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FIELD BOOK

300 A

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30-51

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

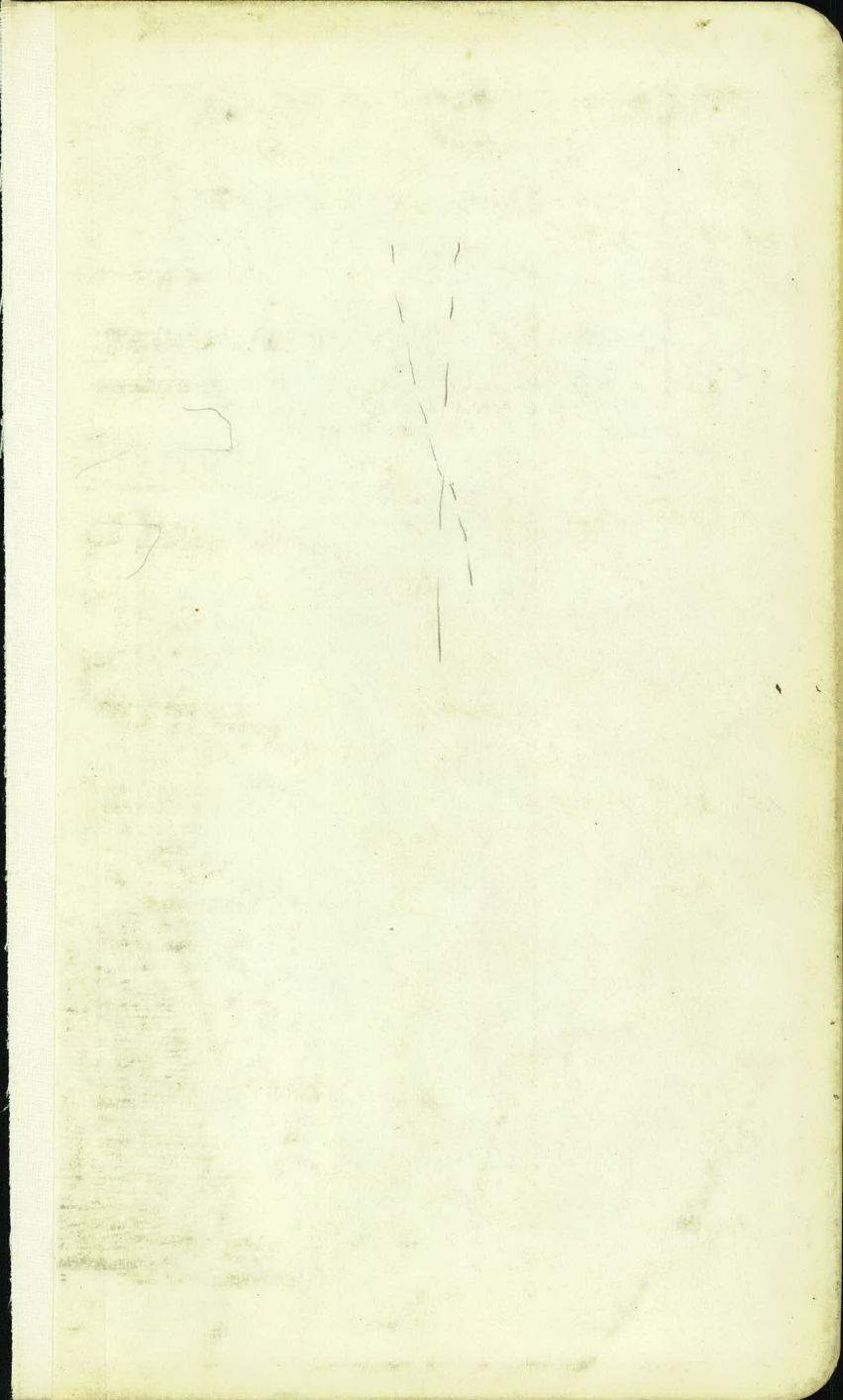
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

*"Copyright, 1895, by Keuffel & Esser Co."*

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.



90071  
885  

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99221

WESTERN AVE PROJ # 30-51.

STA TO STA	DESCRIPTION	PAGE TO	PAGE
0+00	45+14 ALIGNMENT.	1	2
0+00	45+14 ORIGINAL X SECTIONS	3	
0+00	7+00 ORIGINAL X SEC. ON WASSO BLVD. CONN.	13	
0+00	45+00 CROSS DRAINS.	79	
6+00	20+00 Grade change	71	73
0+00	53+00 FINAL X SECTIONS	21	31
	FINAL X SEC. DITCH AT STA 8+00	32	
0+00	53+00 FINAL TOPOG.	33	
	8+00 Culvert + L Ditch Elevations	74	6-3-30
=	Guard Rail =	34	

STA. POINT A LT. A. RT.

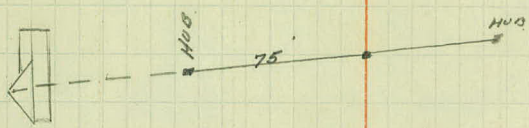
31+75<sup>0</sup> P.O.T.

26+09<sup>i</sup> P.I. 0'-02<sup>i</sup>

15+36<sup>55</sup> P.O.T.  
63.95

0+00

5-9-30



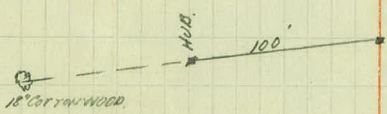
50.00  
 36.55  
 1345

BOTTOM OF CRACK  
 IN EAVE OF HOUSE.

CENTER BOLT IN X AXIS  
 OF HIGH POWER FRAME.



WESTERN AVE.



18' COTTONWOOD

NORTH



SOUTH 1/4 COR. SEC 1-29-23

STN. POINT Δ LT. Δ RT.

46+14<sup>3</sup> P.O.T.

45+14<sup>3</sup> P.O.T.

41+33<sup>8</sup> P.O.T.

40+91<sup>17</sup> P.T.

+50

40

+50

0.17

44°-53<sup>5</sup>

✓ 40°-46<sup>5</sup>

✓ 35°-46<sup>5</sup>

✓ 30°-46<sup>5</sup>

39+29<sup>1</sup> P.I.

39

+50

38

+50

37

+50

36+42<sup>25</sup> P.C.

Δ-89°-47'

✓ 25°-46<sup>5</sup>

D-20°-R.

✓ 20°-46<sup>5</sup>

T-280<sup>85</sup>

✓ 15°-46<sup>5</sup>

L-448<sup>92</sup>

✓ 10°-46<sup>5</sup>

R-287<sup>94</sup>

✓ 5°-46<sup>5</sup>

0.19

✓ 0°-46<sup>5</sup>

7.8

✓ 0°-00

5-9-30



ONASSO BLVD  
 BASE LINE

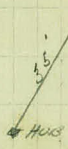
122° 08' 58"

M. COR.  
 STONE MONT.

122° 08'  
 SEMI TRM.

NAIL IN  
 18" DIA

7.75



WESTERN AVE.

STA.	+	H. I.	-	ELEV	ROD.
B.M.	0.15	925.71		919.56	
0+00.				23.5	2.2
				23.31	2.4
				23.2	2.5
1+00				22.1	3.6
				21.4	4.5
				21.1	4.6
2				20.7	5.0
				20.0	5.7
				19.6	6.1
				19.3	6.4
3					
	10.42	930.71	5.42	920.29	
				18.6	12.1
4				17.9	12.8

LT.

PT.

5-9-30

SAX IN 12" OAK 60 LT. 57A. 0730.

3.2	1.2(2.2)	0.5
53		33

4.0	3.2	2.5	2.2	1.6
53	18		16	33

6.2/9.1	9.1	8.5	7.2	8.1	3.3	9.3	6.5	0/7.3
2/-6.6	25	17	10	-0.6	11	19	33	2/-4.8

0/13.9	14.0	12.7	7.4	6.5	7.0	10.0	9.8	6/9.9
3/-10.3	33	17	7	-2.7	10	16	33	2/-6.3

0/8.5	10.0	7.4	7.2	9.2	8.1	7.5	7.6	9.1	9.5	4.7	9/7.3	0/4.7
2/-4.0	33	17	14	11	8	-3.2	13	16	21	23	1/-3.0	2/1.26

7.2	5.3	9.4	8.6	7.8	7.8	8.8	4.6	4.6
33	17	14	11		12	15	20	33

4/3.4	5.8	5.5	9.4	8.7	8.1	8.4	9.4	6.4	6.0	7/6.5
2/-0.4	33	19	15	10	3.1	11	15	19	33	2/-1.5

0/11.2	13.2	11.7	10.1	8.6	8.3	8.7	10.2	8.8	8.8	2/8.8
2/-5.3	33	26	14	8	-2.6	8	14	18	33	1/-3.1

15.8	13.4	8.5	7.8	8.3	9.5	9.6
33	13	8		9	14	33

0/14.4	14.9	12.5	7.8	7.1	7.4	8.6	8.7	1/8.7
2/-8.0	33	16	10	-0.7	10	12	33	1/-2.3

7/10.3	11.2	10.8	9.0	9.6	11.0	10.4	10.3	10.8	11.0	8.6	9.2	6/9.0
2/1.8	33	31	16	12	10	6	11.8	7	9	13	33	2/1.31

0/6.8	7.0	6.7	9.9	9.5	10.2	7.2	7.8	1/8.8
3/6.0	33	18	12	13.3	8	13	33	3/1.5/7.8

STA.	+	H.I.	-	ELEV	SP. ROD.
		930.71			
	+50			17.2 ✓	13.5
5				16.5 ✓	14.2
	+50			15.8 ✓	14.9
6				15.1 ✓	15.6
	0.65	918.67 ✓	12.09	918.02 ✓	
	+50			14.4 ✓	9.3
7				13.7 ✓	5.0
	+50			13.0 ✓	5.7
8			03.8	12.5 ✓	149.64 149
	5.35	912.24 ✓	11.78	906.89 ✓	
	+50		03.6	11.6 ✓	86.06 86
9			03.7	10.9 ✓	85.13 85
	+50		03.8	10.4 ✓	84.18 84
10		15.1	03.9	10.4 ✓	83.18 83

LT.

RT

5-9-30

(12.5)

$\frac{0}{5} \frac{2}{172}$	$\frac{6}{55}$	$\frac{6}{53}$	$\frac{6}{19}$	$\frac{6}{14}$	$\frac{6}{10}$	$\frac{6}{14.4}$	$\frac{6}{10}$	$\frac{6}{11}$	$\frac{6}{16}$	$\frac{6}{21}$	$\frac{6}{33}$	$\frac{6}{35}$	$\frac{6}{173}$
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(14.7)

$\frac{0}{5} \frac{4}{101}$	$\frac{4}{35}$	$\frac{4}{33}$	$\frac{4}{18}$	$\frac{4}{14}$	$\frac{4}{12}$	$\frac{4}{15.2}$	$\frac{4}{8}$	$\frac{4}{11}$	$\frac{4}{20}$	$\frac{4}{33}$	$\frac{4}{35}$	$\frac{4}{179}$
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(14)

$\frac{0}{5} \frac{2}{128}$	$\frac{2}{35}$	$\frac{2}{33}$	$\frac{2}{19}$	$\frac{2}{12}$	$\frac{2}{15.6}$	$\frac{2}{7}$	$\frac{2}{10}$	$\frac{2}{18}$	$\frac{2}{33}$	$\frac{2}{35}$	$\frac{2}{176}$
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(150)

$\frac{0}{5} \frac{7}{182}$	$\frac{7}{33}$	$\frac{7}{33}$	$\frac{7}{20}$	$\frac{7}{18}$	$\frac{7}{14}$	$\frac{7}{13}$	$\frac{7}{13.8}$	$\frac{7}{7}$	$\frac{7}{8}$	$\frac{7}{14}$	$\frac{7}{33}$	$\frac{7}{150}$
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(4.3)

$\frac{0}{5} \frac{1}{130}$	$\frac{1}{33}$	$\frac{1}{21}$	$\frac{1}{17}$	$\frac{1}{15}$	$\frac{1}{5}$	$\frac{1}{11.9}$	$\frac{1}{4}$	$\frac{1}{8}$	$\frac{1}{11}$	$\frac{1}{13}$	$\frac{1}{33}$	$\frac{1}{119}$
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(50)

$\frac{2}{5} \frac{7}{21}$	$\frac{7}{33}$	$\frac{7}{24}$	$\frac{7}{16}$	$\frac{7}{12}$	$\frac{7}{10.4}$	$\frac{7}{10}$	$\frac{7}{33}$	$\frac{7}{2}$	$\frac{7}{10}$	$\frac{7}{10}$
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(57)

$\frac{5}{2} \frac{2}{63}$	$\frac{2}{33}$	$\frac{2}{16}$	$\frac{2}{12}$	$\frac{2}{5.1}$	$\frac{2}{3}$	$\frac{2}{6}$	$\frac{2}{24}$	$\frac{2}{33}$	$\frac{2}{5.2}$
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(64)

$\frac{5}{5} \frac{1}{118}$	$\frac{1}{119}$	$\frac{1}{66}$	$\frac{1}{37}$	$\frac{1}{23}$	$\frac{1}{16}$	$\frac{1}{12}$	$\frac{1}{4.8}$	$\frac{1}{4}$	$\frac{1}{6}$	$\frac{1}{15}$	$\frac{1}{33}$	$\frac{1}{33}$	$\frac{1}{26}$	$\frac{1}{124}$	$\frac{1}{126}$
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(80)

$\frac{4}{5} \frac{7}{119}$	$\frac{7}{116}$	$\frac{7}{64}$	$\frac{7}{37}$	$\frac{7}{27}$	$\frac{7}{26}$	$\frac{7}{15}$	$\frac{7}{13}$	$\frac{7}{5.8}$	$\frac{7}{4}$	$\frac{7}{6}$	$\frac{7}{9}$	$\frac{7}{10}$	$\frac{7}{13}$	$\frac{7}{36}$	$\frac{7}{42}$	$\frac{7}{118}$	$\frac{7}{120}$
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(12)

$\frac{4}{5} \frac{7}{114}$	$\frac{7}{111}$	$\frac{7}{61}$	$\frac{7}{37}$	$\frac{7}{25}$	$\frac{7}{24}$	$\frac{7}{18}$	$\frac{7}{14}$	$\frac{7}{13}$	$\frac{7}{6.1}$	$\frac{7}{3}$	$\frac{7}{4}$	$\frac{7}{7}$	$\frac{7}{13}$	$\frac{7}{14}$	$\frac{7}{37}$	$\frac{7}{59}$	$\frac{7}{113}$	$\frac{7}{117}$
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(13)

$\frac{0}{5} \frac{7}{110}$	$\frac{7}{108}$	$\frac{7}{59}$	$\frac{7}{37}$	$\frac{7}{24}$	$\frac{7}{23}$	$\frac{7}{18}$	$\frac{7}{14}$	$\frac{7}{12}$	$\frac{7}{15.4}$	$\frac{7}{4}$	$\frac{7}{6}$	$\frac{7}{10}$	$\frac{7}{14}$	$\frac{7}{15}$	$\frac{7}{18}$	$\frac{7}{37}$	$\frac{7}{54}$	$\frac{7}{111}$	$\frac{7}{114}$
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(16)

$\frac{4}{5} \frac{7}{114}$	$\frac{7}{112}$	$\frac{7}{56}$	$\frac{7}{37}$	$\frac{7}{21}$	$\frac{7}{20}$	$\frac{7}{17}$	$\frac{7}{15}$	$\frac{7}{14}$	$\frac{7}{12}$	$\frac{7}{5.3}$	$\frac{7}{6}$	$\frac{7}{7}$	$\frac{7}{16}$	$\frac{7}{17}$	$\frac{7}{37}$	$\frac{7}{50}$	$\frac{7}{115}$	$\frac{7}{117}$
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STA	T	H.I.	-	ELEV	OR. ROD
		912.24			
	+50		04.0	10.9 ✓	82 13 82
	9.98	918.22 ✓	4.00	908.24 ✓	
11				11.8	64
	+50			13.3 ✓	4.9
12				15.1 ✓	3.1
	9.99	927.93 ✓	0.28	917.94 ✓	
12				15.1 ✓	128
	+50			17.2 ✓	10.9
13				19.3 ✓	8.6
	+50			21.4 ✓	6.5
14				23.5 ✓	4.4
	+50			25.4 ✓	2.3
	8.86	935.37 ✓	1.42	926.51 ✓	
15				27.4 ✓	8.0
	5.34	935.43 ✓	5.34	930.01 ✓	930.07
	+65			28.6 ✓	6.8

LT

RT

5-9-30

(13)

$\frac{4}{3} \frac{6.8}{7.4}$	$\frac{2}{6} \frac{6.8}{7.4}$	$\frac{0}{2} \frac{6.8}{5.5}$	$\frac{6}{37}$	$\frac{6.8}{23}$	$\frac{7.4}{21}$	$\frac{7.4}{14}$	$\frac{6.8}{12}$	$\frac{6.5}{15.2}$	$\frac{6.7}{6}$	$\frac{7.4}{7}$	$\frac{7.7}{11}$	$\frac{7.2}{17}$	$\frac{6.8}{18}$	$\frac{6.6}{37.4}$	$\frac{6.8}{4.55}$	$\frac{5.7}{24.5}$	$\frac{6.6}{37.4}$
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ON ROCK RT STR 1115.

(64)

$\frac{2}{4} \frac{120}{56}$	$\frac{117}{33}$	$\frac{120}{23}$	$\frac{117}{16}$	$\frac{105}{8}$	$\frac{100}{-3.6}$	$\frac{104}{5}$	$\frac{120}{11}$	$\frac{125}{13}$	$\frac{123}{20}$	$\frac{123}{33}$	$\frac{8}{2} \frac{123}{59}$
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(19)

$\frac{4}{7} \frac{7.1}{22}$	$\frac{7.7}{33}$	$\frac{8.1}{21}$	$\frac{7.0}{14}$	$\frac{7.0}{7}$	$\frac{6.8}{7.9}$	$\frac{7.0}{8}$	$\frac{10.4}{14}$	$\frac{11.2}{16}$	$\frac{11.6}{28}$	$\frac{11.8}{33}$	$\frac{2}{2} \frac{7.1}{67}$
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(9)

$\frac{6}{3} \frac{5.4}{23}$	$\frac{0.4}{22}$	$\frac{3.4}{14}$	$\frac{3.1}{6}$	$\frac{3.2}{0.1}$	$\frac{3.5}{10}$	$\frac{3.9}{18}$	$\frac{5.2}{23}$	$\frac{6.5}{33}$	$\frac{7}{2} \frac{4.6}{15}$	$\frac{4}{9} \frac{3.8}{0.7}$
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(12.8)

$\frac{0}{3} \frac{6.8}{160}$	$\frac{6.8}{33}$	$\frac{7.1}{30}$
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(107)

$\frac{0}{3} \frac{4.1}{166}$	$\frac{4.1}{33}$	$\frac{4.5}{30}$	$\frac{6.5}{24}$	$\frac{10.9}{13}$	$\frac{11.4}{10}$	$\frac{10.3}{8}$	$\frac{10.1}{7}$	$\frac{100}{10.7}$	$\frac{9.9}{3}$	$\frac{10.6}{12}$	$\frac{8.5}{17}$	$\frac{6.2}{19}$	$\frac{6.5}{22}$	$\frac{7.5}{23}$	$\frac{8.2}{33}$	$\frac{5}{2} \frac{4.8}{12.9}$
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(96)

$\frac{2}{3} \frac{3.8}{148}$	$\frac{3.8}{33}$	$\frac{3.8}{30}$	$\frac{5.4}{23}$	$\frac{6.5}{17}$	$\frac{8.3}{14}$	$\frac{7.1}{11}$	$\frac{7.7}{7}$	$\frac{7.1}{11.5}$	$\frac{7.6}{7}$	$\frac{9.7}{13}$	$\frac{6.7}{16}$	$\frac{5.2}{18}$	$\frac{5.0}{25}$	$\frac{4.7}{33}$	$\frac{7}{2} \frac{4.8}{138}$
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(65)

$\frac{2}{2} \frac{3.7}{128}$	$\frac{3.7}{33}$	$\frac{3.7}{20}$	$\frac{4.2}{15}$	$\frac{5.5}{6}$	$\frac{5.2}{11.2}$	$\frac{5.5}{6}$	$\frac{5.5}{7}$	$\frac{5.2}{9}$	$\frac{4.2}{11}$	$\frac{3.4}{17}$	$\frac{4.2}{18}$	$\frac{4.3}{28}$	$\frac{4.4}{33}$	$\frac{3}{2} \frac{4.3}{122}$
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(11)

$\frac{2}{3} \frac{4.5}{-0.1}$	$\frac{4}{4} \frac{4.3}{101}$	$\frac{4.0}{33}$	$\frac{4.4}{34}$	$\frac{4.8}{16}$	$\frac{4.5}{11}$	$\frac{4.4}{5}$	$\frac{4.5}{-0.1}$	$\frac{4.5}{6}$	$\frac{4.9}{8}$	$\frac{6.6}{19}$	$\frac{5.9}{27}$	$\frac{5.5}{33}$	$\frac{5.7}{33}$	$\frac{2}{2} \frac{5.6}{12}$	$\frac{4}{6} \frac{6.1}{12.7}$
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(13)

$\frac{2}{2} \frac{3}{10.9}$	$\frac{3}{30}$	$\frac{1.1}{21}$	$\frac{1.8}{17}$	$\frac{2.5}{10}$	$\frac{2.4}{0.3}$	$\frac{2.6}{8}$	$\frac{2.7}{12}$	$\frac{3.3}{18}$	$\frac{3.2}{25}$	$\frac{3.1}{33}$	$\frac{2.7}{33}$	$\frac{2}{2} \frac{3.2}{0.9}$
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(10)

$\frac{3}{5} \frac{3.8}{142}$	$\frac{3.5}{33}$	$\frac{3.7}{27}$	$\frac{3.8}{20}$	$\frac{6.1}{17}$	$\frac{6.3}{10}$	$\frac{6.3}{11.4}$	$\frac{6.7}{3}$	$\frac{6.3}{9}$	$\frac{6.6}{12}$	$\frac{6.1}{22}$	$\frac{5.8}{33}$	$\frac{8}{2} \frac{6.1}{11.9}$
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(63)

$\frac{2}{6} \frac{8}{1.9}$	$\frac{4.6}{33}$	$\frac{4.8}{26}$	$\frac{4.5}{25}$	$\frac{4.0}{19}$	$\frac{4.5}{18}$	$\frac{4.8}{10}$	$\frac{4.8}{12.0}$	$\frac{4.8}{4}$	$\frac{4.3}{6}$	$\frac{5.0}{8}$	$\frac{5.8}{19}$	$\frac{6.6}{33}$	$\frac{7}{2} \frac{6.3}{10.5}$
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STA.	+	M.I.	-	ELEV	Gr. Rod
		935.43			
16				28.7	67
	+50			28.4	70
17				27.4	80
	+30			26.4	90
	+60			25.2	10.2
18				23.5	11.9
	+37			21.9	13.5
		2.87	924.62	13.68	921.75
	+62			20.9	3.7
19				19.3	5.3
	+50			17.2	7.4
		3.23	915.77	12.08	912.54
20				15.2	0.6
	+50			13.5	2.3
B.M.	1.59	915.78	1.59	914.18	914.19

LT.

RT.

5-20-30

6

(6.7)

$$\begin{array}{r} 0/60 \\ 2/107 \end{array} \quad \begin{array}{r} 63 \\ 33 \end{array} \quad \begin{array}{r} 60 \\ 16 \end{array} \quad \begin{array}{r} 56 \\ 11 \end{array} \quad \begin{array}{r} 57 \\ 7 \end{array} \quad \begin{array}{r} 57 \\ 3 \end{array} \quad \begin{array}{r} 53 \\ 7 \end{array} \quad \begin{array}{r} 56 \\ 10 \end{array} \quad \begin{array}{r} 55 \\ 21 \end{array} \quad \begin{array}{r} 53 \\ 33 \end{array} \quad \begin{array}{r} 55 \\ 2 \end{array} \quad \begin{array}{r} 56 \\ 712 \end{array}$$

(7.0)

$$\begin{array}{r} 4/67 \\ 2/103 \end{array} \quad \begin{array}{r} 70 \\ 33 \end{array} \quad \begin{array}{r} 68 \\ 26 \end{array} \quad \begin{array}{r} 66 \\ 25 \end{array} \quad \begin{array}{r} 65 \\ 13 \end{array} \quad \begin{array}{r} 60 \\ 6 \end{array} \quad \begin{array}{r} 61 \\ 70 \end{array} \quad \begin{array}{r} 60 \\ 9 \end{array} \quad \begin{array}{r} 49 \\ 7 \end{array} \quad \begin{array}{r} 51 \\ 11 \end{array} \quad \begin{array}{r} 47 \\ 18 \end{array} \quad \begin{array}{r} 46 \\ 33 \end{array} \quad \begin{array}{r} 44 \\ 2 \end{array} \quad \begin{array}{r} 44 \\ 712 \end{array}$$

(8.0)

$$\begin{array}{r} 2/45 \\ 2/135 \end{array} \quad \begin{array}{r} 47 \\ 33 \end{array} \quad \begin{array}{r} 48 \\ 28 \end{array} \quad \begin{array}{r} 47 \\ 26 \end{array} \quad \begin{array}{r} 46 \\ 20 \end{array} \quad \begin{array}{r} 64 \\ 17 \end{array} \quad \begin{array}{r} 62 \\ 10 \end{array} \quad \begin{array}{r} 63 \\ 71 \end{array} \quad \begin{array}{r} 67 \\ 7 \end{array} \quad \begin{array}{r} 55 \\ 10 \end{array} \quad \begin{array}{r} 60 \\ 12 \end{array} \quad \begin{array}{r} 60 \\ 23 \end{array} \quad \begin{array}{r} 57 \\ 33 \end{array} \quad \begin{array}{r} 60 \\ 2 \end{array} \quad \begin{array}{r} 60 \\ 712 \end{array}$$

(9.0)

$$\begin{array}{r} 1/41 \\ 3/149 \end{array} \quad \begin{array}{r} 41 \\ 33 \end{array} \quad \begin{array}{r} 41 \\ 29 \end{array} \quad \begin{array}{r} 39 \\ 20 \end{array} \quad \begin{array}{r} 43 \\ 17 \end{array} \quad \begin{array}{r} 66 \\ 11 \end{array} \quad \begin{array}{r} 69 \\ 72 \end{array} \quad \begin{array}{r} 69 \\ 7 \end{array} \quad \begin{array}{r} 51 \\ 9 \end{array} \quad \begin{array}{r} 55 \\ 16 \end{array} \quad \begin{array}{r} 52 \\ 22 \end{array} \quad \begin{array}{r} 49 \\ 33 \end{array} \quad \begin{array}{r} 51 \\ 2 \end{array} \quad \begin{array}{r} 51 \\ 712 \end{array}$$

(10.7)

$$\begin{array}{r} 55 \\ 33 \end{array} \quad \begin{array}{r} 55 \\ 28 \end{array} \quad \begin{array}{r} 53 \\ 20 \end{array} \quad \begin{array}{r} 81 \\ 16 \end{array} \quad \begin{array}{r} 83 \\ 10 \end{array} \quad \begin{array}{r} 82 \\ 5 \end{array} \quad \begin{array}{r} 85 \\ 7 \end{array} \quad \begin{array}{r} 90 \\ 10 \end{array} \quad \begin{array}{r} 75 \\ 18 \end{array} \quad \begin{array}{r} 74 \\ 23 \end{array} \quad \begin{array}{r} 69 \\ 33 \end{array} \quad \begin{array}{r} 65 \\ 33 \end{array}$$

(11.9)

$$\begin{array}{r} 8/107 \\ 2/112 \end{array} \quad \begin{array}{r} 109 \\ 33 \end{array} \quad \begin{array}{r} 110 \\ 18 \end{array} \quad \begin{array}{r} 109 \\ 11 \end{array} \quad \begin{array}{r} 107 \\ 5 \end{array} \quad \begin{array}{r} 106 \\ 113 \end{array} \quad \begin{array}{r} 105 \\ 9 \end{array} \quad \begin{array}{r} 83 \\ 12 \end{array} \quad \begin{array}{r} 85 \\ 15 \end{array} \quad \begin{array}{r} 78 \\ 25 \end{array} \quad \begin{array}{r} 72 \\ 33 \end{array} \quad \begin{array}{r} 76 \\ 3 \end{array} \quad \begin{array}{r} 76 \\ 743 \end{array}$$

(13.5)

$$\begin{array}{r} 125 \\ 33 \end{array} \quad \begin{array}{r} 128 \\ 19 \end{array} \quad \begin{array}{r} 132 \\ 15 \end{array} \quad \begin{array}{r} 130 \\ 14 \end{array} \quad \begin{array}{r} 129 \\ 10 \end{array} \quad \begin{array}{r} 129 \\ 4 \end{array} \quad \begin{array}{r} 133 \\ 6 \end{array} \quad \begin{array}{r} 129 \\ 7 \end{array} \quad \begin{array}{r} 126 \\ 9 \end{array} \quad \begin{array}{r} 114 \\ 11 \end{array} \quad \begin{array}{r} 110 \\ 16 \end{array} \quad \begin{array}{r} 103 \\ 27 \end{array} \quad \begin{array}{r} 99 \\ 33 \end{array}$$

(3.7)

$$\begin{array}{r} 65/20 \\ 2/117 \end{array} \quad \begin{array}{r} 19 \\ 33 \end{array} \quad \begin{array}{r} 19 \\ 28 \end{array} \quad \begin{array}{r} 26 \\ 17 \end{array} \quad \begin{array}{r} 36 \\ 14 \end{array} \quad \begin{array}{r} 38 \\ 10 \end{array} \quad \begin{array}{r} 37 \\ 0 \end{array} \quad \begin{array}{r} 40 \\ 6 \end{array} \quad \begin{array}{r} 36 \\ 7 \end{array} \quad \begin{array}{r} 37 \\ 10 \end{array} \quad \begin{array}{r} 14 \\ 14 \end{array} \quad \begin{array}{r} 12 \\ 21 \end{array} \quad \begin{array}{r} 11 \\ 33 \end{array} \quad \begin{array}{r} 11 \\ 2 \end{array} \quad \begin{array}{r} 11 \\ 712 \end{array}$$

(5.3)

$$\begin{array}{r} 1/69 \\ 2/116 \end{array} \quad \begin{array}{r} 1/72 \\ 2/119 \end{array} \quad \begin{array}{r} 75 \\ 33 \end{array} \quad \begin{array}{r} 73 \\ 20 \end{array} \quad \begin{array}{r} 80 \\ 18 \end{array} \quad \begin{array}{r} 75 \\ 14 \end{array} \quad \begin{array}{r} 69 \\ 5 \end{array} \quad \begin{array}{r} 68 \\ 75 \end{array} \quad \begin{array}{r} 70 \\ 7 \end{array} \quad \begin{array}{r} 67 \\ 8 \end{array} \quad \begin{array}{r} 66 \\ 11 \end{array} \quad \begin{array}{r} 47 \\ 13 \end{array} \quad \begin{array}{r} 41 \\ 17 \end{array} \quad \begin{array}{r} 30 \\ 33 \end{array} \quad \begin{array}{r} 31 \\ 2 \end{array} \quad \begin{array}{r} 31 \\ 712 \end{array}$$

(7.4)

$$\begin{array}{r} 8/133 \\ 2/159 \end{array} \quad \begin{array}{r} 136 \\ 33 \end{array} \quad \begin{array}{r} 132 \\ 20 \end{array} \quad \begin{array}{r} 124 \\ 12 \end{array} \quad \begin{array}{r} 110 \\ 8 \end{array} \quad \begin{array}{r} 110 \\ 8 \end{array} \quad \begin{array}{r} 107 \\ 5 \end{array} \quad \begin{array}{r} 100 \\ 10 \end{array} \quad \begin{array}{r} 90 \\ 15 \end{array} \quad \begin{array}{r} 85 \\ 20 \end{array} \quad \begin{array}{r} 80 \\ 30 \end{array} \quad \begin{array}{r} 76 \\ 33 \end{array} \quad \begin{array}{r} 83 \\ 2 \end{array} \quad \begin{array}{r} 83 \\ 112 \end{array}$$

(10.0)

$$\begin{array}{r} 0/61 \\ 2/155 \end{array} \quad \begin{array}{r} 61 \\ 33 \end{array} \quad \begin{array}{r} 63 \\ 20 \end{array} \quad \begin{array}{r} 59 \\ 12 \end{array} \quad \begin{array}{r} 52 \\ 7 \end{array} \quad \begin{array}{r} 44 \\ 4 \end{array} \quad \begin{array}{r} 40 \\ 34 \end{array} \quad \begin{array}{r} 57 \\ 5 \end{array} \quad \begin{array}{r} 43 \\ 8 \end{array} \quad \begin{array}{r} 43 \\ 19 \end{array} \quad \begin{array}{r} 36 \\ 24 \end{array} \quad \begin{array}{r} 35 \\ 33 \end{array} \quad \begin{array}{r} 0/41 \\ 2/135 \end{array} \quad \begin{array}{r} 50 \\ 7 \end{array} \quad \begin{array}{r} 50 \\ 712 \end{array}$$

(11.0)

$$\begin{array}{r} 2/70 \\ 2/47 \end{array} \quad \begin{array}{r} 62 \\ 33 \end{array} \quad \begin{array}{r} 63 \\ 24 \end{array} \quad \begin{array}{r} 69 \\ 23 \end{array} \quad \begin{array}{r} 70 \\ 21 \end{array} \quad \begin{array}{r} 64 \\ 20 \end{array} \quad \begin{array}{r} 60 \\ 8 \end{array} \quad \begin{array}{r} 49 \\ 5 \end{array} \quad \begin{array}{r} 46 \\ 23 \end{array} \quad \begin{array}{r} 48 \\ 6 \end{array} \quad \begin{array}{r} 56 \\ 9 \end{array} \quad \begin{array}{r} 57 \\ 18 \end{array} \quad \begin{array}{r} 57 \\ 33 \end{array} \quad \begin{array}{r} 51 \\ 17 \end{array} \quad \begin{array}{r} 51 \\ 34 \end{array}$$

STA.	+	H.I.	-	ELEV	CR. ROD
		915.78			
21				12.0	38
	+50			10.8	50
22				09.8	60
	+50			09.1	67
23				08.5	73
	+50			07.9	79
24				07.5	83
	2.54	906.98	11.34	904.42	
	+50			07.5	105
25				07.8	-0.8
	9.36	910.72	5.62	901.36	
25				07.8	29
	+50		GR 6.7	08.5	22
26			GR 5.60	09.4	11

LT.

RT

5-20-30

$$\begin{array}{r} 8 \overline{) 62} \\ \underline{17} \\ -24 \end{array} \quad \begin{array}{r} 61 \\ 33 \end{array} \quad \begin{array}{r} 61 \\ 25 \end{array} \quad \begin{array}{r} 69 \\ 23 \end{array} \quad \begin{array}{r} 69 \\ 22 \end{array} \quad \begin{array}{r} 63 \\ 41 \end{array} \quad \begin{array}{r} 61 \\ 9 \end{array} \quad \begin{array}{r} 5.1 \\ 6 \end{array} \quad \begin{array}{r} 48 \\ 70 \end{array} \quad \begin{array}{r} 50 \\ 5 \end{array} \quad \begin{array}{r} 52 \\ 7 \end{array} \quad \begin{array}{r} 60 \\ 21 \end{array} \quad \begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 4 \overline{) 60} \\ \underline{17} \\ -22 \end{array}$$

5.9

$$\begin{array}{r} 0 \overline{) 60} \\ \underline{70} \\ 2 \end{array} \quad \begin{array}{r} 0 \overline{) 71} \\ \underline{2} \\ -21 \end{array} \quad \begin{array}{r} 63 \\ 33 \end{array} \quad \begin{array}{r} 61 \\ 25 \end{array} \quad \begin{array}{r} 71 \\ 24 \end{array} \quad \begin{array}{r} 71 \\ 22 \end{array} \quad \begin{array}{r} 60 \\ 21 \end{array} \quad \begin{array}{r} 60 \\ 9 \end{array} \quad \begin{array}{r} 5.4 \\ 6 \end{array} \quad \begin{array}{r} 50 \\ 60 \end{array} \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 5.9 \\ 8 \end{array} \quad \begin{array}{r} 60 \\ 18 \end{array} \quad \begin{array}{r} 60 \\ 33 \end{array} \quad \begin{array}{r} 3 \overline{) 61} \\ \underline{2} \\ -11 \end{array}$$

5.0

$$\begin{array}{r} 5 \overline{) 60} \\ \underline{00} \\ 0 \end{array} \quad \begin{array}{r} 0 \overline{) 69} \\ \underline{8} \\ -0.9 \end{array} \quad \begin{array}{r} 63 \\ 33 \end{array} \quad \begin{array}{r} 63 \\ 26 \end{array} \quad \begin{array}{r} 73 \\ 25 \end{array} \quad \begin{array}{r} 72 \\ 23 \end{array} \quad \begin{array}{r} 61 \\ 22 \end{array} \quad \begin{array}{r} 60 \\ 8 \end{array} \quad \begin{array}{r} 53 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 11.1 \end{array} \quad \begin{array}{r} 50 \\ 3 \end{array} \quad \begin{array}{r} 54 \\ 6 \end{array} \quad \begin{array}{r} 61 \\ 8 \end{array} \quad \begin{array}{r} 60 \\ 21 \end{array} \quad \begin{array}{r} 60 \\ 33 \end{array} \quad \begin{array}{r} 0 \overline{) 60} \\ \underline{4} \\ -00 \end{array} \quad \begin{array}{r} 2 \overline{) 61} \\ \underline{1} \\ -21 \end{array}$$

6.0

$$\begin{array}{r} 5 \overline{) 56} \\ \underline{2} \\ -11 \end{array} \quad \begin{array}{r} 54 \\ 33 \end{array} \quad \begin{array}{r} 56 \\ 22 \end{array} \quad \begin{array}{r} 63 \\ 19 \end{array} \quad \begin{array}{r} 75 \\ 17 \end{array} \quad \begin{array}{r} 57 \\ 15 \end{array} \quad \begin{array}{r} 47 \\ 6 \end{array} \quad \begin{array}{r} 48 \\ 11.9 \end{array} \quad \begin{array}{r} 49 \\ 4 \end{array} \quad \begin{array}{r} 52 \\ 8 \end{array} \quad \begin{array}{r} 53 \\ 15 \end{array} \quad \begin{array}{r} 49 \\ 30 \end{array} \quad \begin{array}{r} 48 \\ 33 \end{array} \quad \begin{array}{r} 5 \overline{) 50} \\ \underline{2} \\ -11 \end{array}$$

6.7

$$\begin{array}{r} 9 \overline{) 2.7} \\ \underline{3} \\ -14.6 \end{array} \quad \begin{array}{r} 26 \\ 33 \end{array} \quad \begin{array}{r} 24 \\ 25 \end{array} \quad \begin{array}{r} 60 \\ 21 \end{array} \quad \begin{array}{r} 67 \\ 19 \end{array} \quad \begin{array}{r} 80 \\ 16 \end{array} \quad \begin{array}{r} 65 \\ 15 \end{array} \quad \begin{array}{r} 58 \\ 7 \end{array} \quad \begin{array}{r} 5.7 \\ 11.6 \end{array} \quad \begin{array}{r} 52 \\ 3 \end{array} \quad \begin{array}{r} 54 \\ 7 \end{array} \quad \begin{array}{r} 69 \\ 16 \end{array} \quad \begin{array}{r} 49 \\ 18 \end{array} \quad \begin{array}{r} 43 \\ 23 \end{array} \quad \begin{array}{r} 42 \\ 33 \end{array} \quad \begin{array}{r} 0 \overline{) 46} \\ \underline{2} \\ -12.7 \end{array}$$

7.3

$$\begin{array}{r} 7 \overline{) 5.7} \\ \underline{2} \\ -12.2 \end{array} \quad \begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 61 \\ 23 \end{array} \quad \begin{array}{r} 75 \\ 19 \end{array} \quad \begin{array}{r} 24 \\ 16 \end{array} \quad \begin{array}{r} 85 \\ 12 \end{array} \quad \begin{array}{r} 83 \\ 7 \end{array} \quad \begin{array}{r} 84 \\ 0.5 \end{array} \quad \begin{array}{r} 2.9 \\ 4 \end{array} \quad \begin{array}{r} 80 \\ 9 \end{array} \quad \begin{array}{r} 92 \\ 15 \end{array} \quad \begin{array}{r} 97 \\ 17 \end{array} \quad \begin{array}{r} 72 \\ 22 \end{array} \quad \begin{array}{r} 69 \\ 31 \end{array} \quad \begin{array}{r} 67 \\ 33 \end{array} \quad \begin{array}{r} 3 \overline{) 71} \\ \underline{2} \\ -10.8 \end{array}$$

7.9

$$\begin{array}{r} 2 \overline{) 11.9} \\ \underline{2} \\ -3.6 \end{array} \quad \begin{array}{r} 12.2 \\ 29 \end{array} \quad \begin{array}{r} 12.2 \\ 25 \end{array} \quad \begin{array}{r} 11.7 \\ 23 \end{array} \quad \begin{array}{r} 11.9 \\ 13 \end{array} \quad \begin{array}{r} 11.0 \\ 10 \end{array} \quad \begin{array}{r} 11.0 \\ 6 \end{array} \quad \begin{array}{r} 11.2 \\ 5 \end{array} \quad \begin{array}{r} 11.2 \\ 2 \end{array} \quad \begin{array}{r} 11.1 \\ 9 \end{array} \quad \begin{array}{r} 11.1 \\ 5 \end{array} \quad \begin{array}{r} 10.1 \\ 12 \end{array} \quad \begin{array}{r} 94 \\ 22 \end{array} \quad \begin{array}{r} 94 \\ 33 \end{array} \quad \begin{array}{r} 8 \overline{) 10.7} \\ \underline{1} \\ -2.4 \end{array} \quad \begin{array}{r} 4 \overline{) 7.9} \\ \underline{2} \\ -11.4 \end{array}$$

13

$$\begin{array}{r} 8 \overline{) 7.2} \\ \underline{6} \\ -7.7 \end{array} \quad \begin{array}{r} 7.8 \\ 23 \end{array} \quad \begin{array}{r} 7.8 \\ 31 \end{array} \quad \begin{array}{r} 7.0 \\ 25 \end{array} \quad \begin{array}{r} 6.3 \\ 12 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 4.9 \\ 6 \end{array} \quad \begin{array}{r} 4.5 \\ 5.0 \end{array} \quad \begin{array}{r} 4.2 \\ 6 \end{array} \quad \begin{array}{r} 4.7 \\ 11 \end{array} \quad \begin{array}{r} 4.1 \\ 21 \end{array} \quad \begin{array}{r} 3.0 \\ 29 \end{array} \quad \begin{array}{r} 2.7 \\ 33 \end{array} \quad \begin{array}{r} 0 \overline{) 40} \\ \underline{2} \\ -4.5 \end{array} \quad \begin{array}{r} 9 \overline{) 3.1} \\ \underline{2} \\ -1.7 \end{array}$$

10.2

$$\begin{array}{r} 80 \\ 8 \end{array} \quad \begin{array}{r} 57 \\ 3 \end{array} \quad \begin{array}{r} 5.5 \\ 6.1 \end{array} \quad \begin{array}{r} 5.2 \\ 7 \end{array} \quad \begin{array}{r} 6.6 \\ 10 \end{array} \quad \begin{array}{r} 6.8 \\ 18 \end{array} \quad \begin{array}{r} 6.3 \\ 26 \end{array} \quad \begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 0 \overline{) 6.2} \\ \underline{7} \\ -7.0 \end{array}$$

10.8

$$\begin{array}{r} 4 \overline{) 12.1} \\ \underline{3} \\ -9.2 \end{array} \quad \begin{array}{r} 12.1 \\ 23 \end{array} \quad \begin{array}{r} 12.1 \\ 23 \end{array}$$

2.0

$$\begin{array}{r} 4 \overline{) 12.0} \\ \underline{3} \\ -9.8 \end{array} \quad \begin{array}{r} 12.0 \\ 35 \end{array} \quad \begin{array}{r} 11.9 \\ 18 \end{array} \quad \begin{array}{r} 11.8 \\ 6 \end{array} \quad \begin{array}{r} 9.5 \\ 3 \end{array} \quad \begin{array}{r} 8.8 \\ 1 \end{array} \quad \begin{array}{r} 8.7 \\ 6.4 \end{array} \quad \begin{array}{r} 8.5 \\ 4 \end{array} \quad \begin{array}{r} 8.2 \\ 8 \end{array} \quad \begin{array}{r} 10.0 \\ 12 \end{array} \quad \begin{array}{r} 10.4 \\ 21 \end{array} \quad \begin{array}{r} 10.4 \\ 33 \end{array} \quad \begin{array}{r} 9 \overline{) 10.3} \\ \underline{4} \\ -2.1 \end{array}$$

2.7

$$\begin{array}{r} 3 \overline{) 11.9} \\ \underline{3} \\ -10.8 \end{array} \quad \begin{array}{r} 11.9 \\ 33 \end{array} \quad \begin{array}{r} 12.4 \\ 17 \end{array} \quad \begin{array}{r} 11.6 \\ 9 \end{array} \quad \begin{array}{r} 10.5 \\ 4 \end{array} \quad \begin{array}{r} 7.9 \\ 6.8 \end{array} \quad \begin{array}{r} 7.3 \\ 1 \end{array} \quad \begin{array}{r} 7.1 \\ 6 \end{array} \quad \begin{array}{r} 7.3 \\ 11 \end{array} \quad \begin{array}{r} 7.8 \\ 23 \end{array} \quad \begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 7 \overline{) 7.7} \\ \underline{6} \\ -7.6 \end{array}$$

1.1

STA	+	H.I	-	ELEV	CR ROD
		910.72			
26	+50			11.1 ✓	-0.4
27				12.9 ✓	-2.2
	12.10	922.48 ✓	0.34	910.38 ✓	
27				12.9 ✓	9.4
27	+50			15.1 ✓	7.4
28				17.5 ✓	5.0
	11.92	932.63 ✓	1.77	920.71 ✓	
27	+50			15.1 ✓	17.5
28				17.5 ✓	15.1
	+50			19.9 ✓	12.7
29				22.3 ✓	10.3
	+50			24.5 ✓	8.1
30				26.1 ✓	6.5
	+50			27.3 ✓	5.3

LT

RT

5-20-30

(-0.4)

$\frac{0}{110}$	110	11.7	11.9	10.9	9.9	5.0	4.9	4.6	4.5	4.4	$\frac{8}{4.5}$
$\frac{3.3}{-11.4}$	33	31	18	12	8	-5.4	7	12	24	30	$\frac{2}{-4.9}$

(-2.5)

$\frac{0}{95}$	9.4	8.3	6.1
$\frac{4.3}{-11.6}$	33	17	11

(0.0)

11.2	11.5	11.0	11.0	11.3	10.2	9.5	7.7	7.1	$\frac{2}{7.0}$
2	7.9	7	13	14	16	20	25	33	$\frac{2}{12.0}$

(7.0)

$\frac{8}{7.5}$	9.2	6.0	5.3	5.5	5.4	5.5	5.8	0.7
$\frac{2}{-0.1}$	33	14	3	2	11.8	7	14	20

(6.0)

0.8	1.2	1.7	1.4	1.5	2.1	0.4
4	2	13.3	5	9	13	14

(19.5)

10.9	9.6	8.4	8.2	7.8	$\frac{0}{8.1}$
21	24	28	33	35	$\frac{2}{17.4}$

(5.1)

$\frac{0}{26}$	8.7	8.2	7.5	7.5	9.7	7.0	4.6	3.3	3.3	$\frac{0}{3.5}$
$\frac{5.5}{16.6}$	35	33	21	9	5	19	21	27	33	$\frac{2}{11.8}$

(17.1)

$\frac{6}{7.2}$	7.7	6.6	6.5	8.3	8.9	8.9	8.5	8.7	8.8	8.1	4.5	3.1	2.3	2.4	$\frac{9}{2.4}$
$\frac{3}{15.1}$	33	30	8	5	2	13.8	5	10	12	13	20	21	28	33	$\frac{2}{10.3}$

(10.3)

$\frac{4}{6.7}$	7.0	5.9	5.1	6.2	6.1	5.9	6.1	5.7	3.6	2.2	1.7	1.2	1.4	$\frac{1}{2}$
$\frac{2}{13.6}$	33	21	8	6	14.2	4	12	14	17	21	26	33	36	$\frac{3}{17.1}$

(9.1)

$\frac{8.5}{5.1}$	5.5	4.6	3.7	4.2	4.5	4.4	4.2	4.0	3.1
$\frac{2}{13.0}$	33	19	8	6	9	13.7	5	11	15

(6.5)

$\frac{3}{6.3}$	6.9	6.0	5.5	4.0	3.8	3.3	2.6	1.1
$\frac{2}{10.2}$	33	17	9	3	12.7	11	17	20

(5.3)

$\frac{1.9}{6.7}$	7.5	7.2	6.2	5.3	4.4	3.7	3.2	2.2
$\frac{2}{-1.4}$	33	27	16	8	6	11.4	8	17

STA	+	H. I.	-	ELEV		
		932.63 ✓				
31				27.9 ✓	4.7	
	+50			28.1 ✓	4.5	
32				27.7 ✓	4.9	
	10.89	938.98 ✓	4.54	928.09 ✓		
	29+50			24.5 ✓	14.5	
30				26.1 ✓	12.9	
	30+50			27.3 ✓	11.7	
31				27.9 ✓	11.1	
	31+50			28.1 ✓	10.9	
32				27.7 ✓	11.3	
	2.42	930.51 ✓	10.89	928.09 ✓		
	32+50			27.1 ✓	3.4	
	B.M.	4.44	930.53 ✓	4.44	926.07 ✓	926.09
33				26.5 ✓	4.0	
	+50			25.9 ✓	4.4	

5-20-30

2) 5.8  
 1 5 -7.1

3) 6.5  
 2 -7.8

7.7 6.0 5.1 5.5 3.3 3.2 2.4  
 3.3 1.9 9 7 7.4 7 7.4

8) 6.7  
 1 -2.8

9.1 7.4 6.1 4.7 4.2 4.0 3.4  
 3.3 1.9 1.0 6 7.2 6 1.5

2) 9.0  
 1 -4.1

9.8 9.1 6.7 5.9 5.5 5.1 5.7 2.5  
 3.3 2.0 1.1 5 -0.6 9 1.5 2.4

14.5

6.2 5.7 6.2 5.0 5.1 5.7 3) 5.1  
 1.9 2.2 2.3 2.9 3.3 3.5 3) 1.99

17)

6.7 6.0 5.2 5.3 0) 5.2  
 2.2 2.5 3.3 3.5 3) 1.77

11.7

6.3 4.1 3.1 3.0 0) 3.1  
 3.0 2.5 3.3 3.5 3) 1.8.6

11)

4.5 2.4 1.9 1.9 0) 1.9  
 2.1 2.4 3.3 3.5 3) 1.42

10.9

6.9 5.9 5.3 5.1 4.8 7) 5.1  
 1.9 2.1 2.8 3.3 3.5 3) 1.5.8

11.3

8.6 7) 2.8  
 3.3 2) 1.2.5

7) 5.6  
 1 -2.2

6.5 6.1 5.4 4.4 4.2 4.1 2.7 2.3 1.2 2) 2.0  
 3.3 1.8 1.6 9 -0.8 8 7.2 7.8 8.3 2) 1.14

2) 6.1  
 1 -2.1

6.7 6.8 6.2 5.6 5.9 6.1 5.0 4.6 4.1 4) 4.4  
 3.3 1.9 1.8 1.0 -1.9 8 1.4 2.0 3.3 2) -0.4 1) 5.0  
 1) 2.0 2) -1.0

6) 8.4  
 1 -3.8

8.1 8.2 8.7 8.1 7.4 7.1 7.0 6.5 6.3 6.9 0) 6.6  
 3.3 2.2 1.9 1.8 8 -2.5 7 1.3 1.9 3.3 1) 2.0 2) -1.9

		H.I.	-	ELEY	CR ROD
37A	+	930.53 ✓			
34				253 ✓	52
	+50			24.7 ✓	5.8
35				27.1 ✓	64
	+50			23.5 ✓	69 70 71
B.M.	2.21	928.50 ✓	4.44	926.09 ✓	
36		0.7		22.9 ✓	4.7 5.4 6.1
36	+50	2.35		22.3 ✓	5.1 6.0 7.1
	6.91	931.84 ✓	3.37	924.93 ✓	
36	+50			22.5 ✓	86 95
37		3.4		21.7 ✓	90 10.1 11
	+50	3.4		20.9 ✓	98 10.7 11
38		3.4		19.6 ✓	11.1 12.2 13
	+50	3.4		17.9 ✓	12.8 13.9 15
39		3.4		15.8 ✓	14.7 16.0
	1.69	921.24	12.29	919.55 ✓	

LT

RT

5-20-30

(5.7)

$\frac{6}{17.8}$	$\frac{71}{33}$	$\frac{72}{9}$	$\frac{72}{-2.0}$	$\frac{73}{7}$	$\frac{71}{13}$	$\frac{75}{21}$	$\frac{78}{33}$	$\frac{2}{17.3}$
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(5.8)

$\frac{40}{17.5}$	$\frac{2}{27.5}$	$\frac{62}{33}$	$\frac{64}{25}$	$\frac{62}{16}$	$\frac{66}{8}$	$\frac{68}{70}$	$\frac{76}{8}$	$\frac{75}{10}$	$\frac{77}{14}$	$\frac{77}{24}$	$\frac{77}{33}$	$\frac{3}{27.5}$	$\frac{4}{27.5}$
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(6.2)

$\frac{9}{27.6}$	$\frac{3.8}{33}$	$\frac{45}{18}$	$\frac{41}{16}$	$\frac{70}{13}$	$\frac{65}{7}$	$\frac{67}{0.3}$	$\frac{66}{7}$	$\frac{79}{11}$	$\frac{78}{12}$	$\frac{6.9}{14}$	$\frac{7.5}{23}$	$\frac{27}{33}$	$\frac{5}{27.4}$	$\frac{0}{47.9}$
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(7.0)

$\frac{8}{27.0}$	$\frac{5.9}{33}$	$\frac{3.6}{18}$	$\frac{4.9}{13}$	$\frac{7.3}{12}$	$\frac{7.0}{0.3}$	$\frac{7.3}{9}$	$\frac{7.4}{16}$	$\frac{9.4}{19}$	$\frac{10.6}{30}$	$\frac{13.5}{34}$	$\frac{14.2}{27.4}$	$\frac{6}{43}$	$\frac{11.4}{-4.3}$
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(6.4)

$\frac{4}{17.7}$	$\frac{2}{13.4}$	$\frac{10}{33}$	$\frac{21}{18}$	$\frac{41}{17}$	$\frac{4.9}{13}$	$\frac{4.3}{10}$	$\frac{4.6}{10.8}$	$\frac{5.3}{10}$	$\frac{9.1}{17}$	$\frac{10.3}{19}$	$\frac{13.5}{53}$	$\frac{5}{27.19}$	$\frac{1}{-5.8}$
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(6.0)

$\frac{15}{14}$	$\frac{1.9}{15}$	$\frac{3.6}{12}$	$\frac{3.2}{7}$	$\frac{3.7}{12.3}$	$\frac{4.5}{12}$	$\frac{6.4}{18}$	$\frac{8.2}{24}$	$\frac{10.7}{33}$	$\frac{4.7}{27.9}$	$\frac{5.4}{11.7}$
-----------------	------------------	------------------	-----------------	--------------------	------------------	------------------	------------------	-------------------	--------------------	--------------------

(4.9)

$\frac{8}{17.2}$	$\frac{3.4}{33}$	$\frac{3.9}{21}$
------------------	------------------	------------------

(10.1)

$\frac{8}{17.3}$	$\frac{0.7}{33}$	$\frac{1.8}{25}$	$\frac{3.7}{24}$	$\frac{7.3}{18}$	$\frac{7.6}{14}$	$\frac{6.0}{10}$	$\frac{5.8}{14.5}$	$\frac{6.5}{13}$	$\frac{6.0}{14}$	$\frac{7.6}{21}$	$\frac{10.2}{33}$	$\frac{2}{17.9}$
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(10.9)

$\frac{0}{14.7}$	$\frac{4.0}{33}$	$\frac{5.2}{30}$	$\frac{6.1}{24}$	$\frac{5.5}{25}$	$\frac{4.7}{19}$	$\frac{4.6}{13}$	$\frac{5.0}{4}$	$\frac{5.5}{15.8}$	$\frac{5.1}{13}$	$\frac{7.6}{33}$	$\frac{12.1}{33}$	$\frac{0}{11.2}$
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(12.2)

$\frac{2}{17.7}$	$\frac{4.4}{33}$	$\frac{4.4}{30}$	$\frac{4.5}{24}$	$\frac{5.2}{20}$	$\frac{5.3}{12}$	$\frac{5.8}{15.6}$	$\frac{6.6}{14}$	$\frac{8.1}{21}$	$\frac{9.2}{33}$	$\frac{11.9}{33}$	$\frac{7}{11.4}$	$\frac{1}{12.2}$
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(13.9)

$\frac{0}{17.1}$	$\frac{6.7}{33}$	$\frac{7.6}{9}$	$\frac{8.4}{15.7}$	$\frac{9.7}{14}$	$\frac{11.3}{24}$	$\frac{13.2}{33}$	$\frac{1}{17.8}$	$\frac{1}{12.5}$
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(16.0)

$\frac{8}{17.4}$	$\frac{7.3}{33}$	$\frac{8.0}{15}$	$\frac{9.0}{17.0}$
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721.24<sup>✓</sup>

39

34

15.8<sup>✓</sup>

54 62

+50

34

13.3<sup>✓</sup>

2.8 7.9 93

40

34

10.3<sup>✓</sup>

9.9 10.9

0.13

910.21<sup>✓</sup>

11.16

910.08<sup>✓</sup>

B.M.

10.88

910.18

10.88

899.33<sup>✓</sup>

879.50

40 +00

34

10.3<sup>✓</sup>

-0.1 12

40 +50

34

07.1<sup>✓</sup>

2.1 3.1 49

41

1.1

03.9<sup>✓</sup>

5.5 6.3 72

B.M.

1.62

900.92<sup>✓</sup>

10.88

899.30<sup>✓</sup>

41

1.1

03.9<sup>✓</sup>

-3.0 2

+35

900.6<sup>✓</sup>

-0.1 0.3 67

+75

899.5

1.2

42

982

2.7

+50

960<sup>✓</sup>

4.9

B.M.

1.41

900.71<sup>✓</sup>

1.62

899.50<sup>✓</sup>

$$\begin{array}{r} 51.0 \\ \hline 0.4 \quad 3.6 \quad 6.6 \\ 11 \quad 23 \quad 33 \quad 2/55 \\ \hline 2/71.3 \end{array}$$

$$\begin{array}{r} 4/65 \\ \hline 5.9 \quad 5.9 \quad 6.4 \quad 6.4 \quad 2.6 \quad 1.4 \quad 3.9 \quad 5.0 \quad 12.9 \\ 33 \quad 29 \quad 26 \quad 23 \quad 16 \quad 12 \quad 14.0 \quad 16 \quad 23 \quad 2/11.3 \quad 4/8.5 \\ \hline 2/70.8 \end{array}$$

$$\begin{array}{r} 4/107 \\ \hline 5/10.9 \quad 7.7 \quad 8.7 \quad 10.9 \quad 10.8 \quad 11.3 \quad 11.4 \\ 2/-0.8 \quad 2/-10 \quad 33 \quad 28 \quad 26 \quad 14 \quad -0.4 \quad 3 \end{array}$$

$$\begin{array}{r} 21 \\ \hline 3.0 \quad 4.1 \quad 5.5 \quad 7.9 \quad 8/2.8 \\ 7 \quad 13 \quad 22 \quad 33 \quad 2/5.6 \end{array}$$

$$\begin{array}{r} 6/24 \\ \hline 7.0 \quad 8.3 \quad 9.8 \quad 5.0 \quad 4.6 \quad 5.1 \quad 11.4 \quad 12.8 \quad 0/12.8 \\ 2/-6.3 \quad 33 \quad 23 \quad 13 \quad 9 \quad -1.5 \quad 7 \quad 18 \quad 33 \quad 2/8.4 \end{array}$$

$$\begin{array}{r} 6.2 \\ \hline 2/14.1 \quad 14.2 \quad 14.1 \quad 13.0 \quad 10.2 \quad 9.8 \quad 10.0 \\ 5/-8.6 \quad 33 \quad 21 \quad 10 \quad 5 \quad 3.5 \quad 11 \end{array}$$

$$\begin{array}{r} -2.0 \\ \hline 4.8 \quad 5.3 \quad 9/5.5 \\ 19 \quad 33 \quad 2/7.4 \end{array}$$

$$\begin{array}{r} 0.3 \\ \hline 5.6 \quad 5.1 \quad 4.6 \quad 4.8 \quad 6.2 \quad 6.0 \quad 3.5 \quad 2.7 \quad 0/4.7 \\ 33 \quad 18 \quad -4.3 \quad 12 \quad 16 \quad 20 \quad 22 \quad 33 \quad 2/4.0 \end{array}$$

$$\begin{array}{r} 11 \\ \hline 7.0 \quad 6.3 \quad 6.0 \quad 5.7 \quad 5.5 \quad 4.8 \quad 4.0 \\ 50 \quad 31 \quad 10 \quad 13 \quad 33 \quad 50 \end{array}$$

$$\begin{array}{r} 6/10.5 \\ \hline 11.1 \quad 9.0 \quad 9.2 \quad 7.1 \quad 6.7 \quad 6.5 \quad 7.6 \quad 6.7 \quad 6.0 \quad 0/7.2 \quad 3/6.2 \\ 2/-7.8 \quad 33 \quad 21 \quad 17 \quad 6 \quad -4.0 \quad 11 \quad 21 \quad 23 \quad 33 \quad 2/-4.5 \quad 2/1.0 \end{array}$$

$$\begin{array}{r} 9/12.9 \\ \hline 12.9 \quad 12.5 \quad 10.8 \quad 8.0 \quad 7.9 \quad 7.7 \quad 7.8 \quad 8.9 \quad 9.0 \quad 8.4 \quad 7.5 \quad 1.2/7.0 \\ 2/-8.0 \quad 33 \quad 18 \quad 11 \quad 5 \quad -3.0 \quad 7 \quad 17 \quad 20 \quad 24 \quad 23 \quad 33 \quad 2/-4.1 \end{array}$$

900.71 ✓

43

741 ✓

66

+50

926 ✓

81

44

915 ✓

92

5.03

896.85 ✓

889

891.82 ✓

+50

907 ✓

62

45

903 ✓

64

8.88

900.70 ✓

5.03

891.82 ✓

B.M.

1.40

899.50 ✓

(6.6)

$\frac{4}{1} \frac{83}{17}$	$\frac{96}{33}$	$\frac{94}{26}$	$\frac{83}{12}$	$\frac{90}{10}$	$\frac{89}{7}$	$\frac{80}{5}$	$\frac{79}{7.5}$	$\frac{78}{7}$	$\frac{84}{16}$	$\frac{96}{20}$	$\frac{84}{25}$	$\frac{59}{25}$	$\frac{56}{33}$	$\frac{4}{1} \frac{88}{22}$
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(9.1)

$\frac{4}{1} \frac{83}{17}$	$\frac{0}{1} \frac{31}{11}$	$\frac{2.1}{33}$	$\frac{2.1}{27}$	$\frac{33}{26}$	$\frac{69}{13}$	$\frac{82}{12}$	$\frac{85}{8}$	$\frac{82}{6}$	$\frac{87}{0.0}$	$\frac{80}{7}$	$\frac{86}{16}$	$\frac{90}{18}$	$\frac{80}{21}$	$\frac{25}{26}$	$\frac{34}{33}$	$\frac{2}{1} \frac{33}{148}$	$\frac{0}{1} \frac{26}{-0.5}$
-----------------------------	-----------------------------	------------------	------------------	-----------------	-----------------	-----------------	----------------	----------------	------------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------------------	-------------------------------

(9.2)

$\frac{9}{2} \frac{78}{114}$	$\frac{0}{2} \frac{99}{118}$	$\frac{60}{33}$	$\frac{74}{28}$	$\frac{76}{19}$	$\frac{81}{15}$	$\frac{87}{6}$	$\frac{85}{107}$	$\frac{83}{6}$	$\frac{87}{15}$	$\frac{101}{17}$	$\frac{101}{21}$	$\frac{98}{25}$	$\frac{107}{33}$	$\frac{1}{1} \frac{98}{26}$
------------------------------	------------------------------	-----------------	-----------------	-----------------	-----------------	----------------	------------------	----------------	-----------------	------------------	------------------	-----------------	------------------	-----------------------------

(6.2)

$\frac{9}{1} \frac{74}{32}$	$\frac{84}{33}$	$\frac{93}{23}$	$\frac{95}{15}$	$\frac{52}{8}$	$\frac{50}{71.2}$	$\frac{54}{14}$	$\frac{84}{19}$	$\frac{93}{22}$	$\frac{74}{26}$	$\frac{12.1}{27}$	$\frac{12.1}{29}$	$\frac{79}{30}$	$\frac{99}{33}$	$\frac{1}{1} \frac{62}{00}$
-----------------------------	-----------------	-----------------	-----------------	----------------	-------------------	-----------------	-----------------	-----------------	-----------------	-------------------	-------------------	-----------------	-----------------	-----------------------------

(6.3)

$\frac{6}{1} \frac{97}{33}$	$\frac{97}{20}$	$\frac{99}{17}$	$\frac{102}{14}$	$\frac{92}{11}$	$\frac{63}{6}$	$\frac{61}{105}$	$\frac{66}{14}$	$\frac{97}{19}$	$\frac{97}{27}$	$\frac{127}{20}$	$\frac{121}{27}$	$\frac{101}{30}$	$\frac{101}{33}$	$\frac{4}{1} \frac{66}{00}$
-----------------------------	-----------------	-----------------	------------------	-----------------	----------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	-----------------------------

B.M.	1.38	900.68		899.30	
0 + 33				995	1.2
0 + 60					
0 + 67				99.0	1.7
1 + 00				98.5	2.2
1 + 50				97.9	2.8
2 + 00				97.1	3.6
2 + 50				96.4	4.3
3 + 00				95.6	5.1
	5.07	899.16	6.59	894.09	
3 + 50				94.9	4.3
3 + 92				94.2	5.0
4 + 00					
	6.95	901.04	5.07	894.09	
B.M.			1.74	899.30	

5-23-50

$\frac{0}{2} \frac{0}{-5.0}$	55	61	54	$\frac{0}{2} \frac{0}{-5.7}$	73	88	114	$\frac{6}{9} \frac{0}{-9.5}$
	23	6.2	8	$\frac{0}{2} \frac{0}{-4.5}$	49	52	70	$\frac{2}{9} \frac{0}{-8.8}$

45	50	57	58	65	89	102	111	116	126
23	9	54	7	17	31	37	43	45	60

$\frac{0}{9} \frac{0}{-2.5}$	$\frac{6}{2} \frac{0}{-5.5}$	15	25	36	54	$\frac{0}{5} \frac{0}{-5.9}$	67	73	100	115	123	124	$\frac{0}{2} \frac{0}{-11.8}$	
$\frac{2}{2} \frac{0}{-13.2}$	$\frac{2}{2} \frac{0}{-3.8}$	27	10	9	6	5.6	$\frac{1}{1} \frac{0}{-4.2}$	27	30	36	43	50	60	$\frac{0}{3} \frac{0}{-10.1}$

$\frac{1}{2} \frac{0}{-11.4}$	0.8	0.5	1.3	61	$\frac{0}{8} \frac{0}{-6.0}$	66	76	109	120	125	$\frac{0}{2} \frac{0}{-12.0}$
	23	13	9	60	$\frac{0}{8} \frac{0}{-3.8}$	18	22	27	36	50	$\frac{0}{2} \frac{0}{-10.4}$

$\frac{4}{2} \frac{0}{-2.8}$	2.8	3.3	64	68	63	63	69	77	100	123	127	$\frac{2}{2} \frac{0}{-20}$
$\frac{2}{2} \frac{0}{-0.0}$	25	20	17	14	10	3.5	11	15	17	25	35	$\frac{2}{2} \frac{0}{-9.8}$

$\frac{7}{2} \frac{0}{-3.1}$	30	36	70	68	67	71	77	101	118	125	$\frac{2}{2} \frac{0}{-2.2}$
$\frac{2}{2} \frac{0}{-10.5}$	26	22	17	11	3.1	9	12	17	25	35	$\frac{0}{2} \frac{0}{-8.0}$

$\frac{4}{2} \frac{0}{-2.0}$	20	30	71	67	64	68	73	112	124	$\frac{6}{2} \frac{0}{-11.2}$
$\frac{2}{2} \frac{0}{-71.3}$	27	18	14	12	21	9	14	27	35	$\frac{2}{2} \frac{0}{-6.9}$

$\frac{2}{2} \frac{0}{-4.2}$	43	47	73	71	65	67	71	85	108	119	$\frac{0}{2} \frac{0}{-21}$
$\frac{2}{2} \frac{0}{-10.9}$	27	14	13	11	7.4	7	15	18	51	33	$\frac{2}{2} \frac{0}{-4.0}$

$\frac{1}{2} \frac{0}{-6.8}$	76	70	69	55	50	51	76	85	93	$\frac{6}{2} \frac{0}{-8.1}$
$\frac{1}{2} \frac{0}{-2.5}$	35	28	15	12	0.7	11	17	24	35	$\frac{0}{2} \frac{0}{-3.8}$

$\frac{1}{2} \frac{0}{-5.3}$	90	88	60	54	50	53	71	73	76	$\frac{8}{2} \frac{0}{-7.4}$
$\frac{1}{2} \frac{0}{-0.8}$	25	22	17	13	0.0	11	15	26	31	$\frac{1}{2} \frac{0}{-2.4}$

9.5	9.3	61	5.2	49	5.1	4.9	4.7
26	23	17	13		8	22	35

B.M.	5.78	931.37		926.09	
37+50		3.44		20.8	7.5 10.4 12.5
38		3.44		19.3	11.0 12.1 13.2
+50		3.44		17.3	13.0 14.1 15.2
39		3.44		14.7	15.4 16.7 18.0
	2.11	921.61	11.87	919.50	
39		3.44		14.7	69.8
+50		3.44		11.5	9.0 10.1 11.2
40		3.44		07.9	12.6 13.7 14.8
	0.43	909.74	12.30	909.31	
40		3.44		07.9	1.8 3.2
+30		3.44		04.0	4.7 5.7 7.0
41		1.10		00.1	8.8 9.6 10.4
B.M.	1.32	900.64	10.42	899.32	899.30
41		1.10		00.1	05 14
+55				76.4	42
B.M.			1.32	899.32	899.30

6-12-30

N.E. COR CONC STEP LT STR 34130

$\frac{1}{3} \frac{x}{4.1}$	$\frac{4.6}{16.0}$	$\frac{1}{2} \frac{x}{10.7}$
$\frac{2}{3} \frac{x}{75.4}$		$\frac{2}{2} \frac{x}{71.8}$

$\frac{5}{4} \frac{x}{4.0}$	$\frac{6.1}{16.0}$	$\frac{1}{5} \frac{x}{11.0}$
$\frac{3}{3} \frac{x}{77.0}$		$\frac{5}{5} \frac{x}{72.5}$

$\frac{0}{4} \frac{x}{6.3}$	$\frac{7.8}{16.3}$	$\frac{1}{3} \frac{x}{12.5}$
$\frac{3}{3} \frac{x}{16.7}$		$\frac{3}{3} \frac{x}{73.0}$

$\frac{5}{7} \frac{x}{6.6}$	$\frac{8.5}{18.2}$	$\frac{5}{3.0} \frac{x}{6.5}$
$\frac{3}{3} \frac{x}{79.0}$		$\frac{3}{3} \frac{x}{72.0}$

$\frac{6}{1} \frac{x}{6.6}$	$\frac{4.4}{15.7}$	$\frac{8}{6} \frac{x}{11.9}$
$\frac{2}{2} \frac{x}{72.4}$		$\frac{6}{6} \frac{x}{70.4}$

$\frac{8}{5} \frac{x}{11.4}$	$\frac{11.8}{71.9}$	
$\frac{3}{2} \frac{x}{71.4}$		

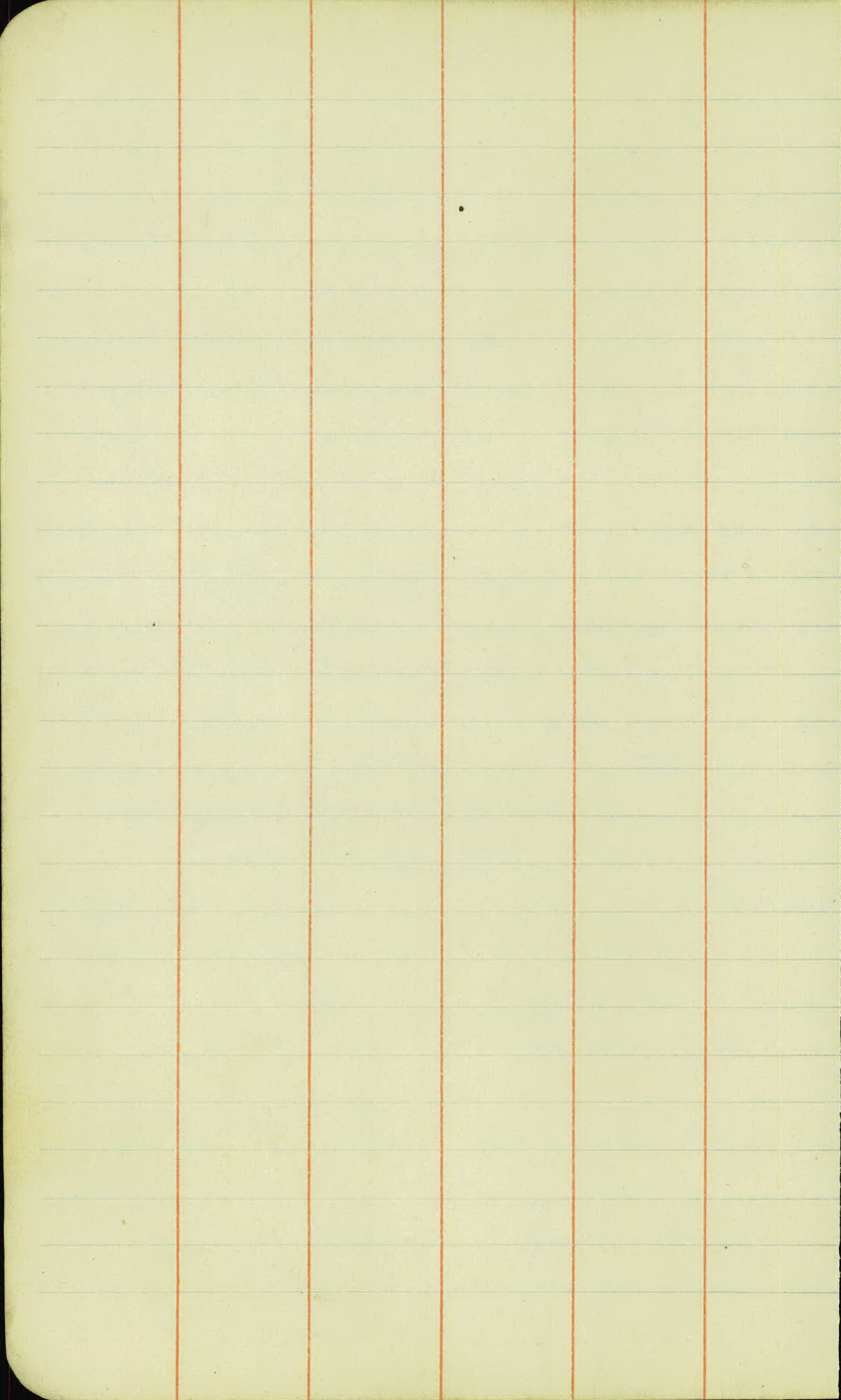
$\frac{4}{9} \frac{x}{4.7}$
$\frac{1}{1} \frac{x}{71.5}$

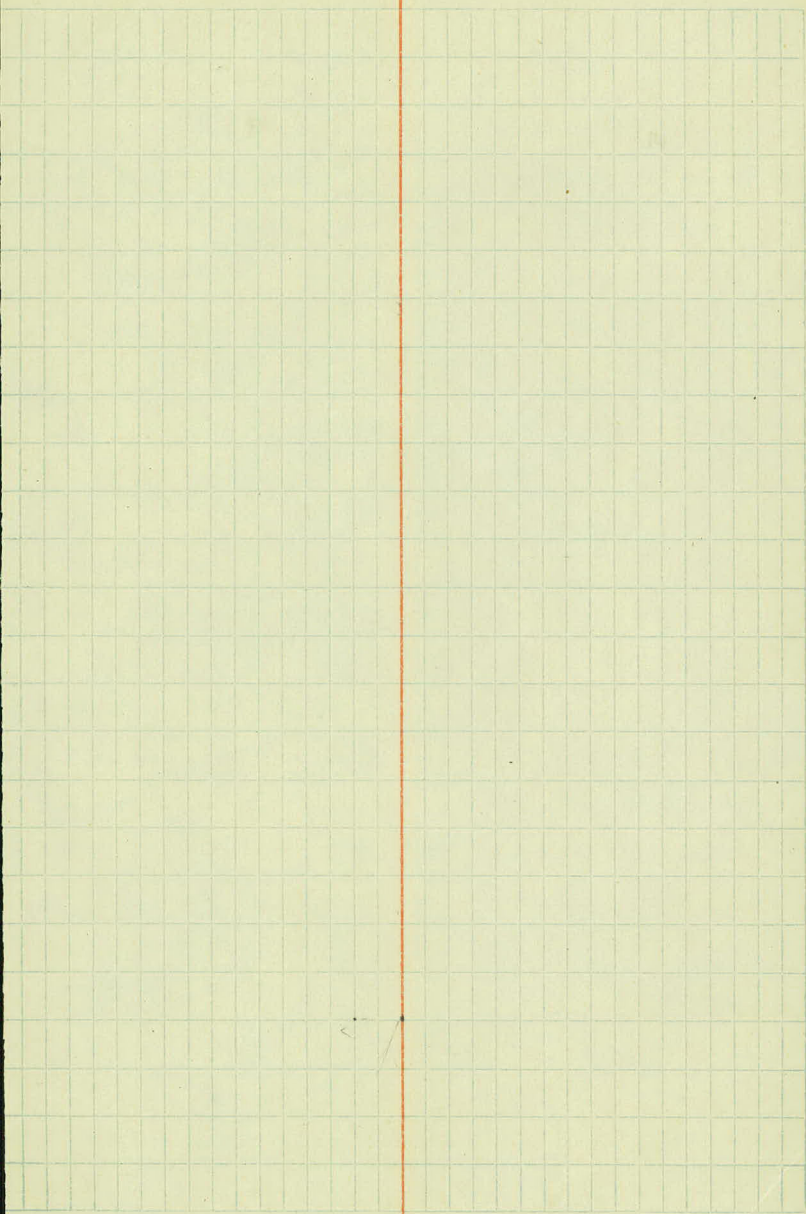
$\frac{4}{8} \frac{x}{7.4}$	$\frac{4.1}{11.4}$	$\frac{5}{5} \frac{x}{11.7}$
$\frac{1}{1} \frac{x}{72.7}$		$\frac{5}{2} \frac{x}{73.7}$

$\frac{4}{2} \frac{x}{3.5}$	$\frac{2.3}{0.3}$	
$\frac{2}{2} \frac{x}{4.7}$		

$\frac{9}{2} \frac{x}{5.5}$
$\frac{2}{2} \frac{x}{73.9}$

$\frac{4}{4} \frac{x}{4.2}$	$\frac{4.2}{0.0}$	$\frac{6}{6} \frac{x}{6.0}$
$\frac{1}{1} \frac{x}{0.6}$		$\frac{6}{1} \frac{x}{71.8}$



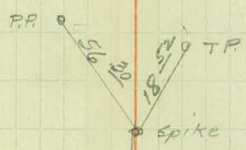


2

$$53 + 30.5$$

$$46 + 14.3$$

Rice St.



← Present Traveled Rd.

1/4 - 1/4 line →



B.M.	0.65	899.95		899.30
T.P.	2.27	894.71	7.51	892.44
46 + 14 <sup>3</sup>				89.7
+50				90.0
47				90.3
+50				90.5
48				91.1
+50				91.7
49				91.1
+50				90.4
50				89.7
T.P.	7.43	897.00	5.14	889.57
+50				89.8
51				90.6
+50				91.0

Left.

Right

spike in 10" Oct 80'So. Sta. 41 + 00

$\frac{7.6}{33}$   $\frac{7.6}{24}$   $\frac{8.2}{21}$   $\frac{8.5}{18}$   $\frac{5.2}{11}$  50  $\frac{5.7}{10}$   $\frac{8.6}{15}$   $\frac{8.7}{19}$   $\frac{8.0}{21}$   $\frac{8.7}{23}$   $\frac{9.7}{24}$   $\frac{9.5}{26}$   $\frac{8.2}{27}$   $\frac{7.8}{33}$

$\frac{7.5}{33}$   $\frac{7.5}{24}$   $\frac{8.0}{20}$   $\frac{8.0}{18}$   $\frac{4.8}{11}$  47  $\frac{5.2}{10}$   $\frac{8.3}{15}$   $\frac{8.0}{22}$   $\frac{9.8}{23}$   $\frac{9.8}{24}$   $\frac{8.2}{25}$   $\frac{7.8}{33}$

$\frac{7.4}{33}$   $\frac{7.3}{19}$   $\frac{4.5}{12}$  44  $\frac{5.1}{10}$   $\frac{7.8}{16}$   $\frac{7.5}{21}$   $\frac{10.4}{23}$   $\frac{10.7}{25}$   $\frac{7.8}{25}$   $\frac{7.7}{33}$

$\frac{7.5}{33}$   $\frac{7.7}{19}$   $\frac{4.2}{11}$  42  $\frac{4.8}{10}$   $\frac{8.0}{17}$   $\frac{7.5}{22}$   $\frac{10.5}{25}$   $\frac{10.5}{26}$   $\frac{8.0}{27}$   $\frac{7.7}{33}$

$\frac{7.2}{33}$   $\frac{7.7}{18}$   $\frac{3.7}{11}$  3.6  $\frac{4.2}{11}$   $\frac{7.5}{17}$   $\frac{7.5}{24}$   $\frac{11.0}{25}$   $\frac{11.0}{26}$   $\frac{1.8}{27}$   $\frac{7.8}{33}$

$\frac{6.9}{33}$   $\frac{6.2}{18}$   $\frac{3.0}{11}$   $\frac{3.3}{9}$  30  $\frac{3.5}{10}$   $\frac{7.3}{16}$   $\frac{7.2}{24}$   $\frac{11.2}{25}$   $\frac{11.2}{26}$   $\frac{7.8}{27}$   $\frac{7.2}{33}$

$\frac{7.6}{33}$   $\frac{7.5}{19}$   $\frac{3.8}{11}$  3.6  $\frac{4.0}{10}$   $\frac{7.7}{17}$   $\frac{7.0}{24}$   $\frac{11.4}{26}$   $\frac{11.4}{27}$   $\frac{7.7}{28}$   $\frac{7.4}{33}$

$\frac{7.5}{33}$   $\frac{8.7}{18}$   $\frac{4.5}{11}$   $\frac{4.6}{10}$  4.3  $\frac{4.9}{11}$   $\frac{8.5}{17}$   $\frac{7.5}{24}$   $\frac{11.0}{26}$   $\frac{11.0}{27}$   $\frac{8.7}{28}$   $\frac{8.7}{33}$

$\frac{8.8}{33}$   $\frac{7.8}{20}$   $\frac{8.8}{17}$   $\frac{5.5}{10}$  50  $\frac{5.4}{10}$   $\frac{8.6}{18}$   $\frac{8.1}{24}$   $\frac{11.2}{26}$   $\frac{11.2}{28}$   $\frac{8.6}{29}$   $\frac{8.3}{33}$

$\frac{10.0}{33}$   $\frac{10.5}{27}$   $\frac{12.0}{22}$   $\frac{11}{16}$   $\frac{7.8}{10}$  7.2  $\frac{7.9}{9}$   $\frac{7.7}{11}$   $\frac{11.4}{17}$   $\frac{10.7}{25}$   $\frac{13.0}{29}$   $\frac{10.2}{30}$   $\frac{11.2}{33}$

$\frac{10.0}{33}$   $\frac{10.4}{25}$   $\frac{11.8}{21}$   $\frac{10.4}{16}$   $\frac{6.8}{10}$  6.4  $\frac{6.9}{9}$   $\frac{8.7}{11}$   $\frac{10.8}{17}$   $\frac{10.7}{27}$   $\frac{13.2}{30}$   $\frac{12.8}{32}$   $\frac{10.7}{33}$

$\frac{10.0}{33}$   $\frac{10.4}{24}$   $\frac{11.7}{21}$   $\frac{10.2}{17}$   $\frac{6.4}{10}$  6.0  $\frac{6.3}{9}$   $\frac{6.2}{11}$   $\frac{11.0}{20}$   $\frac{10.0}{28}$   $\frac{10.5}{33}$

897.00 ✓

52

91.8

+50

93.0

53

94.8

+30.5

96.1

B.M.

6.27

890.73 ✓

Left

£

Right

$\frac{9.9}{33}$	$\frac{10.9}{24}$	$\frac{10.2}{19}$	$\frac{5.6}{10}$	52	$\frac{5.5}{10}$	$\frac{10.1}{19}$	$\frac{10.1}{29}$	$\frac{10.2}{33}$
------------------	-------------------	-------------------	------------------	----	------------------	-------------------	-------------------	-------------------

$\frac{10.0}{33}$	$\frac{10.3}{25}$	$\frac{9.0}{18}$	$\frac{4.4}{10}$	40	$\frac{4.2}{10}$	$\frac{10.2}{21}$	$\frac{9.7}{30}$	$\frac{10.0}{33}$
-------------------	-------------------	------------------	------------------	----	------------------	-------------------	------------------	-------------------

$\frac{9.8}{33}$	$\frac{8.0}{20}$	$\frac{2.7}{10}$	22	$\frac{2.6}{10}$	$\frac{8.0}{19}$	$\frac{9.3}{30}$	$\frac{7.8}{33}$
------------------	------------------	------------------	----	------------------	------------------	------------------	------------------

$\frac{8.0}{33}$	$\frac{6.2}{20}$	$\frac{1.2}{10}$	0.9	$\frac{1.3}{10}$	$\frac{7.2}{20}$	$\frac{8.0}{30}$	$\frac{8.0}{33}$
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Spike in P.P. Lt Sta 52 + 60

B.M.	0.42	899.72		899.30	
	3.00	895.14	7.56	892.16	
44				92.2	30
	+50			92.2	30
45				92.1	29
	+50			92.1	29
46				92.0	32
	+50			92.0	32
47				91.9	33
	+50			91.9	33
48				91.8	34
	+50			91.8	34
49				91.7	35
	3.15	894.80	3.51	891.65	

$$\frac{28}{102}$$

$$\begin{array}{r} 6 \times \\ 4 \overline{) 78} \\ \underline{2} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{3.3}{-0.3}$$

$$\begin{array}{r} 0 \times \\ 2 \overline{) 7.4} \\ \underline{4} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.3} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 2 \overline{) 8.0} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{3.8}{-0.9}$$

$$\begin{array}{r} \times \\ 2 \overline{) 8.0} \\ \underline{4} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.3} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 6 \overline{) 8.4} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{4.6}{-1.7}$$

$$\begin{array}{r} \times \\ 4 \overline{) 8.8} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.6} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.2} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{5.0}{-1.8}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.7} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 4 \overline{) 8.1} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{5.1}{-1.9}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.5} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 4 \overline{) 7.9} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{4.8}{-1.5}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.5} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 4 \overline{) 7.9} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{4.6}{-1.3}$$

$$\begin{array}{r} \times \\ 5 \overline{) 8.5} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 4 \overline{) 7.7} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{4.1}{-0.7}$$

$$\begin{array}{r} \times \\ 4 \overline{) 8.3} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 2 \overline{) 6.9} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{3.4}{0.0}$$

$$\begin{array}{r} \times \\ 4 \overline{) 7.9} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\begin{array}{r} \times \\ 4 \overline{) 8.1} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

$$\frac{4.1}{-0.6}$$

$$\begin{array}{r} \times \\ 5 \overline{) 7.8} \\ \underline{10} \phantom{0} \\ 2 \phantom{0} \phantom{0} \\ \hline \end{array}$$

894.80

f50

91.7

3.1

50

91.6

3.4

f50

91.6

3.2

51

91.5

3.3

f50

91.7

3.1

52

92.3

2.5

B.M.

4.07

890.73

890.73

51+22 X DRAIN 18" X 40' C.M.

EXTENDS 20<sup>5</sup>' LT.

" 19<sup>5</sup>' RT.

$$\begin{array}{r} 8 \overline{) 80} \\ 4 \overline{) 49} \end{array}$$

$$\begin{array}{r} 44 \\ -1.5 \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.1} \\ 5 \overline{) 50} \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.7} \\ 5 \overline{) 55} \end{array}$$

$$\begin{array}{r} 5.0 \\ -1.8 \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.2} \\ 5 \overline{) 50} \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.6} \\ 5 \overline{) 54} \end{array}$$

$$\begin{array}{r} 5.0 \\ -1.8 \end{array}$$

$$\begin{array}{r} 8 \overline{) 8.1} \\ 4 \overline{) 49} \end{array}$$

$$\begin{array}{r} 6 \overline{) 8.1} \\ 4 \overline{) 48} \end{array}$$

$$\begin{array}{r} 4.8 \\ -0.9 \end{array}$$

$$\begin{array}{r} 6 \overline{) 8.1} \\ 4 \overline{) 48} \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.1} \\ 5 \overline{) 50} \end{array}$$

$$\begin{array}{r} 3.8 \\ -0.7 \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.2} \\ 5 \overline{) 51} \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.3} \\ 5 \overline{) 58} \end{array}$$

$$\begin{array}{r} 3.0 \\ -0.5 \end{array}$$

$$\begin{array}{r} 0 \overline{) 8.2} \\ 5 \overline{) 57} \end{array}$$

$$\begin{array}{r} 30.5 \\ 19.5 \\ \hline 600 \end{array}$$

STA.	+	H.I.	-	ELEV.
B.M.	7.01	726.57		919.56
0+00				23.9
+17				23.7
+25				23.5
+95	CROSS DRAIN 24" X 5' P <sup>3</sup>			
1+00				22.2
+50				21.5
+90				21.3
2+00				20.8
+50				20.0
+80				19.4
	3.74	723.51	6.80	919.77
3+00				19.1
+50				18.6

LT.

RT.

7-17-50

SPLIT IN 12" OAK. 00 LT. SP. OF 30

41	(3.0)	14
<u>33</u>	2.7	<u>33</u>

5.8	4.8	3.7	(3.3)	2.5	2.1	1.6
<u>5.0</u>	<u>3.8</u>	<u>1.5</u>	2.9	14	<u>33</u>	<u>50</u>

9.6	5.4	5.9	(3.4)	2.7	2.4	4.8
<u>51</u>	<u>39</u>	<u>14</u>	3.1	17	<u>33</u>	<u>46</u>

13.85
<u>51</u>

11.1
<u>23</u>

1.50	4.6	(4.5)	4.4	10.6	10.7
<u>34</u>	<u>13</u>	4.4	13	<u>26</u>	<u>33</u>

10.3	8.9	5.2	(4.7)	5.0	8.4	2.6	5.6	5.6
<u>33</u>	<u>22</u>	<u>13</u>	5.1	13	20	<u>24</u>	<u>27</u>	<u>33</u>

7.7	6.6	7.2	7.1	5.7	(5.3)	5.4	8.5	2.5	5.2	5.4
<u>33</u>	<u>21</u>	<u>19</u>	<u>16</u>	<u>13</u>	5.3	12	19	<u>22</u>	<u>26</u>	<u>33</u>

6.7	6.2	2.0	7.9	6.0	(5.9)	5.9	2.9	9.0	7.3	6.9
<u>33</u>	<u>23</u>	<u>21</u>	<u>18</u>	<u>13</u>	5.8	13	18	<u>23</u>	<u>24</u>	<u>33</u>

13.5	12.0	6.7	(6.1)	6.8	7.8	7.5
<u>33</u>	<u>14</u>	<u>13</u>	6.6	13	19	<u>33</u>

14.6	7.3	(7.0)	7.4	10.0	10.0
<u>33</u>	<u>13</u>	7.2	13	18	<u>33</u>

12.9	4.5	(4.2)	4.4	6.6	6.6	6.5
<u>33</u>	<u>13</u>	4.4	13	<u>11</u>	<u>22</u>	<u>33</u>

3.8	3.0	7.1	7.1	4.9	(4.9)	5.2	7.0	7.2	2.0	2.1
<u>33</u>	<u>26</u>	<u>20</u>	<u>14</u>	<u>13</u>	4.9	13	17	<u>22</u>	<u>29</u>	<u>33</u>

STA.	+	M.I.	-	ELEV
		923.51 ✓		
4+00				17.9
	+50			17.3
5+00				16.5
	+50			15.7
6+00				15.1
	+50			
	10.96	930.73 ✓	3.74	719.77 ✓
4+00				
	+50			
5+00				
	+50			
6+00				
	1.25	918.56 ✓	13.42	917.31 ✓
	+50			12.4
7+00				13.5
	2.78	915.56 ✓	5.78	912.78 ✓

LT

RT

$\frac{76}{20}$	$\frac{74}{16}$	$\frac{56}{13}$	(4.6)	$\frac{56}{13}$	$\frac{72}{16}$	$\frac{74}{21}$	$\frac{0.6}{32}$	$\frac{0.6}{33}$
-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{82}{19}$	$\frac{81}{16}$	$\frac{63}{13}$	(6.3)	$\frac{63}{13}$	$\frac{77}{17}$	$\frac{77}{21}$
-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------

$\frac{86}{19}$	$\frac{86}{15}$	$\frac{71}{13}$	(7.0)	$\frac{71}{13}$	$\frac{87}{16}$	$\frac{87}{21}$
-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------

$\frac{73}{19}$	$\frac{72}{15}$	$\frac{77}{13}$	(7.7)	$\frac{77}{13}$	$\frac{91}{15}$	$\frac{90}{20}$
-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------

$\frac{101}{19}$	$\frac{100}{15}$	$\frac{86}{13}$	(8.4)	$\frac{85}{13}$	$\frac{99}{17}$	$\frac{99}{21}$	$\frac{3.3}{32}$	$\frac{3.4}{33}$
------------------	------------------	-----------------	-------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{67}{33}$	$\frac{67}{32}$	(12.8)
-----------------	-----------------	--------

$\frac{63}{35}$	$\frac{63}{33}$	(3.3)	$\frac{63}{33}$	$\frac{64}{35}$
-----------------	-----------------	-------	-----------------	-----------------

$\frac{40}{35}$	$\frac{41}{33}$	(4.7)	$\frac{43}{33}$	$\frac{43}{35}$
-----------------	-----------------	-------	-----------------	-----------------

$\frac{19}{35}$	$\frac{22}{33}$	(11.9)	$\frac{63}{33}$	$\frac{64}{35}$
-----------------	-----------------	--------	-----------------	-----------------

$\frac{74}{35}$	$\frac{75}{33}$	(15.1)
-----------------	-----------------	--------

$\frac{10}{33}$	$\frac{15}{29}$	$\frac{62}{20}$	$\frac{60}{14}$	$\frac{43}{13}$	(4.7)	$\frac{44}{13}$	$\frac{61}{17}$	$\frac{61}{21}$	$\frac{2.3}{28}$	$\frac{2.2}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------	------------------	------------------

$\frac{73}{33}$	$\frac{74}{23}$	$\frac{73}{19}$	$\frac{55}{13}$	(4.9)	$\frac{56}{13}$	$\frac{67}{16}$	$\frac{67}{22}$	$\frac{66}{24}$	$\frac{5.6}{33}$
-----------------	-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------	-----------------	------------------

STA.	+	H.I	-	ELEV
		915.56		
7+50				12.1
8+00				10.3
8+00	CROSS DRAIN 24" X 54" P <sup>s</sup>			
8+50				9.0
9+00				8.4
+50				8.2
10+00				8.0
+50				8.9
11+00				10.3
+50				11.9
	9.67	925.90	1.33	914.23
12+00				13.9
+50				16.2
13+00				18.4

LT.

RT.

<u>91</u>	<u>83</u>	<u>37</u>	<u>9.0</u>	<u>4.0</u>	<u>75</u>	<u>76</u>
53	24	13	3.5	13	22	33

<u>9.6</u>	<u>118</u>	<u>118</u>	<u>71</u>	<u>80</u>	<u>5.3</u>	<u>6.7</u>	<u>5.9</u>	<u>88</u>	<u>9.0</u>	<u>11.6</u>	<u>11.6</u>	<u>91</u>
56	52	30	25	22	13	5.3	13	21	27	50	52	36

13.05

12.50

<u>64</u>	<u>10.9</u>	<u>10.9</u>	<u>85</u>	<u>79</u>	<u>78</u>	<u>6.7</u>	<u>4.0</u>	<u>20</u>	<u>27</u>	<u>78</u>	<u>9.0</u>	<u>11.2</u>	<u>11.2</u>	<u>85</u>
40	32	31	28	24	16	13	6.2	13	19	23	27	29	31	35

<u>47</u>	<u>10.6</u>	<u>10.6</u>	<u>77</u>	<u>64</u>	<u>76</u>	<u>75</u>	<u>4.7</u>	<u>7.6</u>	<u>8.2</u>	<u>7.6</u>	<u>8.8</u>	<u>11.1</u>	<u>11.2</u>	<u>6.7</u>
41	33	31	28	24	14	13	7.2	13	16	23	26	28	30	37

<u>6.2</u>	<u>10.4</u>	<u>10.4</u>	<u>8.3</u>	<u>7.9</u>	<u>8.5</u>	<u>7.7</u>	<u>5.2</u>	<u>7.6</u>	<u>8.7</u>	<u>7.2</u>	<u>7.9</u>	<u>11.0</u>	<u>11.1</u>	<u>6.9</u>
38	31	30	27	21	16	13	7.4	13	17	24	27	29	31	38

<u>8.1</u>	<u>10.2</u>	<u>10.2</u>	<u>71</u>	<u>71</u>	<u>8.4</u>	<u>7.5</u>	<u>5.7</u>	<u>8.0</u>	<u>9.1</u>	<u>7.8</u>	<u>8.7</u>	<u>11.1</u>	<u>11.0</u>	<u>8.1</u>
36	31	30	28	25	17	13	7.6	13	18	24	26	30	32	36

<u>9.5</u>	<u>10.5</u>	<u>10.4</u>	<u>9.8</u>	<u>8.9</u>	<u>6.7</u>	<u>4.7</u>	<u>7.0</u>	<u>9.7</u>	<u>9.7</u>	<u>10.5</u>	<u>10.5</u>	<u>9.1</u>
34	32	27	27	20	13	6.7	13	19	27	30	32	35

<u>9.1</u>	<u>8.8</u>	<u>5.4</u>	<u>3.8</u>	<u>5.6</u>	<u>9.4</u>	<u>9.4</u>
33	23	13	5.3	13	22	33

<u>4.5</u>	<u>4.6</u>	<u>5.1</u>	<u>5.1</u>	<u>5.7</u>	<u>7.3</u>	<u>5.7</u>	<u>8.6</u>	<u>9.0</u>
33	22	20	16	13	3.7	13	26	33

<u>3.1</u>	<u>2.7</u>	<u>11.7</u>	<u>11.6</u>	<u>10.0</u>	<u>4.9</u>	<u>10.1</u>	<u>11.7</u>	<u>11.9</u>	<u>10.6</u>	<u>11.9</u>
35	33	20	16	13	10.0	13	14	21	22	33

<u>0.0</u>	<u>0.2</u>	<u>9.7</u>	<u>9.4</u>	<u>7.8</u>	<u>6.7</u>	<u>7.9</u>	<u>9.6</u>	<u>9.6</u>	<u>3.7</u>	<u>4.2</u>
35	34	19	14	13	7.7	13	17	20	29	33

<u>10.2</u>	<u>0.0</u>	<u>7.4</u>	<u>7.3</u>	<u>5.6</u>	<u>4.6</u>	<u>5.9</u>	<u>7.4</u>	<u>7.6</u>	<u>0.7</u>	<u>1.0</u>
33	32	21	18	13	5.5	13	14	20	30	33

STA.	f	H.I.	-	ELEV	
		923.90			
13 +50				20.4	
	11.71	934.48	1.13	922.77	
14 +00				24.5	
				24.0	
15 +00				25.5	
				26.2	
16 +00				26.5	
P.M.	3.97	934.06	4.45	930.05	930.07
	130			26.5	
17				25.7	
				25.1	
				24.2	
18				22.7	
				21.4	

LT.

RT.

7-17-30

10.7 10.4 4.9 4.9 3.5 7.2 3.5 5.1 5.1 0.3 0.3  
 33 29 20 17 13 3.5 13 14 20 27 33

10.5 11.2 13.7 13.7 12.1 10.9 12.3 14.1 14.2 12.2 11.8  
 33 24 20 17 13 12.1 13 14 19 22 33

7.5 8.0 12.2 12.2 10.6 8.8 10.7 12.7 12.7 10.6 9.5  
 29 25 20 14 13 10.5 13 14 19 23 33 DRIVE WAY

2.7 2.9 11.0 11.0 9.2 11.1 9.7 11.2 11.3 5.2 4.9  
 33 31 19 16 13 9.0 13 16 19 28 33

3.8 4.0 10.5 10.3 8.5 5.9 8.7 10.5 10.5 5.4 5.2  
 33 27 19 14 13 8.3 13 14 18 26 33

5.4 5.2 10.0 9.9 8.3 5.7 8.5 10.2 10.3 4.8 4.4  
 33 26 20 14 13 8.0 13 16 18 26 33

5.7 5.4 9.4 9.5 7.7 5.6 7.7 9.6 9.7 3.5 3.3  
 33 26 19 14 13 7.4 13 14 19 26 33

3.2 3.2 10.5 10.5 8.4 11.0 8.5 10.4 10.4 4.7 4.5  
 33 30 20 14 13 8.4 13 17 20 27 33

2.7 2.7 11.2 11.2 9.1 7.6 9.0 11.2 11.3 3.8 3.8  
 33 31 20 16 13 9.0 13 17 20 30 33

4.2 4.2 11.8 11.8 10.1 10.8 9.9 12.0 12.0 5.4 5.3  
 33 29 20 16 13 9.9 13 17 21 30 33

9.4 9.3 13.2 13.1 11.2 11.3 11.5 13.2 13.3 6.3 5.9  
 33 24 20 14 13 11.4 13 17 21 30 33

11.2 11.2 14.7 14.7 12.8 12.7 12.7 14.7 14.7 8.8 8.7  
 33 24 21 17 13 12.7 13 17 22 29 33

STA	t	H.I	-	FLEV
		734.05 ✓		20.3
	1.45	722.49 ✓	13.02	721.04 ✓
19				18.4
	1.50			16.2
20				14.5
	1.50			13.1
	3.58	915.57 ✓	10.50	911.79 ✓
21				11.8
	1.40	915.59 ✓	1.40	914.17 ✓
	1.50			10.7
22				9.6
	1.50			9.1
23				8.5
	1.50			8.0
24				7.7 ✓
	4.52	912.52 ✓	7.59	908.00 ✓

L.T.

R.T.

7-21-36

114	117	158	158	140	13.1	13.8	15.8	158	10.6	10.6
33	26	21	16	13	13.8	13	17	21	28	33

52	54	60	60	45	3.2	3.8	5.9	60	11	0.9
33	23	22	17	13	4.1	13	17	21	26	33

115	111	97	106	105	95	66	5.3	6.3	7.2	9.3	63	5.4
33	26	24	23	22	21	13	6.3	13	16	21	23	33

12.9	12.7	8.2	7.3	8.2	10.9	10.8	10.4
33	25	13	8.0	13	18	22	33

13.0	13.6	9.3	9.0	9.6	12.5	12.5
33	23	13	9.4	13	19	33

60	60	60	39	3.6	3.9	5.7	5.8	5.8
33	25	20	13	3.8	13	18	26	33

5.9	6.2	6.8	6.5	4.9	4.8	7.0	7.0	5.9	5.9	
33	25	22	18	13	4.9	13	19	23	24	33

61	62	70	7.8	7.6	61	5.8	7.6	7.7	5.9	5.8	
33	27	23	20	17	13	6.0	13	18	22	24	33

5.0	5.8	8.0	8.1	6.5	6.6	6.4	8.0	8.0	4.8	4.5
33	23	21	17	13	6.5	13	18	21	27	33

2.2	2.2	7.9	8.8	7.2	7.1	7.0	8.6	8.7	4.3	5.9
33	31	20	17	13	7.1	13	18	21	29	33

5.4	5.8	9.8	9.5	8.0	7.7	7.6	7.6	9.5	9.5	6.9	6.5
33	28	20	17	13	7.6	13	17	21	25	33	

11.5	11.9	12.6	12.6	11.1	7.9	8.0	11.5	11.5	9.6	9.2	
33	27	26	25	20	13	7.9	13	20	23	25	33

STA.	+	M.I.	-	ELEV.
		712.32		
24	+50			7.9
	160 CROSS DRAIN 24" X 48 10 <sup>3</sup>			
25				8.2
25	+50			8.9
26				10.1
26	+50			11.2
27		12.45	924.38	0.39
				711.73
27				12.9
27	+50			15.3
28				17.7
28	+50			20.1
29				22.1
		9.63	932.74	1.27
				723.11
28				

LT

RT

7-21-30

$\frac{128}{33}$   $\frac{12.2}{28}$   $\frac{4.8}{13}$   $\frac{4.8}{4.4}$   $\frac{44}{13}$   $\frac{9.2}{23}$   $\frac{104}{24}$   $\frac{106}{26}$   $\frac{24}{30}$   $\frac{8.1}{33}$   
 $\frac{136}{33}$   $\frac{13.5}{28}$   $\frac{4.2}{13}$   $\frac{4.5}{4.1}$   $\frac{59}{13}$   $\frac{11.4}{28}$   $\frac{12.1}{29}$   $\frac{12.2}{31}$   $\frac{11.2}{32}$   $\frac{11.2}{33}$

$\frac{13.4}{33}$   $\frac{13.1}{30}$   $\frac{3.6}{13}$   $\frac{3.9}{3.4}$   $\frac{3.2}{13}$   $\frac{11.6}{29}$   $\frac{11.7}{33}$

$\frac{130}{33}$   $\frac{128}{33}$   $\frac{24}{13}$   $\frac{2.7}{2.2}$   $\frac{2.1}{13}$   $\frac{9.2}{28}$   $\frac{9.5}{33}$

$\frac{132}{35}$   $\frac{13.0}{33}$   $\frac{1.4}{13}$   $\frac{1.7}{1.1}$   $\frac{10}{13}$   $\frac{4.6}{23}$   $\frac{5.7}{31}$   $\frac{5.7}{33}$

$\frac{10.9}{33}$   $\frac{10.9}{31}$

$\frac{11.7}{13}$   $\frac{11.5}{11.5}$   $\frac{11.6}{13}$   $\frac{13.0}{17}$   $\frac{13.2}{22}$   $\frac{9.4}{25}$   $\frac{8.7}{33}$

$\frac{10.8}{33}$   $\frac{10.0}{24}$   $\frac{11.2}{20}$   $\frac{11.3}{14}$   $\frac{9.5}{13}$   $\frac{9.1}{9.1}$   $\frac{9.2}{13}$   $\frac{10.5}{16}$   $\frac{10.6}{20}$   $\frac{0.0}{33}$

$\frac{0.7}{35}$   $\frac{0.6}{33}$   $\frac{9.0}{22}$   $\frac{8.9}{17}$   $\frac{7.0}{13}$   $\frac{6.7}{6.7}$   $\frac{7.0}{13}$   $\frac{8.4}{14}$   $\frac{8.5}{18}$   $\frac{1.5}{24}$

$\frac{6.0}{22}$   $\frac{6.2}{17}$   $\frac{4.6}{13}$   $\frac{4.5}{4.5}$   $\frac{4.7}{13}$   $\frac{6.5}{16}$   $\frac{6.6}{17}$   $\frac{0.1}{24}$

$\frac{4.2}{22}$   $\frac{4.2}{17}$   $\frac{2.6}{13}$   $\frac{2.3}{2.3}$   $\frac{2.6}{13}$   $\frac{4.3}{14}$   $\frac{4.4}{19}$   $\frac{0.1}{23}$

$\frac{3.4}{34}$   $\frac{3.4}{35}$

STA	+	H.I.	-	ELEV
		732.74		
28+50				
29				
29+50				24.1
30				25.9
30+50				27.4
31				27.9
31+50				27.7
32				27.8
	11.95	940.52	4.37	928.37
29+50				
30				
30+50				
31+00				

L.T.

R.T.

7-21-30

$$\frac{80}{35} \quad \frac{78}{32}$$

12.8

$$\frac{2.6}{33} \quad \frac{2.7}{35}$$

$$\frac{74}{33} \quad \frac{68}{29}$$

10.4

$$\frac{1.5}{33} \quad \frac{1.5}{35}$$

$$\frac{58}{33} \quad \frac{55}{38} \quad \frac{10.2}{22} \quad \frac{10.2}{17} \quad \frac{8.7}{13} \quad \frac{8.7}{13} \quad \frac{9.1}{13} \quad \frac{10.7}{16} \quad \frac{10.8}{19} \quad \frac{6.1}{24}$$

8.5

$$\frac{70}{33} \quad \frac{68}{34} \quad \frac{8.6}{22} \quad \frac{8.6}{17} \quad \frac{6.7}{13} \quad \frac{6.7}{13} \quad \frac{6.9}{13} \quad \frac{8.6}{17} \quad \frac{8.6}{20} \quad \frac{4.6}{26}$$

6.0

$$\frac{7.7}{33} \quad \frac{7.0}{33} \quad \frac{7.7}{32} \quad \frac{7.7}{18} \quad \frac{5.1}{13} \quad \frac{5.1}{13} \quad \frac{5.5}{5.5} \quad \frac{7.2}{13} \quad \frac{7.3}{16} \quad \frac{3.8}{19} \quad \frac{3.8}{24}$$

3.4

$$\frac{7.8}{33} \quad \frac{7.0}{24} \quad \frac{7.4}{23} \quad \frac{7.2}{18} \quad \frac{5.1}{13} \quad \frac{5.1}{13} \quad \frac{4.8}{4.8} \quad \frac{5.0}{13} \quad \frac{6.7}{16} \quad \frac{6.8}{19} \quad \frac{1.7}{24}$$

4.8

$$\frac{9.3}{33} \quad \frac{8.1}{22} \quad \frac{7.4}{20} \quad \frac{6.7}{17} \quad \frac{5.2}{13} \quad \frac{5.2}{13} \quad \frac{4.9}{5.0} \quad \frac{9.0}{13} \quad \frac{6.8}{17} \quad \frac{6.8}{21}$$

4.0

$$\frac{10.0}{33} \quad \frac{9.0}{21} \quad \frac{5.0}{13} \quad \frac{4.9}{4.9} \quad \frac{5.0}{13} \quad \frac{6.5}{17} \quad \frac{6.7}{22} \quad \frac{2.6}{28} \quad \frac{2.3}{23}$$

6.0

15.8

$$\frac{6.5}{34} \quad \frac{6.5}{33}$$

14.2

$$\frac{6.7}{33} \quad \frac{6.5}{35}$$

13.0

$$\frac{4.4}{37} \quad \frac{4.4}{35}$$

12.4

$$\frac{3.3}{33} \quad \frac{3.3}{33}$$

STA	+	H.I.	-	ELEV.
		940.52		
31+50				
	2.26	930.63	11.95	928.37
32+50				27.3
33+00				26.7
33+50				25.9
34+00				25.2
34+50				24.9
35+00				24.3
B.M.	3.61	929.70	4.54	926.09
35+50				23.6
36+00				23.0
36+50				22.5
37+00				22.0
37+50				21.2

LT.

RT.

7-21-30

(12)

$$\frac{6.6}{31} \quad \frac{6.4}{33}$$

$$\frac{6.3}{33} \quad \frac{5.8}{18} \quad \frac{3.6}{13} \quad \frac{3.5}{33} \quad \frac{5.4}{13} \quad \frac{5.4}{17} \quad \frac{2.1}{22} \quad \frac{1.3}{26} \quad \frac{1.3}{33}$$

$$\frac{6.9}{33} \quad \frac{6.8}{19} \quad \frac{6.3}{18} \quad \frac{4.1}{13} \quad \frac{4.1}{39} \quad \frac{5.7}{13} \quad \frac{5.8}{16} \quad \frac{4.6}{22} \quad \frac{4.3}{24} \quad \frac{4.3}{33}$$

$$\frac{8.2}{33} \quad \frac{8.4}{20} \quad \frac{4.7}{13} \quad \frac{4.7}{4.7} \quad \frac{5.0}{13} \quad \frac{7.1}{17} \quad \frac{7.3}{21} \quad \frac{6.7}{23} \quad \frac{7.0}{33}$$

$$\frac{7.8}{33} \quad \frac{8.1}{21} \quad \frac{5.3}{13} \quad \frac{5.3}{5.4} \quad \frac{5.5}{13} \quad \frac{7.8}{17} \quad \frac{8.1}{21} \quad \frac{7.7}{22} \quad \frac{7.9}{33}$$

$$\frac{6.1}{33} \quad \frac{6.3}{24} \quad \frac{7.8}{22} \quad \frac{7.7}{18} \quad \frac{5.9}{13} \quad \frac{5.9}{5.7} \quad \frac{6.0}{13} \quad \frac{8.0}{17} \quad \frac{8.2}{21} \quad \frac{7.8}{22} \quad \frac{7.7}{33}$$

$$\frac{3.2}{33} \quad \frac{3.8}{28} \quad \frac{8.2}{23} \quad \frac{8.1}{19} \quad \frac{6.2}{13} \quad \frac{6.2}{6.3} \quad \frac{6.6}{13} \quad \frac{8.6}{17} \quad \frac{8.7}{21} \quad \frac{7.6}{22} \quad \frac{7.9}{33}$$

$$\frac{6.7}{33} \quad \frac{3.0}{25} \quad \frac{7.6}{23} \quad \frac{7.6}{18} \quad \frac{5.8}{13} \quad \frac{6.1}{6.1} \quad \frac{6.4}{13} \quad \frac{10.9}{24} \quad \frac{11.4}{29} \quad \frac{12.9}{33}$$

$$\frac{2.4}{33} \quad \frac{2.7}{29} \quad \frac{7.9}{23} \quad \frac{8.2}{14} \quad \frac{6.1}{13} \quad \frac{6.1}{6.7} \quad \frac{7.3}{14} \quad \frac{13.4}{26} \quad \frac{15.1}{33}$$

$$\frac{1.3}{33} \quad \frac{1.3}{32} \quad \frac{8.3}{23} \quad \frac{8.6}{17} \quad \frac{6.3}{13} \quad \frac{7.4}{7.2} \quad \frac{8.3}{15} \quad \frac{10.3}{20} \quad \frac{10.6}{24} \quad \frac{10.2}{26} \quad \frac{12.1}{33}$$

$$\frac{11.3}{33} \quad \frac{8.5}{21} \quad \frac{9.2}{17} \quad \frac{7.0}{13} \quad \frac{7.0}{7.7} \quad \frac{7.1}{16} \quad \frac{11.0}{21} \quad \frac{11.4}{26} \quad \frac{7.8}{31} \quad \frac{8.3}{33}$$

$$\frac{2.9}{33} \quad \frac{5.3}{31} \quad \frac{10.1}{21} \quad \frac{10.1}{17} \quad \frac{7.7}{13} \quad \frac{7.7}{8.5} \quad \frac{10.2}{10} \quad \frac{11.8}{19} \quad \frac{12.2}{24} \quad \frac{9.1}{29} \quad \frac{9.9}{33}$$

STATION	T	H. I.	-	ELEV
38		929.70		
38 + 50				
39				
T.P.	2.81	921.94	10.57	919.13
38 + 50				17.7
39				15.0
39 + 50				11.5
	5.44	919.72	12.66	909.28
40				8.3
40 + 50				4.2
	0.06	901.61	13.17	901.55
40 + 50				
41				900.4
41 + 55				896.9
41 + 75				95.9

LT

RT

7-21-30

$\frac{2.4}{35}$	$\frac{2.5}{33}$	$\frac{11.5}{23}$	$\frac{11.4}{17}$	$\frac{9.3}{13}$	(10)	$\frac{11.6}{17}$	$\frac{13.3}{20}$	$\frac{13.5}{24}$	$\frac{9.4}{31}$	$\frac{9.8}{33}$
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$\frac{4.6}{35}$	$\frac{4.6}{34}$
------------------	------------------

(11)

$\frac{5.0}{40}$	$\frac{5.0}{37}$
------------------	------------------

(13.9)

$\frac{5.4}{23}$	$\frac{5.2}{17}$	$\frac{3.3}{13}$	(40)	$\frac{5.6}{15}$	$\frac{7.4}{18}$	$\frac{7.7}{24}$	$\frac{2.9}{31}$	$\frac{3.7}{33}$
------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{7.6}{24}$	$\frac{7.6}{16}$	$\frac{6.1}{13}$	(61)	$\frac{8.3}{16}$	$\frac{9.9}{19}$	$\frac{10.4}{24}$	$\frac{6.7}{30}$	$\frac{7.5}{33}$
------------------	------------------	------------------	------	------------------	------------------	-------------------	------------------	------------------

$\frac{6.5}{40}$	$\frac{6.6}{37}$	$\frac{7.2}{33}$	$\frac{7.3}{27}$	$\frac{11.0}{17}$	$\frac{11.3}{17}$	$\frac{9.4}{14}$	(8.4)	$\frac{11.6}{15}$	$\frac{13.1}{18}$	$\frac{13.5}{22}$	$\frac{11.4}{25}$	$\frac{13.7}{33}$
------------------	------------------	------------------	------------------	-------------------	-------------------	------------------	-------	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{1.2}{33}$	$\frac{1.8}{30}$	$\frac{3.7}{28}$	$\frac{4.1}{27}$	$\frac{7.0}{22}$	$\frac{7.0}{16}$	$\frac{5.6}{14}$	(44)	$\frac{8.1}{16}$	$\frac{9.7}{20}$	$\frac{10.8}{25}$	$\frac{12.6}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------	------------------	------------------	-------------------	-------------------

$\frac{13.0}{33}$	$\frac{13.0}{23}$	$\frac{11.7}{17}$	$\frac{9.9}{13}$	(76)	$\frac{12.0}{16}$
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~~55~~

$\frac{3.9}{29}$	$\frac{4.2}{33}$
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$\frac{5.2}{39}$	$\frac{5.2}{22}$	$\frac{1.1}{13}$	(23)	$\frac{2.0}{15}$	$\frac{4.9}{23}$	$\frac{5.4}{27}$	$\frac{6.1}{28}$	$\frac{6.1}{30}$	$\frac{5.1}{31}$	$\frac{4.4}{33}$
------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.5}{33}$	$\frac{6.1}{25}$	$\frac{5.2}{13}$	(10)	$\frac{5.0}{13}$	$\frac{6.4}{22}$	$\frac{7.4}{31}$	$\frac{7.4}{26}$	$\frac{4.9}{29}$	$\frac{4.5}{33}$
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$\frac{7.5}{33}$	$\frac{6.4}{13}$	(21)	$\frac{5.5}{18}$	$\frac{5.0}{33}$
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STA.	+	H. I	-	ELEV.
		901.61		
42				94.7
42+50				93.4
43				93.0
43+50				92.6
44+00				92.2
	3.47	895.59	9.49	892.12
44+50				92.1
45+00				91.6
46+14 <sup>3</sup>				91.0
46+50				91.0
47+00				91.0
47+50				91.1
48+00				91.3

LT

PT

7-21-50

120	111	82	76	34	66	80	80	67	68
33	30	20	8	6.9	21	25	28	30	33

138	124	25	96	28	90	90	81	81
33	14	9	8.2	21	25	31	33	35

102	87	96	90	72	85	96	96	91	91
33	14	10	8	8.6	21	25	31	32	33

3.1	30	42	46	78	90	89	9.0	8.7	10.1	9.9	9.4	9.4
33	28	26	23	13	12	9	9.0	21	25	30	32	33

90	85	90	93	10.1	9.2	10.3	10.4	10.2	10.9
33	19	15	9	9.4	21	24	28	29	33

79	73	81	82	3.9	4.8	3.7	8.6	8.6
33	25	23	19	10	3.5	20	28	33

88	88	90	44	5.3	4.4	8.8	8.9
33	23	19	9	4.0	21	28	33

8.9	9.4	5.1	5.9	5.0	9.7	9.1
33	23	15	4.4	15	23	33

8.6	8.1	4.9	5.6	5.0	9.5	9.2
33	25	15	4.6	15	23	33

8.4	8.4	4.3	5.3	5.0	9.2	9.0
33	25	15	4.4	15	23	33

8.4	8.6	4.4	5.7	4.8	9.1	9.0
33	24	15	4.5	15	23	33

8.0	8.2	4.2	4.3	4.8	9.4	8.7
33	25	15	4.3	15	25	33

STA.	+	H.I.	-	ELEV.	-
		895.59 <sup>✓</sup>			
48+50				91.7	
49+00				91.1	
49+50				90.3	
	5.42	895.50 <sup>✓</sup>	5.51	890.08 <sup>✓</sup>	
50+00				89.7	
50+50				89.7	
51+00				90.5	
51+50				91.0	
52+00				91.8	
52+50				892.1	
52+62	END OF GRADING.				
D.M.	3.74	895.68	3.68	891.82 <sup>✓</sup>	
	10.85	901.88	4.65	891.03	
	13.77	915.38	0.27	901.61	
	11.97	926.83	0.52	914.86	
	6.53	929.39	3.97	922.86	
B.M.			3.27	926.12	926.09
				926.02	

LT.

RT.

7-21-30

77	73	40	(3.9)	4.8	20	25
33	25	15	3.9	14	25	33

87	86	51	(4.3)	4.9	24	28
33	25	15	4.5	15	25	33

91	93	57	(5.2)	5.6	10.1	90
33	20	15	5.3	15	25	33

93	101	64	(5.8)	5.8	10.0	90
33	26	15	5.8	15	27	33

91	102	64	(5.7)	6.2	9.1	93
33	27	15	5.8	15	26	33

89	97	57	(4.9)	5.5	9.2	93
33	24	15	5.0	15	29	33

90	93	53	(4.5)	5.0	9.0	92
33	23	15	4.5	15	30	33

90	96	45	(3.7)	4.4	9.4	94
33	25	15	3.7	15	30	33

90	88	47	(2.5)	2.9	6.8	29	27
33	26	18	2.4	9	25	29	33

0 + 00 BEG OF DITCH. LT. OF STA. 8100

0 + 25

0 + 50

0 + 75

1 + 03 END OF DITCH.

$$\begin{array}{r} \underline{90} \\ 00 \end{array} \quad \begin{array}{r} \underline{120} \\ 2 \end{array} \quad \begin{array}{r} \underline{120} \\ 3.6 \end{array} \quad \begin{array}{r} \underline{90} \\ 6 \end{array}$$

$$\begin{array}{r} \underline{91} \\ 00 \end{array} \quad \begin{array}{r} \underline{120} \\ 2.3 \end{array} \quad \begin{array}{r} \underline{120} \\ 3.5 \end{array} \quad \begin{array}{r} \underline{90} \\ 6.0 \end{array}$$

$$\begin{array}{r} \underline{90} \\ 00 \end{array} \quad \begin{array}{r} \underline{121} \\ 2.3 \end{array} \quad \begin{array}{r} \underline{120} \\ 3.8 \end{array} \quad \begin{array}{r} \underline{90} \\ 6.2 \end{array}$$

$$\begin{array}{r} \underline{92} \\ 00 \end{array} \quad \begin{array}{r} \underline{120} \\ 2.3 \end{array} \quad \begin{array}{r} \underline{120} \\ 4.0 \end{array} \quad \begin{array}{r} \underline{91} \\ 6.1 \end{array}$$

$$\begin{array}{r} \underline{92} \\ 00 \end{array} \quad \begin{array}{r} \underline{120} \\ 2.2 \end{array} \quad \begin{array}{r} \underline{120} \\ 4.2 \end{array} \quad \begin{array}{r} \underline{87} \\ 6 \end{array}$$

57A

CO. YD.  
FILLCO. YD.  
CUT

0795	CROSS DRAIN		
6790	FIELD ENT RT.	5	1
8700	CROSS DRAIN		
13714	FARM ENT LT.	12	30
14740	FARM ENT LT.	8	8
14755	FIELD ENT RT.	7	4
19711	FARM ENT LT.	9	7
19763	FIELD ENT RT.	7	
24736	FIELD ENT LT.	30	
24760	CROSS DRAIN		
27748	FIELD ENT RT.		
31775	FARM ENT LT.	19	
34708	FARM ENT LT.	14	
34712	FIELD ENT RT.	14	
41777	FARM ENT RT.		
41770	OWASSO BLVD. LT.		
44705	FARM ENT LT.		
51722	CROSS DRAIN		

7-22-30

24" X 54 P<sup>3</sup>

12" X 16 C.M. OLD

24" X 54 P<sup>3</sup>

15" X 20 C.M. NEW.

15" X 20 C.M. NEW

15" X 20 C.M. NEW.

15" X 20 C.M. NEW

13" X 20 C.M. NEW.

18" X 20 C.M. NEW

24" X 48 P<sup>3</sup>

10" X 14 C.M. OLD.

15" X 20 C.M. NEW

15" X 24 C.M. OLD.

12" X 42 P<sup>3</sup> & 12" X 12 C.M. OLD.

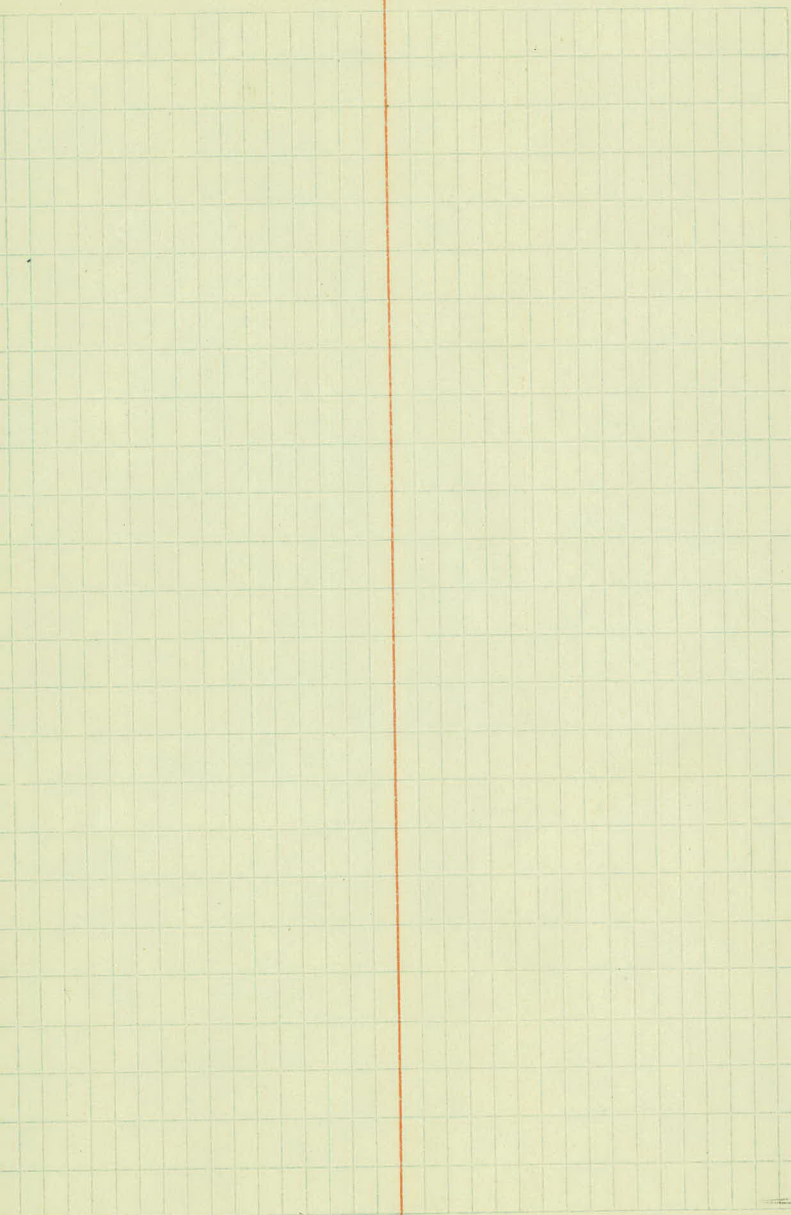
15" X 20 C.M. OLD.

18" X 40 C.M. OLD.

Sta.	Right. Lind Ft.	Sta.	Left. Lind Ft.
0+17	132'	0+00	156'
24+10	264'	2+35	84'
36+25	108'	19+30	156'
40+00	144'	24+58	276'

Right      Sept 17-30      Left.

Sta.	To Sta.	Lind. Ft.	Anchors	Sta.	To Sta.	Lind. Ft.	Anchors
0+17	1+29	132	2	0+17	1+34	156'	2
24+10	26+45	264.5	2	2+35	3+19	84'	2
36+25	37+33	108	2	19+31	20+81	156'	2
40+00	41+32	132.5	2	24+58	27+34	276'	2
		639.1 ✓	8 ✓			672 ✓	8 ✓
						637.1	
						1309.1	
Total		1309.1 ✓					



T.P.

1.70

902.39

900.69

42

750

43

750

44

IN T.P. RT. 51240150

8.20 894.20 W. END OF CURV

8.30 894.10 E. END OF CURV

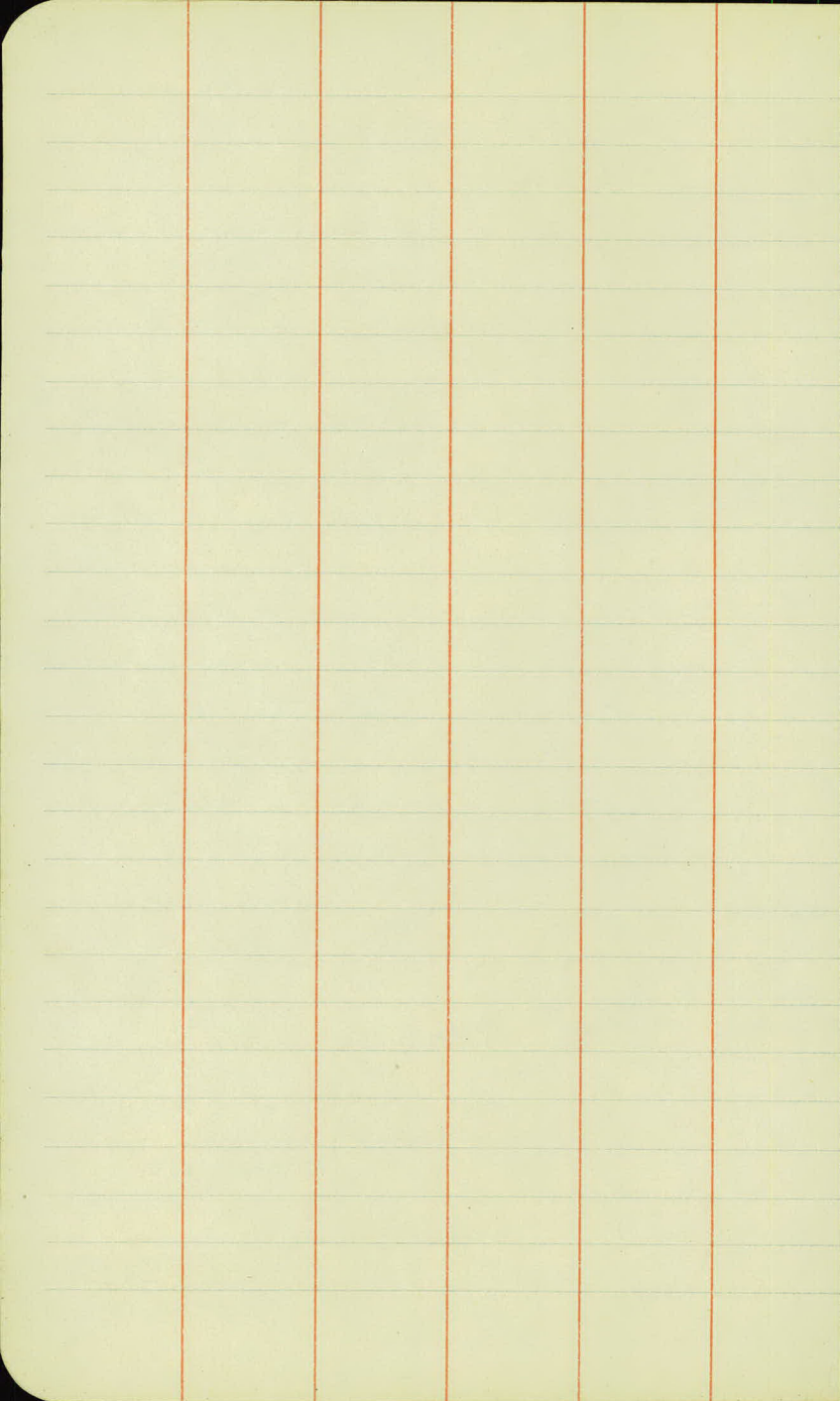
7.2 8.40  $\begin{array}{r} 7/29 \\ 3 \\ \hline 2/105 \end{array}$

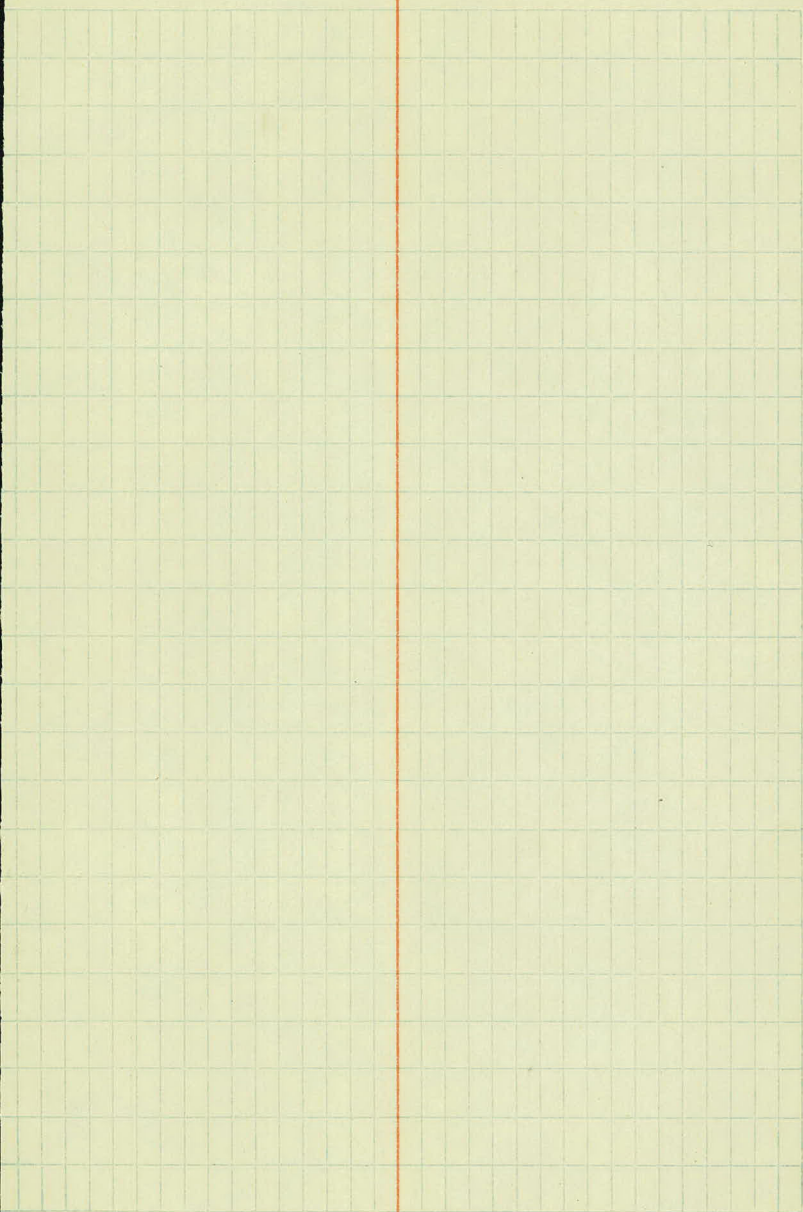
8.7 8.50  $\begin{array}{r} 30/99 \\ 2 \\ \hline 2/10 \end{array}$

9.1  $\begin{array}{r} 30/105 \\ 2 \\ \hline 2/10 \end{array}$

9.7  $\begin{array}{r} 35/108 \\ 2 \\ \hline 2/10 \end{array}$

10.0  $\begin{array}{r} 35/110 \\ 2 \\ \hline 2/10 \end{array}$





# Grade Change Sta. 6 to 20

Sta.				Elev.	
B.M.	7.64	927.20		919.56	
T.P.	0.64	919.31	8.53	918.67	
6				915.1	√ 4.21
+50				14.3	√ 5.01
7				13.4	√ 5.91
+50				12.3	√ 7.01
8				11.0	√ 8.31
+50				09.9	√ 9.41
9				09.2	√ 10.11

spike in 12" Oct 60 Lt Sta. 0130

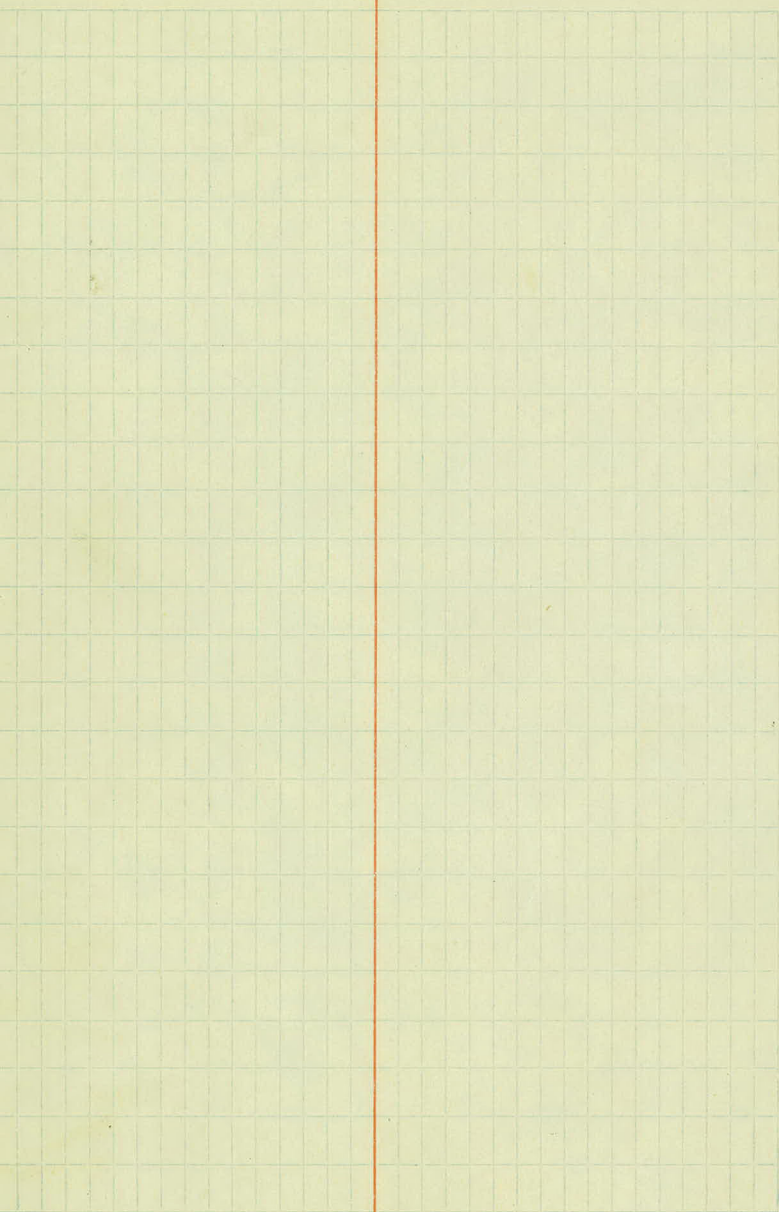
91931

9	+50				909.0	√ 10.31
10					09.1	√ 10.21
	+50				09.8	√ 9.51
11					10.8	√ 8.53
	+50				12.3	√ 7.01
12					14.2	√ 5.11
T.P.	9.85	925.23	3.93		915.38	
	+50				16.3	√ 8.93
13					18.5	√ 6.73
	+50				20.6	√ 4.63
14					22.8	√ 2.43
	+50				24.6	0.63
T.P.	8.41	931.96	1.68		923.55	
15					25.6	6.36
B.M.			1.89		930.07	
	+50				26.8	5.16

Bottom cobble Stone Lt 14+70

931.96

16				927.2	4.76
+50				27.0	4.96
17				26.3	5.66
+50				25.0	6.86
18				23.2	8.76
+50				21.2	10.76
T.F.	1.90	923.10	10.76	921.20	
19				19.1	4.0
+50				17.1	6.0
20				15.1	8.0



B.M.	0.80	930.87		930.07
T.P.	1.53	921.57	10.83	920.04
T.P.	1.37	910.82	12.12	909.45

910.82

0+00 = Toe of New Fill at Intesection of Ditch 50.

+50

1

+50

T.P.	5.73	911.40	5.15	905.67
------	------	--------	------	--------

2

+36

$\Delta H$  in Ditch.

+50

3

+50

4

T.P.	9.04	910.33	1.11	910.29
------	------	--------	------	--------

+36

$\Delta H$  in Ditch. Et.

+50

T.P.	3.34	902.66	11.01	899.32
------	------	--------	-------	--------

5

+40

Appr. Edge of Pothole

Cobble Stone Lt Sta. 14+70'

(6-3-30)

This end is in place Elev =  $\frac{7.65}{903.17}$  ← Flowline →  $\frac{7.32}{903.50}$  This end not yet in place. (Stake set)

903.30      ~~£~~ Ditch South.

10.40      903.20      7.3 = 903.52

✓ 10.45      903.15      6.9 = 903.92

✓ 10.50      903.10      6.9 = "

✓ 10.55      903.05      6.9 = "

✓ 10.60      903.00      8.1 = 903.30

8.0 = 903.40

✓ 10.65      902.95      8.1 = 903.30

✓ 10.70      902.90      8.4 = 903.00

10.75      902.85      8.4 = 903.00

10.80      902.80      9.7 = 901.70

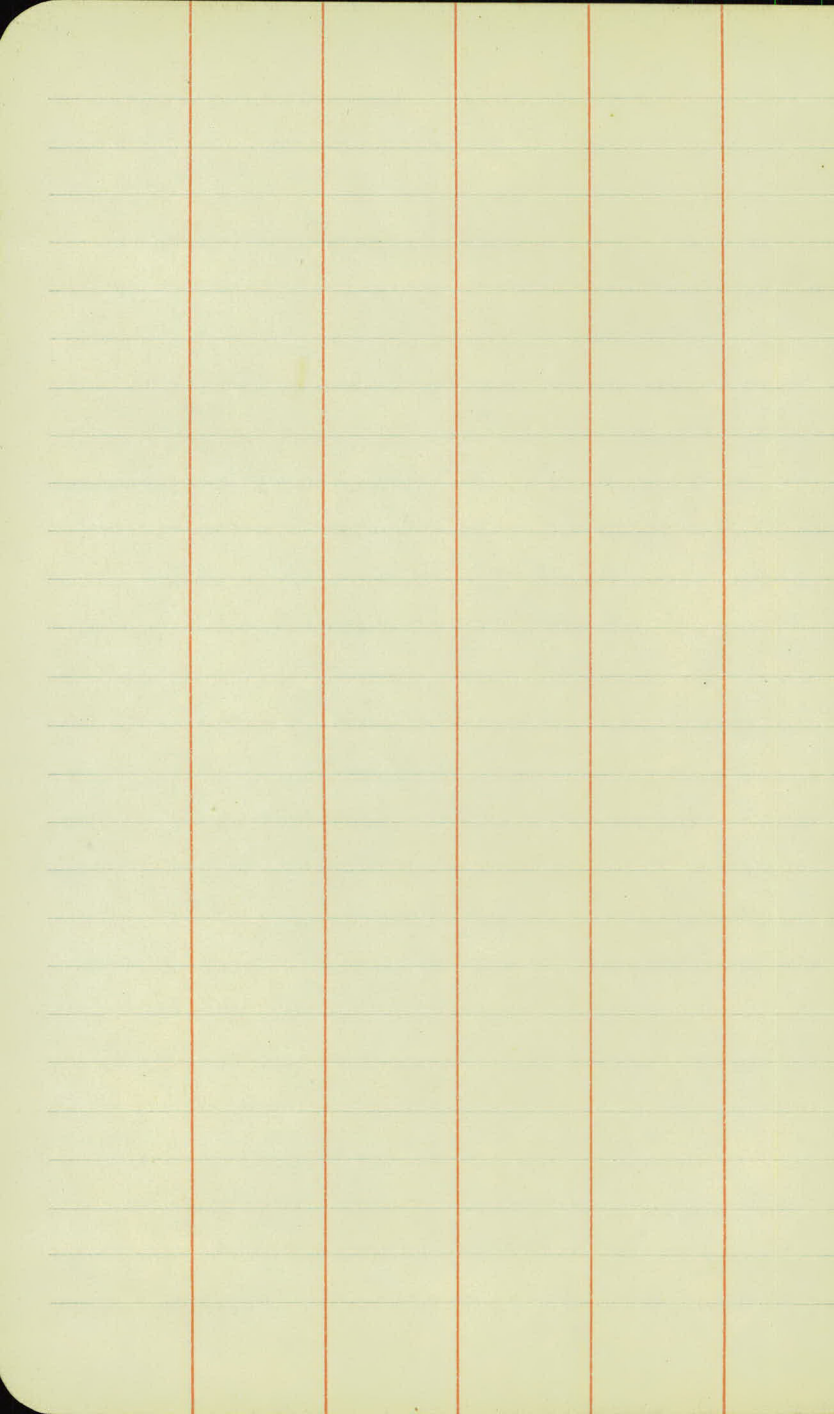
11.1 = 899.23

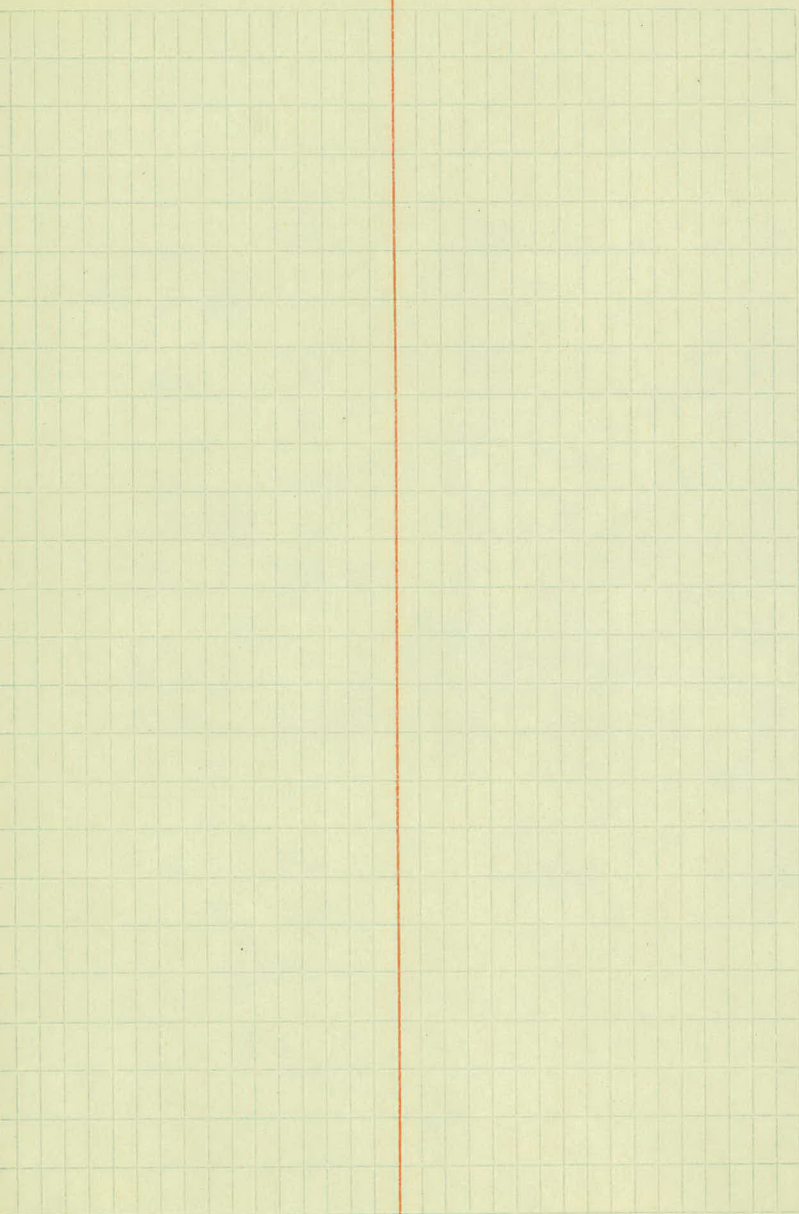
12.3 = 898.03

6.6 = 896.06

8.3 = 894.36

903.17 = Elev.  
894.36 = Pit hole.  
- 8.81





35

750	0.0	+0.13	-0.13	23.5
-----	-----	-------	-------	------

36	0.70	+0.67	-0.70	22.9 ✓
----	------	-------	-------	--------

750	2.35	+0.92	-1.06	22.3 ✓
-----	------	-------	-------	--------

37	3.44	+1.07	-1.36	21.7 ✓
----	------	-------	-------	--------

750	3.44	+1.08	-1.37	20.8 ✓
-----	------	-------	-------	--------

38	"	"	"	19.3 ✓
----	---	---	---	--------

750	"	"	"	17.3 ✓
-----	---	---	---	--------

39	"	"	"	14.7 ✓
----	---	---	---	--------

750	"	"	"	11.5 ✓
-----	---	---	---	--------

40	3.44	+1.08	-1.37	07.9 ✓
----	------	-------	-------	--------

750	3.44	+1.04	-1.31	04.0 ✓
-----	------	-------	-------	--------

41	1.10	+0.40	-0.56	00.1 ✓
----	------	-------	-------	--------

755	0.0	+0.00	-0.00	96.4 ✓
-----	-----	-------	-------	--------

42		+0.05	-0.05	94.2
----	--	-------	-------	------

750				92.8
-----	--	--	--	------

43				92.2
----	--	--	--	------

750				92.1
-----	--	--	--	------

44				92.1
----	--	--	--	------

750				
-----	--	--	--	--

45



0 + 95 24" X 54' 10<sup>3</sup>

8 + 00 24" X 54' 10<sup>3</sup>

24 + 60 24" X 48' 10<sup>3</sup>

41 + 70 L 24" X 48' 10<sup>3</sup>

912.0  
50.7

915.80  
23.3

<sup>x</sup>  
543/100.  
5/128

<sup>x</sup>  
5/128

903.3  
27

903.5  
27

<sup>x</sup>  
543/100  
5/127

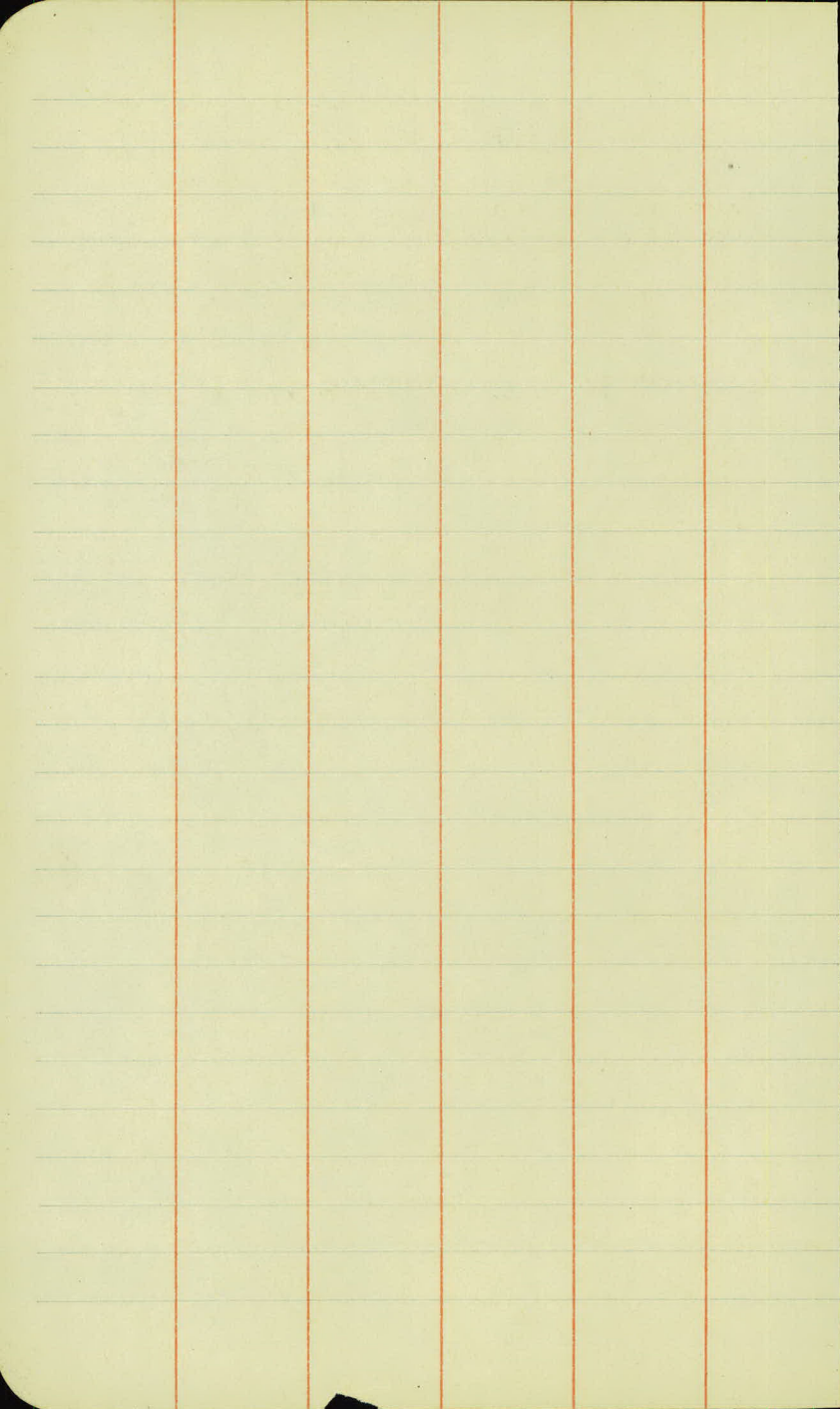
<sup>x</sup>  
50/100  
5/150

899.00  
27

900.0  
21

894.50

989.40



# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or I. P.= $23^{\circ} 20'$  to the R. at Station  
542+72.

Ext. in Tab. IV opposite  $23^{\circ} 20'$ =120.87

$120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20'$ =1183.1

$1183.1 \div 10 = 118.31$ .

Tab. V. correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur.=0.16

$118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)

Ang.  $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 = \text{L. C.}$

$2^{\circ} 19\frac{1}{2}' = \text{def. for sta.}$	542	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}' = \text{" " "}$	+50	Tan.=	1.18 47
$7^{\circ} 19\frac{1}{2}' = \text{" " "}$	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' = \text{" " "}$	+50	L. C.=	2.33.33
$11^{\circ} 40' = \text{" " "}$	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$   
 $2^{\circ} 19\frac{1}{2}' = \text{def. for sta. 542.}$

Def. for 50 ft.= $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)

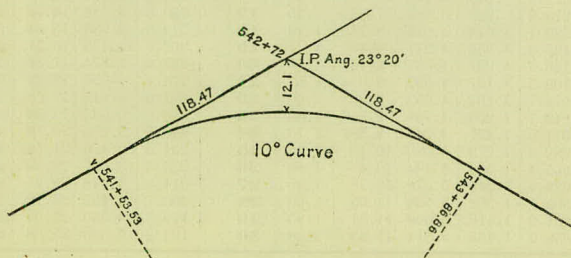


TABLE I. — Minutes in Decimals of a Degree.

<b>1'</b>	.0167	<b>11'</b>	.1833	<b>21'</b>	.3500	<b>31'</b>	.5167	<b>41'</b>	.6833	<b>51'</b>	.8500
<b>2</b>	.0333	<b>12</b>	.2000	<b>22</b>	.3667	<b>32</b>	.5333	<b>42</b>	.7000	<b>52</b>	.8667
<b>3</b>	.0500	<b>13</b>	.2167	<b>23</b>	.3833	<b>33</b>	.5500	<b>43</b>	.7167	<b>53</b>	.8833
<b>4</b>	.0667	<b>14</b>	.2333	<b>24</b>	.4000	<b>34</b>	.5667	<b>44</b>	.7333	<b>54</b>	.9000
<b>5</b>	.0833	<b>15</b>	.2500	<b>25</b>	.4167	<b>35</b>	.5833	<b>45</b>	.7500	<b>55</b>	.9167
<b>6</b>	.1000	<b>16</b>	.2667	<b>26</b>	.4333	<b>36</b>	.6000	<b>46</b>	.7667	<b>56</b>	.9333
<b>7</b>	.1167	<b>17</b>	.2833	<b>27</b>	.4500	<b>37</b>	.6167	<b>47</b>	.7833	<b>57</b>	.9500
<b>8</b>	.1333	<b>18</b>	.3000	<b>28</b>	.4667	<b>38</b>	.6333	<b>48</b>	.8000	<b>58</b>	.9667
<b>9</b>	.1500	<b>19</b>	.3167	<b>29</b>	.4833	<b>39</b>	.6500	<b>49</b>	.8167	<b>59</b>	.9833
<b>10</b>	.1667	<b>20</b>	.3333	<b>30</b>	.5000	<b>40</b>	.6667	<b>50</b>	.8333	<b>60</b>	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
<b>0° 0'</b>	34377.	.036	.145	.291	0.05'	<b>7°</b>	819.0	1.528	6.105	12.21	2.10'
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	<b>8</b>	716.8	1.746	6.976	13.95	2.40
<b>1</b>	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	<b>9</b>	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
<b>2</b>	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	<b>10</b>	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2292.0	.545	2.181	4.363	0.75	<b>11</b>	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	<b>12</b>	478.3	2.620	10.45	20.91	3.60
<b>3</b>	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	<b>13</b>	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	<b>14</b>	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	<b>15</b>	383.1	3.277	13.05	26.11	4.50
<b>4</b>	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	<b>16</b>	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.781	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	<b>17</b>	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	<b>18</b>	319.6	3.935	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	<b>19</b>	302.9	4.155	16.51	33.01	5.70
<b>5</b>	1146.3	1.091	4.362	8.724	1.50	<b>20</b>	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	<b>21</b>	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	<b>22</b>	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	<b>23</b>	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	<b>24</b>	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	<b>25</b>	231.0	5.476	21.64	43.28	7.50
<b>6</b>	955.4	1.309	5.234	10.47	1.80	<b>26</b>	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	<b>27</b>	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	<b>28</b>	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	<b>29</b>	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	<b>30</b>	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>1°</b>	50.00	.22	<b>11°</b>	551.70	26.50	<b>21°</b>	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
<b>2</b>	100.01	.87	<b>12</b>	602.21	31.56	<b>22</b>	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
<b>3</b>	150.04	1.96	<b>13</b>	652.81	37.07	<b>23</b>	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
<b>4</b>	200.08	3.49	<b>14</b>	703.51	43.03	<b>24</b>	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
<b>5</b>	250.16	5.46	<b>15</b>	754.32	49.44	<b>25</b>	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
<b>6</b>	300.28	7.86	<b>16</b>	805.25	56.31	<b>26</b>	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
<b>7</b>	350.44	10.71	<b>17</b>	856.30	63.63	<b>27</b>	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
<b>8</b>	400.66	13.99	<b>18</b>	907.49	71.42	<b>28</b>	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
<b>9</b>	450.93	17.72	<b>19</b>	958.81	79.67	<b>29</b>	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
<b>10</b>	501.28	21.89	<b>20</b>	1010.3	88.39	<b>30</b>	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>31°</b>	1589.0	216.3	<b>41°</b>	2142.2	387.4	<b>51°</b>	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
<b>32</b>	1643.0	230.9	<b>42</b>	2199.4	407.6	<b>52</b>	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
<b>33</b>	1697.2	246.1	<b>43</b>	2257.0	428.5	<b>53</b>	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
<b>34</b>	1751.7	261.8	<b>44</b>	2314.9	450.0	<b>54</b>	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
<b>35</b>	1806.6	278.1	<b>45</b>	2373.3	472.1	<b>55</b>	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.4	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
<b>36</b>	1861.7	294.9	<b>46</b>	2432.1	494.8	<b>56</b>	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
<b>37</b>	1917.1	312.2	<b>47</b>	2491.3	518.2	<b>57</b>	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
<b>38</b>	1972.9	330.2	<b>48</b>	2551.0	542.2	<b>58</b>	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
<b>39</b>	2029.0	348.6	<b>49</b>	2611.2	566.9	<b>59</b>	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
<b>40</b>	2085.4	367.7	<b>50</b>	2671.8	592.3	<b>60</b>	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>61°</b>	3375.0	920.2	<b>71°</b>	4086.9	1308.2	<b>81°</b>	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
<b>62</b>	3442.7	954.8	<b>72</b>	4162.8	1352.6	<b>82</b>	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
<b>63</b>	3511.1	990.2	<b>73</b>	4239.7	1398.0	<b>83</b>	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
<b>64</b>	3580.3	1026.6	<b>74</b>	4317.6	1444.6	<b>84</b>	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
<b>65</b>	3650.2	1063.9	<b>75</b>	4396.5	1492.4	<b>85</b>	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
<b>66</b>	3720.9	1102.2	<b>76</b>	4476.5	1541.4	<b>86</b>	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
<b>67</b>	3792.4	1141.4	<b>77</b>	4557.6	1591.6	<b>87</b>	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
<b>68</b>	3864.7	1181.6	<b>78</b>	4639.8	1643.0	<b>88</b>	5533.1	2225.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
<b>69</b>	3937.9	1222.7	<b>79</b>	4723.2	1695.8	<b>89</b>	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
<b>70</b>	4011.9	1265.0	<b>80</b>	4807.7	1749.9	<b>90</b>	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>91°</b>	5830.5	2444.9	<b>101°</b>	6950.6	3278.1	<b>111°</b>	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
<b>92</b>	5933.2	2518.5	<b>102</b>	7075.5	3374.9	<b>112</b>	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
<b>93</b>	6037.8	2594.0	<b>103</b>	7203.2	3474.4	<b>113</b>	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
<b>94</b>	6144.3	2671.6	<b>104</b>	7333.6	3576.8	<b>114</b>	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
<b>95</b>	6252.8	2751.3	<b>105</b>	7467.0	3682.3	<b>115</b>	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
<b>96</b>	6363.4	2833.2	<b>106</b>	7603.5	3791.0	<b>116</b>	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
<b>97</b>	6476.2	2917.3	<b>107</b>	7743.2	3902.9	<b>117</b>	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
<b>98</b>	6591.2	3003.8	<b>108</b>	7886.2	4018.2	<b>118</b>	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
<b>99</b>	6708.6	3092.7	<b>109</b>	8032.7	4137.1	<b>119</b>	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
<b>100</b>	6828.3	3184.1	<b>110</b>	8182.8	4259.7	<b>120</b>	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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For Tangents Add															
ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°		.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°		.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°		.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°		.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°		.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°		.11	.22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°		.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°		.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°		.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°		.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°		.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°		.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°		.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°		.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°		.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°		.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°		.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°		.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.49	4.98	5.38	5.83
100°		.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

## For External Add

ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°		.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°		.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°		.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°		.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°		.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°		.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°		.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°		.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°		.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°		.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°		.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°		.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°		.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°		.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°		.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°		.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°		.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°		.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°		.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

## CURVE FORMULAS.

$$T = R \tan \frac{1}{2} I$$

$$T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } D}$$

$$\text{Sin. } D = \frac{50}{R}$$

$$\text{Sin. } D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{50}{\text{Sin. } D}$$

$$E = R \text{ ex. sec. } \frac{1}{2} I$$

$$E = T \tan \frac{1}{4} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{\frac{1}{2} I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.— Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

## Natural Sines

DEG.	0'	10'	20'	30'	40'	50'	DEG.	DEG.	0'	10'	20'	30'	40'	50'	DEG.
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1276	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	DEG.	60'	50'	40'	30'	20'	10'	DEG.

DEG.	0'	10'	20'	30'	40'	50'	DEG.
80	9848	9853	9858	9863	9868	9872	9
81	9877	9881	9886	9890	9894	9899	8
82	9903	9907	9911	9914	9918	9922	7
83	9925	9929	9932	9936	9939	9942	6
84	9945	9948	9951	9954	9957	9959	5
85	9962	9964	9967	9969	9971	9974	4
86	9976	9978	9980	9981	9983	9985	3
87	9986	9988	9989	9990	9992	9993	2
88	9994	9995	9996	9997	9997	9998	1
89	9998	9999	9999	9999	I.0000	I.0000	0
DEG.	60'	50'	40'	30'	20'	10'	DEG.

## Natural Cosines

Natural Tangents

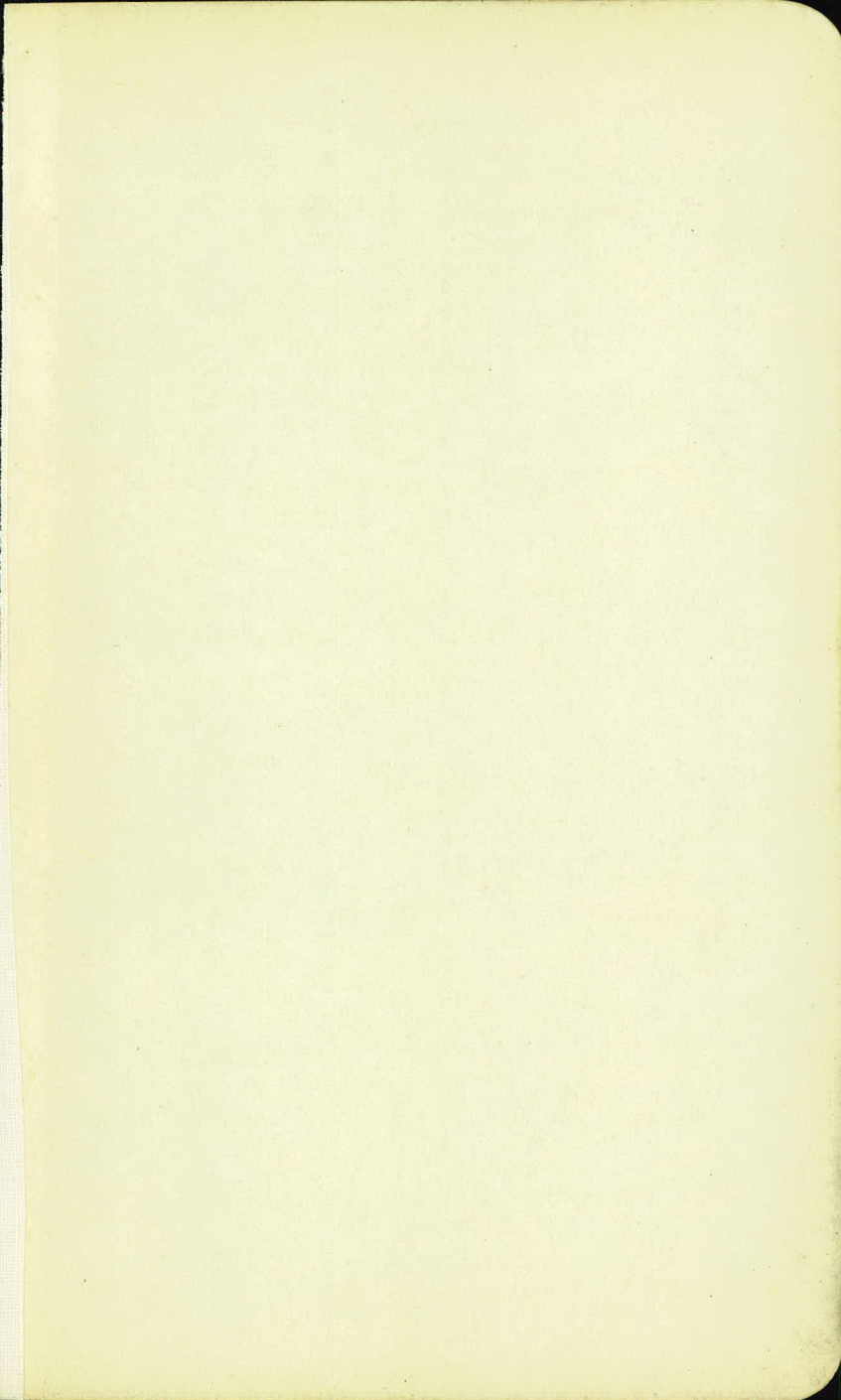
DEG.	0'	10'	20'	30'	40'	50'	DEG.	0'	10'	20'	30'	40'	50'	DEG.	
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2450	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8667	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10

DEG.	60'	50'	40'	30'	20'	10'	DEG.	60'	50'	40'	30'	20'	10'	DEG.
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DEG.	0'	10'	20'	30'	40'	50'	DEG.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.064	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.770	0

DEG.	60'	50'	40'	30'	20'	10'	DEG.
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Natural Cotangents



94.71  
23  

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2.41

931  
15  

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2687

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

02524