

OFFICE OF COUNTY ENGINEER  
RAMSEY CO. MINN.

Construction Survey

HODGSON ROAD

From Rice St. To N. Co. Line

Road Acc't. No. 1

Date Filed 4-12-30

FIELD BOOK

360 A

APR 29 1930

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

*"Copyright, 1895, by Keuffel & Esser Co."*

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

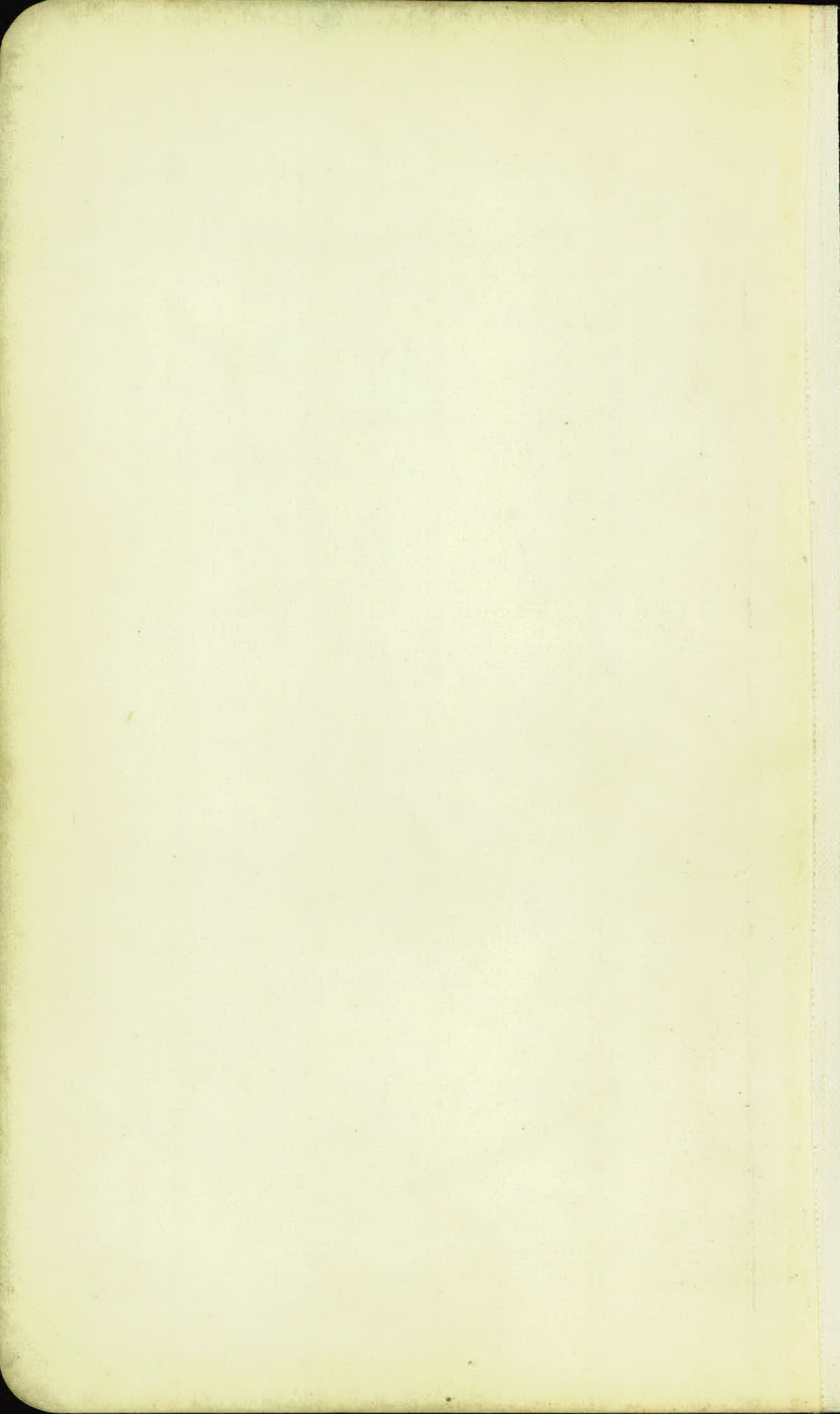
For Keith's Railroad Curve Tables see end of book.

16

$$\begin{array}{r} .4 \\ \hline \sqrt{2000} \\ \underline{200} \end{array}$$

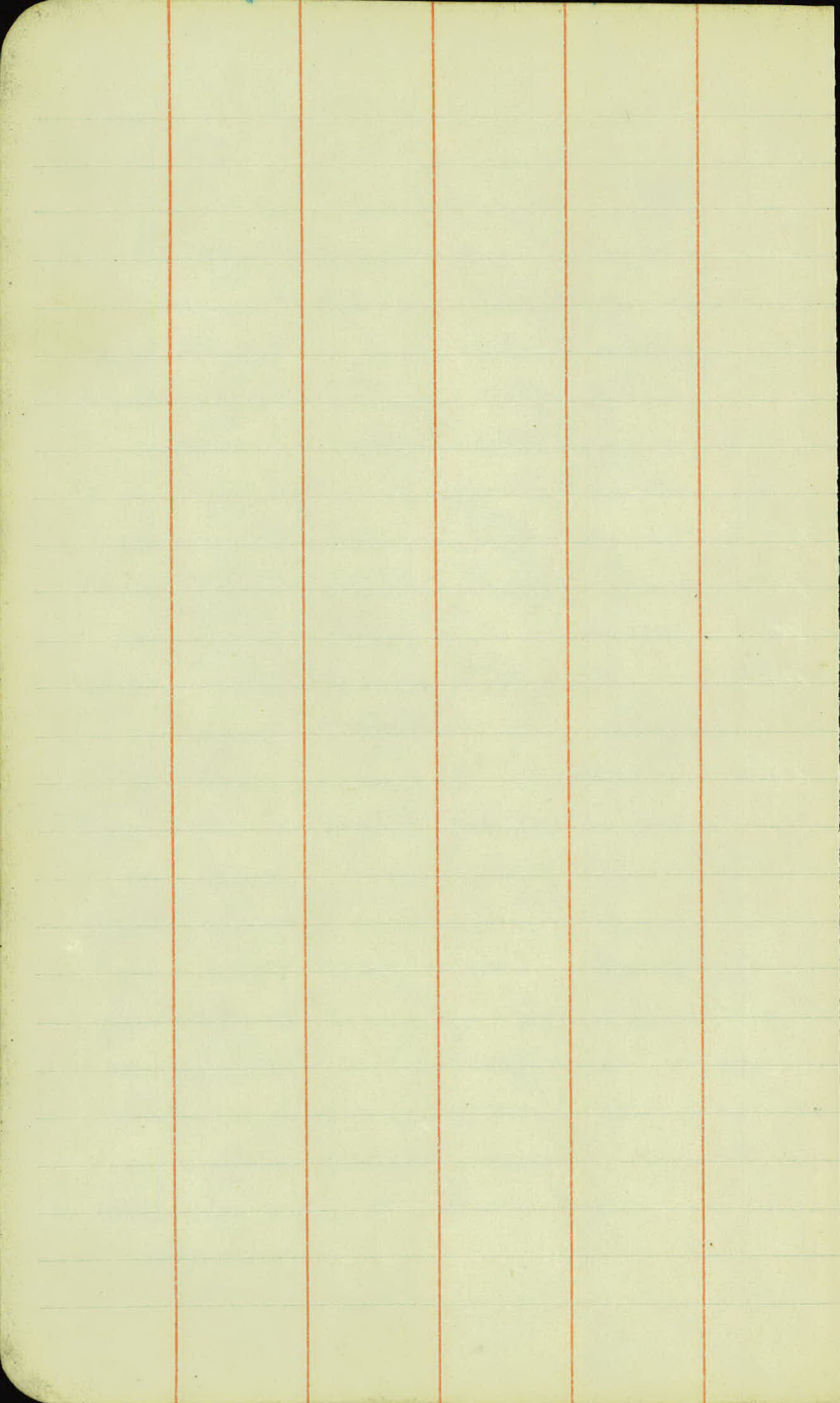
$$\begin{array}{r} .15 \\ \hline \sqrt{50} \\ \underline{4} \\ .20 \end{array}$$

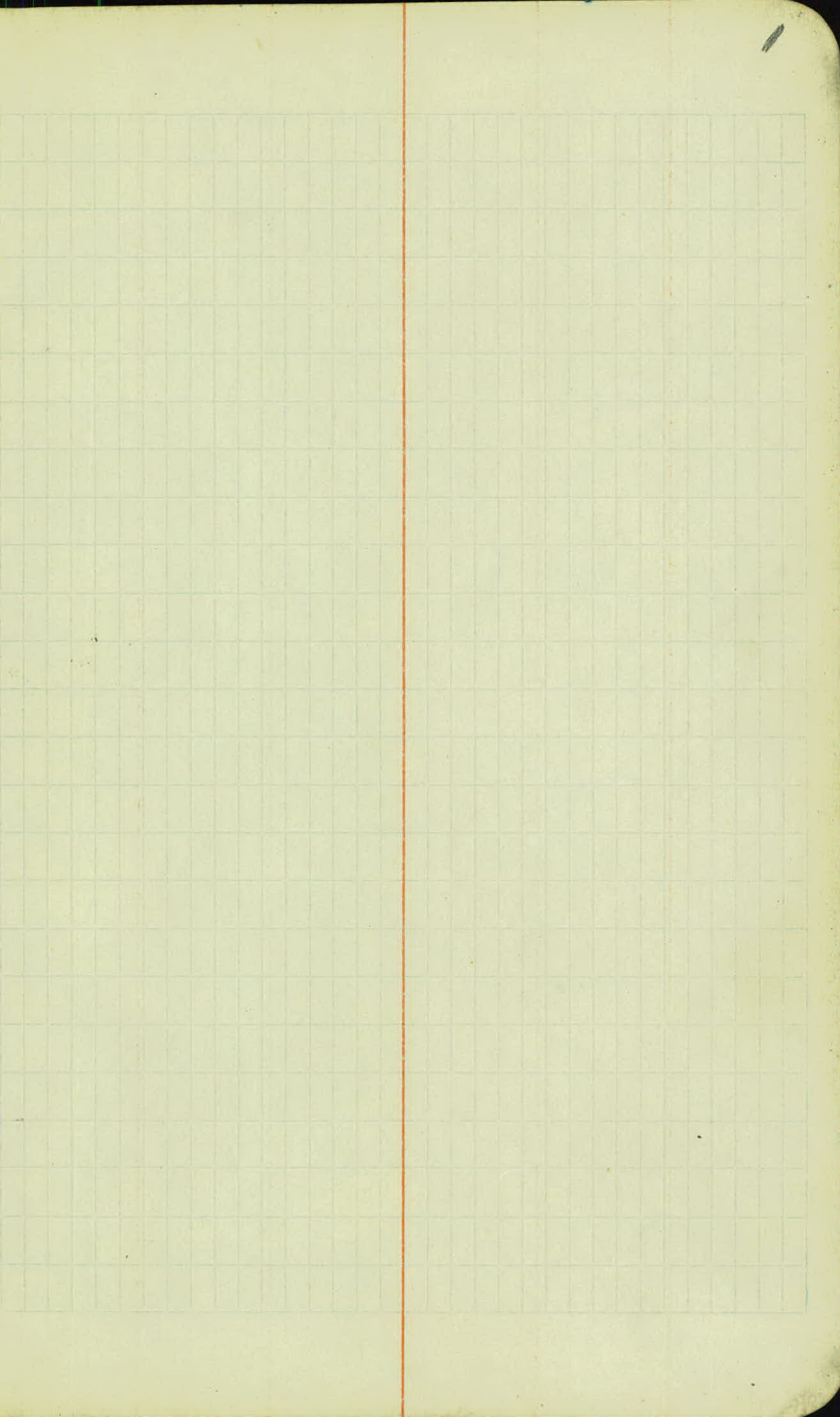
$$\begin{array}{r} .15 \\ \hline \sqrt{5} \\ \underline{5} \end{array}$$



PROJ. # 29-01

STA	To	STA	DESCRIPTION	PAGE	To	PAGE
0+00		244	ALIGNMENT	1		7
72	X	98	ORIGINAL X SECTIONS	15		19
51	X	72	ORIGINAL X SECTIONS	20		23
15	X	51	ORIGINAL X SECTIONS	25		31
122	X	202	ORIGINAL X SECTIONS	32		
202	X	209	ORIGINAL X SECTIONS	62		63
209	X	216	ORIGINAL X SECTIONS	60		61
216	X	222	ORIGINAL X SECTIONS	46		47
10	X	15	ORIGINAL X SECTIONS	55		
98	X	103	ORIGINAL X SECTIONS	59		58
117	X	122	ORIGINAL X SECTIONS	56		
	X		ORIGINAL X SEC. BORROW PIT. # 1	66		
			BENCH MARKS	79		
10		244	GRADES - SUPER ELEV.	67		75





STA POINT Δ LT. Δ RT.

✓ 6716<sup>04</sup> 24°38'<sup>30</sup>  
 6 20°  
 +50 22°  
 5 20°  
 +50 18°  
 4 16°  
 +50 14°

N 49°-17' W.

✓ 3728<sup>8</sup> P.I. A-49°-17' ✓  
 3 12° D-8°-1. ✓  
 +50 10° T-328<sup>8</sup> ✓  
 2 8° L-616<sup>04</sup> ✓  
 +50 6° R-716<sup>78</sup> ✓  
 1 4°  
 +50 02°0'

✓ 0700 P.C.

N 00°-00' E.

✓ 252762<sup>65</sup> P.O.T.

CO. ROAD E.  
STONE MT.

803 45



HOLE IN PAVE.

PRICE ST.

37A. POINT A 67. A RT

✓ 43 + 29 <sup>2</sup> P.O.T.

N 18° - 17' W

✓ 19 + 95 <sup>33</sup> P.T.

15° - 30

750

✓ 14° - 22

19

✓ 13° - 07

750

✓ 11° - 52

18

✓ 10° - 37

750

✓ 7° - 22

17

✓ 5° - 07

✓ 16 + 93 <sup>2</sup> P.I.

Δ - 31° - 00 ✓

750

✓ 6° - 52 P - 5° - N ✓

16

✓ 5° - 37 T - 317 <sup>57</sup> ✓

750

✓ 4° - 22 L - 620° ✓

15

✓ 3° - 07 R - 1146 <sup>28</sup> ✓

750

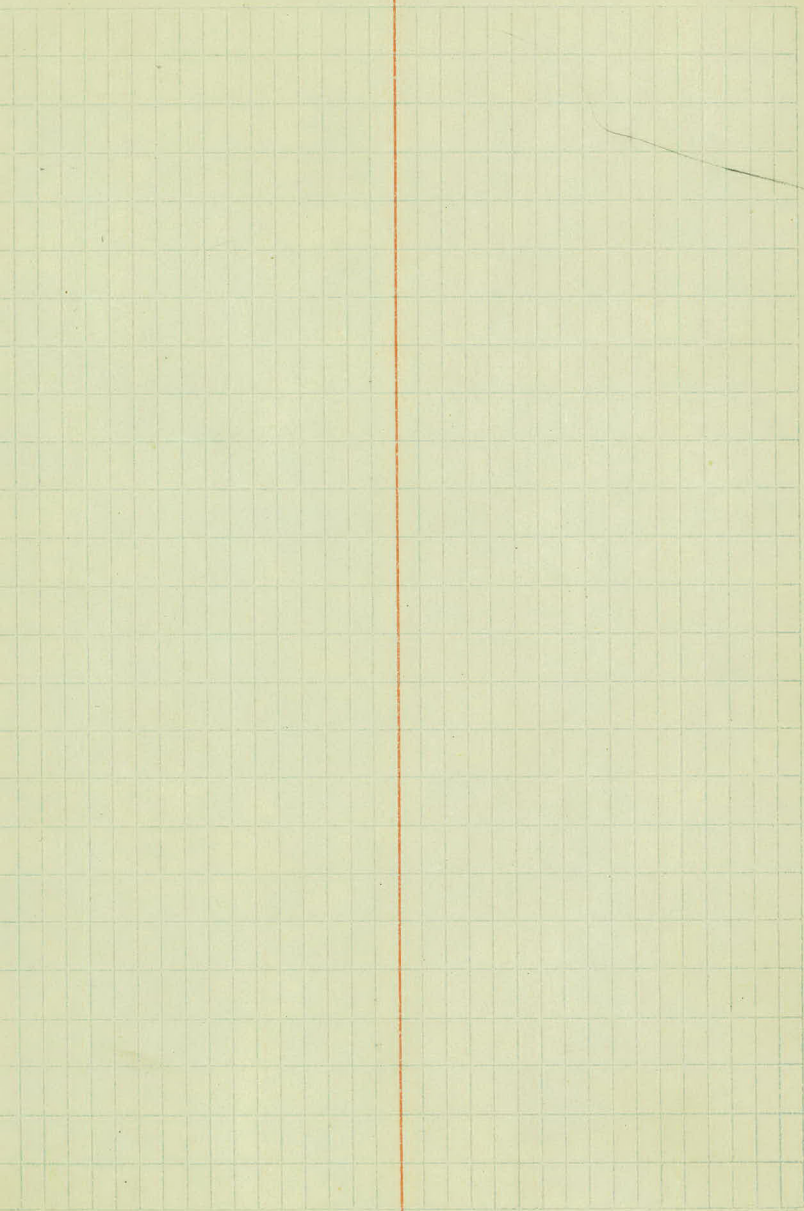
✓ 1° - 52

14

✓ 0° - 37

✓ 13 + 75 <sup>33</sup> P.C.

0° - 00



STA.	POINT	$\Delta$ LT	$\Delta$ RT
85+84 <sup>05</sup>	P.T.	2°-12'	
+50		1°-51' <sup>E</sup>	
85+00		1°-21' <sup>E</sup>	
84+74 <sup>12</sup>	P.I.		$\Delta$ -4°-24' ✓
+50		0°-51' <sup>E</sup>	D.-2°-L. ✓
84+00		0°-21' <sup>E</sup>	T.-110 <sup>07</sup> ✓
83+64 <sup>05</sup>	P.C.	0°-00'	L.-220 <sup>00</sup> ✓
			R.-2864 <sup>25</sup> ✓

N 22°-20' W

71+35<sup>4</sup> P.O.T.

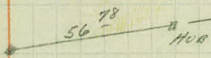
N 25°-41' W

43+55<sup>8</sup> P.I. 0°-21' ✓

9-21-29

Tro. 75.15

TOP OF PLATE  
FALL ON HILLS  
FRANK



71°-55'

CO. ROAD G.

70.80

HUB

G. 2'

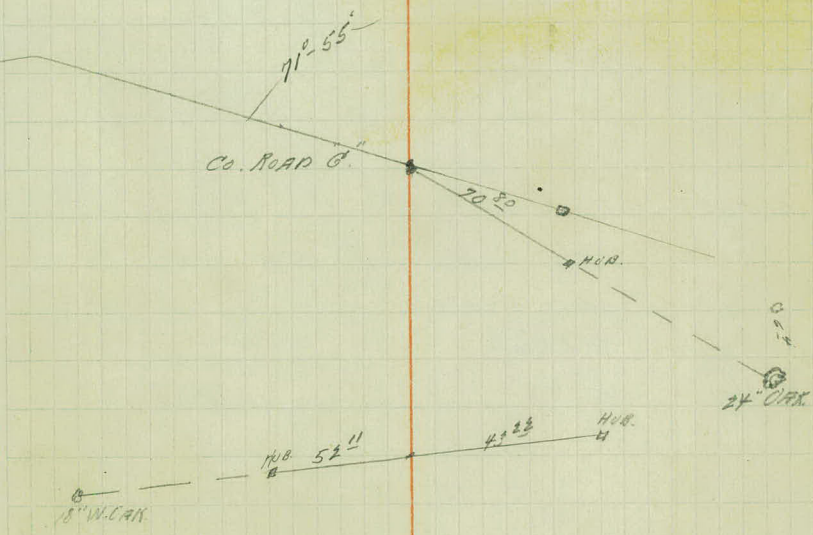
24" CRK.

HUB 52.11

41.25

HUB

15" W. CRK.



STA POINT Δ LT A RT.

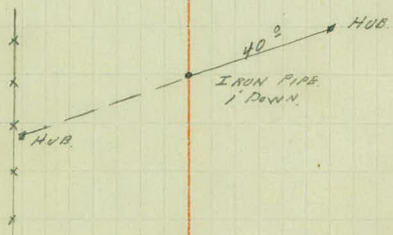
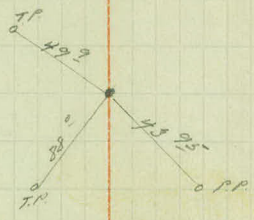
N 60°-32' W

✓ 127+03 <sup>43</sup>	P.T.		20°-37	
127			20°-32	
+50			17°-17	
126			18°-02	
+50			16°-47	
125			15°-32	
+50			14°-17	
124			15°-02	
+50			11°-47	
✓ 123+10°	P.I.			Δ-41°-14 ✓
123			10°-32	
+50			9°-17	D-5°-R ✓
122			8°-02	23 ✓
+50			6°-47	T-431 ✓
121			5°-32	60 ✓
+50			4°-17	L-824 ✓
120			3°-02	38 ✓
+50			1°-47	R-1146 ✓
119 <sup>77</sup>			0°-32	
✓ 118+78	P.C.		0°-00	

N 41°-45' W

✓ 100+92 <sup>98</sup>	P.T.	9°-43	✓	
+50		8°-38 <sup>5</sup>	✓	
100		7°-23 <sup>5</sup>	✓	
+50		6°-08 <sup>5</sup>	✓	
✓ 99+00°	P.I.			Δ-19°-26 ✓
99		4°-53 <sup>5</sup>	✓	P-5°-L ✓
+50		5°-38 <sup>5</sup>	✓	T-196 <sup>28</sup> ✓
98		2°-23 <sup>5</sup>	✓	L-388 <sup>60</sup> ✓
+50		1°-08 <sup>5</sup>	✓	R-1146 <sup>28</sup> ✓
32				
✓ 97+04	P.C.	0°-00		

9-21-29



STA. POINT ALT. Δ PT.

✓ 184730<sup>3</sup> P. I. 0°-26' ✓

N 00°-03' E.

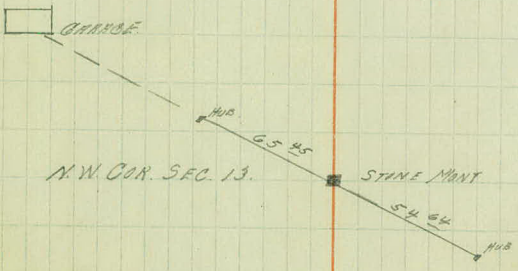
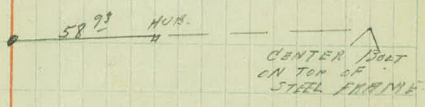
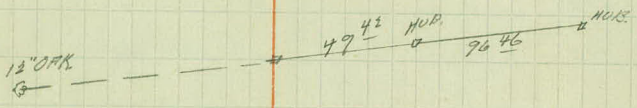
✓ 158710<sup>6</sup> P. I. 0°-14' ✓

✓ 152755<sup>85</sup> P.O.T.

N 00°-11' W.

✓ 131765<sup>7</sup> P. I. 0°-21' ✓

10-2-29



STA POINT Δ LT Δ RT

✓ 243+16<sup>7</sup> P.T

3°-05<sup>E</sup>

243

2°-46

150

1°-46

✓ 242+59<sup>5</sup> P.I

A-6°-11' ✓

242

0°-46' D°-4°-R. ✓

✓ 241+62<sup>12</sup> P.C.

0°-00' T-77<sup>58</sup> ✓

L-154<sup>58</sup> ✓

R-1432<sup>69</sup> ✓

✓ 224+72<sup>3</sup> P.O.T.

N00°-08' W

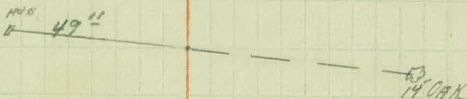
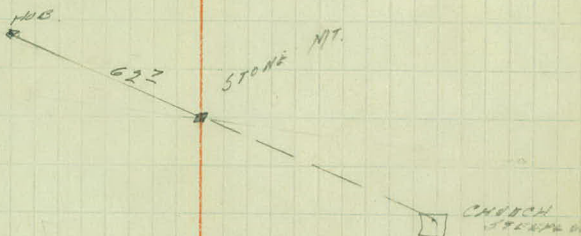
✓ 210+69<sup>55</sup> P.I.

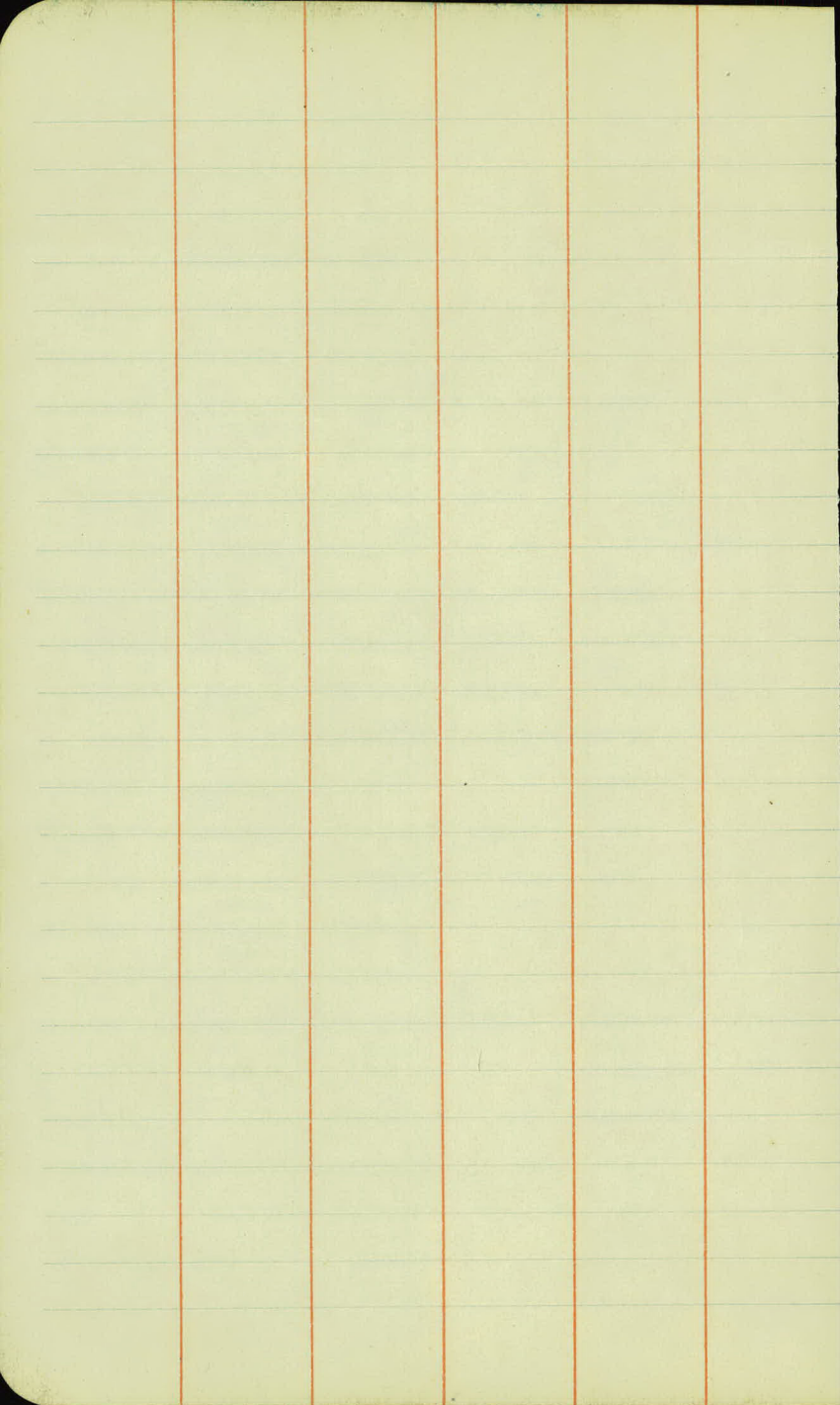
0°-15' ✓

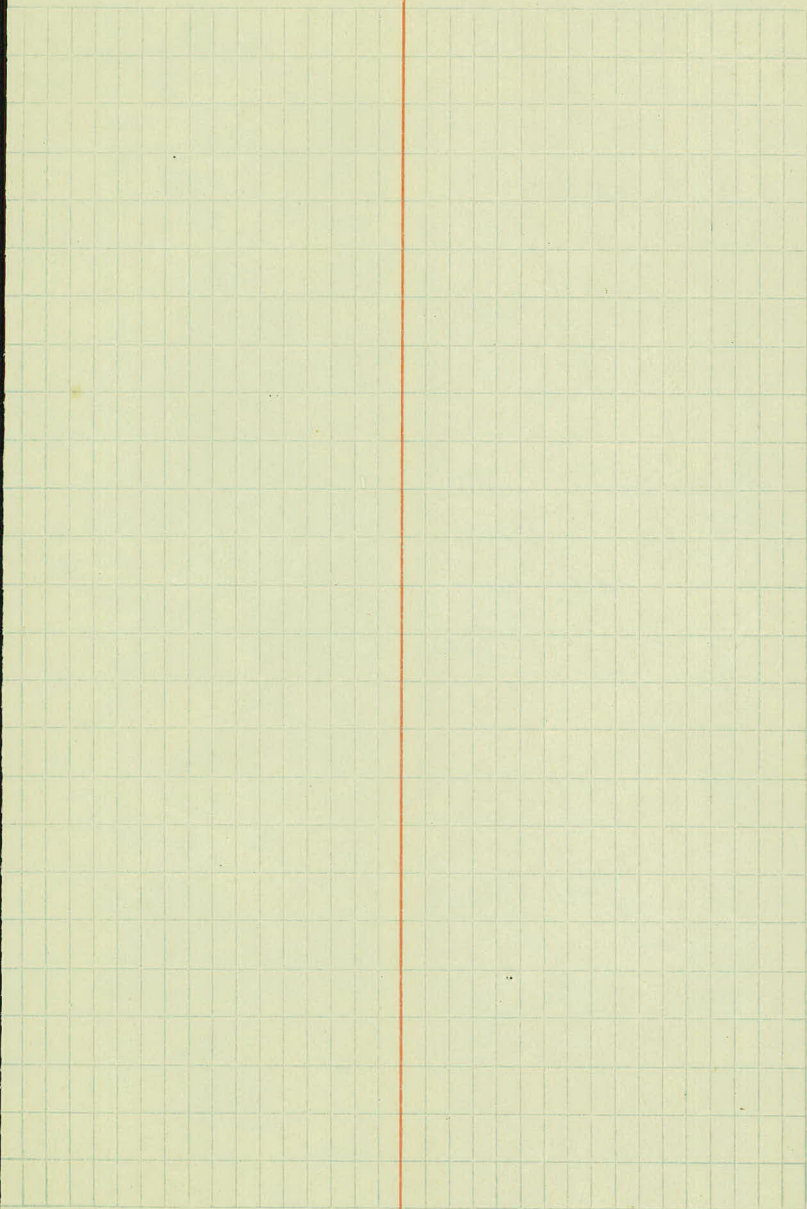
N00°-23' W

500  
167  
---  
333

10-3-29







STA.	T	H.I	-	ELEV	CR. ROD
B.M.	5.86	932.94	✓	927.08	
72				28.7	42 -
+50				28.75	42 -
73				28.8	41 -
+50				28.85	41 -
74				28.9	40 -
+50				28.95	40 -
75				29.0	39 -
+50				29.05	39 -
	5.26	934.11	✓	928.85	
76			4.09	29.1	5.0 -
+50				29.15	5.0 -
77				29.2	49 -
+50				29.25	49 -

LEFT

RIGHT 7-23-29  
Close

SPK IN 18" OAK 35 FT. STA 70+15.

52	1/52	5/52	53	56	48	42	54	3/56	3/55	55
33	5/-10	2/-10	18	12	06	15	2/44	2/-13		33

47	5/47	5/47	48	53	47	42	54	1/56	6/53	52
33	3/-05	2/-05	17	11	05	13	2/13	3/-11		33

48	2/48	5/46	49	52	47	41	56	61	61	55	1/54	3/54	54
33	5/-07	2/-05	12	11	06	17	18	19	20	2/-13	3/-13		33

63	2/61	5/56	53	55	49	41	60	62	3/60	2/57	56	
33	2/-20	2/-15	13	10	08	16	17	18	19	2/-16		33

73	5/70	63	55	49	40	56	60	66	60	3/59	2/56	55
33	2/-30	16	11	09	12	17	18	21	22	2/-19	2/-16	33

74	3/49	60	53	47	40	54	51	54	57	5/55	4/52	52
33	2/-29	21	12	07	12	15	17	19	20	2/-15	3/-12	33

66	63	7/60	52	51	45	39	50	42	1/52	7/49	49
33	27	2/-21	17	11	06	13	16	2/-13	3/-10		33

60	4/58	55	2/52	51	44	48	42	39	46	44	45	9/51	46	3/45	45
33	2/-19	26	2/-13	19	12	11	09	12	13	19	2/72	28	3/-06		33

63	4/61	7/55	52	48	40	54	50	3/58	5/54	54
33	3/-12	2/-06	11	10	2	11	14	2/-09	3/-05	33

59	0/57	9/51	50	47	40	53	50	9/56	4/48	47
33	3/-08	9/-02	11	10	3	13	14	2/-07	3/01	33

60	4/60	2/51	42	46	49	49	5/48	1/44	44	
33	3/-13	2/-03	11	10	3	12	17	00	2/104	33

61	1/58	59	1/51	45	52	46	49	5/48	41	3/41	41		
33	5/-10	26	2/-03	13	11	10	3	13	17	00	26	3/107	35

STA.	T	H.I.	-	ELEV	Cor. Pol.
		934.11			
78				293	4.8 -
	+50			293.5	4.8 -
79				294	4.7 -
	+50			293	4.8 -
80				292	4.9 -
T.P.	3.39	933.84	3.66	930.45	
	+50			290	4.8 -
81				287	5.1 -
	+50			283	5.5 -
82				279	5.9 -
	+50			275	6.3 -
83				271	6.7 -
	4.05	931.84	4.05	927.79	
	+50			267	5.4 5.1 - 4.0

9-23-29

$\frac{60}{33}$	$\frac{3}{3} \frac{60}{73}$	$\frac{3}{3} \frac{51}{74}$	45	52	46	(44)	50	43	$\frac{42}{3}$	40
			15	10	10	12	10	8	10	33

$\frac{59}{33}$	$\frac{9}{3} \frac{56}{79}$	$\frac{5}{2} \frac{52}{75}$	48	52	47	(48)	51	48	$\frac{9}{3} \frac{49}{79}$	47
			16	11	10	11	11	10	8	33

$\frac{60}{33}$	$\frac{3}{3} \frac{59}{73}$	$\frac{9}{9} \frac{48}{72}$	44	51	46	(47)	50	44	$\frac{1}{2} \frac{49}{79}$	$\frac{1}{3} \frac{47}{71}$	47
			15	10	10	11	16	2	2	3	33

$\frac{57}{33}$	$\frac{9}{3} \frac{56}{79}$	45	45	53	48	(48)	50	$\frac{6}{9} \frac{47}{77}$	$\frac{5}{3} \frac{45}{72}$
		20	18	11	00	11	11	00	5

$\frac{61}{33}$	$\frac{9}{3} \frac{60}{72}$	$\frac{5}{9} \frac{48}{72}$	47	52	48	(49)	52	48	46	$\frac{2}{3} \frac{48}{72}$
			17	12	10	10	14	17	5	00

$\frac{60}{33}$	$\frac{6}{3} \frac{59}{71}$	54	51	54	52	47	51	46	45	$\frac{3}{3} \frac{47}{71}$	47
		25	20	14	10	10	11	16	22	3	33

$\frac{60}{33}$	$\frac{3}{3} \frac{57}{76}$	57	48	58	56	52	56	49	$\frac{6}{3} \frac{48}{76}$	48
		23	16	13	10	11	11	17	3	33

$\frac{60}{33}$	$\frac{6}{3} \frac{59}{74}$	55	50	62	62	58	61	51	$\frac{8}{3} \frac{51}{74}$	51
		22	18	13	10	13	11	19	3	33

$\frac{68}{33}$	$\frac{12}{3} \frac{66}{77}$	58	64	67	65	67	63	63	$\frac{6}{3} \frac{62}{78}$	62
		24	15	13	11	12	12	12	3	33

$\frac{64}{33}$	$\frac{2}{3} \frac{68}{70}$	63	69	69	70	64	69	67	$\frac{0}{3} \frac{71}{71}$	72
		20	17	12	11	13	11	12	3	33

$\frac{54}{35}$	$\frac{3}{3} \frac{54}{73}$	64	67	73	69	(67)	73	70	$\frac{3}{3} \frac{73}{73}$	73
		28	19	12	12	11	13	13	3	33

$\frac{32}{35}$	$\frac{0}{3} \frac{32}{72}$	49	54	50	55	(51)	52	$\frac{0}{2} \frac{51}{73}$	$\frac{6}{3} \frac{52}{74}$	52
		14	13	10	11	13	13	2	3	33

STA.	+	H.I.	✓	-	ELEV	CR. POP.
		931.84				
84					263	60 55.5
	+50				260	64 58.5
85					257	67 61.5
	+50				254	69 64.5
B.M.	1.53	928.64	✓	4.83	927.01	927.01
86					25.2	3.6 33.5
B.M.				3.31	925.23	
	+50				25.0	3.5
87					24.8	3.7
	+50				24.7	3.8
88					24.6	3.9
	+50				24.6	3.9
89					24.6	3.9
	+50				24.6	3.9
	5.37	929.47	✓	4.44	924.10	

7-24-27

$\frac{26}{35}$	$\frac{0}{3} \frac{28}{152}$	$\frac{48}{14}$	$\frac{56}{13}$	$\frac{52}{10.8}$	$\frac{59}{12}$	$\frac{51}{17}$	$\frac{5}{8} \frac{48}{102}$	$\frac{48}{33}$
-----------------	------------------------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	-----------------

$\frac{30}{35}$	$\frac{0}{3} \frac{28}{136}$	$\frac{46}{23}$	$\frac{46}{14}$	$\frac{62}{11}$	$\frac{58}{0.0}$	$\frac{65}{14.1}$	$\frac{1}{9} \frac{53}{01}$	$\frac{51}{21}$	$\frac{5}{3} \frac{50}{102}$	$\frac{50}{33}$
-----------------	------------------------------	-----------------	-----------------	-----------------	------------------	-------------------	-----------------------------	-----------------	------------------------------	-----------------

$\frac{49}{35}$	$\frac{0}{3} \frac{47}{120}$	$\frac{46}{18}$	$\frac{70}{11}$	$\frac{65}{-0.4}$	$\frac{71}{15}$	$\frac{9}{9} \frac{57}{-02}$	$\frac{42}{24}$	$\frac{0}{3} \frac{47}{108}$	$\frac{47}{35}$
-----------------	------------------------------	-----------------	-----------------	-------------------	-----------------	------------------------------	-----------------	------------------------------	-----------------

$\frac{62}{33}$	$\frac{5}{3} \frac{67}{102}$	$\frac{63}{15}$	$\frac{25}{12}$	$\frac{7}{-0.7}$	$\frac{73}{14.2}$	$\frac{1}{2} \frac{67}{-08}$	$\frac{3}{3} \frac{58}{101}$	$\frac{58}{35}$
-----------------	------------------------------	-----------------	-----------------	------------------	-------------------	------------------------------	------------------------------	-----------------

$\frac{62}{33}$	$\frac{8}{2} \frac{52}{22}$	$\frac{9}{2} \frac{53}{77}$	$\frac{51}{20}$	$\frac{40}{16}$	$\frac{48}{11}$	$\frac{42}{0.9}$	$\frac{46}{14}$	$\frac{1}{2} \frac{48}{-13}$	$\frac{5}{2} \frac{48}{-18}$	$\frac{46}{33}$
-----------------	-----------------------------	-----------------------------	-----------------	-----------------	-----------------	------------------	-----------------	------------------------------	------------------------------	-----------------

S.P.K. IN 12" CAN. 40 LT. STR. 25+70.

$\frac{72}{33}$	$\frac{9}{2} \frac{72}{57}$	$\frac{62}{20}$	$\frac{55}{18}$	$\frac{51}{11}$	$\frac{46}{1.1}$	$\frac{52}{15}$	$\frac{58}{19}$	$\frac{3}{2} \frac{59}{24}$	$\frac{56}{33}$
-----------------	-----------------------------	-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------------------	-----------------

$\frac{85}{33}$	$\frac{6}{2} \frac{82}{45}$	$\frac{72}{20}$	$\frac{59}{17}$	$\frac{58}{12}$	$\frac{52}{-1.3}$	$\frac{55}{14}$	$\frac{61}{16}$	$\frac{3}{2} \frac{62}{29}$	$\frac{65}{33}$
-----------------	-----------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	-----------------------------	-----------------

$\frac{79}{33}$	$\frac{7}{2} \frac{70}{82}$	$\frac{63}{19}$	$\frac{58}{12}$	$\frac{51}{-1.5}$	$\frac{57}{13}$	$\frac{62}{16}$	$\frac{3}{2} \frac{67}{29}$	$\frac{65}{33}$
-----------------	-----------------------------	-----------------	-----------------	-------------------	-----------------	-----------------	-----------------------------	-----------------

$\frac{64}{33}$	$\frac{8}{2} \frac{62}{28}$	$\frac{58}{26}$	$\frac{52}{14}$	$\frac{57}{13}$	$\frac{50}{-1.1}$	$\frac{57}{15}$	$\frac{61}{15}$	$\frac{2}{2} \frac{61}{22}$	$\frac{60}{33}$
-----------------	-----------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	-----------------------------	-----------------

$\frac{62}{33}$	$\frac{9}{2} \frac{58}{79}$	$\frac{55}{23}$	$\frac{47}{15}$	$\frac{54}{13}$	$\frac{47}{-0.8}$	$\frac{54}{15}$	$\frac{50}{26}$	$\frac{1}{2} \frac{56}{-17}$	$\frac{56}{33}$
-----------------	-----------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	-----------------

$\frac{61}{33}$	$\frac{9}{2} \frac{58}{19}$	$\frac{56}{20}$	$\frac{52}{14}$	$\frac{55}{13}$	$\frac{45}{-0.6}$	$\frac{52}{15}$	$\frac{56}{25}$	$\frac{2}{2} \frac{56}{-17}$	$\frac{54}{33}$
-----------------	-----------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	-----------------

$\frac{54}{33}$	$\frac{8}{2} \frac{51}{16}$	$\frac{46}{15}$	$\frac{51}{13}$	$\frac{45}{-0.6}$	$\frac{51}{15}$	$\frac{56}{24}$	$\frac{1}{2} \frac{60}{-21}$	$\frac{54}{33}$
-----------------	-----------------------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	-----------------

STA.	+	H.I. ✓	-	ELEV	GR. ROD.
		929.47			
90				247	48.
	+50			24.75	4.7.
91				24.8	4.7.
	+50			24.85	4.6.
			3.54		
92				24.9	4.6.
	+50			24.95 ✓	4.5.
		2.31	929.76 ✓	2.02	927.45
93				25.0	4.8.
	+50			25.05	4.7.
94				25.1	4.7.
	+50			25.15	4.6.
95				25.2	4.4.
	+50			25.25	4.5. 4.4

7-24-27

5.3 5/5.3 5.2 4.5 5.7 5.2 6.0 6.5 5/6.0 6.5  
 33 3/-0.5 21 17 13 04 13 26 2/-1.8 33

(4.6)

5.0 5/5.0 4.7 4.9 4.6 5.6 5.2 6.1 6/6.0 6.1  
 33 3/-0.3 28 20 15 12 0.5 16 2/-1.9 33

(4.7)

4.5 5/4.5 4.9 5.7 5.2 6.0 6/6.2 6.2  
 33 3/0.2 15 11 0.5 15 3/-1.5 33

(4.7)

4.9 9/4.9 4.4 4.0 5.4 4.9 5.7 4.5 5.8 5.8  
 33 3/-0.3 22 17 14 0.3 1.5 3/-1.2 33

(4.6)

NAIL IN T.P. LT. STAR 91 165

3.7 0/3.7 3.8 5.4 4.8 5.4 4.9 5/5.2 5.2  
 35 3/1.09 19 14 0.2 15 16 3/-0.6 33

(4.6)

4.0 0/3.8 3.3 3.8 5.4 4.0 5.2 5.0 9/4.7 4.2  
 35 3/1.07 27 16 13 0.1 14 16 3/-0.2 33

(4.5)

NAIL IN T.P. LT. STAR 93 100

4.1 0/4.1 3.4 4.1 5.5 4.9 5.3 4.5 5/4.2 4.6  
 35 3/1.07 19 14 13 0.1 15 19 3/1.02 33

(4.8)

3.8 0/3.8 3.8 3.1 5.4 5.0 5.4 4.4 9/4.2 4.8  
 35 3/1.09 22 18 13 0.3 13 24 3/1.15 33

(4.7)

3.3 0/3.3 3.4 5.4 5.0 5.6 4.8 1/4.8 4.8  
 35 3/1.14 21 10 0.3 13 18 3/0.1 33

(4.7)

3.7 0/3.7 3.9 4.0 5.5 5.0 5.5 5.0 2/5.3 5.5  
 35 3/1.09 25 18 13 0.4 14 16 3/0.7 33

(4.6)

4.5 3/4.5 4.0 5.7 5.0 5.7 5.1 6/5.7 5.7  
 33 3/1.01 18 13 0.4 14 16 3/0.1 33

(4.6)

4.8 3/4.5 4.6 3.9 5.5 4.9 5.5 5.0 9/5.0 5.6  
 35 3/1.01 21 18 13 0.4 13 18 3/0.6 3/0.11 33

(4.5)

929.74 ✓

96

25.3 4.7 45.4

f50

25.35 5.2 44.3

97

25.4 5.6 44.3

f50

25.45 5.7 43.29

98

25.5 5.9 43.29 ✓

4.36

930.70

3.42

926.34 ✓

B.M

4.84

925.86 ✓

925.83 ✓

SEE PAGE 57

9-24-29  
Claus

50  $\frac{1}{5} \times$  44 40 54 49  $\frac{4}{15}$  54  $\frac{3}{5} \times$  56  $\frac{0}{3} \times$  56 56  
 33  $\frac{8}{-01}$  20 16 13 04 13  $\frac{2}{-09}$  28  $\frac{3}{-15}$  33

50  $\frac{8}{48}$  49 45 56 49  $\frac{4}{15}$  56 53  $\frac{7}{57}$   $\frac{8}{59}$  60  
 35  $\frac{8}{-04}$  20 16 13 05 13 19  $\frac{3}{-21}$   $\frac{8}{-23}$  33

48  $\frac{6}{60}$  71 21 54 48  $\frac{4}{15}$  52  $\frac{1}{55}$  57 60  
 34  $\frac{3}{-04}$   $\frac{2}{-16}$  17 11 04 13  $\frac{2}{-23}$  28 33

76  $\frac{9}{77}$  76  $\frac{5}{62}$  56 45  $\frac{4}{15}$  44 44  $\frac{3}{53}$  65 56  
 23  $\frac{2}{-20}$  27  $\frac{2}{-05}$  14 02 14 20  $\frac{4}{-24}$  30 33

75  $\frac{7}{74}$  73  $\frac{5}{57}$  53 45  $\frac{4}{15}$  40 40  $\frac{3}{53}$  63 50  
 33  $\frac{2}{-17}$  28  $\frac{1}{00}$  13 02 13 20  $\frac{4}{-24}$  30 33.5

SPK IN 24" ORX 100 LT. 57A. 100700

B.M.	7.16	928.96		924.80	
B.M.			4.12	924.84	
51				24.05	49'
+50				24.12	48'
	4.67	929.11	4.52	924.44	
52				24.3	48'
+50				24.45	47'
53				24.6	45'
+50				24.75	44'
54				24.9	42'
+50				25.05	41'
55				25.2	39'
+50				25.04	41'
56				25.47	36'

9-27-29

SPK IN 24" OAK 40 LT STA 42+50

SPK IN 18" OAK 55 LT STA 42+85

58 0/5.7 5/5.4 5.1 4.8 5.1 4.4 4/3.6 5.9  
33 3/-0.8 2/-0.5 11 10.1 12 15 3/1.5 4.3

5.3 5/5.3 4.7 4.5 5.0 4.6 5.0 3.8 4/3.3 5.3  
33 3/-0.5 20 11 10 10.2 12 13 3/1.5 4.3

4.8 3/4.7 3.8 5.1 4.7 4.9 3.2 0/2.9 3.5  
33 3/10.1 13 11 10.1 11 15 3/1.9 4.3

5.2 5/5.2 7/4.8 4.8 5.1 4.6 4.9 3.9 2/5.7 5.8  
33 3/-0.5 1/-0.1 13 11 10.1 11 14 3/1.0 4.3

5.8 4/5.7 3/5.4 5.3 5.2 4.5 5.0 4.6 9/4.7 5/2.8 4.6 4.6  
33 8/-1.2 2/-0.9 14 11 0.0 11 13 9/-0.2 5/-0.8 3.3 4.3

5.6 3/5.0 2/5.1 5.2 5.2 4.7 5.2 4.9 5/4.9 3/5.0 4.8  
33 3/-0.6 2/-0.7 17 11 -0.3 11 13 2/-0.5 3/-0.6 3.3

5.4 5.1 5.0 3/6.1 5.0 5.1 4.7 5.3 4.9 3/4.6 6/4.6 4.5  
33 -0.9 2.7 2/-1.9 13 12 -0.5 11 13 5/-0.4 3/1.1 3.3

6.2 5/5.7 7/5.2 5.1 5.0 4.7 5.1 4.5 4.0 3/4.0 3.8  
33 2/-7.8 2/-1.1 19 12 -0.6 11 12 20 3/10.1 3.3

6.6 4.3/6.3 6.0 5.1 4.6 5.2 5.1 9/4.6 0/4.7 4.4  
33 2/4.3 -2.4 14 13 -0.7 9 14 2/-0.7 3/-0.8 3.3

6.6 9/6.3 5.8 5.4 4.5 5.0 5.4 1/4.9 0/4.7 4.9  
33 3/-2.2 17 14 -0.4 12 13 2/-0.8 3/0.8 3.3

6.2 4.3/6.0 5.7 5.1 4.4 4.9 4.7 2/4.9 6/4.7 5.1  
33 2/2.4 15 13 -0.8 11 12 2/1.8 3/-1.1 3.3

✓  
729.11

f50

25.61

3.5 .

57

25.7

3.4 .

f50

25.8

3.3 .

58

25.9

3.2 .

5.09

729.95

4.25

724.86 ✓

f50

26.0

4.0 .

59

26.1

3.9 .

f50

26.2

3.8 .

60

26.3

3.7 .

f50

26.4

3.6 .

61

26.5

3.5 .

f50

26.6 ✓

3.4 .

B.M.

4.75

729.96

4.75

725.20

725.21

62

26.7

3.3 .

9-27-29

52	$\frac{2}{3} \frac{1}{5.7}$	$\frac{3}{2} \frac{1}{5.4}$	45	48	42	47	40	$\frac{9}{2} \frac{1}{4.2}$	$\frac{7}{3} \frac{1}{4.5}$	45
33	$\frac{2}{1} \frac{1}{2.2}$	$\frac{2}{1} \frac{1}{-1.9}$	13	12	-0.7	10	12	$\frac{2}{1} \frac{1}{-0.7}$	$\frac{3}{1} \frac{1}{-1.0}$	33

(3.1)

59	$\frac{2}{3} \frac{1}{5.8}$	$\frac{5}{2} \frac{1}{5.6}$	50	46	40	44	$\frac{3}{1} \frac{1}{4.3}$	$\frac{2}{1} \frac{1}{3.4}$	3.4
33	$\frac{2}{1} \frac{1}{2.4}$	$\frac{2}{1} \frac{1}{-2.2}$	17	12	-0.6	13	$\frac{2}{1} \frac{1}{-0.9}$	$\frac{2}{1} \frac{1}{0.0}$	33

(3.4)

52	$\frac{1}{3} \frac{1}{4.7}$	$\frac{7}{2} \frac{1}{4.4}$	44	41	44	36	$\frac{9}{1} \frac{1}{3.5}$	$\frac{2}{3} \frac{1}{3.2}$	3.2
33	$\frac{3}{1} \frac{1}{-1.4}$	$\frac{2}{1} \frac{1}{-1.1}$	12	-0.8	12	13	$\frac{1}{1} \frac{1}{-0.2}$	$\frac{3}{1} \frac{1}{1.01}$	33

(3.3)

56	$\frac{1}{3} \frac{1}{3.6}$	$\frac{2}{1} \frac{1}{3.6}$	37	45	40	44	35	$\frac{9}{1} \frac{1}{3.4}$	$\frac{5}{2} \frac{1}{3.0}$	3.0
33	$\frac{3}{1} \frac{1}{-0.4}$	$\frac{2}{1} \frac{1}{-0.4}$	12	11	-0.8	12	13	$\frac{1}{1} \frac{1}{-0.8}$	$\frac{2}{1} \frac{1}{1.02}$	33

(3.2)

32	$\frac{2}{3} \frac{1}{3.2}$	36	5.4	49	53	36	3.8	$\frac{2}{1} \frac{1}{3.3}$	3.4
35	$\frac{3}{1} \frac{1}{1.8}$	12	11	-0.9	12	16	20	$\frac{2}{1} \frac{1}{1.07}$	35

(4.0)

24	$\frac{2}{3} \frac{1}{2.4}$	26	5.1	47	51	35	$\frac{2}{1} \frac{1}{3.4}$	3.7
35	$\frac{3}{1} \frac{1}{1.5}$	14	11	-0.8	13	16	$\frac{2}{1} \frac{1}{1.05}$	35

(3.9)

20	$\frac{3}{1} \frac{1}{2.0}$	3.0	4.4	50	47	51	4.5	$\frac{1}{2} \frac{1}{4.4}$	$\frac{9}{3} \frac{1}{4.4}$	4.4
35	$\frac{3}{1} \frac{1}{1.8}$	17	12	11	-0.9	13	14	$\frac{2}{1} \frac{1}{-0.6}$	$\frac{3}{1} \frac{1}{-0.6}$	33

(3.8)

32	$\frac{2}{3} \frac{1}{3.2}$	$\frac{2}{1} \frac{1}{4.0}$	4.5	4.9	4.5	5.0	4.8	$\frac{7}{2} \frac{1}{4.9}$	$\frac{3}{1} \frac{1}{5.0}$	5.0
35	$\frac{3}{1} \frac{1}{1.05}$	$\frac{2}{1} \frac{1}{-0.3}$	12	11	-0.8	11	13	$\frac{2}{1} \frac{1}{-1.2}$	$\frac{3}{1} \frac{1}{-1.3}$	33

(5.7)

47	$\frac{2}{3} \frac{1}{4.8}$	$\frac{7}{2} \frac{1}{4.7}$	4.9	4.5	4.7	5.1	5.1	$\frac{2}{1} \frac{1}{5.0}$	$\frac{2}{1} \frac{1}{5.1}$	5.1
33	$\frac{3}{1} \frac{1}{-1.2}$	$\frac{2}{1} \frac{1}{-1.1}$	11	11	-0.9	11	16	$\frac{2}{1} \frac{1}{-1.4}$	$\frac{3}{1} \frac{1}{-1.5}$	33

(3.6)

5.1	$\frac{2}{3} \frac{1}{5.0}$	$\frac{5}{2} \frac{1}{5.0}$	5.0	4.8	4.4	4.8	5.2	$\frac{7}{2} \frac{1}{5.1}$	$\frac{9}{3} \frac{1}{5.7}$	5.6
33	$\frac{3}{1} \frac{1}{-1.3}$	$\frac{2}{1} \frac{1}{-1.5}$	19	12	-0.9	12	18	$\frac{2}{1} \frac{1}{-1.6}$	$\frac{2}{1} \frac{1}{-2.2}$	33

(3.3)

5.3	$\frac{2}{3} \frac{1}{5.2}$	$\frac{9}{2} \frac{1}{5.1}$	5.0	4.5	5.0	4.7	5.2	$\frac{2}{1} \frac{1}{5.2}$	$\frac{2}{1} \frac{1}{5.2}$	5.2
33	$\frac{2}{1} \frac{1}{-1.8}$	$\frac{2}{1} \frac{1}{-1.7}$	13	-1.1	10	14	$\frac{2}{1} \frac{1}{-1.8}$	$\frac{2}{1} \frac{1}{-1.8}$	33	

(3.4)

SPK IN 18" MAX 50, LT 57A 61+80.

6.1	$\frac{7}{2} \frac{1}{5.9}$	5.6	5.1	4.5	4.8	4.1	$\frac{1}{2} \frac{1}{4.1}$	$\frac{6}{1} \frac{1}{4.4}$	4.5
33	$\frac{2}{1} \frac{1}{-2.6}$	15	13	-1.0	12	14	$\frac{2}{1} \frac{1}{-0.8}$	$\frac{2}{1} \frac{1}{-1.1}$	33

(5.5)

929.76 ✓

f50

268

3.2 ✓

63

267

3.1 ✓

f50

270

3.0 ✓

64

271

2.9 ✓

3.39

931.51 ✓

1.84

928.12 ✓

f50

272

4.5 ✓

65

273

4.2 ✓

f50

274

4.1 ✓

66

275

4.0 ✓

f50

276

3.9 ✓

67

277

3.8 ✓

f50

278

3.7 ✓

5.08

931.85 ✓

4.74

926.77 ✓

B.M.

4.77

927.08 ✓

B.M.

4.08

927.77 ✓

9-27-29

60	59	3/41	41	48	45	46	43	7/38	6/36	35
33	29	2/29	17	13	7.1	12	13	2/0.6	5/04	33

(32)

50	5/49	2/47	42	46	40	43	35	9/33	2/31	31
53	2/1.8	2/76	15	14	09	12	13	9/02	2/00	33

(31)

36	3/36	0/33	32	43	38	41	31	2/30	2/30	29
33	3/26	2/03	15	13	0.8	11	14	9/20	3/00	33

(30)

27	5/27	7/30	30	40	51	42	35	0/32	2/30	37
33	3/10.2	9/01	15	12	08	11	17	2/03	3/07	35

(29)

49	5/48	5/50	51	57	53	58	51	2/49	3/49	48
33	3/05	2/07	14	12	7.0	11	14	2/06	3/16	33

(28)

49	2/49	2/48	49	57	53	58	47	5/47	5/47	47
33	3/07	2/06	13	12	7.1	12	15	2/05	3/05	33

(27)

44	8/44	0/44	44	56	52	54	44	9/47	6/45	44
33	3/03	2/03	14	12	7.1	13	16	2/06	3/04	33

(26)

37	6/37	35	56	50	55	38	35	0/33	33
33	3/103	15	12	7.0	12	14	20	3/107	33

(25)

29	0/29	29	55	50	55	28	0/26	26
33	3/10	16	13	7.1	11	14	3/113	33

(24)

28	0/28	27	53	49	54	27	0/26	26
33	3/110	15	13	7.1	11	14	3/112	33

(23)

33	8/33	32	51	47	53	29	0/30	30
33	3/104	15	13	7.0	12	14	3/107	33

(22)

SRK IN 18" OAK 75 RTSTP. 70+55.

B.M.	4.53	932.30	927.77	
68			27.9	4.4
+50			28.0	4.3
69			28.1	4.2
+50			28.2	4.1
70			28.3	4.0
+50			28.4	3.9
71			28.5	3.8
+16			28.5	3.8
+35			28.6	3.7
+80			28.7	
B.M.	4.53	927.77		

SEE PAGE 15

9-28-29

SPK IN 18" OAK 75' RT STA. 70+55.

$\frac{46}{33}$	$\frac{9}{3}/\frac{46}{-02}$	$\frac{37}{20}$	$\frac{43}{14}$	$\frac{58}{13}$	$\frac{52}{-08}$	$\frac{58}{14}$	$\frac{1}{2}/\frac{62}{-18}$	$\frac{41}{27}$	$\frac{0}{3}/\frac{59}{+05}$	$\frac{59}{35}$
-----------------	------------------------------	-----------------	-----------------	-----------------	------------------	-----------------	------------------------------	-----------------	------------------------------	-----------------

$\frac{47}{33}$	$\frac{1}{3}/\frac{47}{-04}$	$\frac{9}{19}/\frac{44}{-01}$	$\frac{44}{14}$	$\frac{53}{12}$	$\frac{50}{-07}$	$\frac{55}{14}$	$\frac{64}{17}$	$\frac{1}{4}/\frac{66}{-25}$	$\frac{9}{8}/\frac{65}{-22}$	$\frac{66}{33}$
-----------------	------------------------------	-------------------------------	-----------------	-----------------	------------------	-----------------	-----------------	------------------------------	------------------------------	-----------------

$\frac{55}{33}$	$\frac{0}{3}/\frac{55}{-13}$	$\frac{7}{2}/\frac{53}{-11}$	$\frac{49}{13}$	$\frac{52}{12}$	$\frac{48}{-06}$	$\frac{52}{12}$	$\frac{45}{18}$	$\frac{50}{27}$	$\frac{0}{3}/\frac{56}{-14}$	$\frac{67}{33}$
-----------------	------------------------------	------------------------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------	------------------------------	-----------------

$\frac{60}{33}$	$\frac{9}{2}/\frac{60}{-19}$	$\frac{5}{2}/\frac{51}{-10}$	$\frac{51}{17}$	$\frac{56}{14}$	$\frac{50}{-09}$	$\frac{56}{11}$	$\frac{1}{2}/\frac{59}{-18}$	$\frac{0}{3}/\frac{51}{-10}$	$\frac{51}{33}$
-----------------	------------------------------	------------------------------	-----------------	-----------------	------------------	-----------------	------------------------------	------------------------------	-----------------

$\frac{56}{33}$	$\frac{9}{2}/\frac{57}{-17}$	$\frac{1}{2}/\frac{58}{-18}$	$\frac{56}{15}$	$\frac{48}{-08}$	$\frac{57}{14}$	$\frac{59}{27}$	$\frac{2}{4}/\frac{60}{-20}$	$\frac{59}{33}$
-----------------	------------------------------	------------------------------	-----------------	------------------	-----------------	-----------------	------------------------------	-----------------

$\frac{47}{33}$	$\frac{5}{3}/\frac{44}{-05}$	$\frac{5}{2}/\frac{49}{-10}$	$\frac{45}{13}$	$\frac{50}{12}$	$\frac{47}{-07}$	$\frac{53}{12}$	$\frac{48}{13}$	$\frac{7}{2}/\frac{55}{-16}$	$\frac{4}{3}/\frac{51}{-12}$	$\frac{54}{33}$
-----------------	------------------------------	------------------------------	-----------------	-----------------	------------------	-----------------	-----------------	------------------------------	------------------------------	-----------------

$\frac{37}{33}$	$\frac{5}{2}/\frac{36}{+02}$	$\frac{9}{19}/\frac{40}{-02}$	$\frac{40}{14}$	$\frac{47}{12}$	$\frac{47}{-06}$	$\frac{46}{12}$	$\frac{54}{2}/\frac{48}{-10}$	$\frac{7}{3}/\frac{48}{-10}$	$\frac{47}{33}$
-----------------	------------------------------	-------------------------------	-----------------	-----------------	------------------	-----------------	-------------------------------	------------------------------	-----------------

$\frac{23}{33}$	$\frac{36}{23}$	$\frac{41}{16}$	$\frac{44}{12}$	$\frac{47}{-}$	$\frac{45}{12}$	$\frac{49}{33}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------

$\frac{46}{33}$	$\frac{44}{23}$	$\frac{39}{-02}$	$\frac{40}{14}$	$\frac{43}{33}$
-----------------	-----------------	------------------	-----------------	-----------------

SEE ORIGINAL NOTES

SPK IN 18" OAK 75' RT STA. 70+55.

~~13.41 1.54 921.41 719.87~~

~~15 17.4 56 40 5~~

VOID.

~~+50 17.0 50 44 5~~

~~16 16.7 53 47.6~~

~~+50 16.4 50 50 0~~

~~17 16.4 56 50 6~~

VOID.

~~+50 16.4 56 50 0~~

~~18 16.6 54 48 6~~

~~SPX IN 24" ORK 60 AT STR 15725~~

~~5.2 30 78 8/20 43 37 44 53 3/54 66 92  
43 38 31 2/-44 20 15 -04 15 9/00 32 43~~

~~VOID~~

~~6.2 64 2/78 72 43 47 9/60 65 8/85 89 58 5.8  
43 39 2/-48 26 20 -03 9/-02 23 2/-28 34 41 45~~

~~64 67 2.8 5/85 64 48 49 59 5/61 67 0/86 97 52 5.4  
43 39 33 2/-50 25 20 -0.2 18 9/00 23 4/-25 31 40 43~~

~~8 60 8.1 8.7 7/82 80 60 48 90 60 9/62 65 0/89 94 90 48  
3 41 34 32 2/-46 27 24 27 0.0 18 9/102 28 2/-25 31 34 43~~

~~5.2 55 73 9/83 72 52 5.1 41 3/64 67 0/89 95 8.7 48  
43 37 33 2/-47 26 20 -0.1 18 9/00 28 2/-25 30 35 43~~

~~VOID~~

~~5.1 55 72 8.1 3/79 71 64 50 5.2 9/62 84 0/88 85 47  
41 37 33 30 2/-84 27 25 20 -0.2 9/102 20 2/-24 33 43~~

~~1.2 29 74 1/72 69 47 51 5/62 63 86 0/87 91 8.3 45 45  
43 36 29 2/-38 26 20 -0.5 9/00 22 27 2/00 29 33 40 43~~

NOTE SEE PAGE 55 FOR X SEC. FROM  
 STA. 11+00 TO STA. 14+50



B.M.	1.55	921.42		917.87	
15				174	26 40
+50				170	50 44
16				167	53 47
+50				164	36 50
17				164	36 50
+50				164	36 50
18				166	54 48
+50				169	51 45
	4.94	922.79	3.59	917.85	
19				172	42 54
+50				175	39 53
20				177	58 49
+50				183	57 45



9-30-29

SPK IN 24" CAN GO LT 577. 15 + 25  
 5.1 31 79 76 44 38 44 <sup>(4.0)</sup> 5.4 7.3  
 43 37 30 26 20 17 24 17 43

62 68 74 <sup>3/25</sup> 73 44 47 <sup>(4.4)</sup> 59  
 43 32 30 <sup>2/45</sup> 26 20 23 19.5 <sup>8/25</sup> 8.7 5.8 5.8  
 2/2.5 33 41 43

65 67 84 <sup>5/28</sup> 48 49 <sup>(4.7)</sup> 61 66 <sup>2/26</sup> 73 5.2 5.2  
 43 40 33 <sup>1/45</sup> 20 -0.2 19.5 23 <sup>2/25</sup> 30 40 43

58 61 83 <sup>7/27</sup> 48 53 <sup>(5.0)</sup> 6.2 7 <sup>1/29</sup> 58 4.9  
 43 41 33 <sup>2/41</sup> 20 00 19.5 2/2.5 33 43

52 55 76 <sup>5/26</sup> 52 55 <sup>(5.0)</sup> 64 86 <sup>8/29</sup> 85 4.8  
 43 27 32 <sup>2/40</sup> 20 -0.2 19.5 27 <sup>4/25</sup> 34 43

50 55 76 <sup>5/27</sup> 51 52 <sup>(5.0)</sup> 62 79 <sup>2/24</sup> 82 4.7 4.7  
 43 37 33 <sup>2/35</sup> 20 -0.2 19.5 26 <sup>2/20</sup> 33 41 43

29 71 <sup>3/25</sup> 71 4.7 5.2 <sup>(4.8)</sup> 5/6.2 84 <sup>5/27</sup> 86 4.5 4.5  
 36 30 <sup>2/39</sup> 26 20 -0.4 1/20 27 <sup>1/2.5</sup> 31 40 43

26 24 66 <sup>3/20</sup> 70 4.8 5.0 <sup>(4.3)</sup> 61 <sup>3/25</sup> 64 7.9 <sup>9/21</sup> 85 4.5  
 43 35 31 <sup>1/39</sup> 26 20 -0.5 17 <sup>5/24</sup> 22 25 <sup>1/3.2</sup> 33 42

50 57 81 <sup>1/26</sup> 83 7.2 66 <sup>(5.6)</sup> 6.2 <sup>3/24</sup> 74 9.1 <sup>2/25</sup> 73 6.0 6.0  
 43 35 21 <sup>1/48</sup> 26 21 20 -0.4 <sup>2/24</sup> 26 <sup>2/2.5</sup> 35 41 43

70 71 <sup>3/24</sup> 83 5.1 5.9 <sup>(7.3)</sup> 70 <sup>9/24</sup> 7.7 86 <sup>3/22</sup> 64 6.5  
 43 32 <sup>2/45</sup> 26 19 26 75 <sup>2/27</sup> 24 27 <sup>3/2.5</sup> 39 43

7.7 <sup>9/20</sup> 80 5.9 5.6 <sup>(4.9)</sup> 64 <sup>3/20</sup> 20 24 <sup>6/24</sup> 72 6.9  
 43 <sup>2/42</sup> 25 17 -0.7 16 <sup>4/10</sup> 25 28 <sup>2/24</sup> 33 43

68 <sup>6/20</sup> 69 5.7 5.7 <sup>(4.5)</sup> 5.9 66 <sup>3/27</sup> 6/24 66  
 33 <sup>2/33</sup> 16 11 -0.7 13 15 <sup>2/14</sup> 8/11 33

922.79 ✓

21

18.4 58. 42.4

+50

189 39.

22

193 3.5.

+50

197 3.1.

23

200 2.8.

+50

203 ✓ 2.5.

6.73

926.56 ✓

2.94

919.83

24

206 60.

+50

208 5.8.

25

211 ✓ 5.5.

13. M.

4.85

926.54 ✓

4.85

921.71 ✓

921.69

+50

212 5.3.

26

214 5.1.

+50

216 4.7.

9-30-29

48 4/1.0 0/5.2 5.8 42 4.2 5.2 5/5.1 5/5.1 5.0  
 53 8/7.2 2/7.14 7 7 -0.7 7 2/7.25 3/7.25 53

(42)

39 2/5.9 59 5.2 39 4.1 4.8 4.5 4.7 4.4 1/4.2 5/4.2 4.4  
 33 3/2.0 22 18 16 13 10 -0.6 12 13 2/7.08 3/7.08 33

(39)

35 2/3.5 59 4.4 4.2 4.7 3.7 3.4 9/3.7 3.7  
 33 3/2.0 13 12 -1.7 12 13 20 3/7.08 33

(35)

35 8/3.4 0/3.4 3.6 4.0 3.2 4.2 3.5 5/3.6 6/3.8 3.4  
 33 3/7.08 2/7.08 13 12 -0.7 13 16 2/7.25 3/7.04 33

(31)

33 0/3.3 7/3.4 3.3 3.8 3.4 3.5 3.1 3/4.2 9/3.0 3.0  
 33 3/7.08 2/7.06 14 12 -0.6 12 17 2/7.04 3/7.02 33

(33)

32 2/3.2 7/3.1 2.8 3.5 3/3.5 2.4 2.2 2/2.2 2.3  
 33 3/7.07 2/7.06 12 12 -0.6 12 15 20 3/7.08 33

(32)

64 0/6.4 59 6.1 6.9 6.7 7.0 5.1 0/4.5 4.5  
 33 3/7.04 20 14 11 -0.7 12 16 3/7.15 33

(60)

5.7 2/5.7 5.2 5.3 6.8 6.5 6.8 3.8 0/3.0 3.0  
 33 3/7.01 20 14 12 -0.7 12 16 3/7.22 33

(57)

53 6/5.2 5.2 4.6 4.3 6.6 6.5 6.6 3.0 0/3.8 2.7  
 33 3/7.03 24 20 15 11 -0.8 12 18 3/7.27 33

(53)

SPIN IN 24" OAK 45 LT. 57M. 25+35.

55 1/5.4 4.7 4.8 6.3 6.5 4.0 0/4.2 4.2  
 33 3/7.01 23 14 11 -0.8 12 15 3/7.11 33

(55)

65 0/6.6 6.6 5/6.1 5.8 6.2 6.0 6.7 5.8 1/5.9 5.9  
 33 3/7.15 25 12 11 -0.9 11 12 2/7.08 3/7.08 33

(65)

74 1/7.0 9/7.1 6.2 6.3 6.1 6.5 9/6.6 7/6.6 6.8  
 33 2/7.01 2/7.04 10 12 -1.2 12 2/7.17 2/7.17 33

(74)

926.54 ✓

27

216

49'

+50

2165

49'

28

8.70

929.19 ✓

6.05

217 ✓  
920.49

48'

+50

21.75

74'

29

218

74'

+50

2185

74'

30

219

73'

+50

21.95

72'

31

220

72'

+50

2205

71'

32

221

71'

+50

2215

70'

7-30-27

$\frac{80}{38}$	$\frac{7}{2} \frac{75}{-26}$	$\frac{76}{24}$	$\frac{68}{22}$	$\frac{67}{19}$	$\frac{63}{7.9}$	$\frac{65}{12}$	$\frac{70}{20}$	$\frac{9}{2} \frac{71}{-22}$	$\frac{7}{2} \frac{71}{-22}$	$\frac{7.5}{59}$
-----------------	------------------------------	-----------------	-----------------	-----------------	------------------	-----------------	-----------------	------------------------------	------------------------------	------------------

(4.9)

$\frac{8.5}{38}$	$\frac{3}{2} \frac{75}{-24}$	$\frac{6.5}{23}$	$\frac{62}{14}$	$\frac{64}{12}$	$\frac{63}{7.9}$	$\frac{6.5}{12}$	$\frac{60}{18}$	$\frac{5}{2} \frac{64}{-75}$	$\frac{6}{2} \frac{73}{-24}$	$\frac{7.5}{53}$
------------------	------------------------------	------------------	-----------------	-----------------	------------------	------------------	-----------------	------------------------------	------------------------------	------------------

(4.9)

$\frac{84}{38}$	$\frac{7.8}{27}$	$\frac{5}{2} \frac{65}{-75}$	$\frac{58}{14}$	$\frac{62}{13}$	$\frac{60}{7.2}$	$\frac{63}{12}$	$\frac{5.5}{19}$	$\frac{3}{2} \frac{5.7}{-29}$	$\frac{1}{2} \frac{62}{-74}$	$\frac{6.6}{53}$
-----------------	------------------	------------------------------	-----------------	-----------------	------------------	-----------------	------------------	-------------------------------	------------------------------	------------------

(4.9)

$\frac{100}{85}$	$\frac{7}{2} \frac{100}{-26}$	$\frac{83}{19}$	$\frac{87}{12}$	$\frac{84}{10}$	$\frac{85}{12.4}$	$\frac{85}{12.4}$	$\frac{1}{2} \frac{82}{-28}$	$\frac{7}{2} \frac{84}{-70}$	$\frac{8.5}{53}$
------------------	-------------------------------	-----------------	-----------------	-----------------	-------------------	-------------------	------------------------------	------------------------------	------------------

(7.4)

$\frac{85}{35}$	$\frac{4}{2} \frac{85}{-71}$	$\frac{9}{2} \frac{81}{-77}$	$\frac{79}{18}$	$\frac{83}{12}$	$\frac{81}{-0.7}$	$\frac{85}{12}$	$\frac{76}{13}$	$\frac{71}{19}$	$\frac{74}{24}$	$\frac{5}{2} \frac{82}{-102}$	$\frac{7.2}{59}$
-----------------	------------------------------	------------------------------	-----------------	-----------------	-------------------	-----------------	-----------------	-----------------	-----------------	-------------------------------	------------------

(7.4)

$\frac{82}{35}$	$\frac{0}{2} \frac{65}{-70.8}$	$\frac{60}{28}$	$\frac{56}{16}$	$\frac{85}{11}$	$\frac{81}{-0.8}$	$\frac{81}{13}$	$\frac{50}{19}$	$\frac{0}{2} \frac{60}{-71.3}$	$\frac{61}{35}$
-----------------	--------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	--------------------------------	-----------------

(7.3)

$\frac{49}{35}$	$\frac{0}{2} \frac{4.9}{-72.4}$	$\frac{41}{27}$	$\frac{46}{17}$	$\frac{82}{11}$	$\frac{81}{-0.8}$	$\frac{82}{13}$	$\frac{40}{18}$	$\frac{4.5}{24}$	$\frac{0}{2} \frac{5.1}{-71.2}$	$\frac{5.1}{55}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------	---------------------------------	------------------

(7.3)

$\frac{45}{35}$	$\frac{0}{2} \frac{4.5}{-72.7}$	$\frac{38}{28}$	$\frac{29}{21}$	$\frac{80}{11}$	$\frac{81}{-0.9}$	$\frac{83}{13}$	$\frac{49}{19}$	$\frac{5.3}{26}$	$\frac{0}{2} \frac{5.9}{-71.3}$	$\frac{6.0}{55}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------	---------------------------------	------------------

(7.3)

$\frac{57}{35}$	$\frac{0}{2} \frac{5.7}{-71.0}$	$\frac{53}{24}$	$\frac{55}{14}$	$\frac{80}{11}$	$\frac{80}{-0.8}$	$\frac{79}{12}$	$\frac{63}{15}$	$\frac{6.7}{23}$	$\frac{71}{25}$	$\frac{9}{2} \frac{7.8}{-76}$	$\frac{7.9}{53}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------	-----------------	-------------------------------	------------------

(7.3)

$\frac{62}{35}$	$\frac{0}{2} \frac{6.2}{-70.9}$	$\frac{53}{20}$	$\frac{62}{14}$	$\frac{80}{11}$	$\frac{80}{-0.9}$	$\frac{80}{11}$	$\frac{69}{13}$	$\frac{6}{2} \frac{71}{-70}$	$\frac{74}{22}$	$\frac{0}{2} \frac{82}{-71}$	$\frac{8.5}{53}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	-----------------	------------------------------	------------------

(7.1)

$\frac{57}{35}$	$\frac{0}{2} \frac{5.7}{-71.4}$	$\frac{44}{24}$	$\frac{40}{17}$	$\frac{82}{11}$	$\frac{81}{-1.0}$	$\frac{81}{13}$	$\frac{71}{15}$	$\frac{5}{2} \frac{71}{-70}$	$\frac{7.6}{24}$	$\frac{9}{2} \frac{80}{-79}$	$\frac{8.2}{53}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	------------------------------	------------------	------------------------------	------------------

(7.1)

$\frac{61}{35}$	$\frac{0}{2} \frac{6.1}{-70.9}$	$\frac{53}{24}$	$\frac{46}{14}$	$\frac{58}{19}$	$\frac{81}{10}$	$\frac{81}{-1.1}$	$\frac{81}{12}$	$\frac{76}{14}$	$\frac{6}{2} \frac{75}{-70.5}$	$\frac{7.7}{23}$	$\frac{1}{2} \frac{80}{-70}$	$\frac{8.2}{53}$
-----------------	---------------------------------	-----------------	-----------------	-----------------	-----------------	-------------------	-----------------	-----------------	--------------------------------	------------------	------------------------------	------------------

(7.0)

929.14 ✓

33

22.2

70 ✓

4.73

927.58 ✓

6.54

922.65 ✓

f50

22.25

5.3 ✓

34

22.3

5.3 ✓

f50

22.35

5.2 ✓

35

22.4

5.2 ✓

f50

22.45

5.1 ✓

36

22.5

5.1 ✓

f50

22.55

5.0 ✓

B.M.

2.15

925.98 ✓

3.74

923.84 ✓

923.83

37

22.6

3.4 ✓

f50

22.65

3.3 ✓

38

22.7

3.3 ✓

f50

22.75

3.2 ✓

10-1-29

75 0/74 66 60 22 21 82 78 75 22 1/84 84  
 33 3/-24 25 16 11 7.1 13 15 22 24 3/-74 33

(10)

61 0/61 57 46 43 68 64 66 5/68 69 4/65 67  
 33 3/-28 27 25 19 11 7.1 14 2/-70 24 3/-12 33

(33)

63 7/62 52 60 65 64 66 62 5/60 65 3/66 67  
 33 3/-29 19 13 11 7.1 13 14 2/-07 25 3/-13 33

(33)

53 2/52 49 44 54 64 62 64 60 7/58 62 7/62 63  
 33 3/00 29 21 16 10 7.0 13 14 2/-06 25 3/-10 33

(32)

42 0/41 35 37 63 62 62 53 49 54 3/57 56  
 35 3/11 24 15 11 7.0 13 15 20 25 3/-05 33

(32)

27 0/27 17 33 62 61 60 43 47 2/51 52  
 35 3/22 19 13 9 7.0 13 15 27 3/00 33

(31)

34 0/34 33 28 40 61 61 52 3/51 7/61 61  
 35 3/17 26 17 13 10 7.0 15 15 9/00 8/70 33

(31)

48 5/48 9/57 56 62 61 64 3/64 9/69 71  
 33 3/22 2/07 15 10 7.1 14 2/-17 2/-19 33

(30)

SPR IN 36" OAK 45 LT. 5774 36700

46 4/46 2/47 56 51 46 52 56 7/55 61  
 33 3/12 2/-13 13 11 7.2 14 22 2/-21 33

(33)

66 1/66 65 51 47 49 63 61 2/67 68  
 33 2/-33 14 10 7.4 13 71 24 2/-34 33

(33)

88 0/86 82 53 49 54 82 23 76 1/76 77  
 33 3/53 16 11 7.6 13 78 23 26 2/-43 33

(33)

106 2/106 95 51 49 56 81 7/83 80  
 35 3/-74 18 8 7.7 14 18 2/-51 33

(32)

925.98 ✓

39

22.8

32

+50

22.85

31

40

22.9

31

+50

22.95

30

41

23.0

30

+50

23.05

29 ✓

5.41

726.86 ✓

4.53

921.45 ✓

42

23.1

38

+50

23.15

37

43

23.2

37

+50

23.25

36

44

23.3 ✓

34

10.85

932.30 ✓

1.72

925.14 ✓

921.45

10-1-29

118	0/115	100	51	41	52	9/64	68
35	3/-81	20	9	-15	14	3/32	33

(32)

101	0/100	81	55	40	53	5/51	50
35	3/-69	19	13	-15	15	3/20	33

(31)

72	0/67	68	49	40	50	7/52	1/52	51
33	2/-36	25	7	-15	13	3/21	2/-21	33

(31)

71	0/62	60	48	45	50	1/43	9/47	47
33	3/-32	20	10	-15	14	3/18	2/-17	33

(30)

73	0/67	50	44	49	45	50	3/40	4/42	41
33	2/-37	22	14	-15	14	3/10	3/-12	33	

(30)

81	0/77	20	47	49	40	49	9/46	4/45	44
33	2/-48	26	18	13	-17	14	3/17	3/-16	33

(29)

ON ROCK

101	0/91	54	59	54	60	64	3/23	6.3
33	3/-53	20	14	-16	13	15	3/25	33

(38)

90	0/56	55	55	52	58	64	64	1/55	4/50	5.7
33	3/-19	23	11	-15	13	16	19	3/18	2/-19	33

(37)

66	2/57	7/43	41	53	49	55	1/50	0/52	5.3
33	2/-20	2/06	17	13	-12	14	2/-13	3/7.5	33

(37)

49	4/53	3.7	5.1	4.7	4.8	4.3	0/40	2/36	3.0
33	3/-12	20	14	-1.1	10	13	3/-24	3/10	33

(36)

3.2	4/29	2.2	3.0	4.9	4.0	4.7	19	2/1.5	10
43	3/10.7	2.2	15	12	-1.0	12	17	3/12.1	13

(36)

NAIL IN STUMP LT STA. 44+10

ON ROCK

932.30 ✓

f50

23.35

90 .

45

23.4

89 .

f50

23.45

89 .

46

9.33

932.26 ✓

9.57

922.93 ✓

23.5

88 .

f50

23.55

87 .

47

23.6

87 .

f50

23.65

86 .

48

23.7

86 .

f50

7.08

930.63 ✓

8.71

923.55 ✓

23.75 ✓

85 .

49

23.8

88 .

f50

23.85

68 .

f82

23.9

67 .

10-1-29

69	$\frac{8}{5} \frac{6.6}{2.4}$	67	$\frac{9.9}{1.5}$	79	$\frac{10.0}{1.9}$	50	$\frac{7}{3} \frac{5.2}{1.8}$	5.2
43		22	13	-0.9	10	19		43

(9.0)

56	$\frac{7}{3} \frac{5.2}{1.7}$	45	28	97	99	4.2	$\frac{9}{8} \frac{4}{4.5}$	4.8
43		23	11	-0.8	11	20		43

(8.9)

40	$\frac{5}{9} \frac{4.0}{4.9}$	3.7	29	97	97	4.4	$\frac{7}{3} \frac{5.2}{1.7}$	5.4
43		22	14	11	-0.5	11	20	43

(8.9)

40	$\frac{4}{9} \frac{4.0}{4.8}$	3.8	26	97	97	4.7	$\frac{7}{3} \frac{5.3}{1.5}$	5.6
43		21	10	-0.6	13	20		43

(8.8)

41	$\frac{9}{8} \frac{4.2}{4.5}$	4.1	91	95	96	5.0	$\frac{6}{7} \frac{5.1}{1.6}$	5.3
43		19	11	-0.5	12	17		43

(8.7)

47	$\frac{0}{8} \frac{4.8}{1.7}$	4.9	90	92	94	5.2	$\frac{9}{3} \frac{5.5}{1.2}$	5.8
43		16	11	-0.5	12	18		43

(8.7)

61	$\frac{4}{5} \frac{6.0}{1.3}$	6.6	8.9	90	90	6.8	$\frac{7}{3} \frac{6.9}{1.7}$	6.8
43		14	11	-0.4	12	15		43

(8.6)

7.7	$\frac{8}{3} \frac{8.0}{10.6}$	8.2	92	90	93	8.2	$\frac{6.6}{20} \frac{7}{3} \frac{7.8}{10.8}$	7.7
43		14	11	-0.4	14	15		43

(8.6)

86	$\frac{4}{3} \frac{8.5}{10.6}$	7.2	8.5	92	8.9	7.3	$\frac{8.3}{3} \frac{7.9}{10.6}$	7.9
43		19	12	11	-0.4	14	15	43

(8.5)

70	$\frac{9}{3} \frac{7.0}{10.2}$	6.8	7.2	6.8	70	6.8	5.0	$\frac{7}{3} \frac{5.1}{1.7}$
43		14	12	-0.2	14	15		43

(8.5)

5.7	$\frac{3}{3} \frac{5.7}{11.1}$	5.6	5.4	70	6.8	70	5.2	3.5	$\frac{2}{3} \frac{4.4}{4.4}$	4.8
43		28	19	12	0.0	13	15	29		43

(8.4)

5.5	5.3	6.5	70	6.0	70	40	1.2	1.5	5.4	4.2
43	13	12	11		12	14	20	27	30	43

(8.1)

✓  
930.63

50

23.9

6.7

735

24.0 ✓

6.6

B.M.

5.77

724.86

72484

SEE PAGE 20

10-1-29

5.3	<sup>x</sup> 3/53	5.3	67	65	(67)	68	61	40	<sup>x</sup> 8/4.5	40
43	3/11.4	14	11	70.2	19	27	33	3	7.24	43

61	62	62	(66)	68	56	<sup>x</sup> 5/4.4	43
53	15	70.4	15	24	5	7.23	43

SPK IN 18" OAX. 55 LT 57A. 48185.

NOTE: SEE PAGE 56 FOR X-SEC.  
FROM 117+00 TO 122+00

B.M.	1.13	924.98 ✓		923.85	
122				21.5	2.1 3.5.4
+50				21.5	2.1 3.5.4
123				21.4	2.2 3.6.5
+50				21.4	2.2 3.6.5
124				21.3	2.3 3.7.
+50				21.3	2.3 3.7.5
125				21.3	2.3 3.7.
+50				21.4	2.2 3.6.5
124				21.5	2.1 3.5.4.9
+50				21.65	1.9 3.3.4.5
	4.95	926.95 ✓	2.98	922.00 ✓	
127				21.8	4.0 5.2.6.4
+50				21.95	4.2 5.0.5.8

10-8-29

$\frac{57}{45} \frac{56}{30} \frac{7}{58} \frac{34}{18} \frac{31}{03} \frac{49}{14} \frac{1}{52} \frac{70}{-03} \frac{2}{24} \frac{70}{-25} \frac{40}{35} \frac{39}{45}$

(3.5)

$\frac{55}{45} \frac{57}{28} \frac{1}{54} \frac{56}{-33} \frac{43}{27} \frac{33}{22} \frac{39}{18} \frac{50}{-04} \frac{14}{14} \frac{3}{53} \frac{57}{-04} \frac{72}{24} \frac{3}{74} \frac{79}{29} \frac{52}{-25} \frac{49}{32} \frac{49}{36} \frac{49}{45}$

(3.5)

$\frac{58}{45} \frac{56}{29} \frac{1}{50} \frac{37}{-28} \frac{40}{19} \frac{37}{04} \frac{53}{16} \frac{5}{55} \frac{57}{23} \frac{70}{27} \frac{79}{-25} \frac{55}{33} \frac{54}{38} \frac{54}{45}$

(3.6)

$\frac{46}{41} \frac{55}{37} \frac{57}{33} \frac{53}{28} \frac{5}{47} \frac{44}{-25} \frac{35}{23} \frac{42}{18} \frac{53}{-04} \frac{17}{17} \frac{9}{57} \frac{68}{-07} \frac{68}{26} \frac{2}{73} \frac{75}{-23} \frac{49}{31} \frac{48}{36} \frac{48}{43}$

(3.6)

$\frac{43}{56} \frac{39}{39} \frac{48}{27} \frac{1}{41} \frac{37}{-18} \frac{4}{18} \frac{50}{-04} \frac{16}{16} \frac{9}{53} \frac{66}{-02} \frac{2}{71} \frac{76}{-20} \frac{67}{33} \frac{32}{36} \frac{32}{45}$

(3.7)

$\frac{42}{50} \frac{45}{45} \frac{43}{38} \frac{37}{31} \frac{1}{36} \frac{36}{-13} \frac{37}{14} \frac{37}{-02} \frac{15}{15} \frac{9}{53} \frac{54}{-02} \frac{47}{22} \frac{26}{28} \frac{2}{67} \frac{78}{-12} \frac{61}{33} \frac{60}{34} \frac{60}{44} \frac{60}{45}$

(3.7)

$\frac{41}{38} \frac{34}{36} \frac{46}{31} \frac{1}{45} \frac{37}{-32} \frac{37}{26} \frac{9}{45} \frac{33}{-12} \frac{37}{18} \frac{37}{-02} \frac{42}{12} \frac{1}{54} \frac{74}{-03} \frac{60}{33} \frac{20}{37} \frac{20}{45}$

(3.7)

$\frac{36}{40} \frac{32}{37} \frac{48}{33} \frac{54}{30} \frac{5}{47} \frac{45}{-25} \frac{35}{24} \frac{35}{20} \frac{32}{02} \frac{43}{10} \frac{47}{16} \frac{9}{52} \frac{64}{-02} \frac{64}{26} \frac{2}{70} \frac{71}{-20} \frac{64}{32} \frac{23}{35} \frac{23}{44} \frac{23}{45}$

(3.6)

$\frac{34}{45} \frac{37}{37} \frac{32}{36} \frac{50}{31} \frac{1}{59} \frac{46}{-38} \frac{33}{23} \frac{32}{19} \frac{32}{01} \frac{42}{11} \frac{1}{50} \frac{66}{-01} \frac{69}{27} \frac{75}{-20} \frac{63}{22} \frac{21}{24} \frac{21}{42} \frac{21}{45}$

(3.3)

$\frac{42}{45} \frac{46}{34} \frac{41}{34} \frac{54}{27} \frac{1}{53} \frac{53}{-34} \frac{38}{26} \frac{38}{20} \frac{38}{00} \frac{38}{14} \frac{5}{47} \frac{49}{00} \frac{63}{21} \frac{65}{27} \frac{66}{-18} \frac{60}{32} \frac{39}{35} \frac{39}{40} \frac{39}{45}$

(3.3)

$\frac{63}{45} \frac{67}{35} \frac{62}{33} \frac{3}{80} \frac{76}{-40} \frac{55}{25} \frac{51}{18} \frac{51}{12} \frac{51}{10} \frac{58}{14} \frac{6}{62} \frac{70}{102} \frac{71}{25} \frac{67}{27} \frac{64}{30} \frac{69}{-00} \frac{60}{34} \frac{60}{37} \frac{60}{41}$

(3.2)

$\frac{61}{-19} \frac{60}{26} \frac{63}{24} \frac{57}{23} \frac{5}{57} \frac{54}{-15} \frac{57}{18} \frac{58}{16} \frac{51}{14} \frac{57}{-01} \frac{54}{12} \frac{1}{52} \frac{58}{13} \frac{5}{62} \frac{58}{706} \frac{67}{23} \frac{64}{-01} \frac{69}{33} \frac{60}{33}$

(3.0)

926.95 ✓

128

22.1 4.5 4.9.3

+50

22.25 4.7.

129

4.78

927.28 ✓

4.45

22.4 ✓ 4.6.

922.50

+50

22.55 4.7.

130

22.7 4.6.

+50

22.85 4.4.

131

23.0 4.3.

+50

23.15 4.1.

132

23.3 4.0.

+50

23.45 3.8.

133

23.6 ✓ 3.7.

B.M.

1.39

925.89 925.86

B.M.

2.54

926.41 ✓

923.85 ✓

5.77

928.38 ✓

3.80

922.61 ✓

10-8-29

59	$\frac{3}{5} \frac{58}{73}$	58	57	$\frac{1}{2} \frac{54}{-09}$	55	49	55	52	$\frac{5}{9} \frac{45}{108}$	49	$\frac{30}{5} \frac{43}{71.0}$	44
50	$\frac{3}{5} \frac{73}{73}$	29	24	$\frac{1}{2} \frac{-09}{-09}$	19	0.0	12	13	$\frac{1}{108}$	24	$\frac{30}{5} \frac{71.0}{71.0}$	35

(4.9)

5.9	$\frac{6}{9} \frac{58}{71}$	58	62	52	$\frac{5}{2} \frac{57}{-10}$	55	46	51	42	44	$\frac{0}{3} \frac{41}{10.6}$	41
59	$\frac{6}{9} \frac{71}{71}$	26	26	25	$\frac{1}{2} \frac{-10}{-10}$	14	10.1	12	13	20	$\frac{3}{5} \frac{10.6}{10.6}$	35

(4.7)

2.0	$\frac{4}{5} \frac{58}{12}$	59	62	57	$\frac{9}{2} \frac{58}{72}$	58	53	46	5.0	48	45	$\frac{5}{9} \frac{46}{0.0}$	51	$\frac{2}{2} \frac{47}{3.01}$	48
19	$\frac{4}{5} \frac{12}{12}$	28	25	23	$\frac{1}{2} \frac{72}{72}$	17	14	0.0	11	13	16	$\frac{1}{9} \frac{0.0}{0.0}$	26	$\frac{3}{2} \frac{0.1}{0.1}$	35

(4.10)

62	$\frac{3}{5} \frac{60}{-1.3}$	41	64	57	$\frac{5}{2} \frac{57}{-10}$	57	42	52	49	$\frac{9}{1} \frac{49}{-0.2}$	51	$\frac{6}{3} \frac{51}{-0.4}$	51
33	$\frac{3}{5} \frac{60}{-1.3}$	29	25	23	$\frac{1}{2} \frac{-10}{-10}$	13	-0.1	11	15	$\frac{1}{9} \frac{-0.2}{-0.2}$	22	$\frac{1}{3} \frac{-0.4}{-0.4}$	33

(4.7)

5.5	$\frac{9}{3} \frac{55}{-0.7}$	5.6	$\frac{7}{2} \frac{52}{-0.6}$	5.4	5.6	46	5.3	49	48	45	41	$\frac{9}{3} \frac{39}{10.7}$	39
33	$\frac{9}{3} \frac{-0.7}{-0.7}$	23	$\frac{1}{2} \frac{-0.6}{-0.6}$	15	14	0.0	12	13	18	20	22	$\frac{3}{5} \frac{10.7}{10.7}$	35

(4.6)

54	$\frac{1}{2} \frac{54}{-1.0}$	58	51	$\frac{1}{2} \frac{54}{-0.8}$	5.5	47	6.2	50	$\frac{1}{9} \frac{45}{-2.1}$	37	$\frac{0}{3} \frac{34}{71.0}$	33
32	$\frac{1}{2} \frac{-1.0}{-1.0}$	23	22	$\frac{1}{2} \frac{-0.8}{-0.8}$	14	-0.3	12	13	$\frac{1}{9} \frac{-2.1}{-2.1}$	24	$\frac{0}{3} \frac{71.0}{71.0}$	33

(4.4)

59	$\frac{3}{2} \frac{57}{-1.6}$	59	64	$\frac{4}{2} \frac{60}{77}$	57	56	56	48	54	52	$\frac{6}{2} \frac{50}{-0.7}$	46	44	$\frac{2}{3} \frac{43}{0.0}$	42
33	$\frac{3}{2} \frac{-1.6}{-1.6}$	25	24	$\frac{1}{2} \frac{77}{77}$	21	20	13	-0.5	12	13	$\frac{1}{2} \frac{-0.7}{-0.7}$	23	27	$\frac{2}{3} \frac{0.0}{0.0}$	35

(4.3)

6.6	$\frac{4}{2} \frac{67}{-2.6}$	6.6	62	5.5	48	5.5	56	52	$\frac{9}{2} \frac{58}{-1.7}$	$\frac{9}{3} \frac{56}{-1.5}$	55
33	$\frac{4}{2} \frac{-2.6}{-2.6}$	21	15	12	-0.7	13	17	19	$\frac{1}{2} \frac{-1.7}{-1.7}$	$\frac{1}{3} \frac{-1.5}{-1.5}$	33

(4.1)

2	$\frac{4}{2} \frac{59}{-1.9}$	60	$\frac{2}{2} \frac{56}{-1.6}$	58	62	57	48	5.5	5.9	6.5	$\frac{5}{2} \frac{60}{-2.0}$	64
1	$\frac{4}{2} \frac{-1.9}{-1.9}$	20	$\frac{1}{2} \frac{-1.6}{-1.6}$	21	18	13	-0.8	13	17	21	$\frac{1}{2} \frac{-2.0}{-2.0}$	35

(4.0)

5	$\frac{8}{2} \frac{54}{7.6}$	53	$\frac{1}{2} \frac{49}{-1.1}$	60	57	5.5	52	46	51	54	6.3	$\frac{1}{5} \frac{60}{-2.8}$	67	62
1	$\frac{8}{2} \frac{7.6}{7.6}$	18	$\frac{1}{2} \frac{-1.1}{-1.1}$	18	17	15	12	-0.8	12	14	19	$\frac{1}{5} \frac{-2.8}{-2.8}$	28	33

(3.6)

5.6	$\frac{6}{2} \frac{55}{-1.8}$	$\frac{1}{2} \frac{50}{-1.3}$	55	51	54	5.1	43	51	54	5.5	62	$\frac{9}{2} \frac{62}{-2.7}$	62
33	$\frac{6}{2} \frac{-1.8}{-1.8}$	$\frac{1}{2} \frac{-1.3}{-1.3}$	18	17	14	13	-0.6	12	13	17	20	$\frac{1}{2} \frac{-2.7}{-2.7}$	33

(3.7)

928.38 ✓

133+50

23.75

46 ✓

134

23.7

45 ✓

+50

24.05

43 ✓

135

24.2

44 ✓

+50

24.35

40 ✓

136

24.5

39 ✓

+50

24.65

37 ✓

137

24.8 ✓

36 ✓

5.19

930.43 ✓

3.14

925.24

+50

24.95

55 ✓

138

25.1

53 ✓

+50

25.25

52 ✓

139

25.4

50 ✓

10-14-29

$$\begin{array}{r} 62 \\ 33 \end{array} \begin{array}{r} 9/27 \\ 2/2.1 \end{array} \begin{array}{r} 9/29 \\ 2/7.7 \end{array} \begin{array}{r} 44 \\ 21 \end{array} \begin{array}{r} 57 \\ 13 \end{array} \begin{array}{r} 52 \\ 0.6 \end{array} \begin{array}{r} 52 \\ 12 \end{array} \begin{array}{r} 69 \\ 18 \end{array} \begin{array}{r} 1/24 \\ 2/28 \end{array} \begin{array}{r} 70 \\ 38 \end{array}$$

(4.6)

$$\begin{array}{r} 60 \\ 33 \end{array} \begin{array}{r} 9/28 \\ 2/7.9 \end{array} \begin{array}{r} 57 \\ 26 \end{array} \begin{array}{r} 52 \\ 23 \end{array} \begin{array}{r} 9/24 \\ 2/0.9 \end{array} \begin{array}{r} 61 \\ 19 \end{array} \begin{array}{r} 56 \\ 13 \end{array} \begin{array}{r} 49 \\ 0.5 \end{array} \begin{array}{r} 57 \\ 12 \end{array} \begin{array}{r} 64 \\ 17 \end{array} \begin{array}{r} 1/65 \\ 2/20 \end{array} \begin{array}{r} 7/62 \\ 2/17 \end{array} \begin{array}{r} 60 \\ 38 \end{array}$$

(4.5)

$$\begin{array}{r} 45 \\ 33 \end{array} \begin{array}{r} 9/44 \\ 2/2.1 \end{array} \begin{array}{r} 57 \\ 23 \end{array} \begin{array}{r} 9/44 \\ 2/0.1 \end{array} \begin{array}{r} 50 \\ 16 \end{array} \begin{array}{r} 52 \\ 13 \end{array} \begin{array}{r} 46 \\ 0.8 \end{array} \begin{array}{r} 52 \\ 12 \end{array} \begin{array}{r} 5/57 \\ 2/14 \end{array} \begin{array}{r} 6/51 \\ 2/0.8 \end{array} \begin{array}{r} 49 \\ 33 \end{array}$$

(4.3)

$$\begin{array}{r} 37 \\ 35 \end{array} \begin{array}{r} 9/35 \\ 2/7.7 \end{array} \begin{array}{r} 31 \\ 33 \end{array} \begin{array}{r} 39 \\ 20 \end{array} \begin{array}{r} 45 \\ 17 \end{array} \begin{array}{r} 47 \\ 14 \end{array} \begin{array}{r} 42 \\ 0.0 \end{array} \begin{array}{r} 49 \\ 12 \end{array} \begin{array}{r} 52 \\ 15 \end{array} \begin{array}{r} 47 \\ 17 \end{array} \begin{array}{r} 5/52 \\ 2/7.0 \end{array} \begin{array}{r} 3/48 \\ 2/0.6 \end{array} \begin{array}{r} 49 \\ 38 \end{array}$$

(4.2)

$$\begin{array}{r} 39 \\ 35 \end{array} \begin{array}{r} 9/36 \\ 2/7.4 \end{array} \begin{array}{r} 35 \\ 24 \end{array} \begin{array}{r} 9/41 \\ 2/0.1 \end{array} \begin{array}{r} 46 \\ 16 \end{array} \begin{array}{r} 39 \\ 10.1 \end{array} \begin{array}{r} 44 \\ 11 \end{array} \begin{array}{r} 1/5.5 \\ 2/1.8 \end{array} \begin{array}{r} 56 \\ 24 \end{array} \begin{array}{r} 3/53 \\ 2/7.3 \end{array} \begin{array}{r} 5.4 \\ 33 \end{array}$$

(4.0)

$$\begin{array}{r} 58 \\ 33 \end{array} \begin{array}{r} 9/38 \\ 2/7.0 \end{array} \begin{array}{r} 39 \\ 26 \end{array} \begin{array}{r} 3/39 \\ 2/0.0 \end{array} \begin{array}{r} 41 \\ 14 \end{array} \begin{array}{r} 45 \\ 13 \end{array} \begin{array}{r} 37 \\ 10.2 \end{array} \begin{array}{r} 42 \\ 11 \end{array} \begin{array}{r} 7/4.5 \\ 2/0.6 \end{array} \begin{array}{r} 47 \\ 25 \end{array} \begin{array}{r} 3/45 \\ 2/1.6 \end{array} \begin{array}{r} 46 \\ 33 \end{array}$$

(3.9)

$$\begin{array}{r} 39 \\ 33 \end{array} \begin{array}{r} 1/3.8 \\ 2/0.1 \end{array} \begin{array}{r} 37 \\ 15 \end{array} \begin{array}{r} 40 \\ 12 \end{array} \begin{array}{r} 3.5 \\ 10.2 \end{array} \begin{array}{r} 3.9 \\ 11 \end{array} \begin{array}{r} 32 \\ 15 \end{array} \begin{array}{r} 34 \\ 20 \end{array} \begin{array}{r} 6/33 \\ 2/7.4 \end{array} \begin{array}{r} 3.3 \\ 33 \end{array}$$

(3.7)

$$\begin{array}{r} 35 \\ 33 \end{array} \begin{array}{r} 5/34 \\ 2/7.2 \end{array} \begin{array}{r} 36 \\ 14 \end{array} \begin{array}{r} 39 \\ 12 \end{array} \begin{array}{r} 3.4 \\ 10.2 \end{array} \begin{array}{r} 3.7 \\ 11 \end{array} \begin{array}{r} 3.4 \\ 12 \end{array} \begin{array}{r} 28 \\ 17 \end{array} \begin{array}{r} 2/2.6 \\ 2/1.0 \end{array} \begin{array}{r} 2.6 \\ 35 \end{array}$$

(3.6)

$$\begin{array}{r} 44 \\ 35 \end{array} \begin{array}{r} 9/44 \\ 2/7.1 \end{array} \begin{array}{r} 45 \\ 22 \end{array} \begin{array}{r} 52 \\ 15 \end{array} \begin{array}{r} 57 \\ 14 \end{array} \begin{array}{r} 51 \\ 10.4 \end{array} \begin{array}{r} 54 \\ 11 \end{array} \begin{array}{r} 51 \\ 12 \end{array} \begin{array}{r} 46 \\ 16 \end{array} \begin{array}{r} 9/48 \\ 2/7.7 \end{array} \begin{array}{r} 48 \\ 35 \end{array}$$

(3.5)

$$\begin{array}{r} 32 \\ 35 \end{array} \begin{array}{r} 6/35 \\ 2/1.5 \end{array} \begin{array}{r} 38 \\ 28 \end{array} \begin{array}{r} 48 \\ 16 \end{array} \begin{array}{r} 55 \\ 13 \end{array} \begin{array}{r} 49 \\ 10.4 \end{array} \begin{array}{r} 54 \\ 11 \end{array} \begin{array}{r} 49 \\ 14 \end{array} \begin{array}{r} 41 \\ 19 \end{array} \begin{array}{r} 6/44 \\ 2/7.9 \end{array} \begin{array}{r} 4.5 \\ 35 \end{array}$$

(3.3)

$$\begin{array}{r} 31 \\ 35 \end{array} \begin{array}{r} 9/31 \\ 2/7.1 \end{array} \begin{array}{r} 32 \\ 29 \end{array} \begin{array}{r} 44 \\ 19 \end{array} \begin{array}{r} 51 \\ 14 \end{array} \begin{array}{r} 55 \\ 13 \end{array} \begin{array}{r} 47 \\ 10.5 \end{array} \begin{array}{r} 52 \\ 12 \end{array} \begin{array}{r} 49 \\ 14 \end{array} \begin{array}{r} 46 \\ 20 \end{array} \begin{array}{r} 9/45 \\ 2/7.7 \end{array} \begin{array}{r} 46 \\ 38 \end{array}$$

(3.2)

$$\begin{array}{r} 36 \\ 35 \end{array} \begin{array}{r} 9/38 \\ 2/7.2 \end{array} \begin{array}{r} 39 \\ 24 \end{array} \begin{array}{r} 46 \\ 19 \end{array} \begin{array}{r} 52 \\ 14 \end{array} \begin{array}{r} 54 \\ 10 \end{array} \begin{array}{r} 47 \\ 10.3 \end{array} \begin{array}{r} 53 \\ 12 \end{array} \begin{array}{r} 56 \\ 18 \end{array} \begin{array}{r} 6/53 \\ 2/7.3 \end{array} \begin{array}{r} 6/54 \\ 2/7.2 \end{array} \begin{array}{r} 5.5 \\ 33 \end{array}$$

(3.0)

730.43 ✓

f50

25.55

4.9

140

25.7

4.9

f50

25.85

4.6

141

26.0

4.4

f50

26.15

4.3

142

26.3 ✓

4.1

3.90

730.71 ✓

3.62

726.81 ✓

f50

26.45

4.3

143

26.6

4.1

f50

26.7

4.0

144

26.8

3.9

f50

27.0

3.7

145

27.0 ✓

3.7

B.M.

3.41

730.73 ✓

3.41

727.30 ✓

727.32

10-14-29

$\frac{4.5}{3.5}$	$\frac{8}{3}$	$\frac{4.5}{7.04}$	$\frac{1}{1.9}$	$\frac{5.1}{-0.2}$	$\frac{5.1}{12}$	$\frac{4.7}{7.02}$	$\frac{4.9}{12}$	$\frac{5.2}{18}$	$\frac{5.7}{18}$	$\frac{1}{2}$	$\frac{1.5}{-0.8}$	$\frac{3}{3}$	$\frac{6.1}{-1.8}$	$\frac{6.1}{3.8}$
-------------------	---------------	--------------------	-----------------	--------------------	------------------	--------------------	------------------	------------------	------------------	---------------	--------------------	---------------	--------------------	-------------------

(4.9)

$\frac{5.4}{3.8}$	$\frac{3}{8}$	$\frac{1.5}{-0.6}$	$\frac{1}{2}$	$\frac{1.5}{-0.6}$	$\frac{5.0}{12}$	$\frac{5.3}{11}$	$\frac{4.2}{7.01}$	$\frac{4.3}{13}$	$\frac{9.5}{-1.1}$	$\frac{1}{3}$	$\frac{1.5}{-1.1}$	$\frac{5.8}{7.1}$	$\frac{5.8}{3.8}$
-------------------	---------------	--------------------	---------------	--------------------	------------------	------------------	--------------------	------------------	--------------------	---------------	--------------------	-------------------	-------------------

(4.1)

$\frac{5.4}{3.8}$	$\frac{2}{3}$	$\frac{1.5}{-0.7}$	$\frac{1}{2}$	$\frac{1.5}{-0.8}$	$\frac{4.9}{14}$	$\frac{5.3}{13}$	$\frac{4.4}{7.02}$	$\frac{5.4}{14}$	$\frac{5.2}{19}$	$\frac{1}{2}$	$\frac{1.5}{-0.6}$	$\frac{4.7}{27}$	$\frac{2}{3}$	$\frac{4.6}{0.0}$	$\frac{4.6}{3.8}$
-------------------	---------------	--------------------	---------------	--------------------	------------------	------------------	--------------------	------------------	------------------	---------------	--------------------	------------------	---------------	-------------------	-------------------

(4.6)

$\frac{4.2}{3.8}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{1.5}{-0.2}$	$\frac{4.7}{-0.3}$	$\frac{4.4}{16}$	$\frac{4.9}{14}$	$\frac{4.1}{7.03}$	$\frac{4.1}{12}$	$\frac{1.8}{17}$	$\frac{1}{2}$	$\frac{1.5}{-0.6}$	$\frac{4.3}{25}$	$\frac{8}{3}$	$\frac{4.0}{-0.4}$	$\frac{4.2}{3.5}$
-------------------	---------------	---------------	--------------------	--------------------	------------------	------------------	--------------------	------------------	------------------	---------------	--------------------	------------------	---------------	--------------------	-------------------

(4.4)

$\frac{3.5}{3.5}$	$\frac{8}{3}$	$\frac{1}{2}$	$\frac{1.5}{-0.4}$	$\frac{3.9}{15}$	$\frac{4.6}{12}$	$\frac{4.0}{7.03}$	$\frac{4.7}{12}$	$\frac{5.2}{19}$	$\frac{1}{2}$	$\frac{1.5}{-0.5}$	$\frac{4.2}{22}$	$\frac{8}{3}$	$\frac{4.0}{-0.3}$	$\frac{4.9}{3.3}$
-------------------	---------------	---------------	--------------------	------------------	------------------	--------------------	------------------	------------------	---------------	--------------------	------------------	---------------	--------------------	-------------------

(4.3)

$\frac{3.5}{3.5}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{1.5}{-0.6}$	$\frac{4.0}{23}$	$\frac{1}{2}$	$\frac{1.4}{-0.3}$	$\frac{4.6}{16}$	$\frac{4.5}{12}$	$\frac{4.1}{0.0}$	$\frac{4.1}{13}$	$\frac{5.2}{19}$	$\frac{1}{2}$	$\frac{1.5}{-1.0}$	$\frac{3}{3}$	$\frac{5.4}{-1.3}$	$\frac{5.4}{3.8}$
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(4.1)

$\frac{4.6}{3.8}$	$\frac{6}{3}$	$\frac{1}{2}$	$\frac{1.4}{-0.3}$	$\frac{1}{1.7}$	$\frac{1.4}{-0.1}$	$\frac{4.7}{18}$	$\frac{5.0}{12}$	$\frac{4.4}{0.1}$	$\frac{5.1}{13}$	$\frac{5.8}{19}$	$\frac{1}{2}$	$\frac{1.5}{-1.5}$	$\frac{1}{3}$	$\frac{1.5}{-1.4}$	$\frac{5.6}{3.8}$
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(4.7)

$\frac{4.4}{3.8}$	$\frac{8}{3}$	$\frac{1}{2}$	$\frac{1.4}{-0.3}$	$\frac{1}{2}$	$\frac{1.4}{-0.6}$	$\frac{4.5}{14}$	$\frac{5.1}{13}$	$\frac{4.3}{0.1}$	$\frac{5.0}{13}$	$\frac{4.9}{14}$	$\frac{5.3}{19}$	$\frac{1}{2}$	$\frac{1.5}{-1.0}$	$\frac{1}{3}$	$\frac{1.5}{-1.2}$	$\frac{5.3}{3.8}$
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(4.1)

$\frac{4.7}{3.8}$	$\frac{1}{3}$	$\frac{1}{2}$	$\frac{1.4}{-0.7}$	$\frac{4.7}{20}$	$\frac{4.8}{17}$	$\frac{4.6}{14}$	$\frac{5.2}{0.3}$	$\frac{4.3}{14}$	$\frac{5.3}{16}$	$\frac{5.0}{16}$	$\frac{1}{2}$	$\frac{1.5}{-1.3}$	$\frac{1}{3}$	$\frac{1.5}{-1.0}$	$\frac{5.1}{3.8}$
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(4.8)

$\frac{5.3}{3.8}$	$\frac{8}{3}$	$\frac{1}{2}$	$\frac{1.5}{-1.4}$	$\frac{3}{6}$	$\frac{1.5}{-1.4}$	$\frac{5.0}{17}$	$\frac{5.5}{16}$	$\frac{4.4}{-0.5}$	$\frac{5.4}{14}$	$\frac{5.8}{16}$	$\frac{1}{2}$	$\frac{1.5}{-1.5}$	$\frac{1}{2}$	$\frac{1.5}{-1.6}$	$\frac{5.6}{3.8}$
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(4.9)

$\frac{5.7}{3.8}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1.5}{-2.1}$	$\frac{1}{2}$	$\frac{1.5}{-2.0}$	$\frac{5.2}{14}$	$\frac{5.6}{15}$	$\frac{4.6}{-0.7}$	$\frac{5.2}{13}$	$\frac{6.0}{19}$	$\frac{1}{2}$	$\frac{1.5}{-2.3}$	$\frac{1}{2}$	$\frac{1.5}{-2.4}$	$\frac{6.1}{3.8}$
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(3.1)

$\frac{5.5}{3.8}$	$\frac{3}{2}$	$\frac{1}{2}$	$\frac{1.5}{-1.8}$	$\frac{1}{2}$	$\frac{1.5}{-1.9}$	$\frac{5.2}{17}$	$\frac{5.5}{15}$	$\frac{4.4}{0.7}$	$\frac{5.4}{13}$	$\frac{5.9}{18}$	$\frac{1}{2}$	$\frac{1.5}{-2.6}$	$\frac{6.4}{3.8}$
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(3.1)

SPI IN 12" DIA 60 LT. STA 145+05.

930.73 ✓

750

2705

3.7

146

27.1 ✓

3.6

T.P.

4.36

931.40 ✓

3.67

727.04 ✓

750

27.15

4.3

147

27.2

4.2

750

27.25

4.2

148

27.3

4.1

750

27.4

4.0

149

27.4

4.0

750

27.45 ✓

4.0

6.07

933.39 ✓

4.08

727.32 ✓

150

27.5

5.9

750

27.55

5.8

151

27.6

5.8

10-14-29

(31)

52	1/51	2/54	47	53	49	44	51	55	1/60	2/58	57
33	3/74	2/77	16	15	12	07	11	15	2/23	2/21	33

(36)

50	2/49	3/45	45	53	49	42	49	54	3/56	4/55	55
33	3/73	2/77	17	15	12	06	11	18	2/20	2/19	33

(43)

57	5/61	2/61	57	54	47	54	60	2/56	0/58	58
33	2/78	2/78	20	12	04	13	18	2/19	3/15	33

(42)

53	1/52	2/52	54	51	49	48	53	3/52	2/49	47
33	5/70	2/70	15	12	02	10	15	2/10	3/07	33

(42)

43	1/44	1/45	45	54	50	42	47	52	1/50	3/48	47
33	3/02	2/03	18	16	13	00	10	13	2/08	3/06	33

(41)

36	2/36	37	52	49	44	51	47	7/52	3/47	47
33	5/03	17	15	12	03	12	14	2/11	3/06	33

(40)

37	5/38	5/45	45	50	45	52	50	56	2/53	0/52	48
33	3/02	2/05	16	12	05	12	14	19	2/13	3/08	33

(40)

43	8/43	1/46	47	51	49	50	55	3/54	2/52	51
33	3/03	2/06	16	13	09	11	13	2/19	3/12	33

(40)

52	4/52	53	3/44	47	53	50	40	45	50	46	2/47	3/46	42
33	3/12	26	2/04	17	16	13	01	10	13	14	2/07	3/06	33

(39)

74	0/74	5/67	73	67	59	66	66	3/63	2/61	61
33	3/13	2/10	15	12	00	11	12	2/04	3/02	33

(34)

78	4/77	2/75	63	59	64	67	61	2/60	3/56	56
33	2/19	2/17	11	11	10	13	15	2/22	3/02	33

(34)

88	3/82	79	68	67	59	63	66	58	3/58	2/57	57
33	2/34	23	17	13	01	9	12	15	2/00	3/01	33

733.39 ✓

750

27.4

6.0

152

27.2

6.2

750

26.8

6.4

153

26.3

7.1

750

25.7

7.7

154

25.0

8.4

750

24.1

9.3

155

23.1

10.3

750

22.1 ✓

11.5

3.64

724.40

12.63

720.76

156

20.9

3.5

750

19.8

4.6

157

18.6

5.8

10-14-29

(60)

21	1/81	78	5/70	68	73	67	58	65	60	51	0/53	52
3	21	25	2/10	15	16	14	102	12	14	18	3/107	35

(62)

75	4/75	0/65	65	66	57	64	58	46	0/54	54
33	3/71	2/53	18	14	105	13	14	19	3/78	43

(66)

73	5/71	71	63	67	57	65	55	46	4/53	50
33	3/65	21	19	17	109	12	14	23	3/118	43

(71)

61	0/61	56	72	69	69	44	2/44	44
35	3/110	20	16	107	12	19	5/121	43

(77)

53	2/51	49	21	75	20	39	3/34	42
43	3/126	21	13	102	11	24	3/143	43

(84)

54	2/53	49	27	25	27	47	9/46	46
43	3/131	21	14	101	12	26	3/138	43

(93)

72	3/72	67	101	95	99	51	3/52	50
43	3/121	23	15	102	13	26	3/141	43

(103)

23	2/22	78	114	107	111	61	9/65	64
73	3/121	21	14	114	13	27	3/138	43

(113)

27	2/26	25	113	122	126	119	123	50	4/85	26
43	3/127	33	19	16	12	-06	13	24	3/128	35

(33)

21	2/20	20	30	47	39	44	15	20	0/23	23
35	3/115	29	22	15	-04	12	23	27	3/112	43

(110)

56	9/55	7/53	50	57	50	57	54	9/48	4/49	50
34	3/109	3/107	18	16	-04	12	15	11/102	3/103	43

(58)

74	9/80	9/75	67	62	70	75	5/68	5/76	77
32	2/122	2/117	12	104	12	18	5/110	9/118	33

72440 ✓

f50

17.5 ✓

69

2.34

918.87 ✓

7.87

916.53

158

16.3 ✓

26

B.M.

2.84

918.87 ✓

2.84

916.03

716.03

f50

15.2

37

159

14.1

48

f50

13.2

57

160

12.4 ✓

65

T.P.

7.19

915.64 ✓

10.44

908.45

f50

11.8

38

161

11.3

43

f50

11.0

46  
17

162

10.7

49

f50

10.45

52

163

10.2

54

10-14-29

(61)

100	91	88	88	80	74	71	5/94	77
33	2/21	5/19	17	12	-0.5	12	5/25	33

(62)

59	1/47	46	3.6	29	34	5/41	44
33	5/23	16	12	-0.3	12	5/13	33

PK IN 12" OAK 60' LT. 574. 157+30

(63)

74	1/26	81	49	43	50	64	7/73	75
33	2/37	20	11	-0.6	12	18	5/36	33

(64)

89	5/20	94	99	94	62	57	62	94	101	7/79	100
33	5/45	25	23	19	11	-0.9	12	20	24	2/51	33

(65)

90	2/25	100	98	73	67	72	10.5	11.1	7/115	114
33	2/36	22	19	11	-1.0	12	20	26	5/56	33

(66)

74	0/75	37	84	85	76	72	48	89	108	11.5	5/117	117
33	5/18	2/21	20	13	10	-0.6	13	17	20	25	5/52	33

(67)

VAR. IN PP AT 574. 160+40

2	2/53	34	1/49	52	55	53	47	43	50	63	73	9/74	80
3	105	26	2/71	21	16	15	11	-0.3	13	18	25	2/36	33

(68)

30	0/25	30	40	50	50	44	50	66	6/64	69
35	5/18	23	19	13	11	-0.1	13	17	6/21	33

(69)

32	0/59	42	58	53	47	52	1/57	5/59	61
35	5/17	19	13	10	-0.1	12	2/11	5/13	33

(70)

3.5	0/55	42	5/49	50	58	55	50	54	7/57	0/57	58
35	5/14	24	1/20	17	12	11	-0.1	12	2/08	5/08	33

(71)

2	0/40	45	5/52	54	60	60	53	54	5/52	2/52	52
3	7/12	25	1/00	17	14	12	-0.1	12	9/00	5/00	33

(72)

45	0/44	47	65	64	58	61	63	53	48	5/42	42
33	5/10	18	14	10	-0.1	12	15	20	39	5/12	33

915.64 ✓

+50

09.95

5.7

164

09.7

5.9

+50

09.45

6.4

165

5.02

911.54 ✓

7.12

09.2 ✓

6.4

208.52

+50

08.95

2.6

166

08.7

2.8

+50

08.45

3.1

167

08.2

3.3

+50

07.95

3.6

168

07.7

3.8

+50

07.4

3.9

169

07.5

4.0



911.54 ✓

+50

07.6

39

170

07.7 ✓

38

B.M.

4.49

912.73 ✓

3.28

908.26 ✓

908.24

+50

07.8

47

171

08.0

47

+50

08.2

45

172

08.4

43

+50

08.6

41

173

08.8 ✓

39

5.67

914.27 ✓

4.13

908.60

+50

09.0

53

174

09.2

51

+50

09.4

49

175

09.6 ✓

47

2.91

911.34

10-17-29

(39)

59	69	7/7.7	82	68	5.9	5.3	4.5	5.2	9.1	3.98	98
38	52	2/5.8	41	78	14	12	-0.6	12	20	2/5.9	33

(38)

5.0	5.5	9/5.9	5.0	6.0	5.0	4.5	4.9	6.7	5/6.8	7.1
33	32	2/2.1	2/2.0	2.0	11	-0.5	13	21	2/3.0	33

PK IN 12" CAR. RT STA 170+30

(39)

0/4.2	9.5	6.4	5/6.6	6.4	6.0	5.4	5.9	8.3	1/8.7	8.0	7.1
3/10.7	3.1	2.6	2/7.5	13	11	-0.5	13	22	2/3.8	3.0	3.3

(37)

2.1	0/2.6	2.8	9/5.8	6.0	6.2	5.9	5.3	5.9	7.3	9/7.4	7.5	5.9
5	3/12.1	3.0	2/7.1	2.0	14	11	-0.6	14	21	2/2.7	2.7	3.3

(35)

2.1	0/2.4	2.8	9/5.7	6.1	5.7	5.2	5.5	6.5	1/7.5	6.9	4.5
3.5	3/12.1	3.1	2/1.2	1.7	10	-0.7	11	18	2/2.8	2.7	3.3

(33)

5.3	4/5.5	5/5.0	5.0	5.4	5.3	4.8	5.4	6.5	1/7.1	6.9	5.6
3.3	3/1.2	2/0.7	1.9	1.6	10	-0.5	13	19	2/2.8	2.8	3.3

(31)

3.5	3/4.0	4.5	5/5.1	5.2	4.6	5.1	6.0	1/6.4	6.6	6.7
3.3	3/1.1	2.7	2/1.0	1.1	-0.5	14	17	2/2.3	2.9	3.3

(29)

0/1.8	2.3	2.9	5.8	9/5.1	5.7	4.9	4.4	5.1	5/6.4	6.9
3/7.1	3.0	2.9	2.4	2/7.2	1.7	10	-0.5	14	2/2.5	3.3

(27)

3.0	0/3.3	5.0	3/6.7	7.2	6.6	6.1	5.7	6.6	7.5	7/8.4	9.2	9.2
3.5	3/1.8	2.6	2/7.4	1.7	12	10	-0.4	14	23	2/3.1	3.0	3.3

(25)

2.5	0/2.7	4.1	4.8	1/6.4	6.9	6.1	5.6	6.3	7.4	9.6	6/10.1	10.0
3.3	3/12.4	2.7	2.6	2/1.3	1.6	10	-0.5	15	23	2.7	2/5.0	3.3

(23)

2.1	0/2.4	2.8	7/5.5	4.4	5.8	5.3	6.0	6.6	7.0	10.3	9/11.1	11.2
3.3	3/12.5	3.0	2/2.6	1.4	10	-0.4	15	17	20	2.6	3/6.2	3.3

(21)

1.9	0/3.2	4.8	5/5.7	6.6	5.6	5.1	5.8	6.9	11.5	0/12.5	12.3
3.5	3/11.5	2.8	2/1.0	1.6	10	-0.4	14	19	2.9	3/7.5	3.3

NAIL IN TREE RT STA 177+45.

B.M.	5.26	913.50		908.24	
	4.71	915.39	2.82	910.68	
175750				09.8	5.6
176				10.0	5.4
750				10.2	5.2
177				10.4	5.0
755				10.6	4.8
	11.19	923.49	3.09	912.50	
178				10.8	12.7
750				11.0	12.5
179				11.2	12.3
750				11.4	12.1
180				11.5	12.0
750				11.4	11.9
	2.64	915.65	10.48	913.01	
B.M.	4.65	916.88	3.42	912.21	912.23

10-19-29

SAX N 12" OAK AT STA. 170+30

60 3/62 70 9/73 80 64 57 65 110 124 9/26 13.7  
 33 3/70 26 2/17 16 11 0.1 13 22 31 3/70 35

(56)

64 6/65 5/74 79 63 58 53 60 70 10.4 9/116 12.0  
 33 3/71 2/20 17 12 10 10.1 13 17 25 3/62 35

(5.4)

(53)

52 3/58 9/64 67 60 53 42 53 64 8.4 7/8.9 9.6  
 35 3/70 2/12 18 13 9 10.4 12 16 24 6/37 33

(50)

40 3/40 3/50 5.3 5.0 4.3 5.0 5/60 66 5/68 68 72  
 43 3/70 1/60 15 10 10.7 13 2/70 26 2/78 33 43

(4.8)

25 4/60 1.7 2.1 3.0 4.7 4.4 3.7 4.3 5.5 4.3 2/41 4.5  
 43 3/72 3.5 2.2 2.0 1.4 1.1 1.2 1.7 2.5 3/10.7 4.5

(12.1)

24 9/5 9.89 8.8 9.3 9.7 12.2 11.9 11.2 12.1 11.7 11.5 10.4 7/10.5 10.7  
 13 40 5/72 3.6 3.0 2.2 1.6 1.0 1.5 1.6 2.0 2.6 3.0 3/72 4.3

(12.5)

44 1/73 6.9 6.0 7.0 7.6 10.9 11.6 11.2 10.6 11.3 11.1 7.8 7.1 2/78 7.4  
 3 4/75 5.8 3.5 3.2 2.0 1.8 1.4 1.0 1.9 1.3 2.4 3.3 3.7 3/74.7 4.3

(12.3)

5.4 5/54 4.8 4.5 5.2 9.9 11.1 10.9 10.2 10.9 9.7 4.6 3/47 4.9  
 4.5 4/76.9 3.8 3.3 2.7 2.0 1.5 1.1 1.2 1.7 2.4 3.4 4/77.6 4.5

(12.1)

60 5/5.9 5.9 5.5 5.5 9.7 10.4 10.3 9.7 10.2 10.2 9.0 5.2 4/5.5 5.4  
 4.3 4/76.2 3.9 3.7 3.0 2.4 2.0 1.2 1.2 1.2 2.1 2.6 3.5 4/76.8 4.5

(12.0)

85 86 9/82 8.1 7.8 8.5 10.6 10.2 9.6 10.4 10.6 7.7 7.1 9/70 6.9  
 43 3.9 3/73.8 3.7 3.1 1.9 1.4 1.1 1.2 1.4 1.4 2.2 3.1 3.5 3/75.0 4.3

(11.9)

9.9 9.9 9/9.7 9.2 10.6 11.2 10.4 10.0 10.5 11.1 10.5 9.0 8.4 1/8.6 8.6  
 4.3 3.7 3/73.5 3.7 2.1 1.5 1.1 1.1 1.2 1.4 2.5 3.0 3.5 3/73.3 4.3

916.88 ✓

181 11.6 53

+50 11.6 53

182 11.5 54

+50 11.4 55

183 11.2 57

+50 11.0 59

184 10.7 62

+30 10.5 64

+60 10.4 65

185 10.2 67

+50 10.0 69 ✓

4.35 914.63 660 ✓

910.28 ✓

186 09.7 49

10-21-29

(5.3)

45	4.1	4/3.7	3.6	5.0	5.1	4.7	5.9	4.5	5.0	4.7	3/5.2	5.4
43	3.7	3/1.6	3.5	2.2	1.6	1.2	1.4	1.3	1.6	2.7	3/2.1	4.8

(5.3)

45	7/4.3	4.4	5.9	5.0	4.5	5.2	1/5.6	5.8	0/4.7	4.8
35	3/1.0	2.7	2.0	1.0	1.0	1.2	2/-0.3	2.7	3/1.6	3.5

(5.3)

4	9/2.3	6.7	3/6.8	7.0	5.6	5.3	4.9	5.5	6.8	5/6.9	6.7	8/7.0	7.2
	3/1.0	2.7	2/-1.4	1.9	1.2	1.7	1.5	1.3	1.9	2/-1.5	2.9	2/1.6	3.3

(5.3)

7.0	2.0	2/8.1	8.3	6.0	5.8	5.4	5.9	7.4	5/7.5	4/7.4	7.4
3.3	3.0	2/-2.6	2.5	1.2	1.0	1.0	1.1	2.0	2/-2.0	2/-1.9	3.3

(5.1)

8.7	7.3	3/7.1	8.8	6.7	6.4	5.9	6.4	7.4	3/7.6	5/7.5	7.3
3.3	3.1	2/-3.4	2.0	1.2	1.1	1.2	1.0	1.8	2/-1.9	2/-1.8	3.3

(5.9)

8.5	5/8.7	8.7	6.7	6.9	6.7	7.6	7/7.5	0/7.4	7.3
3.3	2/-2.8	1.9	1.3	1.5	1.2	1.8	2/1.6	2/1.5	3.3

(6.2)

10.3	7/9.5	7.7	6.7	6.4	6.7	5/7.7	8/7.8	7.9
3.3	2/-3.1	1.9	1.0	1.2	1.3	2/-1.5	2/-1.6	3.3

(6.4)

6.7	6.7	6.3	6.3	6.5
3.3	1.9	1.9	1.9	3.3

(6.7)

5	2/6.5	6.5	6.8	6.0	2/7.0	7.0	7.1	6.5	6.9	6.3	6.4	8/6.8	6.9
3	3/1.0	3.1	2.8	2.4	2/-0.5	1.8	1.3	0.0	1.1	1.6	2.0	3/-0.3	3.3

(6.7)

7.5	2/7.4	5/7.2	6.9	7.3	6.0	6.8	6.7	7.0	7/6.8	6.3	4.1	2/4.0	4.4
3.3	3/-0.7	2/-0.5	1.3	1.0	1.0	1.2	1.4	1.6	1/-0.1	2.5	3.5	3/2.7	4.8

(6.9)

6.0	0/6.8	5.6	6.8	7.5	7.3	6.6	7.1	7.6	5/6.9	9/6.4	5.9
3.5	3/1.1	2.9	1.9	1.6	1.2	1.0	1.2	1.5	1/1.0	3/1.5	4.3

(4.9)

4.2	3/4.0	3.9	4.6	5.4	4.7	4.2	4.8	5.4	4/3.4	3.7	3.7
3.5	3/1.0	3.0	1.9	1.4	1.1	1.0	1.1	1.4	3/1.5	1.0	4.3

914.63 ✓

750

09.5

51.

187

09.2

54.

750

09.0

56.

188

08.7

57.

750

08.5

61.

189

08.2

64.

750

08.0 ✓

64.

6.07

911.35

955

905.28

190

07.7

37.

750

07.5

37.

191

07.2

42.

750

07.0

44.

192

06.7

47.

(5.1)

43	0/41	40	45	49	37	44	49	57	52	0/28	29
35	3/110	26	19	13	12	13	18	28	5/123	43	

(5.4)

47	0/45	48	45	52	46	40	48	37	37	28	34	0/3.2	34
35	3/70.9	28	21	15	10	11.4	13	17	20	22	26	3/122	43

(5.6)

46	0/44	44	42	58	53	47	53	59	49	40	0/41	41
35	3/70.8	29	25	15	12	10.9	11	13	19	33	3/71.5	43

(5.9)

56	0/54	62	0/66	67	60	5.5	61	65	0/61	5.7	0/54	58
35	3/70.5	26	2/-0.7	14	11	10.4	11	14	0/-0.2	28	3/70.5	43

(6.1)

63	5/59	78	3/80	80	73	65	62	69	82	5/81	78	74	3/74	72
35	3/102	26	2/-1.9	20	15	11	2.1	12	26	5/-20	27	28	3/-15	33

(6.4)

78	91	5/89	91	75	71	77	89	5/89	91
33	28	4/-2.5	21	11	-0.7	13	22	4/-2.5	33

(6.6)

99	1/97	101	80	77	84	103	1/104	102
33	1/3.1	20	11	-1.1	11	19	2/-3.8	33

(3.7)

52	64	5/67	70	55	50	47	52	73	0/79	80
33	31	2/-3.0	18	15	10	-1.0	12	17	1/-4.2	33

(3.9)

44	5/44	54	3/58	50	49	56	75	0/76	77
33	3/-0.6	26	2/7.9	11	-1.0	12	18	0/-3.7	33

(3.2)

40	0/41	41	53	5/57	51	48	54	67	0/64	461	63
33	3/10.1	31	27	2/16	11	-0.6	13	19	2/-2.2	2/7.9	33

(4.4)

45	3/43	50	0/45	52	49	46	47	63	5/64	5/62	61
33	3/70.1	27	1/-0.1	18	11	-0.2	10	17	2/-2.0	2/-1.8	33

(4.7)

57	0/54	0/54	49	47	51	66	3/66	4/66	67
33	3/-0.7	2/0.9	11	10	11	19	2/7.9	2/-1.9	33

911.35 ✓

750

064

5.0

193

060

54

750

05.7

5.7

194

05.2

6.2

750

04.7

6.7

195

04.2

7.2

750

03.7 ✓

7.7 ✓

2.84

909.87 ✓

4.32

707.03

196

03.2

6.7

750

02.7

7.2

197

02.2

7.7

750

01.7 ✓

8.2 ✓

B.M.

1.52

908.37 ✓

3.04

906.83

906.85

198

01.2

7.2

10-21-29

65  $\frac{1}{3} \frac{2}{4}$   $\frac{1}{2} \frac{5}{4}$  50 53 47 52 49 54 69  $\frac{3}{2} \frac{6}{9}$   $\frac{4}{2} \frac{6}{9}$  20  
 33  $\frac{3}{2} \frac{1}{14}$   $\frac{1}{2} \frac{1}{14}$  12 10 103 9 10 15 20  $\frac{3}{2} \frac{1}{14}$   $\frac{2}{2} \frac{1}{14}$  53

(6.0)

49  $\frac{1}{2} \frac{4}{6}$  51 45 99 47 50  $\frac{3}{2} \frac{6}{0}$  61 63  
 43  $\frac{3}{2} \frac{1}{16.8}$  19 109 9 10 19  $\frac{1}{2} \frac{1}{16.8}$  33 43

(6.4)

34  $\frac{2}{3} \frac{3}{0}$  16 39 48 50 40 50 48 45 40  $\frac{2}{3} \frac{4}{2}$  48  
 43  $\frac{3}{2} \frac{1}{127}$  27 24 11 10 11.1 9 10 17 25  $\frac{3}{2} \frac{1}{127}$  35

(6.1)

30  $\frac{2}{3} \frac{4}{4}$  12 11 49 50 46 50 46 47 30  $\frac{2}{3} \frac{4}{4}$  46  
 43  $\frac{3}{2} \frac{1}{138}$  32 29 14 10 11.6 7 10 13 22  $\frac{3}{2} \frac{1}{138}$  45

(6.2)

36  $\frac{5}{2} \frac{1}{5}$  07 40 49 49 49 47 25 32  $\frac{4}{3} \frac{5}{9}$  40  
 43  $\frac{3}{2} \frac{1}{142}$  29 17 12 12.3 9 12 20 32  $\frac{3}{2} \frac{1}{142}$  43

(6.7)

37  $\frac{3}{2} \frac{3}{1}$  13 49 47 49 42 29  $\frac{2}{3} \frac{3}{6}$  40  
 43  $\frac{3}{2} \frac{1}{141}$  30 14 12.8 9 12 22  $\frac{3}{2} \frac{1}{141}$  45

(7.2)

49  $\frac{2}{3} \frac{3}{7}$  17 51 44 49 48 45 43  $\frac{2}{3} \frac{5}{0}$  47  
 43  $\frac{3}{2} \frac{1}{140}$  30 15 13.3 9 10 19 24  $\frac{3}{2} \frac{1}{140}$  43

(7.1)

46  $\frac{2}{3} \frac{3}{9}$  28 38 41 42 57 42 39 37 50  $\frac{8}{5} \frac{6}{6}$  54  
 43  $\frac{3}{2} \frac{1}{128}$  31 25 20 11 13.0 10 14 18 23  $\frac{3}{2} \frac{1}{111}$  43

(6.1)

66  $\frac{6}{4} \frac{5}{2}$  45 57 53 42 51 57 49 48 65  $\frac{2}{3} \frac{5}{5}$  65  
 43  $\frac{3}{2} \frac{1}{116}$  31 26 11 12.4 10 12 13 24 28  $\frac{3}{2} \frac{1}{107}$  45

(7.2)

83  $\frac{2}{3} \frac{2}{0}$  63 64 67 61 67 63 51  $\frac{1}{2} \frac{6}{5}$  69  
 43  $\frac{3}{2} \frac{1}{107}$  20 12 10 11.4 11 14 23  $\frac{3}{2} \frac{1}{71.2}$  43

(7.1)

88  $\frac{2}{3} \frac{2}{2}$  86 74 79 73 78 56 61  $\frac{2}{3} \frac{5}{1}$  54  
 33  $\frac{3}{2} \frac{1}{100}$  28 22 13 10.9 11 20 22  $\frac{3}{2} \frac{1}{131}$  43

(6.2)

94  $\frac{1}{2} \frac{8}{7}$  80 73 70 76 65 67 37  $\frac{1}{2} \frac{3}{3}$  31  
 43  $\frac{3}{2} \frac{1}{11.5}$   $\frac{1}{2} \frac{1}{10.6}$  15 11 10.2 11 18 22 29  $\frac{3}{2} \frac{1}{13.9}$  43

(7.2)

✓  
708.37

f50

00.7

7.7

199

3.05

✓  
901.79

7.63

00.2 ✓  
898.74

82

f50

99.7

122 2.1

200

99.2

124 2.4

f50

98.7

126 3.1

201

98.2

128 3.4

f50

9.85

✓  
908.59

3.05

97.7 ✓  
898.74 ✓

130 4.1

B.M.

1.74

906.85

906.85

SEE PAGE 62

11.5 107 10.5  $\frac{3}{96}$  9.1 9.3 86 81  $\frac{27}{84}$  9.1 81  $\frac{3}{86}$  5.1  $\frac{5}{48}$  4.5  
 4.3 3.3 2.6  $\frac{2}{19}$  2.0 1.6 1.2 -0.4 1.0 1.3 1.6 2.1 -0.9 3.0 3.1 4.3

(17)

14.4 9.1 12.6 9.5 9.1 7.5 10.1 7.1 10.0 7.0 9.6 5.7  
 4.3 4.8 -4.7 2.5 1.1 -0.9 1.0 1.3 1.7  $\frac{2}{18}$  -1.8 3.0  $\frac{4}{114}$  4.3

(22)

9.8 4.7 9.8 1.9 8.0 4.4 4.1 4.5 4.2 5.3 2.4 1.5  
 4.5 4.1 3.6 3.3 -7.1 2.4 1.1 -2.0 1.0 1.8 2.3 3.1 -0.3 4.3

(21)

11.4 10.5 10.1 5.8 5.4 5.7 6.3 5.5 6.2 6.9 9.6 4.9 4.6 5.0  
 4.5 4.1 4.0 3.5 -7.8 2.5 1.2 2.8 1.0 1.3 1.6 1.8 2.3 2.3 3.0 3.1 4.3

(26)

12.2 11.4 7.2 6.6 7.0 7.0 8.8 3.7 6.8 6.5 6.1  
 4.5 4.1 3.0 2.3 1.1 -5.5 1.0 2.2 2.2 3.1 -4.4 3.0 3.1 4.3

(31)

12.2 11.8 9.1 7.7 7.3 7.9 8.0 10.5 10.7 9.2 8.5 8.4  
 4.5 4.1 3.0 2.3 1.1 -3.7 1.0 1.4 2.1 2.8 3.1 -5.6 4.1 4.3

(36)

11.8 11.7 9.1 8.1 7.6 8.2 8.0 11.0 11.4 11.0 11.0  
 4.3 4.1 3.0 2.3 1.1 -3.5 1.0 1.8 3.1 -7.3 4.1 4.3

(41)

13. M	4.53	908.80 ✓		904.27 ✓	
	1.82	903.45 ✓	7.11	901.63 ✓	
	5.66	898.49	8.62	894.89	
216 + 50				95.2	33 -
217				95.4	31 -
+ 50				95.6	29 -
218				95.8	27 -
+ 50				96.1 ✓	24 -
	7.86	902.69	3.66	894.83	
219				96.4	23 -
+ 50				96.8	21 -
220				97.2	19 -
+ 50				97.6	17 -
221				98.0	15 -
+ 50				98.4 ✓	13 -
	8.47	908.84 ✓	2.32	900.37	

11-5-29

SUN IN 18" TREE 60 LT. 57R 22720

(3.3)

4/16 IN T.P. 14 57R 118725.  
 47 48 61 5/68 66 55 56 49 47 49 50 52 97 94 9/81 65 70 70  
 48 52 28 2/35 21 17 15 10 14 10 13 17 25 27 2/48 52 41 43

(3.1)

51 57 1/69 72 52 48 43 41 46 46 47 94 98 7/77 56 61  
 43 39 2/38 23 23 14 10 10 9 10 17 24 27 2/46 51 43

(2.9)

55 57 9/71 66 48 37 34 37 44 44 96 94 9/79 53 57  
 43 25 2/42 21 17 11 10 11 12 15 24 27 2/45 51 43

(2.7)

59 48 9/69 65 51 52 50 34 38 95 95 9/95 49 54  
 43 35 2/42 22 17 9 10 11 16 24 27 2/46 31 43

(2.4)

45 52 60 60 44 52 24 28 54 90 91 8/68 43 41 46  
 43 34 28 20 16 11 10 12 14 25 27 2/44 31 38 43

(6.3)

85 85 5/72 101 92 69 63 61 68 77 95 95 150 153 9/114 107 114  
 43 27 2/27 23 20 14 10 10 11 14 17 21 24 28 2/51 32 43

(5.9)

95 1/100 105 100 65 52 56 59 65 68 9/21 112 120  
 43 2/41 24 20 14 10 10 10 13 17 2/32 50 43

(5.5)

75 80 3/79 103 101 55 50 48 50 50 6/55 105 102  
 43 28 2/34 23 21 13 9 10 11 18 2/10 33 43

(5.1)

66 67 5/79 91 90 43 40 43 5/51 94 97  
 43 29 2/28 23 19 10 11 10 2/20 27 43

(4.7)

74 74 46 5/57 56 38 33 31 34 38 48 7/57 60  
 43 2/27 2/17 17 14 10 11 11 20 27 2/10 43

(4.3)

27 2/25 24 34 28 2.5 28 29 2.7 6/27 2.7  
 43 3/32 23 16 10 11 11 22 23 3/16 43

✓  
908.84

222				98.8	10.0
+50				99.2	9.6
223				99.4	9.2
+50				00.0	8.8
224				00.4	8.4
	4.56	908.83	4.56	904.28	904.28
+50				00.8	8.0
225				01.2	7.6
+50				01.6	7.2
226				02.0	6.8
+50				02.4	6.4
227				02.8	6.0
+50				03.2	5.6

11-5-29

$$\begin{array}{r} 62 \\ 43 \end{array} \quad \begin{array}{r} 7 \overline{) 68} \\ 3 \overline{) 87} \end{array} \quad \begin{array}{r} 80 \\ 12.0 \end{array} \quad \begin{array}{r} 8 \overline{) 59} \\ 3 \overline{) 70} \end{array} \quad \begin{array}{r} 62 \\ 43 \end{array}$$

$$\begin{array}{r} 53 \\ 43 \end{array} \quad \begin{array}{r} 5 \overline{) 54} \\ 3 \overline{) 72} \end{array} \quad \begin{array}{r} 72 \\ 12.4 \end{array} \quad \begin{array}{r} 5 \overline{) 44} \\ 3 \overline{) 52} \end{array} \quad \begin{array}{r} 46 \\ 43 \end{array}$$

$$\begin{array}{r} 45 \\ 43 \end{array} \quad \begin{array}{r} 7 \overline{) 47} \\ 3 \overline{) 43} \end{array} \quad \begin{array}{r} 66 \\ 11.6 \end{array} \quad \begin{array}{r} 5 \overline{) 30} \\ 4 \overline{) 152} \end{array} \quad \begin{array}{r} 51 \\ 43 \end{array}$$

$$\begin{array}{r} 36 \\ 43 \end{array} \quad \begin{array}{r} 5 \overline{) 39} \\ 3 \overline{) 77} \end{array} \quad \begin{array}{r} 60 \\ 12.8 \end{array} \quad \begin{array}{r} 9 \overline{) 30} \\ 4 \overline{) 158} \end{array} \quad \begin{array}{r} 30 \\ 43 \end{array}$$

$$\begin{array}{r} 22 \\ 43 \end{array} \quad \begin{array}{r} 5 \overline{) 22} \\ 4 \overline{) 762} \end{array} \quad \begin{array}{r} 53 \\ 13.1 \end{array} \quad \begin{array}{r} 5 \overline{) 22} \\ 4 \overline{) 762} \end{array} \quad \begin{array}{r} 38 \\ 43 \end{array}$$

$$\begin{array}{r} 70 \\ 43 \end{array} \quad \begin{array}{r} 2 \overline{) 40} \\ 3 \overline{) 70} \end{array} \quad \begin{array}{r} 50 \\ 11.0 \end{array} \quad \begin{array}{r} 7 \overline{) 30} \\ 3 \overline{) 750} \end{array} \quad \begin{array}{r} 30 \\ 43 \end{array}$$

$$\begin{array}{r} 8 \overline{) 51} \\ 3 \overline{) 125} \end{array} \quad \begin{array}{r} 50 \\ 11.6 \end{array} \quad \begin{array}{r} 3 \overline{) 51} \\ 3 \overline{) 125} \end{array} \quad \begin{array}{r} 51 \\ 35 \end{array}$$

$$\begin{array}{r} 5 \overline{) 58} \\ 3 \overline{) 74} \end{array} \quad \begin{array}{r} 50 \\ 12.2 \end{array} \quad \begin{array}{r} 5 \overline{) 54} \\ 3 \overline{) 118} \end{array} \quad \begin{array}{r} 54 \\ 35 \end{array}$$

$$\begin{array}{r} 57 \\ 35 \end{array} \quad \begin{array}{r} 3 \overline{) 57} \\ 3 \overline{) 111} \end{array} \quad \begin{array}{r} 49 \\ 11.9 \end{array} \quad \begin{array}{r} 6 \overline{) 65} \\ 3 \overline{) 105} \end{array} \quad \begin{array}{r} 65 \\ 35 \end{array}$$

$$\begin{array}{r} 58 \\ 35 \end{array} \quad \begin{array}{r} 3 \overline{) 58} \\ 3 \overline{) 106} \end{array} \quad \begin{array}{r} 49 \\ 11.5 \end{array} \quad \begin{array}{r} 8 \overline{) 60} \\ 3 \overline{) 104} \end{array} \quad \begin{array}{r} 60 \\ 35 \end{array}$$

$$\begin{array}{r} 59 \\ 35 \end{array} \quad \begin{array}{r} 3 \overline{) 59} \\ 3 \overline{) 101} \end{array} \quad \begin{array}{r} 50 \\ 11.0 \end{array} \quad \begin{array}{r} 6 \overline{) 57} \\ 3 \overline{) 103} \end{array} \quad \begin{array}{r} 57 \\ 35 \end{array}$$

$$\begin{array}{r} 51 \\ 35 \end{array} \quad \begin{array}{r} 8 \overline{) 52} \\ 3 \overline{) 104} \end{array} \quad \begin{array}{r} 50 \\ 10.6 \end{array} \quad \begin{array}{r} 15 \overline{) 9} \\ 3 \overline{) 103} \end{array} \quad \begin{array}{r} 2 \overline{) 63} \\ 3 \overline{) 107} \end{array} \quad \begin{array}{r} 64 \\ 33 \end{array}$$

708.85

228

03.5

5.3

+50

03.7

5.1

229

03.9

4.9

+50

04.0

4.8

230

04.1

4.7

4.84

708.76

4.71

903.92

+50

04.1

4.7

231

04.0

4.8

+50

03.9

4.9

232

03.8

5.0

+50

03.7

5.1

233

03.6

5.2

6.37

908.50

6.63

902.13

+50

03.5

5.0

$$\begin{array}{r} 50 \\ 35 \end{array} \begin{array}{r} 6 \\ 3 \end{array} \begin{array}{r} 50 \\ 703 \end{array} \quad \begin{array}{r} 49 \\ 10.4 \end{array} \quad \begin{array}{r} 5 \\ 19 \end{array} \begin{array}{r} 53 \\ 00 \end{array} \quad \begin{array}{r} 1 \\ 3 \end{array} \begin{array}{r} 54 \\ -01 \end{array} \quad \begin{array}{r} 54 \\ 33 \end{array}$$

$$\begin{array}{r} 46 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 46 \\ 705 \end{array} \quad \begin{array}{r} 47 \\ 10.4 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 44 \\ 707 \end{array} \quad \begin{array}{r} 43 \\ 35 \end{array}$$

$$\begin{array}{r} 32 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 32 \\ 717 \end{array} \quad \begin{array}{r} 49 \\ 0.0 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 26 \\ 723 \end{array} \quad \begin{array}{r} 30 \\ 35 \end{array}$$

$$\begin{array}{r} 32 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 32 \\ 716 \end{array} \quad \begin{array}{r} 4.8 \\ 0.0 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 24 \\ 724 \end{array} \quad \begin{array}{r} 24 \\ 33 \end{array}$$

$$\begin{array}{r} 27 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 24 \\ 723 \end{array} \quad \begin{array}{r} 49 \\ 0.2 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 27 \\ 720 \end{array} \quad \begin{array}{r} 30 \\ 33 \end{array}$$

$$\begin{array}{r} 3.1 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 31 \\ 716 \end{array} \quad \begin{array}{r} 47 \\ 0.0 \end{array} \quad \begin{array}{r} 6 \\ 3 \end{array} \begin{array}{r} 43 \\ 704 \end{array} \quad \begin{array}{r} 46 \\ 33 \end{array}$$

$$\begin{array}{r} 32 \\ 35 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 32 \\ 716 \end{array} \quad \begin{array}{r} 4.9 \\ -0.1 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 43 \\ 705 \end{array} \quad \begin{array}{r} 46 \\ 35 \end{array}$$

$$\begin{array}{r} 30 \\ 33 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 35 \\ 714 \end{array} \quad \begin{array}{r} 50 \\ -0.1 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 42 \\ 707 \end{array} \quad \begin{array}{r} 40 \\ 35 \end{array}$$

$$\begin{array}{r} 30 \\ 33 \end{array} \begin{array}{r} 30 \\ 3 \end{array} \begin{array}{r} 34 \\ 716 \end{array} \quad \begin{array}{r} 50 \\ 0.0 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 30 \\ 712 \end{array}$$

$$\begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 44 \\ 707 \end{array} \quad \begin{array}{r} 48 \\ 703 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 46 \\ 705 \end{array}$$

$$\begin{array}{r} 30 \\ 33 \end{array} \begin{array}{r} 6 \\ 3 \end{array} \begin{array}{r} 49 \\ 703 \end{array} \quad \begin{array}{r} 4.9 \\ 703 \end{array} \quad \begin{array}{r} 5 \\ 21 \end{array} \begin{array}{r} 63 \\ 70 \end{array} \quad \begin{array}{r} 0 \\ 3 \end{array} \begin{array}{r} 67 \\ -15 \end{array} \quad \begin{array}{r} 67 \\ 33 \end{array}$$

$$\begin{array}{r} 3.6 \\ 33 \end{array} \begin{array}{r} 5 \\ 3 \end{array} \begin{array}{r} 35 \\ 703 \end{array} \quad \begin{array}{r} 4.8 \\ 70.2 \end{array} \quad \begin{array}{r} 2 \\ 21 \end{array} \begin{array}{r} 60 \\ 70 \end{array} \quad \begin{array}{r} 5 \\ 4 \end{array} \begin{array}{r} 68 \\ 78 \end{array} \quad \begin{array}{r} 70 \\ 33 \end{array}$$

90850

234

03.4

5.1

+50

03.3

5.2

235

03.2

5.3

+50

03.1

5.4

236

03.1

5.4

+35 ✓

03.0

5.5

237 ✓

03.1

5.4

+40 ✓

03.1

5.4

238 ✓

03.2

5.3

+50

03.3

5.2

239

03.4

5.1

+50

03.6

4.7

$$\begin{array}{r} 58 \\ 33 \end{array} \begin{array}{r} 1/55 \\ 3/-02 \end{array} \begin{array}{r} 50 \\ 101 \end{array} \begin{array}{r} 7/67 \\ 2/-16 \end{array} \begin{array}{r} 9/71 \\ 2/-20 \end{array} \begin{array}{r} 72 \\ 33 \end{array}$$

$$\begin{array}{r} 0/47 \\ 3/105 \end{array} \begin{array}{r} 49 \\ 103 \end{array} \begin{array}{r} 1/68 \\ 2/-76 \end{array} \begin{array}{r} 4/22 \\ 2/-20 \end{array} \begin{array}{r} 71 \\ 33 \end{array}$$

$$\begin{array}{r} 0/42 \\ 3/111 \end{array} \begin{array}{r} 49 \\ 114 \end{array} \begin{array}{r} 5/68 \\ 2/-10 \end{array} \begin{array}{r} 9/70 \\ 2/-17 \end{array} \begin{array}{r} 69 \\ 33 \end{array}$$

$$\begin{array}{r} 0/42 \\ 3/112 \end{array} \begin{array}{r} 49 \\ 105 \end{array} \begin{array}{r} 5/54 \\ 1/00 \end{array} \begin{array}{r} 0/62 \\ 3/-08 \end{array} \begin{array}{r} 63 \\ 33 \end{array}$$

$$\begin{array}{r} 0/40 \\ 3/114 \end{array} \begin{array}{r} 50 \\ 104 \end{array} \begin{array}{r} 6/54 \\ 2/00 \end{array}$$

$$\begin{array}{r} 0/41 \\ 3/114 \end{array} \begin{array}{r} 49 \\ 106 \end{array} \begin{array}{r} 8/99 \\ 2/-44 \end{array}$$

$$\begin{array}{r} 0/47 \\ 3/107 \end{array} \begin{array}{r} 5/64 \\ 2/-10 \end{array} \begin{array}{r} 51 \\ 103 \end{array} \begin{array}{r} 0/57 \\ 2/-08 \end{array} \begin{array}{r} 5/59 \\ 3/-05 \end{array} \begin{array}{r} 60 \\ 33 \end{array}$$

$$\begin{array}{r} 5/114 \\ 3/-20 \end{array} \begin{array}{r} 50 \\ 104 \end{array} \begin{array}{r} 9/71 \\ 2/-17 \end{array} \begin{array}{r} 5/72 \\ 2/-78 \end{array} \begin{array}{r} 72 \\ 33 \end{array}$$

$$\begin{array}{r} 84 \\ 33 \end{array} \begin{array}{r} 9/85 \\ 2/-32 \end{array} \begin{array}{r} 52 \\ 101 \end{array} \begin{array}{r} 1/26 \\ 2/-25 \end{array} \begin{array}{r} 78 \\ 33 \end{array}$$

$$\begin{array}{r} 8/96 \\ 2/-44 \end{array} \begin{array}{r} 54 \\ 102 \end{array} \begin{array}{r} 6/85 \\ 2/-33 \end{array} \begin{array}{r} 85 \\ 33 \end{array}$$

$$\begin{array}{r} 107 \\ 33 \end{array} \begin{array}{r} 5/104 \\ 3/-55 \end{array} \begin{array}{r} 54 \\ 103 \end{array} \begin{array}{r} 1/94 \\ 2/-43 \end{array} \begin{array}{r} 75 \\ 33 \end{array}$$

$$\begin{array}{r} 5/114 \\ 3/-63 \end{array} \begin{array}{r} 54 \\ 106 \end{array} \begin{array}{r} 5/103 \\ 3/0/54 \end{array} \begin{array}{r} 104 \\ 33 \end{array}$$

908.50

240

037

48

+50

039

46

B.M.

5.71

910.06

4.16

904.34

904.35

241

04.0

5.5 61 6

+50

04.2

5.0 5.9 6

242

04.3

4.7 5.8 6

+50

04.5

4.5 5.6

243

04.6

4.5 5.5 6

+50

04.8

4.4 5.3 6

244

04.9

4.9 5.0

B.M.

5.71

904.35

$\frac{9}{3} \frac{x}{110}$	$\frac{5.2}{-0.4}$	$\frac{5}{3} \frac{x}{103}$	$\frac{10.3}{33}$
-----------------------------	--------------------	-----------------------------	-------------------

$\frac{3}{9} \frac{x}{100}$	$\frac{4.8}{-0.2}$	$\frac{9}{2} \frac{x}{98}$	$\frac{9.8}{33}$
-----------------------------	--------------------	----------------------------	------------------

$\frac{10.3}{33}$	$\frac{5}{9} \frac{x}{105}$	$\frac{5.3}{10.3}$	$\frac{x}{-4.0}$	$\frac{10.3}{33}$
-------------------	-----------------------------	--------------------	------------------	-------------------

$\frac{7.6}{33}$	$\frac{3}{4} \frac{x}{74}$	$\frac{5.5}{10.4}$	$\frac{x}{-0.8}$	$\frac{8.6}{33}$
------------------	----------------------------	--------------------	------------------	------------------

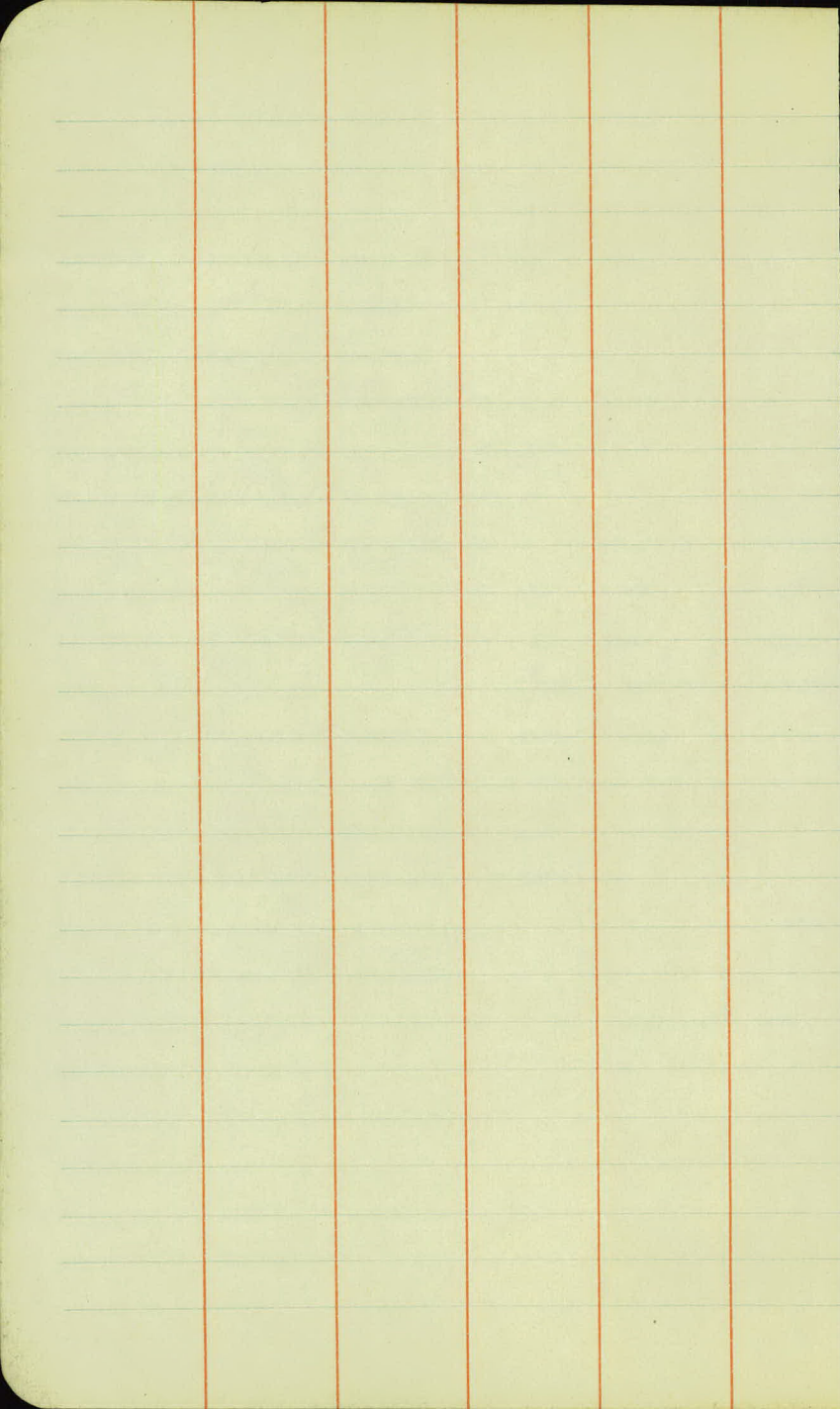
$\frac{8.5}{10.2}$	$\frac{7}{4} \frac{x}{75}$	$\frac{5.3}{10.5}$	$\frac{5}{9} \frac{x}{5.8}$	$\frac{6.4}{33}$
--------------------	----------------------------	--------------------	-----------------------------	------------------

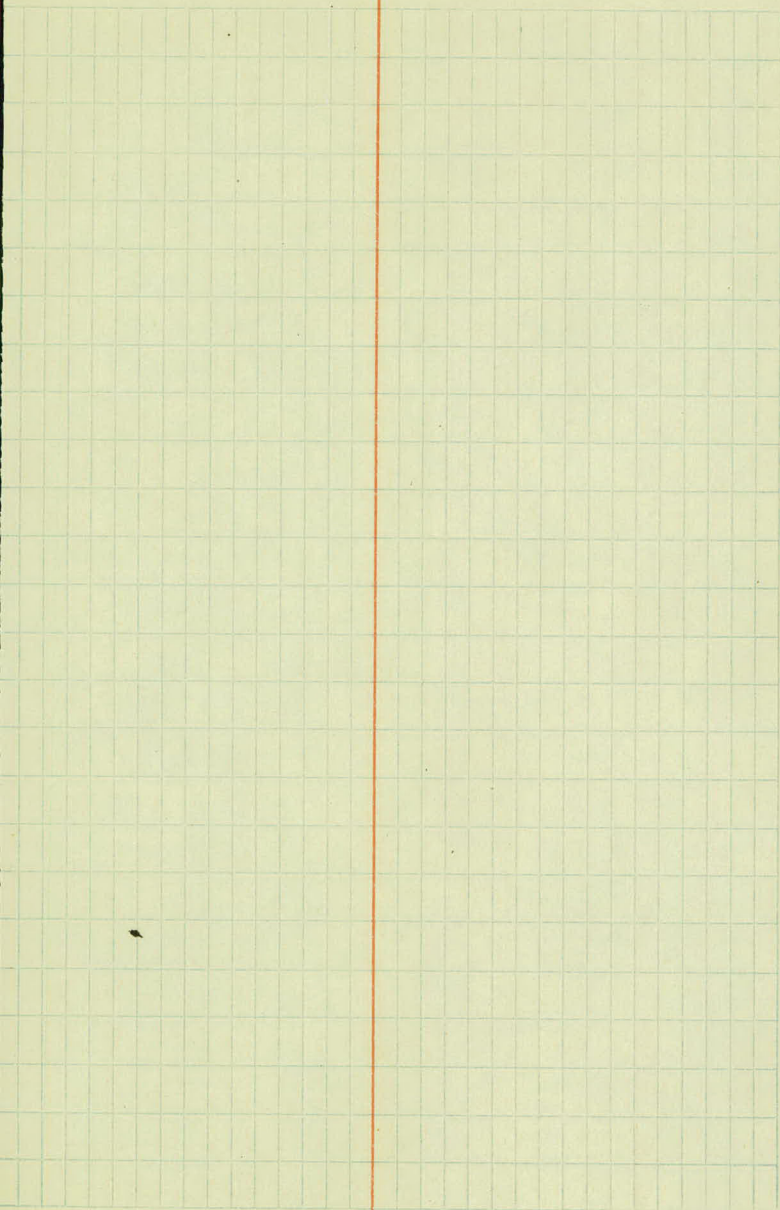
$\frac{3}{3} \frac{x}{5.6}$	$\frac{3}{2} \frac{x}{67}$	$\frac{5.0}{10.6}$	$\frac{5}{19} \frac{x}{5.4}$	$\frac{x}{1.2}$
-----------------------------	----------------------------	--------------------	------------------------------	-----------------

$\frac{3}{3} \frac{x}{3.9}$	$\frac{2}{2} \frac{x}{72}$	$\frac{5.3}{10.4}$	$\frac{5}{5} \frac{x}{8.0}$	$\frac{3}{3} \frac{x}{4.9}$
-----------------------------	----------------------------	--------------------	-----------------------------	-----------------------------

$\frac{3}{3} \frac{x}{4.6}$	$\frac{5}{6} \frac{x}{74}$	$\frac{5.3}{0.0}$	$\frac{2}{2} \frac{x}{7.5}$	$\frac{3}{3} \frac{x}{5.0}$
-----------------------------	----------------------------	-------------------	-----------------------------	-----------------------------

$\frac{3}{3} \frac{x}{5.5}$	$\frac{5}{2} \frac{x}{77}$	$\frac{4.9}{10.3}$	$\frac{3}{2} \frac{x}{7.3}$	$\frac{3}{5} \frac{x}{5.4}$
-----------------------------	----------------------------	--------------------	-----------------------------	-----------------------------





B.M. 2.75 922.62 ✓ 919.87

10 19.3

+50 19.1

11 19.0

+50 18.7

12 18.4

+50 18.0

13 17.9

+50 17.6

14 17.4

+50 17.3

B.M. 2.75 919.87 ✓

10-30-29

$\frac{51}{45}$   $\frac{51}{45}$   $\frac{53}{34}$   $\frac{63}{30}$   $\frac{60}{26}$   $\frac{40}{20}$  ✓  $\frac{40}{20}$   $\frac{7.5}{28}$   $\frac{8.5}{43}$

$\frac{49}{45}$   $\frac{49}{45}$   $\frac{52}{33}$   $\frac{62}{29}$   $\frac{62}{27}$   $\frac{41}{20}$  ✓  $\frac{3.9}{19}$   $\frac{7.8}{29}$   $\frac{8.5}{43}$   $\frac{8.5}{45}$

$\frac{4.5}{45}$   $\frac{44}{45}$   $\frac{5.2}{54}$   $\frac{6.5}{31}$   $\frac{64}{27}$   $\frac{45}{30}$  ✓  $\frac{4.3}{19}$   $\frac{8.1}{28}$   $\frac{8.8}{43}$

$\frac{4.3}{45}$   $\frac{44}{45}$   $\frac{46}{36}$   $\frac{67}{31}$   $\frac{65}{27}$   $\frac{45}{20}$  ✓  $\frac{46}{20}$   $\frac{8.0}{27}$   $\frac{8.6}{43}$

$\frac{4.5}{45}$   $\frac{48}{45}$   $\frac{5.3}{36}$   $\frac{7.2}{31}$   $\frac{7.1}{27}$   $\frac{47}{20}$  ✓  $\frac{4.9}{20}$   $\frac{8.0}{27}$   $\frac{9.0}{43}$

$\frac{4.7}{45}$   $\frac{47}{45}$   $\frac{5.3}{35}$   $\frac{7.5}{30}$   $\frac{7.2}{27}$   $\frac{49}{20}$  ✓  $\frac{5.0}{20}$   $\frac{8.5}{27}$   $\frac{9.0}{43}$

$\frac{4.8}{45}$   $\frac{4.5}{45}$   $\frac{5.5}{35}$   $\frac{7.8}{30}$   $\frac{7.7}{27}$   $\frac{5.1}{20}$  ✓  $\frac{5.4}{20}$   $\frac{8.9}{28}$   $\frac{9.7}{43}$

$\frac{5.4}{45}$   $\frac{5.2}{45}$   $\frac{5.7}{34}$   $\frac{8.6}{30}$   $\frac{8.6}{27}$   $\frac{5.0}{20}$  ✓  $\frac{5.8}{20}$   $\frac{9.3}{28}$   $\frac{9.9}{43}$

$\frac{5.7}{45}$   $\frac{5.8}{45}$   $\frac{6.0}{38}$   $\frac{9.1}{32}$   $\frac{9.0}{26}$   $\frac{5.4}{20}$  ✓  $\frac{6.4}{20}$   $\frac{9.1}{27}$   $\frac{10.0}{43}$

$\frac{5.5}{45}$   $\frac{5.4}{45}$   $\frac{5.9}{39}$   $\frac{9.1}{33}$   $\frac{9.1}{29}$   $\frac{5.3}{20}$  ✓  $\frac{6.6}{20}$   $\frac{9.9}{28}$   $\frac{10.2}{31}$   $\frac{10.2}{34}$   $\frac{8.9}{43}$

B.M.	1.75	725.60 ✓	923.85
117			22.1
-			
+50			22.0
118			21.9
+50			21.7
119			21.7
+50			21.6
120			21.5
+50			21.5
121			21.2
+50			

B.M. 1.75 923.85 ✓

SEE PAGE 32

<u>54</u>	<u>71</u>	<u>64</u>	<u>3.9</u>	✓	<u>4.5</u>	<u>68</u>	<u>72</u>	<u>5.5</u>	<u>54</u>
<u>43</u>	<u>39</u>	<u>52</u>	<u>21</u>	<u>3.5</u>	<u>21</u>	<u>30</u>	<u>37</u>	<u>43</u>	<u>45</u>

<u>55</u>	<u>69</u>	<u>62</u>	<u>3.9</u>	✓	<u>4.2</u>	<u>61</u>	<u>7.2</u>	<u>5.1</u>	<u>5.0</u>
<u>44</u>	<u>39</u>	<u>29</u>	<u>20</u>	<u>3.6</u>	<u>20</u>	<u>27</u>	<u>37</u>	<u>43</u>	<u>45</u>

<u>60</u>	<u>72</u>	<u>64</u>	<u>4.0</u>	✓	<u>4.4</u>	<u>67</u>	<u>74</u>	<u>4.9</u>	<u>4.8</u>
<u>43</u>	<u>39</u>	<u>50</u>	<u>10</u>	<u>3.7</u>	<u>20</u>	<u>29</u>	<u>37</u>	<u>43</u>	<u>45</u>

<u>59</u>	<u>59</u>	<u>67</u>	<u>62</u>	<u>3.7</u>	✓	<u>4.8</u>	<u>72</u>	<u>7.5</u>	<u>5.1</u>	<u>5.1</u>
<u>43</u>	<u>36</u>	<u>33</u>	<u>28</u>	<u>20</u>	<u>3.9</u>	<u>20</u>	<u>28</u>	<u>37</u>	<u>44</u>	<u>45</u>

<u>62</u>	<u>60</u>	<u>3.0</u>	✓	<u>5.2</u>	<u>71</u>	<u>7.9</u>	<u>5.7</u>	<u>5.6</u>
<u>43</u>	<u>28</u>	<u>20</u>	<u>3.9</u>	<u>21</u>	<u>27</u>	<u>36</u>	<u>43</u>	<u>43</u>

<u>62</u>	<u>62</u>	<u>3.8</u>	✓	<u>5.5</u>	<u>73</u>	<u>8.0</u>	<u>5.7</u>	<u>5.6</u>
<u>43</u>	<u>28</u>	<u>20</u>	<u>4.0</u>	<u>21</u>	<u>27</u>	<u>35</u>	<u>41</u>	<u>45</u>

<u>62</u>	<u>58</u>	<u>3.9</u>	✓	<u>5.6</u>	<u>76</u>	<u>8.0</u>	<u>5.2</u>	<u>5.3</u>
<u>43</u>	<u>26</u>	<u>20</u>	<u>4.1</u>	<u>21</u>	<u>27</u>	<u>32</u>	<u>38</u>	<u>43</u>

<u>61</u>	<u>57</u>	<u>4.1</u>	✓	<u>5.6</u>	<u>7.6</u>	<u>8.0</u>	<u>5.4</u>	<u>5.4</u>
<u>43</u>	<u>25</u>	<u>20</u>	<u>4.1</u>	<u>22</u>	<u>28</u>	<u>32</u>	<u>38</u>	<u>43</u>

<u>62</u>	<u>57</u>	<u>3.9</u>	✓	<u>5.4</u>	<u>7.5</u>	<u>8.0</u>	<u>5.1</u>	<u>4.9</u>
<u>43</u>	<u>27</u>	<u>20</u>	<u>4.4</u>	<u>20</u>	<u>27</u>	<u>33</u>	<u>38</u>	<u>43</u>

SEE ORINBP X SEC.

B.M

5.11

930.94 ✓

925.83

97

+50

98

+50

25.2

99

25.6

+25

25.7

+50

25.7

+75

25.8

100

25.9

+50

25.8

101

25.8

+50

25.8

$\frac{54}{70}$   $\frac{54}{50}$   $\frac{60}{56}$   $\frac{66}{58}$

$\frac{46}{76}$   $\frac{52}{50}$   $\frac{52}{42}$   $\frac{82}{56}$   $\frac{70}{58}$

5.4

$\frac{38}{102}$   $\frac{36}{68}$   $\frac{47}{48}$   $\frac{82}{56}$   $\frac{87}{58}$

5.4

$\frac{45}{125}$   $\frac{46}{100}$   $\frac{47}{70}$   $\frac{45}{48}$   $\frac{89}{35}$   $\frac{72}{54}$   $\frac{90}{29}$   $\frac{66}{20}$  ✓  $\frac{52}{20}$   $\frac{71}{26}$   $\frac{74}{52}$   $\frac{59}{34}$   $\frac{58}{50}$   $\frac{61}{60}$

$\frac{54}{144}$   $\frac{55}{100}$   $\frac{53}{76}$   $\frac{52}{48}$   $\frac{79}{35}$   $\frac{84}{34}$   $\frac{82}{28}$   $\frac{65}{21}$  ✓  $\frac{49}{26}$   $\frac{58}{39}$   $\frac{71}{45}$   $\frac{75}{50}$

$\frac{68}{153}$   $\frac{58}{150}$   $\frac{57}{100}$   $\frac{59}{83}$   $\frac{53}{47}$   $\frac{72}{48}$   $\frac{72}{38}$   $\frac{62}{51}$  ✓  $\frac{48}{21}$   $\frac{68}{26}$   $\frac{72}{30}$   $\frac{50}{35}$   $\frac{63}{47}$   $\frac{60}{50}$

$\frac{59}{163}$   $\frac{62}{150}$   $\frac{63}{120}$   $\frac{59}{100}$   $\frac{60}{72}$   $\frac{66}{72}$   $\frac{66}{74}$   $\frac{58}{50}$   $\frac{63}{24}$  ✓  $\frac{47}{21}$   $\frac{68}{26}$   $\frac{71}{31}$   $\frac{51}{34}$   $\frac{62}{50}$

$\frac{58}{172}$   $\frac{60}{150}$   $\frac{58}{110}$   $\frac{49}{84}$   $\frac{61}{50}$   $\frac{53}{47}$   $\frac{46}{90}$   $\frac{78}{38}$   $\frac{82}{28}$   $\frac{64}{20}$  ✓  $\frac{49}{20}$   $\frac{66}{25}$   $\frac{70}{31}$   $\frac{57}{38}$   $\frac{61}{50}$

$\frac{58}{78}$   $\frac{62}{150}$   $\frac{57}{104}$   $\frac{49}{11}$   $\frac{50}{100}$   $\frac{64}{72}$   $\frac{50}{36}$   $\frac{49}{50}$   $\frac{46}{71}$   $\frac{85}{32}$   $\frac{84}{29}$   $\frac{67}{21}$  ✓  $\frac{47}{20}$   $\frac{64}{26}$   $\frac{69}{31}$   $\frac{56}{35}$   $\frac{62}{50}$

$\frac{47}{163}$   $\frac{52}{114}$   $\frac{63}{123}$   $\frac{50}{116}$   $\frac{42}{106}$   $\frac{43}{70}$   $\frac{53}{42}$   $\frac{87}{38}$   $\frac{83}{28}$   $\frac{68}{22}$  ✓  $\frac{49}{20}$   $\frac{63}{37}$   $\frac{66}{50}$

$\frac{43}{212}$   $\frac{53}{188}$   $\frac{44}{163}$   $\frac{40}{150}$   $\frac{50}{100}$   $\frac{53}{39}$   $\frac{80}{33}$   $\frac{84}{32}$   $\frac{51}{27}$   $\frac{65}{21}$  ✓  $\frac{47}{20}$   $\frac{67}{26}$   $\frac{71}{30}$   $\frac{63}{32}$   $\frac{63}{43}$   $\frac{70}{50}$

$\frac{38}{136}$   $\frac{42}{112}$   $\frac{44}{100}$   $\frac{47}{50}$   $\frac{49}{39}$   $\frac{74}{32}$   $\frac{77}{26}$   $\frac{60}{21}$  ✓  $\frac{47}{20}$   $\frac{67}{26}$   $\frac{72}{31}$   $\frac{54}{34}$   $\frac{61}{50}$



930.94

+85

26.0

102

25.9

+50

B.M.

5.11

925.83

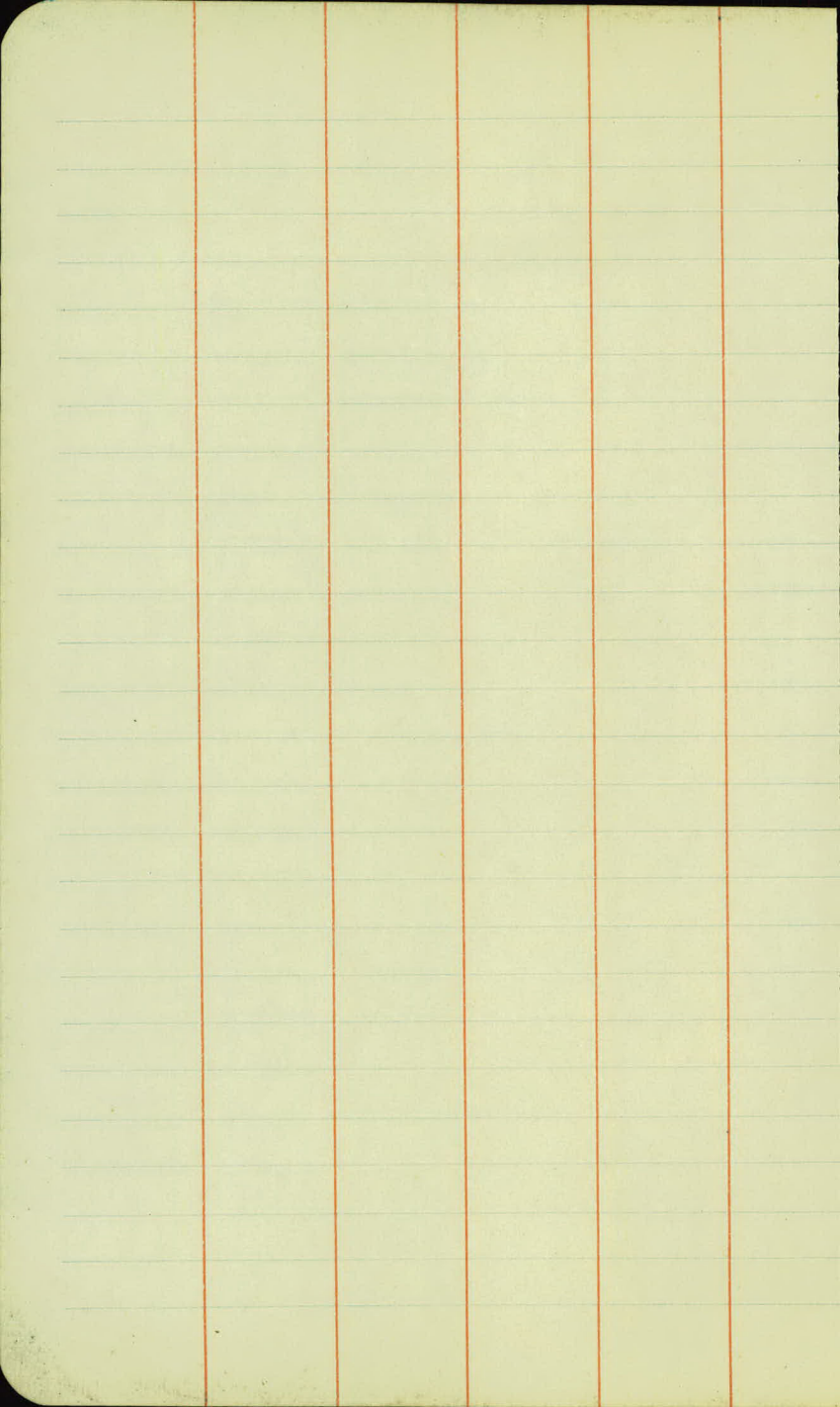
26.1 ✓

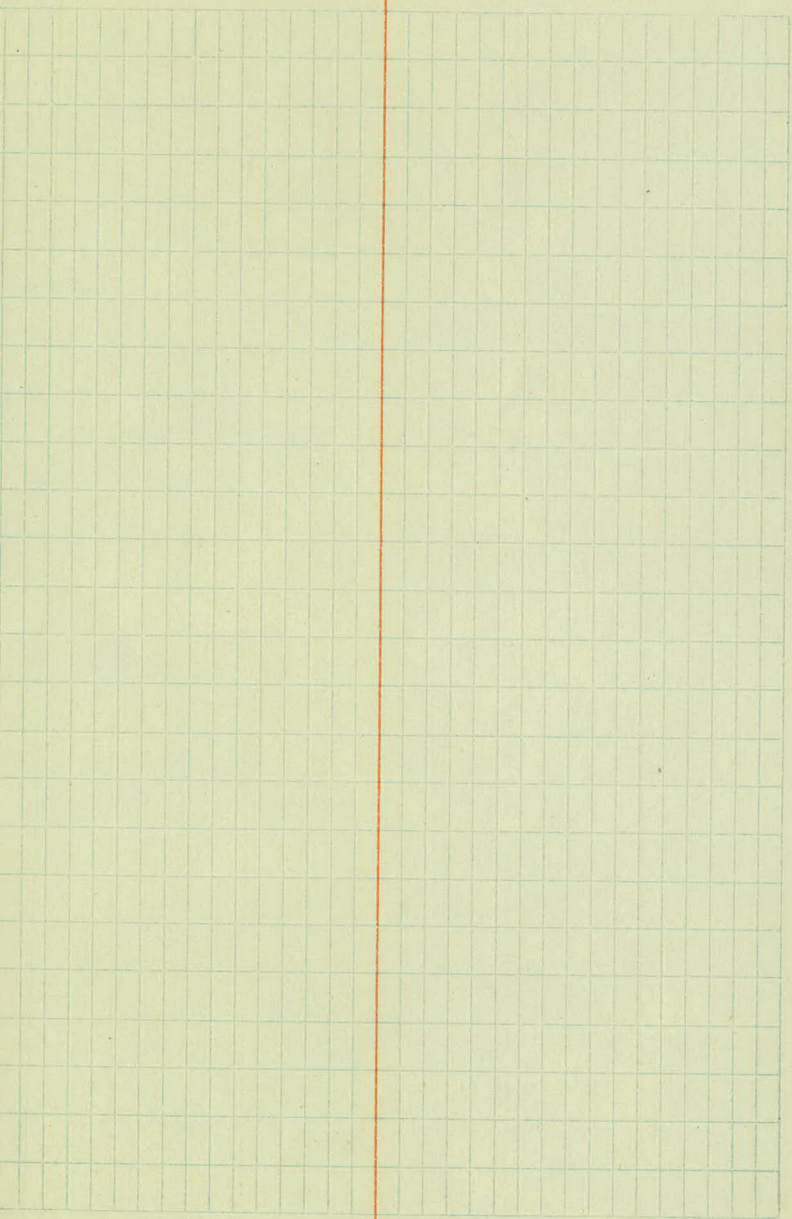
SEE PAGE 56

<u>44</u>	<u>46</u>	<u>72</u>	<u>75</u>	<u>51</u>		<u>50</u>	<u>68</u>	<u>74</u>	<u>58</u>	<u>56</u>
50	57	32	26	20	49	19	25	30	34	50

<u>47</u>	<u>47</u>	<u>72</u>	<u>74</u>	<u>55</u>		<u>49</u>	<u>69</u>	<u>75</u>	<u>55</u>	<u>56</u>
50	57	31	25	20	50	20	24	31	35	50

<u>46</u>	<u>48</u>	<u>72</u>	<u>74</u>	<u>55</u>		<u>49</u>	<u>68</u>	<u>73</u>	<u>52</u>	<u>53</u>
50	57	32	24	20	48	20	24	31	25	50





13. MI. 1.12 902.87 ✓ 901.75  
207.50 95.55 119 73'

210 95.5 123 74'

+50 95.43 127 74'

211 95.4 ✓ 131 75'

4.35 297.96 9.26 293.61

+50 95.35 86 26'

212 95.3 90 27'

+50 95.25 94 27.9'

213 95.2 98 28'

+50 95.15 102 28.1'

214 95.1 106 29.1'

+50 95.05 110 29.1'

215 95.0 ✓ 109 30.10'

5.13 898.39 4.70 893.26 ✓

10-16-29

(7.3)

78 5/80 7/74 75 81 80 95 77 72 78 27 102 5/108 70 8/98 75  
73 3/57 2/21 81 16 12 11 10 70 1 11 15 24 2/30 28 5/12.1 45

(7.4)

113 6/114 5/114 131 11 94 22 24 79 84 71 70 112 5/119 4/116 115  
43 3/109 2/40 86 18 15 10 9 -0.5 10 13 15 19 5/45 3/107 43

(7.4)

116 4/117 6/123 120 123 112 95 87 8.2 74 92 75 113 116 7/115 105 8/103 103  
73 3/110 2/49 88 26 18 14 8 -0.2 11 12 16 19 26 2/41 30 3/135 41

(7.5)

5 7/104 105 5/110 123 109 99 96 28 88 84 89 87 94 72 113 3/109 96 8/90 90  
2/27 67 3/33 24 17 15 12 11 9 -0.9 10 11 13 16 20 2/34 24 4/111 43

(7.6)

57 7/58 56 7/62 25 69 54 43 42 3.8 44 53 4 65 72 9/69 52 4/48 47  
43 3/72 28 2/36 25 20 18 10 9 -1.2 11 14 16 18 23 2/32 27 4/138 45

(7.7)

89 8/86 6/86 7/83 81 58 50 49 45 49 54 54 21 75 5/67 7/67 1/65 63  
43 4/74 3/104 3/56 24 12 10 9 -1.8 11 13 16 21 26 2/40 3/123 4/127 43

(7.7)

89 3/89 7/91 3/91 88 92 81 70 66 56 50 54 54 62 64 75 80 28 21 3/21 2/25 6/22 20  
4/105 3/109 3/64 28 27 17 17 14 11 -2.9 10 12 15 16 19 22 27 29/54 2/114 1/116 43

(7.8)

6 6/92 4/92 3/91 94 86 69 65 59 5.5 59 67 81 88 78 4 8/81 1/87 6.7  
4/106 3/106 3/23 28 17 15 16 10 -2.7 11 13 20 22 3/56 5/110 4/111 73

(7.8)

92 0/72 0/92 3/91 94 28 75 69 63 5.7 61 69 87 71 84 3/87 1/82 0/92 72  
3/110 3/110 3/28 27 20 18 13 11 12.9 10 12 18 27 28 3/57 3/110 4/110 43

(7.9)

94 2/74 5/91 7/91 23 28 78 21 61 59 63 70 74 85 92 1/87 5/91 0/90 91  
43 4/112 3/115 3/102 28 20 17 13 10 -3.0 10 12 14 16 26 3/58 3/115 4/116 43

(7.9)

83 7/83 6/76 3/88 25 22 71 61 53 62 71 90 1/88 3/92 0/90 91  
45 2/127 3/134 2/49 27 19 13 10 -2.9 10 12 20 3/59 3/118 4/120 43

(3.0)

93 192 0/89 9/92 73 87 74 69 62 56 59 66 78 89 97 72 87 5/85 6/85 8/88 88  
43 4/117 3/120 3/62 28 21 16 13 10 -2.6 10 12 17 23 25 28 29 3/55 3/124 3/121 43

898.39 ✓

750

95.1

107 33'

216

95.1 ✓

101 33'

B.M.

5.13

293.26

293.21

SEE PAGE 46.

(33)

$\begin{array}{r} 93 \\ 43 \end{array} \begin{array}{l} 4/93 \\ 4/714 \end{array} \begin{array}{l} 4/21 \\ 5/114 \end{array} \begin{array}{l} 1/96 \\ 3/263 \end{array} \begin{array}{l} 96 \\ 27 \end{array} \begin{array}{l} 27 \\ 21 \end{array} \begin{array}{l} 67 \\ 16 \end{array} \begin{array}{l} 61 \\ 10 \end{array} \begin{array}{l} 57 \\ 24 \end{array} \begin{array}{l} 61 \\ 10 \end{array} \begin{array}{l} 67 \\ 12 \end{array} \begin{array}{l} 77 \\ 17 \end{array} \begin{array}{l} 93 \\ 24 \end{array} \begin{array}{l} 103 \\ 26 \end{array} \begin{array}{l} 102 \\ 28 \end{array} \begin{array}{l} 27 \\ 30 \end{array} \begin{array}{l} 5/98 \\ 3/55 \end{array} \begin{array}{l} 1/68 \\ 3/214 \end{array} \begin{array}{l} 8/2 \\ 1/18 \end{array} \begin{array}{l} 92 \\ 43 \end{array}$

(33)

$\begin{array}{r} 92 \\ 13 \end{array} \begin{array}{l} 1/91 \\ 4/110 \end{array} \begin{array}{l} 1/2 \\ 3/109 \end{array} \begin{array}{l} 9/90 \\ 3/57 \end{array} \begin{array}{l} 90 \\ 30 \end{array} \begin{array}{l} 88 \\ 21 \end{array} \begin{array}{l} 65 \\ 15 \end{array} \begin{array}{l} 61 \\ 13 \end{array} \begin{array}{l} 54 \\ 10 \end{array} \begin{array}{l} 52 \\ 19 \end{array} \begin{array}{l} 56 \\ 10 \end{array} \begin{array}{l} 70 \\ 13 \end{array} \begin{array}{l} 87 \\ 24 \end{array} \begin{array}{l} 91 \\ 25 \end{array} \begin{array}{l} 97 \\ 27 \end{array} \begin{array}{l} 0 \\ 3 \end{array} \begin{array}{l} 1/20 \\ -5.5 \end{array} \begin{array}{l} 6/23 \\ 3/244 \end{array} \begin{array}{l} 9/58 \\ 1/19 \end{array} \begin{array}{l} 28 \\ 43 \end{array}$

B.M1	1.19	909.04		906.85	
	2.06	899.12	11.98	897.06	
202				972	115 19.
+50				967	106 2.2.
203				965	103 26.
+50				963	101 22.
204				961	98 30.
+50				961	96 30.
	5.83	900.63	4.32	894.80	
205				960	108 44.
+50				960	46.
206				959	47.
+50				958.5	48.
	7.38	903.00	5.01	895.62	
207				958	72.



903.00 ✓

f50

95.75

73

208

95.7

73

f50

95.65

7.4

207

95.4 ✓

7.4

B.M.

1.25

901.75

901.75

SEE PAGE 60.

(73)

$\frac{2.6}{43}$	$\frac{4/25}{3/748}$	$\frac{2.6}{37}$	$\frac{61}{27}$	$\frac{70}{19}$	$\frac{76}{14}$	$\frac{76}{11}$	$\frac{74}{0.1}$	$\frac{78}{12}$	$\frac{97.5}{1.02}$	$\frac{5.5}{30}$	$\frac{6/5.8}{3/714}$	$\frac{6.0}{43}$
------------------	----------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	-----------------	---------------------	------------------	-----------------------	------------------

(73)

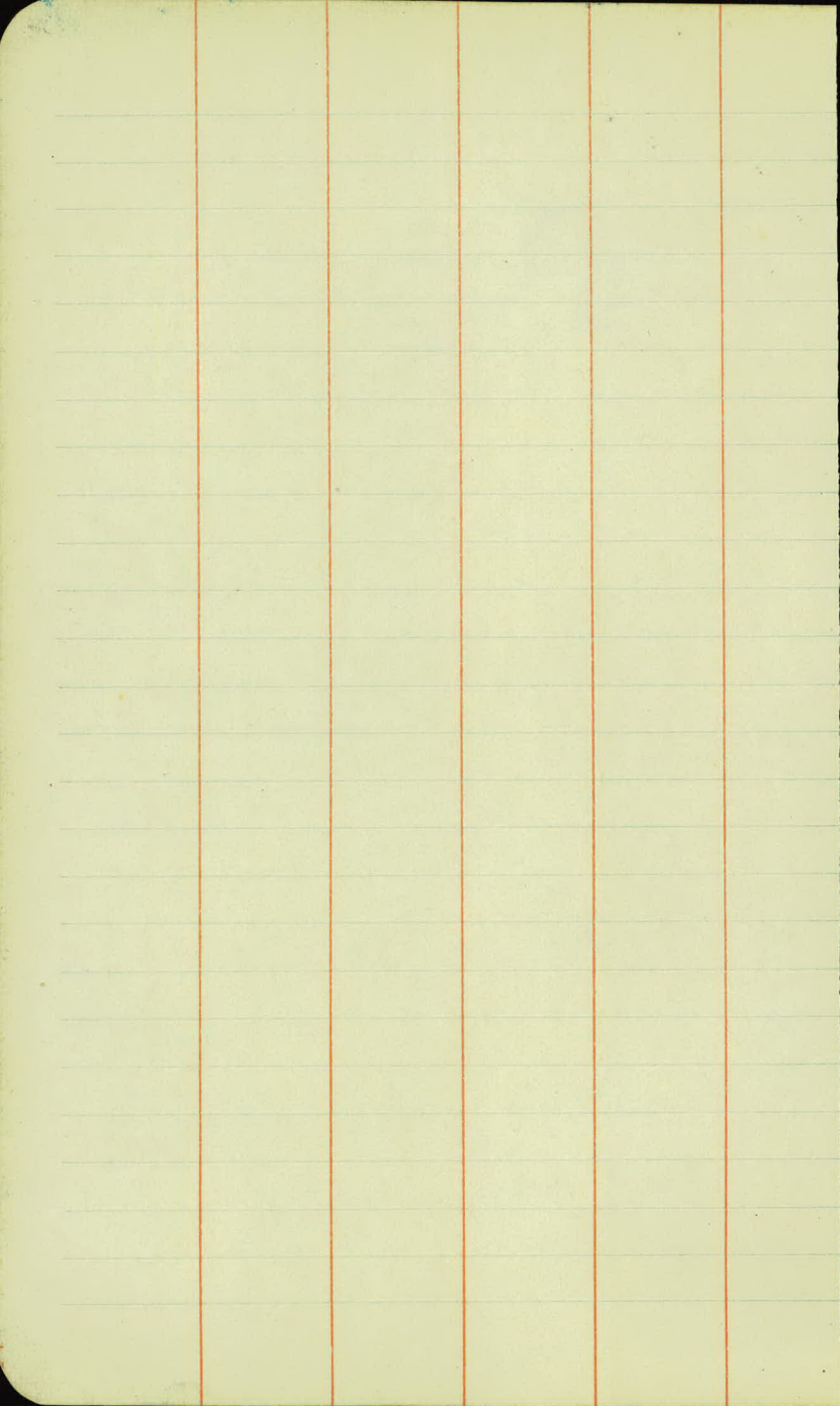
$\frac{3.0}{43}$	$\frac{8/29}{3/44}$	$\frac{3.0}{35}$	$\frac{53}{29}$	$\frac{72}{19}$	$\frac{7.5}{11}$	$\frac{72}{101}$	$\frac{76}{14}$	$\frac{7.1}{19}$	$\frac{5.1}{25}$	$\frac{4.7}{333}$	$\frac{1/4.9}{126}$	$\frac{5.2}{43}$
------------------	---------------------	------------------	-----------------	-----------------	------------------	------------------	-----------------	------------------	------------------	-------------------	---------------------	------------------

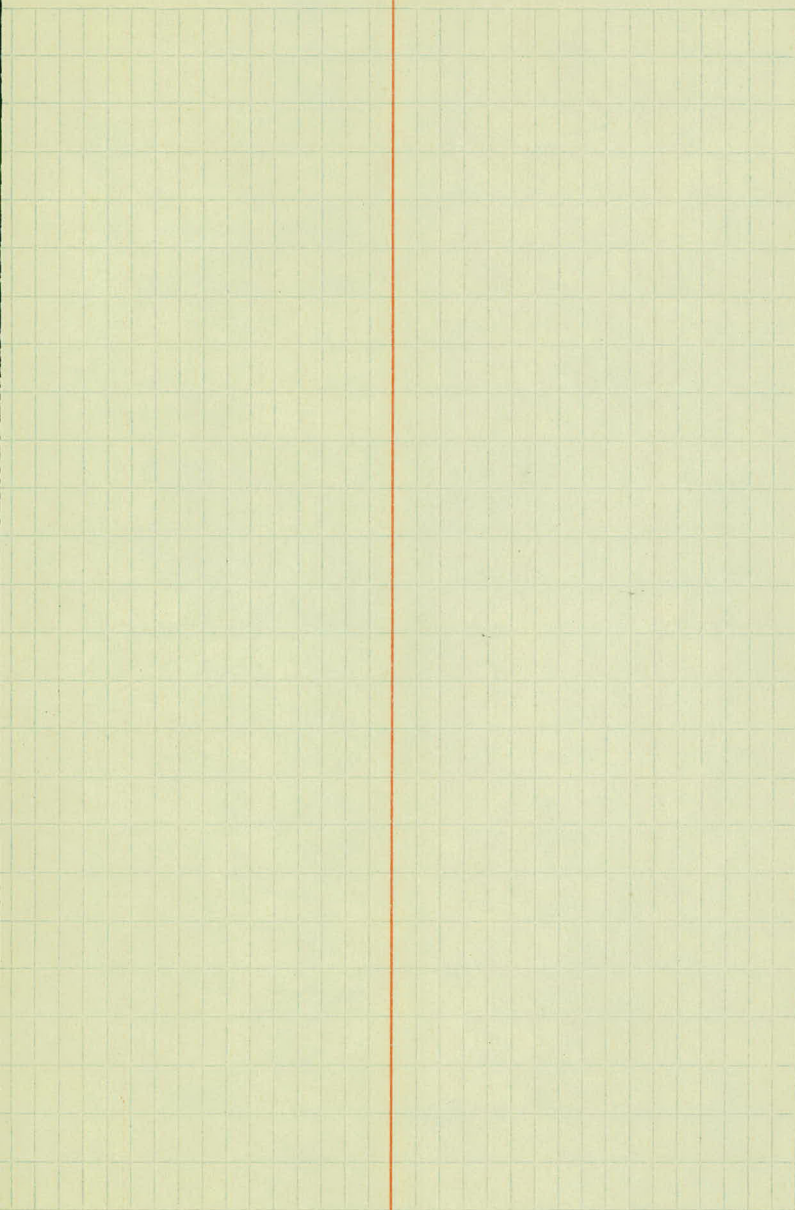
(74)

$\frac{4.5}{43}$	$\frac{1/48}{3/130}$	$\frac{4.4}{36}$	$\frac{6.5}{27}$	$\frac{7.0}{20}$	$\frac{7.5}{10}$	$\frac{7.2}{10.2}$	$\frac{7.5}{11}$	$\frac{7.1}{22}$	$\frac{4.4}{29}$	$\frac{6.2/46}{3/12.8}$	$\frac{5.3}{43}$
------------------	----------------------	------------------	------------------	------------------	------------------	--------------------	------------------	------------------	------------------	-------------------------	------------------

(74)

$\frac{6.3}{43}$	$\frac{1/64}{3/110}$	$\frac{5/74}{1.00}$	$\frac{7.2}{10}$	$\frac{7.5}{10.1}$	$\frac{7.6}{12}$	$\frac{7.6}{17}$	$\frac{7.0}{20}$	$\frac{6.7}{22}$	$\frac{5.9}{29}$	$\frac{4/5.9}{3/11.5}$	$\frac{6.5}{43}$
------------------	----------------------	---------------------	------------------	--------------------	------------------	------------------	------------------	------------------	------------------	------------------------	------------------





B.M. 4.48 932.25 927.77

0+33 27.8

0+50 27.7

1+75 27.6

1+00 27.6

1+50 27.3

2+00 26.5

B.M. 4.48 927.77

71+35<sup>4</sup> P.O.T.

LEFT.

RIGHT.

10-12-29

$\frac{3.6}{40}$	$\frac{2.0}{33}$	$\frac{1.9}{20}$	$\frac{4.8}{13}$	45	$\frac{5.3}{19}$	$\frac{3.5}{24}$	$\frac{4.3}{35}$
------------------	------------------	------------------	------------------	----	------------------	------------------	------------------

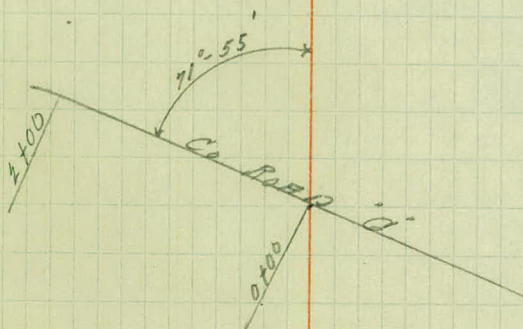
$\frac{2.8}{40}$	$\frac{1.4}{33}$	$\frac{1.9}{19}$	$\frac{5.2}{13}$	46	$\frac{5.6}{18}$	$\frac{5.5}{20}$	$\frac{3.4}{25}$	$\frac{4.1}{33}$	$\frac{4.2}{40}$
------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{3.6}{40}$	$\frac{2.1}{33}$	$\frac{2.2}{20}$	$\frac{5.3}{15}$	$\frac{5.3}{12}$	47	$\frac{5.9}{17}$	$\frac{3.8}{24}$	$\frac{4.0}{33}$	$\frac{3.8}{40}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------

$\frac{3.7}{40}$	$\frac{3.5}{33}$	$\frac{2.9}{19}$	$\frac{5.1}{13}$	47	$\frac{5.4}{17}$	$\frac{3.1}{23}$	$\frac{3.4}{33}$	$\frac{3.1}{40}$
------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------

$\frac{4.9}{40}$	$\frac{4.7}{33}$	$\frac{4.2}{24}$	$\frac{3.4}{18}$	$\frac{5.2}{15}$	$\frac{5.6}{13}$	50	$\frac{5.5}{14}$	$\frac{5.3}{15}$	$\frac{4.9}{18}$	$\frac{3.4}{21}$	$\frac{2.9}{25}$	$\frac{3.5}{33}$	$\frac{2.5}{40}$
------------------	------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.6}{40}$	$\frac{5.3}{33}$	$\frac{4.8}{24}$	$\frac{4.4}{18}$	$\frac{6.1}{15}$	$\frac{6.4}{12}$	58	$\frac{6.5}{12}$	$\frac{6.1}{13}$	$\frac{5.5}{17}$	$\frac{3.8}{21}$	$\frac{4.3}{33}$	$\frac{4.5}{40}$
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121		+1.40	-1.40	21.6	✓
	+50	+1.40	-1.40	21.55	✓
122		"	"	21.5	✓
	+50	"	"	21.5	
123		"	"	21.4	
	+50	"	"	21.4	
124		"	"	21.3	
	+50	"	"	21.3	
125		"	"	21.3	
	+50	"	"	21.4	✓
126		+1.40	-1.40	21.5	✓
	+50	+1.37	-1.37	21.65	✓
127		+1.17	-1.17	21.80	✓
	+50	+0.80	-0.80	21.95	✓
128		+0.40	-0.40	22.1	✓
	+50	+0.05	-0.05	22.25	✓
129				22.4	✓
	+50			22.55	✓
130				22.7	✓
	+50			22.85	✓
131				23.0	✓
	+50			23.15	✓
132				23.3	✓
	+50			23.45	✓
133				23.6	✓

	150	23.75	✓
134	-	23.9	✓
	150	24.05	✓
135		24.2	✓
	150	24.35	✓
136		24.5	✓
	150	24.65	✓
137		24.8	✓
	150	24.95	✓
138		25.1	✓
	150	25.25	✓
139		25.4	✓
	150	25.55	✓
140		25.7	✓
	150	25.85	✓
141		26.0	✓
	150	26.15	✓
142		26.3	✓
	150	26.45	✓
143		26.6	✓
	150	26.7	✓
144		26.8	✓
	150	27.0	✓
145		27.0	✓
	150	27.05	✓

146		27.1	✓
750		27.15	✓
147		27.2	✓
750		27.25	-
148		27.3	✓
750		27.4	✓
149		27.4	✓
750		27.45	✓
150		27.5	-
750		27.55	✓
151		27.6	✓
750		27.4	✓
152		27.2	✓
750	927.58 T.P.L.T. STA 158760.	26.8	✓
153		26.3	✓
750		25.7	✓
154		25.0	✓
750		24.1	✓
155		23.1	✓
750		22.1	✓
156		20.9	✓
750		19.8	✓
157		18.6	✓
750		17.5	✓
158		16.3	✓

159	750	15.2	✓
	750	14.1	✓
160	750	13.2	✓
	750	12.4	✓
161	750	11.8	✓
	750	11.3	✓
162	750	11.0	✓
	750	10.7	✓
163	750	10.45	✓
	750	10.2	✓
164	750	09.95	✓
	750	09.7	✓
165	750	09.45	✓
	750	09.2	✓
166	750	08.95	✓
	750	08.7	✓
167	750	08.45	✓
	750	08.2	✓
168	750	07.95	✓
	750	07.7	✓
169	750	07.6	✓
	750	07.5	✓
170	750	07.4	✓
	750	07.7	✓
	750	07.8	✓

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172		08.4	✓
	+50	08.6	✓
173		08.8	✓
	+50	09.0	✓
174		09.2	✓
	+50	09.4	✓
175		09.6	✓
	+50	09.8	✓
176		10.0	✓
	+50	10.2	
177		10.4	✓
	+50	10.6	✓
178		10.8	✓
	+50	11.0	✓
179		11.2	✓
	+50	11.4	✓
180		11.5	✓
	+50	11.6	✓
181		11.6	✓
	+50	11.6	✓
182		11.5	✓
	+50	11.4	✓
183		11.2	✓

	f50	11.0	
184		10.7	
	f50	10.4	
185		10.2	✓
	f50	10.0	✓
186		09.7	-
	f50	09.5	✓
187		09.2	-
	f50	09.0	✓
188		08.7	✓
	f50	08.5	2
189		08.2	✓
	f50	08.0	✓
190		07.7	✓
	f50	07.5	✓
191		07.2	✓
	f50	06.95	✓ X
192		06.61	✓
	f50	06.26	✓
193		05.86	✓
	f50	05.42	✓
194		04.95	✓
	f50	04.45	✓
195		03.95	✓
	f50	03.45	✓

196		02.95	✓
	+50	02.45	✓
197		01.95	✓
	+50	01.45	✓
198		00.95	✓
	+50	00.40	✓
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	+50	99.30	✓
200		98.75	✓
	+50	98.20	✓
201		97.65	✓
	+50	97.10	✓
202		96.75	✓
	+50	96.40	✓
203		96.15	✓
	+50	95.95	✓
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205		95.75	✓
	+50	95.70	✓
206		95.65	✓
	+50	95.60	✓
207		95.55	✓
	+50	95.50	✓
208		95.45	✓

	+50	95.40	✓
209		95.35	✓
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	+50	95.2	✓
211		95.15	✓
	+50	95.10	✓
212		95.05	✓
	+50	95.00	✓
213		94.95	✓
	+50	94.9	✓
214		94.85	✓
	+50	94.80	✓
215		94.75	✓
	+50	94.70	✓
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	+50	94.74	✓
217		94.85	✓
	+50	95.05	✓
218		95.30	✓
	+50	95.62	✓
219		96.03	✓
	+50	96.5	✓
220		97.00	✓
	+50	97.50	✓

221		98.0	✓
	+50	98.35	✓
222		98.90	✓
	+50	99.30	✓
223		99.70	✓
	+50	00.10	✓
224		00.50	✓
	+50	00.90	✓
225		01.30	✓
	+50	01.7	✓
226		02.1	✓
	+50	02.4	✓
227		02.7	✓
	+50	03.0	✓
228		03.25	✓
	+50	03.50	✓
229		03.7	✓
	+50	03.8	✓
230		03.9	✓
	+50	03.9	✓
231		03.85	✓
	+50	03.8	✓
232		03.75	✓
	+50	03.7	✓
233		03.65	✓
	+50	03.60	✓

234				03.55	✓
	+50			03.50	✓
235				03.45	✓
	+50			03.4	✓
236				03.35	✓
	+50			03.35	✓
237				03.35	✓
	+50			03.38	✓
238				03.45	✓
	+50			03.55	✓
239				03.65	✓
	+50			03.75	✓
240				03.85	✓
	+50			03.95	✓
241				04.05	
	+50			04.15	
242				04.25	
	+50			04.30	
243				04.45	
	+50			04.55	
244				04.65	
12		0.00	0.00	18.4	
	+50	+0.20	-0.20	18.2	✓
13		+0.51	-0.51	18.0	
	+50	+1.00	-1.00	17.8	✓

14		+1.30	-1.30	17.6	✓
	-50	+1.40	-1.40	17.4	✓
15		+1.40	-1.40	17.2	✓
	+50	"	"	17.0	✓
16		"	"	16.7	✓
	+50	"	"	16.4	✓
17		"	"	16.4	✓
	+50	"	"	16.4	✓
18		"	"	16.6	✓
	+50	"	"	16.9	✓
19		+1.40	-1.40	17.2	✓
	+50	+1.37	-1.37	17.5	✓
20		+1.07	-1.07	17.9	✓
	+50	+0.80	-0.80	18.3	✓
21		+0.40	-0.40	18.6	✓
	+50	+0.05	-0.05	18.9	✓
22				19.3	✓
	+50			19.7	✓
23				20.0	✓
	+50			20.3	✓
24				20.4	✓
	+50			20.8	✓
25				21.1	✓
	+50			21.2	✓
26				21.4	✓

-	+50	21.5	✓
27		21.6	✓
	+50	21.65	✓
28		21.7	✓
	+50	21.75	✓
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30		21.9	✓
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	+50	22.15	✓
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	+50	22.25	✓
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	+50	22.35	✓
35		22.4	✓
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	+50	22.55	✓
37		22.6	✓
	+50	22.65	✓
38		22.7	✓
	+50	22.75	✓

39		22.8	✓
	+50	22.85	✓
40		22.9	✓
	+50	22.95	✓
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	+50	23.05	✓
42		23.1	✓
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	+50	23.35	
45		23.4	
	+50	23.45	
46		23.5	
	+50	23.55	✓
47		23.6	✓
	+50	23.65	✓
48		23.7	✓
	+50	23.75	✓
49		23.8	✓
	+50	23.85	✓
50		23.9	✓
	+50	24.0	✓
51		24.05	✓

	150	24.12	✓
52		24.3	✓
	150	24.45	✓
53		24.6	✓
	150	24.75	✓
54		24.9	✓
	150	25.05	✓
55		25.2	✓
	150	25.35	✓
56		25.5	✓
	150	25.61	✓
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	150	25.8	✓
58		25.9	✓
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59		26.1	✓
	150	26.2	✓
60		26.3	✓
	150	26.4	✓
61		26.5	✓
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62		26.7	✓
	150	26.8	✓
63		26.9	✓
	150	27.0	✓

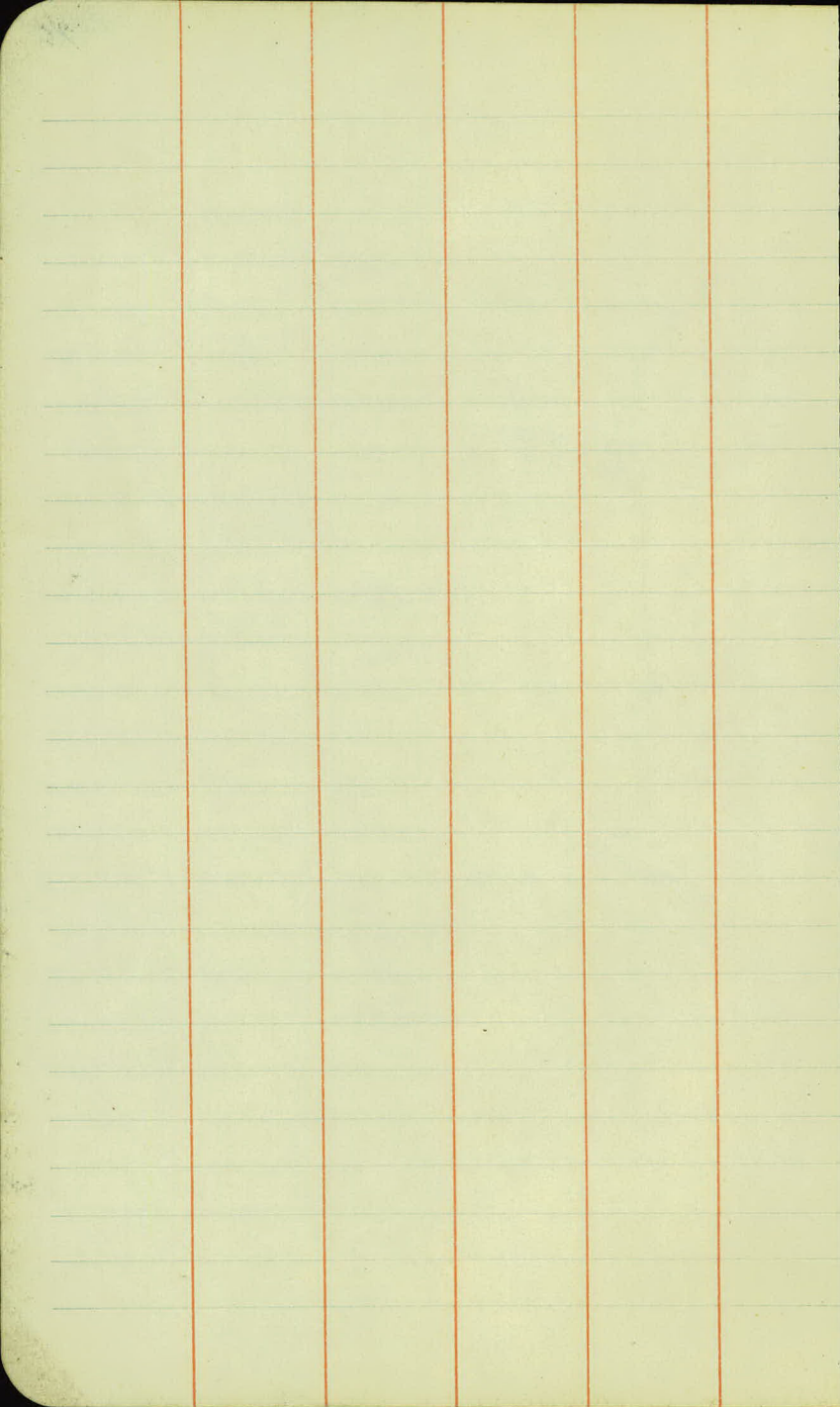
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	+50	274	✓
66		275	✓
	+50	276	✓
67		277	✓
	+50	278	✓
68		279	✓
	+50	280	✓
69		281	✓
	+50	282	✓
70		283	✓
	+50	284	✓
71		285	✓
	+50	286	✓
72		287	✓
	+50	28.75	✓
73		28.8	✓
	+50	28.85	✓
74		28.9	✓
	+50	28.95	✓
75		29.0	✓
	+50	29.05	✓
76		29.10	✓

	150			29.15	✓
77				29.2	✓
	150			29.25	✓
78				29.3	✓
	150			29.35	✓
79				29.40	✓
	150			29.30	✓
80				29.2	✓
	150			29.0	✓
81				28.7	✓
	150			28.3	✓
82				27.9	✓
	150			27.5	✓
83				27.1	✓
	150	-0.30	+0.30	26.7	✓
84		-0.52	+0.52	26.3	✓
	150	-0.57	+0.57	26.0	✓
85		-0.57	+0.57	25.7	✓
	150	-0.50	+0.50	25.4	✓
86		-0.30	+0.30	25.2	✓
	150			25.0	✓
87				24.8	✓
	150			24.7	✓
88				24.6	✓
	150			24.6	✓

89				24.6	✓
	+50			24.6	✓
90				24.7	✓
	+50			24.75	✓
91				24.8	✓
	+50			24.85	✓
92				24.9	✓
	+50			24.95	✓
93				25.0	✓
	+50			25.05	✓
94				25.1	✓
	+50			25.15	✓
95		-0.00	+0.00	25.2	✓
	+50	-0.05	+0.05	25.25	✓
96		-0.40	+0.40	25.3	✓
	+50	-0.80	+0.80	25.35	✓
97		-1.17	+1.17	25.4	✓
	+50	-1.37	+1.37	25.45	✓
98		-1.40	+1.40	25.5	✓
	+50	-1.40	+1.40	25.55	✓
99		-1.40	+1.40	25.6	✓
	+50	-1.40	+1.40	25.65	✓
100		-1.40	+1.40	25.7	✓
	+50	-1.35	+1.35	25.75	✓
101		-1.16	+1.16	25.8	✓

117				22.0	
	+50	+0.20	-0.20	21.95	✓
118		+0.60	-0.60	21.9	✓
	+50	+0.96	-0.96	21.85	✓
119		+1.27	-1.27	21.8	✓
	+50	+1.35	-1.35	21.75	✓
120		+1.40	-1.40	21.7	✓
	+50	+1.40	-1.40	21.65	✓
121					

101+50		-0.80	+0.80	25.85	✓
102		-0.40	+0.40	25.9	✓
	+50	-0.05	-0.05	25.95	✓
103		0.00	0.00	26.0	



The image shows a page of graph paper with a grid of small squares. A vertical red line runs down the center of the page, dividing the grid into two equal halves. The grid consists of 20 columns and 30 rows of squares. The paper is off-white and shows signs of age.

B.M.	5.00	931.06		926.06
B.M.			3.74	927.32
B.M.	6.15	922.49		916.34
B.M.			6.44	916.05
B.M.	3.53	910.38		906.85
B.M.			4.27	906.11
B.M.	6.75	899.96		893.21
B.M.			3.23	896.73
B.M.	4.62	908.75		904.13
B.M.			4.48	904.27 ✓
B.M.	3.65	909.49		905.84
B.M.			5.14	904.35

SPX IN 12" CARK 60 LT STA 145+05.

SPX IN 12" CARK 60 LT STA 159+30

SPX IN 10" CARK 50 117 STA 195+80

SPX IN PP 100 LT STA. 218+60.

SPX IN 18" TREE 60 LT STA. 227+20.

SPX IN T.P. 70 197 STA. 242+25.

STA	<sup>LT</sup> ELEV	<sup>RT</sup> ELEV	
87+00	$\frac{9218}{28.5}$	$\frac{9198}{25.5}$	24" X 54 P <sup>3</sup>
88+50	$\frac{9145}{33}$	$\frac{9174}{33}$	24" X 66 P <sup>3</sup>
168+00	$\frac{9026}{29}$	$\frac{9015}{31}$	24" X 60 P <sup>3</sup>
202+28	$\frac{880}{36}$	$\frac{884}{36}$	24" X 72 P <sup>3</sup>
214+60	$\frac{863}{36}$	$\frac{866}{30}$	24" X 72 P <sup>3</sup>
239+60	$\frac{951}{30}$	$\frac{955}{30}$	24" X 60 P <sup>3</sup>

# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or L. P.= $23^{\circ} 20'$  to the R. at Station  
 $542+72$ .

Ext. in Tab. IV opposite  $23^{\circ} 20'$ =120.87  
 $120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20'$ =1183.1  
 $1183.1 \div 10 = 118.31$ .

Tab. V, correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur.=0.16  
 $118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)  
Ang.  $23^{\circ} 20'$ = $23.33^{\circ} \div 10 = 2.3333$ =L. C.

$2^{\circ} 19\frac{1}{2}'$ =def. for sta.	542	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}'$ = " " "	+50	Tan.=	1.18.47
$7^{\circ} 19\frac{1}{2}'$ = " " "	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}'$ = " " "	+50	L. C.=	2.33.33
$11^{\circ} 40'$ = " " "	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3'$  (def. for 1 ft. of  $10^{\circ}$  Cur.) =  $139.41'$  =  
 $2^{\circ} 19\frac{1}{2}'$  = def. for sta. 542.

Def. for 50 ft. =  $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft. =  $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)

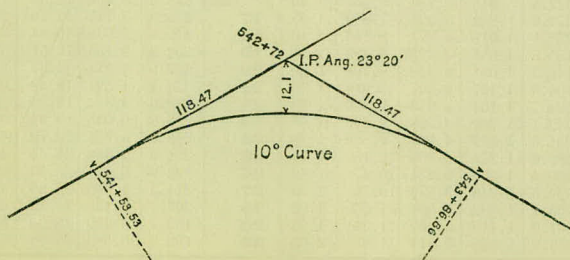


TABLE I. — Minutes in Decimals of a Degree.

<b>1'</b>	.0167	<b>11'</b>	.1833	<b>21'</b>	.3500	<b>31'</b>	.5167	<b>41'</b>	.6833	<b>51'</b>	.8500
<b>2</b>	.0333	<b>12</b>	.2000	<b>22</b>	.3667	<b>32</b>	.5333	<b>42</b>	.7000	<b>52</b>	.8667
<b>3</b>	.0500	<b>13</b>	.2167	<b>23</b>	.3833	<b>33</b>	.5500	<b>43</b>	.7167	<b>53</b>	.8833
<b>4</b>	.0667	<b>14</b>	.2333	<b>24</b>	.4000	<b>34</b>	.5667	<b>44</b>	.7333	<b>54</b>	.9000
<b>5</b>	.0833	<b>15</b>	.2500	<b>25</b>	.4167	<b>35</b>	.5833	<b>45</b>	.7500	<b>55</b>	.9167
<b>6</b>	.1000	<b>16</b>	.2667	<b>26</b>	.4333	<b>36</b>	.6000	<b>46</b>	.7667	<b>56</b>	.9333
<b>7</b>	.1167	<b>17</b>	.2833	<b>27</b>	.4500	<b>37</b>	.6167	<b>47</b>	.7833	<b>57</b>	.9500
<b>8</b>	.1333	<b>18</b>	.3000	<b>28</b>	.4667	<b>38</b>	.6333	<b>48</b>	.8000	<b>58</b>	.9667
<b>9</b>	.1500	<b>19</b>	.3167	<b>29</b>	.4833	<b>39</b>	.6500	<b>49</b>	.8167	<b>59</b>	.9833
<b>10</b>	.1667	<b>20</b>	.3333	<b>30</b>	.5000	<b>40</b>	.6667	<b>50</b>	.8333	<b>60</b>	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	<sup>1</sup> / <sub>8</sub>	3-16	<sup>1</sup> / <sub>4</sub>	5-16	<sup>3</sup> / <sub>8</sub>	<sup>1</sup> / <sub>2</sub>	<sup>5</sup> / <sub>8</sub>	<sup>3</sup> / <sub>4</sub>	<sup>7</sup> / <sub>8</sub>
.0052	.0078	.0104	.0156	.0208	.0269	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
<b>0°</b>	34377.	.036	.145	.291	0.05'	<b>7°</b>	819.0	1.528	6.105	12.21	2.10'
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	<b>8</b>	716.8	1.746	6.976	13.95	2.40
<b>1</b>	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	<b>9</b>	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
<b>2</b>	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	<b>10</b>	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2292.0	.545	2.181	4.363	0.75	<b>11</b>	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	<b>12</b>	478.3	2.620	10.45	20.91	3.60
<b>3</b>	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	<b>13</b>	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	<b>14</b>	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	<b>15</b>	383.1	3.277	13.05	26.11	4.50
<b>4</b>	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	<b>16</b>	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.781	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	<b>17</b>	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	<b>18</b>	319.6	3.935	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	<b>19</b>	302.9	4.155	16.51	33.01	5.70
<b>5</b>	1146.3	1.091	4.362	8.724	1.50	<b>20</b>	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	<b>21</b>	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	<b>22</b>	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	<b>23</b>	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	<b>24</b>	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	<b>25</b>	231.0	5.476	21.64	43.28	7.50
<b>6</b>	955.4	1.309	5.234	10.47	1.80	<b>26</b>	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	<b>27</b>	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	<b>28</b>	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	<b>29</b>	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	<b>30</b>	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>1°</b>	50.00	.22	<b>11°</b>	551.70	26.50	<b>21°</b>	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
<b>2</b>	100.01	.87	<b>12</b>	602.21	31.56	<b>22</b>	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
<b>3</b>	150.04	1.96	<b>13</b>	652.81	37.07	<b>23</b>	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
<b>4</b>	200.08	3.49	<b>14</b>	703.51	43.03	<b>24</b>	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
<b>5</b>	250.16	5.46	<b>15</b>	754.32	49.44	<b>25</b>	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
<b>6</b>	300.28	7.86	<b>16</b>	805.25	56.31	<b>26</b>	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
<b>7</b>	350.44	10.71	<b>17</b>	856.30	63.63	<b>27</b>	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
<b>8</b>	400.66	13.99	<b>18</b>	907.49	71.42	<b>28</b>	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
<b>9</b>	450.93	17.72	<b>19</b>	958.81	79.67	<b>29</b>	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
<b>10</b>	501.28	21.89	<b>20</b>	1010.3	88.39	<b>30</b>	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>31°</b>	1589.0	216.3	<b>41°</b>	2142.2	387.4	<b>51°</b>	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
<b>32</b>	1643.0	230.9	<b>42</b>	2199.4	407.6	<b>52</b>	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
<b>33</b>	1697.2	246.1	<b>43</b>	2257.0	428.5	<b>53</b>	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
<b>34</b>	1751.7	261.8	<b>44</b>	2314.9	450.0	<b>54</b>	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
<b>35</b>	1806.6	278.1	<b>45</b>	2373.3	472.1	<b>55</b>	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.4	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
<b>36</b>	1861.7	294.9	<b>46</b>	2432.1	494.8	<b>56</b>	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
<b>37</b>	1917.1	312.2	<b>47</b>	2491.3	518.2	<b>57</b>	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
<b>38</b>	1972.9	330.2	<b>48</b>	2551.0	542.2	<b>58</b>	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
<b>39</b>	2029.0	348.6	<b>49</b>	2611.2	566.9	<b>59</b>	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
<b>40</b>	2085.4	367.7	<b>50</b>	2671.8	592.3	<b>60</b>	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>61°</b>	3375.0	920.2	<b>71°</b>	4086.9	1308.2	<b>81°</b>	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
<b>62</b>	3442.7	954.8	<b>72</b>	4162.8	1352.6	<b>82</b>	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
<b>63</b>	3511.1	990.2	<b>73</b>	4239.7	1398.0	<b>83</b>	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
<b>64</b>	3580.3	1026.6	<b>74</b>	4317.6	1444.6	<b>84</b>	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
<b>65</b>	3650.2	1063.9	<b>75</b>	4396.5	1492.4	<b>85</b>	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
<b>66</b>	3720.9	1102.2	<b>76</b>	4476.5	1541.4	<b>86</b>	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
<b>67</b>	3792.4	1141.4	<b>77</b>	4557.6	1591.6	<b>87</b>	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
<b>68</b>	3864.7	1181.6	<b>78</b>	4639.8	1643.0	<b>88</b>	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
<b>69</b>	3937.9	1222.7	<b>79</b>	4723.2	1695.8	<b>89</b>	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
<b>70</b>	4011.9	1265.0	<b>80</b>	4807.7	1749.9	<b>90</b>	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>91°</b>	5830.5	2444.9	<b>101°</b>	6950.6	3278.1	<b>111°</b>	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.2	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
<b>92</b>	5933.2	2518.5	<b>102</b>	7075.5	3374.9	<b>112</b>	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
<b>93</b>	6037.8	2594.0	<b>103</b>	7203.2	3474.4	<b>113</b>	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
<b>94</b>	6144.3	2671.6	<b>104</b>	7333.6	3576.8	<b>114</b>	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
<b>95</b>	6252.8	2751.3	<b>105</b>	7467.0	3682.3	<b>115</b>	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
<b>96</b>	6363.4	2833.2	<b>106</b>	7603.5	3791.0	<b>116</b>	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
<b>97</b>	6476.2	2917.3	<b>107</b>	7743.2	3902.9	<b>117</b>	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
<b>98</b>	6591.2	3003.8	<b>108</b>	7886.2	4018.2	<b>118</b>	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
<b>99</b>	6708.6	3092.7	<b>109</b>	8032.7	4137.1	<b>119</b>	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
<b>100</b>	6828.3	3184.1	<b>110</b>	8182.8	4259.7	<b>120</b>	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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		For Tangents Add													
ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
		10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68	
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90	
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14	
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39	
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66	
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94	
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21	
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48	
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77	
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07	
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39	
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72	
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09	
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46	
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89	
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32	
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.49	4.98	5.38	5.83	
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34	

## For Externals Add

ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020	
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083	
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135	
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188	
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264	
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341	
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445	
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550	
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700	
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851	
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01	
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17	
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.897	.997	1.07	1.18	1.29	
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62	
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91	
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20	
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58	
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96	

# VIII

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

## CURVE FORMULAS.

$$T = R \tan \frac{1}{2} I$$

$$T = \frac{50 \tan \frac{1}{2} I}{\sin. D}$$

$$\sin. D = \frac{50}{R}$$

$$\sin. D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{50}{\sin. D}$$

$$E = R \text{ ex. sec. } \frac{1}{2} I$$

$$E = T \tan \frac{1}{4} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{\frac{1}{2} I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.— Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

Natural Sines

DEG.	0'	10'	20'	30'	40'	50'	DEG.	DEG.	0'	10'	20'	30'	40'	50'	DEG.
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1276	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	DEG.	60'	50'	40'	30'	20'	10'	DEG.

DEG.	0'	10'	20'	30'	40'	50'	DEG.
80	9848	9853	9858	9863	9868	9872	9
81	9877	9881	9886	9890	9894	9899	8
82	9903	9907	9911	9914	9918	9922	7
83	9925	9929	9932	9936	9939	9942	6
84	9945	9948	9951	9954	9957	9959	5
85	9962	9964	9967	9969	9971	9974	4
86	9976	9978	9980	9981	9983	9985	3
87	9986	9988	9989	9990	9992	9993	2
88	9994	9995	9996	9997	9997	9998	1
89	9998	9999	9999	9999	I.0000	I.0000	0
DEG.	60'	50'	40'	30'	20'	10'	DEG.

Natural Cosines

Natural Tangents

DEG.	0'	10'	20'	30'	40'	50'	DEG.	0'	10'	20'	30'	40'	50'	DEG.	
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8667	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	60'	50'	40'	30'	20'	10'	DEG.	
DEG.	0'	10'	20'	30'	40'	50'	DEG.	0'	10'	20'	30'	40'	50'	DEG.	
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9								
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8								
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7								
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6								
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5								
85	11.430	11.826	12.250	12.706	13.197	13.727	4								
86	14.300	14.924	15.605	16.350	17.169	18.075	3								
87	19.081	20.206	21.470	22.903	24.542	26.432	2								
88	28.636	31.242	34.368	38.189	42.964	49.104	1								
89	57.290	68.750	85.940	114.588	171.885	343.77	0								
DEG.	60'	50'	40'	30'	20'	10'	DEG.								

Natural Cotangents

1584  
296

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 $\frac{1}{2}$  TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

U 2512