

PLANS SURVEY

COUNTY RD. "J"
OR
NORTH CO. LINE

From Turtle Lake Rd. to Centerville Rd.

RAMSEY COUNTY PROJ. 27-63

Road a/c N°63

File N°12

2863

2-11-27

12

PROJ. 28-63

Alignment.

North County Line
From Turtle Lake Road
to Centerville Road.
From 0+00 to 113+52.46

Checked 2-11-27
C. J. [unclear]
[unclear]

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

2-11-27

12

Sta. Point A-Lt. A-Rt. Calculated Magnetic Bearing Bear.

453.33 P.T. ✓ 45° 40'
 4+00 40° 00'
 +50 35° 00'
 3+00 30° 00'
 02+91.3 P.I. 90° 40'
 +50 75° 00'
 2+00 70° 00'
 +50 15° 00'
 1+00 10° 00'
 +50 5° 00'
 0+00 P.C. ✓ 0° 00'

589° 26' E

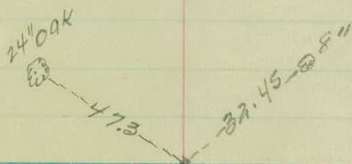
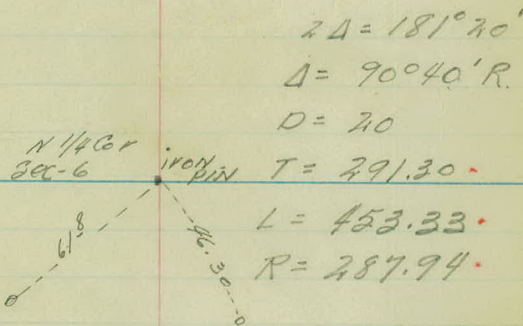
N 00° 06' W

110+83.4 P.O.T. Austin's Survey

1-21-27

H.I. Wistosen = Cold
D.S
A.B
A.M

ANOKA CO.
RAMSEY CO.



Sta Point Δ-Lt. Δ-Rt Cal. Bear Mag. Bear.

37464⁶⁰ P.O.T.

589°47'E

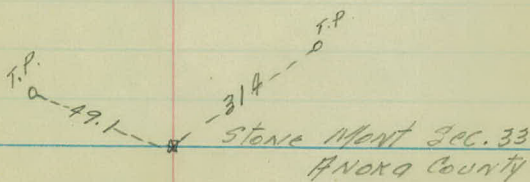
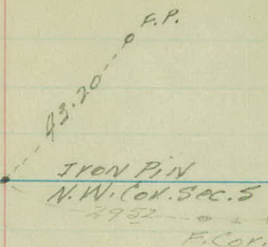
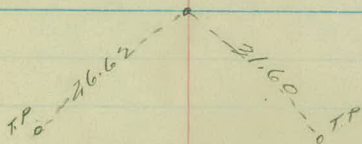
78401¹⁹ P.E. 0°21'

589°26'E

16402⁰ P.O.T.

1-21-24-27

(H.H. Whistson Cold
D.S.
A.B.
A.M.)



Sta.	Point	A-L	A-R	cal. Bear.	Mag. Bear.
70+39.69	P.T. ✓	45°34'30"			
70+00		41°36'			
+50		36°36'			
69+00		31°36'			
68+77.70	P.T.	91°09'			
+50		26°36'			
68+00		21°36'			
+50		16°36'			
67+00		11°36'			
+50		6°36'			
66+00		1°36'			
65+83.94	P.C. ✓	0-00'			
54+42.40	P.O.T.				
52+46.80	P.O.T.				


✓
N 95° 0' W

✓
E 47° 5' S

1-25-27

H.L. Wislhusen (Cold)
D. 3
A. B
A.M.
P. B.

$\angle A = 182^{\circ} - 18'$
 $A = 91^{\circ} - 09' \text{ Lt.}$
 $D = 70^{\circ}$
 $T = 293.76$
 $L = 455.75$
 $R = 287.94$

12"  51.35 67.40 T.P.

N. 1/4 Cor. Sec. 5
 Estab 2640' E. from
 iron pin N.W. Cor
 Sec. 5 running E to
 N 1/4 Cor Sec. 4
 P. R. BANISTER

41.15 F.P.
 46.10 F.P.

Sta. Point Δ = Lt. Δ = Rt. Cal. Mag. Bear. Bear.

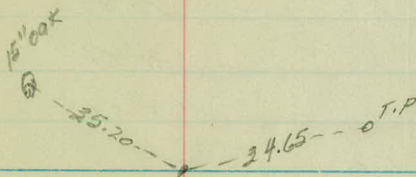
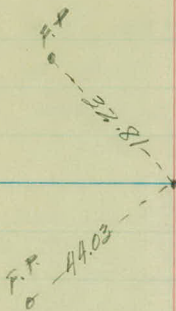
97+00 P.O.T.

7,750.685

82+44.59	P.T. ✓	45°-31'
82+00		41°-04'
+50		36°-04'
81+00		31°-04'
80+87.48	P.T.	91°-04'
+50		26°-04'
80+00		21°-04'
+50		16°-04'
79+00		11°-04'
+50		6°-04'
78+00		1°-04'
77+89.33	P.C. ✓	0°-00'

1-26-27

H. Wilshusen Cold
D.S.
P.B.
A.M.
A.B.



$Z-A = 187^{\circ}04'$
 $A = 91^{\circ}04'$
 $D = 20^{\circ}R.$
 $T = 293.15$
 $L = 455.17$
 $R = 287.94$

Sta.	Point	A-Left	A-Right	Cal. Bsect.	Mag. Bsect.
113+45.09	P.T. ✓	54°-31'½			
113+00		50°-01'½			
+50		45°-01'½			
112+03.9	P.I.	102°03'			
112+00		40°-01'½			
+50		35°-01'½			
111+00		30°-01'½			
+50		25°-01'½			
110+00		20°-01'½			
+50		15°-01'½			
109+00		10°-01'½			
+50		5°-01'½			
108+00		0°-01'½			
107+99.34 107+98.94	P.C.	0°-00'			
113+53.46	P.T. ✓		35°-28'½		
113+00			30°-07'½		
+50			25°-07'½		
112+03.90	P.I.		70°57'		
112+00			70°-07'½		
+50			15°-07'½		
111+00			10°-07'½		
+50			5°-07'½		
110+00			0°-07'½		
109+98.71	P.C. ✓		0°-00'		

N. 18° 57' W.

70° 57' 40"

18° 57' E

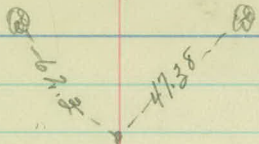
289° 59' E

1-27-27

Al Wishusen
D.S.
A.B.
F.M.
P.B.

12" elm.

12" Br. elder cold.



$$\Delta = 218^{\circ}06'$$

$$A = 109^{\circ}03' \text{ Lt.}$$

$$D = 20^{\circ}$$

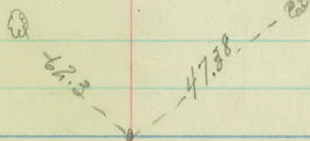
$$T = 404.06$$

$$L = 545.25$$

$$R = 287.94$$

12" elm

12" Br. elder



$$\Delta = 141^{\circ}54'$$

$$A = 70^{\circ}57' \text{ Rt.}$$

$$D = 20^{\circ}$$

$$T = 205.19$$

$$L = 354.75$$

$$R = 287.94$$

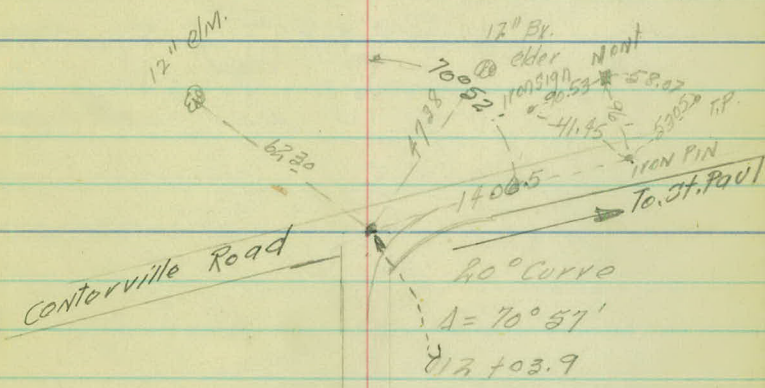
Station	Point	A-Lt	A-Rt	Cal Bearing
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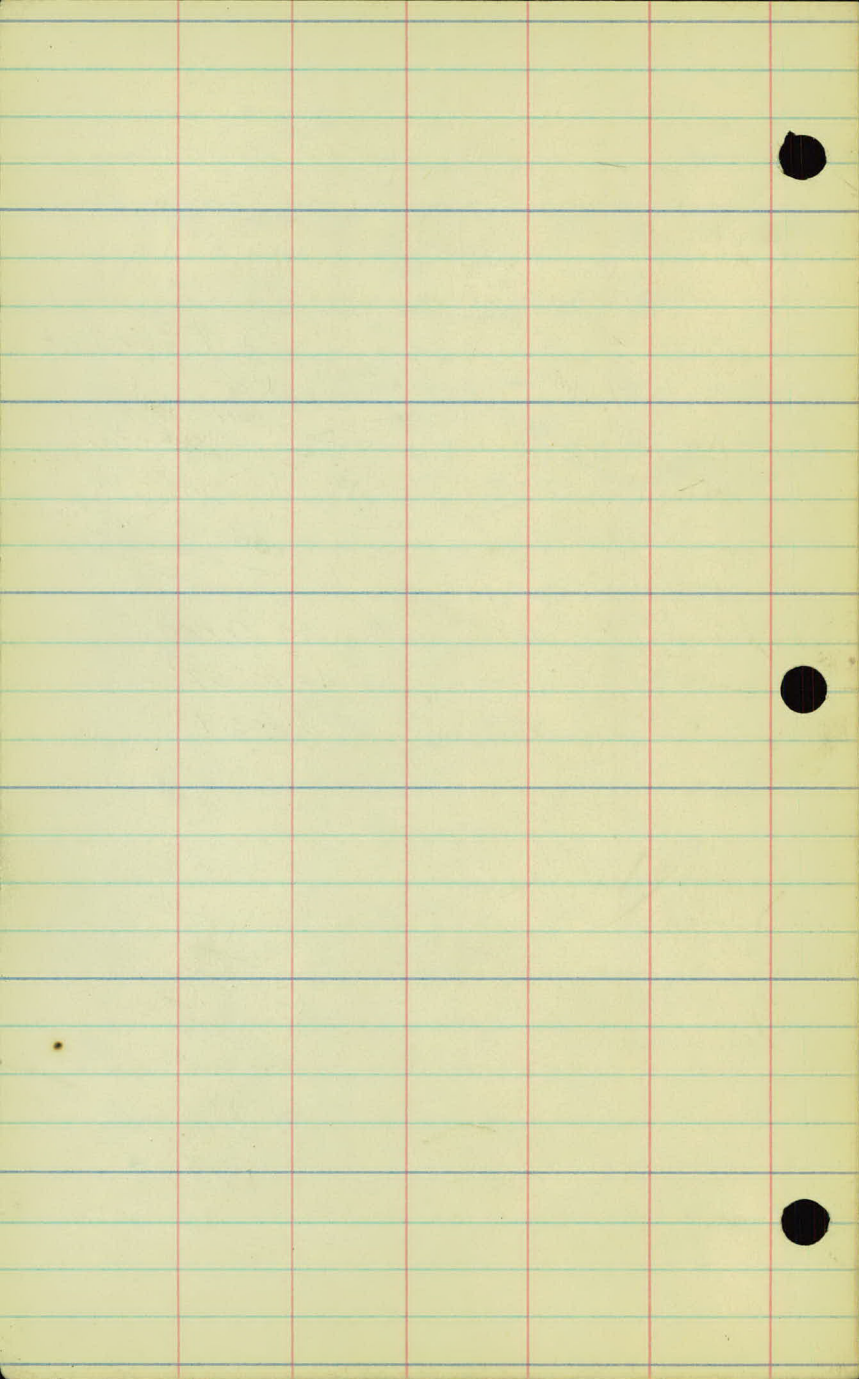
1171039

2-7-27

Warm Snow - ?
Wishusen
D.S.
L.B.
F.M.
P.B.

N 1/4 Cor. Sec. 4





Project 27-63

Topography

North County Line
from Turtle Lake Road
to Centerville Road.

6+00

5+00

4+00

3+00

2+00

1+00

0+00

Meadow

Meadow

#19 T.P. 20

#93 T.P. 10

#40 Rd 8'

#50 Rd 23'

#32 T.P. 5'

#64 T.P. 14'

Rd 40'

#40 T.P. 14'

#08 T.P. 61'

Rd 16'

#81 T.P. 4'

Cultivated

Rd 31'

Road

Meadow

Cultivated

Rd 11'

Rd 10'



13+00

12+00

11+00

10+00

9+00

8+00

7+00

194 T.P. 24

0

161 T.P. 14

o

Ref. II

Ref. 9'

102 T.P. 24

0

151 T.P. 14

o

Vertical

Vertical

177-75-13

o

101 T.P. 24

0

109 T.P. 14

40y

Vertical

Vertical

113 T.P. 24

0

104 T.P. 14

o

Ref. II

Ref. 11'

20+00

19+00

18+00

17+00

102

* Road 12.4 ft

16+00

15+00

14+00

Cultivated

F. Cor 19
+96 TP 25'

+ 1 + 1 + 0

T.P. 14' F. 12'

F. 18

F. 20'

+78 TP. 14'

+11 T.P. 25'
F. 19

0

F. 19'

+53 TP 14'

F. 181

+04 F. Cor. 21

Woods pasture

Woods

+20 F. Cor 20'
+19 TP 24'

+31 TP. 14'
B
+22 TP. 14'

+11 T.P. 25' Rd. B

Rd. A +29 TP. 14'

Woods

Woods



29+00

26+00

25+00

24+00

23+00

22+00

21+00

145 T.P. 17'

152 T.P. 26

o

120 T.P. 17'

Cultivated

197 T.P. 26'

o

190 T.P. 15'

Cultivated

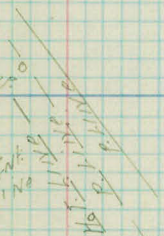
169 T.P. 19'

116 T.P. 25'

110 ENT P.P.

185 ENT P. LINE

159 ENT P. LINE



Cultivated

156 T.P. 14'

108 H.T. Tower 29
105 F. Cor 29

177 T.P. 15'

Cultivated

Woods - Pasture

106 T.P. 14'

1.41

34+00

+ 33

F ENTRANCE LT

33+00

32+00

31+00

30+00

29+00

28+00

+82 T.P. 23'

Cultivated



+13 T.P. 24'

+38 T.P. 24'

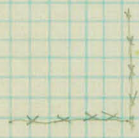
+74 F. 17'

+19 F. Cor. 17'

+59 T.P. 75'

Cultivated

Cultivated



+93 T.P. 24'

F. 28'

+71 T.P. 23'

F. 22'

+48 T.P. 22'

F. 31'

+18 T.P. 20'
F. 30'

F. 30.5
+96 T.P. 17'

F. 30'

+67 T.P. 19'

1/2 Cor. 200'

Hill Farm

Hill Farm

41+00

40+00

39+00

38+00

37+00

36+00

35+00

1-28-27

+40 T.P. 20'

F. 15'

F. 18'

+43 T.P. 21'

F. 17'

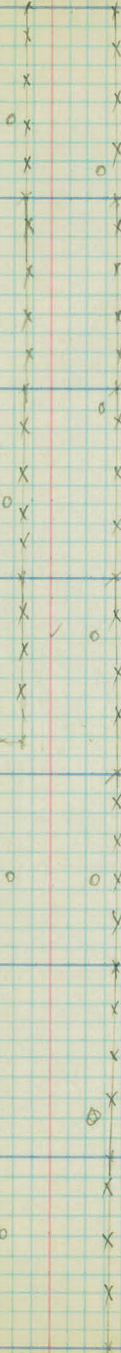
+15 F. Cor. 18' ~~-----~~

+48 T.P. 21'

+60 T.P. 23'

Cultivated

Cultivated



+15 T.P. 25'
F 36

F. 86'
+90 T.P. 28'

F. 86'

+70 T.P. 27'

F. 36'

+46 T.P. 26'

F. 86'

+20 T.P. 25'
F 36

Hill Corn

Hill Corn

F 36

48+00

47+00

46+00

45+00

45?

± E. Entrance St.

44+00

43+00

42+00

Cultivated

+28 T.P. 19'

F. 103 F.G. 21'

F.L. 21'

+41 T.P. 19'

+39 F.G. 14' F. 23'

+32 F. Trees 14'

F. 13'

F. 13' trees 14'

+41 T.P. 20'
+39 F. House 14'
+36 C.P. House 14'
F. 13'

+35 B. Rail trees 14'

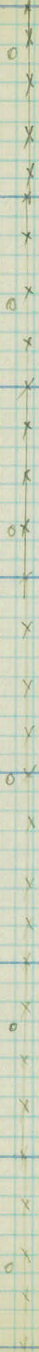
+10 F. h. 21'
+10 B.F. 13'
F. 13'

Produce

approx 14 trees in Row



Field



+26 T.P. 29'

F. 25.5'

+46 T.P. 29'

F. 36'

Hill Farm

+24 T.P. 28'

F. 36'

F. 27'

+26 T.P. 28'

F. 27'

+27 T.P. 28'
+27 T.P. 28'

Hill Farm

F. 36'

+43 T.P. 28'

F. 13'

58+00

54+00

53+00

52+00

51+00

50+00

49+00

1-28-27

Cult

+46 F.L. 9'
+28 T.P. 17'
+18 Cor. School House 110' 0
+0 B. Tree 8'
+09 Tree 20'

+81 Tree 9'
+68 Tree 20'
+62 Cor. School yard

+05 T.P. 28'
F. 33

F. 1-33

+60 T.P. 25'

+21 T.P. 18'

F. 34'

Cultivated

+57 T.P. 29'
+98 F-KIN 934

F. 34'

+28 T.P. 18'

+51 T.P. 29'

F. 34'

Cultivated

Hill Farm

435

+03 T.P. 28'

+37 T.P. 19'

435'

62+00

61+00

60+00

59+00

58+00

57+00

56+00

69+00

68+00

67+00

66+00

65+00

64+00

63+00

+85 T.P. 16'

Road

93.29 F 42'
+95 - T.P. 43'

Cultivated

F. 62
94.25 T.P. 60' T.P. 105'
Ed. 80'

158 T.P. 45'-96'

F 56'

+40 T.P. 11'

Cultivated

+43 T.P. 29'

F 30

+96 T.P. 15'

+24 T.P. 25'

F. 30'

Hill Farm

F 30'

+84 T.P. 25

Cultivated

T.P. 15'

F 20.5

76+00

75+00

+95 F-ENTRANCE 15'

74+00

73+00

72+00

71+00

70+00

F 26'

462 T.P. 26'
462 T.P. 14'

F. 27'

495 T.P. 29'
450 " " "
470 " " "
460 T.P. 28'
451 F 26'

F. 18'

484 T.P. 14' F.L.

F 16'

F 15'

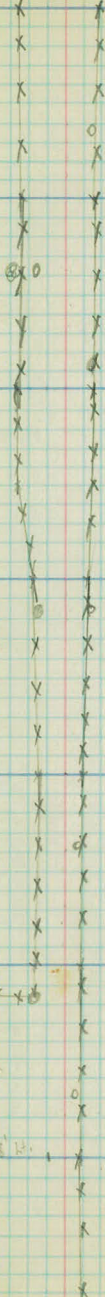
484 T.P. 18'

pasture

Cultivated

486 S.H.

road



439 T.P. 16'

F. 16'

412 T.P. 14'
F. 14'

Cultivated

F 12'

484 T.P. 12'

F 10'

460 T.P. 9'

F 9'

432 T.P. 7'

F. 7'

Cultivated

404 T.P. 7'
F.A.

83+00

82+00

81+00

80+00

79+00

78+00

77+00

1-28-37

+13 T.P. 22'
F 23'

F 26'

+144 T.P. 40'
+130 T.P. 5'

F. 18' & Rd. 43'

+147 T.P. 115' 1/2 Cor.
+143 T.P. 79'

+145 T.P. 166'
+125 F. Cor. 84'
+105 T.P. 012'

+119 T.P. 121' 57'

+150 F. 71' 35'

+121 T.P. 11'
+112 T.P. 111' 5'

+150 F. 34'

+110 F. 110' 18'
F. 26'

+159 T.P. 15'

+116

Cultivated

Cultivated

Cultivated



+188 T.P. 16'

+132-2 Trees 88'

F F 14'

+157 T.P. 14'

+15 T.P. 17'
F 13'

+131 Int.

+150 F 35'

+108 Rd. 84'

+110 Rd. 50'

+110 Rd. 26'

+100

+100

Rd. 6

Rd. 3'

Rd. 3'

Cultivated

+159 F. Int.

+126 F. 13'

+179 T.P. 17'

Cultivated

+15'

90+00

89+00

+84 $\frac{1}{2}$ F. ENTRANCE

88+00

87+00

+61 $\frac{1}{2}$ F. ENTRANCE

86+00

85+00

+96 $\frac{1}{2}$ DRIVE AT

84+00

1-28-27

+52 = KING 28'
+75 1/2 22'
+15 3/4 18 5/8
24' C.M.

+10 T.P. 24'
F. 27'

F. 26'
+90 F. Car 26'

+62 T.P. 28'
+46 Stump 24'

F. 26'

+78 Stump 24'

+40 Stump 24'

F. 24'

+80 T.P. 22'

+55 Stump 22'

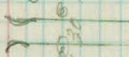
F. 23'

F. 22'
+93 T.P. 22'

F. 21'

Mature forest

Cultivated



+18 F. KING 22'
+61 Tree 22'

+39 Tree 27'

+31/2 26'
F. 25'

+87

+38 C. BARN 24.9

+28 1/2 drive
+16 F. Tree 25'

+61 F.P. 15'
+61 M.B. 9'

+46 F.F. 24'

F. 23'

+75 B. yard

+48 T.P. 15'

F. 24' Tree 25'

+51 T.P. 15'

+36 1/2 F. Entrance

F. 22'

+45 B.P. Tree 26'

+17 T.P. 16'

+20 Tree 26'

Yard

Cultivated

97+00

96+00

95+00

94+00

93+00

92+00

+67 ♀ F Entrance R

+52 ♀ F Entrance h

91+00

+82 T.P. 23'

F. 31'

Pasture

+27 F Xing 21' → → →

F 31'

+43 P.P. 21'

F 30'

Cultivated

Rd. 5'

+71 F Cor 29'

+65 Tree 28'

+58 T.P. 19'

+72 F.L. 28'

x x x

+16 Tree 22'

+90 Tree 24'

x 46 Tree 30'

x 95 Tree 35'

+12 P.P. 19'

row trees 25'

✓

pas & drive

28' tree 24' P. Cor

Yard

Hay Meadow

+14 Tree 16'

+81 T.P. 19'

+80 M. 5x13
+78 F 28'

Pasture

4.19'

6.11

257

♀ F. ENTRANCE LT

104+00

278

♀ F. ENTRANCE LT.

262

♀ F. ENTRANCE LT

103+00.

102+00

101+00

100+00

99+00

98+00

1-28-27
+ 83 R.P. 29'
+ 89 Cor. House 43'

House

218 330V 37'

467 R. Trees
+ 33 R. S/6 62'
+ 23 C. Barn
+ 21 F.F. 87'
+ 15 T.P. 28
F. 36
+ 15 Cor. Barn 62'

Yard
Eggs & Truss



Cultivated

+ 70 F. Cor. 9'

F. 36'

Pasture F 9'

+ 26 T.P. 26'
F 34'

F 9'

F. 26'

Pasture

F 9'

+ 19 T.P. 25'
F 34'

4 Rd. 5'

Pasture

+ 78 F. Cor. 9'

F. 33'

Pasture

Hay Meadow

111+00

110+00

109+00

108+00

107+00

106+00

105+00

+80 of Carborville Rd. 15'

+85 Trap 9'

+50 of Rd. 46'

+84 P.P. 19'

+29 of Dy 28'

of Rd. 19'

Int. 100 Edge Rd

+24 P.P. 35'

Rd. 12'

Cultivated

+31 Trap 32'

Rd. 12'

Cultivated

+75 - 2 Trap 31

+60 P.P. 30'

+77 P.P. 31'

Cultivated

Cultivated

+86 P. King 40'

+86 F. King 40'

114 +00

113 +00

112 +00

453.46 Rd. 15

450 1.0. 28'

4 Rd. 4'

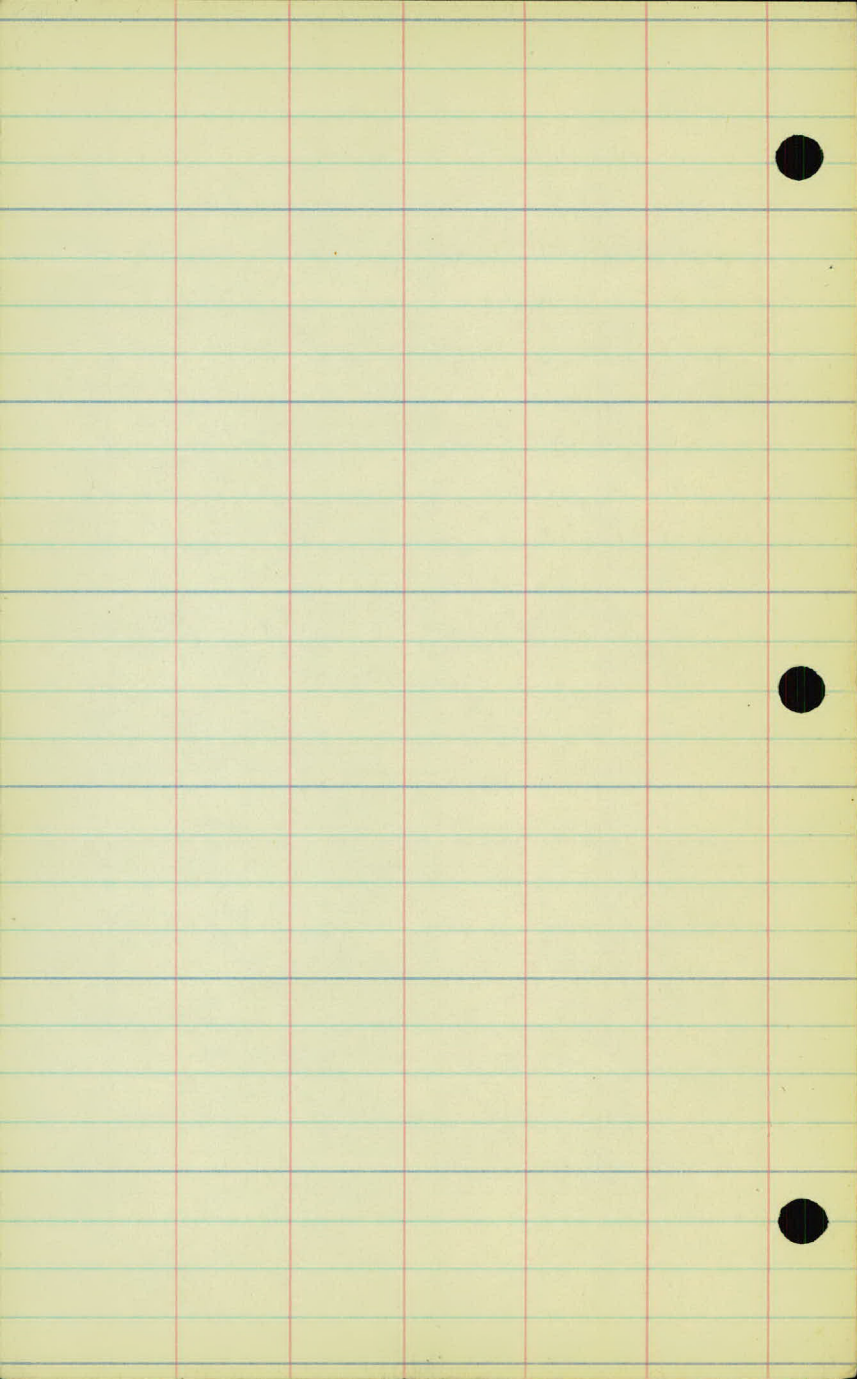
450 4' Con. Rd. 19' also edge Rd.

4 Con Rd. 60'

Cultivated

Rd. 15' 453.46

Cultivated



Curve to the

114+00

113+00

112+00

111+00

110+00

109+00

108

1-27-27

+45 Edge Cen Rd 8'

+36 P.P. 32'

Edge Cen Rd 8'

+69 G. Pole 22'

+65 Swamp 35'

+18 Iron 21 1/2'

+13 IN. P.L.

P.L. 54'



+45 Edge C. Rd
25' & 10'

¢ Cen Rd. 9'
+93 P.P. 32'

+60 Edge C. Rd.
+80¢ Cen Rd. 17'

+13 E.F. 1'

P.P. 70' ¢ Cen Rd. 43'

+16 P.P. 23

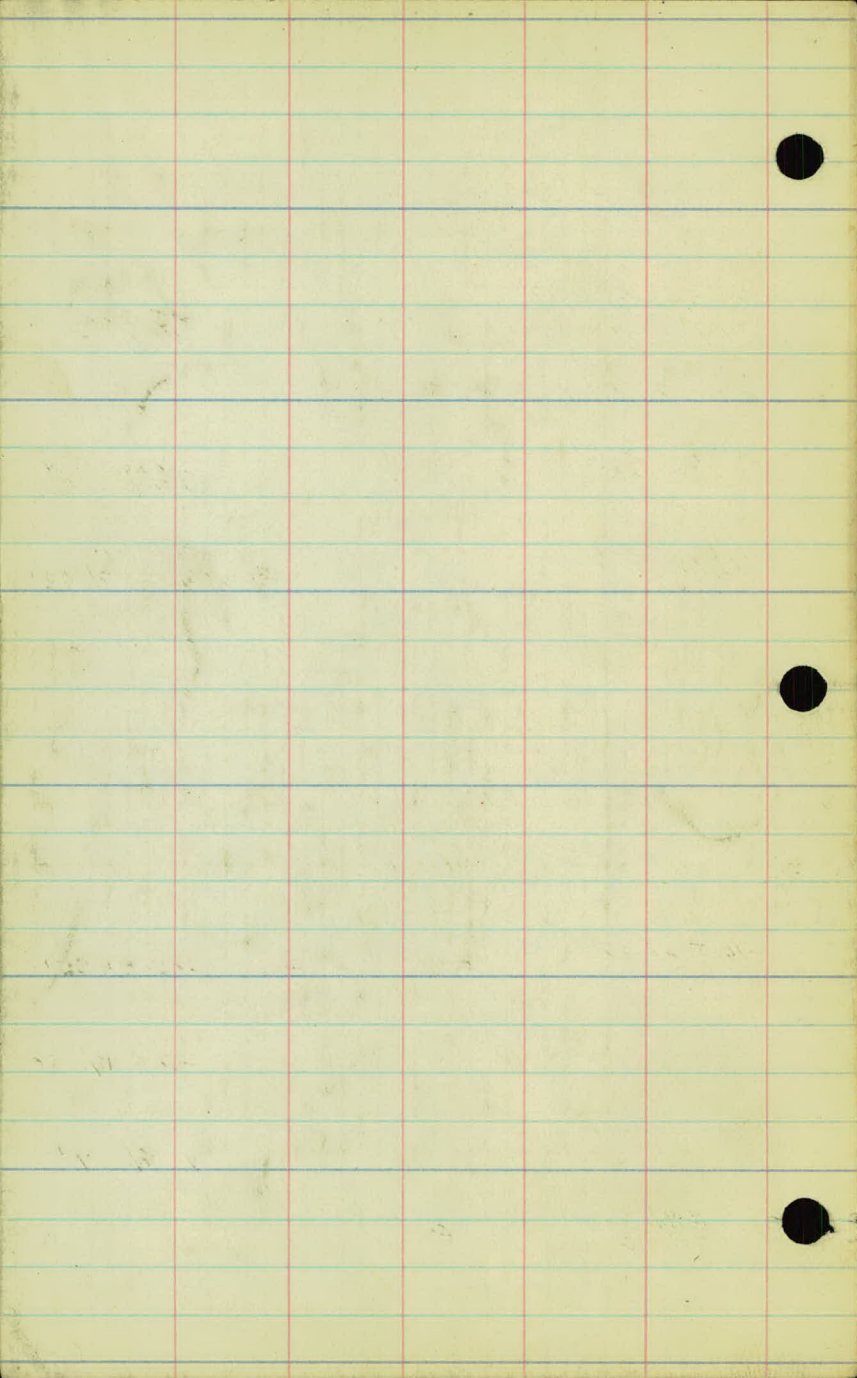
+10. T. 100 37'

+05 P.P. 55'

+50¢ Rd. 50

¢ Rd. 21'

+75 E.F. 1'
+68 P.P. 23



Project 27-63

Levels

North County Line
from Turtle Lake Road
to Centerville Road

Station	B.S.	I.I.	F.S.	Rod	Elev.
B.M.	7.93	915.37	✓		907.44
0+00				8.2	07.20
+50				8.2	07.20
+78				8.8	06.60
+91				10.5 ^{04.9}	96.90
1+00				10.5 ^{04.9}	96.90
+05				8.8	06.60
+50				7.2	08.20
2+00				5.4	10.0
+50				5.1	10.30
3+00				5.5	09.9
+15				6.6	08.80
+43				7.8	07.60
+50				8.8	06.60
+59				8.8	06.60
+83				8.5	06.90
4+00				8.2	07.20
+50				9.2	06.20
5+00				10.0	05.40
+50				11.0	04.40
6+00				11.5	03.9
T.P.	1.07	905.89	✓	10.55	904.82
+50				2.0	03.9
7+00				2.0	03.9
+50				2.3	03.6
8+00				2.9	03.0
+50				3.5	02.4

2-1-27

Spike on T.P. 30' Rt. Sta. - 1450

Edge of ditch

Bottom " "

" " "

Edge " "

Edge of Cut

Bottom ditch

" " "

" " "

Edge " "

Station	B.S.	H.I.	F.S.	Rod	Elev.
		905.89			
9+00				4.0	01.9
+50				4.6	01.3
10+00				5.2	00.7
+50				5.2	00.7
11+00				4.9	01.0
+50				4.4	01.5
12+00				3.8	02.1
+50				3.6	02.3
13+00				3.2	02.7
+50				3.1	02.8
14+00				3.2	02.7
+50				3.6	02.3
15+00				3.8	02.1
T.P.	6.32	906.11	4.10		901.79
+50				6.2	01.9
16+00				5.7	02.4
+20				5.8	02.3
+50				6.7	01.4
17+00				6.3	01.8
B.M.		915.37	5.19		902.92
+50				6.1	02.0
18+00				5.6	02.5
+50				4.6	03.5
19+00				3.3	04.8
T.P.	11.66	918.93	0.84		907.27

14.65
 7.89
 7.26
 915.37
 7.26
 908.11
 CHECK
 H.I. 5.19

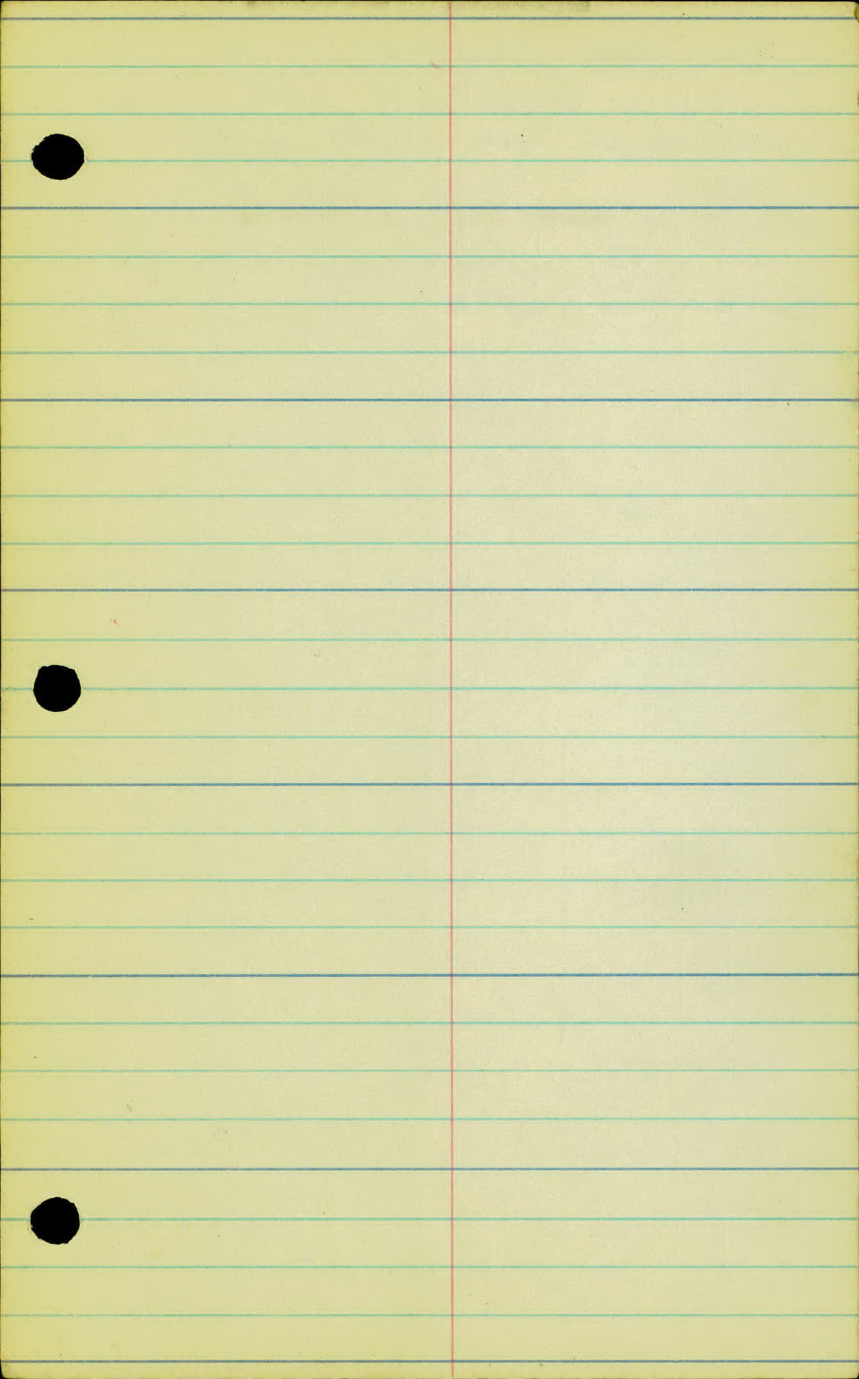
26	35	48	56
200	150	100	50

Spike in 30" 40' RT. Sta. 17+10.

Station	B.S.	I.I.	F.S.	Rod	Elev.
		918.93			
+50				12.2	06.7
20+00				10.2	08.7
+50				9.2	09.7
21+00				7.4	11.5
+50				5.3	12.6
22+00				5.2	13.7
+50				5.2	13.7
23+00				5.0	13.9
+50				4.2	14.7
24+00				3.3	15.6
+50				2.7	16.2
25+00				2.1	16.8
+50				1.0	17.9
T.P.	11.70	930.27	0.26		918.57
26+00				11.3	19.0
+50				7.8	20.5
27+00				8.2	22.1
+50	23.36	908.11		6.1	24.2
B.M.	1.20	2216		5.69	924.58
	22.16	930.27			
	CHK. H.A.W.				
28+00				3.9	26.4
+50				2.7	27.6
29+00				2.3	28.0
+50				1.8	28.5
30+00				1.5	28.8
+50				1.7	28.6

Spike in T.P. 20' Rt. Sta. 27+40

Station	B.S.	I.L.	F.S.	Red	Elev
		930.27 ✓			
31+00				2.1	28.2
+50				3.0	27.3
32+00				3.2	27.1
T.P.	8.07	934.67 ✓	3.67		926.60 ✓
+50				7.7	27.0
33+00				7.4	27.3
+50				6.7	28.0
34+00				5.9	29.0
+50				4.1	30.6
35+00				2.8	31.9
+50				3.5	29.0 31.2
36+00				4.6	28.0 30.1
+50				5.4	29.3
37+00				5.2	29.5
+50				4.5	30.2
38+00				4.1	30.6
+50				4.4	30.3
39+00				6.8	27.9
+50				8.8	25.9
40+00				10.0	24.7
T.P.	4.16	931.32 ✓	7.51		927.16 ✓
+50				7.7	23.6
41+00				8.4	22.9
+50				8.2	23.1
42+00				7.3	24.0
+50				6.2	25.1



Station	B.S.	H.I.	F.S.	Rod	Elev.
		931.32			
B.M.	12.23 11.18 1.05	930.27 1.05	2.91		928.41
43+00		931.32		4.5	26.8
+50				3.0	28.3
44+00	CHK. H. 2			4.1	27.2
+50				5.4	25.9
45+00				5.8	25.5
+50				5.6	25.7
46+00				5.6	25.7
+50				5.6	25.7
47+00				6.1	25.2
+50				7.3	24.1
T.P.	0.06	925.55	5.83		925.49
48+00				2.5	23.1
+50				3.1	22.5
49+00				3.5	22.1
+50				3.6	22.0
50+00				3.8	21.8
+50				4.7	20.9
51+00				4.7	20.9
+50				4.0	21.6
52+00				2.9	22.7
+50				2.1	23.5
53+00				3.5	22.1
+50				5.2	20.4
54+00				7.0	18.6
+50				9.0	16.6

2-6-27

Cold & Windy

Spike in 2 1/2" oak 35' ht. 56. 42 + 75

Station	BS	I.I.	FS	Red	Elev.
		925.55	✓		
55+00	6.86 871	925.55		9.7	15.9
B.M.	3.77	919.64	✓	9.68	915.87 ✓
+50				4.3	15.3
56+00				4.3	15.3
+50				2.6	16.0
57+00				3.8	15.8
+50				3.8	15.8
58+00				2.6	16.0
+50				4.0	15.6
59+00				4.3	15.3
+50				4.3	15.3
60+00				4.6	15.0
+50				4.4	15.2
+75				4.6	15.0
61+00				6.0	13.6
+50				9.0	10.6
62+00				11.0	08.6
T.P.	6.84	916.19	✓	10.29	909.35 ✓
+50				9.0	07.2
63+00				9.8	06.4
+50				10.7	06.0
64+00				10.0	06.2
+50				8.4	07.8
65+00				7.3	08.9
+50				7.7	08.5
66+00				8.7	07.5

2-1-27

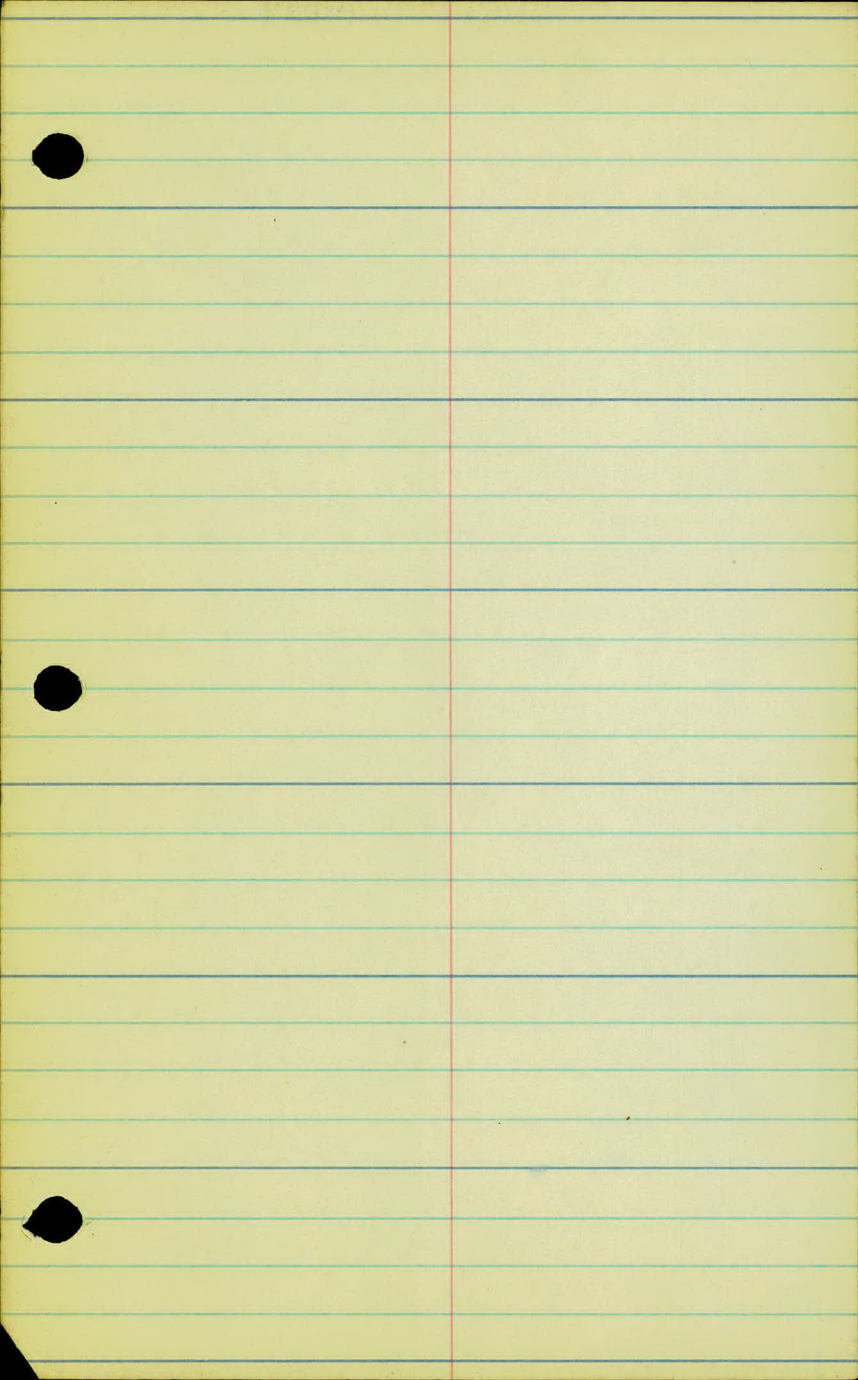
Windy - Cold.

Spike in 18" dia 35' ht. str. 55+05

Station	B.S.	I.I.	F.S.	Rod	Elev.
		916.19	✓		
+50				8.8	07.4
67+00				10.4	05.8
+50				10.8	05.2
68+00				11.2	05.0
+50				9.2	07.0
69+00				7.8	08.4
+50				7.6	08.60
70+00				6.4	09.8
+50				7.8	08.4
71+00				10.2	06.0
+50				11.0	05.2
T.P.	4.28	910.87	✓	9.70	906.49
72+00				5.0	05.9
+50				4.7	06.2
73+00				4.5	06.4
+50				4.0	06.9
74+00				3.4	07.5
+50				3.7	07.2
B.M.			5.80		905.07
75+00	29.67 14.99	925.55 14.65		4.9	06.0
+50	14.68	910.87		5.0	05.9
	off H. L. W				
76+00				5.9	05.0
+50				6.7	04.2
77+00				6.7	04.2
+50				6.7	04.2
78+00				6.1	04.8

Spike in 12" OAK. 100' Lt. Sta. 72+95

station	BS	H.I.	FS	Rod	Elev.
		910.87			
+50				5.1	05.8.
79+00				4.0	06.9.
+50				3.2	07.7.
80+00				4.2	06.7.
+50				5.4	05.5.
81+00				5.6	05.3.
T.P.	6.60	913.41	4.06		906.81
+37				8.2	05.2.
+41				8.8	04.6.
+50				8.0	05.4.
82+00				6.8	06.6.
+50				6.2	07.2.
83+00				5.2	08.2.
+50				4.0	09.4.
84+00				4.2	09.2.
+50				3.9	07.5.
85+00				7.0	06.4.
+50				7.7	05.7.
86+00				7.8	05.6.
+50				7.8	05.6.
87+00				8.0	05.4.
+50				8.6	04.8.
88+00				9.6	03.8.
+50				11.0	02.4.
89+00				12.3	01.1.



Station	B.S.	H.I.	F.S.	Red.	Elev.
T.P.	3.27	906.64	10.04		903.37 ✓
B.M.			2.56		904.08 ✓
+50	16.10 9.87	910.87 423		6.7	899.9 ✓
90+00	4.23	906.64		7.6	99.0 ✓
+50		CHK. H.I. W.		7.8	98.8 ✓
91+00				7.6	99.0 ✓
+50				7.3	99.3 ✓
92+00				6.6	00.0 ✓
+50				5.2	01.4 ✓
93+00				4.8	01.8 ✓
+50				5.3	01.3 ✓
94+00				5.5	01.1 ✓
+50				5.5	01.1 ✓
95+00				6.0	00.6 ✓
+75				6.0	00.6 ✓
+50				5.4	01.2 ✓
96+00				4.0	02.6 ✓
+50				1.7	04.9 ✓
T.P.	6.24	912.50 ✓	0.38		906.26 ✓
97+00				5.1	07.4 ✓
+50				4.0	08.5 ✓
98+00				5.4	07.1 ✓
+50				7.3	05.2 ✓
99+00				8.6	03.9 ✓
+50				9.0	03.5 ✓
100+00				8.1	04.4 ✓
+50				8.4	04.1 ✓

2-1-27

Spike in 30" Cottonwood 25' Rt. Sta. 89+00

Station	B.S.	I.I.	F.S.	Red	Elev.
		912.50			
101+00				9.3	03.2
+25				8.7	03.8
+50				9.0	03.5
102+00				7.7	04.8
+50				5.6	06.9
103+00				3.5	09.0
+50				2.5	10.0
T.P.	11.90	922.96	0.44		912.06
104+00				13.3	10.7
+50				13.0	11.0
105+00	18.14 1.82	906.64 17.32		12.3	11.7
B.M.	17.32	923.96	10.80		913.16
		CHK. H.A.W.			
+50				11.6	12.4
106+00				9.6	14.4
+50				7.2	16.8
107+00				5.3	18.7
+50				4.4	19.6
+79.84				4.6	19.4
+50				5.5	18.5
109+00				7.0	17.0
+50				8.6	15.4
110+00				10.8	13.2
+50				11.7	12.8
111+00				13.0	11.0
+50				13.6	10.4
112+00				15.0	09.0

2-1-27

cold. windy

S.E. Cor. of Conc. Perch 75' Lt. Sta. 104+85

Curve to Lt.

Station	B.S.	H.L.	F.S.	Red	Elev.
		923.96 ✓			
+20				15.0	09.0 •
+50				11.0	13.0 •
112+00				10.2	13.8 •
+45.9				9.8	14.2 •
+50				9.5	14.2 •
114+00				10.0	14.0 •
+50				10.1	13.9 •
115+00				10.3	13.7 •
108+50				5.2	18.8 •
109+00				6.0	18.0 •
+50				6.2	17.8 •
+98.21	P.C.			6.6	17.4 •
110+50				6.2	17.8 •
+15				6.2	17.8 •
+96				7.4	16.6 •
111+00				7.7	16.3 •
+50				5.7	18.3 •
112+00				3.7	20.3 •
+20				2.4	21.6 •
+27				5.4	18.6 •
+40				4.6	19.4 •
+50				3.6	20.4 •
113+00				1.5	22.5 •
T.P.	6.27	927.97 ✓	2.26	921.70 ✓	
+53.46	P.T.			4.8	23.2 •

End of survey

1/2 Centerville Road

" " "

" " "

" " "

Curve to Rt.

Edge of road

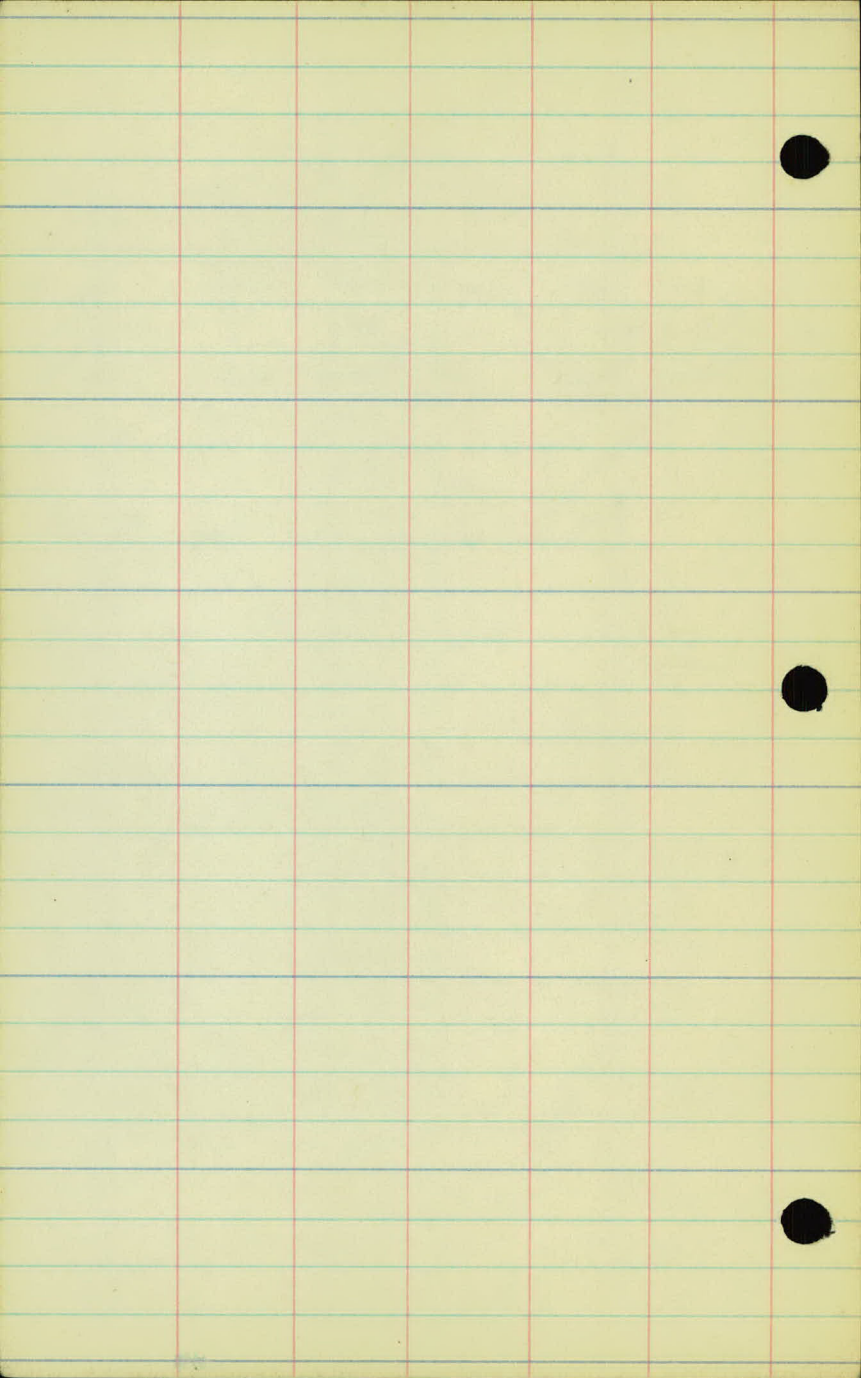
1/2 of Centerville Road

" " " "

Station	B.S.	I.I.	F.S.	Rod.	Elev.
			927.97 ✓		
114+00				4.0	24.0 .
+50				3.0	25.0 .
115+00				2.3	25.7 .
+50				1.5	26.2 .
B.M.			7.11		920.86 ✓
	6.27	923.96			
	2.26	<u>4.01</u>			
	4.01	927.97			
	CHK. H.L.W.				

2-1-27

Spike in 30' By. elder N.E. cor of Intersection



Project 27-63

Culverts.

Station	H.I.	inlet	outlet	Present	Culv	Condition
---------	------	-------	--------	---------	------	-----------

905.84

90+74

$\frac{6.7}{12'}$

$\frac{6.6}{12'}$

Wooden
box

poor

904.43

90+75

$\frac{10.9}{14.5}$

$\frac{12.3}{18.5}$

24"
C.M.

good

Lt.

2-2-27

$\frac{8.5}{200}$, $\frac{8.4}{150}$, $\frac{8.5}{100}$, $\frac{7.4}{50}$

Drains to Lt.

Rt.

Wishusen
A.S.
A.M.
A.B.
P.B.

$\frac{6.7}{20}$, $\frac{7.2}{100}$, $\frac{6.8}{150}$, $\frac{6.9}{200}$

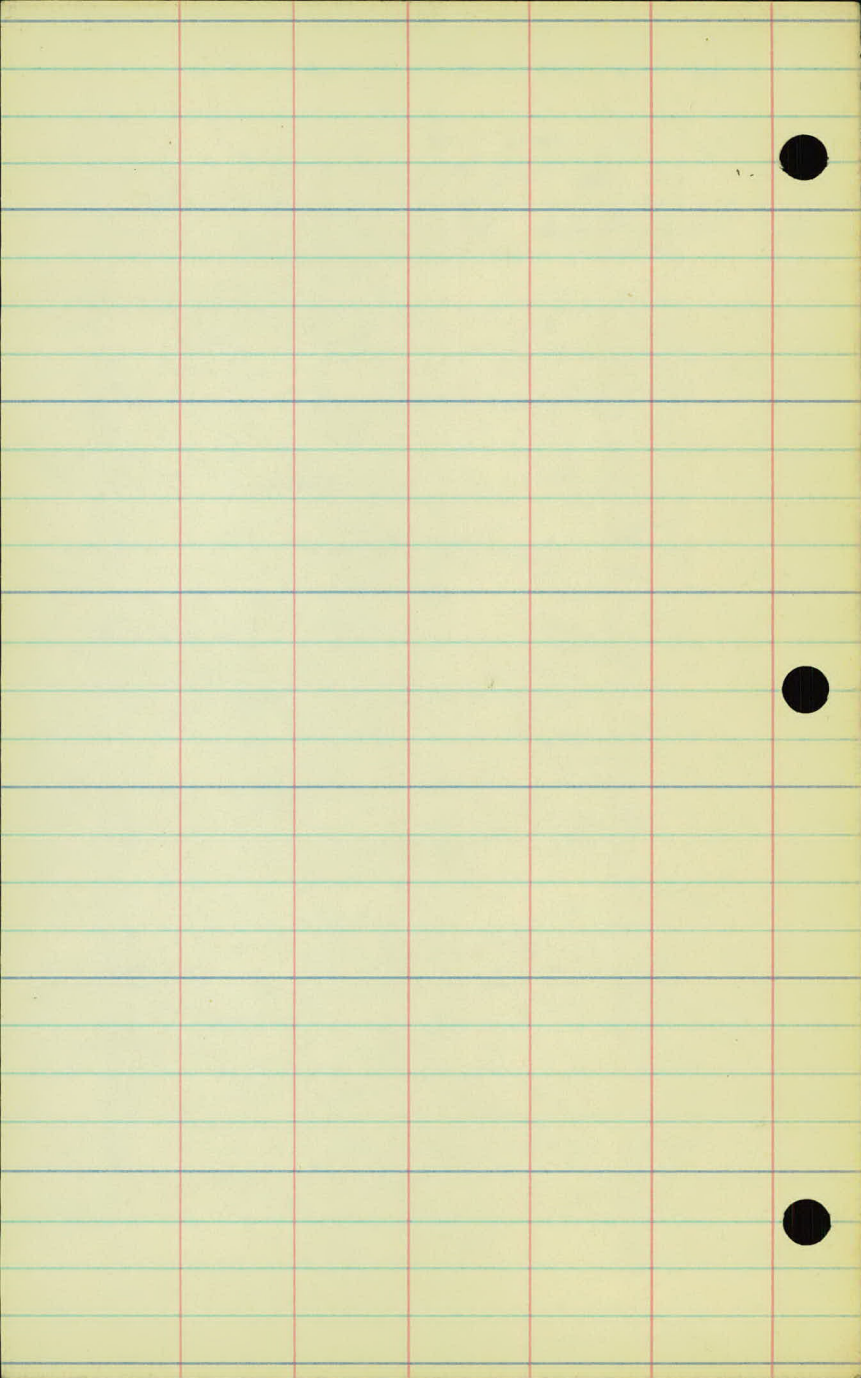
Drains to Rt.

2-7-27

$\frac{8.5}{100}$, $\frac{9.0}{50}$

$\frac{10.0}{50}$, $\frac{10.5}{100}$

Drains to Rt.



Project- 27-63

check Levels

North County line
from Turtle Lake Road
to Centerville Road

station	B.S.	I.I.	F.S.	Elev.	
B.M.	3.11	923.95		990.86	✓
B.M.			10.78	913.17	✓
T.P.	0.77	912.28	12.19	911.76	
T.P.	6.77	908.51	10.77	901.74	
B.M.			4.42	904.09	✓
T.P.	5.98	913.40	1.09	907.42	
T.P.	3.22	911.92	5.29	908.11	
B.M.			6.86	905.07	✓
T.P.	12.76	919.09	5.60	906.33	
B.M.	9.80	925.67	3.22	915.87	✓
T.P.	5.67	931.16	0.18	925.49	
B.M.			2.75	928.41	✓
T.P.	5.60	936.07	0.69	930.47	
T.P.	0.07	929.37	6.77	929.30	
B.M.			4.78	924.59	✓
T.P.	1.14	919.13	11.38	917.99	
T.P.	1.00	907.61	12.52	906.61	
B.M.			4.66	902.95	✓
T.P.	7.46	909.17	5.90	901.71	
T.P.	4.32	912.13	4.36	907.81	
B.M.			4.68	907.45	✓

Spike in 30" Br. elder N.E. Cor. of Intersection
S.E. Cor of Conc. Perch 75' Lt. Sta. 104+85

Spike in 30" Cottonwood 25' Rt. Sta. 89+00

Spike in 12" Oak 200' Lt. Sta. 73+95

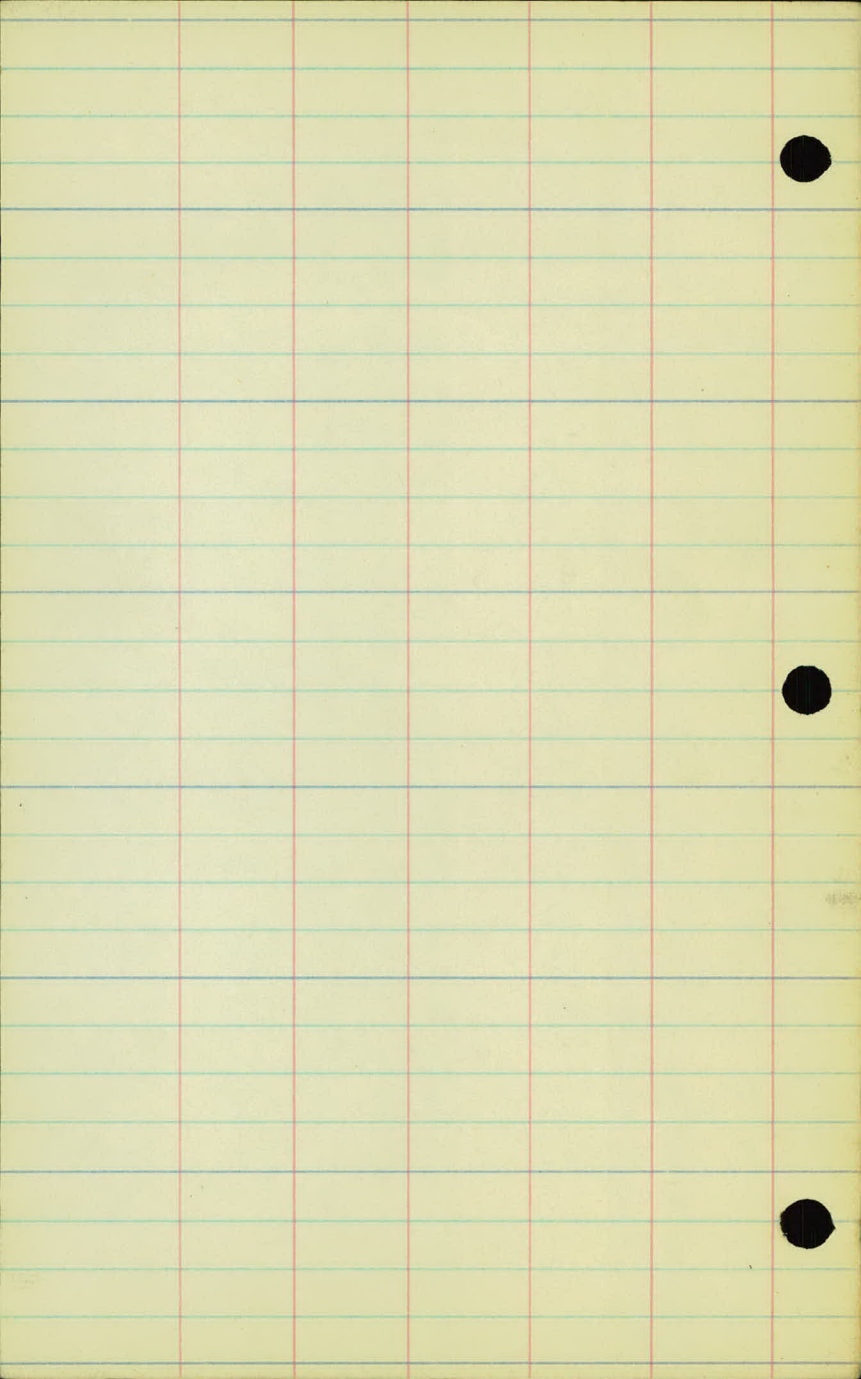
Spike in 19" elm 35' Lt. Sta. 55+05

Spike in 24" Oak 35' Lt. Sta. 42+75

Spike in T.P. 20' Rt. Sta. 27+40

Spike in 30" Br. elder 40' Rt. Sta. 17+10

Spike on T.P. 30' Rt. Sta. - 1+50



Project 27-63
Cross Sections
North County Line
from Turtle Lake Road
to Centerville Road
From 0+00 to 113+53.46

Station	+ or -	Elev.	Soil
0+00		07.70	
+50		07.70	
+78		06.60	
+91		04.9 <u>06.90</u>	
1+00		04.9 <u>06.90</u>	
+05		06.60	
+50		08.70	
2+00		10.0	
+50		10.30	
3+00		09.9	
+15		08.8	
+50		06.60	
+83		06.90	

2-2-27

Cold-Windy

H. Wischhusen

	90	100	98	92	87	♀	87	98	105	100	RT.	D.S. H.B. A.M. P.B. 1-0 80 75 21 33
	33	17	16	14	13	10	8.3	9	13	14	18	
	102	95	100	102	86	82	87	103	103	76	6.8	
L.O.	33	26	24	22	19	7	8.6	5	8	12	16	

10	107	90	82	104	103	74	6.8	
33	30	26	12	9.8	5	8	12	33

106	71	83	70	106	84	74	6.8	
33	30	17	5	10.6	3	8	19	33

92	84	90	106	84	76	6.8		
23	20	9	3	10.6	5	14	33	L.O.

90	84	90	104	104	77	70	7.0	
33	22	10	6	4	8.7	12	16	33

88	71	105	102	90	80	67	66	6.0	
33	30	28	25	12	12	7.2	12	21	33

25	67	63	46	43		
33	26	16	5.5	22	33	L.O.

6.8	5.8	4.6	4.6	
33	18	5.1	2.0	33

82	82	85	85	73	63	6.0	
33	30	27	20	12	5.6	34	33

76	78	85	87	66	80	66	6.0	
33	29	21	17	10	7	6.7	20	33

84	80	78	83	86	8.8	80	63	6.0	
33	27	21	11	6	9.8	4	10	21	33

84	86	88	87	80	90	98	86	76
33	30	23	17	10	9.0	70	23	33

Station	+ or -	Elev.	Soil
4+00		07.20	
	+50	06.70	
5+00		05.40	
	+50	04.40	
6+00		03.9	
	+50	03.9	
7+00		03.9	
	+50	03.6	
8+00		03.0	
	+50	02.4	
9+00		01.9	
	+50	01.3	
10+00		00.7	

2-2-27
Cold

Lt.

±

Rt.

H.L. Wilhanson

9.5
7.8
A.M.
P.B.

70 82 88 86 90 96 92 88
32 25 18 10 8 13 24 23

60 26 17 20 30 28 26 40
32 12 5 16 8 16 28 32

25 24 32 28 27 27 47 60
33 16 10 24 7 13 20 32

56 60 65 60 46 34 42 62 77 77
23 27 18 14 7 3.4 7 11 17 23 32 26

2.5 77 78 73 59 45 40 46 73 75 73 70
33 25 16 13 10 3.8 8 11 17 21 28 32

77 76 54 44 40 48 58 27 5.4
23 18 11 8 3.8 8 12 16 26 33

2.5 25 52 43 40 46 53 59 36 40
33 26 10 31 6 13 15 18 21 32

50 48 45 44 5.2 57 58 52 55
32 14 7 4.1 8 12 15 16 19 32

58 62 52 2.2 62 75 74 77
33 24 9 4.7 7 11 15 25 33

1.0 28 72 57 58 68 77 80
33 15 7 5.3 8 12 14 32 L.O

82 80 65 63 77 80
33 15 8 5.8 7 13 33

64 77 68 66 80 84
33 19 7 6.4 7 15 33

64 94 77 70 70 85 77
33 16 9 7.0 7 18 77

Station +cc- Eject. Soil

+50 900.7

11+00 01.0

+50 01.5

12+00 02.1

+50 02.3

13+00 02.7

+50 02.8

14+00 02.7

+50 02.3

15+00 02.1

+50 01.9

+76 02.4

+76 02.3

2-2-27
cold-windy.

St.

E

St.

H. L. Wilshusen
D. S.
A. S.
W. M.
P. B.

84 86 77 72 82 82
33 16 7 70 9 19 33

84 86 75 72 76 85 84 90
33 17 8 67 8 11 14 18 33

80 84 66 66 80 82
33 19 9 62 9 16 33

R.O. 27 78 68 62 62 80 82
33 16 13 9 7 15 33

R.O. 58 74 62 60 75 82
33 14 9 5.7 7 12 33

R.O. 52 58 73 56 56 80 82
33 28 12 7 5.4 4 16 33

55 62 66 54 57 62 75 84
33 23 12 9 5.4 4 8 14 33 L.O.

55 66 70 57 55 70 78
33 24 12 9 5.2 4 14 33

70 75 77 61 63 78 80
33 26 16 7 5.6 8 16 33

80 80 80 72 61 60 67 78 80 81 81
33 19 16 12 8 6.0 4 8 11 15 16 33

78 77 81 66 60 77 77 77
33 24 17 10 6.0 6 11 15 33

76 70 66 62 58 63 70 69
33 25 17 10 5.5 12 17 26 33

17 64 54 15
33 23 14 33

Station	+ or -	Elev.	Soil
16+00		902.4	
+09	+ 00	902.4	
+20		02.3	
+50		01.4	
17+00		01.8	
+50		02.0	
18+00		02.5	
+50		03.5	
19+00		04.8	
+50		06.7	
20+00		08.7	
+50		09.7	
21+00		11.5	

2-2-27

H. L. Wilshusen
D. S.
A. B.
A. M.
P. B.

$\frac{57}{33}$ $\frac{56}{15}$ $\frac{55}{55}$ $\frac{5.2}{14}$ $\frac{5.2}{33}$

$\frac{58}{33}$ $\frac{60}{22}$ $\frac{58}{12}$ $\frac{56}{55}$ $\frac{5.3}{10}$ $\frac{5.3}{33}$

$\frac{74}{33}$ $\frac{69}{19}$ $\frac{68}{12}$ $\frac{59}{59}$ $\frac{59}{19}$ $\frac{69}{19}$ $\frac{67}{22}$

L.O $\frac{75}{33}$ $\frac{76}{11}$ $\frac{69}{7}$ $\frac{64}{64}$ $\frac{6.0}{7}$ $\frac{7.4}{10}$ $\frac{71}{33}$

$\frac{75}{33}$ $\frac{77}{19}$ $\frac{79}{11}$ $\frac{66}{10}$ $\frac{6.0}{6.0}$ $\frac{5.7}{6}$ $\frac{7.4}{10}$ $\frac{67}{33}$ R.O

L.O $\frac{76}{33}$ $\frac{77}{11}$ $\frac{66}{10}$ $\frac{6.8}{6.8}$ $\frac{6.0}{6}$ $\frac{7.2}{8}$ $\frac{71}{15}$ $\frac{6.3}{33}$

$\frac{78}{33}$ $\frac{77}{19}$ $\frac{76}{18}$ $\frac{59}{9}$ $\frac{53}{53}$ $\frac{57}{7}$ $\frac{65}{7}$ $\frac{5.1}{33}$

$\frac{133}{33}$ $\frac{130}{17}$ $\frac{123}{11}$ $\frac{108}{10}$ $\frac{10.0}{10.0}$ $\frac{10.1}{4}$ $\frac{10.8}{8}$ $\frac{10.7}{19}$ $\frac{10.4}{25}$ $\frac{9.6}{33}$ R.O

$\frac{114}{33}$ $\frac{112}{29}$ $\frac{10.8}{20}$ $\frac{10.2}{14}$ $\frac{9.0}{10}$ $\frac{8.7}{8.7}$ $\frac{9.0}{4}$ $\frac{9.4}{6}$ $\frac{9.0}{9}$ $\frac{7.5}{11}$ $\frac{7.5}{15}$ $\frac{7.2}{4}$ $\frac{6.0}{33}$

$\frac{115}{33}$ $\frac{105}{19}$ $\frac{106}{12}$ $\frac{114}{11}$ $\frac{10.8}{10}$ $\frac{10.4}{10.4}$ $\frac{9.6}{4}$ $\frac{10.2}{10}$ $\frac{7.4}{20}$ $\frac{6.4}{30}$ $\frac{6.0}{33}$

$\frac{84}{33}$ $\frac{82}{16}$ $\frac{84}{14}$ $\frac{87}{10}$ $\frac{8.7}{8.7}$ $\frac{8.8}{3}$ $\frac{8.0}{4}$ $\frac{8.0}{11}$ $\frac{4.5}{19}$ $\frac{4.0}{33}$

$\frac{54}{33}$ $\frac{53}{16}$ $\frac{60}{15}$ $\frac{64}{13}$ $\frac{63}{6}$ $\frac{6.6}{6.6}$ $\frac{7.6}{2}$ $\frac{8.2}{8}$ $\frac{8.0}{13}$ $\frac{3.0}{18}$ $\frac{2.6}{33}$

$\frac{25}{33}$ $\frac{38}{18}$ $\frac{4.7}{14}$ $\frac{4.5}{14}$ $\frac{5.0}{14}$ $\frac{v.v.}{v.v.}$ $\frac{7.4}{3}$ $\frac{7.4}{10}$ $\frac{7.8}{11}$ $\frac{7.6}{13}$ $\frac{6.0}{15}$ $\frac{0.5}{19}$ $\frac{0.0}{33}$

Station	+ or -	Elev.	Soil
	+50	13.6	
22+00		13.7	
	+50	13.7	
23+00		13.9	
	+50	14.7	
24+00		15.6	
	+50	16.2	
25+00		16.8	
	+50	17.9	
26+00		19.0	
	+50	20.5	
27+00		22.1	
	+50	24.2	

2-3-27

H. Wishtusen

D.S.

A.M.

A.B.

P.B.

$\frac{33}{33}$	$\frac{32}{22}$	$\frac{36}{18}$	$\frac{36}{13}$	$\frac{34}{6}$		$\frac{25}{7}$	$\frac{52}{8}$	$\frac{53}{10}$	$\frac{17}{14}$	$\frac{12}{33}$
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$\frac{77}{33}$	$\frac{73}{25}$	$\frac{70}{15}$	$\frac{64}{9}$	$\frac{66}{3}$		$\frac{64}{6.6}$	$\frac{70}{5}$	$\frac{84}{8}$	$\frac{70}{12}$	$\frac{65}{14}$
-----------------	-----------------	-----------------	----------------	----------------	--	------------------	----------------	----------------	-----------------	-----------------

$\frac{77}{33}$	$\frac{78}{20}$	$\frac{63}{11}$	$\frac{66}{6.6}$	$\frac{63}{18}$	$\frac{85}{26}$	$\frac{85}{33}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------

$\frac{74}{33}$	$\frac{66}{21}$	$\frac{66}{17}$	$\frac{58}{7}$	$\frac{65}{6.5}$	$\frac{70}{4}$	$\frac{74}{5}$	$\frac{79}{12}$	$\frac{76}{22}$	$\frac{80}{33}$
-----------------	-----------------	-----------------	----------------	------------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{59}{33}$	$\frac{60}{21}$	$\frac{54}{7}$	$\frac{57}{5.7}$	$\frac{62}{4}$	$\frac{70}{12}$	$\frac{72}{25}$	$\frac{74}{33}$
-----------------	-----------------	----------------	------------------	----------------	-----------------	-----------------	-----------------

$\frac{42}{33}$	$\frac{47}{16}$	$\frac{53}{12}$	$\frac{52}{6}$	$\frac{4.8}{4.8}$	$\frac{55}{6}$	$\frac{55}{9}$	$\frac{62}{10}$	$\frac{58}{16}$	$\frac{57}{33}$
-----------------	-----------------	-----------------	----------------	-------------------	----------------	----------------	-----------------	-----------------	-----------------

$\frac{30}{33}$	$\frac{37}{20}$	$\frac{42}{12}$	$\frac{42}{6}$	$\frac{4.2}{4.2}$	$\frac{40}{7}$	$\frac{47}{9}$	$\frac{44}{16}$	$\frac{47}{33}$
-----------------	-----------------	-----------------	----------------	-------------------	----------------	----------------	-----------------	-----------------

$\frac{27}{33}$	$\frac{32}{24}$	$\frac{30}{12}$	$\frac{33}{11}$	$\frac{33}{6}$	$\frac{3.6}{3.6}$	$\frac{36}{5}$	$\frac{36}{10}$	$\frac{36}{29}$	$\frac{36}{33}$
-----------------	-----------------	-----------------	-----------------	----------------	-------------------	----------------	-----------------	-----------------	-----------------

$\frac{25}{33}$	$\frac{25}{16}$	$\frac{25}{11}$	$\frac{20}{6}$	$\frac{24}{24}$	$\frac{3.2}{6}$	$\frac{30}{18}$	$\frac{30}{33}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{12}{33}$	$\frac{12}{16}$	$\frac{10}{6}$	$\frac{1.5}{1.5}$	$\frac{12}{3}$	$\frac{12}{16}$	$\frac{12}{33}$
-----------------	-----------------	----------------	-------------------	----------------	-----------------	-----------------

$\frac{116}{33}$	$\frac{115}{17}$	$\frac{116}{12}$	$\frac{11.6}{11.6}$	$\frac{118}{7}$	$\frac{118}{14}$	$\frac{116}{33}$
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$\frac{96}{33}$	$\frac{97}{26}$	$\frac{96}{15}$	$\frac{95}{7}$	$\frac{9.9}{9.9}$	$\frac{96}{5}$	$\frac{10.4}{6}$	$\frac{10.4}{15}$	$\frac{10.4}{21}$	$\frac{10.7}{33}$
-----------------	-----------------	-----------------	----------------	-------------------	----------------	------------------	-------------------	-------------------	-------------------

$\frac{75}{33}$	$\frac{75}{17}$	$\frac{80}{14}$	$\frac{80}{7}$	$\frac{7.7}{7.7}$	$\frac{77}{6}$	$\frac{80}{17}$	$\frac{82}{33}$
-----------------	-----------------	-----------------	----------------	-------------------	----------------	-----------------	-----------------

Station	+ or -	Elev.	Soil
28+00		26.4	
+50		27.6	
29+00		28.0	
+50		28.5	
30+00		28.8	
+50		28.6	
31+00		28.2	
+50		27.3	
32+00		27.1	
+50		27.0	
33+00		27.3	
+50		28.0	
34+00		29.0	

2-3-27

Lt.

f

Rt.

Wishawson
D.S.
A.M.
P.B.
P.B.

Cold-Windy

$\frac{62}{33}$ $\frac{60}{27}$ $\frac{60}{19}$ $\frac{55}{5}$ $\frac{55}{60}$ $\frac{48}{6}$ $\frac{44}{11}$ $\frac{57}{17}$ $\frac{52}{33}$

$\frac{58}{33}$ $\frac{55}{25}$ $\frac{52}{17}$ $\frac{50}{9}$ $\frac{43}{8}$ $\frac{44}{44}$ $\frac{41}{9}$ $\frac{32}{20}$ $\frac{27}{33}$

$\frac{65}{33}$ $\frac{59}{23}$ $\frac{56}{14}$ $\frac{44}{8}$ $\frac{40}{40}$ $\frac{38}{5}$ $\frac{43}{12}$ $\frac{28}{17}$ $\frac{25}{26}$ $\frac{19}{33}$

$\frac{73}{33}$ $\frac{60}{23}$ $\frac{53}{16}$ $\frac{41}{8}$ $\frac{35}{35}$ $\frac{37}{6}$ $\frac{32}{14}$ $\frac{29}{20}$ $\frac{18}{33}$

$\frac{63}{23}$ $\frac{58}{22}$ $\frac{54}{14}$ $\frac{61}{13}$ $\frac{58}{11}$ $\frac{47}{9}$ $\frac{41}{4.1}$ $\frac{45}{7}$ $\frac{43}{13}$ $\frac{35}{15}$ $\frac{25}{24}$ $\frac{22}{33}$

$\frac{55}{23}$ $\frac{52}{20}$ $\frac{53}{11}$ $\frac{44}{7}$ $\frac{43}{4.3}$ $\frac{44}{4}$ $\frac{48}{10}$ $\frac{46}{13}$ $\frac{40}{15}$ $\frac{28}{33}$

$\frac{56}{33}$ $\frac{51}{20}$ $\frac{54}{14}$ $\frac{62}{11}$ $\frac{54}{10}$ $\frac{47}{4.7}$ $\frac{52}{8}$ $\frac{47}{11}$ $\frac{35}{21}$ $\frac{35}{33}$

$\frac{65}{33}$ $\frac{63}{26}$ $\frac{54}{17}$ $\frac{70}{12}$ $\frac{63}{11}$ $\frac{56}{5.6}$ $\frac{56}{6}$ $\frac{57}{15}$ $\frac{49}{18}$ $\frac{40}{22}$ $\frac{43}{33}$

$\frac{79}{33}$ $\frac{76}{25}$ $\frac{74}{17}$ $\frac{72}{10}$ $\frac{64}{7}$ $\frac{58}{5.8}$ $\frac{67}{10}$ $\frac{73}{13}$ $\frac{67}{17}$ $\frac{58}{23}$ $\frac{57}{33}$

$\frac{76}{33}$ $\frac{73}{21}$ $\frac{73}{14}$ $\frac{76}{11}$ $\frac{68}{8}$ $\frac{5.8}{5.8}$ $\frac{59}{6}$ $\frac{66}{8}$ $\frac{72}{13}$ $\frac{65}{18}$ $\frac{57}{23}$ $\frac{62}{33}$

$\frac{75}{33}$ $\frac{66}{23}$ $\frac{58}{16}$ $\frac{68}{11}$ $\frac{61}{8}$ $\frac{5.6}{5.6}$ $\frac{68}{8}$ $\frac{52}{11}$ $\frac{49}{18}$ $\frac{41}{33}$

$\frac{74}{33}$ $\frac{65}{21}$ $\frac{60}{12}$ $\frac{64}{11}$ $\frac{57}{8}$ $\frac{4.9}{4.9}$ $\frac{48}{8}$ $\frac{52}{11}$ $\frac{46}{17}$ $\frac{38}{24}$ $\frac{33}{33}$

$\frac{76}{33}$ $\frac{70}{21}$ $\frac{66}{16}$ $\frac{71}{13}$ $\frac{60}{5}$ $\frac{5.1}{5.1}$ $\frac{55}{6}$ $\frac{65}{12}$ $\frac{48}{11}$ $\frac{39}{33}$

Station	+or-	Elev.	Mail
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	+50	30.6	
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35+00		31.9	
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	+50	31.2 29.2	
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36+00		30.1 28.1	
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	+50	29.3	
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37+00		29.5	
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	+50	30.2	
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38+00		30.6	
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	+50	30.3	
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39+00		27.9	
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	+50	25.9	
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40+00		24.7	
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	+50	23.6	
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2-3-27

Lt.

S

Rt.

A.L. Wisniewski

Cold-Windy

0.5
H.M.
P.B.
R.B.

60	45	53	53	45		43	4.7	41	39	35
33	17	13	10	5	44	5	8	14	23	33

47	40	32	42	34		25	40	35	30	34
33	18	11	10	6	2.9	12	14	16	21	33

46	34	40	47	40		33	43	26	3.2	34
33	16	11	8	6	3.4	8	14	16	21	33

56	56	46	52	51	50		48	49	42	36
33	21	17	12	9	6	46	8	14	17	33

63	52	54	60	64	57		58	59	50	24	23
33	24	18	12	9	6	5.4	8	15	18	25	33

62	54	45	60	58	54		49	57	50	53
33	21	18	11	7	3	5.2	11	15	23	33

72	64	49	54	50		45	46	42		
33	25	19	14	7	4.5	11	21	33		

75	58	43	44	45		40	43	26	1.9	13
33	25	19	14	9	4.1	8	12	17	25	33

102	83	69	74	76		73	69	79	80	40	35
33	21	19	12	6	7.4	8	13	14	18	25	35

114	98	84	92	28	29		28	25	82	80	7.7
33	21	17	14	10	6	9.9	7	14	14	19	33

81	63	61	60	57		54	49	50	50	46
33	19	14	10	34	5.3	7	12	16	21	33

87	77	70	73			67	60	60	64	
33	22	14	10		6.3	9	14	21	33	

24	73	83	82	75		76	80	73	72	
33	17	10	6	3	7.4	12	15	20	33	

Station	tor-	Elev	Soil
41+00		22.9	
	+50	23.1	
42+00		24.0	
	+50	25.1	
43+00		26.8	
	+50	28.3	
44+00		27.2	
	+50	25.9	
45+00		28.5	
	+50	28.7	
46+00		25.7	
	+50	25.7	
47+00		25.2	

2-3-27 Lt.
cold windy

2

Rt.

W. Johnson
D.S.
F.A.
P.M.
P.D.

$\frac{87}{33}$ $\frac{84}{19}$ $\frac{85}{10}$ $\frac{85}{5}$ 80 8 82 $\frac{87}{13}$ $\frac{76}{16}$ $\frac{73}{21}$ $\frac{73}{33}$

$\frac{81}{33}$ $\frac{83}{20}$ $\frac{85}{12}$ $\frac{80}{4}$ 79 7 82 $\frac{87}{18}$ $\frac{88}{24}$ $\frac{88}{33}$

$\frac{60}{33}$ $\frac{60}{16}$ $\frac{55}{12}$ $\frac{66}{8}$ $\frac{72}{5}$ 70 6 69 $\frac{68}{10}$ $\frac{70}{15}$ $\frac{74}{21}$ $\frac{80}{33}$

$\frac{46}{33}$ $\frac{48}{18}$ $\frac{43}{8}$ $\frac{57}{2}$ 5.8 8 5.8 $\frac{58}{8}$ $\frac{53}{15}$ $\frac{53}{25}$ $\frac{61}{33}$

$\frac{25}{33}$ $\frac{28}{12}$ $\frac{28}{10}$ $\frac{40}{4}$ 43 7 41 $\frac{42}{10}$ $\frac{45}{23}$ $\frac{40}{27}$ $\frac{40}{33}$

$\frac{25}{33}$ $\frac{25}{12}$ $\frac{25}{9}$ 2.8 8 27 $\frac{28}{13}$ $\frac{21}{25}$ $\frac{34}{33}$

$\frac{28}{33}$ $\frac{28}{20}$ $\frac{30}{7}$ 36 6 37 $\frac{40}{15}$ $\frac{41}{25}$ $\frac{48}{33}$

$\frac{38}{33}$ $\frac{49}{12}$ 4.9 8 46 $\frac{52}{18}$ $\frac{39}{25}$ $\frac{64}{33}$

$\frac{45}{33}$ $\frac{50}{13}$ $\frac{48}{5}$ 34 11 5.3 $\frac{56}{19}$ $\frac{61}{33}$

$\frac{43}{33}$ $\frac{47}{19}$ $\frac{51}{10}$ 5.1 8 47 $\frac{56}{15}$ $\frac{54}{24}$ $\frac{60}{33}$

$\frac{37}{33}$ $\frac{39}{20}$ $\frac{41}{10}$ $\frac{47}{5}$ 5.1 7 46 $\frac{49}{11}$ $\frac{55}{15}$ $\frac{55}{20}$ $\frac{56}{26}$ $\frac{58}{33}$

$\frac{40}{33}$ $\frac{40}{23}$ $\frac{43}{18}$ $\frac{47}{8}$ 5.1 12 5.7 $\frac{57}{22}$ $\frac{57}{33}$

$\frac{57}{33}$ $\frac{53}{18}$ $\frac{56}{8}$ $\frac{58}{3}$ 5.6 7 5.4 $\frac{54}{10}$ $\frac{61}{11}$ $\frac{52}{23}$ $\frac{57}{33}$

Station	+0.1-	Elev.	Soil
	+50	24.1	
48+00		23.1	
	+50	22.5	
49+00		22.1	
	+50	22.0	
50+00		21.8	
	+50	20.9	
51+00		20.9	
	+50	21.6	
52+00		22.7	
	+50	23.5	
53+00		22.1	
	+50	20.4	

2-3-4-27

14.

2

Rt.

Wishuson

0.3
1.0
1.8
2.8

$\frac{65}{33}$ $\frac{64}{22}$ $\frac{63}{14}$ $\frac{62}{7}$ $\frac{61}{6}$ $\frac{60}{11}$ $\frac{59}{21}$ $\frac{58}{26}$ $\frac{57}{33}$

$\frac{36}{33}$ $\frac{35}{21}$ $\frac{34}{9}$ $\frac{33}{7}$ $\frac{32}{41}$ $\frac{31}{5}$ $\frac{30}{14}$ $\frac{29}{19}$ $\frac{28}{25}$ $\frac{27}{32}$

$\frac{49}{33}$ $\frac{48}{28}$ $\frac{47}{16}$ $\frac{46}{8}$ $\frac{45}{4.7}$ $\frac{44}{7}$ $\frac{43}{18}$ $\frac{42}{27}$ $\frac{41}{33}$

$\frac{49}{22}$ $\frac{48}{23}$ $\frac{47}{15}$ $\frac{46}{6}$ $\frac{45}{5.0}$ $\frac{44}{7}$ $\frac{43}{13}$ $\frac{42}{18}$ $\frac{41}{22}$ $\frac{40}{32}$

$\frac{55}{32}$ $\frac{54}{20}$ $\frac{53}{15}$ $\frac{52}{8}$ $\frac{51}{5}$ $\frac{50}{6.1}$ $\frac{49}{6}$ $\frac{48}{14}$ $\frac{47}{20}$ $\frac{46}{28}$ $\frac{45}{32}$

h.o. $\frac{60}{33}$ $\frac{60}{21}$ $\frac{61}{10}$ $\frac{62}{63}$ $\frac{63}{7}$ $\frac{64}{19}$ $\frac{65}{32}$

$\frac{73}{32}$ $\frac{72}{22}$ $\frac{71}{11}$ $\frac{70}{7.2}$ $\frac{69}{7.2}$ $\frac{68}{9}$ $\frac{67}{15}$ $\frac{66}{16}$ $\frac{65}{20}$ $\frac{64}{25}$ $\frac{63}{33}$

$\frac{70}{32}$ $\frac{70}{19}$ $\frac{72}{7}$ $\frac{73}{7.3}$ $\frac{74}{3}$ $\frac{75}{4}$ $\frac{76}{12}$ $\frac{77}{15}$ $\frac{78}{18}$ $\frac{79}{21}$ $\frac{80}{33}$

$\frac{66}{32}$ $\frac{67}{29}$ $\frac{68}{19}$ $\frac{69}{10}$ $\frac{70}{6.5}$ $\frac{71}{7}$ $\frac{72}{21}$ $\frac{73}{22}$ $\frac{74}{28}$ $\frac{75}{32}$

$\frac{63}{33}$ $\frac{48}{18}$ $\frac{50}{12}$ $\frac{53}{8}$ $\frac{54}{4}$ $\frac{55}{5.4}$ $\frac{56}{7}$ $\frac{57}{13}$ $\frac{58}{17}$ $\frac{59}{20}$ $\frac{60}{25}$ $\frac{61}{30}$ $\frac{62}{33}$

h.o. $\frac{56}{33}$ $\frac{52}{21}$ $\frac{52}{14}$ $\frac{52}{9}$ $\frac{52}{4.6}$ $\frac{53}{5}$ $\frac{54}{6}$ $\frac{55}{7}$ $\frac{56}{7}$ $\frac{57}{21}$ $\frac{58}{32}$

$\frac{64}{33}$ $\frac{60}{20}$ $\frac{62}{9}$ $\frac{60}{5}$ $\frac{60}{6.0}$ $\frac{61}{3}$ $\frac{62}{4}$ $\frac{63}{7}$ $\frac{64}{16}$ $\frac{65}{24}$ $\frac{66}{32}$

$\frac{70}{32}$ $\frac{71}{15}$ $\frac{71}{9}$ $\frac{71}{4}$ $\frac{71}{7.7}$ $\frac{72}{4}$ $\frac{73}{9}$ $\frac{74}{14}$ $\frac{75}{21}$ $\frac{76}{24}$ $\frac{77}{33}$

Station	Cor-	Elev.	Soil
54+00		18.6 <u>18.9</u>	
+50		16.6	
55+00		15.9	
+50		15.3	
56+00		15.3	
+50		16.0	
57+00		15.8	
+50		15.8	
58+00		16.0	
+50		15.6	
59+00		15.3	
+50		15.3	
60+00		15.0	

2-4-27

Lt.

\$

Rt

11/5/2027

7.17
75.
P.B.

10. $\frac{8.8}{33}$ $\frac{9.0}{13}$ $\frac{9.4}{8}$ $\frac{9.8}{5}$ 9.5 $\frac{10.0}{4}$ $\frac{10.4}{7}$ $\frac{8.8}{12}$ $\frac{8.6}{7.9}$ $\frac{8.2}{27}$ $\frac{8.5}{33}$

$\frac{11.0}{33}$ $\frac{11.0}{15}$ $\frac{11.5}{5}$ 11.5 $\frac{11.5}{7}$ $\frac{11.2}{12}$ $\frac{11.5}{16}$ $\frac{11.5}{21}$ $\frac{11.0}{33}$

$\frac{5.0}{33}$ $\frac{5.5}{18}$ $\frac{5.5}{8}$ 4.8 $\frac{4.5}{9}$ $\frac{4.8}{10}$ $\frac{5.5}{14}$ $\frac{6.0}{17}$ $\frac{6.6}{25}$ $\frac{6.0}{33}$

$\frac{5.2}{33}$ $\frac{5.7}{14}$ $\frac{5.7}{7}$ $\frac{6.0}{4}$ 5.5 $\frac{5.0}{5}$ $\frac{5.4}{14}$ $\frac{6.0}{18}$ $\frac{6.2}{20}$ $\frac{6.4}{21}$ $\frac{6.8}{33}$

$\frac{5.2}{33}$ $\frac{5.3}{14}$ $\frac{5.3}{3}$ 5.4 $\frac{4.7}{8}$ $\frac{4.7}{12}$ $\frac{5.2}{14}$ $\frac{5.5}{19}$ $\frac{5.2}{24}$ $\frac{4.6}{33}$

$\frac{4.2}{33}$ $\frac{4.4}{13}$ $\frac{4.6}{4}$ 4.7 $\frac{4.2}{4}$ $\frac{4.0}{8}$ $\frac{4.2}{11}$ $\frac{5.0}{15}$ $\frac{4.2}{18}$ $\frac{3.6}{33}$

$\frac{5.3}{33}$ $\frac{5.3}{15}$ $\frac{5.2}{3}$ $\frac{5.0}{2}$ 4.8 $\frac{4.4}{8}$ $\frac{5.2}{13}$ $\frac{4.6}{17}$ $\frac{4.6}{23}$ $\frac{4.5}{33}$

$\frac{5.6}{33}$ $\frac{5.6}{15}$ $\frac{5.5}{6}$ $\frac{5.2}{4}$ 4.8 $\frac{5.0}{7}$ $\frac{5.5}{12}$ $\frac{5.1}{13}$ $\frac{5.0}{16}$ $\frac{4.8}{21}$ $\frac{4.6}{33}$

$\frac{5.5}{33}$ $\frac{6.0}{20}$ $\frac{6.0}{11}$ $\frac{5.0}{6}$ 4.8 $\frac{5.0}{5}$ $\frac{5.7}{7}$ $\frac{6.2}{8}$ $\frac{6.2}{17}$ $\frac{6.2}{23}$ $\frac{5.8}{33}$

$\frac{5.6}{33}$ $\frac{6.2}{24}$ $\frac{6.4}{16}$ $\frac{6.0}{10}$ $\frac{5.1}{6}$ 4.8 $\frac{5.6}{5}$ $\frac{6.5}{8}$ $\frac{6.7}{16}$ $\frac{6.8}{23}$ $\frac{7.0}{33}$

$\frac{6.2}{33}$ $\frac{6.8}{26}$ $\frac{6.5}{15}$ $\frac{6.0}{10}$ 5.3 $\frac{5.6}{4}$ $\frac{6.5}{8}$ $\frac{4.4}{15}$ $\frac{6.2}{20}$ $\frac{5.1}{33}$

$\frac{5.8}{33}$ $\frac{5.8}{17}$ $\frac{6.0}{11}$ $\frac{5.4}{8}$ 5.4 $\frac{5.4}{3}$ $\frac{6.2}{4}$ $\frac{6.3}{6}$ $\frac{5.8}{7}$ $\frac{5.8}{15}$ $\frac{6.4}{17}$ $\frac{6.0}{19}$

$\frac{5.7}{33}$ $\frac{6.0}{20}$ $\frac{6.0}{15}$ $\frac{5.6}{10}$ 5.7 $\frac{5.7}{5}$ $\frac{6.4}{15}$ $\frac{7.0}{18}$ $\frac{6.0}{21}$ $\frac{6.4}{24}$

(5.5 5.2
21 33

Station	Top-	Elev.	3011
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150		15.2	
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61+00		13.6	
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150		10.6	
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62+00		08.6	
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150		07.2	
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63+00		06.4	
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150		06.0	
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64+00		06.2	
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150		07.8	
-----	--	------	--

65+00		08.7	
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150		08.5	
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66+00		07.5	
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150		07.4	
-----	--	------	--

2-4-27

H.

F

R4

W/5/10/5/11
0.5
2.1
1.8
1.8

47	54	55	53	58	62	66	56	52	
33	22	14	8	55	4	13	15	18	33

67	67	74	70	72	73	62	62	67	62	50	
33	20	11	6	70	3	6	7	12	14	18	21

114	107	107	105	104	96	74	82	84	
33	23	14	7	101	4	6	17	24	33

87	84	87	85	77	77	78	74	70	73	71	
33	21	13	8	6	73	6	12	16	21	25	33

90	90	90	88	90	90	90	86	82	84	85	
33	25	19	12	5	88	4	8	11	16	22	33

96	102	102	10.8	10.8	96	100	10.8	105	108	110	
33	25	19	13	10	7	96	6	11	15	22	33

116	118	117	115	10.4	10.2	98	10.4	11.8	12.2	12.5	
33	28	21	13	10	6	5	9.8	5	10	15	33

110	106	107	100	102	110	105	105	
33	15	10	5	7.8	7	12	17	33

70	74	76	85	82	87	78	77	67	
33	19	13	5	82	7	11	12	18	33

55	61	64	67	70	74	70	73	80	80	70	70	
33	26	21	14	7	3	7.2	5	10	13	20	28	33

5.2	56	63	70	72	73	84	84	78	
33	28	18	8	3	7.6	5	15	22	33

48	57	65	73	86	88	85	87	
33	21	11	1	85	5	12	18	33

54	64	73	77	92	10.8	110	113	110	
33	21	16	9	8.7	5	8	14	22	23

Sta/Sec

-01-

Elev.

301

67+00

05.8

+50

05.4

68+00

05.0

+50

07.0

69+00

08.4

+50

08.6

70+00

09.8

J

+50

08.4

71+00

06.0

+50

05.7

72+00

05.9

+50

06.2

73+00

06.4
06.3

Station	100-	Elev.	Soil
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	+50	06.9	
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74+00		07.5	
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	+50	07.2	
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75+00		06.0	
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	+50	05.9	
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76+00		05.0	
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	+50	04.2	
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77+00		04.2	
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	+50	04.2	
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78+00		04.8	
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	+50	05.8	
--	-----	------	--

79+00		06.9	
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	+50	07.7	
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Wilschusen
0.5
4.11
9.3
9.8

2-4-27
Cold winds

14.									
106	100	92	90	94	90	80	72		
33	20	10	5	92	4	8	17	33	

90	70	64		70	52	45			
33	13	9	6.4	13	18	33			

80	68	64		74	72	53	42	37	
33	16	8	6.6	9	17	23	28	33	L.O.

74	70	68	82	85	77	78	80	75	65	38	
33	27	25	22	17	11	8.0	7	11	15	23	33

70	80	92	97	82		83	80	65	50	
33	23	18	14	8	8.0	8	19	30	33	

L.O.	11.6	10.4	10.0	9.2		8.7	7.0	6.5		
	33	24	14	8	8.8	9	10	23		

11.6	11.6	11.7	11.4	10.4		9.7	10.4	9.7	9.0	8.0
33	14	19	10	6	9.7	5	9	17	10	33

L.O.

12.5	12.4	12.2	11.6	10.3		10.0	11.0	11.2	10.8	11.0	10.0	9.5
33	23	19	13	6	10.0	6	10	11	17	11	22	33

12.3	12.2	12.0	10.2			10.1	10.8	11.0	10.6	10.6	7.8	
33	22	11	6	10.1	6	9	13	18	22	33		

10.5	10.0	9.8				10.0	7.8	9.2				
33	21	9	9.5	8	12	33						

8.0	8.2	9.4	8.8	8.4	8.4		8.1	7.5	7.6			
33	25	14	20	14	4	8.4	6	21	33			

7.3	7.2	7.7	7.5			7.2	7.5					
33	22	18	13	7.2	21	33						

6.4	6.4					6.4	6.8					
33	10	6.3	23	33								

Station	+or-	Elev.	Soil
80+00		06.7	
	+50	05.5	
81+00		05.3	
	+37	05.2	
	+41	04.6	
	+50	05.4	
82+00		06.6	
	+50	07.4	
83+00		08.2	
	+50	09.4	
84+00		09.2	
	+50	07.5	
85+00		06.4	

2-4-27
Col. Windy Lt.

9.

84

W. W. Johnson
D.S.
P.B.
H.M.
P.B.

$\frac{76}{33}$ $\frac{76}{20}$ 74 $\frac{76}{18}$ $\frac{76}{33}$

8.8 $\frac{70}{15}$ 84 $\frac{84}{19}$ $\frac{84}{33}$

$\frac{77}{33}$ $\frac{90}{25}$ $\frac{92}{17}$ $\frac{86}{11}$ 8.8 $\frac{86}{20}$ $\frac{86}{33}$

$\frac{87}{33}$ $\frac{80}{20}$ $\frac{87}{8}$ $\frac{87}{3}$ 8.8 $\frac{86}{5}$ $\frac{84}{23}$ $\frac{83}{33}$

$\frac{98}{33}$ $\frac{93}{28}$ $\frac{95}{19}$ $\frac{99}{10}$ $\frac{105}{5}$ 11.1 $\frac{105}{4}$ $\frac{101}{9}$ $\frac{101}{16}$ $\frac{100}{33}$

10.4 $\frac{100}{28}$ $\frac{95}{24}$ $\frac{94}{14}$ $\frac{96}{6}$ 10.5 $\frac{11}{4}$ $\frac{10.6}{9}$ $\frac{9.6}{17}$ $\frac{9.6}{33}$

$\frac{83}{33}$ $\frac{89}{25}$ $\frac{99}{21}$ $\frac{94}{16}$ $\frac{90}{8}$ 9.1 $\frac{97}{4}$ $\frac{10.1}{8}$ $\frac{10.1}{14}$ $\frac{9.6}{20}$ $\frac{9.3}{33}$

$\frac{6.3}{33}$ $\frac{71}{23}$ $\frac{8.7}{19}$ $\frac{8.6}{11}$ $\frac{8.6}{6}$ 8.6 $\frac{8.9}{6}$ $\frac{9.5}{11}$ $\frac{9.7}{16}$ $\frac{9.7}{25}$ $\frac{9.5}{33}$

$\frac{5.2}{33}$ $\frac{56}{23}$ $\frac{75}{21}$ $\frac{79}{18}$ $\frac{77}{13}$ $\frac{76}{6}$ 7.5 $\frac{8.1}{9}$ $\frac{8.7}{14}$ $\frac{8.5}{21}$ $\frac{8.5}{33}$

$\frac{54}{33}$ $\frac{44}{23}$ $\frac{77}{20}$ $\frac{70}{18}$ $\frac{6.7}{11}$ 6.8 $\frac{7.2}{7}$ $\frac{7.7}{11}$ $\frac{7.5}{16}$ $\frac{7.7}{23}$ $\frac{6.7}{29}$ $\frac{6.7}{33}$

$\frac{5.9}{33}$ $\frac{5.1}{23}$ $\frac{6.6}{21}$ $\frac{7.2}{16}$ $\frac{6.6}{6}$ 6.6 $\frac{7.1}{10}$ $\frac{7.9}{13}$ $\frac{7.3}{17}$ $\frac{6.3}{25}$ $\frac{6.4}{33}$

$\frac{7.5}{33}$ $\frac{6.7}{24}$ $\frac{6.8}{19}$ $\frac{8.3}{16}$ $\frac{8.3}{12}$ 8.3 $\frac{7.9}{6}$ $\frac{8.3}{15}$ $\frac{7.8}{24}$ $\frac{7.8}{33}$

$\frac{9.4}{33}$ $\frac{9.2}{26}$ $\frac{9.9}{22}$ $\frac{10.5}{16}$ $\frac{9.7}{12}$ 9.3 $\frac{9.9}{11}$ $\frac{9.5}{16}$ $\frac{9.2}{23}$ $\frac{9.3}{33}$

Station	TOR-	Elev.	Soil
	+50	05.7	
86+00		05.6	
	+50	05.6	
87+00		05.4	
	+50	04.8	
88+00		03.8	
	+50	02.4	
89+00		01.1	
	+50	99.9	
90+00		99.0	
	+50	98.8	
91+00		99.0	
	+50	99.3	

2-4-27

4. ?

4

87.

W. Shusen
05.
4.8
4.11
P.B

$\frac{10.8}{33}$ $\frac{10.6}{25}$ $\frac{11.1}{4}$ $\frac{11.9}{20}$ $\frac{10.9}{11}$ $\frac{10.3}{7}$ $\frac{10.4}{10}$ $\frac{11.1}{10}$ $\frac{11.7}{17}$ $\frac{10.7}{33}$

$\frac{5.8}{33}$ $\frac{6.1}{24}$ $\frac{6.7}{21}$ $\frac{6.6}{18}$ $\frac{5.5}{13}$ $\frac{4.8}{8}$ $\frac{4.8}{8}$ $\frac{6.2}{11}$ $\frac{6.3}{18}$ $\frac{6.0}{21}$ $\frac{5.3}{33}$

$\frac{5.3}{33}$ $\frac{5.7}{25}$ $\frac{5.7}{20}$ $\frac{6.7}{17}$ $\frac{5.8}{13}$ $\frac{4.7}{7}$ $\frac{4.4}{7}$ $\frac{5.0}{9}$ $\frac{5.8}{13}$ $\frac{5.4}{14}$ $\frac{5.4}{23}$ $\frac{5.1}{33}$

$\frac{4.6}{33}$ $\frac{4.6}{22}$ $\frac{5.8}{20}$ $\frac{7.6}{17}$ $\frac{6.1}{13}$ $\frac{4.6}{7}$ $\frac{4.8}{6}$ $\frac{5.7}{9}$ $\frac{6.5}{13}$ $\frac{3.7}{17}$ $\frac{3.5}{26}$ $\frac{3.8}{33}$

$\frac{5.0}{33}$ $\frac{4.9}{27}$ $\frac{5.4}{22}$ $\frac{7.8}{19}$ $\frac{7.5}{13}$ $\frac{4.9}{10}$ $\frac{5.3}{6}$ $\frac{5.3}{5.2}$ $\frac{5.5}{6}$ $\frac{6.4}{9}$ $\frac{4.2}{14}$ $\frac{3.5}{15}$ $\frac{4.2}{23}$ $\frac{4.2}{33}$

$\frac{5.7}{33}$ $\frac{5.7}{25}$ $\frac{7.3}{23}$ $\frac{8.8}{19}$ $\frac{8.7}{15}$ $\frac{6.2}{11}$ $\frac{6.3}{6}$ $\frac{6.3}{6.3}$ $\frac{7.3}{6}$ $\frac{6.7}{11}$ $\frac{4.8}{14}$ $\frac{5.1}{16}$ $\frac{5.1}{33}$

$\frac{7.7}{33}$ $\frac{7.7}{25}$ $\frac{7.6}{20}$ $\frac{7.3}{19}$ $\frac{7.4}{15}$ $\frac{7.6}{7}$ $\frac{7.7}{7.7}$ $\frac{7.4}{8}$ $\frac{8.3}{11}$ $\frac{8.3}{14}$ $\frac{6.2}{18}$ $\frac{5.8}{33}$

$\frac{9.8}{33}$ $\frac{9.4}{25}$ $\frac{9.7}{19}$ $\frac{9.5}{16}$ $\frac{8.5}{11}$ $\frac{8.7}{8}$ $\frac{8.9}{8.9}$ $\frac{9.7}{10}$ $\frac{9.2}{15}$ $\frac{7.7}{19}$ $\frac{7.6}{23}$

$\frac{7.3}{33}$ $\frac{7.1}{25}$ $\frac{6.7}{19}$ $\frac{7.8}{18}$ $\frac{6.8}{14}$ $\frac{6.9}{7}$ $\frac{7.1}{7.1}$ $\frac{7.1}{12}$ $\frac{6.7}{19}$ $\frac{6.8}{28}$ $\frac{6.8}{33}$

$\frac{8.2}{33}$ $\frac{8.5}{26}$ $\frac{8.8}{20}$ $\frac{8.8}{14}$ $\frac{7.9}{9}$ $\frac{8.1}{8.1}$ $\frac{8.1}{18}$ $\frac{8.4}{23}$ $\frac{8.4}{33}$

$\frac{10.5}{33}$ $\frac{10.8}{30}$ $\frac{10.2}{22}$ $\frac{10.0}{14}$ $\frac{9.6}{7}$ $\frac{8.3}{7}$ $\frac{8.1}{8.1}$ $\frac{7.1}{9}$ $\frac{7.4}{14}$ $\frac{7.4}{26}$ $\frac{7.4}{33}$

$\frac{11.1}{33}$ $\frac{10.9}{25}$ $\frac{11.0}{20}$ $\frac{10.6}{13}$ $\frac{8.1}{8}$ $\frac{7.9}{7.9}$ $\frac{8.2}{9}$ $\frac{10.0}{12}$ $\frac{11.3}{17}$ $\frac{11.2}{19}$ $\frac{10.1}{20}$ $\frac{9.6}{33}$

$\frac{9.7}{33}$ $\frac{9.1}{22}$ $\frac{8.8}{18}$ $\frac{9.1}{12}$ $\frac{7.6}{7.6}$ $\frac{7.7}{8}$ $\frac{9.7}{13}$ $\frac{10.6}{16}$ $\frac{10.4}{18}$ $\frac{8.7}{20}$ $\frac{9.5}{33}$

Station	for-	Elev.	Soil
94+00		00.0	
+50		01.7	
94+00		01.8	
+50		01.3	
94+00		01.1	
+50		01.1	
95+00		00.6	
+25		00.6	
+50		01.7	
96+00		02.6	
+50		04.9	
97+00		07.4	
+50		08.5	

2-4-5-27 Lt.

7

xt.

Wisthusen

03
02
01
00

$\frac{44}{33} \frac{67}{17} \frac{48}{8} \quad 70 \quad 72 \frac{80}{10} \frac{93}{14} \frac{76}{17} \frac{87}{18} \frac{84}{22} \frac{84}{33}$

$\frac{31}{33} \frac{42}{33} \frac{57}{17} \frac{65}{15} \frac{58}{10} \quad 55 \frac{8}{8} \frac{23}{14} \frac{76}{20} \frac{78}{22} \frac{21}{27} \frac{78}{33}$

$\frac{26}{33} \frac{29}{28} \frac{40}{21} \frac{60}{17} \frac{62}{14} \frac{52}{9} \quad 51 \frac{61}{9} \frac{13}{13} \frac{72}{15} \frac{72}{18} \frac{84}{21} \frac{82}{24} \frac{63}{33}$

$\frac{56}{33} \frac{56}{26} \frac{64}{22} \frac{65}{20} \frac{62}{15} \frac{58}{10} \quad 57 \frac{60}{6} \frac{70}{7} \frac{92}{14} \frac{74}{16} \frac{78}{18} \frac{72}{22} \frac{63}{33}$

$\frac{94}{33} \frac{75}{28} \frac{93}{23} \frac{71}{18} \frac{75}{14} \frac{61}{11} \frac{52}{4} \quad 58 \frac{64}{6} \frac{84}{8} \frac{96}{12} \frac{72}{17} \frac{81}{19} \frac{77}{24} \frac{68}{33}$

$\frac{117}{33} \frac{117}{31} \frac{117}{24} \frac{115}{21} \frac{105}{20} \frac{85}{15} \frac{80}{7} \quad 93 \frac{113}{4} \frac{123}{10} \frac{115}{16} \frac{115}{33}$

$\frac{100}{33} \frac{97}{30} \frac{78}{24} \frac{85}{16} \frac{82}{11} \quad 70 \frac{108}{7} \frac{110}{10} \frac{110}{17} \frac{116}{33}$

$\frac{92}{33} \frac{94}{30} \frac{95}{23} \frac{82}{15} \frac{80}{8} \quad 90 \frac{96}{6} \frac{106}{19} \frac{106}{33}$

$\frac{85}{33} \frac{85}{30} \frac{85}{19} \frac{78}{15} \frac{75}{8} \frac{80}{3} \quad 85 \frac{70}{5} \frac{90}{11} \frac{94}{27} \frac{100}{33}$

$\frac{54}{33} \frac{55}{30} \frac{75}{24} \frac{64}{20} \frac{62}{12} \frac{62}{7} \frac{64}{4} \quad 70 \frac{76}{6} \frac{87}{21} \frac{88}{23}$

$\frac{27}{33} \frac{30}{30} \frac{43}{27} \frac{45}{23} \frac{38}{17} \frac{40}{12} \frac{40}{6} \frac{42}{4} \quad 46 \frac{57}{8} \frac{63}{16} \frac{68}{33}$

$\frac{40}{33} \frac{40}{28} \frac{45}{27} \frac{70}{25} \frac{90}{20} \frac{27}{14} \frac{77}{10} \quad 74 \frac{87}{8} \frac{82}{11} \frac{85}{21} \frac{94}{33}$

$\frac{10}{30} \frac{10}{15} \frac{09}{33} \frac{35}{29} \frac{62}{16} \frac{75}{21} \frac{68}{14} \frac{6}{9} \quad 70 \frac{65}{5} \frac{52}{14} \frac{64}{26} \frac{68}{33}$

Station Elev. Soil

98+00 07.1

+50 05.2

99+00 03.9

+50 03.5

100+00 04.4

+50 04.1
04.0

101+00 03.7

+50 03.5
03.9

102+00 04.3
03.3

+50 06.7
04.9

103+00 09.0
06.9

+50 10.0
09.0

104+00 10.7
0.0

2-5-27

Lt.

F

Rt.

Wishuson
D.S.
H.B.
H.M.P.B.

42	42	48	50	70	86	80							
40	23	28	24	21	18	12	8.4	2	6	12	26	33	

Cold

102	100	107	104	100									
33	30	22	17	11	10.4	4	10.7	4	10.4	10.4	10.6	23	33

85	87	84	64	60									
33	28	21	14	6	6.5	6	80	80	75	75	26	33	

88	88	88	68	62	62									
33	28	20	15	7	1	6.8	4	8	15	33	77	77	73	70

72	75	80	84	63	62									
33	27	23	21	16	3	6.0	8	16	29	33	68	60	57	57

72	74	81	80	62	60									
33	27	23	20	13	3	6.2	6	12	11	33	68	65	62	6.2

84	82	65	62											
33	27	17	8	6.8	6	16	75	70	70	23	23			

65	66	55	55											
33	24	16	4	6.8	4	12	75	70	60	8.8	21	33		

37	52	55	46	50										
33	28	25	16	3	5.4	5	5.8	50	57	5.7	30	33		

98	117	115	107	107										
33	31	26	14	4	11.0	4	11.2	10.2	10.5	10.5	22	33		

97	95	92	85											
33	25	13	4	9.0	8	18	87	85	8.8	33				

90	85	85	81											
33	28	19	5	8.0	3	18	77	74	7.0	33				

6	80	82	80											
33	26	10	9	7.2	8	13	72	70	64	6.2	26	33		

Station +/- Elev. Soil

150 11.0

105+00 11.7

+50 12.4

106+00 14.4

+50 16.8

107+00 18.7

+50 19.6

2 Curves

108+00 19.4

+50 18.8

109+00 18.0

+50 17.8

110+00 17.4

+50 17.8

2-5-27

Lt.

±

Rt.

Wishusen
D.S.
H.B.
H.M.
P.B.

$\frac{82}{33} \frac{77}{15} \frac{72}{9}$ $\frac{70}{48} \frac{72}{3} \frac{72}{6}$ $\frac{72}{7} \frac{70}{15} \frac{62}{33}$

$\frac{65}{33} \frac{70}{21} \frac{64}{9}$ $\frac{65}{64} \frac{64}{5} \frac{60}{11} \frac{50}{17} \frac{50}{33}$

Lo $\frac{43}{33} \frac{47}{26} \frac{55}{18} \frac{50}{17} \frac{45}{4}$ $\frac{60}{56} \frac{58}{4} \frac{56}{10} \frac{52}{14} \frac{52}{33}$ 10

$\frac{24}{33} \frac{24}{30} \frac{30}{18} \frac{32}{10}$ $\frac{42}{36} \frac{45}{5} \frac{37}{9} \frac{37}{11} \frac{32}{19} \frac{32}{33}$

Lo $\frac{84}{33} \frac{84}{26} \frac{82}{20} \frac{82}{16} \frac{80}{12} \frac{80}{81}$ $\frac{88}{5} \frac{90}{10} \frac{83}{23} \frac{83}{33}$

$\frac{58}{33} \frac{60}{26} \frac{60}{10} \frac{60}{13} \frac{62}{5}$ $\frac{64}{61} \frac{65}{9} \frac{66}{23} \frac{66}{33}$ 10

$\frac{37}{33} \frac{55}{30} \frac{56}{17} \frac{52}{8}$ $\frac{53}{53} \frac{57}{5} \frac{53}{13} \frac{53}{33}$

$\frac{62}{33} \frac{65}{25} \frac{62}{18} \frac{48}{12} \frac{52}{6}$ $\frac{52}{54} \frac{60}{8} \frac{47}{15} \frac{47}{33}$

$\frac{70}{33} \frac{68}{25} \frac{67}{19} \frac{55}{12}$ $\frac{60}{60} \frac{58}{5} \frac{64}{11} \frac{68}{16} \frac{67}{17} \frac{63}{20} \frac{56}{33}$

$\frac{80}{33} \frac{78}{18} \frac{68}{7}$ $\frac{70}{70} \frac{73}{8} \frac{70}{13} \frac{70}{33}$

$\frac{70}{33} \frac{87}{24} \frac{87}{18} \frac{73}{6}$ $\frac{74}{70} \frac{78}{11} \frac{70}{19} \frac{70}{33}$

$\frac{100}{33} \frac{97}{26} \frac{92}{17} \frac{87}{11} \frac{77}{6}$ $\frac{70}{72} \frac{80}{9} \frac{80}{17} \frac{80}{22} \frac{77}{33}$

$\frac{84}{33} \frac{64}{24} \frac{84}{11} \frac{77}{9}$ $\frac{72}{70} \frac{90}{4} \frac{84}{12} \frac{80}{19} \frac{80}{33}$

Station + or - Elev. Soil

192

^{19.0}
16.3

111 + 00

^{19.0}
16.3

+50

18.3 ^{18.3}

112 + 00

20.3

+70

21.6

+90

19.4

+50

20.4

113 + 00

22.5

+53.46

23.2

2-5-27

14.

4

14.

Wilshusen
D.S.
A.B.
P.M.
P.B.

76	76	67	66	70	86	86	86
33	31	19	13	6	6	13	33

74	66	66	70	82	87	88	88	85	85
33	28	15	10	4	22	96	4	10	14

60	70	66	64	70	77
33	27	22	16	68	15

67	74	86	88	71	70	78
33	27	21	18	12	70	24

62	65	76	78	74	60	64
33	16	12	4	2	58	15

57	57	61	62	83	50	55	55
33	28	14	6	78	3	9	26

37	37	60	80	60	40	50	54
33	19	1	67	5	11	12	24

68	73	50	47	51	75	66	50	50
33	28	10	6	48	12	10	24	27

33	58	58	43	44	63	24	31
33	29	14	16	40	19	14	30

Station + or - Elev. Soil

Curve Left

107+99.24 P.C. 19.4'

108+50 18.5'

108+95 18.1'

109+00 17.0'

109+50 15.4'

110+00 13.7'

110+50 12.8'

111+00 11.0'

111+50 10.4'

112+00 09.0'

112+50 09.0'

113+00 13.0'

113+00 13.8'

+45.09 P.T. 14.71'

2-7-27

11.

~~11~~

11

Wibhuson
D.S
A.B
F.M
P.B

22 20 22 23 22 20 21
32 17 18 6 2.3 8 23 33

40 37 27 35 36 32 30
33 15 7 3.8 19 22 24 33

46 46 44 35 36 44 40 40
33 16 7 2.2 3 7 27 30 33

55 52 52 65 4.2 4.2 4.8
33 24 11 4.8 4 18 27 33

50 75 65 57 37 42
33 22 8 6.4 17 26 33

74 72 88 86 80 82
33 28 10 8.6 10 26 33

110 108 100 83 78 75
33 15 9 9.0 11 25 33

12.9 12.0 11.4 10.0 8.4 7.7
33 27 19 10.8 10 28 33

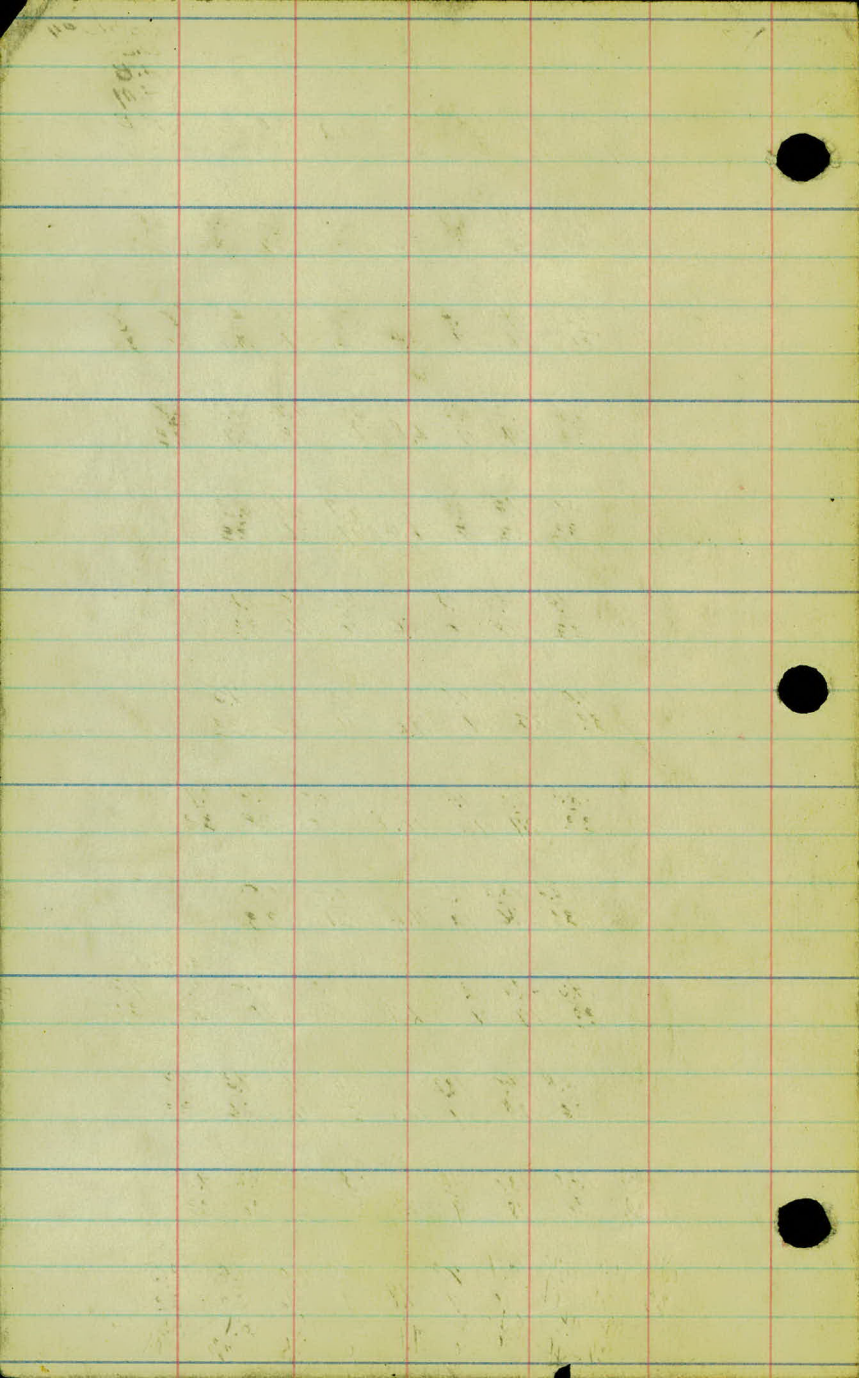
125 123 123 10.4 10.0
33 26 13 11.4 21 33

E. Road
145 145 131 12.2 12.2 7.5 7.2
33 19 9 12.7 6 10 23 33

144 140 132 9.4 9.0 7.2 7.3
33 24 9 12.6 5 14 26 33

142 140 130 110 7.8 7.7 8.2 8.3
33 30 18 9 8.4 2 16 30 33

167 104 92 8.7 7.5 7.8 7.0 11.4 12.5
33 30 17 10 7 7.6 9 26 30 33
99 93 81 78 83 98 10.7 150
33 30 10 9 10 28 33 41 T slope



NORTH CO. LINE RD.

28-63

Plans in Hand.

D.R.V.K.
W.S.M.
A.M.M.

2-27-28

- ✓ ✓ 7+10 Drive Rt. & Lt. - No culv. req.
- ✓ ✓ 9+10 Look up culv. imp. - P. 24" B. Drains Rt.
- ✓ ✓ 16+02 - P. 15" x 30' on Rt. P. 15" x 24' Lt.
- ✓ ✓ 17+00 to 22+00 - Cl. & Gr. 40 T.
- ✓ ✓ 20+00 - P. 15" x 24' C.M. Rt.
- ✓ ✓ 22+20 - Rt. - P. 15" x 24' C.M.
- ✓ ✓ 23+00 - Lt. - " "
- ✓ ✓ 29+00 to 30+00 - Cl. & Gr. 4 T.
- ✓ ✓ 33+00 - P. 24" B. - Drains Lt.
- ✓ ✓ 35+00 - Drive on Lt. - No culv. req.
- ✓ ✓ 42+00 to 46+00 - Cl. 29 T. Gr. 43 T.
- ✓ ✓ 44+57 - P. 15" x 24' C.M.
- ✓ ✓ 46+50 to 49+00 - Gr. 10 T.
- ✓ ✓ 55+00 to 56+00 - Cl. 5 T. Gr. 6 T.
- ✓ ✓ 63+50 - No culv. req.
- ✓ ✓ 64+00 - Drive on Lt. - No culv. req.
- ✓ ✓ 67+00 - ~~P. 15" x 24' C.M.~~ Drive on Rt. - No culv. req. Rt.
- ✓ ✓ 68+50 to 69+00 - Cl. & Gr. 1 T.
- ✓ ✓ 74+25 - Drive on Lt. No culv. req. P. 15" x 24' on Rt.
- ✓ ✓ 74+50 to 75+50 - Cl. 4 T. Gr. 5 T.
- ✓ ✓ 77+00 - P. 24" B. - Drains Lt.
- ✓ ✓ 81+00 - Drive on Lt. - No culv. req.
- ✓ ✓ 84+00 - " " Rt. & Lt. - " " "
- ✓

- ✓ 84-50 to 89-50 - Cl. 26F - Gr. 33T.
- ✓ 89-28 - P-15" x 24' C.M. Rt.
- ✓ 90-75 - P-24" P₃ - Drains Lt.
- ✓ 91-52 - No culv. req. on Rt. - P-15" x 24' C.M.
- ✓ 92+00 to 94+00 - Cl. 14T, Gr. 15T.
- ✓ 98+00 - No culv. req. on Rt.
- ✓ 101+00 - P-24" P₃ - Drains Lt.
- ✓ 103+30 Rt. - P-15" x 24' C.M.
- ✓ 104+57 - Lt. - " " "
- ✓ 111+00 to 112+00 - Cl. ~~3~~ 3T, Gr. 4T.
- ✓ 114-00 - P-24" P₃ - Drains Lt.