	470'	8.0	18.0 ✓
" "	187° -	447'	9.6	16.4 ✓
SWP	192° 40'	390'	9.9	16.1 -
GRD.	187° -	480'	5.1	20.9 ✓
"	189° 30'	500'	0.3	25.7 ✓
TOE SLOPE	195° 40'	372'	9.3	16.7 -
" "	191° 40	310'	9.6	16.4 -
Ground	173° -	374'	10.0	16.0 ✓
15" C.M. SIDE DRAIN	174° -	345'	9.4	16.6 -
	174° -	318'	9.3	16.7
15" C.M. SIDE DRAIN	174° -	240'	9.65	16.38 -
	173° 40'	220'	9.60	16.43 ✓
SHLDR	172° -	120'	6.4	19.6 ✓
GRD.	156° -	143'	7.2	18.8 -
± 3' SIDE DRAIN	167° -	122	9.7	16.3
" " " "	162° -	81	9.4	16.6 ✓
TOP BACKS LOPE	163° 40'	122	7.3	18.7
B.M			325	1022.78 -

OBJECT	PL	AZ	DIST	ROD	ELEV
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low shots on East side of road.

Top S.W. COR. Top STEP ENT TO STORE LARP + EAST AVE

