

Book- 1a - Dr. 6

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

C.W.A. CONST. Survey

EAST COUNTY LINE ROAD

From S.T.H. No. 12 To Co. Rd. "C"

Road Acc't. No. S.T.H. 100

Date Filed 1934

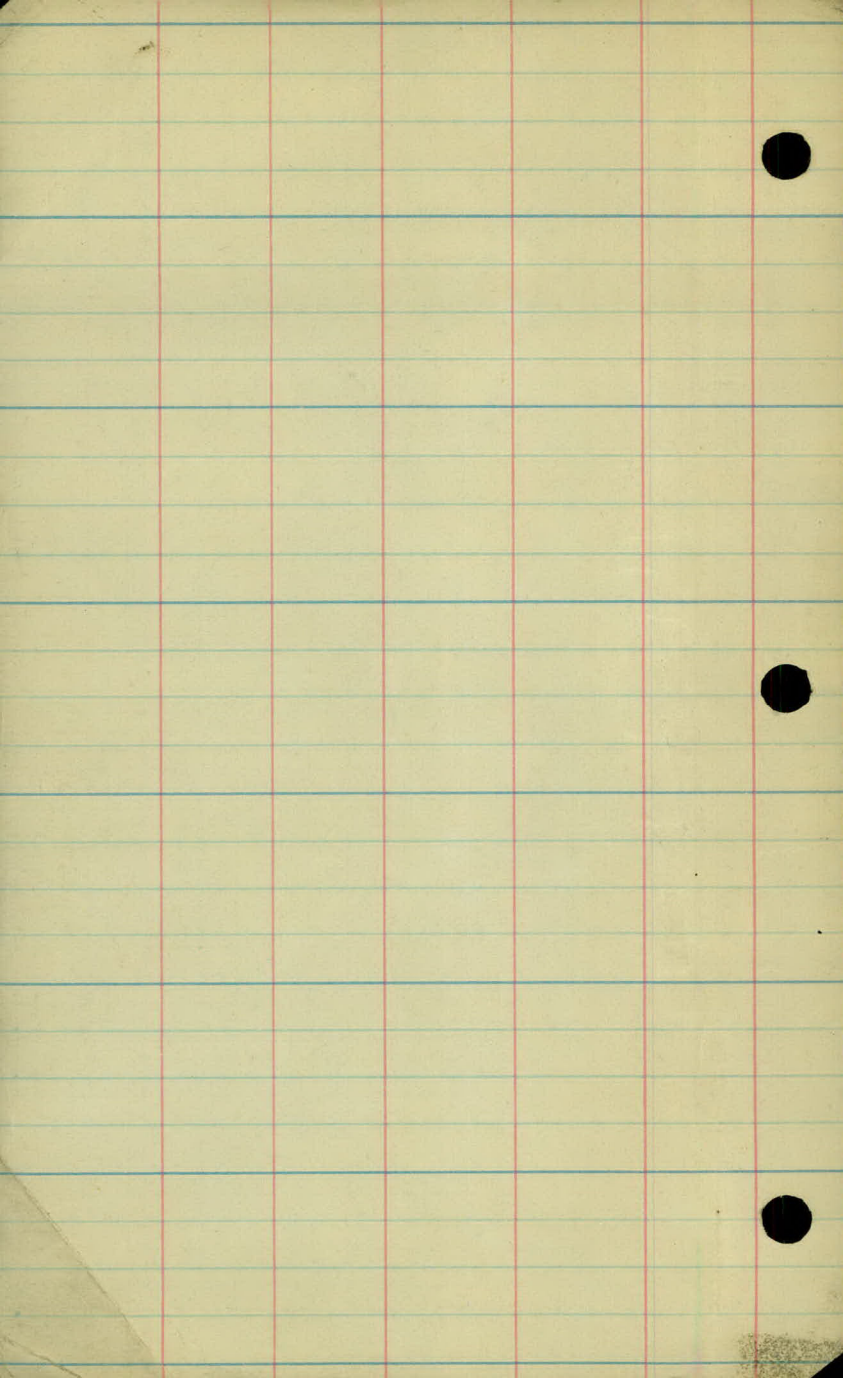
File 10-6

II  
SEC. TIES

EAST CO. LINE RD.

S. T. H. No. 12 to Co. Rd. "C"

II





①

P.T. 139+17.47 5°16' G.P.  
 139+00 4°55'  
 138+00 2°55' 64.83  
 P.I. 137+86.2  
 137+00 0°55'  
 P.C. 136+54.14 0°00'

4° Curve RT  
 $\Delta = 10°32'$   
 $T = 132.06$   
 $L = 263.33$

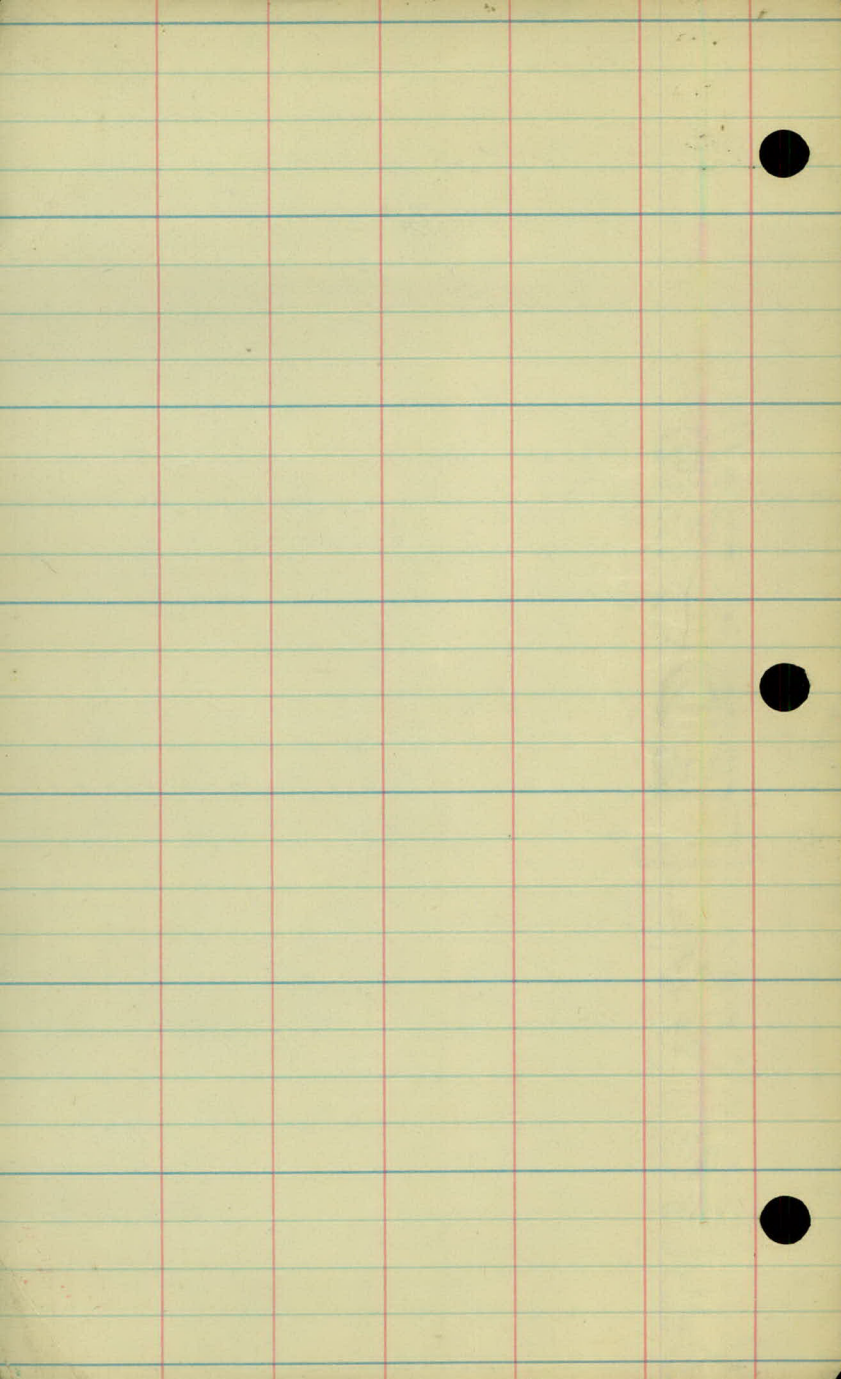
P.T. 135+51.7 3°02 1/2'  
 135+00 2°16'  
 P.I. 134+50.4 1°31'  
 134+00 2°16' 38.65  
 P.C. 133+48.9 0°00' Tree

3° Curve LT  
 $\Delta = 6°05'$   
 $T = 101.49$   
 $L = 202.78$

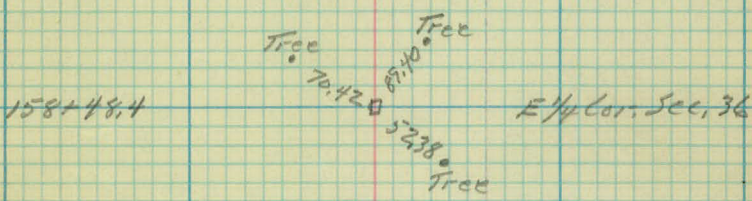
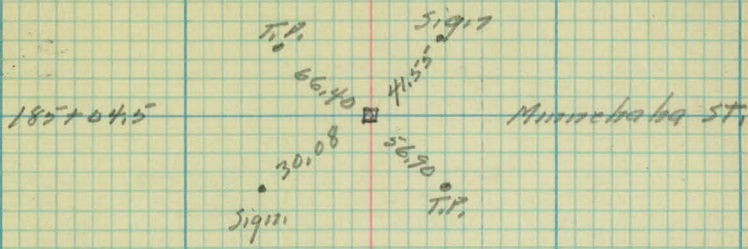
131+89.3  
 59.31  
 13.99  
 89.30  
 72.4  
 59.17  
 G.R. Post

S.T.H. No. 12





(2)



P.T. 143+54.2 2°13 1/2' F.P. 32.25

143+00 1041'

P.I. 142+43.0

142+00 0041'

P.C. 141+31.7 0000'

40.30

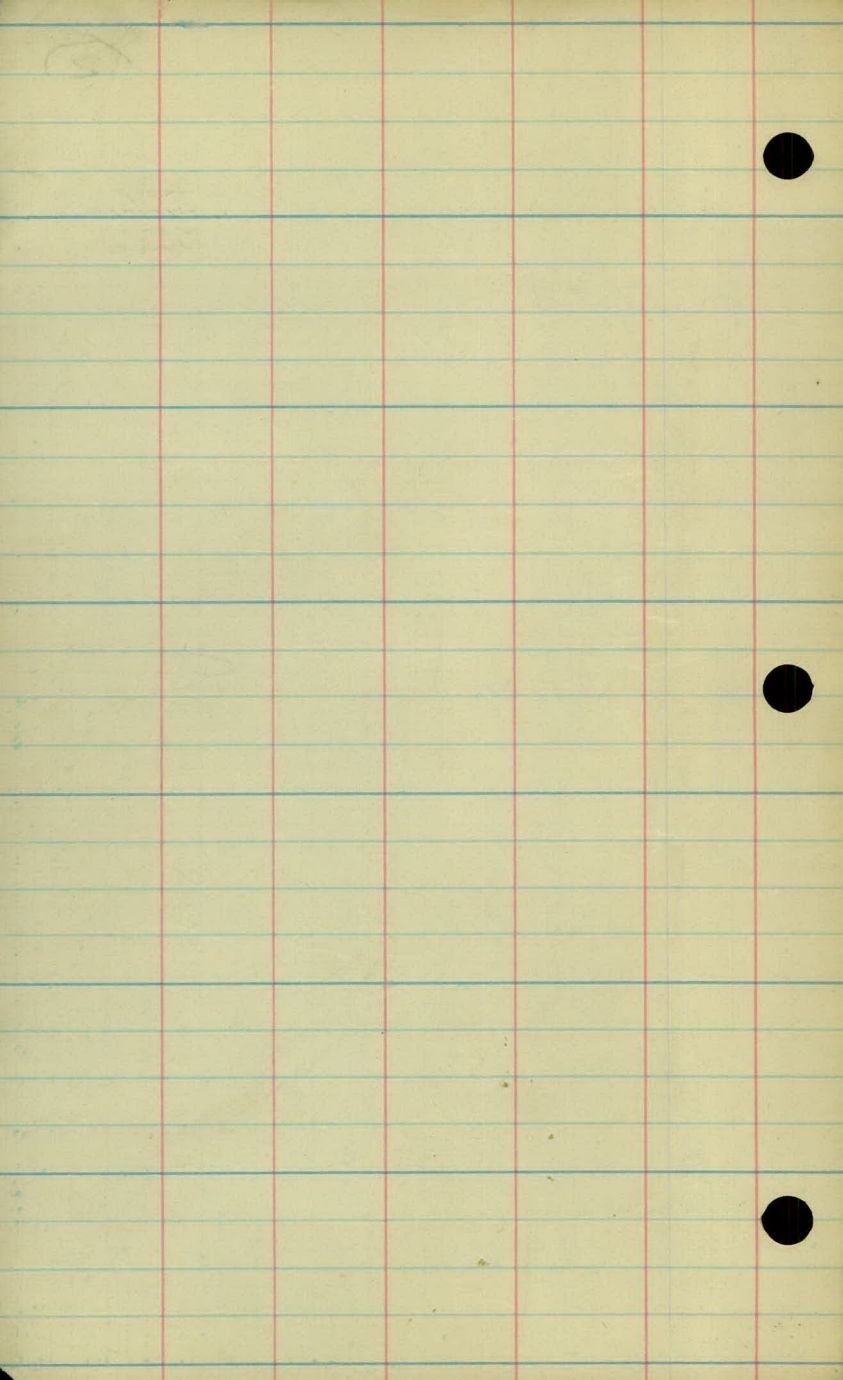
F.P.

2° Curve Lt

$\Delta = 4027'$

$T = 111.32$

$L = 222.50$





343+64.10

Tree  
46.60  
House  
55.85  
72.58  
47.30  
T.P.

N.E. Cor. Sec. 13

317+36.25

T.P.  
27.32  
44.40  
43.82  
T.P.

E 1/4 Cor. Sec. 13

290+89.9

G.P.  
53.12  
62.57  
35.28  
T.P.  
G.P.

N.E. Cor. 24

264+43.60

25.52  
41.74  
Tree  
T.P.

Found  
E 1/4 Cor. Sec. 24

237+97.70

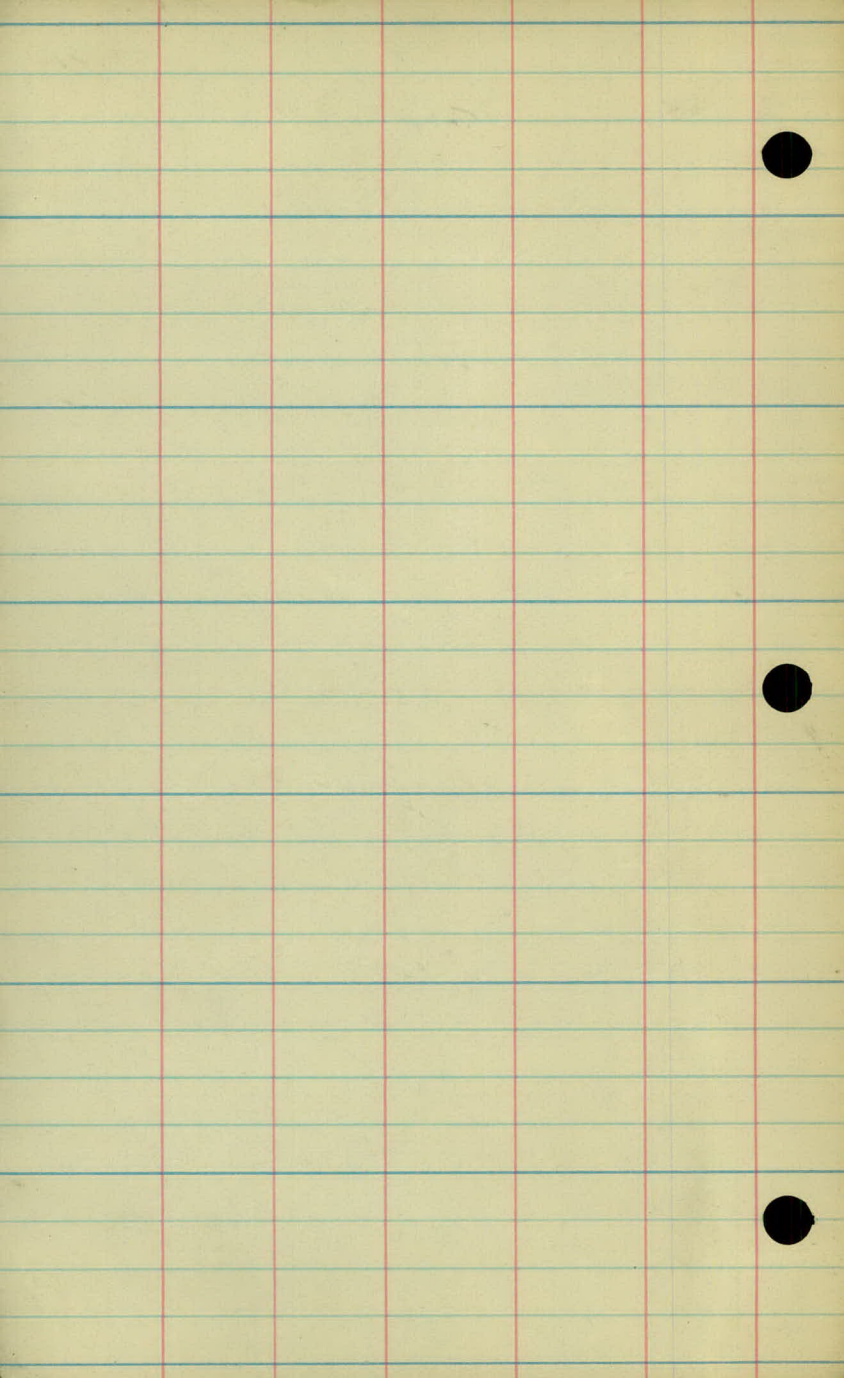
T.P.  
28.63  
34.20  
Tree

N.E. Cor. Sec. 25

211+44.9

T.P.  
63.35  
68.88  
Tree  
40.42  
T.P.

E 1/4 Cor. Sec. 25



4

396 + 40.1

Tree  
30.15  
52.2  
Tree

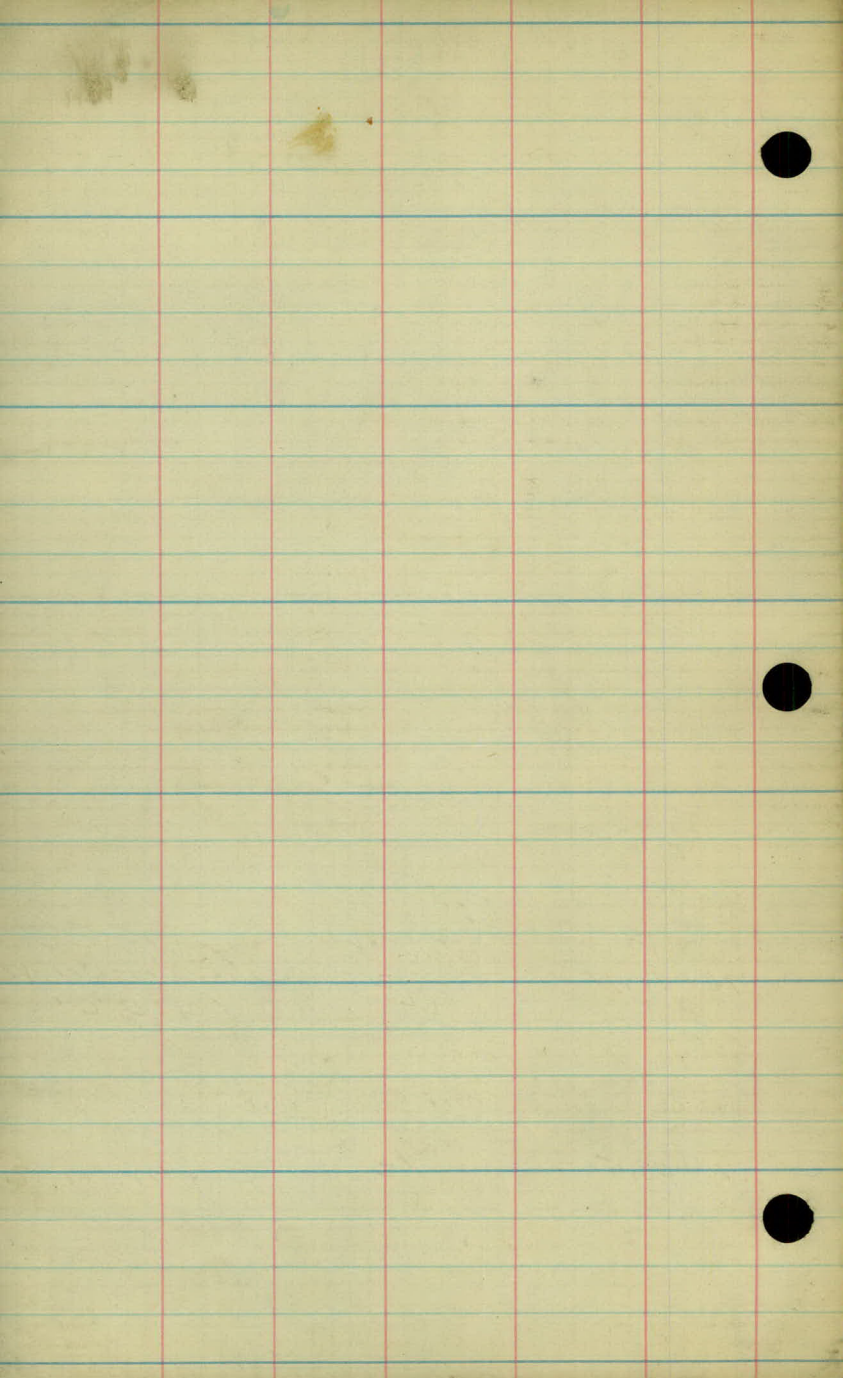
N.E. Cor. Sec. 12  
Co. RD. "C"

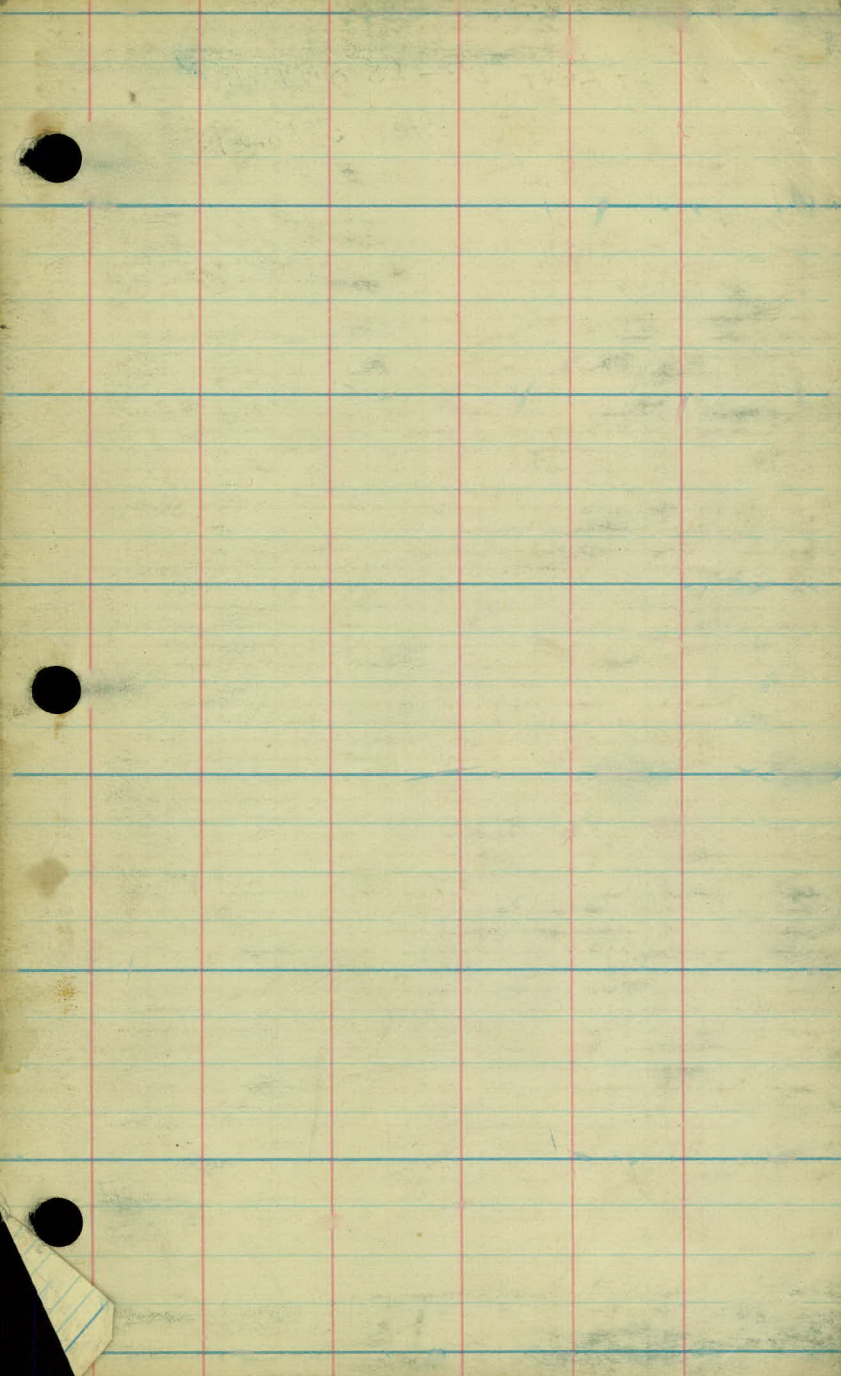
370 + 08.5

Tree  
48.64  
69.65  
House  
46.46  
Tree

E. 1/4 Cor. Sec. 12







T.P. 20 ft Left 23+25 on F.P.

Elev. 578.89.



7

SPX.

□

| STA. | +    | H.I.   | - | ELEV. C.P. RD. |
|------|------|--------|---|----------------|
| B.M. | 7.60 | 507.60 |   | 500.00         |
| 1+00 |      |        |   | 60             |

$$\begin{array}{r} 6.0 \quad \frac{64}{15} \quad \frac{72}{20} \quad \frac{80}{33} \quad \frac{90}{-20} \end{array}$$



Sta

Alt A Pt.

105+50 =

100+00

P.P.

• 4942

□ Mant.

59<sup>58</sup>

• G.P.

$\Delta L \quad \Delta R$

$79+15^{65}$  P.I.

$70+00$  P.O.T.

$70+00$

$52+33^9$

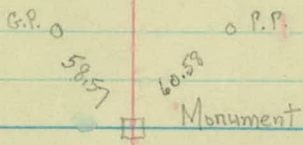
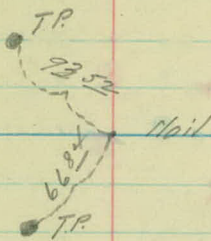
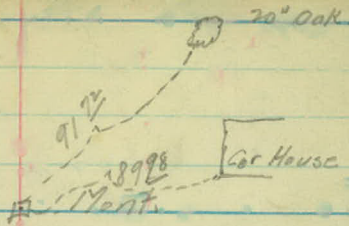
$45+00$  P.O.T.

Nail

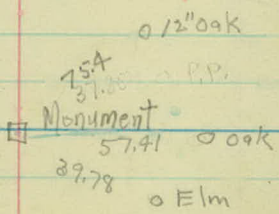
$26+31^4$  P.I.

$0^{\circ}15'$





Linwood Road



Ridge

STP POINT A L. Δ P.

36+ P.I. 0°-00'

P.O.T.

0+00 P.O.T.

Recopied. C.W. Boutwell

1/31/34.

Alignment.

East Co. Line.

Sta 0+00-131+89½.

Sta. Point Alt. Δ Rt.

70+00 P.O.T.

52+73<sup>20</sup>

45+00 P.O.T.

Nail

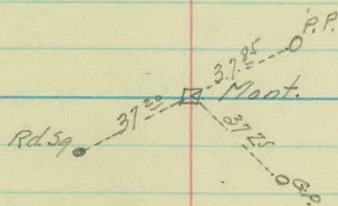
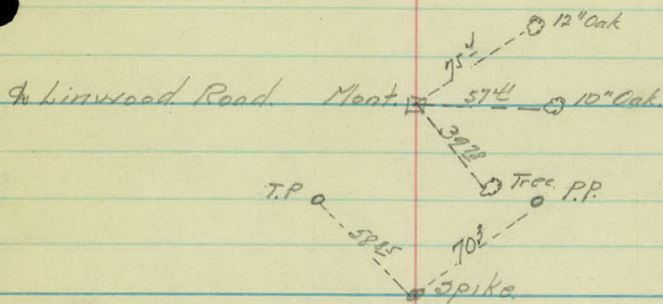
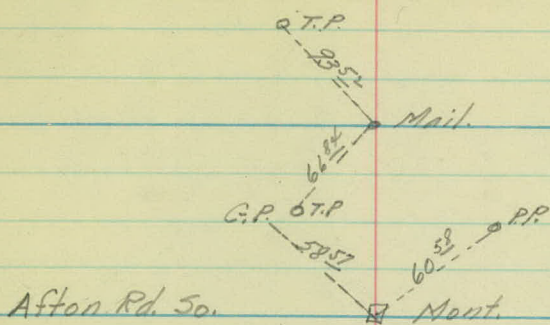
26+31.4 P.I.

0°-15'

14+98.8 P.O.T.

0+00 Beg East Co Line at Hynwood Rd.





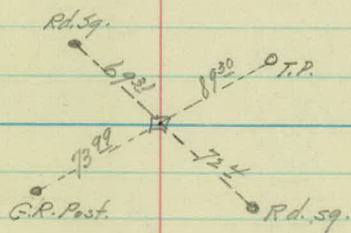
Sta Point Abt. Alt.

131+896 Pl. 0°.

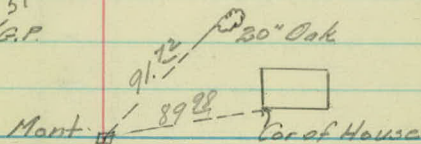
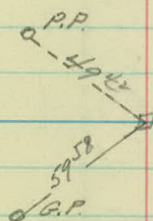
128+002

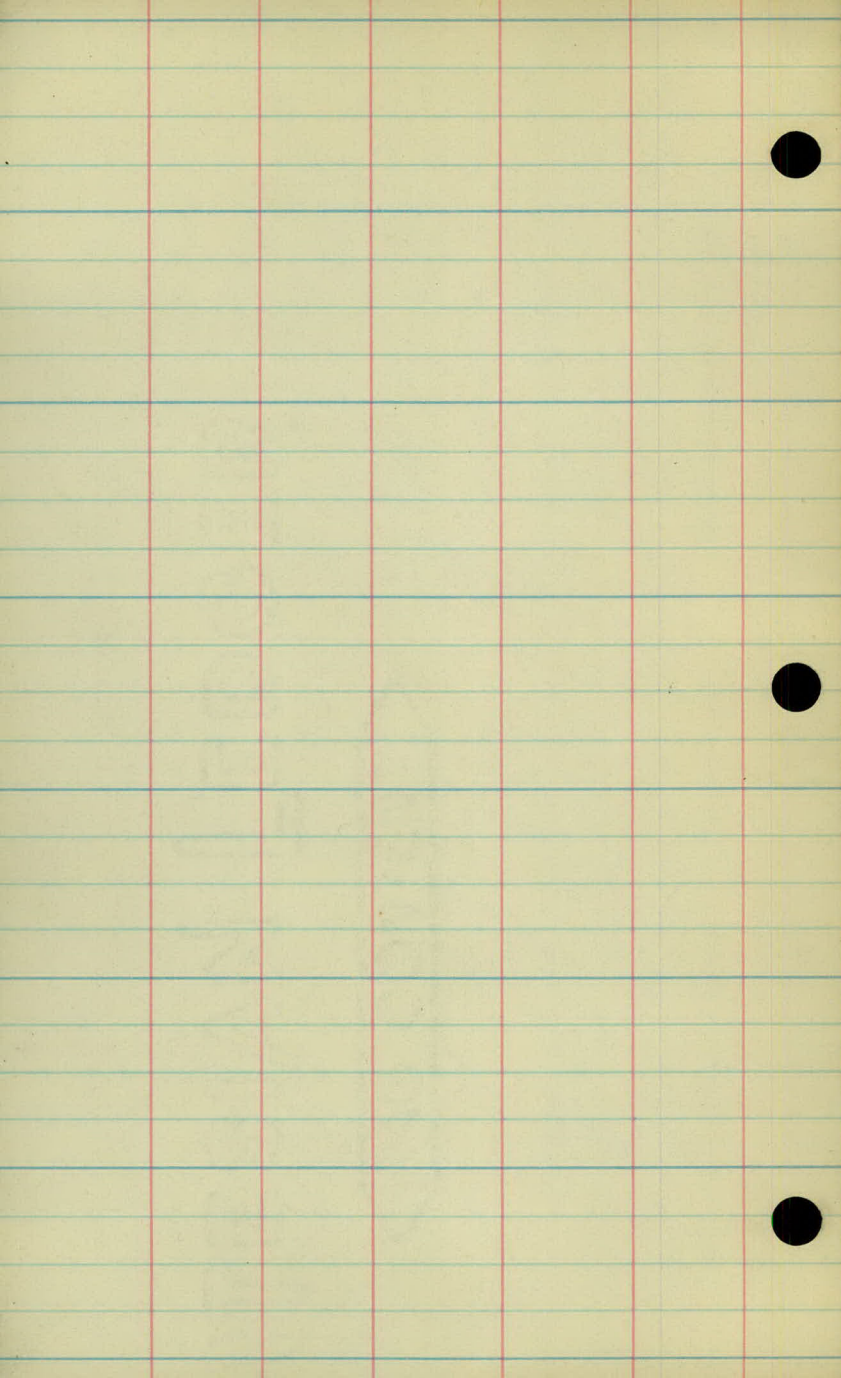
105+502 Pl. 0°-23'

79+15<sup>65</sup> Pl.



Afton Rd 50.







Cross Section  
Slope Stakes

East Co. line

East County Line Road.

Station Point  $\Delta L \Delta R$ .

26+31<sup>8</sup> P.I.

14+98<sup>8</sup> P.O.T.

0+00 P.O.T.

Sta 0+00 = Intersection of E. Co Line & Highwood Road.

11/29/33

o 12' Oak

75A

57.91 o Oak

59.78 o Tree

o P.P.

T.P. o 58.85

70.3

o Spike

37.85 o P.P.

Point of Beginning of Highway Road

Monument

o 37.20

37.75

o G.P.

Rd. Sign

# East County Line Road

| Sta  | + H.I | -                  | Elev  | Gr. Pd.            |
|------|-------|--------------------|-------|--------------------|
| BM   |       |                    | 502.0 |                    |
|      | 850   | 508.50             |       |                    |
| 0+00 |       |                    |       | 502.1              |
| +07  |       |                    |       | 602.1              |
| +12  |       |                    |       | 02.1               |
| +50  |       |                    |       | 01.6               |
| 1+00 |       |                    |       | 01.1               |
| +27  |       |                    |       | 01.3               |
| +40  |       |                    |       | 01.5               |
| 2+00 |       |                    |       | 034                |
| T.P. | 7.75  | 516.04<br>(515.04) | 0.21  | 508.29<br>(507.29) |
| 3+00 |       |                    |       | 08.6               |
| +40  |       |                    |       | 11.3               |
| 4+00 |       |                    |       | 14.8               |
| T.P. | 11.29 | 527.12<br>(526.12) | 0.21  | 515.83<br>(514.83) |
| +50  |       |                    |       | 17.2               |



11/29/33

B.N. R. Spike in Power Pole 25' R + 40 + 20 Elev. Assumed.

$$\begin{array}{cccccccccccc}
 4.1 & 4.7 & 6.4 & 6.1 & & 6.4 & 6.6 & 6.5 & 6.6 & 6.3 & 7.0 & 7.2 \\
 4.0 & 3.0 & 2.0 & 1.0 & & 6.4 & 7.0 & 1.0 & 1.6 & 2.0 & 3.0 & 4.0 \\
 4.1 & 4.7 & 5.2 & 6.1 & & 6.4 & 6.7 & 7.0 & 7.1 & 7.9 & 9.2 \\
 4.0 & 3.0 & 2.0 & 1.0 & & 6.4 & 6.7 & 7.0 & 7.1 & 7.9 & 9.2 \\
 4.8 & 5.2 & 5.7 & 6.1 & & 6.4 & 6.7 & 6.9 & 11.1 & 11.7 & 11.4 & 12.7 \\
 4.0 & 3.0 & 2.0 & 1.0 & & 6.4 & 6.7 & 6.9 & 11.1 & 11.7 & 11.4 & 12.7
 \end{array}$$

$$\begin{array}{cccccccccccc}
 8.6 & 8.5 & 8.6 & 6.6 & & 7.9 & 7.3 & 7.5 & 12.0 & 12.1 & 12.8 \\
 4.0 & 3.0 & 2.1 & 1.7 & & 12.9 & 7.0 & 14 & 22.2 & 30 & 40
 \end{array}$$

$$\begin{array}{r}
 7.4 \\
 0.0 \\
 \hline
 7.4
 \end{array}$$

$$\begin{array}{cccccccccccc}
 9.8 & 9.8 & 9.5 & 7.1 & & 7.3 & 7.6 & 7.6 & 11.3 & 11.9 & 12.4 \\
 4.0 & 3.0 & 2.2 & 1.8 & & 12.2 & 7.4 & 8.0 & 14 & 20 & 30 & 40
 \end{array}$$

$$\begin{array}{cccccccccccc}
 10.3 & 10.5 & 11.1 & 10.4 & 7.3 & & 7.1 & 7.6 & 7.5 & 12.9 & 13.2 & 13.1 \\
 4.0 & 3.4 & 2.9 & 1.9 & 1.3 & & 11 & 8.0 & 13 & 21 & 30 & 40
 \end{array}$$

$$\begin{array}{cccccccccccc}
 10.9 & 10.1 & 9.7 & 7.7 & 4.9 & & 7.6 & 7.4 & 13.1 & 13.3 & 12.6 \\
 4.0 & 3.0 & 2.0 & 1.4 & 1.1 & & 8.0 & 7.0 & 12.0 & 18 & 30 & 40
 \end{array}$$

$$\begin{array}{r}
 5.1 \\
 0.0 \\
 \hline
 5.1
 \end{array}$$

$$\begin{array}{cccccccccccc}
 8.2 & 7.7 & 7.6 & 5.4 & & 5.2 & 5.4 & 5.5 & 10.5 & 10.7 & 11.8 \\
 4.0 & 3.0 & 2.1 & 1.8 & & 11 & 9.0 & 14 & 22 & 30 & 40
 \end{array}$$

$$\begin{array}{r}
 7.4 \\
 0.0 \\
 \hline
 7.4
 \end{array}$$

$$\begin{array}{cccccccccccc}
 8.6 & 9.2 & 8.4 & 7.0 & & 7.6 & 7.2 & 7.5 & 10.7 & 10.7 & 10.5 \\
 4.0 & 3.0 & 1.8 & 1.4 & & 9.0 & 7.4 & 10.2 & 16.2 & 21.8 & 30 & 40
 \end{array}$$

$$\begin{array}{cccccccccccc}
 3.9 & 5.9 & 6.2 & 5.5 & 6.4 & 6.3 & 5.9 & & 5.2 & 5.1 & 7.1 & 7.1 & 5.6 & 5.7 & 5.8 \\
 3.5 & 3.0 & 2.5 & 2.0 & 1.9 & 1.6 & 1.5 & & 10.2 & 4.7 & 12.0 & 18 & 21 & 23 & 26.4 & 30 & 40
 \end{array}$$

$$\begin{array}{cccccccccccc}
 0.4 & 9.5 & 9.3 & 6.3 & 6.6 & 2.5 & 2.7 & 1.9 & 1.4 & 1.3 & 1.4 & 1.9 & 3.6 & 3.6 & 4.1 & 1.9 & 2.1 \\
 +0.4 & 10 & 3.7 & 2.8 & 2.4 & 1.4 & 1.2 & 1.6 & 1.4 & 9.0 & 1.2 & 11 & 16.2 & 18 & 19.6 & 21.8 & 30 & 40
 \end{array}$$

$$\begin{array}{cccccccccccc}
 8.8 & 6.2 & 6.2 & 9.0 & 8.5 & 10.8 & 10.2 & 10.1 & & 10.5 & 10.7 & 12.4 & 12.8 & 11.5 & 12.0 \\
 +1.1 & 4.0 & 3.5 & 3.0 & 2.8 & 3.8 & 1.5 & 1.5 & & 11.0 & 9.9 & 10 & 13 & 16.2 & 21.7 & 25 & 40
 \end{array}$$

Sta + H.I - Elev Gr Rod.

527.12  
526.12

5+00

196

+50

220

6+00

249

T.P. 12.19

536.93  
535.93

2.38

524.74  
523.74

+50

7+00

T.P.

6.31

530.62  
529.62

On Rock 25' of 7+15

12/1/83

T.P.

542.51  
11.93 541.55

529.62

7+50

143

8+00

+50

9+00

T.P.

12.34

554.31  
553.35

0.54

542.01  
541.01

+50

11/29/33

$$\frac{7.1}{10.4} \frac{42}{42} \frac{6.7}{37} \frac{6.6}{30} \frac{7.0}{240} \frac{9.0}{222} \frac{8.9}{17} \frac{7.9}{14} \left( \frac{7.9}{10} \right) 7.5 \left( \frac{8.0}{10.2} \right) \frac{8.1}{12.5} \frac{10.3}{16.2} \frac{10.6}{19.8} \frac{10.0}{24.8} \frac{11.0}{30} \frac{11.5}{40} \frac{10.8}{\infty} \frac{10.8}{2.9}$$

$$\frac{5.1}{0.0} \frac{3.7}{40} \frac{4.9}{30} \frac{4.1}{14.2} \frac{6.4}{22.2} \frac{6.2}{18.8} \frac{5.3}{15} \frac{5.2}{10} 5.1 \left( \frac{5.6}{10.2} \right) \frac{5.7}{12.6} \frac{7.7}{16.9} \frac{8.3}{21} \frac{8.7}{30} \frac{8.8}{40} \frac{8.2}{\infty} \frac{8.2}{-1.7}$$

$$\frac{3.0}{D.C.1.2} \frac{2.2}{2.2} \frac{3.0}{0.8} \frac{2.8}{40} \frac{3.2}{30} \frac{3.3}{22.6} \frac{3.2}{17} \frac{2.8}{15} \frac{2.5}{10.2} 2.2 \left( \frac{3.0}{10} \right) \frac{3.2}{12.5} \frac{4.0}{16.2} \frac{3.8}{20} \frac{5.0}{30} \frac{5.1}{40} \frac{3.9}{\infty} \frac{3.9}{-1.7}$$

$$\frac{10.9}{D.C.0.16} \frac{11.3}{11.3} \frac{11.3}{11.3} \frac{10.8}{11.3} \frac{11.0}{10.8} \frac{10.8}{17.4} \frac{10.1}{15.6} \frac{9.7}{10} 9.5 \frac{10.1}{10.0} \frac{11.0}{12.4} \frac{11.8}{16.8} \frac{11.6}{21.8} \frac{12.4}{30} \frac{12.8}{40} \frac{11.6}{\infty} \frac{11.6}{-2.1}$$

$$\frac{7.9}{D.C.1.3} \frac{7.5}{0.3} \frac{8.6}{40} \frac{8.4}{30} \frac{7.7}{21.8} \frac{7.9}{19} \frac{7.6}{16} \frac{7.5}{10} 7.2 \frac{7.8}{10.2} \frac{8.1}{14.2} \frac{8.0}{18.0} \frac{10.1}{30} \frac{10.5}{40} \frac{9.1}{\infty} \frac{8.9}{-1.7} \frac{D.C.0.0}{2.12}$$

12/1/33

On Rock 25' Left of Sta 7+15

$$\frac{11.4}{D.C.1.4} \frac{11.0}{-0.2} \frac{11.1}{40} \frac{11.7}{30} \frac{11.8}{22.2} \frac{11.4}{19.2} \frac{11.1}{16} \left( \frac{11.2}{10} \right) 11.8 \left( \frac{11.1}{10} \right) \frac{11.2}{16} \frac{12.0}{2.5} \frac{11.5}{2.6} \frac{11.7}{30} \frac{11.7}{40} \frac{11.8}{\infty} \frac{11.8}{D.C.0.9}$$

$$\frac{9.4}{D.C.0.6} \frac{8.9}{-0.2} \frac{8.2}{40} \frac{8.3}{30} \frac{8.2}{24.2} \frac{8.4}{23.2} \frac{8.4}{21} \frac{8.6}{20} \left( \frac{8.4}{10} \right) 8.0 \left( \frac{8.1}{10} \right) \frac{9.2}{26.4} \frac{7.5}{27.8} \frac{8.1}{40} \frac{8.7}{-0.7} \frac{8.9}{D.C.1.1}$$

$$\frac{7.2}{D.C.0.4} \frac{6.0}{-0.4} \frac{2.3}{40} \frac{3.7}{30} \frac{3.8}{25.6} \frac{7.2}{21.8} \frac{7.2}{18.2} \frac{6.2}{17.4} \left( \frac{5.9}{10} \right) 5.6 \left( \frac{5.9}{10} \right) \frac{6.5}{23.8} \frac{4.8}{25.4} \frac{5.4}{40} \frac{6.2}{-0.6} \frac{6.2}{D.C.1.2}$$

$$\frac{D.C.0.0}{2.1} \frac{9.7}{15} \frac{11.3}{40} \frac{10.7}{30} \frac{5.0}{21.2} \frac{5.0}{18} \frac{3.8}{16.8} \left( \frac{3.2}{10} \right) 2.9 \left( \frac{3.3}{10} \right) \frac{3.8}{19.7} \frac{1.6}{21.9} \frac{2.0}{30} \frac{2.6}{40} \left( \frac{-0.2}{10} \right) \frac{1.8}{2.4} \frac{1.8}{D.C.1.0}$$

$$\frac{7.4}{40} \frac{7.9}{27.2} \frac{11.4}{25} \frac{14.7}{21.2} \frac{13.6}{18.2} \frac{13.1}{17.2} \left( \frac{13.6}{10} \right) 12.3 \left( \frac{12.5}{10} \right) \frac{13.0}{20} \frac{12.2}{21} \frac{12.3}{24.4} \frac{11.8}{15.2} \frac{12.0}{40} \left( \frac{-0.4}{10} \right) \frac{1.2}{3.0} \frac{1.2}{D.C.1.0}$$

| Sta   | + | H.I                 | - | Elev |
|-------|---|---------------------|---|------|
| 10+00 |   | (5.53.35)<br>554.35 |   | 10.0 |

|     |  |  |  |     |
|-----|--|--|--|-----|
| +50 |  |  |  | 7.8 |
|-----|--|--|--|-----|

|       |  |  |  |     |
|-------|--|--|--|-----|
| 11+00 |  |  |  | 5.7 |
|-------|--|--|--|-----|

|     |  |  |  |     |
|-----|--|--|--|-----|
| +50 |  |  |  | 3.7 |
|-----|--|--|--|-----|

|       |  |  |  |     |
|-------|--|--|--|-----|
| 12+00 |  |  |  | 1.7 |
|-------|--|--|--|-----|

|      |       |                    |      |                  |
|------|-------|--------------------|------|------------------|
| T.P. | 12.98 | 566.40<br>(565.40) | 0.93 | 553.45<br>552.52 |
|------|-------|--------------------|------|------------------|

|     |  |  |  |      |
|-----|--|--|--|------|
| +50 |  |  |  | 12.1 |
|-----|--|--|--|------|

|       |  |  |  |      |
|-------|--|--|--|------|
| 13+00 |  |  |  | 10.2 |
|-------|--|--|--|------|

|     |  |  |  |     |
|-----|--|--|--|-----|
| +50 |  |  |  | 8.5 |
|-----|--|--|--|-----|

|       |  |  |  |     |
|-------|--|--|--|-----|
| 14+00 |  |  |  | 7.0 |
|-------|--|--|--|-----|

|     |  |  |  |     |
|-----|--|--|--|-----|
| +50 |  |  |  | 5.7 |
|-----|--|--|--|-----|

|       |  |  |  |     |
|-------|--|--|--|-----|
| 15+00 |  |  |  | 4.5 |
|-------|--|--|--|-----|

|     |  |  |  |     |
|-----|--|--|--|-----|
| +50 |  |  |  | 3.2 |
|-----|--|--|--|-----|

|      |  |  |      |                  |
|------|--|--|------|------------------|
| T.P. |  |  | 0.92 | 565.48<br>564.48 |
|------|--|--|------|------------------|





|       | +    | H.I.             | -    | Elev             | Gr.Rd. |
|-------|------|------------------|------|------------------|--------|
|       | 9.01 | 574.59<br>573.99 |      |                  |        |
| 16+00 |      |                  |      |                  | 9.8    |
| +50   |      |                  |      |                  | 8.8    |
| +88   |      |                  |      |                  |        |
| 17+00 |      |                  |      |                  | 8.2    |
| +50   |      |                  |      |                  | 7.9    |
| 18+00 |      |                  |      |                  | 7.6    |
| +18   |      |                  |      |                  | 7.7    |
| TIP   | 7.61 | 573.76<br>572.16 | 8.94 | 565.55<br>564.55 |        |
| +35   |      |                  |      |                  | 6.3    |
| +50   |      |                  |      |                  | 6.3    |
| 19+00 |      |                  |      |                  | 5.7    |
| +13   |      |                  |      |                  |        |
| +50   |      |                  |      |                  | 4.9    |
| 20+00 |      |                  |      |                  | 3.9    |
| +38   |      |                  |      |                  |        |
| +50   |      |                  |      |                  | 3.0    |
| 21+00 |      |                  |      |                  | 2.1    |

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$$\frac{7.8}{0.20} \bigg| 25.0$$

$$\frac{7.2}{40} \frac{7.5}{30} \frac{7.6}{28} \frac{10.3}{2.2} \left( \frac{10.1}{10} \right) 9.8 \left( \frac{10.3}{10} \right) \frac{10.3}{16} \frac{12.7}{20.6} \frac{12.4}{25} \frac{12.3}{20} \frac{12.0}{40} \frac{12.0}{20} \frac{12.7}{2.9}$$

$$\frac{5.9}{0.2.9} \bigg| 25.9$$

$$\frac{5.2}{40} \frac{5.4}{30} \frac{5.5}{24} \frac{9.1}{22} \left( \frac{9.1}{10} \right) 8.8 \left( \frac{9.5}{10} \right) \frac{9.0}{15} \frac{11.2}{19} \frac{10.9}{30} \frac{10.5}{40} \frac{11.3}{20} \frac{11.3}{2.5}$$

D.C.00

$$\frac{3.8}{0.4.4} \bigg| 27.2$$

$$\frac{2.8}{40} \frac{3.4}{30} \frac{3.6}{23} \frac{8.6}{20} \left( \frac{8.3}{10} \right) 8.2 \left( \frac{8.8}{10} \right) \frac{8.5}{14} \frac{10.1}{17} \frac{9.3}{20} \frac{8.6}{40} \frac{9.7}{15} \frac{9.7}{2.05}$$

$$\frac{4.2}{0.2.7} \bigg| 26.7$$

$$\frac{3.7}{40} \frac{3.8}{30} \frac{4.7}{25} \frac{8.4}{22} \left( \frac{8.1}{10} \right) 7.9 \frac{8.3}{10} \frac{9.0}{15} \frac{7.6}{30} \frac{6.9}{40} \frac{8.3}{22.5} \frac{8.3}{2.16}$$

$$\frac{8.7}{D.C.09} \bigg| 21.9$$

$$\frac{7.2}{40} \frac{8.0}{30} \frac{8.6}{18} \frac{7.8}{11} 7.6 \frac{7.9}{10} \frac{9.1}{15} \frac{9.2}{30} \frac{9.0}{40} \frac{9.0}{21} \frac{9.0}{D.C.05}$$

$$\frac{7.6}{40} \frac{8.2}{30} \frac{8.8}{18} \frac{7.8}{11} 7.7 \left( \frac{7.8}{10} \right) \frac{8.0}{16} \frac{9.7}{21} \frac{9.8}{30} \frac{10.0}{40} \frac{9.2}{21.0} \frac{9.2}{2.00}$$

$$\frac{6.3}{40} \frac{7.1}{30} \frac{7.5}{18} \frac{6.6}{11} 6.3 \left( \frac{6.5}{10} \right) \frac{6.6}{14} \frac{13.4}{25} \frac{13.5}{30} \frac{13.5}{40} \quad \times$$

$$\frac{8.3}{D.C.00} \bigg| 21.0$$

$$\frac{6.3}{40} \frac{7.5}{30} \frac{7.9}{18} \frac{6.5}{11} 6.3 \left( \frac{6.5}{10} \right) \frac{6.5}{15} \frac{13.3}{24.6} \frac{14.1}{30} \frac{14.0}{40} \frac{14.1}{30.5} \frac{14.1}{F.7.8}$$

$$\frac{7.3}{D.C.0.4} \bigg| 21.4$$

$$\frac{6.3}{40} \frac{7.4}{30} \frac{7.8}{17} \frac{6.2}{11} 5.7 \left( \frac{5.9}{10} \right) \frac{5.8}{15.4} \frac{9.3}{21.2} \frac{10.2}{30} \frac{10.5}{40} \frac{9.5}{22.5} \frac{9.5}{F.3.8}$$

D.C.00

$$\frac{7.7}{F.2.8} \bigg| 20.6$$

$$\frac{7.5}{40} \frac{7.6}{30} \frac{7.8}{18} \frac{5.2}{11} 4.9 \left( \frac{5.2}{10} \right) \frac{5.3}{16.2} \frac{9.7}{22.8} \frac{10.8}{30} \frac{11.8}{40} \frac{10.1}{22.0} \frac{10.1}{F.5.4}$$

$$\frac{6.6}{F.2.7} \bigg| 20.4$$

$$\frac{7.0}{40} \frac{6.9}{30} \frac{6.7}{19} \frac{9.3}{11} 3.9 \left( \frac{9.0}{10} \right) \frac{3.8}{16.2} \frac{7.3}{22} \frac{7.4}{30} \frac{7.6}{40} \frac{7.3}{22.8} \frac{7.3}{F.3.2}$$

D.C.00

$$\frac{4.7}{D.C.0.2} \bigg| 21.3$$

$$\frac{4.8}{40} \frac{4.4}{30} \frac{4.7}{17} \frac{3.2}{12} 3.0 \left( \frac{3.2}{10} \right) \frac{3.1}{16.2} \frac{4.6}{19.4} \frac{5.6}{30} \frac{6.7}{40} \frac{4.6}{22.5} \frac{4.6}{F.7.5}$$

$$\frac{2.6}{D.C.0.5} \bigg| 22.5$$

$$\frac{0.5}{36} \frac{1.2}{30} \frac{2.1}{20} \frac{2.1}{12} 2.1 \left( \frac{2.3}{10} \right) \frac{2.3}{17} \frac{6.9}{23.9} \frac{7.1}{30} \frac{8.0}{40} \frac{6.6}{21.0} \frac{6.6}{F.7.5}$$

|       | +    | H.I                                  | -    | Elev                                 | Gr Rod |
|-------|------|--------------------------------------|------|--------------------------------------|--------|
| 21+50 |      |                                      |      |                                      | 1.1    |
| T.P   | 8.75 | <sup>581.01</sup><br><u>(580.01)</u> | 0.90 | <sup>572.26</sup><br><u>(571.26)</u> |        |
| +60   |      |                                      |      |                                      |        |
| +72   |      |                                      |      |                                      | 8.4    |
| 22+00 |      |                                      |      |                                      | 7.5    |
| +18   |      |                                      |      |                                      |        |
| +30   |      |                                      |      |                                      | 6.6    |
| +50   |      |                                      |      |                                      | 5.9    |
| +60   |      |                                      |      |                                      |        |
|       |      |                                      |      |                                      | 4.0    |
| 23+00 |      |                                      |      |                                      |        |
| T.P.  |      |                                      | 1.12 | <sup>578.89</sup><br><u>(578.89)</u> |        |



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$$\frac{1.6}{D.C.1.5} \left| \frac{1}{2.2.5} \right.$$

$$\frac{0.3}{40} \frac{1.1}{30} \frac{1.6}{20} \frac{1.2}{10} 1.1 \left( \frac{1.5}{10} \right) \frac{1.4}{16} \frac{6.4}{24} \frac{7.1}{30} \frac{7.4}{40} \quad 2.4 \left| \frac{6.8}{F.5.7} \right.$$

D.C.00

$$\frac{13.6}{40} \frac{14.2}{30} \frac{13.8}{20} \frac{8.6}{10} 8.4 \left( \frac{8.6}{10} \right) \frac{8.6}{16} \frac{14.2}{24} \frac{14.3}{30} \frac{14.6}{40}$$

$$\frac{11.8}{F.4.3} \left| \frac{3}{2.2.5} \right.$$

$$\frac{10.7}{40} \frac{11.5}{30} \frac{11.7}{20} \frac{10.8}{16} \frac{7.8}{11} 7.5 \frac{7.9}{11} \frac{11.6}{16} \frac{12.2}{24} \frac{12.5}{30} \frac{12.6}{40} \quad 2.4 \left| \frac{13.0}{F.5.5} \right.$$

D.C.00

$$\frac{7.5}{40} \frac{6.8}{30} \frac{6.6}{14} \frac{6.8}{10} 6.6 \frac{7.0}{11} \frac{8.6}{18} \frac{8.3}{30} \frac{8.1}{40} \quad 2.4 \left| \frac{8.6}{D.C.00} \right.$$

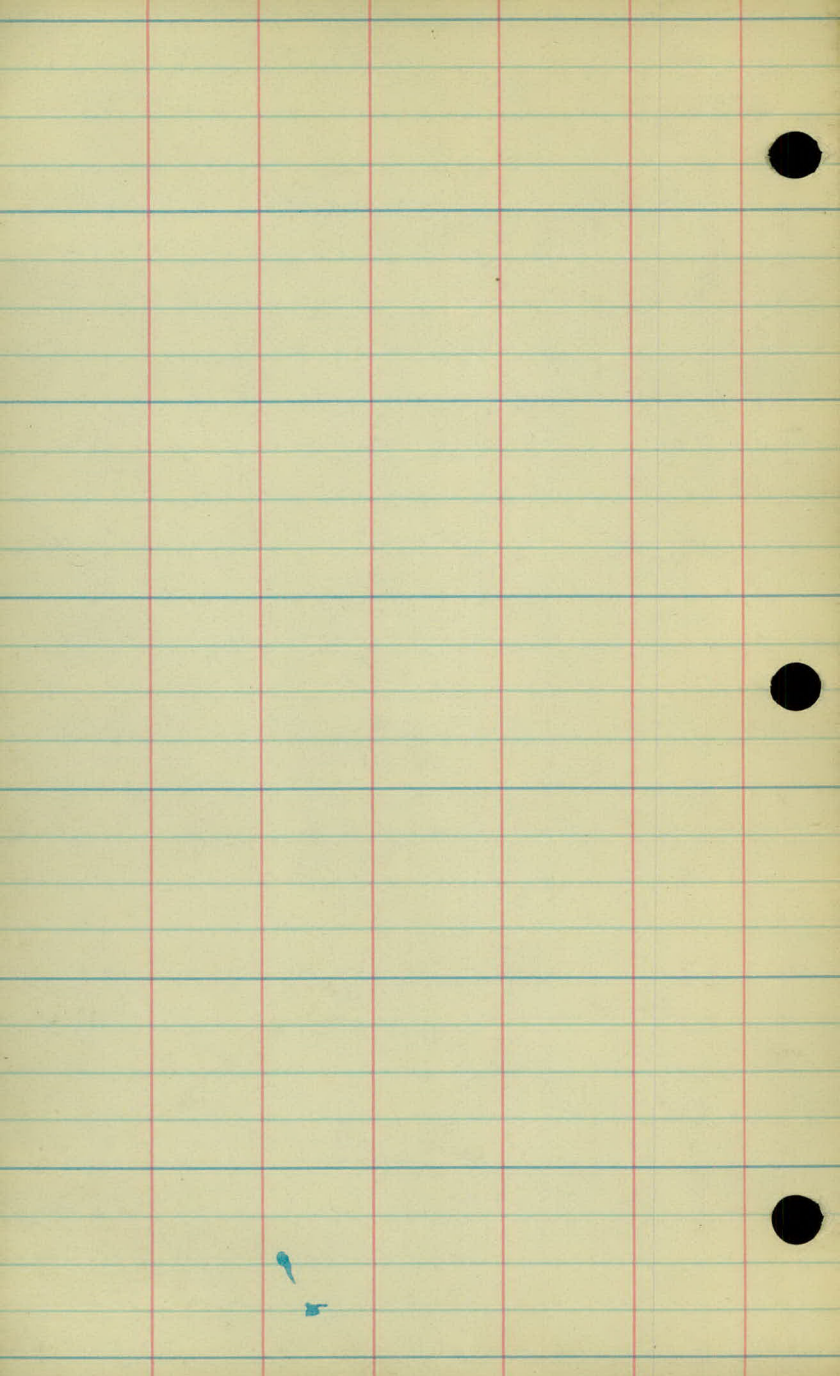
$$\frac{7.8}{D.C.0.5} \left| \frac{1.6}{2.2.5} \right.$$

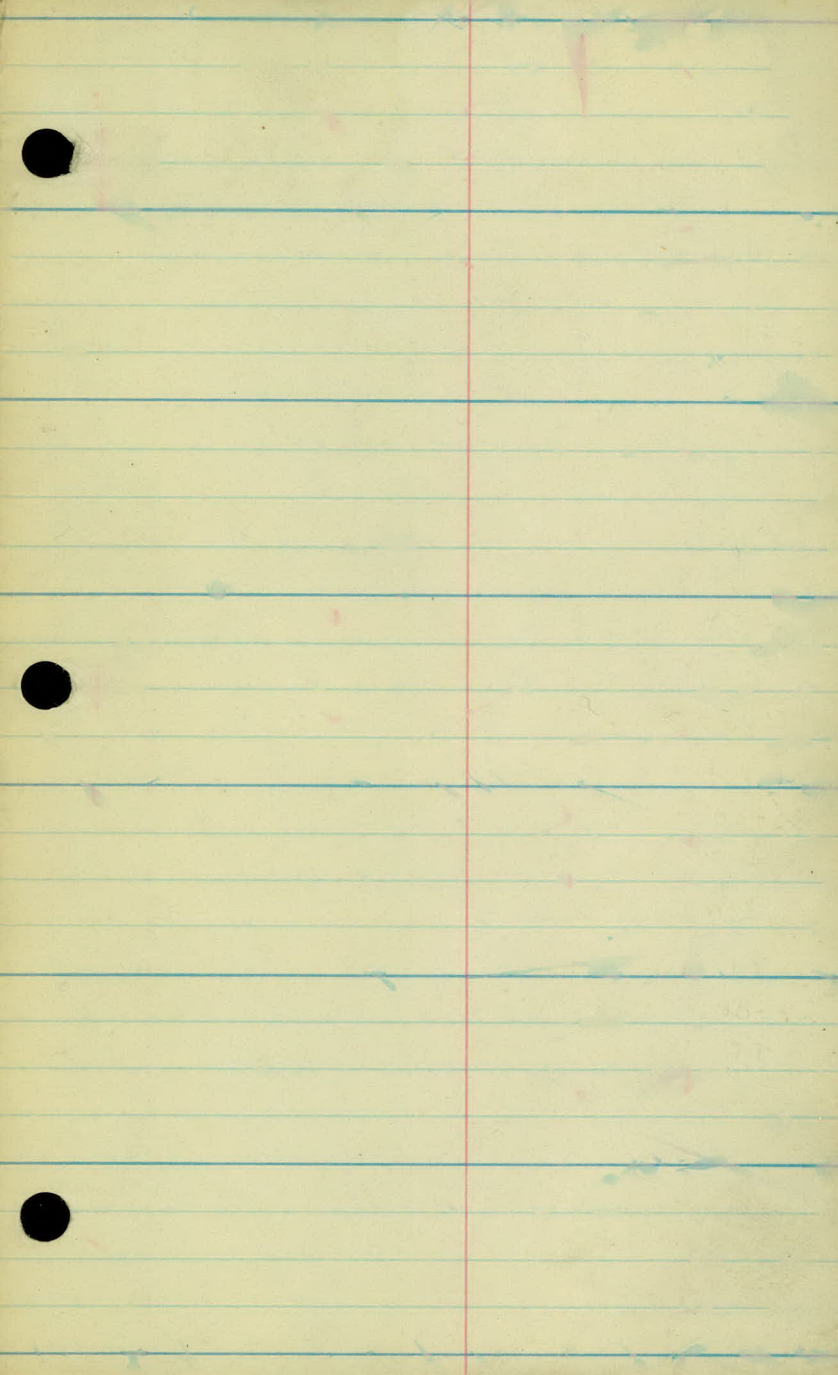
$$\frac{8.5}{40} \frac{8.1}{30} \frac{7.2}{18} \frac{6.0}{13} \frac{6.0}{11} 5.9 \frac{6.2}{10} \frac{6.2}{14} \frac{6.0}{18} \frac{4.9}{30} \frac{4.3}{40} \quad 2.4 \left| \frac{5.7}{D.C.1.8} \right.$$

D.C.00

$$\frac{8.0}{F.4.0} \left| \frac{0}{2.2.5} \right. \quad \frac{7.5}{40} \frac{8.0}{30} \frac{7.8}{21} \frac{7.5}{17} \frac{4.4}{11} 4.0 \left( \frac{4.1}{10} \right) \frac{4.8}{18} \frac{4.2}{19} \frac{3.8}{30} \frac{2.9}{40} \quad 2.3.0 \left| \frac{4.0}{D.C.2.0} \right.$$

20 ft. Left of 23+2.5 on Top Fence Post





6+9

+

H.1

-

Gr Red

T.P.

11.85

591.44  
590.45

23+27

23+50

24+00

+10

+30

+50

+75

+84

25+00

+18

+50

+63

26+00

T.P.

3.06

588.38

587.38



12/2/33

15.4  
D.C.00.0

13.8 14.1 15.2 13.9 13.7 14.6 14.2 14.1 14.1  
40 30 18 10 13.4 10 18 14 30 20

10.5 10  
C.2.0 14

3.6 12.1 12.7 12.4 13.0 12.5 12.8 13.6 12.8 12.7 12.8  
20 10 20 15 10 10 10 18 18 30 40 20 12.7  
20 0.0

0.6 0.7  
C.4.9 14

0.3 0.5 8.0 11.7 10.9 10.5 11.2 10.8 4.1 3.7 4.0  
40 30 20 10 10 10 10 21.8 26 30 40 20 3.6  
20 C.6.9

-0.8 -0.6 8.6 10.8 10.5 10.2 10.5 10.4 3.1 3.1 2.6  
40 31 19 16 10 10 10 21 27 30 40

9.8 6.0 5.3 9.7 9.5 9.4 9.7 9.3 3.1 2.7  
40 32 21 16 10 10 10 21 26 40

3.8 1  
C.4.7 14

6.0 4.1 4.6 9.0 9.5 8.9 8.6 2.9 2.9 3.1 2.9  
40 30 21 16 10 10 10 17 19 30 40 6 2.9  
6 C.5.6

12.0 10.3 7.5 7.3 7.8 7.7 7.9 7.3 3.1 3.1 3.1  
40 30 19 16 10 10 10 14 26 30 40

D.C.00

13.0 10  
F.6.0 27

14.3 13.2 12.4 11 7.2 7.0 7.0 6.4 5.6 5.2 5.1 6.1  
40 30 23 16 10 10 10 20 30 40 20 6.1  
20 C.0.9

12.0 10  
F.6.3 27

12.4 12.2 11.0 6.2 6.2 5.7 5.8 8.0 8.4 2.4 2.4 8.0  
40 30 22 15 10 10 11 13 27 40 20 8.0  
20 F.1.2

D.C.00

D.C.00

4.0 4.4 4.8 4.1  
11 15 14.8

On Top of "X" Culvert Marker 35ft left of 26+10

|      |       |                         |                                         |
|------|-------|-------------------------|-----------------------------------------|
| T.P. | 12.11 | 601.49<br><u>600.49</u> | 588.38<br><u>587.38</u>                 |
| B.M. | 11.53 | 601.49                  | 11.53<br><u>587.96</u><br><u>586.96</u> |

+95

26+00

+18

+45

+53

+63

27+00

+35

+50

28+00

+50

+84

+93

29+00

12/4/33

On Top of 4x4" Culvert Marker 35 ft Left of 26+10  
 R.R. Spike in Reference Tree 50 ft R of 26+35  
 D.C.00

$$\frac{12.2}{0.01.0} \left| \begin{array}{c} 12.0 \\ 12.0 \end{array} \right.$$

$$\frac{17.5}{40} \frac{15.5}{30} \frac{15.1}{20} \frac{14.6}{10} 14.2 \frac{14.5}{10} \frac{14.8}{16.0} \frac{14.3}{16.8} \frac{13.8}{27} \frac{14.0}{40.0} \frac{22.1}{14.5} \left| \begin{array}{c} 14.5 \\ 20.17 \end{array} \right.$$

$$\frac{13.6}{40} \frac{13.6}{30} \frac{13.6}{20} \frac{13.8}{10} 13.5 \frac{13.8}{11} \frac{13.2}{16.0} \frac{13.7}{19.0} \frac{13.5}{30} \frac{13.9}{40}$$

$$\frac{12.8}{0.02.0} \left| \begin{array}{c} 12.0 \\ 23.0 \end{array} \right.$$

$$\frac{12.8}{40} \frac{12.7}{30} \frac{12.8}{20} \frac{12.8}{10} 12.8 \frac{13.1}{11} \frac{13.6}{15.6} \frac{13.3}{17.8} \frac{13.3}{30} \frac{13.0}{40} \frac{15.1}{18.4} \left| \begin{array}{c} 18.4 \\ 20.14 \end{array} \right.$$

$$\frac{15.1}{40} \frac{12.2}{30} \frac{12.7}{20} \frac{12.7}{10} 12.5 \frac{13.0}{11} \frac{13.3}{20} \frac{13.1}{20} \frac{12.9}{40}$$

$$\frac{8.9}{40} \frac{10.8}{30} \frac{11.7}{21.2} \frac{13.0}{20} \frac{12.5}{10} 12.3 \frac{12.8}{11} \frac{13.0}{20} \frac{12.6}{30} \frac{12.4}{40}$$

$$\frac{8.4}{0.2.8} \left| \begin{array}{c} 8.0 \\ 25.8 \end{array} \right.$$

$$\frac{7.2}{40} \frac{8.0}{30} \frac{8.7}{21.4} \frac{11.9}{18.8} \frac{11.5}{11} 11.2 \frac{11.4}{11} \frac{11.4}{18} \frac{9.7}{21} \frac{9.9}{30} \frac{9.7}{40} \frac{24.5}{9.9} \left| \begin{array}{c} 9.9 \\ 01.3 \end{array} \right.$$

$$\frac{4.0}{40} \frac{5.1}{30} \frac{6.2}{23} \frac{10.9}{18.2} \frac{10.6}{11} 10.4 \frac{10.7}{11} \frac{10.8}{16.8} \frac{6.5}{21.9} \frac{7.1}{30} \frac{7.6}{40}$$

$$\frac{4.2}{0.5.8} \left| \begin{array}{c} 4.0 \\ 21.8 \end{array} \right.$$

$$\frac{3.0}{40} \frac{4.1}{30} \frac{5.3}{22.8} \frac{10.5}{19} \frac{10.3}{11} 10.0 \frac{10.4}{11} \frac{10.6}{17.2} \frac{6.7}{21.8} \frac{7.0}{30} \frac{7.8}{40} \frac{25.9}{7.1} \left| \begin{array}{c} 7.1 \\ 02.9 \end{array} \right.$$

$$\frac{3.7}{0.5.4} \left| \begin{array}{c} 3.0 \\ 28.4 \end{array} \right.$$

$$\frac{2.2}{40} \frac{3.5}{30} \frac{5.2}{22.4} \frac{9.4}{20.2} \frac{9.4}{11} 9.1 \frac{9.3}{11} \frac{9.6}{16.4} \frac{7.5}{17.8} \frac{7.9}{30} \frac{8.2}{40} \frac{24.5}{7.6} \left| \begin{array}{c} 7.6 \\ 01.5 \end{array} \right.$$

$$\frac{7.4}{0.5.2} \left| \begin{array}{c} 7.0 \\ 20.2 \end{array} \right.$$

$$\frac{3.2}{40} \frac{3.2}{30} \frac{3.4}{21.4} \frac{8.7}{18.8} \frac{8.6}{11} 8.6 \frac{9.0}{11} \frac{9.1}{16.6} \frac{7.4}{18.2} \frac{8.2}{30} \frac{8.6}{40} \frac{23.4}{8.0} \left| \begin{array}{c} 8.0 \\ 00.0 \end{array} \right.$$

$$\frac{3.8}{40} \frac{4.2}{30} \frac{6.2}{20.4} \frac{9.1}{18.2} \frac{8.8}{11} 8.6 \frac{9.0}{11} \frac{9.2}{18} \frac{10.4}{30} \frac{11.9}{40}$$

D.C.00

$$\frac{5.3}{0.3.2} \left| \begin{array}{c} 5.0 \\ 26.2 \end{array} \right.$$

$$\frac{4.5}{40} \frac{5.1}{30} \frac{6.1}{19.6} \frac{9.0}{18} \frac{8.7}{11} 8.5 \frac{9.0}{11} \frac{9.0}{19.4} \frac{11.0}{24.9} \frac{13.0}{30} \frac{14.1}{40} \frac{00}{15}$$

601.49  
600.49

29+50

30+00

+50

31+00

+50

32+00

T.P.

5.50

520.45

594.45

11.54

588.95

588.95

+50

+68

33+00

+50

34+00

T.P.

12.54

606.99

588.95

+05

+50

35+00

+50



R  
12/4/33

$$\frac{6.1}{C2.8} \left| \frac{25.8}{25.8} \right|$$

$$\frac{4.8}{40} \frac{6.0}{30} \frac{7.5}{19.6} \left( \frac{8.7}{11} \right) \leftarrow 8.7 \frac{3.3}{11} \frac{3.6}{15.8} \frac{7.6}{24.6} \frac{10.7}{30} \frac{12.0}{40}$$

$$\frac{11.0}{F8.2}$$

$$\frac{2.5}{C6.4} \left| \frac{29.4}{29.4} \right|$$

$$\frac{1.2}{40} \frac{2.3}{30} \frac{4.8}{22} \frac{9.4}{18} \left( \frac{12}{11} \right) \leftarrow 8.9 \frac{3.4}{11} \frac{3.5}{16.2} \frac{8.4}{23.6} \frac{10.0}{30} \frac{11.7}{40}$$

$$\frac{9.1}{F6.3}$$

$$\frac{3.8}{C5.3} \left| \frac{25.3}{25.3} \right|$$

$$\frac{2.3}{40} \frac{3.4}{28} \frac{5.6}{22.2} \frac{9.3}{19} \left( \frac{9.2}{11} \right) \leftarrow 9.1 \frac{3.7}{11} \frac{3.6}{17.2} \frac{7.2}{22.6} \frac{9.7}{30} \frac{12.4}{40}$$

$$\frac{7.5}{F4.5}$$

$$\frac{3.8}{C5.5} \left| \frac{25.5}{25.5} \right|$$

$$\frac{3.2}{40} \frac{3.9}{26} \frac{5.2}{23} \frac{9.7}{19} \left( \frac{9.5}{11} \right) \leftarrow 9.3 \frac{3.5}{11} \frac{3.6}{18.4} \frac{5.7}{22} \frac{8.6}{30} \frac{10.9}{40}$$

$$\frac{10.0}{15}$$

$$\frac{7.2}{C2.4} \left| \frac{25.4}{25.4} \right|$$

$$\frac{4.3}{40} \frac{6.4}{30} \frac{7.4}{23.6} \frac{10.2}{20.2} \left( \frac{10.2}{11} \right) \leftarrow 9.4 \frac{3.9}{11} \frac{3.9}{16.6} \frac{7.0}{24} \frac{9.9}{30} \frac{10.0}{40}$$

$$\frac{9.8}{F6.3}$$

$$\frac{10.7}{D.C.14} \left| \frac{22.4}{22.4} \right|$$

$$\frac{8.9}{40} \frac{10.6}{30} \frac{10.7}{23} \frac{10.0}{20} \left( \frac{10.0}{11} \right) \leftarrow 10.1 \frac{4.8}{11} \frac{5.2}{14.4} \frac{7.6}{21} \frac{7.5}{30} \frac{8.2}{40}$$

$$\frac{9.6}{F5.6}$$

Top of Culvert Marker 15 ft Rt of 32+40

$$\frac{9.2}{F8.2} \left| \frac{25.4}{25.4} \right|$$

$$\frac{9.3}{40} \frac{9.3}{30} \frac{9.2}{24} \frac{4.8}{17.4} \left( \frac{4.9}{11} \right) \leftarrow 4.0 \frac{4.3}{11} \frac{4.8}{16.8} \frac{8.1}{22.4} \frac{6.2}{30} \frac{3.5}{40}$$

$$\frac{8.0}{F4.0}$$

D.C.00

$$\frac{10.0}{F6.2} \left| \frac{27.6}{27.6} \right|$$

$$\frac{10.2}{40} \frac{7.9}{30} \frac{9.9}{26.4} \frac{4.7}{19} \left( \frac{4.2}{11} \right) \leftarrow 3.7 \frac{11.1}{11} \frac{11.2}{19.4} \frac{7.9}{23.8} \frac{6.0}{30} \frac{2.8}{40}$$

$$\frac{6.8}{C4.0}$$

$$\frac{9.9}{F6.4} \left| \frac{27.8}{27.8} \right|$$

$$\frac{10.0}{40} \frac{10.1}{30} \frac{9.7}{26.2} \frac{4.1}{17.8} \left( \frac{3.9}{11} \right) \leftarrow 3.5 \frac{10.7}{11} \frac{11.0}{19.6} \frac{4.3}{24.4} \frac{3.7}{30} \frac{3.8}{40}$$

$$\frac{3.7}{C6.9}$$

$$\frac{3.7}{40} \frac{4.9}{30} \frac{5.3}{22.2} \frac{3.8}{19.2} \left( \frac{3.7}{11} \right) \leftarrow 3.2 \frac{10.5}{11} \frac{10.9}{20} \frac{4.2}{25.2} \frac{3.9}{30} \frac{3.1}{40}$$

$$\frac{4.0}{C6.3}$$

D.C.00

$$\frac{6.7}{C3.6} \left| \frac{26.6}{26.6} \right|$$

$$\frac{5.3}{40} \frac{6.4}{30} \frac{6.9}{22.4} \frac{11.0}{20} \left( \frac{10.7}{11} \right) \leftarrow 10.3 \frac{10.3}{11} \frac{10.6}{20} \frac{4.1}{2.5} \frac{4.1}{30} \frac{3.8}{40}$$

$$\frac{4.1}{C6.2}$$

$$\frac{5.6}{C5.1} \left| \frac{28.1}{28.1} \right|$$

$$\frac{4.2}{40} \frac{5.5}{30} \frac{5.1}{22} \frac{11.6}{14.2} \frac{11.2}{12} \left( \frac{11.2}{11} \right) \leftarrow 10.7 \frac{11.1}{11} \frac{4.8}{19.6} \frac{5.0}{25.2} \frac{5.6}{30} \frac{5.6}{40}$$

$$\frac{4.8}{C5.9}$$

$$\frac{9.0}{C2.0} \left| \frac{28.0}{28.0} \right|$$

$$\frac{8.4}{40} \frac{8.8}{30} \frac{9.2}{24.6} \frac{10.7}{15.4} \frac{11.4}{14.2} \frac{11.3}{12} \left( \frac{11.2}{11} \right) \leftarrow 11.0 \frac{11.4}{11} \frac{11.4}{19.2} \frac{3.0}{26} \frac{1.3}{30} \frac{1.3}{40}$$

$$\frac{2.4}{C8.6}$$

606.99

25478

36400

+12

+50

B.M.

1.51

598.78

9.72

597.27

+56

+64

37400

+50

38400

+50

39400

+16

~~40~~+50

B.M.

12.72

608.95

2.55

596.23

+60

40400

+50

12/4/33

$$\frac{57}{40} \frac{60}{30} \frac{60}{24.2} \frac{122}{14.8} \frac{116}{12} \frac{11.1}{11.1} \frac{112}{11} \frac{10}{19} \frac{0.8}{25.6} \frac{10}{30} \frac{10}{40}$$

$$\frac{3.2}{C.81} \frac{3.1}{3.1}$$

$$\frac{2.7}{40} \frac{3.1}{30} \frac{3.1}{27} \frac{11.9}{14.2} \frac{11.7}{12} \frac{11.3}{11.3}$$

$$\frac{11.2}{11} \frac{11.8}{15} \frac{3.9}{24.8} \frac{4.1}{80} \frac{4.2}{40}$$

$$\frac{30.1}{C.7.1} \frac{4.2}{4.2}$$

$$\frac{2.7}{40} \frac{2.3}{30} \frac{2.0}{26.2} \frac{12.0}{14} \frac{11.8}{12} \frac{11.5}{11.5}$$

$$\frac{11.6}{11} \frac{11.7}{13.6} \frac{5.8}{23.2} \frac{6.3}{30} \frac{7.5}{40}$$

$$\frac{10.5}{C.14} \frac{4}{4}$$

$$\frac{11.7}{40} \frac{11.3}{30} \frac{9.8}{17.2} \frac{12.8}{13.8} \frac{12.2}{11} \frac{11.9}{11.9}$$

$$\frac{12.1}{11} \frac{12.6}{20} \frac{13.0}{30} \frac{13.2}{40}$$

$$\frac{12}{80} \frac{13.1}{D.C.0.8}$$

Top of Rock 40ft Rt of 36+30

D.C.0.0

D.C.0.0

$$\frac{10.9}{F.6.1} \frac{12.2}{12.2}$$

$$\frac{11.1}{40} \frac{11.0}{30} \frac{10.8}{2.5} \frac{5.2}{16} \frac{5.1}{11} \frac{4.8}{4.8}$$

$$\frac{5.1}{11} \frac{5.1}{16} \frac{10.2}{24} \frac{11.2}{30} \frac{11.5}{40}$$

$$\frac{1}{10} \frac{10.8}{F.6.0}$$

$$\frac{12.5}{F.6.7} \frac{12.4}{12.4}$$

$$\frac{12.6}{40} \frac{11.5}{30} \frac{12.1}{24.6} \frac{6.7}{17} \frac{6.3}{11} \frac{5.8}{5.8}$$

$$\frac{6.2}{11} \frac{6.2}{17.2} \frac{12.9}{26.2} \frac{13.2}{30} \frac{13.2}{40}$$

$$\frac{29.8}{F.7.4} \frac{13.2}{13.2}$$

$$\frac{12.7}{F.6.6} \frac{12.2}{12.2}$$

$$\frac{12.6}{40} \frac{12.8}{30} \frac{12.1}{25.6} \frac{6.5}{17.4} \frac{6.5}{11} \frac{6.1}{6.1}$$

$$\frac{6.2}{11} \frac{6.2}{16.4} \frac{13.2}{25.8} \frac{13.6}{30} \frac{14.0}{40}$$

$$\frac{30.0}{F.7.5} \frac{13.6}{13.6}$$

$$\frac{11.9}{F.6.9} \frac{12.8}{12.8}$$

$$\frac{11.7}{40} \frac{11.9}{30} \frac{11.5}{24.2} \frac{5.3}{15} \frac{5.4}{11} \frac{5.0}{5.0}$$

$$\frac{5.3}{11} \frac{5.5}{15} \frac{13.2}{27} \frac{13.4}{30} \frac{13.7}{40}$$

$$\frac{32.0}{F.8.5} \frac{13.2}{13.2}$$

$$\frac{8.2}{F.4.2} \frac{12.4}{12.4}$$

$$\frac{7.6}{40} \frac{8.0}{30} \frac{7.9}{20} \frac{4.3}{11} \frac{4.0}{4.0}$$

$$\frac{4.5}{11} \frac{4.7}{13.4} \frac{10.4}{21.8} \frac{10.6}{30} \frac{10.6}{40}$$

$$\frac{10.6}{F.6.6} \frac{10.6}{10.6}$$

D.C.0.0

$$\frac{3.7}{D.C.1.1} \frac{12.5}{12.5}$$

$$\frac{2.8}{40} \frac{2.9}{30} \frac{3.5}{15.8} \frac{2.1}{11} \frac{2.8}{2.8}$$

$$\frac{3.1}{11} \frac{3.1}{14} \frac{5.1}{18} \frac{5.9}{30} \frac{6.1}{40}$$

$$\frac{19.8}{F.2.4} \frac{5.2}{5.2}$$

Top of Rock 25ft left of 39+85

D.C.0.0

$$\frac{12.2}{D.C.1.1} \frac{12.5}{12.5}$$

$$\frac{11.2}{40} \frac{12.0}{30} \frac{12.6}{14.8} \frac{12.1}{12} \frac{11.7}{11.7}$$

$$\frac{12.0}{11} \frac{12.1}{16.2} \frac{12.9}{18} \frac{13.0}{25.4} \frac{13.2}{30} \frac{13.2}{40}$$

$$\frac{13.2}{D.C.0.5} \frac{13.2}{13.2}$$

$$\frac{9.5}{C.1.0} \frac{12.0}{12.0}$$

$$\frac{9.1}{40} \frac{8.9}{30} \frac{8.8}{25.6} \frac{11.2}{20} \frac{11.4}{15.2} \frac{10.8}{12} \frac{10.5}{10.5}$$

$$\frac{10.9}{11} \frac{10.9}{15.8} \frac{11.6}{18} \frac{11.0}{24} \frac{7.4}{31.4} \frac{7.1}{48}$$

$$\frac{11.3}{D.C.1.2} \frac{11.3}{11.3}$$

608.95

41+00

+50

42+00

+50

43+00

+50

44+00

+50

B.M.

0.25

603.80

5.40

603.55

45+00

+50

46+00

+50

47+00

+50

B.M.

5.39

598.41



$$\frac{9.7}{17.5/8} \left| \frac{2.3}{2.5} \right.$$

$$\frac{5.7}{40} \frac{6.4}{30} \frac{7.1}{26} \frac{7.6}{23} \left( \frac{7.8}{11} \right) 9.5 \frac{9.8}{11} \frac{10.1}{17} \frac{9.6}{22.2} \frac{4.3}{31.8} \frac{4.7}{40} \left| \frac{2.2}{2.5} \right| \frac{9.6}{25.19}$$

$$\frac{6.3}{C.2.2.7} \left| \frac{2.5}{2.5} \right.$$

$$\frac{4.8}{40} \frac{5.4}{30} \frac{6.2}{24.8} \frac{8.8}{22.2} \left( \frac{8.8}{11} \right) 8.5 \frac{9.0}{12.2} \frac{9.9}{15.2} \frac{9.3}{17} \frac{8.5}{22.2} \frac{3.8}{30.6} \frac{4.2}{40} \left| \frac{2.5}{2.5} \right| \frac{8.3}{26.22}$$

$$\frac{5.2}{C.2.2.4} \left| \frac{2.5}{2.5} \right.$$

$$\frac{4.9}{40} \frac{4.8}{30} \frac{5.4}{24.2} \frac{8.1}{21.3} \left( \frac{8.0}{11} \right) 7.8 \left( \frac{7.9}{11} \right) \frac{8.3}{14} \frac{7.9}{22} \frac{4.2}{26.8} \frac{4.4}{30} \frac{4.3}{40} \left| \frac{2.5}{2.5} \right| \frac{4.2}{26.3.4}$$

$$\frac{5.6}{C.1.7} \left| \frac{2.4}{2.4} \right.$$

$$\frac{5.4}{40} \frac{5.9}{30} \frac{5.7}{24} \frac{7.1}{21.2} \left( \frac{7.6}{11} \right) 7.3 \left( \frac{7.6}{11} \right) \frac{7.4}{22} \frac{4.7}{26} \frac{4.7}{30} \frac{4.8}{40} \left| \frac{2.5}{2.5} \right| \frac{6.8}{26.0.5}$$

$$\frac{6.0}{C.1.1} \left| \frac{2.4}{2.4} \right.$$

$$\frac{5.6}{40} \frac{5.6}{30} \frac{6.2}{20.2} \frac{7.4}{20} \left( \frac{7.3}{11} \right) 7.1 \left( \frac{7.4}{11} \right) \frac{7.7}{22} \frac{4.9}{25.6} \frac{5.1}{30} \frac{5.3}{40} \left| \frac{2.4}{2.4} \right| \frac{5.5}{26.1.6}$$

$$\frac{5.9}{C.0.8} \left| \frac{2.3}{2.3} \right.$$

$$\frac{5.6}{40} \frac{5.6}{30} \frac{6.9}{18.8} \frac{7.4}{18.2} \left( \frac{7.3}{11} \right) 7.1 \left( \frac{7.4}{11} \right) \frac{7.7}{23.8} \frac{5.4}{26.8} \frac{5.6}{30} \frac{5.9}{40} \left| \frac{2.2}{2.2} \right| \frac{7.7}{26.6.4}$$

$$\frac{5.8}{C.1.3} \left| \frac{2.4}{2.4} \right.$$

$$\frac{5.1}{40} \frac{5.5}{30} \frac{6.9}{17.2} \frac{7.3}{16.6} \left( \frac{7.1}{11} \right) 7.1 \left( \frac{7.2}{11} \right) \frac{7.6}{24.4} \frac{5.8}{26.2} \frac{5.8}{30} \frac{6.1}{40} \left| \frac{2.2}{2.2} \right| \frac{7.7}{26.1.4}$$

$$\frac{6.0}{C.1.2} \left| \frac{2.4}{2.4} \right.$$

$$\frac{5.2}{40} \frac{5.6}{30} \frac{6.5}{17.2} \frac{7.4}{16.4} \left( \frac{7.3}{11} \right) 7.2 \left( \frac{7.5}{11} \right) \frac{7.7}{24.6} \frac{6.1}{26.1} \frac{6.3}{30} \frac{6.4}{40} \left| \frac{2.2}{2.2} \right| \frac{7.8}{26.1.4}$$

Top of Stake nailed to power pole 25 ft Rt of 44+90 Pole # 25

$$\frac{1.4}{C.1.1} \left| \frac{2.4}{2.4} \right.$$

$$\frac{0.7}{40} \frac{1.4}{30} \frac{1.9}{17} \frac{2.8}{16.2} \left( \frac{2.8}{11} \right) 2.5 \left( \frac{2.8}{11} \right) \frac{3.1}{25} \frac{1.9}{26} \frac{2.2}{30} \frac{2.5}{40} \left| \frac{2.2}{2.2} \right| \frac{3.0}{26.1.5}$$

$$\frac{2.6}{C.0.6} \left| \frac{2.6}{2.6} \right.$$

$$\frac{2.2}{40} \frac{2.4}{30} \frac{3.0}{17.2} \frac{3.7}{16.6} \left( \frac{3.5}{11} \right) 3.2 \left( \frac{3.6}{11} \right) \frac{4.0}{22} \frac{3.1}{22.4} \frac{3.0}{30} \frac{3.1}{40} \left| \frac{2.2}{2.2} \right| \frac{3.0}{26.2.2}$$

$$\frac{3.8}{D.C.2.2} \left| \frac{2.3}{2.3} \right.$$

$$\frac{3.4}{40} \frac{3.6}{30} \frac{3.9}{17.2} \frac{4.7}{16.6} \left( \frac{4.4}{11} \right) 4.0 \left( \frac{4.3}{11} \right) \frac{4.7}{20.2} \frac{4.1}{20.6} \frac{3.7}{30} \frac{3.6}{40} \left| \frac{2.3}{2.3} \right| \frac{4.0}{26.2.0}$$

$$\frac{4.6}{D.C.1.9} \left| \frac{2.2}{2.2} \right.$$

$$\frac{4.5}{40} \frac{4.6}{30} \frac{4.6}{17.2} \frac{5.0}{16} \left( \frac{4.8}{11} \right) 4.5 \left( \frac{4.7}{11} \right) \frac{5.1}{19} \frac{4.5}{19.4} \frac{4.5}{30} \frac{4.5}{40} \left| \frac{2.2}{2.2} \right| \frac{4.5}{26.2.0}$$

$$\frac{5.4}{D.C.1.5} \left| \frac{2.2}{2.2} \right.$$

$$\frac{5.6}{40} \frac{5.6}{30} \frac{5.2}{16} \frac{5.2}{11} 4.9 \frac{5.0}{11} \frac{4.9}{18} \frac{5.1}{30} \frac{5.0}{40} \left| \frac{2.1}{2.1} \right| \frac{5.0}{26.1.9}$$

$$\frac{6.5}{D.C.0.8} \left| \frac{2.1}{2.1} \right.$$

$$\frac{6.8}{40} \frac{6.8}{30} \frac{5.8}{15} \left( \frac{5.7}{11} \right) 5.3 \frac{5.4}{11} \frac{5.8}{19} \frac{6.2}{30} \frac{6.0}{40} \left| \frac{2.2}{2.2} \right| \frac{6.0}{26.1.3}$$

Top of Stake nailed to power pole # 24 25 ft Rt of 49+00

|       |   |      |        |        |
|-------|---|------|--------|--------|
| Sta.  | + | H.I. | -      | Elev.  |
| B.M.  |   | 2.76 | 601.17 | 598.41 |
| 48+00 |   |      |        |        |

+50

49+00

+50

50+00

+50

51+00

+50

52+00

+50

|       |      |        |      |        |
|-------|------|--------|------|--------|
| T.P.  | 9.63 | 605.63 | 5.17 | 596.00 |
| 53+00 |      |        |      |        |

+50

54+00

Lst.

RT. Clear Cold Windy  
12/6/33

R

Top stake nailed to RP #124 Rt Sta 49400

$$\frac{4.6}{40} \quad 21.7/\frac{4.4}{AC.0.9} \quad \frac{4.7}{16} \quad \frac{3.2}{13} \quad 31 \quad \frac{3.1}{12} \quad \frac{3.6}{16.5} \quad \frac{3.9}{AC.1.3} \quad \frac{3.3}{2.5} \quad \frac{3.6}{40}$$

$$\frac{4.6}{40} \quad 21.8/\frac{4.8}{AC.0.9} \quad \frac{5.1}{15} \quad \frac{3.9}{12} \quad 31 \quad \frac{3.9}{11} \quad \frac{4.5}{15} \quad \frac{4.5}{AC.1.2} \quad \frac{4.2}{2.2} \quad \frac{4.3}{40}$$

$$\frac{4.8}{40} \quad 22.0/\frac{5.0}{AC.1.0} \quad \frac{5.0}{21} \quad \frac{5.4}{15} \quad \frac{4.1}{12} \quad 40 \quad \frac{4.4}{11} \quad \frac{4.8}{14} \quad \frac{4.8}{AC.1.2} \quad \frac{4.2}{2.2} \quad \frac{4.6}{40}$$

$$\frac{4.6}{40} \quad 22.3/\frac{4.9}{AC.1.3} \quad \frac{4.9}{19} \quad \frac{5.4}{15} \quad \frac{4.4}{11} \quad 42 \quad \frac{4.6}{11} \quad \frac{5.1}{16} \quad \frac{4.7}{AC.1.5} \quad \frac{4.2}{2.2} \quad \frac{4.6}{40}$$

$$\frac{4.5}{40} \quad 22.4/\frac{5.0}{AC.1.4} \quad \frac{5.0}{22} \quad \frac{5.6}{15} \quad \frac{4.4}{12} \quad 44 \quad \frac{4.6}{10} \quad \frac{5.3}{14} \quad \frac{4.9}{18} \quad \frac{4.6}{AC.1.8} \quad \frac{4.8}{2.8} \quad \frac{4.7}{40}$$

$$\frac{5.3}{40} \quad 22.5/\frac{5.1}{AC.1.5} \quad \frac{5.1}{20} \quad \frac{5.5}{14} \quad \frac{4.6}{11} \quad 44 \quad \frac{4.7}{10} \quad \frac{5.4}{14} \quad \frac{4.8}{18} \quad \frac{4.4}{AC.2.0} \quad \frac{4.4}{2.3} \quad \frac{4.5}{40}$$

$$\frac{4.7}{40} \quad 22.6/\frac{4.4}{AC.1.6} \quad \frac{5.3}{19} \quad \frac{5.6}{15} \quad \frac{5.0}{12} \quad 46 \quad \frac{4.7}{9} \quad \frac{5.6}{13} \quad \frac{4.4}{18} \quad \frac{4.0}{C.0.6} \quad \frac{4.0}{2.6} \quad \frac{4.3}{40}$$

$$\frac{5.5}{40} \quad 22.7/\frac{5.4}{AC.1.7} \quad \frac{5.9}{19} \quad \frac{6.1}{14} \quad \frac{5.1}{11} \quad 48 \quad \frac{5.2}{10} \quad \frac{5.8}{15} \quad \frac{5.0}{19} \quad \frac{4.8}{AC.2.0} \quad \frac{4.8}{2.0} \quad \frac{4.9}{40}$$

$$\frac{6.6}{40} \quad 21.3/\frac{6.7}{AC.0.3} \quad \frac{6.9}{19} \quad \frac{5.3}{15} \quad \frac{5.2}{12} \quad 5.0 \quad \frac{5.3}{10} \quad \frac{6.4}{16} \quad \frac{6.4}{AC.0.6} \quad \frac{21.6}{21.6} \quad \frac{6.5}{40}$$

$$\frac{7.6}{40} \quad 20.7/\frac{7.6}{F.2.6} \quad \frac{7.6}{20} \quad \frac{5.2}{15} \quad \frac{5.2}{12} \quad 5.0 \quad \frac{5.2}{10} \quad \frac{6.8}{16} \quad \frac{7.1}{F.2.1} \quad \frac{7.1}{19.2} \quad \frac{7.4}{40}$$

$$\frac{12.4}{40} \quad 20.4/\frac{12.4}{F.2.7} \quad \frac{9.9}{15} \quad \frac{9.8}{12} \quad 9.7 \quad \frac{10.0}{11} \quad \frac{12.0}{18} \quad \frac{12.0}{F.2.3} \quad \frac{19.6}{19.6} \quad \frac{11.9}{40}$$

$$\frac{12.4}{40} \quad 20.4/\frac{12.4}{F.2.7} \quad \frac{12.4}{19} \quad \frac{9.8}{14} \quad \frac{9.6}{11} \quad 9.7 \quad \frac{10.0}{11} \quad \frac{9.9}{15} \quad \frac{11.7}{F.2.0} \quad \frac{19.0}{19.0} \quad \frac{11.6}{40}$$

$$\frac{12.6}{40} \quad 19.8/\frac{12.1}{F.2.4} \quad \frac{12.1}{19} \quad \frac{9.9}{12} \quad \frac{9.9}{12} \quad 9.7 \quad \frac{9.9}{13} \quad \frac{9.7}{16} \quad \frac{11.0}{21} \quad \frac{11.0}{AC.0.9} \quad \frac{11.1}{11.1} \quad \frac{11.1}{40}$$

Sta + H.I. - Elev.

605.63

54+50

55+00

+50

+80

56+00

B.M. 887 613.40 1.10 604.53.

+22

+40

+50

+75

57+00

+50

58+00



$$\frac{12.0}{40} \quad 19.7/11.2 \quad \frac{11.1}{19} \quad \frac{9.4}{15} \quad \left(\frac{9.3}{11}\right) \quad 91 \quad \frac{9.4}{14} \quad \frac{9.9}{19} \quad \frac{22}{12.14/22.4} \quad \frac{9.8}{40}$$

$$\frac{10.9}{40} \quad 20.7/10.7 \quad \frac{8.5}{15} \quad \left(\frac{8.3}{10}\right) \quad 81 \quad \left(\frac{8.0}{14}\right) \quad \frac{8.0}{16} \quad \frac{8.8}{20} \quad \frac{8.9}{12.12/20.2} \quad \frac{9.1}{40}$$

$$\frac{9.5}{40} \quad 20.4/9.3 \quad \frac{6.8}{14} \quad \left(\frac{6.9}{15}\right) \quad 6.6 \quad \left(\frac{6.8}{14}\right) \quad \frac{6.8}{18} \quad \frac{8.0}{21} \quad \frac{8.0}{12.06/21.6} \quad \frac{8.1}{40}$$

$$\frac{8.0}{40} \quad \frac{8.2}{20} \quad \frac{6.2}{16} \quad \frac{6.1}{13} \quad 5.7 \quad \left(\frac{5.8}{16}\right) \quad \frac{6.0}{21} \quad \frac{6.9}{25} \quad \frac{6.9}{40}$$

$$\frac{6.8}{40} \quad \frac{7.1}{20} \quad \frac{5.4}{16} \quad \frac{5.4}{11} \quad 4.9 \quad \frac{4.9}{17} \quad \frac{4.6}{23} \quad \frac{4.4}{40}$$

P.R. spike in T.P. SW cor Aston Rd & East Co Line

$$\frac{14.2}{40} \quad \frac{12.3}{18} \quad \frac{12.0}{11} \quad 11.8 \quad \frac{12.1}{13} \quad \frac{12.3}{21} \quad \frac{13.7}{30} \quad \frac{13.0}{40}$$

$$\frac{11.9}{40} \quad \frac{11.6}{19} \quad \frac{11.5}{13} \quad 11.3 \quad \frac{11.5}{11} \quad \left(\frac{12.1}{19}\right) \quad \frac{12.5}{23} \quad \frac{11.2}{27} \quad \frac{10.8}{40}$$

$$\frac{12.0}{40} \quad \frac{11.7}{20} \quad \frac{11.4}{12} \quad 11.1 \quad \frac{11.4}{13} \quad \left(\frac{11.7}{19}\right) \quad \frac{12.1}{12.10/20} \quad \frac{10.2}{27} \quad \frac{10.0}{40}$$

$$\frac{11.3}{40} \quad 24.4/10.3 \quad \frac{10.3}{20} \quad \left(\frac{11.6}{16}\right) \quad \frac{11.1}{12} \quad 11.7 \quad \frac{10.9}{13} \quad \left(\frac{11.0}{18}\right) \quad \frac{11.3}{22} \quad \frac{8.4}{13.3/26.3} \quad \frac{8.8}{40}$$

$$\frac{7.5}{40} \quad 25.0/8.0 \quad \frac{8.6}{20} \quad \frac{11.2}{18} \quad \left(\frac{10.8}{16}\right) \quad \frac{10.6}{12} \quad 10.0 \quad \frac{10.3}{15} \quad \left(\frac{10.4}{18}\right) \quad \frac{10.9}{21} \quad \frac{6.6}{26} \quad \frac{6.6}{13.4/26.8} \quad \frac{6.6}{40}$$

$$\frac{6.6}{40} \quad 25.4/6.1 \quad \frac{6.8}{20} \quad \frac{9.5}{17} \quad \frac{9.0}{14} \quad \frac{8.9}{12} \quad 8.5 \quad \frac{8.6}{13} \quad \left(\frac{8.7}{18}\right) \quad \frac{9.1}{21} \quad \frac{3.9}{12.16/27.6} \quad \frac{4.0}{40}$$

$$\frac{5.5}{40} \quad 25.0/5.1 \quad \frac{5.7}{19} \quad \frac{8.1}{19} \quad \left(\frac{7.7}{14}\right) \quad \frac{7.4}{11} \quad 7.1 \quad \frac{7.1}{12} \quad \left(\frac{7.6}{19}\right) \quad \frac{7.8}{21} \quad \frac{3.6}{25.1/28.5} \quad \frac{3.1}{28} \quad \frac{2.8}{40}$$

579 + H.I. - E140.

613.40

58+50

59+00

+50

60+00.

+50

61+00

TP 8.41 621.03 0.78 612.62

+50

62+00

+50

*Back to line*

63+00

BM 7.36 626.47 1.92 619.11

+20

+50

15.0  
6.6  
8.6

Clear Cold Windy  
12/6/93

$$\frac{5.1}{40} \quad 23.9/4.8 \quad \frac{4.9}{20} \quad \frac{6.7}{18} \quad \left(\frac{6.3}{15}\right) \quad \frac{6.0}{12} \quad 5.7 \quad \frac{6.0}{12} \quad \left(\frac{6.2}{18}\right) \quad \frac{6.4}{21} \quad \frac{0.3}{27} \quad \frac{1.0}{27} \quad \frac{0.9}{36} \quad \frac{0.9}{40}$$

$$\frac{6.8}{40} \quad 21.6/5.8 \quad \frac{5.7}{17} \quad \frac{4.6}{14} \quad \left(\frac{4.6}{11}\right) \quad \frac{4.6}{13} \quad \left(\frac{4.8}{18}\right) \quad \frac{5.1}{21} \quad \frac{1.2}{27} \quad \frac{1.2}{27} \quad \frac{0.5}{40}$$

$$\frac{7.6}{40} \quad 21.2/6.4 \quad \frac{6.2}{20} \quad \frac{3.5}{14} \quad \left(\frac{3.4}{11}\right) \quad \frac{3.3}{12} \quad \left(\frac{3.7}{17}\right) \quad \frac{4.2}{22} \quad \frac{4.1}{22} \quad \frac{3.3}{40}$$

$$\frac{6.8}{40} \quad 21.6/5.6 \quad \frac{5.4}{20} \quad \frac{2.5}{14} \quad \left(\frac{2.0}{11}\right) \quad \frac{2.3}{12} \quad \left(\frac{2.4}{15}\right) \quad \frac{3.1}{21} \quad \frac{3.1}{22} \quad \frac{2.5}{24} \quad \frac{1.5}{40}$$

$$\frac{6.7}{40} \quad 23.8/5.6 \quad \frac{5.1}{19} \quad \frac{1.4}{13} \quad \left(\frac{1.6}{10}\right) \quad 1.2 \quad \frac{1.3}{15} \quad \frac{1.5}{18} \quad \frac{2.2}{20} \quad \frac{2.1}{25} \quad \frac{2.6}{40}$$

$$\frac{8.0}{40} \quad 21.1/7.3 \quad \frac{6.9}{21} \quad \frac{0.2}{14} \quad \left(\frac{0.1}{8}\right) \quad 0.0 \quad \left(\frac{0.1}{14}\right) \quad \frac{0.0}{19} \quad \frac{4.6}{22} \quad \frac{4.3}{40}$$

$$\frac{15.2}{40} \quad 32.7/15.0 \quad \frac{14.7}{26} \quad \frac{6.8}{14} \quad \left(\frac{6.6}{9}\right) \quad 6.4 \quad \left(\frac{6.4}{12}\right) \quad \frac{6.4}{20} \quad \frac{9.4}{20} \quad \frac{8.7}{40}$$

$$\frac{11.1}{40} \quad 24.1/9.5 \quad \frac{8.7}{20} \quad \frac{5.4}{15} \quad \left(\frac{5.3}{12}\right) \quad 4.9 \quad \left(\frac{4.8}{11}\right) \quad \frac{4.9}{15} \quad \frac{5.8}{18} \quad \frac{5.8}{20} \quad \frac{5.1}{27} \quad \frac{8.00}{37}$$

$$\frac{5.3}{40} \quad 23.7/2.7 \quad \frac{2.3}{21} \quad \frac{4.8}{18} \quad \frac{4.8}{17} \quad \frac{3.9}{15} \quad \left(\frac{3.8}{11}\right) \quad 3.4 \quad \left(\frac{3.5}{12}\right) \quad \frac{3.5}{15} \quad \frac{4.6}{18} \quad \frac{4.6}{21} \quad \frac{3.8}{20} \quad \frac{3.0}{26} \quad \frac{0.0}{30}$$

$$\frac{5.9}{40} \quad 22.6/2.2 \quad \frac{2.3}{20} \quad \frac{3.4}{19} \quad \frac{3.4}{17} \quad \left(\frac{2.1}{15}\right) \quad \frac{2.7}{12} \quad 2.3 \quad \left(\frac{2.3}{11}\right) \quad \left(\frac{2.3}{15}\right) \quad \frac{3.3}{18} \quad \frac{3.3}{21} \quad \frac{1.8}{20} \quad \frac{1.5}{26}$$

R.R. Spike in TP 15 Lt 540 63+00

$$\frac{12.9}{40} \quad 21.3/9.2 \quad \frac{8.4}{17} \quad \left(\frac{7.8}{14}\right) \quad \frac{7.8}{11} \quad \frac{7.5}{13} \quad \frac{7.4}{15} \quad \left(\frac{8.3}{18}\right) \quad \frac{8.3}{20} \quad \frac{6.0}{26} \quad \frac{2.6}{26} \quad \frac{2.1}{27}$$

$$\frac{16.5}{40} \quad 21.0/13.1 \quad \frac{10.0}{18} \quad \frac{7.6}{14} \quad \frac{7.5}{10} \quad 7.1 \quad \frac{7.1}{12} \quad \frac{7.0}{15} \quad \frac{8.0}{18} \quad \frac{7.9}{20} \quad \frac{6.0}{26} \quad \frac{6.0}{26} \quad \frac{4.1}{29} \quad \frac{2.1}{33} \quad \frac{2.0}{40}$$

Sta + H.I. - E/cu

626.47

64+00

+50

65+00

+50

T.P. 6.38 615.00 5.09 621.38

66+00

+50

67+00

+50

+7.7

68+00

+50

69+00

T.P. 5.08 616.13 3.95 611.05



Cloudy Cold Windy  
12/7/33.

$$\frac{126}{40} \quad 21^0/86 \quad 86 \quad 69 \quad 70 \quad 66 \quad 62/66/73 \quad 75 \quad 58 \quad 8 \quad 52 \quad 48 \quad 50$$

$$\frac{93}{40} \quad 21^0/69 \quad 68 \quad 72 \quad 72 \quad (66/65) \quad 62 \quad 62/64 \quad 78 \quad 75 \quad 65 \quad 12 \quad 758 \quad 57$$

$$\frac{75}{40} \quad 23^0/57 \quad 56 \quad 69 \quad 69 \quad (64/63) \quad 60 \quad 60 \quad 61/70 \quad 71 \quad 54 \quad 236 \quad 58 \quad 16 \quad 16.4$$

$$\frac{31}{40} \quad 25^0/31 \quad 31 \quad 62 \quad (60) \quad 59 \quad 55 \quad 57 \quad (59) \quad 64 \quad 67 \quad 62 \quad 23 \quad 47 \quad 4752$$

$$\frac{91}{40} \quad 29^0/89 \quad 89 \quad 68 \quad (67) \quad 64 \quad 65/67 \quad 76 \quad 72 \quad 115 \quad 118 \quad 12.1$$

$$\frac{110}{40} \quad 23^0/102 \quad 91 \quad 62 \quad (62) \quad 60 \quad (63) \quad 62 \quad 118 \quad 118 \quad 118$$

$$\frac{110}{40} \quad 23^0/93 \quad 92 \quad 74 \quad 58 \quad (60) \quad 56 \quad (59) \quad 57 \quad 102 \quad 102 \quad 29 \quad 114 \quad 110$$

$$\frac{79}{40} \quad 19^0/73 \quad 73 \quad 53 \quad (53) \quad 57 \quad (55) \quad 57 \quad 77 \quad 77 \quad 12 \quad 89 \quad 91 \quad 93$$

$$\frac{56}{40} \quad 21^0/49 \quad 50 \quad 56 \quad 54 \quad (52) \quad 48 \quad (53) \quad 53 \quad 65 \quad 57 \quad 64$$

$$\frac{52}{40} \quad 23^0/40 \quad 44 \quad 53 \quad (49) \quad 49 \quad 46 \quad 51 \quad (52) \quad 59 \quad 17 \quad 29 \quad 26$$

$$\frac{65}{40} \quad 21^0/55 \quad 49 \quad (50) \quad 46 \quad 44 \quad 47/51 \quad 54 \quad 26 \quad 25 \quad 29$$

$$\frac{23}{40} \quad 21^0/44 \quad 24 \quad 49 \quad (48) \quad 46 \quad 40 \quad 43 \quad 45 \quad 47 \quad 23 \quad 06 \quad 18 \quad 13$$

Sta + H.I. - Elev

616.13

69+50

70+00

+50

71+00

+50

72+00

72+00

+50

73+00

B.M. 0.17 608.79 7.51 608.62

+50

74+00

+50

75+00

75+00 1.95

75+00 1.32

75+00 1.32

75+00 1.32

41

42

Cloudy Cold Windy  
12/2/33

$$\frac{10}{40} \quad 26.9 \frac{11}{C3.9} \quad \frac{10}{20} \quad \frac{5.8}{16} \quad \left( \frac{5.8}{12} \right) \quad 50 \quad \frac{5.2}{11} \quad \left( \frac{5.3}{18} \right) \quad \frac{5.7}{22} \quad \frac{0.9}{C4.1/22.1} \quad \frac{11}{40}$$

$$\frac{11}{40} \quad 27.8 \frac{0.4}{C4.8} \quad \frac{0.3}{22} \quad \frac{5.9}{16} \quad \left( \frac{5.9}{12} \right) \quad 52 \quad \frac{5.4}{11} \quad \left( \frac{5.4}{15} \right) \quad \frac{5.6}{22} \quad \frac{0.3}{27} \quad \frac{0.0}{C5.2/27.8} \quad \frac{0.5}{40}$$

$$\frac{3.6}{40} \quad 26.2 \frac{2.3}{C0.2} \quad \frac{1.7}{22} \quad \frac{6.4}{16} \quad \left( \frac{6.1}{12} \right) \quad 5.5 \quad \frac{5.6}{10} \quad \left( \frac{5.8}{17} \right) \quad \frac{6.2}{21} \quad \frac{2.1}{25} \quad \frac{1.6}{C3.9/26.9} \quad \frac{9.21}{30} \quad \frac{2.4}{40}$$

$$\frac{5.3}{40} \quad 24.7 \frac{4.5}{C1.7} \quad \frac{4.2}{24} \quad \frac{7.2}{15} \quad \left( \frac{6.9}{12} \right) \quad 6.2 \quad \left( \frac{6.3}{14} \right) \quad \frac{6.8}{21} \quad \frac{3.6}{25} \quad \frac{3.4}{C2.1/25.8} \quad \frac{3.6}{40}$$

$$\frac{7.0}{40} \quad 24.2 \frac{5.9}{C1.2} \quad \frac{6.5}{17} \quad \frac{8.0}{15} \quad \left( \frac{7.5}{10} \right) \quad 7.1 \quad \frac{7.1}{11} \quad \left( \frac{7.3}{17} \right) \quad \frac{8.0}{21} \quad \frac{5.9}{C1.2/24.2} \quad \frac{4.7}{36} \quad \frac{5.4}{40}$$

$$\frac{8.7}{40} \quad 23.5 \frac{7.2}{C0.5} \quad \frac{7.6}{18} \quad \frac{9.0}{15} \quad \left( \frac{8.6}{11} \right) \quad 8.2 \quad \frac{8.3}{13} \quad \frac{8.8}{20} \quad \frac{5.7}{24} \quad \frac{5.1}{C2.5/23.5} \quad \frac{6.6}{33} \quad \frac{6.9}{40}$$

$$\frac{9.6}{40} \quad 23.9 \frac{8.3}{C0.9} \quad \frac{7.8}{18} \quad \frac{9.8}{15} \quad \left( \frac{9.5}{10} \right) \quad 9.2 \quad \frac{9.4}{12} \quad \frac{9.5}{16} \quad \frac{10.0}{20} \quad \frac{6.9}{24} \quad \frac{6.9}{C2.3/23.9} \quad \frac{8.2}{33} \quad \frac{8.9}{40}$$

$$\frac{11.0}{40} \quad 22.6 \frac{10.5}{C0.6} \quad \frac{10.2}{20} \quad \frac{10.9}{16} \quad \left( \frac{10.7}{12} \right) \quad 10.1 \quad \frac{10.4}{10} \quad \left( \frac{10.7}{17} \right) \quad \frac{11.0}{21} \quad \frac{8.9}{24} \quad \frac{8.8}{C1.3/22.6} \quad \frac{10.2}{40}$$

RRSpiko T.P. 15' Lt 54 72+50

$$\frac{4.7}{40} \quad 22.6 \frac{4.3}{C0.6} \quad \frac{4.4}{18} \quad \frac{4.9}{17} \quad \left( \frac{4.4}{14} \right) \quad \frac{4.3}{11} \quad 3.9 \quad \frac{3.9}{9} \quad \left( \frac{4.2}{17} \right) \quad \frac{4.7}{21} \quad \frac{3.6}{C0.2/22.6} \quad \frac{3.3}{35} \quad \frac{4.1}{40}$$

$$\frac{5.6}{40} \quad 22.8 \frac{5.4}{C0.5} \quad \frac{5.2}{17} \quad \frac{5.8}{16} \quad \left( \frac{5.3}{14} \right) \quad \frac{5.2}{11} \quad 4.9 \quad \frac{5.0}{13} \quad \left( \frac{5.3}{16} \right) \quad \frac{5.6}{20} \quad \frac{5.4}{22} \quad \frac{5.1}{C0.18/22.8} \quad \frac{7.1}{31} \quad \frac{5.6}{40}$$

$$\frac{6.6}{40} \quad 23.2 \frac{5.8}{C0.2} \quad \frac{5.9}{19} \quad \frac{7.0}{17} \quad \frac{7.0}{15} \quad \left( \frac{6.5}{14} \right) \quad \frac{6.4}{10} \quad 6.0 \quad \frac{6.3}{12} \quad \left( \frac{6.5}{16} \right) \quad \frac{7.0}{17} \quad \frac{6.9}{20} \quad \frac{5.9}{22} \quad \frac{5.9}{C0.1/23.2} \quad \frac{5.2}{34} \quad \frac{5.7}{40}$$

$$\frac{7.4}{40} \quad 24.4 \frac{6.0}{C0.4} \quad \frac{5.8}{18} \quad \frac{8.2}{16} \quad \frac{8.2}{14} \quad \left( \frac{7.6}{12} \right) \quad \frac{7.5}{9} \quad 7.4 \quad \frac{7.6}{10} \quad \left( \frac{7.9}{16} \right) \quad \frac{8.4}{17} \quad \frac{8.4}{19} \quad \frac{7.3}{22} \quad \frac{6.9}{C0.5/24.4} \quad \frac{6.5}{25} \quad \frac{6.6}{29} \quad \frac{7.4}{40}$$

Sta + H/L - E/ev

608.79

75+50

76+00

+50

77+00

T.P. 6.06 60200 12.85 595.94

+50

78+00

B.M. 2.47 591.19 13.28 588.72

+50

79+00

B.M. 1.10 589.82 2.47 588.72

+50

+50

80+00

+50

T.P. 0.76 581.67 8.91 580.91

81+00



Lt

 cloudy Cold Windy  
 12/7/33.

$$\frac{8.0}{40} \frac{2.5}{30} \frac{6.7}{22.1} \frac{6.5}{18} \frac{7.7}{15} \frac{7.7}{14} \left( \frac{9.0}{12} \right) \frac{9.0}{10} 8.8 \frac{9.1}{9} \left( \frac{9.2}{10} \right) \frac{9.4}{20} \frac{4.7}{24} \frac{4.0}{0.48} \frac{5.2}{27.8} \frac{5.4}{34} \frac{4.0}{40}$$

$$\frac{7.3}{46} \frac{2.5}{27.5} \frac{2.0}{0.35} \frac{6.2}{22} \frac{11.3}{17} \frac{11.6}{14} \left( \frac{10.6}{13} \right) \frac{10.7}{9} 10.5 \frac{10.8}{11} \left( \frac{11.0}{16} \right) \frac{11.3}{17} \frac{11.6}{20} \frac{5.4}{26} \frac{5.6}{0.92} \frac{9.58}{33} \frac{4.7}{40}$$

$$\frac{6.2}{40} \frac{2.1}{29.1} \frac{6.0}{0.61} \frac{5.5}{26} \frac{13.3}{18} \frac{13.3}{15} \left( \frac{12.5}{13} \right) \frac{12.4}{10} 12.1 \frac{12.4}{10} \left( \frac{12.5}{16} \right) \frac{13.3}{18} \frac{13.5}{23} \frac{4.8}{29} \frac{4.8}{0.73} \frac{2}{80} \frac{4.7}{40}$$

$$\frac{4.8}{50} \frac{3.2}{32} \frac{4.6}{0.93} \frac{4.4}{32} \frac{14.8}{18} \frac{14.7}{15} \frac{14.2}{13} \frac{14.1}{10} 13.9 \frac{14.0}{11} \left( \frac{14.2}{16} \right) \frac{14.9}{23} \frac{5.7}{0.82} \frac{5.8}{31} \frac{5.8}{40}$$

$$\frac{0.0}{40} \frac{3.2}{32} \frac{4.0}{9.5} \frac{4.6}{31} \frac{9.6}{19} \left( \frac{8.6}{14} \right) \frac{9.1}{11} 8.9 \frac{9.1}{10} \left( \frac{9.3}{15} \right) \frac{10.3}{17} \frac{10.3}{20} \frac{9.2}{0.17} \frac{2.7}{29} \frac{9.3}{29} \frac{4.3}{40}$$

$$\frac{7.4}{40} \frac{2.6}{26.3} \frac{7.7}{0.33} \frac{7.6}{25} \frac{11.5}{18} \frac{11.6}{14} \left( \frac{11.1}{13} \right) \frac{11.0}{10} 11.2 \left( \frac{11.3}{15} \right) \frac{12.0}{17} \frac{12.0}{19} \frac{10.6}{21} \frac{10.3}{0.71} \frac{2.7}{32} \frac{10.7}{32} \frac{10.5}{40}$$

R.R. spike in T.P. 16' Lt Sta 78+75

$$\frac{1.8}{40} \frac{2.3}{23.8} \frac{1.4}{0.08} \frac{1.2}{19} \frac{3.3}{18} \frac{3.2}{15} \left( \frac{2.4}{13} \right) \frac{2.2}{10} 2.2 \frac{2.3}{9} \left( \frac{2.5}{15} \right) \frac{3.3}{19} \frac{2.3}{20} \frac{2.0}{0.02} \frac{1.9}{23.2} \frac{1.9}{40}$$

$$\frac{4.4}{40} \frac{2.3}{23.0} \frac{4.2}{0.00} \frac{4.1}{20} \frac{5.6}{19} \frac{5.9}{17} \frac{4.4}{14} \left( \frac{4.2}{11} \right) 4.2 \left( \frac{4.3}{9} \right) \frac{4.5}{11} \frac{6.1}{14} \frac{6.3}{16} \frac{4.2}{19} \frac{4.2}{0.01} \frac{4.2}{23.0} \frac{4.2}{40}$$

R.R. spike in T.P. 16' Lt Sta 78+75 12/8/33

$$\frac{3.0}{40} \frac{2.3}{23.8} \frac{4.1}{0.08} \frac{6.0}{22} \frac{6.0}{19} \frac{5.2}{17} \left( \frac{5.0}{12} \right) 4.9 \left( \frac{5.3}{11} \right) \frac{5.4}{14} \frac{6.5}{17} \frac{6.8}{20} \frac{5.9}{21} \frac{5.9}{0.19} \frac{2.0}{24} \frac{1.9}{40}$$

$$\frac{8.2}{40} \frac{2.0}{20.8} \frac{7.7}{22.9} \frac{7.7}{20} \frac{7.3}{16} \frac{7.1}{11} 6.8 \left( \frac{7.1}{9} \right) \frac{7.2}{14} \frac{9.0}{17} \frac{9.0}{18} \frac{8.2}{20} \frac{8.2}{0.01} \frac{1.1}{21} \frac{11.3}{40}$$

$$\frac{10.1}{40} \frac{11.6}{12.3} \frac{11.0}{21} \frac{11.0}{19} \frac{8.9}{16} \left( \frac{8.8}{12} \right) 8.7 \frac{9.1}{11} \frac{9.2}{15} \frac{10.8}{18} \frac{10.8}{19} \frac{10.2}{20} \frac{10.3}{0.04} \frac{4.4}{31} \frac{13.6}{40}$$

$$\frac{2.5}{40} \frac{2.0}{20.0} \frac{3.4}{0.10} \frac{3.9}{20} \frac{3.7}{18} \frac{2.5}{15} \left( \frac{2.5}{11} \right) 2.4 \frac{2.9}{10} \frac{3.1}{15} \frac{4.2}{18} \frac{4.2}{16} \frac{6.9}{26} \frac{8.5}{40}$$

| Sta | + | H.I. | - | Elev |
|-----|---|------|---|------|
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|--|--|--------|--|--|
|  |  | 581.67 |  |  |
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| 81+50 |  |  |  |  |
|-------|--|--|--|--|

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|-------|--|--|--|--|
| 82+00 |  |  |  |  |
|-------|--|--|--|--|

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|------|--|--|--|--|
| T.P. |  |  |  |  |
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|     |      |        |      |        |
|-----|------|--------|------|--------|
| +50 | 0.70 | 573.17 | 9.20 | 572.47 |
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|-------|--|--|--|--|
| 83+00 |  |  |  |  |
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| 84+00 |  |  |  |  |
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| 85+00 |  |  |  |  |
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| 86+00 |  |  |  |  |
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|------|------|--------|-------|--------|
| T.P. | 2.26 | 563.33 | 12.10 | 561.07 |
|------|------|--------|-------|--------|

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| +50 |  |  |  |  |
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|-------|--|--|--|--|
| 87+00 |  |  |  |  |
|-------|--|--|--|--|

Clear Cold gusty blow  
Windy Nice for Cheeks

12/8/33

$$\frac{2.9}{40} \quad \frac{2.8}{40} \quad \frac{4.6}{18} \quad \frac{4.7}{20} \quad \frac{5.7}{19} \quad \frac{5.6}{17} \quad \frac{4.6}{14} \quad \left(\frac{4.5}{11}\right) \quad \frac{4.4}{12} \quad \frac{5.0}{12} \quad \frac{5.0}{15} \quad \frac{8.0}{22} \quad \frac{8.1}{22} \quad \frac{4}{12} \quad \frac{11.3}{40}$$

$$\frac{5.5}{40} \quad \frac{2.3}{40} \quad \frac{6.2}{20} \quad \frac{6.4}{22} \quad \frac{7.9}{20} \quad \frac{8.0}{16} \quad \frac{6.5}{14} \quad \left(\frac{6.7}{9}\right) \quad \frac{6.5}{10} \quad \frac{7.0}{14} \quad \frac{11.4}{22} \quad \frac{11.1}{22} \quad \frac{4.2}{12} \quad \frac{13.5}{40}$$

$$\frac{0.1}{40} \quad \frac{1.3}{24} \quad \frac{2.1}{20} \quad \frac{2.0}{19} \quad \frac{2.0}{16} \quad \frac{0.2}{13} \quad \left(\frac{0.2}{9}\right) \quad \frac{0.1}{9} \quad \frac{0.3}{9} \quad \frac{0.4}{15} \quad \frac{4.7}{22} \quad \frac{4.8}{22} \quad \frac{4.2}{12} \quad \frac{5.6}{40}$$

$$\frac{3.3}{40} \quad \frac{2.7}{40} \quad \frac{3.3}{20} \quad \frac{3.2}{18} \quad \frac{3.6}{17} \quad \frac{3.6}{15} \quad \frac{2.1}{13} \quad \left(\frac{2.0}{9}\right) \quad \frac{2.0}{11} \quad \frac{2.2}{16} \quad \frac{6.8}{24} \quad \frac{6.7}{24} \quad \frac{4.4}{12} \quad \frac{6.9}{40}$$

$$\frac{5.8}{40} \quad \frac{4.4}{40} \quad \frac{4.3}{20} \quad \frac{4.6}{18} \quad \frac{4.7}{16} \quad \frac{5.6}{12} \quad \left(\frac{5.6}{9}\right) \quad \frac{3.8}{12} \quad \frac{4.0}{12} \quad \frac{4.1}{15} \quad \frac{7.4}{22} \quad \frac{7.4}{22} \quad \frac{4.2}{12} \quad \frac{7.7}{40}$$

$$\frac{3.8}{40} \quad \frac{2.4}{40} \quad \frac{4.8}{20} \quad \frac{5.2}{17} \quad \frac{6.5}{16} \quad \frac{6.5}{14} \quad \frac{5.1}{12} \quad \left(\frac{5.2}{9}\right) \quad \frac{5.2}{12} \quad \left(\frac{5.5}{12}\right) \quad \frac{5.4}{15} \quad \frac{8.4}{32} \quad \frac{4.8}{30} \quad \frac{8.5}{40}$$

$$\frac{4.2}{40} \quad \frac{2.4}{40} \quad \frac{5.2}{20} \quad \frac{5.4}{20} \quad \frac{6.6}{19} \quad \left(\frac{6.1}{14}\right) \quad \frac{6.4}{13} \quad \frac{7.2}{13} \quad \frac{10.4}{17} \quad \frac{8.0}{20} \quad \frac{8.0}{20} \quad \frac{4.4}{21} \quad \frac{8.3}{40}$$

$$\frac{5.5}{40} \quad \frac{2.4}{40} \quad \frac{6.8}{20} \quad \frac{7.6}{19} \quad \frac{8.8}{17} \quad \frac{8.8}{14} \quad \frac{8.0}{12} \quad \left(\frac{8.0}{9}\right) \quad \frac{8.0}{12} \quad \frac{8.1}{8} \quad \frac{8.2}{12} \quad \frac{8.3}{20} \quad \frac{8.2}{40} \quad \rightarrow$$

$$\frac{9.2}{40} \quad \frac{10.0}{30} \quad \frac{9.2}{21} \quad \frac{11.8}{16} \quad \frac{11.1}{16} \quad \frac{7.6}{13} \quad \frac{7.7}{11} \quad \frac{9.7}{11} \quad \frac{10.0}{9} \quad \frac{10.1}{11} \quad \frac{12.1}{16} \quad \frac{12.0}{20} \quad \frac{11.3}{20} \quad \frac{11.4}{21} \quad \frac{10.4}{40}$$

$$\frac{11.9}{40} \quad \frac{12.9}{25} \quad \frac{11.4}{25} \quad \frac{13.3}{22} \quad \frac{13.4}{20} \quad \frac{11.0}{13} \quad \left(\frac{11.0}{9}\right) \quad \frac{11.1}{11} \quad \frac{11.3}{15} \quad \frac{11.2}{19} \quad \frac{10.8}{29} \quad \frac{9.5}{40} \quad \rightarrow$$

$$\frac{3.6}{40} \quad \frac{4.0}{24} \quad \frac{2.0}{20} \quad \frac{4.8}{22} \quad \frac{4.8}{17} \quad \frac{2.3}{13} \quad \left(\frac{2.4}{10}\right) \quad \frac{2.3}{13} \quad \left(\frac{2.8}{9}\right) \quad \frac{3.1}{14} \quad \frac{4.9}{18} \quad \frac{4.9}{18} \quad \frac{4.9}{24} \quad \frac{0.7}{32} \quad \frac{0.7}{40}$$

$$\frac{3.7}{40} \quad \frac{4.8}{25} \quad \frac{2.0}{20} \quad \frac{6.4}{22} \quad \frac{6.3}{21} \quad \frac{6.5}{19} \quad \frac{4.0}{14} \quad \left(\frac{4.0}{10}\right) \quad \frac{3.7}{9} \quad \frac{4.0}{12} \quad \frac{7.1}{18} \quad \frac{6.8}{18} \quad \frac{4.6}{25} \quad \frac{6.8}{32} \quad \frac{16}{38} \quad \frac{10}{38} \quad \frac{0.7}{40}$$

Sta + H.I. - Elev

563.33

87+50

88+00

T.P. 4.06 556.67 10.72 552.61

+50

89+00

+50

90+00

+50

T.P. 1.20 546.23 11.64 545.03

91+00

+50

92+00

+50

93+00



12/8/33.

$$\frac{46}{40} \frac{23^0}{C90} \frac{55}{20} \frac{78}{19} \frac{81}{14} \frac{55}{10} \frac{56}{55} \frac{58}{8} \frac{60}{11} \frac{90}{16} \frac{86}{F31} / 21 \frac{83}{24} \frac{53}{29} \frac{47}{40}$$

$$\frac{60}{40} \frac{66}{26} \frac{19^0}{F21} \frac{90}{20} \frac{70}{15} \frac{71}{11} \frac{69}{7} \frac{73}{11} \frac{74}{22} \frac{113}{24} \frac{110}{24} / 32 \frac{92}{28} \frac{92}{40}$$

$$\frac{0.4}{40} \frac{0.8}{26} \frac{22^0}{C01} \frac{20}{21} \frac{29}{18} \frac{29}{15} \frac{25}{10} \frac{23}{21} \frac{26}{8} \frac{26}{11} \frac{61}{18} \frac{62}{F42} / 34 \frac{53}{28} \frac{53}{40}$$

$$\frac{0.8}{40} \frac{1.8}{28} \frac{19^0}{F24} \frac{63}{19} \frac{42}{13} \frac{41}{10} \frac{39}{8} \frac{43}{11} \frac{44}{20} \frac{81}{20} \frac{75}{13.6} / 22 \frac{75}{25} \frac{80}{40}$$

$$\frac{07}{40} \frac{2.7}{30} \frac{76}{22} \frac{19^0}{F21} \frac{77}{16} \frac{63}{16} \frac{58}{13} \frac{57}{10} \frac{56}{57} \frac{59}{8} \frac{60}{11} \frac{65}{14} \frac{87}{17} \frac{86}{19} \frac{86}{F3.0} / 21 \frac{95}{40}$$

$$\frac{44}{40} \frac{51}{29} \frac{26^0}{F21} \frac{76}{17} \frac{83}{13} \frac{77}{9} \frac{76}{75} \frac{78}{8} \frac{79}{12} \frac{102}{20} \frac{112}{F3.7} / 21 \frac{86}{26} \frac{78}{40}$$

$$\frac{95}{40} \frac{102}{26} \frac{21^0}{D001} \frac{114}{21} \frac{114}{16} \frac{102}{10} \frac{98}{95} \frac{100}{9} \frac{102}{13} \frac{102}{15} \frac{130}{17} \frac{110}{D004} / 21 \frac{119}{40}$$

$$\frac{39}{40} \frac{30}{26} \frac{21^0}{D002} \frac{27}{20} \frac{13}{13} \frac{12}{11} \frac{09}{8} \frac{10}{11} \frac{11}{17} \frac{48}{22} \frac{16}{22} \frac{16}{D013} / 22 \frac{24}{40}$$

$$\frac{60}{40} \frac{61}{26} \frac{21^0}{F3.0} \frac{56}{20} \frac{56}{13} \frac{30}{10} \frac{39}{26} \frac{29}{9} \frac{30}{11} \frac{52}{20} \frac{50}{F24} / 19 \frac{40}{29} \frac{44}{40}$$

$$\frac{69}{40} \frac{74}{26} \frac{21^0}{F30} \frac{74}{16} \frac{67}{11} \frac{47}{44} \frac{46}{8} \frac{47}{11} \frac{55}{15} \frac{56}{D008} / 18 \frac{60}{40}$$

$$\frac{48}{40} \frac{57}{26} \frac{21^0}{D005} \frac{76}{18} \frac{80}{12} \frac{62}{10} \frac{62}{61} \frac{64}{9} \frac{64}{11} \frac{81}{16} \frac{72}{20} \frac{76}{D005} / 21 \frac{90}{40}$$

$$\frac{6.6}{40} \frac{23^0}{C03} \frac{76}{22} \frac{74}{17} \frac{97}{12} \frac{83}{10} \frac{82}{79} \frac{82}{7} \frac{82}{10} \frac{94}{17} \frac{95}{D004} / 21 \frac{112}{40}$$

D000  
210

| Sta | + | H.I.   | - | Elev |
|-----|---|--------|---|------|
|     |   | 546.23 |   |      |

93+50

|    |     |       |      |       |
|----|-----|-------|------|-------|
| TP | 355 | 53813 | 1165 | 53458 |
|----|-----|-------|------|-------|

94+00

+50

95+00

+50

96+00

+50

B.M.

0.12 538.01

C.W. Soukup  
C. Brettschnitter (N)  
E. Esboldt (State)  
H. Dally (Chairman)  
M. Gross (R.d.)

12/8/33.

$$\frac{9.7}{40} \quad 2\frac{2}{3} \left/ \frac{9.9}{F3.6} \right. \quad \frac{11.8}{18} \quad \frac{9.6}{11} \quad 9.5 \left( \frac{9.9}{8} \right) \quad \frac{10.0}{14} \quad \frac{13.0}{20} \quad \frac{13.2}{F3.7} \left/ 2\frac{1}{2} \right. \quad \frac{13.7}{40}$$

$$\frac{6.3}{40} \quad 2\frac{2}{3} \left/ \frac{6.5}{F3.6} \right. \quad \frac{5.7}{20} \quad \left( \frac{13.4}{12} \right) \quad 2.9 \left/ \frac{3.1}{7} \right. \left/ \frac{3.3}{13} \right. \quad \frac{2.4}{20} \quad \frac{2.6}{F4.7} \left/ 2\frac{1}{2} \right. \quad \frac{2.5}{40}$$

$$\frac{8.1}{40} \quad \left( 2\frac{2}{3} \left/ \frac{8.0}{F4.0} \right. \right) \quad \frac{4.7}{20} \quad \frac{4.7}{14} \quad \frac{4.4}{10} \left( \frac{4.5}{10} \right) \quad \frac{4.2}{19} \quad \left( \frac{9.0}{27.0} \right) \quad \frac{8.8}{40}$$

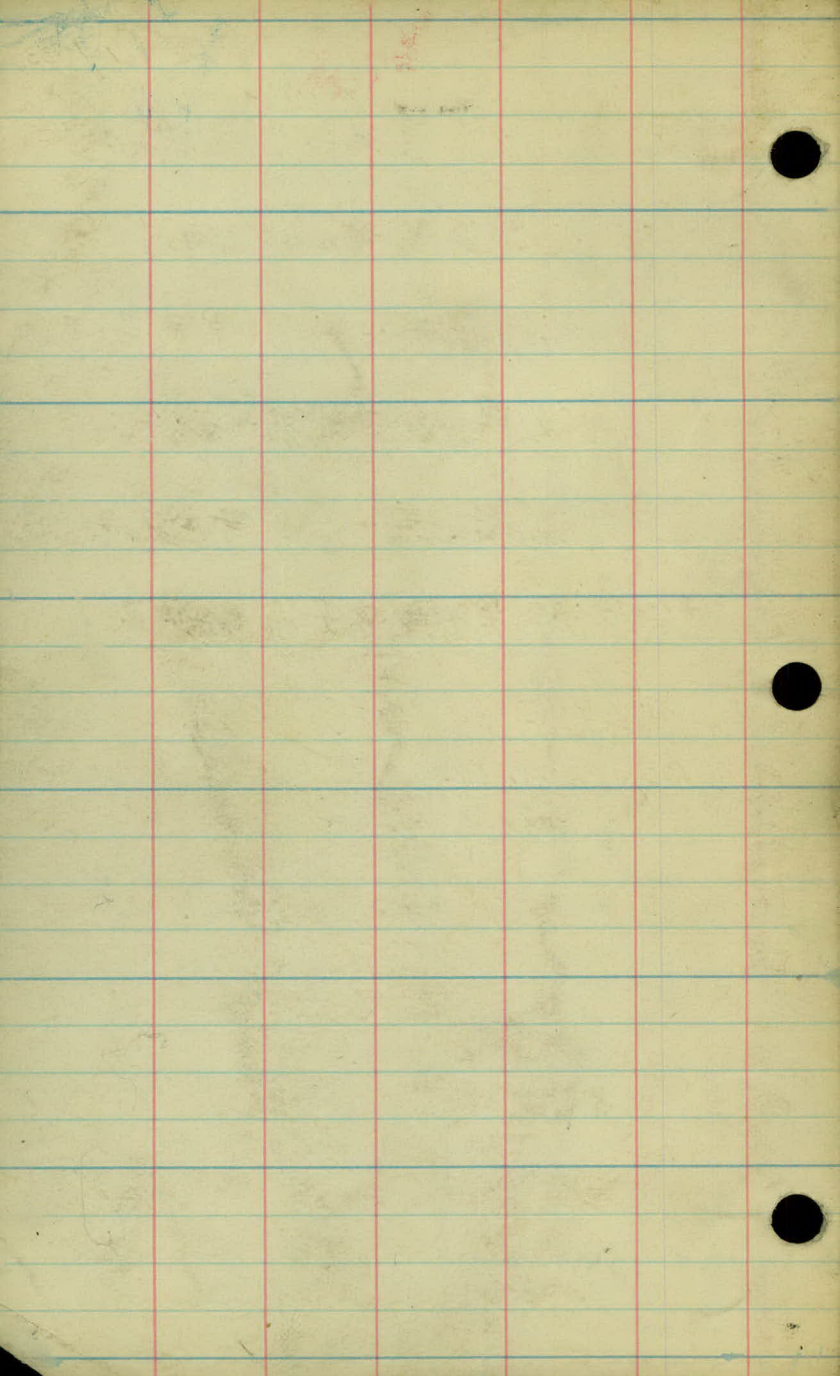
$$\frac{2.6}{40} \quad \left( 2\frac{2}{3} \left/ \frac{2.4}{F4.1} \right. \right) \quad \frac{5.7}{20} \quad \left( \frac{5.6}{10} \right) \quad 5.3 \left( \frac{5.3}{10} \right) \left/ \frac{5.1}{19} \right. \quad \left( \frac{8.8}{13.5} \right) \left/ 2\frac{1}{2} \right. \quad \frac{2.7}{40}$$

$$\frac{10.0}{40} \quad \left( 2\frac{2}{3} \left/ \frac{9.5}{F3.7} \right. \right) \quad \frac{6.1}{21} \quad \left( \frac{6.0}{12} \right) \quad 5.6 \quad \frac{5.8}{10} \quad \frac{5.1}{19} \quad \left( \frac{8.4}{F2.8} \right) \left/ 2\frac{1}{2} \right. \quad \frac{7.8}{40}$$

$$\frac{10.5}{40} \quad 2\frac{2}{3} \left/ \frac{10.1}{F4.7} \right. \quad \frac{5.6}{18} \quad \left( \frac{5.7}{12} \right) \quad 5.4 \quad \frac{5.7}{10} \quad \frac{5.4}{20} \quad \left( \frac{9.1}{F3.7} \right) \left/ 2\frac{1}{2} \right. \quad \frac{8.8}{40}$$

$$\frac{11.0}{40} \quad 2\frac{2}{3} \left/ \frac{11.0}{F6.3} \right. \quad \frac{11.4}{25} \quad \frac{4.9}{18} \quad \left( \frac{5.0}{12} \right) \quad 4.7 \quad \left( \frac{5.0}{10} \right) \quad \frac{4.7}{18} \quad \left( \frac{9.5}{F4.8} \right) \left/ 2\frac{1}{2} \right. \quad \frac{9.5}{40}$$

R.R. spike in T.P. 15 Lt 2t 97+98





{ Murphy  
Topley  
Graham  
Pratt  
White

CROSS SECTIONS AND  
SLOPE STAKES, ON  
EAST CO. LINE ROAD

Sta. 97+00 to -

131+89.6

128+00.91 POT on Hill

105+50.2 Monument  $\Delta = 0^{\circ}23'$

North ↑

←  $\Delta = 0^{\circ}23'$  left

NORTH AFTON ROAD

EAST CO LINE ROAD

Party

12-18-33

## X-SECTIONS AND SLOPE

Murphy STAKES ON EAST C LINE RD

Topley

Graham

Pratt

White

Sta +  $\pi$  - Elev.

BM 2.16 540.17 538.01

97+00

+50

98+00

T.P. 11.63 550.99 0.81 539.36



RR spike in T.P. 15' L of Sta 97+98

$$\begin{array}{cccccccc} F.7.7 & 13.0 & 5.6 & 5.3 & 5.4 & 9.9 & F4.6 & 9.9 \\ \hline 38.1 & 30 & 19 & & 17 & 25.6 & 28.8 & 40 \end{array}$$

$$\begin{array}{cccccccc} 10.2 & F6.0 & 9.8 & 4.0 & 3.8 & 4.2 & F3.5 & 7.3 \\ \hline 40 & 33.2 & 27.5 & 19 & & 14 & 25.5 & 40 \end{array}$$

$$\begin{array}{cccccccc} 8.8 & F6.0 & 8.2 & 2.4 & 2.2 & 2.0 & F2.4 & 3.9 \\ \hline 40 & 33.2 & 27 & 19 & & 18 & 22.2 & 40 \end{array}$$

Sta +  $\pi$  - Elev

550.99

98+50

99+00

T.P. 797 556.95 2.01 548.98

+50

100+00

+50

101+00

$$\frac{-6.0}{40} \quad F. \frac{4.8}{29.4} \quad \frac{10.8}{20} \quad 10.8 \quad \frac{11.0}{19} \quad \frac{9.4}{24} \quad \frac{7.1}{27} \quad C \frac{3.7}{31.4} \quad \frac{7.0}{40}$$

$$\frac{9.0}{40} \quad C \frac{1.7}{27.4} \quad \frac{7.0}{22} \quad \frac{8.7}{17} \quad \frac{8.7}{0} \quad \frac{8.8}{12} \quad \frac{9.1}{26} \quad \frac{0.7}{35} \quad C \frac{8.0}{40.0}$$

$$\frac{9.1}{40} \quad C \frac{4.0}{32.0} \quad \frac{8.1}{21} \quad \frac{13.4}{17} \quad \frac{12.7}{0} \quad \frac{12.9}{15} \quad \frac{12.3}{22} \quad \frac{8.7}{29} \quad \frac{3.9}{32} \quad C \frac{8.8}{41.6}$$

$$\frac{5.0}{40} \quad C \frac{6.3}{36.6} \quad \frac{4.6}{27} \quad \frac{11.4}{20} \quad 10.9 \quad \frac{11.0}{21} \quad \frac{7.3}{28} \quad \frac{1.5}{33} \quad C \frac{9.4}{42.8}$$

$$\frac{2.8}{40} \quad C \frac{6.5}{37.0} \quad \frac{2.1}{28} \quad \frac{10.6}{20} \quad \frac{9.9}{12} \quad 9.5 \quad \frac{9.6}{14} \quad \frac{10.3}{19} \quad \frac{5.7}{26} \quad \frac{2.1}{30} \quad C \frac{7.4}{38.8}$$

$$\frac{3.8}{40} \quad C \frac{4.4}{32.8} \quad \frac{3.2}{25} \quad \frac{8.7}{17} \quad 8.2 \quad \frac{8.3}{12} \quad \frac{9.1}{19} \quad \frac{3.0}{25} \quad C \frac{5.2}{34.4} \quad \frac{3.4}{40}$$

Sta      +       $\pi$       -      Elev.

556.95

101+50

102+00

T.P. Set

5.02      551.93

(12-19-33)

390 <sup>✓</sup> 555.83

551.93

102+50

103+00

103+50



$$\begin{array}{ccccccccccc} 4.3 & C2.7 & 4.3 & 7.8 & & 7.1 & 8.0 & 4.6 & C2.4 & 4.6 \\ \hline 40 & 29.4 & 23 & 20 & 7.0 & 12 & 20 & 25 & 28.8 & 40 \end{array}$$

$$\begin{array}{ccccccccccc} 4.3 & C2.8 & 7.8 & 7.1 & 7.1 & 7.3 & 8.2 & 5.7 & C.14 & 5.1 \\ \hline 40 & 29.6 & 20 & 13 & 7.1 & 12 & 19 & 22 & 26.8 & 40 \end{array}$$

Top of stake  
Right of 102+00

$$\begin{array}{ccccccccccccccc} 5.8 & C1.2 & 4.8 & 7.9 & 6.9 & 6.6 & 6.8 & 7.5 & 4.8 & C1.8 & 4.7 \\ \hline 40 & 26.4 & 22 & 20 & 14 & 6.6 & 11 & 18 & 21 & 27.6 & 40 \end{array}$$

$$\begin{array}{ccccccccccccccc} 1.0 & C1.6 & 5.9 & 9.0 & 8.0 & 7.6 & 7.5 & 8.7 & 4.5 & C3.1 & 4.7 \\ \hline 40 & 27.2 & 22 & 20 & 12 & 7.6 & 13 & 20 & 24 & 30.2 & 40 \end{array}$$

$$\begin{array}{ccccccccccccccc} 7.6 & C2.2 & 6.1 & 10.2 & 9.3 & 9.0 & 9.4 & 10.2 & 5.0 & C4.0 & 4.8 \\ \hline 40 & 28.4 & 23 & 21 & 11 & 9.0 & 13 & 21 & 25 & 32.0 & 40 \end{array}$$

| + | $\pi$ | - | Elev |
|---|-------|---|------|
|---|-------|---|------|

|  |        |  |  |
|--|--------|--|--|
|  | 555.83 |  |  |
|--|--------|--|--|

|        |  |  |  |
|--------|--|--|--|
| 104+00 |  |  |  |
|--------|--|--|--|

|        |  |  |  |
|--------|--|--|--|
| 104+50 |  |  |  |
|--------|--|--|--|

|    |      |        |       |        |
|----|------|--------|-------|--------|
| TP | 3.99 | 547.92 | 11.90 | 543.93 |
|----|------|--------|-------|--------|

|        |  |  |  |
|--------|--|--|--|
| 105+00 |  |  |  |
|--------|--|--|--|

|          |   |            |       |
|----------|---|------------|-------|
| 105+50.2 | E | N. A. 15.4 | Road- |
|----------|---|------------|-------|

|        |  |  |  |
|--------|--|--|--|
| 105+75 |  |  |  |
|--------|--|--|--|

|        |  |  |  |
|--------|--|--|--|
| 106+00 |  |  |  |
|--------|--|--|--|

$$\frac{8.7}{40} \quad C \frac{2.8}{29.6} \quad \frac{7.2}{23} \quad \frac{11.7}{20} \quad 10.7 \quad \frac{11.5}{20} \quad \frac{7.6}{26} \quad C \frac{3.1}{30.2} \quad \frac{6.7}{40}$$

$$\frac{10.9}{40} \quad C \frac{1.9}{27.8} \quad \frac{10.1}{23} \quad \frac{13.7}{21} \quad \frac{12.6}{12} \quad 12.3 \quad \frac{13.1}{21} \quad \frac{10.7}{22} \quad C \frac{2.0}{28.0} \quad \frac{10.5}{40}$$

$$\frac{4.8}{40} \quad \frac{0.0}{24} \quad \frac{4.4}{28} \quad \frac{6.4}{22} \quad \frac{5.4}{12} \quad 4.5 \quad \frac{4.9}{16} \quad \frac{5.5}{23} \quad \frac{3.3}{25} \quad \frac{3.3}{30} \quad \frac{4.4}{40} \quad C \frac{1.4}{26}$$

$$\frac{8.1}{40} \quad \frac{8.0}{31} \quad \frac{6.5}{29} \quad \frac{9.8}{27} \quad \frac{9.7}{25} \quad \frac{8.4}{24} \quad 7.8 \quad \frac{8.2}{13} \quad \frac{8.6}{18} \quad \frac{9.6}{20} \quad \frac{9.7}{22} \quad \frac{7.5}{24} \quad \frac{8.3}{30} \quad \frac{8.5}{40}$$

$$\frac{9.4}{31} \quad \frac{8.5}{24} \quad \frac{9.7}{22} \quad \frac{9.4}{19} \quad \frac{8.7}{16} \quad \frac{8.5}{14} \quad 8.1 \quad \frac{8.3}{9} \quad \frac{8.9}{17} \quad \frac{9.6}{20} \quad \frac{7.9}{22} \quad \frac{8.0}{26} \quad C \frac{0.0}{24.0} \quad \frac{8.0}{40}$$

$$F \frac{0.6}{16.8}$$

$$\frac{9.3}{40}$$

$$C \frac{0.0}{24.0} \quad \frac{8.0}{40}$$

+  $\pi$  - Elex  
547.92

106+50

107+00 X

T.P. 0.69 536.96 11.65 536.27

107+50

T.P. 1.10 536.69 1.37 35.59 ✓

108+00

108+50

109



$$\begin{array}{cccccccccccccccc}
 \frac{107}{40} & \frac{107}{34} & \frac{107}{23} & \frac{114}{22} & \frac{109}{19} & \frac{105}{18} & \frac{102}{16} & 9.6 & \frac{99}{9} & \frac{10.2}{17} & \frac{10.8}{16} & \frac{10.9}{18} & \frac{9.5}{40} & \frac{9.2}{20} & \frac{8.7}{23}
 \end{array}$$

$DC \frac{0.6}{22}$

$$\begin{array}{cccccccccccccccc}
 \frac{121}{40} & \frac{119}{22} & \frac{131}{21} & \frac{129}{19} & \frac{114}{17} & 11.0 & \frac{11.0}{9} & \frac{11.7}{15} & \frac{12.2}{17} & \frac{12.4}{19} & \frac{10.6}{21} & \frac{10.2}{20}
 \end{array}$$

$DC \frac{0.5}{22.0}$

$$\begin{array}{cccccccccccccccc}
 \frac{29}{35} & \frac{28}{28} & \frac{23}{27} & \frac{18}{22} & \frac{32}{21} & \frac{30}{19} & \frac{17}{13} & 1.4 & \frac{1.5}{10} & \frac{2.2}{15} & \frac{2.8}{17} & \frac{3.0}{20} & \frac{0.1}{22} & \frac{0.2}{25}
 \end{array}$$

$DC \frac{0.0}{21.0}$

$$\begin{array}{cccccccccccccccc}
 \frac{0.0}{24} & \frac{3.6}{40} & \frac{2.7}{22} & \frac{4.2}{21} & \frac{4.1}{19} & \frac{3.3}{16} & 2.7 & \frac{2.9}{10} & \frac{3.5}{15} & \frac{4.0}{18} & \frac{2.6}{20} & \frac{2.9}{21} & \frac{2.9}{40}
 \end{array}$$

$DC \frac{1.5}{24.0}$

$$\begin{array}{cccccccccccccccc}
 \frac{5.4}{40} & \frac{4.9}{24} & \frac{5.8}{21} & \frac{5.7}{19} & \frac{4.7}{15} & 4.2 & \frac{4.2}{11} & \frac{5.2}{20} & \frac{4.0}{22} & \frac{4.3}{26} & \frac{4.0}{40} & \frac{0.0}{24}
 \end{array}$$

$DC \frac{0.0}{21.0}$

$$\begin{array}{cccccccccccccccc}
 \frac{7.3}{40} & \frac{7.2}{27} & \frac{6.4}{23} & \frac{7.3}{21} & \frac{7.2}{19} & \frac{6.1}{15} & 5.5 & \frac{5.9}{15} & \frac{6.5}{17} & \frac{6.5}{19} & \frac{4.5}{22} & \frac{0.0}{26} & \frac{4.0}{40}
 \end{array}$$

$DC \frac{0.0}{22.0}$

+  $\pi$  - Elev

536.69

109+50

110+00

110+50

111+00

✓

T.P. 7.89 533.50 11.08 525.61

111+50

112+00

$$\frac{8.0}{40} \quad \frac{00}{24} \quad \frac{7.0}{21} \quad \frac{8.5}{20} \quad \frac{8.4}{19} \quad \frac{7.0}{14} \quad 6.9 \quad \frac{7.4}{15} \quad \frac{7.9}{19} \quad \frac{4.3}{21} \quad C \quad \frac{2.2}{28.4} \quad \frac{4.5}{40}$$

$$\frac{7.9}{40} \quad \frac{0.4}{24.8} \quad \frac{7.2}{21} \quad \frac{9.2}{19} \quad \frac{9.0}{16} \quad \frac{8.2}{14} \quad 8.0 \quad \frac{8.2}{12} \quad \frac{8.7}{18} \quad \frac{5.1}{22} \quad C \quad \frac{3.2}{30.4} \quad \frac{4.8}{40}$$

$$\frac{8.2}{40} \quad \frac{0.12}{26.4} \quad \frac{7.8}{22} \quad \frac{10.1}{20} \quad \frac{10.2}{17} \quad \frac{9.3}{14} \quad 9.2 \quad \frac{9.2}{10} \quad \frac{10.0}{17} \quad \frac{5.8}{22} \quad C \quad \frac{3.8}{31.6} \quad \frac{5.4}{40}$$

$$\frac{8.5}{40} \quad \frac{0.20}{28.0} \quad \frac{8.4}{22} \quad \frac{11.4}{20} \quad \frac{11.4}{17} \quad \frac{10.6}{14} \quad 10.4 \quad \frac{10.8}{10} \quad \frac{11.3}{17} \quad \frac{6.4}{23} \quad C \quad \frac{4.4}{32.8} \quad \frac{6.0}{40}$$

$$\frac{6.4}{40} \quad \frac{0.22}{28.4} \quad \frac{6.3}{22} \quad \frac{9.3}{19} \quad \frac{9.3}{17} \quad \frac{8.7}{15} \quad 8.6 \quad \frac{8.9}{12} \quad \frac{9.4}{17} \quad \frac{4.2}{22} \quad C \quad \frac{5.3}{34.6} \quad \frac{3.4}{40}$$

$$\frac{6.7}{40} \quad C \quad \frac{2.6}{29.2} \quad \frac{7.4}{22} \quad \frac{10.3}{20} \quad \frac{9.9}{16} \quad 9.8 \quad \frac{10.2}{12} \quad \frac{11.1}{16} \quad \frac{10.9}{19} \quad \frac{4.1}{27} \quad C \quad \frac{6.435}{36.8} \quad \frac{3.5}{40}$$

+ T - Elev

533.50

112+50

BM Set

8.31 525.19

113+00

BM (Above) 3.50 528.69

525.19

113+50

114+00

12-20-33

BM 11.9 530.38

529.19

114+50

+60- 6' Corr. Culv Out 22.0

115+00

TP 4.76 522.63 12.51 511.87



$$\frac{7.2}{40} \quad \frac{C2.9}{29.8} \quad \frac{9.1}{21} \quad \frac{11.6}{19} \quad \frac{11.6}{17} \quad \frac{11.3}{16} \quad 11.1 \quad \frac{11.3}{13} \quad \frac{12.5}{20} \quad \frac{4.2}{31} \quad \frac{C6.8}{37.6} \quad \frac{4.3}{40}$$

Stake Nailed to power pole 30' L of 112+80

$$\frac{8.6}{40} \quad \frac{C3.1}{30.2} \quad \frac{10.1}{22} \quad \frac{12.9}{20} \quad \frac{12.6}{17} \quad 12.5 \quad \frac{12.9}{13} \quad \frac{13.7}{18} \quad \frac{13.0}{21} \quad \frac{5.9}{33} \quad \frac{C6.6}{37.2} \quad \frac{5}{4}$$

$$\frac{6.5}{40} \quad \frac{C3.0}{30.2} \quad \frac{6.5}{22} \quad \frac{10.4}{16} \quad \frac{9.7}{12} \quad 9.5 \quad \frac{9.8}{16} \quad \frac{10.8}{17} \quad \frac{3.8}{36} \quad \frac{C6.2}{36.4} \quad \frac{3.5}{40}$$

$$\frac{10.0}{40} \quad \frac{C1.4}{26.8} \quad \frac{9.3}{21} \quad \frac{11.7}{18} \quad \frac{11.6}{15} \quad \frac{10.9}{12} \quad 11.0 \quad \frac{11.8}{15} \quad \frac{15.7}{18} \quad \frac{15.7}{21} \quad \frac{13.7}{23} \quad \frac{10.2}{36} \quad \frac{F2.7}{23.1}$$

$$\frac{C2.3}{28.6} \quad \frac{10.2}{40} \quad \frac{6.9}{22} \quad \frac{11.2}{18} \quad \frac{11.0}{14} \quad \frac{10.5}{14} \quad 10.1 \quad \frac{10.2}{11} \quad \frac{17.1}{19} \quad \frac{17.1}{22} \quad \frac{4.3}{30} \quad \frac{6.0}{33} \quad \frac{9}{40}$$

(Not 5' Skod)

$$\frac{C1.8}{27.6} \quad \frac{11.3}{40} \quad \frac{9.3}{28} \quad \frac{9.3}{24} \quad \frac{14.0}{18} \quad \frac{12.3}{16} \quad \frac{11.6}{13} \quad 11.5 \quad \frac{12.7}{26} \quad \frac{24.6}{42} \quad \frac{29.1}{60} \quad \frac{33.2}{100} \quad \frac{F2.0}{15}$$

Top of So. End of 6' Culv Sk 114+60

+  $\pi$  - Elev

115+08 End 6' Culv - 33' R  
522.63

115+50

116+00

116+50

117+00

BM 266 520.53 517.87

115+50 17.4

116+00 16.7

+50 16.5

$$F \frac{19.3}{72.9}$$

$$\frac{5.6}{12} \quad 5.2 \quad \frac{5.1}{11} \quad \frac{6.0}{14} \quad \frac{22.5}{40} \quad \frac{24.5}{65} \quad \frac{24.0}{100}$$

$$F \frac{18.9}{71.7}$$

$$\frac{6.7}{14} \quad \frac{6.0}{11} \quad 5.9 \quad \frac{5.9}{11} \quad \frac{8.3}{17} \quad \frac{21.8}{35} \quad \frac{26.9}{54} \quad \frac{25.0}{85}$$

$$\frac{7.5}{15} \quad \frac{6.5}{10} \quad 6.2 \quad \frac{6.4}{13}$$

$$\frac{6.1}{14} \quad 5.5 \quad \frac{5.5}{12} \quad \frac{6.6}{17}$$

Top of So. end of 6' Cul. R. of Sta. 114+60

$$\frac{3.4}{12} \quad 3.1$$

$$\frac{4.7}{15} \quad \frac{3.9}{12} \quad 3.8$$

$$\frac{5.0}{15} \quad \frac{4.6}{12} \quad 4.0$$

Sta + H.I. - E/cv

520.53

117

17.1

+50

T.P. 8.13 515.09 13.57 506.96 ✓

115+50 17.4

116+00

16.7

T.P. 0.26 501.63 13.72 501.37

116+50 576.5

117+0

17.1

T.P. 13.28 514.65 0.26 501.37

T.P. 6.21 520.67 0.19 514.46

B.M. 2.85 520.72 2.85 517.82 577.87

116.50

B.M. 4.50 522.37 2.85 517.87

117+00

+50

T.P. 10.56 530.48 2.45 519.92

118+00

+50



$$\frac{4.1}{15} \quad \frac{3.7}{12} \quad 3.4$$

$$\frac{2.3}{50} \quad 3.1 \frac{10.2}{180} \frac{8.4}{29} \frac{10.7}{26} \frac{10.3}{24} \frac{3.3}{14} \frac{2.7}{12} \quad 2.2$$

2.3-

$$\frac{4.2}{50} \quad 35.7 \frac{4.6}{169} \frac{3.9}{30} \frac{3.3}{20}$$

$$\frac{13.4}{60} \quad 58.1 \frac{12.8}{114.4} \frac{11.1}{49} \frac{14.1}{51} \frac{11.1}{30} \quad 1.6-$$

1.49-

$$\frac{3.2}{80} \quad 7.1 \frac{4.8}{119.2} \frac{3.3}{62} \frac{6.3}{55} \frac{4.6}{40} \frac{3.1}{36}$$

1.5.5-

$$80.4 \frac{6.3}{152.8} \frac{5.6}{80} \frac{6.5}{70} \frac{3.9}{50} \frac{0.7}{40}$$

1

$$4.2 \frac{12.0}{23} \frac{18.3}{31} \frac{14.7}{42} \frac{15.2}{48} \frac{15.7}{58}$$

Top of 50. end of 6" Cul. Rt of Stall 460

$$5.3 \frac{5.5}{13} \frac{12.6}{25} \frac{12.5}{28} \quad \frac{10.3}{130.3} \frac{1.5}{39} \quad \frac{0.2}{46}$$

$$4.1 \frac{4.1}{12} \frac{4.5}{18} \frac{6.3}{20} \frac{6.5}{22} \frac{2.5}{25} \frac{3.5}{25} \frac{1.2}{25} \quad \frac{1.7}{41}$$

$$\frac{6.1}{45} \quad 3.1 \frac{5.7}{64.7} \frac{5.9}{32} \frac{10.3}{27} \frac{11.2}{23} \frac{12.3}{20} \frac{11.4}{19} \frac{10.4}{12} \quad 10.4 \frac{10.8}{12} \frac{13.5}{16} \frac{13.8}{18} \frac{10.2}{21} \frac{9.6}{24} \frac{0.9}{41} \frac{0.8}{46} \frac{1.3}{43} \frac{1.6}{50}$$

$$\frac{8.2}{40} \frac{7.4}{30} \frac{10.0}{25} \frac{11.9}{21} \frac{9.8}{21} \frac{9.1}{15} \quad 8.8 \frac{8.9}{11} \frac{10.5}{14} \frac{11.2}{16} \frac{7.8}{20} \frac{6.0}{24} \frac{0.8}{24} \frac{0.6}{24} \quad \frac{4.4}{40}$$

Sto + H.T. - Elev  
530.48

119+00

+50

120+00

T.P. 1259 541.32 1.75 528.73

50

121+00

+50

122+00

B.M. 726 545.76 2.84 538.50

+50

123+00

+50

124+00

+50

$$\frac{63}{40} \frac{49}{32} \frac{10}{21} \frac{83}{11} \frac{83}{26} \frac{82}{19} \frac{71}{15} 68 \frac{71}{11} \frac{101}{16} \frac{101}{18} \frac{29}{33} \frac{27}{41} \frac{20}{40}$$

$$\frac{34}{40} \frac{26}{32} \frac{61}{26} \frac{1}{0.02} \frac{64}{20} \frac{64}{20} \frac{59}{15} \frac{51}{11} \frac{51}{17} \frac{52}{20} \frac{25}{27} \frac{21}{0.39} \frac{1.3}{41}$$

$$\frac{1.1}{40} \frac{0.5}{32} \frac{46}{26} \frac{1}{0.00} \frac{48}{20} \frac{36}{14} \frac{34}{11} \frac{35}{20} \frac{41}{21} \frac{39}{27} \frac{0.0}{0.33} \frac{0.1}{30.6} \frac{0.1}{40}$$

$$\frac{8.5}{40} \frac{85}{32} \frac{1}{0.41} \frac{139}{11} \frac{140}{26} \frac{129}{19} \frac{12.6}{15} \frac{12.6}{13} \frac{130}{21} \frac{86}{28} \frac{86}{0.43} \frac{9.0}{40}$$

$$\frac{50}{40} \frac{36}{32} \frac{46}{26} \frac{45}{33} \frac{113}{27} \frac{116}{18} \frac{112}{14} 109 \frac{110}{14} \frac{114}{16} \frac{114}{20} \frac{62}{30} \frac{62}{0.37} \frac{6.0}{31.4} \frac{6.0}{40}$$

$$\frac{1.7}{50} \frac{39}{32} \frac{1.6}{0.25} \frac{1.7}{33} \frac{100}{19} \frac{94}{14} 91 \frac{91}{11} \frac{98}{18} \frac{96}{21} \frac{34}{31} \frac{3.7}{0.54} \frac{3.7}{40}$$

$$\frac{1.5}{45} \frac{36}{32} \frac{1.3}{0.63} \frac{0.9}{32} \frac{7.5}{23} \frac{94}{19} \frac{79}{14} 76 \frac{77}{11} \frac{82}{18} \frac{78}{21} \frac{1.5}{30} \frac{1.5}{0.61} \frac{1.5}{36} \frac{1.5}{45}$$

Top stake nailed to TP 20' Rt 549 123700

$$\frac{6.9}{40} \frac{62}{30} \frac{62}{32} \frac{109}{29} \frac{112}{21} \frac{109}{18} \frac{106}{15} 104 \frac{106}{14} \frac{112}{19} \frac{53}{28} \frac{51}{0.51} \frac{53}{44}$$

$$\frac{6.8}{40} \frac{28}{32} \frac{64}{26} \frac{62}{25} \frac{76}{21} \frac{72}{19} \frac{89}{13} 87 \frac{88}{14} \frac{98}{19} \frac{93}{22} \frac{52}{27} \frac{52}{0.35} \frac{5.3}{31.0} \frac{5.3}{40}$$

$$\frac{5.8}{40} \frac{26}{32} \frac{62}{26} \frac{62}{25} \frac{76}{19} \frac{74}{16} \frac{72}{12} 72 \frac{74}{13} \frac{81}{18} \frac{80}{21} \frac{44}{27} \frac{47}{0.25} \frac{4.0}{29.0} \frac{4.8}{40}$$

$$\frac{4.2}{40} \frac{26}{32} \frac{44}{26} \frac{43}{22} \frac{48}{18} \frac{60}{15} \frac{59}{12} 56 \frac{52}{12} \frac{64}{18} \frac{65}{22} \frac{40}{27} \frac{40}{0.16} \frac{4.0}{21.2} \frac{4.4}{40}$$

$$\frac{3.9}{40} \frac{24}{32} \frac{39}{26} \frac{38}{20} \frac{42}{15} \frac{43}{12} 41 \frac{42}{11} \frac{50}{17} \frac{51}{20} \frac{32}{24} \frac{32}{0.09} \frac{3.8}{25.8} \frac{3.8}{40}$$

Sta + H.I. - Elev  
545.76

125

+50

T.P. 1031 55421 1.86 54390

126

+50

127

+50

BM 2.88 557.33



$\frac{46}{40}$      $2.0 \frac{1/4.2}{F1.7}$      $\frac{3.7}{16}$      $\frac{3.0}{18}$      $2.5$      $\frac{2.6}{18}$      $\frac{3.1}{16}$      $\frac{3.4}{19}$      $\frac{3.5}{21}$      $\frac{1.8}{25}$      $\frac{1.8}{C47}$      $\frac{1.8}{28.4}$      $\frac{2.6}{40}$

$$\frac{33}{40} \quad 1\frac{9}{16} \quad \frac{30}{19} \quad \frac{18}{12} \quad 1.4 \quad \frac{13}{10} \quad \frac{2.2}{20} \quad \frac{1.4}{600} \quad 240 \quad \frac{1.3}{40}$$

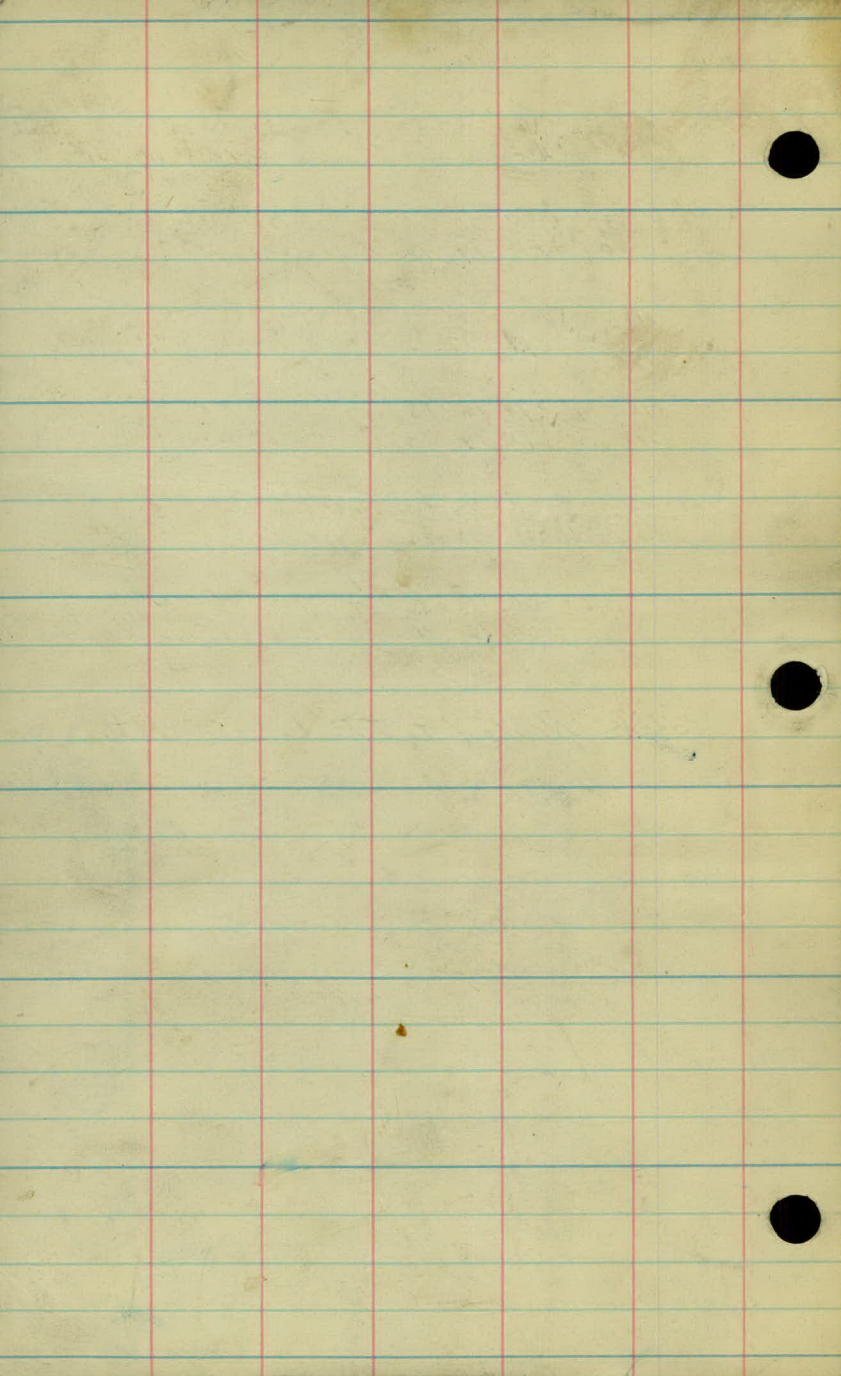
$$\frac{110}{40} \approx \frac{10.5}{17} \approx \frac{9.2}{13} \approx 8.8 \approx \frac{8.9}{13} \approx \frac{9.6}{18} \approx \frac{8.6}{22} \approx \frac{8.4}{20.4} \approx 4.8 \approx \frac{8.9}{40}$$

$$\frac{9.8}{40} \quad \frac{9.8}{24} \quad \frac{9.8}{15} \quad \frac{9.2}{19} \quad \frac{8.5}{14} \quad 7.9 \quad \frac{8.1}{14} \quad \frac{8.4}{18} \quad \frac{7.1}{22} \quad \frac{7.0}{0.09} \quad \frac{5.8}{5.8} \quad \frac{7.5}{4}$$

$$\frac{80}{40} \quad 2.12 / \frac{8.1}{200.1} \quad \frac{82}{18} \quad \frac{71}{12} \quad 67 \quad \frac{70}{14} \quad \frac{76}{19} \quad \frac{49}{23} \quad \frac{54}{0.13/26.6} \quad \frac{53}{40}$$

$$\frac{5.6}{40} \approx \frac{1.8/6.7}{20.4} \approx \frac{6.6}{20} \approx \frac{6.3}{16} \approx \frac{5.6}{11} \approx \frac{5.6}{5.6} \approx \frac{5.9}{13} \approx \frac{6.5}{18} \approx \frac{2.9}{25} \approx \frac{3.5}{21} \approx \frac{3.1}{22} \approx \frac{3.1}{22}$$

Top Stake Nailed to T.P. 128+55 Rt



12/13/33

Cold Clear.

C. W. Sealtup

C. Brattschneider

Daly

Gross

Esbolt.

# Topography

East Co Line

Sta 0+00 - 100+00

5+00

+12 Drive way Lt 18' C19 20' X 12"

+10 Drive way Rt 19' A23' X 12"

4+00

+54 & Dr Way Rt 19' C19 19.5' X 18' X 12"

3+00

2+00

+34 X Drain 30' X 42' C.M.

1+00

0+00 & Hyvveed Ave



12/13/23

+36 TP 31'

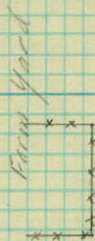
56 Rd. Sq 17'

+30-2-MB 15'

+85 End F 25'

+85 TP 33'

+28 F Cor 25'

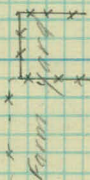


Drive +10

Drive +54

+34 RP 27'

+22 End F 25'



+39 TP 30'

+90 Beg F 25'

15' 15'

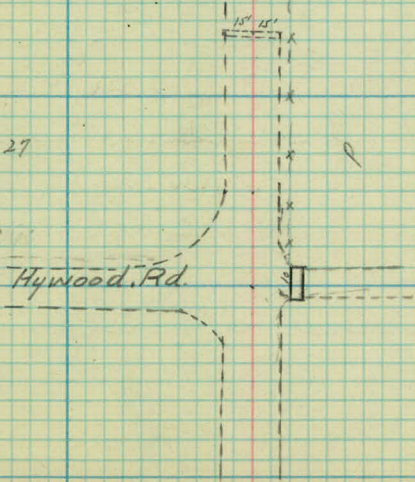
+93 TP 27'

+50 2-178'

+29 RP 27'

Hywood Rd.

100 Cattle Pass 20'



11+00

10+00

9+00

8+00

7+00

6+00

12/13/53

+61-PP.27'

+11 TP.30'

+76 Gate G. 50.50'  
+68 TP.30'

Cul

Cul

+23 TP.30'

+61 PP.27'

+77 TP.30

Orchard



17+00

16+00

15+00

14+00

13+00

12+00



12/12/

+93 TP 25'

+50 TP 27'

+61 PP 27'

+04 TP 27'

+58 TP 28'

127

127

23+00

22+00

21+00

Lt +83 to Drive Way No Curb Lt

Rt +66 to Drive Way No Curb Rt

20+00

19+00

18+00

12/13/33

+90 P.P. 27'

410 X Enc 28'

04 Pg 59 20'

409 T.P. 241

469 x Fenec 30'

458 T. 17. 23'

407.M.B.13

483 Drive.

Drive #66

+60 End Br. 25'

+97 T.P. 23  
+94 5g. 4-8.

+ 94 59. 4-8.

+71 PR 26'

+47 TP.25'

416 Beg. Brush 23'



114 A. W. Lt +50-26'

29+00

28+00

27+00

Lt+31 A Linwood Ave Lt 42' x 24" No 76-18

26+00

+38 X Train 31 x 12" C.M. No 4-9

25+00

+93 Lt Drive Way Rt No 606

24+00



12/13/22

+75 Rd Sq 16'

Cul.

Woods

Side Drain 43'

+32 Linwood Rd.

+06 St. & Sq 27'  
+02 Rd Sq 27'

+62 PP 27'

+32 F Cor 28'

+32 14" Tr 25'

+00 12" Tr 24'  
F 28

+14 Tr 14" 23

+35 20" BL Tr 20

+09 F Cor 29'

16' 15'

DRIVE +93

+83 M.B 11'

+36 T.P 26'

35+00

34+00

33+00

+40 X Drain 24" x 40' C.M.

32+00

+81 Lt R. Stone Way No C.M.

31+00

30+00

Lt

Rt

12/13/33

+50 PP 27'

Swamp

24 4

+81 Drive

WOOPER  
PASTURE

+63 PP 28'



4100

4000

3900

+91 X Grain 33'x36 CM No 4-11

3800

3700

3600



12/13/33

Cul.

Cul.

+77 E Fence 19'

+15 PP 26

F 17.

STER

+97 Fence Cul 17

Pot Hole

Pot Hole

+64 X Fence 19'

47+00

46+00

45+00

44+00

43+00

42+00

12/13/33

+84 PP. 26'



114 X Drain 32" x 24" C.M. No 4-12

53+00

52+00

51+00

50+00

49+00

48+00



12/13/23

+21 GP 15'

+29 PP 26'

Col

Col

+76-RSq 18'

+02 PP 27'

Col

Col

59+00

58+00

57+00

123 A After R/So Lt.

56+00

55+00

54+00

12/13/33

+89 TP 18

F 27'

+21 TP 19'

F 30'

F 27'

+69 T.P. 19'

AFTON

+40 E. acc. Cor 28

Rd. So.

+25 R.S. 26'



65+00

64+00

63+00

62+00

+18 X Drain 45' x 24" C.M. No 4-13

61+00

60+00



12/12/33

+64 T.P. 17'

Cul

Cul

+98 T.P. 17'

+100 End F. 36'

+38 T.P. 20'

F 35'

F 31'

Cul

Cul

F 26'

71400

70400

69400

68400

67400

66400

12/13/33

+92 TP 17'

Cult

Cult

+357 P. 17

+79 TP 18'

Cult

Cult

+24 TP 17'



77

76

75

74

73

72



12/2/33

+22 T.P. 17'

Cul

Cul

+64 T.P. 17'

+10 T.P. 17'

Cul

Cul

+52 T.P. 17'

I

83+00

82+00

81+00

80+00

+20 ~~to~~ H. Way. ht No. Cul.

+20 X Drain 40" X <sup>15</sup>14" C.M. 16'

+20 ~~to~~ H.W. Rt 17' 20" X 18" C.M.

79+00

78+00

I

12/13/33

+85 TP. 18

+11 TP. 19'

+45 TP. 19'

+62 M/B. 16

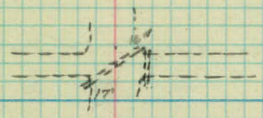
+9 Beg. Cul. 17'

+77 TP. 19'

Pasture.

Cul.

Wood.



F 23

+45 F. Cor. 23

F 23'

F 24'

F 24'

+71 F. Cor. 24.

+99 Beg. Cul. 16'



89

88

87

86

+88 B Driveway Rt 21' CM 20' X 18"

85 CM. Extend By Boiler Plate 17'

+90 & Driveway 16' CM. 20' X 18"

+30 & A. Wayht No Cule

+24 X Drain 40' X 18 CM.

No 4-16

8400



12/13/30

F 27'

+62 T.P. 18'

F 26

F 24  
+98 T.P. 17'

F 25'  
+80 M.B. 15'  
+48 T.P. 18'  
+24 F.C. 24'

+20 M.B. 16'  
+12 Beg. Culu 15'



15' Long 5' wide  
+09 Concrete Culu 15'  
+07 T.P. 13'

F30 Drive

+69 E.F. Culu 23'  
+35 End Culu 15'  
F 2V

95

94

+56 R Drive Way Lt 17' 6" 18" X 18'

93

92

91

+87 R Drive Way 18' Tile Curb 15" X 24" Rt.

90

12/13/23

+87 T.P. 19'

+35 T.P. 18'

+39 End Fence 29  
F 26'

+77 T.P. 18'

F 26'

+88 M.B. 14  
+16 T.P. 18'

F 29'

+56 Drive

Cul.

Pasture

+87 Drive

Cul.

Marsh

+33 X Fence 63'



101+00

100+00

99+00

98+00

97+00

+38 X Drain 50' x 28" CM 1/6 4-19

96+00



12/13/83

+ 47 ft. P. 21'

4122

7/12

+ 97 T.P. 20'

2-45 End Cols 240

439 J.P. 20

+ 08 x Fence 35'

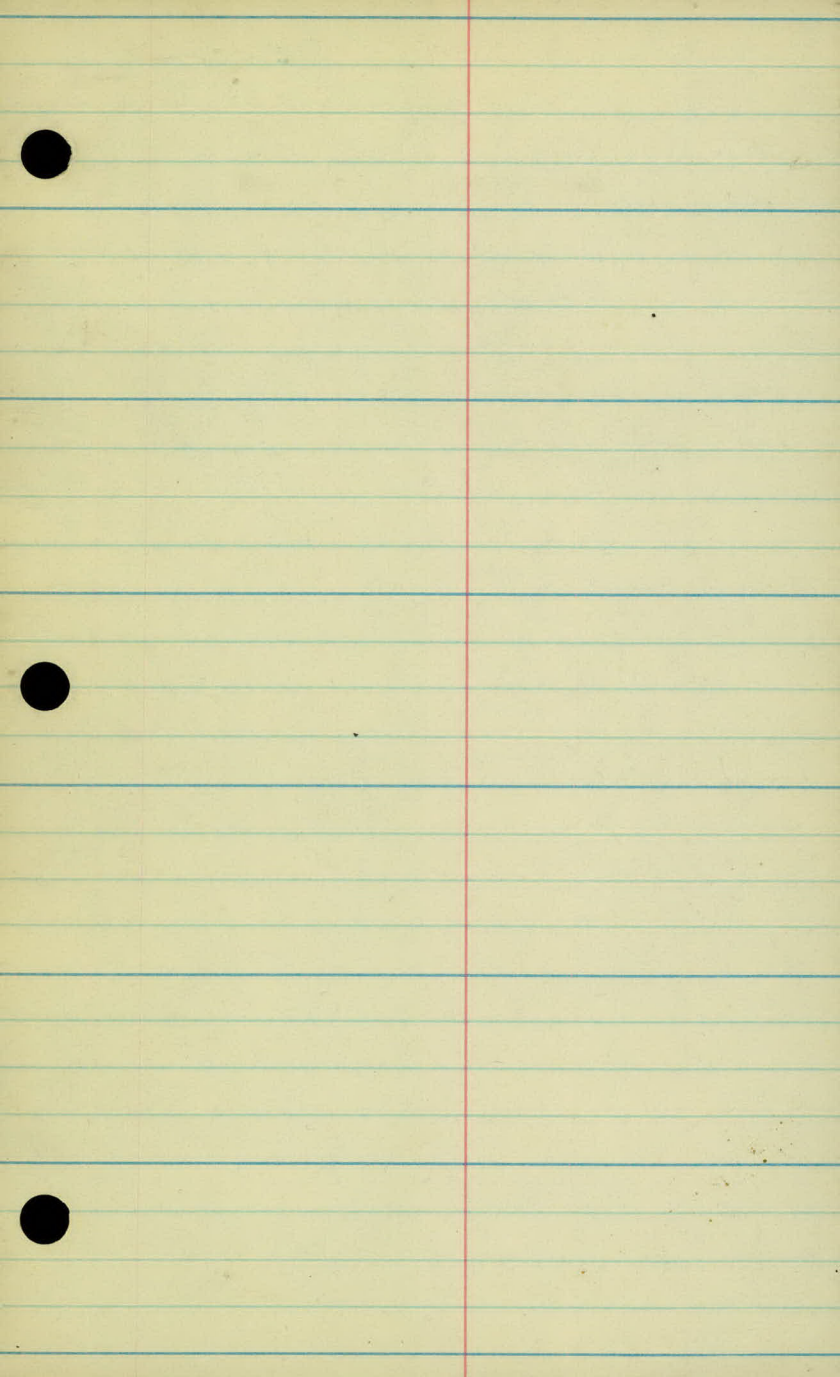
+30 Beg Catu 23'

105400

104400

103400

102400



+50.2. After 30. 49' X 18" C 17. Good Side Drain

105+00

104+00

103+00

102

101+00

100+00



+93 PP. 24  
76 Rdsg 21  
+71 GP 2V  
+11 TP 2V  
+11 Rdsg 22

AFTON SO.

+82 TP 24  
+65 Rdsg 27  
+56 ECols. 24

+08 Bay Cols. 41'

+91 GP-23'

+93 TP 2V

+50 TP. 20'

+97 TP. 20'

111

110

109

108

107

106

+50 T.P. 25'

+22 P.P. 27'

+49 T.P. 23'

+21 T.P. 23'

+96 T.P. 20'

+45 R/39 23'  
+43 P.P. 26'

+61 T.P. 23'

+41 T.P. 24'

+65 T.P. 22'

+59 P.P. 25'

+60 T.P. 22'

+86 T.P. 23'

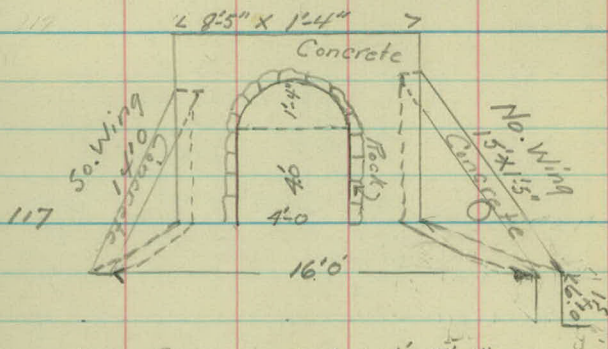
Cut

Cut

H.P. 10  
+53 T.P. 19'-25'



East side



+25 R Drain 67' X 4' X 5'4"

116

115

+82 S Drain 72" X 49'

114

+22 D. Way 21' X 12" Vit Pipe & C.M.

113

112



+77 End GR 12'

36

+49 Rd. Drive 12" x 31' - 11"

GR 13 F 32'

+11 Beg GR 13'

F 23'

+41 X F 23'

F 22'

+34 Beg Fence 22'

+34 End Cul. 15'

+11 Beg Cul. 16'

+05 TP 26'

+76 PP 28'

+28 E. GR 13

+34 X Fence 50'

+34 TP 23'

F 4 V CR 13

+71 Fence 23'-31'

+71 TP - 23'

GR 12 F 25'

+36 TP 23'

+11 Beg GR 12'

+08 End Cul. 33'

F 25'

+81 F 29'

+61 Beg Cul. 21'

+27 Beg Fence 39'

+09 TP 23'

+12 M.B. 14'

+76 TP 24'

123

122

121

120

119

+45 Drive Way 20' X 24" CM. Good.

118

+96 T.P. 23'

+61 T.P. 23'

+99 T.P. 23'

141 E. Pond 44

+17 T.P. 23'

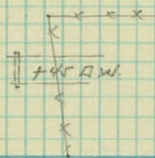
F 45

F 49.0

+19 T.P. 23'

+72 X F 35'-50'

F 35'



+71 End F 35'

+55 End Culo 16'

+35 Bg Culo 16'

+00 T.P. 23'

F 41'



129-

128

1<sup>st</sup> J. M.

127

126

125

124



+67 TP 24'

+54 TP 24'

+90 TP 24'

+54 Rdsq 20'

+90 TP 24'

+64 TP 24'

+23 TP 23'

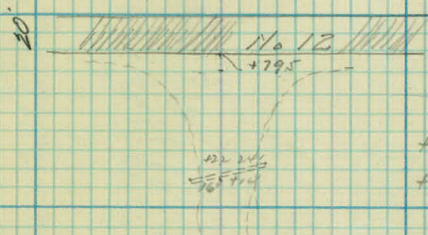
133-

134

+17 X Drain 18" X 40' CM. Co-d.

131

130



+16 Rd Sq 20  
+03 MB 13

66 GP 24  
+28 TP 33

+50 TP 27



