

Dr. 6 - BK. 101

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

NORTH CO. LINE RD.
Rice St. Wilkenson La.
From Centerville Rd Co. Otter Lake R.

Road Acc't. No. 30

Date Filed. 1936

File B. 101 D. 6

Alignment

No. Co. Line

E Rice St Ext'd to

angle.

Sta.	Point	Lt.	Rt.
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363+54.80	P.I.		
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337+15.39	P.I. Mon.	$0^{\circ} 11\frac{1}{2}'$ rd	
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311+50.17	Trans Mon.	$0^{\circ} 03'$	
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W.H. Carlson
Anker
Hendrix
Moescher

(2"x2" Hub)
Est.

29.52'

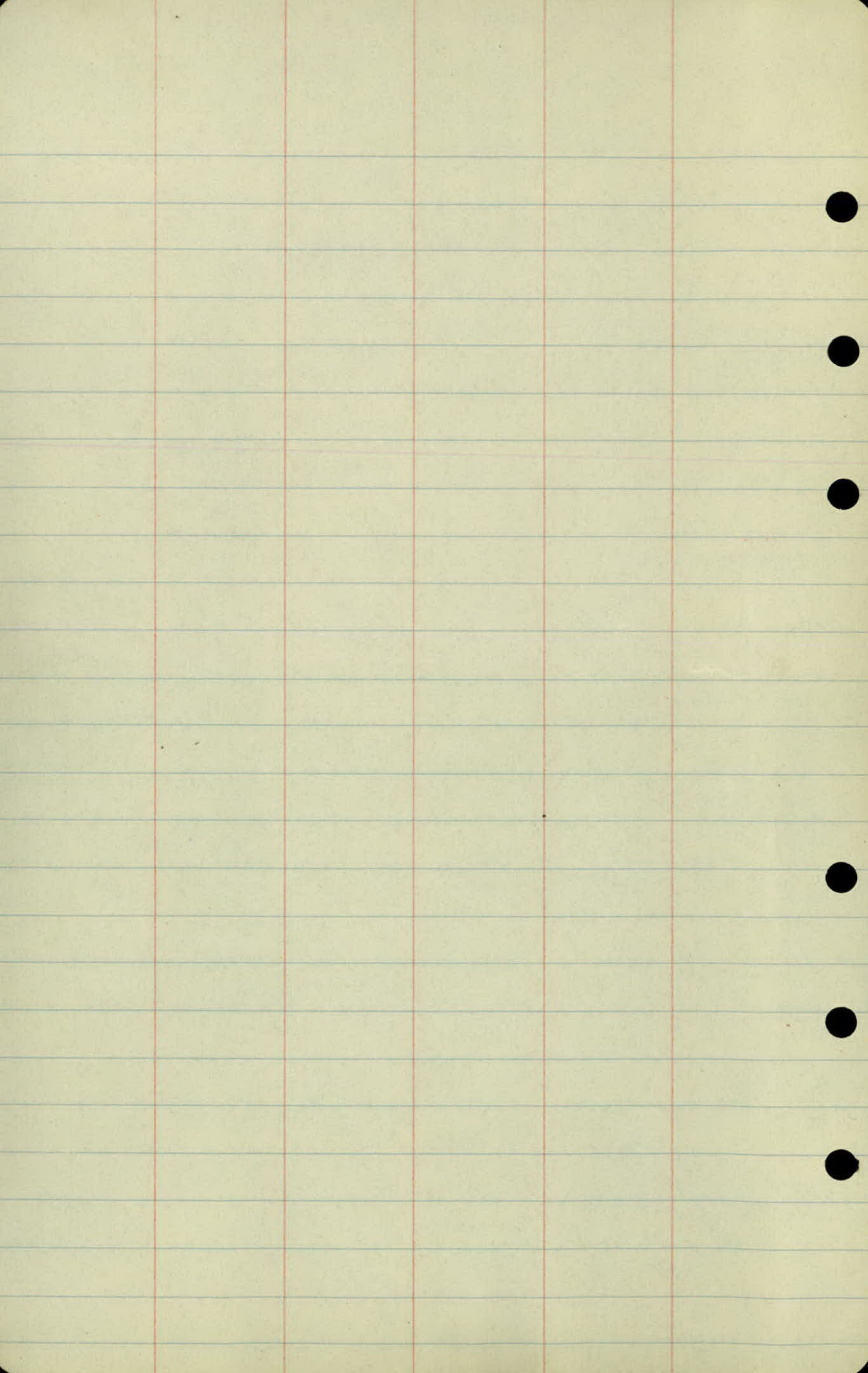
F. Cor.

Gate
H.P.
4.11
3

Iron/Box & Turtle Lake Rd.

50.50

P.P.



Topography

3/3

12.8

3/2

11 8

+50.17- ¹⁵⁰⁰ / 1705.

3/1

475 350 11

Mentow.



+99-T.P.12'

F-26 - F-43

+76-T.P.12'

320

11-11

319

11-10

318

12-10

317

11'-11'

+41' ϕ 18" x 36' c.m.

316

11-9'

315

10-9'

314

12 8

313

Tree Brush Line
29

F-76
Tree Brush 26'

+10-T.P.

Small Pop. Brush.

F-76

+77-T.P. 12'

Small Brush.

+74-F. Cor. 28

+62-T.P. 12'

+33-End Curve
15'

+10-F. Cor. 27

+40-T.P. 13'

+22-T.P. 13'

F-27

+73-F. Cor. 43

+70-Pop. Paper 35

+50-End Curve
16'

Rangeto Fence NW

Ditch

Ditch

11-8'

326

11-11

325

12-11

324

11-12

323

11-11

322

12-11

321

11-10

320

463-T.P. 13'

F-76

Meadow

+10

441 T.P. 13'

+17-T.P. 13'

+183-F. Cor. 28'

485-T.P. 13'

F-76

+61-T.P. 12'

Small Popo
Bush

Waste Land

End of Popo
+ Bush

24'

494-T.P. 12'

11-8

333

9-9'

154-2 12" X 30" CM

16-14

332

10-8'

331

10-8

330

9-9

329

9-9'

328

10-8

327

Pro Cult.

+94-T.P. 13'

+35-Farm to 150'

Farm
yard

+75-Ent.

Meadow

+57-T.P. 13'

+42-Range to Fence

+31-E. Cor. 31'

+30-T.P. 13'

Low Land

+06-T.P.
F-76

Meadow

Small Brush

+80-T.P. 13'

341

10/10

340

11-13'

+50 10-21

339

11'-12-15!38

+50 40-60

338

10-10'

83'—115'

+15.39 1000 Mon.
Δ0.1 1/2 Rt.

337

10 10

336

10-8'

335

10-10'

334

+74-P.P. 28'

+75-T.P. 28'

+78-P.P. 28'

Cut-

+30-F. Cor. 32'

+44-T.P. 22'

+52-T.P. 20'

+25- $\frac{1}{2}$ Gate to Cemetery Ent.
F-32'

+26
Turntable Rd.
+08

+87-P.P. 26'

+88-P.P. 43'

+56-T.P. 17'

+70-F. Cor. 33'

+70-Gov. B.M. 28.4

+35-T.P. 13'

+15-T.P. 13'

12' 11'

347

11 10

~~347~~

346

11 11

345

11-10

+66- ϕ 24" X 37" Conc.

19'-18'

344

11-11

Gravel Width

343

342

12-10

341

+60. Sin Ditch 23'
+53-R.P. 28'

Ditch

Ditch

+Ditch 33'
+85-T.P. 28'

+52-T.P. 28'

+Ditch 30'
Small.

Ditch.

+61-R.P.

Ditch

+12-T.P. 28'

+68-R.P. 28'

Meadow.

+88-T.P. 28'

+41-Ent Field

Meadow.

+31-F. Cor. 30'

+50-T.P. 28'

+50-Road 28'
To Fence

355

13-9

354

12-9

353

12-10

352

12-11

351

11-11

350

11-11

349

11-11

348

F-29

+10-P.R. 28'

F-28'

+67-R.D. 28

+72-F. Cor. 29'
+72-P.P. 28'

+56 Rd. 15' x 30' C.M.
+ at End Culv. 23

+17-P.P. 28'

~~+17-P.P. 28'~~
Ditch 25'

+48-P.P. 27'

Bag
Pasture

Ditch to
Drain Bag.

Culv. Ditch

+65-55' x 15' x 24' C.M.
+54-F. Cor. 28' 22'
+32-T.P. 28'

Scattered oaks.
Pasture.

+66-T.P. 28'
F-28'

+57-F. Cor. 29'

+72-T.P. 28

+59
+50
+55-57' x 12' x 32' C.M.
+39-F. Culv. 30'

End of Ditch.

+38-T.P. 28'

+42-T.P. 28

E-Ditch 31'

+13-T.P. 28

362

14'-9"

361

14'-10"

360

13'-9"

359

14'-8"

+64-± High Ten. Line.

+37-± Feather Line.

+09-± High Tension Area.

358

14'-9"

357

14'-9"

356

14'-8"

F-28'

+74-T.P. 28'

+50-P.P. 28'

+42-T.P. 28'

+23-T.P. 28'

F-29'

+81-T.P. 34'

+69-P.P. 28'

+52-ENT. 15" X 24" C.M.
22'

+31-P.P. 29'

+06-F. cor. 30'

{ +12-ENT. 15" X 24" C.M.
+81-End. Ch. 10.25'
+78-T.P. 28'
+65-Highway 40
+59-Highway 34

+81-T.P. 28'

Waste land.

+51-F. Cor. 30'
+49-P.P. 28'

+50-T.P. 28'

+20-ENT. 14" X 20"
125'

South
side
Dikes.

378

377

366

365

364

363

14-8

362

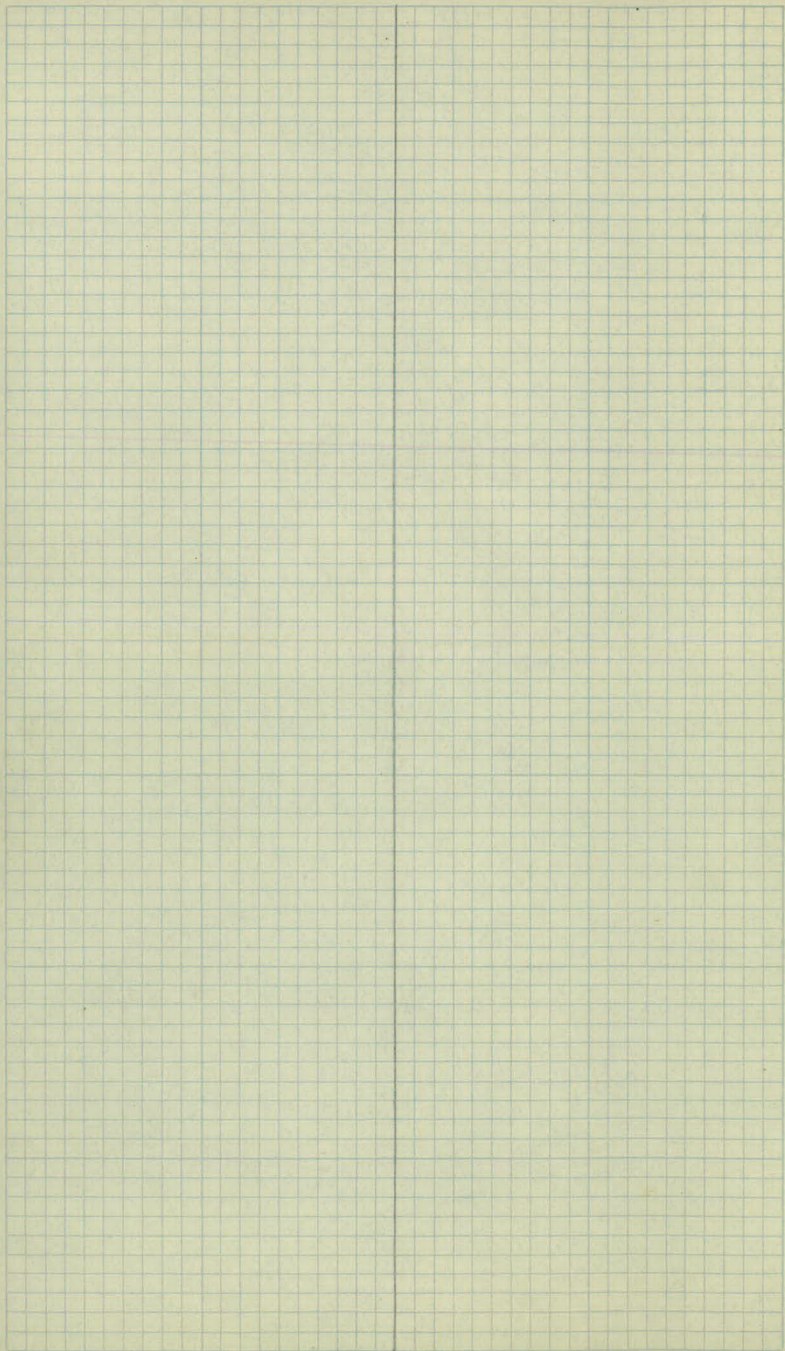
Water level.

Still Form.

+55-F. Cor. 29.52

+98-T.O. 26'

+94-R.D. 28'



Cross-Sections
County Road J

Sta. 311+50.17 to

Sta.	+	Σ	-	Elev.
B.M.	511	899.06		893.95

311	+50.17			93.7
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312				93.6
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	+60			93.3
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313				93.6
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	+55			93.6
--	-----	--	--	------

314				93.7
-----	--	--	--	------

	+50			94.0
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315				94.3
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	+50			93.8
--	-----	--	--	------

316				93.8
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+40 Ditch x 5
~~5~~ X

Lt.

E

Rt.

Spike in 6" Poplar 85' Rt. Sta. 313 490

$\frac{77}{50}$	$\frac{77}{26}$	$\frac{82}{24}$	$\frac{82}{17}$	$\frac{58}{12}$	$\frac{54}{-}$	$\frac{6.0}{11}$	$\frac{8.5}{20}$	$\frac{7.8}{23}$	$\frac{7.1}{28}$	$\frac{7.0}{50}$
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$\frac{7.3}{50}$	$\frac{7.6}{25}$	$\frac{8.1}{23}$	$\frac{8.0}{18}$	$\frac{6.1}{12}$	$\frac{5.5}{-}$	$\frac{5.6}{8}$	$\frac{8.6}{19}$	$\frac{8.8}{21}$	$\frac{7.7}{25}$	$\frac{7.7}{50}$
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$\frac{7.8}{50}$	$\frac{7.4}{25}$	$\frac{7.9}{24}$	$\frac{7.8}{17}$	$\frac{5.6}{13}$	$\frac{5.8}{-}$	$\frac{5.6}{13}$	$\frac{8.2}{20}$	$\frac{8.3}{22}$	$\frac{5.8}{26}$	$\frac{5.7}{50}$
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$\frac{8.0}{50}$	$\frac{7.8}{25}$	$\frac{8.4}{23}$	$\frac{8.3}{18}$	$\frac{6.0}{13}$	$\frac{5.5}{-}$	$\frac{5.4}{9}$	$\frac{6.6}{14}$	$\frac{8.3}{19}$	$\frac{8.3}{22}$	$\frac{6.5}{25}$	$\frac{6.4}{42}$	$\frac{6.0}{50}$
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$\frac{7.7}{50}$	$\frac{7.6}{34}$	$\frac{7.8}{26}$	$\frac{8.5}{24}$	$\frac{8.5}{19}$	$\frac{6.1}{12}$	$\frac{5.5}{-}$	$\frac{5.6}{8}$	$\frac{6.9}{13}$	$\frac{8.9}{18}$	$\frac{8.9}{21}$	$\frac{7.7}{24}$	$\frac{7.5}{50}$
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$\frac{7.8}{50}$	$\frac{7.6}{25}$	$\frac{8.4}{24}$	$\frac{8.3}{18}$	$\frac{5.6}{11}$	$\frac{5.4}{-}$	$\frac{6.0}{11}$	$\frac{7.1}{16}$	$\frac{8.6}{20}$	$\frac{8.6}{22}$	$\frac{7.4}{25}$	$\frac{7.3}{50}$
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$\frac{6.8}{50}$	$\frac{7.6}{25}$	$\frac{7.3}{23}$	$\frac{7.0}{17}$	$\frac{5.4}{13}$	$\frac{5.1}{-}$	$\frac{5.3}{10}$	$\frac{6.3}{15}$	$\frac{8.2}{21}$	$\frac{8.2}{22}$	$\frac{7.2}{24}$	$\frac{7.3}{50}$
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$\frac{6.8}{50}$	$\frac{6.4}{24}$	$\frac{7.3}{23}$	$\frac{7.3}{19}$	$\frac{5.4}{14}$	$\frac{4.8}{-}$	$\frac{5.4}{10}$	$\frac{6.5}{15}$	$\frac{8.6}{21}$	$\frac{8.6}{22}$	$\frac{7.2}{25}$	$\frac{7.0}{50}$
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$\frac{7.2}{50}$	$\frac{6.8}{25}$	$\frac{7.6}{24}$	$\frac{7.6}{18}$	$\frac{5.8}{13}$	$\frac{5.3}{-}$	$\frac{5.5}{12}$	$\frac{7.5}{17}$	$\frac{7.8}{20}$	$\frac{8.6}{22}$	$\frac{8.6}{23}$	$\frac{7.1}{28}$	$\frac{6.9}{29}$	$\frac{7.0}{50}$
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$\frac{7.5}{50}$	$\frac{7.4}{25}$	$\frac{8.1}{24}$	$\frac{8.1}{18}$	$\frac{5.7}{14}$	$\frac{5.3}{-}$	$\frac{5.6}{9}$	$\frac{7.6}{16}$	$\frac{7.9}{19}$	$\frac{8.7}{21}$	$\frac{8.7}{22}$	$\frac{7.5}{24}$	$\frac{8.1}{50}$
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in ditch. $\frac{8.9}{100}$ $\frac{9.8}{-}$ pipe. $\frac{9.6}{-}$ pipe $\frac{9.3}{125}$ in ditch

Sta. + π - Elev.

899.06

316 +50

93.5

317

93.9

+50

94.2

318

93.9

+50

93.9

T.P.

2.20

896.26

5.00

894.06

319

93.4

+50

92.8

320

91.7

+50

91.1

321

91.5

3rv

91.6

4.

2

24.

$$\frac{74}{50} \quad \frac{74}{27} \quad \frac{84}{17} \quad \frac{57}{12} \quad \frac{56}{11} \quad \frac{56}{11} \quad \frac{84}{17} \quad \frac{83}{23} \quad \frac{78}{24} \quad \frac{28}{50}$$

$$\frac{76}{50} \quad \frac{78}{25} \quad \frac{83}{24} \quad \frac{83}{17} \quad \frac{53}{12} \quad \frac{52}{12} \quad \frac{56}{12} \quad \frac{81}{17} \quad \frac{81}{23} \quad \frac{77}{25} \quad \frac{77}{25} \quad \frac{7.6}{50}$$

$$\frac{76}{50} \quad \frac{77}{25} \quad \frac{83}{24} \quad \frac{81}{18} \quad \frac{54}{13} \quad \frac{49}{13} \quad \frac{51}{10} \quad \frac{82}{15} \quad \frac{84}{24} \quad \frac{29}{25} \quad \frac{80}{50}$$

$$\frac{78}{50} \quad \frac{78}{25} \quad \frac{84}{24} \quad \frac{79}{18} \quad \frac{53}{13} \quad \frac{52}{13} \quad \frac{53}{10} \quad \frac{84}{16} \quad \frac{84}{23} \quad \frac{78}{25} \quad \frac{78}{50}$$

$$\frac{77}{50} \quad \frac{77}{25} \quad \frac{85}{23} \quad \frac{86}{18} \quad \frac{52}{12} \quad \frac{52}{12} \quad \frac{52}{10} \quad \frac{83}{16} \quad \frac{83}{24} \quad \frac{77}{26} \quad \frac{77}{50}$$

(= 41) int. p.

$$\frac{50}{50} \quad \frac{51}{25} \quad \frac{56}{23} \quad \frac{60}{17} \quad \frac{27}{11} \quad \frac{29}{11} \quad \frac{30}{11} \quad \frac{58}{17} \quad \frac{57}{24} \quad \frac{50}{25} \quad \frac{49}{50}$$

$$\frac{53}{50} \quad \frac{53}{25} \quad \frac{60}{23} \quad \frac{63}{17} \quad \frac{34}{12} \quad \frac{35}{12} \quad \frac{39}{10} \quad \frac{51}{13} \quad \frac{54}{16} \quad \frac{61}{17} \quad \frac{60}{20} \quad \frac{50}{24} \quad \frac{5.2}{50}$$

$$\frac{4.5}{50} \quad \frac{50}{25} \quad \frac{59}{23} \quad \frac{62}{17} \quad \frac{46}{13} \quad \frac{46}{13} \quad \frac{47}{11} \quad \frac{54}{13} \quad \frac{53}{16} \quad \frac{60}{17} \quad \frac{59}{24} \quad \frac{53}{26} \quad \frac{53}{50}$$

$$\frac{52}{50} \quad \frac{52}{25} \quad \frac{62}{23} \quad \frac{65}{18} \quad \frac{51}{15} \quad \frac{52}{15} \quad \frac{51}{11} \quad \frac{57}{17} \quad \frac{63}{18} \quad \frac{60}{24} \quad \frac{54}{25} \quad \frac{52}{50}$$

$$\frac{48}{50} \quad \frac{49}{30} \quad \frac{52}{24} \quad \frac{60}{23} \quad \frac{65}{16} \quad \frac{48}{12} \quad \frac{48}{12} \quad \frac{51}{11} \quad \frac{57}{16} \quad \frac{61}{18} \quad \frac{61}{24} \quad \frac{53}{25} \quad \frac{56}{50}$$

$$\frac{50}{50} \quad \frac{51}{25} \quad \frac{60}{23} \quad \frac{64}{17} \quad \frac{60}{14} \quad \frac{45}{12} \quad \frac{47}{12} \quad \frac{47}{11} \quad \frac{58}{14} \quad \frac{59}{17} \quad \frac{65}{18} \quad \frac{62}{24} \quad \frac{52}{26} \quad \frac{50}{50}$$

Sta.	+	Σ	-	Elev.
322 +50		896.26		92.1.
323				92.3.
324				92.8.
T.P.	5.94	899.23	2.97	893.29
325				93.9.
+50				94.4.
326				94.4.
+60				94.6.
327				94.6.
+90				94.0.
328				93.6.
329				92.8.

47.

48.

49.

$$\frac{4.9}{50} \quad \frac{5.0}{28} \quad \frac{6.0}{23} \quad \frac{6.3}{16} \quad \frac{4.6}{12} \quad \frac{4.2}{-} \quad \frac{4.4}{11} \quad \frac{5.6}{15} \quad \frac{5.6}{17} \quad \frac{6.2}{18} \quad \frac{6.1}{24} \quad \frac{5.0}{25} \quad \frac{5.0}{50}$$

$$\frac{4.9}{50} \quad \frac{4.9}{28} \quad \frac{5.8}{21} \quad \frac{6.1}{16} \quad \frac{4.3}{12} \quad \frac{4.0}{-} \quad \frac{4.3}{11} \quad \frac{5.6}{15} \quad \frac{5.5}{17} \quad \frac{6.2}{19} \quad \frac{6.1}{24} \quad \frac{5.1}{26} \quad \frac{5.0}{50}$$

$$\frac{4.9}{50} \quad \frac{4.9}{24} \quad \frac{6.0}{20} \quad \frac{5.2}{14} \quad \frac{3.9}{12} \quad \frac{3.5}{-} \quad \frac{3.9}{12} \quad \frac{5.0}{15} \quad \frac{5.0}{18} \quad \frac{5.9}{19} \quad \frac{5.8}{24} \quad \frac{4.8}{26} \quad \frac{4.2}{50}$$

$$\frac{7.6}{50} \quad \frac{7.6}{24} \quad \frac{8.2}{23} \quad \frac{8.3}{18} \quad \frac{5.3}{12} \quad \frac{5.3}{-} \quad \frac{5.7}{11} \quad \frac{7.3}{14} \quad \frac{7.5}{17} \quad \frac{8.4}{19} \quad \frac{8.2}{24} \quad \frac{7.5}{26} \quad \frac{7.5}{50}$$

$$\frac{7.5}{50} \quad \frac{7.5}{23} \quad \frac{8.2}{22} \quad \frac{8.1}{17} \quad \frac{4.9}{12} \quad \frac{4.8}{-} \quad \frac{5.1}{10} \quad \frac{7.1}{14} \quad \frac{7.3}{18} \quad \frac{8.2}{18} \quad \frac{8.3}{25} \quad \frac{7.5}{26} \quad \frac{7.5}{50}$$

$$\frac{7.6}{50} \quad \frac{7.5}{23} \quad \frac{8.1}{22} \quad \frac{8.1}{16} \quad \frac{5.0}{12} \quad \frac{4.8}{-} \quad \frac{4.7}{11} \quad \frac{6.5}{15} \quad \frac{6.7}{18} \quad \frac{7.4}{19} \quad \frac{7.5}{26} \quad \frac{6.6}{27} \quad \frac{7.0}{50}$$

$$\frac{7.6}{50} \quad \frac{7.1}{28} \quad \frac{7.7}{23} \quad \frac{7.4}{17} \quad \frac{5.4}{13} \quad \frac{4.6}{-} \quad \frac{4.7}{10} \quad \frac{5.7}{18} \quad \frac{6.6}{19} \quad \frac{6.5}{24} \quad \frac{5.1}{26} \quad \frac{5.2}{50}$$

$$\frac{7.5}{50} \quad \frac{6.9}{23} \quad \frac{7.4}{22} \quad \frac{7.2}{17} \quad \frac{5.2}{12} \quad \frac{4.6}{-} \quad \frac{4.7}{18} \quad \frac{6.2}{20} \quad \frac{6.2}{23} \quad \frac{5.0}{26} \quad \frac{4.7}{50}$$

$$\frac{7.3}{50} \quad \frac{7.1}{24} \quad \frac{7.7}{22} \quad \frac{7.6}{17} \quad \frac{5.7}{13} \quad \frac{5.2}{-} \quad \frac{5.5}{8} \quad \frac{7.1}{13} \quad \frac{7.1}{18} \quad \frac{8.2}{19} \quad \frac{8.2}{25} \quad \frac{7.6}{26} \quad \frac{7.7}{50}$$

$$\frac{7.7}{50} \quad \frac{7.5}{23} \quad \frac{8.2}{22} \quad \frac{8.2}{17} \quad \frac{6.5}{13} \quad \frac{5.6}{-} \quad \frac{5.9}{9} \quad \frac{7.5}{13} \quad \frac{7.5}{18} \quad \frac{8.4}{19} \quad \frac{8.3}{25} \quad \frac{7.5}{26} \quad \frac{7.5}{50}$$

$$\frac{7.7}{50} \quad \frac{7.6}{23} \quad \frac{8.5}{22} \quad \frac{8.5}{15} \quad \frac{6.7}{12} \quad \frac{6.4}{-} \quad \frac{6.2}{11} \quad \frac{7.6}{13} \quad \frac{7.7}{19} \quad \frac{8.4}{20} \quad \frac{8.5}{26} \quad \frac{7.5}{27} \quad \frac{8.0}{50}$$

Sta.	+	π	-	Elev.
		899.23		
330.				93.1.
T.P.	6.62	901.14	4.71	894.52
+70				93.9.

331				94.5.
+65				95.6.

332				95.7.
+50				95.6.

333				96.6.
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+60				98.3.
T.P.	10.86	910.38	1.62	899.52
334				99.5.

+40				00.6.
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335				02.3.
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4.

5

pt.

$\frac{2.5}{50}$ $\frac{2.6}{23}$ $\frac{8.3}{21}$ $\frac{8.4}{16}$ $\frac{6.5}{12}$ $\frac{6.1}{12}$ $\frac{7.4}{14}$ $\frac{7.5}{19}$ $\frac{8.3}{20}$ $\frac{8.3}{26}$ $\frac{7.3}{27}$ $\frac{7.7}{50}$

$\frac{9.4}{50}$ $\frac{9.5}{23}$ $\frac{10.2}{22}$ $\frac{10.2}{16}$ $\frac{7.7}{11}$ $\frac{7.2}{10}$ $\frac{7.5}{10}$ $\frac{9.1}{14}$ $\frac{9.4}{19}$ $\frac{10.0}{20}$ $\frac{10.0}{26}$ $\frac{9.2}{27}$ $\frac{9.1}{50}$

$\frac{9.1}{50}$ $\frac{9.1}{22}$ $\frac{9.5}{21}$ $\frac{9.5}{16}$ $\frac{7.2}{11}$ $\frac{6.6}{11}$ $\frac{7.0}{11}$ $\frac{8.3}{16}$ $\frac{8.3}{19}$ $\frac{8.9}{20}$ $\frac{8.9}{26}$ $\frac{8.1}{27}$ $\frac{8.3}{50}$

$\frac{5.2}{50}$ $\frac{5.2}{23}$ $\frac{5.7}{16}$ $\frac{5.8}{9}$ $\frac{5.5}{9}$ $\frac{5.8}{9}$ $\frac{5.6}{15}$ $\frac{4.8}{19}$ $\frac{5.2}{22}$ $\frac{5.1}{50}$

$\frac{3.4}{50}$ $\frac{4.5}{27}$ $\frac{5.0}{18}$ $\frac{5.7}{11}$ $\frac{5.4}{10}$ $\frac{5.7}{10}$ $\frac{6.6}{14}$ $\frac{8.1}{50}$

$\frac{5.8}{50}$ $\frac{6.8}{28}$ $\frac{7.8}{17}$ $\frac{6.1}{13}$ $\frac{5.5}{11}$ $\frac{5.8}{11}$ $\frac{8.6}{17}$ $\frac{8.8}{50}$

$\frac{6.8}{50}$ $\frac{7.6}{33}$ $\frac{7.4}{22}$ $\frac{5.7}{13}$ $\frac{4.5}{10}$ $\frac{4.7}{10}$ $\frac{8.2}{16}$ $\frac{8.1}{50}$

$\frac{2.9}{50}$ $\frac{2.7}{33}$ $\frac{5.0}{31}$ $\frac{5.0}{24}$ $\frac{3.8}{22}$ $\frac{3.2}{13}$ $\frac{2.8}{12}$ $\frac{3.1}{20}$ $\frac{3.1}{50}$

$\frac{9.7}{50}$ $\frac{9.4}{33}$ $\frac{12.8}{30}$ $\frac{12.5}{23}$ $\frac{11.3}{15}$ $\frac{10.9}{9}$ $\frac{11.1}{9}$ $\frac{11.5}{11}$ $\frac{7.9}{15}$ $\frac{8.9}{50}$

$\frac{7.8}{50}$ $\frac{7.0}{32}$ $\frac{11.4}{30}$ $\frac{11.5}{23}$ $\frac{12.1}{18}$ $\frac{12.8}{11}$ $\frac{10.1}{11}$ $\frac{5.4}{18}$ $\frac{6.0}{50}$

$\frac{5.5}{50}$ $\frac{4.8}{30}$ $\frac{10.2}{29}$ $\frac{9.8}{21}$ $\frac{8.8}{17}$ $\frac{8.5}{12}$ $\frac{8.1}{11}$ $\frac{8.4}{11}$ $\frac{3.8}{19}$ $\frac{4.3}{25}$ $\frac{4.7}{50}$

Sta.	+	$\bar{x}$	-	Elev.
		910.38		
336				04.4.
B.M.			1.67	908.71
337				06.4.
+15				06.6.
+50				06.9.
T.P.	5.14	912.25	3.27	909.11
338				07.2.
+60				07.6.
339				07.9.
+50				07.4.
340				06.7.
+65				05.9.
341				05.5.

4.

E

RT.

$\frac{2.8}{50}$ $\frac{2.5}{29}$ $\frac{2.4}{27}$ $\frac{6.9}{18}$ $\frac{6.2}{13}$ $\frac{6.0}{12}$ $\frac{6.4}{12}$ $\frac{5.3}{13}$ $\frac{3.7}{18}$ $\frac{4.6}{26}$ $\frac{6.1}{50}$

U.S. & S. State Survey (Sta. T.8) Elev. conc. Brass (g/l)

$\frac{4.2}{50}$ $\frac{4.1}{24}$ $\frac{5.1}{23}$ $\frac{5.1}{17}$ $\frac{4.3}{15}$ $\frac{4.0}{14}$ $\frac{4.8}{13}$ $\frac{3.0}{19}$ $\frac{5.3}{50}$

$\frac{1.0}{50}$ $\frac{0.9}{25}$ $\frac{4.6}{22}$ $\frac{4.5}{26}$ $\frac{4.0}{14}$ $\frac{3.8}{25}$ $\frac{3.7}{25}$ $\frac{3.8}{50}$ $\frac{4.0}{100} = 2 \text{ rd.}$

$\frac{0.0}{50}$ $\frac{0.0}{25}$ $\frac{4.7}{23}$ $\frac{4.3}{17}$ $\frac{3.7}{15}$ $\frac{3.5}{14}$ $\frac{3.2}{24}$ $\frac{2.0}{50}$ $\frac{2.3}{50}$

$\frac{0.4}{50}$ $\frac{1.5}{25}$ $\frac{6.2}{24}$ $\frac{6.0}{17}$ $\frac{5.4}{15}$ $\frac{5.1}{14}$ $\frac{5.2}{15}$ $\frac{5.5}{22}$ $\frac{4.0}{23}$ $\frac{3.4}{46}$ $\frac{5.1}{47}$ $\frac{4.5}{60}$

$\frac{1.6}{50}$ $\frac{2.5}{25}$ $\frac{6.1}{24}$ $\frac{6.2}{17}$ $\frac{5.0}{15}$ $\frac{4.7}{14}$ $\frac{4.6}{11}$ $\frac{5.7}{15}$ $\frac{4.1}{25}$ $\frac{4.8}{25}$ $\frac{4.8}{25} - \text{Road } 50 = 2 \text{ rd.}$

$\frac{1.8}{50}$ $\frac{2.1}{36}$ $\frac{3.8}{26}$ $\frac{5.7}{24}$ $\frac{5.6}{17}$ $\frac{5.1}{15}$ $\frac{4.4}{14}$ $\frac{4.7}{16}$ $\frac{5.2}{28}$ $\frac{5.8}{28}$ $\frac{7.2}{41}$ $\frac{7.2}{50}$ $= \text{Ditch of Rd.}$

$\frac{2.0}{50}$ $\frac{2.4}{40}$ $\frac{4.3}{24}$ $\frac{5.8}{23}$ $\frac{6.2}{15}$ $\frac{5.1}{13}$ $\frac{4.9}{14}$ $\frac{6.0}{22}$ $\frac{7.5}{29}$ $\frac{7.6}{33}$ $\frac{4.4}{40}$ $\frac{4.4}{50}$

$\frac{3.3}{50}$ $\frac{5.2}{27}$ $\frac{6.9}{22}$ $\frac{6.9}{17}$ $\frac{5.5}{16}$ $\frac{5.6}{16}$ $\frac{6.6}{16}$ $\frac{8.3}{22}$ $\frac{7.3}{28}$ $\frac{8.2}{50}$

$\frac{6.2}{50}$ $\frac{7.7}{32}$ $\frac{8.0}{23}$ $\frac{7.7}{19}$ $\frac{6.9}{16}$ $\frac{6.4}{14}$ $\frac{7.3}{16}$ $\frac{11.1}{24}$ $\frac{12.2}{38}$ $\frac{12.6}{50}$

$\frac{9.8}{50}$ $\frac{10.8}{29}$ $\frac{9.5}{20}$ $\frac{7.6}{16}$ $\frac{6.8}{14}$ $\frac{7.6}{16}$ $\frac{12.7}{24}$ $\frac{12.8}{50}$

Sta.	+	π	-	Elev.
		912.25		
341+45				05.1.
342				04.7.
+55				04.3.
T.P.	2.64	906.57	832	903.93
343-				04.0.
+50				03.5.
344				02.9.
+60 ✓				02.5.
+66	2 Ditch			
345				01.5.
+50				00.6.
346				00.6.

Lt.

E

Rt.

$\frac{12.4}{50}$	$\frac{12.8}{38}$	$\frac{120}{24}$	$\frac{8.1}{15}$	7.2	$\frac{7.9}{15}$	$\frac{12.1}{25}$	$\frac{11.2}{50}$
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$\frac{12.7}{50}$	$\frac{13.5}{28}$	$\frac{8.5}{15}$	$\frac{1.6}{1}$	$\frac{8.2}{15}$	$\frac{11.1}{24}$	$\frac{11.1}{26}$	$\frac{10.6}{27}$	$\frac{10.0}{50}$
-------------------	-------------------	------------------	-----------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{10.7}{50}$	$\frac{10.4}{21}$	$\frac{8.7}{15}$	$\frac{8.0}{1}$	$\frac{8.5}{15}$	$\frac{9.9}{21}$	$\frac{10.0}{24}$	$\frac{8.3}{27}$	$\frac{8.1}{50}$
-------------------	-------------------	------------------	-----------------	------------------	------------------	-------------------	------------------	------------------

$\frac{3.8}{50}$	$\frac{3.8}{33}$	$\frac{4.4}{20}$	$\frac{3.1}{16}$	$\frac{3.6}{1}$	$\frac{3.0}{15}$	$\frac{3.7}{18}$	$\frac{5.0}{21}$	$\frac{5.1}{23}$	$\frac{4.3}{25}$	$\frac{4.7}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.8}{50}$	$\frac{3.3}{21}$	$\frac{3.8}{13}$	$\frac{3.1}{1}$	$\frac{3.6}{76}$	$\frac{6.8}{24}$	$\frac{6.8}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{6.6}{50}$	$\frac{6.0}{14}$	$\frac{4.3}{15}$	$\frac{3.7}{1}$	$\frac{4.3}{76}$	$\frac{7.2}{22}$	$\frac{7.8}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{7.5}{50}$	$\frac{7.3}{21}$	$\frac{4.6}{15}$	$\frac{4.1}{1}$	$\frac{4.8}{74}$	$\frac{7.5}{21}$	$\frac{7.8}{50}$
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$\frac{8.5}{100}$	$\frac{8.7}{50}$	Ditch	$\frac{8.0}{50}$	$\frac{8.2}{100}$
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$\frac{7.9}{50}$	$\frac{7.7}{20}$	$\frac{5.5}{15}$	$\frac{5.1}{1}$	$\frac{5.8}{13}$	$\frac{5.7}{21}$	$\frac{7.8}{21}$	$\frac{8.0}{33}$	$\frac{8.6}{34}$	$\frac{7.8}{35}$	$\frac{7.9}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.0}{50}$	$\frac{8.1}{22}$	$\frac{6.5}{16}$	6.0	$\frac{6.5}{16}$	$\frac{8.3}{21}$	$\frac{7.8}{31}$	$\frac{8.6}{32}$	$\frac{8.6}{34}$	$\frac{8.0}{34}$	$\frac{8.0}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.2}{50}$	$\frac{8.4}{30}$	$\frac{6.6}{16}$	$\frac{6.0}{1}$	$\frac{6.7}{17}$	$\frac{7.6}{19}$	$\frac{8.0}{31}$	$\frac{8.9}{31}$	$\frac{8.9}{33}$	$\frac{7.9}{34}$	$\frac{7.8}{50}$
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Sta.	+	π	-	Elev.
346+50		906.57		00.6

+58- in Ditch Left

347				01.6
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+60				02.2
-----	--	--	--	------

348				02.1
-----	--	--	--	------

+55				02.1
-----	--	--	--	------

349				02.2
-----	--	--	--	------

350				02.2
-----	--	--	--	------

+45				02.1
-----	--	--	--	------

351				02.1
-----	--	--	--	------

13.M.	6.45	911.00	2.02	904.55
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H. L. H.

$\frac{7.7}{50}$ $\frac{7.9}{20}$ $\frac{6.4}{15}$ $\frac{6.0}{16}$ $\frac{6.4}{20}$ $\frac{8.1}{20}$ $\frac{7.8}{31}$ $\frac{8.6}{32}$ $\frac{8.5}{33}$ $\frac{8.0}{34}$ $\frac{7.9}{50}$

$\frac{8.7}{100}$ $\frac{8.9}{50}$ in ditch

$\frac{7.6}{50}$ $\frac{7.5}{24}$ $\frac{8.0}{23}$ $\frac{8.0}{22}$ $\frac{7.6}{22}$ $\frac{5.9}{7.4}$ $\frac{5.0}{15}$ $\frac{5.6}{20}$ $\frac{7.6}{31}$ $\frac{7.7}{31}$ $\frac{8.3}{34}$ $\frac{8.0}{34}$ $\frac{7.9}{50}$

$\frac{6.0}{50}$ $\frac{6.7}{27}$ $\frac{7.3}{25}$ $\frac{7.5}{23}$ $\frac{7.1}{23}$ $\frac{5.3}{16}$ $\frac{4.4}{15}$ $\frac{5.1}{20}$ $\frac{6.9}{30}$ $\frac{7.2}{30}$ $\frac{7.8}{33}$ $\frac{7.3}{33}$ $\frac{7.3}{50}$

$\frac{3.9}{50}$ $\frac{5.8}{26}$ $\frac{2.3}{23}$ $\frac{2.3}{22}$ $\frac{6.5}{21}$ $\frac{5.2}{16}$ $\frac{4.5}{16}$ $\frac{5.0}{20}$ $\frac{6.5}{31}$ $\frac{7.2}{31}$ $\frac{7.6}{33}$ $\frac{7.2}{33}$ $\frac{7.2}{50}$

$\frac{3.8}{50}$ $\frac{3.9}{29}$ $\frac{6.3}{24}$ $\frac{6.5}{22}$ $\frac{6.5}{21}$ $\frac{5.3}{17}$ $\frac{4.5}{15}$ $\frac{4.8}{20}$ $\frac{6.7}{30}$ $\frac{7.0}{31}$ $\frac{7.3}{33}$ $\frac{7.0}{50}$

$\frac{2.4}{50}$ $\frac{4.2}{29}$ $\frac{6.9}{24}$ $\frac{6.9}{23}$ $\frac{6.1}{22}$ $\frac{4.8}{14}$ $\frac{4.4}{17}$ $\frac{4.7}{22}$ $\frac{6.4}{30}$ $\frac{6.8}{31}$ $\frac{7.4}{32}$ $\frac{6.9}{50}$

$\frac{4.9}{50}$ $\frac{6.1}{27}$ $\frac{7.1}{26}$ $\frac{7.1}{25}$ $\frac{6.4}{24}$ $\frac{4.9}{15}$ $\frac{4.4}{15}$ $\frac{5.2}{15}$ $\frac{7.0}{19}$ $\frac{7.3}{30}$ $\frac{7.7}{31}$ $\frac{7.7}{32}$ $\frac{7.4}{33}$ $\frac{7.3}{50}$

$\frac{5.9}{50}$ $\frac{6.8}{27}$ $\frac{7.2}{26}$ $\frac{7.2}{25}$ $\frac{6.8}{25}$ $\frac{5.4}{17}$ $\frac{4.5}{14}$ $\frac{5.3}{14}$ $\frac{7.4}{20}$ $\frac{7.5}{29}$ $\frac{7.8}{31}$ $\frac{7.5}{32}$ $\frac{7.3}{50}$

$\frac{6.1}{50}$ $\frac{6.8}{40}$ $\frac{6.9}{76}$ $\frac{7.4}{76}$ $\frac{7.4}{75}$ $\frac{6.9}{15}$ $\frac{4.5}{14}$ $\frac{5.3}{14}$ $\frac{7.0}{70}$ $\frac{7.1}{78}$ $\frac{7.5}{79}$ $\frac{7.5}{31}$ $\frac{7.2}{31}$ $\frac{6.5}{50}$

Spike in 24" Pop. 75 ft. str. 351+45

Sta.	+	7	-	Elev.
		911.00		
351 + 38				02.4.
+54				02.5.
+74				02.5.
352				02.4.
353				02.9.
354				04.2.
+55				05.2.
355				06.0.
	10.67	918.85	2.82	908.18
356				08.2.
+60				09.8.
357				10.7.

41. 2 21.

110 110 113 113 107 93 86 91 108 111 118 109 105
50 32 31 30 29 28 24 24 29 30 31 50

L.Rd. $\frac{88}{50}$ $\frac{8.7}{12}$ $\frac{85}{10}$ $\frac{8.9}{10}$ $\frac{7.8}{50}$ L.Rd.

118 118 111 9.0 85 8.8 10.7 11.0 11.4 11.0 10.0
50 31 23 17 14 14 28 29 31 50

11.7 11.5 9.4 86 8.9 11.0 10.5 9.7
50 21 16 14 20 41 50

11.9 11.6 8.9 81 8.4 10.2 10.3 9.3
50 22 16 14 19 31 50

11.4 10.8 10.2 7.9 6.8 7.1 8.1 7.7 5.6
50 26 20 15 13 19 29 50

9.6 8.3 7.8 6.4 5.8 5.9 7.1 7.5 4.2 2.0
50 27 20 21 13 18 23 28 50

7.6 5.2 6.5 6.4 5.5 5.0 5.4 6.7 6.5 0.4 4.5
50 25 23 17 14 15 19 23 32 50

7.9 7.5 1.25 1.26 11.2 10.7 11.3 12.4 11.4 4.2 3.7
50 30 24 19 15 15 17 21 31 50

6.2 5.3 10.9 11.1 9.8 9.1 9.6 10.7 10.7 1.7 1.0
50 31 24 18 15 12 17 19 32 50

6.2 5.7 1.4 1.4 8.9 8.2 8.7 12.0 10.0 2.8 2.2
50 30 23 21 16 13 18 20 32 50

Sta.	+	π	-	Elev.
		918.85		
55				11.9
358				12.9
359				15.0
360				17.4
T.P.	11.70	930.21	0.34	918.51
361				19.3
362				21.8
363				24.0
+54.8				25.1
B.M.			3.16	927.05
T.P. #51			3.84	926.37

Cold & Windy

40 Hb - Rec.
K. R. - Red
L. B. H. - Red
A. M. - Tape
L. B. - Tape
M. G. - Tape

H. E. RT

$\frac{72}{50}$ $\frac{66}{78}$ $\frac{92}{78}$ $\frac{92}{71}$ $\frac{77}{17}$ $\frac{70}{-}$ $\frac{73}{74}$ $\frac{88}{18}$ $\frac{87}{21}$ $\frac{52}{29}$ $\frac{61}{50}$

$\frac{70}{50}$ $\frac{70}{76}$ $\frac{82}{24}$ $\frac{82}{21}$ $\frac{66}{17}$ $\frac{60}{-}$ $\frac{62}{14}$ $\frac{73}{19}$ $\frac{23}{31}$ $\frac{65}{50}$

$\frac{42}{50}$ $\frac{48}{75}$ $\frac{56}{72}$ $\frac{45}{76}$ $\frac{39}{-}$ $\frac{41}{16}$ $\frac{5.8}{20}$ $\frac{5.9}{29}$ $\frac{61}{50}$

$\frac{1.6}{50}$ $\frac{2.1}{75}$ $\frac{3.3}{73}$ $\frac{2.1}{18}$ $\frac{15}{-}$ $\frac{1.8}{16}$ $\frac{3.1}{22}$ $\frac{3.5}{50}$

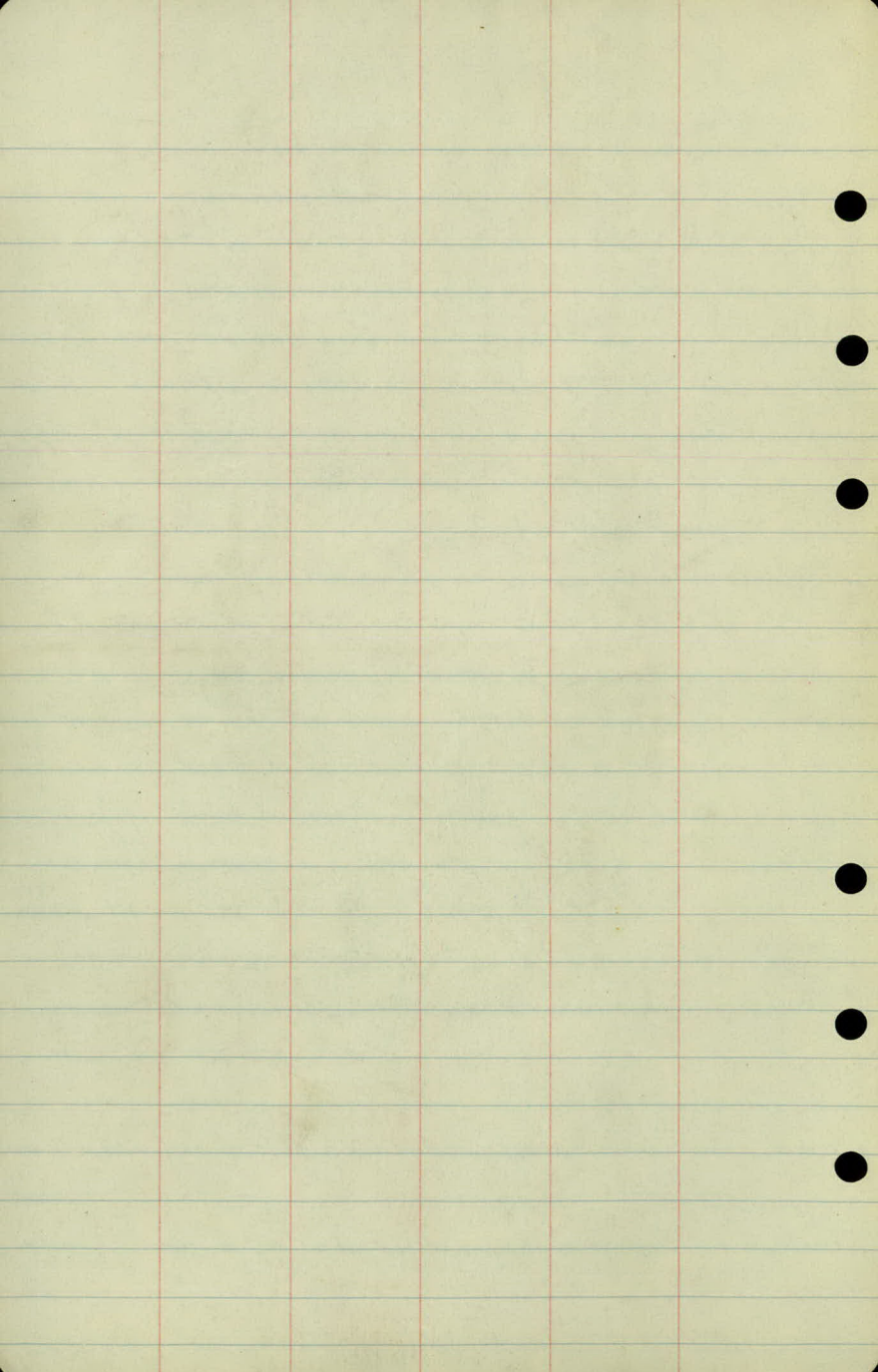
$\frac{12.1}{50}$ $\frac{12.5}{20}$ $\frac{11.4}{16}$ $\frac{10.9}{-}$ $\frac{11.3}{15}$ $\frac{13.0}{19}$ $\frac{12.9}{30}$ $\frac{12.5}{50}$

$\frac{10.1}{50}$ $\frac{10.0}{75}$ $\frac{10.6}{24}$ $\frac{9.0}{18}$ $\frac{8.4}{-}$ $\frac{8.5}{15}$ $\frac{10.1}{20}$ $\frac{9.9}{29}$ $\frac{9.8}{50}$

$\frac{6.0}{50}$ $\frac{6.2}{75}$ $\frac{8.1}{72}$ $\frac{6.9}{17}$ $\frac{6.2}{-}$ $\frac{6.2}{14}$ $\frac{2.9}{29}$ $\frac{2.1}{23}$ $\frac{6.6}{26}$ $\frac{7.3}{50}$

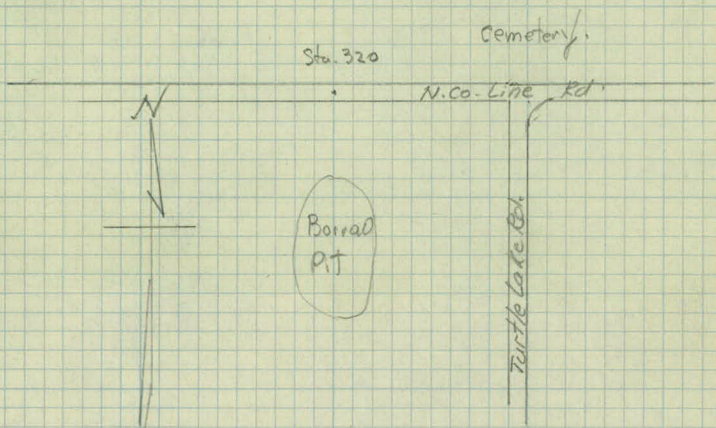
$\frac{4.7}{50}$ $\frac{4.6}{77}$ $\frac{6.6}{73}$ $\frac{6.8}{20}$ $\frac{5.6}{17}$ $\frac{5.1}{-}$ $\frac{5.4}{13}$ $\frac{6.7}{19}$ $\frac{6.7}{22}$ $\frac{3.3}{27}$ $\frac{4.1}{50}$

High Pt. Stone @ Fence Cor. 30' H. Sta. 363754.8
in P.P. at H. Sta. (51)

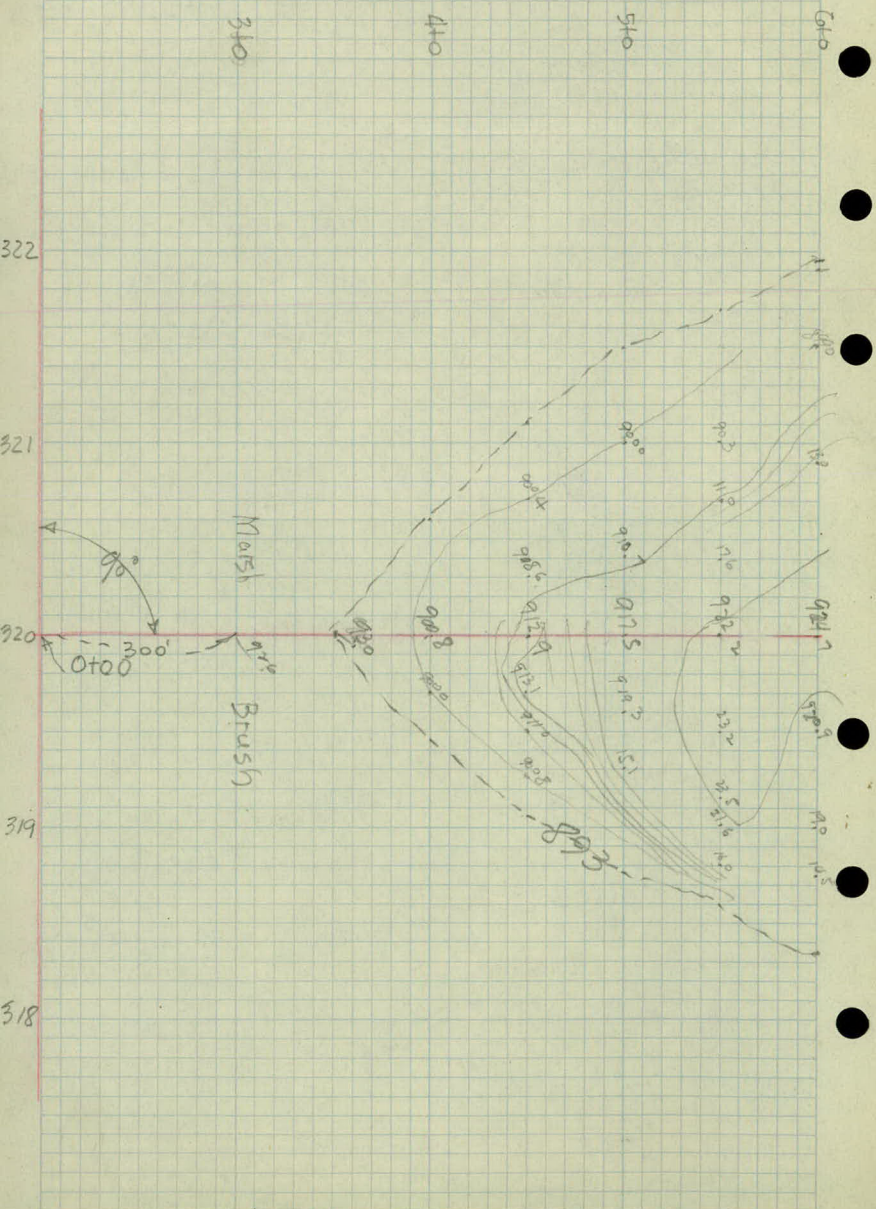


Proposed
Borrow Pit

South Sta. 320 - N. Co. Line Rd.



W. H. Carlson
Nov. 10, 1936

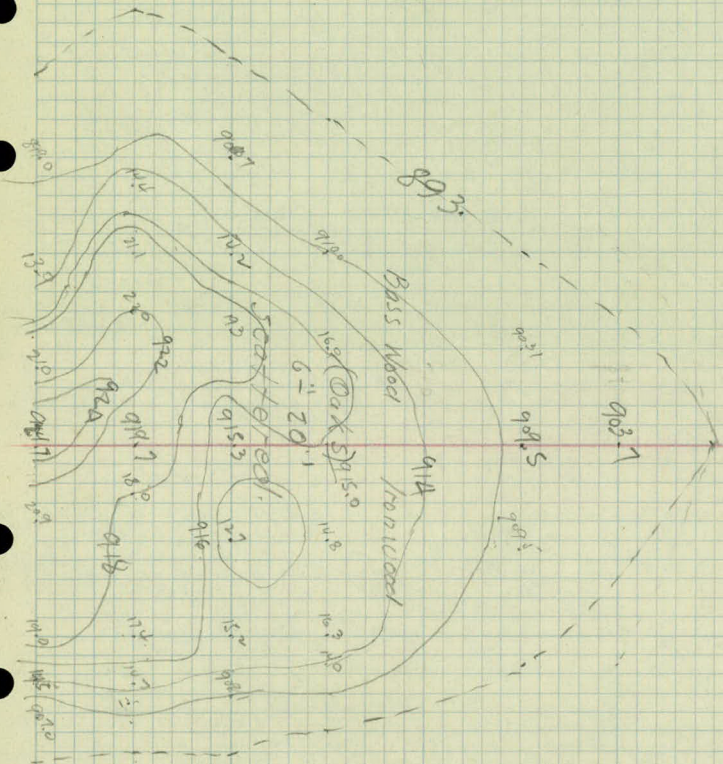


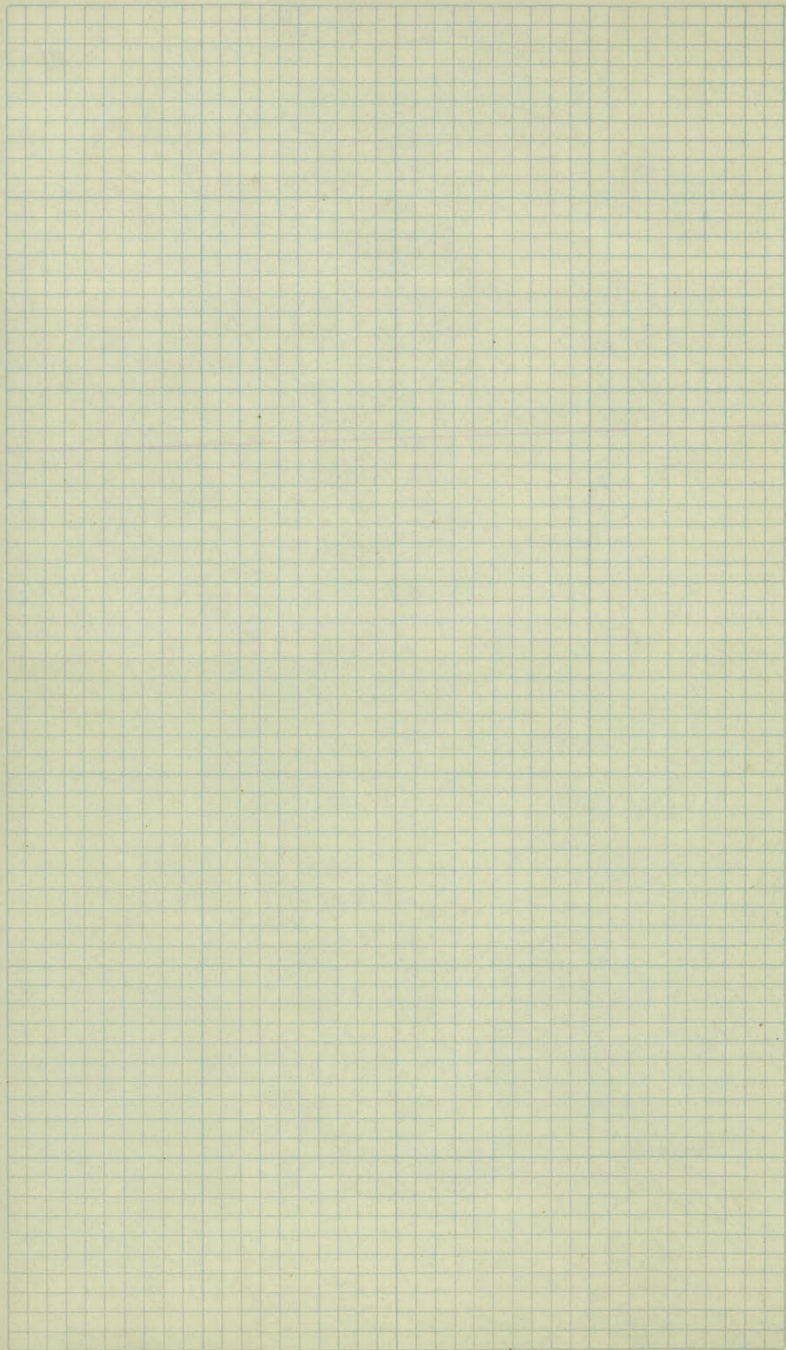
9+0

8+0

7+0

6+0





X-Section
Proposed Borrow Pit

Sta.	+	π	-	Elev.
	2.90	896.96		894.06

0+0 = 320+00 90° H.

5

1

2

3

91.4

T.P.	5.39	897.73	4.62	892.34
------	------	--------	------	--------

3+60				893.0
------	--	--	--	-------

T.P.	12.22	909.44	0.51	897.22
------	-------	--------	------	--------

4+0				00.8
-----	--	--	--	------

T.P.	13.14	920.78	1.80	907.64
------	-------	--------	------	--------

4+50				12.9
------	--	--	--	------

5+0				17.5
-----	--	--	--	------

T.P.	10.38	930.08	1.08	919.70
------	-------	--------	------	--------

5+50				22.2
------	--	--	--	------

✓ 6+0				24.7
-------	--	--	--	------

6+50				19.7
------	--	--	--	------

T.P.	1.79	922.09	9.78	920.30
------	------	--------	------	--------

7+0				15.3
-----	--	--	--	------

7+50				14.9
------	--	--	--	------

8+50				09.5
------	--	--	--	------

9+00				903.7
------	--	--	--	-------

0+40

East

Z

West

5.2

6.1

5.4

$$\frac{5.6}{100}$$

5.6

$$\frac{5.6}{100}$$

893.0

$$\frac{6.2}{100}$$

$$\frac{4.7}{0}$$

$$\frac{6.8}{100}$$

$$\frac{893.0}{60}$$

$$\frac{8.6}{-}$$

$$\frac{9.5}{30} \quad \frac{893.0}{55}$$

$$\frac{893.0}{110}$$

$$\frac{20.4}{70}$$

$$\frac{12.2}{30}$$

$$\frac{7.9}{-}$$

$$\frac{7.7}{30}$$

$$\frac{9.8}{47}$$

$$\frac{20.0}{75}$$

$$\frac{893.0}{95}$$

$$\frac{893.0}{150}$$

$$\frac{20.8}{100}$$

$$\frac{10.1}{40}$$

$$\frac{3.3}{-}$$

$$\frac{1.5}{40}$$

$$\frac{5.7}{70}$$

$$\frac{893.0}{125}$$

$$\frac{893.0}{170}$$

$$\frac{27.0}{100}$$

$$\frac{19.0}{70}$$

$$\frac{13.4}{40}$$

$$\frac{7.9}{-}$$

$$\frac{6.9}{50}$$

$$\frac{6.6}{85}$$

$$\frac{8.5}{100}$$

$$\frac{14.0}{120}$$

$$\frac{893.0}{146}$$

$$\frac{893.0}{195}$$

$$\frac{31.0}{150}$$

$$\frac{17.0}{90}$$

$$\frac{9.0}{40}$$

$$\frac{5.4}{-}$$

$$\frac{9.2}{50}$$

$$\frac{11.2}{100}$$

$$\frac{15.5}{125}$$

$$\frac{23.0}{142}$$

$$\frac{893.0}{165}$$

$$\frac{893.0}{225}$$

$$\frac{45.7}{145}$$

$$\frac{9.0}{100}$$

$$\frac{8.1}{70}$$

$$\frac{10.4}{-}$$

$$\frac{12.1}{75}$$

$$\frac{12.7}{100}$$

$$\frac{15.4}{125}$$

$$\frac{893.0}{160}$$

$$\frac{893.0}{200}$$

$$\frac{18.4}{150}$$

$$\frac{7.9}{100}$$

$$\frac{2.8}{60}$$

$$\frac{6.8}{-}$$

$$\frac{9.4}{50}$$

$$\frac{6.9}{100}$$

$$\frac{13.0}{130}$$

$$\frac{893.0}{160}$$

$$\frac{893.0}{170}$$

$$\frac{12.3}{100}$$

$$\frac{6.3}{50}$$

$$\frac{7.2}{-}$$

$$\frac{7.8}{50}$$

$$\frac{5.8}{100}$$

$$\frac{8.2}{115}$$

$$\frac{893.0}{150}$$

$$\frac{893.0}{100}$$

$$\frac{19.0}{50}$$

$$\frac{12.6}{-}$$

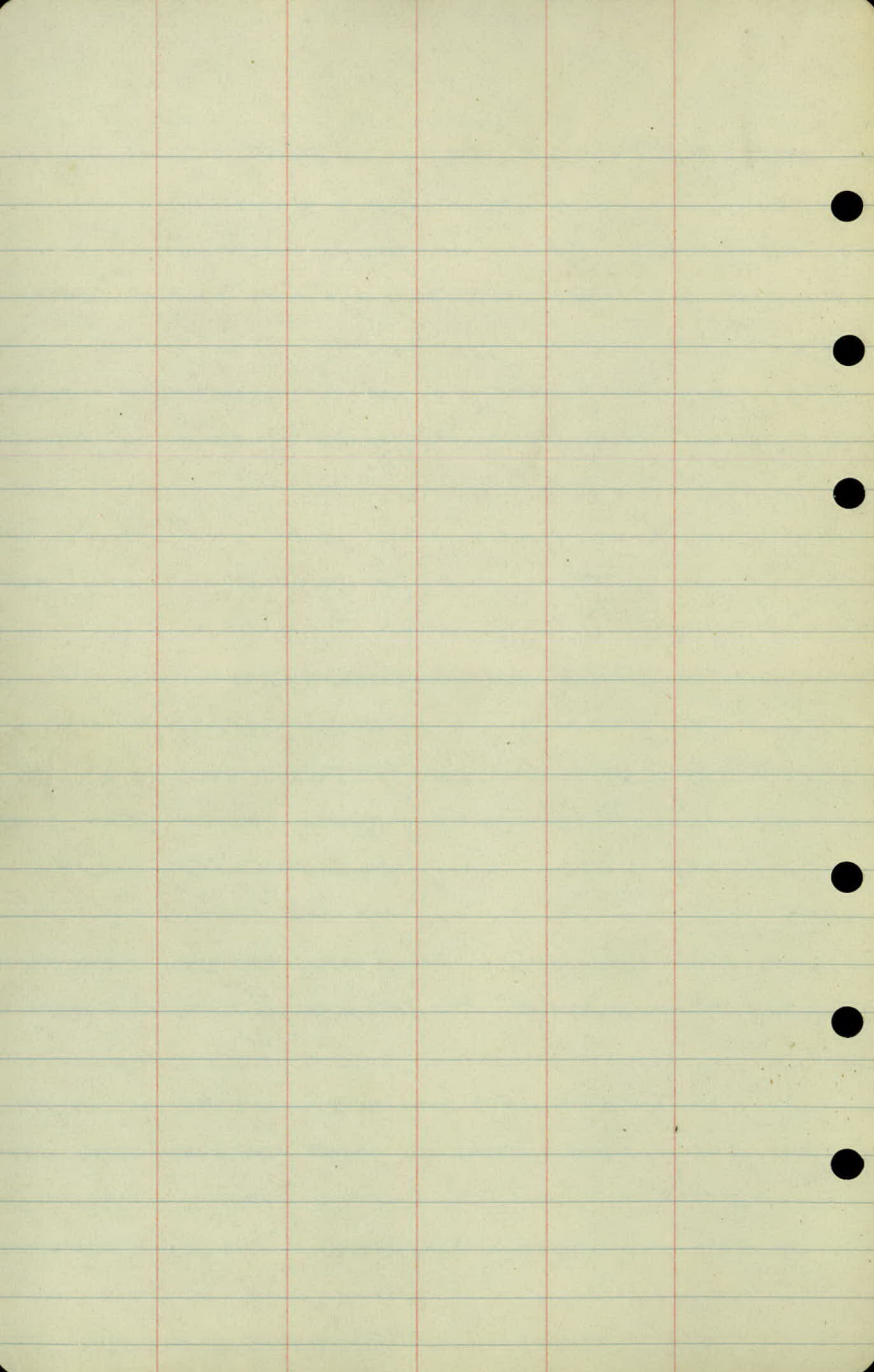
$$\frac{12.3}{55}$$

$$\frac{12.3}{90}$$

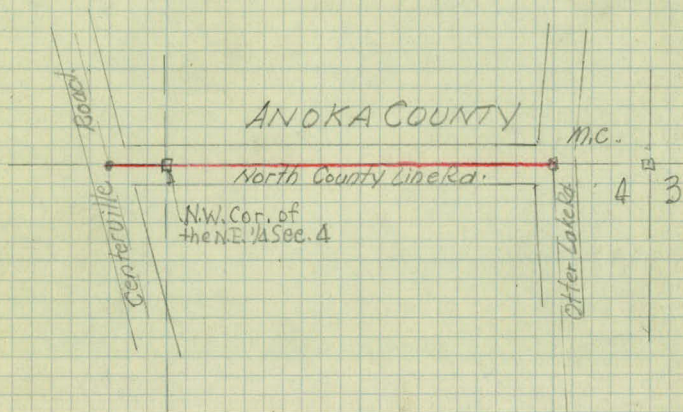
$$\frac{893.0}{115}$$

18.4

Elev. 892.7



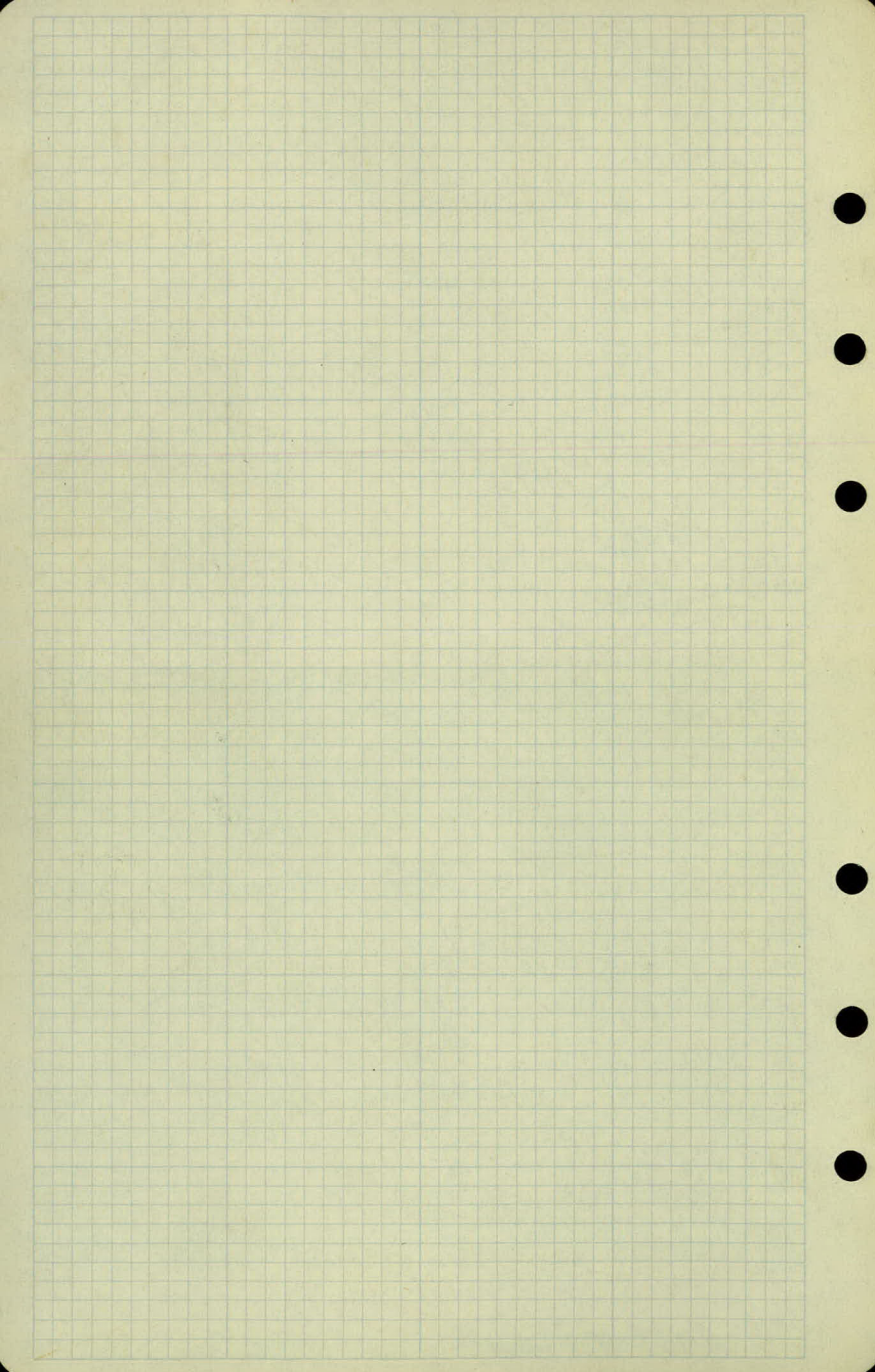
Plan Survey
 North County Line Road
 Centerville Rd. to Otter Lake Rd.



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W. H. Carlson
 Nov. 19, 1936



alignment

N. County Line

Centerville Rd. to Otter Lake Rd.

Station Point angle.
 Lt Rt.

470+70.6 N. C.

470+50.6 P.I. =
 Sta. 225+67.96
 Offset 6 to R.

468+83.81 P.O.T. = (P.T. 226+58.57 Offset 6 to R.)

465+85.95 P.O.T.

448+53.65 P.I. MOD.

0°-57'

447+57.6

Computed Stationing.

(363+54.8 = 2840.1)

363+54.8
 84402.8
 447+57.6

Otter Lake Rd. P.I.
Sta. 220+98.82

W. H. Carlson

K. Anker

L. B. Hendrix

A. Moeschter

Nov. 19, 1936

M.C.

200

Boat Spike

to Otter Lake as Loc. Oct. 1936

92.00

Boat Spike.

Stone Mon.

P. 7P.

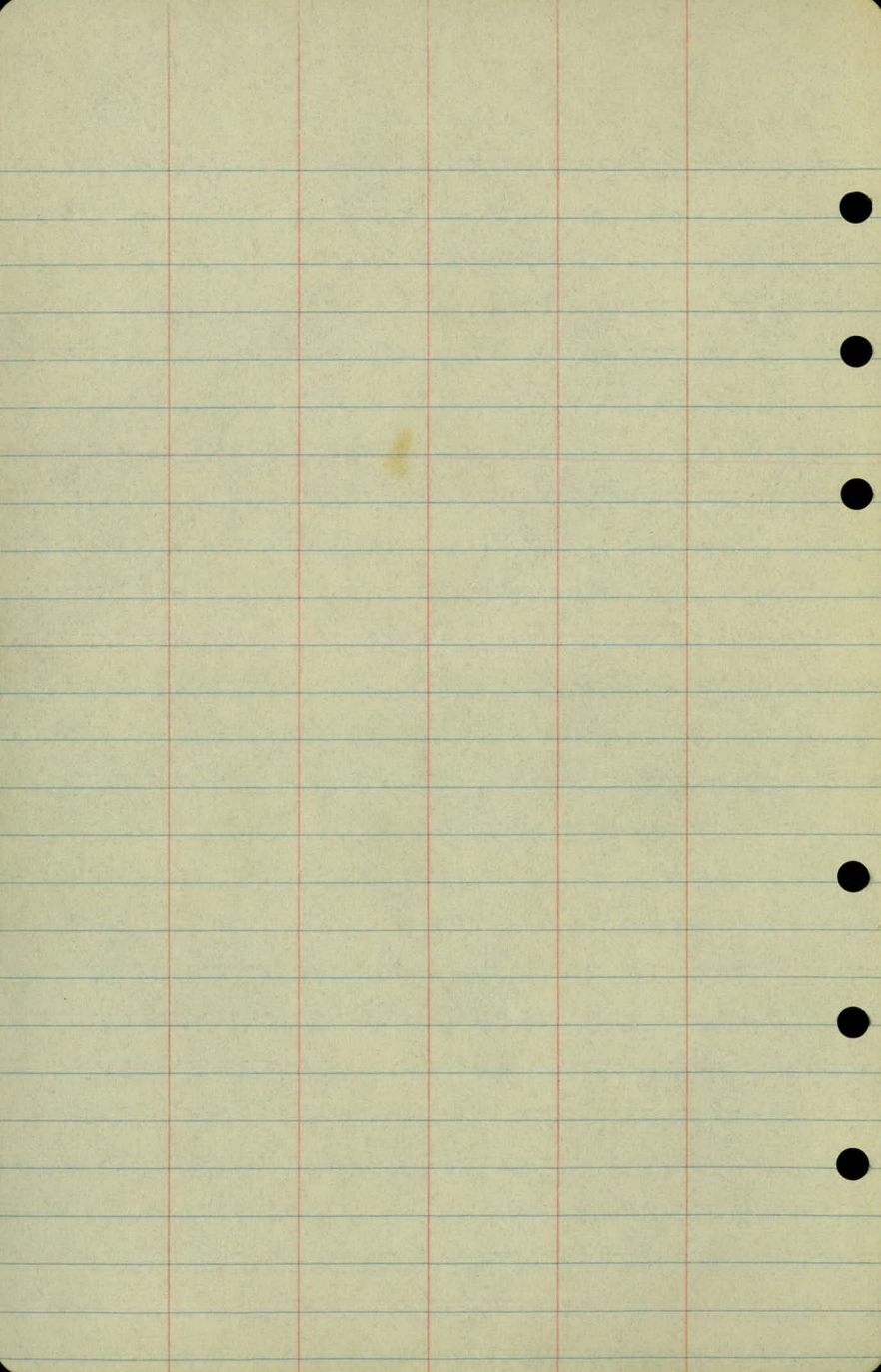
53.65

Boat Spike

Centerville Rd.

27.8

Spike in Tree



Topography
No. Co. Line
centerville Rd to Otter Lk Rd.

451

13

13

450

12

12

449 ^{+09.88-23'}

12'

11'

+53 12'

11'

448

12'

12'

+80

17'

37' + 20

+57.6 ²/₅ Centerville Rd. 41'

41'

447

F-28'

F-24'

+78 F Cor. 24'

F-28'

Cult.

Cult.

F 23'

+53 F 27'

+53 F 24'

+02 T.P. 29'
+01 Bsq. 22'

+80 F Cor. 22'

Centerville Rd.

11

12

+57-PP-26'

458 Fc-26'

11

12

457

12

15

456 Bcs-Fc-27'

14

16

+35-PP-27'

shoulder

455

13

16

454

14'

15'

+80-End Fc-26'

453

14'

14'

+48 E 12" X 40' C.M. OK.

20'

20'

+22-PP-25'

452

~~F-6~~

~~F-6~~

~~F-17~~

~~F-19~~

~~F-9~~



Cult.

X X X - F-43 - F-44 - 23

F-24

Cult.

Cult.

F-25

F-24

X X 70

F-21

Meadow

Meadow

172-Fc Cor.-28'

11-11

465

175-RR-28'

11-11

464 Fc-27'

12-11

463

12-12

120-2-15"X40'CM.
BK.

(21-23')

462 Fc-27'

12-12

+72-PP-27'

461

12-12

460 Fc-27'

12-12

459 Fc

~~186-F. cor. 21~~

~~F-20~~

~~F-20~~

~~F-20~~

~~F-19~~

~~F-18~~

~~F-17~~

~~190~~

Meadow

Cult.

Scattered oaks - pasture

F-19

F-20

191-F. cor. 22

F-22

F-22

Cult.

+70.6 Meander Cor.

+50.6 = $\pm$ Otter Lake Rd.

(Per. Survey Oct 1936)

470

7- N

10 x 80

469

10-10

468

10-10

467

+20. P.P. - 27'

12-11

466

See Otter Lake Survey
of Oct. 1936 and
Nov. 1936

W.
+05-End. culv. 25'

+93-A in F. 19'

Pasture.

+90-N.E. Cor.
+12-F. Cor. 19'



+49-N.E. Cor. Burd. 94'
+40-E. S. 10'

F-73'

Wasteland

+12-Box
at

+70-N.E. Cor. Gen 94'

+76-N.W. Cor. Carr 96'
+21-N.W. Cor. Gen-97'



+06-8" Box. 76'

F-73

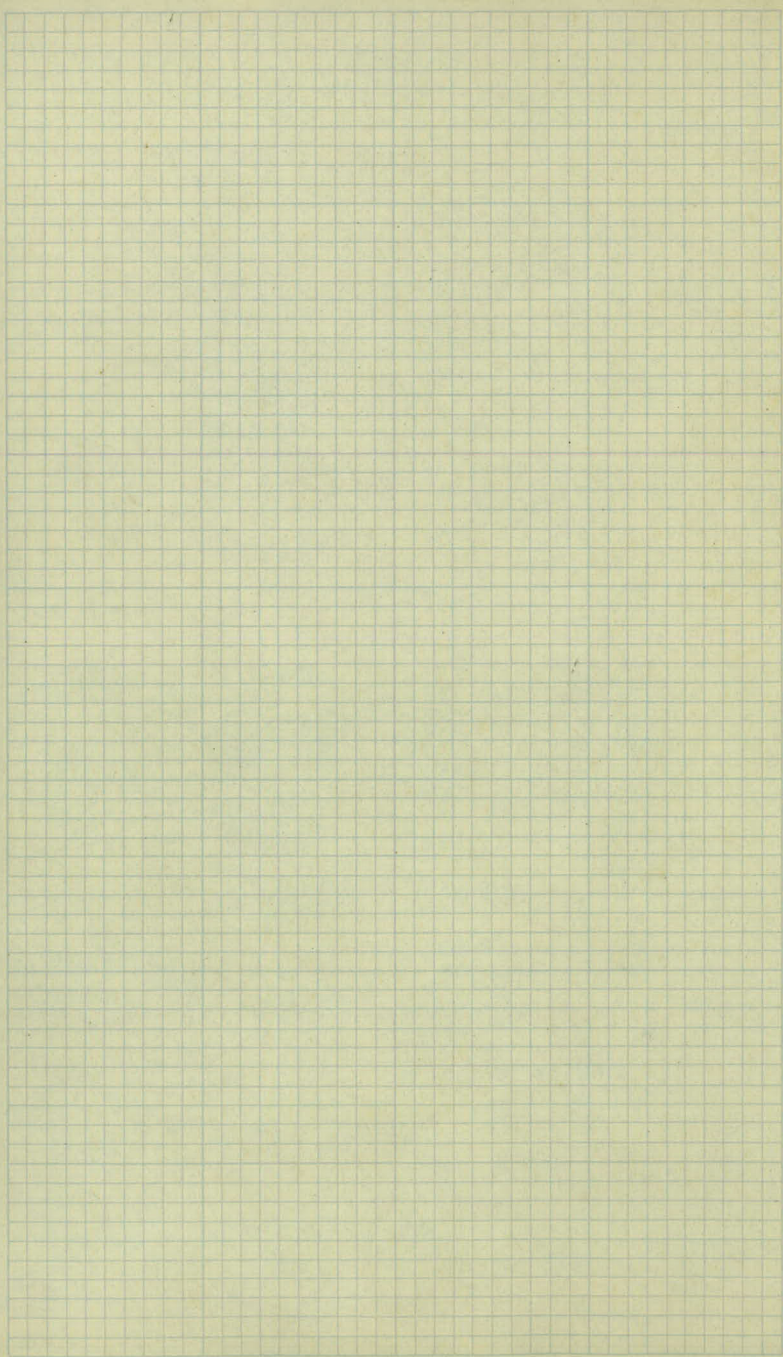
+91-15" Box. 24'

+53-F. Cor. 23'

+01-End 8' 12"

+26-End 12' 8" 76' C.M.

+29-F. Cor. 24'



Cross Sect
No Co Line Rd
Centerville Rd
To
Otter Lake Rd No

Sta.	+	Σ	-	Elev.
B.M	2.99	935.92		932.93

447+57 ⁶⁰		Centerville Rd.		32.5
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+47				32.0
-----	--	--	--	------

448				31.6
-----	--	--	--	------

+53 ⁶⁵		4.5 hp	Mont	31.5
-------------------	--	--------	------	------

449				31.5
-----	--	--	--	------

+50				31.1
-----	--	--	--	------

450				30.5
-----	--	--	--	------

+50				29.9
-----	--	--	--	------

451				28.9
-----	--	--	--	------

+50				28.5
-----	--	--	--	------

452				28.2
-----	--	--	--	------

+48		12" C.M.P.		
-----	--	------------	--	--

+50				28.4
-----	--	--	--	------

T.P.	9.15	937.39	7.68	928.24
------	------	--------	------	--------

Lt.

E

Rt.

Spt. in 18" B.E. S.W. Cor Cent. & No Poline

$\frac{3.9}{100}$ $\frac{3.8}{50}$ 3.4 $\frac{3.6}{50}$ $\frac{3.8}{100}$

$\frac{5.7}{50}$ $\frac{5.2}{40}$ $\frac{6.3}{25}$ $\frac{5.5}{21}$ 3.9 $\frac{4.3}{18}$ $\frac{5.4}{28}$ $\frac{6.3}{34}$ $\frac{6.3}{50}$

$\frac{5.7}{33}$ $\frac{5.7}{29}$ $\frac{6.6}{23}$ $\frac{6.0}{17}$ $\frac{5.0}{13}$ 4.3 $\frac{5.2}{16}$ $\frac{6.3}{19}$ $\frac{6.6}{25}$ $\frac{6.0}{30}$ $\frac{6.1}{33}$

$\frac{5.7}{33}$ $\frac{5.4}{28}$ $\frac{6.3}{25}$ $\frac{6.3}{20}$ $\frac{4.8}{14}$ 4.4 $\frac{5.6}{16}$ $\frac{6.7}{19}$ $\frac{6.8}{24}$ $\frac{6.3}{33}$

$\frac{5.0}{33}$ $\frac{5.2}{29}$ $\frac{6.3}{24}$ $\frac{6.2}{20}$ $\frac{6.2}{15}$ 4.4 $\frac{5.1}{12}$ $\frac{6.8}{18}$ $\frac{6.5}{24}$ $\frac{6.1}{33}$

$\frac{5.7}{33}$ $\frac{5.7}{29}$ $\frac{6.7}{24}$ $\frac{6.8}{18}$ $\frac{5.4}{13}$ 4.8 $\frac{5.4}{13}$ $\frac{7.0}{19}$ $\frac{6.6}{29}$ $\frac{6.3}{33}$

$\frac{6.6}{33}$ $\frac{6.7}{26}$ $\frac{7.9}{25}$ $\frac{7.7}{18}$ $\frac{6.1}{13}$ 5.4 $\frac{6.1}{13}$ $\frac{7.5}{18}$ $\frac{7.5}{24}$ $\frac{7.4}{33}$

$\frac{8.0}{33}$ $\frac{8.0}{27}$ $\frac{8.7}{25}$ $\frac{8.7}{19}$ $\frac{6.6}{14}$ 6.0 $\frac{6.9}{13}$ $\frac{8.4}{18}$ $\frac{8.6}{25}$ $\frac{8.3}{33}$

$\frac{8.8}{33}$ $\frac{8.8}{26}$ $\frac{10.0}{24}$ $\frac{10.0}{19}$ $\frac{7.7}{14}$ 7.0 $\frac{7.6}{14}$ $\frac{9.4}{19}$ $\frac{9.7}{26}$ $\frac{9.2}{33}$

$\frac{9.6}{33}$ $\frac{9.7}{26}$ $\frac{10.4}{25}$ $\frac{10.4}{20}$ $\frac{8.2}{15}$ 7.4 $\frac{8.4}{15}$ $\frac{9.9}{19}$ $\frac{10.2}{25}$ $\frac{9.5}{27}$ $\frac{9.5}{33}$

$\frac{10.0}{33}$ $\frac{10.0}{26}$ $\frac{10.6}{25}$ $\frac{10.5}{19}$ $\frac{8.4}{14}$ 7.7 $\frac{8.5}{15}$ $\frac{10.5}{19}$ $\frac{10.7}{25}$ $\frac{10.2}{26}$ $\frac{10.2}{33}$

$\frac{9.8}{33}$ $\frac{9.8}{27}$ $\frac{10.8}{25}$ $\frac{10.7}{22}$ $\frac{10.3}{19}$ $\frac{8.3}{16}$ 7.5 $\frac{8.1}{16}$ $\frac{10.6}{21}$ $\frac{10.7}{26}$ $\frac{10.2}{30}$ $\frac{10.2}{33}$

Sta.	+	K _v	-	Elev.
		937.39		

453				28.8
-----	--	--	--	------

+50				29.6
-----	--	--	--	------

454				30.5
-----	--	--	--	------

+50				31.1
-----	--	--	--	------

455				31.9
-----	--	--	--	------

+50				32.6
-----	--	--	--	------

456				33.6
-----	--	--	--	------

+50				34.7
-----	--	--	--	------

457				35.5
-----	--	--	--	------

T. P.	5.45	✓ 941.33	1.57	✓ 935.88
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+50				35.9
-----	--	--	--	------

458				36.4
-----	--	--	--	------

+50				36.5
-----	--	--	--	------

Lt.

E

Rt.

$$\frac{11.3}{33} \frac{11.1}{26} \frac{12.0}{24} \frac{12.4}{22} \frac{11.6}{19} \frac{9.4}{15} 8.6 \frac{9.3}{14} \frac{11.5}{19} \frac{11.7}{24} \frac{11.2}{27} \frac{11.2}{33}$$

$$\frac{10.8}{33} \frac{10.6}{27} \frac{11.4}{26} \frac{10.7}{19} \frac{8.6}{15} 7.8 \frac{8.5}{15} \frac{10.6}{21} \frac{10.4}{33}$$

$$\frac{9.7}{33} \frac{10.0}{20} \frac{7.4}{14} 6.9 \frac{7.2}{16} \frac{9.9}{21} \frac{9.8}{33}$$

$$\frac{8.7}{33} \frac{8.7}{19} \frac{6.7}{13} 6.3 \frac{6.5}{16} \frac{8.2}{20} \frac{8.5}{23} \frac{8.6}{29} \frac{8.6}{33}$$

$$\frac{7.0}{33} \frac{7.4}{18} \frac{6.2}{13} 5.5 \frac{5.8}{16} \frac{7.5}{21} \frac{7.5}{27} \frac{7.3}{33}$$

$$\frac{5.7}{33} \frac{6.3}{17} \frac{5.3}{13} 4.8 \frac{5.3}{16} \frac{6.7}{20} \frac{6.4}{27} \frac{6.0}{33}$$

$$\frac{4.8}{33} \frac{5.4}{18} \frac{4.3}{12} 3.8 \frac{4.0}{16} \frac{5.3}{19} \frac{5.2}{22} \frac{4.7}{25} \frac{4.2}{33}$$

$$\frac{4.0}{33} \frac{2.9}{16} \frac{3.3}{12} 2.7 \frac{2.7}{17} \frac{3.6}{19} \frac{3.5}{22} \frac{3.2}{24} \frac{3.1}{27} \frac{2.7}{33}$$

$$\frac{1.9}{33} \frac{2.3}{11} 1.9 \frac{2.4}{15} \frac{2.8}{17} \frac{2.8}{18} \frac{1.2}{22} \frac{1.3}{33}$$

$$\frac{4.6}{33} \frac{5.1}{17} \frac{5.7}{11} 5.4 \frac{6.0}{11} \frac{5.7}{14} \frac{5.8}{18} \frac{2.9}{21} \frac{2.7}{33}$$

$$\frac{3.7}{33} \frac{4.0}{21} \frac{4.4}{15} \frac{5.2}{11} 4.9 \frac{5.4}{10} \frac{5.1}{12} \frac{5.0}{16} \frac{1.6}{21} \frac{1.3}{33}$$

$$\frac{3.6}{33} \frac{4.3}{16} \frac{5.2}{12} 4.8 \frac{5.0}{16} \frac{1.0}{21} \frac{1.0}{33}$$

Sta	+	π ✓	-	Elev
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459		941.33		36.3
-----	--	--------	--	------

+50				36.3
-----	--	--	--	------

460				36.3
-----	--	--	--	------

+50				35.9
-----	--	--	--	------

461				35.4
-----	--	--	--	------

+50				34.9
-----	--	--	--	------

462				35.1
-----	--	--	--	------

+25		15" C.M.P		
-----	--	-----------	--	--

+50				35.8
-----	--	--	--	------

463				37.9
-----	--	--	--	------

+50		✓		42.3
-----	--	---	--	------

T.P.	13.74	954.62	0.45	940.88 ✓
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464				43.2
-----	--	--	--	------

+50				46.0
-----	--	--	--	------

LA & RT

$$\frac{4.6}{33} \quad \frac{5.0}{16} \quad \frac{5.4}{12} \quad 5.0 \quad \frac{5.5}{11} \quad \frac{4.9}{17} \quad \frac{1.7}{21} \quad \frac{1.0}{33}$$

$$\frac{5.5}{33} \quad \frac{5.1}{14} \quad \frac{5.6}{12} \quad 5.0 \quad \frac{5.3}{11} \quad \frac{5.0}{17} \quad \frac{1.8}{21} \quad \frac{1.3}{33}$$

$$\frac{6.2}{33} \quad \frac{5.4}{20} \quad \frac{6.0}{17} \quad \frac{5.6}{12} \quad 5.0 \quad \frac{5.4}{17} \quad \frac{2.3}{20} \quad \frac{1.7}{33}$$

$$\frac{8.0}{33} \quad \frac{7.1}{17} \quad \frac{6.1}{13} \quad 5.4 \quad \frac{5.2}{15} \quad \frac{5.9}{16} \quad \frac{5.8}{18} \quad \frac{4.1}{21} \quad \frac{3.5}{33}$$

$$\frac{9.7}{33} \quad \frac{8.6}{18} \quad \frac{6.5}{13} \quad 5.9 \quad \frac{5.8}{16} \quad \frac{7.0}{18} \quad \frac{7.0}{20} \quad \frac{6.2}{22} \quad \frac{5.8}{23}$$

$$\frac{10.5}{33} \quad \frac{9.7}{20} \quad \frac{7.2}{15} \quad 6.4 \quad \frac{6.4}{16} \quad \frac{8.1}{19} \quad \frac{8.2}{24} \quad \frac{8.2}{33}$$

$$\frac{10.7}{33} \quad \frac{10.1}{21} \quad \frac{7.1}{15} \quad \frac{6.6}{13} \quad 6.2 \quad \frac{6.7}{15} \quad \frac{9.4}{20} \quad \frac{9.8}{26} \quad \frac{9.8}{33}$$

$$\frac{9.4}{33} \quad \frac{9.4}{29} \quad \frac{8.8}{22} \quad \frac{5.8}{8} \quad 5.5 \quad \frac{6.0}{19} \quad \frac{9.9}{22} \quad \frac{10.7}{26} \quad \frac{10.7}{33}$$

$$\frac{6.4}{33} \quad \frac{6.2}{21} \quad \frac{3.3}{18} \quad \frac{9.4}{Inv} \quad 3.4 \quad \frac{3.9}{16} \quad \frac{8.5}{23} \quad \frac{8.5}{33}$$

$$\frac{4.0}{33} \quad \frac{3.7}{22} \quad \frac{1.4}{18} \quad 1.0 \quad \frac{1.9}{14} \quad \frac{6.4}{21} \quad \frac{6.4}{33}$$

$$\frac{13.2}{33} \quad \frac{13.2}{21} \quad \frac{11.6}{18} \quad 11.4 \quad \frac{12.2}{12} \quad \frac{15.3}{17} \quad \frac{15.6}{33}$$

$$\frac{8.4}{50} \quad \frac{8.8}{13} \quad \frac{9.2}{11} \quad 8.6 \quad \frac{9.5}{15} \quad \frac{10.5}{17} \quad \frac{10.7}{21} \quad \frac{13.3}{50}$$

Sta	+	π	$\checkmark$	-	Elev
					954.62 $\checkmark$
465			$\checkmark$		47.6 $\checkmark$
B.M	1.10	954.62	1.10		953.52
+50					48.1

466					47.8
+50					46.7

467			$\checkmark$		44.8 $\checkmark$
T.P	6.12	952.60	8.14		946.48
+50					42.4

+71					41.2
468					39.1

+50

T.P		$\checkmark$			$\checkmark$
T.P	0.17	939.68	13.09		939.51

468

+50

35.5

(468 + 83.91
 2226 + 58.37 - other lake Survey Nov. 1936

469

32.1

LT 2 RT

$$\frac{3.0}{50} \frac{3.2}{19} \frac{7.4}{14} 7.0 \frac{7.5}{13} \frac{5.4}{16} \frac{6.7}{39} \frac{9.5}{50}$$

#C24 U.S.G.S 22' L1 519 405+49

$$\frac{3.8}{50} \frac{2.8}{43} \frac{1.4}{19} \frac{7.2}{11} 6.5 \frac{7.0}{13} \frac{2.3}{18} \frac{5.2}{50} \frac{12.5}{100} \frac{15.2}{125} \frac{17.7}{150}$$

$$\frac{4.8}{50} \frac{3.8}{31} \frac{2.8}{20} \frac{7.4}{14} 6.8 \frac{7.3}{13} \frac{1.9}{18} \frac{2.7}{50} \frac{5.6}{100} \frac{9.0}{150} \frac{11.9}{200} \frac{16.7}{250} \frac{19.4}{300}$$

$$\frac{6.3}{50} \frac{4.0}{19} \frac{8.6}{14} 7.9 \frac{7.8}{15} \frac{2.9}{20} \frac{2.5}{50} \frac{3.7}{100} \frac{2.6}{150} \frac{5.3}{212} \frac{8.8}{223} \frac{12.4}{250}$$

$$\frac{11.0}{50} \frac{8.4}{27} \frac{7.0}{20} \frac{10.6}{18} 9.8 \frac{10.3}{11} \frac{9.8}{16} \frac{4.5}{21} \frac{6.2}{50} \frac{5.8}{82} \frac{2.8}{106} \frac{1.1}{160} \frac{2.9}{200}$$

$$\frac{13.8}{50} \frac{10.1}{25} \frac{8.2}{20} \frac{11.1}{15} 10.2 \frac{10.5}{15} \frac{3.4}{23} \frac{3.0}{50} \frac{3.7}{100} \frac{11.0}{250} \frac{7.6}{243} \frac{1.1}{12. \text{Gang}}$$

$$\frac{16.5}{50} \frac{13.7}{25} \frac{12.0}{21} \frac{12.4}{12} 11.4 \frac{11.9}{17} \frac{6.7}{22} \frac{4.8}{29} \frac{3.9}{50} \frac{2.9}{100}$$

$$\frac{13.6}{135} \frac{9.7}{18} \frac{8.3}{22} \frac{7.2}{34} \frac{6.3}{37} \frac{4.7}{50} \frac{4.7}{100}$$

$$(17.1) \frac{17.4}{9} \frac{16.4}{16} \frac{14.4}{19} \frac{13.4}{32} \frac{11.8}{36} \frac{10.3}{50} \frac{6.9}{100}$$

$$\frac{7.5}{50} \frac{5.1}{23} \frac{1.4}{17} (0.6)$$

$$\frac{11.9}{50} \frac{9.5}{23} \frac{5.1}{15} 4.2$$

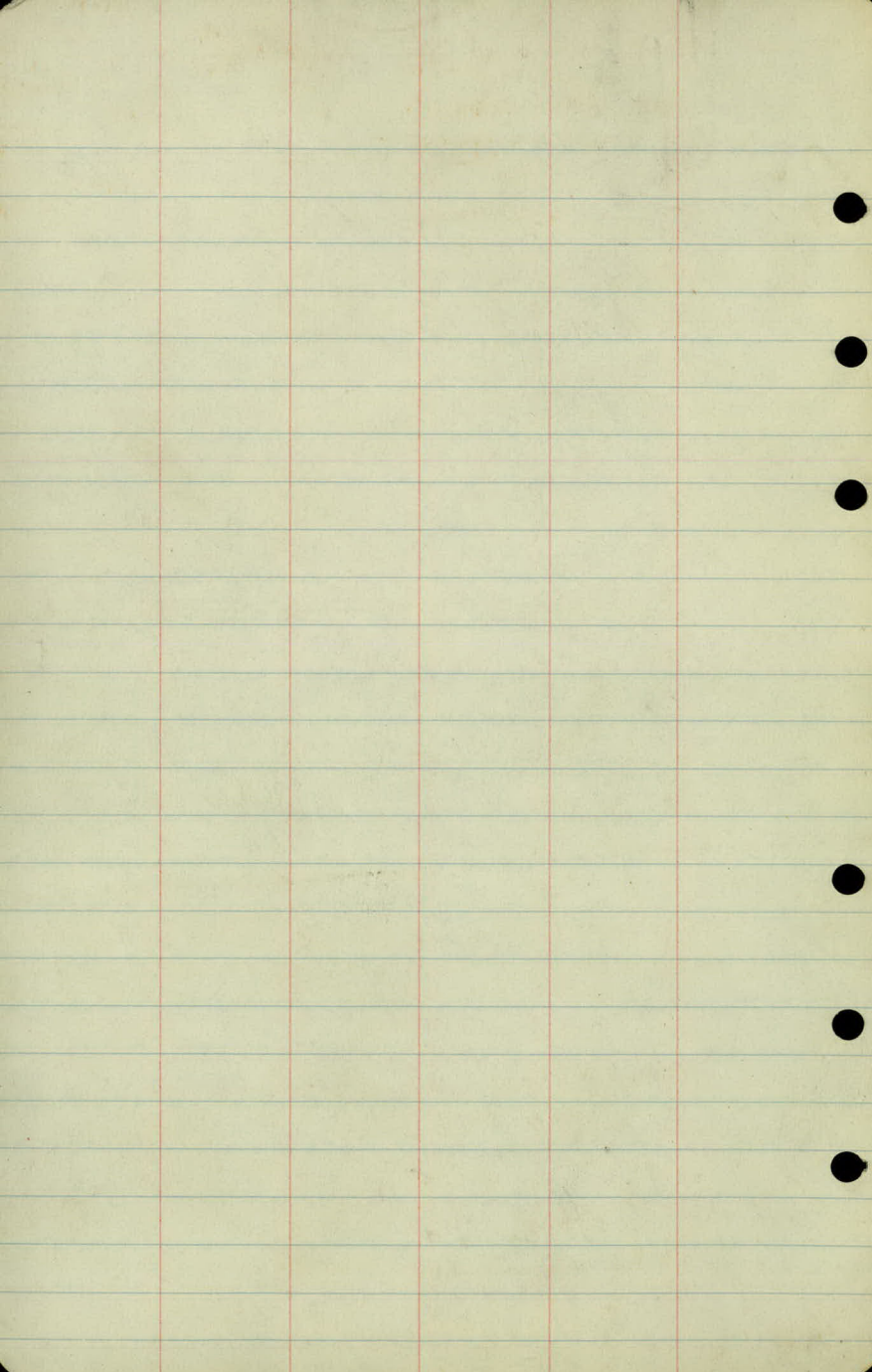
$$\frac{9.7}{50} \frac{10.2}{23} \frac{8.4}{17} \frac{8.2}{13} \frac{8.4}{10} 7.6 \frac{8.4}{11} \frac{6.9}{15} \frac{4.2}{50} \frac{2.8}{100}$$

Sta	+	π	-	Elev
		939.68		
469+50		✓		28.4
T.P.	1.59	929.88	11.39	928.29 ✓
B.M.			12.27	917.61 ✓

Lt ~~2~~ Rt

$\frac{140}{50}$	$\frac{15.2}{22}$	$\frac{12.2}{15}$	$\frac{11.8}{9}$	$\frac{12.1}{10}$	$\frac{13.2}{15}$	$\frac{13.6}{22}$	$\frac{10.9}{50}$	$\frac{8.1}{76}$	$\frac{6.7}{100}$
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Top Meander Cor



Additional X-Sec.
for Borrow.

N. Co. Line Road-
Sta. 456 to 467

X-Sections are based on $\pm$ Existing Rd.

W. N. Carlson
Nov 28, 1936

Sta.

Elev.

4/56

+50

4/57

+50

4/58

+50

4/59

+50

4/60

+50

4/61

+50

44.

9

24

$\frac{8.6}{200}$	$\frac{8.4}{150}$	$\frac{8.7}{100}$	$\frac{8.7}{50}$	$\frac{8.4}{50}$	$\frac{9.0}{100}$	$\frac{9.6}{150}$	$\frac{9.5}{200}$
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8.8	7.8	7.5	8.0	6.9	6.8	7.4	7.7	7.5
<u>200</u>	<u>150</u>	<u>100</u>	<u>50</u>		<u>50</u>	<u>100</u>	<u>150</u>	<u>200</u>

$\frac{7.1}{200}$	$\frac{7.1}{150}$	$\frac{7.0}{100}$	$\frac{6.3}{50}$	60	$\frac{4.8}{50}$	$\frac{5.1}{100}$	$\frac{5.3}{150}$	$\frac{5.3}{200}$
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$\frac{59}{200}$	$\frac{53}{150}$	$\frac{61}{100}$	$\frac{55}{50}$	$\frac{56}{0}$	$\frac{27}{50}$	$\frac{30}{100}$	$\frac{36}{150}$	$\frac{35}{200}$
------------------	------------------	------------------	-----------------	----------------	-----------------	------------------	------------------	------------------

$\frac{5.7}{200}$	$\frac{5.7}{150}$	$\frac{5.8}{100}$	$\frac{5.0}{50}$	$\frac{5.1}{50}$	$\frac{1.1}{50}$	$\frac{1.4}{100}$	$\frac{2.4}{150}$	$\frac{3.1}{200}$
-------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{7.5}{200}$	$\frac{6.5}{150}$	$\frac{5.5}{100}$	$\frac{4.8}{50}$	50	0.5	0.7	$\frac{1.7}{150}$	2.0
			$\frac{4.8}{50}$		$\frac{0.5}{50}$	$\frac{0.7}{100}$	$\frac{1.7}{150}$	$\frac{2.0}{200}$

$\frac{10.1}{200}$	$\frac{80}{150}$	$\frac{6.2}{100}$	$\frac{5.3}{50}$	$\frac{5.2}{50}$	$\frac{0.8}{50}$	$\frac{0.5}{100}$	$\frac{1.3}{150}$	$\frac{2.0}{200}$
--------------------	------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{17.5}{200}$	$\frac{9.2}{150}$	$\frac{7.2}{100}$	$\frac{6.2}{50}$	$\frac{5.3}{50}$	$\frac{0.9}{50}$	$\frac{0.7}{100}$	$\frac{1.8}{50}$	$\frac{2.1}{200}$
--------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	------------------	-------------------

$$\begin{array}{r} \frac{11.6}{150} \quad \frac{9.2}{100} \quad \frac{7.3}{50} \quad \frac{5.2}{50} \quad \frac{1.4}{50} \quad \frac{1.1}{100} \quad \frac{1.6}{150} \quad \frac{2.6}{200} \end{array}$$

<u>11.4</u>	<u>8.5</u>	<u>5.6</u>	<u>2.9</u>	<u>7.0</u>	<u>7.9</u>	<u>4.7</u>
100	50		50	100	150	200

<u>6.1</u>	<u>4.8</u>	<u>3.8</u>	<u>4.9</u>	<u>7.1</u>
50	100	150	200	

<u>66</u>	<u>75</u>	<u>67</u>	<u>63</u>	<u>66</u>
50	100	150	200	

Sta.

Elev.

462+50

463

+50

464

+50.

465

+50

466

+50

467

4k 2 21.

$$\frac{11.4}{100} \frac{12.1}{50} 8.7$$

$$\frac{8.3}{100} \frac{9.0}{50} 6.7$$

$$\frac{8.6}{200} \frac{6.9}{150} \frac{6.2}{100} \frac{6.2}{50} \frac{1}{1}$$

$$\frac{13.2}{150} \frac{10.6}{225} \frac{9.7}{200} \frac{9.7}{150} \frac{11.1}{100} \frac{10.8}{50} 8.8$$

$$\frac{9.6}{250} \frac{6.2}{225} \frac{5.9}{200} \frac{7.7}{150} \frac{4.8}{100} \frac{6.2}{50} \frac{6.3}{1}$$

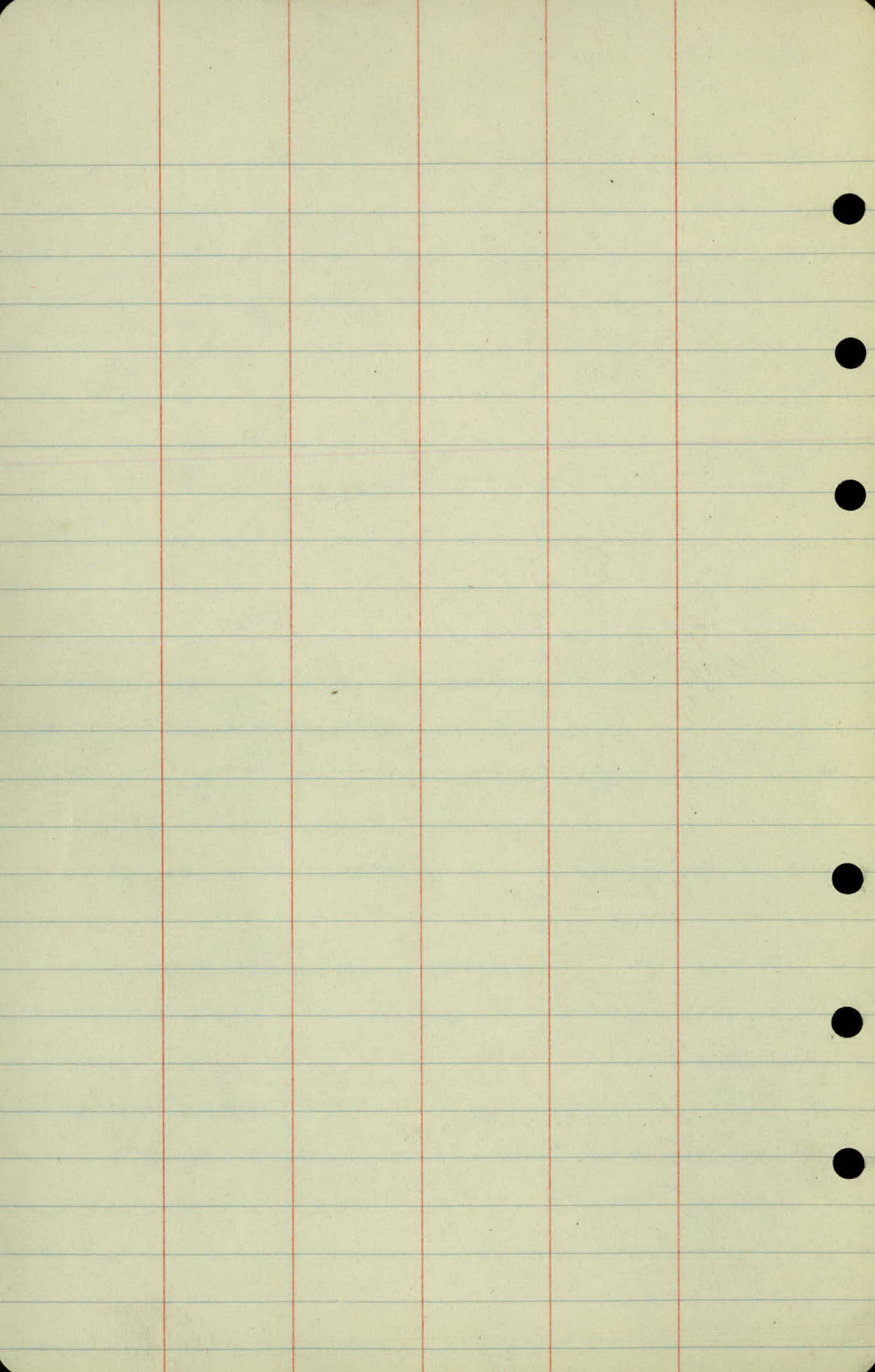
$$\frac{10.6}{270} \frac{6.7}{250} \frac{4.0}{225} \frac{3.0}{190} \frac{5.5}{150} \frac{6.3}{120} \frac{4.6}{100} \frac{1.2}{65} \frac{1.0}{50} \frac{4.3}{1}$$

$$\frac{11.0}{221} \frac{7.6}{250} \frac{5.7}{225} \frac{4.9}{200} \frac{4.7}{180} \frac{6.4}{150} \frac{8.6}{120} \frac{8.8}{100} \frac{4.6}{50} 7.0$$

$$\frac{11.8}{275} \frac{10.2}{250} \frac{7.0}{225} \frac{5.0}{200} \frac{4.2}{150} \frac{6.6}{100} \frac{5.1}{50} 2.3$$

$$\frac{11.5}{226} \frac{9.8}{200} \frac{6.8}{150} \frac{7.8}{100} \frac{8.6}{80} \frac{6.4}{50} 8.4$$

$$\frac{12.4}{200} \frac{13.6}{150} \frac{12.6}{100} \frac{10.7}{50} 10.3$$



1

Bench Levels.

Co. Rd. J. (N. County Line)

10/36 { Brostager
Wilke
Gillen

From S. T. Hy. #10 (Anoka Co.) to
Otter Lake Road.

Sta	+	K	-	Elev.
B.M.				907.97

2.28	910.25
------	--------

T.P.#1	4.11	906.14
--------	------	--------

4.52	910.66
------	--------

B.M.	2.22	908.44
------	------	--------

9.16	917.60
------	--------

T.P.#2	5.22	917.38
--------	------	--------

4.91	917.29
------	--------

B.M.	1.43	915.86
------	------	--------

T.P.#3	5.46	911.83
--------	------	--------

4.62	916.45
------	--------

B.M.	4.08	912.37
------	------	--------

T.P.#4	5.33	911.18
--------	------	--------

2.85	914.97
------	--------

T.P.#5	4.42	910.55
--------	------	--------

7.62	918.17
------	--------

B.M.	8.25	917.92
------	------	--------

B.M.	7.54	910.63
------	------	--------

5.00	915.63
------	--------

T.P.#6	2.21	914.42
--------	------	--------

2.23	915.65
------	--------

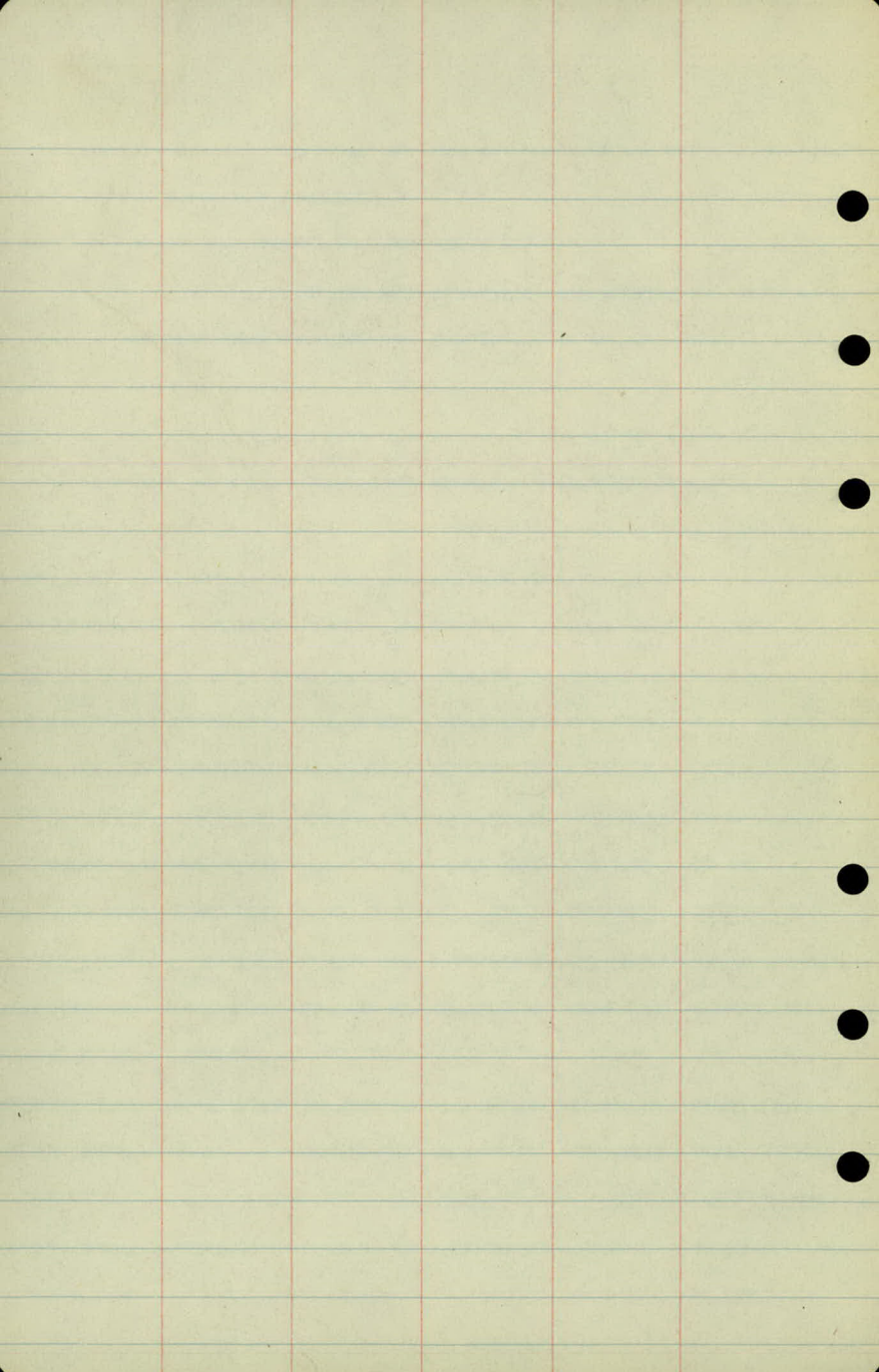
33' Rt. of Sta. 72+50, Spike in 10" Oak 50'
So. of No. County line 550' East of Long
Lake road. (Office Records)

Spike in Cottonwood Tree 33' Lt. of
Sta. 61+63

Spike in porch of house 65' Lt. of
Sta. 50+07

Spike in Oak Tree 40' Rt. of Sta. 41+20

Spike in Oak 50' Lt. of Sta. 24+83
Top of monument Sta. 20+17.3



1

Sta.	+	-	Elev.
		915.65	
B.M.		2.96	912.69
T.P.#7		3.06	912.59
	6.75	919.34	
B.M.		6.41	912.93

B.M.			907.97
	2.14	910.11	
T.P.#1		4.90	905.21
	3.10	908.31	
T.P.#2		3.15	905.16
	4.31	909.47	
T.P.#3		1.41	908.06
	4.71	912.77	
T.P.#4		5.23	907.54
	4.59	912.13	
B.M.		1.20	910.93
T.P.#5		8.48	903.65
	4.99	908.64	
T.P.#6		3.06	905.58
	7.14	912.72	
T.P.#7		2.06	910.66
	2.97	913.63	
B.M.		4.61	909.02

Spike in Oak 40' Rt. Sta. 9+10

Top of pavement at intersection of
Co. Rd. 5 & S.T. Hy. #10 = Sta. 0+00

See page #2 for description.

Spike in road guardrail post. Lt.

" " " " " "

" " " " " "

Spike in Oak 40' Lt. Sta. 95+39

Spike in fence post. Rt. Sta. -

" " " " "

" " " " "

{ Brass plug S.T. Hy. #8 & No. County line.
Data from Office Record = Elev 909.02

Sta.	+	-	Elev.
			909.08
	3.94	912.96	
T.P.#8		2.64	910.32
	3.09	913.41	
T.P.#9		4.14	909.27
	2.61	911.88	
T.P.#10		3.14	908.74
	5.16	913.90	
B.M.		5.14	908.76
	0.25	909.51	
T.P.#11		1.29	908.22
	8.16	916.38	
B.M.		3.98	912.40
T.P.#12		4.69	911.69
	4.40	916.09	
T.P.#13		5.44	910.65
	1.13	911.78	
T.P.#14		2.09	909.69
	6.79	916.48	
T.P.#15		8.50	907.98
	0.60	908.58	
T.P.#16		10.35	898.23
	0.29	898.52	
B.M.		7.35	891.17

Spike in Tel. pole Rt. of Sta. -

Spike in fence post Rt. of Sta. -

Spike in Tel. pole Rt. of Sta. -

Spike in fence post 100' Lt. of Sta. -

Spike in Oak 95' Rt. of Sta. -

Spike in Tel. pole Rt. of Sta. -

Spike in fence post Rt. of Sta. -

Spike in Tel. pole Rt. of Sta. -

" " " " " "

Spike in 18" Box Elder 69' No. East Lexington

& No. County line, Sta. 159 + 36 - 40' Lt.

(Office record = Elev. 871.47) $E_g = 19.70$ ft.

Sta.	+	K	-	Elev.
	0.63	891.80		891.17
T.P.#17			8.97	882.83
	4.99	887.84		
T.P.#18			5.16	882.66
	5.26	888.04		
T.P.#19			4.55	882.47
	9.68	892.15		
B.M.			5.67	887.48
T.P.#20			7.86	885.29
	3.35	888.64		
T.P.#21			3.68	884.96
	4.10	889.06		
T.P.#22			1.95	887.11
	6.16	892.27		
T.P.#23			5.22	888.05
	4.52	892.57		
T.P.#24			1.47	891.10
	9.95	901.05		
B.M.			2.14	898.91
T.P.#25			0.98	900.07
	8.58	908.65		
T.P.#26			9.93	898.74

Top of stake Lt. of Sta.

Stake 13' Lt. of Sta. 171+58

Spike in fence post 33' Rt. of Sta. 178+67

{ Spike in 18" stump 200' So. of N. County
line 1920' East of Lexington Ave. (Office
record of this bench is Elev. 867.77 24
Elevation of 19.71 ft.

Spike in pole 25' Lt. of Sta. 185+25

Spike in fence post 50' Rt. of Sta. 192+75

" " " " 33' Rt. of Sta. 199+51

Top of stake Sta.

" " " "

{ Spike in Oak 150' Lt. of Sta. 215+75
Office record = Elev. 879.14. Elevation of 19.77 ft.
Spike in road Sta. -

Top of boulder Rt. of Sta.

Sta.	+	-	Elev.
	1.58	900.30	898.72
T.P.#27		12.35	887.95
	6.83	894.78	
T.P.#28		0.76	894.02
	10.61	904.63	
T.P.#29		2.24	902.39
	2.98	905.37	
B.M.		1.00	904.37
T.P.#30		4.03	901.34
	5.34	906.68	
T.P.#31		2.62	903.06
	5.55	908.61	
B.M.		2.60	905.01
T.P.#32		2.77	904.84
	5.13	909.97	
T.P.#33		7.83	902.14
	2.06	904.20	
T.P.#34		5.88	898.32
	2.12	900.44	
B.M.		7.11	893.33
T.P.#35		6.81	893.63
	8.04	901.67	
T.P.#36		0.29	901.28
	2.76	904.04	
T.P.#37		6.44	897.60

Top of stake 12' Rt. of Sta. 230+20

Top of stake Rt. of Sta. -

{ Spike in Cottonwood 33' Rt. Sta. 244+65
Office record = Elev. 884.57 $Eg. = 19.80$ ft.

Top of stake Rt. of Sta. -

" " " " " "

{ Top of monument at Hodgson Road &
No. County line, Sta. 258+70?

Spike in power pole 33' Lt. of Sta. -

Spike in tel. pole 30' Rt. of Sta. -

" " " " " " " -

Spike in Willow 250' Rt. of Sta. -

Spike in power pole 33' Lt. Sta. -

Spike in pole 33' Lt. Sta.

" " " " " "

	+	π	-	Elev.
	5.71	902.21		897.60
B.M.			5.61	897.70
T.P.#38			3.38	899.93
	2.93	902.86		
T.P.#39			10.15	892.71
B.M.				891.79
B.M.				896.88
T.P.#39				892.71
	5.86	898.57		
B.M.#40			4.62	892.95
	4.38	898.33		
T.P.#41			4.27	894.06
	2.39	896.45		
T.P.#42			3.17	893.28
	5.80	899.08		
T.P.#43			4.56	894.82
	6.78	901.30		
B.M.			6.36	894.94
T.P.#44			1.00	900.30
	6.92	907.22		

- Spike in Cottonwood 85' Lt. Sta. -
- " " pole 33' Rt. Sta. -

- Spike in fence post 50' Rt. of Sta. 309

See prelim. X-sec. notes. U.S.G.S. monument

- 33' Rt. of Sta. 183+36. Office data. =
Elev. 872.09 = $\frac{1}{4}$ of 19.20 ft.

See prelim. X-sec. notes. U.S.G.S. No. W-6

- 38' Rt. of Sta. 204+03.

See above.

- Spike in 6" Poplar 85' Rt. Sta. 313+90

- Spike in Tel. pole Rt. of Sta.

- " " " " " "

- " " " " " "

- Top of boulder 87' Rt. Sta.
In road.

	+	-	Elev.
T.P.#45		907.22	1.81
	6.14	911.55	905.41
B.M.		2.85	908.70
T.P.#46		6.51	905.04
	2.07	908.11	
T.P.#47		8.07	900.04
	6.87	906.91	
B.M.		2.35	904.56
	4.24	908.80	
B.M.#48		0.59	908.21
	7.70	915.91	
T.P.#49		0.86	915.05
	11.81	926.86	
T.P.#50		0.56	926.30
	5.63	931.93	
T.P.#51		5.54	926.39
	7.40	933.79	
T.P.#52		5.81	928.78
	3.63	931.91	
T.P.#53		4.42	927.49
	2.46	929.95	
B.M.		2.68	927.27
T.P.#54		6.07	923.88
	2.55	926.43	
B.M.		8.21	918.22
	3.21	921.43	

Spike in tel. pole Rt. of Sta. -

U.S.G.S. No T-8, Lt. of Sta. 336+

Spike in power pole Lt. of Sta. -

[" " " " " "]

Spike in 24" Cottonwood 75' Rt. Sta. 351+45

Spike in 12" Oak 50' Rt. Sta.

Spike in fence post 33' Rt. Sta.

" " " " " "

Spike in power pole 33' Lt. of Sta.

" " " " " "

" " " " " "

Spike in 24" Cottonwood 60' Lt. of Sta. -

Spike in power pole 33' Lt. Sta.

Spike in Twin soft maple 75' Lt. Sta.

	+	⌊	-	Elev.
T.P.#55		921.43	6.78	914.65
	1.64	916.29		
B.M.			8.89	907.40
T.P.#56			8.61	907.68
	4.48	912.16		
T.P.#57			3.53	908.63
	3.14	911.77		
B.M.			7.04	904.73
	5.62	910.35		
T.P.#58			3.39	906.96
	4.74	911.70		
B.M.			5.22	906.48
	0.84	907.32		
B.M.			5.82	901.80
	5.15	906.55		
T.P.#59			1.56	905.29
	4.50	909.89		
T.P.#60			0.62	909.27
	10.42	919.69		
B.M.			4.81	914.88
T.P.#61			1.27	918.42
	6.28	924.80		
B.M.			1.66	923.14
	6.73	929.87		
B.M.			3.07	926.80

Spike in power pole 33' Lt. Sta.

Spike in 24" Oak 65' Rt. Sta.

In roadway

Spike in guy pole 33' Rt. Sta.

Spike in 18" Elm 90' Lt. of Sta.

Spike in Tel. pole 33' Rt. Sta.

Spike in 36" Cottonwood 33' Rt. Sta.

Spike in 24" Elm 33' Lt. Sta.

Spike in tel. pole 33' Lt. Sta.

" " " " " " "

Spike in 18" Box Elder 33' Lt. Sta.

" power pole 33' Lt. Sta.

Spike in 24" Cottonwood at intersection of No. County line & Centerville roads.

Spike in 14" Oak 40' Lt. of Sta.

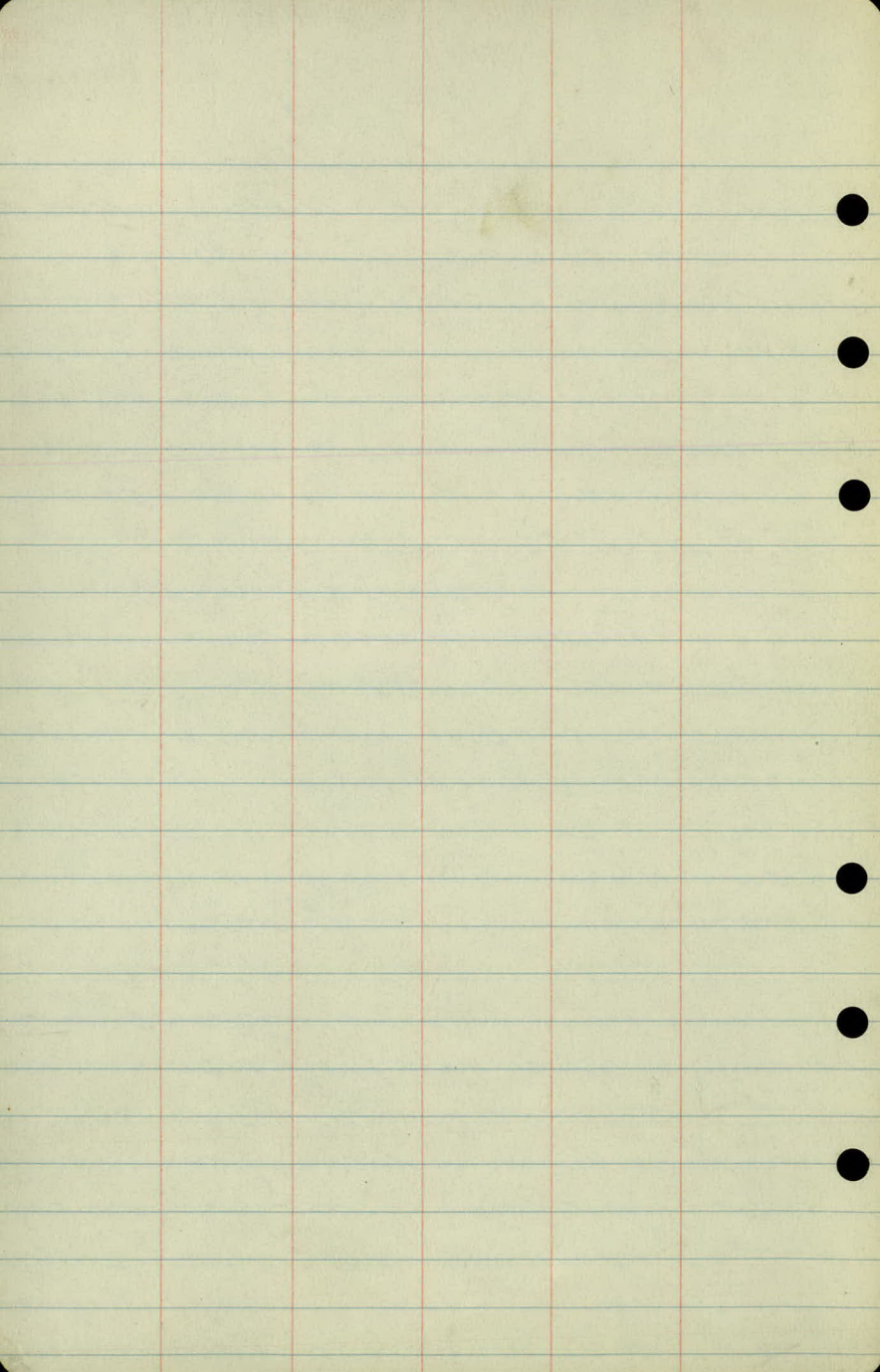
	+	⌞	-	Elev.
	7.95	924.75		926.80
T.P.#62			2.47	932.28
	4.83	937.11		
B.M.			4.18	937.93
T.P.#63			6.72	930.39

● Spike in Tel. pole 33' Lt. of Sta.

● Spike in 18" Box Elder at intersection of
N. County Line & Centerville & Otter Lake roads

Spike in fence post 33' Rt. Sta.

● Note:- Where stationing to Benches
are not given the alignment had not
been run at the time levels were
taken. This data should be secured
when X-sec. are taken.



check levels

North County Line

Hodgson Road to Turtle Lake Rd.

	+	+	-	Elev.	
Check Levels					
B.M.	3.11	908.12		905.01	
	3.49	908.60	3.01	905.11	
	1.21	903.42	6.39	902.21	
B.M.	0.18	903.42	0.18	903.24	
T.P.	5.12	903.42	5.12	898.30	(Bred. 898.32)
✓	5.07	900.01	8.48	894.94	
B.M.	6.67	900.01	6.67	893.34	(893.33) +
T.P.	6.41	900.01	6.41	893.60	(893.63) +
✓	6.05	904.58	1.48	898.53	
✓	6.03	903.62	6.99	897.59	(897.60)
B.M.	4.56	903.62	2.56	899.06	(897.70)
T.P.	2.76	902.68	3.70	899.92	(899.93)
Sta. 303 ±			3.35	(899.3)	
T.P.	4.88	898.67	8.89	893.79	
✓	5.96	898.67	5.96	892.71	(892.71) +
B.M.	4.75	898.69	4.73	893.94	(893.95) +
T.P.	3.21	897.27	4.63	894.06	(894.06)
✓	3.98	897.27	3.98	893.29	(893.28) +
✓	3.30	897.96	2.61	894.66	
✓	3.43	897.96	3.43	894.53	(894.42)
✓	12.05	909.87	0.14	897.82	
B.M.			1.18	908.69	(908.70)

W.H.C.

K.A. Nov. 6, 1936

A.M.

Top Mar. Hodgson Road.

Top culd. Marker Rt. 63-1

R.R Spike in P.P. Lt.

T.P. #34

Spike in Willow 250' Rt Sta. (near creek)

T.P. #35

T.P. #37

3.17
4.63
2.71
1.6

~~Spike in Cottonwood 85' Lt. Sta. 311+40 (Just east of L. 11)~~

T.P. #38

T.P. #39 Spike in P.P. 50' Rt. Sta. 309

(TP#40) Spike in 6" Pop. 85' Rt. Sta. 313+90

T.P. #41

T.P. #42

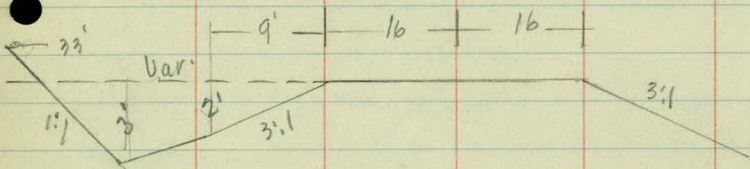
T.P. #43

U.S. G.S. and State Survey Sta. 7-8 Line P. 9

$$363 + 54.8 =$$

$$\begin{array}{r} 109 + 97.71 \\ 2 + 05.19 \end{array}$$

Slope Stakes
No Co. Line Rd.
Rice St to $\frac{1}{2}$ E. Turtle LArd.



Sta.	+	T	-	Grade	Dit Gr. L + RT
	451	898.46			
211+50.17				94.1	91.1
312					91.0
+60					90.9
213					90.8
+55					90.7
314					90.6
+50					90.5
315					90.4
+50					90.3
316					90.2
+50				94.1	90.1
I.P.	4.01	897.92	1.55		

204
a1B. 1.6
1.4

2

W.A.G.

Gr. Rod.

Lt

L

Rt.

Dec 22, 1936

893.95 Spk-6" Pop 85' Rt. Sta 313+90

4.4 7.4

33' / 20
20.64.8
-0.368 / 33
20.6

4.4 7.5

33' / 6.8
20.74.8
-0.473 / 33
20.2

4.4 7.6

33' / 6.9
20.75.1
-0.75.1 / 33
20.5

4.4 7.7

33' / 7.2
20.54.8
-0.45.9 / 33
20.8

4.4 7.8

33' / 7.0
20.84.8
-0.47.2 / 33
20.6

4.4 7.9

33' / 7.1
20.84.7
-0.36.9 / 33
20.10

4.4 8.0

33' / 6.0
20.204.4
-0.06.6 / 33
20.1.4

4.4 8.1

33' / 5.7
20.244.2
-0.26.5 / 33
20.1.6

4.4 8.2

33' / 6.2
20.204.6
-0.26.5 / 33
20.1.7

4.4 8.3

33' / 6.9
20.144.6
-0.27.2 / 33
20.1.1

4.4 8.4

33' / 6.6
20.184.9
-0.57.3 / 33
20.14

893.91

Sta.	+	Σ	-	Grade	Dist. Gr. R. + Lt.
		897.92			
317				94.1	90.15
+50					90.2
318					90.25
+50					90.3
319					90.35
+50					90.4
320					90.45
+50					90.5
321					90.55
Σ					
322				94.1	90.65
T.P.	6.65	898.80	5.77		892.15

Gr. Rd

LT

±

RT

$$3.8 \quad 7.75 \quad 33' \begin{array}{r} 65 \\ 121.3 \\ \hline \end{array} \quad \begin{array}{r} 41 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 65 \\ 121.3 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.7 \quad 33' \begin{array}{r} 65 \\ 121.4 \\ \hline \end{array} \quad \begin{array}{r} 37 \\ +0.1 \\ \hline \end{array} \quad \begin{array}{r} 64 \\ 121.3 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.65 \quad 33' \begin{array}{r} 63 \\ 121.4 \\ \hline \end{array} \quad \begin{array}{r} 40 \\ -0.2 \\ \hline \end{array} \quad \begin{array}{r} 67 \\ 121.0 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.6 \quad 33' \begin{array}{r} 65 \\ 121.1 \\ \hline \end{array} \quad \begin{array}{r} 40 \\ -0.2 \\ \hline \end{array} \quad \begin{array}{r} 68 \\ 121.1 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.55 \quad 33' \begin{array}{r} 65 \\ 121.1 \\ \hline \end{array} \quad \begin{array}{r} 47 \\ -0.9 \\ \hline \end{array} \quad \begin{array}{r} 68 \\ 120.8 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.5 \quad 33' \begin{array}{r} 65 \\ 121.0 \\ \hline \end{array} \quad \begin{array}{r} 52 \\ -1.4 \\ \hline \end{array} \quad \begin{array}{r} 67 \\ 120.8 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.45 \quad 33' \begin{array}{r} 65 \\ 121.0 \\ \hline \end{array} \quad \begin{array}{r} 61 \\ -2.3 \\ \hline \end{array} \quad \begin{array}{r} 66 \\ 120.9 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.4 \quad 33' \begin{array}{r} 65 \\ 120.9 \\ \hline \end{array} \quad \begin{array}{r} 67 \\ -2.9 \\ \hline \end{array} \quad \begin{array}{r} 69 \\ 120.5 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.35 \quad 33' \begin{array}{r} 67 \\ 120.7 \\ \hline \end{array} \quad \begin{array}{r} 64 \\ -2.6 \\ \hline \end{array} \quad \begin{array}{r} 71 \\ 120.3 \\ \hline 33' \end{array}$$

$$3.8 \quad 7.3 \quad 33' \begin{array}{r} 67 \\ 120.6 \\ \hline \end{array} \quad \begin{array}{r} 65 \\ -2.7 \\ \hline \end{array} \quad \begin{array}{r} 70 \\ 120.3 \\ \hline 33' \end{array}$$

Sta.	+	-	Grade	Ditgr. Bl. Mt.
			898.80	

322+50

94.1

90.75

323

90.75

324

90.85

325

90.95

+50

91.00

326

91.05

+60

94.1

91.10

327

94.1

+70

94.1

328

94.2

329

94.3

9.2.

4.

2

Kt.

$$4.7 \begin{array}{c} (3.9) \\ 8.1 \end{array}$$

$$33 \overline{) 74} \\ \underline{207}$$

$$\begin{array}{r} 68 \\ -21 \end{array}$$

$$\begin{array}{r} 79 \\ 20.2 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.8) \\ 8.05 \end{array}$$

$$33 \overline{) 74} \\ \underline{207}$$

$$\begin{array}{r} 67 \\ -20 \end{array}$$

$$\begin{array}{r} 80 \\ 20.1 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.75) \\ 7.95 \end{array}$$

$$33 \overline{) 75} \\ \underline{205}$$

$$\begin{array}{r} 62 \\ -15 \end{array}$$

$$\begin{array}{r} 76 \\ 20.4 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.15) \\ 7.85 \end{array}$$

$$33 \overline{) 715} \\ \underline{2097}$$

$$\begin{array}{r} 49 \\ -32 \end{array}$$

$$\begin{array}{r} 21 \\ 20.7 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.1) \\ 7.80 \end{array}$$

$$33 \overline{) 72} \\ \underline{206}$$

$$\begin{array}{r} 44 \\ 703 \end{array}$$

$$\begin{array}{r} 7.3 \\ 20.5 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.05) \\ 7.75 \end{array}$$

$$33 \overline{) 72} \\ \underline{205}$$

$$\begin{array}{r} 43 \\ 704 \end{array}$$

$$\begin{array}{r} 6.8 \\ 21.0 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} (3.0) \\ 7.7 \end{array}$$

$$33 \overline{) 69} \\ \underline{208}$$

$$\begin{array}{r} 41 \\ 706 \end{array}$$

$$\begin{array}{r} 4.5 \\ 702 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} 7.7 \end{array}$$

$$33 \overline{) 69} \\ \underline{208}$$

$$\begin{array}{r} 41 \\ 706 \end{array}$$

$$\begin{array}{r} 4.3 \\ 70.5 \overline{) 33} \end{array}$$

$$4.7 \begin{array}{c} 7.7 \end{array}$$

$$33 \overline{) 67} \\ \underline{210}$$

$$\begin{array}{r} 47 \\ -00 \end{array}$$

$$\begin{array}{r} 7.3 \\ 20.4 \overline{) 33} \end{array}$$

$$4.6 \begin{array}{c} 7.6 \end{array}$$

$$33 \overline{) 73} \\ \underline{203}$$

$$\begin{array}{r} 5.3 \\ -00 \end{array}$$

$$\begin{array}{r} 2.4 \\ 20.2 \overline{) 33} \end{array}$$

$$4.5 \begin{array}{c} 7.5 \end{array}$$

$$33 \overline{) 72} \\ \underline{203}$$

$$\begin{array}{r} 2.9 \\ -14 \end{array}$$

$$\begin{array}{r} 7.2 \\ 20.3 \overline{) 33} \end{array}$$

Sta.	+	Σ	-	grade
		898.80		
330				94.4
+70				94.5
T.P.	7.10	901.72	4.18	894.62
331				94.7
+65				95.1
332				95.5
+50				96.1
333				96.9
+60				98.0
334				98.9
T.P.	9.09	910.21	0.60	907.12
+40				99.9
335				01.4

Gr. Rod.

K

L

R

$$4.4 \quad 7.4 \quad 33 \overline{) \begin{array}{r} 73 \\ 120.1 \end{array}} \quad \begin{array}{r} 56 \\ -1.2 \end{array} \quad \begin{array}{r} 7.1 \\ 120.3 / 33 \end{array}$$

$$4.3 \quad 7.3 \quad 33 \overline{) \begin{array}{r} 70 \\ 120.3 \end{array}} \quad \begin{array}{r} 48 \\ -0.5 \end{array} \quad \begin{array}{r} 6.9 \\ 120.4 / 33 \end{array}$$

$$7.0 \quad 10.0 \quad 33 \overline{) \begin{array}{r} 96 \\ 120.4 \end{array}} \quad \begin{array}{r} 7.1 \\ +0.1 \end{array} \quad \begin{array}{r} 8.7 \\ 121.3 / 33 \end{array}$$

$$6.6 \quad 9.6 \quad 33 \overline{) \begin{array}{r} 5.5 \\ 71.1 \end{array}} \quad \begin{array}{r} 4.1 \\ +0.5 \end{array} \quad \begin{array}{r} 5.6 \\ 71.0 / 33 \end{array}$$

$$6.2 \quad 9.2 \quad 33 \overline{) \begin{array}{r} 4.9 \\ 71.3 \end{array}} \quad \begin{array}{r} 5.9 \\ +0.3 \end{array} \quad \begin{array}{r} 8.2 \\ 71.0 / 33 \end{array}$$

$$5.6 \quad 8.6 \quad 33 \overline{) \begin{array}{r} 7.3 \\ 121.3 \end{array}} \quad \begin{array}{r} 6.1 \\ -0.5 \end{array} \quad \begin{array}{r} 9.3 \\ -3.7 / 12.1 \end{array}$$

$$4.8 \quad 7.8 \quad 33 \overline{) \begin{array}{r} 8.2 \\ -3.4 \end{array}} \quad \begin{array}{r} 5.2 \\ -0.4 \end{array} \quad \begin{array}{r} 8.8 \\ -4.0 / 28.0 \end{array}$$

$$3.7 \quad 6.7 \quad 33 \overline{) \begin{array}{r} 3.4 \\ 70.3 \end{array}} \quad \begin{array}{r} 3.4 \\ 70.3 \end{array} \quad \begin{array}{r} 4.1 \\ 120.6 / 33 \end{array}$$

$$2.8 \quad 5.8 \quad 33 \overline{) \begin{array}{r} 0.8 \\ 72.0 \end{array}} \quad \begin{array}{r} 2.2 \\ 70.6 \end{array} \quad \begin{array}{r} 8.0 \\ 72.8 / 33 \end{array}$$

$$10.3 \quad 33 \overline{) \begin{array}{r} 6.7 \\ 126 \end{array}} \quad \begin{array}{r} 9.7 \\ 70.6 \end{array} \quad \begin{array}{r} 5.5 \\ 48 / 33 \end{array}$$

$$8.8 \quad 33 \overline{) \begin{array}{r} 4.5 \\ 44.7 \end{array}} \quad \begin{array}{r} 8.0 \\ 70.8 \end{array} \quad \begin{array}{r} 4.3 \\ 44.5 / 33 \end{array}$$

Sta	+	π	-	Grade
	322	910.21 911.93	(1.53)	
336				04.0
B.M.	3.22	911.93	3.22	
337				06.2
+15				06.4
+50				06.9
338				07.4
+60				07.8
339				07.7
+50				07.6
340				07.2
+65				06.5
T.P.	3.72	908.69	6.96	904.97
341				06.2

gr. Rod

H.

L

R.

908.71

$$7.9 \text{ } \underline{2.2} \quad 33 \begin{array}{r} 3.7 \\ +14.2 \end{array}$$

$$\begin{array}{r} 7.7 \\ +0.2 \end{array}$$

$$\begin{array}{r} 6.5 \\ +1.4 \\ \hline 33 \end{array}$$

908.71 U.S. G.S. 28' L 336 + 20

$$5.7 \quad F = 32.5 \begin{array}{r} 2.6 \\ +3.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ +0.1 \end{array}$$

$$\begin{array}{r} 5.3 \\ +0.4 \\ \hline 33 \end{array}$$

5.5

$$5.0 \quad F = 31.8 \begin{array}{r} 1.4 \\ +2.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ +0.0 \end{array}$$

Tiang 10

$$4.5 \quad F = 31.8 \begin{array}{r} 0.8 \\ +3.7 \end{array}$$

$$\begin{array}{r} 4.8 \\ +0.3 \end{array}$$

$$4.1 \quad 33 \begin{array}{r} 1.6 \\ +2.5 \end{array}$$

$$\begin{array}{r} 4.1 \\ +0.3 \end{array}$$

$$4.2 \quad 33 \begin{array}{r} 2.1 \\ +2.1 \end{array}$$

$$\begin{array}{r} 4.0 \\ +0.2 \end{array}$$

$$4.3 \quad 33 \begin{array}{r} 2.5 \\ +1.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ +0.2 \end{array}$$

$$4.7 \quad 7.7 \quad 33 \begin{array}{r} 3.8 \\ +0.9 \end{array}$$

$$\begin{array}{r} 5.3 \\ +0.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ +0.9 \\ \hline 33 \end{array}$$

$$5.4 \quad 8.4 \quad 33 \begin{array}{r} 6.6 \\ +1.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ +0.5 \end{array}$$

$$\begin{array}{r} 10.4 \\ +0.3 \\ \hline 31 \end{array}$$

$$7.5 \quad 5.5 \quad 7.5 \begin{array}{r} 2.0 \\ +4.5 \end{array}$$

$$\begin{array}{r} 3.7 \\ +0.7 \end{array}$$

$$\begin{array}{r} 9.3 \\ +6.8 \\ \hline 33 \end{array}$$

Sta.	+	π	-	grade	Dt+Gr.R.+LT
		908.69			
341+45				05.7	
342				05.2	
+55				04.6	
343				04.2	
+50				03.7	
344				03.2	
T.P.	3.71	906.10	6.30		902.39
+60				02.8	
345				02.5	98.1
+50				02.3	98.2
346				02.1	98.3
+50				02.1	98.4
347				02.0	98.5

Gr. Rod

Lt.

L

Rt

3.0

$$33 \frac{90}{60}$$

$$\frac{37}{-07}$$

$$\frac{80}{-56} / 34.8$$

3.5

$$35 \frac{90}{55}$$

$$\frac{41}{-06}$$

$$\frac{21}{-7.6} / 26.8$$

4.1 Fl

$$33 \frac{65}{100.6}$$

$$\frac{44}{-03}$$

$$\frac{50}{12.1} / 33'$$

4.5 ^{7.5}

$$33 \frac{60}{101.5}$$

$$\frac{48}{-03}$$

$$\frac{65}{121.0} / 33'$$

(246 12.0)

5.0 ^{8.0}

$$33 \frac{21}{100.9}$$

$$\frac{52}{-02}$$

5.5

$$33 \frac{82}{100.3}$$

$$\frac{57}{-02}$$

$$\frac{93}{-78} / 27.4$$

Top Calc. Marker.

3.3

$$27.4 \frac{7.1}{3.8}$$

$$\frac{39}{-06}$$

$$\frac{73}{-4.0} / 28.0$$

3.6

(4.6)

8.0

$$28 \frac{75}{100.5}$$

$$\frac{47}{-1.1}$$

$$\frac{80}{100.0} / 33'$$

3.8

(4.1)

7.9

$$28 \frac{75}{100.4}$$

$$\frac{56}{-1.8}$$

$$\frac{8.2}{-} / 33'$$

4.0

(3.9)

7.8

$$28 \frac{75}{100.3}$$

$$\frac{55}{-1.5}$$

$$81 / 33'$$

4.0

(3.7)

7.7

$$27 \frac{74}{100.2}$$

$$\frac{55}{-1.5}$$

$$\frac{80}{-} / 33'$$

4.1

(3.5)

7.6

$$29 \frac{72}{100.4}$$

$$\frac{46}{-0.5}$$

$$\frac{80}{-} / 33'$$

Sta.	+	π	-	grade	ditg. r. R. + L.
------	---	-------	---	-------	------------------

906.10

34760

02.1 98.6

348

02.2 98.7

+55

02.3 98.8

349

02.4 98.9

350

02.6 99.0

T.P.

5.14

907.23

4.01

902.09

+45

02.7 99.1

351

02.8 99.2

+38

02.9 99.3

B.M.

2.76

+54

02.9 99.3

+74

03.0 99.4

352

03.0 99.5

Gr. Rad.

Lt.

L

Rt.

$$\begin{array}{r} 35 \\ 410 \overline{) 7.5} \end{array}$$

$$33 \overline{) \frac{61}{100.4}}$$

$$\frac{40}{20}$$

$$\frac{72}{100.3} / 33$$

$$39 \overline{) 7.4} \quad (35)$$

$$33 \overline{) \frac{41}{100.2}}$$

$$\frac{41}{-0.2}$$

$$\frac{44}{100.8} / 33$$

$$38 \overline{) 7.3} \quad (35)$$

$$33 \overline{) \frac{35}{10.3}}$$

$$\frac{40}{-0.2}$$

$$\frac{68}{100.5} / 33$$

$$37 \overline{) 7.2} \quad (35)$$

$$33 \overline{) \frac{35}{10.2}}$$

$$\frac{40}{-0.3}$$

$$\frac{65}{100.7} / 33$$

$$35 \overline{) 7.1} \quad (36)$$

$$33 \overline{) \frac{52}{10.1}}$$

$$\frac{39}{-0.4}$$

$$\frac{69}{100.2} / 33$$

$$45 \overline{) 8.1} \quad (36)$$

$$33 \overline{) \frac{75}{100.8}}$$

$$\frac{51}{-0.6}$$

$$\frac{21}{100.0} / 33$$

$$44 \overline{) 8.0} \quad (36)$$

$$33 \overline{) \frac{75}{100.5}}$$

$$\frac{51}{-0.7}$$

$$\frac{77}{100.3} / 33$$

$$43 \overline{) 7.9} \quad (36)$$

$$33 \overline{) \frac{73}{100.6}}$$

$$\frac{44}{-0.6}$$

$$\frac{70}{100.9} / 33$$

904.55 Spk 24" Pop 75' Rt. 351+45

Sta.	+	π	-	grade
------	---	-------	---	-------

353				03.6
-----	--	--	--	------

354				04.6
-----	--	--	--	------

+55				05.4
-----	--	--	--	------

355				06.2
-----	--	--	--	------

356				08.2
-----	--	--	--	------

+60				09.5
-----	--	--	--	------

357				10.4
-----	--	--	--	------

+55				11.6
-----	--	--	--	------

358				12.6
-----	--	--	--	------

359				14.8
-----	--	--	--	------

360				17.0
-----	--	--	--	------

Gr. Rod -

Lt -

E

Rt -

Sta.	+	A	-	Grade
------	---	---	---	-------

361				19.2
-----	--	--	--	------

362				21.4
-----	--	--	--	------

363				73.6
-----	--	--	--	------

+548				24.8
------	--	--	--	------

B.M.

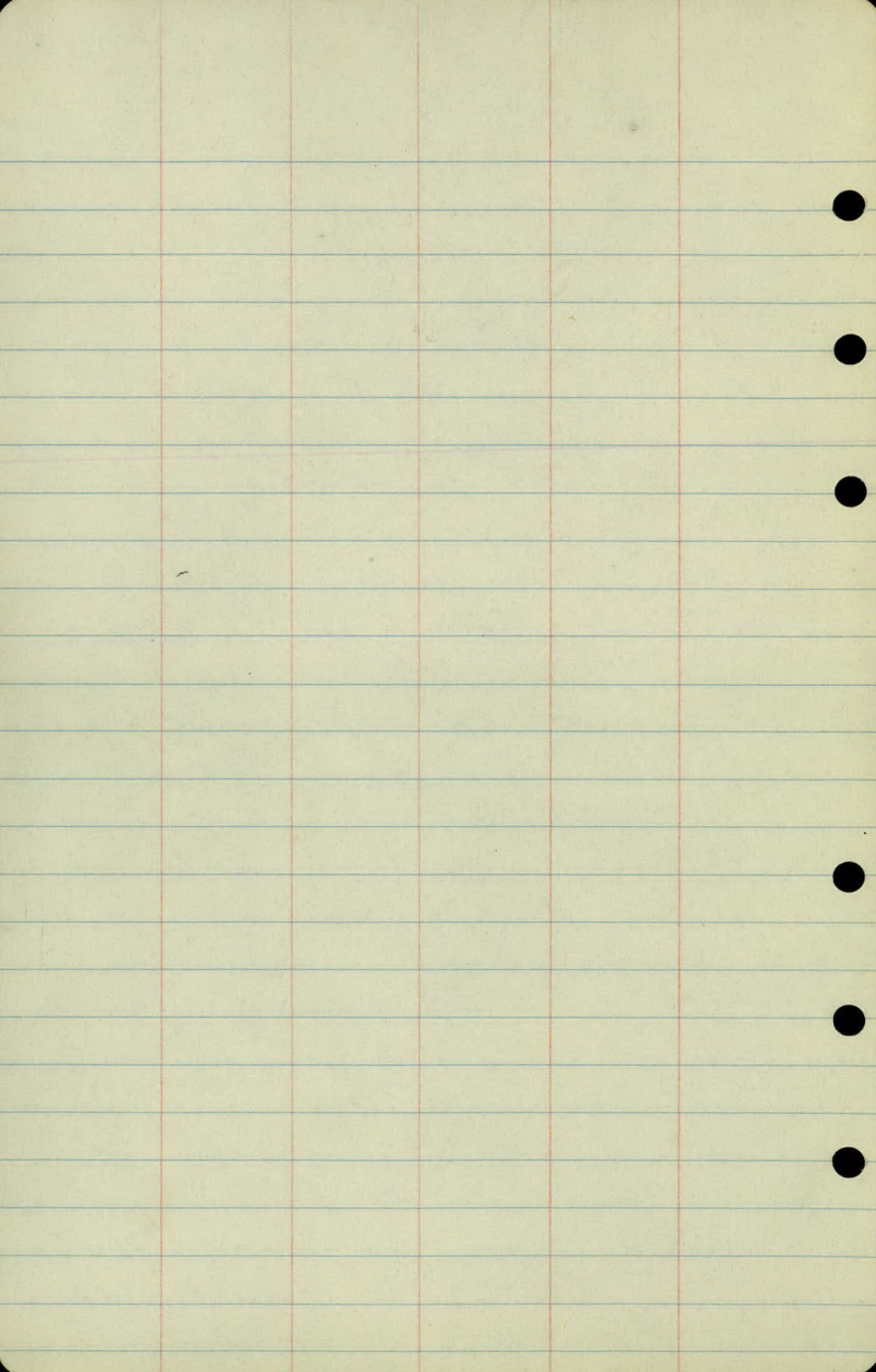
Gr. Rod

H

L

RT.

927.05 High on Rock @ Fen Cor. 30' Rt. 363+55



Slope Stakes

Na. Co. Lino Rd.

from

Centerville Rd to Otter Lk. Rd.

Sta	+	A	-	Grade
B.M.				932.93

447 +57.6

448				31.9
-----	--	--	--	------

+54				31.7
-----	--	--	--	------

449				31.5
-----	--	--	--	------

+50				31.3
-----	--	--	--	------

450				31.1
-----	--	--	--	------

+50				30.9
-----	--	--	--	------

451				30.8
-----	--	--	--	------

+50				30.8
-----	--	--	--	------

452				30.9
-----	--	--	--	------

+50				31.0
-----	--	--	--	------

Gr. Rod Lt. Lt. Rt.

Sph. in 18" BE S.W. Cor. Cent Rd & N. Co. Line

Sta.	+	π	-	Elev.
453				31.1
	+50			31.4
454				31.7
	+50			32.0
455				32.4
	+50			32.8
456				33.1
	+50			33.4
457				33.8
	+50			34.2
458				34.5

Gr Rod

Lt

R

Rt.

Sta.	+	Δ	-	Grade,
458	+50			34.8
459				35.2
	+50			35.6
460				35.9
	+50			36.3
461				36.8
	+50			37.5
462				38.2
	+50			38.9
463				39.9
	+50			41.0

Gr. Rad.

ht

E

Rt

Sta	+	π	-	Grade
464				42.1
	+50			43.2
465				43.8
B.M.				953.52
	+50			43.9
466				43.6
	+50			42.9
467				41.6
	+50			39.9
	+71			39.1
468				37.8
	+50			35.3
B.M.				917.61

Gr. Rod

Lt

£

Rt

U.S.G.S. 21' Lt Sta 465+49

Top M. Cor. #19

Sta

+

π

-

Grade

Dr. 6 - BK 101

Topography

North County Line Road from P.I.
Sta. 311+50.17 to Sta. 342+00

5/4/38

For Alignment refer to Book 101
Drawer #6

Gravelled
Road.
11 11

17

16

13 11

15

14

13 11

13

12

12 12

311 + 50.17 = P.I. - Monument.

+88 T.P. 32'

Brush
@
33'

Brush
@
33' line

Ditch 4' x 2'

60°

33'

35' 2'

+63 T.P. 32'
+60 P.C.

Ditch 4' x 2'

+32'

33'

34' 33'

+10

+39 T.P. 32'

+61 T.P. 32'

34' 34'

43'

+74

Meadow Land

B.W. Fencing

Meadow Land

+00 T.P. 31'

+76 T.P. 31'

35' 43'

43'

26

6-500134
Road.
11 10

25

24

11 11

23

22

11 10

21

20

11 11

19

Meadow

X

Brush
@
33' line

34

Low Road.
Water stands to
level of road.
If lowest here it is
under water

X

X

34

W. Fencing

38.7

34

X

X

+29 T.P. 32'

+17 T.P. 32'

Brush
@
33' line

+33 T.P. 32'

+62 T.P. 32'

+33 T.P. 32'

Field Entr.
320+00 ±
15" x 20" C.M.

+08 T.P. 32'

32

14 8

31

30

11 10

29

28

14 10

27

26

Good
Scattered
Trees
out
40'

+F3 T.P. 32'

15'

+52 C.M. 12" x 21' = #63-6

Grass land

+74 Dm. Ent. 10' d. it

16' Field Ent. 474

+57 T.P. 32'

+23 F.C.

34

35

+30 F.C.

+30 F.C.

+67 Basin Fence.

34

80°

Brush
35' line

+30 T.P. 32'

35

+05 T.P. 32'

Brush 35' line

35

+80 T.P. 32'

Wooden

+62 T.P. 32'

40

11 10

+50 End Gravel }
Beg. Blacktop }

X

39

38

12 9

37

36

11 12

35

34

14 11

173 R.P. 28

Meadow

+26 T.P. 28'

+75 R.P. 28'

40400

Estimated

Cultivated

Blw fencing

10 150

L 27

+150 Rod 6'

+30 R

90°

L 35

53

150 Wye Conn.
20' Back Top

+30 T.P. 27'

48" W.M. Fence, Iron Post

97

Bethany

Cemetery

+42 R.P. 22'

W 60°

+19

250'

Turtle Lake (Rd. 24' from
Black Top)

374 15.39

+87 R.P. 27'

90°

+87 R.P. 43'

+54 R.P. 32'

90°

+20

33

Grass Land

+22 T.P. 32'

Cultivated

+12 T.P. 32'

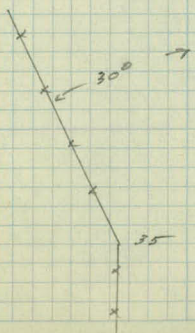
⁴
Black Top.

42

9 9

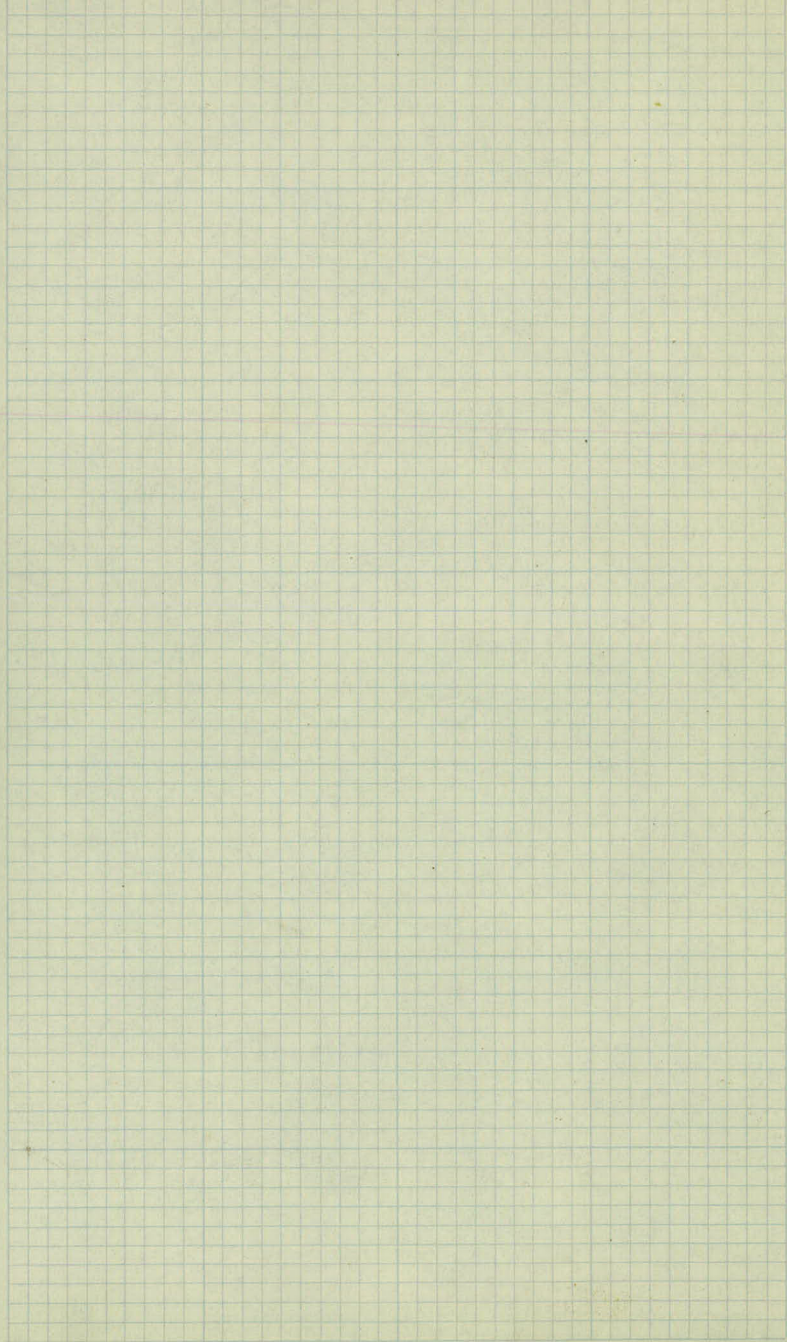
41

9 9



+40 F.C.

+50 T.R. 28'



7

North Co. Line Road.

Cross Section from P.I.

Sta. 311+50.17 to Sta. 344

5/4/38

Sta.	+	x	-	Elev.
B.M.	5.21	899.16		893.95
311 + 50 ¹²				894.1
312				93.9
+ 50				93.8
313				93.8
+ 50				93.8
314				93.9
+ 50				94.0
315				94.2
+ 50				94.0
316				94.1
+ 34		South Ditch		94.0
+ 58		North Ditch		90.5

Lt.

E

Rt.

8

Spike in 6" Poplar 85' Rt. 57 213+90

7.6	7.6	8.5	8.1	5.5	5.5	8.2	8.3	7.6	7.6	7.6
33	33	32	24	14.5	16	25	33	33	37	50

7.1	7.5	8.8	8.4	5.2	5.2	6.2	8.8	7.1	8.0	8.0
30	33	32	25	16	5.3	12	17	25	32	33
									50	

7.5	7.5	8.5	8.3	5.7	5.4	8.2	8.2	6.6	6.1	
50	33	32	24	17	5.4	16	25	32	33	50

7.8	7.8	8.8	8.2	5.9	5.5	7.9	8.1	6.6	5.6	
50	33	32	24	16	5.4	16	25	32	33	50

7.8	7.7	8.6	8.3	7.7	5.6	5.5	8.4	8.8	8.0	7.0
50	33	32	26	22	16	5.4	16	25	32	33
									50	

8.0	7.8	8.9	8.4	7.6	5.6	5.5	8.5	8.5	7.7	7.2
50	33	32	24	21	16	5.3	16	24	32	33
									50	

7.2	6.8	8.5	8.3	5.2	5.7	8.5	8.6	7.3	6.8	
50	33	32	25	16	5.2	16	26	32	33	50

6.9	6.6	8.4	8.4	7.2	5.1	5.7	8.3	8.5	7.2	7.2
50	33	32	25	22	17	5.0	14	27	32	33
									50	

7.3	7.1	8.8	8.7	7.1	5.1	5.4	8.3	8.6	7.2	7.1
50	33	32	24	24	16	5.2	12	27	32	33
									50	

7.2	7.6	9.0	8.6	5.7	5.2	8.7	9.4	8.0	8.4	
50	33	32	24	17	5.1	14	27	32	33	50

7.4	7.4	8.3	8.3	5.6	5.4	7.0	8.8	7.7	7.3	7.0
100	50	32	27	15	5.2	12	17	27	32	33
									50	100

8.8	8.8	8.9								
100	60	50	8.7							

Sta	+	T	-	Elev
-----	---	---	---	------

899.16

317

894.1

+50

94.1

318

93.9

+50

93.9

T.P

5.97

898.33

6.80

892.36

319

93.5

+50

92.9

320

92.1

+50

91.6

321

91.2

+50

91.1

X

322

91.4

+50

91.8

4 2 R

$\frac{7.3}{50} \frac{7.6}{33} \frac{8.7}{32} \frac{8.5}{27} \frac{7.5}{19} \frac{5.5}{14} 5.1$ $\frac{5.5}{13} \frac{7.7}{24} \frac{8.7}{28} \frac{8.8}{32} \frac{7.6}{33} \frac{7.6}{50}$

$\frac{7.4}{50} \frac{7.6}{33} \frac{8.8}{32} \frac{8.4}{27} \frac{5.4}{14} 5.1$ $\frac{5.4}{11} \frac{7.3}{18} \frac{8.6}{27} \frac{8.7}{32} \frac{7.6}{33} \frac{7.5}{50}$

$\frac{7.5}{50} \frac{7.4}{33} \frac{8.2}{32} \frac{7.4}{27} \frac{5.7}{16} 5.3$ $\frac{5.5}{12} \frac{6.5}{14} \frac{8.6}{27} \frac{8.7}{32} \frac{7.4}{33} \frac{6.9}{50}$

$\frac{7.5}{50} \frac{7.4}{33} \frac{8.2}{32} \frac{8.2}{26} \frac{7.3}{19} \frac{5.6}{13} 5.3$ $\frac{5.5}{12} \frac{6.9}{17} \frac{8.1}{26} \frac{8.2}{32} \frac{7.5}{33} \frac{7.0}{50}$

$\frac{6.7}{50} \frac{6.2}{33} \frac{7.5}{32} \frac{7.3}{27} \frac{6.4}{18} \frac{5.1}{13} 4.8$ $\frac{4.9}{10} \frac{6.5}{17} \frac{7.4}{26} \frac{7.4}{32} \frac{6.8}{33} \frac{6.3}{50}$

$\frac{6.6}{50} \frac{6.7}{33} \frac{7.4}{32} \frac{7.4}{27} \frac{5.6}{13} 5.4$ $\frac{5.9}{13} \frac{6.8}{18} \frac{7.4}{32} \frac{6.7}{33} \frac{6.7}{50}$

$\frac{6.5}{50} \frac{6.4}{34} \frac{7.1}{32} \frac{7.5}{18} \frac{6.4}{16} 6.2$ $\frac{6.4}{14} \frac{7.5}{20} \frac{7.5}{20} \frac{6.8}{33} \frac{6.6}{50}$

$\frac{6.6}{50} \frac{6.7}{33} \frac{7.4}{32} \frac{7.5}{25} \frac{7.2}{21} \frac{6.6}{16} 6.7$ $\frac{6.9}{16} \frac{7.7}{19} \frac{7.2}{33} \frac{7.2}{50}$

$\frac{6.8}{50} \frac{6.8}{33} \frac{7.4}{32} \frac{7.7}{24} \frac{7.2}{17} \frac{7.1}{14} 7.1$ $\frac{7.6}{12} \frac{7.9}{17} \frac{8.0}{24} \frac{7.6}{26} \frac{7.2}{32} \frac{7.0}{34} \frac{7.0}{50}$

Elev. Standing Water

$\frac{7.4}{50} \frac{6.8}{33} \frac{7.9}{32} \frac{8.0}{24} \frac{7.7}{17} \frac{7.3}{14} 7.2$ $\frac{7.3}{11} \frac{8.0}{16} \frac{8.4}{21} \frac{7.8}{32} \frac{7.1}{33} \frac{7.1}{50}$

$\frac{6.7}{50} \frac{6.8}{33} \frac{7.4}{32} \frac{7.7}{22} \frac{7.4}{16} \frac{7.1}{14} 6.9$ $\frac{7.2}{13} \frac{7.8}{18} \frac{8.0}{23} \frac{7.7}{26} \frac{7.4}{32} \frac{7.1}{33} \frac{7.1}{50}$

$\frac{6.6}{50} \frac{6.6}{33} \frac{7.3}{32} \frac{7.3}{17} \frac{6.8}{15} 6.5$ $\frac{6.6}{13} \frac{7.7}{19} \frac{8.1}{22} \frac{7.7}{26} \frac{7.7}{32} \frac{7.1}{33} \frac{7.1}{50}$

512. + K - Elev.

898.33

313 892.0

+50 91.9

324 92.5

+50 93.3

315 94.0

316 94.3

+50 94.4

327 94.5

+50 94.1

318 93.8

319 93.4

330 93.7

T.P. 11.44 905.19 4.58 893.75

Lt.

E

Rt.

10

$$\frac{65}{50} \quad \frac{65}{33} \quad \frac{71}{32} \quad \frac{71}{24} \quad \frac{77}{22} \quad \frac{75}{18} \quad \frac{66}{15} \quad \frac{63}{12} \quad \frac{66}{12} \quad \frac{72}{16} \quad \frac{80}{19} \quad \frac{82}{22} \quad \frac{76}{26} \quad \frac{77}{32} \quad \frac{65}{33} \quad \frac{65}{50}$$

$$\frac{66}{50} \quad \frac{66}{33} \quad \frac{71}{32} \quad \frac{75}{20} \quad \frac{66}{18} \quad \frac{64}{11} \quad \frac{67}{11} \quad \frac{73}{14} \quad \frac{74}{19} \quad \frac{81}{21} \quad \frac{81}{25} \quad \frac{76}{27} \quad \frac{74}{37} \quad \frac{65}{33} \quad \frac{67}{50}$$

$$\frac{66}{33} \quad \frac{70}{32} \quad \frac{71}{25} \quad \frac{71}{22} \quad \frac{66}{15} \quad \frac{67}{13} \quad \frac{58}{15} \quad \frac{63}{15} \quad \frac{75}{20} \quad \frac{78}{24} \quad \frac{72}{32} \quad \frac{67}{33} \quad \frac{67}{50}$$

$$\frac{65}{50} \quad \frac{65}{33} \quad \frac{71}{32} \quad \frac{69}{22} \quad \frac{61}{20} \quad \frac{61}{18} \quad \frac{53}{14} \quad \frac{50}{13} \quad \frac{53}{13} \quad \frac{68}{19} \quad \frac{71}{24} \quad \frac{72}{34} \quad \frac{66}{35} \quad \frac{66}{50}$$

$$\frac{65}{50} \quad \frac{65}{33} \quad \frac{70}{32} \quad \frac{67}{32} \quad \frac{63}{21} \quad \frac{60}{17} \quad \frac{45}{14} \quad \frac{43}{13} \quad \frac{47}{13} \quad \frac{57}{18} \quad \frac{64}{19} \quad \frac{70}{24} \quad \frac{71}{32} \quad \frac{65}{33} \quad \frac{65}{50}$$

$$\frac{68}{50} \quad \frac{68}{33} \quad \frac{71}{32} \quad \frac{71}{22} \quad \frac{63}{18} \quad \frac{49}{18} \quad \frac{43}{13} \quad \frac{40}{13} \quad \frac{44}{13} \quad \frac{60}{21} \quad \frac{67}{25} \quad \frac{69}{32} \quad \frac{67}{33} \quad \frac{67}{50}$$

$$\frac{65}{50} \quad \frac{65}{34} \quad \frac{69}{33} \quad \frac{65}{20} \quad \frac{46}{14} \quad \frac{39}{18} \quad \frac{40}{18} \quad \frac{65}{21} \quad \frac{68}{33} \quad \frac{43}{34} \quad \frac{43}{50}$$

$$\frac{66}{50} \quad \frac{65}{33} \quad \frac{67}{32} \quad \frac{63}{22} \quad \frac{56}{18} \quad \frac{43}{14} \quad \frac{38}{14} \quad \frac{37}{14} \quad \frac{41}{18} \quad \frac{65}{22} \quad \frac{69}{30} \quad \frac{41}{31} \quad \frac{40}{50}$$

$$\frac{63}{50} \quad \frac{62}{34} \quad \frac{66}{33} \quad \frac{63}{21} \quad \frac{56}{17} \quad \frac{48}{14} \quad \frac{42}{15} \quad \frac{44}{15} \quad \frac{51}{20} \quad \frac{67}{24} \quad \frac{71}{32} \quad \frac{60}{34} \quad \frac{63}{50}$$

$$\frac{68}{50} \quad \frac{68}{33} \quad \frac{73}{32} \quad \frac{73}{24} \quad \frac{67}{22} \quad \frac{64}{18} \quad \frac{49}{13} \quad \frac{45}{13} \quad \frac{49}{13} \quad \frac{56}{18} \quad \frac{77}{21} \quad \frac{77}{32} \quad \frac{70}{33} \quad \frac{70}{50}$$

$$\frac{64}{50} \quad \frac{64}{34} \quad \frac{69}{33} \quad \frac{67}{21} \quad \frac{55}{17} \quad \frac{53}{14} \quad \frac{49}{13} \quad \frac{51}{13} \quad \frac{56}{19} \quad \frac{72}{21} \quad \frac{72}{32} \quad \frac{63}{33} \quad \frac{63}{50}$$

$$\frac{66}{33} \quad \frac{65}{32} \quad \frac{72}{24} \quad \frac{64}{22} \quad \frac{64}{19} \quad \frac{47}{13} \quad \frac{46}{13} \quad \frac{48}{13} \quad \frac{58}{18} \quad \frac{70}{22} \quad \frac{68}{23} \quad \frac{65}{34} \quad \frac{65}{50}$$

Sta.	+	π	-	Elev.
		905.19		
330+50				894.0 .
331+00				94.6 .
+55				95.5 .
+72	Sec. thru Ent. Rt + Lt.			95.6 .
332				95.7 .
T.P.	5.20	906.58 ✓	3.81	901.38 .
332+10				95.7. x
+82	Sec. thru culvert			95.7. x
333				96.5 .
+80				98.0 .
334				899.6 .
+50				901.00 .
335				02.3 .

14.

2

104.

11

$\frac{135}{50}$ $\frac{135}{33}$ $\frac{138}{32}$ $\frac{140}{25}$ $\frac{139}{22}$ $\frac{130}{17}$ $\frac{114}{13}$ $\frac{112}{11}$ $\frac{114}{11}$ $\frac{126}{17}$ $\frac{126}{20}$ $\frac{140}{22}$ $\frac{140}{33}$ $\frac{132}{34}$ $\frac{132}{50}$

$\frac{131}{50}$ $\frac{131}{34}$ $\frac{131}{33}$ $\frac{138}{24}$ $\frac{133}{19}$ $\frac{111}{13}$ $\frac{106}{11}$ $\frac{108}{11}$ $\frac{119}{15}$ $\frac{123}{23}$ $\frac{137}{27}$ $\frac{137}{32}$ $\frac{132}{34}$ $\frac{122}{50}$

$\frac{97}{50}$ $\frac{97}{34}$ $\frac{111}{33}$ $\frac{111}{25}$ $\frac{100}{31}$ $\frac{98}{14}$ $\frac{97}{11}$ $\frac{98}{11}$ $\frac{103}{18}$ $\frac{130}{24}$ $\frac{132}{30}$ $\frac{93}{33}$ $\frac{93}{50}$

$\frac{85}{50}$ $\frac{91}{22}$ $\frac{97}{11}$ $\frac{96}{9}$ $\frac{98}{9}$ $\frac{100}{31}$ $\frac{95}{33}$ $\frac{101}{50}$

$\frac{74}{50}$ $\frac{81}{18}$ $\frac{95}{16}$ $\frac{97}{12}$ $\frac{95}{10}$ $\frac{98}{10}$ $\frac{106}{16}$ $\frac{124}{25}$ $\frac{124}{30}$ $\frac{118}{31}$ $\frac{120}{50}$

Nail T.P.-134

$\frac{94}{50}$ $\frac{101}{34}$ $\frac{122}{31}$ $\frac{118}{24}$ $\frac{111}{21}$ $\frac{109}{11}$ $\frac{113}{9}$ $\frac{121}{15}$ $\frac{139}{50}$

$\frac{113}{50}$ $\frac{122}{33}$ $\frac{123}{31}$ $\frac{130}{19}$ $\frac{130}{16}$ $\frac{115}{15}$ $\frac{109}{11}$ $\frac{112}{14}$ $\frac{124}{17}$ $\frac{140}{17}$ $\frac{142}{50}$

$\frac{123}{50}$ $\frac{129}{38}$ $\frac{129}{23}$ $\frac{108}{16}$ $\frac{103}{11}$ $\frac{101}{10}$ $\frac{102}{10}$ $\frac{134}{19}$ $\frac{136}{50}$

$\frac{94}{50}$ $\frac{90}{33}$ $\frac{112}{29}$ $\frac{110}{24}$ $\frac{88}{18}$ $\frac{86}{15}$ $\frac{90}{15}$ $\frac{108}{21}$ $\frac{110}{28}$ $\frac{102}{30}$ $\frac{102}{50}$

$\frac{63}{50}$ $\frac{65}{33}$ $\frac{85}{27}$ $\frac{98}{24}$ $\frac{74}{15}$ $\frac{70}{14}$ $\frac{72}{14}$ $\frac{91}{24}$ $\frac{97}{29}$ $\frac{47}{33}$ $\frac{50}{50}$

$\frac{35}{50}$ $\frac{26}{33}$ $\frac{85}{26}$ $\frac{82}{21}$ $\frac{60}{17}$ $\frac{54}{15}$ $\frac{59}{15}$ $\frac{83}{23}$ $\frac{86}{27}$ $\frac{14}{33}$ $\frac{17}{50}$

$\frac{18}{50}$ $\frac{08}{33}$ $\frac{70}{27}$ $\frac{70}{22}$ $\frac{48}{16}$ $\frac{43}{14}$ $\frac{46}{14}$ $\frac{73}{22}$ $\frac{73}{27}$ $\frac{06}{33}$ $\frac{09}{50}$

Sta.	+	π	-	Elev.
		906.58		
T.P.	8.55	912.29 ✓	2.84	903.74 ✓
336+50				03.4
336+08				04.5
+15				04.6
+50				05.3
+95				06.3
337				06.5
+15.39				06.7
+28				06.8
+35				06.9
+48				07.0
+57				07.0

17.

2

21.

$$\frac{57}{50} \quad \frac{52}{34} \quad \frac{114}{24} \quad \frac{110}{20} \quad \frac{51}{15} \quad \frac{89}{15} \quad \frac{92}{15} \quad \frac{117}{22} \quad \frac{118}{27} \quad \frac{62}{33} \quad \frac{71}{50}$$

$$\frac{48}{50} \quad \frac{38}{33} \quad \frac{86}{25} \quad \frac{97}{18} \quad \frac{79}{14}$$

$$\frac{78}{14} \quad \frac{80}{23} \quad \frac{103}{27} \quad \frac{106}{33} \quad \frac{68}{50}$$

$$\frac{43}{50} \quad \frac{37}{34} \quad \frac{77}{15} \quad \frac{77}{15} \quad \frac{78}{13} \quad \frac{103}{23} \quad \frac{104}{27} \quad \frac{67}{33} \quad \frac{78}{50}$$

$$\frac{31}{50} \quad \frac{36}{33} \quad \frac{74}{13} \quad \frac{70}{12} \quad \frac{73}{21} \quad \frac{97}{25} \quad \frac{98}{31} \quad \frac{65}{39} \quad \frac{73}{50}$$

$$\frac{32}{50} \quad \frac{32}{32} \quad \frac{66}{15} \quad \frac{60}{12} \quad \frac{64}{18} \quad \frac{82}{28} \quad \frac{83}{32} \quad \frac{56}{32} \quad \frac{72}{50}$$

$$\frac{26}{50} \quad \frac{29}{32} \quad \frac{64}{15} \quad \frac{62}{13} \quad \frac{58}{14} \quad \frac{61}{14} \quad \frac{64}{50}$$

$$\frac{24}{50} \quad \frac{26}{32} \quad \frac{59}{11} \quad \frac{56}{21} \quad \frac{57}{50} \quad \frac{59}{100} \quad \frac{57}{150} \quad \frac{50}{200} \quad \frac{47}{250}$$

$$\frac{24}{50} \quad \frac{26}{32} \quad \frac{59}{11} \quad \frac{55}{21} \quad \frac{56}{28} \quad \frac{56}{50} \quad \frac{62}{100} \quad \frac{62}{137} \quad \frac{52}{169} \quad \frac{48}{200} \quad \frac{48}{229}$$

$$\frac{18}{50} \quad \frac{20}{32} \quad \frac{54}{15} \quad \frac{57}{11} \quad \frac{54}{21} \quad \frac{56}{23} \quad \frac{66}{25} \quad \frac{69}{50} \quad \frac{67}{100} \quad \frac{64}{100} \quad \frac{44}{188} \quad \frac{47}{200} \quad \frac{49}{224}$$

$$\frac{13}{50} \quad \frac{16}{31} \quad \frac{56}{14} \quad \frac{53}{21} \quad \frac{54}{14} \quad \frac{69}{18} \quad \frac{69}{28} \quad \frac{68}{50} \quad \frac{68}{70} \quad \frac{41}{80} \quad \frac{42}{92} \quad \frac{54}{111} \quad \frac{39}{117} \quad \frac{46}{135}$$

$$\frac{13}{50} \quad \frac{16}{31} \quad \frac{56}{14} \quad \frac{53}{21} \quad \frac{54}{14} \quad \frac{69}{18} \quad \frac{69}{28} \quad \frac{68}{50} \quad \frac{68}{70} \quad \frac{41}{80} \quad \frac{42}{92} \quad \frac{54}{111} \quad \frac{39}{117} \quad \frac{46}{135}$$

Sta.	+	π	-	Elev.
		912.29		
337+89				907.1
338				07.2
+34				07.4
+42				07.5
339				07.8
+50				07.4
340				06.7
+50				06.0
341				05.5
+50				04.9
				04.7
T.P.	2.66	50693 ✓	5.02 ✓	904.27 ✓
B.M.			2.32 ✓	504.61 ✓
				904.56

Book 101 - D. 6 - 139

OK

Lt.

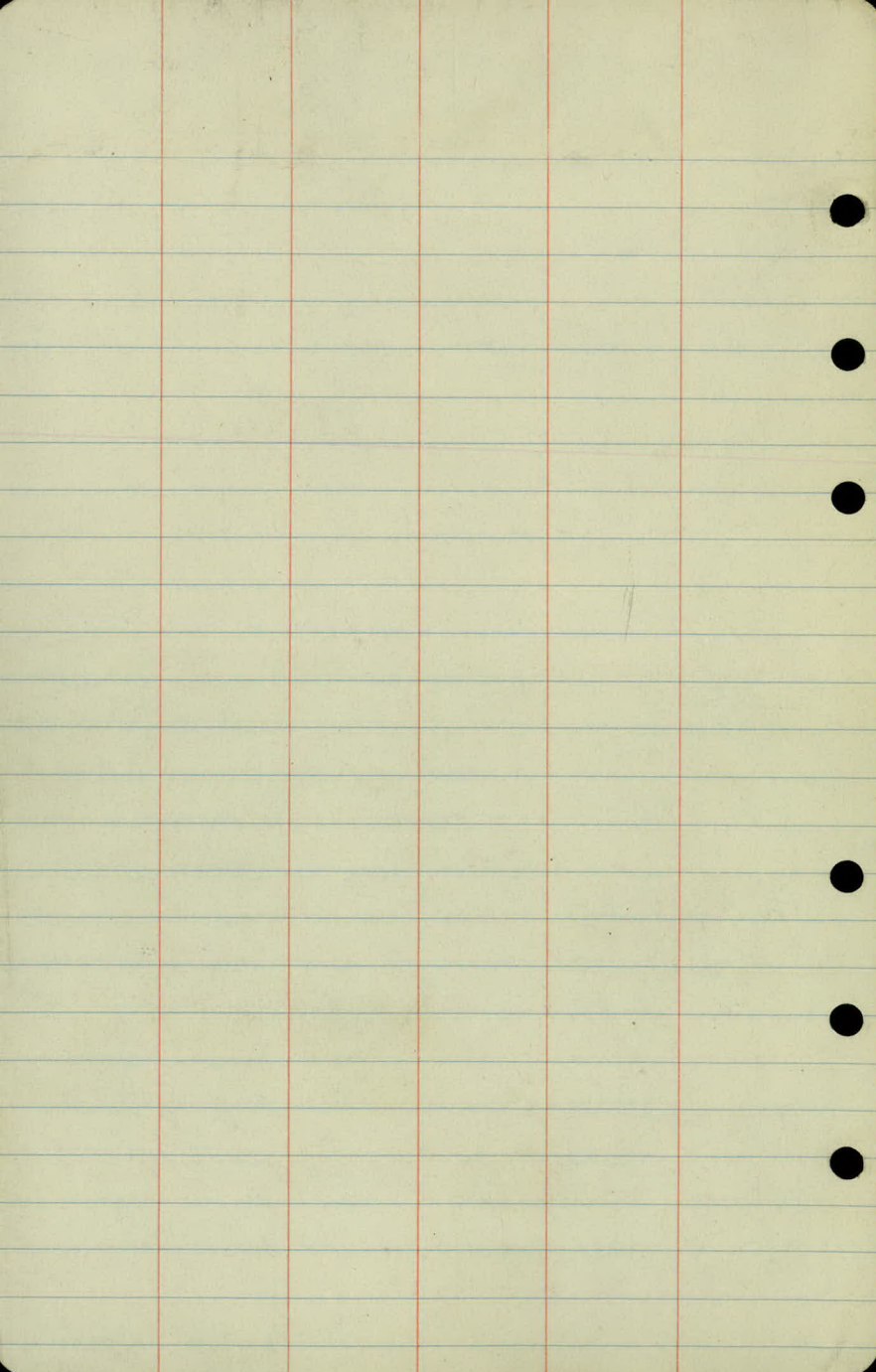
Z

Rt.

13

 $\frac{45}{50} \quad \frac{4.7}{103}$
 $\frac{07}{50} \quad \frac{12}{31} \quad \frac{55}{13} \quad \frac{52}{14} \quad \frac{54}{20} \quad \frac{68}{27} \quad \frac{68}{31} \quad \frac{43}{54} \quad \frac{34}{55} \quad \frac{49}{68} \quad \frac{47}{71}$
 $\frac{00}{50} \quad \frac{12}{31} \quad \frac{54}{14} \quad \frac{51}{13} \quad \frac{52}{17} \quad \frac{56}{24} \quad \frac{53}{32} \quad \frac{41}{44} \quad \frac{34}{46} \quad \frac{50}{55} \quad \frac{48}{63} \quad \frac{40}{73} \quad \frac{46}{76}$
 $\frac{10}{50} \quad \frac{16}{34} \quad \frac{52}{14} \quad \frac{49}{14} \quad \frac{50}{18} \quad \frac{53}{22} \quad \frac{54}{25} \quad \frac{47}{34} \quad \frac{49}{38} \quad \frac{42}{50} \quad \frac{46}{64}$
 $\frac{10}{50} \quad \frac{15}{32} \quad \frac{65}{26} \quad \frac{64}{18} \quad \frac{51}{14} \quad \frac{48}{15} \quad \frac{47}{19} \quad \frac{54}{32} \quad \frac{49}{36} \quad \frac{42}{44} \quad \frac{46}{60}$
 $\frac{17}{50} \quad \frac{21}{34} \quad \frac{69}{28} \quad \frac{69}{22} \quad \frac{51}{13} \quad \frac{45}{11} \quad \frac{46}{26} \quad \frac{51}{36} \quad \frac{61}{42} \quad \frac{22}{45} \quad \frac{23}{58} \quad \frac{21}{56} \quad \frac{37}{71}$
 $\frac{24}{50} \quad \frac{29}{34} \quad \frac{72}{28} \quad \frac{73}{22} \quad \frac{52}{12} \quad \frac{49}{15} \quad \frac{50}{19} \quad \frac{62}{22} \quad \frac{61}{27} \quad \frac{23}{33} \quad \frac{27}{38} \quad \frac{48}{50}$
 $\frac{38}{50} \quad \frac{43}{33} \quad \frac{75}{29} \quad \frac{75}{24} \quad \frac{56}{15} \quad \frac{56}{9} \quad \frac{64}{16} \quad \frac{67}{21} \quad \frac{81}{25} \quad \frac{82}{28} \quad \frac{73}{50}$
 $\frac{58}{50} \quad \frac{67}{33} \quad \frac{90}{31} \quad \frac{91}{23} \quad \frac{73}{19} \quad \frac{67}{16} \quad \frac{63}{14} \quad \frac{71}{23} \quad \frac{97}{50}$
 $\frac{93}{50} \quad \frac{103}{36} \quad \frac{105}{30} \quad \frac{101}{23} \quad \frac{76}{17} \quad \frac{68}{10} \quad \frac{78}{15} \quad \frac{78}{23} \quad \frac{122}{31} \quad \frac{127}{50}$
 $\frac{125}{50} \quad \frac{125}{28} \quad \frac{120}{24} \quad \frac{82}{16} \quad \frac{74}{9} \quad \frac{79}{11} \quad \frac{81}{24} \quad \frac{120}{50}$
 $\frac{126}{50} \quad \frac{126}{30} \quad \frac{120}{24} \quad \frac{85}{16} \quad \frac{76}{11} \quad \frac{83}{23} \quad \frac{109}{26} \quad \frac{110}{50}$

24" Cottonwood 75' Rt 351+45



No. Co. Line

Slope Stakes.

316 - 337.

Sta	+	π	-	Grade	Atb Grade
B.M.	4.87	898.82		892.95	
316				93.9	8.8 90.0
+501				93.9	8.78 90.05
317					8.72 90.1
+50					8.68 90.15
318					8.62 90.2
+50					8.58 90.25
319					8.52 90.3
T.P.	5.20	897.74	6.28	892.54	
+50				93.9	7.40 90.35
320					7.34 90.4
+50					7.3 90.45
321					7.24 90.5

Grade Rod

LH

R

Rt.

Spk in 6" Paper 85' Rk 318100

$$4.9 \quad R. 3.9 \quad \begin{array}{r} 4.9 \\ -9.0 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ +0.2 \\ \hline \end{array} \quad \begin{array}{r} 5.7 \\ -1.0 \\ \hline \end{array} \quad R. 2.9 / 330$$

$$4.9 \quad R. 3.9 \quad \begin{array}{r} 4.9 \\ -9.0 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 5.8 \\ 0.9 \\ \hline \end{array} \quad R. 3.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 4.9 \\ -0.8 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ -0.1 \\ \hline \end{array} \quad \begin{array}{r} 4.72 \\ +0.2 \\ \hline \end{array} \quad R. 4.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 5.68 \\ -0.8 \\ \hline \end{array} \quad \begin{array}{r} 4.7 \\ +0.2 \\ \hline \end{array} \quad \begin{array}{r} 5.68 \\ -0.8 \\ \hline \end{array} \quad R. 3.0$$

$$4.9 \quad R. 2.9 \quad \begin{array}{r} 5.72 \\ -0.8 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 5.02 \\ -0.7 \\ \hline \end{array} \quad R. 3.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 5.58 \\ -0.7 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ 0.0 \\ \hline \end{array} \quad \begin{array}{r} 5.58 \\ -0.7 \\ \hline \end{array} \quad R. 3.0$$

$$4.9 \quad R. 4.9 \quad \begin{array}{r} 5.62 \\ -0.7 \\ \hline \end{array} \quad \begin{array}{r} 5.2 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 5.52 \\ -0.6 \\ \hline \end{array} \quad R. 3.0$$

Nail in T.R. Rk +

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.9 \\ -0.6 \\ \hline \end{array} \quad \begin{array}{r} 4.9 \\ -0.9 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ -0.6 \\ \hline \end{array} \quad R. 3.0$$

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.55 \\ -0.6 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ -1.5 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ -0.6 \\ \hline \end{array} \quad R. 2.90$$

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.3 \\ -0.5 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ -1.2 \\ \hline \end{array} \quad \begin{array}{r} 4.3 \\ -0.5 \\ \hline \end{array} \quad R. 3.0$$

$$R. 3.0 \quad \begin{array}{r} 4.24 \\ -0.4 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ -1.2 \\ \hline \end{array} \quad \begin{array}{r} 4.24 \\ -0.4 \\ \hline \end{array} \quad R. 3.0$$

Sta	+	π	-	Grade	Pkts. Gr.
		897.74			
321	+50			93.9	72.0 90.55
322					7.19 90.6
	+50				7.1 90.65
323					7.05 90.7
	+50				7.0 90.75
324	4.66	898.81	5.59	896.15	8.0 90.8
				93.9	
	+50				7.95 90.85
325					7.9 90.9
	+50				7.85 90.95
326					7.8 91.0
	+50				91.05

60 Rod

LT

R

RT

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.2 \\ -0.4 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ -1.6 \\ \hline \end{array} \quad \begin{array}{r} 4.2 \\ -0.4 \\ \hline \end{array} \quad R. 3.0$$

$$3.8 \quad R. 2.9 \quad \begin{array}{r} 4.2 \\ -0.4 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ -1.9 \\ \hline \end{array} \quad \begin{array}{r} 4.4 \\ -0.3 \\ \hline \end{array} \quad R. 3.0$$

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.1 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 5.4 \\ -1.6 \\ \hline \end{array} \quad \begin{array}{r} 4.1 \\ -0.3 \\ \hline \end{array} \quad R. 3.0$$

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.05 \\ -0.3 \\ \hline \end{array} \quad \begin{array}{r} 5.5 \\ -1.7 \\ \hline \end{array} \quad \begin{array}{r} 4.05 \\ -0.3 \\ \hline \end{array} \quad R. 3.0$$

$$3.8 \quad R. 3.0 \quad \begin{array}{r} 4.0 \\ -0.2 \\ \hline \end{array} \quad \begin{array}{r} 5.6 \\ -1.8 \\ \hline \end{array} \quad \begin{array}{r} 3.0 \\ -1.2 \\ \hline \end{array} \quad R. 2.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 5.0 \\ -0.1 \\ \hline \end{array} \quad \begin{array}{r} 6.1 \\ -1.2 \\ \hline \end{array} \quad \begin{array}{r} 5.0 \\ -0.1 \\ \hline \end{array} \quad R. 3.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 5.95 \\ -0.1 \\ \hline \end{array} \quad \begin{array}{r} 5.3 \\ -0.4 \\ \hline \end{array} \quad \begin{array}{r} 5.95 \\ -0.1 \\ \hline \end{array} \quad R. 2.0$$

$$4.9 \quad R. 3.0 \quad \begin{array}{r} 4.5 \\ -0.0 \\ \hline \end{array} \quad \begin{array}{r} 4.8 \\ -0.1 \\ \hline \end{array} \quad \begin{array}{r} 5.9 \\ -1.0 \\ \hline \end{array} \quad R. 2.0$$

4.9

Sta	+	898.81	-	Grade	Pitch, Grade
T.P.		π			
	6.68	900.80	9.69	894.12	
T.P.	7.83	906.21	2.42	898.38	
327				93.9	91.1
	150				91.15
328					91.2
	150				91.25
329					91.3
				93.9	
	150				91.35
330					91.90
	150				91.45
331				93.9	91.5
	150			94.1	
332	172			94.3	

Gr. Rod.

LA

to

EF

Sta.	+	π	-	Grade
------	---	-------	---	-------

906.21

372			946
-----	--	--	-----

710				947
-----	--	--	--	-----

152				95.5
-----	--	--	--	------

353				94.7
-----	--	--	--	------

150				981
-----	--	--	--	-----

534				99.5
-----	--	--	--	------

1301				900.9
------	--	--	--	-------

935				02.3
-----	--	--	--	------

150				03.6
-----	--	--	--	------

336	408			04.9
-----	-----	--	--	------

J.P.	7.98	910.48	3.27	903.00
------	------	--------	------	--------

415				25.0
-----	--	--	--	------

Gr. Rad.

lt.

R

Rt

$$10.7 \quad 240 / \begin{array}{r} 127 \\ 1540 \end{array} \quad \begin{array}{r} 144 \\ +03 \end{array} \quad \begin{array}{r} 15.6 \\ -28 / 25.6 \end{array}$$

$$9.5 \quad 240 / \begin{array}{r} 115 \\ -20 \end{array} \quad \begin{array}{r} 96 \\ -91 \end{array} \quad \begin{array}{r} 130 \\ -35 / 230 \end{array}$$

$$8.1 \quad 240 / \begin{array}{r} 81 \\ 2400 \end{array} \quad \begin{array}{r} 82 \\ -91 \end{array} \quad \begin{array}{r} 105 \\ -29 / 208 \end{array}$$

$$6.7 \quad 240 / \begin{array}{r} 87 \\ 2400 \end{array} \quad \begin{array}{r} 66 \\ 701 \end{array} \quad \begin{array}{r} 87 \\ 2400 / 240 \end{array}$$

$$5.8 \quad 240 / \begin{array}{r} 73 \\ 2400 \end{array} \quad \begin{array}{r} 53 \\ 00 \end{array} \quad \begin{array}{r} 73 \\ 2400 / 240 \end{array}$$

$$3.9 \quad 240 / \begin{array}{r} 59 \\ 2400 \end{array} \quad \begin{array}{r} 40 \\ -91 \end{array} \quad \begin{array}{r} 70 \\ -31 / 222 \end{array}$$

$$3.6 \quad 240 / \begin{array}{r} 46 \\ 2400 \end{array} \quad \begin{array}{r} 38 \\ -91 \end{array} \quad \begin{array}{r} 57 \\ -31 / 222 \end{array}$$

$$1.3 \quad 240 / \begin{array}{r} 33 \\ 2400 \end{array} \quad \begin{array}{r} 18 \\ -05 \end{array} \quad \begin{array}{r} 45 \\ -32 / 22.9 \end{array}$$

Sta.

+

π

-

Grade

910.48

336 +50

03.6

195

06.3

337

06.9

B.M.

181

908.67

Gr. Rod

9.9

$$\frac{58}{-9.3}$$

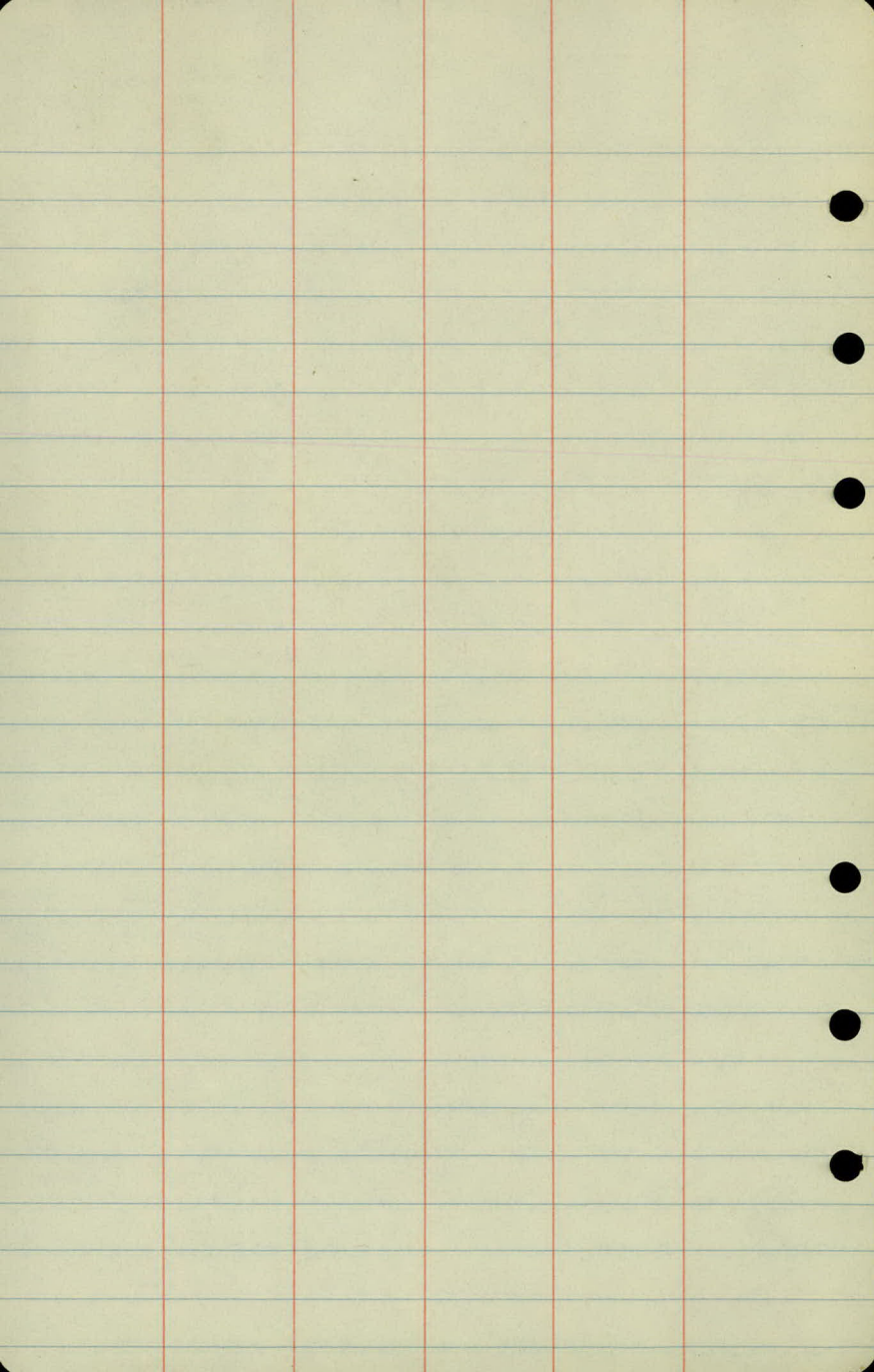
$$\frac{79}{-30/2.40}$$

4.2

$$\frac{4.2}{00}$$

$$\frac{75}{-29/20.6}$$

Nail in P.R. Lt 336+90



NO. CO. LINE.

slope stakes.

179. 10

319

+

A

-

Grade

180

815.0

+50

85.1

181

85.1

+50

85.2

182

85.2

+50

85.5

183

85.3

+50

85.4

184

85.4

+50

85.5

185

85.5

Cor. Rod.

14.

2.

121.

Sta.	+	π	-	Grade.
		894.80		

185	+50			856
-----	-----	--	--	-----

186				856
-----	--	--	--	-----

	+50			85.7
--	-----	--	--	------

187				85.7
-----	--	--	--	------

	+50			85.8
--	-----	--	--	------

188				85.8
-----	--	--	--	------

	+50			85.8
--	-----	--	--	------

189				85.8
-----	--	--	--	------

	+50			85.8
--	-----	--	--	------

190				85.8
-----	--	--	--	------

	+50			85.8
--	-----	--	--	------

Gr Rod.

Lt.

L.

Rt.

4.7

4.7

4.6

4.6

4.5

4.5

4.5

4.5

4.5

4.5

4.5

$$\frac{50}{-0.3}$$

$$\frac{49}{-0.3}$$

$$\frac{46}{-0.1}$$

$$\frac{46}{-0.1}$$

$$\frac{40}{-0.0}$$

$$\frac{5.1}{-0.6}$$

$$\frac{50}{-0.5}$$

$$\frac{49}{-0.4}$$

$$\frac{50}{-0.5}$$

$$\frac{8.8}{-4.3} / 28.5$$

$$\frac{8.8}{4.3} / 28.9$$

$$\frac{8.9}{-8.9} / 27.7$$

$$\frac{8.9}{-8.9} / 27.4$$

$$\frac{7.9}{-8.9} / 26.2$$

$$\frac{7.8}{-8.9} / 25.9$$

$$25.3 / \frac{7.6}{-3.1}$$

$$27.4 / \frac{8.3}{-2.8}$$

$$28.6 / \frac{8.7}{-4.2}$$

$$26.8 / \frac{8.1}{-1.6}$$

$$26.8 / \frac{8.1}{-1.6}$$

$$25.9 / \frac{7.5}{-3.0}$$

Sta.	+	T	-	Grade.
		890.30		
191.				85.7
	+50			85.7
192.				85.6
	+50			85.5
B.M.	3.57	889.19	4.62	885.62
193				85.5
	+50			85.5
194				85.4
	+50			85.3
195				85.3
	+50			85.2
196				85.2

$$\begin{array}{r} 585.02 \\ 7.68 \\ \hline 90.30 \end{array}$$

Gr. Rod

Lt.

L

Rt.

$$\begin{array}{r} 4.6 \\ 28.2 / \begin{array}{r} 7.0 \\ -2.4 \end{array} \end{array} \quad \begin{array}{r} 5.4 \\ -0.8 \end{array} \quad \begin{array}{r} 6.9 \\ -2.3 / 22.9 \end{array}$$

$$\begin{array}{r} 4.6 \\ 33.0 / \begin{array}{r} 4.9 \\ -12.7 \end{array} \end{array} \quad \begin{array}{r} 5.5 \\ -0.9 \end{array} \quad \begin{array}{r} 7.5 \\ -2.9 / 24.7 \end{array}$$

$$\begin{array}{r} 4.7 \\ 37.0 / \begin{array}{r} 4.2 \\ -10.5 \end{array} \end{array} \quad \begin{array}{r} 5.4 \\ -0.7 \end{array} \quad \begin{array}{r} 6.7 \\ 10.00 / 33.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ 4.2 / \begin{array}{r} 3.2 \\ -1.4 \end{array} \end{array} \quad \begin{array}{r} 5.5 \\ -0.7 \end{array} \quad \begin{array}{r} 5.3 \\ 10.15 / 33.0 \end{array}$$

Nail in Cor. Fe Rod Lt.

$$\begin{array}{r} 3.7 \\ 37.0 / \begin{array}{r} 1.3 \\ -2.9 \end{array} \end{array} \quad \begin{array}{r} 9.3 \\ -0.6 \end{array} \quad \begin{array}{r} 5.2 \\ 10.5 / 33.0 \end{array}$$

$$\begin{array}{r} 3.7 \\ 33.0 / \begin{array}{r} 0.0 \\ -1.7 \end{array} \end{array} \quad \begin{array}{r} 4.3 \\ -0.6 \end{array} \quad \begin{array}{r} 5.9 \\ 10.8 / 33.0 \end{array} \quad \begin{array}{r} 5.7 \\ 10.00 / 37.0 \end{array}$$

$$\begin{array}{r} 3.8 \\ 33.0 / \begin{array}{r} 1.9 \\ -5.2 \end{array} \end{array} \quad \begin{array}{r} 4.3 \\ -0.6 \end{array} \quad \begin{array}{r} 4.9 \\ 10.85 / 33.0 \end{array}$$

$$\begin{array}{r} 3.9 \\ 33.0 / \begin{array}{r} 1.5 \\ -4.9 \end{array} \end{array} \quad \begin{array}{r} 4.4 \\ -0.8 \end{array} \quad \begin{array}{r} 3.6 \\ 10.3 / 33.0 \end{array}$$

$$\begin{array}{r} 3.9 \\ 32.0 / \begin{array}{r} 10.6 \\ -4.5 \end{array} \end{array} \quad \begin{array}{r} 4.6 \\ -0.7 \end{array} \quad \begin{array}{r} 8.3 \\ 13.7 / 32.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33.0 / \begin{array}{r} 12.7 \\ -4.7 \end{array} \end{array} \quad \begin{array}{r} 4.6 \\ -0.6 \end{array} \quad \begin{array}{r} 0.0 \\ 10.4 / 33.0 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33.0 / \begin{array}{r} 3.6 \\ -10.4 \end{array} \end{array} \quad \begin{array}{r} 4.5 \\ -0.5 \end{array} \quad \begin{array}{r} 4.8 \\ 10.2 / 33.0 \end{array}$$

Sta	+	T	-	Grade
		889.19		
196	+50			85.1
197				85.2
	+50			85.2
T.P.	7.82	890.65	6.38	882.83
198				85.2
	+50			85.3
199				85.4
	+40			85.5
200				85.7
	+75			86.0
201				86.1
	+55			86.3

Gr Bod

11

2

21

4.1

$$33.0 / \frac{6.1}{20.0}$$

$$\frac{5.1}{-1.0}$$

$$\frac{6.8}{20.0} / 33.0$$

4.0

$$26.5 / \frac{7.5}{-2.5}$$

$$\frac{6.2}{-2.2}$$

$$\frac{7.2}{-3.2} / 23.6$$

41.0
Schrank

4.0

$$\frac{6.6}{-2.6}$$

41.0

5.5

$$25.9 / \frac{8.8}{-3.2}$$

$$\frac{7.7}{-2.2}$$

$$\frac{8.9}{-3.9} / 26.2$$

40.5

5.4

$$33.0 / \frac{7.6}{20.0}$$

$$\frac{6.7}{-1.3}$$

$$\frac{7.5}{20.0} / 33.0$$

5.3

$$33.0 / \frac{7.9}{20.0}$$

$$\frac{6.0}{-0.7}$$

$$\frac{6.1}{21.2} / 33.0$$

5.2

$$33.0 / \frac{6.2}{21.0}$$

$$\frac{5.5}{-0.3}$$

$$\frac{4.9}{20.3} / 33.0$$

5.0

$$33.0 / \frac{5.6}{21.4}$$

$$\frac{5.0}{0.0}$$

$$\frac{0.4}{20.6} / 33.0$$

4.7

$$33.0 / \frac{5.9}{20.1}$$

$$\frac{4.7}{0.0}$$

$$\frac{2.6}{21.1} / 33.0$$

4.6

$$33.0 / \frac{4.9}{21.1}$$

$$\frac{4.9}{-0.3}$$

$$\frac{5.6}{21.0} / 33.0$$

4.4

$$24.4 / \frac{7.6}{-2.8}$$

$$\frac{5.1}{-0.7}$$

$$\frac{6.7}{20.7} / 33.0$$

519.	-	X	-	Consolidate
T.P.	10.33	890.65		
202				86.5
+50				86.7
T.P.	10.33	897.68	230	887.35
203				86.9
+70		897.82 9.50 898.24 2.84 891.08		87.2
204				87.2
B.M.			0.80	896.88
+50				87.4
205				87.4
B.M.	0.94	897.82		896.88
T.P.	2.84	897.08	258	786.29
207				87.5
+50				87.5
208				87.5
+50				87.5

Gd Rod

L

L

Rt

9.2

$$241 / \begin{array}{r} 6.7 \\ -2.7 \end{array}$$

$$\begin{array}{r} 46 \\ -04 \end{array}$$

$$\begin{array}{r} 69 \\ 1208/33.9 \end{array}$$

4.0

$$320 / \begin{array}{r} 0.0 \\ 21.0 \end{array}$$

$$\begin{array}{r} 37 \\ 103 \end{array}$$

$$\begin{array}{r} 55 \\ 10.2/23.9 \end{array}$$

108

105

105

$$320 / \begin{array}{r} 56 \\ 4.7 \end{array}$$

$$\begin{array}{r} 97 \\ 108 \end{array}$$

38' Rt 204+03

38' Rt 204+09

3.6

$$23.5 / \begin{array}{r} 0.1 \\ -2.5 \end{array}$$

$$\begin{array}{r} 37 \\ -01 \end{array}$$

$$\begin{array}{r} 58 \\ -2.2/22.6 \end{array}$$

3.6

$$24.4 / \begin{array}{r} 6.4 \\ -2.8 \end{array}$$

$$\begin{array}{r} 44 \\ -0.8 \end{array}$$

$$\begin{array}{r} 61 \\ -2.5/23.5 \end{array}$$

3.6

$$24.4 / \begin{array}{r} 6.4 \\ -2.8 \end{array}$$

$$\begin{array}{r} 44 \\ -1.3 \end{array}$$

$$\begin{array}{r} 62 \\ -2.6/23.8 \end{array}$$

3.6

$$24.4 / \begin{array}{r} 6.4 \\ -2.8 \end{array}$$

$$\begin{array}{r} 48 \\ 11.2 \end{array}$$

$$\begin{array}{r} 59 \\ -2.3/23.9 \end{array}$$

Sta.

t

T

-

Grade

891.08

209

87.6

+50

87.7

210

87.8

T.R.

727

895.86

2.49

888.59

212 +50

89.0

213

89.4

+50

90.0

214

90.7

Gr. Bod.

$$3.5 \quad 23.5 / \begin{array}{r} 6.0 \\ -2.5 \end{array} \quad \begin{array}{r} 40 \\ -0.5 \end{array} \quad \begin{array}{r} 3.5 \\ -4.0 / 22.0 \end{array}$$

$$3.4 \quad 22.0 / \begin{array}{r} 5.9 \\ -2.0 \end{array} \quad \begin{array}{r} 3.3 \\ +0.1 \end{array} \quad \begin{array}{r} 5.4 \\ -2.0 / 22.0 \end{array}$$

$$6.9 \quad 24.9 / \begin{array}{r} 9.7 \\ -2.8 \end{array} \quad \begin{array}{r} 7.2 \\ -0.3 \end{array} \quad \begin{array}{r} 2.6 \\ -1.7 / 21.1 \end{array}$$

$$6.5 \quad 29.8 / \begin{array}{r} 11.1 \\ -4.6 \end{array} \quad \begin{array}{r} 7.6 \\ -1.1 \end{array} \quad \begin{array}{r} 9.7 \\ -3.2 / 25.6 \end{array}$$

$$5.7 \quad 29.2 / \begin{array}{r} 10.3 \\ -4.4 \end{array} \quad \begin{array}{r} 6.7 \\ -1.0 \end{array} \quad \begin{array}{r} 9.5 \\ -3.6 / 26.8 \end{array}$$

$$5.2 \quad 22.8 / \begin{array}{r} 9.3 \\ -4.1 \end{array} \quad \begin{array}{r} 5.2 \\ 0.6 \end{array} \quad \begin{array}{r} 9.2 \\ -4.0 / 28.0 \end{array}$$

