

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

----- *PLAN* ----- Survey

*NEW BRIGHTON RD. EXTENSION*

From *Co. Rd. "A"* To *Co. Rd. "B"*

Road Acc't. No. *16*

Date Filed.....

File *33-16*

PROJ. 33-16

Alignment

Rd #16

Proj 33-16

STA. POINT

52+53.00

35+79.90 P.O.T.

26+32.20 P.O.T.  $\frac{1}{2}$  Co. Rd. A<sup>2</sup>

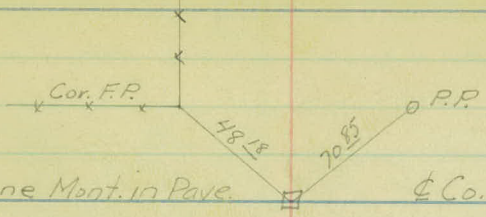
26+02.45 P.O.T.

22+00 P.O.T.

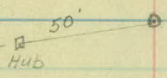
0+00

Stone Mont. in Pav.

Co. Rd. B.

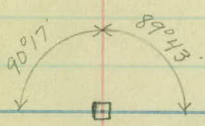


Red Light on N.W. Radio Tower



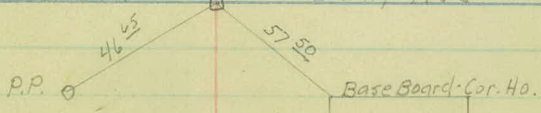
Estab. Iron Mont.

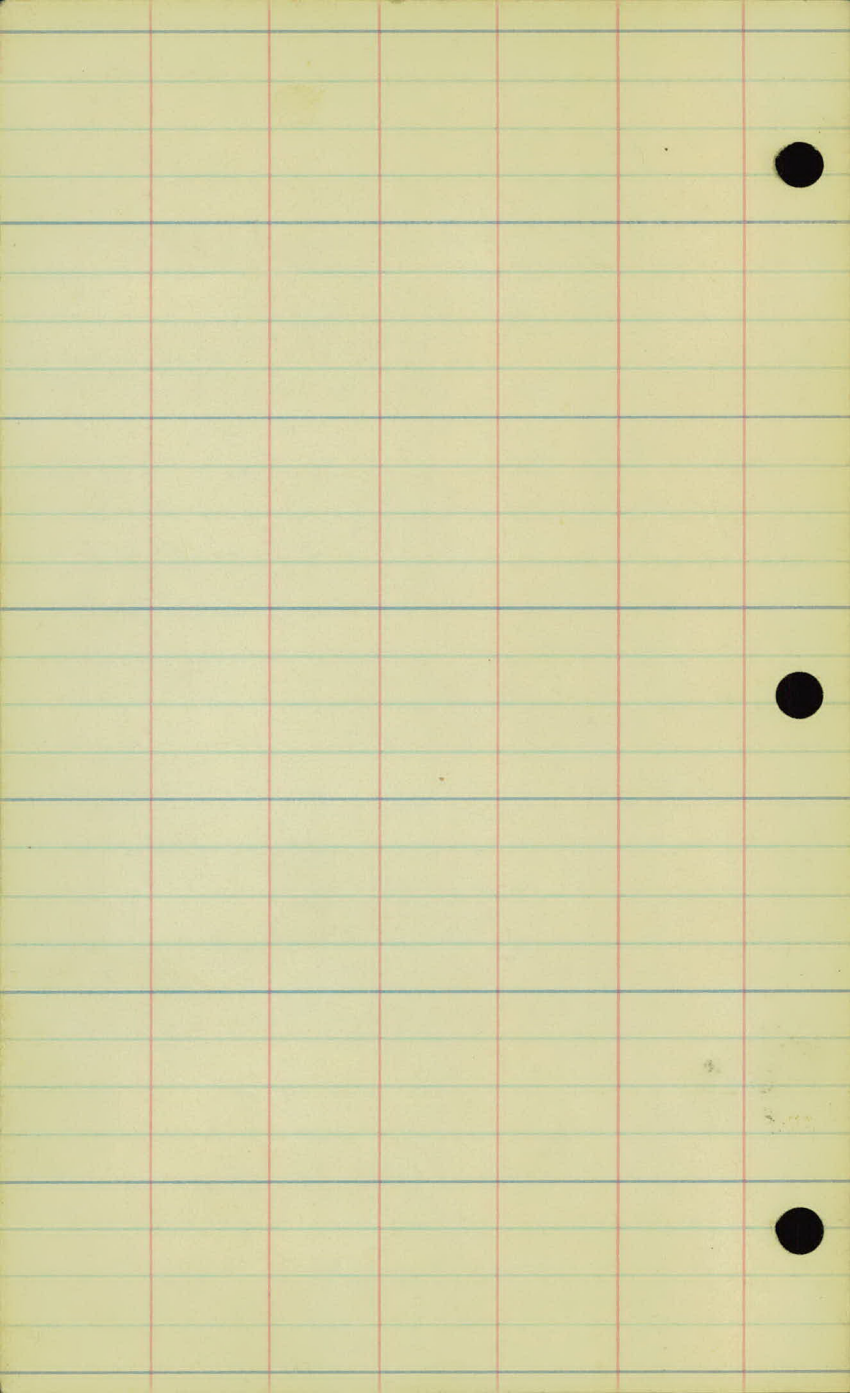
Co. Rd. A



Bolt in Pavement

Co. Larp. Ave





ART. ТИРОС.

STA.

5

4

3

2

1

0+00

f30-F. Int.



Pasture

Cultivated

f32-F. Cor. 2



Pasture

↳ Larp. Ave



20' I.C.C. Pavement

STA.

12

11

10

9

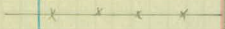
8

7

6

Cultivated

789-F. Int.



Pasture

Cultivated

775-F. Int.



Pasture

57A

19

18

17

16

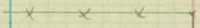
15

14

13

Cultivated

f26-F. Cor.



Cultivated

Cultivated



57A.

26

25

24

23

22

21

20

L-

-R-

6

+50 Edge Cultiv.  
+ 322 E Co. Rd A2 -----

0160 Tel. Pole 50'  
+50 Edge Cultivaco

+05 Tel. Pole 34'  
26+00 END CULTIVATION RT. & L.

STA.

33

32

31

30

29

28

27

-A-

R

-R-

7

3310712' W. OAK 2'L

+34 Bog Fence 2'L

Cultivated

Cultivated

57A

40

39

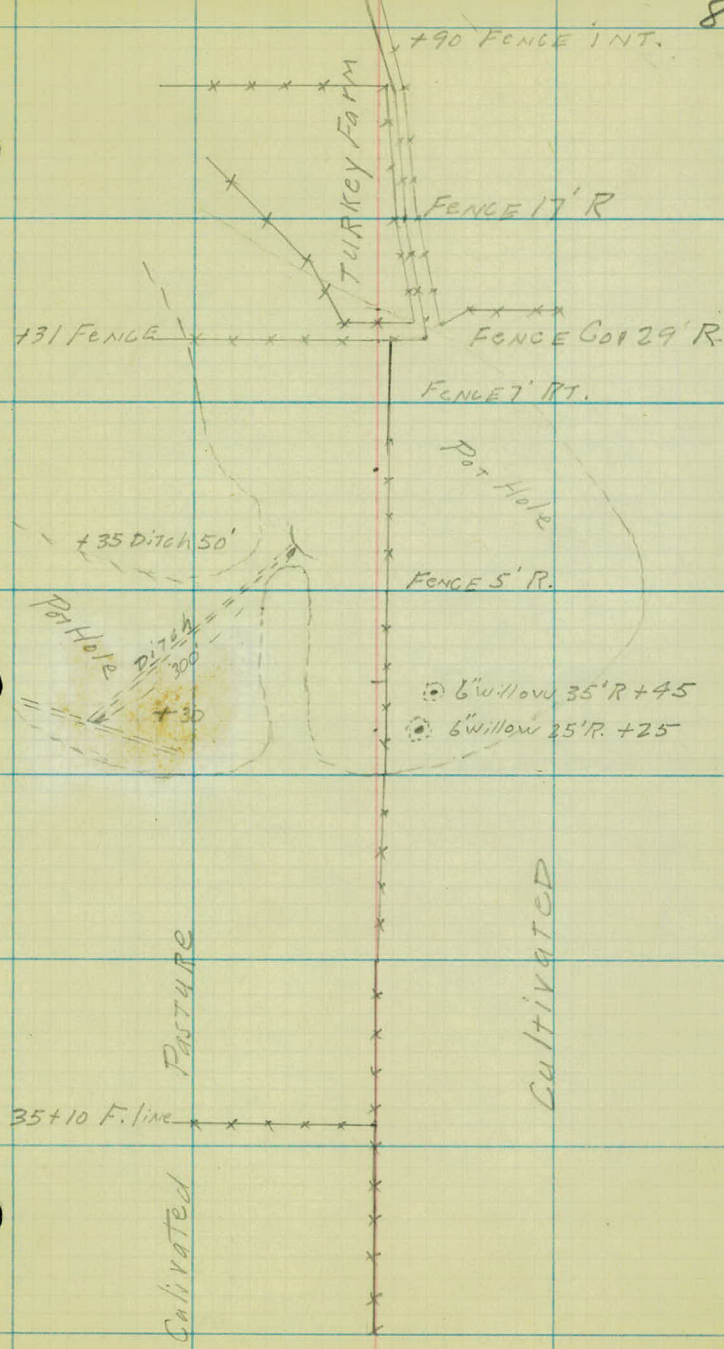
38

37

36

35

34



FENCE 31

TURKEY FARM

+90 FENCE INT.

FENCE 17' R

FENCE 29' R

FENCE 7' RT.

Pot Hole

+35 Ditch 50'

Pot Hole Ditch 300

6" willow 35' R + 45'

6" willow 25' R + 25'

PASTURE

CULTIVATED

35 + 10 F. line

Cultivated

57A.

47

46

45

44

43

42

41

+22 3-8" Willow 18'  
47 to 56" Tile Drain

Ditch

6" Tile

+25-End 6" Tile 49'

Ditch

HAY FIELD

TURKEY PASTURE

Post Hole

FENCE 39'

HAY FIELD

FENCE 21' L

x x x x x

+35 F. Cor.

TURKEY PASTURE

57A

53

52

51

50

49

48

+87-X-Drain

New Brighton Rd.

+75

55'

52+53 Co. Rd. B.

52+26 Tol. Pole  
Sign Boats

52+18 Sign Boats

HZ - Approx. Xing

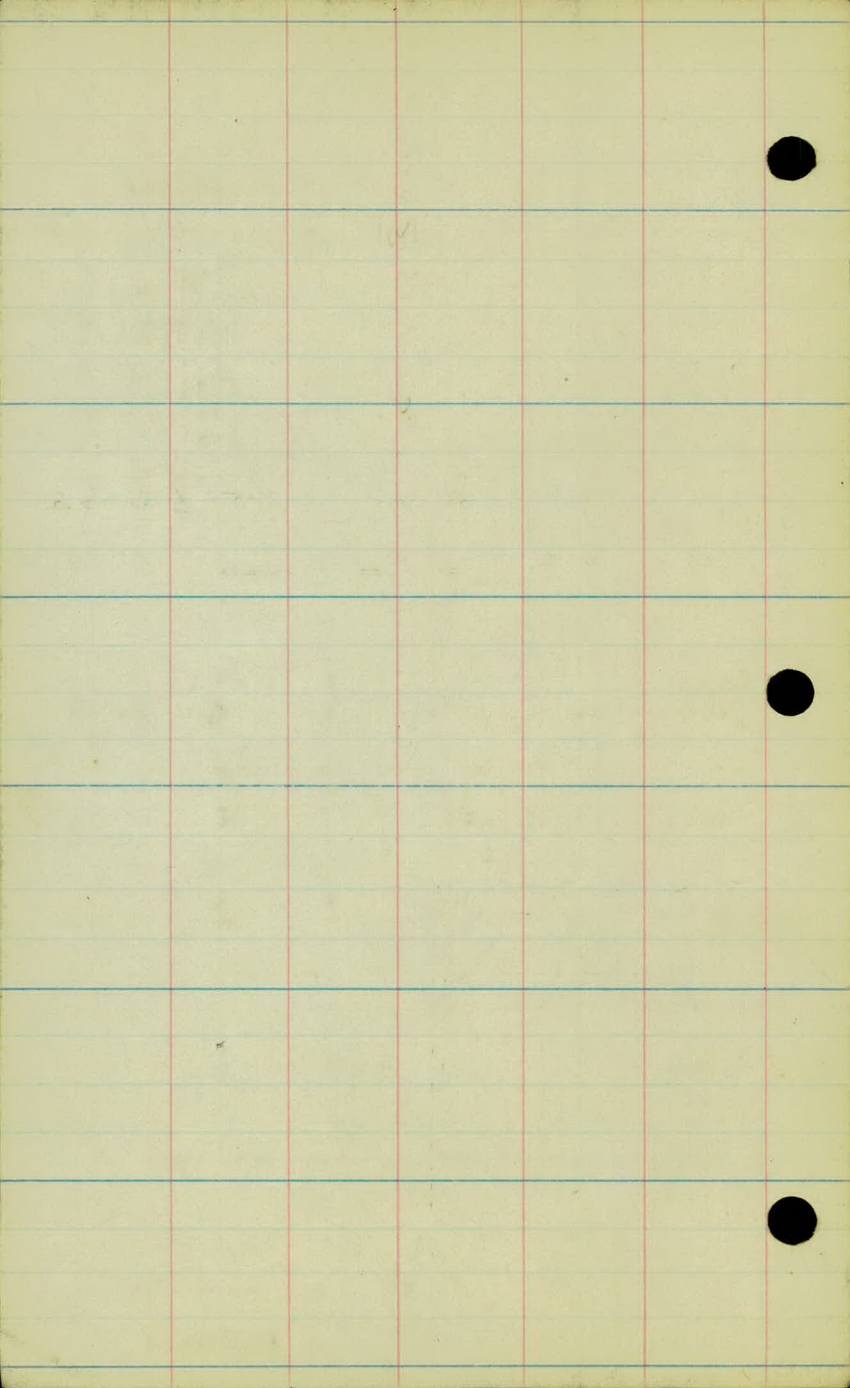
50+44 Beg 6" Tile Drain  
20' L

HAY FIELD

HAY FIELD

102 2-6" willow 20' L





CROSS SECTIONS

Rd. thru S. 16

Sec. 16

STA	+	H.I.	-	ELEV
B.M.	5.06	971.54		966.48
0+00				66.4
+19				66.4
+24				64.3
+28				64.1
+30				65.4
+45				66.4
1				66.7
T.P.	6.00	973.77 ✓	3.77	967.77 ✓
+50				66.8
2				67.0
+50				67.1
3				67.5
+50				68.2

Top of Bolt Sta. 0+00

$$\frac{4.4}{50} \quad 5.1 \quad \frac{5.8}{50}$$

$$\frac{4.3}{50} \quad 5.1 \quad \frac{5.6}{50}$$

$$\frac{6.4}{50} \quad \frac{6.8}{25} \quad 7.2 \quad \frac{7.7}{25} \quad \frac{8.0}{50}$$

$$\frac{6.5}{50} \quad \frac{7.1}{25} \quad 7.4 \quad \frac{7.5}{25} \quad \frac{8.1}{50}$$

$$\frac{5.4}{50} \quad \frac{5.9}{25} \quad 6.1 \quad \frac{6.0}{25} \quad \frac{6.0}{50}$$

$$\frac{4.7}{40} \quad \frac{5.0}{15} \quad 5.1 \quad \frac{5.8}{9} \quad \frac{5.3}{19} \quad \frac{5.5}{40}$$

$$\frac{4.2}{40} \quad \frac{4.5}{20} \quad 4.8 \quad \frac{5.4}{4} \quad \frac{5.1}{14} \quad \frac{5.9}{40}$$

$$\frac{6.1}{40} \quad \frac{6.7}{20} \quad 7.0 \quad \frac{7.8}{4} \quad \frac{7.6}{15} \quad \frac{8.2}{40}$$

$$\frac{6.0}{40} \quad \frac{6.4}{20} \quad 6.8 \quad \frac{7.7}{4} \quad \frac{7.3}{13} \quad \frac{8.0}{40}$$

$$\frac{5.8}{40} \quad \frac{6.2}{20} \quad 6.7 \quad \frac{7.5}{4} \quad \frac{7.2}{12} \quad \frac{7.4}{40}$$

$$\frac{5.4}{40} \quad \frac{5.8}{20} \quad 6.3 \quad \frac{7.1}{4} \quad \frac{6.9}{13} \quad \frac{7.5}{40}$$

$$\frac{4.7}{40} \quad \frac{4.8}{20} \quad 5.6 \quad \frac{6.3}{4} \quad \frac{6.0}{10} \quad \frac{6.5}{40}$$

STA + H.I. / - FLEV

973.77

4 69.0

+50 68.7

5 68.1

+50 67.5

6 67.5

+50 68.0

7 68.8

T.P. 6.42 976.05 4.14 969.63

+50 69.9

8 70.6

+50 71.0

T.P. 5.84 978.21 3.68 972.37

9 71.4

+50 71.5

10 71.4

$$\frac{4.5}{40} \quad \frac{4.6}{20} \quad 4.8 \quad \frac{5.8}{4} \quad \frac{5.4}{9} \quad \frac{5.7}{21} \quad \frac{6.0}{40}$$

$$\frac{5.2}{40} \quad \frac{5.1}{20} \quad 5.1 \quad \frac{6.0}{4} \quad \frac{5.5}{12} \quad \frac{5.9}{40}$$

$$\frac{5.9}{40} \quad \frac{5.7}{20} \quad 5.7 \quad \frac{6.4}{4} \quad \frac{5.9}{10} \quad \frac{6.4}{40}$$

$$\frac{6.3}{40} \quad \frac{6.2}{20} \quad 6.3 \quad \frac{6.9}{4} \quad \frac{6.5}{11} \quad \frac{6.8}{40}$$

$$\frac{6.4}{40} \quad \frac{6.4}{20} \quad 6.3 \quad \frac{6.6}{4} \quad \frac{6.3}{13} \quad \frac{6.5}{40}$$

$$\frac{6.2}{40} \quad \frac{6.1}{20} \quad 5.8 \quad \frac{6.3}{4} \quad \frac{5.9}{14} \quad \frac{5.7}{40}$$

$$\frac{5.9}{40} \quad \frac{5.6}{20} \quad 5.0 \quad \frac{5.6}{3} \quad \frac{5.2}{7} \quad \frac{4.6}{40}$$

$$\frac{7.8}{40} \quad \frac{7.1}{20} \quad \frac{6.8}{3} \quad 6.2 \quad \frac{7.4}{2} \quad \frac{6.6}{8} \quad \frac{6.1}{20} \quad \frac{5.7}{40}$$

$$\frac{7.3}{40} \quad \frac{6.6}{20} \quad \frac{5.9}{2} \quad 5.5 \quad \frac{6.5}{3} \quad \frac{5.7}{10} \quad \frac{5.2}{22} \quad \frac{4.9}{40}$$

$$\frac{6.8}{40} \quad \frac{6.3}{20} \quad \frac{5.5}{2} \quad 5.1 \quad \frac{6.0}{2} \quad \frac{5.2}{8} \quad \frac{4.7}{22} \quad \frac{4.2}{40}$$

Top of Stake Sta. 9

$$\frac{8.7}{40} \quad \frac{8.1}{20} \quad 6.8 \quad \frac{7.6}{2} \quad \frac{7.0}{7} \quad \frac{6.3}{24} \quad \frac{6.0}{40}$$

$$\frac{8.5}{40} \quad \frac{8.0}{20} \quad 6.7 \quad \frac{7.4}{2} \quad \frac{6.4}{24} \quad \frac{6.2}{40}$$

$$\frac{8.4}{40} \quad \frac{8.0}{20} \quad 6.8 \quad \frac{7.3}{2} \quad \frac{6.8}{22} \quad \frac{6.8}{40}$$

STA 7 H.I.J. - ELEV.

978.21

10+50

71.5

11

71.9

+50

72.8

12

73.7

+50

74.5

13

74.9

T.P.

6.33

982.24 ✓

2.30

975.91 ✓

+50

75.0

14

75.4

+50

75.9

15

77.0

+50

77.6

16

77.8

+50

78.0

$$\frac{8.0}{40} \quad \frac{7.6}{20} \quad 6.7 \quad \frac{7.0}{3} \quad \frac{6.7}{20} \quad \frac{6.8}{40}$$

$$\frac{7.3}{40} \quad \frac{6.6}{11} \quad \frac{5.8}{2} \quad 6.3 \quad \frac{6.7}{3} \quad \frac{5.9}{17} \quad \frac{6.2}{40}$$

$$\frac{6.3}{40} \quad \frac{5.5}{6} \quad \frac{5.1}{1} \quad 5.4 \quad \frac{6.3}{3} \quad \frac{5.6}{8} \quad \frac{5.2}{20} \quad \frac{5.0}{40}$$

$$\frac{5.6}{40} \quad \frac{4.9}{15} \quad \frac{4.2}{1} \quad 4.5 \quad \frac{5.5}{2} \quad \frac{4.6}{7} \quad \frac{4.3}{20} \quad \frac{3.8}{40}$$

$$\frac{5.2}{40} \quad \frac{4.5}{15} \quad 3.7 \quad \frac{4.7}{3} \quad \frac{4.0}{7} \quad \frac{3.6}{20} \quad \frac{3.0}{40}$$

$$\frac{5.1}{40} \quad \frac{4.4}{12} \quad 3.3 \quad \frac{3.9}{3} \quad \frac{3.3}{20} \quad \frac{2.5}{40}$$

$$\frac{9.2}{40} \quad \frac{8.5}{13} \quad 7.2 \quad \frac{7.0}{18} \quad \frac{6.4}{40}$$

$$\frac{8.5}{40} \quad \frac{8.0}{13} \quad 6.8 \quad \frac{7.1}{4} \quad \frac{6.6}{21} \quad \frac{5.6}{40}$$

$$\frac{7.6}{40} \quad \frac{6.9}{13} \quad 6.3 \quad \frac{6.6}{8} \quad \frac{5.8}{22} \quad \frac{5.5}{40}$$

$$\frac{6.4}{40} \quad \frac{5.8}{13} \quad \frac{5.5}{1} \quad 5.2 \quad \frac{5.8}{4} \quad \frac{5.4}{23} \quad \frac{4.9}{40}$$

$$\frac{5.7}{40} \quad \frac{5.2}{20} \quad \frac{4.8}{1} \quad 4.6 \quad \frac{5.2}{3} \quad \frac{4.8}{20} \quad \frac{4.7}{40}$$

$$\frac{5.4}{40} \quad \frac{5.0}{13} \quad \frac{4.8}{1} \quad 4.4 \quad \frac{5.0}{6} \quad \frac{4.5}{22} \quad \frac{4.4}{40}$$

$$\frac{5.5}{40} \quad \frac{4.8}{20} \quad \frac{4.6}{1} \quad 4.2 \quad \frac{4.7}{5} \quad \frac{4.3}{21} \quad \frac{4.0}{40}$$

STA + H.I. - ELEV

982.24

17

78.5

+50

78.9

18

T.P.

10.43

991.40

1.27

980.97

80.2

+50

81.3

19

82.6

+50

83.8

20

84.3

+50

84.8

21

85.1

+50

85.9

22

86.6

+50

85.8

23

85.7

$$\frac{5.3}{40} \quad \frac{4.7}{20} \quad \frac{4.2}{1} \quad 3.7 \quad \frac{4.1}{9} \quad \frac{3.7}{22} \quad \frac{3.7}{40}$$

$$\frac{3.4}{40} \quad \frac{3.2}{20} \quad 3.3 \quad \frac{3.5}{3} \quad \frac{3.1}{21} \quad \frac{3.0}{40}$$

$$\frac{2.1}{40} \quad \frac{2.1}{20} \quad 2.0 \quad \frac{2.5}{4} \quad \frac{2.4}{20} \quad \frac{2.5}{40}$$

$$\frac{10.2}{40} \quad \frac{10.2}{20} \quad 10.1 \quad \frac{10.6}{4} \quad \frac{10.4}{20} \quad \frac{10.7}{40}$$

$$\frac{9.2}{40} \quad \frac{9.0}{20} \quad 8.8 \quad \frac{9.4}{3} \quad \frac{9.3}{20} \quad \frac{9.7}{40}$$

$$\frac{8.0}{40} \quad \frac{7.7}{20} \quad 7.6 \quad \frac{8.1}{4} \quad \frac{8.2}{25} \quad \frac{8.8}{40}$$

$$\frac{7.5}{40} \quad \frac{7.3}{20} \quad 7.1 \quad \frac{7.5}{3} \quad \frac{7.6}{20} \quad \frac{7.9}{40}$$

$$\frac{6.7}{40} \quad \frac{6.6}{20} \quad 6.6 \quad \frac{7.3}{3} \quad \frac{6.9}{20} \quad \frac{7.3}{40}$$

$$\frac{6.6}{40} \quad \frac{6.5}{20} \quad 6.3 \quad \frac{7.0}{3} \quad \frac{6.4}{12} \quad \frac{6.2}{40}$$

$$\frac{6.2}{40} \quad \frac{6.0}{20} \quad 5.5 \quad \frac{6.3}{2} \quad \frac{5.7}{12} \quad \frac{5.4}{24} \quad \frac{5.4}{40}$$

$$\frac{5.4}{40} \quad \frac{4.9}{20} \quad 4.8 \quad \frac{5.5}{2} \quad \frac{5.0}{12} \quad \frac{5.0}{27} \quad \frac{5.0}{40}$$

$$\frac{5.9}{40} \quad \frac{5.7}{20} \quad 5.6 \quad \frac{6.2}{3} \quad \frac{5.6}{13} \quad \frac{5.4}{27} \quad \frac{5.5}{40}$$

$$\frac{6.0}{40} \quad \frac{5.9}{20} \quad 5.7 \quad \frac{5.3}{13} \quad \frac{5.2}{27} \quad \frac{5.2}{40}$$

STA	+	HI ✓	-	ELEV.
		991.40		Elev.
23+50				85.6
24				83.2
T. P.		✓	7.50	983.90 ✓
	690	990 <sup>80</sup>		
24+50				81.3
25				80.6
+50				82.0
26				84.3
26+05				84.5
26+07				80.4
26+16				78.6
26+20				80.4
26+32 <sup>20</sup>		E. Co. Rd. A.2		80.8
B.M.			735	983 <sup>45</sup> ✓ = 983 <sup>46</sup>

- L -

- R -

16

$\frac{6.3}{40}$	$\frac{6.0}{20}$	$\frac{6.1}{3}$	5.8	$\frac{6.6}{2}$	$\frac{6.0}{13}$	$\frac{6.4}{27}$	$\frac{6.8}{40}$
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$\frac{7.0}{40}$	$\frac{7.6}{20}$	8.2	$\frac{9.2}{5}$	$\frac{8.8}{13}$	$\frac{9.6}{28}$	$\frac{10.2}{40}$
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Top STAKE STA. 24+00

$\frac{6.8}{40}$	$\frac{8.5}{22}$	$\frac{9.1}{2}$	9.5	$\frac{10.2}{4}$	$\frac{10.7}{20}$	$\frac{11.3}{40}$
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$\frac{8.2}{40}$	$\frac{9.2}{20}$	$\frac{9.6}{3}$	10.2	$\frac{11.0}{5}$	$\frac{11.5}{20}$	$\frac{12.2}{40}$
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$\frac{5.8}{40}$	$\frac{7.6}{20}$	$\frac{8.4}{7}$	8.8	$\frac{9.8}{5}$	$\frac{10.2}{20}$	$\frac{11.7}{40}$
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$\frac{5.0}{40}$	$\frac{5.6}{14}$	$\frac{6.7}{4}$	6.5	$\frac{8.0}{20}$	$\frac{10.2}{40}$
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$\frac{9.8}{40}$	$\frac{5.5}{17}$	$\frac{6.6}{4}$	6.3	$\frac{7.2}{8}$	$\frac{7.5}{23}$	$\frac{8.6}{40}$
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$\frac{9.6}{40}$	$\frac{10.2}{20}$	10.0	$\frac{11.2}{20}$	$\frac{11.4}{40}$
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$\frac{11.2}{40}$	$\frac{11.8}{20}$	12.2	$\frac{12.4}{20}$	$\frac{12.7}{40}$
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$\frac{9.7}{40}$	$\frac{10.0}{20}$	10.4	$\frac{10.6}{20}$	$\frac{10.8}{40}$
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$\frac{9.4}{40}$	10.0	$\frac{10.5}{40}$
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Spike in T. P. 34' RT. STA. 26+05

STA.	+	H. I.	-	Elev.
B.M.	166	985 <sup>12</sup> ✓		983 <sup>46</sup>

26+44				80.7
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26+48				79.5
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26+58				79.7
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27				77.7
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+50				76.0
-----	--	--	--	------

28				74.5
----	--	--	--	------

+50				73.9
-----	--	--	--	------

29				73.8
----	--	--	--	------

+50				74.2
-----	--	--	--	------

30				75.5
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T.P.		885		976 <sup>23</sup> ✓
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- L -

- R -

17

S.P.K. IN T.P. 34' left STA. 26+05

$\frac{4.0}{40}$

$\frac{4.3}{20}$

4.7

$\frac{4.6}{20}$

$\frac{4.9}{40}$

$\frac{5.1}{40}$

$\frac{5.3}{20}$

5.6

$\frac{5.9}{20}$

$\frac{5.9}{40}$

$\frac{5.1}{40}$

$\frac{5.3}{20}$

5.7

$\frac{4.9}{3}$

$\frac{4.9}{20}$

$\frac{4.9}{40}$

$\frac{6.8}{40}$

$\frac{7.1}{20}$

$\frac{7.1}{6}$

7.4

$\frac{7.1}{6}$

$\frac{7.1}{22}$

$\frac{7.4}{40}$

$\frac{8.6}{40}$

$\frac{8.7}{20}$

9.1

$\frac{9.0}{7}$

$\frac{9.0}{22}$

$\frac{9.0}{40}$

$\frac{9.3}{40}$

$\frac{9.7}{20}$

$\frac{10.1}{6}$

10.6

$\frac{10.2}{6}$

$\frac{10.4}{22}$

$\frac{10.6}{40}$

$\frac{10.5}{40}$

$\frac{10.8}{22}$

$\frac{10.9}{4}$

11.2

$\frac{11.0}{10}$

$\frac{11.2}{27}$

$\frac{11.4}{40}$

$\frac{11.0}{40}$

$\frac{11.0}{20}$

11.3

$\frac{11.0}{8}$

$\frac{11.4}{25}$

$\frac{11.5}{40}$

$\frac{10.6}{40}$

$\frac{10.6}{25}$

$\frac{10.6}{9}$

10.9

$\frac{10.7}{8}$

$\frac{10.9}{28}$

$\frac{11.0}{40}$

$\frac{9.6}{40}$

$\frac{9.3}{10}$

$\frac{9.8}{2}$

9.6

$\frac{9.1}{4}$

$\frac{8.8}{20}$

$\frac{8.8}{40}$

TOP STAKE STA. 30+00

STA.	+	H.I. ✓ -	Elev.
T. P.	877	985 <sup>04</sup>	976 <sup>27</sup>

30+50			76.9
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31+00			78.2
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+35			78.8
-----	--	--	------

+50			78.5
-----	--	--	------

32			76.8
----	--	--	------

+50			76.8
-----	--	--	------

33			76.1
----	--	--	------

+50			76.8
-----	--	--	------

34			79.0
----	--	--	------

+50			81.7
-----	--	--	------

35			82.4
----	--	--	------

+50			83.5
-----	--	--	------

$\frac{8.9}{90}$	$\frac{8.9}{25}$	$\frac{8.0}{10}$	$\frac{8.9}{2}$	8.1	$\frac{7.8}{4}$	$\frac{6.8}{20}$	$\frac{6.2}{40}$
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$\frac{8.3}{90}$	$\frac{7.6}{20}$	$\frac{7.1}{3}$	6.8	$\frac{6.9}{4}$	$\frac{5.9}{20}$	$\frac{4.6}{40}$
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$\frac{7.9}{40}$		$\frac{6.7}{13}$	6.2	$\frac{5.7}{4}$	$\frac{4.7}{20}$	$\frac{4.0}{40}$
------------------	--	------------------	-----	-----------------	------------------	------------------

$\frac{7.8}{40}$	$\frac{7.2}{25}$	$\frac{6.6}{12}$	6.5	$\frac{6.0}{4}$	$\frac{4.8}{22}$	$\frac{4.0}{40}$
------------------	------------------	------------------	-----	-----------------	------------------	------------------

$\frac{8.9}{90}$	$\frac{8.2}{25}$	$\frac{8.1}{10}$	8.2	$\frac{7.6}{4}$	$\frac{6.2}{22}$	$\frac{5.0}{40}$
------------------	------------------	------------------	-----	-----------------	------------------	------------------

$\frac{8.7}{40}$		$\frac{8.7}{20}$	8.2	$\frac{9.0}{5}$	$\frac{8.4}{20}$	$\frac{7.7}{40}$
------------------	--	------------------	-----	-----------------	------------------	------------------

$\frac{8.5}{40}$		$\frac{8.5}{20}$	8.9		$\frac{9.3}{20}$	$\frac{9.3}{40}$
------------------	--	------------------	-----	--	------------------	------------------

$\frac{8.3}{40}$		$\frac{8.2}{20}$	8.2		$\frac{8.6}{20}$	$\frac{8.5}{40}$
------------------	--	------------------	-----	--	------------------	------------------

$\frac{5.9}{40}$	$\frac{6.2}{23}$	$\frac{6.6}{8}$	6.0	$\frac{6.7}{5}$	$\frac{5.8}{15}$	$\frac{6.8}{40}$
------------------	------------------	-----------------	-----	-----------------	------------------	------------------

$\frac{4.7}{40}$	$\frac{4.3}{22}$	$\frac{4.1}{5}$	3.3	$\frac{4.0}{10}$	$\frac{3.4}{23}$	$\frac{3.1}{40}$
------------------	------------------	-----------------	-----	------------------	------------------	------------------

$\frac{3.7}{40}$	$\frac{3.0}{22}$	$\frac{3.9}{10}$	2.6	$\frac{2.8}{10}$	$\frac{2.6}{22}$	$\frac{2.9}{40}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{1.2}{40}$		$\frac{1.0}{20}$	1.5	$\frac{2.5}{7}$	$\frac{2.7}{14}$	$\frac{4.8}{40}$
------------------	--	------------------	-----	-----------------	------------------	------------------

STA. + H.I. ✓ EIV.

985.04 ✓

35+85

83.4

36

82.3

+25

79.5

+50

75.8 ✓

T. P. 0 27

974.65 ✓ 1066

974.38 ✓

36+80

72.5

37

71.2  
Edge of Pot Hole on  $\phi$

+50

69.6

38

69.2

+50

69.3

39

69.9

+50

70.4  
Edge of Pot Hole on  $\phi$

T. P.

103

973.62 ✓

-L-

-R-

19

$\frac{1.0}{40}$	$\frac{1.0}{14}$	$\frac{2.0}{6}$	16	$\frac{2.8}{6}$	$\frac{3.8}{21}$	$\frac{5.2}{40}$
------------------	------------------	-----------------	----	-----------------	------------------	------------------

$\frac{1.4}{40}$	$\frac{2.0}{15}$	$\frac{3.0}{5}$	27	$\frac{4.0}{6}$	$\frac{4.7}{22}$	$\frac{5.4}{40}$
------------------	------------------	-----------------	----	-----------------	------------------	------------------

$\frac{3.8}{40}$	$\frac{4.7}{28}$	$\frac{4.6}{11}$	$\frac{5.9}{4}$	5.5	$\frac{6.7}{8}$	$\frac{6.6}{23}$	$\frac{6.3}{40}$
------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------

$\frac{7.6}{40}$	$\frac{8.6}{20}$	$\frac{8.6}{8}$	$\frac{9.6}{4}$	9.2	$\frac{10.3}{12}$	$\frac{9.6}{25}$	$\frac{9.0}{40}$
------------------	------------------	-----------------	-----------------	-----	-------------------	------------------	------------------

$\frac{+0.2}{40}$	$\frac{0.4}{20}$	$\frac{1.4}{8}$	$\frac{2.7}{3}$	2.2	$\frac{2.7}{15}$	$\frac{1.7}{40}$
-------------------	------------------	-----------------	-----------------	-----	------------------	------------------

$\frac{3.5}{40}$  Rt  $\frac{3.7}{20}$

3.5

$\frac{3.3}{20}$  Lt  $\frac{2.0}{40}$

$\frac{4.6}{40}$

$\frac{4.6}{20}$

5.1

$\frac{4.8}{20}$

$\frac{4.8}{40}$

$\frac{4.4}{40}$

$\frac{5.3}{20}$

5.5

$\frac{5.0}{5}$

$\frac{5.2}{20}$

$\frac{5.3}{40}$

$\frac{5.0}{40}$

$\frac{5.4}{20}$

5.4

$\frac{4.9}{20}$

$\frac{4.8}{40}$

$\frac{5.3}{40}$

$\frac{5.3}{20}$

4.8

$\frac{4.6}{20}$

$\frac{4.0}{40}$

$\frac{5.2}{40}$

$\frac{5.0}{20}$

4.3

$\frac{3.6}{25}$

$\frac{3.2}{40}$

STA + H.I. ✓ - E.I.V.  
406 977<sup>68</sup> 973<sup>62</sup>  
40+00 72.3

+50 72.8

T.P. 382 ✓ 977<sup>44</sup> 406 ✓ 973<sup>62</sup>

41 73.8

+50 74.7

42 73.9

+50 72.7

43 71.3

+50 69.9

44 69.2

+35 69.2

+50 69.7

-L-

-R-

$$\frac{7.2}{40}$$

$$\frac{6.8}{20}$$

5.4

$$\frac{4.6}{15}$$

$$\frac{4.1}{20}$$

$$\frac{4.7}{22}$$

$$\frac{4.6}{40}$$

$$\frac{5.5}{40}$$

$$\frac{5.1}{20}$$

4.9

$$\frac{4.8}{8}$$

$$\frac{4.2}{9}$$

$$\frac{5.2}{13}$$

$$\frac{4.7}{40}$$

Top of STAKE.

$$\frac{5.3}{40}$$

$$\frac{5.2}{18}$$

$$\frac{4.5}{9}$$

$$\frac{4.2}{2}$$

3.6

$$\frac{4.4}{3}$$

$$\frac{4.1}{20}$$

$$\frac{4.1}{40}$$

$$\frac{3.4}{40}$$

$$\frac{2.7}{12}$$

$$\frac{2.2}{8}$$

$$\frac{3.0}{6}$$

2.7

$$\frac{3.3}{20}$$

$$\frac{3.5}{31}$$

$$\frac{4.2}{40}$$

$$\frac{4.6}{40}$$

$$\frac{4.0}{20}$$

$$\frac{3.2}{17}$$

$$\frac{3.7}{15}$$

3.5

$$\frac{3.7}{20}$$

$$\frac{4.8}{40}$$

$$\frac{7.0}{40}$$

$$\frac{6.7}{29}$$

$$\frac{5.8}{26}$$

$$\frac{6.2}{24}$$

$$\frac{5.7}{18}$$

4.7

$$\frac{4.4}{12}$$

$$\frac{4.9}{24}$$

$$\frac{5.0}{40}$$

$$\frac{8.0}{40}$$

$$\frac{7.6}{35}$$

$$\frac{7.3}{20}$$

6.1

$$\frac{5.0}{20}$$

$$\frac{4.5}{40}$$

$$\frac{9.1}{40}$$

$$\frac{8.7}{22}$$

$$\frac{8.0}{14}$$

7.5

$$\frac{6.3}{22}$$

$$\frac{6.7}{25}$$

$$\frac{5.9}{40}$$

$$\frac{9.5}{40}$$

$$\frac{9.0}{25}$$

$$\frac{8.8}{11}$$

$$\frac{8.2}{6}$$

8.2

$$\frac{7.6}{14}$$

$$\frac{8.2}{16}$$

$$\frac{6.2}{40}$$

$$\frac{8.8}{40}$$

$$\frac{9.0}{21}$$

$$\frac{8.0}{13}$$

$$\frac{8.5}{8}$$

8.2

$$\frac{8.0}{10}$$

$$\frac{7.0}{25}$$

$$\frac{5.8}{40}$$

$$\frac{7.3}{40}$$

$$\frac{7.8}{20}$$

7.7

$$\frac{7.7}{6}$$

$$\frac{6.4}{22}$$

$$\frac{5.4}{40}$$

STA. + H.I. ✓ - EIV.

977<sup>44</sup>

44+70 70.5

45 72.2

+50 71.2

46 71.6

150 ✓ 70.9

T.P. 798 977<sup>47</sup> 795 969<sup>49</sup> ✓

47 Begin Ditch left. <sup>69.0</sup>

47+05 6" tile drain 12' left ELEV. 967<sup>57</sup>

+50 70.1

48 69.7

+50 69.7

49 69.9

+50 69.9

- L -

- R -

$\frac{7.0}{40}$        $\frac{7.6}{20}$       69       $\frac{5.5}{23}$        $\frac{5.1}{40}$

$\frac{4.9}{40}$        $\frac{5.6}{20}$       52       $\frac{5.1}{25}$        $\frac{5.1}{40}$

$\frac{2.9}{40}$        $\frac{4.6}{20}$       62       $\frac{7.3}{10}$        $\frac{7.3}{25}$        $\frac{7.9}{40}$

$\frac{1.2}{40}$        $\frac{3.7}{20}$       58       $\frac{6.9}{14}$        $\frac{7.9}{27}$        $\frac{8.0}{40}$

$\frac{4.7}{40}$        $\frac{5.8}{22}$       65       $\frac{7.1}{20}$        $\frac{7.8}{40}$

TOP STAKE STA. 47100

$\frac{7.3}{40}$        $\frac{8.6}{15}$        $\frac{9.3}{13}$        $\frac{8.3}{12}$       84       $\frac{8.6}{25}$        $\frac{8.4}{40}$

67.57

990 Flow line

$\frac{8.2}{40}$        $\frac{8.2}{29}$        $\frac{9.0}{21}$        $\frac{9.8}{19}$        $\frac{9.8}{17}$        $\frac{8.6}{16}$        $\frac{7.6}{9}$       74       $\frac{7.7}{25}$        $\frac{8.0}{40}$

$\frac{8.5}{40}$        $\frac{8.5}{22}$        $\frac{10.0}{19}$        $\frac{10.0}{18}$        $\frac{8.6}{16}$        $\frac{8.1}{13}$       78       $\frac{8.0}{23}$        $\frac{7.5}{40}$

$\frac{7.8}{40}$        $\frac{8.7}{24}$        $\frac{10.0}{21}$        $\frac{10.0}{18}$        $\frac{8.0}{16}$       78       $\frac{7.5}{20}$        $\frac{6.8}{40}$

$\frac{8.0}{40}$        $\frac{8.2}{23}$        $\frac{9.2}{22}$        $\frac{9.6}{18}$        $\frac{8.4}{16}$       76       $\frac{7.4}{14}$        $\frac{5.8}{28}$        $\frac{5.2}{40}$

$\frac{8.0}{40}$        $\frac{8.4}{23}$        $\frac{9.7}{22}$        $\frac{9.7}{19}$        $\frac{8.1}{16}$       76       $\frac{7.3}{14}$        $\frac{5.8}{28}$        $\frac{5.3}{40}$

STA + H.I. ✓ - EIV  
977<sup>97</sup>

50 69.5

50+44 Beg. 6" Tile Drain. Flowline 19' left

50+50 68.5  
END of Ditch left.

51 69.2

+50 71.4

+58 72.7

+85 74.1

52 74.1 ✓  
T. P. 4<sup>38</sup> 978<sup>92</sup> 2<sup>93</sup> 974<sup>54</sup>

+25 73.6

+30 72.8

+35 72.5

+39 74.1

-L-

-R-

22

$$\frac{8.3}{40} \quad \frac{9.1}{27} \quad \frac{9.4}{25} \quad \frac{10.0}{19} \quad \frac{8.5}{15}$$

$$8.0 \quad \frac{8.1}{15} \quad \frac{7.6}{20} \quad \frac{7.4}{40}$$

990

EIV. 96757 ✓

$$\frac{8.5}{40} \quad \frac{8.4}{27} \quad \frac{9.3}{24} \quad \frac{9.3}{19} \quad \frac{8.8}{17}$$

90

$$\frac{8.4}{25} \quad \frac{8.1}{40}$$

$$\frac{8.1}{40}$$

$$\frac{8.3}{20}$$

83

$$\frac{8.3}{20}$$

$$\frac{8.2}{40}$$

$$\frac{5.8}{40}$$

$$\frac{5.8}{20}$$

61

$$\frac{6.1}{20}$$

$$\frac{5.8}{40}$$

$$\frac{4.3}{40}$$

$$\frac{4.1}{20}$$

48

$$\frac{5.0}{20}$$

$$\frac{5.0}{40}$$

$$\frac{3.2}{40}$$

$$\frac{3.0}{20}$$

34

$$\frac{4.0}{20}$$

$$\frac{4.7}{40}$$

$$\frac{3.4}{40}$$

$$\frac{3.1}{20}$$

34

$$\frac{4.0}{20}$$

$$\frac{4.9}{40}$$

$$\frac{5.1}{40}$$

$$\frac{5.1}{22}$$

52

$$\frac{5.5}{16}$$

$$\frac{6.7}{40}$$

$$\frac{6.0}{40}$$

$$\frac{6.3}{20}$$

61

$$\frac{6.4}{20}$$

$$\frac{2.0}{40}$$

$$\frac{6.1}{40}$$

$$\frac{5.8}{20}$$

64

$$\frac{6.5}{20}$$

$$\frac{6.8}{40}$$

$$\frac{4.8}{40}$$

$$\frac{4.8}{20}$$

48

$$\frac{5.0}{20}$$

$$\frac{4.9}{40}$$

STA + H.I. - Ely.

978.92

52+43 Edge of Pavement. 73.83

52+53 C Co. Rd. B. 73.86

B.M.

$$5 \overset{06}{\underline{\quad}} \overset{\checkmark}{973 \overset{86}{\underline{\quad}}} = 973 \overset{85}{\underline{\quad}}$$

-L-

-R-

$$\frac{487}{40}$$

$$\frac{505}{20}$$

$$509$$

$$\frac{507}{20}$$

$$\frac{502}{40}$$

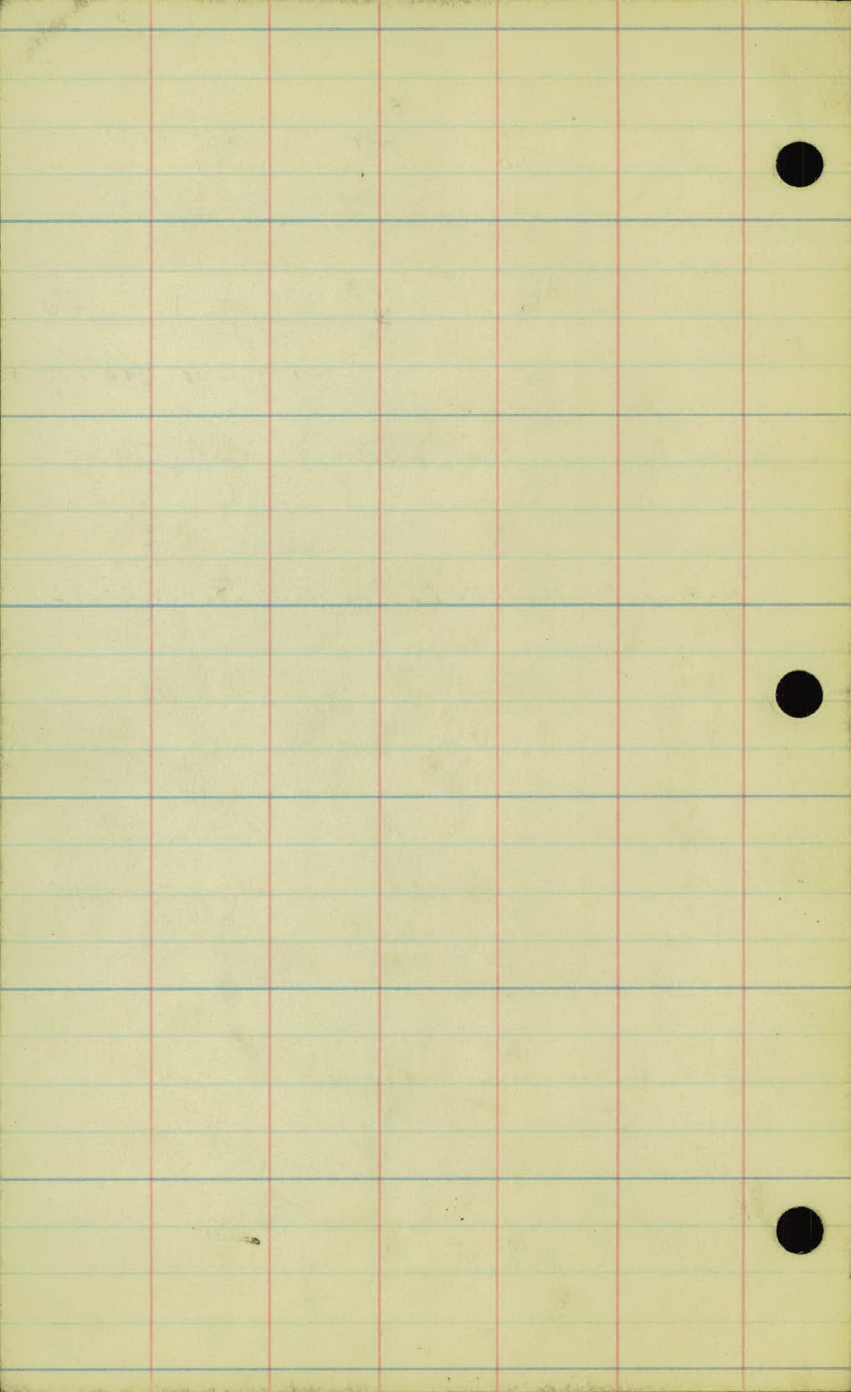
$$\frac{479}{40}$$

$$506$$

$$\frac{492}{40}$$

S.W. COR. MONT.

S.W. COR. MONT. & Co. RD. B. & N.B. RD.



4 Levels

N. & S. Line Thru Cen. Sec. 16

STA	T	H.I. / -	ROD	ELEV.
B.M.	6.42	972.90		966.48
0+00		↳ Larp. Ave	6.4	66.5
1			6.1	66.8
2			5.8	67.1
3			5.4	67.5
4			3.8	69.1
5			4.8	68.1
6			5.3	67.6
7			4.1	68.8
8		✓	2.4	70.5
T.P.	5.94	977.39	1.45	971.45
9			6.0	71.4
10			5.9	71.5
11			5.2	72.2
12			3.6	73.8
13		✓	2.4	75.0
T.P.	2.87	983.80	1.46	975.93
14			8.3	75.5
15			7.1	76.7
16			6.1	77.7
17			5.4	78.4
18			3.7	80.1
19		✓	1.4	82.4
T.P.	9.24	991.48	1.56	982.24
20			7.2	84.3
21			6.5	85.0

Top of Bolt -  $\frac{1}{2}$  Larp. Ave.

6.4

6.1

5.8

5.4

3.8

4.8

5.3

4.1

2.4

6.0

5.9

5.2

3.6

2.4

8.3

7.1

6.1

5.4

3.7

1.4

7.2

6.5

STN T HIJ - ROD ELEV

991.48

22				4.8	86.6
23				5.6	85.9
24				8.2	83.3
25				10.8	80.7
26				7.2	84.3
+08				7.1	84.4
+19				12.8	78.7
+24				11.0	80.5
+35				10.7	80.8
B.M.	0.38	983.84	8.02	983.46	
27				6.0	77.8
28				9.0	74.8
29				10.0	73.8
30				8.5	75.3
31				6.0	77.8
T.P.	6.96	984.74	6.06	977.78	
32				7.8	76.9
33				8.4	76.3
34				5.6	79.1
35				2.2	82.5
36				2.0	82.7
37				13.4	71.1
T.P.	6.26	979.20	11.80	972.94	
38				9.8	69.4
39				9.5	69.7
40				7.0	72.2
41				5.9	73.3

± Co. Rd. A = ✓

?

4.8

5.6

8.2

12.8

7.2

7.1

12.8

11.0

10.7

Spt. in T.P. 34' Rt. Sta. 26+05

6.0

9.0

10.0

8.5

6.0

7.8

8.4

5.6

2.2

2.0

13.6

9.8

9.5

7.0

5.9

979.20 ✓

42				5.2	74.0
43				8.0	71.2
44				10.0	69.2
45				7.0 ✓	72.2
T.P.	4.56	977.29	6.47	972.73	
46				5.5	71.8
47				8.0	69.3
48				7.7	69.6
49				7.5	69.8
50				7.7	69.6
51				8.2	69.1
52				3.3	74.0
455	E Co. Rd. "B"			3.4 ✓	73.9
B.M.			3.44	973.85	

5.2

8.0

10.0

7.0

5.5

8.0

7.7

7.5

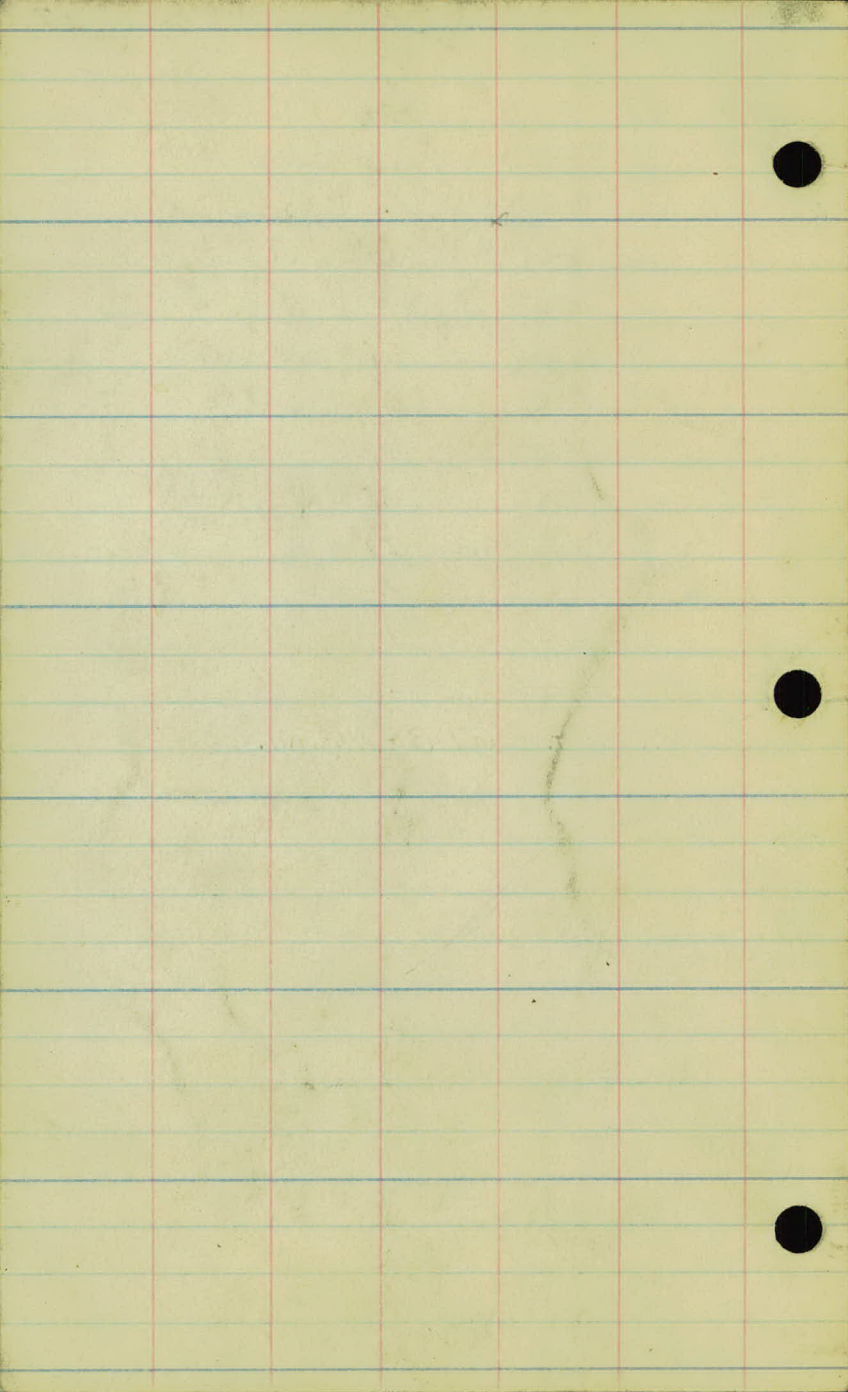
7.7

8.2

3.3

3.4

S.W. Cor. Mont. Co. Rd B & N.B. Rd.



Topog.  
Borrow Pit.  
Rd. #16

7

6

5

4

3

2

1

0+00

1-17-33

+62 - T.P. 26'

+70 - P.P. 23'

F. 29'

+22 - T.P. 26'

+70 - P.P. 22'

F. 29'

+60 - Tr. 35'

+32 - Tr. 35'

+03 - Tr. 36'

+92 - T.P. 27

+76 - Tr. 36'

+48 - Tr. 36'

F. 29'

+71 - P.P. 23'

+52 - P.P. 23'

F. 28'

+97 - Tr. 35'

+69 - Tr. 35'

+58 - T.P. 27'

+43 - Tr. 33'

+21 - P.P. 40'

+00 - & Dr

+71 - P.P. 24'

F. 28'

+92 - F. Int.

+70 - P.P. 24'

+23 - Tr. 18'

F. 30'

+48 - P.P. 24'

+38 - F.C. 30'

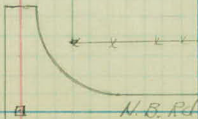
N.B. Rd

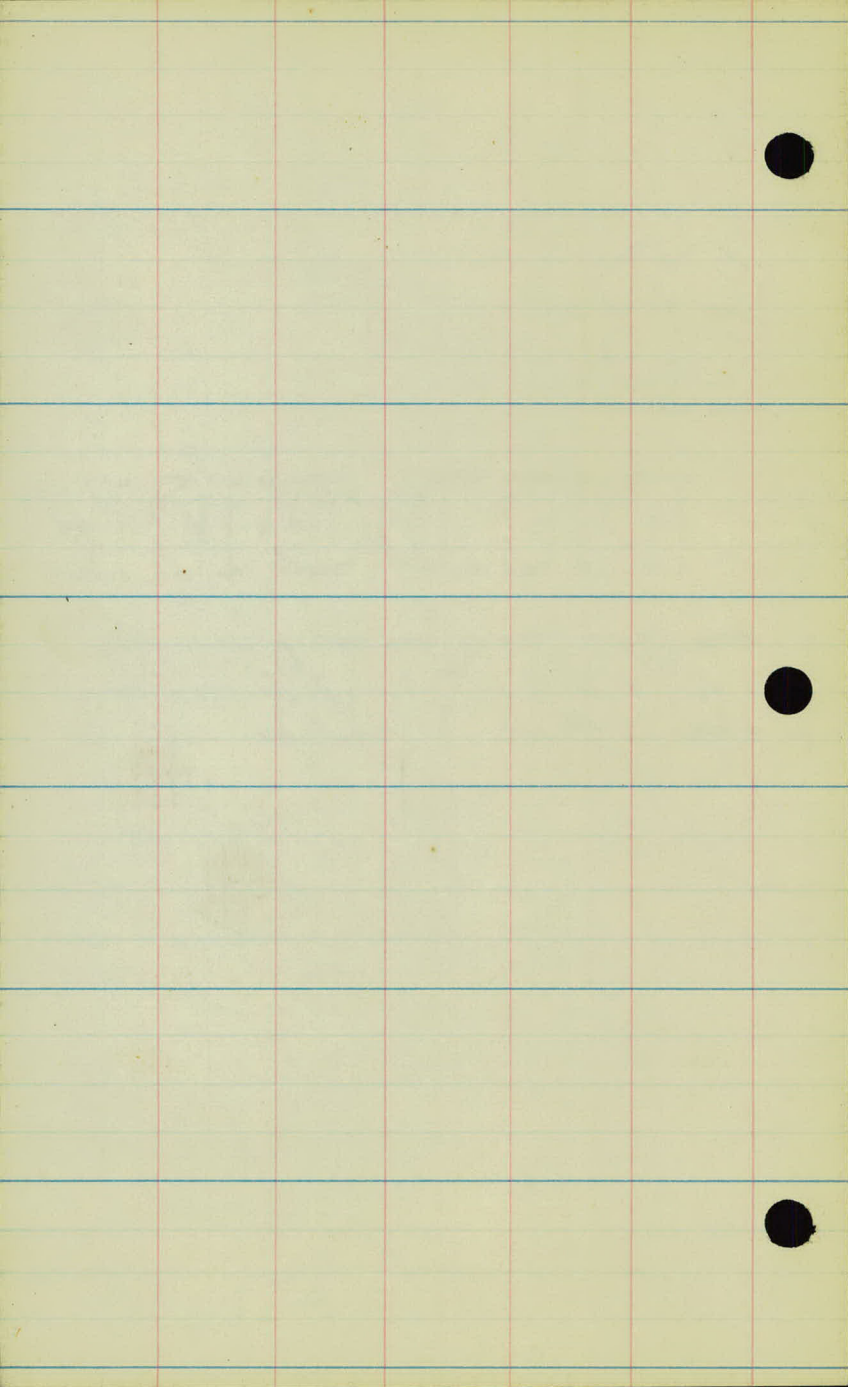
Turkey Farm

& Co. Rd. B

Cultivated

Wooded Pasture





X-Sections

Borrow

Rd. #16

B.M. 9.60 983.45 973.85

0+00

+55 Edge of Pavement

1

2

T.P. 10.44 991.02 2.87 980.58

+21

+50

3

+50

4

+25

+50

T.P. 3.96 983.91 11.07 979.95

5

S. W. Cor. Mont. Co. Rd. "B" + N. B. Rd.

9.6

9.2

7.8

$\frac{1.5}{4.5}$	$\frac{3.0}{17}$	3.3	$\frac{3.8}{13}$	$\frac{5.6}{16}$	$\frac{7.3}{20}$	$\frac{8.7}{26}$	$\frac{9.0}{31}$
-------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.1}{4.5}$	$\frac{5.8}{3.5}$	$\frac{9.1}{2.5}$	$\frac{9.7}{1.9}$	$\frac{10.2}{1.5}$	10.0	$\frac{10.6}{1.3}$	$\frac{11.7}{1.6}$	$\frac{12.9}{2.1}$	$\frac{14.6}{2.9}$
-------------------	-------------------	-------------------	-------------------	--------------------	------	--------------------	--------------------	--------------------	--------------------

$\frac{3.6}{4.5}$	$\frac{3.1}{4.0}$	$\frac{3.8}{3.3}$	$\frac{8.2}{2.3}$	$\frac{9.7}{2.0}$	$\frac{9.8}{1.7}$	$\frac{9.4}{1.4}$	9.0	$\frac{9.5}{1.2}$	$\frac{10.1}{1.3}$	$\frac{10.4}{1.5}$	$\frac{10.4}{1.7}$	$\frac{9.1}{1.9}$	$\frac{9.7}{2.3}$	$\frac{12.2}{3.2}$
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$\frac{2.3}{4.5}$	$\frac{1.9}{3.9}$	$\frac{2.4}{3.4}$	$\frac{7.8}{2.3}$	$\frac{9.2}{2.0}$	$\frac{9.1}{1.7}$	$\frac{8.7}{1.4}$	8.2	$\frac{9.0}{1.3}$	$\frac{8.6}{1.6}$	$\frac{7.6}{1.8}$	$\frac{4.4}{2.1}$	$\frac{5.3}{3.1}$	$\frac{7.5}{4.5}$
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$\frac{3.8}{4.5}$	$\frac{4.6}{3.7}$	$\frac{7.3}{2.5}$	$\frac{9.2}{2.3}$	$\frac{9.8}{2.0}$	$\frac{9.9}{1.7}$	$\frac{9.0}{1.4}$	8.5	$\frac{8.9}{1.2}$	$\frac{9.1}{1.5}$	$\frac{8.8}{1.7}$	$\frac{4.6}{2.4}$	$\frac{5.9}{4.5}$
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$\frac{6.2}{4.5}$	$\frac{6.5}{3.7}$	$\frac{7.7}{3.2}$	$\frac{8.2}{2.6}$	$\frac{10.8}{2.2}$	$\frac{11.0}{1.8}$	$\frac{10.9}{1.6}$	$\frac{10.1}{1.5}$	9.5	$\frac{9.9}{1.1}$	$\frac{10.4}{1.3}$	$\frac{11.0}{1.5}$	$\frac{9.6}{1.8}$	$\frac{9.2}{2.1}$	$\frac{9.2}{2.9}$	$\frac{8.2}{4.5}$
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$\frac{7.2}{4.5}$	$\frac{7.6}{3.6}$	$\frac{9.0}{2.5}$	$\frac{11.2}{2.2}$	$\frac{11.7}{1.8}$	$\frac{10.6}{1.4}$	10.3	$\frac{10.9}{1.3}$	$\frac{11.8}{1.6}$	$\frac{11.2}{1.7}$	$\frac{11.8}{2.7}$	$\frac{11.1}{4.5}$
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$\frac{7.7}{4.5}$	$\frac{7.9}{3.6}$	$\frac{9.7}{2.4}$	$\frac{11.9}{2.1}$	$\frac{12.1}{1.8}$	$\frac{11.5}{1.4}$	11.1	$\frac{11.5}{1.2}$	$\frac{12.3}{1.5}$	$\frac{12.3}{1.7}$	$\frac{11.9}{1.8}$	$\frac{12.0}{2.7}$	$\frac{12.2}{4.5}$
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$\frac{2.2}{4.5}$	$\frac{3.4}{2.4}$	$\frac{6.4}{1.9}$	$\frac{6.4}{1.7}$	5.8	$\frac{6.5}{1.4}$	$\frac{6.8}{1.6}$	$\frac{2.7}{2.2}$	$\frac{2.4}{2.9}$	$\frac{5.2}{4.5}$
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983.91

5+50

6

+50

7

B.M.

10.08

973.83

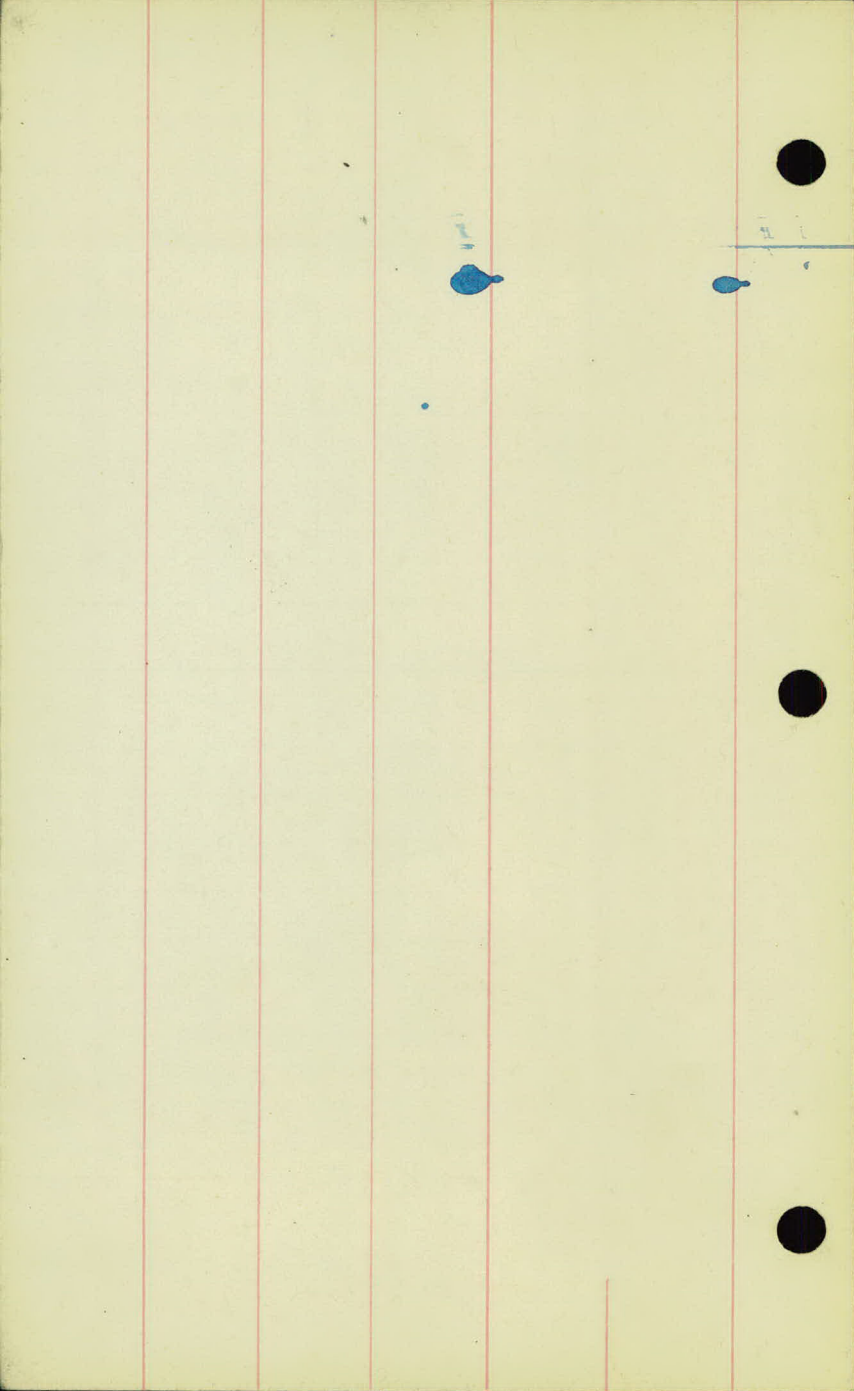
973.85

$\frac{3.0}{45}$   $\frac{2.6}{33}$   $\frac{3.6}{26}$   $\frac{7.9}{20}$   $\frac{8.4}{18}$   $\frac{8.1}{15}$  7.6  $\frac{7.9}{15}$   $\frac{3.0}{23}$   $\frac{4.3}{29}$   $\frac{7.8}{45}$

$\frac{5.3}{45}$   $\frac{4.6}{28}$   $\frac{7.9}{24}$   $\frac{10.2}{20}$   $\frac{10.4}{16}$   $\frac{9.9}{14}$  9.5  $\frac{10.0}{13}$   $\frac{10.2}{17}$   $\frac{7.0}{23}$   $\frac{9.0}{29}$   $\frac{12.9}{45}$

$\frac{10.8}{45}$   $\frac{10.7}{30}$   $\frac{11.9}{22}$   $\frac{13.0}{20}$   $\frac{12.4}{17}$   $\frac{11.7}{14}$  11.4  $\frac{12.2}{15}$   $\frac{13.8}{20}$   $\frac{16.2}{29}$

135



33-16

0+ 18" X 66 P<sub>3</sub>  
2+00 Lt. Pl. 12" X 20' C.M.

26+15 Pl. 18" P<sub>3</sub> X 42'  
28+50 Pl. 18" P<sub>3</sub> X 42'

33-33+50 Cl. & Gr. 1.

33+50 - 31? - drain 50.

37-39 Cl. 2+1-

38+50 Pl. 24" P<sub>3</sub> X 48'

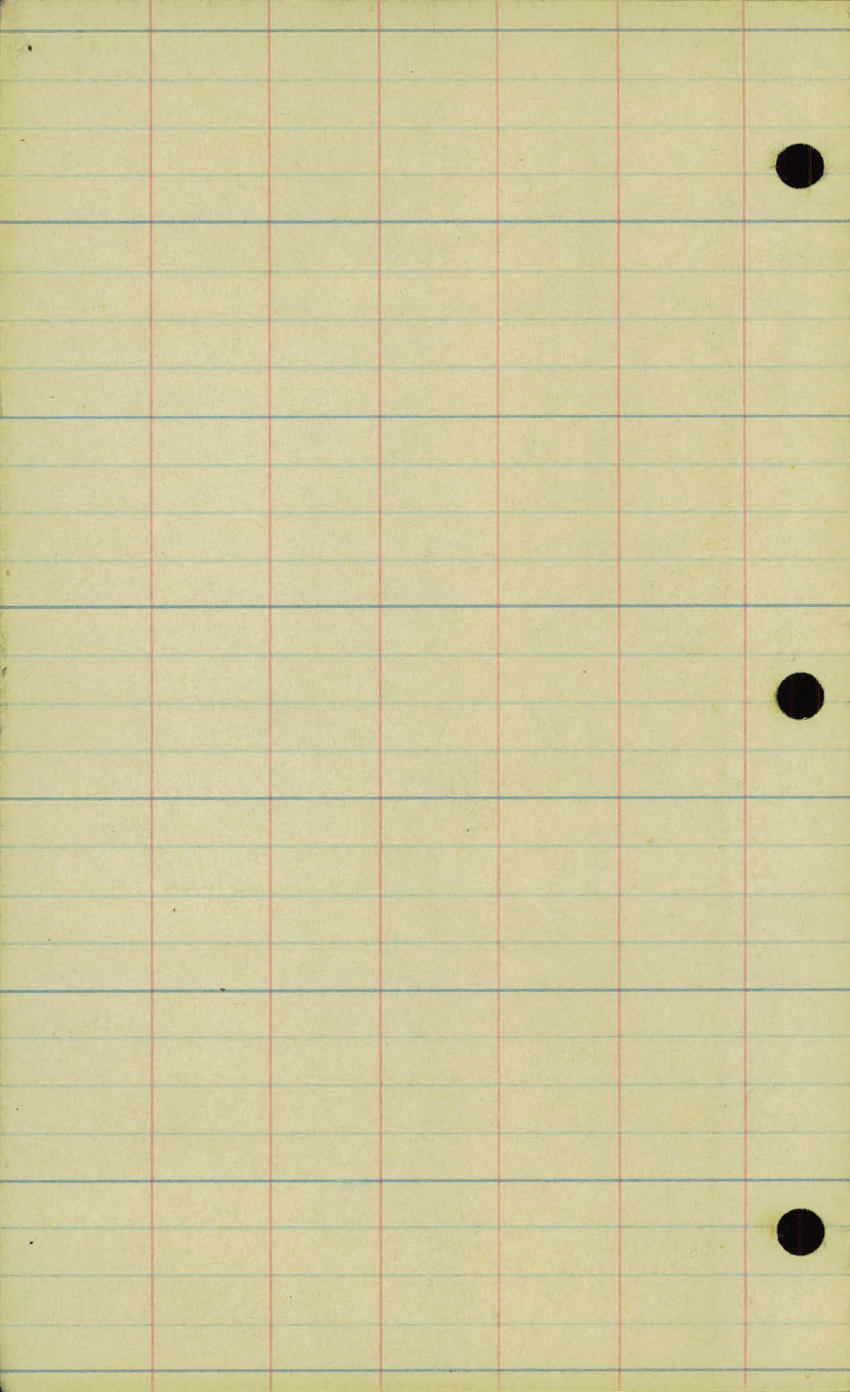
47-48+50 Cl. & Gr. 3

~~50+50  
47+50 - Pl. 18" P<sub>3</sub>~~

Raise Grade Last 400'

X Check drainage on "B"

50+50 - Pl. 18" P<sub>3</sub> X 42'



U 2528