

PLAN SURVEY.  
OF

# COUNTY ROAD 'F'

From S.T.H. No. ~~8~~<sup>8</sup> to S.T.H. No ~~10~~<sup>10</sup> -

PROJ. NO. 29-17

PROJ # 29-17

ALIGNMENT FROM S.T.H. # 63

TO S.T.H. # 62.

Office of Ramsey Co. Engineer  
ST. PAUL, MINN.

Date Filed .....

File No. ....

STA. POINT  $\Delta$  LT.  $\Delta$  RT.

18+65<sup>52</sup> P.T. 4°-22<sup>5</sup> ✓

18 3°-43

+50 3°-13

17 2°-43

+50 2°-13

16+47<sup>0</sup> P.I.  $\Delta$ -8°-45

16 1°-43

D-2° L.

+50 1°-13

T-219<sup>18</sup> ✓

15 0°-43

L-439<sup>5</sup> ✓

+50 0°-13

R-2864.9.3 ✓

14+27<sup>88</sup> P.O. 0°-00 ✓

13+18<sup>48</sup> P.O.T.

0+00

78°-45'

69.20

70.20

48.53

12" OAK

51.35

12" OAK

57.0  
11

WILLOW

52

20

STONE MONT.

50

35.02

WILLOW

STONE MT.

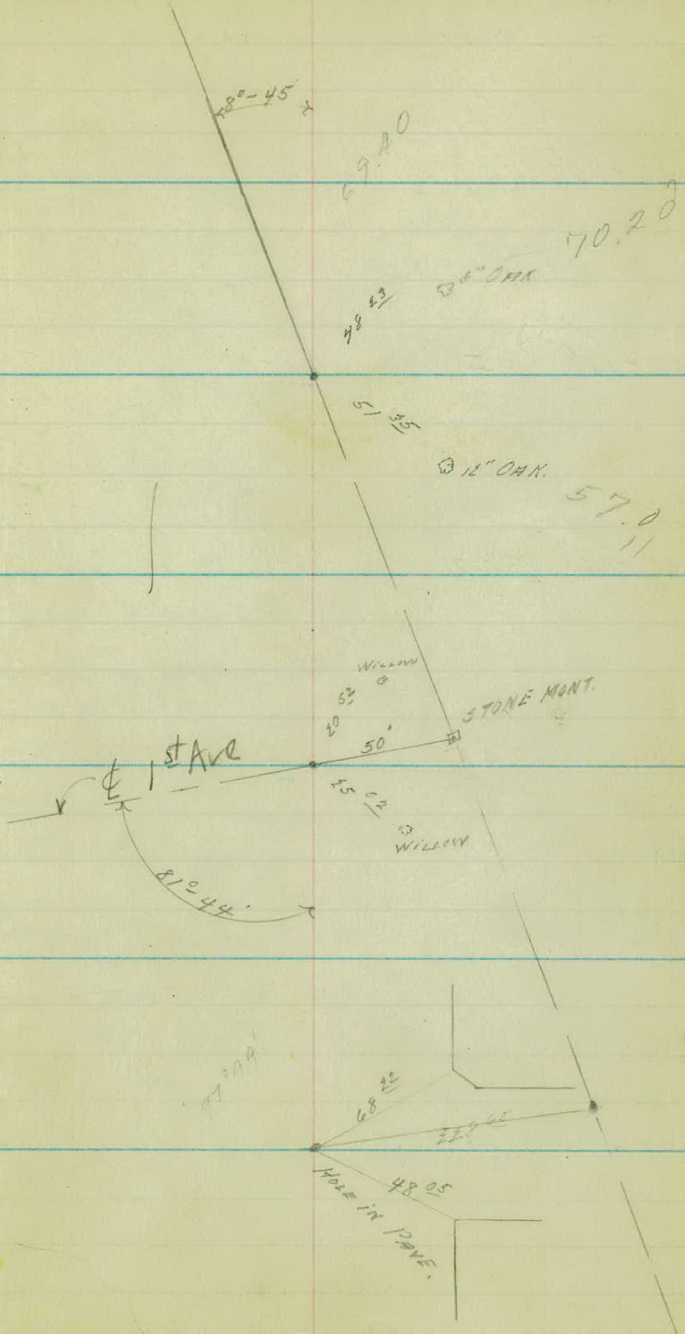
81°-44'

77.94

68.22

22.46

HOLE IN PAVE.  
48.05



STA POINT  $\Delta$  LT.  $\Delta$  RT.

42+76<sup>5</sup> P.O.T.

39+61<sup>25</sup> P.I.

1°-06'

38+66<sup>8</sup> P.O.T.

29+55<sup>75</sup> P.O.T.

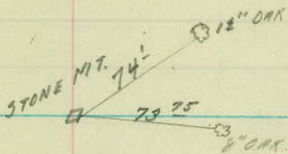
28+20<sup>95</sup> P.O.T.

25+73<sup>0</sup> P.O.T.

50

77

NAIL IN TWING.



STA POINT Δ LT. Δ RT.

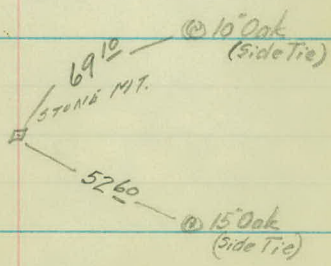
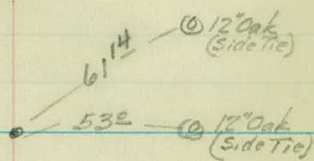
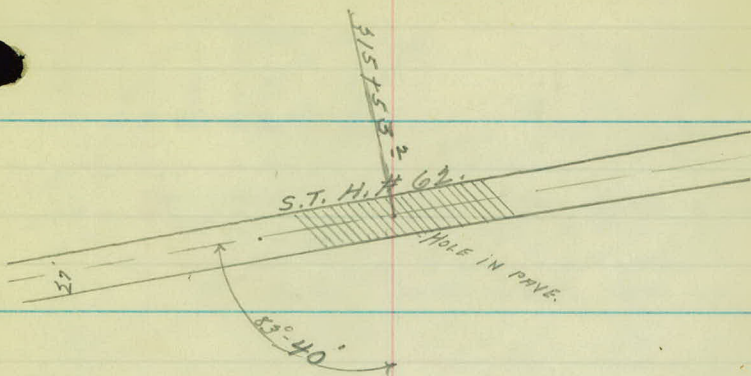
61+51<sup>3</sup>

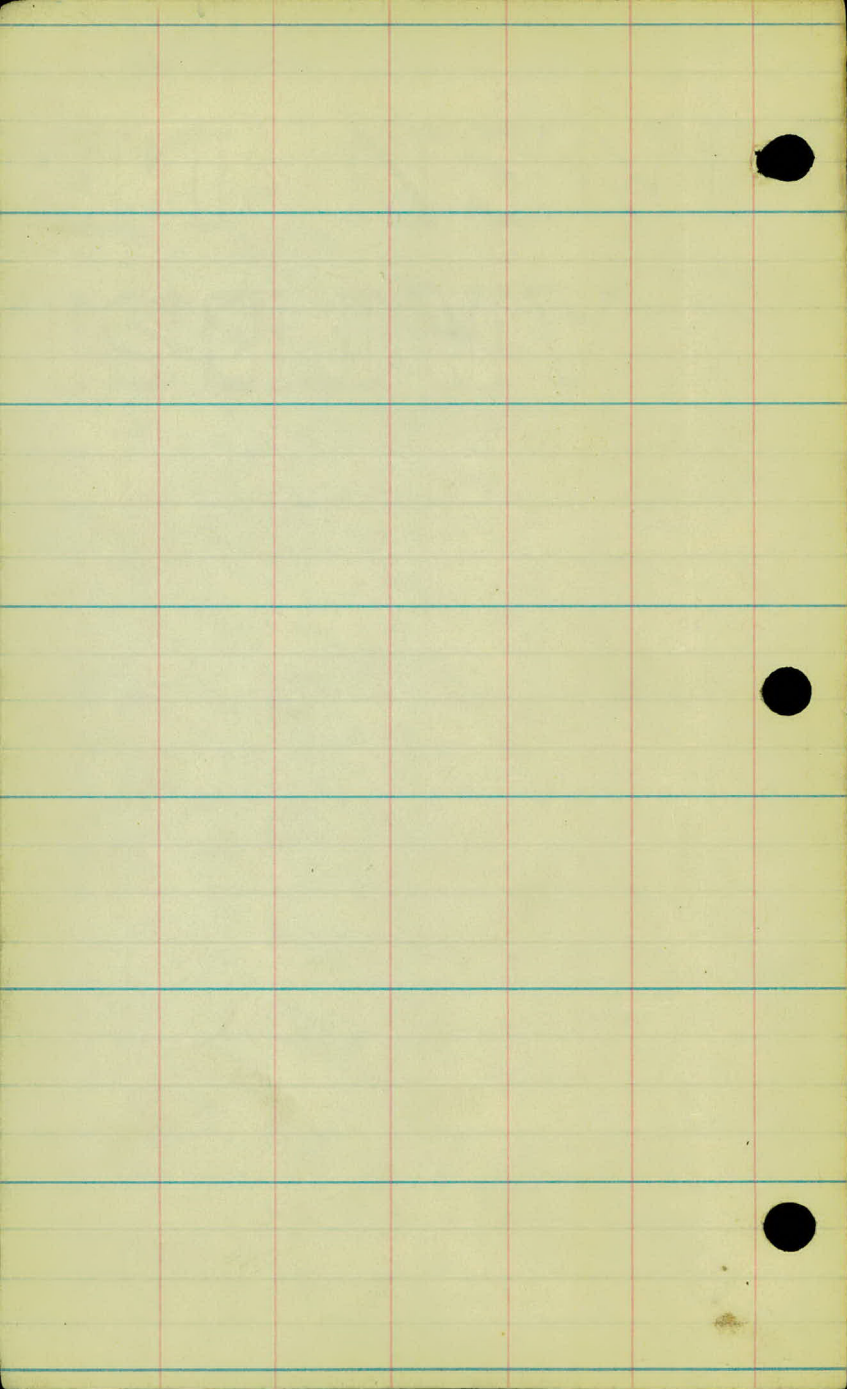
See curve notes

59+29<sup>8</sup> P.O.T.

53+90<sup>2</sup> P.O.T.

52+93<sup>0</sup> P.O.T.





PROJ # 29-17

ART. TOPOG. FROM  
STA 0+00 TO STA. 61+51.

4

3

2

1

0+00

20

Q. ROAD 2

+781 X F. 33

+761 X DRAIN 24  
24" X 44" VIT.

F. 31

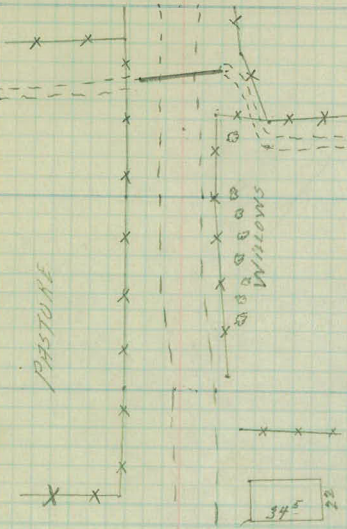
F. 31

+44 F. COR 32

+99 Out House 7  
5' X 10'

+97 Out Shack 7  
+65 Out Shack 7  
6' X 32'  
+32 T.P. 27  
+26 Hyd 21

-23 PAVE 30  
-33 PAVE 19  
-53 PAVE 19  
-53 PAVE 4



+75 F. 30  
+66 X DRAIN 19

+42 F. COR 18  
+39 F. 45  
+25 DITCH 46

Q. ROAD 1  
F. 18

+36 BFG F. 23  
Q. ROAD 2  
+94 ENT.  
+50 X F. 31

+64-12'-7"-29  
+54 BARN 35

+32 BARN 38

+23 BLDG 36

+40 BLDG 38  
+13 PAVE 32

-25 CURB 30

-53 CURB 30

97.44  
81.41  
178.85

10

9

8

7

6

5

4

F. 18

Q ROAD 1

HAY MEADOW

HAY MEADOW

+65 F.E.

Q ROAD 1

+97 F. 18

+87 FIELD ENT

+85 F. 33

F. 36

CULTIVATED

+99 F. COR 30

Q ROAD 1

YARD

+64 F. COR 32

F. 35

CULTIVATED

CULTIVATED

Q ROAD 3

Q ROAD

+60 Q ROAD

F. 34  
Q ROAD 1

CULTIVATED

CULTIVATED

+90 END F. 21

F. 20

+94-1 1/2"-T-21

+49 F. 21

+49-2 1/2"-T-21

16

15

14

13

12

11

10

F. 29

+50 F. 31

F. 32

+53 F. Cor 34

Road 20

112 X F. 22  
F. 22  
R. ROAD 4

R. ROAD 4

F. 16

CULTIVATED

WOODS

+52 F. 2

F. 36

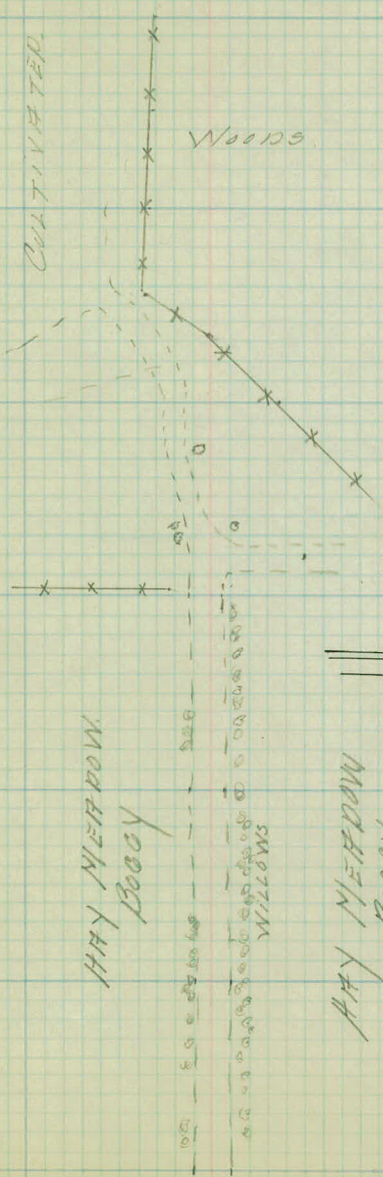
118 F. TRAIL

HAY MEADOW  
Booby

WILLOWS

HAY MEADOW  
Booby

R. ROAD 1



22

21

20

19

18

17

14

F. 7  
& PITCH 00

F. 9

F. 10

F. 11

F. 13  
+ 90 X F.

+ 50 F. 14

F. 21

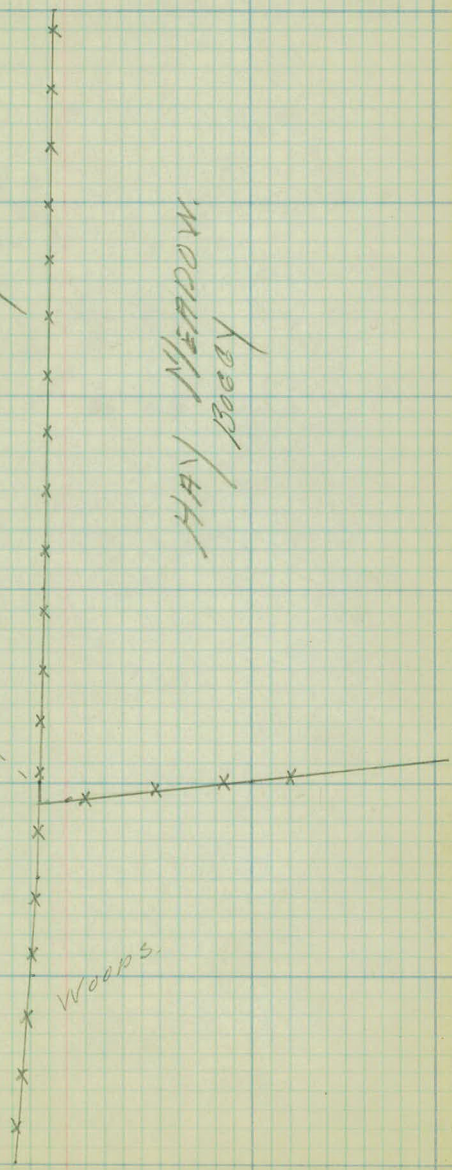
+ 50 F. 24

HAY MEADOW  
BOCCY

HAY MEADOW  
BOCCY

CULTIVATED.

Woods.



28

27

26

25

24

23

22

F.5

F.5

F.6

F.4

F.4

F.4

HAY FIELD.

HAY FIELD.

TREES & BRUSH.

MEADOW

HAY

Boggy  
HAY MEADOW

Boggy

Boggy

+23 DITCH 102

+00 DITCH 69

+00 DITCH 50

5' WIDE.

+00 DITCH 14  
+00 DITCH 130

8' WIDE

+52 & Ditch.  
+27 DITCH 54



34

33

32

31

30

29

28



40

7

39

38

37

36

35

34

F. 2

+ 22 X. F.

F. 1

F. 4

WOODS

HAY FIELD.

WASTE LAND.

+ 31 DITCH 6

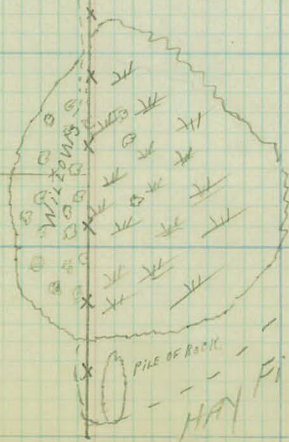
F. 3  
DITCH 5

+ 32 X. F.

F. 4

HAY FIELD

HAY FIELD.



46

45

44

43

42

41

40

SW AMP.

WILLOWS.

FI

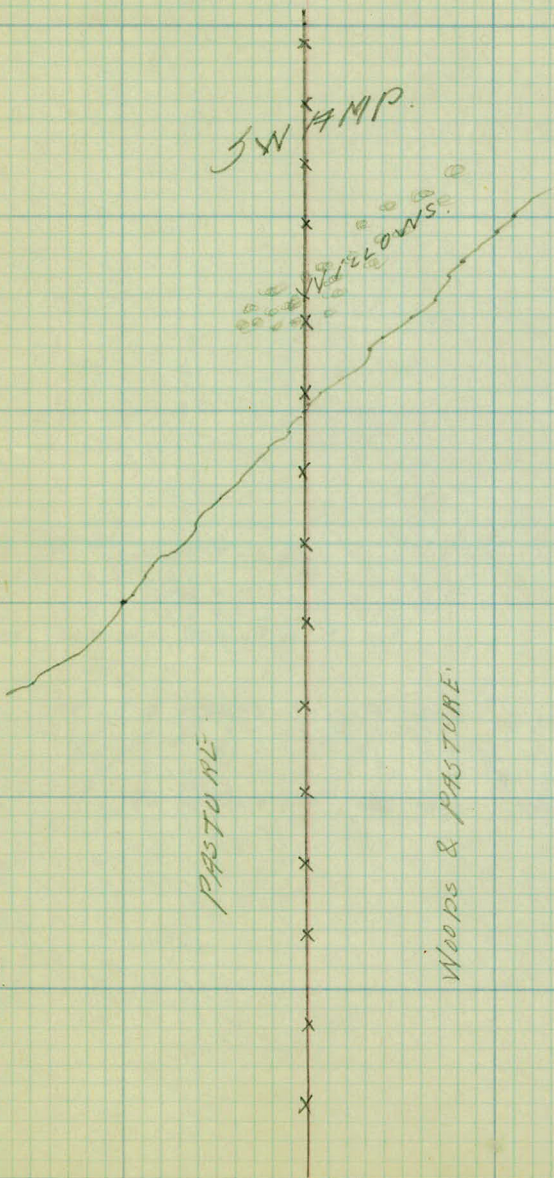
FI

FI

F. P.

PASTURE

WOODS & PASTURE



52

51

50

49

48

47

46

11-22-28

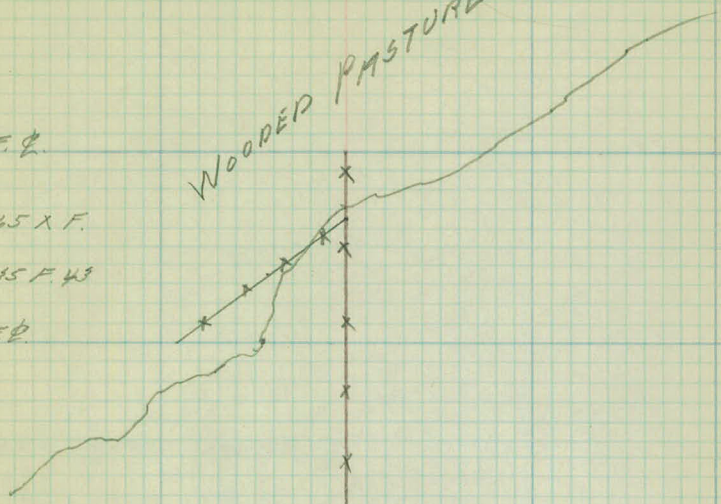
WOODED PASTURE

F. Q.

165 X F.

135 F. 43

F. Q.



SWAMP

58

57

56

55

54

53

52



F. 5

F. 4

F. 2

WOODEN POSTURE

WOODEN POSTURE

F. 5

F. 5

F. 5

64

63

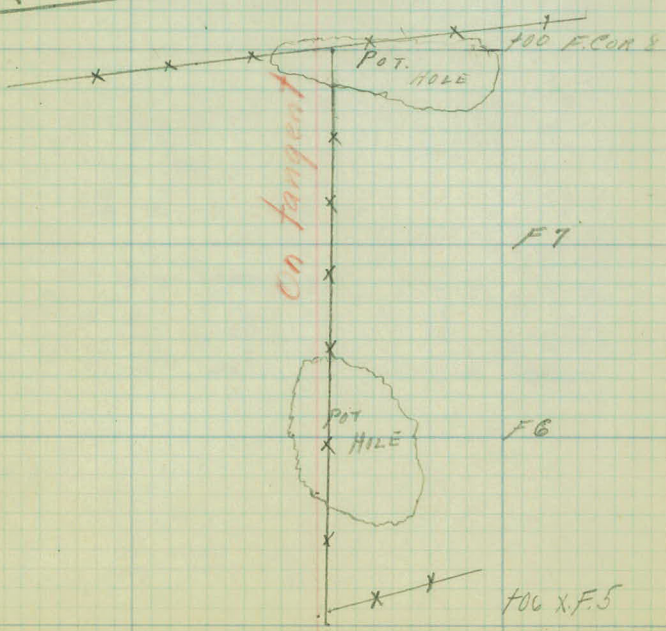
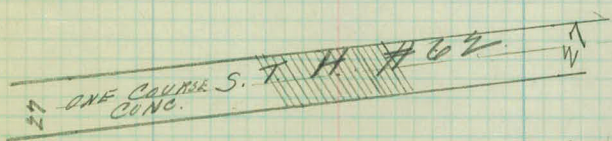
62

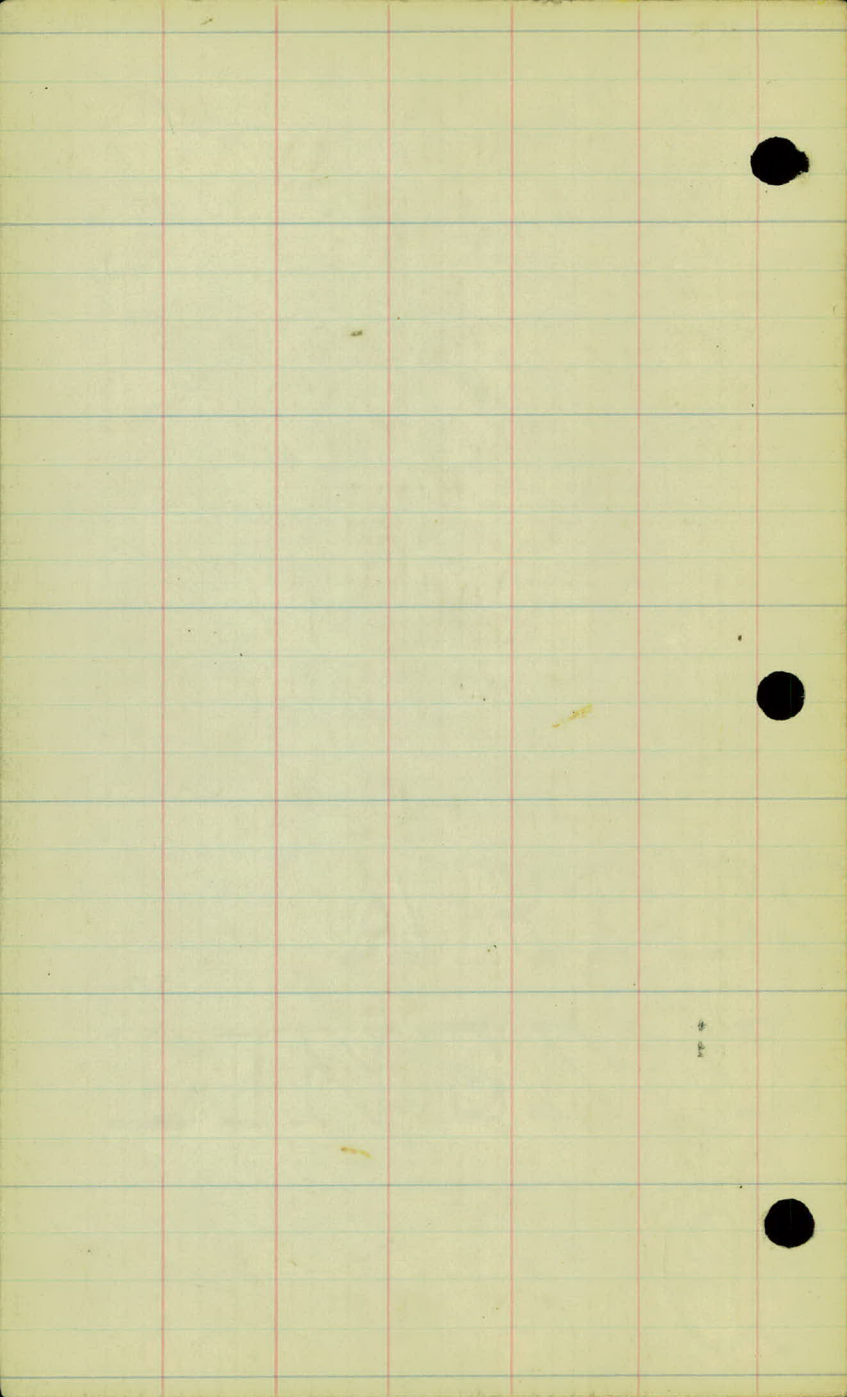
61

60

59

58





PROJ # 29-17

"B" LINE

ALIGNMENT FROM STA. 39+87  
TO S.T.H. # 62.

Office of Ramsey Co. Engineer  
ST. PAUL, MINN.

Date Filed .....

File No. ....

STA. POINT Δ LT. Δ RT.

52+69<sup>86</sup> P.T. ✓ 22°-27'

52 21°-13'

51 19°-28'

50 17°-43'

49 15°-58'

48 14°-13'

47 12°-28'

46+63<sup>51</sup> P.I. ✓

46 10°-43'

45 8°-58'

44 7°-13'

43 5°-28'

42 3°-43'

41 1°-58'

40 0°-13'

39+87<sup>0</sup> P.C. ✓

0°-00'

Δ-44°-54

D-3°-30 N.

T-676<sup>51</sup> ✓

L-1282<sup>86</sup> ✓

R-1637<sup>28</sup> ✓

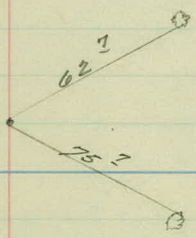
39+61<sup>25</sup> P.I.

1°-06'

12-5-28



□ 2' x 4' HUR



□ STONE MONT

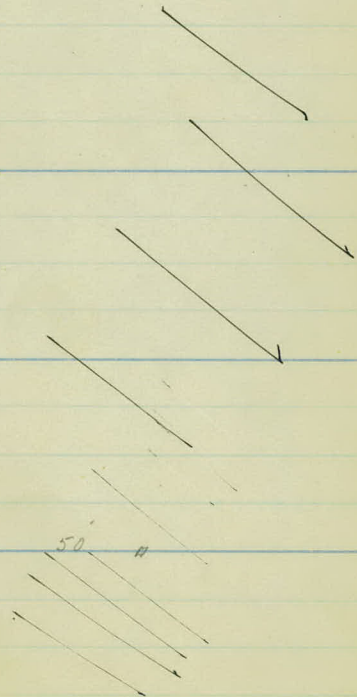
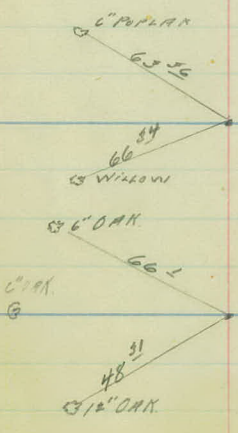
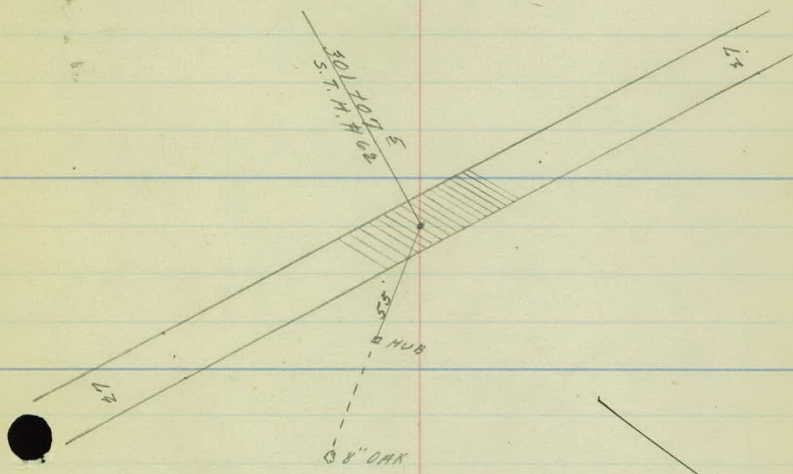
STM POINT ALT. Δ HT.

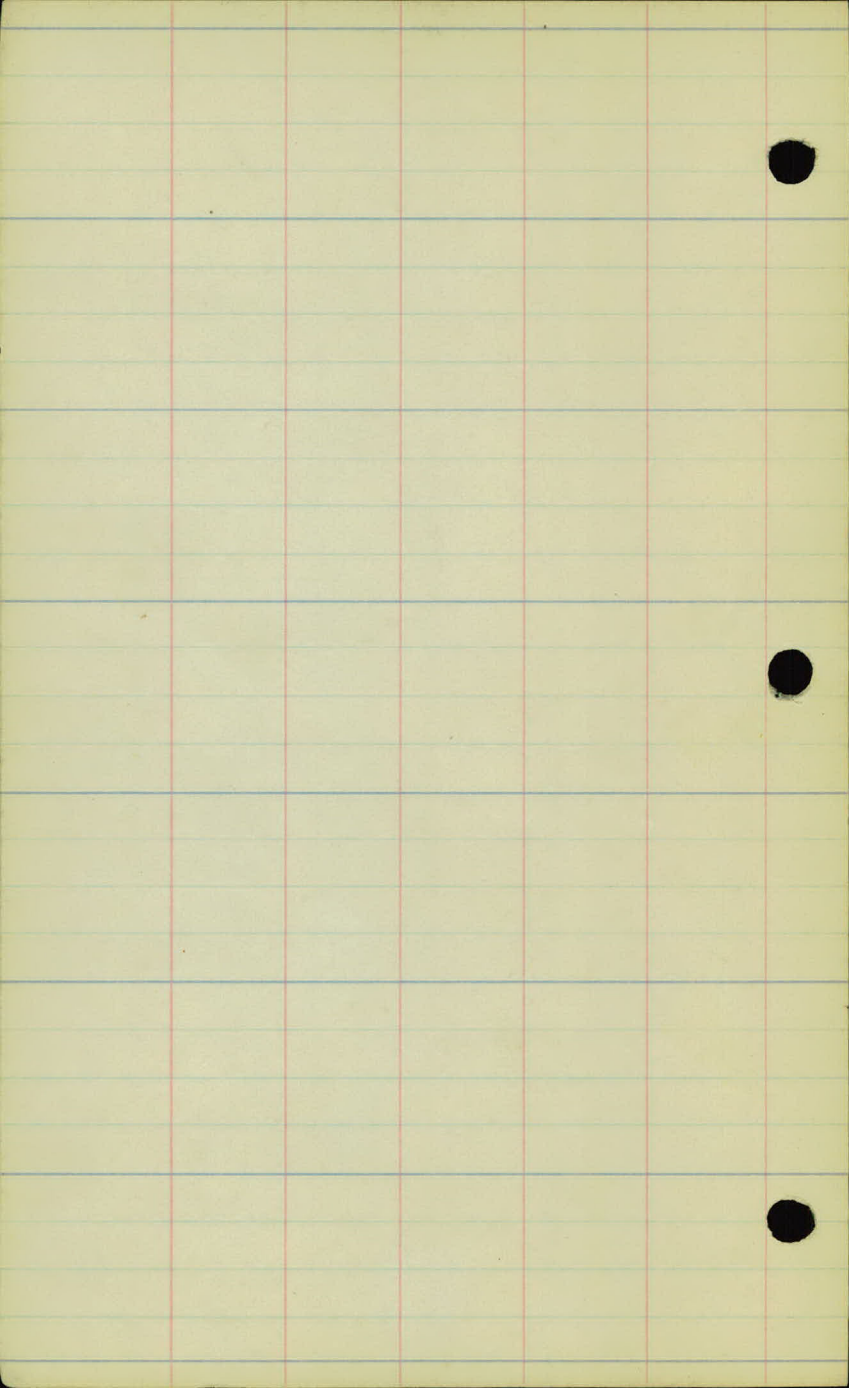
68+06 <sup>88</sup>	P.T. ✓	31°-50	
68		✓ 31°-01	
+50		✓ 27°-31	
67		✓ 24°-01	
+50		✓ 20°-31	
66+08 <sup>3</sup>	P.I. ✓		Δ-63°-00
66		✓ 17°-01	D-14° N ✓
+50		✓ 15°-31	T-251 <sup>42</sup> ✓
65		✓ 10°-01	L-450 <sup>00</sup> ✓
+50		✓ 6°-31	N-410 <sup>28</sup> ✓
64		✓ 3°-01	
63+56 <sup>88</sup>	P.C. ✓	0°-00	

61+47<sup>75</sup> P.O.T.

56+89<sup>48</sup> P.O.T.

100.00  
 56.88  
 43.12  
 43.50





PROJ # 29-17

"B" LINE

AKT TOPOG FROM 5717.39+87  
TO S.T.H. # 62

43

42

41

40

39

38

11-30-28

F. 32

F. 14

F. 4

PASTURE

WOODED PASTURE



49

48

47

46

45

44

43

SWAMP 80

+45 SWAMP 96

+15 SWAMP 25

SWAMP 10

+75 SWAMP 6

SWAMP 30

+50 SWAMP 17

+00 SWAMP 10

+85 SWAMP 6

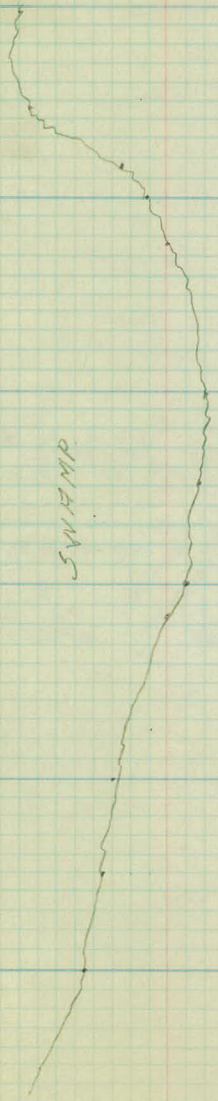
+00 SWAMP 30

+50 SWAMP 25

+00 SWAMP 45

SWAMP

WOODED PASTURE



55

54

53

52

51

50

49

⊕

WOODED PASTURE

⊕

TIMBER LINE

PASTURE & STUMPS

+90 SWAMP 98

⊕

+75 SWAMP 170

+35 SWAMP 32

+50 SWAMP 2

+50 SWAMP 115 Ft  
15' Wide

SWAMP

+100 SWAMP 100

⊕

+50 SWAMP 75

WOODED PASTURE

+10 SWAMP 32

+65 SWAMP 0

+30 SWAMP 65

⊕

61

60

59

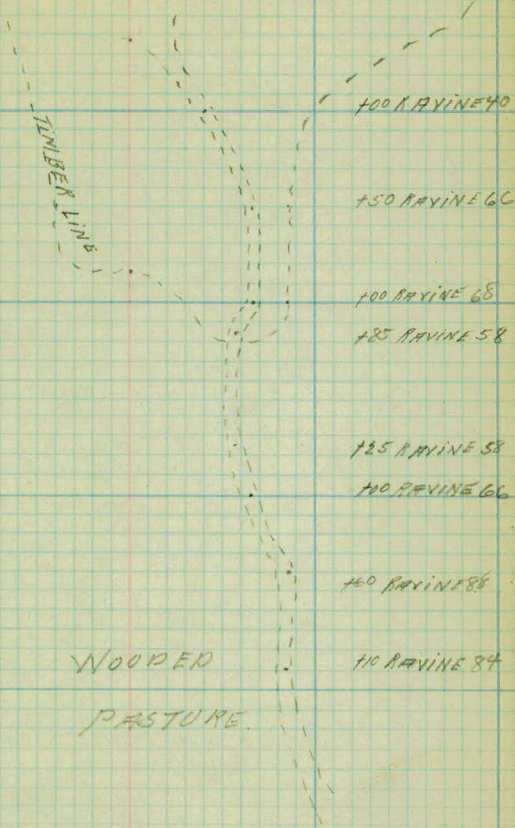
58

57

56

55

11-30-28



TIMBER LINE

400 RAVINE 40

450 RAVINE 66

400 RAVINE 68

425 RAVINE 58

425 RAVINE 58

440 RAVINE 66

460 RAVINE 88

WOODED

410 RAVINE 84

PASTURE

68

67

66

30" x 60" 1/2"

65

64

63

62

61

P.T. F. 70

WOODED PASTURE

+50 F. 60

SWAMP 24  
F. 60

+50 F. 49  
+50 SWAMP 8

F. 27

+49 F. 8

SWAMP 6

+30 SWAMP 6

+00 DITCH 10  
+00 SWAMP 13

+54 X. DRAIN 50  
30 X 60 P.S.  
+51 SWAMP 5

+04 F. 34

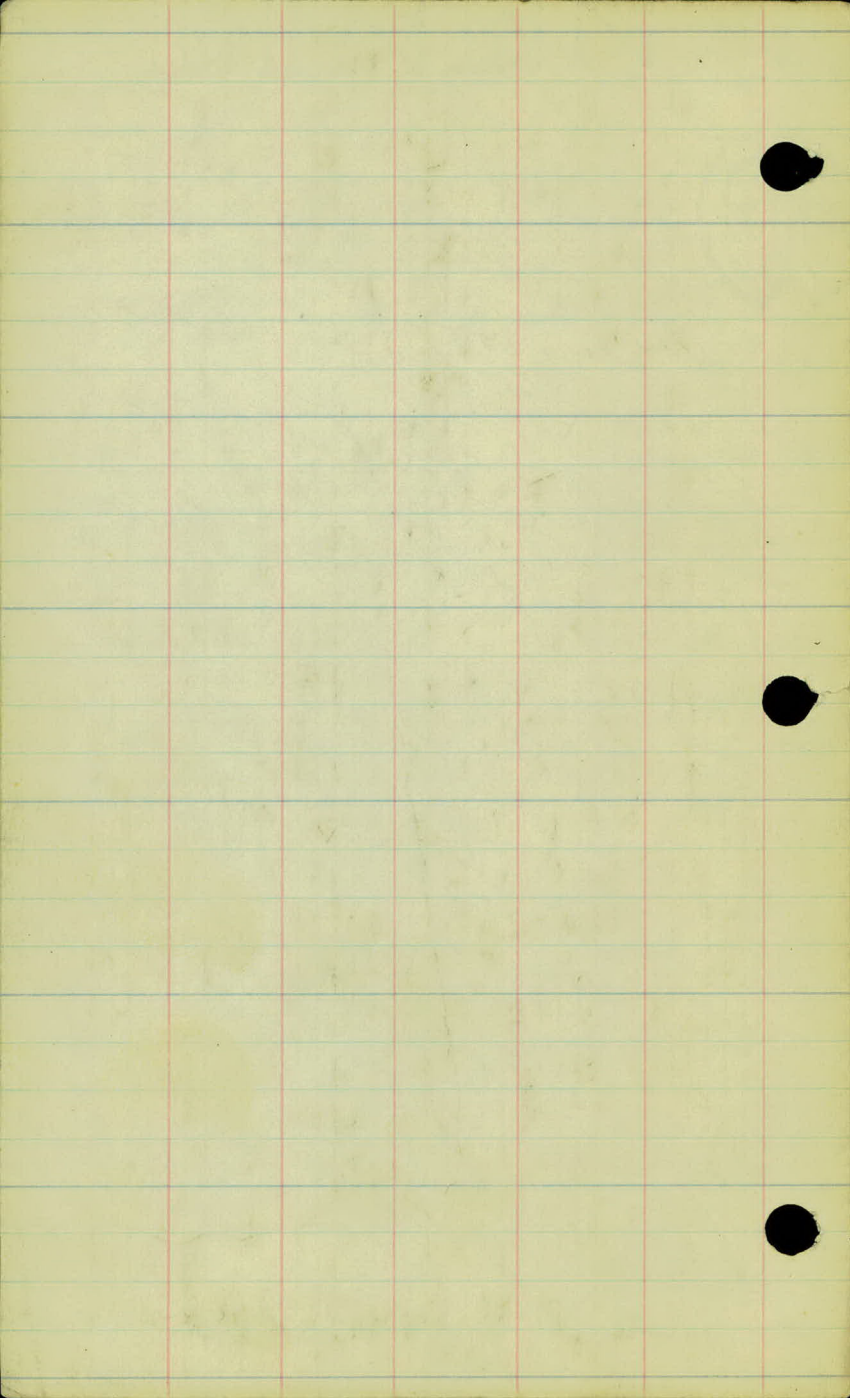
+50 SWAMP 8  
+50 F. 43

F. 55  
SWAMP 12

SWAMP

WOODED PASTURE  
TIMBER LINE





PROJ # 28-17

CENTER LINE LEVELS & CROSS SECTIONS  
FROM S.T.H. # 63 TO S.T.H. # 62.

B.M. 4.09 889.20 ✓ 885.11 ✓ Elev  
0+00 884.40

+13<sup>5</sup> 884.20

+25 882.90

+40 882.00

+83 882.60

1.73 885.33 ✓ 6.80 882.40 ✓

1+00 882.93

+50 882.63

2+00 879.03

+50 880.93

3+00 879.93

+50 879.63

4+00 879.33

+50 879.33

TOP OF CONC. WALK 30 FT. STA. 0783

$\frac{8.17}{200}$	$\frac{7.21}{150}$	$\frac{6.27}{100}$	$\frac{5.47}{50}$		$\frac{4.50}{50}$	$\frac{4.15}{100}$	$\frac{4.26}{150}$	$\frac{4.52}{200}$
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$\frac{5.60}{50}$		$\frac{5.00}{50}$		$\frac{4.56}{50}$
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$\frac{7.4}{50}$	$\frac{5.4}{41}$	$\frac{5.4}{22}$	$\frac{5.8}{14}$		$\frac{4.80}{50}$
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$\frac{14.8}{50}$	$\frac{14.7}{46}$	$\frac{13.5}{43}$	$\frac{10}{23}$	$\frac{6.4}{50}$		$\frac{6.0}{12}$	$\frac{5.2}{28}$	$\frac{4.2}{38}$
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TOP OF WALK

$\frac{12.4}{50}$	$\frac{16.1}{36}$	$\frac{7.6}{19}$	$\frac{7.2}{16}$		$\frac{6.5}{10}$	$\frac{5.4}{30}$	$\frac{4.1}{30}$	$\frac{4.1}{38}$
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TOP OF WALK.

$\frac{13.3}{50}$	$\frac{12.1}{35}$	$\frac{10.3}{29}$	$\frac{3.7}{19}$	$\frac{3.0}{15}$	$\frac{2.4}{2.4}$	$\frac{2.7}{11}$	$\frac{2.6}{23}$	$\frac{2.3}{33}$	$\frac{1.5}{44}$	$\frac{1.3}{50}$
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$\frac{12.8}{50}$	$\frac{11.2}{34}$	$\frac{7.7}{31}$	$\frac{8.7}{26}$	$\frac{5.7}{17}$	$\frac{2.6}{10}$	$\frac{2.0}{8}$	$\frac{2.7}{2.7}$	$\frac{3.5}{10}$	$\frac{3.0}{17}$	$\frac{2.5}{23}$	$\frac{2.5}{36}$	BARR.
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$\frac{12.0}{50}$	$\frac{7.7}{34}$	$\frac{8.8}{29}$	$\frac{4.7}{16}$	$\frac{3.1}{10}$	$\frac{3.7}{6}$	$\frac{3.3}{3.3}$	$\frac{4.1}{4}$	$\frac{3.2}{15}$	$\frac{3.4}{18}$	$\frac{2.5}{27}$	$\frac{2.4}{50}$
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$\frac{7.8}{50}$	$\frac{8.4}{31}$	$\frac{4.2}{8}$	$\frac{4.3}{5}$		$\frac{4.7}{44}$	$\frac{4.5}{5}$	$\frac{5.2}{13}$	$\frac{4.6}{18}$	$\frac{4.9}{36}$	$\frac{4.9}{50}$
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$\frac{8.7}{50}$	$\frac{7.5}{29}$	$\frac{5.2}{14}$	$\frac{4.8}{5}$		$\frac{5.2}{5.4}$	$\frac{8.4}{9}$	$\frac{7.6}{20}$	$\frac{7.6}{30}$	$\frac{7.6}{50}$
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$\frac{12.5}{50}$	$\frac{13.2}{30}$	$\frac{11.2}{22}$	$\frac{6.4}{13}$	$\frac{5.5}{5}$	$\frac{5.7}{5.7}$	$\frac{5.9}{7}$	$\frac{13.4}{28}$	$\frac{14.6}{29}$	$\frac{14.6}{31}$	$\frac{12.1}{38}$	$\frac{11.1}{50}$
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$\frac{14.3}{50}$	$\frac{13.9}{38}$	$\frac{14.3}{34}$	$\frac{13.6}{29}$	$\frac{6.7}{13}$	$\frac{5.6}{7}$	$\frac{6.5}{5}$	$\frac{6.0}{6.0}$	$\frac{5.6}{6}$	$\frac{9.9}{17}$	$\frac{11.5}{27}$	$\frac{11.7}{33}$	$\frac{11.0}{50}$
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$\frac{14.0}{50}$	$\frac{13.3}{39}$	$\frac{12.0}{25}$	$\frac{6.8}{13}$	$\frac{5.9}{9}$	$\frac{6.0}{6.0}$	$\frac{5.7}{7}$	$\frac{6.3}{11}$	$\frac{9.8}{22}$	$\frac{10.4}{34}$	$\frac{9.7}{50}$
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STA + H.I. - ELEV

885.33

5 879.33

+50 879.13

9.93 890.11 ✓ 5.15 890.18 ✓

6 879.41

+35 880.11

+66 879.41

7 878.81

+50 878.41

8 878.01

+50 877.41

4.85 881.45 ✓ 13.51 876.60 ✓

9 876.45

+50 874.95

10 874.05

+50 873.15

$\frac{11.2}{50}$   $\frac{10.2}{25}$   $\frac{6.3}{12}$   $\frac{60}{60}$   $\frac{6.1}{6}$   $\frac{7.6}{21}$   $\frac{8.1}{27}$   $\frac{9.0}{28}$   $\frac{9.0}{40}$   $\frac{9.0}{50}$

$\frac{5.6}{50}$   $\frac{5.2}{39}$   $\frac{4.9}{36}$   $\frac{5.6}{21}$   $\frac{6.4}{14}$   $\frac{6.6}{10}$   $\frac{6.2}{6.2}$   $\frac{6.1}{9}$   $\frac{7.1}{10}$   $\frac{7.1}{14}$   $\frac{5.9}{15}$   $\frac{6.0}{22}$   $\frac{5.9}{50}$

$\sqrt{\frac{60}{50}}$

$\frac{5.9}{37}$   $\frac{4.6}{33}$   $\frac{5.1}{27}$   $\frac{7.8}{21}$   $\frac{1.10}{19}$   $\frac{1.10}{11}$   $\frac{1.02}{7}$   $\frac{10.7}{7}$   $\frac{10.5}{5}$   $\sqrt{10.7}$   $\frac{10.7}{10}$   $\frac{11.2}{16}$   $\frac{7.1}{23}$   $\frac{7.1}{50}$

$\frac{4.8}{50}$   $\frac{3.7}{42}$   $\frac{3.6}{41}$   $\frac{8.9}{30}$   $\frac{10.8}{2}$   $\sqrt{100}$   $\frac{9.7}{8}$   $\frac{9.8}{23}$   $\frac{8.3}{24}$   $\frac{4.6}{30}$   $\frac{3.8}{50}$

$\frac{5.1}{50}$   $\frac{4.2}{37}$   $\frac{10.3}{22}$   $\sqrt{10.7}$   $\frac{10.7}{10}$   $\frac{7.7}{40}$   $\frac{7.1}{50}$   $\frac{5.2}{100}$

$\frac{7.5}{50}$   $\frac{6.4}{50}$   $\frac{12.0}{25}$   $\frac{1.10}{20}$   $\sqrt{11.5}$   $\frac{10.4}{15}$   $\frac{8.7}{22}$   $\frac{5.2}{20}$   $\frac{5.3}{50}$

$\frac{8.6}{50}$   $\frac{7.8}{40}$   $\frac{8.0}{36}$   $\frac{12.1}{33}$   $\frac{1.119}{23}$   $\frac{1.110}{18}$   $\frac{1.116}{3}$   $\frac{1.117}{11.7}$   $\frac{10.6}{6}$   $\frac{9.2}{14}$   $\frac{3.6}{17}$   $\frac{3.3}{24}$   $\frac{3.3}{50}$

$\frac{10.1}{50}$   $\frac{9.1}{37}$   $\frac{12.0}{33}$   $\frac{1.117}{15}$   $\frac{12.0}{9}$   $\frac{1.116}{12.1}$   $\frac{9.6}{6}$   $\frac{5.0}{17}$   $\frac{4.0}{24}$   $\frac{4.0}{29}$   $\frac{4.0}{50}$

$\frac{14.3}{50}$   $\frac{13.7}{49}$   $\frac{1.110}{32}$   $\frac{12.3}{29}$   $\frac{1.130}{12}$   $\frac{12.7}{12.7}$   $\frac{12.6}{6}$   $\frac{10.8}{13}$   $\frac{8.2}{50}$

$\frac{8.1}{50}$   $\frac{5.2}{17}$   $\frac{5.5}{6}$   $\frac{5.0}{5.0}$   $\frac{5.1}{2}$   $\frac{3.8}{7}$   $\frac{2.9}{50}$

$\frac{9.6}{50}$   $\frac{9.5}{23}$   $\frac{8.5}{17}$   $\frac{6.5}{9}$   $\frac{6.5}{6.5}$   $\frac{6.4}{3}$   $\frac{6.2}{27}$   $\frac{6.3}{33}$   $\frac{5.6}{50}$

$\frac{10.3}{50}$   $\frac{10.3}{33}$   $\frac{9.3}{16}$   $\frac{7.7}{10}$   $\frac{7.4}{7.4}$   $\frac{7.8}{11}$   $\frac{8.8}{21}$   $\frac{8.7}{35}$   $\frac{8.4}{50}$

$\frac{10.8}{50}$   $\frac{10.5}{33}$   $\frac{10.7}{17}$   $\frac{10.7}{15}$   $\frac{10.5}{14}$   $\frac{7.9}{6}$   $\frac{8.3}{8.3}$   $\frac{8.6}{3}$   $\frac{8.4}{12}$   $\frac{9.6}{17}$   $\frac{9.6}{33}$   $\frac{9.6}{50}$

881.45

Elev.

11

871.95

12

871.75

493

13

872.45

2.93 877.30 ✓ 7.06 874.37 874.37

+18

872.60

+50

873.20

14

877.90

12.29 887.51 ✓ 2.08 875.22 ✓

+50

877.11

15

882.21

+50

885.11

14

885.51

1.32 885.17 ✓ 3.64 883.85 ✓

+50

882.97

17

880.17

B.M.

6.80 878.37 ✓ 878.37

+40

877.57

108	108	108	115	115	103		99	104	104	104
50	33	18	17	14	9	9.5	12	13	18	30

100	100	112	112	100		102	104
50	40	19	16	9	9.7	15	50

105	105	103	103	95	95		92	90
50	33	21	18	17	13	90	17	50

TOP OF MONT. 50' HT. STA. 13+18

48	48	48		38	29
50	33	22	4.7	33	50

58	57	51		41	39
50	33	18	4.1	33	50

42	46	38	32		22	20
50	33	23	11	4.4	33	50

132	115		98	100
50	33	10.4	33	50

78	51	54		62	64
50	33	31	5.3	33	50

42	23	27		37	40
50	33	30	2.4	33	50

44	31		20	24
50	33	2.0	33	50

29	31	45		07	07
50	33	23	2.2	33	50

52	50	45	54		54	60
50	33	22	19	5.0	33	50

SPK. IN 18" OAK. 70' HT. STA. 17+25

86	87	78		85	89
50	33	20	7.6	33	50

		885.17 ✓		Elev.	
+60				874.57	
	2.85	875.62 / 1240		872.77 ✓	
18				872.02	
				869.92	
+50					
19				869.12	
				868.72	
20					
				868.92	
21					
				868.62	
22					
	+45			76	68.0
	+47			73	66.3
	+50	2 PITCH.		864.62	
	+71			8.5	67.1
	+74			7.5	68.3
23				868.72	1.9
	11.91	881.46 / 6.07		869.55 ✓	
24				868.86	
				868.56	
25					
26				872.16	

$\frac{100}{50}$   $\frac{99}{33}$   $\frac{98}{33} \checkmark$  10.6  $\frac{107}{33}$   $\frac{109}{50}$

$\frac{2.5}{50}$   $\frac{2.6}{33}$   $\frac{3.0}{22} \checkmark$  3.6  $\frac{3.8}{33}$   $\frac{4.0}{50}$

$\frac{5.9}{50}$   $\frac{5.7}{33} \checkmark$  5.7  $\frac{5.5}{33}$   $\frac{5.5}{50}$

$\frac{6.6}{50}$   $\frac{6.6}{33} \checkmark$  6.5  $\frac{6.1}{33}$   $\frac{6.1}{50}$

$\frac{6.9}{50}$   $\frac{7.0}{33} \checkmark$  6.9  $\frac{6.5}{33}$   $\frac{6.4}{50}$

$\frac{6.8}{50}$   $\frac{6.7}{33}$  6.7  $\frac{6.4}{33}$   $\frac{6.4}{50}$

$\frac{7.0}{50}$   $\frac{7.0}{33} \checkmark$  7.0  $\frac{7.0}{33}$   $\frac{7.0}{50}$

675

8.1 860.8 TOP OF WATER 11-24-28.

$\frac{9.8}{200}$   $\frac{9.9}{150}$   $\frac{11.1}{100}$   $\frac{9.8}{50}$  11.0  $\frac{9.9}{50}$   $\frac{10.2}{100}$   $\frac{9.7}{150}$   $\frac{10.0}{200}$

$\frac{7.0}{50}$   $\frac{7.0}{33}$  6.9  $\frac{7.0}{9}$   $\frac{8.2}{11}$   $\frac{8.2}{16}$   $\frac{6.7}{18}$   $\frac{6.7}{33}$   $\frac{6.7}{50}$

$\frac{12.7}{50}$   $\frac{12.6}{33}$  12.6  $\frac{13.0}{47}$   $\frac{13.8}{49}$   $\frac{13.8}{54}$   $\frac{13.0}{56}$

$\frac{11.4}{50}$   $\frac{11.9}{33}$   $\frac{12.5}{27}$  12.9  $\frac{13.1}{33}$   $\frac{13.1}{50}$

$\frac{5.7}{50}$   $\frac{6.2}{33}$  8.3  $\frac{9.4}{15}$   $\frac{10.6}{33}$   $\frac{11.0}{50}$

	881.46 ✓	Elev.
+30		876.26
	13.08 895.34 ✓ 11.20	880.26 ✓
26 + 30		
26 + 75		890.24
27 + 00		
	13.08 905.63 ✓ 0.79	892.55 ✓
26 + 75		
27 + 00		894.13
27 + 20		897.93
27 + 50		
	13.73 918.41 ✓ 0.95	904.68 ✓
27 + 50		908.31
27 + 80		
	13.21 931.14 ✓ 0.48	917.93 ✓
27 + 80		918.84
28 + 00		925.14
28 + 15		927.74

6.9 8.2 9.0  
5.2 15 33 50

TOP OF STAKE

11.4 11.4 10.4 12.7 15.6  
30 43 37 25 13 (17.0)

5.8 8.5 10.6 12.3  
(3.1) 8 25 33 50

(10.8) 0.6 3.7 6.5  
7 33 50

7.3 10.5 11.5 11.7 11.2 12.8 13.3 14.6  
75 60 50 46 37 25 16 5 (15.4)

1.7 4.3 6.5 7.7 7.7 9.1 10.1  
90 68 50 33 27 19 11 11.5

9.0 11.4 13.8  
(1.7) 6 33 50 ?

0.0 10.2 9.5 4.6 5.3 6.0 6.6 7.6  
85 80 63 50 27 21 15 8 4

(+2.7) 1.0 2.4 4.4 7.8 12.0  
22 33 50 77 100

4.2 5.9 6.2 7.0 8.1 8.7 8.7 8.6 9.2 9.2 10.2 12.2  
100 90 80 60 50 46 33 25 21 10 7 101 9

+0.40 1.5 5.8 9.3 14.4 18.2  
9 33 50 77 100

13.0 11.8 11.1 11.2 10.8 10.6 11.6 10.8 11.8  
100 70 50 43 33 24 9 8 5 12.3

11.9 10.0 8.7 6.5 6.5 6.2 5.7 7.6 11.8 14.3 17.8  
100 70 50 23 19 11 8 6.0 7 33 50 80

10.2 8.7 7.4 6.3 5.3 5.3 4.6 3.8 4.2 4.6 4.7 2.1 7.4 14.3  
100 70 50 33 14 19 9 8 6 3.4 4 15 33 50 80

Elev.

931.14 ✓

+50

928.34

8.17 937.21 ✓ 2.10

929.14 ✓

29

931.41

5.61 937.21 5.61

931.60 ✓ 931.61

+50

932.21

30

931.31

+50

929.81

31

926.21

+50

3.06 927.86 ✓ 12.41 924.80 ✓

31

+50

922.56

32

921.66

+50

919.26

33

915.26

3.92 918.79 ✓ 12.99

914.27 ✓

+50

912.49

95 78 63 54 47 51 48 40 2.9 30 2.6 1.2 10 1.3 5.0  
100 70 50 33 24 19 10 9 2.8 2 6 78 41 30 67 100

141  
700

13.6 12.6 11.2 10.3 9.0 8.1 7.1 7.1 5.3 ✓ 5.9 5.2 5.7 5.3 4.7 4.8 5.5  
85 70 50 34 24 21 10 9 7 2 5.8 4 27 44 60 66 70 100

SPK IN 6" OAK 6 LT. STA 29+30

134 119 106 97 89 70 76 70 66 50 ✓ 57.0 47 48 40 3.2 29 33 40  
100 75 50 33 27 22 12 11 7 1 50 5 10 16 33 50 67 80 100

12.5 10.8 9.9 9.9 10.0 9.1 ✓ 5.6 5.0 5.1 4.0 3.5 2.8 3.1  
10 75 50 33 22 9 5.9 7 11 14 31 50 71 100

15.4 14.9 12.0 11.3 10.5 10.7 9.5 8.8 ✓ 7.5 7.0 7.9 6.5 6.0 3.8  
100 84 50 33 27 21 10 9 7.4 7 12 17 29 50 100

104 98 101 83 75 69 64  
11.0 9 13 16 33 50 70 100

14.7 13.6 11.8 9.0 7.5 6.2  
81 35 35 72 100

8.0 6.8 4.6 4.4 3.6 2.9 1.8  
75 50 25 19 11 10 9 1.7

8.8 9.5 7.9 7.2 7.4 6.4 5.4 5.1  
75 50 30 25 20 8 2 5.3 8

7.7 8.2 8.0 7.7 7.4 7.1 6.5 7.0 6.1 6.4 6.6 6.3 6.8 6.0 5.4 5.1 1.7  
75 60 50 21 24 18 10 9 7 2 6.2 3 9 12 15 45 50 62 100

8.0 8.6 9.2 8.8 7.3 7.5 8.7 9.0 8.8 7.3 7.0 9.4 9.0 7.5 7.8 7.4  
75 50 27 24 18 10 7 8.6 1 3 6 1 16 30 47 65 75

11.4 12.5 11.4 11.1 12.7 12.0 12.5 12.6 13.0 12.8 13.3 13.1 12.8 12.3  
75 50 23 17 9 7 4 12.6 4 3 12 14 39 50 75

3.4 2.4 4.5 5.0 6.4 6.2 6.4 6.9 7.4 7.3 7.5  
75 56 33 24 13 8 6.3 3 5 10 30 50

Elev.

918.77

34

908.89

5.45 914.68 / 9.56 909.23 ✓

+50

904.18

35

903.48

+40

902.28

+65

902.18

36

903.98

+50

903.98

37

906.68

+50

916.98

11.95 925.29 / 1.34 913.34 ✓

38

917.79

+50

918.39

39

916.79

+50

913.59

0.66 912.97 / 1.298 912.31 ✓

$\frac{30}{25}$ 

$\frac{41}{29}$   $\frac{63}{50}$   $\frac{70}{28}$   $\frac{90}{17}$   $\frac{99}{71}$   $\frac{96}{8}$   $\frac{98}{6}$   $\frac{106}{3}$   $\frac{106}{99}$   $\frac{79}{1}$   $\frac{102}{5}$   $\frac{106}{10}$   $\frac{105}{14}$   $\frac{112}{24}$   $\frac{105}{50}$

$\frac{34}{75}$   $\frac{74}{50}$   $\frac{88}{34}$   $\frac{93}{21}$   $\frac{103}{11}$   $\checkmark$   $\frac{105}{16}$   $\frac{9.8}{50}$   $\frac{94}{62}$   $\frac{85}{82}$

$\frac{54}{75}$   $\frac{90}{50}$   $\frac{100}{98}$   $\frac{99}{35}$   $\frac{106}{33}$   $\frac{110}{27}$   $\frac{107}{20}$   $\frac{111}{15}$   $\frac{114}{12}$   $\frac{112}{5}$   $\frac{112}{11.2}$   $\frac{113}{12}$   $\frac{112}{36}$   $\frac{110}{50}$   $\frac{109}{60}$

$\frac{98}{60}$   $\frac{103}{50}$   $\frac{104}{41}$   $\frac{113}{33}$   $\frac{114}{18}$   $\checkmark$   $\frac{11.9}{14}$   $\frac{11.9}{28}$   $\frac{11.5}{48}$   $\frac{11.3}{60}$

$\frac{99}{60}$   $\frac{102}{50}$   $\frac{107}{36}$   $\frac{110}{30}$   $\frac{112}{15}$   $\checkmark$   $\frac{11.9}{14}$   $\frac{11.5}{35}$   $\frac{11.1}{50}$   $\frac{109}{60}$

$\frac{75}{60}$   $\frac{73}{50}$   $\frac{76}{41}$   $\frac{72}{37}$   $\frac{97}{35}$   $\frac{102}{19}$   $\frac{109}{11}$   $\checkmark$   $\frac{110}{7}$   $\frac{106}{32}$   $\frac{102}{50}$   $\frac{106}{60}$

$\frac{102}{60}$   $\frac{106}{50}$   $\frac{102}{41}$   $\frac{109}{17}$   $\checkmark$   $\frac{10.1}{24}$   $\frac{9.8}{44}$   $\frac{84}{65}$

$\frac{76}{60}$   $\frac{72}{50}$   $\frac{72}{35}$   $\frac{78}{20}$   $\frac{76}{9}$   $\frac{73}{6}$   $8.0$   $\frac{78}{26}$   $\frac{76}{50}$   $\frac{77}{65}$

$\frac{42}{70}$   $\frac{22}{38}$   $\frac{13}{50}$   $\frac{09}{34}$   $\frac{13}{15}$   $\frac{10}{7}$   $\frac{28}{5}$   $\checkmark$   $\frac{2.3}{12}$   $\frac{3.6}{38}$   $\frac{3.7}{50}$   $\frac{4.1}{65}$

$\frac{118}{70}$   $\frac{118}{62}$   $\frac{101}{50}$   $\frac{94}{27}$   $\frac{74}{6}$   $7.5$   $\frac{7.0}{7}$   $\frac{6.7}{19}$   $\frac{8.1}{50}$   $\frac{8.8}{65}$

$\frac{106}{70}$   $\frac{107}{62}$   $\frac{94}{55}$   $\frac{91}{50}$   $\frac{85}{31}$   $\frac{71}{5}$   $6.9$   $\frac{5.9}{17}$   $\frac{2.8}{45}$   $\frac{2.1}{65}$

$\frac{124}{70}$   $\frac{122}{63}$   $\frac{103}{52}$   $\frac{98}{42}$   $\frac{85}{70}$   $\frac{80}{3}$   $8.5$   $\frac{8.1}{11}$   $\frac{7.6}{33}$   $\frac{6.7}{48}$   $\frac{3.6}{75}$

$\frac{158}{50}$   $\frac{146}{33}$   $\frac{129}{14}$   $\frac{118}{7}$   $11.7$   $\frac{11.2}{26}$   $\frac{10.8}{50}$   $\frac{10.8}{60}$

Elev.

912.97

40

905.97

4.44 912.90 4.44 912.53 1908.46

+50

903.70

41

903.30

+30

904.60

42

906.30

5.97 913.21 5.66 907.24

+60

908.71

43

908.11

+38

907.61

6.39 911.10 8.50 904.71

44

901.70

+50

901.00

45

901.20

9.05 910.16 9.99 901.11

46

900.86

899.96

47

900.86

899.96

93	86	80		58	52
50	29	17	7.0	22	50

SPX IN 12" OAK 60' RT. STA 40+10

11.9	10.9	10.3	✓	8.6	8.4
50	35	19	9.2	30	50

9.1	9.5			9.7	9.2
50	27		9.6	25	50

6.0	7.3			8.7	8.9
50	23	8.3		33	50

4.5	5.4			6.8	7.1
50	27	4.6		33	50

5.7	5.2	4.8		3.6	3.0
50	28	7.6	4.5	34	50

8.0	6.1			3.2	2.7
50	26	5.1		33	50

11.4	8.8			3.3	2.5
50	21	5.5		33	50

10.1	9.8			5.7	2.7
50	33	9.4		33	50

10.2	9.9			9.2	7.7
50	33	10.1		33	50

10.4	10.3			9.6	7.9
50	33	9.9		33	50

→ TOP OF WATER

10.2	9.3			10.2	
50	10.2			50	

10.2	9.3			10.2	
50	10.2			50	

						K/EN
		710.16				
48						900.86 899.96
49						900.86 899.96
50						900.86 899.96
51						901.16
	10.13	914.11	✓ 6.18			903.98 ✓
	+65					901.51
<del>X</del>						
52						903.71
B.M.	1.54	914.04	✓ 1.54			912.59 ✓ 912.50 ✓
	+50					912.84
	4.35	917.78	✓ 0.61			913.43 ✓
	+70					912.18
53						911.48
	+40					911.38
	+23					914.48
54						913.28
	+55					908.48
	0.65	905.78	✓ 12.65			905.13 ✓

10.2 9.3 → TOP OF WATER  
 50 10.2 10.2  
 50 50

10.3 9.5 → TOP OF WATER  
 50 10.2 10.3  
 50 50

10.2 9.5 10.2  
 50 10.2 50

8.4 8.8 9.2  
 50 33 50

2.2 4.5 9.7 ✓ 13.0 13.3  
 60 50 50 12.6 33 50

5.0 5.4 6.4 9.4 12.4 12.8  
 50 33 33 9 10.4 33 50

SRK IN 24" OAK 100 LT. STAIR 51+90.  
 5.6 3.6 2.5 3.2 7.1 10.0  
 50 33 24 1.2 18 35 50

9.7 6.9 ✓ 2.6 3.8 6.2  
 50 24 4.6 18 41 50

10.0 8.3 4.7 1.9  
 50 24 6.3 17 50

7.4 7.4 6.8 5.5 3.7 2.2  
 50 33 30 6.4 14 33 50

5.5 4.9 4.4 2.4 2.0  
 50 33 30 3.3 27 50

7.2 6.2 5.1 3.7 2.8 2.4  
 50 33 12 4.5 15 33 50

11.8 11.6 10.3 9.5 9.6 10.3  
 50 33 16 9.3 18 33 50

Elev.

905.78

55

899.38

B.M.

4.33

905.77

4.33

901.45

901.44

+30

896.47

1.03

897.28

9.52

896.25

56

893.68

+55

889.08

57

889.08

2.58

892.08

7.78

889.50

+50

889.08

58

887.68

+50

883.38

59

881.18

\*

3.29

886.23

9.14

882.94

+50

881.93

~~60~~

~~881.43~~

~~+50~~

~~880.83~~

61

878.03

12.25

892.09

4.39

879.84

108	88	76		58	63	52
50	33	18	6.4	19	33	50

SPX IN 12" OAK 80 LT. STA. 54+75.

145	128	112		85	78	68
50	33	21	9.3	22	33	50

80	73	55	✓	28	0.5	0.0
50	33	16	36	6	26	50

TOP OF WATER

94	87	85	✓	7.1	6.3	5.2	2.3
50	20	18	8.2	3	12	33	50

TOP OF WATER

95	87			7.8	7.3	7.1	6.6
50	14	22	4	18	33	50	

28	26	28		3.4	3.9	4.3
50	33	20	3.0	17	33	50

0.0	2.0	3.4		5.6	6.8	6.4
50	33	17	4.8	12	33	50

16	4.4	7.7		9.4	9.8	9.5
50	33	73	8.7	18	33	50

3.7	8.0	9.8		10.9	10.6	9.6
50	28	14	10.9	12	33	50

10.6	1.9	3.0		4.4	5.7	0.8
50	33	16	4.3	11	33	50

2.6	3.7	5.0		4.7	3.8	2.6
50	33	10	4.8	8	33	50

5.1	3.0	5.2		5.7	6.0	5.6
50	33	14	5.4	12	33	50

6.8	7.4	8.5		7.1	7.1	7.1
50	33	33	8.2	14	33	50

Elev

872.09 ✓

+10

879.59

+32

887.29

+38<sup>2</sup>

887.53

+51<sup>2</sup>

887.59

B.M.

12.41 879.68 ✓ 879.64

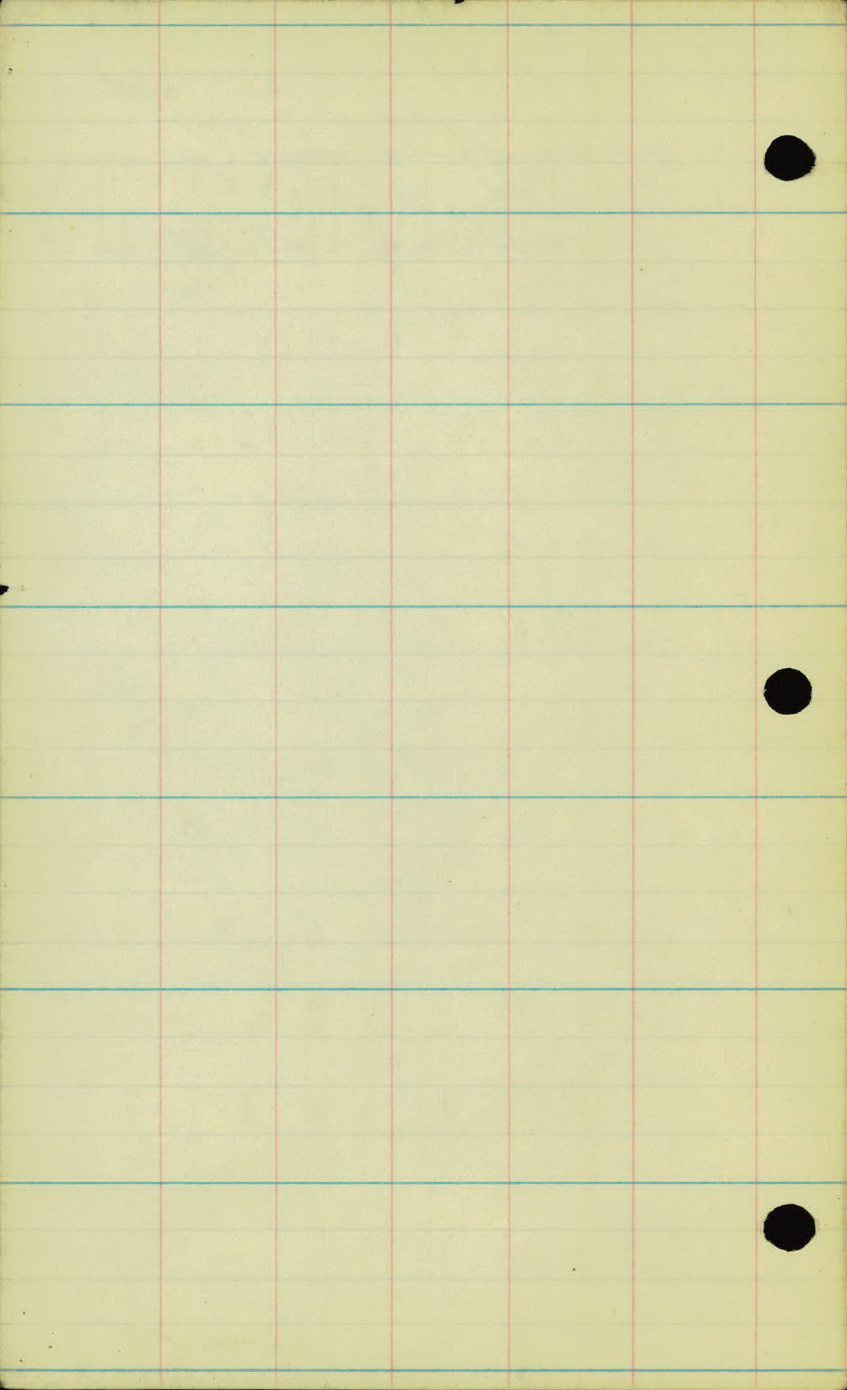
~~$\frac{11.7}{50}$   $\frac{12.7}{24}$  12.5  $\frac{11.9}{20}$   $\frac{11.4}{29}$   $\frac{11.5}{50}$~~

~~$\frac{4.3}{50}$   $\frac{4.4}{37}$  4.8  $\frac{4.7}{33}$   $\frac{5.0}{50}$~~

~~$\frac{4.18}{50}$   $\frac{4.28}{37}$  4.54  $\frac{4.78}{50}$~~

~~$\frac{3.35}{200}$   $\frac{3.60}{150}$   $\frac{3.85}{100}$   $\frac{4.11}{50}$  4.50  $\frac{4.71}{50}$   $\frac{4.67}{100}$   $\frac{4.76}{150}$   $\frac{4.97}{200}$~~

SPK IN C POPLAR 300 FT STA 62+25.



Project #29-17  
Soundings.

Sta.

45+00

46+00

Note:-

47+00 All soundings taken with  
a.  $\frac{3}{4}$ " sounding device.

48+00 All clay tests taken with  
the weight of two men.

49+00

50+00

50+70

## Depth of Sounding

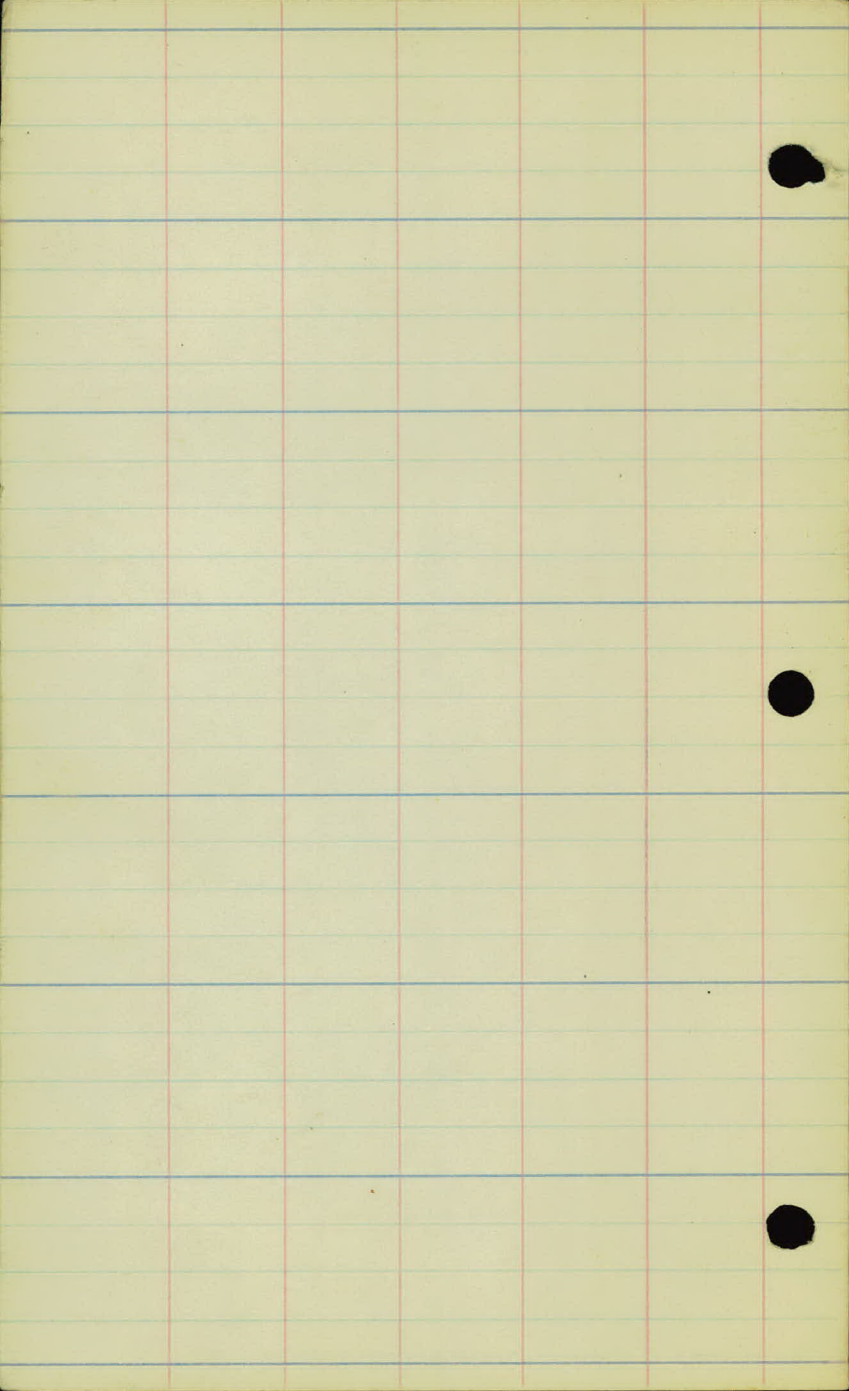
From

To

Kind of Soil.

	0 ft.	4 ft.	Muck. ✓
	4'	6'	Sandy Clay.
	6'	10'	Clay.
	0'	7'	Muck. ✓
	7'	9'	Black Dirt.
	9'	11'	Muck. ✓
	11'	17'	Clay.
	0'	8'	Muck.
	8'	12'	Black Dirt.
	12'	14'	Sand and Water.
	14'	14'	Clay. ✓
	0'	8'	Muck.
	8'	10'	Sandy Clay.
	10'	10'	Clay.
	0'	9'	Muck.
	9'	14'	Sandy Clay.
	14'	14'	Clay. ✓
	0'	4'	Muck and Peat.
	4'	10'	Black Dirt and Sand.
	10'	16'	Sand.
	16'	16'	Clay.
	0'	2'	Muck.
	2'	5'	Sand.

All soundings taken on E





Sta.

18+50

19+00

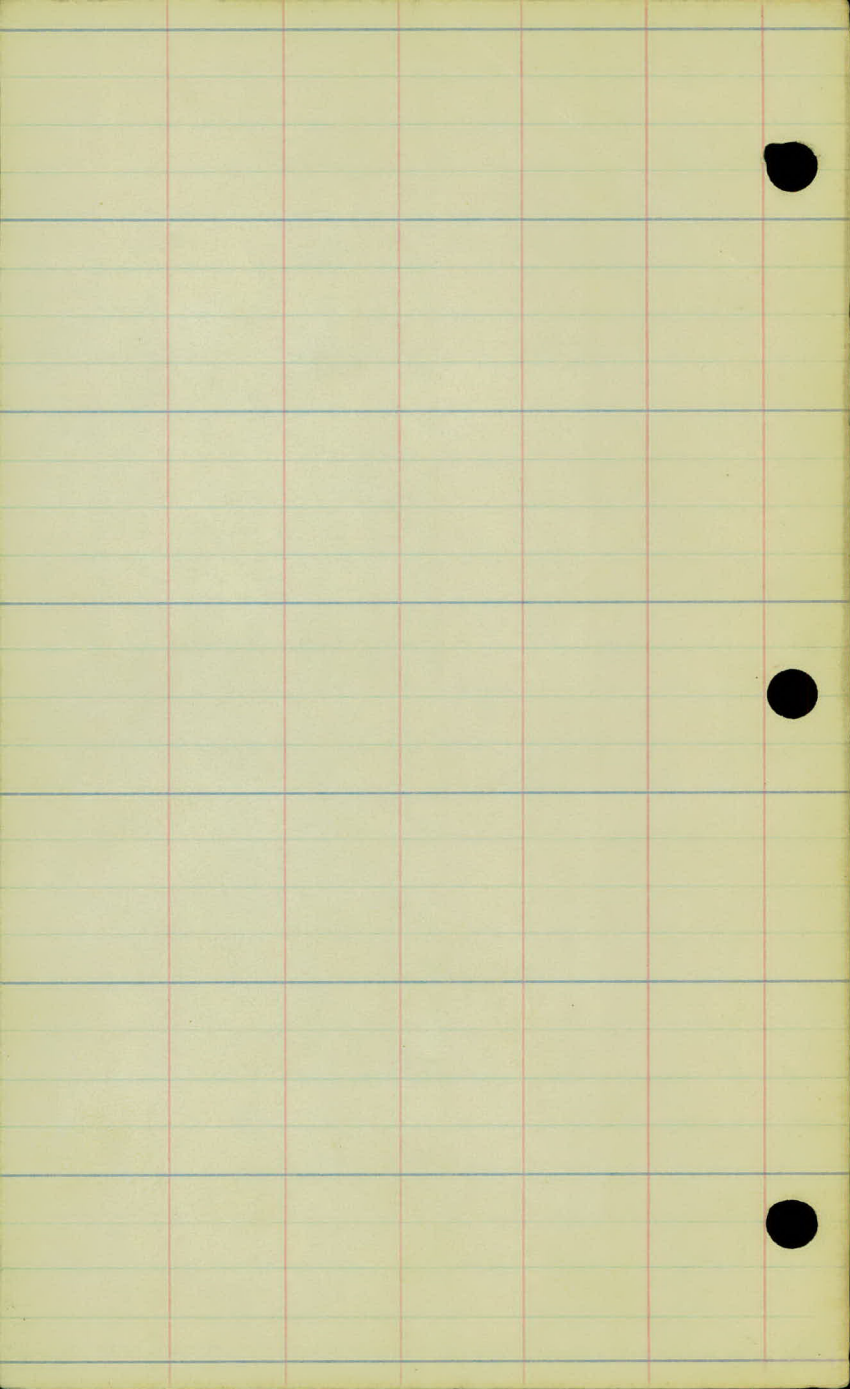
21+00

24+00

25+00

	Depth of Sounding		Kind of Soil.
	From	To	
All Soundings Taken on ♀	0 ft.	8 ft.	Muck.
	8'	13'+	Clay.
	0'	10'	Muck.
	10'	21'+	Soft Clay.
	0'	15'	Muck.
	15'	21'	Soft Clay.
	21'	21'+	Sandy Clay.
	0'	12'	Muck.
	12'	17'	Sandy Clay.
	17'	17'+	Clay. ✓
	0	8	Muck

✓



Proj # 29-17  
DRAINAGE NOTES.

B.M.	0.26	885.37 ✓		885.11 ✓
	1.01	881.28 ✓	5.10	880.27 ✓

14.4  
90

13.6  
50

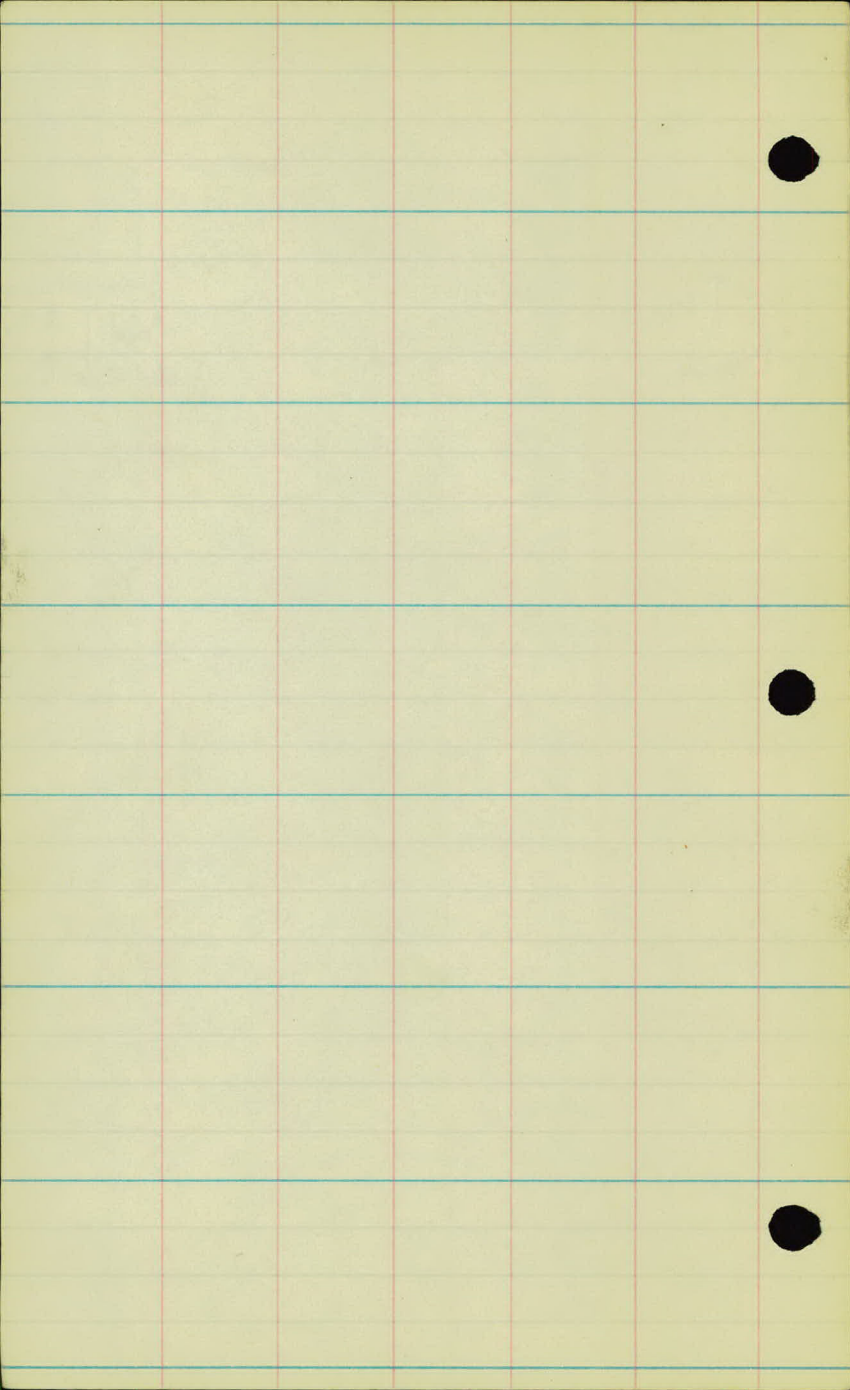
OUTLET.  
↑  
11.90

11.56

9.9  
50

9.2  
100

→ FROM END OF COIL. ←



PROJ # 29-17

CHECK LEVELS FROM S.T.H. # 62  
TO S.T.H. # 63.

B.M.	12.72	892.38 ✓		877.66 ✓
	12.76	901.75 ✓	3.37	888.99 ✓
B.M.	13.24	914.68 ✓	0.31	901.44 ✓
B.M.			2.18	912.50 ✓
	1.81	905.74 ✓	10.75	903.93 ✓
B.M.	9.85	912.84 ✓	2.75	902.99 ✓
	10.98	916.32 ✓	7.50	905.34 ✓
B.M.			7.86	908.46 ✓
	6.46	921.54 ✓	1.44	914.88 ✓
	12.03	932.52 ✓	0.85	920.49 ✓
B.M.			0.91	931.61 ✓
	0.97	920.74 ✓	12.77	919.75 ✓
	1.47	909.18 ✓	13.03	907.71 ✓
	1.03	896.86 ✓	13.35	895.83 ✓
	1.30	885.36 ✓	12.80	884.06 ✓
	12.63	884.49 ✓	13.50	871.86 ✓
B.M.			6.12	878.37 ✓
	3.06	877.79 ✓	7.76	874.73 ✓
B.M.			3.42	874.37 ✓
	10.66	884.92 ✓	3.53	874.26 ✓
	8.12	889.44 ✓	3.60	881.52 ✓
B.M.			4.33	885.11 ✓
	11.03	895.07 ✓	5.40	884.04 ✓
B.M.			2.20	892.87 ✓
				892.44 ✓

SPK IN 6" POPLAR 90' RT. STA. 62+25

SPK IN 18" OAK 20' LT. STA. 54+75.

SPK IN 24" OAK 100' LT. STA. 51+90.

SPK IN 10" POPLAR 50' RT. STA. 45+25.

SPK IN 18" OAK 60' RT. STA. 40+10.

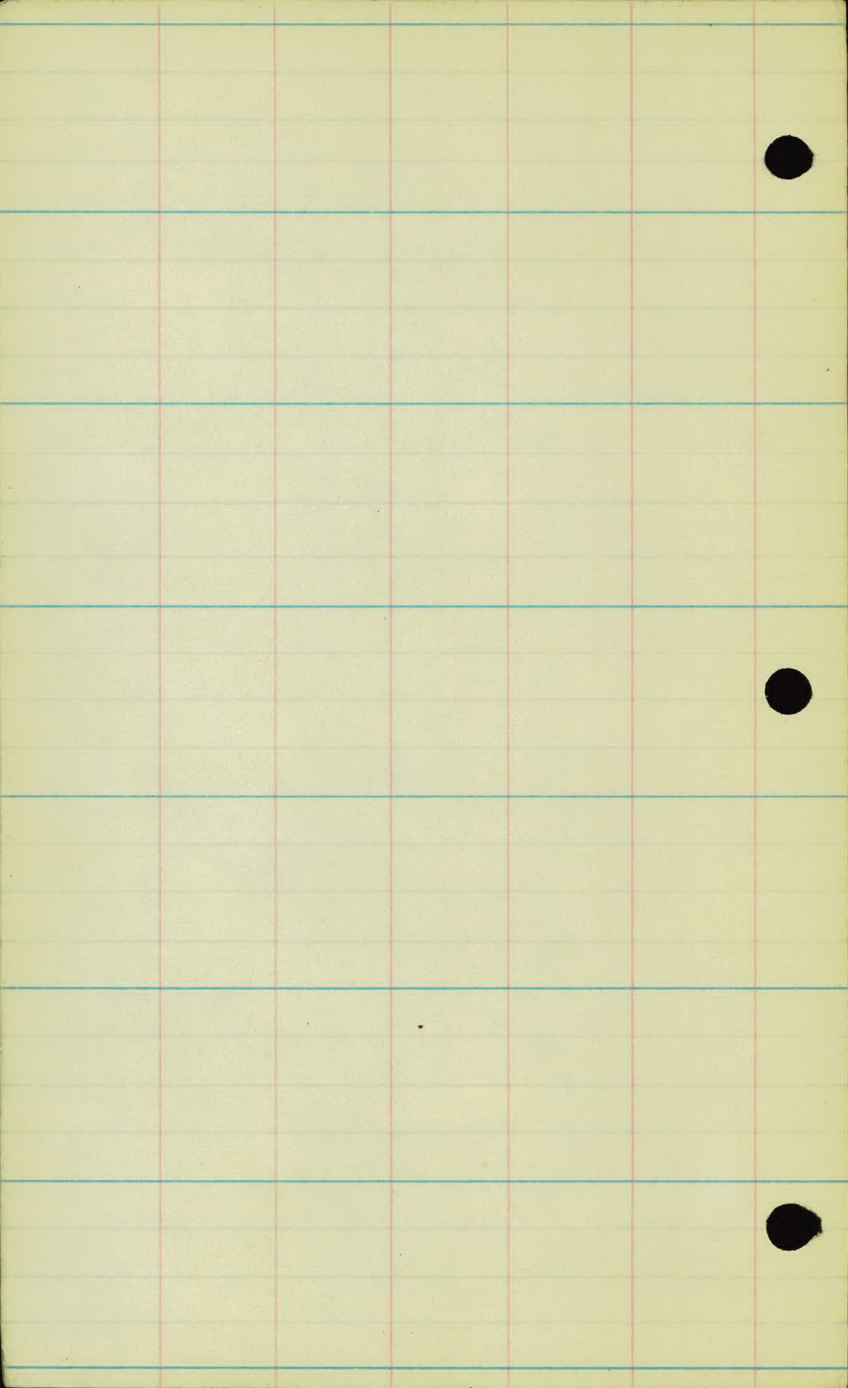
SPK IN 8" OAK 6' LT. STA. 29+30.

SPK IN 18" OAK 70' RT. STA. 17+25.

TOP OF MONT. 50' RT. STA. 13+18

TOP OF CONC. WALK 30' RT. STA. 0+83.

N.W. COR. LOWER STEP 30' LT. STA. 151+00. STA. #63.



PROV # 28-17  
CHECK LEVELS.

B.M. 12.55 892.21 ✓ 879.66 ✓  
12.54 904.44 ✓ 0.31 891.90 ✓

B.M. 2.97 901.47 ✓  
12.54 916.71 ✓ 0.27 904.17 ✓

B.M. 4.17 912.54 ✓  
5.00 908.97 ✓ 12.74 903.97 ✓

B.M. 9.29 912.4 ✓ 5.95 903.02 ✓  
5.17 916.78 ✓ 0.70 911.61 ✓

B.M. 8.27 908.51 ✓  
8.71 923.63 ✓ 1.86 914.92 ✓

10.70 933.92 ✓ 0.61 923.02 ✓  
2.32 931.60 ✓

0.33 921.15 ✓ 13.10 920.82 ✓  
0.53 908.86 ✓ 12.82 908.33 ✓

1.12 896.94 ✓ 13.02 895.84 ✓  
0.67 884.37 ✓ 13.26 883.70 ✓

11.41 882.60 ✓ 13.18 871.19 ✓  
4.17 878.43 ✓

5.02 887.41 ✓ 0.41 882.39 ✓  
8.18 882.61 ✓ 12.98 874.43 ✓

8.62 888.51 ✓ 2.72 879.89 ✓  
3.41 885.10 ✓

B.M. 11.02 895.07 ✓ 4.46 884.05 ✓  
B.M. 2.22 895.07 ✓ 2.22 892.85 ✓ 892.44

4.52 888.57 ✓ 11.02 884.05 ✓  
3.46 885.11 ✓ 885.10 ✓

SPK IN 6" POPLAR 300 RT STA 62725.

SPK IN 18" OAK 80 LT STA 54775

SPK IN 24" OAK 100 LT STA 51790.

ON ROCK.

SPK IN 10" POPLAR 50 RT STA 45725

SPK IN 18" OAK 60 RT STA 40710

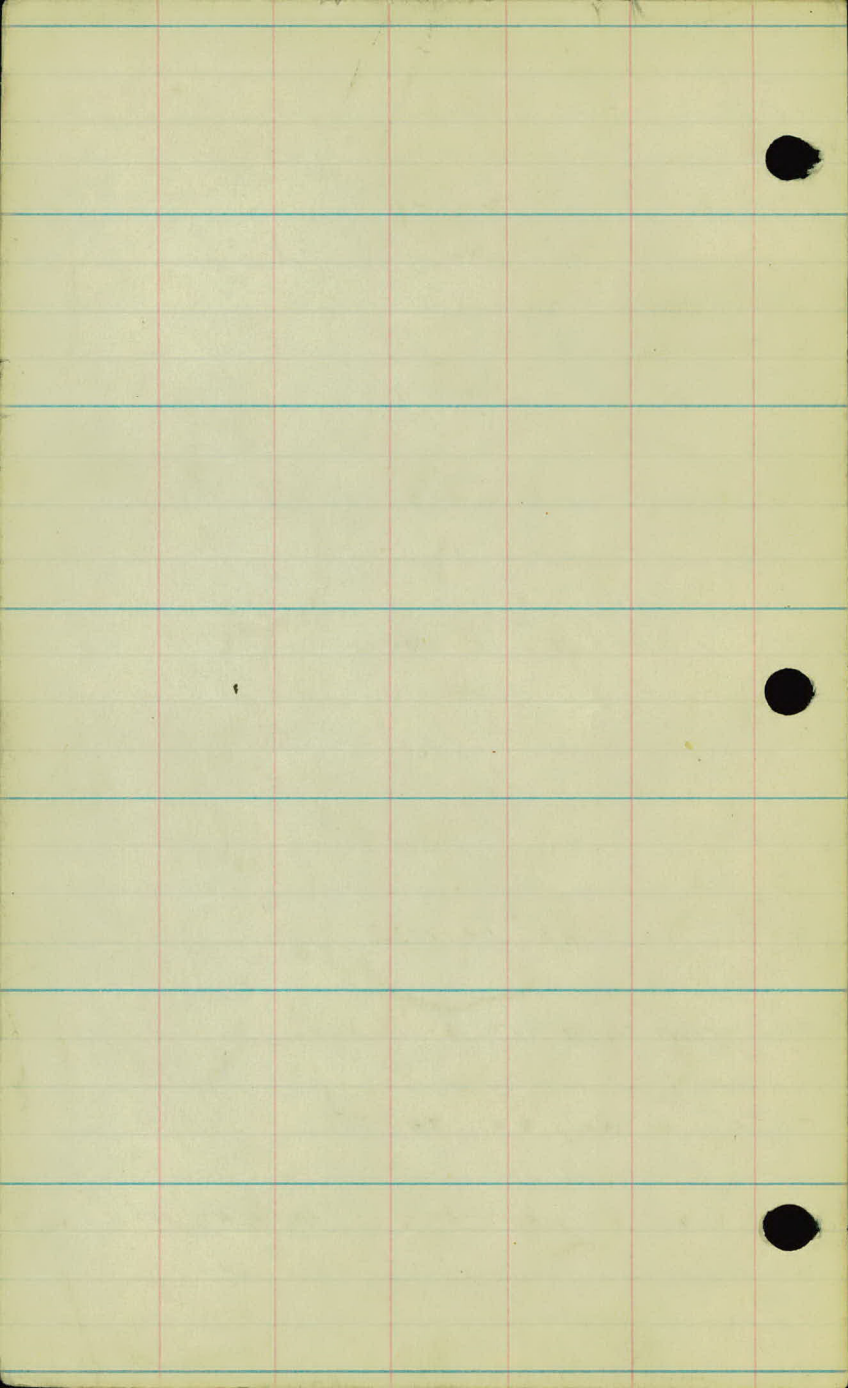
SPK IN 8" OAK 6 LT STA 29730

SPK IN 18" OAK 70 RT STA 17725.

TOP OF MONT. 50 RT STA 13718.

TOP OF CONC. WALK 30 RT STA 0725

N.W. COR LOWER STEP 30 LT STA 15100 S.T.H. # 63.



PROJ # 29-17

"B" LINE.

CENTER LINE LEVELS AND  
CROSS SECTIONS FROM STA. 99189  
TO S.T.M. # 62.

B.M. 0.38 908.84 ✓ 908.46 ✓  
40.750 903.54

41 913.34

+50 904.34

5.50 912.72 ✓ 1.62 907.22 ✓

42 906.72

+50 908.52

43 909.32

+65 910.32

1.93 911.43 ✓ 3.22 909.50 ✓

44 908.72

+50 905.53

45 902.93

B.M. 4.89 907.88 ✓ 8.44 902.99 ✓ 902.99

+50 902.58

46 901.28

+50 901.48

SPR. IN 18" OAK 60 RT. STA. 40 + 10.

$\frac{23}{50} \frac{67}{33} \frac{65}{27} \frac{52}{5} \frac{45}{5.3} \frac{42}{22} \frac{43}{33} \frac{43}{50}$

$\frac{50}{50} \frac{5.3}{33} \frac{5.6}{5} \frac{5.5}{5.5} \frac{5.6}{20} \frac{5.2}{33} \frac{4.9}{50}$

$\frac{1.4}{50} \frac{2.9}{33} \frac{4.2}{10} \frac{4.5}{4.5} \frac{4.7}{19} \frac{4.9}{33} \frac{5.3}{50}$

$\frac{5.4}{50} \frac{5.7}{33} \frac{6.0}{18} \frac{6.3}{15} \frac{6.5}{6.5} \frac{6.9}{20} \frac{7.5}{34} \frac{7.9}{50}$

$\frac{4.4}{50} \frac{4.4}{28} \frac{4.0}{23} \checkmark \frac{4.2}{4.2} \frac{3.8}{20} \frac{4.1}{33} \frac{4.4}{50}$

$\frac{5.6}{50} \frac{4.8}{33} \frac{3.8}{17} \checkmark \frac{3.4}{3.4} \frac{2.3}{2.5} \frac{1.9}{33} \frac{1.4}{50}$

$\frac{9.8}{50} \frac{7.3}{33} \frac{4.7}{17} \frac{2.4}{2.4} \frac{1.3}{2.1} \frac{0.6}{2.6} \frac{0.2}{33} \frac{1.0}{50}$

$\frac{9.9}{50} \frac{8.4}{33} \frac{6.0}{16} \frac{3.9}{2} \checkmark \frac{2.7}{2.7} \frac{0.0}{2.2} \frac{+2.0}{33} \frac{+3.2}{50}$

$\frac{10.0}{50} \frac{9.7}{33} \frac{7.7}{16} \frac{5.9}{5.9} \checkmark \frac{3.0}{2.1} \frac{1.7}{33} \frac{+0.4}{50}$

$\frac{10.0}{50} \frac{9.9}{33} \frac{8.8}{20} \frac{7.5}{7.5} \frac{5.8}{17} \frac{4.6}{33} \frac{3.5}{50}$

$\frac{6.8}{50} \frac{6.5}{33} \frac{6.1}{7} \frac{5.3}{5.3} \frac{4.1}{17} \frac{2.8}{33} \frac{1.6}{50}$

$\frac{6.9}{50} \frac{6.7}{33} \frac{6.6}{6.6} \frac{6.1}{9} \frac{5.3}{16} \frac{3.3}{33} \frac{1.4}{50}$

$\frac{7.0}{50} \frac{6.8}{33} \frac{6.4}{6.4} \frac{5.9}{17} \frac{5.2}{2.1} \frac{3.5}{23} \frac{2.1}{40} \frac{10.1}{50}$

Elev

907.88

47

901.58

+50

901.68

48

902.78

7.73 911.48 / 4.25 913.65 /

+58

909.28

B.M.

0.12 911.44 / 0.12 911.36 / 911.32

+80

909.34

49

908.04

+50

902.74

50

900.94

51

900.74  
900.24

+55

902.04

+83

904.64

9.04 917.07 / 3.43 908.01 /

52

909.37

+17

912.37

$\frac{6.8}{50}$   $\frac{6.6}{33}$  6.3  $\frac{6.1}{22}$   $\frac{5.0}{25}$   $\frac{3.7}{36}$   $\frac{1.8}{43}$   $\frac{0.4}{50}$

$\frac{6.8}{50}$   $\frac{6.7}{33}$  6.2  $\frac{5.1}{21}$   $\frac{3.1}{33}$   $\frac{0.0}{50}$

$\frac{6.6}{50}$   $\frac{6.4}{33}$   $\frac{6.3}{11}$  5.1  $\frac{3.8}{14}$   $\frac{0.3}{33}$   $\frac{7.10}{50}$

$\frac{7.4}{50}$   $\frac{5.8}{33}$   $\frac{4.1}{20}$   $\frac{1.9}{2.2}$   $\frac{1.5}{17}$   $\frac{1.4}{33}$   $\frac{1.4}{50}$

SPK IN 2" OAK 50' AT STA. 48160

$\frac{5.9}{50}$   $\frac{4.0}{33}$   $\frac{3.0}{19}$   $\frac{2.1}{2.1}$   $\frac{2.2}{21}$   $\frac{2.4}{33}$   $\frac{2.4}{50}$

$\frac{6.8}{50}$   $\frac{4.6}{33}$   $\frac{4.0}{18}$  3.4  $\frac{3.3}{22}$   $\frac{3.5}{33}$   $\frac{3.7}{50}$

$\frac{10.0}{50}$   $\frac{10.0}{33}$   $\frac{9.6}{78}$  8.7  $\frac{8.1}{18}$   $\frac{7.5}{33}$   $\frac{6.2}{50}$

$\frac{10.7}{50}$   $\frac{10.7}{33}$   $\frac{10.5}{10.5}$   $\frac{10.5}{33}$   $\frac{10.3}{50}$

TOP OF ICE  
 $\frac{11.2}{50}$   $\frac{10.7}{11.2}$   $\frac{11.2}{50}$

$\frac{9.8}{50}$   $\frac{9.7}{33}$  9.4  $\frac{9.0}{33}$   $\frac{8.3}{50}$

$\frac{8.1}{50}$   $\frac{7.5}{33}$   $\frac{7.3}{19}$  6.8  $\frac{6.1}{33}$   $\frac{6.1}{50}$

$\frac{10.9}{50}$   $\frac{9.7}{35}$   $\frac{9.6}{15}$  7.7  $\frac{7.4}{30}$   $\frac{8.0}{50}$

$\frac{6.9}{50}$   $\frac{5.6}{33}$   $\frac{5.3}{26}$  4.7  $\frac{4.4}{24}$   $\frac{4.8}{33}$   $\frac{5.6}{50}$

Elev

917.07

+53

911.87

53

907.97

+50

909.37

54

911.77

+50

912.57

55

912.67

+50

912.37

56

913.27

1.46 915.63 ✓ 2.90 914.17 ✓

+45

911.63

57

910.93

B.M. 5.77 915.170 ✓ 5.97 909.66 ✓ 909.73

+50

905.10

1.65 907.61 ✓ 7.74 905.96 ✓

57/50

58

901.71

$\frac{7.5}{50}$   $\frac{6.7}{33}$   $\frac{6.5}{33}$  ✓  $\frac{4.8}{29}$   $\frac{4.9}{33}$   $\frac{5.5}{50}$

$\frac{11.1}{50}$   $\frac{9.6}{21}$  ✓  $\frac{9.8}{29}$   $\frac{10.2}{50}$

$\frac{7.7}{50}$   $\frac{6.9}{33}$   $\frac{7.4}{19}$  ✓  $\frac{8.6}{19}$   $\frac{9.1}{33}$   $\frac{9.9}{50}$

$\frac{4.0}{50}$   $\frac{3.8}{33}$   $\frac{4.1}{26}$  ✓  $\frac{7.3}{25}$   $\frac{7.7}{33}$   $\frac{8.7}{50}$

$\frac{3.3}{50}$   $\frac{3.1}{33}$   $\frac{3.2}{24}$   $\frac{4.5}{22}$   $\frac{5.9}{33}$   $\frac{6.4}{33}$   $\frac{6.7}{50}$

$\frac{4.9}{50}$   $\frac{4.2}{33}$   $\frac{4.4}{18}$   $\frac{5.1}{33}$   $\frac{5.8}{33}$   $\frac{5.9}{50}$

$\frac{6.7}{50}$   $\frac{5.5}{33}$   $\frac{4.7}{33}$   $\frac{5.5}{33}$   $\frac{5.9}{50}$

$\frac{5.2}{50}$   $\frac{4.9}{25}$   $\frac{3.8}{33}$   $\frac{5.1}{33}$   $\frac{6.0}{50}$

$\frac{0.7}{50}$   $\frac{1.9}{33}$   $\frac{4.0}{29}$   $\frac{5.4}{33}$   $\frac{5.8}{33}$   $\frac{7.5}{49}$   $\frac{9.7}{50}$

$\frac{1.7}{50}$   $\frac{3.1}{33}$   $\frac{4.7}{23}$   $\frac{7.7}{33}$   $\frac{7.6}{33}$   $\frac{12.1}{50}$

SPK IN 11" OAK 45' LT STR 57150

$\frac{5.9}{50}$   $\frac{2.0}{33}$   $\frac{2.8}{21}$   $\frac{10.6}{21}$

$\frac{5.3}{14}$   $\frac{6.7}{27}$   $\frac{7.2}{33}$   $\frac{7.7}{50}$

$\frac{1.8}{50}$   $\frac{1.9}{33}$   $\frac{4.5}{17}$   $\frac{5.9}{27}$   $\frac{8.0}{27}$   $\frac{9.2}{50}$

Elev.

907.61

+50

900.01

59

898.31

2.06 898.56 ✓ 11.11 896.50 ✓

+50

895.66

60

899.66

2.97 889.28 ✓ 12.25 886.31 ✓

+50

885.78

61

882.08

+48

881.18

4.97 886.38 ✓ 7.87 881.41 ✓

62

879.08

+50

878.18

63

875.58

+57

878.48

64

878.98

+50

879.58

$$\frac{5.1}{50} \quad \frac{6.4}{33} \quad \frac{7.0}{24} \quad 7.6 \quad \frac{8.8}{33} \quad \frac{10.1}{50}$$

$$\frac{6.3}{50} \quad \frac{7.5}{38} \quad \frac{9.2}{22} \quad 9.3 \quad \frac{10.7}{25} \quad \frac{11.9}{33} \quad \frac{13.1}{50}$$

$$\frac{5.6}{50} \quad \frac{6.1}{33} \quad \frac{5.4}{17} \quad \checkmark \quad 2.6 \quad \frac{4.0}{33} \quad 5.6$$

$$\frac{11.1}{50} \quad \frac{11.2}{33} \quad \frac{10.8}{23} \quad 8.9 \quad \frac{7.2}{33} \quad \frac{7.4}{50}$$

$$\frac{5.1}{50} \quad \frac{5.3}{33} \quad \frac{4.9}{24} \quad 3.5 \quad \frac{1.9}{26} \quad \frac{1.6}{33} \quad 1.4$$

$$\frac{8.7}{50} \quad \frac{8.7}{33} \quad 7.2 \quad \frac{5.7}{22} \quad \frac{5.3}{32} \quad \frac{6.6}{35} \quad \frac{6.6}{39} \quad \frac{5.0}{48} \quad \frac{5.1}{50}$$

$$\frac{9.8}{50} \quad \frac{9.5}{33} \quad \frac{8.9}{14} \quad 8.1 \quad \frac{8.6}{50} \quad \frac{8.9}{50}$$

$$\frac{5.1}{50} \quad \frac{6.2}{33} \quad \checkmark \quad \frac{7.8}{33} \quad \frac{8.1}{50}$$

$$\frac{5.8}{50} \quad \frac{6.9}{33} \quad \checkmark \quad \frac{8.3}{33} \quad \frac{8.3}{50}$$

$$\frac{5.3}{50} \quad \frac{6.9}{33} \quad \checkmark \quad \frac{8.2}{33} \quad \frac{8.3}{50}$$

$$\frac{4.2}{50} \quad \frac{4.6}{42} \quad \frac{6.0}{35} \quad \frac{6.2}{31} \quad \checkmark \quad \frac{8.4}{33} \quad \frac{8.4}{50}$$

$$\frac{2.7}{50} \quad \frac{4.1}{37} \quad \frac{5.3}{24} \quad 7.4 \quad \frac{8.3}{33} \quad \frac{8.4}{50}$$

$$\frac{0.0}{50} \quad \frac{1.4}{43} \quad \frac{5.0}{33} \quad \frac{4.0}{25} \quad \frac{5.3}{12} \quad \frac{6.0}{10} \quad 6.8 \quad \frac{7.6}{12} \quad \frac{8.0}{33} \quad \frac{8.2}{50}$$

		Elev.
	886.38	
65		879.98
+50		878.98
66		877.98
+50		880.18
+80		882.38
67		882.48
+50		882.67
68		882.82
+08		
+50		3.53
69		3.50
	Cross R.A.M IN	
B.M.	3.15	883.23 / 883.21

7.05 0.6 3.2 5.5      7.3 8.0 8.2  
50 45 33 7 6.5      9      33 50

4.2 5.6      8.2 8.0  
50 33 7.4      33 50

EDGE OF PAVEMENT

3.84 3.92 4.1 6.1 6.8 8.0      7.6 7.8  
50 44 37 30 19 15      8.4      33 56

EDGE OF PAVE.

4.3 4.31 4.15 4.14 4.1 6.1      6.2 7.2 7.3 7.8 7.9  
50 48 35 17.6 12 3      6.2      5      9      12      33 50

EDGE OF PAVE.

4.3 4.18 4.02 4.05      6.1 7.6 7.6 7.6  
48 39 23 7 4.0 10 23 33 50

EDGE OF PAVE.

4.2 4.12 3.98 3.95      3.8 6.5 7.4 7.7 7.4  
41 33 21 0.5 3.9 8 23 28 33 50

EDGE OF PAVE.

9.0 8.1 3.8 3.91      3.76 3.7 6.0 7.0  
50 41 28 21 3.71 12 20 32 50

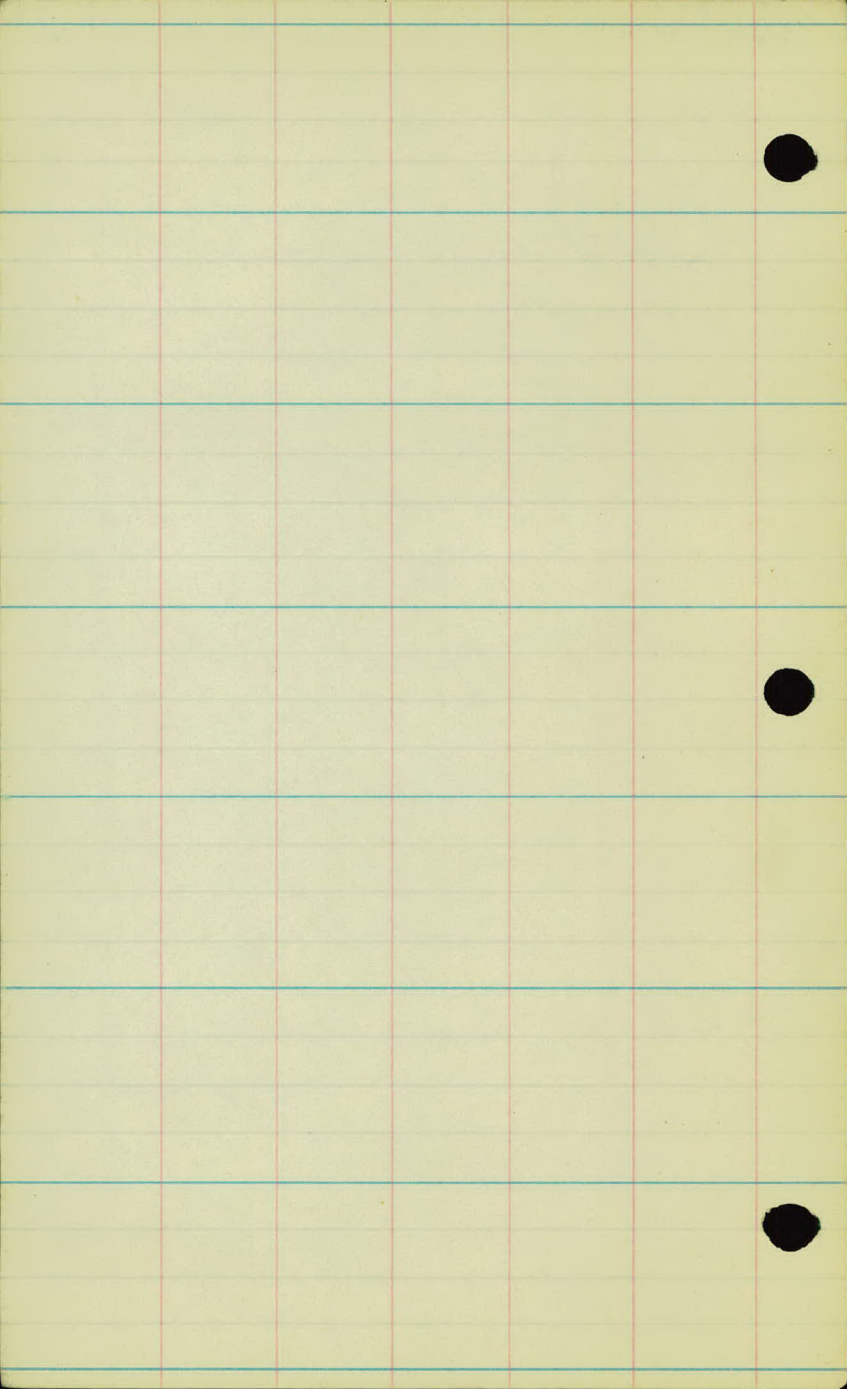
8.1 7.1 6.5 3.6 3.71      3.67 3.6 6.7 7.0 3.5 3.3  
50 33 29 19 13.5 3.56      13.5 19 31 43 50 55

7.4 6.3 3.6 3.68      3.66 3.6 6.7 6.7 3.3 3.0  
50 31 19 13.5 3.56      13.5 20 30 44 50 55

OUTLET ←      INLET  
10.0      9.40

76.38 76.98

SPR. IN 10" OAK 60 RT. STR. 67+90





B.M. 7.20 912.19 ✓ 902.99

B.M. 9.22 911.32 ✓

7.13 917.19 ✓ 4.13 908.06 ✓

3.85 909.82 ✓ 11.22 905.97 ✓

B.M. 0.09 909.73 ✓

0.79 897.29 ✓ 13.32 896.50 ✓

1.98 886.30 ✓ 12.97 884.32 ✓

B.M. 3.09 883.21 ✓

6.76 889.42 ✓ 3.64 882.66 ✓

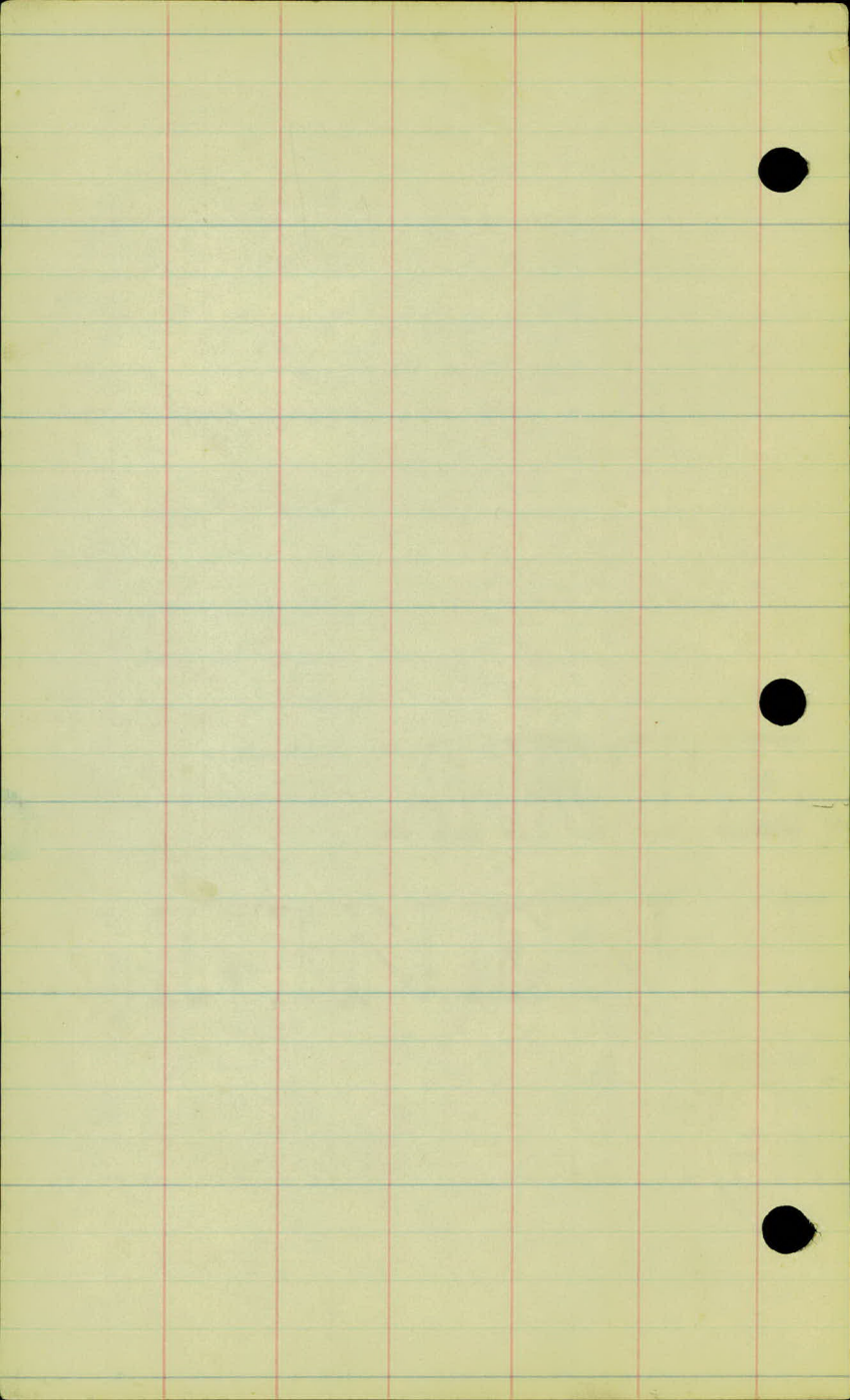
6.04 892.00 ✓ 3.48 885.94 ✓

B.M. 12.30 879.70 ✓

PROD # 29-17

SOUNDINGS

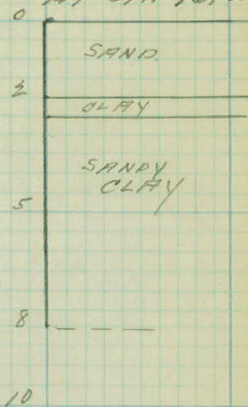
MATERIAL IN CUTS.



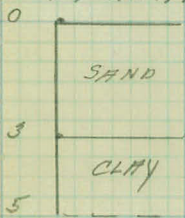
SOUNDING ON  $\frac{1}{2}$   
AT STA 15+00.



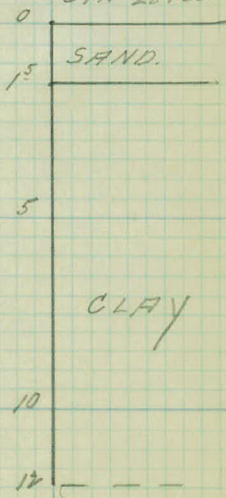
SOUNDING ON  $\frac{1}{2}$   
AT STA 16+00

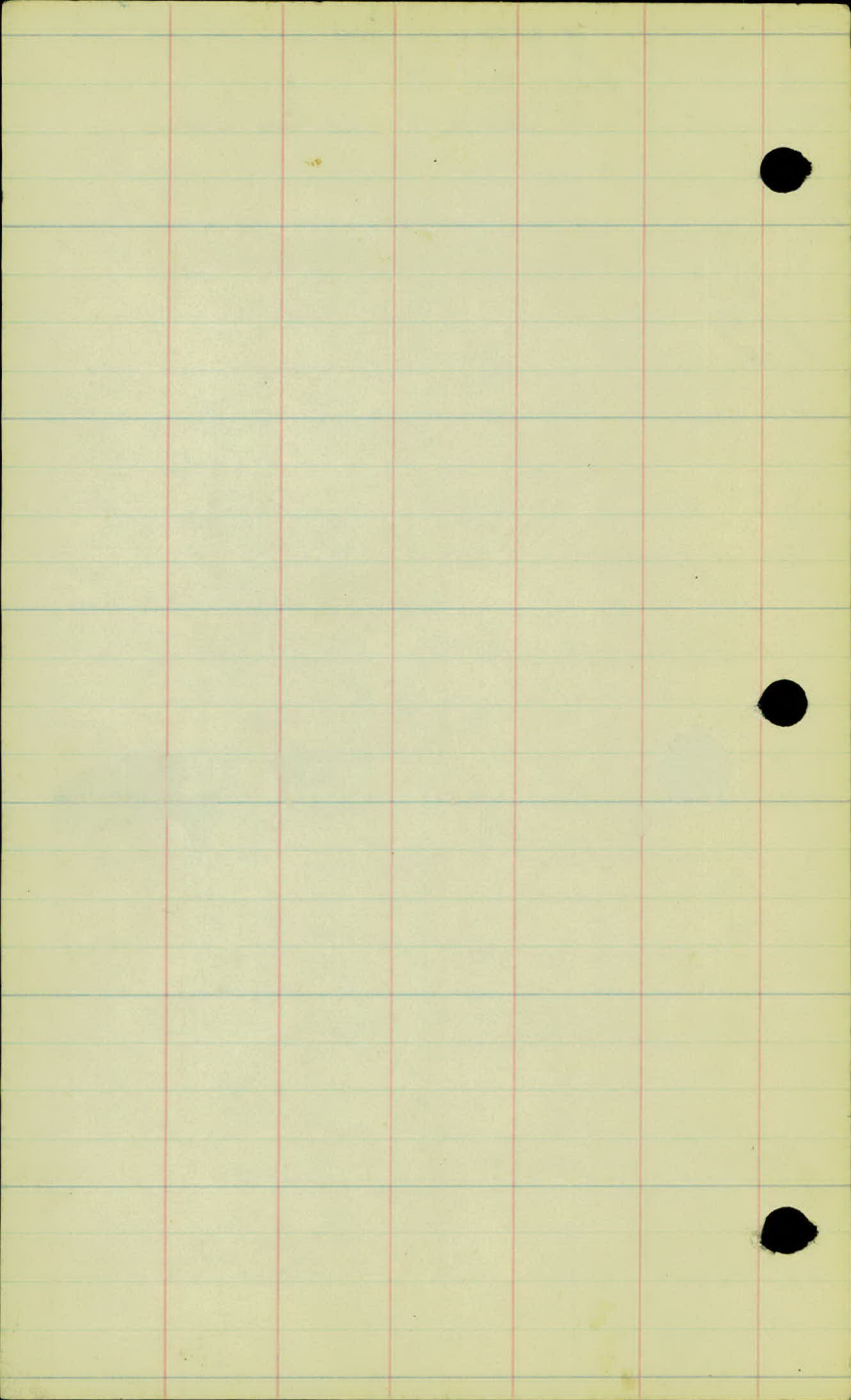


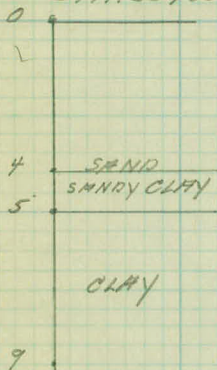
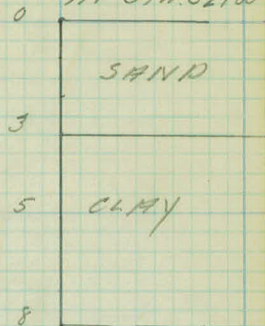
SOUNDING ON  $\frac{1}{2}$   
AT STA 17+00



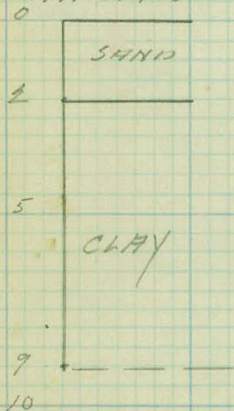
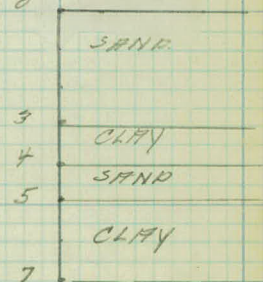
SOUNDING ON  $\frac{1}{2}$   
AT STA 23+00

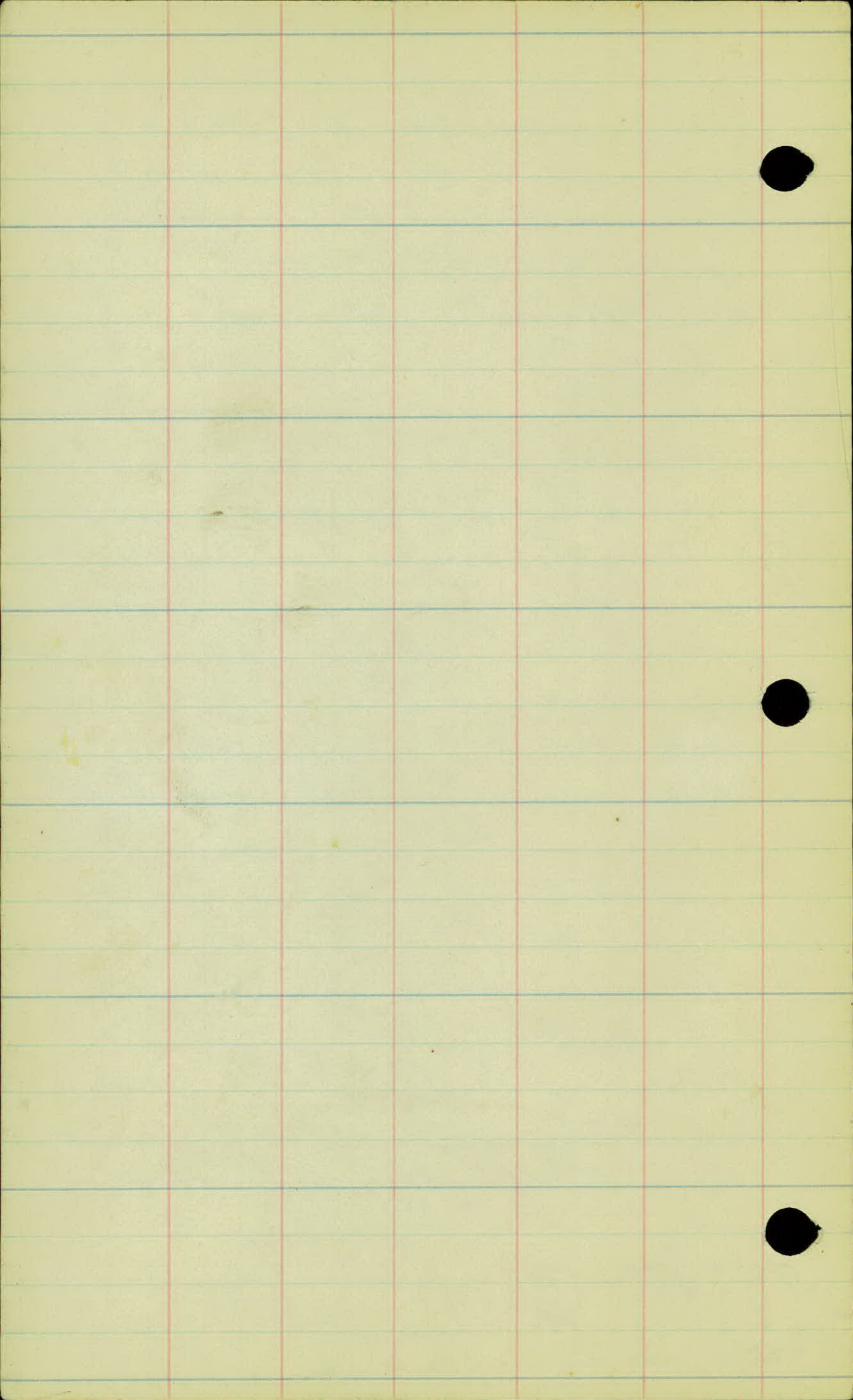




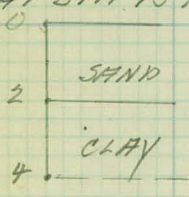
SOUNDING ON  $\phi$   
STA. 30+00.SOUNDING ON  $\phi$   
AT STA. 32+00

STA. 38

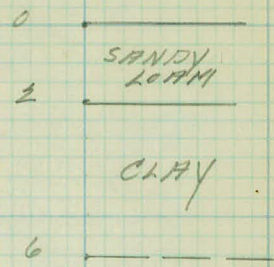
SOUNDING ON  $\phi$   
STA. 38+00SOUNDING ON  $\phi$   
AT STA. 39+00

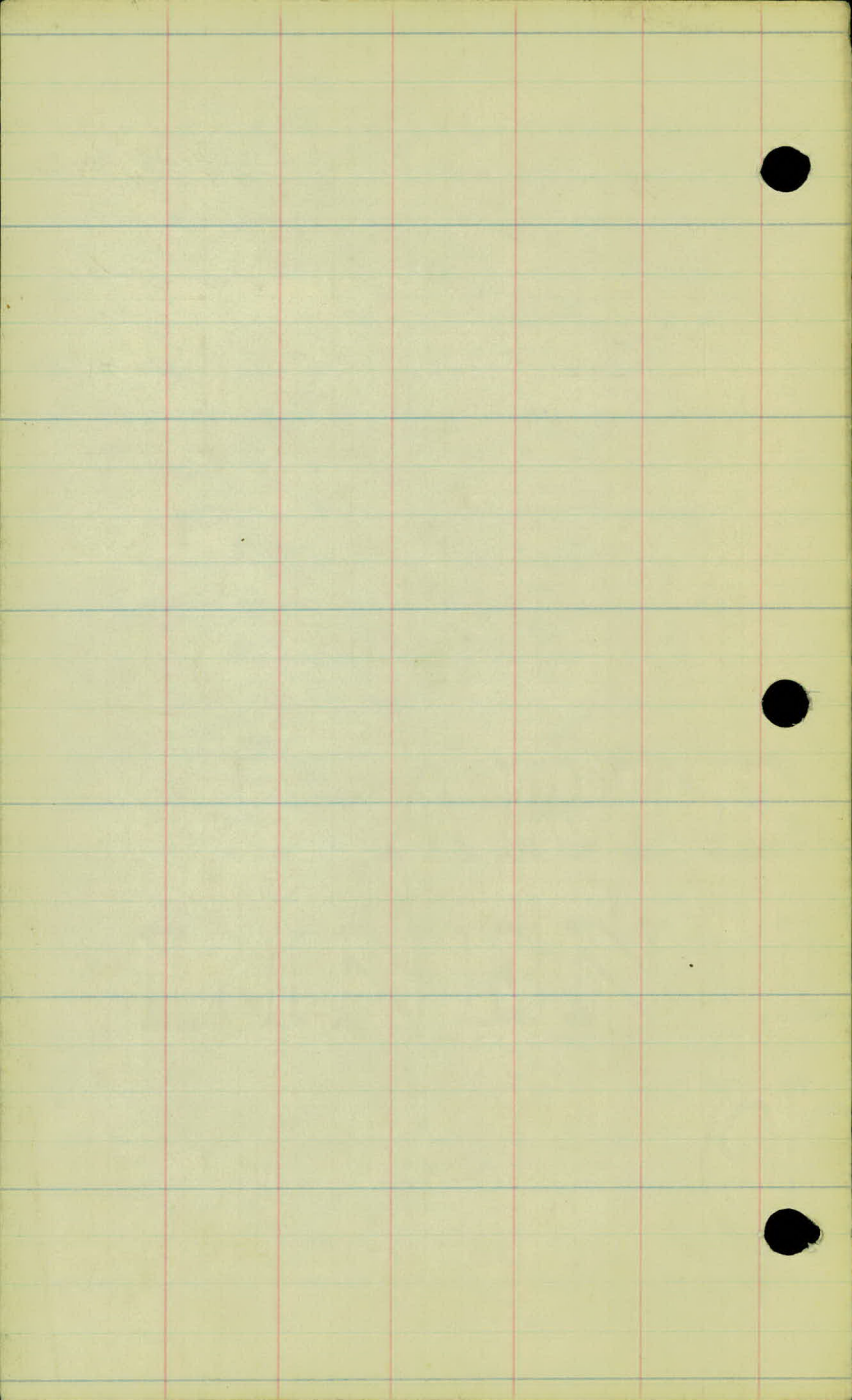


43  
SOUNDING ON  $\phi$   
AT STA 43+00.



SOUNDING ON  $\phi$   
AT STA. 53+00.





PROJ # 29-17

X SECTIONS FOR LINE CHANGE  
FROM STA. 17+00 TO STA. 44+00.

H.I.

13 M. 8.84 287.21 ✓ 878.37  
17 + 00

17 + 50

4.35 279.15 ✓ 12.41 874.80 ✓

18 + 00

19 + 00

20 + 00

21 + 00

22 + 00

12.95 283.46 ✓ 8.64 870.51 ✓

23 + 00

23 + 50

17+00

72.11 73.21 74.3 74.7 79.0 80.9 81.8 81.1 80.5 80.7 79.9 80.2  
300 180 176 167 147 134 100 77 50 33 19

17+50

72.6 73.8 76.2 77.3 77.4 77.0 76.4 76.9 76.5 76.4 76.5 76.1  
300 178 161 151 126 100 83 67 56 33 19

18+00

71.6 71.9 72.2 73.0 75.6 74.2 73.3 72.8 72.7 72.8 73.1 72.4 72.1  
300 273 248 200 164 146 125 92 69 41 33 13

19+00

71.9 71.8 71.8 74.4 74.0 73.2 70.3 69.5 69.2 69.2 69.2  
300 276 244 200 175 155 122 100 73 35

20+00

69.6 71.0 70.8 71.3 71.1 72.0 72.3 71.8 69.2 68.8 68.7 68.8 68.8  
400 382 365 344 300 256 200 191 150 100 67 22

21+00

69.8 69.6 71.1 71.4 71.0 71.5 70.1 69.8 68.8 68.6 68.6 68.9  
400 390 370 300 268 282 207 200 150 100 50

22+00

68.5 69.0 69.9 70.7 70.8 70.5 69.6 69.2 68.4 68.3 68.8 68.7  
500 450 400 350 326 300 250 200 144 100 35

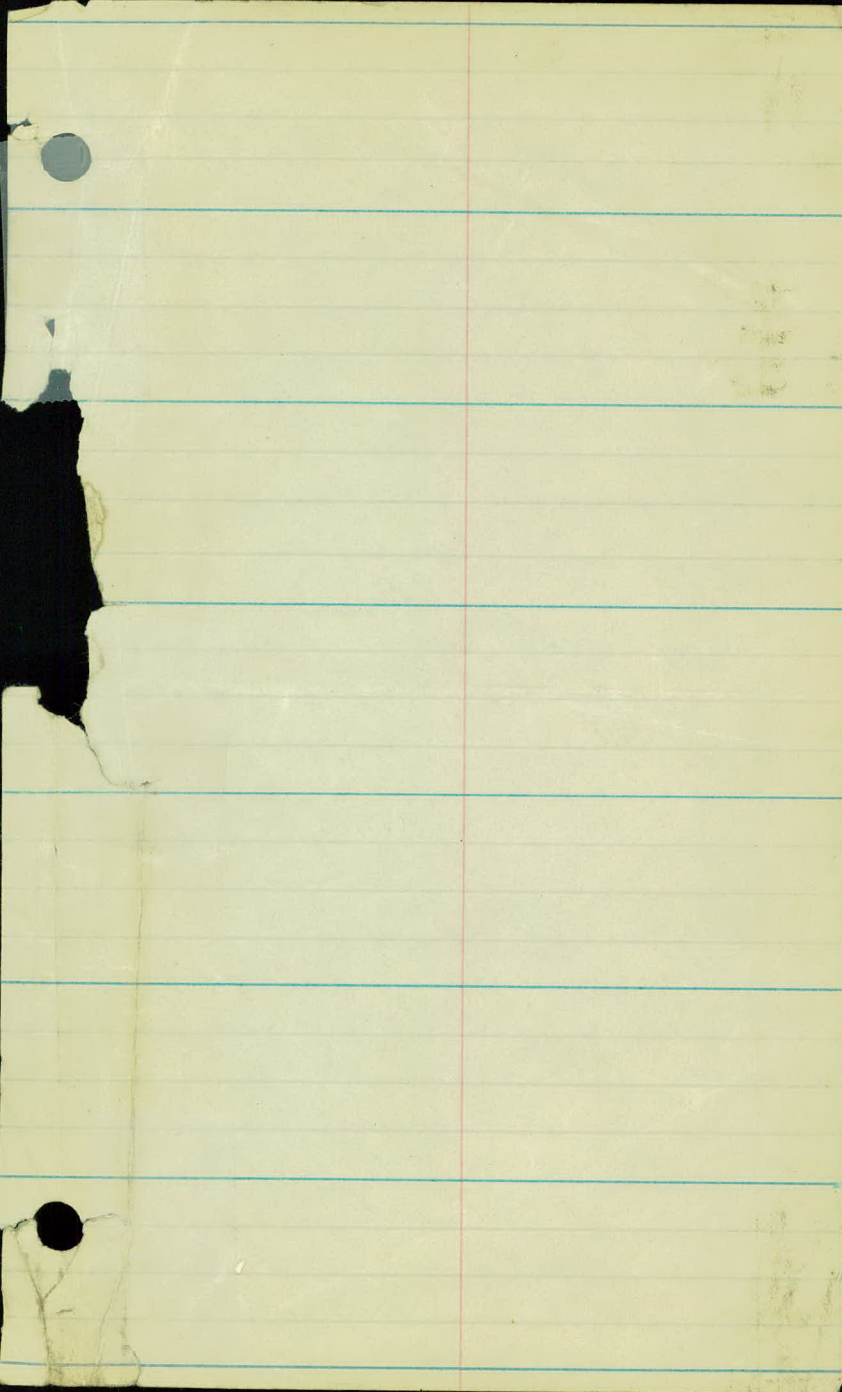
22+00

69.0 69.0 69.8 71.3 71.9 71.8 71.6 71.4 70.6 69.2 68.8 69.0 68.4  
600 547 500 446 400 340 300 243 200 134 100 27

23+50

69.5 69.8 71.0 72.1 73.3 72.7 73.5 73.3 72.7 70.5 69.2 68.8 68.7  
600 548 500 448 400 360 300 338 200 132 100 40

EUGENE DIETZGEN CO., CHICAGO, ILL. WORK NO. 368



A PT

54 <sup>61</sup> 117 P.T.17°-41<sup>5</sup> ✓

5 ✓

17°-25<sup>5</sup> ✓

+50

16°-40<sup>5</sup> ✓

53

X

15°-55<sup>5</sup> ✓

+50

15°-10<sup>5</sup> ✓ ✓

52

14°-25<sup>5</sup> ✓ ✓

+50

13°-40<sup>5</sup> ✓ ✓

51

12°-55<sup>5</sup> ✓ ✓

+50

12°-10<sup>5</sup> ✓ ✓

50

11°-25<sup>5</sup> ✓

+50

10°-40<sup>5</sup> ✓

49

9°-55<sup>5</sup> ✓

+50

9°-10<sup>5</sup> ✓

48

X

8°-25<sup>5</sup> ✓ ✓

+50

7°-40<sup>5</sup> ✓ ✓

47

6°-55<sup>5</sup> ✓ ✓

+50

X

6°-10<sup>5</sup> ✓ ✓

46

5°-25<sup>5</sup> ✓ ✓

+50

4°-40<sup>5</sup> ✓

45

3°-55<sup>5</sup> ✓

+50

3°-10<sup>5</sup> ✓

44

2°-25<sup>5</sup> ✓

+50

1°-40<sup>5</sup> ✓

43

0°-55<sup>5</sup> ✓

+50

0°-10<sup>5</sup> ✓42 + 58 <sup>61</sup> P.C.

0°-00

12.9 14.0 15.1

→ 176 180 200

12.5 8.2 6.3 5.4 6.1 6.7 6.5 7.3

167 147 134 100 77 50 23 19 7.0

10.7 13.4 14.6

→ 161 178 200

9.9 9.8 10.2 10.5 10.3 10.7 10.8 10.7

151 126 100 83 67 56 33 17 11.1

7.3 7.6

→ 273 300

7.0 6.2 3.6 5.0 5.9 6.4 6.5 6.4 6.1 6.8

248 200 174 146 125 94 69 41 23 13 7.1

4.2 7.4 7.4 7.3

→ 200 244 276 300

5.2 6.0 8.9 7.7 10.0 10.0

175 158 122 100 73 25 10.0

8.4 8.2 9.6

→ 365 382 400

7.7 8.1 7.2 6.9 7.4 10.0 10.4 10.5 10.4

348 300 256 200 171 150 100 67 22 10.4

7.3 8.1 7.6 7.4

→ 300 320 390 400

8.2 7.7 9.1 9.4 10.4 10.6 10.6

228 232 307 200 150 100 50 10.3

7.3 10.3 10.7

→ 400 450 500

8.5 8.4 9.2 8.7 9.6 10.0 10.1 10.9 10.4

350 326 316 300 250 200 144 100 35 10.5

14.2 14.5 14.5

→ 500 547 600

12.2 11.6 11.7 11.9 12.1 12.9 14.5 14.7 14.5

446 400 340 300 243 200 134 100 27 15.1

11.4 12.5 13.7 14.0

→ 448 500 548 600

11.2 10.8 10.0 10.2 10.8 13.0 14.3 14.7

400 360 300 238 200 132 100 40 14.8

883.46

24 + 00

24 + 50

25 + 00

25 + 50

26 + 00

26 + 50

13.15 895.22 ✓ 1.39 882.07 ✓

13.26 906.90 ✓ 1.58 893.64 ✓

27 + 00

27 + 50

13.37 919.81 ✓ 0.46 906.74 ✓

12.40 931.33 ✓ 0.68 919.13 ✓

24+00 70.9 71.5 71.6 73.4 74.2 75.9 81.7 81.4 80.1 76.0 72.8 70.5 69.2 68.9  
700 600 552 500 451 400 350 300 250 200 146 100 46 0

+50 72.7 72.5 74.3 75.2 77.5 83.5 86.6 88.8 89.2 89.0 86.2 82.7 80.4 74.4 71.4 69.7 69.0  
700 655 600 546 500 453 436 400 344 300 242 215 200 144 100 50 0

25+00 79.9 77.4 76.2 76.8 76.9 80.7 92.7 95.5 95.2 95.1 94.9 93.4 88.9 81.1 76.7 72.9 70.5 68.5  
800 758 700 650 600 560 500 473 400 356 300 242 200 165 142 100 50 0

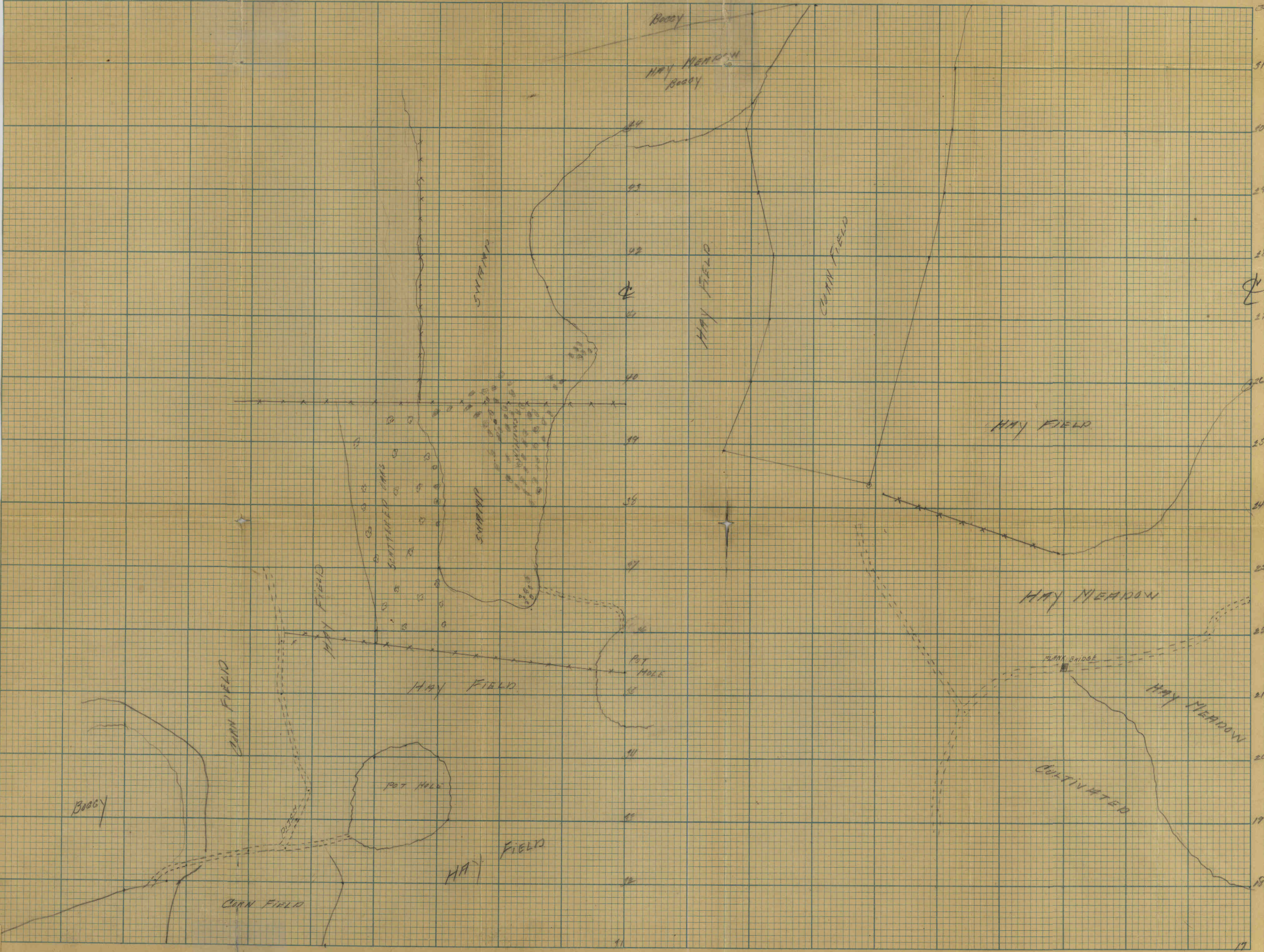
+50 86.2 81.1 79.2 77.2 80.3 82.5 87.5 92.2 99.7 97.1 97.6 96.2 96.7 908.9 901.2 97.8 91.5 85.0 75.6 73.1 69.9  
800 750 700 650 600 582 560 519 500 453 400 354 300 252 223 200 174 148 100 61 0

26+00 90.2 84.5 81.3 80.5 84.0 90.6 95.3 99.2 97.9 97.5 94.6 94.6 99.8 904.7 907.6 904.9 99.9 95.5 86.0 81.9 76.7 73.0  
800 756 700 652 600 566 551 533 500 450 400 347 300 270 236 200 175 150 100 83 50 0

+50 94.3 91.8 89.1 86.0 84.5 86.2 89.3 90.3 93.5 94.2 95.3 96.7 97.4 902.7 911.20 907.6 905.2 900.3 89.9 83.2  
800 780 768 745 700 661 631 600 553 500 454 400 348 300 251 200 144 100 45 0

27+00 99.5 98.2 92.8 97.6 96.5 92.8 94.8 95.6 95.5 02.9 10.0 14.7 12.9 13.4 14.0 09.7 01.9 99.1 94.5  
800 742 700 645 600 545 500 450 400 340 300 255 217 200 142 100 65 40 0

+50 03.4 00.4 01.8 02.5 05.0 03.4 02.6 00.9 02.8 05.1 09.5 14.4 15.2 15.9 18.7 19.1 15.6 11.9 08.3  
800 759 700 649 600 588 500 448 400 363 333 300 242 200 160 131 100 56 0



17  
18  
19

TOPOGRAPHY

12.6 12.0 11.9 10.1 9.3 4.6 1.7 2.1 3.4 7.5 10.7 13.0 14.3  
700 600 552 500 451 400 350 300 250 200 146 100 46 14.6

PROVA HI

10.8 11.0 9.2 8.3 6.0 0.0 +3.1 +5.3 +5.7 +5.3 +2.7 0.8 3.1 9.1 12.1 13.8  
700 655 600 544 500 453 426 400 344 300 242 215 200 144 100 50 14.5

3.6 0.1 7.9 6.7 6.6 2.8 +9.2 +12.0 +11.7 +11.6 +11.4 +10.4 +5.4 2.4 0.8 10.6 13.0  
800 758 700 650 600 540 500 471 400 356 300 242 200 165 142 100 50 15.0

+2.7 2.4 5.2 6.2 3.2 1.0 +4.0 +14.7 +16.2 +13.6 +14.1 +12.7 +12.2 +19.4 +17.7 +16.3 +8.0  
800 750 700 650 600 582 560 519 500 453 400 354 300 253 228 200 174  
→ +1.5 7.7 10.4  
148 100 61 13.6

+15.7 +14.4 +14.0 +11.1 +11.1 +10.3 +20.7 +24.0 +21.4 +16.4 +12.0 +2.5 1.6 6.8  
533 500 450 400 347 310 270 236 200 175 150 100 83 50 10.5  
→ +11.8 +7.1 +2.5 3.0 2.2 +1.0 4.8  
551 506 600 652 700 756 800

+10.0 +6.8 +5.8 +2.8 +1.0 +2.5 +5.0 +2.3 +10.8  
553 600 631 661 700 745 768 780 800  
→ +10.7 +11.8 +13.2 +13.7 +21.4 +22.8 +24.1 +21.7 +16.8 +6.4  
500 454 400 348 300 251 200 144 100 45 0.3

10.4 13.1 12.1 11.3 11.4 4.0 +3.1 +7.8 +6.0 +5.5 +7.1 +2.8 5.0 7.9  
600 525 500 450 400 340 300 255 217 200 142 100 65 40 12.4  
→ 9.3 14.1 13.6 7.4  
645 700 742 800

6.0 4.3 5.3 1.7 4.4 5.1 6.5 3.3  
448 500 538 600 647 700 759 800  
→ 4.1 1.8 +2.6 +7.5 +2.4 +9.0 +11.8 +12.2 +8.7 +5.0  
400 363 333 300 242 200 160 131 100 56 +14

931.33

28+00

28+50

1.58 932.08 ✓ 0.83 930.50 ✓

B.M.

0.47 931.61 ✓ 931.61

29+00

29+50

30+00

30+50

6.27 927.55 ✓ 10.80 921.28 ✓

31+00

2400  $\frac{07.5}{800}$   $\frac{06.0}{763}$   $\frac{08.7}{781}$   $\frac{09.7}{700}$   $\frac{09.4}{657}$   $\frac{08.1}{600}$   $\frac{14.4}{550}$   $\frac{12.7}{500}$   $\frac{13.4}{454}$   $\frac{10.9}{400}$   $\frac{11.4}{363}$   $\frac{14.5}{336}$   $\frac{17.3}{300}$   $\frac{15.8}{240}$   $\frac{17.9}{200}$   $\frac{18.8}{155}$   $\frac{18.6}{124}$   $\frac{19.9}{100}$   $\frac{23.1}{50}$   $\frac{24.9}{25}$   $\frac{25.0}{12}$   $\frac{25.0}{0}$

+50  $\frac{07.7}{800}$   $\frac{08.6}{770}$   $\frac{16.7}{700}$   $\frac{19.2}{667}$   $\frac{12.5}{600}$   $\frac{11.4}{593}$   $\frac{12.9}{564}$   $\frac{20.2}{526}$   $\frac{21.5}{500}$   $\frac{21.6}{450}$   $\frac{18.4}{400}$   $\frac{19.0}{348}$   $\frac{19.0}{300}$   $\frac{18.1}{259}$   $\frac{20.5}{200}$   $\frac{19.8}{149}$   $\frac{21.8}{100}$   $\frac{24.6}{57}$   $\frac{26.1}{33}$   $\frac{28.3}{0}$

2900  $\frac{05.1}{850}$   $\frac{03.6}{800}$   $\frac{07.1}{768}$   $\frac{14.2}{729}$   $\frac{19.1}{700}$   $\frac{21.7}{682}$   $\frac{21.4}{656}$   $\frac{13.9}{600}$   $\frac{13.9}{576}$   $\frac{14.9}{549}$   $\frac{20.9}{524}$   $\frac{23.8}{500}$   $\frac{22.5}{447}$   $\frac{21.6}{423}$   $\frac{21.2}{400}$   $\frac{20.2}{367}$   $\frac{19.3}{334}$   $\frac{18.2}{300}$   $\frac{18.9}{249}$   $\frac{21.6}{200}$   $\frac{20.6}{158}$   $\frac{20.2}{137}$   $\frac{23.0}{100}$   
 $\frac{26.0}{50}$   $\frac{28.2}{20}$   $\frac{31.4}{0}$

+50  $\frac{00.4}{800}$   $\frac{03.5}{767}$   $\frac{07.8}{740}$   $\frac{18.1}{700}$   $\frac{21.8}{671}$   $\frac{20.1}{644}$   $\frac{18.1}{600}$   $\frac{14.1}{576}$   $\frac{13.4}{545}$   $\frac{12.9}{522}$   $\frac{22.1}{500}$   $\frac{23.4}{466}$   $\frac{24.4}{416}$   $\frac{24.8}{400}$   $\frac{23.6}{371}$   $\frac{21.5}{334}$   $\frac{19.8}{300}$   $\frac{19.3}{260}$   $\frac{21.1}{200}$   $\frac{20.2}{172}$   $\frac{20.7}{152}$   $\frac{26.1}{100}$   $\frac{26.3}{66}$   $\frac{27.2}{37}$   $\frac{28.3}{28}$   $\frac{32.1}{0}$

3000  $\frac{91.5}{850}$   $\frac{94.1}{800}$   $\frac{89.5}{762}$   $\frac{83.1}{753}$   $\frac{68.1}{725}$   $\frac{14.1}{700}$   $\frac{30.0}{668}$   $\frac{17.8}{640}$   $\frac{14.9}{600}$   $\frac{12.3}{568}$   $\frac{11.4}{546}$   $\frac{13.1}{528}$   $\frac{18.4}{500}$   $\frac{22.9}{474}$   $\frac{24.6}{450}$   $\frac{26.5}{400}$   $\frac{23.8}{360}$   $\frac{21.8}{335}$   $\frac{20.7}{300}$   $\frac{19.1}{250}$   $\frac{18.5}{200}$   $\frac{20.5}{153}$   $\frac{24.9}{100}$   $\frac{27.3}{50}$   
 $\frac{27.2}{25}$   $\frac{31.3}{0}$

+50  $\frac{88.1}{850}$   $\frac{88.2}{800}$   $\frac{91.8}{756}$   $\frac{83.1}{713}$   $\frac{66.1}{700}$   $\frac{13.6}{668}$   $\frac{16.6}{641}$   $\frac{16.9}{618}$   $\frac{15.4}{600}$   $\frac{10.9}{558}$   $\frac{13.1}{526}$   $\frac{18.5}{500}$   $\frac{21.8}{470}$   $\frac{24.7}{429}$   $\frac{24.5}{400}$   $\frac{20.9}{337}$   $\frac{18.5}{300}$   $\frac{17.3}{239}$   $\frac{17.8}{200}$   $\frac{19.3}{148}$   $\frac{22.1}{100}$   $\frac{24.5}{62}$   $\frac{26.1}{34}$   $\frac{29.8}{0}$

3100  $\frac{87.9}{800}$   $\frac{88.9}{756}$   $\frac{92.1}{724}$   $\frac{98.9}{700}$   $\frac{8.8}{668}$   $\frac{12.5}{640}$   $\frac{12.7}{600}$   $\frac{09.6}{567}$   $\frac{09.8}{545}$   $\frac{11.7}{523}$   $\frac{17.2}{500}$   $\frac{20.7}{471}$   $\frac{19.2}{428}$   $\frac{20.0}{400}$   $\frac{23.0}{345}$   $\frac{21.6}{300}$   $\frac{18.9}{242}$   $\frac{18.8}{200}$   $\frac{19.4}{150}$   $\frac{19.6}{100}$   $\frac{21.1}{50}$   $\frac{23.3}{23}$   $\frac{24.2}{0}$

186 169 23.2 21.9 21.6 22.6 25.3 23.8  
 500 550 600 657 700 731 753 800  
 179 204 19.9 16.8 14.0 15.5 13.4 12.5 12.7 11.4 8.2 6.4 6.3  
 754 400 363 391 300 240 200 155 124 100 50 25 12 6.8

77 12.9 12.3 12.3 13.2 10.8 11.5 7.5 6.7 5.2  
 450 400 348 300 259 200 149 100 57 2.9 3.0  
 78 111 124 129 153 120 146 227 23.6  
 500 526 524 599 600 667 700 770 800

172 112 8.3 7.6 10.5 10.9 11.9 12.8 13.9 13.2 10.5 11.5 11.2 8.5 6.1 3.9  
 549 524 500 447 423 400 367 334 300 249 200 158 137 100 50 20 0.7  
 12.2 12.9 10.7 10.4 13.0 17.9 25.0 22.5 27.0  
 576 600 656 682 700 727 768 800 850

142 127 120 140 120 103 140 22.3 22.6 31.7  
 522 545 576 600 641 671 700 740 767 500  
 100 87 7.7 7.9 8.5 10.6 12.3 12.8 11.0 11.8 11.4 6.0 5.8 4.7 3.8  
 500 466 416 400 371 334 300 260 200 172 152 100 66 37 28 0.0

178 20.7 190 137 7.3 7.5 5.6 8.3 10.3 11.4 12.0 13.6 11.6 7.2 4.8 4.9  
 568 546 528 500 474 450 400 360 335 300 250 200 153 100 50 25 0.8  
 12.2 14.3 12.1 18.0 24.0 27.0 31.6 38.0 40.6  
 600 640 668 700 735 753 762 800 850

10.3 7.4 7.6 11.2 13.6 14.8 14.3 12.3 12.0 7.6 6.0  
 470 429 400 337 300 239 200 148 100 62 34 2.3  
 13.6 120 21.2 16.7 15.2 15.5 19.5 26.0 27.0 40.3 42.5 43.0  
 500 526 558 600 618 641 668 700 713 756 800 850

180 17.9 15.9 10.4 6.9 8.4 7.6 4.6 6.0 8.7 8.8 8.0 8.0 6.5 4.3  
 567 545 523 500 471 428 400 345 300 242 200 150 100 50 23 1.4  
 149 15.1 18.8 28.7 35.5 38.7 39.7  
 600 640 668 700 724 756 800

727.55

31750

32700

32750

2.46 919.00 ✓ 11.01 916.54 ✓

33700

33750

34700

34750

3.26 919.80 ✓ 2.46 916.54 ✓

31+50

87.9	88.9	92.7	98.7	06.7	06.6	04.9	08.6	14.2	16.6	18.3	22.2	23.6	24.7	33.5	20.8	19.4	19.6	21.6	21.6
800	750	700	665	612	600	550	500	450	400	373	338	300	255	200	153	100	50	6	0

24+00

88.5	88.7	90.6	91.3	95.7	98.8	98.6	01.9	06.6	09.8	11.9	13.8	18.9	22.4	22.6	23.0	21.9	20.7	19.9	21.2	21.7
800	770	728	700	655	600	550	500	442	421	400	350	300	253	200	167	142	100	40	8	0

+50

88.8	90.3	92.7	95.1	96.6	95.7	99.0	00.8	00.3	01.5	03.6	10.1	15.3	18.2	19.2	20.2	19.2	19.3
800	747	700	650	600	553	500	446	400	365	337	300	254	200	152	100	41	0

33+00

88.8	92.0	94.4	90.4	00.5	00.4	99.6	98.4	98.4	99.0	99.8	04.7	09.1	12.1	15.4	17.5	15.9	15.3
800	700	646	600	555	500	455	426	400	350	300	258	200	153	100	50	20	0

33+50

88.8	91.8	97.2	03.2	06.6	01.6	00.9	03.0	00.3	98.6	98.3	99.1	00.9	05.5	08.8	12.7	16.3	13.10	12.5
800	700	672	650	600	541	500	470	433	400	353	300	262	200	149	100	57	17	0

34+00

02.1	02.0	03.7	00.3	00.5	02.8	99.3	99.3	02.2	07.1	10.4	12.3	15.5	12.4	09.6	08.9
670	660	600	550	500	460	400	361	300	257	200	147	100	52	24	0

34+50

04.9	02.2	07.9	01.4	99.9	99.5	02.5	02.4	06.2	11.5	14.5	18.0	20.2	16.5	06.9	04.2
700	683	660	600	548	500	452	400	344	300	250	200	144	100	47	0



919.80

35+00

35+50

36+00

36+50

37+00

37+50

38+00

38+50

3.42 917.77 ✓ 5.45 914.35 ✓

39+00

39+50

40+00

40+50

41+00

25400  $\frac{00.2}{600}$   $\frac{99.6}{555}$   $\frac{99.7}{500}$   $\frac{02.9}{452}$   $\frac{06.6}{400}$   $\frac{11.1}{255}$   $\frac{11.2}{300}$   $\frac{11.8}{252}$   $\frac{13.8}{300}$   $\frac{15.2}{153}$   $\frac{12.2}{100}$   $\frac{08.7}{71}$   $\frac{04.9}{43}$   $\frac{03.5}{0}$

35450  $\frac{01.3}{600}$   $\frac{00.5}{555}$   $\frac{00.5}{500}$   $\frac{05.5}{455}$   $\frac{12.5}{420}$   $\frac{12.5}{400}$   $\frac{10.7}{262}$   $\frac{07.8}{300}$   $\frac{10.2}{240}$   $\frac{10.0}{200}$   $\frac{08.3}{137}$   $\frac{06.4}{100}$   $\frac{04.6}{55}$   $\frac{04.2}{0}$

36400  $\frac{17.1}{400}$   $\frac{14.6}{350}$   $\frac{10.9}{300}$   $\frac{8.2}{244}$   $\frac{06.8}{200}$   $\frac{05.9}{152}$   $\frac{04.5}{100}$   $\frac{05.2}{40}$   $\frac{04.0}{0}$

+50  $\frac{21.9}{350}$   $\frac{05.6}{300}$   $\frac{04.1}{289}$   $\frac{01.9}{260}$   $\frac{01.5}{300}$   $\frac{01.9}{165}$   $\frac{02.7}{150}$   $\frac{03.1}{100}$   $\frac{04.8}{54}$   $\frac{04.0}{0}$

37400  $\frac{10.8}{333}$   $\frac{06.2}{320}$   $\frac{01.9}{300}$   $\frac{01.2}{280}$   $\frac{00.8}{250}$   $\frac{00.8}{200}$   $\frac{01.6}{147}$   $\frac{02.5}{143}$   $\frac{04.6}{100}$   $\frac{07.9}{50}$   $\frac{07.2}{15}$   $\frac{07.7}{0}$

37450  $\frac{11.8}{335}$   $\frac{05.0}{318}$   $\frac{02.1}{300}$   $\frac{01.2}{288}$   $\frac{00.9}{250}$   $\frac{00.9}{200}$   $\frac{00.9}{175}$   $\frac{01.4}{150}$   $\frac{02.5}{140}$   $\frac{03.3}{136}$   $\frac{07.3}{100}$   $\frac{11.4}{65}$   $\frac{13.4}{53}$   $\frac{13.8}{10}$   $\frac{13.0}{0}$

38400  $\frac{08.9}{322}$   $\frac{04.8}{312}$   $\frac{02.7}{300}$   $\frac{01.2}{280}$   $\frac{00.9}{250}$   $\frac{00.9}{200}$   $\frac{01.6}{160}$   $\frac{02.9}{139}$   $\frac{04.8}{129}$   $\frac{05.1}{125}$   $\frac{10.0}{100}$   $\frac{13.9}{82}$   $\frac{14.6}{56}$   $\frac{16.7}{16}$   $\frac{17.8}{0}$

+50  $\frac{10.6}{322}$   $\frac{07.1}{312}$   $\frac{03.6}{300}$   $\frac{02.1}{290}$   $\frac{01.0}{262}$   $\frac{00.7}{200}$   $\frac{01.5}{162}$   $\frac{01.7}{150}$   $\frac{04.7}{127}$   $\frac{09.8}{100}$   $\frac{14.0}{80}$   $\frac{16.5}{40}$   $\frac{18.4}{0}$

39400  $\frac{08.0}{325}$   $\frac{02.2}{300}$   $\frac{00.7}{250}$   $\frac{00.8}{200}$   $\frac{00.8}{160}$   $\frac{02.5}{130}$   $\frac{01.4}{125}$   $\frac{06.8}{100}$   $\frac{12.7}{71}$   $\frac{15.7}{37}$   $\frac{16.8}{0}$

450  $\frac{05.9}{333}$   $\frac{02.1}{312}$   $\frac{01.6}{300}$   $\frac{00.9}{255}$   $\frac{00.7}{200}$   $\frac{01.2}{162}$   $\frac{01.8}{124}$   $\frac{02.3}{117}$   $\frac{03.5}{100}$   $\frac{08.8}{55}$   $\frac{11.3}{33}$   $\frac{13.4}{0}$

40400  $\frac{00.8}{300}$   $\frac{00.8}{200}$   $\frac{00.9}{150}$   $\frac{01.3}{100}$   $\frac{03.9}{42}$   $\frac{06.1}{0}$

+50  $\frac{00.8}{200}$   $\frac{00.9}{150}$   $\frac{01.7}{100}$   $\frac{01.9}{52}$   $\frac{03.7}{0}$

41400  $\frac{00.8}{200}$   $\frac{00.9}{150}$   $\frac{03.2}{100}$   $\frac{03.8}{50}$   $\frac{05.4}{0}$

ERIKER DRITZEN CO. CHICAGO, ILL. PHONE NO. 362

$\frac{19.5}{600} \frac{20.2}{555} \frac{20.1}{500} \frac{16.9}{452} \frac{13.2}{400} \frac{8.1}{355} \frac{8.6}{300} \frac{8.0}{252} \frac{6.0}{200} \frac{4.6}{153} \frac{7.6}{100} \frac{11.1}{71} \frac{14.9}{45} \quad 16.3$

$\frac{18.5}{600} \frac{19.3}{555} \frac{19.3}{500} \frac{14.3}{455} \frac{7.3}{420} \frac{7.3}{400} \frac{7.1}{362} \frac{13.0}{300} \frac{7.5}{240} \frac{7.8}{200} \frac{11.6}{137} \frac{13.4}{100} \frac{15.2}{55} \quad 15.0$

$\frac{2.7}{400} \frac{5.2}{350} \frac{8.9}{300} \frac{11.6}{248} \frac{13.0}{200} \frac{13.9}{152} \frac{15.3}{100} \frac{14.6}{40} \quad 15.8$

$\frac{7.2.1}{350} \frac{14.2}{300} \frac{15.7}{289} \frac{17.9}{260} \frac{18.3}{200} \frac{17.9}{165} \frac{17.1}{150} \frac{16.7}{100} \frac{15.0}{54} \quad 15.8$

$\frac{9.0}{333} \frac{13.6}{320} \frac{17.9}{300} \frac{18.6}{280} \frac{19.0}{250} \frac{19.0}{200} \frac{18.2}{147} \frac{17.2}{143} \frac{15.2}{100} \frac{11.9}{50} \frac{12.6}{15} \quad 12.1$

$\frac{8.0}{335} \frac{14.8}{318} \frac{17.7}{300} \frac{18.6}{288} \frac{18.9}{250} \frac{18.9}{200} \frac{18.4}{175} \frac{17.5}{150} \frac{16.5}{140} \frac{12.5}{136} \frac{8.4}{100} \frac{6.4}{65} \frac{6.0}{53} \frac{6.0}{10} \quad 6.8$

$\frac{10.9}{322} \frac{15.0}{312} \frac{17.1}{300} \frac{18.5}{280} \frac{18.9}{250} \frac{18.9}{200} \frac{18.2}{160} \frac{16.9}{139} \frac{15.0}{129} \frac{14.7}{125} \frac{7.8}{100} \frac{6.9}{82} \frac{5.2}{56} \frac{3.1}{16} \quad 2.0$

$\frac{9.2}{322} \frac{12.7}{312} \frac{16.2}{300} \frac{17.7}{290} \frac{18.8}{262} \frac{19.1}{200} \frac{18.3}{162} \frac{18.1}{130} \frac{15.1}{127} \frac{10.0}{100} \frac{5.8}{80} \frac{3.3}{40} \quad 1.4$

$\frac{9.8}{325} \frac{15.6}{300} \frac{17.1}{250} \frac{17.0}{200} \frac{17.0}{160} \frac{15.5}{130} \frac{16.4}{125} \frac{11.0}{100} \frac{5.1}{71} \frac{2.1}{37} \quad 1.0$

$\frac{11.9}{333} \frac{15.7}{312} \frac{16.2}{300} \frac{16.9}{255} \frac{17.1}{200} \frac{16.6}{162} \frac{16.0}{124} \frac{15.5}{117} \frac{14.3}{100} \frac{9.0}{35} \frac{6.5}{23} \quad 4.4$

$\frac{17.0}{300} \frac{17.0}{200} \frac{16.9}{150} \frac{16.5}{100} \frac{13.9}{42} \quad 11.7$

$\frac{17.0}{200} \frac{16.9}{150} \frac{16.1}{100} \frac{15.9}{52} \quad 14.1$

$\frac{17.0}{200} \frac{16.9}{150} \frac{14.6}{100} \frac{14.0}{50} \quad 14.4$

917.77

41 + 50

42 + 00

42 + 50

43 + 00

43 + 50

44 + 00

B.M.

9.29 908.48 ✓ 908.46

$$41+50 \quad \frac{00.8}{200} \quad \frac{01.2}{150} \quad \frac{03.1}{114} \quad \frac{04.6}{100} \quad \frac{07.2}{75} \quad \frac{06.6}{40} \quad \frac{04.8}{0}$$

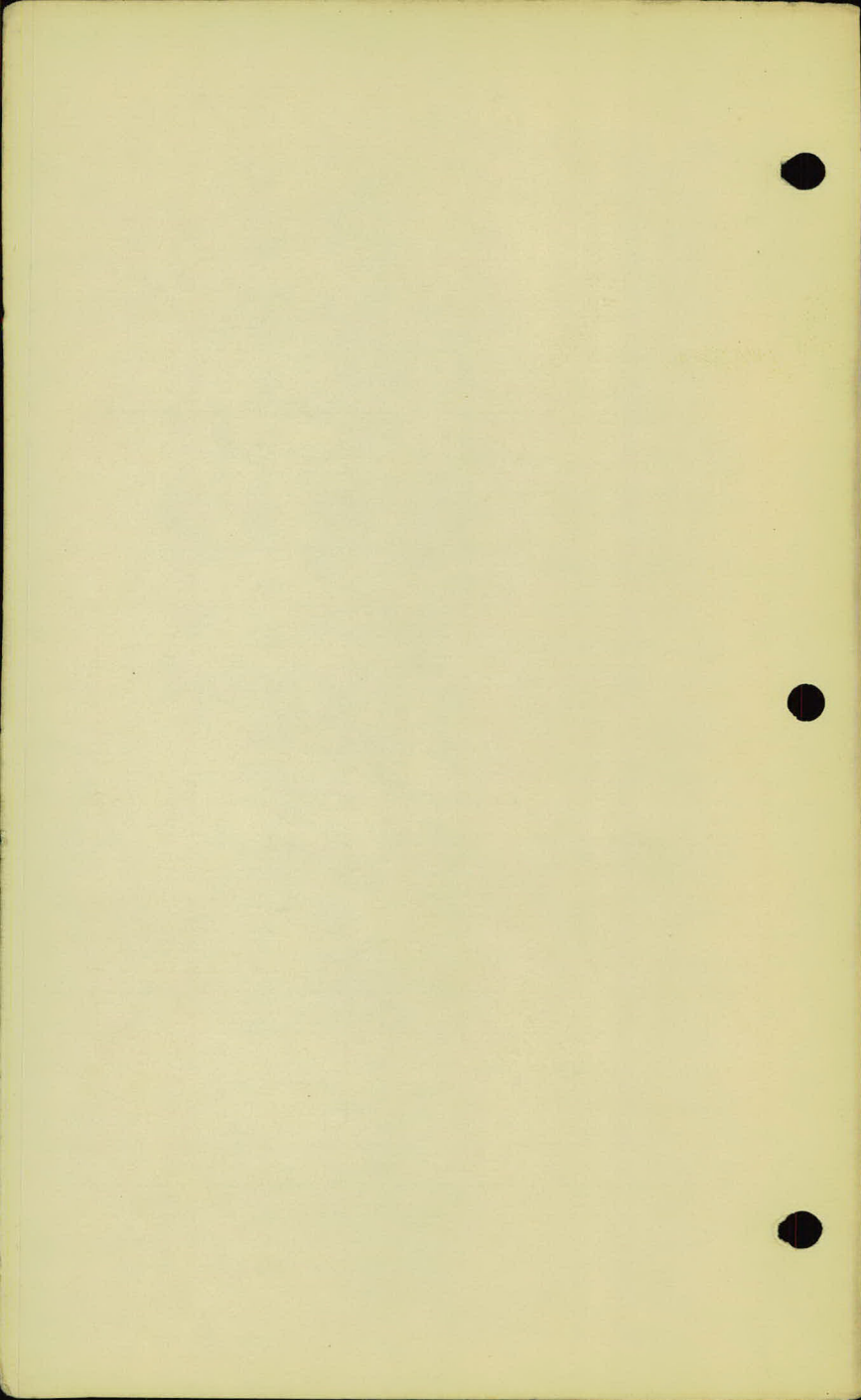
$$42+00 \quad \frac{00.8}{200} \quad \frac{01.8}{154} \quad \frac{04.0}{130} \quad \frac{05.8}{117} \quad \frac{08.2}{100} \quad \frac{09.3}{63} \quad \frac{08.0}{37} \quad \frac{06.6}{0}$$

$$+50 \quad \frac{00.8}{200} \quad \frac{01.8}{150} \quad \frac{04.6}{124} \quad \frac{07.6}{100} \quad \frac{07.6}{50} \quad \frac{08.9}{0}$$

$$43+00 \quad \frac{00.8}{200} \quad \frac{01.6}{150} \quad \frac{02.4}{100} \quad \frac{04.7}{68} \quad \frac{06.8}{40} \quad \frac{08.2}{0}$$

$$+50 \quad \frac{00.8}{150} \quad \frac{01.2}{100} \quad \frac{02.6}{30} \quad \frac{05.9}{0}$$

$$44+00 \quad \frac{00.8}{150} \quad \frac{01.0}{100} \quad \frac{01.4}{50} \quad \frac{01.9}{0}$$



$\frac{17.0}{200}$	$\frac{166}{150}$	$\frac{14.7}{114}$	$\frac{13.2}{100}$	$\frac{10.6}{73}$	$\frac{11.2}{40}$		
							13.0

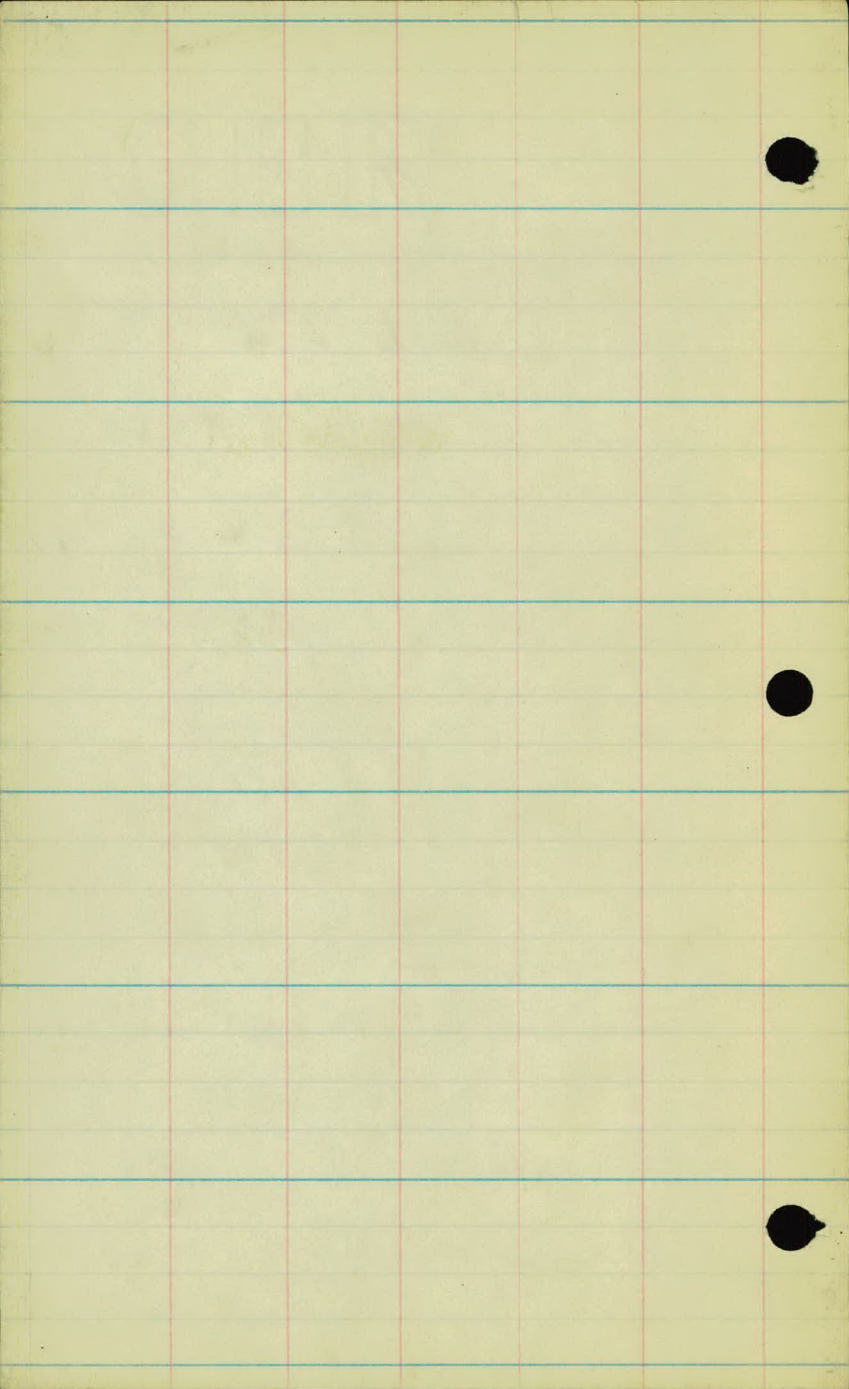
$\frac{17.0}{200}$	$\frac{160}{154}$	$\frac{13.8}{30}$	$\frac{12.0}{117}$	$\frac{9.6}{100}$	$\frac{8.5}{63}$	$\frac{9.8}{37}$	
							11.2

$\frac{17.0}{200}$	$\frac{160}{150}$	$\frac{13.2}{124}$	$\frac{10.2}{100}$	$\frac{10.2}{50}$			
							9.1

$\frac{17.0}{200}$	$\frac{162}{150}$	$\frac{15.4}{100}$	$\frac{13.1}{68}$	$\frac{11.0}{40}$			
							9.6

$\frac{17.0}{150}$	$\frac{166}{100}$	$\frac{15.2}{30}$					
							11.9

$\frac{17.0}{150}$	$\frac{168}{100}$	$\frac{16.4}{500}$					
							15.9



PROJ# 29-17

LINE REVISION FROM STA.  
12+16<sup>19</sup> TO STA. 54+17<sup>81</sup>

STA POINT Δ LT. Δ RT.

$18+62$ <sup>86</sup> ✓ P.T.  $16^{\circ}-10'$   
 $+50$   $15^{\circ}-51'$   
 $18$   $14^{\circ}-36'$   
 $+50$   $13^{\circ}-21'$   
 $17$   $12^{\circ}-06'$   
 $+50$   $10^{\circ}-51'$   
 $16$   $9^{\circ}-36'$   
 $+50$   $8^{\circ}-21'$

$15+48$ <sup>50</sup> P.I. Δ- $32^{\circ}-20'$   
 $15$   $7^{\circ}-06'$  D- $5^{\circ}$  LT.  
 $+50$   $5^{\circ}-51'$  T- $332$ <sup>31</sup> ✓  
 $14$   $4^{\circ}-36'$  L- $646$ <sup>67</sup> ✓  
 $+50$   $3^{\circ}-21'$  R- $1146$ <sup>28</sup> ✓  
 $13$   $2^{\circ}-06'$   
 $+50$  ✓  $0^{\circ}-51'$

$12+16$ <sup>19</sup> ✓ P.C.  $0^{\circ}-00'$   
 $12+15$ <sup>50</sup>

$13+17$ <sup>8</sup> P.O.T.

$0+00$

2-11-29

62.80  
32.2  
7506

F. 10 Pass.

75

29° 50' 12" N

521

1000

81° 43'



.

.

.

STA. POINT A RT. Δ RT.

28+99<sup>9</sup> ✓ P.T. 20°-05'

+50 - 19°-05'

28 ✓ 18°-05'

+50 - 17°-05'

27 ✓ 16°-05'

+50 ✓ 15°-05'

26 ✓ 14°-05'

+50 - 13°-05'

25 - 12°-05'

+50 ✓ 11°-05'

24+19<sup>55</sup> P.I.

24 ✓ 10°-05'

+50 ✓ 9°-05'

23 ✓ 8°-05'

+50 ✓ 7°-05'

22 ✓ 6°-05'

+50 ✓ 5°-05'

21 - 4°-05'

+50 ✓ 3°-05'

20 ✓ 2°-05'

+50 ✓ 1°-05'

19 ✓ 0°-05'

18+95<sup>73</sup> ✓ P.C. 0°-00'

Δ-40°-10

D-4°-R.

T-523<sup>82</sup> ✓

L-1004<sup>17</sup> ✓

R-1432<sup>69</sup> ✓

2-11-29

70

8 10" 70

0

70 7 X

STA POINT Δ LT Δ RT.

37+11	<sup>38</sup> ✓ P.T.		5°-16	
	39		5°-02	
	+50		4°-02	
	38		3°-02	
37+80	<sup>12</sup> P.I.			Δ-10°-32
	+50		2°-02	D-4°-R.
	37		1°-02	T-132 <sup>07</sup> ✓
	+50		0°-02	L-263 <sup>33</sup> ✓
36+48	<sup>05</sup> ✓ P.C.		0°-00	R-1432 <sup>69</sup> ✓

36+45	<sup>85</sup> ✓ P.T.	8°-15		
	36	7°-20		
	+50	6°-20		
	35	5°-20		
	+50	4°-20		
34+41	<sup>08</sup> P.I.			Δ-16°-30
	34	3°-20		D-4°-L.
	+50	2°-20		T-207 <sup>73</sup> ✓
	33	1°-20		L-412 <sup>50</sup> ✓
	+50	0°-20		R-1432 <sup>69</sup> ✓
32+33	<sup>35</sup> ✓ P.C.	0°-00		

Boat Spike

ADAN  
53

60

Boat Spike

Boat Spike

Boat Spike

CENTER LIGHTING ROD  
ON BARN.



80

106.10

99.80



STA. POINT ALT DIST.

53 + 65<sup>83</sup>

54 + 17<sup>81</sup> P.T. =

54	17°-41 <sup>5</sup>
53	17°-25 <sup>5</sup>
52	15°-55 <sup>5</sup>
51	14°-25 <sup>5</sup>
50	12°-55 <sup>5</sup>
49	11°-25 <sup>5</sup>
48	9°-55 <sup>5</sup>

48 + 47<sup>65</sup> P.I.

48	8°-25 <sup>5</sup>
47	6°-55 <sup>5</sup>
46	5°-25 <sup>5</sup>
45	4°-55 <sup>5</sup>
44	2°-25 <sup>5</sup>
43	0°-55 <sup>5</sup>

42 + 38<sup>37</sup> P.C.

0°-00

Δ-35°-23

D-3°-R

T-609<sup>28</sup>

L-1179<sup>44</sup>

R-1910<sup>08</sup>

40 + 17.78 P.O.T.

10" OAK

⊙

55°

51 22

⊙ 10" OAK

⊙ 24" OAK

80°

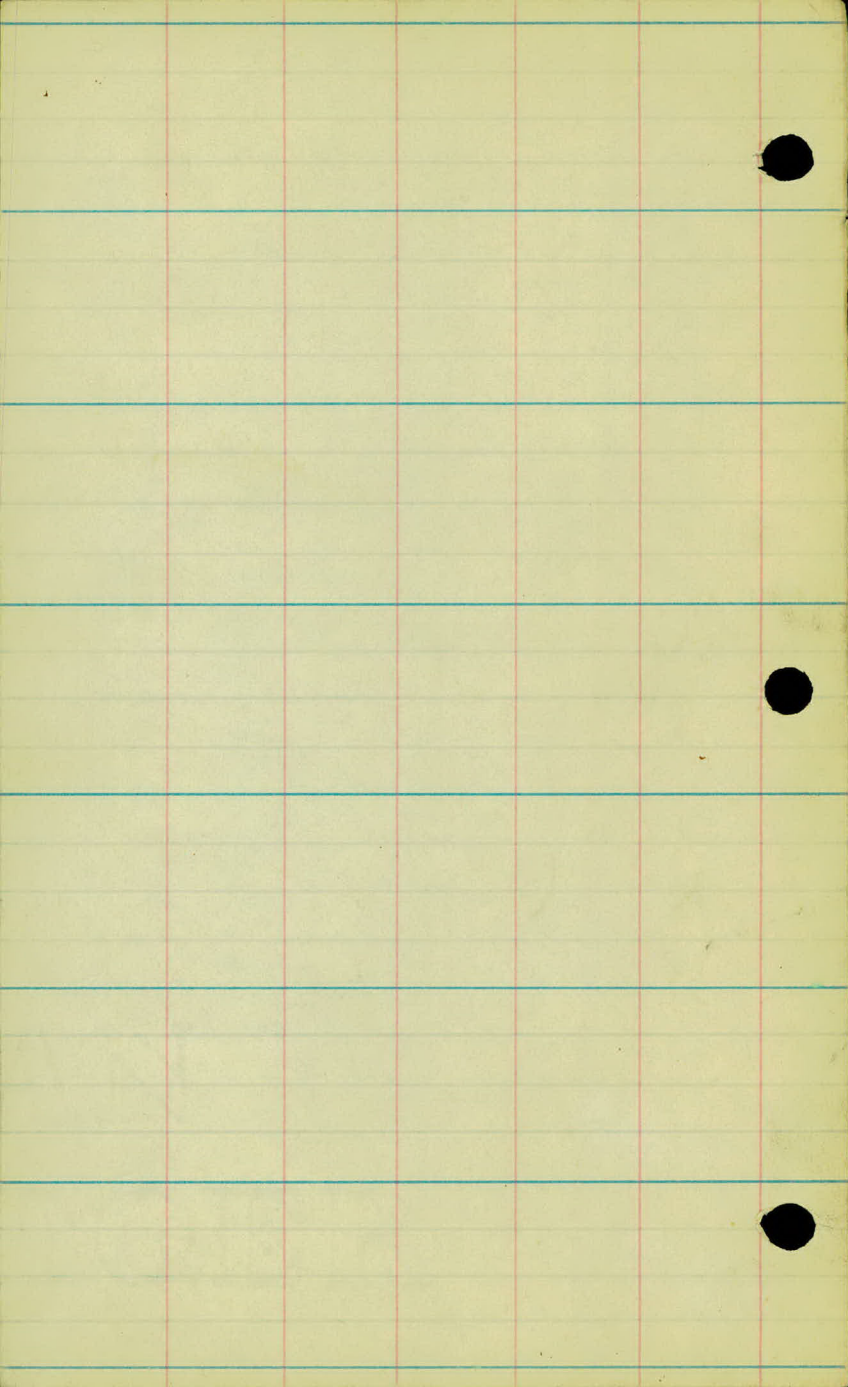
47 96

⊙ 14" OAK

X 22 105

⊙ 6" POP

Boat Spike



PROJ # 29-17  
LINE REVISION  
ART TOPOG FROM STA 12  
TO STA. 54

14

15

14

13

12

11

10

2-16-29

CULTIVATED

Woops

700 X. F.

150 F. 17

700 F. CORN.

155 X. F.

F. 45



22

21

20

19

18

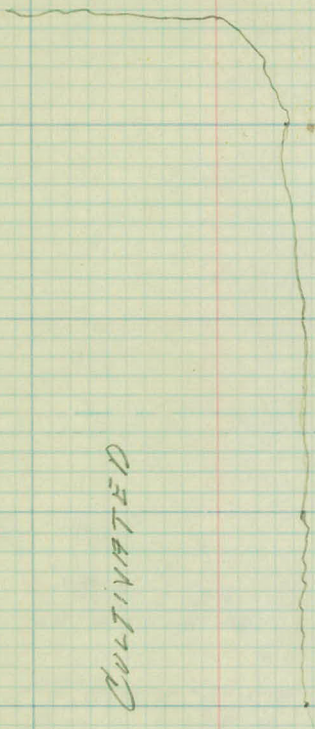
17

16

2-16-29

478 PALM HARBOR RD 52

478 & DITCH



CULTIVATED

Meadow

28

27

24

25

24

23

22

2-16-29

HAY FIELD.



765 F. Co. 1137

HAY MEADOW

34

33

32

31

30

29

28

2-16-29

HAY FIELD

40

39

38

37

36

35

34

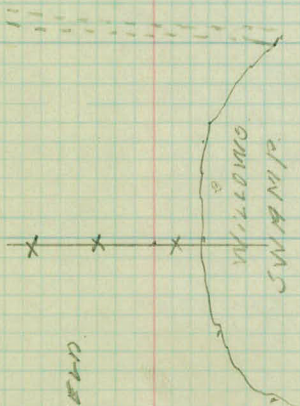
2-16-27

F. 25

HAY FIELD.

WAGT E LAND

705 DITCH.



798 X. F.

HAY FIELD.

46

45

44

43

42

41

40

SWAMP

WOODED PASTURE

F. 27

F. 8

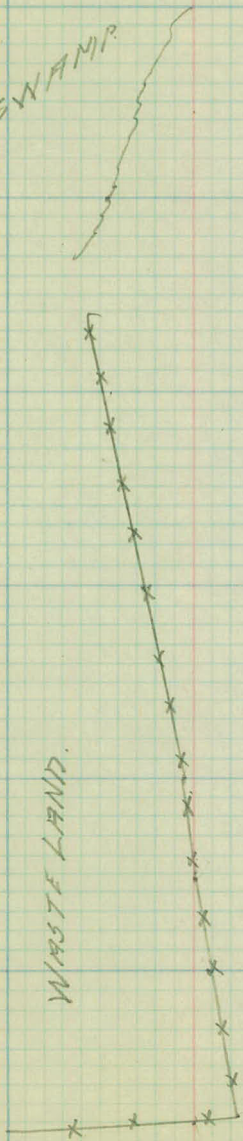
447 X. F.

WASTE LAND.

F. 8

119 X. F.

125 F. CON. 22



57

51

50

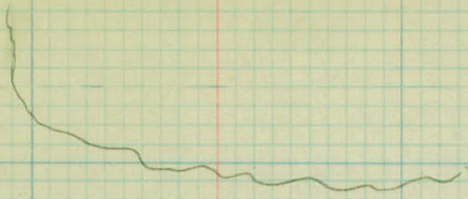
49

48

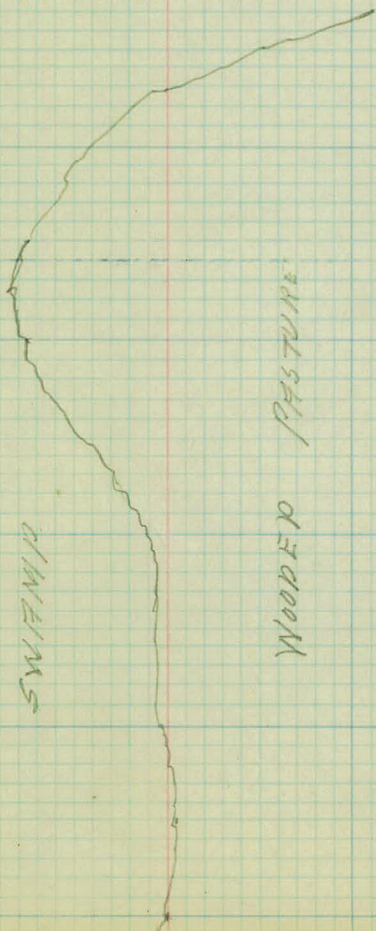
47

46

2-16-29



SWAMP.



SWAMP

WOODED PASTURE

56

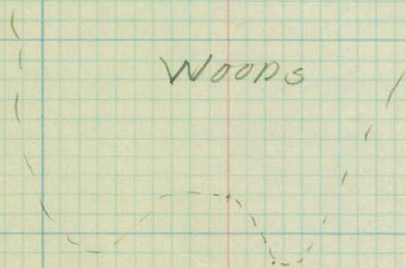
55

54

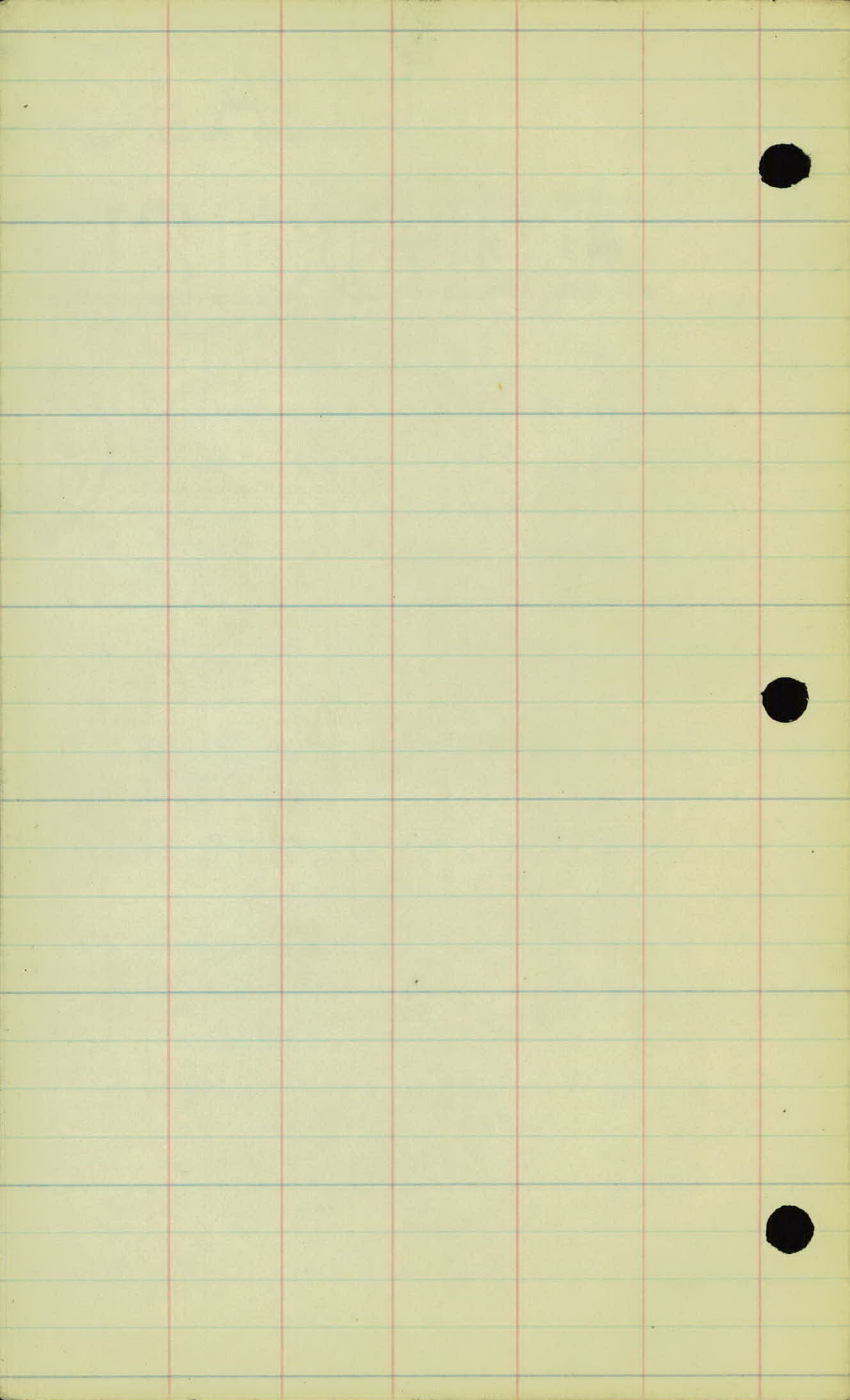
53

52

2-16-29



CUT OVER LAND  
STUMPS.



PROJ # 29-17

LINE REVISION.

CENTER LINE LEVELS & X  
SECTIONS FROM STA. 12+16<sup>19</sup>  
TO STA 54+17<sup>81</sup>

B.M.	3.23	877.60		874.37	
12+50			874.57		72.1
			3.23		
			1776.0		
			3.33		
13+00			874.22		72.6
			12.19		
			886.41		
			11.85		
13+50			875.48		73.3
			3.96		
			879.44		
			1.10		
14+00			878.34		74.2
	12.19	886.46	3.33	874.27	
14+50					75.5
15+00					82.3
15+50					83.8
16+00					83.0
16+50					82.3
17+00					81.6
17+50					79.1
	3.96	879.34	11.08	875.38	
18+00				878.29	73.9
B.M.	1.10	879.47	1.05	878.37	
18+50					72.5

878.37

2-14-29

TOP OF MONT. 50 RT. STA. 13718.

$\frac{70}{50}$	$\frac{68}{50}$	$\frac{66}{20}$	$\frac{70}{18}$	$\frac{63}{10}$	5.5	60	64	54	56
						16	23	40	30

$\frac{66}{50}$	$\frac{63}{22}$	$\frac{62}{16}$	$\frac{56}{15}$	5.0	55	55	52
					19	33	50

$\frac{59}{50}$	$\frac{56}{15}$	$\frac{54}{12}$	$\frac{48}{8}$	4.3	4.3	4.8	4.4
					13	19	30

$\frac{57}{50}$	$\frac{50}{23}$	$\frac{44}{16}$	$\frac{42}{11}$	5.4	3.9	4.6	4.0	2.5
					8	14	22	30

$\frac{14.3}{50}$	$\frac{12.7}{30}$	$\frac{12.5}{19}$	$\frac{11.9}{16}$	11.0	7.3	7.9
					24	50

$\frac{12.4}{50}$	$\frac{11.6}{43}$	$\frac{9.7}{29}$	$\frac{6.7}{14}$	4.2	3.4	4.2
					21	30

$\frac{9.2}{50}$	$\frac{6.9}{31}$	$\frac{5.0}{18}$	2.7	1.7	1.5	1.4	1.5
				14	22	39	50

$\frac{7.7}{50}$	$\frac{6.4}{33}$	$\frac{4.9}{19}$	3.5	2.2	2.0	2.0
				18	33	50

$\frac{7.0}{50}$	$\frac{5.2}{37}$	$\frac{5.1}{17}$	4.2	4.5	4.7	5.0
				24	37	50

$\frac{6.4}{50}$	$\frac{5.2}{25}$	4.9	5.6	6.6	7.1
			17	36	50

$\frac{7.5}{50}$	$\frac{7.6}{24}$	8.4	8.0	11.7
			20	50

$\frac{4.1}{50}$	$\frac{3.2}{41}$	$\frac{4.5}{24}$	5.4	4.6	7.6	8.0
				21	43	50

$\frac{5.5}{50}$	$\frac{4.6}{44}$	$\frac{4.2}{23}$	$\frac{5.7}{11}$	7.0	8.5	8.7	9.2
					22	36	50

879.47

19+00

73.9

19+50

73.3

20+00

72.5

$$\begin{array}{r}
 -79.47 \\
 8.39 \\
 \hline
 874.08 \\
 4.79 \\
 \hline
 878.87 \\
 1.89 \\
 \hline
 873.98 \\
 13.64 \\
 \hline
 887.62
 \end{array}$$

20+50

71.8

21+00

71.4

4.79 875.87 8.39 871.08

21+50

69.9

21+70

68.8

21+75

8.3

67.5

21+78 CENTER OF PITCH

9.5

66.1

21+81

8.3

67.5

21+87

69.7

22+00

69.7

22+50

70.2

23+00

71.2

23+50

72.4

13.64 887.62 1.89 873.98

931.61

$\frac{5.4}{50}$   $\frac{5.1}{20}$  5.6  $\frac{7.2}{20}$   $\frac{8.6}{35}$   $\frac{9.7}{50}$

$\frac{6.5}{50}$   $\frac{5.8}{40}$   $\frac{5.3}{21}$  6.2  $\frac{6.9}{16}$   $\frac{8.1}{31}$   $\frac{9.9}{50}$

$\frac{6.6}{50}$   $\frac{6.3}{19}$  7.0  $\frac{7.8}{19}$   $\frac{9.2}{31}$   $\frac{9.8}{50}$

$\frac{7.2}{50}$   $\frac{7.1}{34}$   $\frac{7.6}{12}$  7.7  $\frac{8.1}{27}$   $\frac{9.9}{39}$   $\frac{10.3}{50}$

$\frac{7.9}{50}$   $\frac{8.1}{30}$  8.1  $\frac{8.7}{20}$   $\frac{10.2}{37}$   $\frac{10.4}{50}$

$\frac{4.8}{50}$   $\frac{5.0}{21}$  6.0  $\frac{6.6}{24}$   $\frac{7.2}{50}$

$\frac{6.5}{50}$   $\frac{6.7}{25}$  7.1  $\frac{7.4}{20}$   $\frac{7.3}{50}$

$\frac{7.8}{50}$   $\frac{8.3}{7.8}$   $\frac{9.8}{50}$  TOP OF ICE 34

$\frac{6.4}{50}$   $\frac{6.4}{22}$  6.2  $\frac{6.8}{27}$   $\frac{7.0}{50}$

$\frac{5.5}{50}$   $\frac{5.8}{22}$  6.2  $\frac{6.6}{25}$   $\frac{6.7}{50}$

$\frac{5.3}{50}$   $\frac{5.3}{24}$  5.7  $\frac{6.2}{27}$   $\frac{6.4}{50}$

$\frac{4.5}{50}$   $\frac{4.6}{20}$  4.7  $\frac{5.0}{22}$   $\frac{5.1}{50}$

$\frac{3.5}{50}$   $\frac{3.5}{22}$  3.5  $\frac{3.2}{23}$   $\frac{3.6}{50}$

887.62

24+00

75.8

24+50

84.9

13.39 900.22 0.79 886.83

25+00

92.0

25+50

96.9

12.14 912.10 0.26 899.94

26+00

01.3

26+50

06.1

27+00

12.4

13.29 924.90 0.49 911.61

27+00

12.4

27+50

15.2

28+00

15.8

28+50

16.6

29+00

20.1

29+50

21.3

$\frac{127}{50}$   $\frac{125}{24}$  11.8  $\frac{11.1}{39}$   $\frac{11.3}{50}$

$\frac{3.0}{60}$   $\frac{2.6}{50}$   $\frac{2.9}{26}$  2.7  $\frac{3.6}{30}$   $\frac{4.8}{50}$   $\frac{5.3}{60}$

$\frac{8.6}{75}$   $\frac{7.5}{50}$   $\frac{8.1}{24}$  8.2  $\frac{7.5}{28}$   $\frac{10.1}{50}$   $\frac{12.2}{75}$

$\frac{3.7}{75}$   $\frac{4.2}{50}$   $\frac{3.9}{26}$  3.9  $\frac{1.5}{24}$   $\frac{2.2}{50}$   $\frac{4.5}{75}$

$\frac{17.4}{75}$   $\frac{16.9}{50}$   $\frac{14.5}{25}$  10.8  $\frac{7.3}{24}$   $\frac{6.2}{50}$   $\frac{8.1}{75}$

$\frac{16.4}{75}$   $\frac{13.9}{50}$   $\frac{8.6}{22}$  6.0  $\frac{3.6}{19}$   $\frac{2.9}{38}$   $\frac{4.4}{50}$   $\frac{6.4}{75}$

$\frac{12.2}{75}$   $\frac{7.4}{50}$   $\frac{6.0}{40}$   $\frac{2.9}{23}$  (+0.3)

12.5  $\frac{11.5}{72}$   $\frac{12.6}{34}$   $\frac{13.7}{50}$   $\frac{14.4}{75}$

$\frac{18.7}{75}$   $\frac{14.0}{50}$   $\frac{10.9}{13}$  7.7  $\frac{10.6}{31}$   $\frac{10.5}{50}$   $\frac{8.8}{75}$

$\frac{11.0}{75}$   $\frac{9.7}{50}$   $\frac{8.3}{23}$  9.1  $\frac{7.6}{25}$   $\frac{8.1}{50}$   $\frac{6.6}{75}$

$\frac{6.2}{75}$   $\frac{6.5}{50}$   $\frac{7.6}{24}$  8.3  $\frac{6.4}{29}$   $\frac{5.3}{50}$   $\frac{5.7}{75}$

$\frac{6.6}{75}$   $\frac{6.5}{50}$   $\frac{6.1}{25}$  4.8  $\frac{2.1}{32}$   $\frac{3.9}{50}$   $\frac{4.5}{75}$

$\frac{6.8}{75}$   $\frac{6.2}{50}$   $\frac{5.0}{31}$  3.4  $\frac{4.0}{30}$   $\frac{4.5}{50}$   $\frac{3.7}{75}$

924.90

30+00

20.5

30+50

18.9

31+00

18.7

31+50

19.5

32+00

20.1

32+50

21.0

4.32 924.49 4.73 920.17

33+00

20.1

33+50

15.9

7.92

34+00

13.8

34+50

15.3

35+00

11.0

35+50

2.44 914.45 12.50 911.99

35+00

$\frac{4.3}{50}$	$\frac{4.2}{25}$	4.4	$\frac{4.5}{21}$	$\frac{3.2}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{7.0}{50}$	$\frac{7.0}{35}$	6.0	$\frac{5.1}{25}$	$\frac{2.0}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{7.1}{50}$	$\frac{7.2}{29}$	6.2	$\frac{5.2}{26}$	$\frac{3.7}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{3.0}{50}$	$\frac{5.3}{21}$	5.4	$\frac{5.3}{33}$	$\frac{5.1}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{1.4}{50}$	$\frac{3.8}{21}$	4.8	$\frac{5.7}{29}$	$\frac{5.7}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{3.0}{50}$	$\frac{3.0}{25}$	3.7	$\frac{5.0}{30}$	$\frac{4.7}{50}$
------------------	------------------	-----	------------------	------------------

STA 35100.

$\frac{7.3}{50}$	$\frac{5.4}{25}$	4.4	$\frac{4.3}{28}$	$\frac{4.7}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{12.7}{50}$	$\frac{10.4}{25}$	8.6	$\frac{7.6}{22}$	$\frac{6.8}{50}$
-------------------	-------------------	-----	------------------	------------------

$\frac{14.6}{50}$	$\frac{13.0}{25}$	10.7	$\frac{8.4}{26}$	$\frac{8.7}{50}$
-------------------	-------------------	------	------------------	------------------

$\frac{10.3}{50}$	$\frac{9.8}{29}$	9.2	$\frac{9.8}{22}$	$\frac{12.8}{50}$
-------------------	------------------	-----	------------------	-------------------

$\frac{5.3}{50}$	$\frac{6.3}{40}$	$\frac{9.2}{20}$	13.5
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$\frac{10.5}{50}$	$\frac{12.3}{26}$
-------------------	-------------------

15.4

3.0

68	8.8
30	30

914.43

35+50

09.1

36+00

05.4

36+50

05.1

37+00

04.2

+02

10.4

+04 CENTER OF PITCH

11.6

02.8

+06

10.1

37+50

06.7

38+00

12.2

7.82 910.84 1.41 913.02

38+50

15.1

39+00

16.2

39+50

16.0

40+00

12.6

1.22 910.34 1.172 709.12

40+50

05.7

B.M.

1.84 910.30 1.84 908.50 908.46

41+00

03.7

908.46 40110

902.99 BIRCH

911.37 48160  
911.52

5.3      7.7      9.6      10.1  
         15      31      50

909.73 57150      7.8      8.3      10.2      10.8      10.9  
         50      20      9.0      17      40      50

10.0      9.9      9.1      9.9  
50      26      9.3      26      50

11.5      10.7      9.9      10.5  
50      24      10.2      28      50

12.2      11.6      11.0  
50      50

10.9      9.0      7.6      8.0  
50      23      7.7      29      50

8.1      5.0      3.3      0.8      1.1  
50      25      5      2.2      20      50

11.3      9.5      11.1      4.8      3.2  
50      40      17      5.7      22      50

7.8      7.8      6.1      3.5      1.2      1.5  
50      40      20      4.6      23      40      50

11.1      8.4      6.9      4.3      3.4      3.0  
50      38      23      4.8      19      33      50

14.5      9.7      7.4      6.1      6.0      5.5  
50      18      8.2      11      25      33      50

7.6      6.0      3.1      1.2      0.4  
50      20      4.4      17      40      50

SPK IN 24" DIA K 100 RT. STA 40+70

86      82      5.6      5.2  
50      30      6.6      30      50

910.30

41750

03.3

42700

04.0

42750

05.7

43700

08.4

6.51 915.29 ✓ 1.52 908.78 ✓

43750

09.8

44700

10.7

44750

10.3

45700

08.1

45750

05.6

46700

04.0

11.56 913.28 ✓ 73.57 901.72 ✓

46750

02.9

16.19

47700

02.0

47750

02.1

$\frac{6.5}{50}$	$\frac{7.2}{28}$	7.0	$\frac{6.4}{30}$	$\frac{6.2}{50}$
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$\frac{3.3}{50}$	$\frac{3.9}{44}$	$\frac{5.6}{17}$	6.3	$\frac{6.5}{26}$	$\frac{6.8}{50}$
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$\frac{2.8}{50}$	$\frac{3.4}{36}$	$\frac{3.9}{19}$	4.6	$\frac{5.1}{29}$	$\frac{5.7}{50}$
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$\frac{1.5}{50}$	$\frac{2.0}{28}$	$\frac{2.1}{16}$	1.9	$\frac{1.9}{22}$	$\frac{2.4}{50}$
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$\frac{7.5}{50}$	$\frac{7.2}{40}$	$\frac{6.7}{24}$	5.5	$\frac{4.6}{21}$	$\frac{4.3}{50}$
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$\frac{7.0}{50}$	$\frac{6.0}{25}$	4.6	$\frac{3.3}{22}$	$\frac{2.2}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{11.9}{50}$	$\frac{10.2}{35}$	$\frac{6.8}{15}$	$\frac{7.4}{5.0}$	$\frac{2.3}{23}$	$\frac{0.2}{50}$
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$\frac{13.5}{50}$	$\frac{12.9}{43}$	$\frac{9.8}{17}$	$\frac{6.1}{7.2}$	$\frac{5.1}{22}$	$\frac{2.9}{50}$
-------------------	-------------------	------------------	-------------------	------------------	------------------

$\frac{13.7}{50}$	$\frac{12.8}{38}$	$\frac{11.3}{17}$	$\frac{4.4}{9.7}$	$\frac{8.0}{20}$	$\frac{6.7}{39}$	$\frac{6.0}{50}$
-------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------

$\frac{13.8}{50}$	$\frac{13.2}{22}$	$\frac{6.7}{11.3}$	$\frac{9.4}{25}$	$\frac{8.5}{50}$
-------------------	-------------------	--------------------	------------------	------------------

$\frac{11.8}{50}$	$\frac{11.6}{30}$	$\frac{11.4}{12}$	$\frac{7.0}{10.4}$	$\frac{8.2}{19}$	$\frac{6.3}{40}$	$\frac{6.4}{50}$
-------------------	-------------------	-------------------	--------------------	------------------	------------------	------------------

$\frac{12.0}{50}$	$\frac{11.8}{30}$	$\frac{11.4}{15}$	$\frac{7.3}{11.3}$	$\frac{9.7}{14}$	$\frac{6.2}{33}$	$\frac{4.4}{50}$
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$\frac{12.0}{50}$	$\frac{11.8}{26}$	$\frac{7.5}{11.2}$	$\frac{9.4}{19}$	$\frac{7.6}{28}$	$\frac{3.5}{50}$
-------------------	-------------------	--------------------	------------------	------------------	------------------

713.28

48+00

02.1

48+50

03.8

49+00

08.9

13.M.

1.95 711.35

49+50

08.8

12.55 715.37 10.46 702.82

50+00

03.8

50+50

01.2

51+00

00.2

52+00

02.0

52+40

05.5

52+75

12.8

53+00

12.5

53+50

08.0

54+00

09.4

0

$\frac{11.8}{50}$	$\frac{11.6}{30}$	11.2	$\frac{9.2}{17}$	$\frac{6.6}{31}$	$\frac{3.9}{50}$
-------------------	-------------------	------	------------------	------------------	------------------

$\frac{11.8}{50}$	$\frac{11.6}{40}$	$\frac{10.9}{18}$	9.5	$\frac{5.6}{23}$	$\frac{4.3}{40}$	$\frac{3.5}{50}$
-------------------	-------------------	-------------------	-----	------------------	------------------	------------------

$\frac{7.0}{50}$	$\frac{6.0}{25}$	4.4	$\frac{3.7}{22}$	$\frac{3.4}{50}$
------------------	------------------	-----	------------------	------------------

SPK IN 8" DIA 40 RT STA 49 + 20.

$\frac{6.2}{50}$	$\frac{4.8}{20}$	4.5	$\frac{5.2}{16}$	$\frac{5.4}{33}$	$\frac{5.2}{50}$
------------------	------------------	-----	------------------	------------------	------------------

$\frac{13.8}{50}$	$\frac{13.0}{27}$	11.6	$\frac{10.2}{26}$	$\frac{8.3}{50}$
-------------------	-------------------	------	-------------------	------------------

$\frac{14.4}{50}$	$\frac{14.0}{30}$	14.2	$\frac{13.9}{26}$	$\frac{13.4}{50}$
-------------------	-------------------	------	-------------------	-------------------

$\frac{15.2}{50}$	15.2	$\frac{15.2}{50}$
-------------------	------	-------------------

$\frac{13.6}{50}$	$\frac{13.5}{34}$	13.4	$\frac{13.3}{27}$	$\frac{13.5}{50}$
-------------------	-------------------	------	-------------------	-------------------

$\frac{11.2}{50}$	$\frac{10.7}{30}$	9.9	$\frac{8.3}{32}$	$\frac{8.0}{50}$
-------------------	-------------------	-----	------------------	------------------

$\frac{5.8}{50}$	$\frac{2.3}{27}$	2.6	$\frac{2.7}{33}$	$\frac{2.7}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{5.7}{50}$	$\frac{4.6}{28}$	2.9	$\frac{2.8}{32}$	$\frac{4.1}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{9.1}{50}$	$\frac{8.1}{30}$	7.4	$\frac{7.6}{25}$	$\frac{8.2}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{6.6}{50}$	$\frac{5.7}{35}$	6.0	$\frac{7.2}{34}$	$\frac{8.0}{50}$
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715.37

54+17<sup>81</sup>

10.3

4.10

916.91

2.56

912.81

B.M.

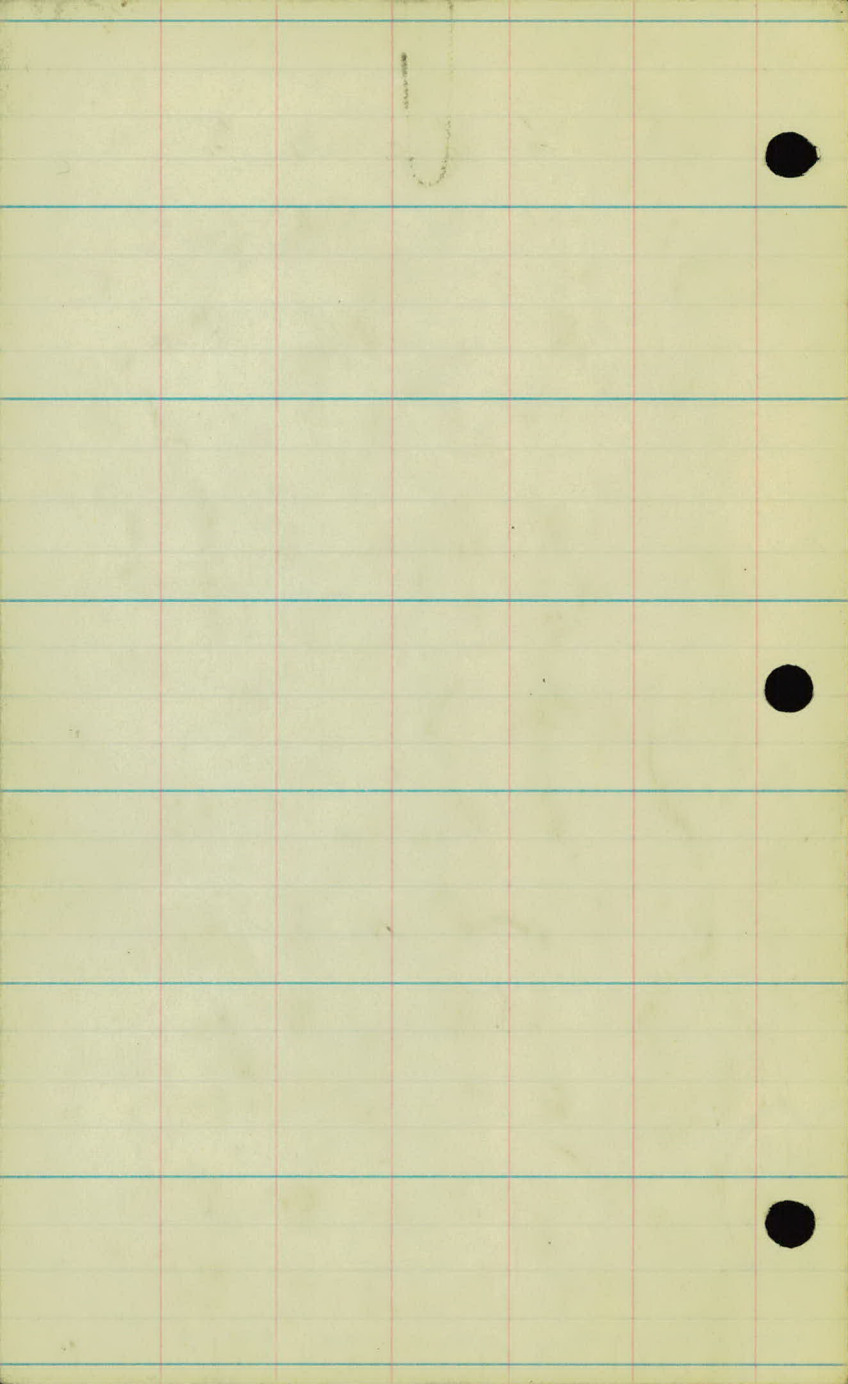
7.19

909.72

909.73

2-15-29

$\frac{3.7}{50}$     $\frac{3.4}{26}$    5.1    $\frac{6.5}{23}$     $\frac{7.7}{50}$



PROJ # 29-17

CURVE ON ORIGINAL LINE  
AT END OF PROJECT

62+79<sup>58</sup> P.T.

+50

62

41°-50'

38°-08'

31°-53'

61+51<sup>7</sup> P.I.

+50

61

+50

60

+50

59+44<sup>91</sup> P.C.

Δ-83°-40'

25°-38'

D.-25° R.

19°-23'

T.-206<sup>79</sup>

13°-08'

L.-334<sup>67</sup>

6°-53'

R.-231<sup>01</sup>

0°-38'

0°-00'

59+29<sup>8</sup> P.O.T.



B. M.	12.42	892.08 ✓	879.66	
60 +00			81.6 ✓	
+50			80.5 ✓	
61 +00			79.3 ✓	
+50			80.9 ✓	
+85			87.2 ✓	
62 +00			87.3 ✓	
+50			87.3 ✓	
+79 <sup>51</sup>			87.2 ✓	
63			4.97	87.11 ✓
+50			5.10	86.98 ✓
64			5.24	86.84 ✓

62+75 CATTLE PASS

B. M. 12.42 879.66 ✓

94	100	105	10.6		10.0	8.6	6.7
50	33	23	10	10.5	17	33	50

12.1	11.9	11.8		11.0	10.5	9.4
50	33	19	11.6	21	33	50

EDGE OF PAVE

4.65	4.7	7.3	9.8	11.5	12.8	12.9	12.6	11.3	
67	59	50	42	33	21	12.8	19	33	50

EDGE OF PAVE

4.85	4.80	4.88	4.8	10.2		13.0	12.6	12.1
50	44	25	19	4	11.2	7	33	50

EDGE OF PAVE

5.6	4.80	4.80	4.70	4.80		12.5	12.9	12.5	12.3	11.9
50	47	39	27	9	4.9	18	22	23	33	50

EDGE OF PAVE

9.4	4.9	4.82	4.7	4.8		4.9	10.4	12.0	12.6	12.3	12.1	11.4
50	37	29	14	0.4	4.8	7	19	24	27	28	33	50

EDGE OF PAVE

6.6	6.5	8.2	8.4	5.0	4.90							9.1	
50	49	44	34	22	16	4.80	72	17	22	24	33	37	40

EDGE OF PAVE

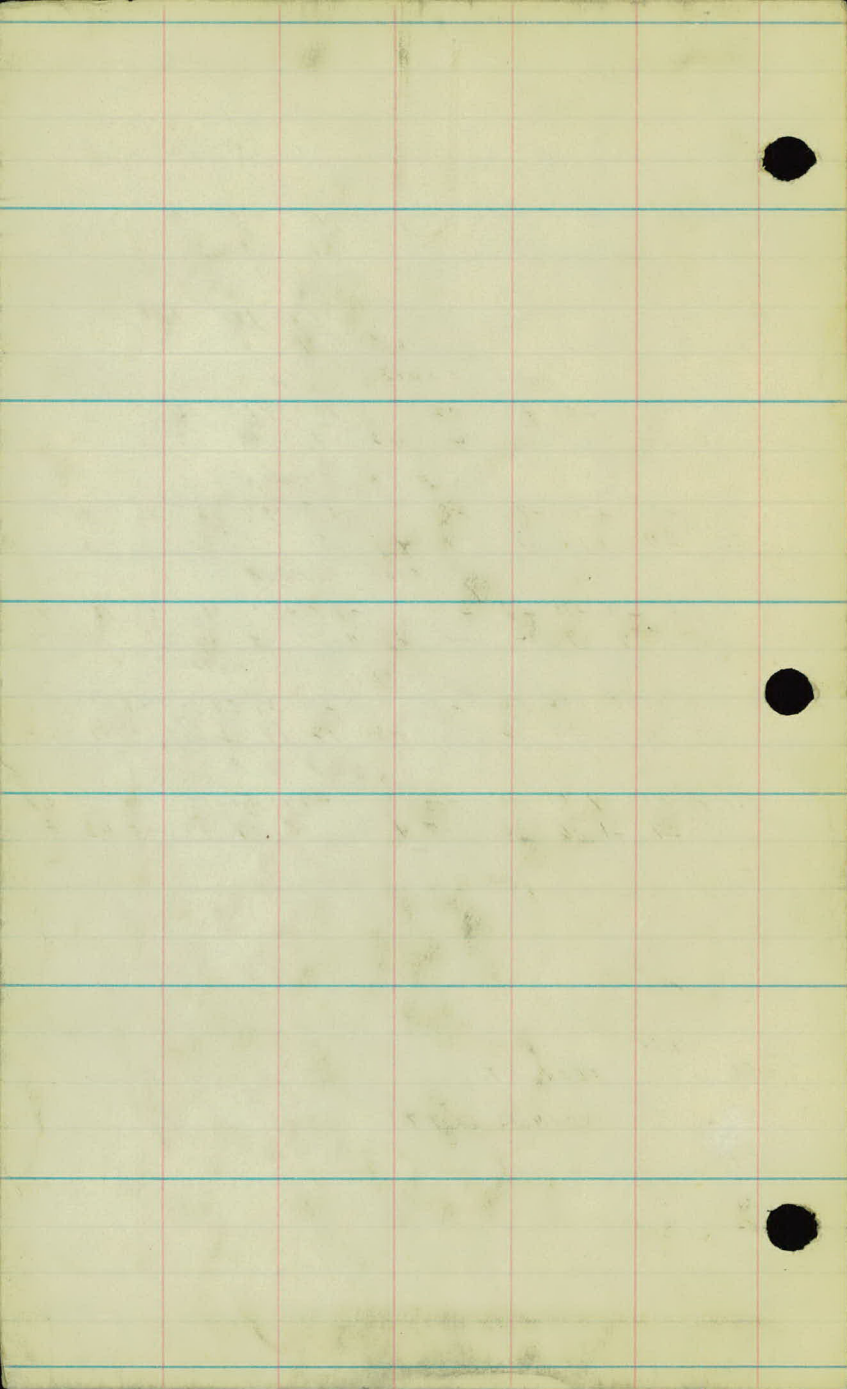
5.7	5.6	7.7	8.1	5.2	5.02		4.97	5.1	12.0	10.4	5.5	9.7
50	47	41	30	20	13.5	4.88	13.5	19	29	35	42	50

TOP ELEV.

13.80

ELEV. RT.

EXTENDS 22<sup>5</sup> RT.



PROD # 29-17

Borrow Pit

Co Rd F & JTH62

B.M.

8.07

891.28 ✓

883.21

0+00

0+50

0+88

1+00

1+50

2+00

2+19

2+35

13.09

903.74 ✓

0.63

890.65 ✓

0+50

0+88

1+00

1+50

5.89

906.94 ✓

2.67

901.07 ✓

0+50

SPX. IN 10" OAK 60 RT. STA. 67+90.

$$\begin{array}{r} 10.2 \quad 11.4 \quad 12.1 \\ 40 \quad 33 \quad 18 \quad 12.7 \end{array} \quad 78.6$$

$$\begin{array}{r} 2.1 \quad 5.7 \quad 9.0 \quad 10.4 \\ 63 \quad 50 \quad 33 \quad 20 \quad 11.9 \end{array} \quad 79.4$$

$$\begin{array}{r} 6.8 \quad 10.1 \\ 36 \quad 5 \quad 10.9 \end{array} \quad 80.4$$

$$\begin{array}{r} 6.4 \quad 8.8 \\ 32 \quad 13 \quad 10.1 \end{array} \quad 81.2$$

$$\begin{array}{r} 1.6 \quad 5.9 \\ 34 \quad 18 \quad 8.8 \end{array} \quad 82.5$$

$$\begin{array}{r} 11.4 \quad 11.7 \quad 7.8 \\ 43 \quad 31 \quad 15 \quad 9.7 \end{array} \quad 81.6$$

→ EDGE OF PAVE

$$\begin{array}{r} 8.65 \quad 8.8 \quad 11.0 \\ 33 \quad 21 \quad 8 \quad 10.9 \end{array} \quad 80.4$$

8.78 EDGE OF PAVE

$$\begin{array}{r} 1.9 \quad 8.8 \\ 100 \quad 81 \end{array} \quad 24.3$$

$$\begin{array}{r} 1.5 \quad 7.1 \quad 13.0 \\ 81 \quad 68 \quad 50 \end{array} \quad 23.3$$

$$\begin{array}{r} 0.0 \quad 4.9 \quad 11.7 \\ 78 \quad 67 \quad 50 \end{array} \quad 22.9$$

$$\begin{array}{r} 0.0 \quad 5.9 \\ 64 \quad 50 \end{array} \quad 21.2$$

$$\begin{array}{r} 6.9 \quad 4.0 \quad 3.0 \quad 3.1 \\ 150 \quad 129 \quad 117 \quad 110 \end{array} \quad 27.6$$

906.96 ✓

0+88

1+00

1+50

2.46 896.58 ✓ 13.04 893.92 ✓

0+88

4.71 887.69 ✓ 13.40 882.98 ✓

0+88

1+00

1+50

2+00

13.M.

4.48 183.21 ✓ 883.21

<u>135</u>	<u>92</u>	<u>58</u>	<u>31</u>	<u>19</u>	<u>2.7</u>	
172	150	133	115	94	88	<u>26.6</u>

<u>15.1</u>	<u>12.9</u>	<u>10.6</u>	<u>5.2</u>	<u>2.2</u>	<u>1.5</u>	<u>2.1</u>
184	164	150	122	100	92	83

(25.8)

<u>3.5</u>	<u>2.4</u>	<u>2.5</u>
86	78	67

(24.5)

<u>4.9</u>
208

16.0

→ EDGE OF PAVE

<u>4.7</u>	<u>4.8</u>	<u>6.0</u>	<u>6.8</u>	<u>5.9</u>
285	279	263	249	137

7.3

→ EDGE OF PAVE

<u>4.98</u>	<u>4.8</u>	<u>6.3</u>	<u>6.8</u>	<u>6.0</u>
263	251	240	230	214

6.5

→ EDGE OF PAVE

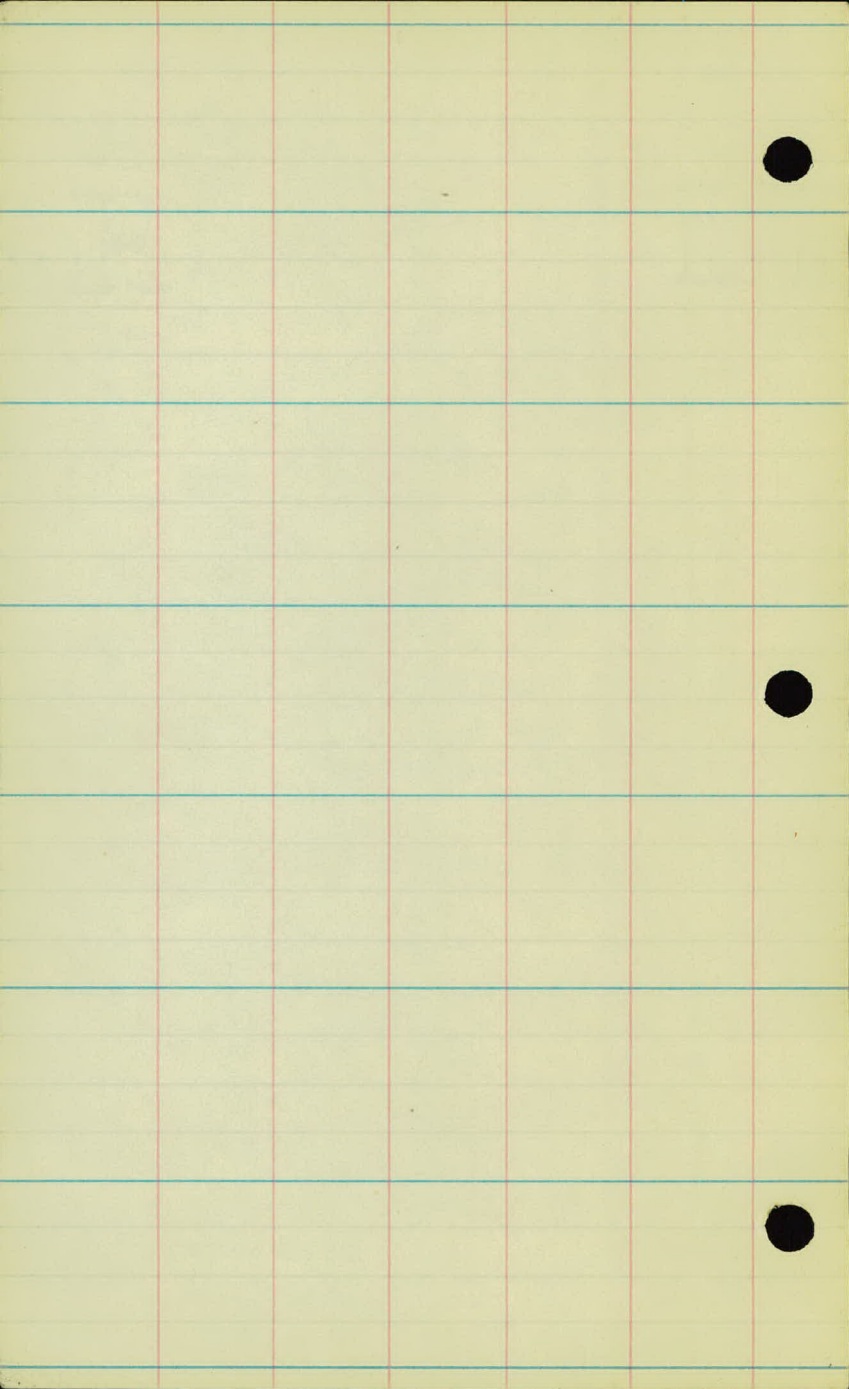
<u>4.53</u>	<u>4.7</u>	<u>7.1</u>	<u>5.6</u>
166	156	133	122

5.2

→ EDGE OF PAVE

<u>4.88</u>	<u>5.2</u>
71	58

6.1



PROJ H 29-17  
SOUNDINGS.

SOUNDING ON  $\Phi$  AT STA. 51+60

0' - 5' MUCK

5' - 7' FINE GRAVEL

7' - ? BLUE CLAY

SOUNDING ON  $\Phi$  AT STA. 51+00

0' - 5' MUCK

5' - 6' BLUE CLAY

6' - 7' FINE SAND

SOUNDING ON  $\Phi$  AT STA. 21+80 IN DITCH

0' - 1' SAND

1' - 4' BLUE CLAY

SOUNDING ON  $\Phi$  AT STA. 17+50

0 - 1' SAND

1' - 5' CLAY

SOUNDING ON  $\Phi$  AT STA. 16+50

0' - 4 1/2' SAND

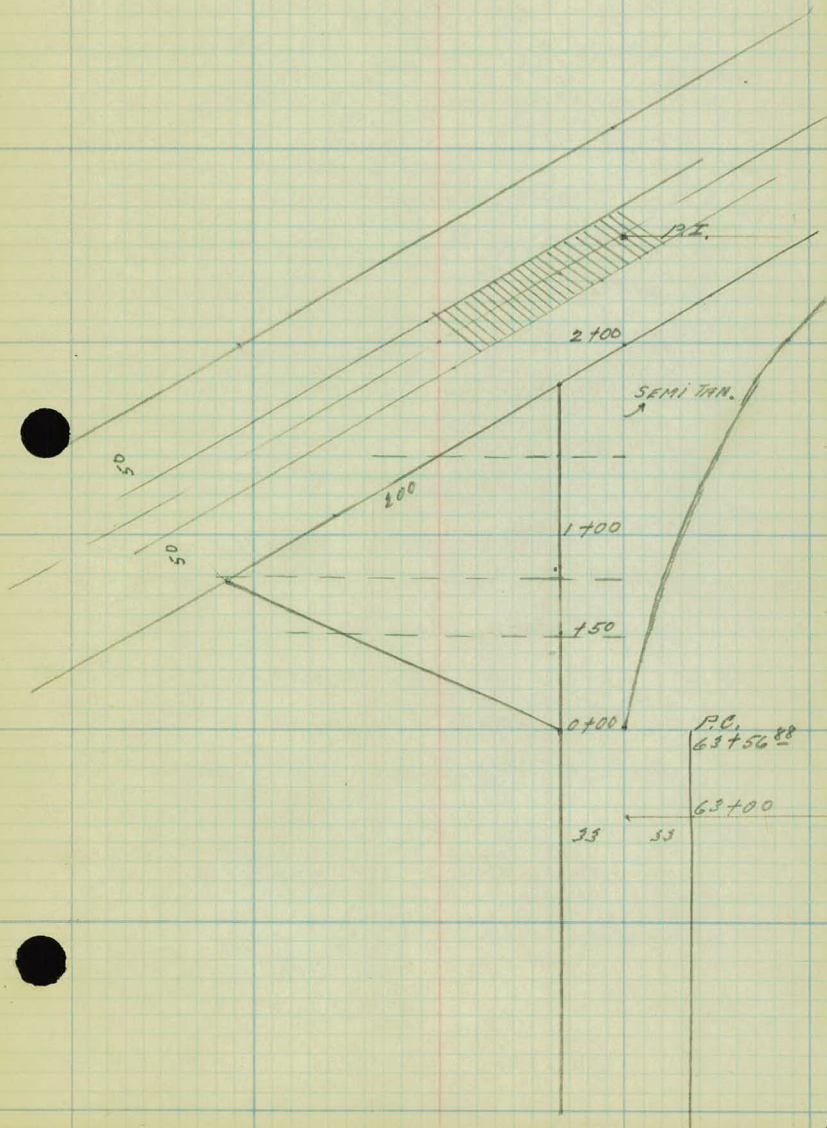
SOUNDING ON  $\Phi$  AT STA. 15+00

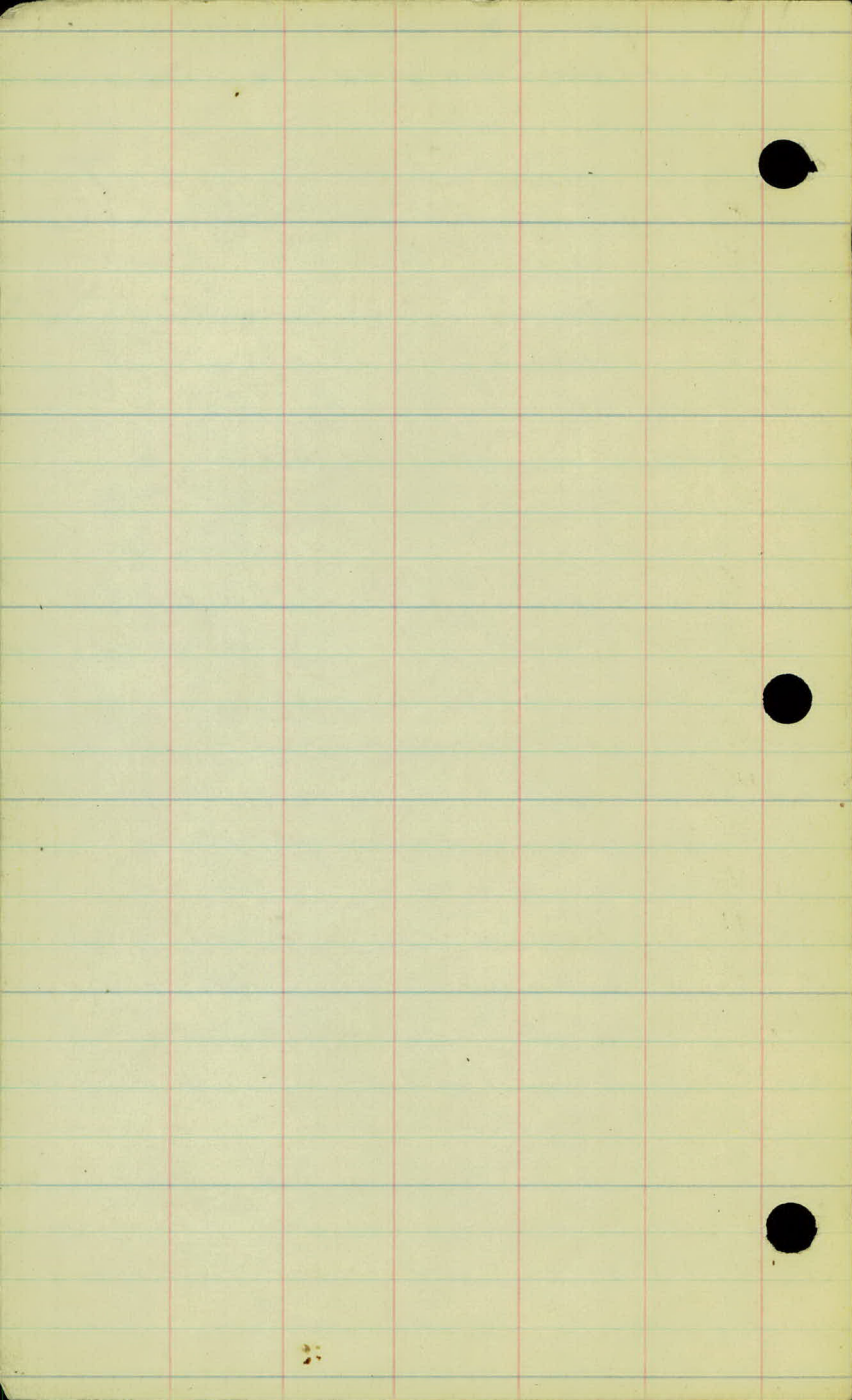
0' - 3 1/2' SAND

3 1/2' - 4' SANDY CLAY

SOUNDING ON  $\Phi$  AT STA. 15+50

0' - 4 1/2' SAND





PLANS IN HAND.

5-8-29

O.R.V.K.  
W.S.M.  
H.L.W.

29-17

- ✓ 1+94<sup>Rt</sup> - P. 12" x 20' C.M.
- ✓ 2+00 to 3+50 - Cl. 14 T. Gr. 6 T.
- ✓ 3+62 - Remove - P. 30" x 60' P<sub>3</sub>.
- ✓ 4+50 to 5+00 - Cl. 2 T.
- ✓ 6+60 Rt - P. 15" x 30' C.M.
- ✓ 8+87 - Lt - P. 15" x 20' C.M.
- ✓ 9+65 - Rt - No culv. req.
- ✓ 9+00 to 12+25<sup>Lt</sup> - Cl. 12' wide. 0.09 Acres
- ✓ 10+00 to 13+00<sup>Rt</sup> - Cl. 15' wide. 0.10 Acres
- ✓ 12+00 - P. 24" x 42' P<sub>3</sub>.
- ✓ 13+25 - Rt - P. 15" x 20' C.M.
- ✓ 13+25 to 14+00 - Cl. + Gr. 5 T.
- ✓ 14+50 to 15+50 - Cl. + Gr. from fence line to R<sub>2</sub>-N. 0.1296'
- ✓ 14+00 - Lt - P. 15" x 20' C.M.
- ✓ 18+25 - Rt - P. 15" x 20' C.M.
- ✓ Get ditch drainage on Lt from 18+00 to 22+00
- ✓ 24+50 R+L - P. 2. 15" x 20' C.M.
- Figure claying from 0+00 to 20+00.
- ✓ 29+00 to 29+50 - Gr. 1 T.
- ✓ 37+05 - P. 24" x 66' P<sub>3</sub>
- ✓ 38+00 - Lt - No culv. req.
- ✓ 40+00 to 40+50 - Cl. + Gr. 2 T.
- ✓ 40+50 to 50+00 - Cl. + Gr. by acre where necessary

- ✓ 41+50 - P. 24" x 54 P<sub>3</sub>.
- ✓ 46+25 - P. 24" x 42 P<sub>3</sub>
- ✓ 48+00 to 50+00 - Ditch for drainage on Rt.
- ✓ 50+30 - P. 24" x 48 P<sub>3</sub> H.D. 400'
- ✓ 52+25 to 54+00 - Gr. by acre.
- ✓ 54+00 to 60+25 - Cl. + Gr. by acre.
- ✓ 60+00 - R. + Lt. - P. 2 - 15" x 20' C.M.
- ✓ 61+50 to 62+00 - Cl. 3T.
- ✓ 61+85 - P. 24" x 54 P<sub>3</sub> H.D. 200'
- ✓ 64+50 to 66+00 - Cl. + Gr. 10 T.
- ✓ 65+50 - P. 30" x 48 P<sub>3</sub>. Ditch to L. at Exc. price.
- 62+00 to 65+50 - H.D. on Rt.

1.3 + 17.8

25.4  
- 1.1  
-----  
24.3

100

95

85

40

30

10

0

U2415