

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan _____ Sub _____

LONG LAKE ROAD

From Cleveland Ave. To Rice Cree^k Rd

Road Acc't. No. 17

Date Filed 11-30-29 1

PROJ. 30-12

Plan Survey
LONG LAKE ROAD
Sta. 0+00 to 96+83.12

Proj. N^o 30-12

Sta. ΔL ΔR

6

5

+71.67 P.T. 2114'

+50 2015'

4 1800'

+50 1545'

3 1330'

+50 1115'

+47.51 P.I.

2 900'

+50 645'

1 430'

+50 215'

0+00 P.C.

$\Delta 4227'$
 $D = 9^\circ$ Lt
 $T = 247.51$
 $L = 471.67$
 $R = 637.27$

-5+20.53

• R.R. spike

42° 27'

2" x 2" Hub.

561

• Fence Post
Site no 3/11/11

• R.R. spike

1/2" x 1/2" R.R.

• Hole in pave.

1/4" G.R. Post

← Pave. 20'

520.53

20'

S.T.H. #63

#8

Sta. Point ΔL . ΔR .

25+85.89 P.O.T.

20+97.4 P.T.

35°24'

+50

31°50'

20

28°05'

+50

24°20'

19

20°35'

18+97.82 P.I.

16°50'

+50

18+

18°05'

+50

9°20'

17

5°35'

+50

1°50'

16+25.4 P.C.

+46.0 P.T. ✓

17°24'

9

14°38'

+50

11°38'

8+05.9 P.I.

8°38'

8

5°38'

+50

2°38'

7

6+56.9 P.C. ✓

2°38'

$\Delta 70.48'$
 $D 15^\circ R$
 $T = 272.22 \checkmark$
 $L = 472.0 \checkmark$
 $R = 383.06 \checkmark$

$\Delta 34.48'$
 $D = 12^\circ R$
 $T = 149.3 \checkmark$
 $L = 290.0 \checkmark$
 $R = 478.34 \checkmark$

65' \odot Cr. Ball on Top
Water Tower New Br.
2" x 2" Hub
2" x 2" Hub

spike

7048
2" x 2" Hub
2296
TR
4434
RR

spike

3448
spike
Ment.

5780
R.R. spike

3833
Guy Rd
Site 77

R.R. spike

Sta.	$\Delta L +$	$\Delta R +$		
+50		36°45'		
53		31°45'	} $\Delta 88.32'$ $D 20^\circ R +$	
+63 ¹⁶	P.I.			
+50		26°45'		T = 280.64 ✓
52		21°45'		L = 442.67 ✓
+50		16°45'	R = 287.94 ✓	
51		11°45'		
+50		6°45'		
50		1°45'		

49+82.5² P.C. ✓

47+63.99 P.T. ✓ 35°26'

+50 34°02'

47 29°02'

+50 24°02'

46+14.5³ P.I. - P.I. Sta. 54+96.5⁵ Road % No. 12

46	19°02'	} $\Delta -70.52$ $D - 20^\circ L +$ $T - 204.87$ ✓ $L - 354.33$ ✓ $R - 287.94$ ✓
+50	14°02'	
45	9°02'	
+50	4°02'	

44+09.66 P.C. ✓

32+31.91 P.O.T. = P.I. Sta. 41+26.4⁵ Road % No. 12

1/4
1920

Sect 122
Line

Guy Pole Side Tie 7.1
= P. 61 + 8460 Road 1/2 No. 12

7.0
4.18

5263.16
28084
28859

569.43

• Spike
• Spike

• P.P. Side Tie
30.18
2" x 2" Hub.
26.5
• Guy Pole. Side Tie.

• Spike

T.P. Side Tie.
20.0
49.1
1" x 2" Hub.
• T.P. Side Tie.

840.	Point	ΔLt	ΔRt
+3875	P.T.		45°44'
84			40°53'
+50			34°38' $\Delta = 9128'$
+0984	P.I.		D 25°
83			28°23' T 236.96
+50			22°08' L 365.87
82			15°53' R 231.01
+50			9°38'
81			3°23'
80+7288	P.C.		
79+4348	P.T. ✓	45°04' ✓	
79		40°45'	$\Delta 9008' Lt$
+50		35°43'	D = 20°
78		30°43'	T = 288.59 ✓
77+814	P.I.		L = 450.67 ✓
+50		25°43'	R = 287.94 ✓
77		20°43'	
+50		15°43'	
76		10°43'	
+50		5°43'	
75		0°43'	
74+9281	P.C.		
62+200	P.O.T. ✓		
54+2519	P.T. ✓		44°16'
54			41°45'

• Spike

2" mil. @ 4.78 • 1" x 2" Hub.

12" mil @ 16.30

149281

5425.19

207762

56945

264705

• Spike

• R.R. spike

25.72 • Fence Post
West

34.39 • P.P.

56 42

72 58

120 40

P.P. @ 29.0

• R.R. spike

28.33 • Fence Post

• Spike

95+21.¹⁹ P.I. \pm of Rice Creek Road established
 from \pm of Present traveled Road.
 at intersection of Long Lake Road.

96+83. ¹¹	P.T.	45 ⁰ 27
+50		42 ⁰ 27
96		37 ⁰ 27
+50		32 ⁰ 27

95+21.¹⁹ P.I.

95		27 ⁰ 27	Δ 91.34'
+50		22 ⁰ 27	D-20°
94		17 ⁰ 27	T=295.91'
+50		12 ⁰ 27	L=457.83'
93		7 ⁰ 27	R=287.94'
+50		2 ⁰ 27	

92+25.²⁸ P.C.

• P.R. spike

9134

34.77 → P.R.

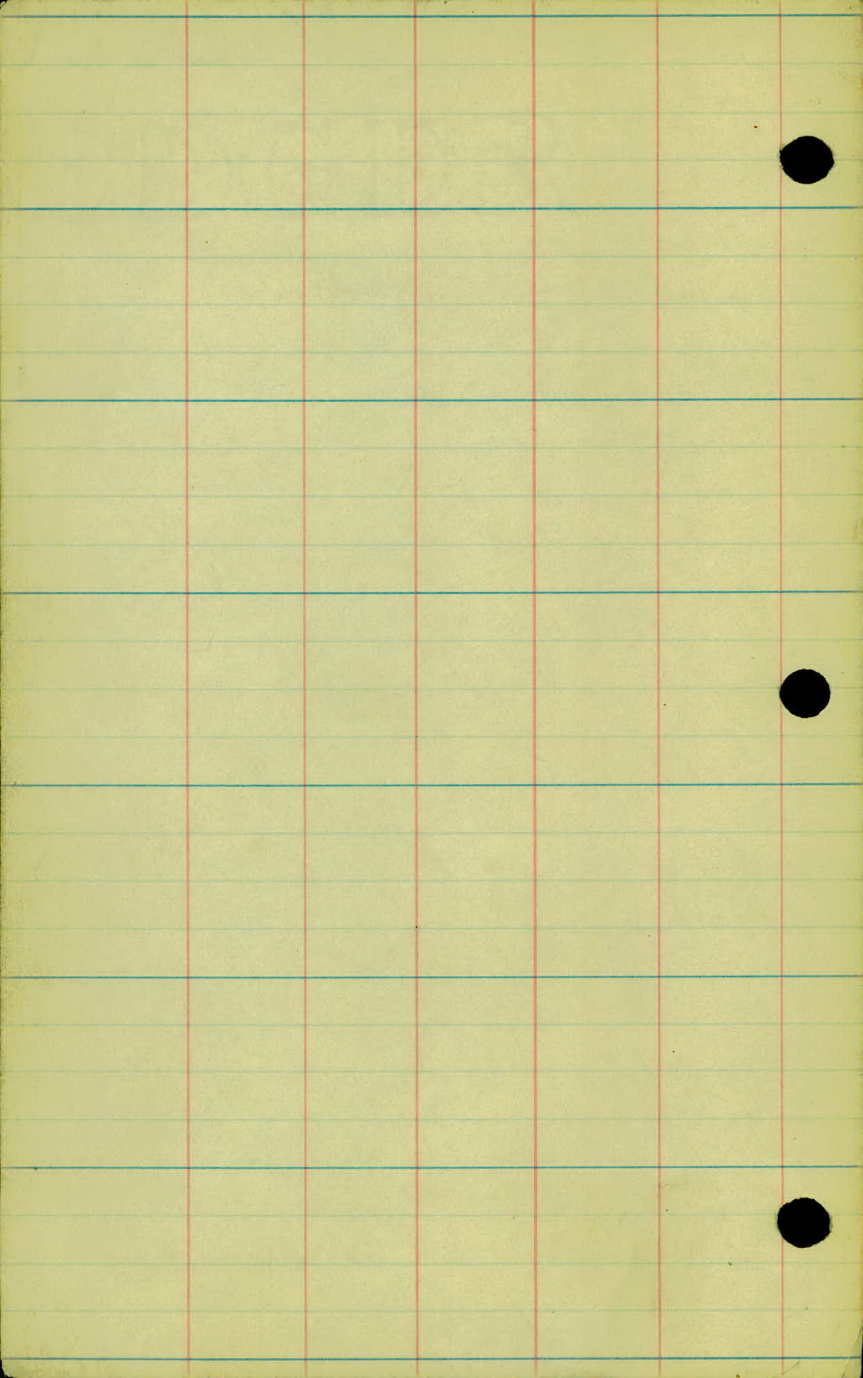
± Rice Creek Rd.

• P.R. spike.

3989

• Guy Polo.

• P.R. spike.



11-13-29

Long Lake Road.

"B" Line.

Sta. 46+14⁵³ To Sta. 87+84¹⁹

+86.77 P.T. 36.77

+50 33.315

89 29.465

+50 26.015

88 22.165

+84.19 P.I.

+50 18.315

87 14.465

+50 11.015

86 7.165

+50 3.315

85+02.99 P.C.

87+84.19 P.I.

$\Delta 72^{\circ} 34'$

$D = 15^{\circ} \text{ LT}$

$T = 281.20$

$L = 483.78$

$R = 383^{\circ} 06'$

$72^{\circ} 34'$

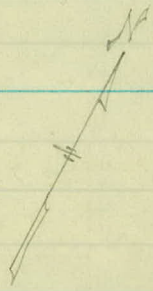
79+61.74 P.O.T.

75+70.5 P.O.T.

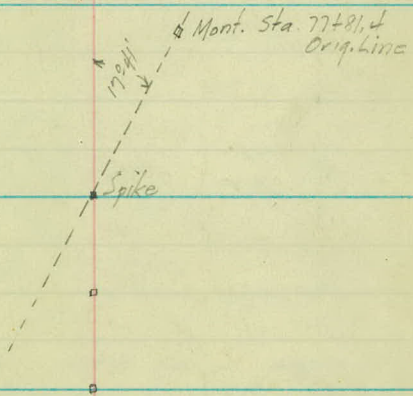
69+31.10 P.O.T. Sta. 73+33.46 (Orig Line)

55+84.72 P.O.T.

46+14.53 Point of beg. on "B" line.



(Intersection)



STA. POINT Δ LT. Δ RT

11-21-29

²⁵
79+54 P.O.T

77+72⁷⁴ ✓ P.T. 1°-08'

+50 1°-01'

77 0°-46'

76+59⁴ P.I.

Δ-2°-16'

+50 0°-31'

P.-1°-17'

76 0°-16'

T.-115⁵³ ✓

+50 0°-01'

L.-226⁶⁷ ✓

75+46⁰⁷ ✓ P.C. 0°-00'

R-572965 ✓

75+70⁵ P.O.T



STATION POINT A LT. Δ RT.

89+99¹⁶ ✓ P.T. 35°-09'

+50 31°-28'

89 27°-43'

+50 23°-58'

88+00² P.I.

88 20°-13'

+50 16°-28'

87 12°-43' .10

+50 8°-58'

86 5°-13'

+50 1°-28'

85+30⁴⁹ ✓ P.C. 0°-00' .05

Δ-70°-18'

D.-15°-17'

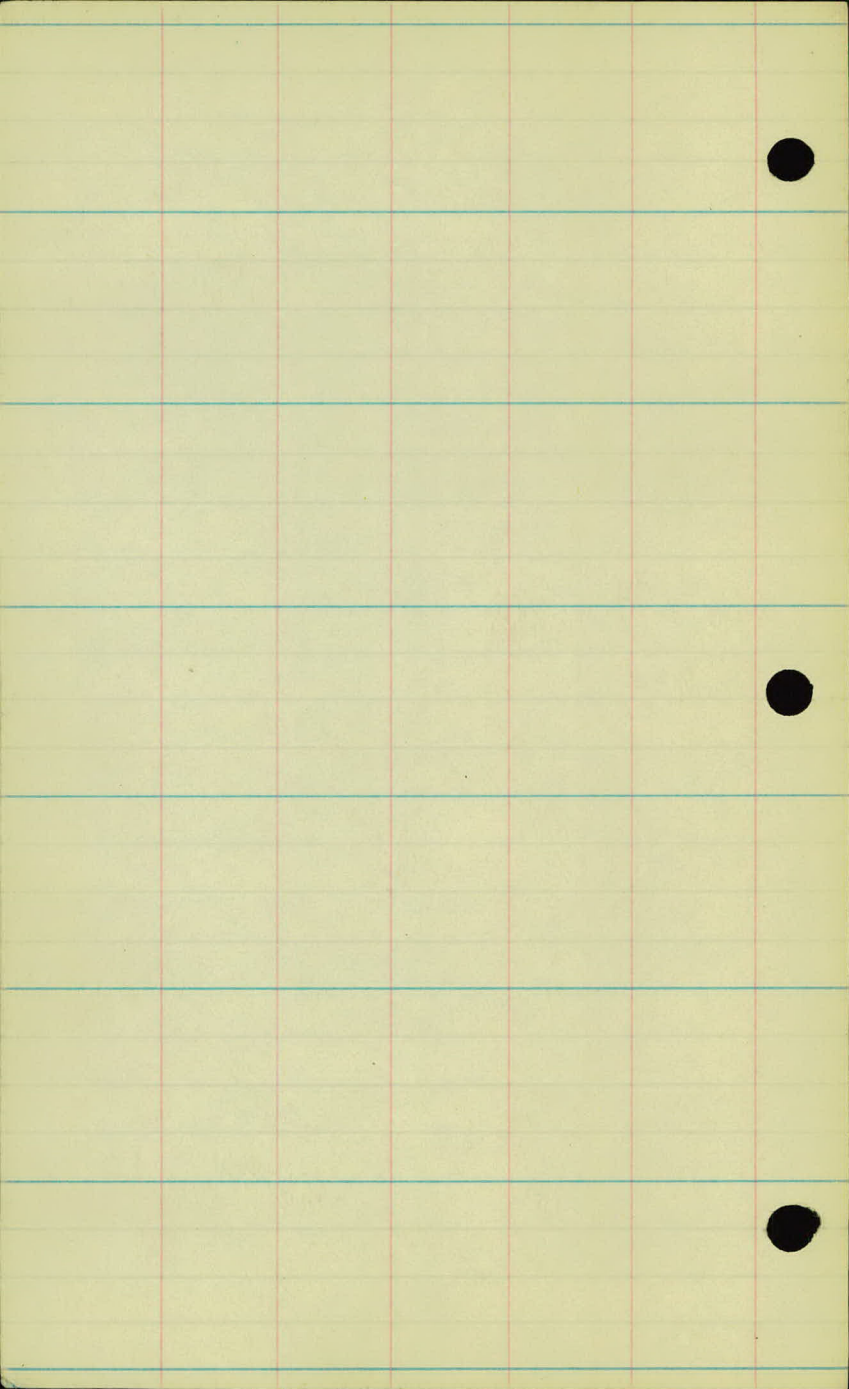
T.-169²¹ ✓

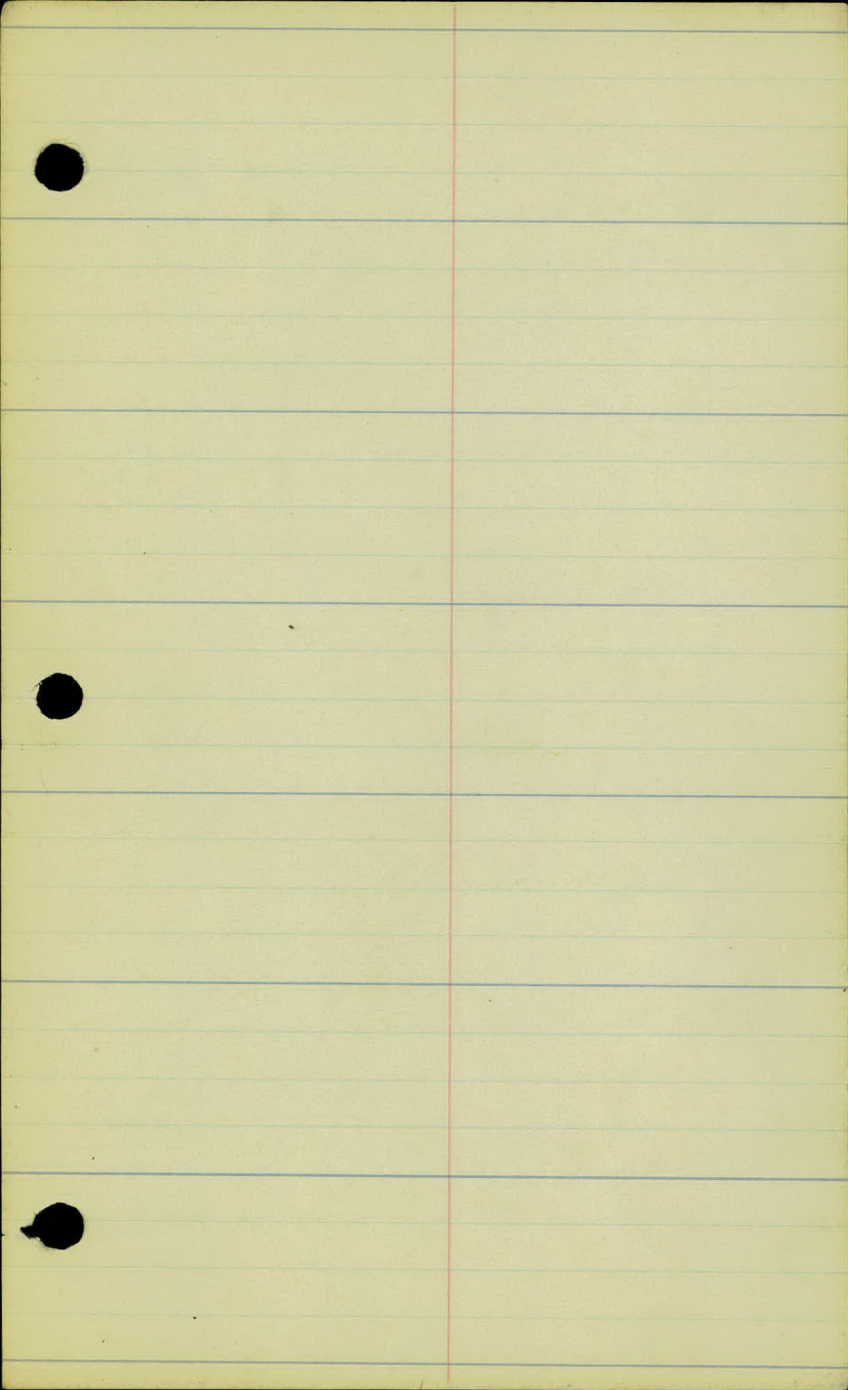
L.-468⁶⁷ ✓

R.-383⁰⁶ ✓

13.72

57.68





+47.51 P.I.

2

1

0+00 { Pavement and Rails }
 { Located from Sub. Chords }

- 50

- 1

-1+50

- 2

-2+50

- 3

-3+50

- 4

+82. Timber Cottonwood 32'

42'

+86. 4' One Way 30'

10' 23'

+51. Conc. Dr 27'
10' Wide.

Pasture

12 17'

+88 F.F. 26'
+86 F. Cor. 27'
+76 F.E.
+50 P.P. 20'

+41 Xing Sq. 22'

15 12'

+10 G.P. 29'

20' 5'

+09. P.P. 15'
+76 F. Cor. 27'

+57 End Pave.

+59 45 E. Rail

+09. P.P. 15'
+76 F. Cor. 27'

200

100

100

100

200

842.7'

162. Pave

94.53'

+14. End G.R. P.P. 14'
14 - 0+00 G.R. 10'

= Pave Located from Sub-
Chord.

83.57'

3540 - +50.
9426

48 @ -1+00

5.1 - 1+50

5.2 - 2+00

5.05 - 3+00

20

469 - 4+00



9

8

7

6

5

4

3

Cultivated

!! +46 P.R. Dr.

+94 T.P. 28'
+80 T.R. 43'

Long Lake Rd.

+76 Gv. Pole 21'
+63 P. Dr.
+54 E Long Lk. Rd.
+44 P.P. 16'

+25 T.P. 19'

11' 11"

8'

33' 7"

12' 9"

7' 13"

30'

6+30 Bsq. Light Clearing.

9' 11"

Low Wet Ground

+89 P.P. 36'

+90 Wood Sq. 16'
+87 Rd Sq. 17'

+61 P.P. 28'

Pasture

12' 10"

13' 10"

12' 12"

Cultivated

+13 P.P. + F. Cor. 24'

+74 Rd Sq. - 16'
+71 R.R. Sq. 17'

8' 18"

+31 P.P. 26'

8' 23"

250

+25

16

15

14

13

12

11

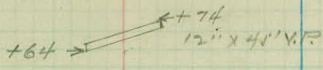
10

+86-P.P. 24'

10' 9"

7' 7"

+09.T.P. 22'



+18 P.P. 27'

+64.T.P. 22'

+18 P.P. Dr.

+80-P.P. 28'

+65 Gy. Pole 28'

+15 T.P. 23'

Cultivation

+65 P.P. 28'

+35 P.P. Dr.

+09. P.P. 27'

+77 T.P. 24'

+60 Reg. Cultivation
+58 = 12" Twin Cat 34'

+83 K2 59.19'

+45 P.P. 28'
+32 P.P. Dr.

+16 T.P. 24'

9' 11"

23

~~24~~

~~25~~

(20) 22

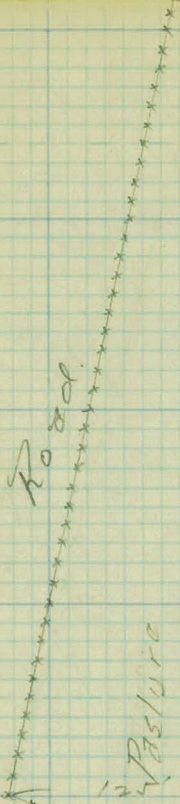
(19) 21

20

19

18

17



Pasture

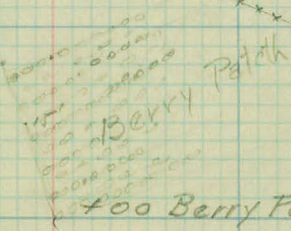
12' Pasture

Pasture

21 + 52 Fence Int.

18 + 85 Berry Patch.

Cultivation



14'
17'3"

Cultivated

30

29

28

27

26

25

Cultivated

Cultivated

+42 Field Ent.

46'

+60 + P 21'

Alfalfa

+28 T.P. 26

+08 F. Int. 47'

+71 = So Side Rd.

+60 = 8" C.W. 23'

+38 = Appr. & Rd.

+30 = 12" C.W. 14'

+02 No. Side Traveled Rd.

+30 P.P. 12'

+66 F. Int.

Pasture

37

36

35

34

33

32

31

+42 T.P. 23'

Cultivated

Cultivated

+44 Bear L. Clear.
+44 P.P. 26

+00 T.P. 23'

+54 T.P. 23

Cultivated

+88 P.P. 27'

+30 T.P. 21'

Cultivated

+31 P.P. 29'

+39 Int. Road

FF

44

43

42

41

40

39

38

+55 T.P. 23'

8'13"

+57 P.P. 30'
Long Lake.



28' Long
Taken from
Road Map



+12 T.P. 24'

+94 P.P. 27'

+15 End Clearing

+70 T.P. 23'

8-6" Oaks

+32 P.P. 27'

+00 Beg. Clearing

+29 T.P. 23'

+55-6" Oak 28'
+44-14" CW 29'
+44 End L. Clearing

+04-2-8" Oaks 25'

Cultivated

Cultivated

+65 P.P. 27'
+57-2-4" Oak 30'
+57 Beg. L. Clearing
+22-8" Oak 20'
+05 Trpl. Oak 19'

+86 T.P. 23'

+05 P.P. 26'
+00 End. Clearing

51

50

49

48

47

46

45

+35-12x30 CM
XDR.



+85 P.P. 12'

+50 In + No Side of Roadbed

+05 T.P. 19'

Hay Meadow.

+19 P.P. 28'

+67 T.P. 16'

+30 E Cultivation
Bog, Hay Meadow.

+75 P.P. 25'

+31 T.P. 13'

5' 13

2'

18'

37'

+13 T.P. 29'

+76 T.P. 25'

25'

Cultivated

4 | Left Shoulder.

58

57

56

55

54

53

52

65

64

63

62

61

60

59

+87 T.P. 28
Fence = 28'

Pasture.

Pasture.

+76 F. Cor 28'
+64 F.E.
+51 T.P. 28

+67 F. Int.

+33 P.P. 15'
+26-10" Will 24'

+95 Pr. Dr.

+65 End of Row.

+30-6-1" C.W. 28'
+20-End of Row.
+73-T.P. 28'
+03-P.P. 17'

Farm Yard

+30: Row of 9-4" Trees 29'

+67 T.P. 27

Pasture

+74 Beg. F.

+86-P.P. 19'
+74-16 Oak 22'

+51-2-10" Oak 15 24'
+41-10 Oak 24'
+29-24 Oak 33'

+14 Pr. Dr.
+08-15 C.W. 30'

+26 T.P. 27'

+03 F.E. 12' x 12' DN. 24'
+93 F. Cor 29' Beg. C.H.

+38 P.P. 22'

+00 End Betty Pains

+59-T.P. DN + 12' x 16' C.W. 12'
+53 F. Cor 29'

+65 Berry Patch 26'

Yard

72

71

70

69

68

67

66

+54 P. Dr.
+40 End Fence 28' x

+54 F.E.

+54 T.P. 28'

+25 Beg. Farm Yard
+25 End Pasture

Cultivation

+94 P.P. 18'

Pasture

+12 T.P. 28'

+51 P.P. 18'
+45 Beg. Cult.
+34 P. Dr.

+45 Beg. Pasture

Farm Yard

+11 End Fence,
15'

+78 P. Dr.
+61 T.P. 28'

+10 P.P. 17'

+68 Int. F

+09 F.E.
+02 Int. K.
+02 Twin Will 18'

+16 T.P. 28'
Fence Line on Poliline

Pasture

+62 P.P. 15'
F.L. on Poliline

Pasture

+12 P.P. 15'
Fence 15'

79

78

77

76

75

74

73

+50 End Swamp 16'

+48 P.P. 22'

+61 So Edge of Rd bed.

+29 T.P. 4'

+00 End Light Clearing 18'

+50 Light Brushing

+00 Swamp 30

+30 End Clearing.

+15 T.P. 4.

+70 Edge Rd bed.

+00 Beg Light Clearing 22'

+85' X Drain 18' X 36'



+54 T.P. 29

Cultivation

+80 P.P. 19

+35 Beg Cultivation.

+16 T.P. 28'

+34 P.P. 19'

86

85

84

83

82

81

80

+73 T.P. 22'

+40 P.P. 27'

+22 Rd Sq. 16'

+17 T.P. 21'

+03, P.P. 28'

Cultivation

Cultivation

+35 Beg Cultiv.

+77 T.P. 30'

+70 = 16" Oak 22'
+73 P.P. 20'
+65 P.P. Dr.
+55 = 12 x 20 C.M.
+50 End Orchard.



Yard

+19-16" Oak 8'
+05-14" Oak 7'

+83 P.P. 22'



+00 = Little Swamp 3'

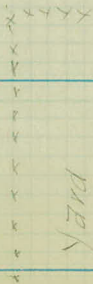
Orchard

+89 - P.P. 8'

+40 T.P. 30'

+49-8" Oak 28'
+38 F. Cor 12'

Cultivated



Yard

+86 P.P. 21

+35 Cluster 4
4' Oaks

+00 T.P. 22'

93

92

91

90

89

88

87

+97 T.P. 28'

+45 End G.R. 14'

+52 End G.R. 14'

+01. P.P. 28'

+86 - T.P. 27

+54 = 24" x 64" P. 3



+79 Bog. G.R. 14'

+21 T.P. 26'

+64 Bog. G.R. 14'

+64 P.P. 29

+47 F.E.

12" x 18" C.M. 24

+66' Rd Sq. 17'

+41 P.P. 29'

+72 T.P. 24'

Hay Field

Hay Field

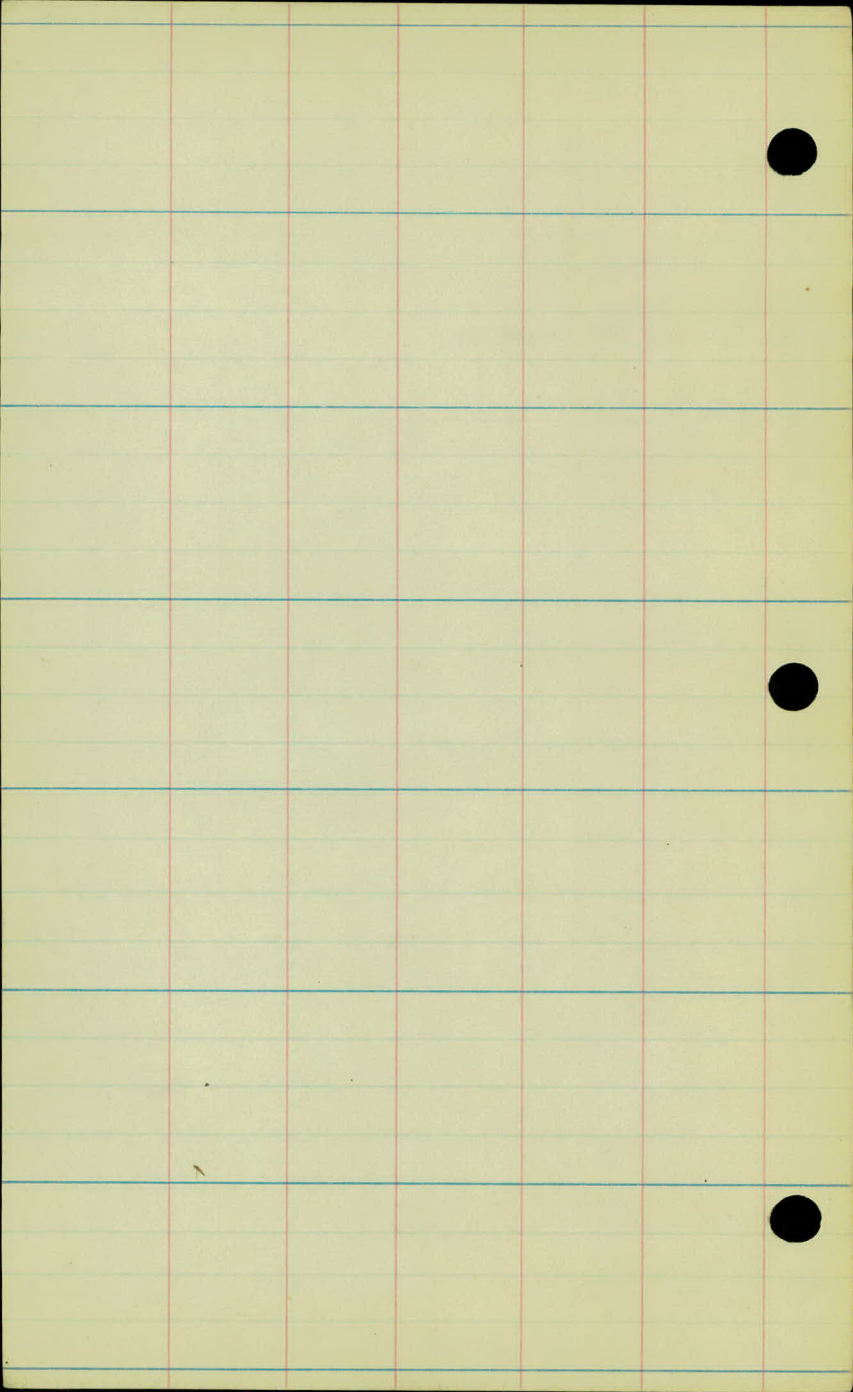
+09 P.P. 23'

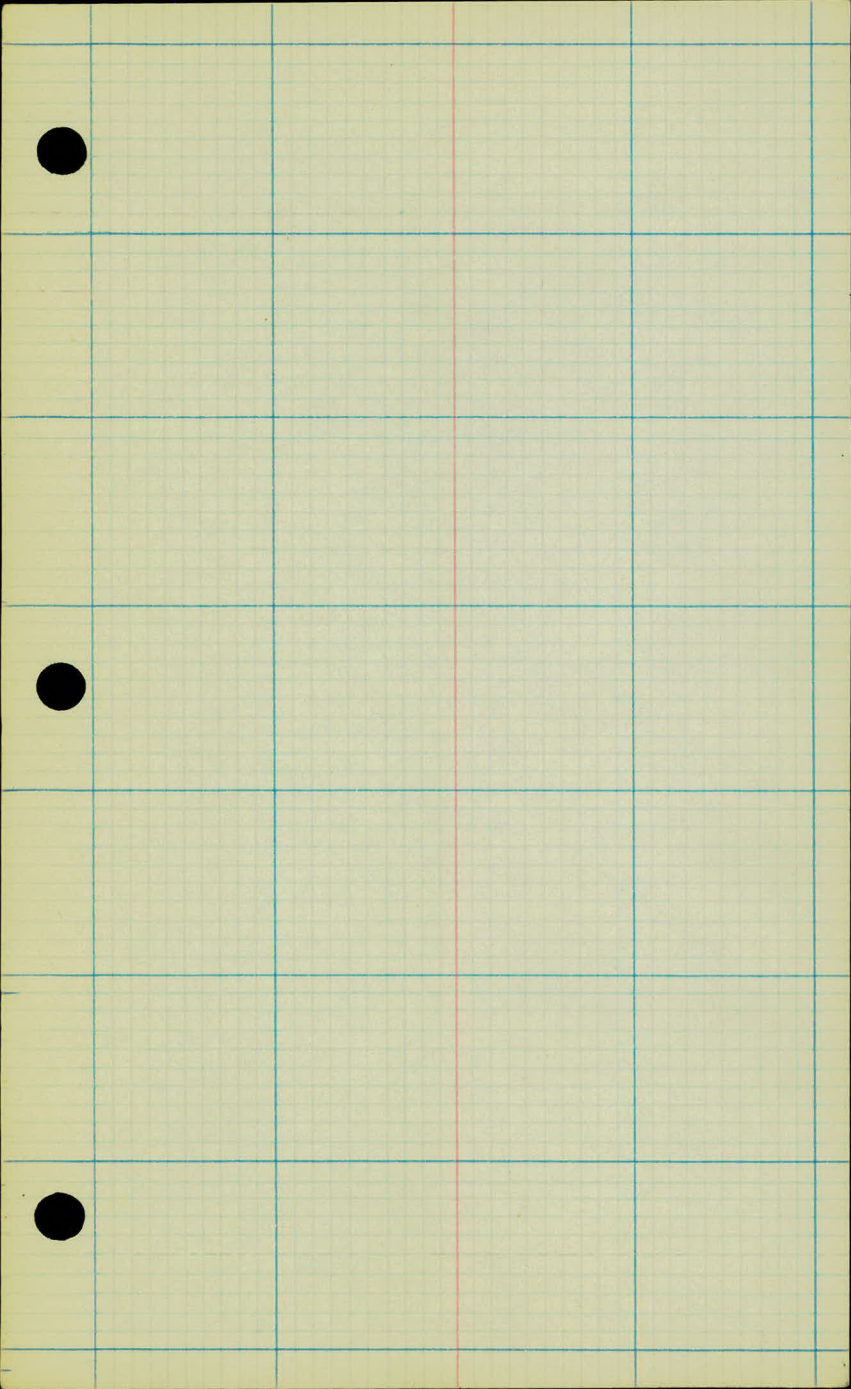
+17 T.P. 23'

Bog. Hay Field.
+50 End Cult.

+79 P.P. 25'

Bog. Hay Measure
+00 End Cultivation





51

50

49

48

47

$46 + 14\sqrt{3} = \text{Beg. of "B" Line}$

11-14-29.

+55 int Fence

Cultivation

← 36' →

Pig Pen

46-98 on "B" Line
245

+80 Int. F.

+75 = 2-10" Cats. 22'
+70 = Clearing

Mont □
+48 & R. 28'

Pig Pen

Shed
180' x 20' H

Ch. Coop
132'

178'

178'

178'

25' F. House
22'

2" x 2" Hub

90°

+76 P.P. 27

50°

01000

6-8' C.H.

150'

58

57

56

55

54

53

52

+90-8" Oak #2
+80-8" Oak #1

Cult.

Cult.

65

64

63

62

61

60

59

+70 Int Fence

Cult.

Pasture

Pasture Cult.

76'

+05-6'00k 25'

+74 Int Fence

Pasture

Pasture

x

+00 Beg. Pasture

+00 Beg. Pasture

72

71

70

69

68

67

66

—
Cultivated

—
Cultivated

79

78

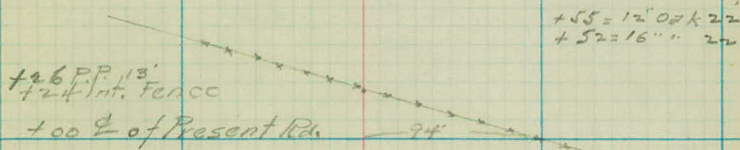
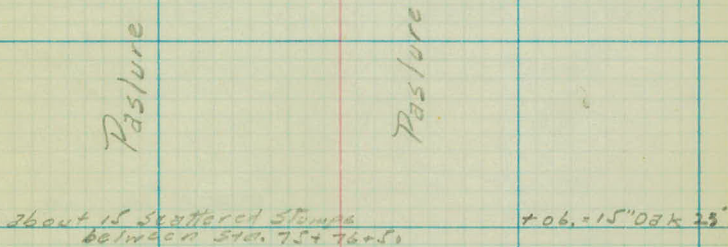
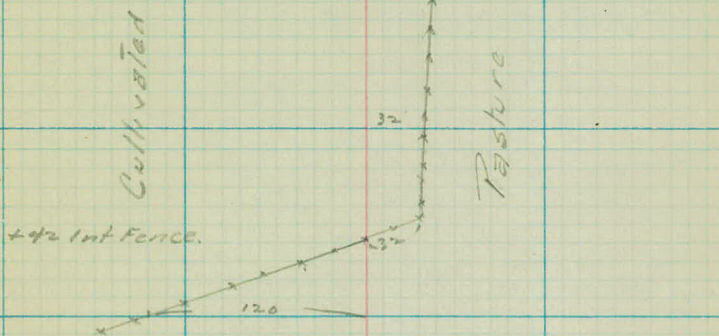
77

76

75

74

73



86

85

84

83

82

81

80

+39 Tri. Will. 25'

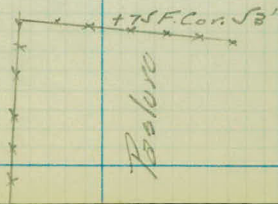
Hay Meadow

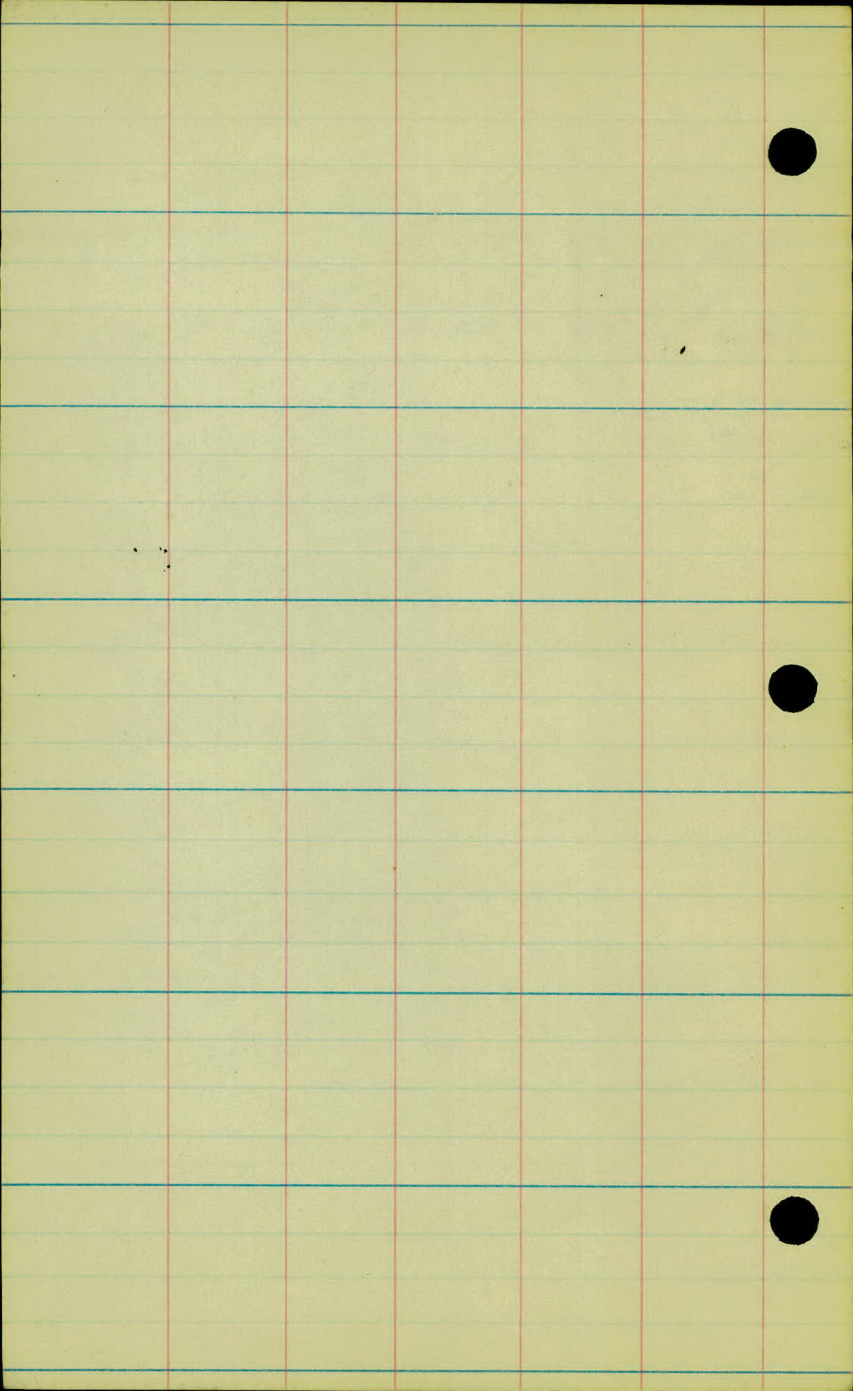
Hay Meadow

+88 Beq. Hay Meadow.

Cult.

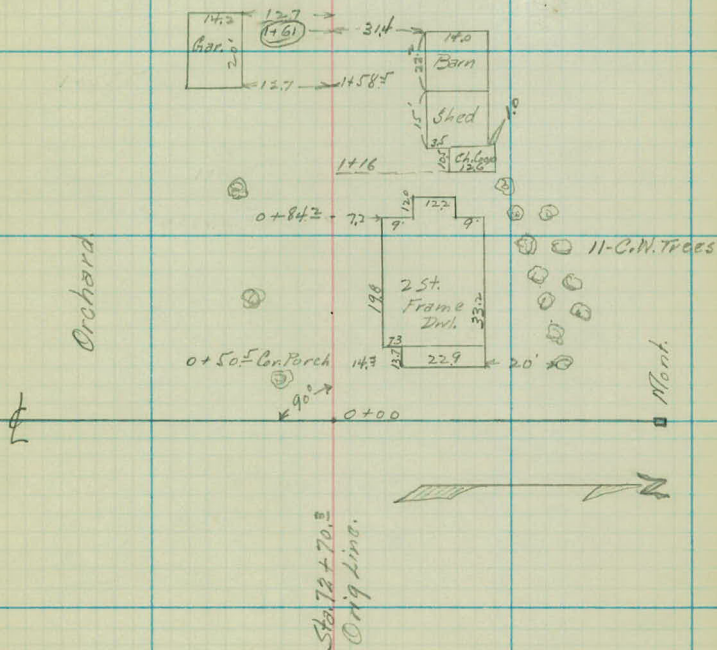
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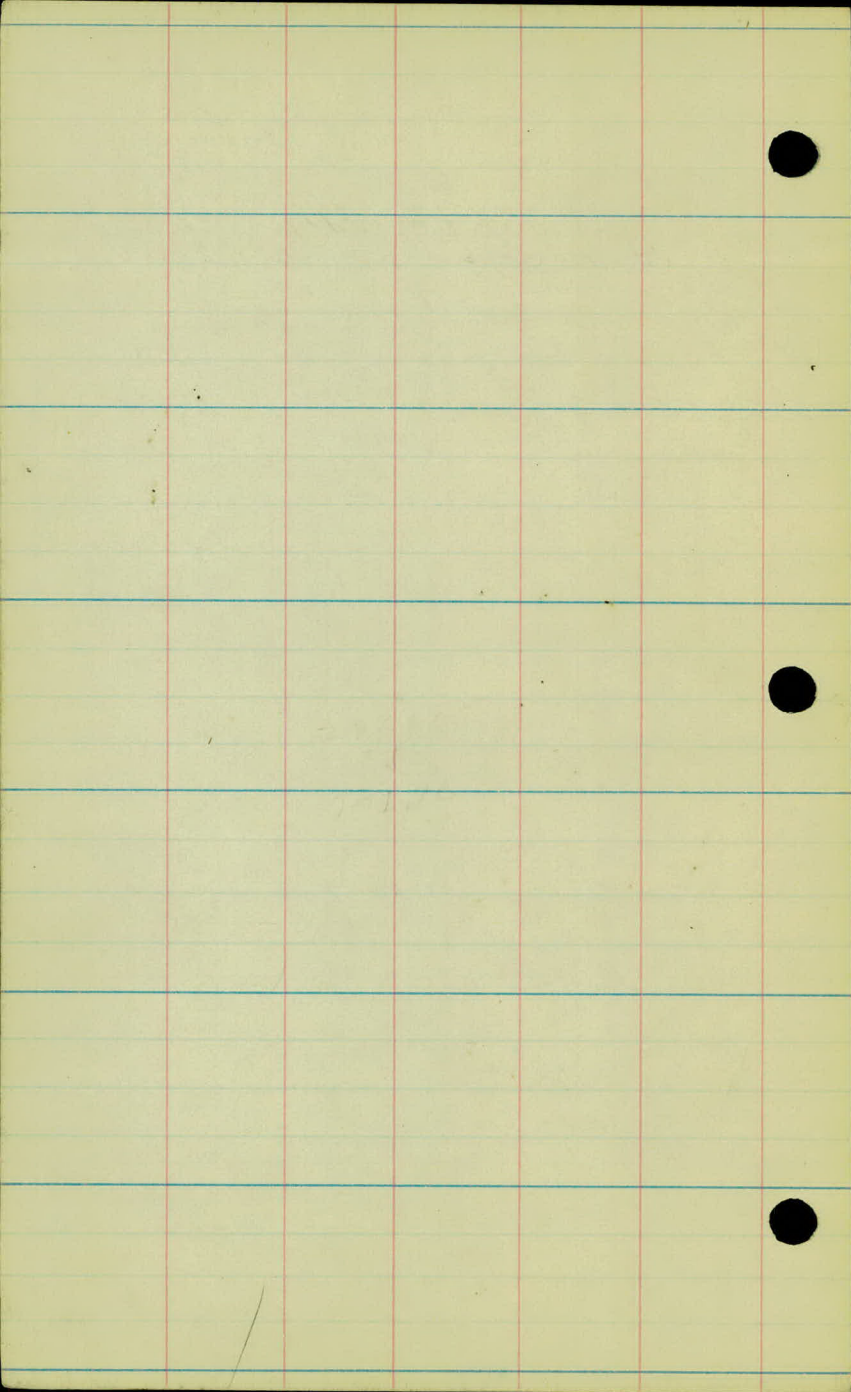




11-14-29

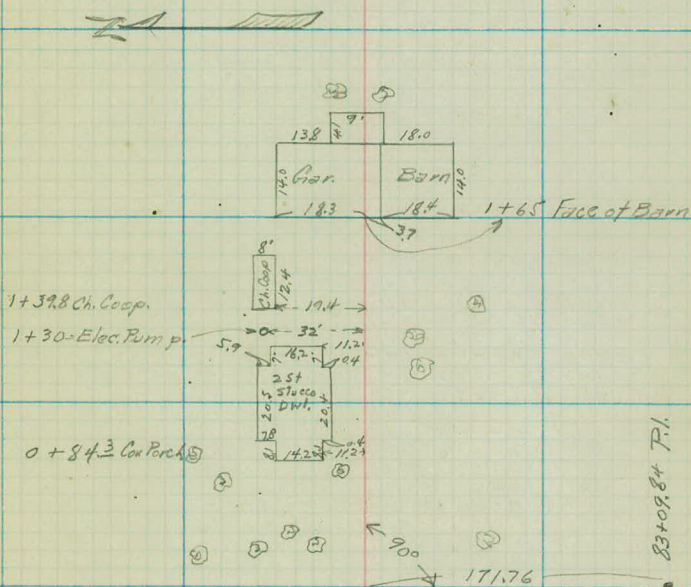
Locations of Bldg's opposite
Sta. 72+70.5 On. Orig. line.

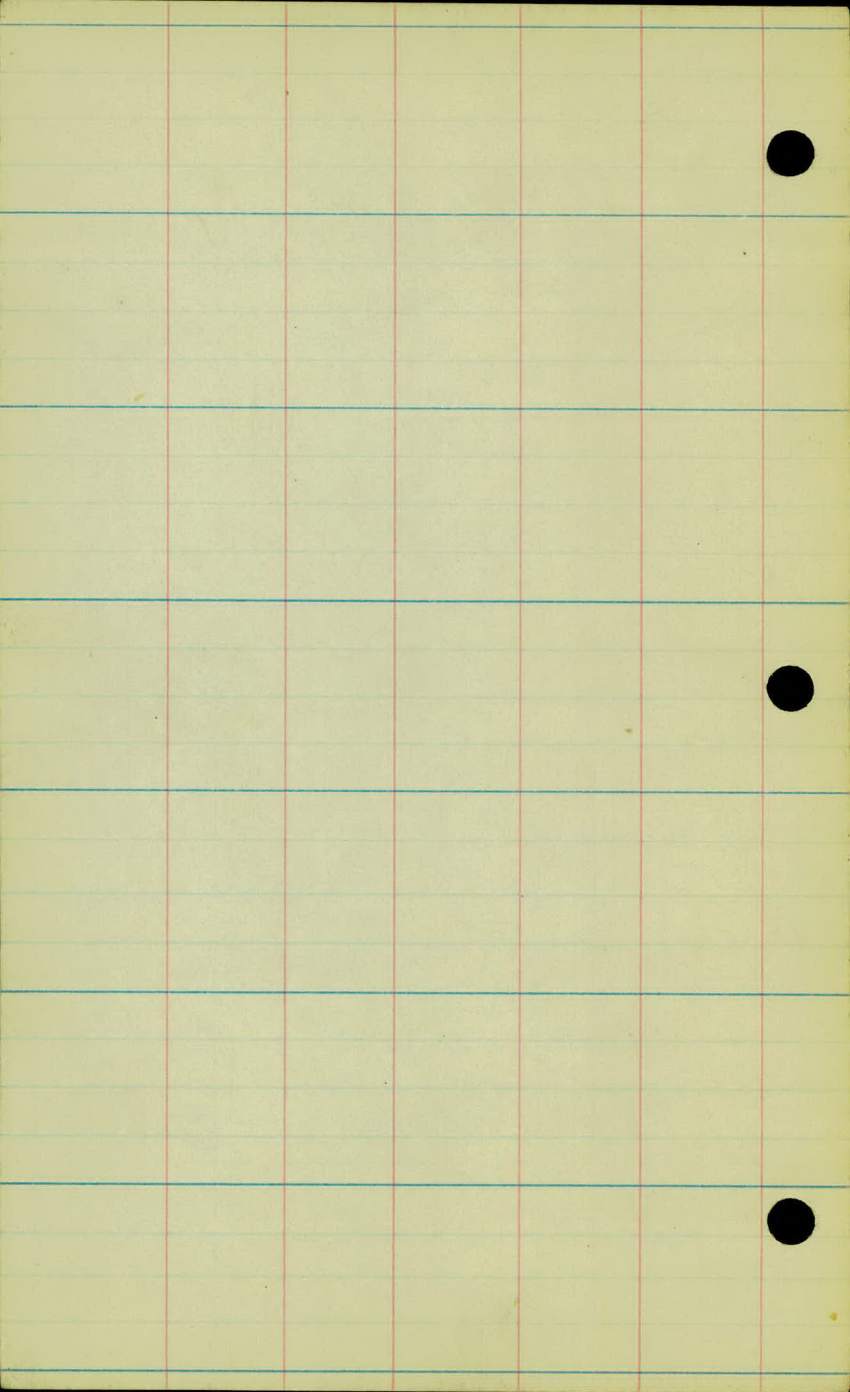




11-14-29

Location of Bldg's 171.76 H.No.
of P.I. at Sta. 83+09.84 Orig Line.





ARTIFICIAL TOPOGRAPHY

"B" LINE

Proj. 30-12

80

79

78

77

76

75

74

+69 F. COX 68

CULTIVATED

F. 37

+40 X. F.

+57 F. COX 33

SWAMP

WOODED PASTURE

86

85

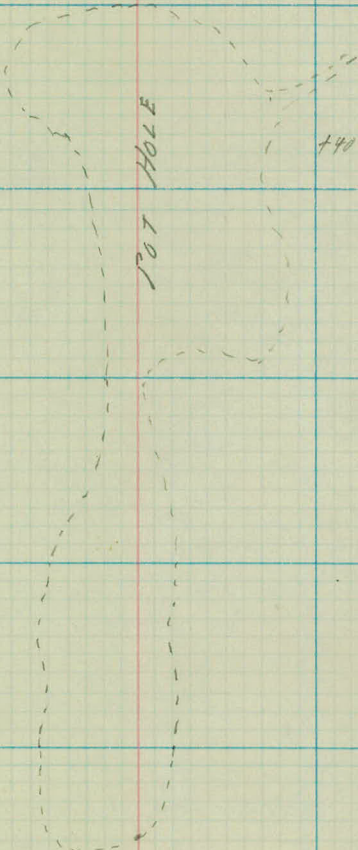
84

83

82

81

80



POT HOLE

40 WILLOW 12

UNCULTIVATED

92

91

90

89

88

87

86

+27 T.P. 24

+00 T.P. 21

+70 T.P. 13

+25 T.P. 38
-20 $\frac{1}{2}$ 190190

+07 P.P.S

98

97

96

95

94

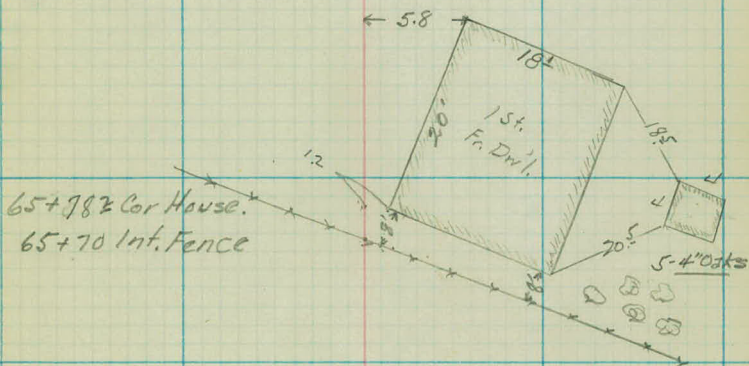
93

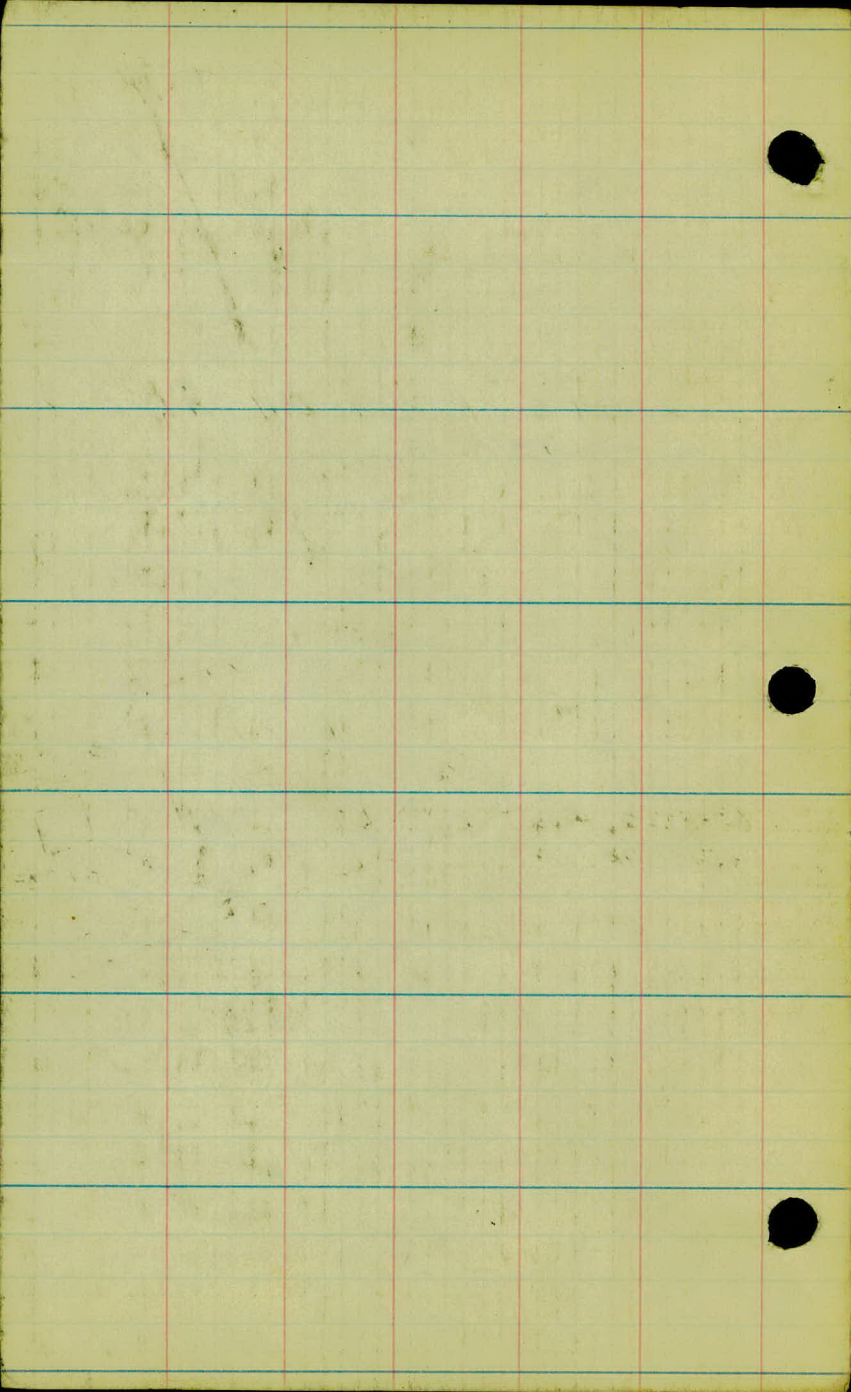
92

11-14-39



Location of Frame Drill on "B" Line
Sta. 65+87.3





New Brighton
LONG LAKE ROAD
"A" LINE

CROSS SECTIONS FROM STA 0+00
TO STA 99+00.

STA	+	H.I.	-	ELEV
B.M.	3.62	89.111		88749

0+00				86.56
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0+50				86.86
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0+59 ^s	TOP OF PAIR			86.93
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0+64 ^s	TOP OF PAIR			87.01
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1+00				86.0
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1+50				86.0
------	--	--	--	------

2+00				85.9
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2+50				85.9
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3+00				86.1
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3+50				86.5
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4+00				87.0
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4+50				86.8
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ON N.W. COR LOWER CONC STEP IN FRONT OF MEN

BRIGHTON POST OFFICE

43 457 448 458 46 10E 103 123 145
 43 18 8 4.55 1 10 12 17 33 43

39 414 50 50
 43 30 4.25 38 43

3.72 4.20
 50 4.18 50

3.69 4.24
 50 4.10 50

57 51 52 58 144 158
 45 22 5.1 7 12 17 43

97 51 5.5 55 94 126
 43 34 17 51 14 27 43

36 35 68 56 58 62 71
 43 30 14 10 5.2 17 25 43

ON PAVED DRIVEWAY
 00 00 62 59 4.9 5.3 47 46
 43 42 26 9 5.2 17 27 37 43

71.5 71.0 41 5.8 5.4 4.8 5.0 4.8
 43 43 32 25 7 50 12 25 43

71.0 06 49 5.2 4.4 4.8 5.4
 43 40 27 14 4.6 7 24 43

00 14 38 46 4.4 5.8 6.3
 43 37 34 15 41 19 35 43

70.5 05 49 5.3 4.6 4.4 4.7 8.1 7.6
 43 39 30 19 16 4.3 10 21 27 43

891.11 ✓

5+00

86.9

T.P

5.64

892.54 ✓

4.21

886.90 ✓

5+50

86.8

6+00

86.7

6+56

86.6

7+00

86.7

7+50

86.9

8+00

86.9

8+50

87.2 ✓

P.M.

4.95

887.59 ✓

9+00

87.2

9+46

86.7

10+00

86.2

10+50

85.9

11+00

88.16 ✓

84.39 ✓

85.4

3.77

883.21

8.15

872.44

$\frac{1.5}{43}$	$\frac{1.5}{41}$	$\frac{5.6}{31}$	$\frac{6.0}{25}$	$\frac{4.5}{15}$	4.2	$\frac{4.2}{13}$	$\frac{11.5}{32}$	$\frac{10.0}{43}$
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$\frac{7.0}{43}$	$\frac{8.0}{38}$	$\frac{8.8}{19}$	$\frac{6.0}{13}$	5.7	$\frac{6.0}{14}$	$\frac{11.3}{27}$	$\frac{12.0}{43}$
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$\frac{10.0}{43}$	$\frac{10.5}{19}$	$\frac{5.9}{10}$	5.8	$\frac{6.1}{14}$	$\frac{11.9}{28}$	$\frac{13.0}{34}$	$\frac{13.2}{43}$
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$\frac{6.5}{43}$	$\frac{10.4}{28}$	$\frac{12.0}{17}$	$\frac{5.9}{9}$	5.9	$\frac{6.3}{16}$	$\frac{11.9}{30}$	$\frac{12.5}{43}$
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$\frac{5.9}{43}$	$\frac{9.4}{26}$	$\frac{9.2}{16}$	$\frac{5.9}{10}$	5.8	$\frac{6.4}{16}$	$\frac{10.8}{24}$	$\frac{12.2}{43}$
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$\frac{7.5}{43}$	$\frac{7.3}{21}$	$\frac{5.5}{14}$	5.6	$\frac{6.4}{12}$	$\frac{9.9}{18}$	$\frac{11.1}{36}$	$\frac{12.5}{43}$
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$\frac{5.9}{43}$	$\frac{5.8}{31}$	$\frac{5.1}{8}$	5.6	$\frac{6.4}{14}$	$\frac{11.4}{22}$	$\frac{13.0}{43}$
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$\frac{4.0}{43}$	$\frac{4.9}{9}$	5.3	$\frac{5.2}{9}$	$\frac{5.1}{19}$	$\frac{6.0}{43}$
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S.W. COR. MONT. INT. LONG H.K. ROAD. OLD S.T.H. #62

$\frac{3.6}{34}$	$\frac{3.2}{30}$	$\frac{4.8}{19}$	$\frac{5.7}{72}$	5.3	$\frac{5.9}{10}$	$\frac{4.8}{14}$	$\frac{5.4}{31}$	$\frac{6.3}{43}$
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$\frac{5.3}{43}$	$\frac{4.1}{35}$	$\frac{4.4}{28}$	$\frac{5.0}{16}$	$\frac{6.2}{12}$	5.8	$\frac{6.0}{14}$	$\frac{5.6}{22}$	$\frac{6.3}{43}$
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$\frac{7.5}{43}$	$\frac{7.0}{24}$	$\frac{6.2}{15}$	$\frac{6.6}{9}$	6.3	$\frac{6.6}{10}$	$\frac{5.5}{24}$	$\frac{5.4}{43}$
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$\frac{8.9}{43}$	$\frac{7.0}{25}$	$\frac{6.9}{9}$	6.6	$\frac{6.8}{19}$	$\frac{5.8}{29}$	$\frac{5.3}{43}$
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$\frac{9.5}{43}$	$\frac{8.6}{36}$	$\frac{7.4}{14}$	7.1	$\frac{7.5}{19}$	$\frac{6.8}{32}$	$\frac{6.7}{43}$
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88.16 ✓
885.21

single space
to here

11+50

84.7

12+00

84.1

12+50

84.1

13+00

84.0

13+50

83.9

14+00

83.2

14+50

83.1

15+00

82.6

15+50

82.4

CROSS DRAIN

16+00

82.8

16+50

83.8

17+00

8.72

895.89 ✓

1.05

87.11

882.16

85.6 ✓

887.11

17+50

85.8

$\frac{29}{43}$ $\frac{74}{36}$ $\frac{63}{26}$ $\frac{46}{20}$ $\frac{54}{13}$ 3.5 $\frac{3.5}{18}$ 4.7 4.9 4.2 $\frac{4.0}{43}$

$\frac{83}{43}$ $\frac{83}{46}$ $\frac{76}{27}$ $\frac{41}{12}$ 4.1 $\frac{4.4}{12}$ $\frac{6.7}{17}$ $\frac{74}{31}$ $\frac{81}{43}$

$\frac{0.5}{43}$ $\frac{0.9}{36}$ $\frac{44}{28}$ $\frac{4.1}{10}$ 4.1 $\frac{4.4}{14}$ $\frac{7.8}{21}$ $\frac{8.0}{43}$

$\frac{0.2}{43}$ $\frac{0.4}{34}$ $\frac{48}{21}$ $\frac{42}{13}$ $\frac{43}{9}$ 4.2 $\frac{4.5}{12}$ $\frac{5.3}{14}$ $\frac{4.5}{25}$ $\frac{5.4}{34}$ $\frac{5.8}{43}$

$\frac{10.5}{43}$ $\frac{10.5}{35}$ $\frac{0.0}{34}$ $\frac{48}{26}$ $\frac{45}{14}$ 4.3 $\frac{4.5}{10}$ $\frac{5.6}{17}$ $\frac{4.2}{21}$ $\frac{4.7}{38}$ $\frac{5.7}{43}$

$\frac{3.7}{43}$ $\frac{3.7}{33}$ $\frac{5.5}{28}$ $\frac{5.2}{13}$ 5.0 $\frac{5.3}{13}$ $\frac{6.4}{18}$ $\frac{7.7}{43}$

$\frac{8.9}{43}$ $\frac{7.7}{21}$ $\frac{5.1}{11}$ 5.1 $\frac{5.3}{11}$ $\frac{10.1}{29}$ $\frac{10.1}{43}$

$\frac{73}{43}$ $\frac{94}{26}$ $\frac{8.4}{20}$ $\frac{60}{11}$ 5.6 $\frac{5.9}{11}$ $\frac{8.0}{15}$ $\frac{10.3}{23}$ $\frac{10.9}{43}$

$\frac{98}{43}$ $\frac{90}{76}$ $\frac{5.7}{9}$ 5.9 $\frac{6.0}{11}$ $\frac{10.1}{20}$ $\frac{10.8}{28}$ $\frac{10.7}{43}$
 12.9 12.9

$\frac{10.6}{43}$ $\frac{10.3}{42}$ $\frac{9.5}{17}$ $\frac{5.5}{10}$ 5.4 $\frac{5.5}{10}$ $\frac{9.5}{15}$ $\frac{10.4}{20}$ $\frac{10.6}{43}$

$\frac{10.5}{43}$ $\frac{10.2}{31}$ $\frac{8.2}{20}$ $\frac{4.1}{12}$ $\frac{4.5}{10}$ 4.4 $\frac{4.5}{10}$ $\frac{8.0}{15}$ $\frac{9.1}{20}$ $\frac{11.2}{43}$

$\frac{8.0}{43}$ $\frac{7.8}{40}$ $\frac{3.0}{29}$ $\frac{2.4}{23}$ $\frac{3.4}{20}$ 2.6 $\frac{2.8}{5}$ $\frac{7.9}{14}$ $\frac{10.5}{23}$ $\frac{10.3}{26}$ $\frac{10.3}{43}$

$\frac{8.2}{43}$ $\frac{8.3}{35}$ $\frac{8.3}{25}$ $\frac{8.6}{11}$ 10.0 $\frac{15.5}{8}$ $\frac{15.6}{18}$ $\frac{16.4}{43}$

		895.83				
18+00						88.3
	12.91	906.83	1.91	893.92		
18+50						96.5
19+00						900.6
19+50						01.7
20+00						02.1
20+50						01.5
21+00						02.3
21+50						03.6
22+00						03.1
22+50						03.0
23+00						03.2
	2.95	906.84	2.94	903.89		
23+50						03.7
24+00						03.0

$\frac{67}{45}$	$\frac{73}{31}$	$\frac{58}{27}$	$\frac{66}{18}$	7.5	$\frac{89}{13}$	$\frac{111}{35}$	$\frac{118}{43}$
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$\frac{146}{50}$	$\frac{142}{45}$	$\frac{74}{28}$	10.3	$\frac{12.9}{20}$	$\frac{14.1}{43}$
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$\frac{67}{43}$	$\frac{67}{22}$	6.2	$\frac{66}{30}$	$\frac{68}{43}$
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$\frac{66}{43}$	$\frac{66}{31}$	$\frac{53}{16}$	5.1	$\frac{45}{27}$	$\frac{42}{43}$
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$\frac{54}{43}$	$\frac{54}{21}$	4.7	$\frac{3.2}{27}$	$\frac{2.8}{43}$
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$\frac{59}{43}$	$\frac{5.7}{21}$	5.3	$\frac{4.9}{43}$
-----------------	------------------	-----	------------------

$\frac{60}{43}$	$\frac{51}{26}$	4.5	$\frac{4.4}{30}$	$\frac{4.4}{43}$
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$\frac{57}{43}$	$\frac{47}{27}$	$\frac{37}{7}$	3.2	$\frac{3.1}{18}$	$\frac{3.0}{43}$
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$\frac{49}{43}$	$\frac{39}{18}$	3.7	$\frac{3.0}{15}$	$\frac{2.7}{43}$
-----------------	-----------------	-----	------------------	------------------

$\frac{50}{43}$	$\frac{44}{17}$	3.8	$\frac{3.3}{18}$	$\frac{2.4}{43}$
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$\frac{49}{43}$	$\frac{43}{23}$	3.6	$\frac{2.8}{15}$	$\frac{1.9}{43}$
-----------------	-----------------	-----	------------------	------------------

$\frac{3.8}{43}$	$\frac{36}{20}$	3.1	$\frac{2.3}{25}$	$\frac{1.5}{43}$
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$\frac{3.2}{43}$	$\frac{35}{20}$	3.8	$\frac{4.0}{15}$	$\frac{3.9}{43}$
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906.84 ✓

24+50

02.6

25+00

03.0

25+50

03.8

26+00

01.8

26+08

900.0

26+70

98.9

27+00

99.3

27+50

96.2

28+00

94.2 ✓

B.M.

✓ 15.97 893.57 893.57

T.P.

0.17 895.43 11.58 895.24 ✓

28+50

93.2

29+00

94.6

29+50

94.5

$\frac{2.2}{43}$ $\frac{2.9}{23}$ 4.2 $\frac{5.9}{23}$ $\frac{7.4}{43}$

$\frac{4.3}{43}$ $\frac{4.4}{38}$ $\frac{1.7}{30}$ $\frac{2.4}{25}$ 3.8 $\frac{6.7}{24}$ $\frac{9.6}{43}$

$\frac{5.0}{43}$ $\frac{4.8}{31}$ $\frac{5.1}{20}$ $\frac{2.1}{19}$ $\frac{5.2}{7}$ 3.5 $\frac{6.5}{22}$ $\frac{9.6}{25}$ $\frac{10.3}{43}$

$\frac{2.3}{43}$ $\frac{1.9}{37}$ $\frac{6.0}{27}$ $\frac{5.9}{17}$ $\frac{6.5}{3}$ 5.0 $\frac{5.5}{8}$ $\frac{6.7}{23}$ $\frac{10.0}{43}$

$\frac{3.4}{43}$ $\frac{2.5}{31}$ $\frac{6.4}{21}$ $\frac{6.2}{12}$ 6.8 $\frac{5.2}{6}$ $\frac{6.3}{18}$ $\frac{7.7}{32}$ $\frac{9.2}{43}$

$\frac{5.6}{43}$ $\frac{5.8}{25}$ $\frac{5.1}{10}$ 7.9 $\frac{8.0}{13}$ $\frac{8.5}{23}$ $\frac{7.9}{26}$ $\frac{8.9}{43}$

$\frac{7.4}{43}$ $\frac{7.3}{23}$ 7.5 $\frac{8.7}{12}$ $\frac{8.5}{21}$ $\frac{9.0}{37}$ $\frac{8.7}{43}$

$\frac{11.6}{43}$ $\frac{11.2}{37}$ 10.4 $\frac{10.2}{16}$ $\frac{9.6}{17}$ $\frac{10.0}{27}$ $\frac{9.8}{37}$ $\frac{10.0}{43}$

$\frac{15.0}{43}$ $\frac{13.7}{20}$ 12.6 $\frac{12.5}{20}$ $\frac{11.6}{33}$ $\frac{11.9}{43}$

SPK IN 12" COTTONWOOD 100' RT. STA. 27750

$\frac{4.5}{43}$ $\frac{3.5}{16}$ 2.2 $\frac{2.2}{14}$ $\frac{1.8}{43}$

$\frac{4.5}{43}$ $\frac{1.2}{11}$ 0.8 $\frac{2.8}{27}$ $\frac{3.8}{43}$

$\frac{1.0}{43}$ $\frac{0.4}{17}$ 0.9 $\frac{3.7}{22}$ $\frac{6.1}{43}$

895.43

30+00					92.2
30+50					88.7
31+00					85.7
31+50					85.1
32+00					86.1
32+37					87.6
33+00					86.4
	676	892.22	7.97	885.46	
33+50					86.7
34+00					86.6
34+50					86.5
35+00					86.4
35+50					86.2
36+00					85.7

$\frac{23}{43}$ $\frac{21}{70}$ 3.2 $\frac{62}{23}$ $\frac{82}{43}$

$\frac{48}{43}$ $\frac{53}{18}$ 6.7 $\frac{91}{20}$ $\frac{113}{43}$

$\frac{20}{43}$ $\frac{82}{17}$ 9.7 $\frac{11.9}{19}$ $\frac{13.1}{51}$ $\frac{15.1}{43}$

$\frac{11.4}{43}$ $\frac{6.5}{22}$ 10.3 $\frac{8.6}{27}$ $\frac{6.0}{43}$

$\frac{138}{43}$ $\frac{121}{19}$ 9.3 $\frac{7.7}{19}$ $\frac{7.4}{54}$ $\frac{7.3}{43}$

$\frac{151}{43}$ $\frac{135}{26}$ $\frac{9.5}{15}$ 7.8 $\frac{7.7}{12}$ $\frac{8.5}{28}$ $\frac{7.5}{43}$

$\frac{151}{43}$ $\frac{137}{23}$ $\frac{9.0}{19}$ 9.0 $\frac{9.2}{11}$ $\frac{8.6}{12}$ $\frac{7.2}{28}$ $\frac{6.1}{43}$

NR16 IN

T.P. 17 STR. 33 + 25
 $\frac{101}{43}$ $\frac{98}{23}$ $\frac{5.5}{17}$ $\frac{5.8}{11}$ 5.5 $\frac{5.7}{9}$ $\frac{5.4}{18}$ $\frac{4.4}{21}$ $\frac{5.4}{33}$ $\frac{2.7}{43}$

$\frac{74}{43}$ $\frac{87}{23}$ $\frac{6.5}{17}$ $\frac{5.5}{11}$ $\frac{6.0}{10}$ 5.4 $\frac{5.8}{10}$ $\frac{5.3}{18}$ $\frac{3.6}{23}$ $\frac{2.2}{43}$

$\frac{8.8}{43}$ $\frac{8.1}{27}$ $\frac{7.0}{24}$ $\frac{5.7}{18}$ $\frac{6.0}{10}$ 5.7 $\frac{5.7}{10}$ $\frac{5.2}{19}$ $\frac{2.2}{26}$ $\frac{1.7}{43}$

$\frac{8.7}{43}$ $\frac{7.9}{23}$ $\frac{5.7}{17}$ $\frac{6.1}{11}$ 5.8 $\frac{5.8}{11}$ $\frac{5.7}{20}$ $\frac{3.0}{26}$ $\frac{2.1}{43}$

$\frac{9.4}{43}$ $\frac{8.7}{24}$ $\frac{5.6}{19}$ $\frac{6.2}{10}$ 6.0 $\frac{6.2}{12}$ $\frac{5.2}{16}$ $\frac{5.3}{21}$ $\frac{3.8}{26}$ $\frac{3.3}{43}$

$\frac{8.5}{43}$ $\frac{8.1}{29}$ $\frac{5.6}{14}$ $\frac{6.8}{8}$ 6.5 $\frac{6.7}{11}$ $\frac{5.1}{12}$ $\frac{2.8}{27}$ $\frac{3.2}{43}$

872.22 ✓

36+50

85.8

37+00

85.6

37+50

85.1

38+00

84.8

38+50

83.9

39+00

5.47

877.58 ✓

10.11

882.11 ✓

83.0

39+50

82.1

40+00

81.1

40+50

80.3

41+00

79.4

41+50

78.4 ✓

B.M.

5.14

882.44 ✓

882.43

42+00

77.5 ✓

1.77

878.41 ✓

10.94

876.64 ✓

42+50

76.3

67	62	58	61	66		66	47	47	01	11
<u>43</u>	<u>29</u>	<u>19</u>	<u>12</u>	<u>7</u>	64	<u>17</u>	<u>19</u>	<u>22</u>	<u>31</u>	<u>43</u>

46	44	3.0	5.2	5.2	67		67	35	1.0	1.3
<u>43</u>	<u>28</u>	<u>24</u>	<u>40</u>	<u>14</u>	7	66	<u>14</u>	<u>24</u>	<u>33</u>	<u>43</u>

75	72	58	69	75		72	58	1.0	0.0
<u>43</u>	<u>27</u>	<u>19</u>	<u>19</u>	<u>9</u>	71	<u>13</u>	<u>21</u>	<u>35</u>	<u>43</u>

11.2	10.7	67	77		77	64	41	4.6
<u>43</u>	<u>26</u>	<u>14</u>	<u>13</u>	74	<u>12</u>	<u>26</u>	<u>52</u>	<u>43</u>

15.0	13.3	8.6	7.2	8.2	8.5		84	7.3	81	9.8	8.8	9.0
<u>43</u>	<u>27</u>	<u>20</u>	<u>15</u>	<u>12</u>	<u>8</u>	8.5	<u>12</u>	<u>16</u>	<u>22</u>	<u>26</u>	<u>18</u>	<u>43</u>

140	133	106	74	95		94	101	94	102	102
<u>43</u>	<u>34</u>	<u>15</u>	<u>15</u>	<u>7</u>	9.2	<u>12</u>	<u>17</u>	<u>32</u>	<u>57</u>	<u>43</u>

7.8	68	57	57		57	50	57	57	59	37	2.3	31
<u>43</u>	<u>26</u>	<u>18</u>	<u>12</u>	5.5	<u>12</u>	<u>14</u>	<u>15</u>	<u>20</u>	<u>25</u>	<u>28</u>	<u>32</u>	<u>43</u>

76	71	60	60	68		67	63	64	30	0.5	10
<u>43</u>	<u>30</u>	<u>23</u>	<u>15</u>	<u>8</u>	65	<u>11</u>	<u>14</u>	<u>20</u>	<u>26</u>	<u>33</u>	<u>43</u>

84	7.3	5.5	7.5		7.5	7.2	6.8	0.8	10.5	10.5
<u>43</u>	<u>31</u>	<u>16</u>	<u>13</u>	7.3	<u>12</u>	<u>14</u>	<u>22</u>	<u>28</u>	<u>33</u>	<u>43</u>

83	7.2	5.8	60	83	85		85	73	1.0	0.0	0.0
<u>43</u>	<u>31</u>	<u>21</u>	<u>17</u>	<u>14</u>	<u>8</u>	8.2	<u>12</u>	<u>18</u>	<u>25</u>	<u>29</u>	<u>43</u>

74	61	50	27		74	27	2.3	14	24
<u>43</u>	<u>31</u>	<u>22</u>	<u>18</u>	9.2	<u>12</u>	<u>15</u>	<u>23</u>	<u>28</u>	<u>43</u>

SPX. IN T.P. 23. LT. ST. 41 + 70.

8.1	7.5	10.3	10.3		10.4	7.5	64	5.3	6.3	70
<u>43</u>	<u>27</u>	<u>22</u>	<u>8</u>	10.1	<u>12</u>	<u>18</u>	<u>24</u>	<u>27</u>	<u>31</u>	<u>43</u>

29	16	31	10	14		2.5	1.7	16	12
<u>43</u>	<u>28</u>	<u>20</u>	<u>9</u>	<u>8</u>	2.1	<u>11</u>	<u>14</u>	<u>34</u>	<u>43</u>

87841 ✓

43+00

75.2

43+50

74.0

CROSS DRAIN

44+00

73.4

44+50

73.3

45+00

72.9

45+50

73.8

46+00

75.6

46+50

76.3

47+00

72.4

47+50

72.0

48+00

71.6

48+50

71.5 ✓

10.51 881.57 7.35 871.06 ✓

49+00

71.2

$\frac{7.7}{43}$ $\frac{7.7}{31}$ $\frac{6.1}{20}$ $\frac{3.5}{9}$ 3.2 $\frac{3.5}{11}$ $\frac{3.0}{14}$ $\frac{4.6}{31}$ $\frac{5.0}{43}$

$\frac{9.5}{43}$ $\frac{9.6}{34}$ $\frac{9.0}{23}$ $\frac{4.8}{11}$ 4.4 $\frac{4.3}{14}$ $\frac{7.0}{23}$ $\frac{7.8}{43}$
13.5 13.8

$\frac{10.9}{43}$ $\frac{10.9}{38}$ $\frac{9.6}{30}$ $\frac{7.0}{24}$ $\frac{5.6}{13}$ 5.0 $\frac{5.1}{13}$ $\frac{8.2}{30}$ $\frac{8.2}{43}$

$\frac{8.6}{43}$ $\frac{6.3}{23}$ $\frac{5.6}{13}$ 5.1 $\frac{5.2}{14}$ $\frac{4.8}{16}$ $\frac{6.3}{43}$

$\frac{6.1}{43}$ $\frac{5.8}{20}$ 5.5 $\frac{5.0}{15}$ $\frac{5.2}{29}$ $\frac{4.6}{32}$ $\frac{5.4}{43}$

$\frac{5.4}{43}$ $\frac{4.5}{20}$ 4.6 $\frac{4.6}{20}$ $\frac{5.7}{27}$ $\frac{4.8}{43}$

$\frac{3.8}{43}$ $\frac{3.2}{20}$ 2.8 $\frac{1.5}{29}$ $\frac{5.5}{36}$ $\frac{5.2}{43}$

$\frac{3.2}{43}$ $\frac{3.0}{14}$ 2.1 $\frac{1.7}{4}$ $\frac{4.4}{7}$ $\frac{6.1}{12}$ $\frac{5.1}{30}$ $\frac{5.5}{43}$

$\frac{5.4}{43}$ $\frac{5.6}{31}$ $\frac{4.6}{10}$ $\frac{6.9}{5}$ 6.0 $\frac{5.5}{13}$ $\frac{5.8}{25}$ $\frac{7.7}{43}$

$\frac{7.8}{43}$ $\frac{8.3}{17}$ $\frac{7.1}{10}$ 6.4 $\frac{6.3}{6}$ $\frac{6.8}{17}$ $\frac{9.0}{34}$ $\frac{9.2}{43}$

$\frac{7.8}{43}$ $\frac{5.1}{16}$ $\frac{6.9}{11}$ 6.8 $\frac{7.1}{13}$ $\frac{10.1}{30}$ $\frac{10.0}{43}$

$\frac{9.3}{43}$ $\frac{9.4}{19}$ $\frac{7.4}{11}$ 6.9 $\frac{7.6}{17}$ $\frac{10.1}{31}$ $\frac{9.3}{43}$

$\frac{12.4}{43}$ $\frac{12.7}{18}$ $\frac{10.7}{9}$ 10.2 $\frac{10.5}{10}$ $\frac{11.3}{18}$ $\frac{11.9}{31}$ $\frac{11.4}{43}$

881.37 ✓

49+50

71.3

50+00

71.4

50+50

71.0

51+00

69.3

51+50

69.4

52+00

69.8 ✓

B.M.

9.09

881.33 ✓

9.09

872.28 ✓

872.34

52+50

72.3

53+00

74.9

53+50

76.0

54+00

77.2

54+50

78.3

55+00

79.4 ✓

10.85

891.08 ✓

1.10

880.23 ✓

55+50

80.7

$\frac{12.6}{43}$	$\frac{12.7}{20}$	$\frac{10.6}{10}$	101	$\frac{10.6}{10}$	$\frac{9.2}{14}$	$\frac{11.1}{27}$	$\frac{9.2}{43}$
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$\frac{12.3}{43}$	$\frac{12.7}{20}$	$\frac{10.5}{12}$	100	$\frac{11.1}{8}$	$\frac{9.9}{10}$	$\frac{10.9}{19}$	$\frac{10.2}{43}$
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$\frac{12.4}{43}$	$\frac{12.4}{31}$	$\frac{10.7}{22}$	$\frac{10.3}{8}$	104	$\frac{11.4}{11}$	$\frac{11.4}{21}$	$\frac{10.1}{43}$
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$\frac{11.1}{43}$	$\frac{10.9}{29}$	$\frac{11.1}{18}$	$\frac{12.1}{9}$	121	$\frac{11.8}{27}$	$\frac{10.8}{43}$
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$\frac{10.7}{43}$	$\frac{11.7}{31}$	120	$\frac{11.3}{26}$	$\frac{10.8}{43}$
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$\frac{11.1}{43}$	$\frac{11.4}{20}$	11.5	$\frac{11.1}{22}$	$\frac{10.2}{43}$
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N.W. COR. OF MONT. SPR. 52753²⁶ P.I.

$\frac{8.8}{43}$	$\frac{7.1}{33}$	$\frac{8.0}{26}$	9.0	$\frac{7.4}{20}$	$\frac{9.5}{43}$
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$\frac{6.9}{43}$	$\frac{6.7}{28}$	$\frac{7.2}{17}$	$\frac{8.8}{12}$	$\frac{8.8}{9}$	64	$\frac{6.1}{8}$	$\frac{7.7}{22}$	$\frac{8.2}{43}$
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$\frac{6.6}{43}$	$\frac{7.1}{32}$	$\frac{6.0}{30}$	$\frac{5.4}{15}$	$\frac{5.5}{3}$	5.3	$\frac{6.0}{4}$	$\frac{8.0}{7}$	$\frac{8.0}{13}$	$\frac{5.8}{18}$	$\frac{2.0}{43}$
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$\frac{4.2}{43}$	$\frac{8.9}{29}$	$\frac{6.1}{24}$	$\frac{6.1}{22}$	$\frac{4.9}{18}$	$\frac{4.0}{6}$	41	$\frac{4.3}{5}$	$\frac{4.4}{12}$	$\frac{6.7}{16}$	$\frac{6.7}{20}$	$\frac{2.9}{28}$	$\frac{2.8}{43}$
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$\frac{2.8}{43}$	$\frac{2.9}{30}$	$\frac{1.0}{28}$	$\frac{2.3}{23}$	$\frac{4.6}{18}$	$\frac{4.6}{13}$	$\frac{3.4}{12}$	3.0	$\frac{3.2}{8}$	$\frac{2.9}{12}$	$\frac{5.0}{18}$	$\frac{4.2}{26}$	$\frac{1.5}{31}$	$\frac{2.5}{43}$
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$\frac{2.4}{43}$	$\frac{2.5}{36}$	$\frac{0.9}{27}$	$\frac{3.7}{20}$	$\frac{2.0}{14}$	$\frac{2.3}{11}$	1.7	$\frac{2.1}{6}$	$\frac{1.3}{14}$	$\frac{2.4}{19}$	$\frac{4.6}{26}$	$\frac{5.9}{43}$
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$\frac{14.5}{43}$	$\frac{14.4}{39}$	$\frac{12.0}{26}$	$\frac{13.2}{23}$	$\frac{10.8}{19}$	$\frac{10.8}{14}$	10.4	$\frac{10.6}{11}$	$\frac{9.5}{13}$	$\frac{11.6}{42}$	$\frac{13.8}{14}$	$\frac{15.2}{32}$	$\frac{15.4}{43}$
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89108 ✓

56+00

81.9

56+50

83.1

57+00

84.4

57+50

85.7

58+00

87.0

8.82

89668 ✓

3.22

89786 ✓

58+50

87.8

59+00

88.4

59+50

89.2

60+00

90.2

60+50

91.2

61+00

91.6

61+50

91.6

62+00

92.3

107 107 91 96 9.5 84 94 124 145 16.2
 43 21 17 11 92 7 15 19 23 50 43

64 62 86 84 83 68 74 124 142 147
 43 28 17 12 8.0 8 12 19 27 30 43

41 41 45 69 70 64 66 82 95
 43 39 26 21 67 8 12 16 26 43

0.1 1.1 4.9 5.8 5.8 4.7 3.2 4.1
 43 27 20 11 5.4 9 13 22 43

10 1.1 5.2 3.8 4.2 4.5 3.2 3.0 2.0 0.0
 43 27 19 16 9 41 12 14 20 23 43

72 70 65 86 10.2 10.2 9.2 9.4 8.3 7.3 5.7 3.2
 43 31 26 18 14 14 11 8.9 11 13 21 24 43

70 80 71 73 9.1 9.1 8.5 86 7.7 6.7 6.7
 43 31 28 16 14 12 11 8.3 12 13 24 43

5.7 6.1 7.4 6.7 8.1 7.8 7.8 7.1 6.6 6.6
 43 28 20 17 13 10 7.5 11 13 24 43

5.9 6.5 8.7 6.9 6.5 6.9 6.9 5.7 5.0 4.4
 43 26 24 22 12 9 6.5 10 13 24 43

66 63 72 76 6.5 5.5 6.0 5.6 4.8 3.9 2.9
 43 28 26 24 22 11 10 5.5 10 13 22 43

8.1 7.6 5.6 5.3 4.4 3.4
 43 26 14 5.1 8 22 43

7.5 7.4 5.6 5.3 4.9 3.9 3.0
 43 24 17 5.1 9 16 22 43

7.0 6.4 4.7 4.7 4.5 5.0 4.0 4.0
 43 24 18 4.4 9 11 15 28 43

✓
896.68

62+60

92.7

63+00

✓
5.06 898.47 3.27 895.41

✓
92.9

63+50

93.1

64+00

93.2

64+50

93.1

65+00

93.1

65+50

93.3

66+00

93.3

66+50

93.3

67+00

93.1

67+50

93.1

68+00

93.1

68+50

93.1

$\frac{5.8}{43}$ $\frac{4.6}{32}$ $\frac{4.3}{22}$ $\frac{5.7}{18}$ $\frac{4.7}{16}$ $\frac{4.1}{12}$ 4.0 $\frac{4.5}{8}$ $\frac{4.4}{15}$ $\frac{3.5}{19}$ $\frac{4.0}{31}$ $\frac{4.0}{43}$

$\frac{7.0}{43}$ $\frac{6.6}{28}$ $\frac{4.1}{12}$ 3.8 $\frac{4.0}{10}$ $\frac{4.9}{19}$ $\frac{4.3}{29}$ $\frac{4.4}{35}$ $\frac{4.5}{43}$

$\frac{8.4}{43}$ $\frac{7.1}{28}$ $\frac{6.0}{16}$ 5.4 $\frac{5.6}{11}$ $\frac{6.2}{22}$ $\frac{5.4}{36}$ $\frac{4.6}{43}$

$\frac{8.7}{43}$ $\frac{8.7}{30}$ $\frac{6.4}{21}$ $\frac{5.7}{11}$ 5.3 $\frac{5.6}{9}$ $\frac{5.4}{17}$ $\frac{8.0}{22}$ $\frac{8.4}{43}$

$\frac{7.4}{43}$ $\frac{7.3}{32}$ $\frac{5.9}{24}$ $\frac{5.6}{12}$ 5.4 $\frac{5.7}{8}$ $\frac{5.0}{14}$ $\frac{8.2}{28}$ $\frac{8.2}{43}$

$\frac{5.7}{43}$ $\frac{5.6}{30}$ $\frac{4.7}{25}$ $\frac{5.6}{17}$ 5.4 $\frac{5.6}{18}$ $\frac{6.4}{12}$ $\frac{5.7}{19}$ $\frac{6.8}{23}$ $\frac{7.0}{43}$

8

$\frac{3.4}{43}$ $\frac{3.5}{28}$ $\frac{3.6}{20}$ $\frac{5.4}{16}$ 5.2 $\frac{5.6}{11}$ $\frac{4.6}{15}$ $\frac{4.1}{20}$ $\frac{5.0}{43}$

$\frac{1.0}{43}$ $\frac{1.1}{29}$ $\frac{1.7}{26}$ $\frac{5.5}{17}$ 5.2 $\frac{5.4}{10}$ $\frac{6.5}{18}$ $\frac{2.0}{43}$

$\frac{1.5}{43}$ $\frac{0.6}{31}$ $\frac{1.4}{24}$ $\frac{5.5}{18}$ $\frac{5.2}{16}$ 5.2 $\frac{5.4}{11}$ $\frac{2.3}{17}$ $\frac{1.2}{43}$

$\frac{2.4}{43}$ $\frac{2.4}{26}$ $\frac{5.9}{18}$ 5.4 $\frac{5.6}{11}$ $\frac{3.5}{17}$ $\frac{2.2}{43}$

$\frac{6.3}{43}$ $\frac{5.4}{27}$ $\frac{6.5}{24}$ $\frac{6.6}{19}$ $\frac{5.5}{14}$ 5.4 $\frac{6.0}{13}$ $\frac{5.4}{16}$ $\frac{6.4}{43}$

$\frac{8.7}{43}$ $\frac{8.6}{25}$ $\frac{5.9}{19}$ 5.4 $\frac{5.6}{7}$ $\frac{6.8}{10}$ $\frac{8.3}{27}$ $\frac{7.5}{43}$

$\frac{6.6}{43}$ $\frac{7.6}{35}$ $\frac{8.0}{25}$ $\frac{8.8}{22}$ $\frac{5.6}{15}$ 5.4 $\frac{5.8}{9}$ $\frac{7.6}{15}$ $\frac{8.1}{31}$ $\frac{7.2}{37}$ $\frac{7.6}{43}$

898.47 ✓

69+00

93.0

69+50

92.7

5.16 897.67 ✓ 5.96 892.51 ✓

70+00

92.6

B.M.

1.65 895.02 895.03 ✓

70+50

92.3

71+00

92.4

71+50

92.5

72+00

92.6

72+50

92.9

73+00

93.0

73+50

92.8

74+00

92.3

74+50

92.1

75+00

92.3

CROSS DRAIN

		897.67				92.6
75+50						
	9.62	902.25	5.04	872.63		
B.M.	3.37	902.60	3.07	899.18	899.23	
76+00						90.0
76+50						92.8
77+00						96.2
77+50						97.0
78+00						95.8
78+50						96.1
79+00						97.9
79+50						98.6
80+00						99.3
	9.41	910.62	1.39	901.21		
80+50						900.0
81+00						10.8

$\frac{5.3}{43}$	$\frac{40}{33}$	$\frac{63}{25}$	$\frac{80}{17}$	$\frac{79}{11}$	$\frac{5.6}{7}$	5.1	$\frac{5.0}{7}$	$\frac{58}{17}$	$\frac{7.9}{22}$	$\frac{11.3}{28}$	$\frac{11.0}{43}$
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SPK IN 18" OAK 100' RT STA 77+75.

$\frac{7.9}{43}$	$\frac{11.0}{32}$	$\frac{12.4}{20}$	12.4	4	$\frac{11.6}{7}$	$\frac{9.9}{9}$	$\frac{9.4}{24}$	$\frac{9.7}{36}$	$\frac{10.8}{43}$
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$\frac{8.8}{43}$	$\frac{11.4}{36}$	$\frac{10.8}{31}$	$\frac{10.6}{17}$	9.8	$\frac{9.5}{10}$	$\frac{10.4}{22}$	$\frac{10.5}{26}$	$\frac{9.2}{32}$	$\frac{8.7}{43}$
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$\frac{10.4}{43}$	$\frac{10.4}{35}$	$\frac{8.3}{30}$	$\frac{7.7}{15}$	6.4	$\frac{4.6}{27}$	$\frac{4.2}{43}$
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$\frac{9.4}{43}$	$\frac{9.1}{33}$	$\frac{7.4}{17}$	5.6	$\frac{5.4}{27}$	$\frac{2.5}{43}$
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$\frac{9.6}{43}$	$\frac{7.5}{20}$	6.8	$\frac{6.9}{13}$	$\frac{7.6}{22}$	$\frac{6.5}{28}$	$\frac{5.5}{43}$
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$\frac{10.5}{43}$	$\frac{10.4}{30}$	$\frac{9.7}{9}$	6.5	$\frac{5.5}{6}$	$\frac{4.9}{17}$	$\frac{5.8}{27}$	$\frac{6.8}{40}$	$\frac{8.0}{43}$
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$\frac{9.5}{43}$	$\frac{9.1}{20}$	$\frac{5.4}{7}$	4.7	15	$\frac{5.0}{27}$	$\frac{9.7}{43}$
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$\frac{6.4}{43}$	$\frac{7.6}{25}$	$\frac{4.0}{13}$	4.0	11	$\frac{4.3}{17}$	$\frac{6.8}{37}$	$\frac{9.6}{43}$
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$\frac{0.4}{43}$	$\frac{2.2}{28}$	$\frac{5.6}{15}$	$\frac{3.7}{13}$	3.3	$\frac{3.6}{12}$	$\frac{7.8}{23}$	$\frac{9.0}{43}$
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$\frac{3.4}{43}$	$\frac{11.2}{30}$	$\frac{13.0}{27}$	$\frac{13.2}{17}$	$\frac{11.6}{14}$	10.6	$\frac{10.8}{12}$	$\frac{12.4}{20}$	$\frac{13.4}{43}$
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$\frac{5.0}{43}$	$\frac{11.3}{33}$	$\frac{11.4}{22}$	$\frac{10.6}{18}$	9.8	11	$\frac{9.7}{19}$	$\frac{11.2}{33}$	$\frac{16.4}{43}$
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910.62 ✓

81750

00.6

82700

99.6

82750

99.9

83700

01.6

83750

03.8

84700

04.8

84750

04.7

85700

04.5

85750

03.9

86700

3.28

906.70 ✓

7.20

903.42 ✓

02.7

86750

01.8

87700

00.9

87750

99.9

$\frac{11.5}{43}$ $\frac{94}{32}$ $\frac{96}{7}$ 10.0 $\frac{11.5}{19}$ $\frac{108}{43}$

$\frac{8.8}{43}$ $\frac{92}{32}$ $\frac{109}{20}$ $\frac{11.2}{7}$ 11.0 $\frac{92}{26}$ $\frac{8.2}{43}$

$\frac{11.6}{43}$ $\frac{116}{35}$ $\frac{114}{6}$ 10.7 $\frac{92}{15}$ $\frac{6.7}{30}$ $\frac{5.8}{43}$

$\frac{8.7}{43}$ $\frac{101}{34}$ $\frac{10.1}{7}$ 9.0 $\frac{5.5}{21}$ $\frac{5.0}{43}$

$\frac{7.9}{43}$ $\frac{83}{35}$ $\frac{6.9}{33}$ $\frac{6.5}{8}$ 6.8 $\frac{4.4}{8}$ $\frac{5.0}{30}$ $\frac{4.9}{43}$

$\frac{7.5}{43}$ $\frac{7.5}{39}$ $\frac{5.2}{30}$ $\frac{6.1}{16}$ 5.8 $\frac{6.1}{7}$ $\frac{6.7}{17}$ $\frac{4.2}{25}$ $\frac{3.7}{43}$

$\frac{5.6}{43}$ $\frac{4.8}{17}$ $\frac{6.4}{14}$ 5.9 $\frac{6.3}{14}$ $\frac{6.1}{21}$ $\frac{2.8}{28}$ $\frac{2.6}{43}$

$\frac{4.9}{43}$ $\frac{3.6}{22}$ $\frac{6.9}{13}$ 6.1 $\frac{6.5}{11}$ $\frac{6.1}{16}$ $\frac{2.9}{29}$ $\frac{3.1}{43}$

$\frac{3.0}{43}$ $\frac{2.4}{26}$ $\frac{8.4}{21}$ $\frac{7.3}{12}$ 6.7 $\frac{7.3}{11}$ $\frac{7.0}{15}$ $\frac{4.8}{22}$ $\frac{5.3}{43}$

$\frac{2.7}{43}$ $\frac{2.2}{29}$ $\frac{9.6}{21}$ $\frac{8.5}{12}$ 7.9 $\frac{8.3}{11}$ $\frac{7.9}{16}$ $\frac{4.3}{25}$ $\frac{5.7}{34}$ $\frac{5.7}{43}$

$\frac{1.3}{43}$ $\frac{1.2}{33}$ $\frac{2.7}{22}$ $\frac{5.4}{13}$ 4.9 $\frac{5.1}{12}$ $\frac{4.4}{18}$ $\frac{2.3}{26}$ $\frac{3.1}{34}$ $\frac{4.0}{43}$

$\frac{5.6}{43}$ $\frac{4.0}{31}$ $\frac{5.1}{20}$ $\frac{6.1}{18}$ $\frac{6.1}{10}$ 5.8 $\frac{6.0}{12}$ $\frac{5.6}{22}$ $\frac{6.7}{34}$ $\frac{6.7}{43}$

$\frac{7.9}{43}$ $\frac{7.7}{33}$ $\frac{5.9}{28}$ $\frac{5.2}{22}$ $\frac{7.2}{18}$ $\frac{7.2}{10}$ 6.8 $\frac{7.5}{11}$ $\frac{7.0}{17}$ $\frac{5.0}{24}$ $\frac{5.9}{43}$

906.70

88+00

98.9

88+50

97.5

89+00

96.0

89+50

94.9

3.41 896.99 13.12 893.58

90+00

93.6

90+50

92.3

91+00

91.2

91+50

90.4

92+00

89.6

5.32 894.71 7.60 889.59

92+50

88.6

CHASS DRAIN

93+00

87.5

93+50

83.2

93+56

85.4

$\frac{109}{43}$ $\frac{99}{36}$ $\frac{61}{28}$ $\frac{61}{25}$ $\frac{81}{18}$ $\frac{82}{11}$ 7.8 $\frac{85}{10}$ $\frac{79}{15}$ $\frac{70}{18}$ $\frac{62}{24}$ $\frac{62}{43}$

$\frac{94}{43}$ $\frac{96}{42}$ $\frac{69}{29}$ $\frac{70}{25}$ $\frac{95}{17}$ $\frac{74}{11}$ 9.2 $\frac{99}{10}$ $\frac{94}{13}$ $\frac{81}{18}$ $\frac{79}{43}$

$\frac{79}{43}$ $\frac{61}{27}$ $\frac{114}{78}$ $\frac{105}{11}$ 10.7 $\frac{110}{19}$ $\frac{74}{21}$ $\frac{86}{34}$ $\frac{90}{43}$

$\frac{90}{43}$ $\frac{76}{26}$ $\frac{125}{17}$ 11.8 $\frac{121}{13}$ $\frac{76}{21}$ $\frac{71}{27}$ $\frac{100}{43}$

$\frac{122}{43}$ $\frac{07}{24}$ $\frac{45}{18}$ $\frac{47}{14}$ $\frac{37}{12}$ 3.4 $\frac{40}{12}$ $\frac{40}{18}$ $\frac{07}{25}$ $\frac{17}{43}$

$\frac{35}{43}$ $\frac{36}{33}$ $\frac{65}{28}$ $\frac{64}{21}$ $\frac{50}{15}$ 4.7 $\frac{52}{15}$ $\frac{63}{17}$ $\frac{63}{24}$ $\frac{29}{31}$ $\frac{33}{43}$

$\frac{68}{43}$ $\frac{60}{28}$ $\frac{76}{25}$ $\frac{71}{17}$ $\frac{60}{10}$ 5.8 $\frac{66}{15}$ $\frac{78}{20}$ $\frac{80}{25}$ $\frac{5.5}{30}$ $\frac{5.9}{43}$

$\frac{96}{43}$ $\frac{55}{20}$ $\frac{72}{74}$ 6.6 $\frac{71}{13}$ $\frac{60}{29}$ $\frac{84}{43}$

$\frac{150}{43}$ $\frac{133}{32}$ $\frac{100}{21}$ $\frac{81}{14}$ 7.4 $\frac{77}{14}$ $\frac{110}{23}$ $\frac{127}{43}$

$\frac{123}{43}$ $\frac{126}{28}$ $\frac{68}{15}$ 6.1 $\frac{67}{19}$ $\frac{116}{51}$ $\frac{122}{43}$
 $\frac{131}{43}$ $\frac{133}{43}$

$\frac{123}{43}$ $\frac{118}{17}$ $\frac{76}{7}$ 7.2 $\frac{77}{29}$ $\frac{117}{37}$ $\frac{125}{43}$

$\frac{108}{43}$ $\frac{102}{24}$ $\frac{96}{3}$ 11.5 $\frac{110}{7}$ $\frac{83}{14}$ $\frac{80}{36}$ $\frac{86}{43}$

$\frac{104}{43}$ $\frac{97}{17}$ 9.5 $\frac{118}{6}$ $\frac{109}{13}$ $\frac{88}{19}$ $\frac{83}{43}$

89471 ✓

94+00

85.8

94+50

85.7

95+00

87.2

95+50

85.6

96+00

85.9

96+50

87.2

96+83¹²

88.2

97+00

6.2

88.5

97+50

5.2

89.5

98+00

4.0

90.7

98+50

2.6

92.1

99+00

1.4

93.3

B.M.

11.43

883.28

883.26

<u>10.1</u>	<u>10.5</u>		<u>7.7</u>	<u>7.5</u>	<u>11.0</u>	<u>11.4</u>
43	22	2.9	17	2.9	36	43

<u>9.7</u>	<u>10.5</u>	<u>10.4</u>		<u>7.7</u>	<u>7.2</u>
43	40	21	9.0	24	43

<u>7.6</u>	<u>8.0</u>		<u>7.7</u>	<u>7.4</u>	<u>10.0</u>
43	23	7.5	24	3.9	44

<u>7.4</u>	<u>8.4</u>		<u>9.7</u>	<u>10.6</u>	<u>9.4</u>	<u>8.8</u>	<u>8.9</u>
43	23	9.1	11	15	21	38	43

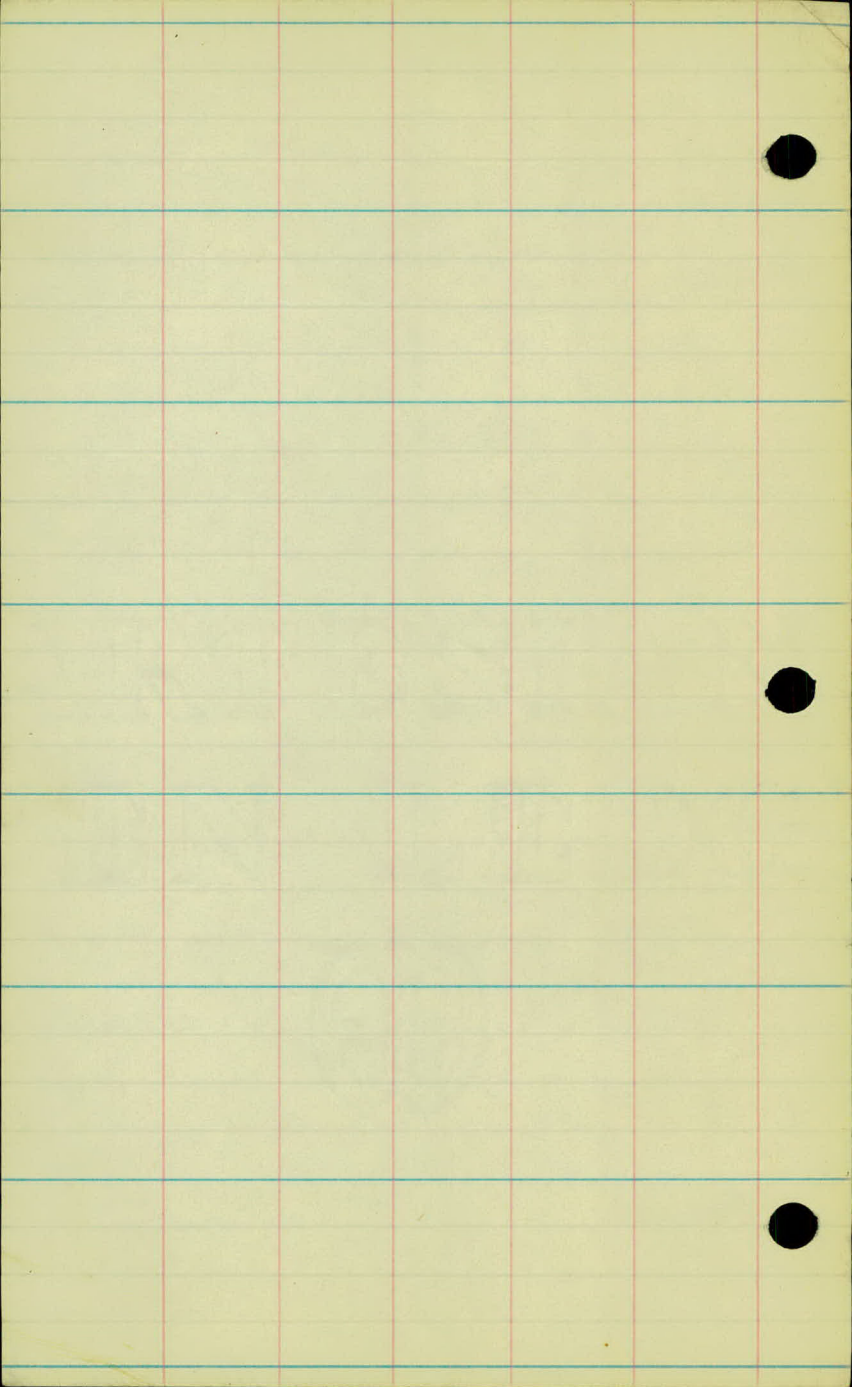
<u>8.0</u>	<u>9.0</u>	<u>10.1</u>		<u>8.5</u>	<u>10.0</u>	<u>11.1</u>	<u>9.2</u>	<u>9.1</u>
43	25	5	2.8	14	31	33	37	43

<u>8.7</u>	<u>7.7</u>	<u>10.4</u>	<u>8.3</u>		<u>8.4</u>	<u>11.2</u>	<u>11.2</u>	<u>10.5</u>
43	33	15	12	7.5	17	22	37	45

<u>8.7</u>	<u>9.5</u>	<u>9.4</u>	<u>7.0</u>		<u>7.4</u>	<u>10.1</u>	<u>10.5</u>	<u>7.7</u>
43	36	17	13	6.5	13	18	34	43
-2.8	-3.4	-0.2	-0.2		-0.5	-4.1	-4.4	-5.7
43	20	14	10		12	18	25	43
-4.2	-5.0	-4.6	-0.4		-0.3	-5.1	-6.1	-5.5
43	33	19	13		12	20	29	43
-4.2	-4.5	-4.4	-0.5		-0.4	-5.0	-6.1	-8.5
43	35	18	12		12	19	28	43
-2.9	-4.1	-4.1	-0.3		-0.3	-5.6	-8.1	-8.0
43	37	20	13		11	19	35	43

<u>+1.0</u>	<u>-0.4</u>	<u>0.0</u>	<u>-2.2</u>	<u>-2.2</u>	<u>-0.5</u>			
43	33	23	19	17	12	-0.3	-3.0	-4.4
						12	19	32
								43

SPK IN P.P. E. SIDE INT. LONG LN. RA & RICE CREEK RA



PROJ. # 30-12
LONG LAKE ROAD.
CHECK LEVELS.

B.M.	+	H.I.	-	885.11
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B.M.	4.63	889.74		
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T.P.	3.97	891.46	2.25	887.49
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...	5.79	892.68	4.57	886.89
-----	------	--------	------	--------

B.M.			5.05	
------	--	--	------	--

T.P.	3.12	887.50	8.30	884.38
------	------	--------	------	--------

..	11.15	898.25	0.40	887.10
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..	7.39	905.64	0.00	898.25
----	------	--------	------	--------

..	1.13	904.23	7.54	903.10
----	------	--------	------	--------

B.M.			10.66	893.57
------	--	--	-------	--------

T.P.	1.05	891.92	13.36	890.87
------	------	--------	-------	--------

..	1.51	887.16	6.27	885.65
----	------	--------	------	--------

B.M.			4.73	882.43
------	--	--	------	--------

T.P.	1.89	878.50	10.55	876.61
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..	4.17	875.19	7.48	871.02
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B.M.	7.68	881.92	2.95	872.24
------	------	--------	------	--------

	10.26	892.18	0.00	881.92
--	-------	--------	------	--------

	6.30	897.90	0.58	891.60
--	------	--------	------	--------

	4.08	897.50	4.48	893.42
--	------	--------	------	--------

B.M.			2.47	895.03
------	--	--	------	--------

	7.08	903.13	3.45	894.05
--	------	--------	------	--------

B.M.			3.90	899.23
------	--	--	------	--------

	5.21	907.69	0.65	902.48
--	------	--------	------	--------

	0.20	894.98	12.91	894.78
--	------	--------	-------	--------

B.M.			11.72	883.24
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Top of wall 30' Rt Sta. 0 + 83

● On N.W. cor of Lower conc. step in front of New Brighton Post office.

S.W. cor. Mont. Int. Long. Lk. Rd. old S.T.H. 62

R.R. spike in 12" Cotton wood 100' Rt Sta. 27 + 50

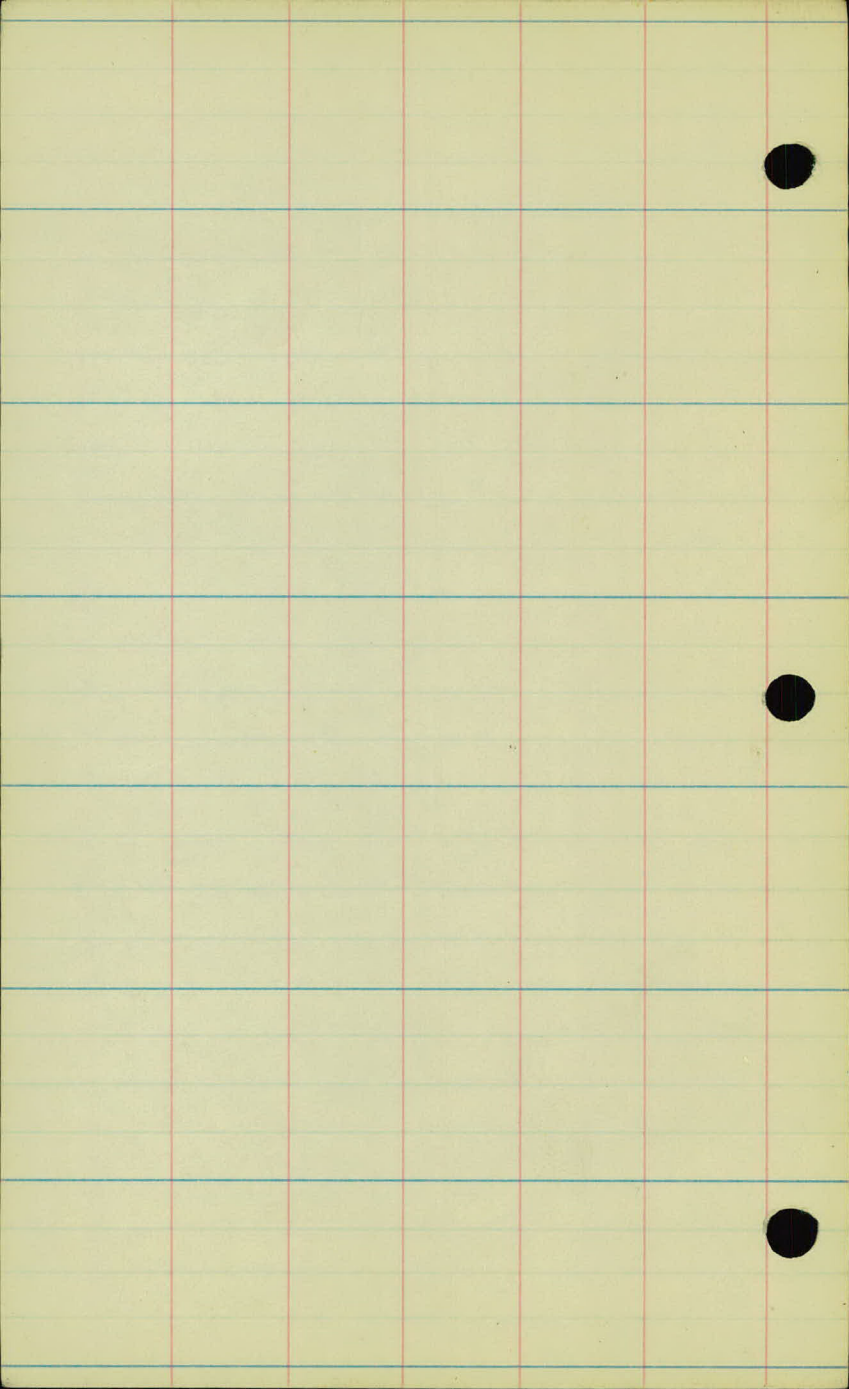
● R.R. spike in T.R. 23' Lt Sta. 41 + 70

N.W. cor. Mont. Sta. 52 + 53¹⁶ P.I.

IN BOTTOM OF CONC. STEP, S.W. COR. LT. OF STA. 69 + 15

SPK IN 18" OAK 100 FT. STA. 77 + 75

● SPK IN P.P.E. SIDE INT. RICE CREEK & LONG LAKE RD



New Brighton
LONG LAKE ROAD
"B" LINE.

CROSS SECTIONS FROM STA. 44150
TO STA. 92700.

STA	+	H. I.	-	ELEV.
B.M.	1.52	883.75		882.43
	4.00	877.65	10.10	873.65
44	+50			73.4
45				73.5
	+50			73.3
46				73.6
	+50			73.0
47				71.4
	+50			70.7
	1.80	850.49	4.96	872.67
48				71.3
	+50			73.1
49				75.6
	+50			75.8
50				74.7

P.P. SPK. IN T.P. 23 17 STR. 41+70.

$\frac{68}{43}$	$\frac{52}{25}$	$\frac{57}{20}$	$\frac{48}{16}$		$\frac{41}{13}$	$\frac{54}{50}$	$\frac{62}{43}$
-----------------	-----------------	-----------------	-----------------	--	-----------------	-----------------	-----------------

$\frac{47}{43}$	$\frac{43}{14}$	$\frac{42}{4.2}$	$\frac{40}{13}$	$\frac{50}{28}$	$\frac{52}{43}$
-----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{65}{43}$	$\frac{37}{17}$	$\frac{49}{11}$	$\frac{44}{4.4}$	$\frac{40}{11}$	$\frac{46}{26}$	$\frac{52}{43}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{14}{43}$	$\frac{13}{34}$	$\frac{51}{22}$	$\frac{41}{4.1}$	$\frac{44}{12}$	$\frac{50}{27}$	$\frac{62}{43}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{50}{43}$	$\frac{49}{21}$	$\frac{47}{4.7}$	$\frac{53}{12}$	$\frac{48}{51}$	$\frac{48}{43}$
-----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{73}{43}$	$\frac{76}{23}$	$\frac{63}{6.3}$	$\frac{56}{19}$	$\frac{36}{43}$
-----------------	-----------------	------------------	-----------------	-----------------

$\frac{91}{43}$	$\frac{83}{22}$	$\frac{73}{11}$	$\frac{70}{7.0}$	$\frac{60}{24}$	$\frac{47}{43}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------

NOIL IN F.P. AT STR 47+90

$\frac{105}{43}$	$\frac{101}{17}$	$\frac{92}{9.2}$	$\frac{86}{13}$	$\frac{77}{43}$
------------------	------------------	------------------	-----------------	-----------------

$\frac{77}{43}$	$\frac{76}{19}$	$\frac{74}{7.4}$	$\frac{70}{22}$	$\frac{73}{43}$
-----------------	-----------------	------------------	-----------------	-----------------

$\frac{45}{43}$	$\frac{49}{34}$	$\frac{49}{4.9}$	$\frac{52}{21}$	$\frac{51}{43}$
-----------------	-----------------	------------------	-----------------	-----------------

$\frac{46}{43}$	$\frac{48}{22}$	$\frac{47}{4.7}$	$\frac{51}{21}$	$\frac{50}{43}$
-----------------	-----------------	------------------	-----------------	-----------------

$\frac{48}{43}$	$\frac{64}{33}$	$\frac{51}{13}$	$\frac{58}{5.8}$	$\frac{64}{25}$	$\frac{66}{43}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------

880.49 ✓

+50

74.1

51

74.6

+50

76.0

52

77.9

T.P.

11.19

889.53 ✓

2.15

878.34 ✓

+50

80.0

53

82.0

+50

84.6

54

86.3

T.P.

9.87

896.72 ✓

2.68

886.85 ✓

+50

88.5

55

90.4

+50

91.5

56

92.0

+50

91.9

$$\frac{71}{43} \quad \frac{67}{12} \quad 6.4 \quad \frac{72}{25} \quad \frac{78}{43}$$

$$\frac{83}{43} \quad \frac{81}{24} \quad \frac{62}{7} \quad 5.9 \quad \frac{77}{18} \quad \frac{87}{43}$$

$$\frac{65}{43} \quad \frac{62}{23} \quad 4.5 \quad \frac{53}{10} \quad \frac{63}{43}$$

$$\frac{26}{43} \quad \frac{26}{30} \quad 2.6 \quad \frac{37}{26} \quad \frac{51}{43}$$

$$\frac{78}{43} \quad \frac{74}{18} \quad 9.5 \quad \frac{10.8}{18} \quad \frac{11.8}{43}$$

$$\frac{5.0}{43} \quad \frac{67}{21} \quad 7.5 \quad \frac{87}{17} \quad \frac{104}{43}$$

$$\frac{1.0}{43} \quad \frac{37}{18} \quad 4.9 \quad \frac{7.0}{27} \quad \frac{8.0}{43}$$

$$\frac{11.5}{43} \quad \frac{0.9}{22} \quad 3.2 \quad \frac{4.0}{21} \quad \frac{47}{43}$$

$$\frac{7.1}{43} \quad \frac{84}{21} \quad 5.2 \quad \frac{7.5}{24} \quad \frac{81}{43}$$

$$\frac{78}{43} \quad \frac{7.0}{18} \quad 6.3 \quad \frac{5.3}{25} \quad \frac{5.3}{43}$$

$$\frac{6.2}{43} \quad \frac{55}{20} \quad 5.2 \quad \frac{4.0}{25} \quad \frac{4.2}{43}$$

$$\frac{4.7}{43} \quad \frac{4.7}{15} \quad 4.7 \quad \frac{3.9}{21} \quad \frac{4.4}{43}$$

$$\frac{4.6}{43} \quad \frac{5.1}{14} \quad 4.8 \quad \frac{4.9}{18} \quad \frac{5.4}{43}$$

896.72 ✓

57 90.9

+50 90.7

58 89.8

+50 88.9

59 88.7

+50 88.8

T.P. 6.45 ✓ 89788 5.19 ✓ 791.43

60 89.9

+50 91.4

61 92.2

+50 92.2

62 92.0

+50 92.3

63 91.6

$$\frac{60}{43} \quad \frac{62}{22} \quad 5.8 \quad \frac{52}{20} \quad \frac{57}{43}$$

$$\frac{63}{43} \quad \frac{63}{20} \quad 6.0 \quad \frac{51}{24} \quad \frac{57}{43}$$

$$\frac{75}{43} \quad \frac{71}{20} \quad 6.7 \quad \frac{54}{27} \quad \frac{55}{43}$$

$$\frac{86}{43} \quad \frac{81}{20} \quad 7.8 \quad \frac{65}{26} \quad \frac{66}{43}$$

$$\frac{82}{43} \quad \frac{85}{23} \quad 8.0 \quad \frac{81}{24} \quad \frac{85}{43}$$

$$\frac{63}{43} \quad \frac{71}{23} \quad 7.7 \quad \frac{27}{17} \quad \frac{84}{25} \quad \frac{87}{43}$$

$$\frac{52}{43} \quad \frac{66}{23} \quad 8.0 \quad \frac{80}{23} \quad \frac{89}{43}$$

$$\frac{46}{43} \quad \frac{34}{19} \quad 6.5 \quad \frac{67}{25} \quad \frac{74}{43}$$

$$\frac{45}{43} \quad \frac{59}{13} \quad 5.7 \quad \frac{55}{13} \quad \frac{71}{43}$$

$$\frac{56}{43} \quad \frac{50}{25} \quad 5.7 \quad \frac{70}{27} \quad \frac{54}{43}$$

$$\frac{42}{43} \quad \frac{49}{20} \quad 5.9 \quad \frac{65}{21} \quad \frac{75}{43}$$

$$\frac{42}{43} \quad \frac{43}{21} \quad 5.6 \quad \frac{67}{20} \quad \frac{92}{43}$$

$$\frac{42}{43} \quad \frac{61}{16} \quad 6.3 \quad \frac{67}{20} \quad \frac{90}{43}$$

✓
897.88

+50

89.6

64

T.P.

1.70

✓
894.75

10.85 897.05

✓
86.6

+50

84.6

65

82.0

+50

82.4

66

86.3

+50

88.1

67

89.1

+50

89.4

68

90.7

+50

90.9

69

T.P.

5.11

✓
897.77

2.07

✓
892.66

92.5

+50

92.8

$\frac{40}{43}$	$\frac{80}{18}$	8.3	$\frac{8.1}{25}$	$\frac{9.9}{43}$
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$\frac{6.7}{43}$	$\frac{103}{21}$	11.8	$\frac{11.7}{21}$	$\frac{15.2}{43}$
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$\frac{6.7}{43}$	$\frac{11.9}{18}$	10.1	$\frac{10.8}{14}$	$\frac{14.1}{20}$	$\frac{15.2}{26}$	$\frac{15.4}{43}$
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$\frac{14.2}{43}$	$\frac{150}{11}$	12.7	$\frac{11.5}{4}$	$\frac{11.1}{15}$	$\frac{15.4}{30}$	$\frac{15.4}{43}$
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$\frac{13.7}{43}$	$\frac{14.2}{12}$	$\frac{13.4}{3}$	12.3	$\frac{10.7}{7}$	$\frac{10.7}{18}$	$\frac{11.7}{24}$	$\frac{12.2}{39}$	$\frac{11.0}{43}$
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$\frac{7.9}{43}$	$\frac{8.1}{22}$	8.4	$\frac{7.1}{16}$	$\frac{6.9}{43}$
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$\frac{5.4}{43}$	$\frac{5.7}{22}$	6.6	$\frac{6.7}{22}$	$\frac{6.4}{40}$	$\frac{7.0}{43}$
------------------	------------------	-----	------------------	------------------	------------------

$\frac{4.0}{43}$	$\frac{5.7}{20}$	5.6	$\frac{7.7}{25}$	$\frac{8.3}{43}$
------------------	------------------	-----	------------------	------------------

$\frac{2.2}{60}$	$\frac{2.6}{50}$	$\frac{2.7}{48}$	$\frac{2.9}{41}$	$\frac{3.4}{37}$	$\frac{4.1}{18}$	5.3	$\frac{6.2}{26}$	$\frac{8.0}{43}$
------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------

$\frac{2.1}{45}$	$\frac{2.8}{29}$	$\frac{2.5}{26}$	$\frac{2.5}{23}$	$\frac{2.9}{20}$	4.0	$\frac{6.1}{22}$	$\frac{8.1}{43}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------

$\frac{1.5}{43}$	$\frac{2.0}{37}$	$\frac{1.8}{28}$	$\frac{3.3}{8}$	$\frac{3.7}{7}$	3.8	$\frac{6.0}{23}$	$\frac{8.3}{43}$
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$\frac{7.0}{43}$	$\frac{0.0}{39}$	$\frac{1.8}{50}$	$\frac{1.6}{12}$	2.2	$\frac{2.7}{8}$	$\frac{4.4}{14}$	$\frac{7.8}{43}$
------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------

$\frac{1.1}{43}$	$\frac{4.1}{22}$	$\frac{6.2}{18}$	$\frac{6.7}{13}$	$\frac{5.1}{7}$	5.0	$\frac{5.4}{17}$	$\frac{8.7}{28}$	$\frac{10.6}{43}$
------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	-------------------

897.77 ✓

70

91.8

+50

93.5

71

94.6

+50

95.3

72

94.5

+45

94.1

73

93.8 ✓

T.P.

6.41

909.11 ✓

0.07

897.70 ✓

+50

96.0

74

CENTER OF ROAD

97.5

+50

97.0 ✓

B.M.

4.88

899.23

899.23

75

97.9

+50

98.9

76

97.2

$\frac{1.2}{43}$	$\frac{4.5}{9}$	$\frac{5.8}{5}$	6.0	$\frac{5.9}{8}$	$\frac{5.4}{21}$	$\frac{6.1}{33}$	$\frac{10.5}{43}$
------------------	-----------------	-----------------	-----	-----------------	------------------	------------------	-------------------

$\frac{0.2}{43}$	$\frac{2.0}{25}$	4.3	$\frac{4.8}{6}$	$\frac{7.6}{12}$	$\frac{7.6}{18}$	$\frac{6.0}{23}$	$\frac{5.5}{37}$	$\frac{5.9}{43}$
------------------	------------------	-----	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{41.2}{48}$	$\frac{2.8}{15}$	3.2	$\frac{3.7}{12}$	$\frac{5.3}{19}$	$\frac{6.7}{26}$	$\frac{8.7}{33}$	$\frac{6.0}{39}$	$\frac{6.0}{43}$
-------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{70.8}{43}$	$\frac{0.3}{21}$	2.5	$\frac{3.2}{16}$	$\frac{4.6}{21}$	$\frac{7.8}{43}$
-------------------	------------------	-----	------------------	------------------	------------------

$\frac{70.8}{43}$	$\frac{0.7}{22}$	3.3	$\frac{3.6}{17}$	$\frac{5.9}{23}$	$\frac{6.8}{33}$	$\frac{7.3}{43}$
-------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{0.4}{43}$	$\frac{2.4}{23}$	3.7	$\frac{6.0}{7}$	$\frac{4.4}{14}$	$\frac{4.8}{34}$	$\frac{4.0}{38}$	$\frac{3.9}{43}$
------------------	------------------	-----	-----------------	------------------	------------------	------------------	------------------

$\frac{5.5}{43}$	$\frac{5.2}{18}$	$\frac{3.5}{6}$	4.0	$\frac{4.0}{3}$	$\frac{2.6}{6}$	$\frac{3.3}{12}$	$\frac{2.0}{20}$	$\frac{0.5}{43}$
------------------	------------------	-----------------	-----	-----------------	-----------------	------------------	------------------	------------------

$\frac{11.4}{43}$	$\frac{11.0}{52}$	$\frac{7.7}{10}$	8.1	$\frac{6.5}{8}$	$\frac{5.6}{17}$	$\frac{9.2}{43}$
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$\frac{8.8}{43}$	$\frac{7.9}{43}$	$\frac{7.2}{32}$	6.6	$\frac{7.3}{34}$	$\frac{9.5}{41}$	$\frac{9.5}{43}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{8.6}{43}$	$\frac{7.4}{28}$	$\frac{6.6}{5}$	7.1	$\frac{6.2}{8}$	$\frac{6.8}{32}$	$\frac{6.7}{43}$
------------------	------------------	-----------------	-----	-----------------	------------------	------------------

SPK IN 18" OAK 100 FT STA. 79+00

$\frac{7.7}{43}$	$\frac{6.3}{24}$	$\frac{5.5}{6}$	6.2	$\frac{5.9}{7}$	$\frac{5.4}{30}$	$\frac{5.9}{43}$
------------------	------------------	-----------------	-----	-----------------	------------------	------------------

$\frac{6.8}{43}$	$\frac{3.9}{24}$	$\frac{3.3}{9}$	$\frac{4.9}{5}$	5.4	$\frac{4.6}{15}$	$\frac{2.2}{24}$	$\frac{2.1}{43}$
------------------	------------------	-----------------	-----------------	-----	------------------	------------------	------------------

$\frac{8.0}{43}$	$\frac{5.3}{10}$	$\frac{6.2}{7}$	6.9	$\frac{5.7}{14}$	$\frac{4.0}{19}$	$\frac{3.0}{43}$
------------------	------------------	-----------------	-----	------------------	------------------	------------------

907.11

+50

94.9

77

93.8

+50

95.5

78

95.9

+50

95.7

79

96.7

+50

T.P.

4.98

905.05

6.04

898.07

98.2

80

96.7

+50

94.7

81

93.0

+50

T.P.

1.25

891.64

12.67

890.41

89.7

82

87.3

+50

85.7

$\frac{12.0}{43}$ $\frac{11.8}{20}$ $\frac{10.5}{11}$ $\frac{9.2}{6}$ 7.2 $\frac{8.7}{10}$ $\frac{10.0}{18}$ $\frac{8.6}{43}$

$\frac{10.7}{43}$ $\frac{11.6}{24}$ $\frac{10.2}{8}$ **10.3**
 $\frac{1.3}{10}$ $\frac{12.6}{25}$ $\frac{11.1}{43}$

$\frac{5.5}{43}$ $\frac{7.4}{18}$ 8.6 $\frac{9.1}{10}$ $\frac{11.0}{32}$ $\frac{11.5}{43}$

$\frac{4.0}{43}$ $\frac{6.7}{21}$ 8.2 $\frac{10.3}{20}$ $\frac{13.1}{43}$

$\frac{4.5}{43}$ $\frac{6.8}{24}$ 8.4 $\frac{10.1}{14}$ $\frac{12.4}{43}$

$\frac{4.0}{43}$ $\frac{6.6}{6}$ 7.4 $\frac{7.0}{17}$ $\frac{8.1}{23}$ $\frac{8.9}{43}$

$\frac{3.2}{43}$ $\frac{5.0}{17}$ 5.9 $\frac{6.3}{25}$ $\frac{7.0}{34}$ $\frac{7.0}{43}$

$\frac{1.5}{43}$ $\frac{3.0}{18}$ 6.4 $\frac{6.6}{20}$ $\frac{7.1}{43}$

$\frac{3.0}{43}$ $\frac{5.9}{12}$ 8.4 $\frac{7.3}{20}$ $\frac{10.5}{43}$

$\frac{4.1}{43}$ $\frac{8.5}{15}$ 10.1 $\frac{10.8}{12}$ $\frac{10.4}{21}$ $\frac{11.2}{43}$

$\frac{11.1}{43}$ $\frac{12.5}{27}$ 13.4 $\frac{12.6}{10}$ $\frac{12.1}{43}$

$\frac{3.7}{43}$ $\frac{4.5}{18}$ 4.4 $\frac{3.8}{2}$ $\frac{2.3}{30}$ $\frac{2.2}{43}$

$\frac{6.2}{43}$ $\frac{7.8}{30}$ $\frac{7.6}{4}$ 6.0 $\frac{5.7}{11}$ $\frac{6.4}{16}$ $\frac{4.8}{43}$

891.66 ✓

83

84.2

+50

83.2

84

82.1

+50

80.9

85

80.0

+50

79.3

86

79.4

+60

T.P.

5.40

891.85 ✓

5.21

886.45 ✓

83.5

+86

86.3

87

85.5

+45

85.0

+65

86.9

88

87.9

$$\begin{array}{r} 7.2 \\ 43 \end{array} \quad \begin{array}{r} 86 \\ 33 \end{array} \quad \begin{array}{r} 87 \\ 7 \end{array} \quad 7.5 \quad \begin{array}{r} 69 \\ 20 \end{array} \quad \begin{array}{r} 56 \\ 35 \end{array} \quad \begin{array}{r} 54 \\ 43 \end{array}$$

$$\begin{array}{r} 67 \\ 43 \end{array} \quad \begin{array}{r} 77 \\ 37 \end{array} \quad \begin{array}{r} 87 \\ 32 \end{array} \quad 8.5 \quad \begin{array}{r} 84 \\ 6 \end{array} \quad \begin{array}{r} 76 \\ 12 \end{array} \quad \begin{array}{r} 71 \\ 48 \end{array}$$

$$\begin{array}{r} 68 \\ 43 \end{array} \quad \begin{array}{r} 73 \\ 26 \end{array} \quad \begin{array}{r} 93 \\ 18 \end{array} \quad \begin{array}{r} 90 \\ 9 \end{array} \quad 96 \quad \begin{array}{r} 94 \\ 7 \end{array} \quad \begin{array}{r} 105 \\ 18 \end{array} \quad \begin{array}{r} 117 \\ 43 \end{array}$$

$$\begin{array}{r} 89 \\ 43 \end{array} \quad \begin{array}{r} 95 \\ 31 \end{array} \quad \begin{array}{r} 116 \\ 12 \end{array} \quad \begin{array}{r} 110 \\ 4 \end{array} \quad 108 \quad \begin{array}{r} 110 \\ 10 \end{array} \quad \begin{array}{r} 123 \\ 16 \end{array} \quad \begin{array}{r} 132 \\ 43 \end{array}$$

$$\begin{array}{r} 99 \\ 43 \end{array} \quad \begin{array}{r} 126 \\ 21 \end{array} \quad \begin{array}{r} 126 \\ 12 \end{array} \quad 11.7 \quad \begin{array}{r} 121 \\ 10 \end{array} \quad \begin{array}{r} 132 \\ 15 \end{array} \quad \begin{array}{r} 142 \\ 35 \end{array} \quad \begin{array}{r} 142 \\ 43 \end{array}$$

$$\begin{array}{r} 111 \\ 43 \end{array} \quad \begin{array}{r} 124 \\ 20 \end{array} \quad 12.4 \quad \begin{array}{r} 122 \\ 13 \end{array} \quad \begin{array}{r} 130 \\ 17 \end{array} \quad \begin{array}{r} 145 \\ 43 \end{array}$$

$$\begin{array}{r} 112 \\ 43 \end{array} \quad \begin{array}{r} 118 \\ 20 \end{array} \quad 12.3 \quad \begin{array}{r} 114 \\ 24 \end{array} \quad \begin{array}{r} 126 \\ 34 \end{array} \quad \begin{array}{r} 126 \\ 43 \end{array}$$

$$\begin{array}{r} 46 \\ 60 \end{array} \quad \begin{array}{r} 50 \\ 50 \end{array} \quad \begin{array}{r} 53 \\ 43 \end{array} \quad \begin{array}{r} 80 \\ 36 \end{array} \quad \begin{array}{r} 80 \\ 21 \end{array} \quad 8.2 \quad \begin{array}{r} 88 \\ 14 \end{array} \quad \begin{array}{r} 105 \\ 30 \end{array} \quad \begin{array}{r} 98 \\ 43 \end{array}$$

$$\begin{array}{r} 55 \\ 43 \end{array} \quad \begin{array}{r} 54 \\ 36 \end{array} \quad \begin{array}{r} 60 \\ 13 \end{array} \quad \begin{array}{r} 73 \\ 8 \end{array} \quad \begin{array}{r} 73 \\ 5 \end{array} \quad 5.4 \quad \begin{array}{r} 62 \\ 12 \end{array} \quad \begin{array}{r} 96 \\ 37 \end{array} \quad \begin{array}{r} 100 \\ 43 \end{array}$$

$$\begin{array}{r} 5.7 \\ 43 \end{array} \quad \begin{array}{r} 5.5 \\ 23 \end{array} \quad 6.4 \quad \begin{array}{r} 75 \\ 7 \end{array} \quad \begin{array}{r} 57 \\ 12 \end{array} \quad \begin{array}{r} 75 \\ 31 \end{array} \quad \begin{array}{r} 9.5 \\ 43 \end{array}$$

$$\begin{array}{r} 50 \\ 43 \end{array} \quad \begin{array}{r} 43 \\ 24 \end{array} \quad \begin{array}{r} 72 \\ 18 \end{array} \quad \begin{array}{r} 85 \\ 5 \end{array} \quad 6.9 \quad \begin{array}{r} 69 \\ 13 \end{array} \quad \begin{array}{r} 63 \\ 28 \end{array} \quad \begin{array}{r} 67 \\ 43 \end{array}$$

$$\begin{array}{r} 61 \\ 43 \end{array} \quad \begin{array}{r} 42 \\ 15 \end{array} \quad 5.0 \quad \begin{array}{r} 73 \\ 6 \end{array} \quad \begin{array}{r} 83 \\ 19 \end{array} \quad \begin{array}{r} 74 \\ 21 \end{array} \quad \begin{array}{r} 66 \\ 43 \end{array}$$

$$\begin{array}{r} 60 \\ 43 \end{array} \quad \begin{array}{r} 47 \\ 16 \end{array} \quad 4.0 \quad \begin{array}{r} 29 \\ 12 \end{array} \quad \begin{array}{r} 30 \\ 23 \end{array} \quad \begin{array}{r} 83 \\ 32 \end{array} \quad \begin{array}{r} 73 \\ 43 \end{array}$$

891.85 ✓

+50

86.6

89

85.4

+50

86.2

+99¹⁶

87.0

90

4.9

87.0

+50

3.5

88.4

91

2.5

89.4

+50

1.0

90.6

92

0.0 ✓

91.9

B.M.

8.57

883.26

883.26

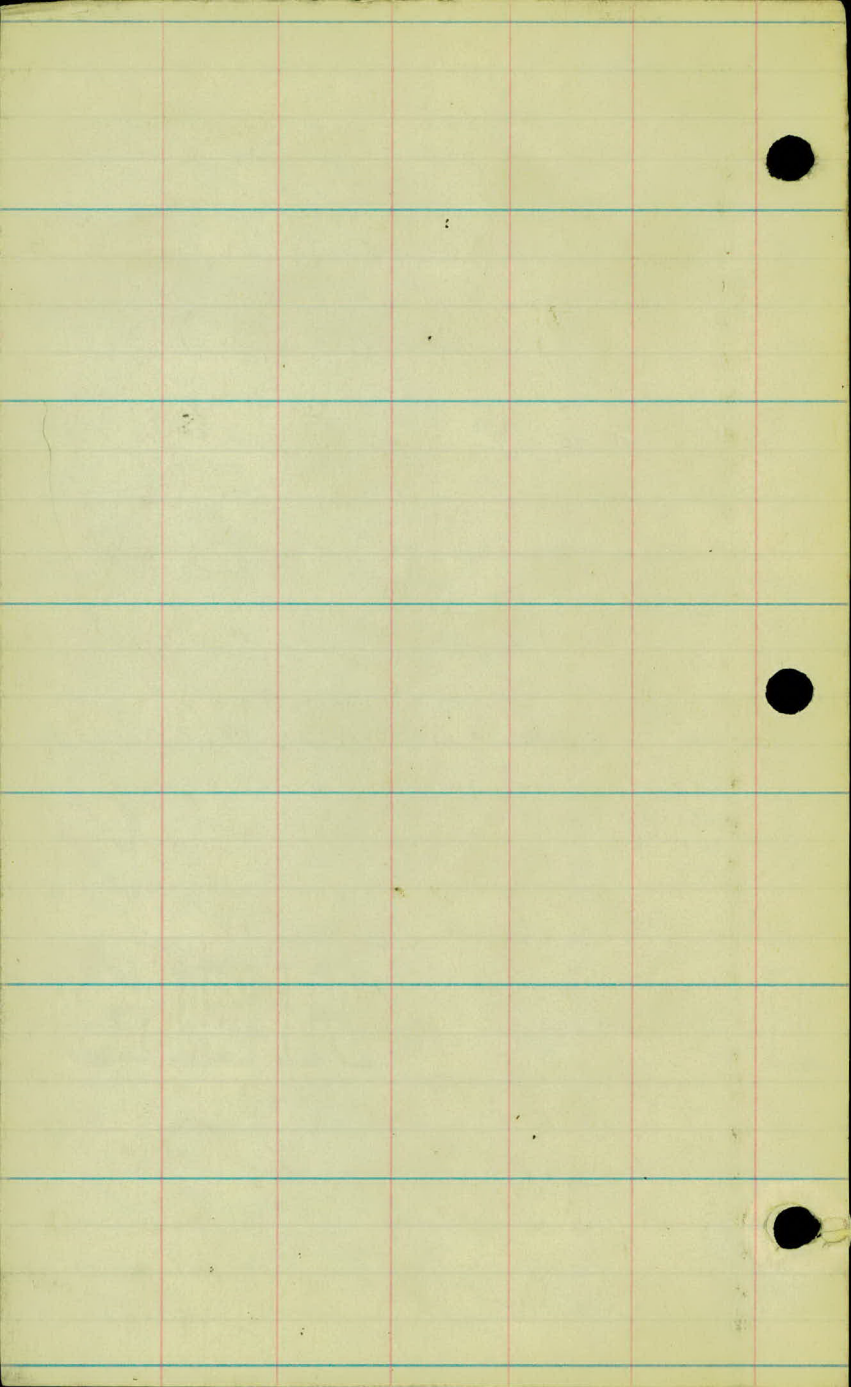
$\frac{5.1}{4.0}$	$\frac{4.7}{2.2}$	5.0	$\frac{4.8}{3}$	$\frac{8.4}{12}$	$\frac{7.0}{18}$	$\frac{6.7}{34}$	$\frac{7.0}{43}$
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$\frac{5.8}{4.3}$	$\frac{6.3}{13}$	$\frac{7.6}{8}$	$\frac{7.6}{5}$	6.5	$\frac{5.8}{13}$	$\frac{6.4}{30}$	$\frac{8.4}{32}$	$\frac{8.4}{36}$	$\frac{4.2}{43}$	$\frac{4.2}{50}$
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$\frac{5.5}{4.3}$	$\frac{7.1}{15}$	$\frac{6.0}{10}$	5.7	$\frac{6.8}{16}$	$\frac{8.1}{20}$	$\frac{8.1}{21}$	$\frac{7.0}{22}$	$\frac{5.7}{43}$
-------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.9}{4.3}$	$\frac{7.0}{32}$	$\frac{7.3}{17}$	$\frac{5.2}{13}$	4.9	$\frac{5.2}{15}$	$\frac{7.8}{19}$	$\frac{7.7}{39}$	$\frac{7.0}{43}$
-------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

S PK IN. P.P. E. SIDE OF INT. RICE CREEK RD. & LONG LAKE RD.



LONG LAKE ROAD - 2-17-30

~~0+00 to 5+00 - City section~~

- x No culv's. req. x
- x 8+63 - R^t. - No culv. req. x
- x 9+46 R^t. - P-15" X 20' C.M. x
- x 12+00 - Remove. 12" X 40' V.P. - P-24" P₃ x
- x Power line on RT. x
- x 12+00 to 13+00 - Cl. & Gr. 3T. R^t. x
- x 12+35 - L^t. No culv. req. x
- x 14+18 - L^t. - P-15" X 20' C.M. x
- x 13+95 - R^t. - No culv. req. x
- x 15+64 - Remove - P-24" P₃. x
- x 26+00 to 27+00 - Cl. & Gr. - 2 T. R^t x
- x 28+50 - R^t. - No culv. req. x
- x 28+50 - L^t. - No culv. req. x
- x 33+00 to 38+00 - L^t. - Gr. 33T. x
- x 36+00 to 42+50 R^t. - Cl. 23T. Gr. 72 x
- x 42+00 to 42+50 - L^t. - Gr. 2T. x
- x 43+70 - Remove - 50° P-36" B₃ - x
- x 36+30 - L^t. No culv. req. x
- x 46+00 - R^t " " x
- x 46+00 L^t. " " x
- x 51+35 - Rem. P-24" P₃ x
- x 53+50 to 55+00 - Gr. 6 T. R^t x
- x 53+80 - L^t. P-15" X 20' C.M. x
- x 56+12 - L^t. - Rem. - " " x
- x 57+00 to 58+00 - Cl. 2 T. Gr. 4 T. L^t. x
- x 57+98 - L^t. Remove - P-15" X 20' C.M. x
- x 59+59 - L^t. - Rem. - P-15" X 20' C.M. x
- x 60+03 - L^t. - " " " x
- x 61+14 - R^t. - P-15" X 20' C.M. x
- x 61+50 to 63+00 - Cl. 15 T. Gr. 16 T. R^t x
- x 64+95 - R^t. - P-15" X 20' C.M. x
- 63+95

- x 64+64 - Lt - P. 15" x 20' C.M. x
- x 64+50 to 65+00 - Gr. 3 T. Rt. x
- x 68+10 - Rt - No culv. req. x
- x 68+78 - Lt - " " " x
- x 68+72 - Reim. 12" x 40' C.M. - P. 24" P₃ x
- x 70+34 - Rt - No culv. req. x
- x 72+54 - Rt - P. 15" x 20' C.M. x
- x 72+54 - Lt - " " " x
- x 74+85 - Reim. - P. 24" P₃ x
- x 77+00 to 78+00 - Gr. 28 T. Lt. x
- x 83+01 to 84+00. C₁ + Gr. 3 T. Rt. x
- x 83+55 - Rt - Reim. + Rep. x
- ~~83+55 - Lt - P. 15" x 20' C.M.~~
- x 83+75 - Lt - No culv. req. x
- x 91+45 - Rt - Imp. - 15" x 20' C.M. - O.K. ✓
- x Remove G.R. on Lt.
- x 92+54 - culv. O.K. ✓

PROJ # 50-12

SOUNDINGS

SOUNDING 24' LT. STA 96+00

0-1' BLACK LOAM.

1'-3' SAND WATER 3' DOWN.

SOUNDING 20' LT. STA. 95+50

0-1' BLACK LOAM

1'-4⁵ SAND WET

SOUNDING 20' LT. STA. 95+00

0-1' SANDY LOAM

1'-3' SAND

3'-5¹/₂+ CLAY

SOUNDING 20' RT. STA. 95+00

0-1' SANDY LOAM

1'-3' SAND

3'- CLAY

SOUNDING 19' RT. STA 94+50

0-3' SAND

3'-4¹/₂+ CLAY

SOUNDING 22' LT. STA 94+50

0-1¹/₂ BLACK DIRT.

1¹/₂-2¹/₂+ WET SAND.

SOUNDING 50 RT STA. 94+50

0' - 2 1/2' SAND

2 1/2' - 6' + CLAY

SOUNDING 22 LT STA. 94+00

0' - 1' BLACK DIRT MUCKY

1' - 2 1/2' + SAND WET.

SOUNDING 19 RT STA. 94+00

0' - 3 1/2' SAND.

3 1/2' - 4' + CLAY

SOUNDING 22 LT STA. 94+00

0' - 2 1/2' SAND

SOUNDING 23 RT STA. 90+00

0' - 4' + SAND

SOUNDING 23 LT STA. 90+00

0' - 4' + SAND

SOUNDING 21 RT STA. 89+00

0' - 2 1/2' SAND

2 1/2' - 4 1/2' CLAY

SOUNDING 33 RT STA 89100

0'-2½ SAND

2½' CLAY

SOUNDING 21 LT. STA 89100

0'-3½ SAND

3½'-4½' CLAY

SOUNDING 33 LT STA. 89100

0'-5½ SAND

5½' CLAY

SOUNDING 22, RT. STA. 88100

0'-4½ SAND

4½' CLAY

SOUNDING 20 LT. STA. 88100

0'-3½ SAND

3½' CLAY

SOUNDING 20 LT. STA. 87100

0'-4' SAND

SOUNDING 20 RT. STA. 87100

0'-4' SAND

SOUNDING 20 RT. STA. 86+00

0' - 2 1/2' SAND

2 1/2' - 4' CLAY

SOUNDING 20 LT. STA. 86+00

0' - 2' CLAY

SOUNDING 21 LT. STA. 85+00

0' - 3' SAND

3' - 4 1/2' CLAY

SOUNDING 21 RT. STA. 85+00

0' - 2' SAND

2' - 5' CLAY

SOUNDING 25 RT. STA. 84+00

0' - 4' SAND

4' - 6' CLAY

SOUNDING 20 LT. STA. 84+00

0' - 2' SAND

SOUNDING 25 RT. STA. 83+00

0' - 13' SAND

13' - 5' CLAY

SOUNDING 25' RT. STA. 82100

0'-2' SAND

2'-4' CLAY

SOUNDING 25' RT. STA. 81100

0'-2' SAND

2' CLAY

SOUNDING 21' RT. STA. 77150

0'-4' SAND

SOUNDING 24' LT. STA. 77150

0'-3' SAND

SOUNDING 21' RT. STA. 77100

0'-4' SAND

SOUNDING 24' LT. STA. 77100

0'-3' SAND

SOUNDING 21' LT. STA. 76150

0'-2½' SAND

SOUNDING 21' LT. STA. 75100

0'-3½' SAND

SOUNDING 21' LT. STA. 72+00

0 - 3' + SAND

SOUNDING 20' RT. STA. 72+00

0 - 2' + SAND

SOUNDING 21' LT. STA. 71+00

0 - 3' + SAND

SOUNDING 18' RT. STA. 71+00

0 - 2' + SAND

SOUNDING 21' LT. STA. 70+00

0 - 2 1/2' + SAND

SOUNDING 18' LT. STA. 69+00

0 - 2' + SAND

SOUNDING 21' RT. STA. 67+00

0 - 4' + SAND

SOUNDING 21' RT. STA. 67+00

0 - 4' + SAND

SOUNDING 21' RT. STA. 66+00

0 - 5' + SAND

SOUNDING 21' LT. STA. 66+00

0'-4' SAND

SOUNDING 21' LT. STA. 65+00

0'-2' SAND

SOUNDING 18' RT. STA. 65+00

0'-2' SAND

SOUNDING 24' RT. STA. 63+00

0'-1' SAND

1'-3' CLAY

SOUNDING 21' RT. STA. 62+00

0'-2' SAND

2'-3½' CLAY

SOUNDING 21' RT. STA. 61+00

0'-2½' SAND

SOUNDING 21' RT. STA. 60+00

0'-2' SAND

2'-3' CLAY

SOUNDING 21' RT. STA. 59+00

0'-2½' SAND

2½'-4' CLAY

SOUNDING 21 LT. STA. 59+00

0'-1' SAND

1'-3' CLAY

SOUNDING 21 RT STA 58+00

0'-2' SAND

2'-4' CLAY

SOUNDING 21 LT. STA. 58+00

0'-2' SAND

2'-3½' CLAY

SOUNDING 21 LT. STA. 57+00

0'-1' SAND

1'-3' SANDY CLAY

SOUNDING 18 RT STA. 57+00

0'-2' SAND

SOUNDING 18 RT. STA 56+00

0'-2½' SAND

SOUNDING 18 RT. STA 55+00

0'-3' SAND

SOUNDING 24 RT. STA. 54100

0' - 2' SAND

2' - 3' SANDY CLAY

SOUNDING 24 RT. STA. 53100

0 - 0.5' BLACK DIRT

0.5' - 2' SAND

SOUNDING 24 RT. STA. 52100

0 - 1' MUCK

SOUNDING 24 RT. STA. 51100

0 - 1.5' MUCK.

SOUNDING 24 LT. STA. 47100

0' - 4' SAND.

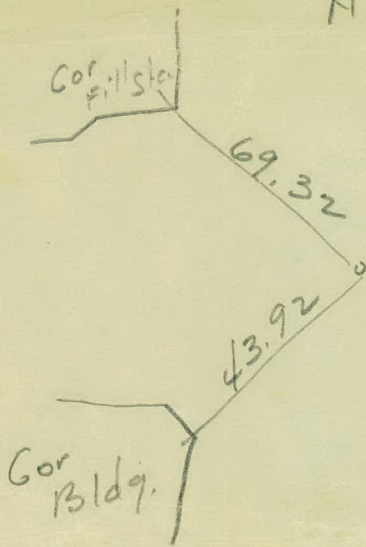
SOUNDING 24 LT. STA. 46100

0' - 4' SAND.

SOUNDING 21 RT. STA. 46100

0' - 4 1/2' SAND.

N.



S.T. H
Front St.

Drill Hole

$$\begin{array}{r}
 8 + 25.90 \\
 \hline
 4 + 71.67 \\
 3 + 34.23 \\
 2 + 7.51 \\
 \hline
 581.94
 \end{array}$$

$$\begin{array}{r}
 179.60 \\
 54.48 \\
 \hline
 145.12
 \end{array}$$

6.91.00
1050.1499
2060.58.15
43091.75

273 45
136 45
179 45

279 60
137 32
275 05
42 24
273 54
136 57

1446
238
1724

23 03

147.00
5815
5115

56.16
151.85
1499