

Dr. 6 - BK. 100

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plat 17 Survey

FLYELL ROAD.

From No. Co. Lutz To S. T. H. 8

Road Acc't. No.

Date Filed 1936

File S. 900 P. 6.

Alignment Notes
ELWELL Grade
Anoka County.

	{	Portell
12		Bratager
<u>22</u>		Wilke
36		Gottfried
		Feist

Angle

Sta. Rt. Lt.

6+86.44 P.C.

1+12.39 P.T.

Curve Data

$D = 46^\circ$

$T = 62.0'$

$L = 112.39'$

0+68 P.I.

$51^\circ 48'$

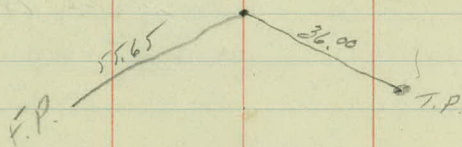
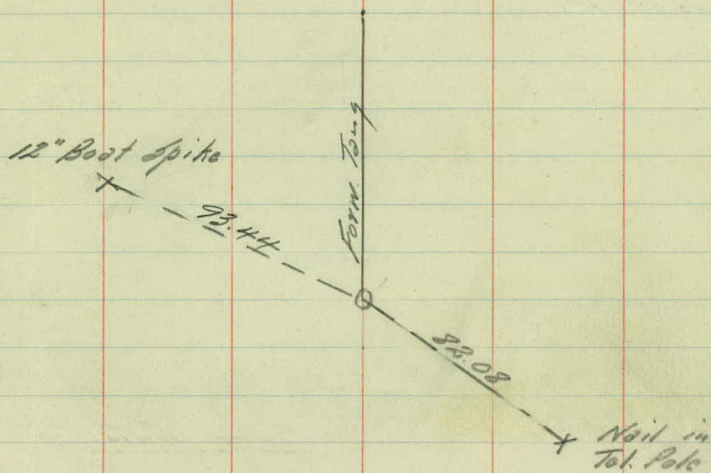
$R = 127.96'$

0 - 6045'
+25 - 11030'
+50 - 17015'
+75 - 230'
1 - 25051'
1+124 -

10+00 P.C. Elwell Grade

159+47.4 P.O.T. No. County Line

Reference Points



Sta. Angle.
 Rt. Lt.

15+55.01 P.O.T.

12+68.7 P.O.T.

9+84.39 P.T.

Curve Data.

$D = 13^\circ$

$T = 155.25$

$L = 297.95$

$R = 441.68$

Deflections

6+86.44 P.C.

7+00 $0^\circ 53'$

7+50 $4^\circ 08'$

8+41.69 P.I. $38^\circ 44'$ 8+00 $7^\circ 23'$

8+50 $10^\circ 38'$

9+00 $13^\circ 53'$

9+50 $17^\circ 08'$

9+84.39 P.T. $19^\circ 22'$

Reference Points

12" Boat Spike.

Nail in Apple Tree.



61.99



Form. Tong.

T.P.

12" Boat Spike.

58.70

91.15

80.48

T.P.
1257

71.64

12" Boat Spike

Angle.

Sto. Rt. Lt.

64+61.9 = $\angle$ S.T. Hy. #8 = Point made in concrete
Permanent.

61+16³⁰ P.O.T.

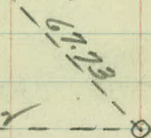
41+98.1 0°18' Pl.

29+00 P.O.T.

Reference Points



Cor. of Garage.



89.67

Nail in Fence Post.

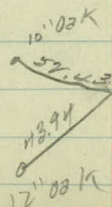


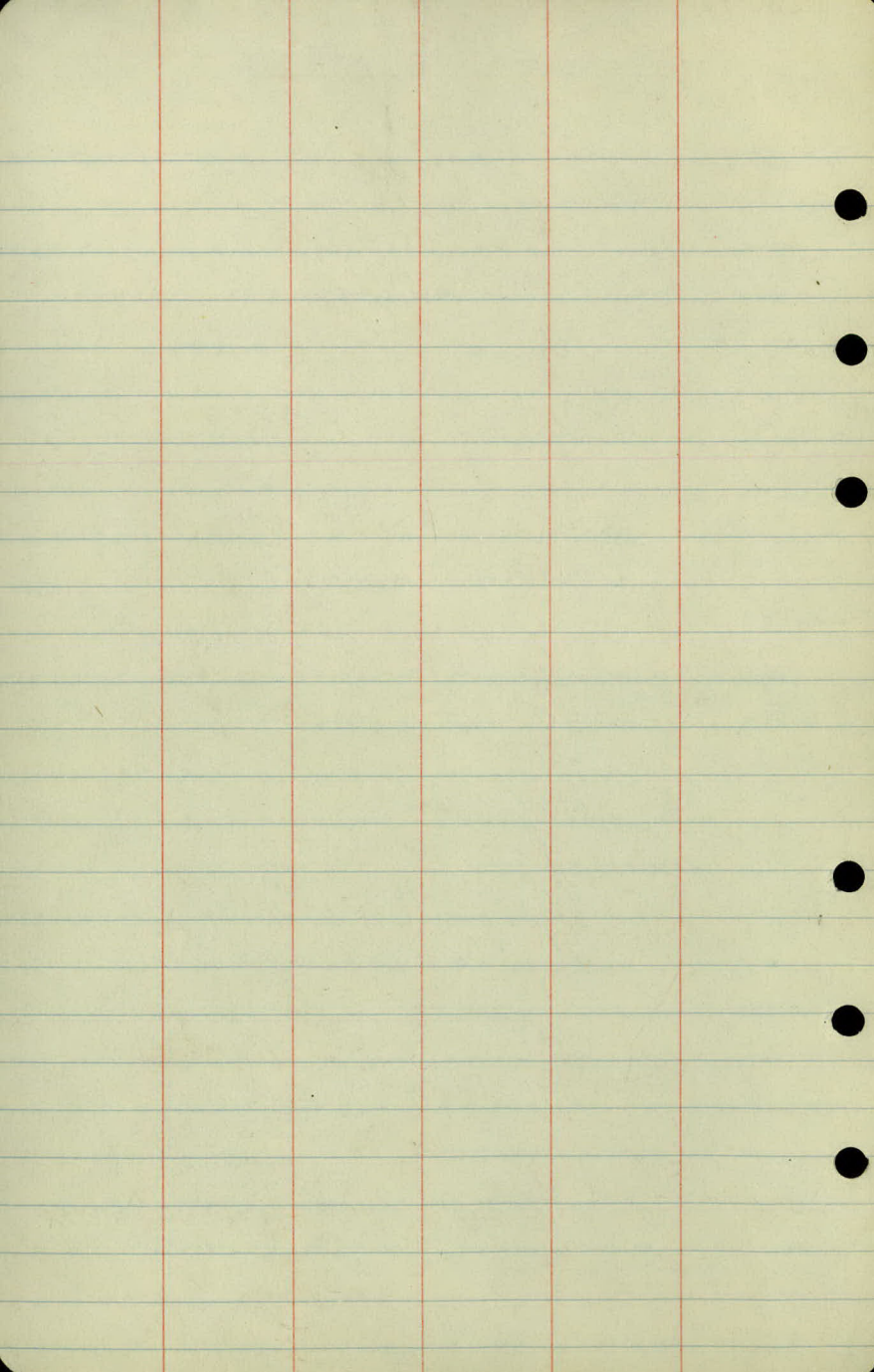
86.81

Nail in 12" Oak

90.53

Nail in 8" Oak.





ELLWELL Grade.

Topography Anoka County.

1/14/37

{ Bratager
Wilke
Goldberg
Eottfried

Fair Day
20 Above.

North of No. Co. Line Sta. 0+00 =
Sta. 159+47.4 No. Co. Line

543.
7400

6
5488 T.P. 24' Rt.

5

406 T.P. 26' Rt.
4

3

416 T.P. 28' Rt.

2

1468 = 12" C.M. x 40'

1

0400

8' 1" - 6'

①

②

Open
Hillside

Meadow
Land

7' 1" - 7'

③

7' 1" - 7'

Traveled
Road.

7' 1" - 7'

14

13100 T.P. 24' Rt.

12

11

+98 T.P. 27' Rt.

10

9

+92 T.P. 29' Rt.

8

+61 T.P. 27' Rt.

+50

7

7' ~~7'~~ 7'

Cultivated

x

6' 7' - 8' ①

4' 7' - 10'

Meadow
Land

Open
Hillside

3' 7' - 11' ①

8' 7' - 6'

9' 7' - 5' ①

9' 7' - 5'

8' 7' - 6' ①

Truncated Road

21

+50 T.P. 22' Rt.

20

19

+67 End of Scattered Oaks Rt.

+60 T.P. 23' Rt.

+56 End windbreak 24' Rt.

18

+91 Farm Drivelling 165' Rt.

+67 Begin Windbreak 23' Rt.

+53 Farm Entrance Rt.

+35 End Poplar windbreak 14' Rt.

17

16

+73 Poplar windbreak 14' Rt.

+20 Begin Orchard 23' Rt.

15

+85 T.P. 24' Rt.

14

7' 7'

0

7' 7'

Cultivated

Cultivated

7' 7'

0 8" for E. H. H. H.

Scattered Oaks

7' 7'



Entrance - Out Road

14" Poplars @ 8' C. H. S.

Orchard.

7' 7'

Cultivated

7' 7' 0

Meadow

28

27

+22 T.P. 22' Rt.

26

25

+23 T.P. 22' Rt.

+05 Fence Cor 22' Lt.

24

23

+48 T.P. 22' Rt.

22

21

28' 29' 30'

Pasture land

29' 30'

Cultivated

4 Sted. O.W.
posts in' chs.

31' 32'

Pasture land

31' 32'

x x x x x x x x

31' 32'

Cultivated

31' 32'

Cultivated

31' 32'

35

34

+55 T.P. 22' Rt.

+09 Fence Cor. 25' Lt.

33

32

+66 T.P. 22' Rt.

31

30

+88 T.P. 22' Rt.

29

+59 Long Rt. + F. Cor. 24' Lt.

+08 T.P. 22' Rt.

+06 O.K. 24' Lt. 26'

28

7' 1" 7'

Meadow Land

7' 1" 7'

Meadow

○

7' 1" 7'

Oak Timber

○

7' 1" 7'

7' 1" 7'

○

Oak Timber

4 Std. B.M. posts — 7' 1" 7'

@ 12' cts.

Meadow Land

— x — x — x — x — x —

Zone

Pasture.

Cultivated

○

44 P.P. 75' Lt.

129 R.P. & T.P. 21' Rt.

166 End scattered Oaks. Lt.

146 End scrub Oak Rt 18'

41

184 R.P. & T.P. 20' Rt.

157 Farm Dwelling 200' Lt.

125 Begin Scrub Oak 18' Rt.

40

187 Farm Entrance. Lt.

105 T.P. 22' Rt.

39

195 Fence Cor. 35' Lt.

163 Oak Tree 24" Lt. 30'

139

129 } 2 Oak Trees 18" dia. 28' Lt.

38

124 T.P. 22' Rt.

37

198 Fence Cor 28' Lt.

36

139 T.P. 22' Rt.

35

2 W. v.

Xing

Diet Zone -

Meadow
land

 $7' 2' 1' 2'$

Scrub Oak

28' 14' Frame

Scattered

2' f. 49'

Dirt Road

Oaks

Meadow Land

2' 4 2'

5 Str. B.W. poste
© 19' ctus.

$$7' \times 4 \times 7'$$

Meadow Land.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
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Meadow Land

24 421

Meadow Land

$$2' \quad 4' \quad 1' \quad 4' \quad 2'$$

6

49

+06 P.P. 22' Rt.

48

+15 End Row of trees 16' Rt.

47

+49 P.P. 20' Rt.

+54 - Farm Dwelling - Frame - 81' Rt.

+34 Farm Entrance - Dirt Drive way

46

+70 Begin Row of trees 16' Rt.

+5 = 36" Cottonwood tree 40' Lt.

+97 P.P. 21' Rt.

44

+44 P.P. 21' Rt.

43

42

12' 2'

Cultivated

12' 2'

Meadow Land

11' 3' 5-6" to 10" Box Elders



10' 4'

8' 6'

8' 6'

8' 6'

Cultivated

Turned Road

Meadow Land

56

+66 P.P. 23' Rt.
+49 Fence Cor 30' Rt.
+43 T.P. 18' Lt + 65' Rt.
+30 Dist + Fence Rt.

55

+10 P.P. 22' Rt.

54

53

+63 P.P. 22' Rt.

52

+14 P.P. 22' Rt.

51

50

+60 P.P. 22' Rt.

49

Scattering Oak
Timber

7' 1/2 - 7' 1/2

5' 1/2 - 9' 1/2

Land

5' 1/2 - 9' 1/2

Land

6' 1/2 - 8' 1/2

7' 1/2 - 7' 1/2

Cultivated

10' 1/2 - 4' 1/2

Meadow

61

+27 P.P. 25' Rt.

60 -

+74 T.P. 19' Lt.

59

+74 P.P. 25' Rt.

58

+84 T.P. 20' Lt.

+18 P.P. 24' Rt.

57

+30 T.P. 18' Lt.

56

Land.

Cultivated

7' 4' 7' 4'

3 Strd B.W. & 24" W. Wire

7' 2' 3' 7'

Timber

6' 2' 8'

Oak

6' 2' 8' 20'

Scattered Oak

7' 2' 7'

3 Strd. B.W. & 24" Woven Wire Posts in this.

64+61.9 Intersect U.S. Hwy. #8 - 27' Conc. Boring

64

+78 Ornamental Light 34' Lt.

+64 P.P. 23' Rt.

+54 T.P. 18' Lt.

63 - Filling Station, 8'x8' Stucco

+61 - Harvey's Tavern

+31 - Harvey's Tavern, 1 Story Stucco

62 = P.P. 33' Lt.

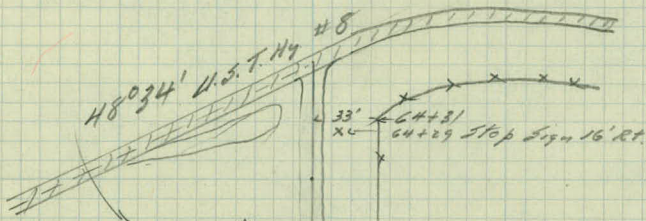
+80 P.P. 24' Rt.

+73 Frame Garage on Conc. Block Fdn.

+65 T.P. 19' Lt.

+18 Fence Line 33' Lt.

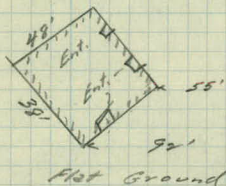
61



V.O.I. Pump 22
8'

48'

46'



55'

92'

33'

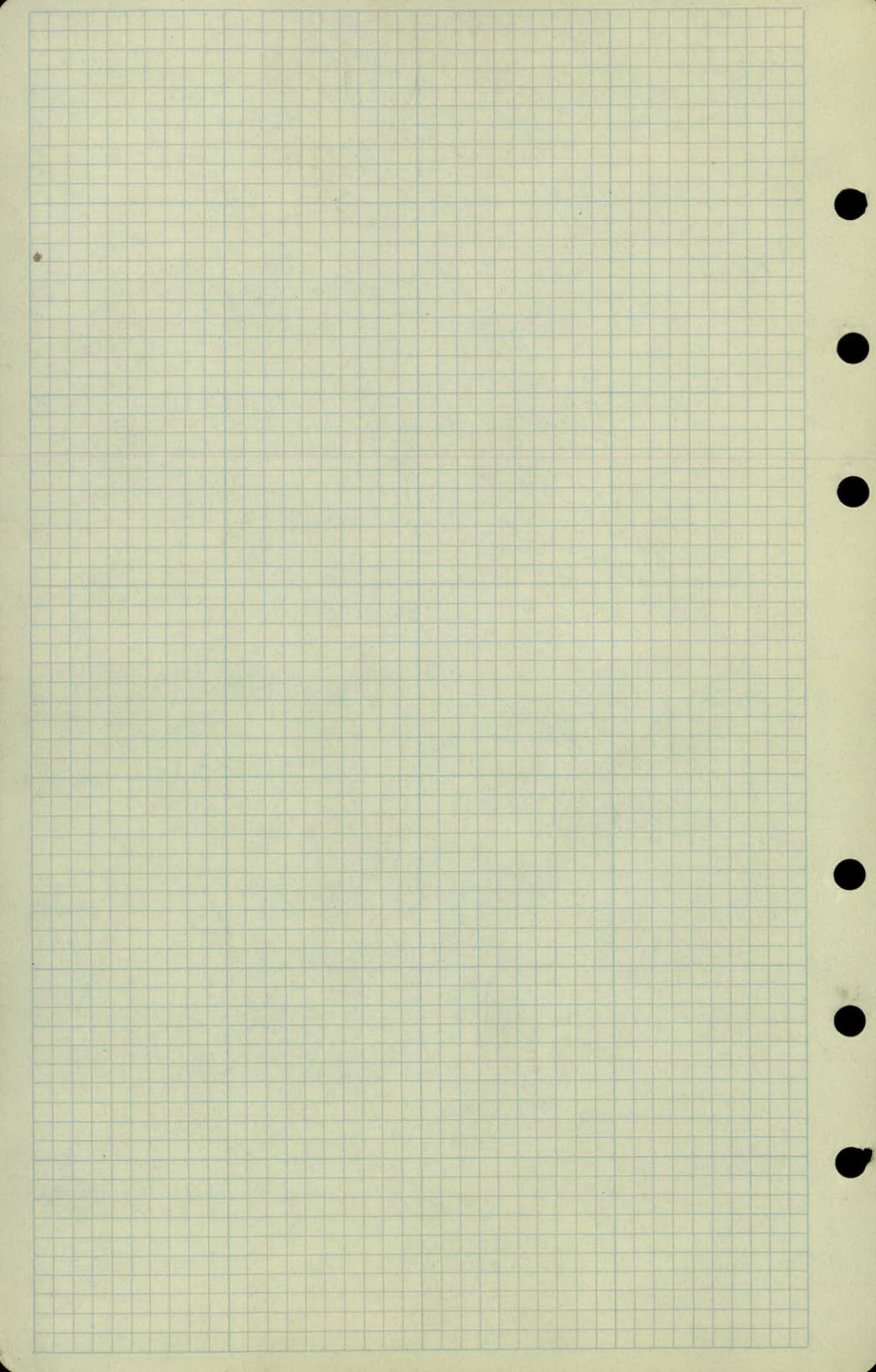
24'

18'

Scattering Oak
Timber

35' d. B.W. & 24" W.W.

Posts Only



64+61.9 $\neq$ 577.48

41+98- P1 $\Delta 0^{\circ} 18' \text{Rt}$

15+55.02 P6T

9+84.39 PT

8+41.69 P1.

A 38°44'41

B 13

T 155.25

L 297.95

R 441.68

6+86.44 PC.

1+12.39 PT

0+62.0 P1

A 51°42'41

D 46°

T 62'

L 112.39

R 127.96

~~6459~~
0400 E/W

159+474 P0T=

Preliminary X- Sec.
Ellwell Grade.

No. of No. County Line
Anoka County

Sta.	+	-	Elev.
B.M.	1.77	898.87	898.10
0+00			90.5
1+14.39 P.T.			87.2.
1+68 = 12" C.M.			87.5.
2+00			87.6.
2+50			87.9.
3+00			88.5.
3+50			89.2.
T.P.		2.72	890.15 ✓
	8.80	898.95 ✓	
4+00			89.8.
4+50			90.4.
5+00			91.3.
5+50			91.6.
6+00			92.4.

45

2

27

Spike in Box Elder Cox & No. Co Line

See Elev. N. Co. Line Survey.

$\frac{2.7}{100}$ $\frac{5.3}{65}$ $\frac{6.7}{40}$ $\frac{6.6}{26}$ $\frac{5.7}{17}$ $\frac{5.7}{57}$ $\frac{6.0}{8}$ $\frac{9.0}{16}$ $\frac{8.4}{21}$ $\frac{8.1}{44}$ $\frac{6.1}{50}$ $\frac{6.5}{99}$ $\frac{10.0}{110}$

$\frac{10.6}{88}$ $\frac{4.4}{100}$ $\frac{5.9}{76}$ $\frac{7.7}{61}$ $\frac{7.8}{20}$ $\frac{5.7}{12}$ $\frac{5.4}{54}$ $\frac{6.0}{11}$ $\frac{8.3}{18}$ $\frac{9.3}{100}$ $\frac{10.6}{8.95}$

$\frac{6.1}{100}$ $\frac{7.6}{88}$ $\frac{8.3}{18}$ $\frac{5.5}{8}$ $\frac{5.2}{52}$ $\frac{5.8}{11}$ $\frac{9.0}{20}$ $\frac{8.3}{25}$ $\frac{8.8}{100}$

$\frac{8.0}{100}$ $\frac{8.2}{50}$ $\frac{5.3}{36}$ $\frac{7.4}{16}$ $\frac{5.0}{8}$ $\frac{5.0}{50}$ $\frac{5.3}{12}$ $\frac{8.6}{21}$ $\frac{8.1}{28}$ $\frac{8.4}{10}$ $\frac{8.6}{100}$

$\frac{6.3}{100}$ $\frac{6.1}{93}$ $\frac{5.2}{16}$ $\frac{5.1}{18}$ $\frac{4.5}{10}$ $\frac{4.4}{44}$ $\frac{4.6}{11}$ $\frac{5.0}{17}$ $\frac{5.8}{24}$ $\frac{8.4}{64}$ $\frac{8.8}{100}$

$\frac{1.9}{100}$ $\frac{1.4}{84}$ $\frac{1.6}{57}$ $\frac{1.7}{41}$ $\frac{4.1}{16}$ $\frac{3.7}{9}$ $\frac{3.7}{57}$ $\frac{3.6}{13}$ $\frac{5.5}{20}$ $\frac{5.7}{24}$ $\frac{3.8}{29}$ $\frac{4.5}{41}$ $\frac{8.2}{76}$ $\frac{8.7}{100}$

$\frac{4.3}{100}$ $\frac{4.5}{87}$ $\frac{5.5}{49}$ $\frac{8.7}{19}$ $\frac{9.2}{9}$ $\frac{9.2}{52}$ $\frac{2.4}{14}$ $\frac{11.3}{21}$ $\frac{11.4}{25}$ $\frac{8.6}{29}$ $\frac{10.4}{42}$ $\frac{14.8}{74}$ $\frac{14.8}{100}$

$\frac{7}{100}$ $\frac{0.8}{41}$ $\frac{6.4}{39}$ $\frac{7.6}{21}$ $\frac{8.4}{10}$ $\frac{8.0}{13}$ $\frac{8.4}{13}$ $\frac{10.5}{21}$ $\frac{11.2}{23}$ $\frac{10.3}{29}$ $\frac{14.5}{53}$ $\frac{14.7}{100}$

$\frac{12.0}{100}$ $\frac{0.3}{84}$ $\frac{3.8}{10}$ $\frac{7.8}{10}$ $\frac{7.7}{13}$ $\frac{8.2}{13}$ $\frac{11.8}{24}$ $\frac{14.9}{41}$ $\frac{15.0}{100}$

$\frac{13.0}{100}$ $\frac{0.6}{13}$ $\frac{3.3}{10}$ $\frac{6.6}{11}$ $\frac{7.3}{11}$ $\frac{7.4}{11}$ $\frac{7.4}{11}$ $\frac{12.9}{22}$ $\frac{14.1}{40}$ $\frac{14.5}{100}$

$\frac{14.0}{100}$ $\frac{0.0}{11}$ $\frac{3.2}{10}$ $\frac{5.8}{11}$ $\frac{6.1}{11}$ $\frac{6.6}{11}$ $\frac{6.7}{11}$ $\frac{13.0}{24}$ $\frac{14.6}{40}$ $\frac{14.6}{100}$

St.	+	Σ	-	Elev.
6+50		898.95		93.3.
7+00				94.3.
7+50				95.5.
8+00				97.0.
T.P.			1.58	897.37 v
	6.67	904.04 ✓		
8+50				98.4.
9+00		904.04 33 903.71 10.44 914 11		00.0.
9+50				01.5.
10+00				03.2.
T.P.			0.33	903.71
	10.44	914.15		
9+50				01.5.
10+00				03.2.
10+50				05.0.

$$\begin{array}{r} +5.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 0.3 \\ \hline 69 \end{array} \quad \begin{array}{r} 2.8 \\ \hline 80 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 21 \end{array} \quad \begin{array}{r} 5.8 \\ \hline 11 \end{array} \quad \begin{array}{r} 5.7 \\ \hline \end{array} \quad \begin{array}{r} 5.9 \\ \hline 9 \end{array} \quad \begin{array}{r} 11.6 \\ \hline 23 \end{array} \quad \begin{array}{r} 13.9 \\ \hline 44 \end{array} \quad \begin{array}{r} 14.6 \\ \hline 60 \end{array} \quad \begin{array}{r} 14.8 \\ \hline 100 \end{array}$$

$$\begin{array}{r} +5.5 \\ \hline 100 \end{array} \quad \begin{array}{r} 0.9 \\ \hline 62 \end{array} \quad \begin{array}{r} 1.9 \\ \hline 50 \end{array} \quad \begin{array}{r} 3.7 \\ \hline 34 \end{array} \quad \begin{array}{r} 4.7 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.7 \\ \hline \end{array} \quad \begin{array}{r} 4.8 \\ \hline 7 \end{array} \quad \begin{array}{r} 9.8 \\ \hline 19 \end{array} \quad \begin{array}{r} 12.6 \\ \hline 36 \end{array} \quad \begin{array}{r} 14.6 \\ \hline 18 \end{array} \quad \begin{array}{r} 15.0 \\ \hline 100 \end{array}$$

$$\begin{array}{r} +5.5 \\ \hline 100 \end{array} \quad \begin{array}{r} 0.9 \\ \hline 57 \end{array} \quad \begin{array}{r} 1.6 \\ \hline 46 \end{array} \quad \begin{array}{r} 2.8 \\ \hline 22 \end{array} \quad \begin{array}{r} 3.7 \\ \hline 14 \end{array} \quad \begin{array}{r} 3.5 \\ \hline \end{array} \quad \begin{array}{r} 3.5 \\ \hline 8 \end{array} \quad \begin{array}{r} 9.9 \\ \hline 23 \end{array} \quad \begin{array}{r} 12.5 \\ \hline 41 \end{array} \quad \begin{array}{r} 15.0 \\ \hline 65 \end{array} \quad \begin{array}{r} 15.4 \\ \hline 100 \end{array}$$

$$\begin{array}{r} +6.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 0.9 \\ \hline 80 \end{array} \quad \begin{array}{r} 1.6 \\ \hline 30 \end{array} \quad \begin{array}{r} 2.4 \\ \hline 17 \end{array} \quad \begin{array}{r} 2.0 \\ \hline \end{array} \quad \begin{array}{r} 2.0 \\ \hline 9 \end{array} \quad \begin{array}{r} 3.5 \\ \hline 18 \end{array} \quad \begin{array}{r} 10.5 \\ \hline 33 \end{array} \quad \begin{array}{r} 13.1 \\ \hline 51 \end{array} \quad \begin{array}{r} 15.1 \\ \hline 71 \end{array} \quad \begin{array}{r} 15.1 \\ \hline 100 \end{array}$$

$$\begin{array}{r} +3.5 \\ \hline 100 \end{array} \quad \begin{array}{r} 0.2 \\ \hline 70 \end{array} \quad \begin{array}{r} 1.6 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 35 \end{array} \quad \begin{array}{r} 5.5 \\ \hline 16 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 10 \end{array} \quad \begin{array}{r} 5.6 \\ \hline \end{array} \quad \begin{array}{r} 5.6 \\ \hline 11 \end{array} \quad \begin{array}{r} 7.3 \\ \hline 19 \end{array} \quad \begin{array}{r} 13.7 \\ \hline 36 \end{array} \quad \begin{array}{r} 16.8 \\ \hline 50 \end{array} \quad \begin{array}{r} 20.2 \\ \hline 77 \end{array} \quad \begin{array}{r} 20.2 \\ \hline 100 \end{array}$$

$$\begin{array}{r} +5.6 \\ \hline 100 \end{array} \quad \begin{array}{r} +4.0 \\ \hline 25 \end{array} \quad \begin{array}{r} 0.2 \\ \hline 42 \end{array} \quad \begin{array}{r} 1.3 \\ \hline 37 \end{array} \quad \begin{array}{r} 2.4 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 12 \end{array} \quad \begin{array}{r} 4.0 \\ \hline \end{array} \quad \begin{array}{r} 4.0 \\ \hline 10 \end{array} \quad \begin{array}{r} 9.2 \\ \hline 26 \end{array} \quad \begin{array}{r} 12.9 \\ \hline 43 \end{array} \quad \begin{array}{r} 17.3 \\ \hline 72 \end{array} \quad \begin{array}{r} 20.2 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 2.8 \\ \hline 11 \end{array} \quad \begin{array}{r} 2.5 \\ \hline \end{array} \quad \begin{array}{r} 2.6 \\ \hline 11 \end{array} \quad \begin{array}{r} 6.0 \\ \hline 24 \end{array} \quad \begin{array}{r} 17.0 \\ \hline 95 \end{array} \quad \begin{array}{r} 19.0 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 0.9 \\ \hline 14 \end{array} \quad \begin{array}{r} 0.8 \\ \hline \end{array} \quad \begin{array}{r} 1.0 \\ \hline 13 \end{array} \quad \begin{array}{r} 0.8 \\ \hline 18 \end{array} \quad \begin{array}{r} 2.5 \\ \hline 28 \end{array} \quad \begin{array}{r} 14.6 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 100 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 76 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 34 \end{array} \quad \begin{array}{r} 7.8 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline 100 \end{array} \quad \begin{array}{r} 6.3 \\ \hline 37 \end{array} \quad \begin{array}{r} 10.4 \\ \hline 19 \end{array} \quad 11.0$$

$$\begin{array}{r} 6.1 \\ \hline 100 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 30 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 22 \end{array} \quad \begin{array}{r} 9.4 \\ \hline 14 \end{array} \quad \begin{array}{r} 9.2 \\ \hline \end{array} \quad \begin{array}{r} 9.3 \\ \hline 14 \end{array} \quad \begin{array}{r} 9.5 \\ \hline 15 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 22 \end{array} \quad \begin{array}{r} 8.3 \\ \hline 29 \end{array} \quad \begin{array}{r} 18.7 \\ \hline 100 \end{array}$$

Sta	+	-	Elev	
		914.15	06.6	
11+00				
11+50			08.0	
		914.15 1.50 912.65		
12+00				
T.P.	6.18	912.83	1.50	09.6 ↑ 912.65
13			10.8	
14			12.4	
15			13.7	
16			13.6	
17 ✓			13.5	
T.P.	5.09	919.12	4.80	914.03
18			14.0	
19			13.1	
B.M.	4.20	919.06	4.20	914.92 914.86

414.86

47.

≤

12+

$\frac{5.7}{100}$ $\frac{4.3}{30}$ $\frac{3.7}{21}$ $\frac{6.8}{13}$ $\frac{7.7}{9}$ $\frac{4.6}{12}$ $\frac{7.7}{12}$ $\frac{7.6}{16}$ $\frac{5.7}{27}$ $\frac{13.7}{100}$

$\frac{4.3}{100}$ $\frac{3.0}{29}$ $\frac{2.1}{19}$ $\frac{5.0}{17}$ $\frac{6.2}{10}$ $\frac{6.2}{11}$ $\frac{6.4}{17}$ $\frac{5.1}{17}$ $\frac{4.1}{36}$ $\frac{8.7}{85}$ $\frac{9.5}{100}$

$\frac{3.0}{100}$ $\frac{2.2}{30}$ $\frac{1.7}{16}$ $\frac{4.4}{11}$ $\frac{4.9}{10}$ $\frac{4.8}{11}$ $\frac{5.0}{11}$ $\frac{3.2}{20}$ $\frac{2.6}{40}$ $\frac{5.7}{76}$ $\frac{6.3}{100}$

Nail in Tel. Pole.

$\frac{7.0}{100}$ $\frac{6.9}{16}$ $\frac{8.0}{10}$ $\frac{8.0}{12}$ $\frac{7.9}{12}$ $\frac{7.4}{16}$ $\frac{6.5}{28}$ $\frac{9.6}{100}$

$\frac{4.7}{100-64}$ $\frac{5.1}{18}$ $\frac{6.4}{9}$ $\frac{6.4}{10}$ $\frac{6.5}{10}$ $\frac{5.9}{17}$ $\frac{8.5}{100}$

$\frac{3.2}{100}$ $\frac{3.4}{84-19}$ $\frac{5.1}{10}$ $\frac{5.1}{8}$ $\frac{5.1}{8}$ $\frac{4.6}{13}$ $\frac{7.6}{73-100}$ $\frac{8.2}{100}$

$\frac{3.4}{100}$ $\frac{3.7}{85}$ $\frac{4.3}{50}$ $\frac{5.3}{11}$ $\frac{5.2}{9}$ $\frac{5.3}{12}$ $\frac{4.9}{16}$ $\frac{5.8}{100}$ $\frac{7.9}{100}$

$\frac{5.3}{100-85}$ $\frac{5.4}{10}$ $\frac{5.3}{9}$ $\frac{5.4}{12}$ $\frac{5.1}{12}$ $\frac{7.6}{59}$ $\frac{1.0}{100}$

$\frac{5.7}{100-84}$ $\frac{5.8}{39}$ $\frac{5.3}{13}$ $\frac{5.1}{15}$ $\frac{5.8}{15}$ $\frac{7.0}{40}$ $\frac{7.5}{67}$ $\frac{6.7}{100}$

Floor to 6.0

$\frac{3.8}{100}$ $\frac{6.0}{42}$ $\frac{6.1}{13}$ $\frac{6.0}{12}$ $\frac{6.1}{19}$ $\frac{7.0}{46}$ $\frac{7.6}{100}$ $\frac{5.4}{100}$

SpK in 30" Oak ^{85'} RT Sta 18+88

Sta.	+	π	-	Elev.
		919.06		
20				913.6
21				14.4
22				14.7
23				14.7
24				13.8
25	4.45	918.33	5.18	913.88
26				14.0
27				14.3
28				14.6
TP	5.60	918.31	5.62	912.71

Lt.

E

Rt.

$\frac{4.1}{100}$	$\frac{5.1}{67}$	$\frac{5.3}{13}$	5.5	$\frac{5.6}{11}$	$\frac{5.4}{15}$	$\frac{7.2}{60}$	$\frac{6.0}{100}$
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$\frac{3.2}{100}$	$\frac{3.5}{58}$	$\frac{4.0}{17}$	$\frac{4.9}{11}$	4.7	$\frac{4.8}{14}$	$\frac{4.6}{17}$	$\frac{5.7}{100}$
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$\frac{3.8}{100}$	$\frac{4.0}{42}$	$\frac{4.4}{12}$	4.4	$\frac{4.6}{15}$	$\frac{5.3}{22}$	$\frac{6.1}{57}$	$\frac{6.5}{100}$
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$\frac{1.7}{100}$	$\frac{1.9}{32}$	$\frac{3.4}{20}$	$\frac{4.4}{14}$	4.4	$\frac{4.5}{15}$	$\frac{5.6}{58}$	$\frac{7.0}{100}$
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$\frac{4.4}{100}$	$\frac{5.3}{64}$	$\frac{5.5}{15}$	5.3	$\frac{5.3}{13}$	$\frac{5.8}{20}$	$\frac{7.3}{64}$	$\frac{7.8}{100}$
-------------------	------------------	------------------	-----	------------------	------------------	------------------	-------------------

$\frac{4.5}{100}$	$\frac{4.8}{58}$	$\frac{5.0}{21}$	$\frac{4.6}{16}$	4.3	$\frac{4.6}{11}$	$\frac{5.3}{24}$	$\frac{7.0}{100}$
-------------------	------------------	------------------	------------------	-----	------------------	------------------	-------------------

$\frac{3.2}{100}$	$\frac{4.3}{33}$	$\frac{5.2}{21}$	$\frac{4.3}{16}$	4.0	$\frac{4.2}{11}$	$\frac{5.7}{23}$	$\frac{5.3}{28}$	$\frac{6.5}{100}$
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$\frac{1.2}{100}$	$\frac{1.9}{54}$	$\frac{3.4}{36}$	$\frac{4.7}{22}$	$\frac{3.9}{18}$	3.7	$\frac{4.0}{11}$	$\frac{4.9}{19}$	$\frac{6.4}{100}$
-------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	-------------------

$\frac{3.5}{100}$	$\frac{5.6}{50}$	$\frac{6.0}{21}$	$\frac{5.0}{15}$	4.7	$\frac{4.7}{9}$	$\frac{8.0}{19}$	$\frac{6.9}{100}$
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Nail in T.P. ^{20'} 12+ Sta 28+05

Sta.	+	π	-	Elev.
		918.31		
29				13.5
30				13.5
31 $\rightarrow$				13.3
32 $\checkmark$				12.4
33				11.7
34				10.2
④	4.28	913.92	8.67	909.64
35				08.9
36				08.1
37				08.3
38				09.5

4.

2

at

Land Sec. 28-912.71 in Twp/Plk

$\frac{7.1}{100}$ $\frac{7.6}{50}$ $\frac{7.2}{23}$ $\frac{5.3}{15}$ 4.8 $\frac{4.7}{7}$ $\frac{9.3}{19}$ $\frac{7.4}{25}$ $\frac{8.2}{50-70}$ $\frac{9.8}{100}$

$\frac{5.5}{100-50}$ $\frac{5.3}{22}$ $\frac{5.8}{18}$ $\frac{5.0}{15}$ 4.8 $\frac{5.0}{11}$ $\frac{7.7}{19}$ $\frac{5.9}{25}$ $\frac{6.6}{50-80}$ $\frac{8.1}{100}$

$\frac{5.8}{100-50}$ $\frac{6.0}{18}$ $\frac{5.4}{12}$ 5.0 $\frac{5.1}{11}$ $\frac{7.8}{21}$ $\frac{6.5}{25}$ $\frac{6.6}{50-80}$ $\frac{7.6}{100}$

$\frac{5.5}{100}$ $\frac{5.3}{50}$ $\frac{5.1}{21}$ $\frac{6.4}{16}$ $\frac{6.0}{12}$ 5.9 $\frac{6.0}{12}$ $\frac{7.4}{20}$ $\frac{6.5}{24}$ $\frac{5.6}{31}$ $\frac{6.0}{50}$ $\frac{8.0}{100}$

$\frac{4.1}{100}$ $\frac{4.0}{50}$ $\frac{4.4}{24}$ $\frac{6.4}{18-11}$ 6.6 $\frac{6.9}{12}$ $\frac{6.1}{15}$ $\frac{7.0}{20}$ $\frac{8.3}{25}$ $\frac{11.2}{50}$ $\frac{11.2}{100}$

$\frac{10.5}{100}$ $\frac{9.5}{50}$ $\frac{9.2}{24}$ $\frac{8.3}{13}$ 8.1 $\frac{7.8}{12}$ $\frac{9.3}{19}$ $\frac{9.6}{50}$ $\frac{12.5}{100}$

$\frac{14.2}{100}$ $\frac{13.6}{50}$ $\frac{12.1}{27}$ $\frac{10.9}{22}$ $\frac{5.2}{13}$ 5.0 $\frac{5.3}{11}$ $\frac{10.5}{20}$ $\frac{10.0}{30}$ $\frac{9.2}{34}$ $\frac{8.7}{50}$ $\frac{7.4}{100}$

$\frac{16.4}{100-50}$ $\frac{15.2}{31}$ $\frac{14.0}{23}$ $\frac{5.7}{12}$ 5.8 $\frac{6.2}{11}$ $\frac{10.2}{18}$ $\frac{11.1}{27}$ $\frac{10.0}{36}$ $\frac{9.7}{50}$ $\frac{8.7}{100}$

$\frac{17.2}{100}$ $\frac{16.4}{50}$ $\frac{14.3}{33}$ $\frac{12.5}{22}$ $\frac{5.6}{13}$ 5.6 $\frac{5.6}{11}$ $\frac{10.5}{22-30}$ $\frac{5.9}{38-50}$ $\frac{5.4}{100}$

$\frac{13.0}{100}$ $\frac{11.7}{50}$ $\frac{9.4}{27}$ $\frac{8.5}{22}$ $\frac{8.2}{17}$ $\frac{4.7}{10}$ 4.4 $\frac{4.9}{13}$ $\frac{7.5}{19}$ $\frac{8.5}{24}$ $\frac{7.8}{31}$ $\frac{3.4}{38}$ $\frac{4.0}{50}$ $\frac{3.5}{100}$

Sta.	+	Σ	-	Elev.	
		913.92			
39				09.9	
40				10.9	
41				10.9	
42	4.68	915.28	3.32	910.60	
43				10.6	
44				10.1	
45				10.2	
46				10.4	
B.M.	8.11	915.28	8.11	907.17	907.20
47				10.3	
48				10.0	

LT

LT

RT

907.20

$\frac{5.6}{100}$ $\frac{3.1}{50-26}$ $\frac{4.5}{16}$ $\frac{4.3}{12}$ 4.0 $\frac{4.2}{13}$ $\frac{5.3}{20}$ $\frac{5.6}{28}$ $\frac{5.1}{30}$ $\frac{2.1}{36}$ $\frac{2.8}{50}$ $\frac{3.4}{100}$

$\frac{+0.2}{100}$ $\frac{0.1}{50}$ $\frac{0.9}{25}$ $\frac{3.1}{15}$ 3.0 $\frac{3.2}{13}$ $\frac{4.7}{19}$ $\frac{4.5}{28}$ $\frac{5.6}{37}$ $\frac{3.3}{50}$ $\frac{3.0}{100}$

$\frac{0.0}{100}$ $\frac{0.7}{50}$ $\frac{2.2}{23}$ $\frac{3.3}{16}$ 3.0 $\frac{3.3}{14}$ $\frac{2.1}{16}$ $\frac{1.5}{50}$ $\frac{1.7}{100}$

~~5.4~~

$\frac{3.2}{100}$ $\frac{4.2}{50}$ $\frac{4.4}{26}$ $\frac{4.7}{15}$ 4.7 $\frac{4.4}{11}$ $\frac{4.6}{16}$ $\frac{4.4}{34}$ $\frac{5.9}{50}$ $\frac{8.5}{100}$

$\frac{5.5}{100}$ $\frac{5.7}{50}$ $\frac{5.8}{24}$ $\frac{5.2}{14}$ 5.2 $\frac{5.1}{10}$ $\frac{5.2}{14}$ $\frac{6.1}{18}$ $\frac{7.4}{27}$ $\frac{9.2}{50}$ 9.5

$\frac{6.0}{100}$ $\frac{6.5}{50}$ $\frac{6.4}{32}$ $\frac{5.8}{23}$ $\frac{5.2}{15}$ 5.1 $\frac{5.3}{9}$ $\frac{6.4}{13}$ $\frac{7.3}{23}$ $\frac{8.7}{50}$ $\frac{5.5}{100}$

$100-$ $\frac{6.4}{50}$ $\frac{7.2}{29}$ $\frac{6.2}{22}$ $\frac{5.2}{16}$ 4.9 $\frac{4.8}{9}$ $\frac{5.4}{12}$ $\frac{5.7}{21}$ $\frac{7.7}{50}$ $\frac{5.5}{100}$

only 100 RT 56 45

$100-$ $\frac{6.8}{50}$ $\frac{7.4}{23}$ $\frac{5.5}{18}$ 5.0 $\frac{5.2}{8}$ $\frac{6.3}{13}$ $\frac{6.3}{50}$ $\frac{7.0}{100}$ Floor Ho
 $\frac{6.1}{907.2}$

$100-50$ $\frac{6.3}{23}$ $\frac{5.7}{17}$ 5.3 $\frac{5.4}{7}$ $\frac{6.0}{11}$ $\frac{6.2}{15-100}$

Sta.	+	Δ	-	Elev.
		915.28		
48				09.3
49				09.5
50	4.65	915.66	4.27	911.01
				09.6
51				09.3
52	4.93	915.94	4.65	911.01
				09.4
53				09.6
54				09.7
55				09.6
56				09.0
57	5.07	914.41	6.60	909.34

LT.

E

RT.

$\frac{7.4}{100}$ $\frac{7.3}{50}$ $\frac{7.0}{22}$ $\frac{6.1}{17}$ 6.0 $\frac{6.1}{9}$ $\frac{7.0}{14}$ $\frac{7.5}{19}$ $\frac{8.8}{50}$ $\frac{9.4}{100}$

$\frac{7.4}{100}$ $\frac{7.1}{50}$ $\frac{6.7}{23}$ $\frac{6.0}{19}$ 5.8 $\frac{5.7}{10}$ $\frac{6.1}{16}$ $\frac{6.5}{27}$ $\frac{6.8}{50}$ 100

$\frac{7.2}{100}$ $\frac{7.3}{50}$ $\frac{7.5}{24}$ $\frac{6.5}{18}$ 6.1 $\frac{6.2}{9}$ $\frac{6.6}{15}$ $\frac{6.2}{19}$ $\frac{7.0}{20}$ $\frac{6.5}{100}$

$\frac{6.4}{50}$ $\frac{5.9}{25}$ $\frac{6.6}{17}$ 6.7 $\frac{6.3}{8}$ $\frac{5.8}{16}$ $\frac{6.7}{27}$ $\frac{6.5}{50}$

$\frac{5.8}{100}$ $\frac{5.5}{50}$ $\frac{5.2}{22}$ $\frac{5.6}{17}$ $\frac{6.5}{12}$ 6.5 $\frac{6.4}{10}$ $\frac{5.5}{14}$ $\frac{5.2}{21}$ $\frac{6.4}{28}$ $\frac{6.3}{50}$ 100

$\frac{5.6}{100}$ $\frac{5.3}{50}$ $\frac{5.0}{17}$ $\frac{6.4}{10}$ 6.3 $\frac{6.4}{12}$ $\frac{5.1}{17}$ $\frac{5.7}{28}$ $\frac{5.8}{50}$ $\frac{6.3}{100}$

$\frac{5.5}{100}$ $\frac{4.9}{50}$ $\frac{4.7}{20}$ $\frac{5.0}{16}$ $\frac{6.2}{11}$ 6.2 $\frac{6.2}{12}$ $\frac{3.6}{19}$ $\frac{4.3}{27}$ $\frac{4.6}{50}$ $\frac{5.0}{100}$

$\frac{3.9}{100}$ $\frac{4.4}{50}$ $\frac{4.8}{22}$ $\frac{5.3}{16}$ $\frac{6.2}{10}$ 6.3 $\frac{6.3}{9}$ $\frac{4.6}{20}$ $\frac{5.5}{28}$ $\frac{5.7}{50}$ $\frac{6.4}{100}$

$\frac{7.0}{100}$ $\frac{6.4}{50}$ $\frac{5.2}{22}$ $\frac{5.7}{15}$ $\frac{6.7}{10}$ 6.9 $\frac{6.6}{10}$ $\frac{7.7}{15}$ $\frac{8.7}{50}$ 100

56. + x - Elev

914.41

57 09.0

58 09.3

59 09.1

60 08.6

⊙ 3.50 912.99 4.92 909.49

61 08.2

62 08.8

63 09.5

64

BM 3.54 909.45 909.48

⊙ 4.34 913.81 3.52 909.47

Lt.

L

Rt.

909178

$\frac{7.0}{100}$	$\frac{6.3}{50}$	$\frac{5.2}{23}$	$18 - \frac{5.5}{14}$	5.4	$\frac{5.4}{8}$	$\frac{7.3}{13}$	$\frac{6.8}{17}$	$\frac{7.0}{29}$	$\frac{7.5}{50}$	$\frac{8.0}{100}$
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$100 - \frac{6.0}{50}$	$\frac{4.6}{15}$	$\frac{5.3}{11}$	5.1	$\frac{5.1}{9}$	$\frac{7.0}{16}$	$\frac{6.1}{29}$	$\frac{6.0}{50}$	$\frac{5.5}{100}$
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$\frac{6.5}{100}$	$\frac{6.3}{50}$	$\frac{5.0}{29}$	$\frac{3.8}{22}$	$\frac{5.4}{14}$	5.3	$\frac{5.4}{16}$	$\frac{6.6}{33-50}$	$\frac{6.8}{100}$
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$\frac{8.2}{100}$	$\frac{8.0}{50}$	$\frac{7.1}{33}$	$\frac{6.4}{27}$	$\frac{5.9}{13}$	5.8	$\frac{5.8}{11}$	$\frac{8.2}{16-50}$	$\frac{9.2}{100}$
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Top from Mont 33' LASH No. 1, 10 T.P. Lt Stn 59+80

$\frac{7.5}{100}$	$\frac{6.7}{50}$	$\frac{7.4}{36}$	$\frac{7.2}{22}$	$\frac{5.6}{17}$	$\frac{5.6}{14}$	4.8	$\frac{4.8}{12}$	$\frac{7.5}{16}$	$\frac{8.0}{50}$	$\frac{8.5}{100}$
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$100 - \frac{5.0}{50}$	$38 - \frac{4.9}{16}$	4.2	$\frac{4.5}{12}$	$\frac{6.0}{18}$	$\frac{5.0}{20}$	$\frac{5.5}{32-50}$	$\frac{6.1}{100}$
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4.8 Floor Gar
37' Lt

Face (Gar Room)

Tavern Floor 3.2	$50 \frac{4.0}{16}$	3.5	$\frac{3.8}{13}$	$\frac{4.0}{19}$	$\frac{2.9}{22}$	$\frac{2.7}{33}$	$\frac{2.4}{50}$	$\frac{2.0}{100}$
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913.81

Elev

04.

09.4.

09.81

+43.7 So Edge 27' Conc Pavement

+619

10.0.

$$\begin{array}{r} 61.9 \\ 182 \\ \hline 437 \end{array}$$

Edged Paper

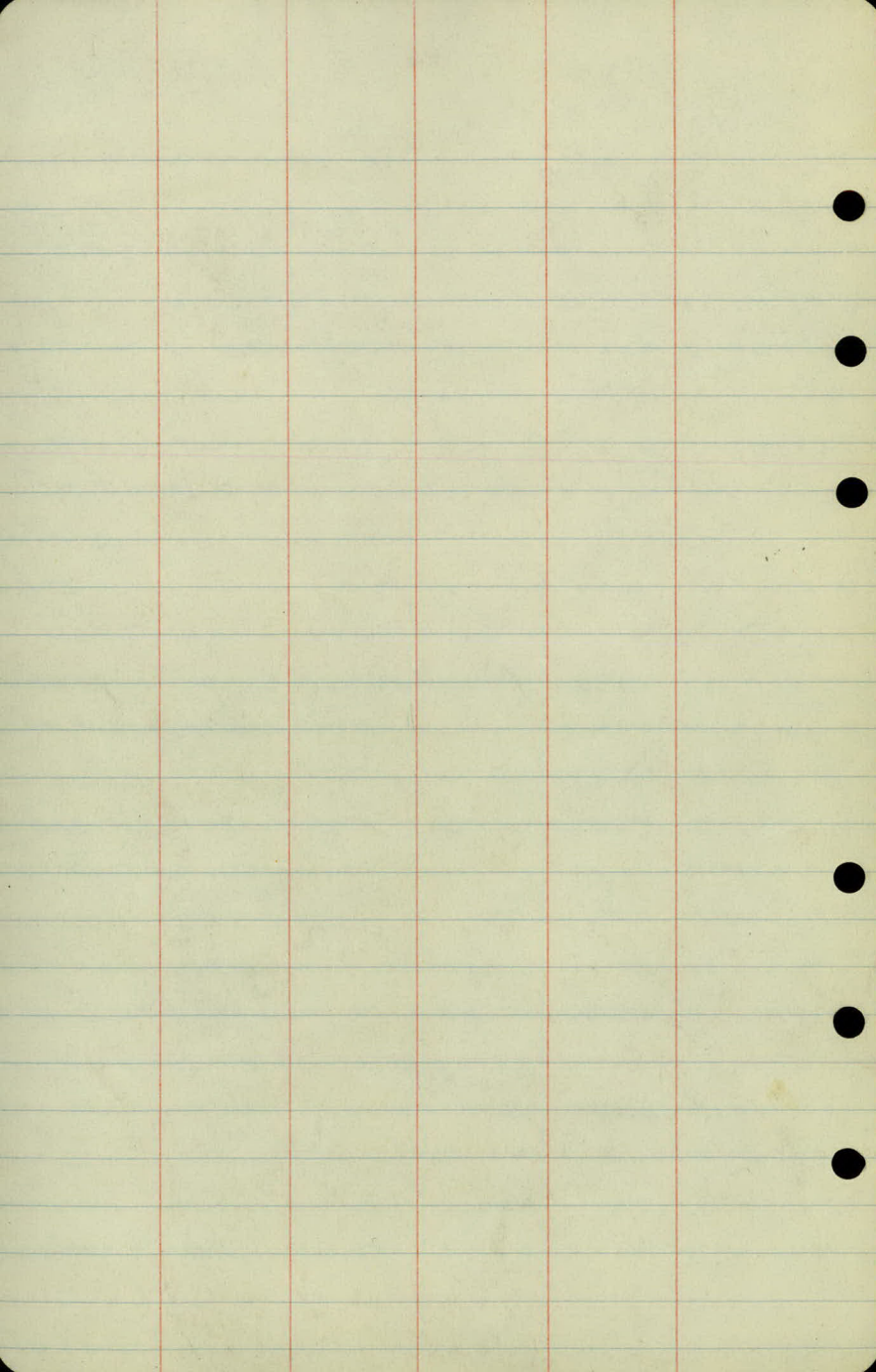
$$- \frac{4.0}{44} \quad \frac{4.5}{30} \quad \frac{5.0}{13} \quad 4.4 \quad \frac{4.5}{11} \quad \frac{6.4}{19} \quad \frac{5.6}{32-50} \quad \frac{6.2}{100}$$

$$\frac{4.0}{50}$$

$$4.00$$

$$\frac{4.0}{50}$$

$$38$$



Profile & Bench Levels

Lexington Ave. Extended No. of
No. 6 Line Road. (Anoka County)

$\frac{12}{2} / 36$

Sta.	+	Σ	-	Elev.
B.M.	1.09	894.19		891.10
0			3.9	
1			5.0	
✓			4.1	
3			3.0	
4			1.6	
T.P.			1.06	891.13
5	12.44	903.57	11.8	
6			10.2	
7			8.0	
8			5.0	
9			1.8	
T.P.			0.56	903.01
10	14.60	915.61	10.4	
11			7.5	

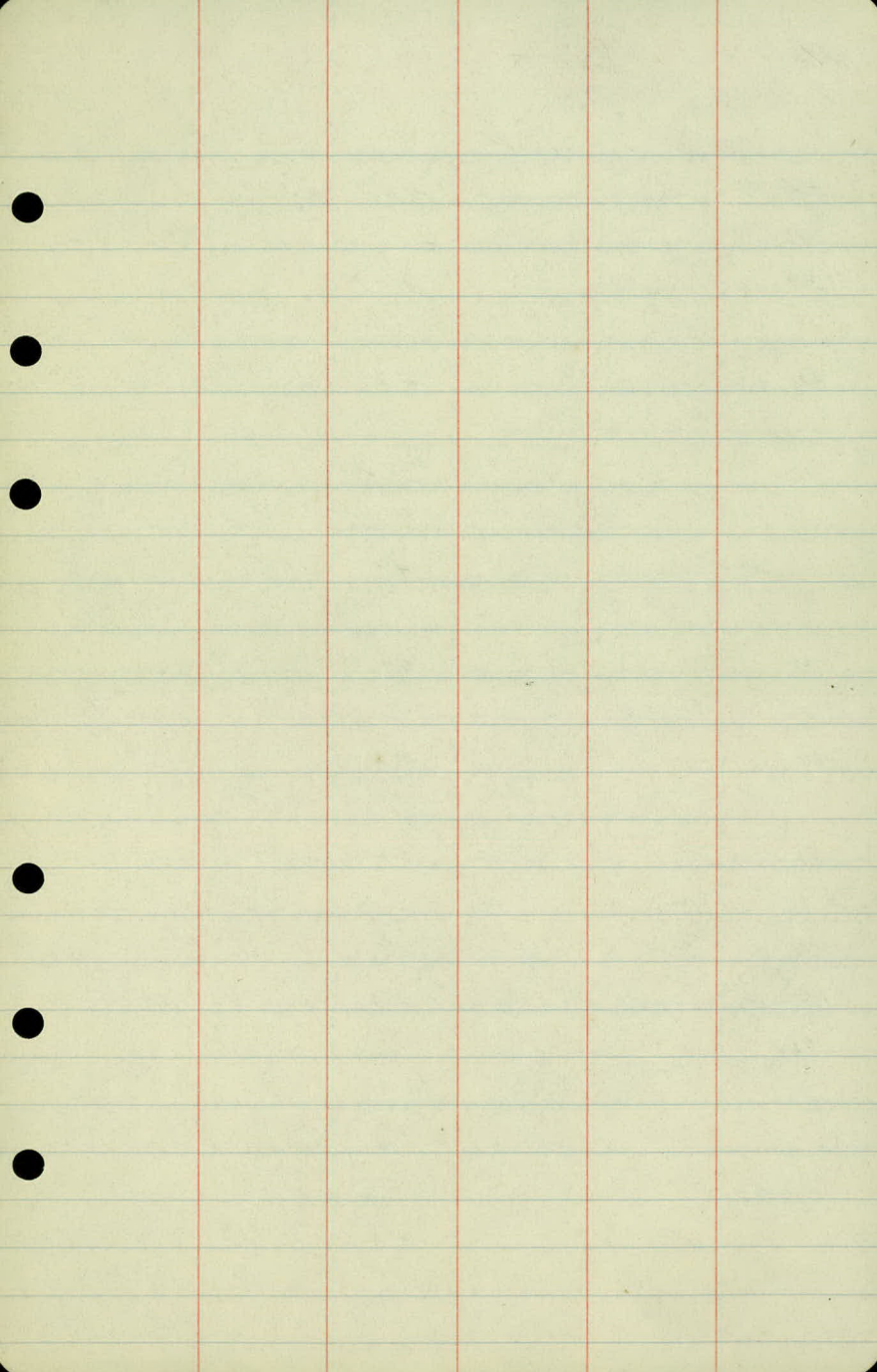
Spike in 18" Box Elder - 30' Sta 158+40
No. Co. Line Road.

No. Co. Line Road & Lexington Ave.

Sta.	+	T	-	Elev.
		915.61		
12			5.4	
13			4.1	
14			2.4	
15			1.8	
16			2.0	
T.P.			1.95	913.66
17	5.49	919.15	5.3	
18			5.7	
B.M.			4.29	914.86
	4.29	919.15		
19			5.8	
20			5.0	
21			4.8	
22			4.4	
23			4.5	

Spike in 24" Osk 70' RT. 18+35

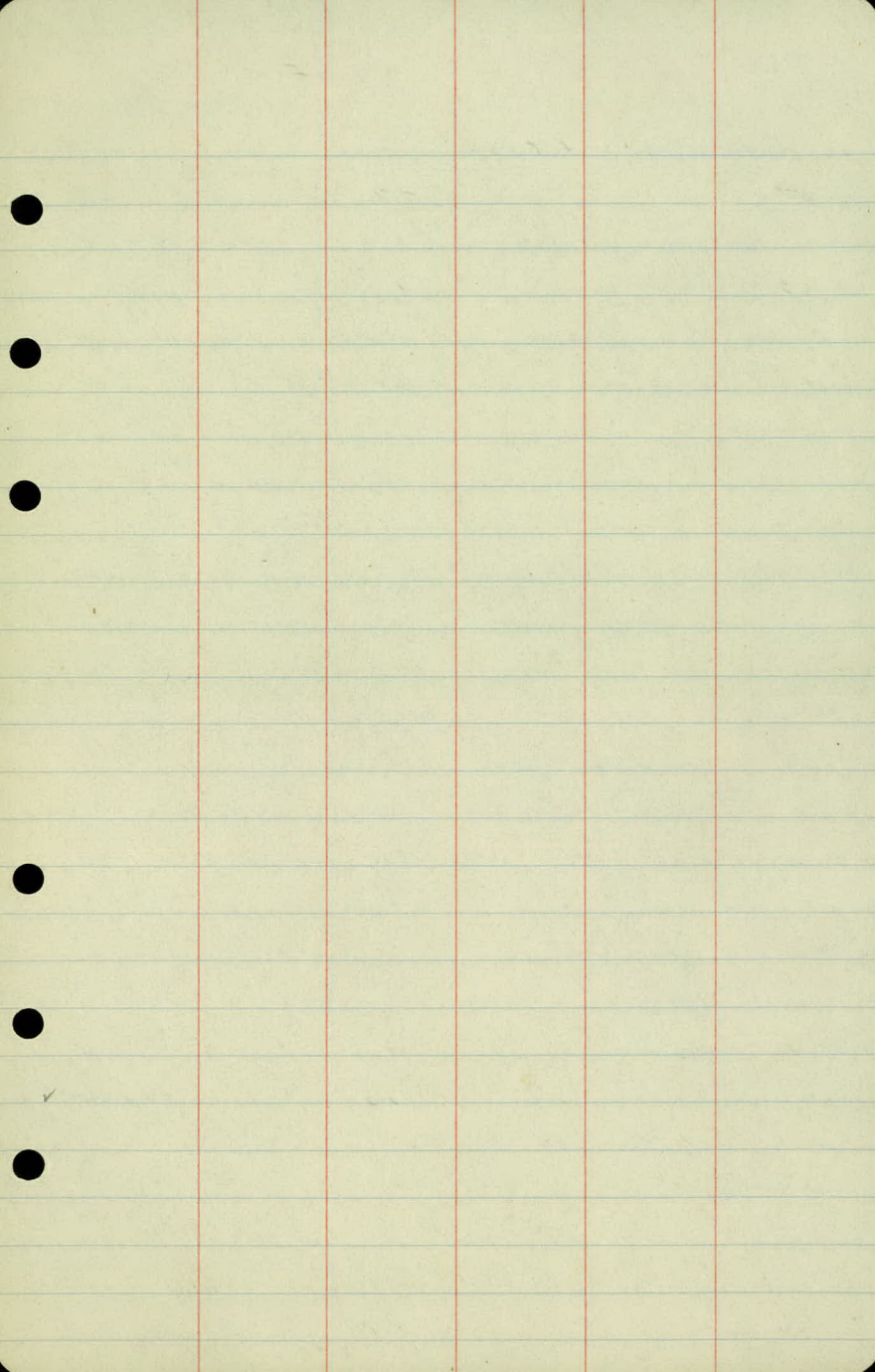
Sta.	+	π	-	Elev.
		919.15		
24			5.5	
T.P.			5.53	913.62
25	4.65	918.29	4.0	
26			4.0	
27			4.2	
28			4.9	
29 ²⁸			4.9	
30			4.7	
31			5.6	
32			6.2	
T.P.			6.34	6.34 911.93
33	1.42	913.35	2.2	
34			4.1	
35			5.1	
36			5.2	



Sta.	+	π	-	Elev.
		913.35		
37			4.3	
38			3.3	
39			2.7	
40			2.2	
T.P.			2.03	911.32
41	4.13	915.45	4.7	
42			5.2	
43			5.4	
44			4.9	
B.M.			8.25	907.20
45	8.25	915.45		
45			5.2	
46				
46			5.3	
47			5.6	
48			6.1	

Spike in 14" O2 K 100' Rt Sts 45

Sta.	+	Σ	-	Elev.
		915.45		
49			5.8	
50			6.1	
T.P.			5.97	909.48
51	5.25	914.73	5.5	
52			5.1	
53			5.1	
54			4.9	
55			5.4	
56			5.8	
57			5.7	
58			5.4	
T.P.			5.54	909.19
59	5.00	914.19	5.3	
60			6.0	
61			5.7	



Sta.	+	X	-	Elev.
		914.19		
62			4.7	
67				
63			4.7	
+	E. Pave.		4.7	910.00
B.M.			4.71	909.48
	4.71	914.19		
T.P.			5.00	909.19
	5.48	914.67		
T.P.			5.18	909.49
	5.75	915.24		
B.M.			8.04	907.20
	8.04	915.24		
T.P.			3.90	911.34
T.P.	1.79	912.13	0.20	914.93
T.P.	5.48	918.41	4.74	912.67
T.P.	5.36	919.03		
B.M.	4.15	919.03	4.15	914.88
T.P.	2.74	916.43	5.34	915.69
T.P.	0.55	903.63	13.35	903.08
T.P.	1.54	893.35	11.84	891.81
B.M.			2.20	891.15

CHECK TO U.S. G. S. BENCH

B.M.	5.49	914.97		909.48
U.S. G. S. B.M.			4.24	(910.92) 910.73

U.S. #8 Hy.

Spike in 20" OAK TO RT. STA. 61+35

907.20

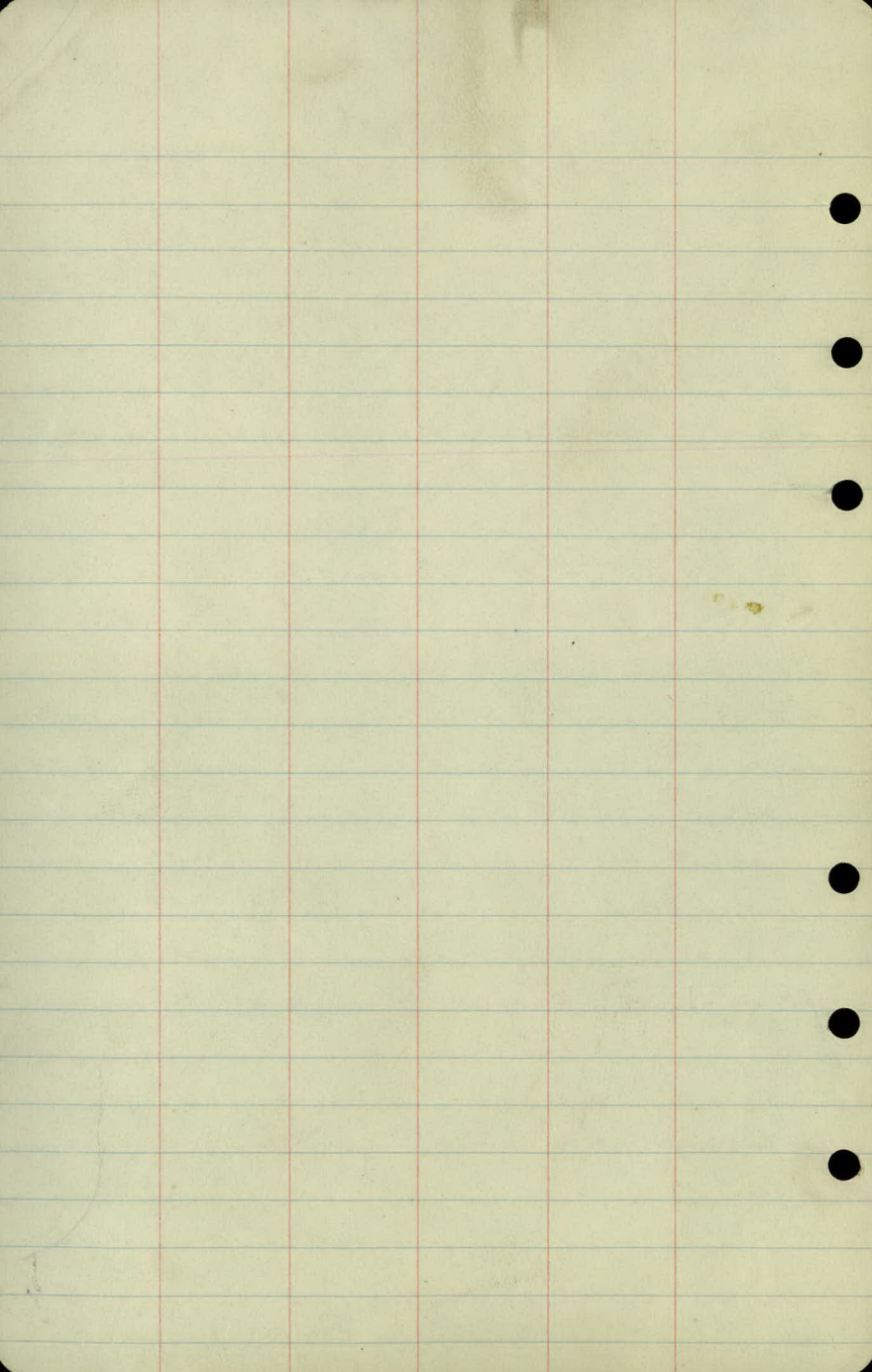
914.86

891.10

W.L. 5/12/37

SPIKE IN 20" OAK TO RT. STA. 61+35

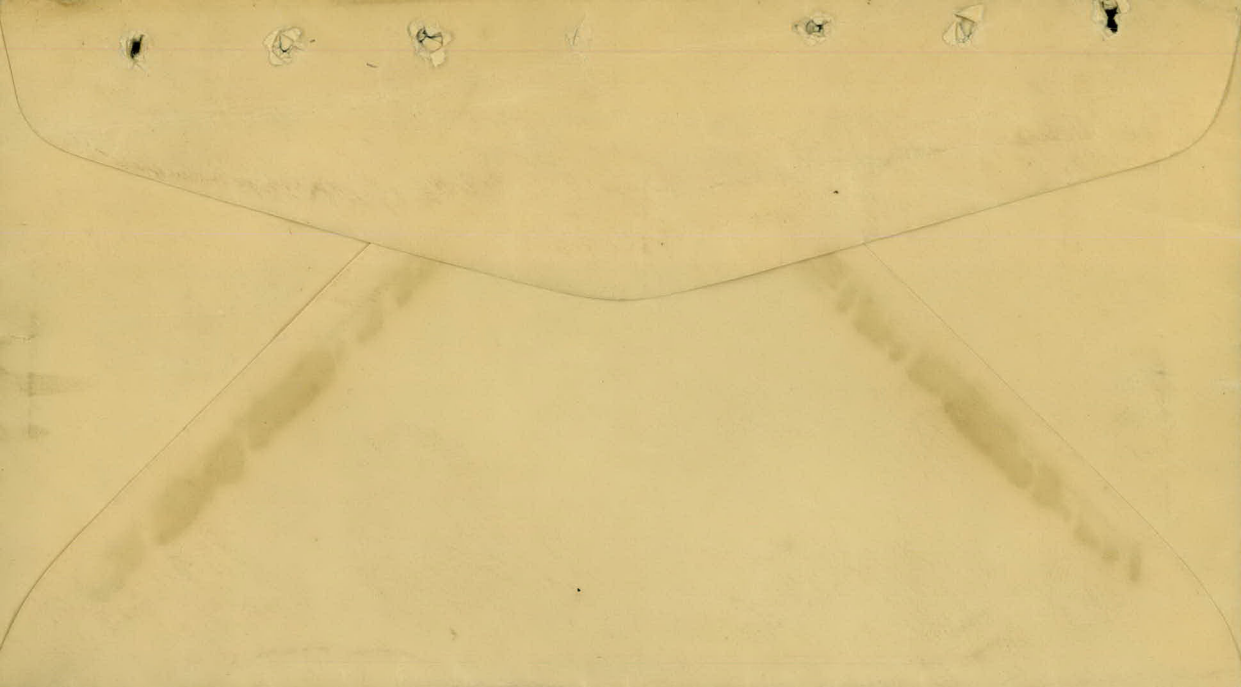
N.E. COR. OLD ROAD INTER. 400' N. OF S.T.H. #8
ON ELWELL RD.



AFTER FIVE DAYS RETURN TO

H. E. BLEWETT

COUNTY ENGINEER ANOKA COUNTY
STATE HIGHWAY DEPARTMENT
ANOKA, MINNESOTA



State Highway Department

Harold E. Blewett

District Engineer Anoka County

REGISTERED UNDER STATE LAWS OF MINNESOTA

Anoka, Minnesota

December 21st 1936

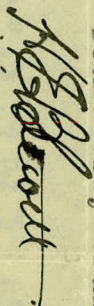
Mr. Emil H. Schulz
Ramsey County Surveyor
Saint Paul, Minnesota

Dear Schulz:

I have stated the center line of the
Elwell Grade from the North County Line to T.H. 8

The alignment follows the center of the
travelled road.

Yours very truly,



H.E. Blewett

ELWELL RD.

Slope Stakes

Sta.	+	-	Grade
B.M.	8.38	915.58	907.20
8.17		1.95	913.63
38			908.8
	+50		02.0
39			09.3
	+50		09.5
40			09.7
	+50		0.99
41			910.0
	+50		10.1
42			10.1
	+50		10.1
43			10.1

Cor Road

Lt

Rt

Rt

3pk. in Oak 100' Rf 512.95

3pk in 24" Oak 90' Lt. 411.50

$$6.8 \quad \frac{98}{93.0/10.0} \quad \frac{60}{108}$$

$$6.6 \quad \frac{76}{41.0/10.0} \quad \frac{56}{110}$$

$$6.3 \quad \frac{48}{51.0/11.0} \quad \frac{58}{105}$$

$$6.1 \quad \frac{26}{59.0/13.5} \quad \frac{50}{111}$$

$$5.9 \quad \frac{29}{52.0/13.0} \quad \frac{47}{112}$$

$$5.7 \quad \frac{15}{61.8/14.2} \quad \frac{44}{113}$$

$$5.6 \quad \frac{18}{59.8/13.6} \quad \frac{48}{108} \quad \frac{93}{113/59.2}$$

$$5.5 \quad \frac{30}{55.0/12.5} \quad \frac{50}{105} \quad \frac{43}{112/49.8}$$

$$5.5 \quad \frac{45}{49.0/11.0} \quad \frac{51}{104} \quad \frac{58}{113/45.8}$$

$$5.5 \quad \frac{52}{45.4/10.1} \quad \frac{53}{102} \quad \frac{68}{113.7/59.8}$$

$$5.5 \quad \frac{63}{41.8/10.2} \quad \frac{56}{101} \quad \frac{85}{110.0/37.9}$$

5/9.	+	A	-	Grade.
		915.58		

43	+50			10.1
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44				10.0
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T.P.	3.12	915.13	3.57	910.01
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	+50			10.0
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45				09.9
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	+50			09.9
--	-----	--	--	------

46				09.8
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	+50			09.8
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T.P.	3.12	914.64	3.07	911.96
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47				09.7
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	+50			09.7
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48				09.6
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	+50			09.6
--	-----	--	--	------

Gr. Rod

Lt

L

Rt

$$5.5 \quad 40.6 / \begin{array}{r} 6.6 \\ 48.19 \end{array} \quad \begin{array}{r} 56 \\ -0.1 \end{array} \quad \begin{array}{r} 85 \\ 42.00 / 33.9 \end{array}$$

$$5.6 \quad 40.6 / \begin{array}{r} 6.7 \\ 48.19 \end{array} \quad \begin{array}{r} 55 \\ 10.1 \end{array} \quad \begin{array}{r} 81 \\ 42.03 / 25.0 \end{array}$$

$$5.1 \quad 39.8 / \begin{array}{r} 6.7 \\ 46.7 \end{array} \quad \begin{array}{r} 47 \\ 10.9 \end{array} \quad \begin{array}{r} 70 \\ 42.10 / 37.4 \end{array}$$

$$5.2 \quad 40.2 / \begin{array}{r} 6.9 \\ 47.18 \end{array} \quad \begin{array}{r} 47 \\ 10.5 \end{array} \quad \begin{array}{r} 68 \\ 42.14 / 38.6 \end{array}$$

$$5.2 \quad 37.8 / \begin{array}{r} 7.0 \\ 44.8 \end{array} \quad \begin{array}{r} 49 \\ 10.3 \end{array} \quad \begin{array}{r} 58 \\ 42.24 / 42.6 \end{array}$$

$$5.3 \quad 38.6 / \begin{array}{r} 6.9 \\ 45.4 \end{array} \quad \begin{array}{r} 48 \\ 10.6 \end{array} \quad \begin{array}{r} 6.1 \\ 42.22 / 41.8 \end{array}$$

$$5.3 \quad 41.0 / \begin{array}{r} 6.3 \\ 47.0 \end{array} \quad \begin{array}{r} 50 \\ 10.3 \end{array} \quad \begin{array}{r} 6.3 \\ 42.20 / 48.0 \end{array}$$

Top stamp Rt 46 + 58

$$4.9 \quad 41.8 / \begin{array}{r} 5.7 \\ 47.2 \end{array} \quad \begin{array}{r} 47 \\ 10.2 \end{array} \quad \begin{array}{r} 5.5 \\ 42.24 / 42.6 \end{array}$$

$$4.9 \quad 41.4 / \begin{array}{r} 5.8 \\ 47.1 \end{array} \quad \begin{array}{r} 49 \\ 10.0 \end{array} \quad \begin{array}{r} 56 \\ 42.3 / 42.2 \end{array}$$

$$5.0 \quad 38.2 / \begin{array}{r} 7.7 \\ 45.9 \end{array} \quad \begin{array}{r} 53 \\ -0.3 \end{array} \quad \begin{array}{r} 76 \\ 42.04 / 39.6 \end{array}$$

$$5.0 \quad 37.0 / \begin{array}{r} 7.0 \\ 44.0 \end{array} \quad \begin{array}{r} 54 \\ -0.4 \end{array} \quad \begin{array}{r} 80 \\ 42.00 / 35.5 \end{array}$$

579.

7

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Grade

9/4.64

49

09.5

450

09.5

50

09.4

450

09.4

51

09.3

+50

09.3

52

09.2

T.P.

5.71

9/5.01

529

909.30

150

092

53

09.1

450

09.1

59

090

Gr. Road

Lt

R

Rt

$$5.1 \quad 398 \frac{4.9}{2.17} \quad \frac{51}{00} \quad \frac{63}{21.8/40.2}$$

$$5.1 \quad 40.6 \frac{6.3}{2.17} \quad \frac{51}{00} \quad \frac{55}{22.6/43.8}$$

$$5.2 \quad 40.2 \frac{6.4}{2.18} \quad \frac{51}{01} \quad \frac{60}{22.2/41.8}$$

$$5.2 \quad 40.6 \frac{6.9}{2.19} \quad \frac{53}{-01} \quad \frac{62}{22.0/41.0}$$

$$5.3 \quad 45.0 \frac{7.3}{2.0} \quad \frac{52}{-01} \quad \frac{55}{22.8/44.2}$$

$$5.3 \quad 49.0 \frac{7.3}{2.0} \quad \frac{55}{-01} \quad \frac{55}{22.8/44.2}$$

$$5.4 \quad 50.2 \frac{7.1}{2.13} \quad \frac{52}{10.2} \quad \frac{51}{19.3/46.2}$$

$$5.8 \quad 49.8 \frac{7.6}{2.2} \quad \frac{55}{10.3} \quad \frac{51}{10.7/47.8}$$

$$5.9 \quad 50.6 \frac{7.5}{2.2} \quad \frac{55}{10.4} \quad \frac{48}{11.8/49.4}$$

$$5.9 \quad 50.2 \frac{7.6}{2.3} \quad \frac{56}{10.3} \quad \frac{43}{11.6/51.4}$$

$$6.0 \quad 52.6 \frac{7.1}{2.2} \quad \frac{53}{10.7} \quad \frac{34}{12.6/55.4}$$

Sta	+	A	-	Grade
		915.01		
54	+50			09.0
55				08.9
	+50			08.9
56				08.8
	+50			08.8
57				08.7
T.P.	5.08	914.12	597	909.04
	+50			08.7
58				08.6
	+50			08.6
59				08.5
	+50			08.5

Gr Rod.

L1

L2

R1

$$6.0 \quad 53.8 / \frac{38}{12.2} \quad \frac{53}{10.7} \quad \frac{37}{12.3} / 54.2$$

$$6.1 \quad 53.8 / \frac{34}{12.7} \quad \frac{53}{10.7} \quad \frac{47}{11.9} / 50.6$$

$$6.1 \quad 53.0 / \frac{41}{12.0} \quad \frac{56}{10.5} \quad \frac{66}{12.25} / 43.0$$

$$6.2 \quad 47.4 / \frac{56}{10.6} \quad \frac{60}{10.2} \quad \frac{7.3}{11.9} / 40.6$$

$$6.2 \quad 43.8 / \frac{63}{12.7} \quad \frac{61}{10.1} \quad \frac{7.3}{11.9} / 40.4$$

$$6.3 \quad 43.0 / \frac{68}{12.5} \quad \frac{64}{10.1} \quad \frac{7.8}{11.5} / 39.0$$

$$5.4 \quad 45.2 / \frac{56}{12.8} \quad \frac{52}{10.2} \quad \frac{68}{12.16} / 39.4$$

$$5.5 \quad 49.2 / \frac{57}{12.88} \quad \frac{50}{10.5} \quad \frac{64}{12.21} / 41.4$$

$$5.5 \quad 40.6 / \frac{56}{12.9} \quad \frac{50}{10.6} \quad \frac{61}{12.4} / 42.6$$

$$5.6 \quad 44.2 / \frac{58}{12.85} \quad \frac{53}{10.8} \quad \frac{64}{12.2} / 41.8$$

$$5.6 \quad 41.0 / \frac{66}{12.0} \quad \frac{53}{10.3} \quad \frac{71}{12.15} / 39.0$$

Sta + X - Grade

9/4.12

60

08.4

+50

08.4

61

08.3

+50

08.3

T.P. 7

5.12

9/4.56

5.28

908.84

62

08.2

+50

08.3

63

08.4

+50

08.8

64

09.2

B.M.

507

709.49

909.45

Cor. Rod.

4

5

6

$$5.7 \quad 38.6 / \frac{73}{41.9} \quad \frac{57}{00} \quad \frac{81}{10.6} / 35.4$$

$$5.7 \quad 36.2 / \frac{79}{40.5} \quad \frac{59}{-0.2} \quad \frac{81}{10.0} / 33.0$$

$$5.8 \quad 37.0 / \frac{78}{41.0} \quad \frac{60}{-0.2} \quad \frac{83}{10.0} / 35.0$$

$$5.8 \quad \frac{58}{00} \quad \frac{73}{10.15} / 39.0$$

$$6.4 \quad \frac{59}{10.5} \quad \frac{68}{10.26} / 43.4$$

$$6.3 \quad \frac{59}{10.9} \quad \frac{45}{11.8} / 52.2$$

$$6.2 \quad \frac{51}{11.1} \quad \frac{41}{12.1} / 53.9$$

$$5.8 \quad \frac{52}{10.6} \quad \frac{53}{10.5} / 47.0$$

$$5.4 \quad \frac{52}{10.2} \quad \frac{69}{10.20} / 41.0$$

Spk. in 20' oct. 70' at 62.25

