

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN:

PLAN Survey

COUNTY RD. G

From Birch Lake Blvd. S. To Centerville Rd

Road Acc't. No. ....

Date Filed 11-8-29

File .....

PROJ. 30-11

10-25-29  
(Clear Warm)

K Weber  
Beaton  
Bell

Transit Notes.  
County Road "G."  
From So. Birch Lake Rd To  
Centerville Road.  
Sta. 64+68<sup>1</sup>/<sub>2</sub> To Sta. 105+16.<sup>4</sup>/<sub>2</sub>

PROJ - 30 - 11

89+00.<sup>63</sup>

Triangulation over Swamp.

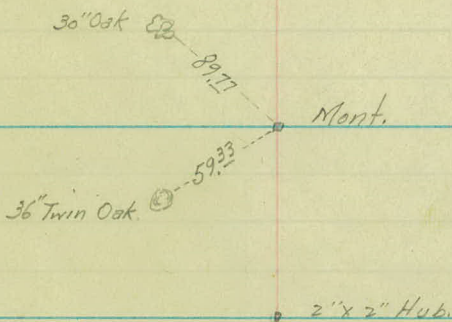
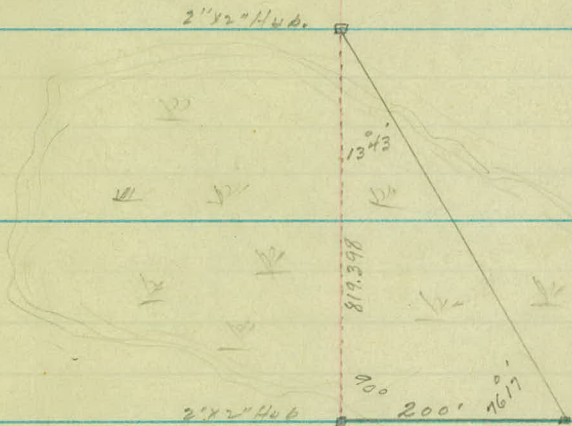
80+81<sup>23</sup>

78+68.<sup>0</sup> No. East cor. Sec. 21 - R30 W - T. 22 N.

73+73.<sup>2</sup>

64+68.<sup>12</sup>

10-25-29



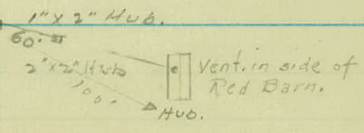
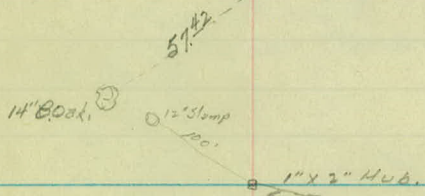
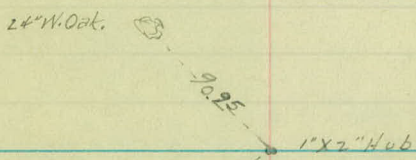
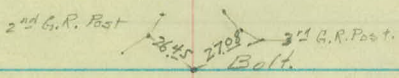
2648.42 = Meas. Dist  
2647.87 = Rec. "  
.55 Error

105+16.43 North  $\frac{1}{4}$  Cor Sec. 21-T30N-R22W.

101+00 P.O.T.

91+52.28 P.O.T.

10-25-29



Sta.

B.M. 3.67 936.63 932.96

T.P. 4.39 936.37 4.65 931.98

5.96 939.62 2.71 933.66

B.M. 3.84 935.78

4.05 935.57

T.P. 1.99 928.78 12.83 926.79

T.P. 5.67 924.17 10.28 918.50

10.61 933.15 1.63 922.54

10.85 943.64 0.36 932.79

B.M. 1.43 942.21

T.P. 1.06 931.82 12.88 930.76

5.89 926.47 11.24 920.58

B.M. 11.95 934.27 4.15 922.32

13.08 946.90 0.45 933.82

13.27 959.91 0.26 946.64

8.84 968.75 0.00 959.91

B.M. 2.76 965.99

7.02 967.22 8.55 960.20

B.M. 5.00 962.22

5.44 961.78

Clear Warm 10-25-29

Spike in 20" Oak 60' Lt Sta. 64-43

Top Sta. Near Sta 70+00

Spike in 20" Oak 60' Lt Sta. 77+90.

Top Mont. Sta. 78+68.0

R.R. spike in 60' Lt. Sta 91+90

Top State 92+50

Spike in 24" Oak 60' Lt Sta 99+75

Spike in 24" Oak 65' Lt Sta. 101+70

Spike in 20" Oak 12' Lt Sta 104+80

of Centerville Pave.

Sta					
64	3.54	936.50 ✓		932.96 ✓	
+83					33.1.
+90	Bottom Ditch				30.8.
+96					32.0.
65					31.9.
66					32.8.
67					31.6.
68					31.5.
69					31.4.
70					31.8.
T.P.	4.04	936.02 ✓	4.52	931.98 ✓	
71					30.2.
+50					26.5.
72					23.9.

LT E Rt.

spike in 20" oak 60' Lt Sta 64+43 10-26-29

$\frac{3.7}{40}$   $\frac{3.5}{37}$   $\frac{3.0}{22}$  3 4  $\frac{5.1}{8}$   $\frac{4.7}{17}$   $\frac{5.0}{40}$   $\frac{5.0}{50}$

$\frac{3.0}{40}$   $\frac{2.9}{37}$   $\frac{3.5}{12}$  5.7  $\frac{4.6}{7}$   $\frac{4.2}{14}$   $\frac{4.7}{40}$   $\frac{4.8}{50}$

$\frac{2.9}{40}$   $\frac{3.5}{17}$   $\frac{5.1}{9}$   $\frac{5.2}{4}$  4.5  $\frac{4.6}{20}$   $\frac{4.9}{40}$   $\frac{5.0}{50}$

$\frac{3.0}{40}$   $\frac{3.4}{25}$   $\frac{4.7}{12}$   $\frac{4.3}{3}$  4.6  $\frac{4.6}{20}$   $\frac{4.9}{40}$   $\frac{5.0}{50}$

$\frac{5.0}{40}$   $\frac{4.8}{7}$  3.7  $\frac{4.7}{20}$   $\frac{5.0}{40}$   $\frac{5.0}{50}$

$\frac{4.7}{40}$   $\frac{4.7}{20}$  4.9  $\frac{4.9}{20}$   $\frac{5.2}{40}$

$\frac{5.0}{40}$   $\frac{4.8}{20}$  5.0  $\frac{4.9}{20}$   $\frac{5.0}{40}$

$\frac{5.1}{40}$   $\frac{5.2}{20}$  5.1  $\frac{5.0}{20}$   $\frac{5.1}{40}$

$\frac{5.2}{40}$   $\frac{4.9}{20}$  4.7  $\frac{4.7}{20}$   $\frac{4.6}{40}$

$\frac{7.1}{40}$   $\frac{6.7}{20}$  5.8  $\frac{4.7}{20}$   $\frac{4.1}{40}$

$\frac{12.2}{40}$   $\frac{11.0}{20}$  9.5  $\frac{7.5}{20}$   $\frac{5.2}{40}$

$\frac{13.8}{40}$   $\frac{13.6}{20}$  12.1  $\frac{9.6}{20}$   $\frac{6.9}{40}$

72		936.02 ✓				
+50						24.9.
73						27.5.
+75						32.5.
74						32.9.
75						32.0.
76						33.5.
T.P.	6.25	939.91 ✓	2.36	933.66 ✓		
77						34.3.
B.M.			4.13	935.78 ✓		
78						34.6.
B.M.						
79						35.6.
+70						35.1.
80						30.4.
T.P.	134	928.15 ✓	13.12	926.79 ✓		
+17						24.8.
+28						20.9.

Lt                      Lt                      Pt. 10-76-29

$\frac{14.2}{40}$     $\frac{13.3}{20}$    11.1    $\frac{9.4}{20}$     $\frac{7.4}{40}$

$\frac{11.8}{40}$     $\frac{10.4}{20}$    8.5    $\frac{5.5}{30}$     $\frac{5.8}{40}$

$\frac{5.6}{40}$     $\frac{5.2}{30}$     $\frac{3.7}{7}$    3.5    $\frac{3.9}{20}$     $\frac{3.7}{40}$

$\frac{5.3}{40}$     $\frac{4.4}{20}$    3.1    $\frac{3.2}{20}$     $\frac{3.0}{40}$

$\frac{4.8}{40}$     $\frac{4.6}{20}$    4.0    $\frac{4.2}{20}$     $\frac{4.2}{40}$

$\frac{3.4}{40}$     $\frac{3.3}{20}$    2.5    $\frac{3.2}{20}$     $\frac{3.8}{40}$

Top of Stake at Sta. 76+00

$\frac{6.6}{40}$     $\frac{6.2}{20}$    5.6    $\frac{5.9}{20}$     $\frac{6.1}{40}$

Spike in 20" oak 60' ht Sta. 77+90

$\frac{4.9}{40}$     $\frac{5.0}{20}$    5.3    $\frac{5.0}{20}$     $\frac{5.0}{40}$

$\frac{4.3}{40}$     $\frac{4.0}{20}$    4.3    $\frac{4.5}{20}$     $\frac{4.4}{40}$

$\frac{4.2}{40}$     $\frac{4.6}{20}$    4.8    $\frac{4.9}{20}$     $\frac{5.1}{40}$

$\frac{7.5}{40}$     $\frac{8.5}{20}$    9.5    $\frac{10.7}{20}$     $\frac{10.4}{40}$

3.3    $\frac{3.7}{4}$     $\frac{6.2}{10}$     $\frac{6.6}{20}$     $\frac{6.9}{40}$

$\frac{6.8}{40}$     $\frac{7.0}{20}$    7.2    $\frac{7.3}{20}$     $\frac{8.0}{40}$

928.13 ✓

81 Beg. Swamp 17.4.

+50 16.2.

+70 15.4. ✓

T.P. 5.33 923.82 ✓ 9.64 918.49 ✓

" " 7.19 929.74 ✓ 1.27 922.55 ✓

86 915.94 ✓ 15.9. ✓  
Lorr.

87. 16.2.

88 16.4.

+50 17.9.

89 20.0.

+80 23.1.

90 24.7. ✓

T.P. 13.49 939.17 ✓ 4.06 925.68 ✓

+50 29.2.

91 34.7.

10-28-29

$\frac{10.7}{40}$   $\frac{10.7}{20}$  10.7  $\frac{10.6}{20}$   $\frac{11.0}{40}$

$\frac{11.9}{40}$  11.9  $\frac{11.9}{40}$

12.7

See late X-sections for this  
138 space.

13.5

$\frac{12.7}{40}$   $\frac{12.8}{20}$  13.3  $\frac{13.1}{20}$   $\frac{13.2}{40}$

$\frac{12.2}{40}$   $\frac{12.0}{20}$  11.8  $\frac{12.0}{20}$   $\frac{12.1}{40}$

$\frac{9.9}{40}$   $\frac{9.7}{20}$  9.7  $\frac{9.4}{20}$   $\frac{10.0}{40}$

$\frac{3.8}{40}$   $\frac{5.5}{20}$  5.6  $\frac{7.2}{4}$   $\frac{7.6}{20}$   $\frac{7.7}{40}$

$\frac{1.3}{40}$   $\frac{3.6}{20}$  5.0  $\frac{6.0}{5}$   $\frac{6.5}{20}$   $\frac{6.2}{40}$

$\frac{5.5}{40}$   $\frac{8.2}{20}$  10.0  $\frac{10.1}{3}$   $\frac{10.5}{20}$   $\frac{9.5}{40}$

$\frac{6.2}{40}$   $\frac{6.1}{20}$  4.5  $\frac{3.9}{20}$   $\frac{3.6}{40}$   $\frac{3.6}{50}$

		939.17 ✓			938.66 ✓	
T.P.	4.68	943.34 ✓	0.51			
91						
	+50					39.0.
B.M.			1.12	942.22	942.21	
	+85					38.1.
92						36.8.
	+50					30.8.
		0.28	931.05 ✓	12.57	930.77 ✓	
93						25.0.
	+50					21.4.
94						20.2
			10.47	920.58 ✓		
95						20.6.
T.P.	6.00	927.03 ✓	10.02	921.03 ✓		
96						20.8.
97						21.1.
98						21.4.
99						22.0.

10-28-29

R.R. spike in 20" oak 60' Lt Sta. 91 1/2 90

$\frac{60}{40}$	$\frac{5.3}{20}$	4.3	$\frac{4.6}{20}$	$\frac{4.7}{40}$
$\frac{3.0}{40}$	$\frac{4.2}{20}$	5.2	$\frac{5.2}{20}$	$\frac{6.0}{37}$
				$\frac{6.9}{45}$

$\frac{3.0}{40}$	$\frac{5.1}{20}$	6.5	7.3	$\frac{8.4}{40}$
------------------	------------------	-----	-----	------------------

$\frac{7.7}{40}$	$\frac{10.8}{20}$	12.5	$\frac{14.2}{3}$	$\frac{16.6}{20}$	$\frac{17.6}{40}$
------------------	-------------------	------	------------------	-------------------	-------------------

(1.9)

1.9	$\frac{3.0}{40}$	$\frac{3.9}{12}$	6.1	7.2	7.8	$\frac{8.3}{40}$	$\frac{8.3}{50}$
-----	------------------	------------------	-----	-----	-----	------------------	------------------

(6.0)

$\frac{6.9}{40}$	$\frac{8.4}{20}$	9.7	$\frac{10.2}{20}$	$\frac{10.1}{40}$
------------------	------------------	-----	-------------------	-------------------

(8.0)

$\frac{10.4}{40}$	$\frac{10.8}{20}$	10.9	$\frac{10.7}{20}$	$\frac{10.4}{40}$
-------------------	-------------------	------	-------------------	-------------------

(8.1)

$\frac{10.4}{40}$	$\frac{10.5}{20}$	10.5	$\frac{10.4}{20}$	$\frac{10.3}{40}$
-------------------	-------------------	------	-------------------	-------------------

(3.2)

$\frac{6.1}{40}$	$\frac{6.2}{20}$	6.2	$\frac{6.2}{20}$	$\frac{6.0}{40}$
------------------	------------------	-----	------------------	------------------

(0.8)

$\frac{6.0}{40}$	$\frac{6.1}{20}$	5.9	$\frac{6.0}{20}$	$\frac{6.0}{40}$
------------------	------------------	-----	------------------	------------------

(-3.3)

$\frac{5.9}{40}$	$\frac{5.7}{20}$	5.6	$\frac{5.6}{20}$	$\frac{5.5}{40}$
------------------	------------------	-----	------------------	------------------

(-8.3)

$\frac{5.5}{40}$	$\frac{5.3}{20}$	5.0	$\frac{4.4}{20}$	$\frac{4.0}{40}$
------------------	------------------	-----	------------------	------------------

99 927.03 ✓  
 +40 22.6 ✓  
 T.P. 12.02 934.34 ✓ 4.71 922.32 ✓  
 +50 24.6 ✓  
 B.M. 12.91 946.74 ✓ .51 933.83 ✓ (933.82)  
 100+00 41.3 ✓

+25 46.5 ✓  
 T.P. 13.49 960.15 ✓ 0.08 946.66 ✓  
 +50 52.1 ✓  
 T.P. 8.86 968.75 ✓ 0.26 959.89 ✓  
 101+00 61.1 ✓

+50 63.2 ✓  
 102 62.4 ✓

+50 62.7 ✓  
 103 60.0 ✓

104 59.7 ✓  
 10 +50 61.1 ✓

+83 E P / w Centerville Rd. Top Slope. 62.5 ✓  
 T.P. 6.90 967.09 ✓ 8.56 960.19 ✓

10-28-29

$$\frac{5.2}{40} \quad \frac{4.8}{20} \quad 4.4 \quad \frac{4.0}{20} \quad \frac{5.4}{40}$$

$$\frac{9.4}{40} \quad \frac{9.7}{20} \quad 9.7 \quad \frac{10.0}{20} \quad \frac{9.4}{40}$$

$$\frac{4.4}{40} \quad \frac{4.7}{20} \quad 5.4 \quad \frac{7.3}{13} \quad \frac{7.9}{20} \quad \frac{9.3}{40}$$

$$\frac{+2.3}{40} \quad \frac{+1.0}{20} \quad 0.2 \quad \frac{1.6}{10} \quad \frac{4.4}{30} \quad \frac{4.9}{40}$$

$$\frac{1.7}{45} \quad \frac{4.0}{20} \quad 8.1 \quad \frac{10.2}{14} \quad \frac{10.9}{30} \quad \frac{11.3}{40}$$

$$\frac{9.3}{40} \quad \frac{7.7}{20} \quad 7.7 \quad \frac{8.8}{20} \quad \frac{9.8}{40}$$

$$\frac{5.4}{40} \quad \frac{4.8}{20} \quad 5.6 \quad \frac{7.0}{12} \quad \frac{8.7}{30} \quad \frac{10.3}{40}$$

$$\frac{3.4}{40} \quad \frac{5.2}{20} \quad 6.4 \quad \frac{6.9}{4} \quad \frac{7.5}{20} \quad \frac{8.1}{40}$$

$$\frac{5.8}{40} \quad \frac{5.6}{20} \quad 6.1 \quad \frac{5.9}{20} \quad \frac{5.6}{40}$$

$$\frac{10.8}{40} \quad \frac{10.5}{20} \quad 8.8 \quad \frac{7.8}{2} \quad \frac{7.1}{15} \quad \frac{4.8}{40}$$

$$\frac{12.0}{40} \quad \frac{12.0}{30} \quad 9.1 \quad \frac{8.0}{2} \quad \frac{8.1}{15} \quad \frac{7.0}{40}$$

$$\frac{10.1}{40} \quad \frac{8.4}{20} \quad 7.7 \quad \frac{8.1}{20} \quad \frac{8.0}{40}$$

$$\frac{10.5}{40} \quad \frac{9.0}{20} \quad 6.3 \quad \frac{7.6}{7} \quad \frac{7.3}{30} \quad \frac{7.5}{40}$$

104

96709

+ 92

Bottom Ditch. 58.2.

105 + 03

Top of Shoulder. 61.8.

+ 16.42

± Pavc Centerville Rd. 61.8.

B.M.

4.89 962.20 962.22

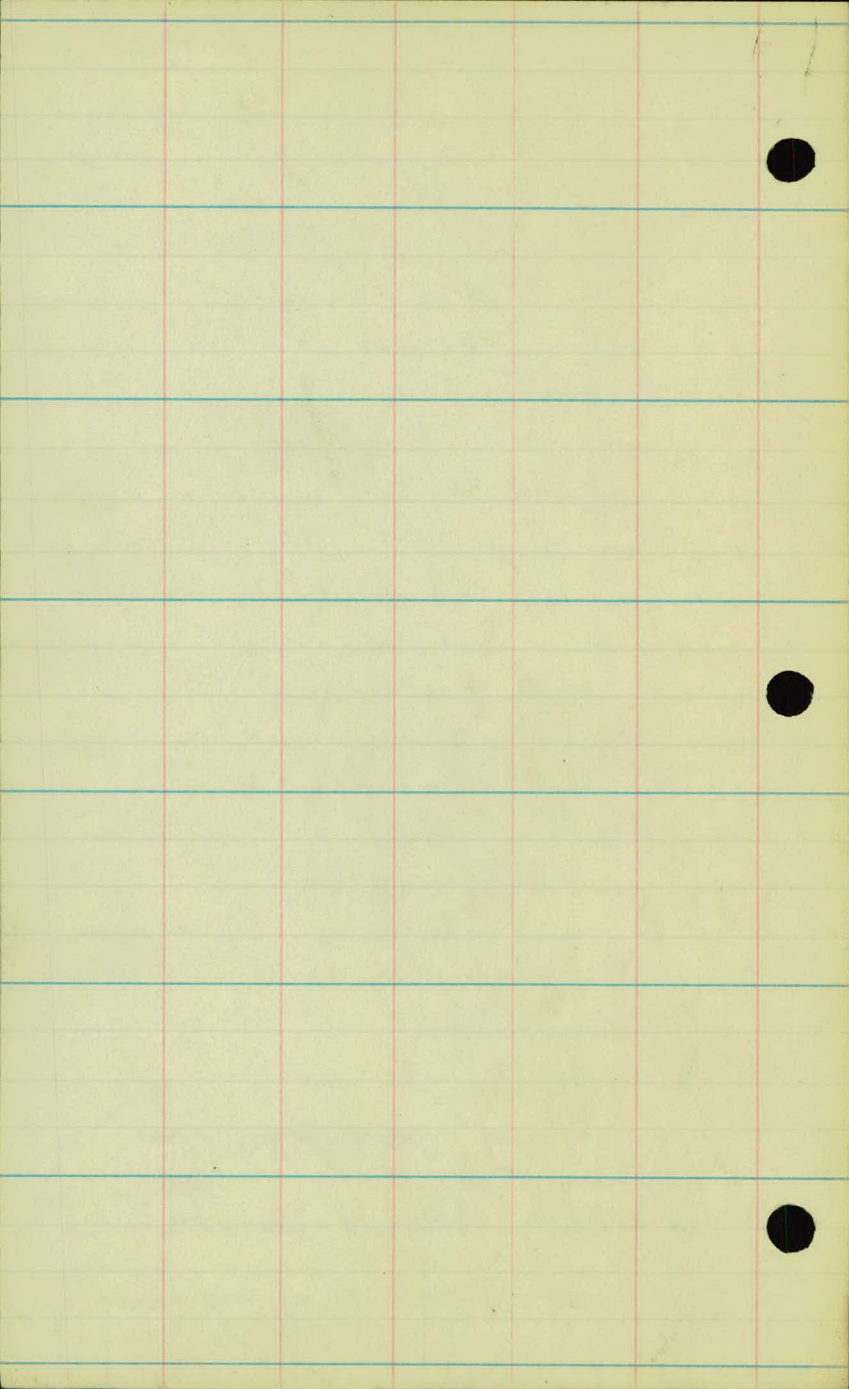
10-28-29

$\frac{8.7}{40}$   $\frac{8.9}{20}$  8.9  $\frac{8.3}{20}$   $\frac{8.2}{40}$

$\frac{5.0}{40}$   $\frac{5.0}{20}$  5.3  $\frac{5.7}{20}$   $\frac{5.8}{40}$

$\frac{4.8}{50}$  5.3  $\frac{5.85}{50}$

spike in 20" Oak 12 ft Sta. 104 + 80





B.M. 3.93 739.71 ✓ 735.78 ✓

1.58 728.81 ✓ 12.48 727.23 ✓

82 . 16.0 .

83 . 15.8 .

84 . 15.9 .

85 . 15.9 .

86 . 16.1 .

87 . 16.2 .

12.60 739.83 ✓ 1.58 727.23 ✓

B.M. 4.05 735.78 ✓

$$\frac{130}{43}$$

4.5

$$12.8$$

$$\frac{130}{50}$$

$$\frac{130}{43}$$

$$\frac{130}{40}$$

4.6

$$13.0$$

$$\frac{130}{40}$$

$$\frac{12.9}{40}$$

4.7

$$12.9$$

$$\frac{12.9}{40}$$

$$\frac{12.9}{40}$$

4.8

$$12.9$$

$$\frac{12.9}{40}$$

$$\frac{12.7}{40}$$

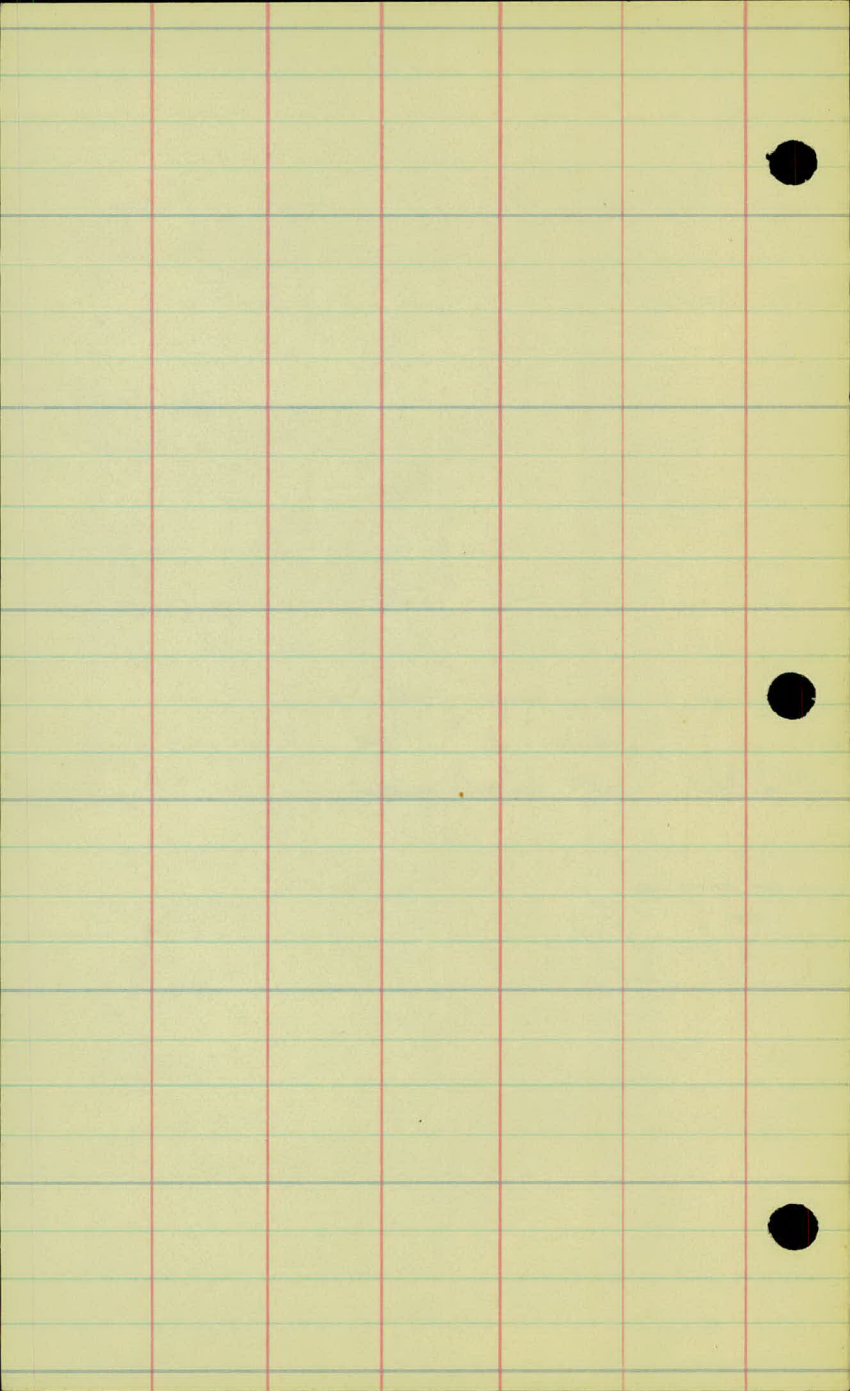
$$12.7$$

$$\frac{12.6}{40}$$

$$\frac{12.4}{40}$$

$$12.6$$

$$\frac{12.3}{40}$$



10-28-29

Topog. Notes.  
Co "Road G"

So. Birch Lake Rd. To Centerville Rd.  
Sta. 64+68'2 To

74

73

72

71

~~70~~

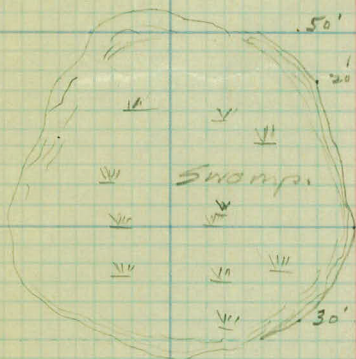
66

65

10-28-29

+58 = 16" Apple 10.1  
Twin.

+10-12" Apple 10'  
+00 = B&F. Orchard.



Cultivated

o Iron

Cultivated

+567 Iron and  
End Fence.  
3'

+83 = Shoulder

+ So Birch, LL Bl.

+95 F. Cor. 4'  
+77 T.P. 20'

82

81

80

79

78

77

76

10-28-29



SWAMP

+00 = Beg. Swamp

+22 <sup>12"</sup> Twin Oak 28'  
+20 = 15" Oak 22'

Pasture

+68 - Mont & Int. Fence.  
+46 - 14' Oak 19'  
+30 - 24' Oak 32'

Mont. x x x x x x x x x x

+80 - 20" Oak 33'

+55 = Fence x x x x x x x x x x

Orchard.

Cultivated

93

92

91

90

89

88

10-28-29

+00 End Cultivation

End Cult. RT

+26 = 12' Oak 2'  
+10 = 12' Oak 2'

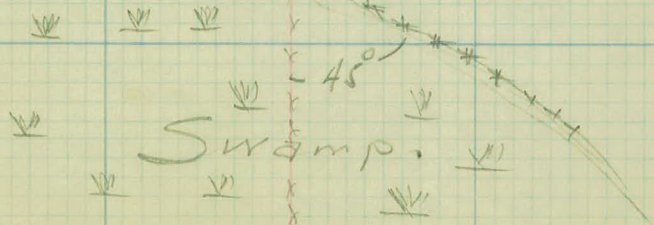
+96 = 6" Oak 6'    xxxxxxxx  
+92 = 10" W.O. 33' 4 F. Cor.

Cultivated

Cultivated

+00 = Beg. Cultivation

+46 End Swamp  
+46 Int. Fence RT



99

98

97

96

95

94

93

+50 - 15" Oak 6'

10 - 28 x 29

89 = 6" Oak E

+84 = 8" Oak 3'

+65 = Group of 5  
10" Oaks.

Fence is on Rt.

+00 = Edge Low Land.

+31 = Fence Int.

Fence 2' Rt of

+15 = F. Int. Cor. x x x x x  
190

200'

+70 = End Clearing

+45 = Light Clearing 20'

180'

Low Boggy Land.

100'

+50. Edge Low Land

105

Centerville Pave.

104

103

102

101

100

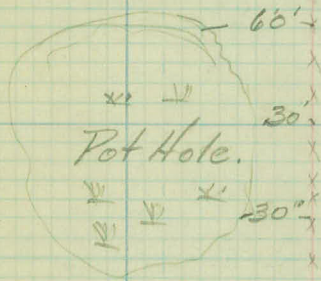
10-28-29



+83 Int. Fence.  
+80 = 18" Oak 15'

xxxxxxxxxxxx

+03. G. R.  
+97 = Rd 59. E  
+80 = 12" B.F. 2'



Farm Yard.

+68 = 10" Oak 22'  
+28 = 8" Oak 01.  
+24 = 6" Oak 01.  
+11 = 8" Oak 10'  
+05 = 10" Oak 9'  
+96 = 8" Oak 5'

+22 = 10" Oak 32'

xxxxx +28 Int. Fence.

+40 = 20" Oak 14'  
+10 = 15" Oak 14'

+68 = 24" Oak 6'  
+19 = 6" Oak 5'  
+93 = 15" Oak 3'

F. is 2 Rt.

+22 = 20" Oak 14'

Fence 3' Rt.

150



Sounding's

30:11

SOUNDING # 1 30 RT STA. 81+00

0-5' MUCK. VERY WET.

5'-12' FINE SAND. " "

6' FIRM BOTTOM.

SOUNDING # 2 15 RT STA. 81+00

0-5' MUCK. VERY WET.

5'-10' FINE SAND

6' FIRM BOTTOM.

SOUNDING # 3 ON CAT STA 81+00

0-5' MUCK VERY WET

5'-11' FINE SAND

6' FIRM BOTTOM.

SOUNDING # 4 15 LT. OF STA 81+00

0-4<sup>5</sup>' MUCK VERY WET

4<sup>5</sup>'-8' FINE SAND.

6' FIRM BOTTOM.

SOUNDING # 5 30 LT. OF STA 81+00

0-4<sup>5</sup>' MUCK VERY WET.

4<sup>5</sup>'-8' FINE SAND.

6' FIRM BOTTOM.

Crane made soundings  
at Sta. 81+00

Sounding #1 30' Rt Sta. 82+00  
0-13 Wet Black Muck  
13-16 Fine Sand + Soft Clay.  
16' Plus 2' Compact sand

Sounding #2 15' Rt. Sta. 82+00  
0-13 Wet Muck  
13-16 Fine sand + Soft Clay.  
16 Plus 1' Compact sand.

Sounding #3 On L at Sta. 82+00  
0-14 Wet Muck  
14-16 Fine sand + Soft Blue Clay  
16' Plus 1' Compact Sand

Sounding #4 15' Lt Sta. 82+00  
0-13 Wet Muck.  
13-16 Fine sand + Blue Clay  
16-Plus 2' = Compact sand

Sounding #5 30' Lt Sta 82+00  
0-13 = Wet Muck soft.  
13-16 = Soft Blue Clay + Fine sand.  
16-Plus 1' Compact sand.

These soundings were taken with  $\frac{1}{2}$ " pipe and a plunger connection on lower end, for taking samples. Forcing pipe to different depths with the aid of three (3) men. Total weight appr. 500 lbs.

Sounding # 1 = 30' Rt Sta 83+00  
0-14 Wet Black Muck  
14-20 Soft Clay + Black Sand  
20-Plus 2' Compact Sand

Sounding # 2 15' Rt Sta. 83+00  
0-14 Wet Black Mush  
14-21 Soft Clay + Fine Sand  
21 Plus 1' = Compact Sand

Sounding # 3 on L at Sta 83+00  
0-15 Wet Black Muck  
15-21 Soft Clay + Black Sand  
21-Plus 1' = Compact Sand

Sounding # 4 15' Lt Sta 83+00  
0-15 = Wet soft Muck  
15-21 = Fine Sand + Soft Clay  
21-Plus 1' Compact Sand

Sounding # 5 30' Lt Sta 83+00  
0 To 14 Wet Black Muck  
14-20 Soft Clay + Black Sand  
20 To Plus 1' = Compact Sand

Soundings Sta 83+00 taken same as  
at Sta. 82+00

Sounding # 1 = 30' Rt. Sta. 84+00  
 0-18' = Wet Black Muck  
 18-27 = Fine sand + Soft Clay  
 27-Plus 2' = Firm Bottom

Sounding # 2 15' Rt. Sta. 84+00  
 0-17.5 Wet Black Muck  
 17.5-29 Soft Clay + Fine sand  
 29-Plus 1' = Firm Bottom.

Sounding # 3 Lt. Sta 84+00  
 0+18 Wet Black Muck  
 18-29.5 Soft Clay + Fine Sand  
 29.5-Plus 1.5 Firm Bottom.

Sounding # 4 15' Lt. Sta. 84+00  
 0-18' Wet Black Muck  
 18-29.5 Soft Clay + Fine sand  
 29.5-Plus 2' = Firm Bottom.

Sounding # 5 30' Lt. Sta. 84+00  
 0-18 = Muck  
 18-28.5 = Soft Clay  
 28.5 Plus 1.5 Firm Bottom.

Soundings take at Sta.  
84+00 taken same as at  
Sta. 83+00

Sounding # 1 30' Rt Sta. 85+00  
0-16 Wet Muck  
16-26' Soft Clay  
26' Plus 1' Firm Bottom.

" # 2 15' Rt  
0-16 Wet Muck  
16-27 Soft Clay  
27-Plus 1' Firm Bottom

" # 3 on E of Sta. 85+00  
0-16 Wet Muck  
16-29 Soft Clay.  
29-Plus Firm Bottom Clay + Fine sand.

" # 4 15' Lt 85+00  
0-16 Wet Muck  
16-26.5 Soft Clay.  
26.5 Plus 0.5 Firm Bottom

" # 5 30' Lt 85+00  
0-16.5 Wet Muck  
16.5-26.5 Soft Clay  
26.5 Plus 1' Firm Bottom.

Sta. 85+00 Soundings made same as  
at Sta. 84+00

Sounding #1 30' RT Sta 86+00  
0-14' Wet Muck  
14-18' Soft Clay  
18 Plus 1' Firm Bottom.

" #2 15' RT of Sta 86+00  
0-15' Wet Muck  
15-19' Soft Clay  
19 Plus as Firm Bottom.

" #3 on E at Sta 86+00  
0-16' Wet Soft Muck  
16-19<sup>5</sup>' Soft Clay  
19<sup>5</sup> Plus 1' Firm Bottom Fine sand.

" #4 = 15' Lt - same as #3 ±

" #5 30' Lt = same as #3

Soundings at Sta 86+00 taken  
same as at Sta. 85+00

{ (P.S.) When last sounding was  
made at this Sta. on raising  
pipe discovered plunger  
was missing.

12-26-29

Sounding #1 30' Rt Sta 87+00  
0-10<sup>5</sup> Muck  
10<sup>5</sup>-14 Soft Clay.  
14 Plus 1' Firm Stiff Clay

" #2 15' Rt Sta 87+00  
0-11 Wet Muck  
11-14 Soft Clay  
14 Plus 1' Firm Bottom Stiff Clay

Sounding #3 00<sup>2</sup> at Sta 87+00  
0-11 Wet Muck  
11-13<sup>5</sup> Soft Clay.  
13<sup>5</sup> Plus 1' Firm Bottom Stiff Clay

" #4 15' Lt Sta. 87+00  
0-12 Wet Muck  
12-14<sup>5</sup> Soft Clay  
14<sup>5</sup>-Plus Firm Stiff Clay

" #5 30' Lt  
0-12 Muck  
12-15 Soft Clay  
15' Plus 1' Firm Stiff Clay

Soundings at Sta. 87+00 were  
take in same manner as at  
Sta. 86+00 with exception of  
plunger.

9-27-29

Sounding #1 30' Rt Sta. 88+00  
0+10<sup>5</sup> Soft Muck  
10<sup>5</sup> Plus 1' Firm Stiff -- Clay

" #2 15' Rt Sta 88+00  
Same as #1

" #3 On  $\pm$  Sta 88+00  
0-11<sup>5</sup> Wet Muck  
11<sup>5</sup> Plus 1' Firm Stiff Clay.

" #4 15' Lt Sta 88+00  
Same as #5

" #5 30' Lt  
0-13 Soft Muck  
13 Plus 1' Firm Clay.

{ These soundings were  
made in same manner as  
preceding soundings with  
exceptions of plunger.

9-27-29

Sounding # 1 30' Rt. Sta. 94+00  
0-2' Moist Peat  
2'-5' Fressed Blue Clay.  
5'-12' Soft Blue Clay.  
12-Plus 1' Firm. Fine sand Clay + Gravel.

# 2 15' Rt. Sta. 94+00  
0-5 Same as 1st Sounding.

" # 3 on E Sta 94+00  
0-5' Moist Peat  
5'-12<sup>5</sup> Clay + Fine sand  
12<sup>5</sup>-14 Firm Bottom sand, Gravel  
and Clay.

" # 4 15' Lt Sta. 94+00  
Same as 5

" # 5 30' Lt. Sta. 94+00  
0-4' Moist Peat  
4'-14' Soft Clay + Fine sand  
14-Plus 0.5 Firm, Fine sand Clay and  
Gravel

Soundings No. 1-2-3-4 and 5  
at Sta. 94+00 were taken  
by means of a two (2") inch  
auger attached to  $\frac{1}{2}$ " pipe  
and specimens take at  
1-ft intervals

4-27-29

Sounding #1 30' Rt Sta 95+00  
0-9' Moist Peat  
9'-Plus Firm Clay + Gravel Bottom

" No. 2 15' Rt of Sta 95+00  
0-12 Moist Peat  
12-Plus 0.5 Firm Clay + Gravel

" #3 on  $\frac{1}{2}$  at Sta. 95+00  
0-17 Moist Peat  
17-Plus 1.5 Firm Clay + Gravel Bottom.

" #4 15' Lt Sta. 95+00  
0-19 Moist Peat  
19-Plus 1' Firm Clay + Gravel Bottom

" #5 30' Lt. Sta 95+00  
0-14 Moist Peat  
14-21<sup>5</sup> Brown Loam (Loose)  
21<sup>5</sup> Plus 1' Firm Clay + Gravel Bottom

Soundings at Sta. 95+00 were  
take in same manner as  
at Sta. 94+00

- 12-28-29  
-Sat. A.M.
- Sounding #1 30' Bt. Sta. 96+00  
0-8 Moist Peat.  
8-12<sup>5</sup> Soft Blue Clay.  
12<sup>5</sup>-Plus 1' Stiff Blue Clay Fine sand & Gravel.  
12-30-29
- " #2 Sounding same as #1
- " #3 Sta. 96+00 12-28-29  
0-10 Medium wet Peat  
10-13 Dark Soft Clay or Loam  
13-16<sup>5</sup> Pure Blue Clay (Medium Soft)  
16<sup>5</sup>-Plus 1<sup>5</sup>' Clay fine sand & Gravel (Firm)  
12-30-29
- #4 Sounding same as #3
- #5 30' Lt 12-30-29  
0-9<sup>5</sup> Wet Peat  
9<sup>5</sup>-12<sup>5</sup> Dark Grey Clay  
12<sup>5</sup>-14 " " " and Peat  
14-16<sup>5</sup> Blue Clay.  
16<sup>5</sup>-Plus 1' Firm Clay fine sand & Gravel.

Sta. 96+00 These soundings taken as  
at Sta. 95+00

12-30-9

#1 30' Lt Sta. 97+00  
0-9" Moist Peat  
9"-11" Firm Fine sand Clay + Gravel.

15' Lt.  
#2 Sounding as at #1

#3 Lt on Sta. 97+00  
0-9" Moist Peat.  
9-11" Soft Blue Clay  
11" Plus 1' Firm fine sand Clay + Gravel

#4 15' Lt.  
Same as at #5

#5 30' Lt Sta 97+00  
0-9" Moist Peat  
9-12" Loose Clay + Fine Sand.  
12 Plus 2' Firm Clay Fine sand and Gravel.

Soundings were made  
same as preceding one.

Sounding #1 30' RT Sta 98+00  
0-9 Moist Peat.  
9-12 Thick Blue Clay  
12 Plus Firm Clay + Fine sand + Gravel

" #2 15' RT  
0-8.5 Med. to Wet Peat  
8.5-13.5 Thick Blue Clay  
13.5 Plus 1' Firm Clay + Gravel.

" #3 Lt Sta. 98+00  
0-8 Medium to wet Peat.  
8-14 Thick Blue Clay.  
14 Plus 1' Firm Clay sand + Gravel

" #4 15' Lt  
Same soundings as #

" #5 30' Lt Sta.  
0-8.5 Medium to wet Peat.  
8.5-14 Thick Blue Clay  
14 Plus Firm Bottom.

Sta 98+00 Soundings made as at  
Sta 97+00

12.30-29

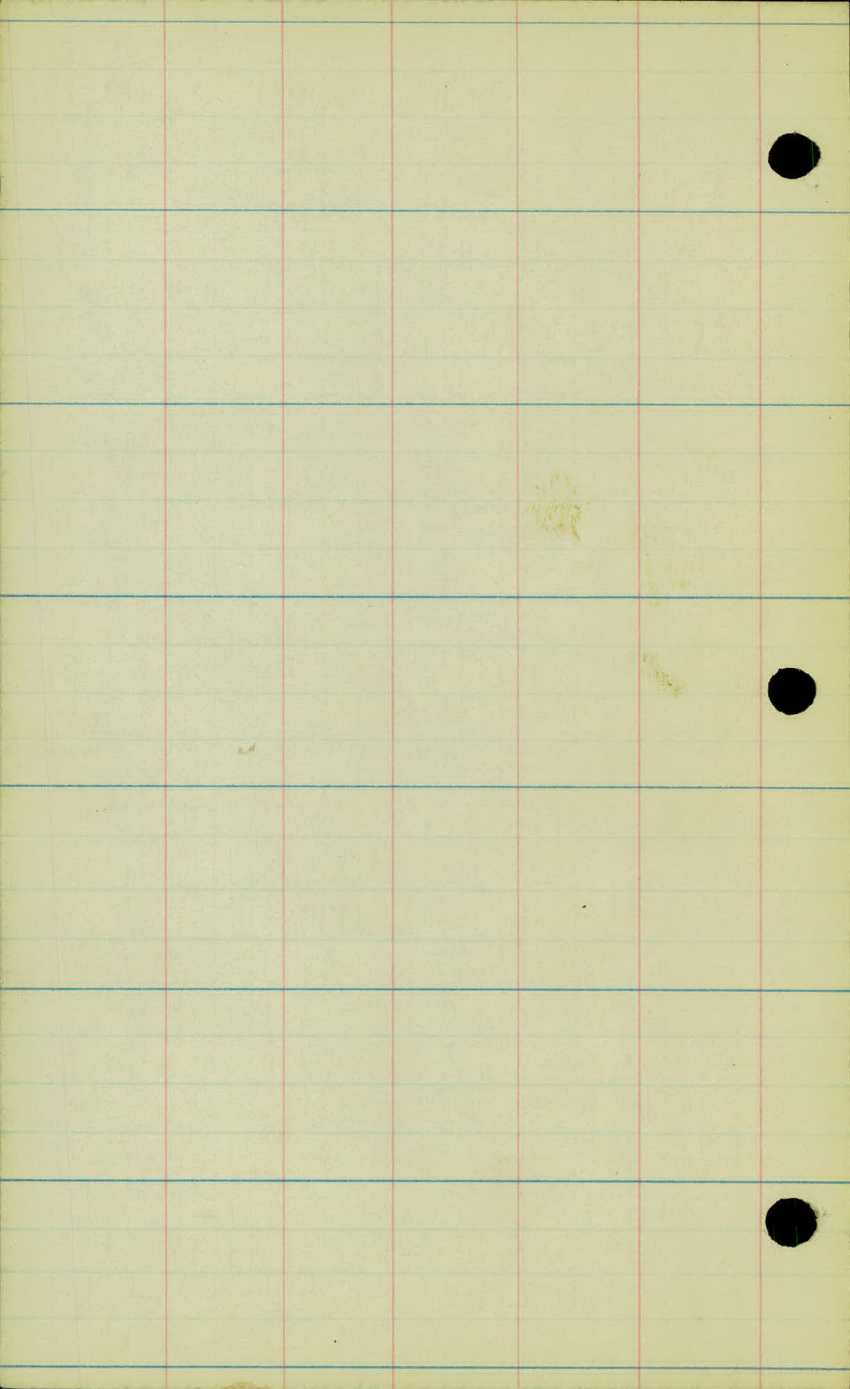
Sounding # 1 30' Rt. of Sta. 99+00  
0-2 Compressed Loam  
2-7.5 Moist Peat  
7.5-9.5 Blue Clay & Quick sand.  
9.5-15 Thick compressed Clay.  
15 Plus Firm Bottom

" #2 15' Rt.  
Sounding east of #3

" #3 Lt. Sta. 99+00  
0-2 Comp. Loam  
2-7.5 Moist Peat  
7.5-9.5 Clay & Quick sand.  
9.5-15 Compressed Clay  
15 Plus Firm Bottom.

" #5 30' Lt. Sta. 99+00  
0-1.5 Compressed Loam  
1.5-5.5 Peat  
5.5-7.5 Sandy Clay.  
7.5-10 Compressed Blue Clay  
10' Plus Firm Bottom.

Soundings made same  
as at Sta 98.



Co. ROAD "C"  
PROJ # 30-11  
ART. TOROS. ON CONN.  
AT END OF PROJ.

108

107

106

105

104  
25  
79

+74 G. RAIL 14<sup>3</sup>

+30 BEG G. RAIL 27

+77 END G. RAIL 27

+58 G. RAIL 13  
+51 BEG G. RAIL 12

+09 SIGN BOARD 33

+54 SIGN BOARD 46

+47 T.P. 32  
+49 STOP SIGN 18  
+45 END G. RAIL 13<sup>2</sup>  
+38 G. RAIL 16  
+34 G. RAIL 22  
+30 G. RAIL PLANS 29

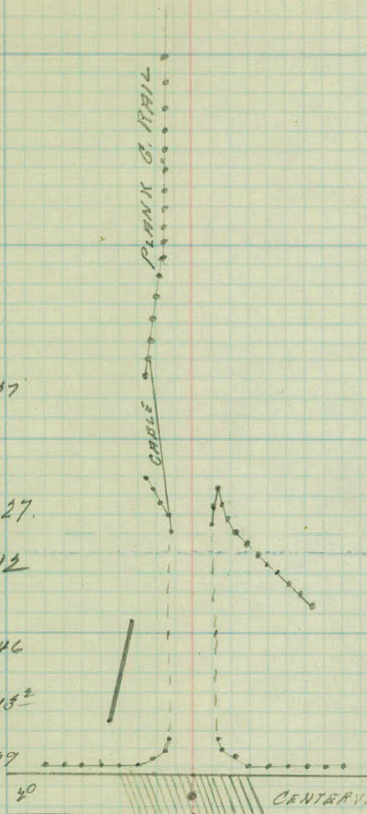
PLANK G. RAIL  
CABLE

+27<sup>2</sup> EDGE OF PINE

+66 X NO SIGN 18  
+62 STOP SIGN 11<sup>2</sup>  
+66 G. RAIL 20  
+71 G. RAIL 18<sup>0</sup>  
+62 G. RAIL 10<sup>2</sup>  
+55 BEG G. RAIL 11<sup>2</sup>

+30 G. RAIL 43

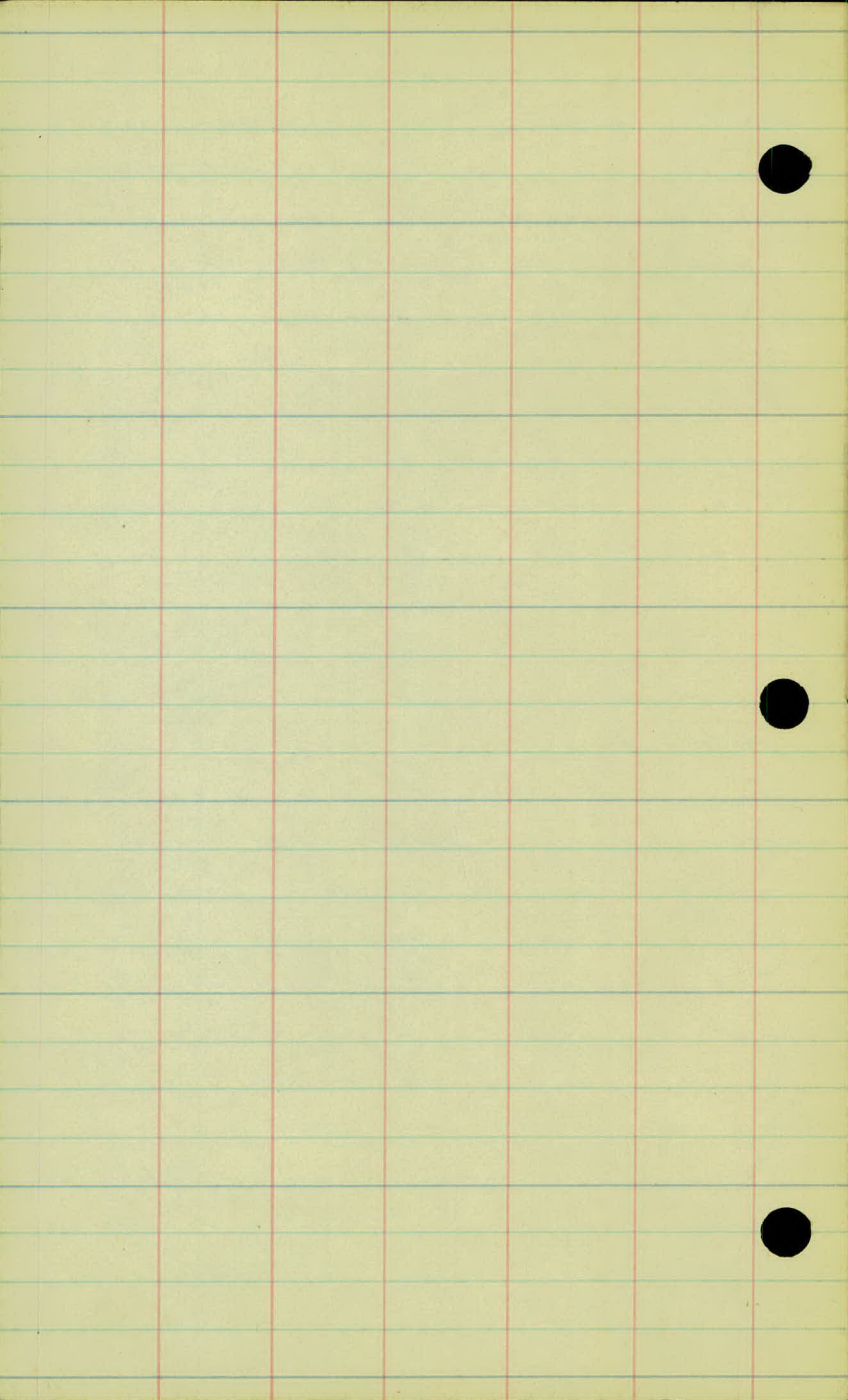
+37 I.H. SIGN 18  
+45 END G. RAIL 12<sup>0</sup>  
+50 G. RAIL 15<sup>2</sup>  
+34 G. RAIL 22  
+30 G. RAIL 29<sup>2</sup>



105 + 26<sup>42</sup> P.I.  
A - 0° - 02' R.

40

CENTREVILLE ROAD



Co. ROAD "C"

PROD. # 30-11

X SEC. ON CONN. AT END  
OF PROD.

B.M.	5.62	767.84	762.22
105+26 <sup>42</sup>		EDGE OF PAVE.	61.8
105+30			61.8
105+40			61.9
105+70			61.4
106+00			61.7
106+42			62.6
106+70			63.6
107+00			64.5
107+29 <sup>8</sup>			64.8
107+65			65.0
108+00			65.3
108+50		1.60	66.24
109+00		0.75	67.09
109+50		+0.70	68.54
110+00		+1.70	69.54
B.M.	5.62	762.22	

SIX IN 20 OAK 12 LT STR 104+80

EDGE OF PINE

5.74 6.44 6.63 6.95 6.97 6.97  
33 6.08 33 50 100 150 156

E.M.  
57 6.0 6.3 6.5 7.0 6.9 6.80  
38 21 6.0 21 50 100 150 158

E.P.  
103 101 6.2 6.6 7.6 10.5 11.7 10.5 6.7 6.84  
33 22 13 5.7 13 22 50 100 117 134 150

103 106 6.8 6.4 6.4 7.0 10.6 11.8 11.5 6.0 6.29  
33 18 11 8 6.4 9 13 20 50 76 96 105

E.P.  
10.4 10.4 6.6 6.2 6.1 6.5 10.7 10.4 5.6 5.60  
33 18 11 7 6.1 8 11 19 49 64 70

E.P.  
103 25 5.6 5.4 5.2 5.6 8.6 7.0 4.7 4.80  
33 19 12 8 5.2 7 11 17 24 34 40

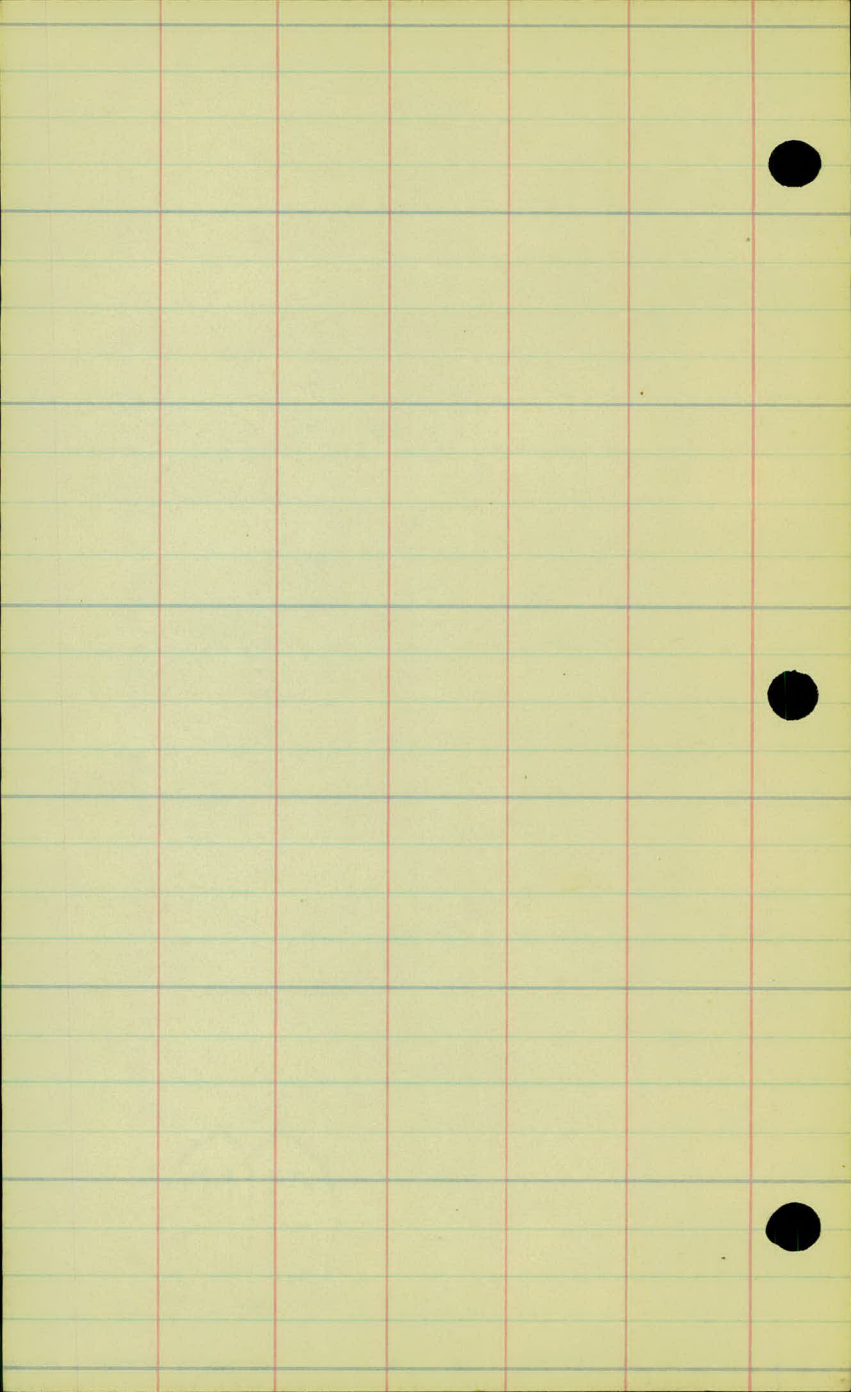
E.P.  
8.5 4.5 4.4 4.1 4.13 5.68 5.36 5.4  
33 23 10 4.2 8 22 46 46 50

E.P.  
8.2 8.1 3.6 3.4 3.57 5.30 4.97 5.2  
33 27 25 13 3.3 9 34 34 40

E.P.  
7.7 2.7 2.9 3.04 4.81 4.51 4.7  
36 25 6 24 24 30

E.P.  
7.7 7.3 2.5 2.52 3.78 3.67 3.7  
35 27 20 7 2.83 16 16 22

E.P.  
6.8 6.1 2.3 2.12 3.11 2.78 2.7  
33 22 15 10 2.45 12 12 18



Co. ROAD "C"

PROJ. # 30-11.

X SEC. FOR BORROW PIT.

BETWEEN STA. 89+50 TO 93+50.

B.M. 0.80 943.02 ✓ 742.22 ✓  
T.P. 0.82 933.62 ✓ 10.22 932.80 ✓  
89+50 22.2'

90+00 24.7'

90+50 29.2' ✓  
10.97 943.79 ✓ 0.82 932.80 ✓

90+50

91+00 34.7'

91+50 39.3'

92+00 36.8'

92+50 30.7'

93+00 2.40 933.19 ✓ 13.00 930.79 ✓

92+00

92+50

93+00 25.0'

LEFT

RIGHT.

$\frac{87}{150}$   $\frac{89}{151}$   $\frac{83}{100}$   $\frac{82}{83}$   $\frac{94}{50}$   $\frac{111}{20}$   $\frac{107}{2}$   $\frac{114}{24}$   $\frac{127}{50}$   $\frac{129}{78}$   $\frac{122}{100}$   $\frac{114}{111}$   $\frac{107}{150}$   $\frac{83}{150}$   $\frac{56}{150}$

$\frac{37}{150}$   $\frac{38}{130}$   $\frac{27}{100}$   $\frac{23}{80}$   $\frac{45}{50}$   $\frac{75}{22}$   $\frac{79}{3}$   $\frac{89}{4}$   $\frac{94}{22}$   $\frac{101}{50}$   $\frac{99}{73}$   $\frac{81}{100}$   $\frac{59}{125}$   $\frac{36}{150}$   $\frac{23}{150}$

$\frac{26}{36}$   $\frac{32}{17}$   $\frac{37}{2}$   $\frac{47}{44}$   $\frac{50}{6}$   $\frac{44}{28}$   $\frac{41}{50}$   $\frac{21}{66}$   $\frac{18}{70}$   $\frac{17}{100}$   $\frac{17}{123}$   $\frac{17}{50}$

$\frac{102}{150}$   $\frac{95}{123}$   $\frac{77}{100}$   $\frac{63}{88}$   $\frac{54}{72}$   $\frac{83}{50}$

14.6

$\frac{73}{150}$   $\frac{88}{131}$   $\frac{103}{100}$   $\frac{105}{50}$   $\frac{108}{42}$   $\frac{94}{6}$   $\frac{88}{71}$   $\frac{83}{8}$   $\frac{90}{33}$   $\frac{104}{50}$   $\frac{109}{64}$   $\frac{98}{83}$   $\frac{82}{100}$   $\frac{93}{123}$   $\frac{105}{150}$

$\frac{50}{150}$   $\frac{52}{132}$   $\frac{65}{100}$   $\frac{66}{80}$   $\frac{63}{50}$   $\frac{47}{7}$   $\frac{50}{45}$   $\frac{49}{14}$   $\frac{58}{39}$   $\frac{99}{50}$   $\frac{110}{73}$   $\frac{109}{100}$   $\frac{111}{106}$   $\frac{122}{127}$   $\frac{122}{150}$

$\frac{45}{150}$   $\frac{35}{119}$   $\frac{21}{100}$   $\frac{18}{92}$   $\frac{32}{50}$   $\frac{63}{16}$   $\frac{76}{70}$   $\frac{114}{27}$   $\frac{130}{50}$   $\frac{60}{60}$

X

$\frac{39}{150}$   $\frac{33}{140}$   $\frac{12}{100}$   $\frac{16}{88}$   $\frac{64}{50}$   $\frac{114}{21}$   $\frac{120}{11}$   $\frac{119}{7}$   $\frac{131}{131}$

$\frac{19}{150}$   $\frac{21}{137}$   $\frac{57}{100}$   $\frac{91}{80}$   $\frac{134}{50}$

18.8

13.6

$\frac{39}{85}$   $\frac{43}{100}$   $\frac{60}{135}$   $\frac{70}{150}$

$\frac{59}{3}$   $\frac{68}{23}$   $\frac{79}{50}$   $\frac{80}{83}$   $\frac{68}{100}$   $\frac{63}{134}$   $\frac{82}{150}$

$\frac{49}{29}$   $\frac{60}{12}$   $\frac{72}{7}$   $\frac{70}{8}$   $\frac{101}{26}$   $\frac{102}{50}$   $\frac{98}{85}$   $\frac{92}{100}$   $\frac{103}{127}$   $\frac{122}{150}$

733.19 ✓

93750

215 ✓

12.91

743.70 ✓

2.40

930.79 ✓

B.M.

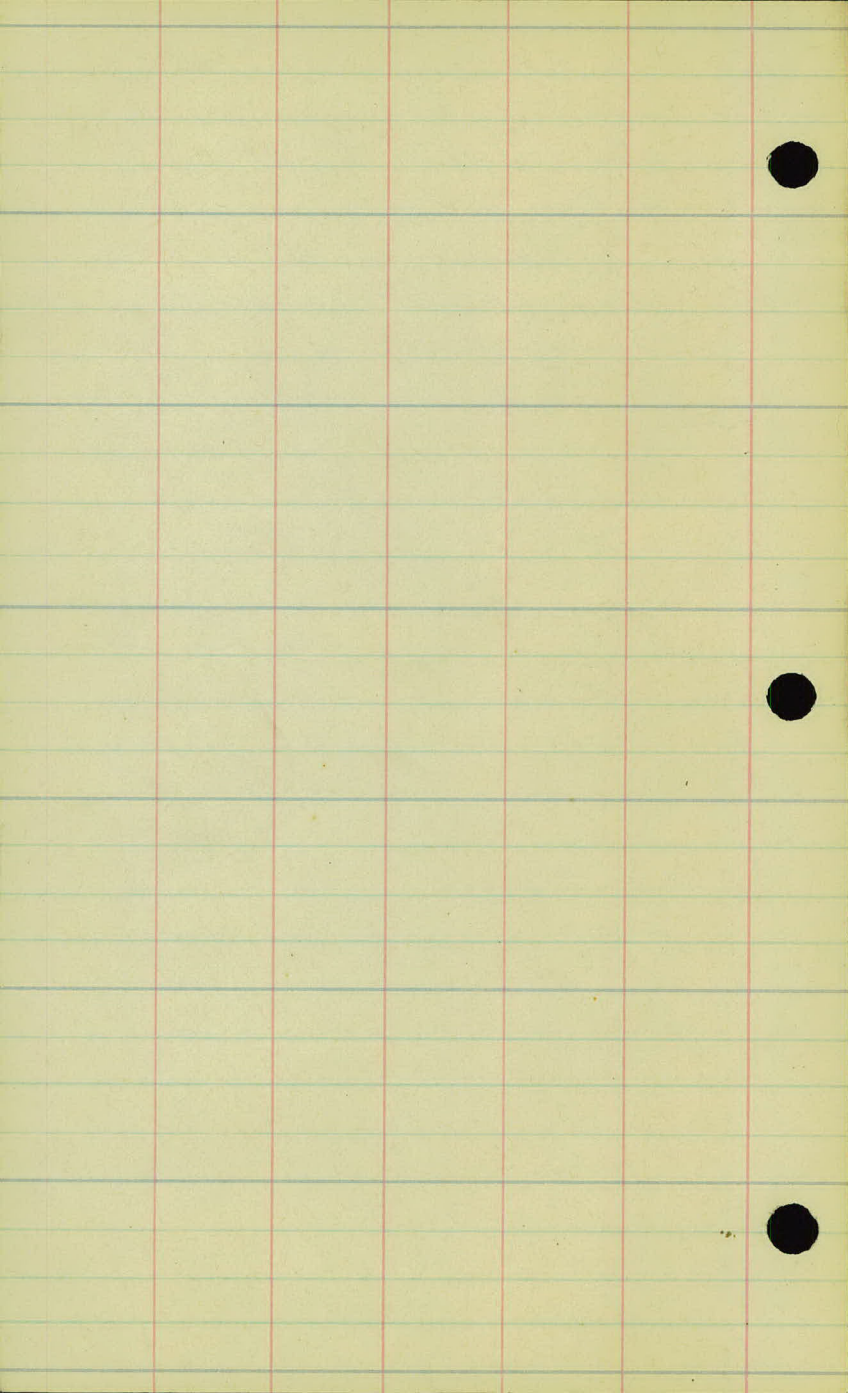
1.48

942.22 ✓

LEFT

RIGHT

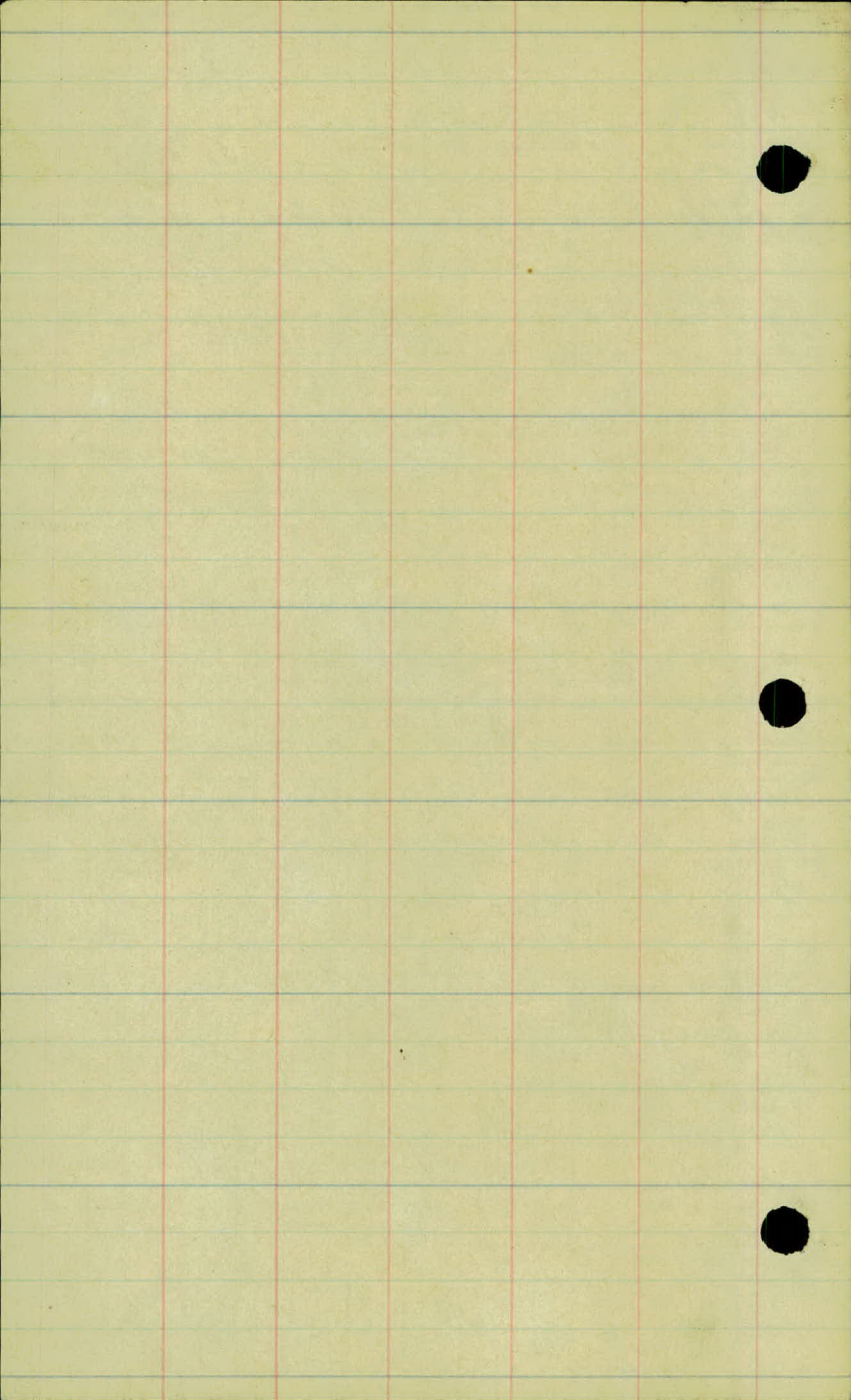
<u>128</u>	<u>120</u>	<u>18</u>	<u>34</u>	<u>54</u>	<u>77</u>	<u>94</u>	<u>120</u>	<u>117</u>	<u>111</u>	<u>121</u>	<u>123</u>	<u>124</u>
150	136	100	89	63	50	27	25	50	60	85	100	150



- x x 65+00 to 66+00 - Gr. 1 T.
- x x 74+00 to 80+15 - Cl. 28 T. Gr. 33 T. Lt.
- x x 77+00 Lt. - P. 15' x 20' C.M.
- x x 78+68 to 80+15 - Gr. 50' wide on Rt. 0.17 Ac.
- x x 81+00 - P. 36' x 60' P<sub>3</sub>. Haul 25.92 Inv 9174
- x x 91+50 to 92+50 - Cl. 5 T Gr. 21 T. Lt.
- x x 93+70 - P. 24' B x ~~72~~ H.D. Haul 23.80 Inv 9188
- x x 93+50 to 98+00 - H.D. on Rt & Lt
- x x 95+00 to 96+00 - Cl. 7 T. Lt.
- x x 99+50 to 103+00 - Cl. & Gr. 50' wide on Lt. 0.40 AC
- x x 103+00 to 104+00 - Cl. & Gr. 1 T. Rt.
- x x 104+50 to 105+00 - Cl. & Gr. 2 T. Lt.
- x x 105+03 - Remove 100' G.R.

All driveways from property lines.  
Remove G.R. at end of Proj.

- x 68+00 Rt - 15" x 20 C.M.
- x 68+00 Lt "
- x 73+00 Rt "
- x 73+00 Lt "
- x 80+20 Rt. "
- x 90+00 Rt "
- x 90+00 Lt "
- x 103+50 Rt "
- x 103+50 Lt "



M. W. Carley

U 2522