

Dr. 6 - Bk. 103

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plot 17. Survey

COUNTY RD. "F"

From Rice To McMenamy

Road Acc't. No.

Date Filed 1936

File D. 6 B. 103

1
± Levels

County Road "F"

Rice St. to McMenamy.

Note:

See Rd. Map Survey
for align + topog.

See: Plan Survey Notes for
X-sections near McMenamy

W. H. Carlson

May. 14, 1936

Sta.	+	T	-	Elev.
	13.63	945.13✓		931.50✓
61402.95			13.63	31.50 -
61			13.3	31.8 -
+70			12.0	33.1 -
60			9.4	35.7 -
59			6.2	38.9 -
58			3.2	41.9 -
+50			1.8.	43.3 -
57			1.0	44.1 -
+50			0.6	44.5 -
56			1.0	44.1 -
+50			2.2	42.9 -
55			4.0	41.1 -
T.P.	0.08	941.00✓	4.21	940.92✓
54			3.5	37.5 -
53			8.0	933.0 -
52			12.6	28.4 -
T.P.	0.94	928.27✓	12.67	927.33✓
+50			2.0	76.3 -
51			4.9	23.4 -
50			9.5	18.8 -
+50			11.4	16.9 -
49			13.3	15.0 -
T.P.	2.45	917.41✓	13.31	914.96✓
+8+50			3.6	913.8 -

Top Stone Mon. M. Menemey & Co. Rel F

W. S. G.

K. A.

May 7, 1930

$$\frac{-0.6}{1.5}$$

$$\frac{0}{1}$$

$$\frac{-0.4}{10}$$

CROWN of Rd

Boat Spike in T.P. 18' Lt. Sta. 54175

$$\frac{10.2}{11}$$

$$\frac{7.5}{1}$$

$$\frac{70.4}{15}$$

W.S. - 14.4 to 9.7

9.7 = W.S. 49 to

Sta.	+	Σ	-	Elev.
		917.41 ✓		
4840			4.1	913.3 -
47			4.6	12.8 -
+50			5.1	12.3 -
46			6.0	11.4 -
+50			6.7	10.7 -
45			8.0	09.4 -
+50			9.1	08.3 -
44			11.0	06.4 -
T.P.	0.18	906.73 ✓	10.86	906.55 ✓
43			3.6	903.1 -
B.M.			1.55	905.18 ✓
+50			5.5	901.2 -
42			7.3	899.4 -
+50			8.5	98.2 -
41			8.9	97.8 -
+50			9.1	97.6 -
+19	2 Box Culv.		8.8	97.9 -
40 to			8.3	98.4 -
+50			6.9	899.8 -
39 to			5.3	901.4 -
T.P.	7.88	912.71 ✓	1.90	904.83 ✓
38			8.0	904.7 -
+50			6.3	906.4 -
37			5.0	907.7 -
36 +50			4.3	908.4 -

Lt.

E

Rt.

3

$$\frac{11.5}{116.0} = \frac{12.5}{904.9}$$

$$\frac{8.1}{9}$$

$$\frac{8.0}{1}$$

$$\frac{8.2}{15}$$

R.R. spike in T.P. 15' Lt. $42+80$

(= 210.74)

$$\frac{7.0}{15}$$

$$83$$

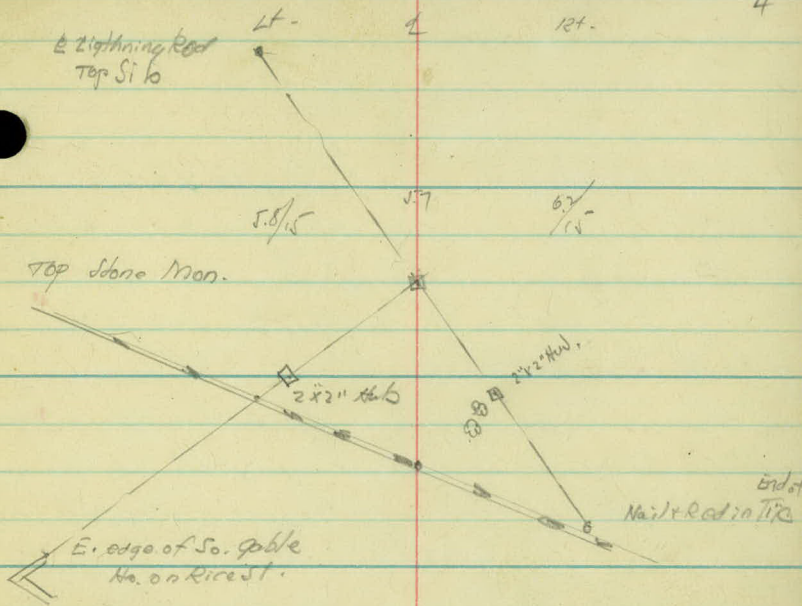
$$\frac{8.7}{15}$$

Top Bag 9.R. Rt. 38+84

Sta. + π - Elev.

912.71✓

36			4.8	907.9-
+50			5.2	07.5-
35			5.7	07.0-
34+67.10			6.47	906.24-
+50			6.5	06.2-
34			7.2	05.5-
+50				
33			8.9	03.8-
+50			9.8	02.9-
32			10.2	02.5-
+50			10.3	02.4-
31			10.0	02.7-
T.P.	0.62	903.57✓	7.76	902.95✓
30+48.1	Top East Rai ^l		0.62	902.95✓
30+44.6	E L ⁰⁰ INE			
30+44.1	Top West Rai ^l		0.61	02.96✓
30			1.7	901.9-
+50			2.9	899.7-
29			5.9	97.7-
+50			7.0	96.6-
28			7.8	95.8-
+50			8.2	95.4-
27			8.2	95.4-
+50			7.9	95.7-
26			7.5	96.1-



$$\frac{6.4}{7.3}$$

$$\frac{5.7}{11}$$

$$\frac{6.3}{11}$$

$$28+53-12' \times 40 \text{ c.h. } \frac{889.0}{22}$$

$$\frac{890.4}{18}$$

Sta.	T	T	-	Elev.
		903.57✓		
	7.86	903.60✓	7.53	896.04✓
25+50			6.6	897.0.
25+0			6.2	97.4.
+50			5.2	98.4.
24			4.1	99.5.
23			1.1	902.2.
T.P.	10.70	912.98✓	0.32	903.28✓
22			9.3	904.7.
21			7.3	906.7.
20			5.3	908.7.
19			2.9	911.1.
+50			1.6	912.4.
T.P.	12.16	925.78✓	0.66	913.32✓
18			11.8	12.0.
+50			9.9	15.9.
17	Approx Ent Lt.		7.8	18.0.
+50			5.9	19.9.
16			4.5	21.3.
+50	Ent. Lt.		3.1	22.7.
15			1.8	24.0.
+50			0.8	25.0.
T.P.			0.10	925.68✓

$$\frac{6.8}{15}$$

$$\frac{6.2}{1}$$

$$\frac{6.7}{12}$$

$$\frac{6.2}{14}$$

$$\frac{\sqrt{3}}{1}$$

$$\frac{6.1}{13}$$

$$\frac{2.4}{2.4}$$

$$\frac{1.8}{1}$$

$$\frac{2.2}{15}$$

Sta.	+	π ✓	-	Elev.
	5.47	931.15		925.68
1440			5.3	25.9 .
+50			4.9	26.3 .
13			4.7	26.5 .
+50			4.7	26.5 .
12			5.0	26.2 .
+50			5.4	25.8 .
1140			5.6	25.6 .
462 -			5.1	26.1 .
+45.9			4.69	26.46 .
104289 Stone Mon.			4.67	26.48 ✓
2 Rice				

X-Sections

Co. Road "F"

Rice St. to McMenamy.

W. H. Carlson.
May 20, 1936

Sta.	+	π	-	Grade	926.48
	4.59	931.07			

11			24.7	25.6	
----	--	--	------	------	--

+50			24.6	25.9	
-----	--	--	------	------	--

12	(0.2 Crown)		24.5	26.2	Ditch Gr. Left 24.5 4.6
----	-------------	--	------	------	----------------------------------

+50			24.4	26.4	24.4
-----	--	--	------	------	------

13				26.3	24.3
----	--	--	--	------	------

+50				26.1	24.5
-----	--	--	--	------	------

14				25.6	23.4
----	--	--	--	------	------

+50				24.8	
-----	--	--	--	------	--

15				23.9	
----	--	--	--	------	--

T.P.	2.35	920.107	8.35		922.72
------	------	---------	------	--	--------

+50				22.7	
-----	--	--	--	------	--

16				21.3	
----	--	--	--	------	--

+50				19.6	
-----	--	--	--	------	--

L

H.

E

Rt.

8

9. Rad.

$$\begin{array}{r} 5.5 \\ 5.5 - \end{array}$$

$$\begin{array}{r} 5.4 \\ 5.2 - \end{array}$$

$$\begin{array}{r} 5.1 \quad 5.1 \\ 4.9 - \quad 32 \quad \begin{array}{r} 4.0 \\ 10.9 \end{array} \quad \begin{array}{r} 4.8 \\ 2.9 \end{array} \quad \begin{array}{r} 5.4 \\ 1.4 \end{array} \\ \text{D.C. 2.6} \end{array}$$

$$\begin{array}{r} 4.9 \quad 4.9 \\ 4.7 - \quad 32 \quad \begin{array}{r} 4.1 \\ 10.6 \end{array} \quad \begin{array}{r} 5.0 \\ 2.0 \end{array} \quad \begin{array}{r} 5.1 \\ 1.8 \end{array} \end{array}$$

$$\begin{array}{r} 4.8 \quad 5.0 \\ 4.8 - \quad 32 \quad \begin{array}{r} 3.7 \\ 11.1 \end{array} \quad \begin{array}{r} 5.2 \\ 2.9 \end{array} \quad \begin{array}{r} 5.2 \\ 1.5 \end{array} \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.2 \\ 5.0 - \quad 32 \quad \begin{array}{r} 3.2 \\ 11.8 \end{array} \quad \begin{array}{r} 4.9 \\ 2.9 \end{array} \quad \begin{array}{r} 5.3 \\ 1.8 \end{array} \end{array}$$

$$\begin{array}{r} 5.5 \quad 5.5 \\ 5.5 - \quad 32 \quad \begin{array}{r} 3.5 \\ 12.9+2.0 \end{array} \quad \begin{array}{r} 5.7 \\ 2.9 \end{array} \quad \begin{array}{r} 5.7 \\ 1.4 \end{array} \end{array}$$

$$\begin{array}{r} 6.3 \quad 6.3 \\ 6.3 - \quad 32 \quad \begin{array}{r} 4.5 \\ 11.9 \end{array} \quad \begin{array}{r} 6.3 \\ 2.8 \end{array} \quad \begin{array}{r} 6.7 \\ 1.5 \end{array} \end{array}$$

$$\begin{array}{r} 7.2 \quad 7.2 \\ 7.2 - \quad 32 \quad \begin{array}{r} 6.2 \\ 11.0 \end{array} \quad \begin{array}{r} 7.6 \\ 2.9 \end{array} \quad \begin{array}{r} 7.6 \\ 1.5 \end{array} \end{array}$$

(Pl. 15"x20" C.M. Sta. 15+50)

$$\begin{array}{r} 2.4 \quad 2.4 \\ 2.4 - \quad 32 \quad \begin{array}{r} 1.0 \\ 11.4 \end{array} \quad \begin{array}{r} 2.7 \\ 2.9 \end{array} \quad \begin{array}{r} 2.8 \\ 1.8 \end{array} \end{array}$$

$$\begin{array}{r} 3.8 \quad 3.8 \\ 3.8 - \quad 32 \quad \begin{array}{r} 3.8 \\ 11.9 \end{array} \quad \begin{array}{r} 4.1 \\ 2.6 \end{array} \quad \begin{array}{r} 4.5 \\ 1.7 \end{array} \end{array}$$

$$\begin{array}{r} 5.5 \quad 5.5 \\ 5.5 - \quad 32 \quad \begin{array}{r} 2.5 \\ 12.0 \end{array} \quad \begin{array}{r} 5.8 \\ 2.6 \end{array} \quad \begin{array}{r} 6.0 \\ 1.8 \end{array} \end{array}$$

$$\begin{array}{r} 9.5. \\ 5.6 \\ 5.6 - \end{array}$$

$$\begin{array}{r} 5.5 \quad 6.0 \quad 6.0 \quad 5.0 \\ 1.5 \quad 1.8 \quad 2.0 \quad 3.2 \end{array} / C-0.5$$

$$\begin{array}{r} 25.7. \\ 5.4 \\ 5.4 - \end{array}$$

$$\begin{array}{r} 5.6 \quad 5.9 \quad 6.0 \quad 5.0 \\ 1.5 \quad 1.7 \quad 2.0 \quad 3.2 \end{array} / C-0.2$$

$$\begin{array}{r} 26.2. \\ 4.9 \\ 4.9 - \end{array}$$

$$\begin{array}{r} 5.1 \quad 5.6 \quad 5.4 \quad 4.5 \\ 1.5 \quad 1.8 \quad 2.0 \quad 2.2 \end{array} / C-0.4$$

$$\begin{array}{r} 26.5. \\ 4.6 \\ 4.6 - \end{array}$$

$$\begin{array}{r} 4.7 \quad 5.1 \quad 5.1 \quad 3.7 \\ 1.5 \quad 1.7 \quad 2.9 \quad 11.0 \end{array} / 32$$

$$\begin{array}{r} 26.4 \\ 4.7 \\ 4.7 - \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.2 \quad 5.1 \quad 3.6 \\ 1.5 \quad 1.8 \quad 2.9 \quad 11.2 \end{array} / 32$$

$$\begin{array}{r} 26.2 \\ 4.9 \\ 4.9 - \end{array}$$

$$\begin{array}{r} 5.0 \quad 5.3 \quad 5.1 \quad 3.2 \\ 1.5 \quad 1.8 \quad 2.9 \quad 11.8 \end{array} / 32$$

$$\begin{array}{r} 25.9. \\ 5.2 \\ 5.2 - \end{array}$$

$$\begin{array}{r} 5.5 \quad 5.8 \quad 5.1 \quad 3.2 \\ 1.5 \quad 1.7 \quad 2.9 \quad 12.3 \end{array} / 32$$

$$\begin{array}{r} 25.0. \\ 6.1 \\ 6.1 - \end{array}$$

$$\begin{array}{r} 6.4 \quad 6.4 \quad 4.4 \\ 1.7 \quad 2.8 \quad 11.9 \end{array} / 32$$

$$\begin{array}{r} 24.0. \\ 7.1 \\ 7.1 - \end{array}$$

$$\begin{array}{r} 7.3 \quad 7.3 \quad 5.8 \\ 1.7 \quad 2.9 \quad 11.4 \end{array} / 32$$

$$\begin{array}{r} 22.7. \\ 3.4 \\ 3.4 - \end{array}$$

$$\begin{array}{r} 3.7 \quad 1.7 \\ 2.0 \quad 10.7 \end{array} / 32$$

$$\begin{array}{r} 21.3. \\ 3.8 \\ 3.8 - \end{array}$$

$$\begin{array}{r} 4.2 \quad 3.8 \quad 2.6 \\ 1.2 \quad 2.0 \quad 11.2 \end{array} / 32$$

$$\begin{array}{r} 19.8. \\ 5.3 \\ 5.3 - \end{array}$$

$$\begin{array}{r} 5.5 \quad 5.2 \quad 3.4 \\ 1.5 \quad 2.9 \quad 12.1 \end{array} / 32$$

(Pl. 15"x20" C.M. 16+70)

Stn.	+	T ✓	-	Grade	Elev.
		928.07			
17				17.1	
+50				15.8	
18				14.0	
T.P.	11.3	913.08 ✓	12.72		912.35 ✓
+50				12.4	
19				11.0	
+50				09.7	
20				08.5	
+50				07.5	
					908.86
21				06.4	
+50				05.4	
22				04.3	
+50				03.3	
T.P.	4.32	906.21 ✓	11.59		901.89 ✓

GR.

Lt.

L

LH-

9

$$74 - 32 \begin{array}{r} 4.2 \\ 13.2 \end{array} \quad \frac{7.8}{26} \quad \frac{7.6}{12} \quad \frac{18.0}{7.1} \quad \frac{2.5}{17} \quad \frac{7.4}{28} \quad \frac{4.9}{+2.5} / 32'$$

$$9.3 - 32 \begin{array}{r} 5.1 \\ +3.6 \end{array} \quad \frac{7.9}{28} \quad \frac{9.8}{17} \quad \frac{15.9}{9.2} \quad \frac{9.7}{15} \quad \frac{9.5}{27} \quad \frac{7.1}{+2.2} / 32'$$

$$11.1 - 32 \begin{array}{r} 8.2 \\ +2.9 \end{array} \quad \frac{11.6}{27} \quad \frac{11.6}{17} \quad \frac{14.0}{11.1} \quad \frac{11.6}{16} \quad \frac{11.6}{29} \quad \frac{10.5}{+0.6} / 32'$$

$$1.1 - 32 \begin{array}{r} 2.0 \\ 0.1 \end{array} \quad \frac{2.1}{18} \quad \frac{1.2}{15} \quad \frac{12.4}{7.1} \quad \frac{1.7}{15} \quad \frac{1.7}{2.0} / 31'$$

$$2.5 - 32 \begin{array}{r} 6.3 \\ 0.0 \end{array} \quad \frac{4.9}{19.8} \quad \frac{4.8}{17} \quad \frac{3.2}{14} \quad \frac{11.0}{2.5} \quad \frac{3.1}{14} \quad \frac{4.7}{17} \quad \frac{4.6}{-2.1} / 19.2 \quad \frac{5.3}{0.005} / 32'$$

$$3.8 - 29.8 \begin{array}{r} 11.2 \\ -7.4 \end{array} \quad \frac{10.8}{27} \quad \frac{4.1}{13} \quad \frac{09.8}{3.7} \quad \frac{4.6}{14} \quad \frac{8.6}{20} \quad \frac{8.8}{-5.0} / 25.0$$

$$5.0 - 37.6 \begin{array}{r} 13.8 \\ -8.8 \end{array} \quad \frac{13.0}{28} \quad \frac{5.6}{14} \quad \frac{08.6}{4.9} \quad \frac{5.6}{13} \quad \frac{8.7}{18} \quad \frac{10.0}{-5.0} / 25.0$$

$$6.0 - 19.8 \begin{array}{r} 8.4 \\ -2.4 \end{array} \quad \frac{8.1}{17} \quad \frac{6.2}{13} \quad \frac{07.7}{5.8} \quad \frac{6.7}{14} \quad \frac{7.6}{17} \quad \frac{7.8}{-1.8} / 18.6$$

Nail in T.P. about 1060

$$7.1 - 32 \begin{array}{r} 5.6 \\ +1.0 \end{array} \quad \frac{7.5}{28} \quad \frac{7.5}{17} \quad \frac{06.6}{6.9} \quad \frac{7.4}{17} \quad \frac{7.2}{28} \quad \frac{4.7}{+2.4} / 23$$

$$8.1 - 32 \begin{array}{r} 5.7 \\ +2.4 \end{array} \quad \frac{8.7}{27} \quad \frac{8.7}{16} \quad \frac{05.5}{8.0} \quad \frac{8.2}{17} \quad \frac{8.2}{26} \quad \frac{4.3}{+3.8} / 32'$$

$$9.2 - 32 \begin{array}{r} 7.1 \\ +2.1 \end{array} \quad \frac{9.6}{28} \quad \frac{9.6}{18} \quad \frac{04.7}{8.8} \quad \frac{9.2}{16} \quad \frac{9.0}{26} \quad \frac{5.0}{+4.2} / 32'$$

$$10.2 - 32 \begin{array}{r} 8.7 \\ +1.5 \end{array} \quad \frac{10.9}{28} \quad \frac{11.2}{18} \quad \frac{10.5}{13} \quad \frac{03.4}{10.1} \quad \frac{10.8}{11} \quad \frac{10.4}{23} \quad \frac{4.9}{+5.3} / 32'$$

Nail in T.P. 16' Lt. Sta 73+12

22

+

✓

Grade Elev.

906.21

23

02.2

+50

01.2

24

900.1

+50

99.1

25

98.0

+50

97.0

3.75

✓
900.26

9.70

✓
896.51

26

96.1

+50

95.9

27

95.9

+50

96.5

28

97.6

+50

99.2

T.P.

6.65

✓
904.12

2.79

✓
897.47

G.R.

Lt.

E

Rt.

10

$$4.0 - 32 \begin{array}{r} 36 \\ 70.4 \end{array} \quad \begin{array}{r} 56 \\ 78 \end{array} \quad \begin{array}{r} 55 \\ 18 \end{array} \quad \begin{array}{r} 43 \\ 15 \end{array} \quad \begin{array}{r} 90.2 \\ 40 \\ 20 \end{array} \quad \begin{array}{r} 47 \\ 11 \end{array} \quad \begin{array}{r} 42 \\ 23 \end{array} \quad \begin{array}{r} (+14) \\ +5.4 \end{array} / 32$$

$$5.0 - 32 \begin{array}{r} 82 \\ 2600 \end{array} \quad \begin{array}{r} 174 \\ 198 \\ 24 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad \begin{array}{r} 54 \\ -0.4 \end{array} \quad \begin{array}{r} 59 \\ 10 \end{array} \quad \begin{array}{r} 54 \\ 15 \end{array} \quad \begin{array}{r} 52 \\ 29 \end{array} \quad \begin{array}{r} 32 \\ +1.8 \end{array} / 32$$

$$6.1 - 32 \begin{array}{r} 126 \\ -6.5 \end{array} \quad \begin{array}{r} 124 \\ 24 \end{array} \quad \begin{array}{r} 118.73 \\ 21 \end{array} \quad \begin{array}{r} 13 \\ 13 \end{array} \quad \begin{array}{r} 84.5 \\ 67 \\ -0.6 \end{array} \quad \begin{array}{r} 79 \\ 13 \end{array} \quad \begin{array}{r} 9.8 \\ -3.7 \end{array} / 22.4 \quad \begin{array}{r} 84 \\ R.C. 1.1 \end{array} / 32$$

$$7.1 - 32 \begin{array}{r} 15.3 \\ -8.2 \end{array} \quad \begin{array}{r} 152 \\ 28 \end{array} \quad \begin{array}{r} 86 \\ 14 \end{array} \quad \begin{array}{r} 79 \\ -0.8 \end{array} \quad \begin{array}{r} 8.7 \\ 12 \end{array} \quad \begin{array}{r} 11.3 \\ 18 \end{array} \quad \begin{array}{r} 11.7 \\ -4.6 \end{array} / 24.2 \quad \text{Low Speed} \\ \text{R.C. 0.00} / 32$$

$$8.2 - 32 \begin{array}{r} 116 \\ R.C. 0.0 \end{array} \quad \begin{array}{r} 226 \\ -3.8 \end{array} \quad \begin{array}{r} 120 \\ 21 \end{array} \quad \begin{array}{r} 7.3 \\ 15 \end{array} \quad \begin{array}{r} 88 \\ 67 \\ -0.6 \end{array} \quad \begin{array}{r} 94 \\ 13 \end{array} \quad \begin{array}{r} 10.4 \\ 16 \end{array} \quad \begin{array}{r} 10.7 \\ -7.5 \end{array} / 20.0 \quad \begin{array}{r} 10.2 \\ R.C. 1.6 \end{array} / 32$$

898.62 - Nail in T.P. 24+54

$$9.2 - 32 \begin{array}{r} 76 \\ R.C. 1.6 \end{array} \quad \begin{array}{r} 108 \\ 79 \end{array} \quad \begin{array}{r} 107 \\ 18 \end{array} \quad \begin{array}{r} 98 \\ 14 \end{array} \quad \begin{array}{r} 94.5 \\ 91 \\ -0.2 \end{array} \quad \begin{array}{r} 98 \\ 12 \end{array} \quad \begin{array}{r} 10.2 \\ 12 \end{array} \quad \begin{array}{r} 76 \\ R.C. 2.3 \end{array} / 32$$

$$10.1 + 4.2 - 32 \begin{array}{r} 28 \\ +14 \end{array} \quad \begin{array}{r} 53 \\ 28 \end{array} \quad \begin{array}{r} 52 \\ 17 \end{array} \quad \begin{array}{r} 48 \\ 15 \end{array} \quad \begin{array}{r} 46 \\ 42 \\ 5 \end{array} \quad \begin{array}{r} 46 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 16 \end{array} \quad \begin{array}{r} 3.2 \\ 28 \end{array} \quad \begin{array}{r} 2.8 \\ +1.4 \end{array} / 32$$

$$11.4 - 32 \begin{array}{r} 40 \\ 70.4 \end{array} \quad \begin{array}{r} 60 \\ 29 \end{array} \quad \begin{array}{r} 60 \\ 17 \end{array} \quad \begin{array}{r} 50 \\ 14 \end{array} \quad \begin{array}{r} 46 \\ 46 \\ -0.2 \end{array} \quad \begin{array}{r} 49 \\ 12 \end{array} \quad \begin{array}{r} 5.8 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 35 \\ 24 \end{array} \quad \begin{array}{r} 35 \\ +0.9 \end{array} / 32$$

G.P.
70

$$11.4 - 32 \begin{array}{r} 62 \\ R.C. 0.8 \end{array} \quad \begin{array}{r} 70 \\ 20 \end{array} \quad \begin{array}{r} 65 \\ 17 \end{array} \quad \begin{array}{r} 54 \\ 14 \end{array} \quad \begin{array}{r} 49 \\ 49 \\ -0.5 \end{array} \quad \begin{array}{r} 5.2 \\ 12 \end{array} \quad \begin{array}{r} 6.2 \\ 16 \end{array} \quad \begin{array}{r} 6.7 \\ 23 \end{array} / 19.6 \quad \begin{array}{r} 70 \\ R.C. 0.0 \end{array} / 32$$

(P. 15' x 20' C.M. 27+25)

$$12.8 - 32 \begin{array}{r} 88 \\ 45 \end{array} \quad \begin{array}{r} 79 \\ 18 \end{array} \quad \begin{array}{r} 54 \\ 12 \end{array} \quad \begin{array}{r} 50 \\ 50 \\ -1.1 \end{array} \quad \begin{array}{r} 5.3 \\ 12 \end{array} \quad \begin{array}{r} 76 \\ 17 \end{array} \quad \begin{array}{r} 86 \\ -4.8 \end{array} / 24.6 \quad \begin{array}{r} 8.7 \\ 32 \end{array}$$

$$12.7 - 32 \begin{array}{r} 11.2 \\ -8.5 \end{array} \quad \begin{array}{r} 103 \\ 21 \end{array} \quad \begin{array}{r} 5.3 \\ 13 \end{array} \quad \begin{array}{r} 48 \\ 48 \\ -1.1 \end{array} \quad \begin{array}{r} 4.8 \\ 12 \end{array} \quad \begin{array}{r} 70 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ -4.3 \end{array} / 28.6 \quad \begin{array}{r} 6.3 \\ 32 \end{array}$$

$$1.1 - 32 \begin{array}{r} 113 \\ -10.1 \end{array} \quad \begin{array}{r} 105 \\ 43 \end{array} \quad \begin{array}{r} 4.5 \\ 13 \end{array} \quad \begin{array}{r} 3.7 \\ 3.7 \\ -7.6 \end{array} \quad \begin{array}{r} 4.3 \\ 12 \end{array} \quad \begin{array}{r} 79 \\ 20 \end{array} \quad \begin{array}{r} 78 \\ -6.7 \end{array} / 78.4$$

S/A. + π - E/cv.

904.12 ✓

29

900.8

+50

01.9

30

02.6

+

03.0

T.P.

1.14

902.98 ✓
902.96

+

+

7 1/2

910.38 ✓

902.96

31+0

02.8

Revised
Grade

+50

To here

02.8

02.9

7.5

32

02.9

03.1

7.3

+50

03.0

03.5

6.9

33

03.2

04.1

6.3

+50

03.4

04.8

5.6

4.

E

RT.

11

$$3.3 \cdot \begin{array}{r} 32 \overline{) 14.8} \\ \underline{-11.5} \end{array} \quad \begin{array}{r} 13.2 \\ 22 \end{array} \quad \begin{array}{r} 6.8 \\ 73 \end{array} \quad \begin{array}{r} 97.1 \\ 64 \\ \underline{-3.1} \end{array} \quad \begin{array}{r} 6.8 \\ 11 \end{array} \quad \begin{array}{r} 12.4 \\ 20 \end{array} \quad \begin{array}{r} 12.9 \\ \underline{-9.6} \end{array} / 32$$

$$2.2 \cdot \begin{array}{r} 33 \overline{) 10.5} \\ \underline{-6.6} \end{array} \quad \begin{array}{r} 11.5 \\ 22 \end{array} \quad \begin{array}{r} 4.6 \\ 73 \end{array} \quad \begin{array}{r} 99.6 \\ 15 \\ \underline{-7.5} \end{array} \quad \begin{array}{r} 5.0 \\ 12 \end{array} \quad \begin{array}{r} 12.1 \\ 22 \end{array} \quad \begin{array}{r} 12.9 \\ \underline{-10.6} \end{array} / 38$$

$$1.5 \cdot \begin{array}{r} 33 \overline{) 12.6} \\ \underline{-12.1} \end{array} \quad \begin{array}{r} 10.3 \\ 24 \end{array} \quad \begin{array}{r} 2.4 \\ 12 \end{array} \quad \begin{array}{r} 901.9 \\ 32 \\ \underline{-0.7} \end{array} \quad \begin{array}{r} 2.5 \\ 7 \end{array} \quad \begin{array}{r} 3.8 \\ 15 \end{array} \quad \begin{array}{r} 3.8 \\ 20 \end{array}$$

1.1 -

Top W. Rail

$$7.6 \cdot \begin{array}{r} 250 \overline{) 12.7} \\ \underline{-5.0} \end{array} \quad \begin{array}{r} 14.0 \\ 20 \end{array} \quad \begin{array}{r} 8.0 \\ 10 \end{array} \quad \begin{array}{r} 902.7 \\ 7.7 \\ \underline{-0.1} \end{array} \quad \begin{array}{r} 8.2 \\ 12 \end{array} \quad \begin{array}{r} 17.0 \\ 26 \end{array} \quad \begin{array}{r} 18.0 \\ \underline{-10.4} \end{array} / 35.8$$

$$7.6 \cdot \begin{array}{r} 418 \overline{) 21.0} \\ \underline{-13.4} \end{array} \quad \begin{array}{r} 19.0 \\ 26 \end{array} \quad \begin{array}{r} 9.5 \\ 11 \end{array} \quad \begin{array}{r} 02.4 \\ 8.0 \\ \underline{-0.4} \end{array} \quad \begin{array}{r} 8.5 \\ 12 \end{array} \quad \begin{array}{r} 14.2 \\ 23 \end{array} \quad \begin{array}{r} 14.8 \\ \underline{-8.4} \end{array} / 31.8$$

$$7.5 \cdot \begin{array}{r} 26.4 \overline{) 18.2} \\ \underline{-10.7} \end{array} \quad \begin{array}{r} 15.0 \\ 20 \end{array} \quad \begin{array}{r} 8.7 \\ 17 \end{array} \quad \begin{array}{r} 02.5 \\ 7.9 \\ \underline{-0.4} \end{array} \quad \begin{array}{r} 8.3 \\ 12 \end{array} \quad \begin{array}{r} 13.6 \\ 21 \end{array} \quad \begin{array}{r} 14.2 \\ \underline{-6.7} \end{array} / 28.5$$

$$7.4 \cdot \begin{array}{r} 26.4 \overline{) 17.0} \\ \underline{-35.1} \end{array} \quad \begin{array}{r} 15.0 \\ 23 \end{array} \quad \begin{array}{r} 8.3 \\ 12 \end{array} \quad \begin{array}{r} 03.5 \\ 7.4 \\ \underline{-0} \end{array} \quad \begin{array}{r} 7.8 \\ 13 \end{array} \quad \begin{array}{r} 17.6 \\ 20 \end{array} \quad \begin{array}{r} 12.4 \\ \underline{-3.5} \end{array} / 6.0$$

$$6.8 \cdot \begin{array}{r} 31.8 \overline{) 14.7} \\ \underline{-30} \end{array} \quad \begin{array}{r} 13.5 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 12 \end{array} \quad \begin{array}{r} 03.8 \\ 6.6 \\ \underline{-0.3} \end{array} \quad \begin{array}{r} 7.1 \\ 14 \end{array} \quad \begin{array}{r} 10.4 \\ 18 \end{array} \quad \begin{array}{r} 10.5 \\ \underline{-3.3} \end{array} / 2.5 \quad \begin{array}{r} 7.8 \\ \underline{-12.12} \end{array} / 3.2$$

$$7.0 \cdot \begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 15.9 \\ 23 \end{array} \quad \begin{array}{r} 5.7 \\ 11.3 \end{array} \quad \begin{array}{r} 04.7 \\ 5.7 \\ \underline{-11.3} \end{array} \quad \begin{array}{r} 6.2 \\ 11 \end{array} \quad \begin{array}{r} 7.8 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ \underline{-7.0} \end{array} / 32.0 \quad \begin{array}{r} 6.98 \\ \underline{-5.2} \end{array} / 13.2$$

See Rev. Stakes

Sta.	+	π ✓ 910.78	-	Elev.	Revised Grade.	
34				903.7	05.65	4.7
+50		✓		04.0	06.45	3.9
	11.71	917.96	4.13		906.75	
35				04.2	06.9	11.1
+50				04.2	07.1	10.9
36				03.9	07.0	11.0
+50				03.5	06.57	11.4
37				02.8	05.8	12.2
+50				01.9	04.8	13.2
38		✓		00.9	03.45	14.5
	3.63	909.88	11.71		900.25	
+50				99.9	01.95	7.9
+7.5				99.4	01.20	8.7
39		✓		98.9	00.45	9.4
T.P.	014	914.95	5.07		904.81	
+50				98.1	99.2	5.8

6.7

$$\begin{array}{r}
 1.0 \quad 1.0 \quad 1.0 \quad 1.0 \quad 1.0 \\
 27.0 \quad 27.0 \quad 27.0 \quad 27.0 \quad 27.0 \\
 \times \quad 23 \quad 33 \quad 33 \quad 33 \\
 \hline
 142 \quad 5.5 \quad 5.2 \quad 5.2 \quad 5.2 \\
 25 \quad 13 \quad 12 \quad 12 \quad 12 \\
 \hline
 905.5 \quad 49 \quad 49 \quad 49 \quad 49 \\
 118 \quad 12 \quad 12 \quad 12 \quad 12 \\
 \hline
 0.620 \quad 0.620 \quad 0.620 \quad 0.620 \quad 0.620 \\
 42 \quad 42 \quad 42 \quad 42 \quad 42 \\
 \hline
 5.0 \quad 5.0 \quad 5.0 \quad 5.0 \quad 5.0 \\
 17 \quad 17 \quad 17 \quad 17 \quad 17 \\
 \hline
 3.7 \quad 3.7 \quad 3.7 \quad 3.7 \quad 3.7 \\
 12.7 \quad 12.7 \quad 12.7 \quad 12.7 \quad 12.7 \\
 \hline
 \text{Cut } 136 \quad \text{Cut } 136 \quad \text{Cut } 136 \quad \text{Cut } 136 \quad \text{Cut } 136 \\
 57.0 \quad 57.0 \quad 57.0 \quad 57.0 \quad 57.0 \\
 17.0 \quad 17.0 \quad 17.0 \quad 17.0 \quad 17.0
 \end{array}$$

6.4

$$\begin{array}{r}
 32 \quad 84 \quad 78 \quad 46 \quad 5.0 \quad 3.7 \quad \text{Cut } 150 \\
 \text{D.C.O.O} \quad 73 \quad 13 \quad 17 \quad 17 \quad 12.7 \quad 50.0 \\
 \hline
 19.0
 \end{array}$$

13.8

$$\begin{array}{r}
 56 \quad 56 \quad 114 \quad 113 \quad 07.0 \quad 11.2 \quad 10.0 \quad 15 \quad 11.5 \\
 50 \quad 32 \quad 22 \quad 15 \quad 12.8 \quad 17 \quad 32 \quad 51 \quad 51.5 \\
 \hline
 19.0
 \end{array}$$

13.8

$$\begin{array}{r}
 45 \quad 40 \quad 110 \quad 105 \quad 10.0 \quad 10.8 \quad 10.5 \quad 88 \quad 12.2 \quad 12.2 \\
 50 \quad 32 \quad 21 \quad 11 \quad 13.3 \quad 17 \quad 27 \quad 32 \quad 50 \quad 17.0 \quad 52.5
 \end{array}$$

14.1

$$\begin{array}{r}
 44.4 \quad 35 \quad 30 \quad 10.5 \quad 10.4 \quad 07.9 \quad 10.4 \quad 10.8 \quad 83 \quad 12.0 \quad 12.2 \\
 50 \quad 33 \quad 21 \quad 13 \quad 17.0 \quad 17 \quad 24 \quad 32 \quad 48 \quad 17.3 \quad 52.0
 \end{array}$$

14.5

$$\begin{array}{r}
 4.3 \quad 40 \quad 10.2 \quad 9.5 \quad 10.2 \quad 10.7 \quad 9.5 \quad 10.8 \quad 11.0 \quad 11.0 \\
 50 \quad 32 \quad 22 \quad 50 \quad 17 \quad 25 \quad 32 \quad 48 \quad 14.1 \quad 15.8
 \end{array}$$

15.2

$$\begin{array}{r}
 5.5 \quad 5.1 \quad 10.9 \quad 10.2 \quad 10.7 \quad 10.8 \quad 10.1 \quad 1.2 \quad 0.5 \\
 50 \quad 32 \quad 23 \quad 50 \quad 14 \quad 29 \quad 32 \quad 47 \quad 15.7 \quad 50.6
 \end{array}$$

16.1

$$\begin{array}{r}
 7.2 \quad 6.6 \quad 12.1 \quad 12.0 \quad 06.2 \quad 12.2 \quad 11.7 \quad 2.8 \quad 2.8 \\
 50 \quad 32 \quad 24 \quad 15 \quad 11.8 \quad 30 \quad 32 \quad 47 \quad 14.3 \quad 47.0
 \end{array}$$

17.1

$$\begin{array}{r}
 11.4 \quad 10.5 \quad 14.2 \quad 13.4 \quad 14.2 \quad 14.2 \quad 8.3 \quad 12.7 \\
 50 \quad 32 \quad 26 \quad 13.7 \quad 23 \quad 32 \quad 47 \quad 19.7
 \end{array}$$

10.0

$$\begin{array}{r}
 31.5 \quad 8.0 \quad 7.5 \quad 7.3 \quad 8.2 \\
 130 \quad 15 \quad 18 \quad 18 \quad 21.8 \quad 31.2
 \end{array}$$

10.5

$$\begin{array}{r}
 27.0 \quad 11.5 \quad 10.4 \quad 8.1 \quad 7.7 \quad 8.3 \quad 9.8 \quad 11.5 \\
 100 \quad 11.5 \quad 21 \quad 13 \quad 12.8 \quad 15 \quad 17 \quad 17.0
 \end{array}$$

11.0

$$\begin{array}{r}
 12.0 \quad 13.1 \quad 11.0 \quad 9.7 \quad 8.5 \quad 8.8 \quad 11.0 \quad 13.1 \quad 13.4 \\
 33 \quad 23 \quad 18.0 \quad 15 \quad 12.5 \quad 14 \quad 18.4 \quad 22 \quad 30
 \end{array}$$

Top End G.R. Post Rt.

$$\begin{array}{r}
 11.0 \quad 6.9 \quad 6.6 \quad 5.1 \quad 5.4 \quad 6.9 \quad 12.6 \\
 7 \quad 14.1 \quad 18 \quad 11.8 \quad 14 \quad 17 \quad 27
 \end{array}$$

470-Cu/Yds removed
these 1-Station

Sta.	+	Σ	-	Elev.	Revised Grade.	
		904.95				
40				92.6	98.45	6.5
B.M.						
+50				97.4	98.2	6.7
41				97.7	98.45	6.5
+50				98.2	99.2	5.8
42				99.05	00.45	4.5
T.P.	0.68	906.34	4.29		900.66	
	6.37	895.90	11.81		889.53	
B.M.			10.32		885.58	
	10.39	911.05			900.66	
42+0				99.2	00.45	10.6
42+30				900.1	01.95	9.1
B.M.	5.87	911.05	5.87		905.18	
43+0				901.15	03.45	7.6
43+50				902.2	04.95	6.1
44+0				903.25	06.45	4.6
	17.02	928.20			905.18	

7.4 $\frac{18.0}{29.0}$ $\frac{10}{10} \frac{7.4}{8.0}$ $\frac{98.4}{70.8}$ $\frac{7.0}{15} \frac{7.4}{8.0} \frac{1}{16.0}$ City
 B.M. Top S.W. cor. of H.W. Sq. end of Conc. Box C.W. 191.19

7.6 $\frac{9.6}{15}$ $\frac{7.8}{12}$ $\frac{7.8}{10.2}$ 97.7 $\frac{7.6}{8.0} \frac{1}{15}$

7.3 $\frac{19.0}{36} \frac{19.0}{31}$ $\frac{7.5}{12}$ $\frac{97.9}{70.2}$ $\frac{7.7}{15}$ $\frac{18.4}{32}$ $\frac{18.6}{11.3} \frac{1}{37.6}$

6.8 $\frac{16.0}{33} \frac{16.0}{26}$ $\frac{7.5}{14}$ $\frac{98.4}{70.2}$ $\frac{7.3}{15}$ $\frac{14.6}{27}$ $\frac{15.0}{8.2} \frac{1}{31.4}$

5.9 $\frac{7.4}{20} \frac{8.6}{10.4} \frac{6.0}{9}$ $\frac{99.6}{70.5}$ $\frac{5.6}{15}$ $\frac{11.0}{24}$ $\frac{11.1}{5.9} \frac{1}{25.4}$

= (City/Datum 191.19) Description as Above.

12.0 $\frac{12.9}{33}$
 10.95 $\frac{9.1}{32} \frac{10.9}{27.0} \frac{10.9}{60.0}$ $\frac{11.6}{25}$ $\frac{11.8}{18}$ $\frac{10.5}{12}$ $\frac{90.1.2}{7.9}$ $\frac{10.4}{15}$ $\frac{15.4}{29}$

R.R. 15' Lt. 4480
 9.9 $\frac{8.0}{50}$ $\frac{8.0}{32}$ $\frac{8.3}{20}$ $\frac{8.7}{7.9}$ $\frac{8.0}{11.9}$ $\frac{8.5}{16}$ $\frac{13.6}{38}$

8.85 $\frac{6.9}{14}$ $\frac{04.8}{6.3}$ $\frac{6.8}{17}$ $\frac{11.6}{38}$ Prop 6.0 p. 11.

7.8 $\frac{4.4}{16}$ $\frac{06.5}{4.6}$ $\frac{5.2}{20}$ $\frac{8.5}{47}$

Cont'd next Page.

Sta.	+	T ✓	-	Elev.	Revised Grade	
		922.20				
43+50				902.2	04.95	17.3
44+0				903.75	06.45	15.8
+50				904.3	07.85	14.4
45				905.35	09.05	13.2
	10.03	915.21 ✓	17.02		905.18 ✓	
44+50					07.85	7.4
45+0					09.05	6.2
+50					10.05	5.2
46+0					10.85	4.4
+50					11.15	4.1
47+0					12.25	3.0
T.P.	7.35	920.38 ✓	2.18		913.03 ✓	
47+50					12.95	7.4
48					13.78	6.6

Lt.

E

Rt.

14

W.H.C.

K.A.

L.B.H.

A.M.

5/10/36

200

 $\frac{5.4}{50}$ $\frac{5.0}{32}$ 189 $\frac{1.2}{50}$ $\frac{1.8}{32}$ 179 $\frac{1.6}{50}$ $\frac{2.8}{32}$ $\frac{4.7}{50}$ $\frac{6.1}{32}$ $\frac{08.2}{7.0}$ $\frac{7.6}{12}$ $\frac{6.8}{9}$ $\frac{7.4}{20}$ $\frac{13.1}{33}$ $\frac{13.0}{60}$ $\frac{09.5}{5.7}$ $\frac{6.1}{19}$ $\frac{5.6}{8}$ $\frac{7.2}{21}$ $\frac{10.4}{38}$ $\frac{10.6}{4.6}$ $\frac{7.0}{50}$ $\frac{7.8}{21}$ $\frac{4.5}{27}$ $\frac{4.5}{9}$ $\frac{5.7}{26}$ $\frac{9.0}{37}$ $\frac{11.4}{3.8}$ $\frac{4.0}{50}$ $\frac{4.7}{20}$ $\frac{5.4}{15}$ $\frac{5.8}{10}$ $\frac{4.1}{7}$ $\frac{3.6}{8}$ $\frac{4.3}{20}$ $\frac{5.8}{28}$ $\frac{8.5}{35}$ $\frac{12.3}{2.9}$ $\frac{4.8}{40}$ $\frac{5.2}{21}$ $\frac{5.3}{12}$ $\frac{3.1}{7}$ $\frac{2.8}{8}$ $\frac{3.6}{18}$ $\frac{6.1}{24}$ $\frac{8.1}{37}$ $\frac{12.8}{2.4}$ $\frac{3.6}{40}$ $\frac{3.2}{19}$ $\frac{3.2}{11}$ $\frac{2.8}{7}$ $\frac{2.3}{7}$ $\frac{2.6}{18}$ $\frac{2.6}{25}$ $\frac{1.2}{35}$ $\frac{12.9}{1.5}$ $\frac{7.9}{40}$ $\frac{8.0}{14}$ $\frac{7.9}{7}$ $\frac{7.2}{5}$ $\frac{7.7}{25}$ $\frac{6.1}{37}$

47490 - Ent. no Crib. Repd 13.4

 $\frac{8.8}{40}$ $\frac{8.1}{15}$ $\frac{7.2}{8}$ $\frac{7.0}{-}$ $\frac{6.9}{5}$ $\frac{7.4}{16}$ $\frac{8.6}{21}$ $\frac{8.9}{35}$

Sta.	+	π ✓ 920.38	-	Elev.	Revised Grade.
48+50				14.87	5.5
49+0				16.21	4.2
+50				17.80	2.6
50		✓		19.68	0.7
T.P.	9.47	929.08		919.61	
+50				21.80	7.3
51				24.05	5.0
+50				26.30	2.8
+75				27.42	1.7
T.P.	11.03	✓ 939.45	066	✓ 928.42	
52				28.55	10.9
+50				30.80	8.7
53		✓		33.05	6.4
T.P.	11.56	947.07	394	✓ 935.51	
+50				35.30	11.8

4.

8

14.

15

$$\frac{11.2}{40} \quad \frac{10.0}{14} \quad \frac{7.0}{9}$$

$$\frac{13.8}{66}$$

$$\frac{6.6}{6} \quad \frac{7.2}{16} \quad \frac{10.3}{23} \quad \frac{11.4}{35}$$

9.15

$$\frac{15.0}{54}$$

$$\frac{6.0}{16} \quad \frac{12.0}{24} \quad \frac{12.9}{31} = \text{WS} \quad \frac{12.5}{38}$$

$$\text{L.O.} \quad \frac{15.0}{24} \text{ WS} = \frac{12.9}{21} \quad \frac{6.0}{10}$$

b. 1/14

$$\text{L.O.} \quad \frac{15.0}{30} \quad \frac{13.9}{25} \quad \frac{4.6}{12}$$

$$\frac{16.8}{8.6}$$

$$\frac{3.4}{5} \quad \frac{3.9}{16} \quad \frac{12.0}{27} \quad \frac{12.9}{30} \quad \frac{14.0}{40} \quad \frac{14.6}{46}$$

18.8

$$\text{L.O.} \quad \frac{15.0}{33} \quad \frac{12.9}{28} \quad \frac{2.3}{12}$$

$$\frac{1.6}{1.6}$$

$$\frac{1.5}{4} \quad \frac{2.6}{16} \quad \frac{12.0}{30} \quad \frac{12.9}{33} \quad \frac{14.5}{40}$$

$$\frac{23.0}{40} \quad \frac{9.07.5}{21.6} \quad \frac{8.1}{12}$$

$$\frac{21.1}{8.0}$$

$$\frac{8.0}{5} \quad \frac{8.5}{15} \quad \frac{9.09.0}{20.0} \quad \frac{22.0}{40}$$

$$\frac{18.3}{40} \quad \frac{18.0}{28} \quad \frac{6.2}{11}$$

$$\frac{23.5}{5.6}$$

$$\frac{6.4}{15} \quad \frac{16.0}{27} \quad \frac{18.7}{34} \quad \frac{22.0}{40}$$

$$\frac{10.6}{29} \quad \frac{7.1}{16} \quad \frac{3.2}{9}$$

$$\frac{26.2}{2.9}$$

$$\frac{3.1}{7} \quad \frac{x}{3.9} \quad \frac{10.5}{28} \quad \frac{12.1}{35}$$

$$\frac{+0.5}{40} \quad \frac{+0.2}{16} \quad \frac{3.9}{23} \quad \frac{2.3}{10}$$

$$\frac{27.3}{1.8}$$

$$\frac{2.1}{8} \quad \frac{7.6}{17} \quad \frac{4.5}{24} \quad \frac{6.2}{35}$$

$$\frac{6.2}{50} \quad \frac{7.0}{32} \quad \frac{12.1}{22} \quad \frac{11.7}{14}$$

$$\frac{28.5}{11.0}$$

$$\frac{11.7}{15} \quad \frac{12.0}{30} \quad \frac{11.6}{32} \quad \frac{11.6}{38}$$

$$\frac{+2.5}{50} \quad \frac{+1.0}{33} \quad \frac{9.3}{20}$$

30.7

$$\frac{8.8}{15} \quad \frac{9.7}{15} \quad \frac{9.4}{23} \quad \frac{8.4}{23} \quad \frac{5.3}{29} \quad \frac{5.8}{39} \quad \frac{10.5}{50}$$

$$\frac{+1.5}{50} \quad \frac{+7.3}{35} \quad \frac{5.3}{23} \quad \frac{7.1}{19}$$

$$\frac{33.1}{6.4}$$

$$\frac{7.1}{15} \quad \frac{5.4}{22} \quad \frac{1.8}{29} \quad \frac{2.2}{33} \quad \frac{4.7}{50}$$

$$\frac{1.3}{50} \quad \frac{0.3}{33} \quad \frac{11.0}{20} \quad \frac{12.6}{18} \quad \frac{12.2}{16}$$

35.9

$$\frac{11.5}{13} \quad \frac{12.5}{21} \quad \frac{10.6}{21} \quad \frac{6.7}{29} \quad \frac{2.6}{39} \quad \frac{9.1}{50}$$

Sta.	+	π ✓	-	Elev.	Revised Grade
		947.07			
5440		✓			37.55 9.5
B.M.	14.37	955.32	6.12		947.95 ✓ 945.92
+50					39.80 15.5
55					41.95 13.4
+50					43.51 11.8
56					44.47 10.9
+50					44.76 10.6
5740				9440	44.43 10.9
			14.37		945.95 ✓
+85					42.47
58					42.00
+40					40.98
59					38.9
+50					37.35
60					35.8
+50					34.3
+75					33.5

Lt.

E

Rt.

16

28	1.0	9.5	10.6	9.8	37.6				
50	33	24	18	16	9.5	10.3	83	0.0	1.0
						11	21	34	50

74	63	155	164	39.3					
50	33	24	21	100	16.5	16.0	14.7	2.7	3.7
					11	13	19	36	50

40	30	138	148	41.0					
50	26	24	15	143	14.7	13.7	13.7	0.7	1.7
					2	12	15	37	50

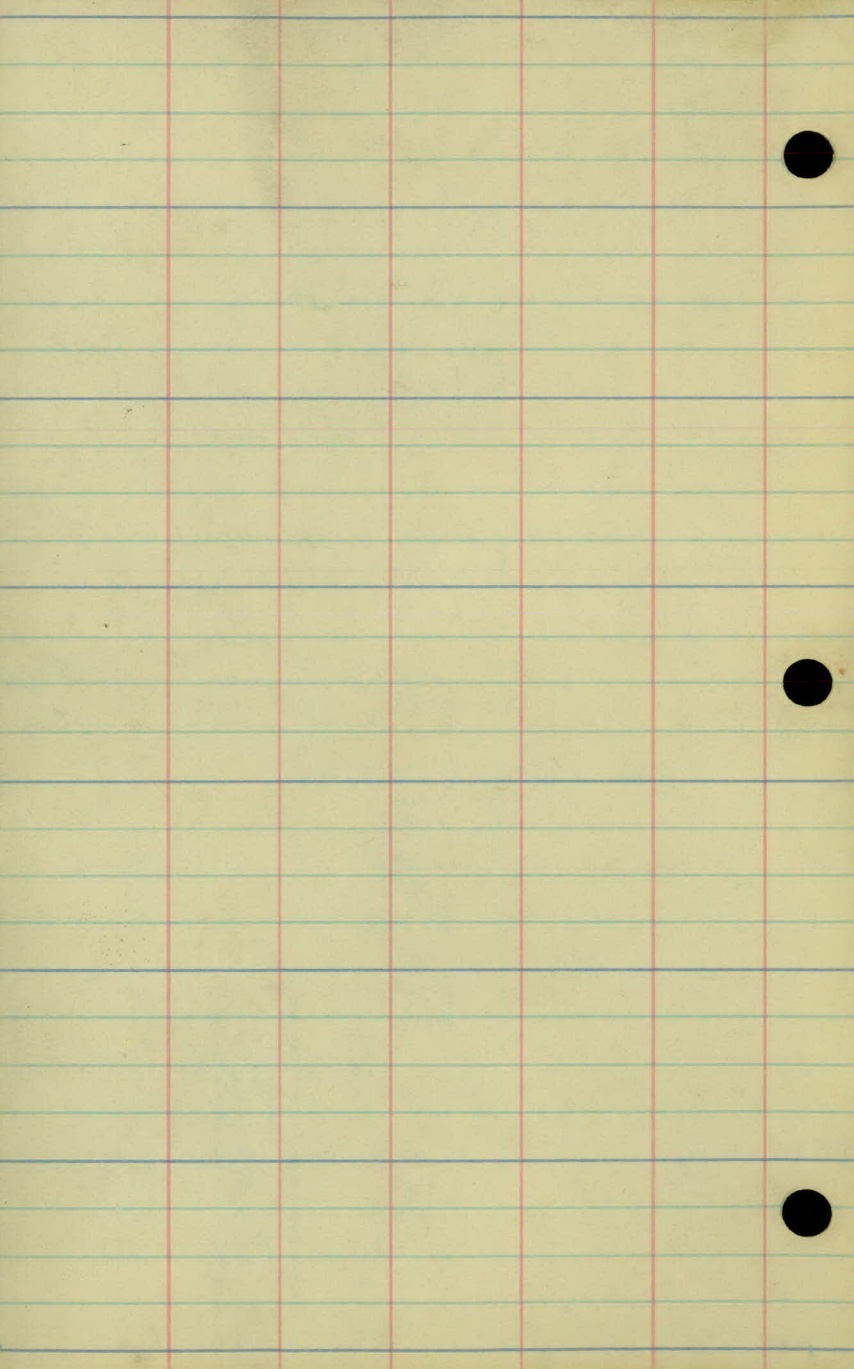
3.2	20	11.2	12.9	42.8					
50	25	26	16	125	12.6	6.3	8.0	0.2	1.0
					16	28	36	50	50

4.3	26	10.4	12.0	44.1					
50	23	26	16	112	11.4	7.2	0.7	1.7	
					15	21	31	50	

5.1	4.7	11.2		44.4					
50	32	25		109	11.4	10.6	10.6	0.8	3.0
					10	12	15	29	50

6.8	5.8	11.6		44.0					
50	32	22		143	11.7	9.1	3.4	4.6	
				0	14	16	26	50	

For Cross Sections from Sta. 57 to McMenamy
see 1925 Survey of Co. Rd. 'F'



Slope stakes
Co. Bel "F"
Sta. 32 to

Sta. + + - Grade.

B.M. 6.21 91245 90624

32+0 03.1 7.9

+50 03.5 2.0

33 04.1 6.4

+50 04.8 5.7

34 10.5 05.7

76

+50 2.8 06.5

7.7

35 9869
352
91048

+50 07.1

36 07.0

+50 06.6

37 05.8

0.00 = End of segment. 6.21 90624

Lt.

T

Rt.

Top Mon.

Grled -

1' Balun
Sub Groc

$$\begin{array}{r} 9.35 \\ 73 \end{array} \quad \begin{array}{r} 9.35 \\ 8.35 \end{array} \quad 33$$

$$\begin{array}{r} 86 \\ 00 \end{array}$$

$$\begin{array}{r} 27 \\ -0.3 \end{array} / 33$$

$$\begin{array}{r} 7.65 \\ 7.65 \end{array} \quad \begin{array}{r} 8.65 \\ 7.65 \end{array}$$

$$\begin{array}{r} 13.0 \\ 786 \end{array} / -5.3$$

$$\begin{array}{r} 7.7 \\ 00 \end{array}$$

$$\begin{array}{r} 9.0 \\ -0.3 \end{array} / 33$$

$$\begin{array}{r} 6.8 \\ 52.5 \end{array}$$

$$\begin{array}{r} 6.75 \\ 6.75 \end{array} \quad \begin{array}{r} 7.75 \\ 6.75 \end{array}$$

$$\begin{array}{r} 13.3 \\ 280 \end{array} / -6.5$$

$$\begin{array}{r} 6.4 \\ -0.1 \end{array}$$

$$\begin{array}{r} 6.7 \\ +1.0 \end{array} / 33$$

$$\begin{array}{r} 6.20 \\ 57.0 \end{array}$$

$$\begin{array}{r} 5.95 \\ 5.95 \end{array} \quad \begin{array}{r} 6.95 \\ 5.95 \end{array}$$

$$\begin{array}{r} 9.8 \\ 228 \end{array} / 7.9$$

$$\begin{array}{r} 6.2 \\ -0.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ +2.0 \end{array} / 33$$

$$\begin{array}{r} 6.13.2 \\ 59.4 \end{array}$$

$$\begin{array}{r} 5.55 \\ 5.55 \end{array}$$

$$\begin{array}{r} 73 \end{array}$$

$$\begin{array}{r} 5.4 \\ +0.2 \end{array}$$

$$33$$

$$\begin{array}{r} 6.13.7 \\ 60.4 \end{array}$$

$$\begin{array}{r} 5.35 \\ 5.35 \end{array}$$

$$\begin{array}{r} 5.1 \\ +0.3 \end{array}$$

$$\begin{array}{r} 6.14.2 \\ 61.4 \end{array}$$

$$\begin{array}{r} 5.45 \\ 5.45 \end{array}$$

$$\begin{array}{r} 4.6 \\ +0.4 \end{array}$$

$$\begin{array}{r} 6.14.2 \\ 62.4 \end{array}$$

$$\begin{array}{r} 5.85 \\ 5.85 \end{array}$$

$$\begin{array}{r} 4.0 \\ +1.9 \end{array}$$

$$\begin{array}{r} 6.13.7 \\ 60.4 \end{array}$$

$$\begin{array}{r} 6.65 \\ 6.65 \end{array}$$

$$\begin{array}{r} 4.7 \\ +2.0 \end{array}$$

$$\begin{array}{r} 6.12.7 \\ 58.4 \end{array}$$

6.09 912.33

906.24

37+50

04.8

38

03.5

+50

02.0

0.05 904.86 7.52

904.81

+75

01.75

39+0

00.5

+50

99.0

40

98.0

+50

97.0

41

97.6

+50

98.2

T.P 7.84 908.52 4.18 900.68

42

99.4

42+50

01.0

3.34

905.18

4-

2

Rt

$$\begin{array}{r} 8.5 \\ 7.5 \overline{) 73} \end{array}$$

$$\begin{array}{r} 6.2 \\ +1.3 \end{array}$$

$$\begin{array}{r} C-120 \\ 59.0 \end{array}$$

$$\begin{array}{r} 9.8 \\ 8.8 \overline{) 73} \end{array}$$

$$\begin{array}{r} 7.8 \\ +1.0 \end{array}$$

$$\begin{array}{r} C-7.0 \\ 47.0 \end{array}$$

$$\begin{array}{r} 11.3 \\ 10.3 \overline{) 11.3} \end{array}$$

$$\begin{array}{r} 9.4 \\ +1.4 \end{array}$$

$$\begin{array}{r} 10.3 \\ +1.0 \overline{) 33} \end{array}$$

C.R. Post

$$3.6$$

$$\begin{array}{r} 2.7 \\ +0.9 \end{array}$$

$$\begin{array}{r} 5.0 \\ -1.4 \overline{) 17.8} \end{array}$$

$$4.86$$

$$\begin{array}{r} 3.4 \\ +1.0 \end{array}$$

$$\begin{array}{r} 8.3 \\ -4.0 \overline{) 23.0} \end{array}$$

$$8.9$$

$$\begin{array}{r} 8.9 \\ 1.5 \end{array}$$

$$\begin{array}{r} 5.0 \\ +0.9 \end{array}$$

$$\begin{array}{r} 13.3 \\ -7.4 \overline{) 29.8} \end{array}$$

$$6.9$$

$$\begin{array}{r} 7.2 \\ 1.5 \end{array}$$

$$\begin{array}{r} 6.4 \\ +0.5 \end{array}$$

$$\begin{array}{r} 6.9 \\ 0.0 \overline{) 15} \end{array}$$

$$7.4$$

$$\begin{array}{r} 7.4 \\ 0.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ 7.5 \end{array}$$

$$7.3$$

$$\begin{array}{r} 7.0 \\ +0.3 \end{array}$$

$$\begin{array}{r} 7.8 \\ 1.5 \end{array}$$

$$\begin{array}{r} 18.6 \\ -11.3 \overline{) 37.6} \end{array}$$

$$6.7$$

$$\begin{array}{r} 6.5 \\ +0.2 \end{array}$$

$$\begin{array}{r} 6.7 \\ 1.5 \end{array}$$

$$\begin{array}{r} 15.2 \\ -8.5 \overline{) 32.0} \end{array}$$

$$7.1$$

$$\begin{array}{r} 7.1 \\ 0 \end{array}$$

$$\begin{array}{r} 7.3 \\ 1.5 \end{array}$$

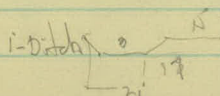
$$\begin{array}{r} 15.3 \\ -6.2 \overline{) 27.4} \end{array}$$

$$7.5$$

$$7.5 \overline{) 2.000}$$

$$\begin{array}{r} 7.3 \\ +0.2 \end{array}$$

$$\begin{array}{r} 7.7 \\ 1.5 \end{array}$$



8.41 913.59

905.18

43

02.7

+50

04.4

44

06.0

+50

07.4

45

08.7

+50

09.8

T.P.

6.55

917.93

2.21

911.38

46

10.7

+50

11.5

47

12.1

+50

12.6

48

12.9

+50

13.5

$$\frac{11.1}{109} \text{ } 23$$

$$200 \left| \frac{9.4}{20.30} \right.$$

$$\frac{11.1}{10.00}$$

$$\frac{105}{10.4}$$

$$9.2 \text{ } 20$$

$$\frac{8.8}{10.4}$$

$$7.6 \text{ } 20$$

$$\frac{7.1}{10.5}$$

$$6.2 \text{ } 20$$

$$\frac{5.4}{10.8}$$

$$4.9 \text{ } 24$$

$$\frac{4.1}{10.8}$$

$$3.8 \text{ } 24 \text{ } 32 \left| \frac{1.3}{20.45} \right.$$

$$\frac{2.9}{10.9}$$

$$\frac{5.8}{20.00} / 31.1$$

$$7.2 \text{ } 24$$

$$32 \left| \frac{7.3}{20.19} \right.$$

$$\frac{6.5}{10.7}$$

$$\frac{9.2}{20.00} / 20.7$$

$$6.4 \text{ } 24$$

$$32 \left| \frac{7.6}{20.10} \right.$$

$$\frac{5.6}{10.8}$$

$$\frac{8.6}{20.00} / 20.7$$

$$5.8 \text{ } 24$$

$$32 \left| \frac{6.4}{20.14} \right.$$

$$\frac{5.2}{10.6}$$

$$\frac{4.1}{20.37} / 23$$

$$5.3 \text{ } 24$$

$$32 \left| \frac{5.4}{20.19} \right.$$

$$\frac{5.1}{10.7}$$

$$\frac{4.1}{20.32} / 32$$

$$5.0 \text{ } 24$$

$$\frac{4.6}{10.4}$$

$$\frac{6.3}{20.09} / 32$$

$$4.4$$

$$21 \left| \frac{7.6}{20} \right.$$

$$\frac{4.2}{10.2}$$

$$\frac{4.1}{15}$$

$$\frac{8.0}{14.6}$$

91793

49+0

14.7

49+50

16.3

T.P.

8.75

916.50

0.18

917.75

50+0

18.6

750

21.1

51

23.6

+50

26.0

T.P.

9.02

935.30

0.17

916.33

+75

27.2

52

28.4

+50

30.8

53

33.1

T.P.

9.30

943.69

0.86

934.49

+50

35.3

54

37.6

$$32 \begin{array}{r} 24 \\ 16 \end{array}$$

$$\begin{array}{r} 30 \\ 102 \end{array}$$

$$\begin{array}{r} 31 \\ 15 \end{array}$$

$$16$$

$$\begin{array}{r} 12 \\ 04 \end{array}$$

$$\begin{array}{r} 16 \\ 15 \end{array}$$

W
u
u
u

$$79 \begin{array}{r} 81 \end{array}$$

$$\begin{array}{r} 22 \\ 102 \end{array}$$

$$54 \begin{array}{r} 86 \end{array}$$

$$\begin{array}{r} 54 \\ 5 \end{array}$$

$$79 \begin{array}{r} 31 \end{array}$$

$$\begin{array}{r} 30 \\ 01 \end{array}$$

$$0.1 \begin{array}{r} 0.7 \end{array}$$

$$232 \begin{array}{r} 46 \\ -41 \end{array}$$

$$\begin{array}{r} 04 \\ 101 \end{array}$$

$$\begin{array}{r} 13 \\ 15 \end{array}$$

$$810 \begin{array}{r} 83 \\ 101 \end{array}$$

$$32 \begin{array}{r} 53 \\ 1245 \end{array}$$

$$\begin{array}{r} 80 \\ 0 \end{array}$$

$$\begin{array}{r} 103 \\ 2020/22? \end{array}$$

$$70 \begin{array}{r} 72 \\ 85 \end{array}$$

$$75 \begin{array}{r} 60 \\ 2025 \end{array}$$

$$\begin{array}{r} 70 \\ 100 \end{array}$$

$$\begin{array}{r} 85 \\ 2020/25 \end{array}$$

$$46 \begin{array}{r} 48 \\ 01 \end{array}$$

$$23 \begin{array}{r} 31 \\ 230 \end{array}$$

$$\begin{array}{r} 46 \\ 0 \end{array}$$

$$\begin{array}{r} 46 \\ 2015 \\ 24 \end{array}$$

$$72 \begin{array}{r} 25 \\ 38 \end{array}$$

$$21 \begin{array}{r} 72 \\ 1215 \end{array}$$

$$\begin{array}{r} 20 \\ 0 \end{array}$$

$$\begin{array}{r} 23 \\ 2015/23' \end{array}$$

$$84 \begin{array}{r} 86 \\ 99 \end{array}$$

$$21 \begin{array}{r} 89 \\ 00 \end{array}$$

$$\begin{array}{r} 89 \\ 15 \end{array}$$

$$\begin{array}{r} 84 \\ 00 \end{array}$$

$$\begin{array}{r} 84 \\ 2015/22 \end{array}$$

$$61 \begin{array}{r} 03 \\ 16 \end{array}$$

$$21$$

$$\begin{array}{r} 63 \\ 02 \end{array}$$

$$\begin{array}{r} 52 \\ 21 \end{array}$$

94269

54+50

2

39.8

D.M.

8.01

94893

2.80

940.89

94892

55

42.0

+50

43.5

56

44.5

+50

44.8 - Summit

57

44.4

+50

42.5

+85

42.5

58

42.0

0.84

94333

644

94249

+50

40.8

59

38.9

+50

37.4

$$38 \overline{) \frac{41}{54}}$$

$$21 \overline{) \frac{47}{-}}$$

$$\frac{43}{-0.4}$$

$$\frac{1.9}{-} \overline{) 21}$$

$$69 \overline{) \frac{71}{84}}$$

$$21 \overline{) \frac{83}{15}}$$

$$\frac{7.8}{-0.9}$$

$$\frac{4.5}{-} \overline{) 21'} \text{ diff } 1.5$$

$$54 \overline{) \frac{56}{64}}$$

$$21 \overline{) \frac{61}{17.0} \frac{6.5}{10}}$$

$$\frac{61}{-0.7}$$

$$33 \overline{) 21}$$

$$44 \overline{) \frac{46}{59}}$$

$$21 \overline{) 5.3}$$

$$\frac{48}{-0.4}$$

$$13 \overline{) 21}$$

$$41 \overline{) \frac{43}{56}}$$

$$\frac{5.3}{22} \quad \frac{5.1}{15}$$

$$\frac{4.5}{-0.4}$$

$$\frac{4.6}{15}$$

$$1.3 \overline{) 21'}$$

$$4.5 \overline{) \frac{47}{60}}$$

$$22 \overline{) \frac{5.3}{15}}$$

$$\frac{4.9}{-0.4}$$

$$\frac{5.2}{15}$$

$$\frac{3.7}{-} \overline{) 22}$$

$$54 \overline{) \frac{56}{64}}$$

$$23 \overline{) -}$$

$$\frac{6.4}{15}$$

$$\frac{5.7}{-0.3}$$

$$\frac{6.2}{15}$$

$$\frac{6.2}{-} \overline{) 23}$$

X

X

$$69 \overline{) \frac{71}{84}}$$

$$24 \overline{) \frac{76}{-}}$$

$$\frac{7.5}{15}$$

$$\frac{7.0}{-0.1}$$

$$\frac{7.5}{15}$$

$$\frac{7.4}{-} \overline{) 24}$$

$$2.8 \overline{) \frac{30}{4.3}}$$

$$24 \overline{) \frac{3.4}{-}}$$

$$\frac{3.3}{11}$$

$$\frac{3.9}{-0.1}$$

$$\frac{3.8}{15}$$

$$\frac{3.8}{-} \overline{) 24}$$

$$4.4 \overline{) \frac{4.6}{5.9}}$$

$$24 \overline{) \frac{4.6}{-}}$$

$$\frac{5.0}{15}$$

$$\frac{4.5}{-0.1}$$

$$\frac{4.7}{15}$$

$$\frac{4.7}{-} \overline{) 24}$$

$$59 \overline{) \frac{61}{7.4}}$$

$$24 \overline{) \frac{4.7}{-}}$$

$$\frac{6.8}{15}$$

$$\frac{61}{-0.2}$$

$$\frac{6.3}{15}$$

$$61 \overline{) 24}$$

94333

6040

35.8

+50

34.3

+60

33.9

+75

33.5

60488

6040295

11.83

931.50

$$7.5 \overline{) 7.7} \\ \underline{9.0}$$

$$24 \overline{) 7.5} \\ \underline{1}$$

$$\frac{8.2}{15}$$

$$\frac{7.7}{-0.2}$$

$$\frac{7.7}{15}$$

$$\frac{7.7}{24}$$

$$9.0 \overline{) 9.2} \\ \underline{10.5} \quad 11.0 \quad 24 \overline{) 9.2}$$

$$\frac{9.0}{-0.5}$$

$$\frac{9.9}{15}$$

$$\frac{10.5}{24.2010}$$

