PLANS SURVEY
OF

COUNTY R.D. "A2"

From Lexington Ave to Victoria Street

PROJ. 29-65

8/2/28
C.W.S.
D.P.
W.H
H.T.

Alignment
Co. Rd. "A"
Lexington Ave.
To
Victoria Ave.

PROJECT 29-65

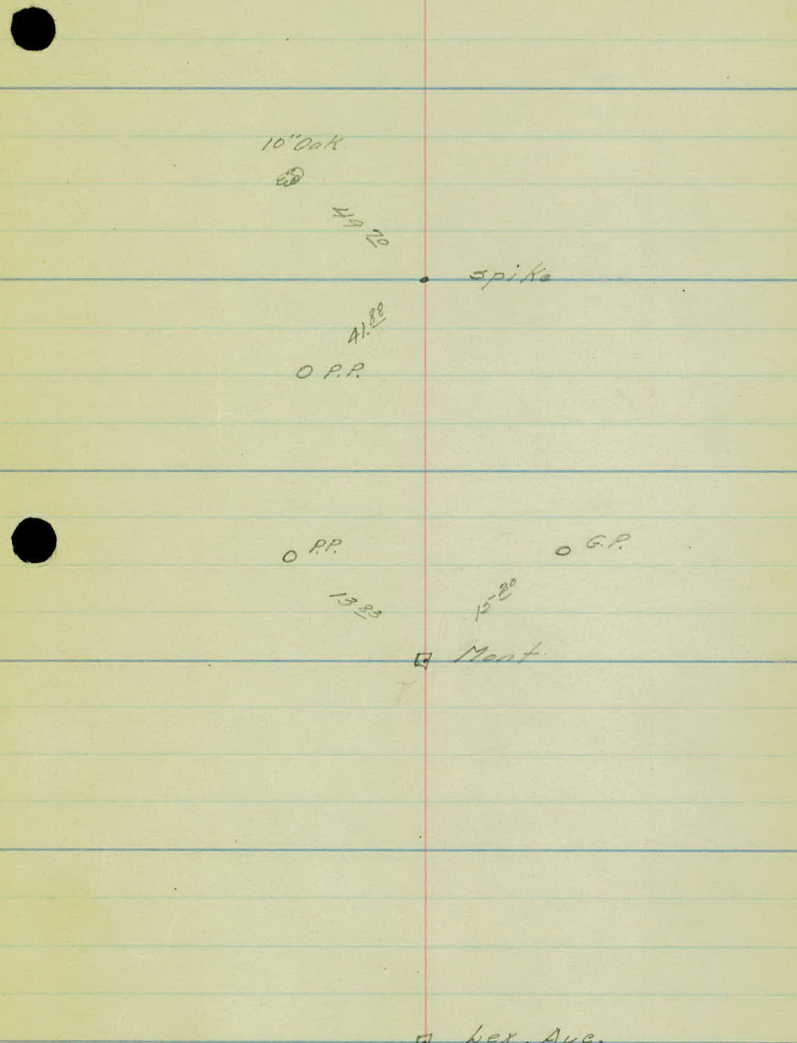
Received [signature]
8-11-28

2 to Point Δ Rt Δ Lt.

15+72.75

13+09.2 P.I. 0°-03

0+00


10" Oak
Spike
O P.P.
O P.P.
O G.P.
Mont.
Lex. Ave.

STA POINT A LT A RT.

20+24^{4} P.I. 13°-36'

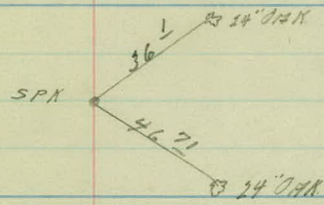
18+09^{5} P.I. 23°-35'

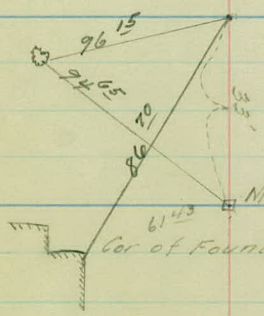
17+76^{5} P.O.T

179-60
156-25
23-35

156-26
314-52

156-26





8/3/28
CW 3
D.P. T
W.H. Rod
H.T.

Check Levels.
Co Rd. "A"
Re Levels.
Lexington Ave
To
Victoria Ave

Sta.	+	H.I.	−	Elev.
B.M.	5.01	923.94		918.93
T.P.	5.85	925.73	4.06	919.88
T.P.	5.25	926.59	4.39	921.34
T.P.	2.62	920.90	8.31	918.28
T.P.	8.99	925.46	4.43	916.47
T.P.	13.58	935.60	3.44	922.02
T.P.	3.37	938.32	0.65	934.95
T.P.	12.45	945.60	5.17	933.15
T.P.	13.10	958.08	0.62	944.98
T.P.	13.57	971.47	0.18	957.90
T.P.	9.90	981.21	0.16	971.31
B.M.	6.25	979.66	7.80	973.41
T.P.	1.09	969.78	10.97	968.69
B.M.	6.52	969.78	6.52	963.26
T.P.	0.24	956.73	13.29	956.49
T.P.	1.38	949.31	8.80	947.93
B.M.	2.54	949.70	3.15	946.16
B.M.			5.55	944.15

Top Mont. Dale and Harp. Ave.

78.37

3 pike in 10" Oak 50' Lt sta 17+35.

2 pike in T.P. 75' Lt sta 13+12

Top East Cor of Bottom step of House Lt sta 4+50

Top of Mont at Hex. Ave & Co Rd A½.

Sta	+	HI	−	Elev.	
BM	5.55	949.70 ✓		944.15 ✓	
0+00			5.5	944.2	
+16			6.3	944.4	
+50			5.0	944.7	
1+00			4.9	944.8	
+50			5.5	944.2	
2+00			6.1	943.6	
+50			6.2	943.5	
3+00			5.9	943.8	
+50			6.2	943.5	
4+00			6.5	943.2	
+50			6.3	943.4	
5+00			5.7	944.0	
BM.	4.33	950.41 ✓	3.52	946.18 ✓	946.18
+50			6.0	944.4	
6+00			5.7	944.7	
+50			5.2	945.2	
7+00			4.6	945.8	
+50			4.2	946.2	
8+00			3.0	947.4	
+50			2.2	948.2	
9+00			1.3	949.1	
T.P.	10.31	959.48 ✓	12.4	949.17 ✓	
+50			10.0	949.5	

Top Mont at Lex Ave 2nd Co Rd A"

Top East Cor of Bottom step of House Hotel 450

Sta	+	HI	−	Elev
		959.48 ✓		
10+00			9.7	949.8
+50			9.0	950.5
11+00			7.7	951.8
+50			5.6	953.9
12+00			2.9	956.6
+50			0.1	959.4
T.P.	11.30	970.43 ✓	0.35	959.13 ✓
13+00			8.1	962.3
+11			7.5	962.9
B.M.			7.15	963.28 = 963.26
+50			5.2	965.2
14+00			2.3	968.1
+50			0.5	969.9
T.P.	9.42	979.55 ✓	0.30	970.13 ✓
15+00			7.4	972.2
+50			5.0	974.6
16+00			3.2	976.4
B.M.	4.35	977.76 ✓	6.12	973.43 = 973.41
+50			3.3	974.5
17+00			5.0	972.8
+50			5.1	972.7
18+00			4.9	972.9
+09 ℄			4.8	973.0
B.M.			4.35	973.41

Spike in T.P. 75' Lt of Sta 13+13'

Spike in 16" Oak 50' Lt of Sta 17+35'

Spike in 16" Oak 50' Lt of Sta 17+35

2ft	+	HI	−	Elev.
B.M.	6.25	979.66		973.41
T.P.	1.55	977.86	3.35	976.31
T.P.	0.25	964.74	13.37	964.49
T.P.	0.19	952.03	12.90	951.84
T.P	0.63	942.04	10.62	941.41
T.P.	4.83	937.99	8.88	933.16
T.P.	1.65	936.53	3.11	934.88
T.P.	2.37	926.76	12.14	924.39
T.P.	2.43	920.78	8.41	918.35
T.P.	3.14	924.09	4.83	915.95
T.P.	4.35	926.10	2.34	921.75
T.P.	4.37	924.15	6.32	919.78
B.M.			5.18	918.97 = 918.93

H.L.W.

8/4/28
C.W.S.
D.P.T.
W.H. Rod.
H.T.

Spike in 16" Oak 50' Lt Sta 17+35

Top Mont Dale at 4 Larp. Ave

8/3/29.
C.W.S.
O.B.
H.T.
W.H.

X Section
Lexington Ave
To
Victoria Ave.

2+0	L	HI	-	1.5 L
0+00		& 20 x Ave.	9442	✓
+16			444	✓
+50			447	✓
1+00			448	✓
+50			442	✓
2+00			436	✓
+50			435	✓
3+00			438	✓
+50			435	✓
4+00			432	✓
+50			434	✓
5+00			440	✓

39/40	40/20	40	41/19	41/40									
40/40	40/20	40/13	38	40/13	41/26	43/40							
37/40	38/23	39/14	44/13	43/10	37/9	32/5	35	40/12	42/17	42/29	43/40		
32/40	42/20	42/13	47/12	46/11	40/9	34/5	34	39/11	41/16	40/34	41/40		
59/40	53/30	52/13	52/12	49/9	39/6	40	46/11	47/16	50/18	44/26	44/40		
59/40	53/30	49/17	57/15	57/13	50/17	41/7	42/6	40	51/11	54/15	53/22	25/40	
50/40	47/30	44/19	47/16	48/14	49/13	48/10	47/7	46	51/11	51/18	53/28	28/40	
49/40	45/19	46/15	57/14	51/12	42/7	43	50/12	51/16	51/21	52/40			
51/40	50/25	53/15	56/13	50/10	45/4	46	54/12	53/16	56/21	59/40			
55/40	55/27	57/17	58/12	47/5	49	55/14	57/20	57/40					
52/40	53/29	54/17	56/12	48/7	47	51/12	54/19	55/30	52/40				
49/40	47/21	49/15	49/14	41/13	40/11	41	44/9	44/14	48/19	47/30	49/40		

Sta	+	HI	-	Elev
5+50				44.4 ✓
6+00				44.7 ✓
+50				45.2 ✓
7+00				45.8 ✓
+50				46.2 ✓
8+00				47.4 ✓
+50				48.2 ✓
9+00				49.1 ✓
+50				49.5 ✓
10+00				49.8 ✓
+50				50.5 ✓
11+00				51.8 ✓

$\frac{45}{40}$ $\frac{43}{33}$ $\frac{41}{23}$ $\frac{38}{14}$ $\frac{43}{15}$ $\frac{41}{13}$ $\frac{37}{12}$ $\frac{36}{5}$ 3.8 $\frac{39}{9}$ $\frac{40}{16}$ $\frac{40}{28}$ $\frac{42}{40}$

$\frac{44}{40}$ $\frac{40}{28}$ $\frac{38}{16}$ $\frac{39}{15}$ $\frac{40}{14}$ $\frac{34}{12}$ $\frac{35}{5}$ 3.4 $\frac{34}{10}$ $\frac{32}{14}$ $\frac{39}{18}$ $\frac{34}{26}$ $\frac{34}{40}$

$\frac{36}{40}$ $\frac{34}{28}$ $\frac{34}{17}$ $\frac{38}{15}$ $\frac{35}{12}$ $\frac{36}{10}$ $\frac{27}{5}$ 2.8 $\frac{27}{9}$ $\frac{29}{16}$ $\frac{26}{30}$ $\frac{26}{40}$

$\frac{35}{40}$ $\frac{34}{38}$ $\frac{32}{27}$ $\frac{30}{10}$ $\frac{23}{5}$ 2.3 $\frac{23}{11}$ $\frac{23}{16}$ $\frac{25}{24}$ $\frac{25}{40}$

$\frac{118}{40}$ $\frac{116}{29}$ $\frac{116}{13}$ $\frac{107}{6}$ 10.7 $\frac{106}{10}$ $\frac{105}{15}$ $\frac{105}{30}$ $\frac{107}{40}$

$\frac{108}{40}$ $\frac{105}{23}$ $\frac{108}{11}$ $\frac{97}{8}$ $\frac{98}{6}$ 9.8 $\frac{97}{8}$ $\frac{98}{11}$ $\frac{96}{15}$ $\frac{91}{28}$ $\frac{88}{110}$

$\frac{99}{40}$ $\frac{98}{27}$ $\frac{98}{11}$ $\frac{93}{9}$ $\frac{88}{6}$ 8.8 $\frac{84}{7}$ $\frac{80}{16}$ $\frac{80}{32}$ $\frac{79}{40}$

$\frac{95}{40}$ $\frac{93}{28}$ $\frac{93}{12}$ $\frac{79}{6}$ 7.8 $\frac{77}{9}$ $\frac{74}{16}$ $\frac{72}{30}$ $\frac{69}{40}$

$\frac{88}{40}$ $\frac{86}{27}$ $\frac{87}{11}$ $\frac{73}{6}$ 7.4 $\frac{73}{8}$ $\frac{71}{17}$ $\frac{70}{34}$ $\frac{69}{40}$

$\frac{82}{40}$ $\frac{81}{29}$ $\frac{81}{13}$ $\frac{70}{7}$ 7.1 $\frac{68}{9}$ $\frac{69}{12}$ $\frac{68}{27}$ $\frac{658}{40}$

$\frac{78}{40}$ $\frac{75}{28}$ $\frac{72}{13}$ $\frac{69}{11}$ $\frac{64}{6}$ 6.4 $\frac{64}{7}$ $\frac{64}{14}$ $\frac{659}{29}$ $\frac{52}{40}$

$\frac{63}{40}$ $\frac{56}{28}$ $\frac{63}{14}$ $\frac{51}{7}$ 5.1 $\frac{53}{6}$ $\frac{54}{10}$ $\frac{51}{14}$ $\frac{53}{25}$ $\frac{45}{40}$

Sta	+	HI	−	Elev
11+50				9.53.9 ✓
12+00				56.6 ✓
+50				59.4 ✓
13+00				62.3 ✓
+11				62.9 ✓
+50				65.2 ✓
14+00				68.1 ✓
+50				69.9 ✓
15+00				72.2 ✓
+50				74.6 ✓
+60	+0.4			75.0 (76.8)
+85	+0.8			75.8 (75.6)

31/40	32/32	40/14	30/8	30	31/9	44/12	34/30	28/40	
107/40	108/27	116/12	105/6	107	108/7	118/10	122/13	125/15	116/17	112/35	110/40
80/40	80/29	89/12	77/6	78	79/9	95/11	103/15	93/19	91/40		
52/40	52/19	54/15	54/10	51/6	50	54/11	68/15	72/33	69/40		
41/40	43/24	43/13	44	44/9	48/14	42/15	41/33	42/40			
10/40	13/26	19/10	19/5	20	19/8	27/12	24/14	20/16	20/33	25/40	
104/40	103/29	100/14	109/6	109	110/10	114/13	102/16	111/34	112/40		
65/40	63/15	91/10	91/6	92	91/8	92/14	58/20	61/40			
85/40	90/17	111/11	120/6	120.00	120/10	119/15	65/22	75/40			
48/40	42/29	53/14	96/7	96	95/11	82/23	26/33	31/40			
43/40	39/29	92/23	86/13	89/7	92	92/10	86/20	23/31	30/40		
27/40	09/26	43/24	63/19	84/12	84	82/11	76/18	38/23	55/40		

Sta	+	H I	−	Elev
16+00				976.4 ✓
+50				74.5 ✓
17+00				72.8 ✓
		Sea 20° Curve		
+50				72.7 ✓
+76.5	+02			72.9 ✓
18+00				72.9 ✓
+09.5		& Victoria.		73.0 ✓
B.M.	4.29	777.70		773.41
+40				71.5
+70				71.3
19+00				72.7
+32				71.8
+48				69.9
+60				69.8

8/3/28

1.9 1.7 2.1 5.8 8.1 7.8 7.9 7.7 5.7 7.3
40 33 18 15 10 10 13 15 40

+08 00 07 1.8 3.1 3.3 3.3 3.6 4.8 5.1
40 29 26 12 9 6 10 25 40

3.1 4.3 5.3 5.1 5.0 5.2 5.7 5.8
40 24 14 8 8 21 40

4.6 6.0 6.4 5.8 5.1 5.3 6.0 6.1 6.1
40 30 17 11 5 16 31 40

5.9 5.9 6.2 5.5 4.9 5.1 5.5 5.7 5.5
40 31 18 15 6 15 29 40

6.0 5.6 5.3 4.9 4.8 5.0 4.7 4.7
40 30 22 12 16 31 40

5.6 5.2 5.0 4.9 4.2 4.5 4.5
40 32 22 16 33 40

SPR IN 16" DRN 50 LT. 5 7/8 17 7/35.
5.9 5.1 5.0 5.1 6.0 6.8 5.7 5.0
30 42 33 22 9 6.2 13 33 50

5.5 5.3 5.7 6.2 5.9 6.8 5.9 5.4
50 33 21 16 12 6.4 14 33 50

8.0 7.2 5.3 5.7 5.7 5.8 5.9 5.8
50 45 43 33 18 5.0 16 33 50

9.0 7.9 6.1 6.1 5.7 5.7 6.4 6.1 5.1 5.0 4.3 4.5 4.4 5.2 5.2
50 39 35 33 22 10 8 6 4 5.9 6 8 27 33 49 50

10.0 7.3 6.3 6.3 5.9 6.1 7.1 7.5 3.8 4.3 4.6
50 45 33 30 18 7 4 7.8 5 11 33 50

12.4 8.9 7.8 6.6 6.0 6.2 8.0 4.2 4.4 4.0
50 33 29 27 15 5 7.9 10 15 33 50

		777.70		
7 87				71.3
20 700				71.4
	712 CROSS DRAIN 12"X 30' C.M.			
	724			71.4
	750		6.2	71.5
21 700			5.7	72.0
B.M		4.29	773.41	

123

15.0/42 (2.3/33) 9.1/24 7.0/21 6.2/9 6.4 6.8/5 8.5/7 8.3/17 6.9/21 5.8/33 4.8/50

15.2/40 12.0/25 6.9/18 6.2/6 6.3 6.8/5 8.3/9 8.1/17 7.1/22 6.4/33 4.2/50

10.6/20 8.70/10

16.5/13 12.3/20 7.5/13 6.3 6.7/11 8.6/14 8.3/18 7.8/19 6.1/33 5.8/40

Topograph.

Co. Rd "A"

Lexington Ave.

To

Victoria Ave.

5+00

+67 @ F.E.E 12"X 23' V.R. Poor.

4+00

3+00

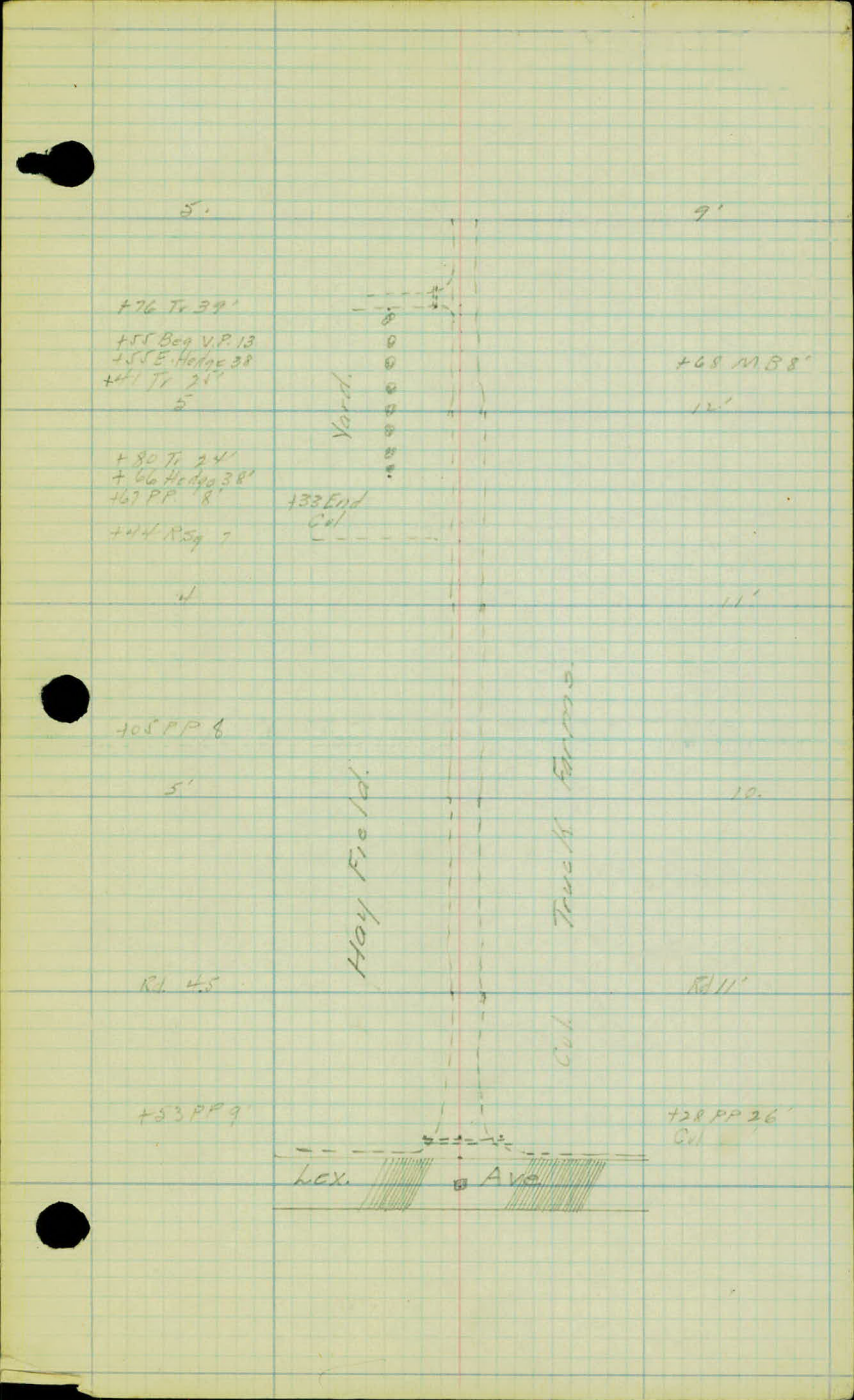
2+00

1+00

+22' X Drain 15"X 40' C.M. +22 Rt 19 Lt

+13' Edge Pav.

0+00


5'
9'
+76 Tr 39'
+55 Beg V.P. 13
+55 E. Hedge 38
+41 Tr 24'
5'
+80 Tr 34'
+66 Hedge 38'
467 PP 8'
+44 R Sq 7
W
+68 M 88'
12'
11'
Yard.
+33 End Cul
+05 PP 8
5'
10'
Hay Field
Truck Farm
Rd 45'
Rd 11'
Cul
+53 PP 9'
+38 PP 26'
Cul
Lucx.
A V8

10+00

9+00

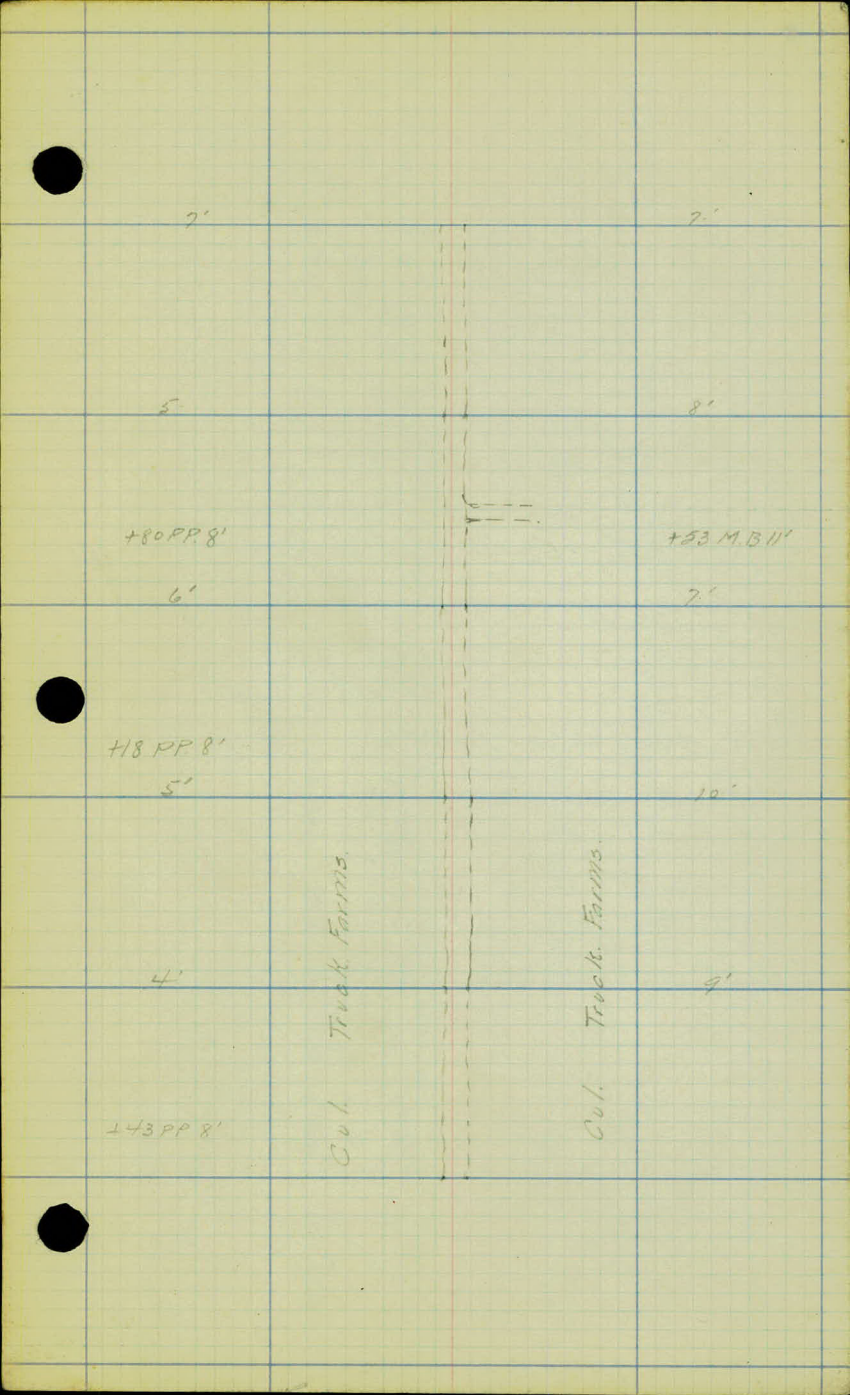
+48 FE Rt No Cob.

8+00

7+00

6+00

5+00


7'
7'
5'
8'
+80 PP 8'
+53 M.B 11'
6'
7'
+18 PP 8'
5'
10'
Cul. Truck Farms.
Cul. Truck Farms.
4'
9'
143 PP 8'

15+00

14+00

+27 Rd. Rt.

+07 & F E Lt. 10"X16" C.M. Poor.

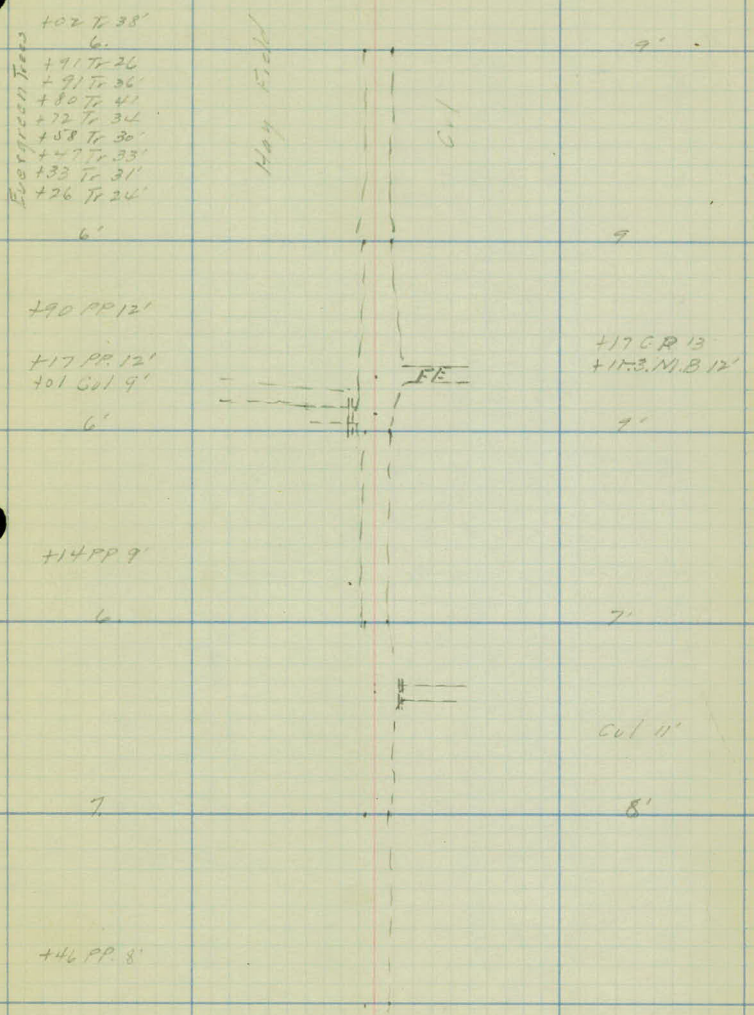
13+00

12+00

+65 F E Rt. 10"X12" M. Can be used

11+00

10+00


+02 Tr 38'
6.
9'
Existing Trees
+91 Tr 26'
+91 Tr 36'
+80 Tr 41'
+72 Tr 34'
+58 Tr 30'
+47 Tr 33'
+33 Tr 31'
+26 Tr 24'
6'
9'
+90 PP 12'
+17 PP 12'
+01 Col 9'
FE
+17 C.B 13
+11 S.M.B 12'
6'
9'
+14 PP 9'
6.
7'
Col 11'
7.
8'
+46 PP 8'

20

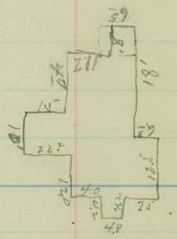
19

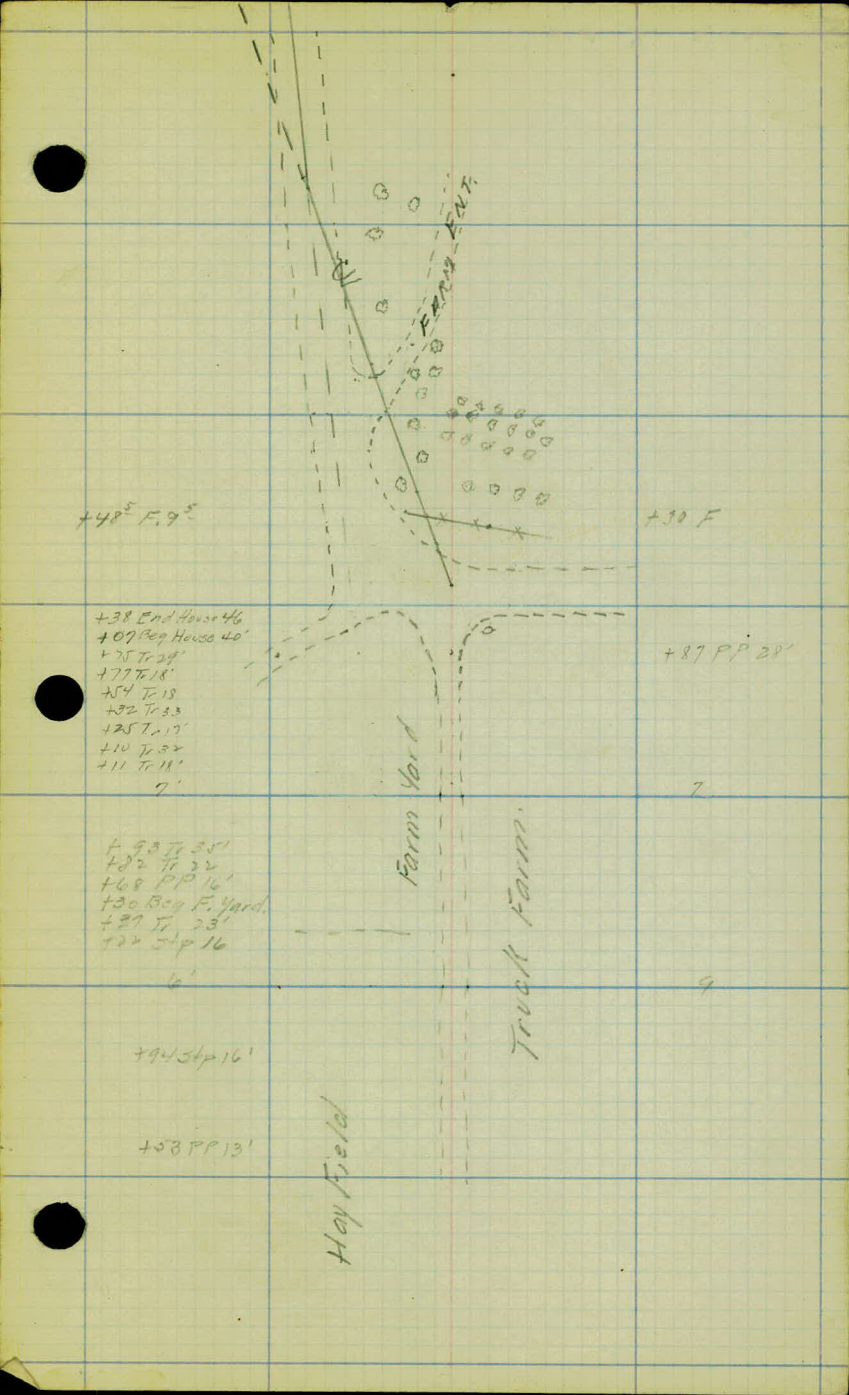
18+00

17+00

16+00

15+00



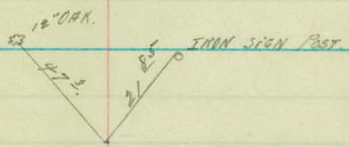

FENCE
+48 F. 9
+30 F
+38 End House 46
+69 Beg House 40'
+75 Tr 29'
+77 Tr 18'
+54 Tr 18
+32 Tr 33
+25 Tr 17'
+10 Tr 32
+11 Tr 11'
+87 P.P. 28'
Z
Z
+93 Tr 35'
+82 Tr 32
+68 P.P. 16'
+30 Beg F. Yard.
+29 Tr 23'
+24 Stp 16
6'
9
+94 Stp 16'
+98 P.P. 13'
Farm Yard
Truck Farm.
Hay Field

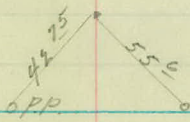
PROV. # 29-65

29 Couve

STA	POINT	Δ LT.	Δ RT.
20+24.4	P.I.		
3+08.48	P.O.T. =		
2+75.86	P.T.	40°-00	
+50		36°-15	
2+00		29°-00	
1+67.57	P.I.		Δ - 80°-00
+50		21°-45	D - 29°-R.
1+00		14°-30	T. - 167.57
+50		7°-15	L - 275.86
0+00	P.C.	0°-00	R. - 197.20

2-25-29





Proj # 29-65.

B.M.	6.32	977.73		973.41	
-2+00				3.1	
-1+50				3.3	
-1+00				3.9	
-0+50				4.4	
0+00				4.9	74.8
0+50				6.1	73.6
		977.83		973.41	
	4.42	984.15	6.32	977.73	
1+00				6.6	71.2
1+50				6.5	71.3
2+00				5.6	72.2
2+50				6.2	71.6
2+75.86				6.4	71.4
			4.42	977.73	
				973.41	

2-25-29

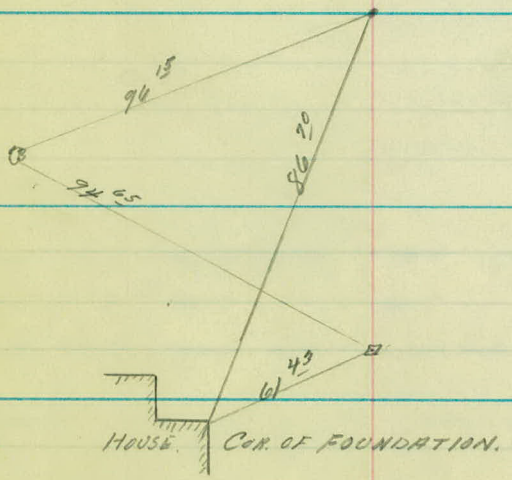
6.0	5.8	5.3				5.1	6.3	5.5	3.2	2.2	1.5
50	14	7	4.9			11	21	31	33	38	50
7.4	6.3	7.2	6.2	5.9		6.5	6.4	3.7	3.3		
50	37	23	14	7	6.1	8	22	29	50		
4.8	4.9	4.8	5.2	5.4	6.2	5.5	5.0	4.6	4.5		
50	39	30	21	14	11	6.6	15	26	43	50	
5.3	5.4	5.4	5.9	6.1	6.3	6.4	6.2	6.0			
50	43	33	23	16	8	6.5	18	33	50		
8.9	8.7	8.5	6.3	5.9	5.7	5.9	5.1	4.7	5.3		
50	43	37	27	23	15	5	5.6	11	30	50	
17.6	15.6	13.2	10.7	9.0	7.0	6.4	6.9	8.5	8.9	5.7	4.6	4.7
50	40	35	25	19	14	10	6.2	11	18	21	26	41	50
19.5	13.5	11.9	7.0				7.1	8.8	7.0	5.9	5.1
50	28	22	12			6.4	12	19	29	41	50

PROJ. # 29-65

20° CURVE TO THE LEFT

AT END OF PROJ.

STA	POINT	Δ Lt.	Δ Rt.
17+61.65			
18+90.0	P.T. =	16°-45'	0.17
+50		12°-45'	
18+09.15	P.I.		Δ - 33°-30
18+00		7°-45'	D - 20°-Lt.
+50		2°-45'	T. - 86.65
17+22.50	P.C.	0°-00'	0.13 L - 167.50
			R - 287.94
17+76.15	P.O.T.		


96 15
86 20
94 45
43
61
HOUSE.
COR. OF FOUNDATION.

Proj. # 29-65

X SECTIONS ON 20° CURVE

B.M. 17+50	4.98	978.39 ✓		973.41	972.7
18+00					72.8
18+50					71.6
18+90					72.4
			4.98	973.41 ✓	

5.0	5.7	6.8	6.7		5.8	6.2	6.6	6.8
50	35	26	16	5.7	12	16	38	50

6.5	6.2	6.0		5.3	5.3	
50	38	15	5.6	25	50	

6.0	5.9	5.8	6.4		7.0	6.9	6.7	6.6
50	39	22	8	6.8	14	28	39	50

9.0	8.8	6.7	6.5	6.2		5.7	6.0	6.0	5.8
50	42	31	23	12	6.0	15	25	40	50

Proj #29-65

54° CURVE RT.

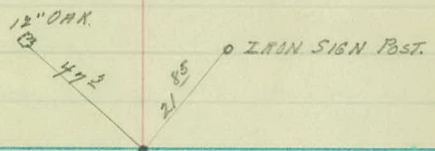
STA	POINT	Δ Lt.	Δ Rt.

.45

$2+35\frac{29}{}$	P.T.	$40°-00'$	
$2+00$		$34°-00'$	$29°45'$
$+50$		$25°-30'$	
$1+43\frac{5}{}$	P.I.		$\Delta - 80°-00'$
$1+00$		$17°-00'$	$D - 34°-R.$
$+50$		$8°-30'$	$T - 143\frac{50}{}$
$0+00$	P.C.	$0°-00'$	$L - 235\frac{29}{}$
			$R - 171\frac{02}{}$

.55

107.57
143.50
44.07



PROJ # 29-65

X SECTIONS ON 34° CURVE.

B.M.	4.99	978.40 ✓	973.41	
-1+00			2.9	975.5
-0+50			3.4	74.0
0+00			4.0	74.4
0+50				73.2
1+00				71.4
1+50				72.4
1+75				72.0
2+00				71.9
2+35.22				71.6
2+50			6.9	71.5
3+00			7.0	71.4
3+50			6.6 ✓	71.8
		4.99	973.41	

LEFT

5.1	5.2	5.0	4.1			
50	19	15	8	4.0		
6.0	5.8	4.9	5.1			
50	23	19	7	5.2		
6.0	5.9	5.6	6.4	6.5	7.0	
50	42	28	17	10	6	7.0
8.0	7.6	6.3	6.0	6.2	6.2	
50	42	38	28	17	6	6.0
8.1	8.1	8.8	7.5	6.7	6.3	
50	45	34	27	22	9	6.4
9.0	8.5	9.3	7.1	6.5		
50	37	26	18	7	6.5	
16.0	14.0	10.8	7.4			
50	35	20	12	6.8		

RIGHT

4.2	4.8	5.4	5.0	1.9	1.0	0.7
9	16	23	27	33	40	50
5.2	6.4	6.2	4.8	3.8	3.5	
6	11	20	25	30	50	
7.0	6.2	6.4	6.5			
10	23	40	50			
6.6	6.4	6.7				
18	33	50				
5.6	5.5	5.8	5.8			
17	28	38	50			
7.1	6.2	5.1	5.3	5.5		
12	22	27	38	50		
7.6	9.2	9.1	6.0	5.1	5.0	
13	17	21	29	44	50	

29-65 3-18-29

O.R.Y.K.
W.S.M.

Remove and replace 12"X30' C.M. at Tomers Drive
Place 24" culv. at 2+40 on curve. 44'
Gr. 15 Tr. on curve.
Cl. 4 Tr. Gr. 8 Tr. 15+50 to 17+50
Remove + replace on Lt. 13+27
P. -15"X30' C.M. on Lt. 13+27
P. 15" X24' C.M. on Rt. 9+48
4+67 - Remove - P. 15" X 24' C.M.
0+22 - Remove + replace.

U2517