

OFFICE OF  
RAMLEY COUNTY ENGINEER

# CONSTRUCTION NOTES

NORTH CO. LINE ROAD

PROJ. - 28-63

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FIELD BOOK

360

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# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

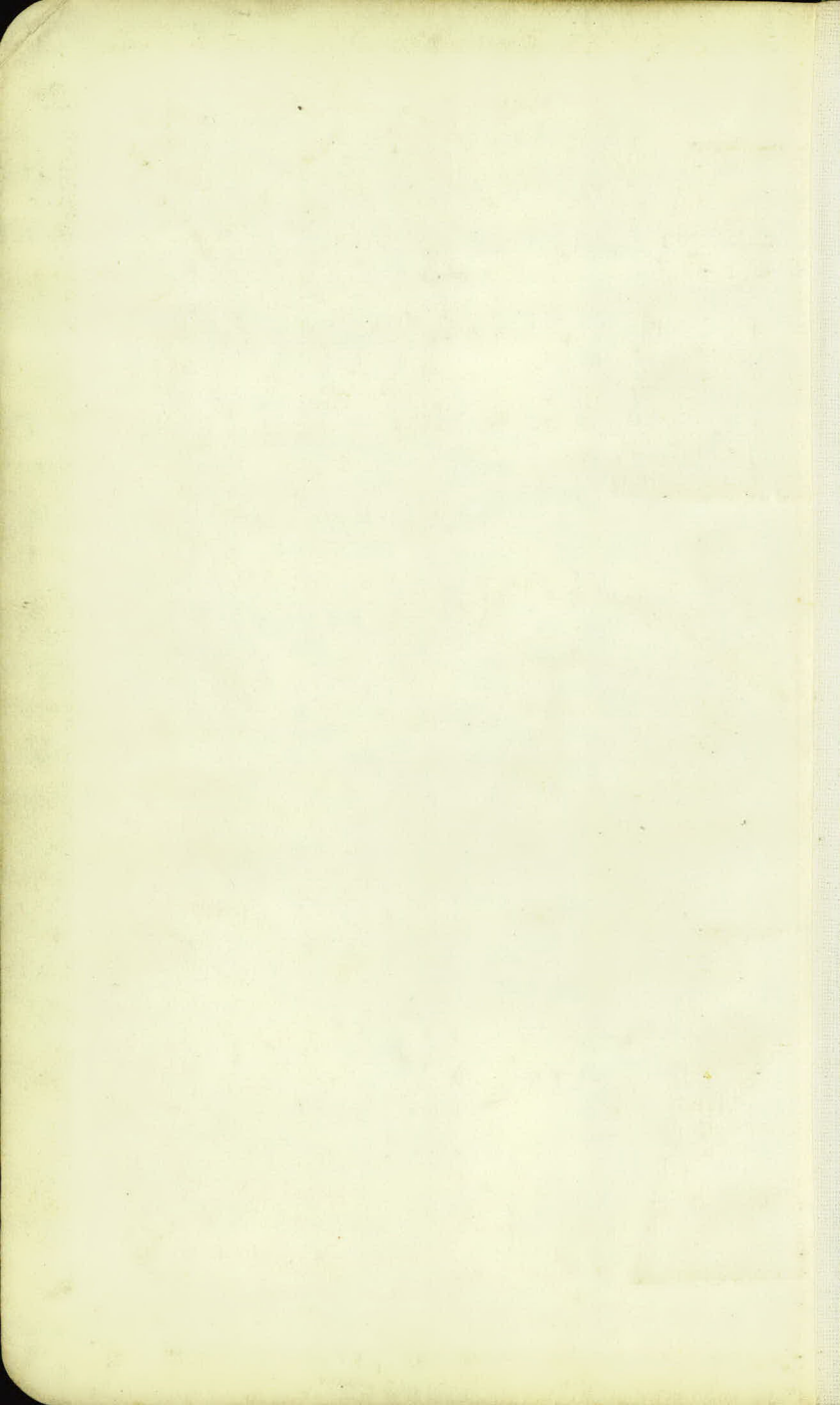
Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

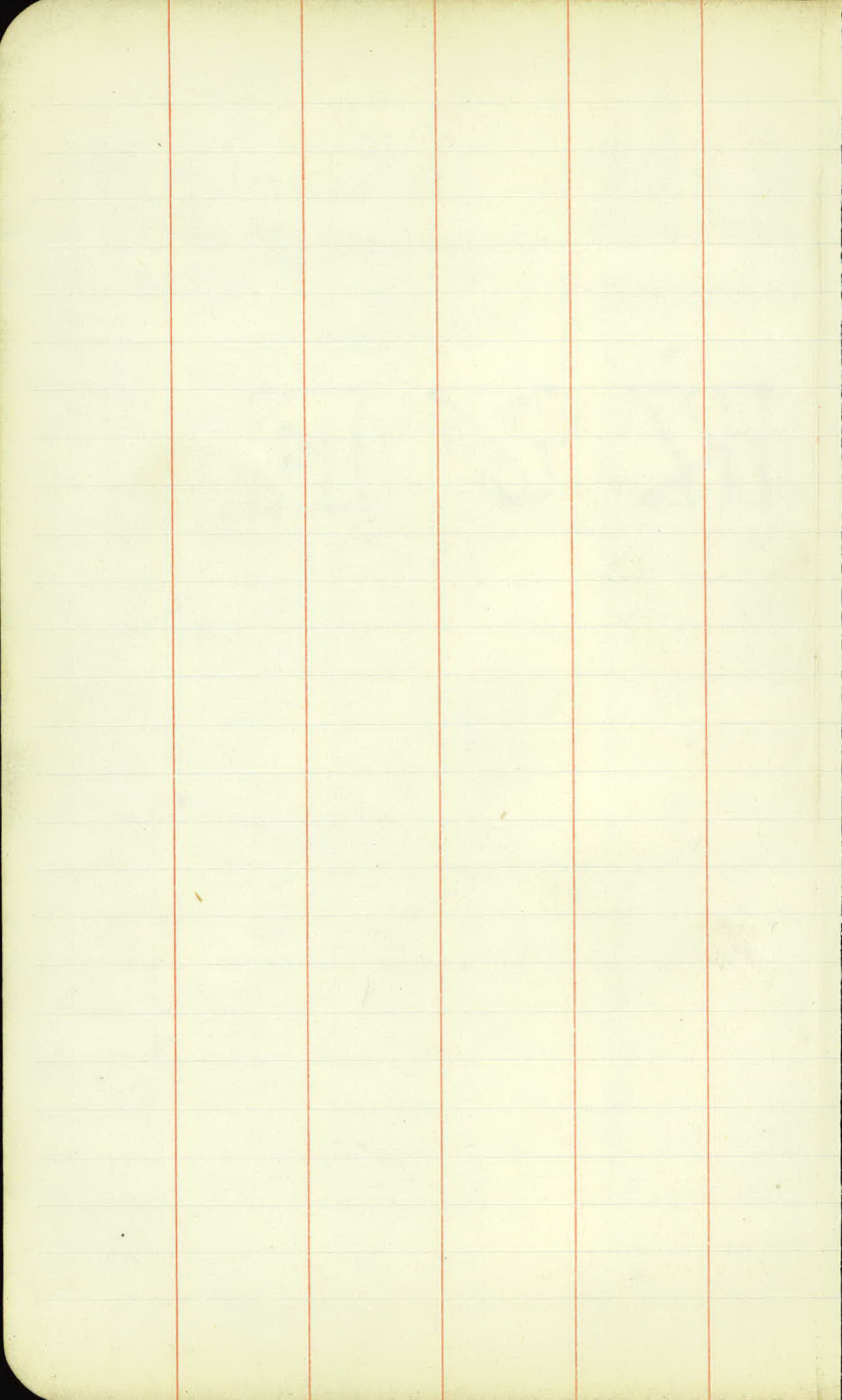
John Miller

Dayton's Bluff

Rt. 4



<u>Page</u>	<u>to page</u>	<u>DESCRIPTION</u>	<u>Sta</u>	<u>to Sta</u>
1	6	Alignment	0+00	113+53.46
8-	24	Slope Stakes	0+00	113+53.46
25-	26	Culv. Stakes	0+00	113+53.46
27		LOCATION GRAVEL PIT		
28	29	ORIGINAL X. SEC. GRAVEL PIT		
30	- 48	FINAL X SECTION.	0+00	- 114+00
50	- 114	FINAL ART. TOPOG.	0+00	- 114+00
49	-	FARM ENT.	0+00	- 114+00
90		STRIPPING X SEC. GRAVEL PIT		



909.92 S.W. COR. IRON PLATE @ OF GATE TO CEMETERY

STA. Point Δ LT Δ RT

16+02<sup>2</sup> P.O.T.  
10+01<sup>2</sup>

S. 89° 26' E.

4+53<sup>33</sup> P.T.

45°-20'

4+00

40°-00'

1+50

35°-00'

3+00

30°-00'

A-90°-40'

2+91<sup>30</sup> P.I.

90°-40'

D-20°-R.

2+50

25°-00'

T-291<sup>30</sup>

2+00

20°-00'

L-455<sup>59</sup>

1+50

15°-00'

R-287<sup>94</sup>

1+00

10°-00'

1+50

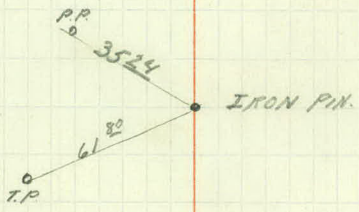
5°-00'

0+00 P.C.

0°-00'

N 00°-26' W.

5-24-28



17960  
9040  
1720

STA      POINT      Δ LT      Δ RT

54743<sup>4</sup>      P.O.T

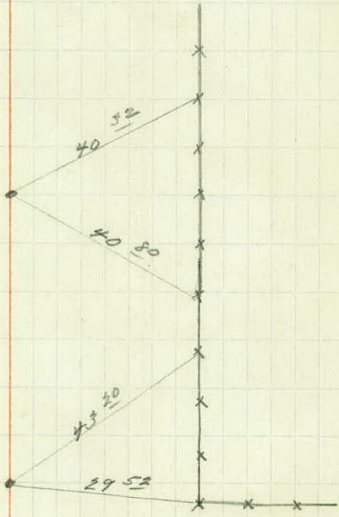
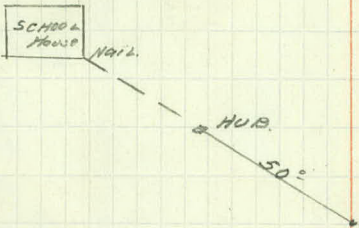
37764<sup>5</sup>  
1654      P.O.T

28701<sup>4</sup>  
28 100<sup>2</sup>      P.I      0°-21'

S. 89°-47 E

S. 89°-26 E

5-4-28



Sta	Point	Lt	Rt.
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=70+38.12

70+39<sup>32</sup> =

45°-27<sup>5</sup>'

70

41°-31<sup>5</sup>'

+50

36°-34<sup>5</sup>'

69

31°-31<sup>5</sup>'

+77<sup>30</sup> P.I.

90°55'

+50

26°-31<sup>5</sup>'

68

21°-31<sup>5</sup>'

+50

16°-31<sup>5</sup>'

67

11°-31<sup>5</sup>'

+50

6°-31<sup>5</sup>'

66

1°-31<sup>5</sup>'

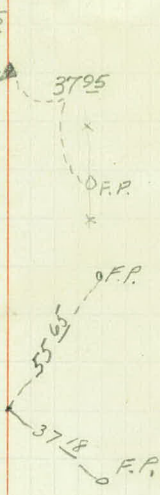
65+84<sup>72</sup>

0°-0'

5-6-28

Carley  
Wheeler  
Thompson  
Kinsler,

This curve  
Relocated



$\Delta = 90^{\circ}55'$   
 $D = 20^{\circ} \text{ Lt.}$   
 $T = 292.58 \text{ V}$   
 $L = 454.60 \text{ V}$

Sta. Point Lt. Rt.

97+00 P.S.T.

+44<sup>2</sup> P.T.

45°-31'

82

41°-04'

+50

36°-04'

81

31°-04'

+82<sup>48</sup> P.I.

91°02'

+50

26°-04'

80

21°-04'

+50

16°-04'

79

11°-04'

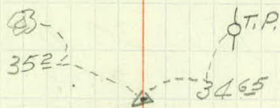
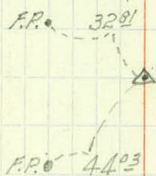
+50

6°-04'

78

1°-04'

77+89<sup>33</sup> P.G.



$$\Delta = 91^{\circ}02'$$

$$D = 200 \text{ ft.}$$

$$T_1 = 293.15'$$

$$L = 455.17'$$

Sta. Point Lt. Rt.

+53.46

35°-29'

113

30°-08'

+50

25°-08'

+022 P.I.

70°-57'

112

20°-08'

+50

15°-08'

111

10°-08'

110+50

5°-08'

109+087/2

109+077/2 =

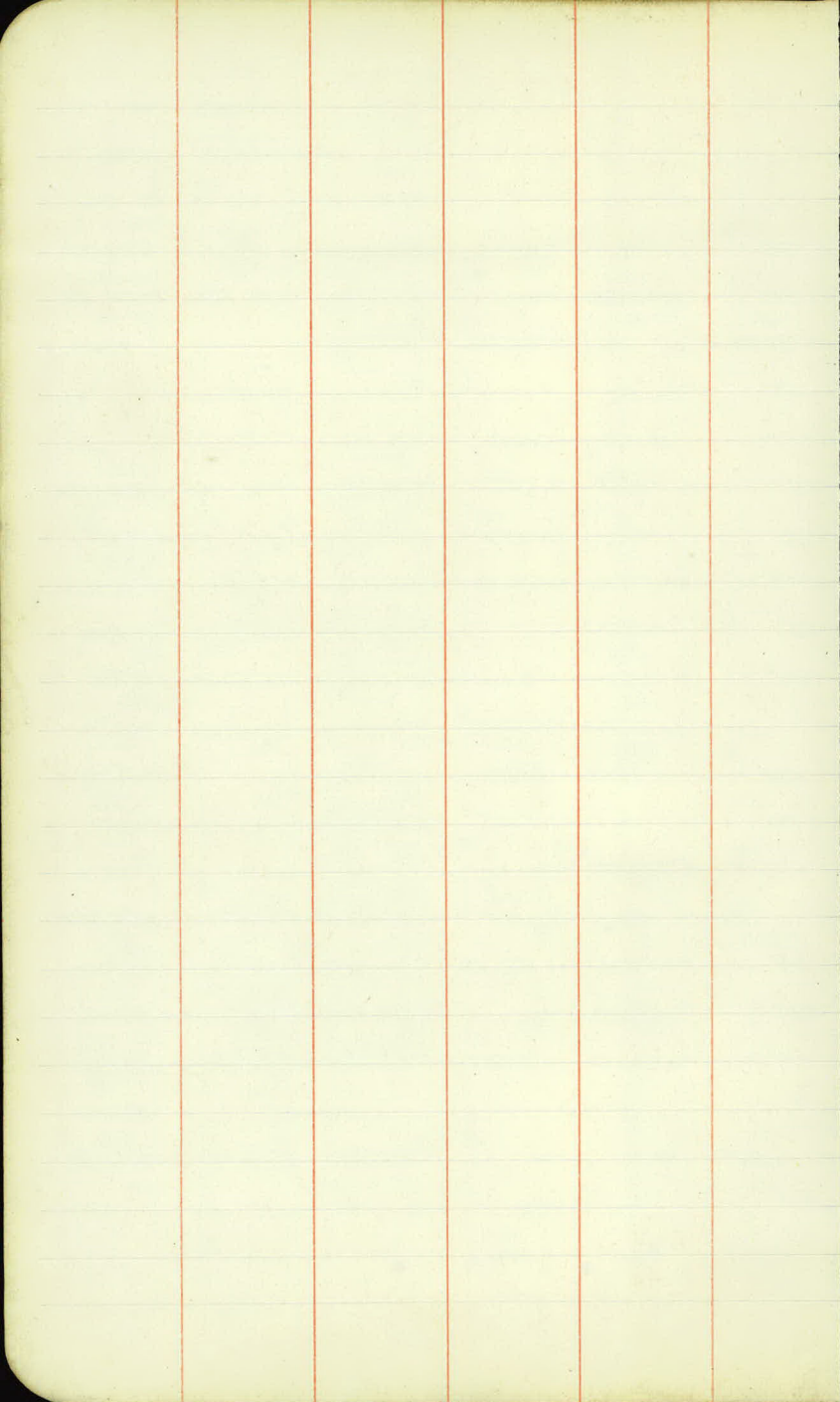


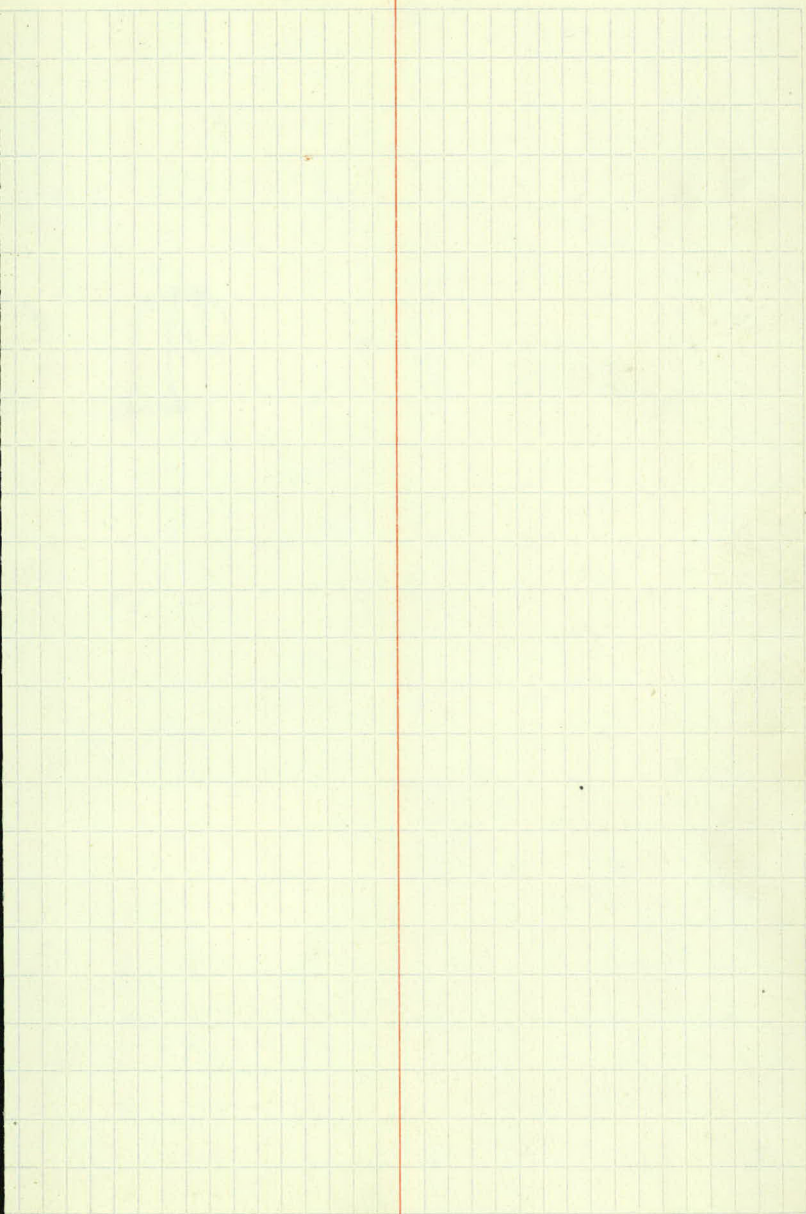
$\Delta$  70°57'

D. 20° RT.

T. 205.19

L 354.75





Sta.	+	H.I.	-	Grade	Gr. Rd.
B.M.	6.67	914.11.		907.44	6.9 8.4
0				06.5	7.6.
+50				06.8	6.4 8.5
					7.3.
1				07.1	6.1 8.2
					7.0.
+50				07.4	5.8 7.9
					6.7.
2				07.6	5.6 7.7
					6.5.
+50				07.6	5.6 7.7
					6.5.
3				07.5	5.7 7.8
					6.6.
+15				7.4	6.7
+50				07.2	6.0 8.1
					6.9.
4				06.8	6.4 8.5
					7.3.
T.P.	3.09	909.93.	7.27	906.84.	2.8 4.9
+50				06.4.	3.5.
5				06.0	3.4 4.4
					3.9.

6-20-28

Lt L Rt

Carley  
11/13/07  
Wheeler8  
- Width

	J.P.K. 112 T.P. 30 Rt. 50 1750															
0.7	(8.2) (24.1)	7.5 /40	8.4 /34	8.7 /18	7.7 /15	7.7 /10	(7.2)	7.7 /8	7.5 /11	9.2 /15	7.0 /21	7.4 /25	5.8 /40	(6.6) (28.7)	0.8	2.0
0.9	F2.4 (8.8) (19.8)	7.9 /39	8.4 /23	8.8 /19	7.7 /13	(7.3)	7.5 /4	7.7 /6	7.5 /11	9.3 /18	6.4 /30	5.5 /40	5.5 /40	(5.5) (34.5)	1.2	4.0
0.9	ROAD (7.8) (19.0)	7.4 /35	8.1 /27	7.4 /19	8.0 /10	9.3 /12	(7.0)	7.2 /15	7.3 /16	6.3 /16	5.6 /40	(5.6) (33.9)			1.2	4.0
0.9	F2.0 (7.8) (19.0)	7.8 /31	9.1 /27	7.4 /20	7.7 /16	(6.7)	5.9 /21	5.2 /40	4.3 /40			(4.5) (35.1)			1.2	4.0
0.9	(5.2) (26.6)			6.1 /40	5.2 /15	(6.5)	4.0 /19	3.5 /19	2.9 /40			(2.9) (37.2)			1.2	4.0
0.9	(5.0) (26.9)			5.6 /40	4.9 /16	(6.5)	3.8 /20	3.1 /20	3.1 /40			(3.1) (36.9)			1.2	4.0
0.9	D.C.0.5 (7.2) (23.8)	6.4 /42	6.9 /35	7.5 /24		(6.6)	4.2 /19	4.1 /19	4.6 /40			(4.6) (34.8)			1.2	4.0
0.9		6.3 /41	6.6 /31	7.7 /15		(6.7)	5.4 /13	4.0 /13	4.4 /26	4.6 /40					1.2	4.0
0.9	D.C.1.2 (6.8) (24.8)	7.0 /40	7.0 /28	6.5 /22	6.9 /12	7.2 /19	(6.9)	7.5 /3	7.7 /26	4.4 /26	4.9 /40			(4.7) (35.1)	1.2	4.0
0.9	D.C.1.6 (6.8) (25.4)	4.6 /40	6.4 /30	7.8 /17	7.5 /12	7.2 /5	(7.3)	7.4 /4	7.6 /13	7.9 /24	7.8 /24	6.6 /34		(6.5) (33.0)	1.2	4.0
0.7	D.C.1.8 (3.1) (25.7)	2.1 /33	3.5 /23	4.7 /11	4.2 /19	3.9 /19	(3.5)	4.3 /8	6.0 /22	4.7 /29	5.7 /40			D.C.0.8 (6.6) (26.2)	0.9	2.0
0.5	D.C.0.4 (5.1) (23.6)	4.6 /33	5.0 /20	5.4 /17	4.9 /19	4.6 /19	(3.9)	5.2 /8	7.3 /19	8.2 /33				F3.0 (7.4) (21.0)	0.5	

Sta.	*	H.I.	-	Grade	Gr. Rd
		909.93.			
5 + 50				05.6.	4.1 4.3 4.5
6				05.2.	4.7
TP	1.73	905.77.	5.89	904.04.	
7				04.4.	1.4
+50				04.0.	1.8
8				03.6.	2.2
9				02.9.	2.9
10				02.5.	3.3
11				02.2.	3.6
12				02.2.	3.6
TP	4.68	906.61.	3.84	901.93.	
+50				02.3.	4.3
13				02.3.	4.3
14				02.4.	4.2
15				02.5.	4.1
+86				02.6.	4.0

42   41   40

$\begin{matrix} 64.2 \\ 8.2 \\ 23.4 \end{matrix}$     $\begin{matrix} 8.4 \\ 33 \end{matrix}$     $\begin{matrix} 8.3 \\ 26 \end{matrix}$     $\begin{matrix} 8.7 \\ 19 \end{matrix}$     $\begin{matrix} 5.9 \\ 17 \end{matrix}$     $\begin{matrix} 5.5 \\ 17 \end{matrix}$     $\begin{matrix} 6.1 \\ 9 \end{matrix}$     $\begin{matrix} 1.0 \\ 21 \end{matrix}$     $\begin{matrix} 1.0 \\ 33 \end{matrix}$     $\begin{matrix} F5.6 \\ 10.1 \\ 26.2 \end{matrix}$    -0.2

$\begin{matrix} F5.3 \\ 10.0 \\ 25.6 \end{matrix}$     $\begin{matrix} 10.0 \\ 33 \end{matrix}$     $\begin{matrix} 10.4 \\ 19 \end{matrix}$     $\begin{matrix} 6.6 \\ 19 \end{matrix}$     $\begin{matrix} 6.3 \\ 6 \end{matrix}$     $\begin{matrix} 6.2 \\ 6 \end{matrix}$     $\begin{matrix} 6.2 \\ 17 \end{matrix}$     $\begin{matrix} 9.7 \\ 18 \end{matrix}$     $\begin{matrix} 9.1 \\ 33 \end{matrix}$     $\begin{matrix} F4.8 \\ 9.5 \\ 24.6 \end{matrix}$

No. in   T.P.   Pts.   (100)   44   Stopped here and left for 28-015-2 D.C. 1.7  
 D.C.  $\begin{matrix} 3.2 \\ 23.3 \end{matrix}$     $\begin{matrix} 3.6 \\ 33 \end{matrix}$     $\begin{matrix} 2.8 \\ 14 \end{matrix}$     $\begin{matrix} 2.3 \\ 17 \end{matrix}$     $\begin{matrix} 2.0 \\ 20 \end{matrix}$     $\begin{matrix} 2.1 \\ 6 \end{matrix}$     $\begin{matrix} 2.4 \\ 9 \end{matrix}$     $\begin{matrix} 3.4 \\ 17 \end{matrix}$     $\begin{matrix} 1.6 \\ 21 \end{matrix}$     $\begin{matrix} 1.8 \\ 33 \end{matrix}$     $\begin{matrix} 1.7 \\ 25.5 \end{matrix}$   
 D.C.  $\begin{matrix} 2.8 \\ 24.5 \end{matrix}$     $\begin{matrix} 2.9 \\ 33 \end{matrix}$     $\begin{matrix} 2.6 \\ 22 \end{matrix}$     $\begin{matrix} 3.0 \\ 11 \end{matrix}$     $\begin{matrix} 2.7 \\ 17 \end{matrix}$     $\begin{matrix} 2.4 \\ 9 \end{matrix}$     $\begin{matrix} 2.7 \\ 17 \end{matrix}$     $\begin{matrix} 2.4 \\ 9 \end{matrix}$     $\begin{matrix} 4.0 \\ 15 \end{matrix}$     $\begin{matrix} 3.3 \\ 29 \end{matrix}$     $\begin{matrix} 3.5 \\ 33 \end{matrix}$     $\begin{matrix} 3.4 \\ 23.6 \end{matrix}$  D.C. 0.4  
 F2.0  $\begin{matrix} 4.2 \\ 19.0 \end{matrix}$     $\begin{matrix} 4.1 \\ 33 \end{matrix}$     $\begin{matrix} 4.3 \\ 16 \end{matrix}$     $\begin{matrix} 3.3 \\ 6 \end{matrix}$     $\begin{matrix} 3.1 \\ 6 \end{matrix}$     $\begin{matrix} 3.4 \\ 6 \end{matrix}$     $\begin{matrix} 5.6 \\ 15 \end{matrix}$     $\begin{matrix} 5.8 \\ 25 \end{matrix}$     $\begin{matrix} 5.7 \\ 33 \end{matrix}$     $\begin{matrix} 5.8 \\ 22.2 \end{matrix}$    F3.6

$\begin{matrix} F3.5 \\ 6.4 \\ 22.0 \end{matrix}$     $\begin{matrix} 6.4 \\ 33 \end{matrix}$     $\begin{matrix} 6.2 \\ 18 \end{matrix}$     $\begin{matrix} 5.7 \\ 14 \end{matrix}$     $\begin{matrix} 4.6 \\ 18 \end{matrix}$     $\begin{matrix} 4.3 \\ 18 \end{matrix}$     $\begin{matrix} 4.4 \\ 7 \end{matrix}$     $\begin{matrix} 5.4 \\ 11 \end{matrix}$     $\begin{matrix} 6.0 \\ 15 \end{matrix}$     $\begin{matrix} 6.4 \\ 33 \end{matrix}$     $\begin{matrix} 6.3 \\ 21.8 \end{matrix}$

$\begin{matrix} F3.3 \\ 6.6 \\ 21.6 \end{matrix}$     $\begin{matrix} 6.5 \\ 33 \end{matrix}$     $\begin{matrix} 6.7 \\ 18 \end{matrix}$     $\begin{matrix} 5.9 \\ 12 \end{matrix}$     $\begin{matrix} 5.7 \\ 8 \end{matrix}$     $\begin{matrix} 5.4 \\ 18 \end{matrix}$     $\begin{matrix} 5.5 \\ 6 \end{matrix}$     $\begin{matrix} 6.5 \\ 14 \end{matrix}$     $\begin{matrix} 6.3 \\ 31 \end{matrix}$     $\begin{matrix} 7.1 \\ 33 \end{matrix}$     $\begin{matrix} 6.4 \\ 21.2 \end{matrix}$

$\begin{matrix} F2.9 \\ 6.5 \\ 20.8 \end{matrix}$     $\begin{matrix} 6.4 \\ 33 \end{matrix}$     $\begin{matrix} 6.8 \\ 16 \end{matrix}$     $\begin{matrix} 5.6 \\ 19 \end{matrix}$     $\begin{matrix} 5.1 \\ 19 \end{matrix}$     $\begin{matrix} 5.4 \\ 16 \end{matrix}$     $\begin{matrix} 5.9 \\ 19 \end{matrix}$     $\begin{matrix} 6.4 \\ 13 \end{matrix}$     $\begin{matrix} 6.4 \\ 32 \end{matrix}$     $\begin{matrix} 7.1 \\ 33 \end{matrix}$     $\begin{matrix} 6.5 \\ 20.8 \end{matrix}$

$\begin{matrix} F2.1 \\ 5.7 \\ 19.2 \end{matrix}$     $\begin{matrix} 5.7 \\ 33 \end{matrix}$     $\begin{matrix} 5.7 \\ 17 \end{matrix}$     $\begin{matrix} 4.0 \\ 18 \end{matrix}$     $\begin{matrix} 3.9 \\ 18 \end{matrix}$     $\begin{matrix} 4.0 \\ 16 \end{matrix}$     $\begin{matrix} 5.8 \\ 15 \end{matrix}$     $\begin{matrix} 6.1 \\ 31 \end{matrix}$     $\begin{matrix} 6.8 \\ 33 \end{matrix}$     $\begin{matrix} 5.9 \\ 19.6 \end{matrix}$

$\begin{matrix} D.C. 1.0 \\ 5.3 \\ 21.5 \end{matrix}$     $\begin{matrix} 4.8 \\ 33 \end{matrix}$     $\begin{matrix} 5.1 \\ 26 \end{matrix}$     $\begin{matrix} 5.9 \\ 15 \end{matrix}$     $\begin{matrix} 4.8 \\ 18 \end{matrix}$     $\begin{matrix} 4.6 \\ 18 \end{matrix}$     $\begin{matrix} 4.7 \\ 17 \end{matrix}$     $\begin{matrix} 6.3 \\ 14 \end{matrix}$     $\begin{matrix} 6.7 \\ 31 \end{matrix}$     $\begin{matrix} 7.3 \\ 33 \end{matrix}$     $\begin{matrix} 6.4 \\ 19.2 \end{matrix}$

$\begin{matrix} 0.10 \\ 4.3 \\ 26.0 \end{matrix}$     $\begin{matrix} 3.7 \\ 33 \end{matrix}$     $\begin{matrix} 4.3 \\ 27 \end{matrix}$     $\begin{matrix} 5.7 \\ 14 \end{matrix}$     $\begin{matrix} 4.6 \\ 18 \end{matrix}$     $\begin{matrix} 4.3 \\ 18 \end{matrix}$     $\begin{matrix} 4.5 \\ 16 \end{matrix}$     $\begin{matrix} 6.4 \\ 16 \end{matrix}$     $\begin{matrix} 6.4 \\ 30 \end{matrix}$     $\begin{matrix} 7.3 \\ 32 \end{matrix}$     $\begin{matrix} 6.7 \\ 33 \end{matrix}$     $\begin{matrix} 6.5 \\ 17.6 \end{matrix}$

$\begin{matrix} D.C. 1.0 \\ 5.2 \\ 24.5 \end{matrix}$     $\begin{matrix} 5.2 \\ 20.2 \end{matrix}$     $\begin{matrix} 4.5 \\ 33 \end{matrix}$     $\begin{matrix} 5.8 \\ 14 \end{matrix}$     $\begin{matrix} 4.8 \\ 19 \end{matrix}$     $\begin{matrix} 4.8 \\ 17 \end{matrix}$     $\begin{matrix} 6.0 \\ 14 \end{matrix}$     $\begin{matrix} 7.2 \\ 30 \end{matrix}$     $\begin{matrix} 6.4 \\ 33 \end{matrix}$     $\begin{matrix} 6.3 \\ 19.2 \end{matrix}$

$\begin{matrix} F2.6 \\ 6.7 \\ 20.2 \end{matrix}$     $\begin{matrix} 6.6 \\ 33 \end{matrix}$     $\begin{matrix} 6.7 \\ 18 \end{matrix}$     $\begin{matrix} 7.2 \\ 18 \end{matrix}$     $\begin{matrix} 7.2 \\ 16 \end{matrix}$     $\begin{matrix} 5.3 \\ 18 \end{matrix}$     $\begin{matrix} 4.9 \\ 16 \end{matrix}$     $\begin{matrix} 5.3 \\ 12 \end{matrix}$     $\begin{matrix} 6.8 \\ 12 \end{matrix}$     $\begin{matrix} 7.4 \\ 30 \end{matrix}$     $\begin{matrix} 6.8 \\ 33 \end{matrix}$     $\begin{matrix} 6.8 \\ 20.4 \end{matrix}$

$\begin{matrix} D.C. 0.4 \\ 5.6 \\ 24.6 \end{matrix}$     $\begin{matrix} 5.5 \\ 21.0 \end{matrix}$     $\begin{matrix} 6.2 \\ 33 \end{matrix}$     $\begin{matrix} 5.5 \\ 22 \end{matrix}$     $\begin{matrix} 5.7 \\ 15 \end{matrix}$     $\begin{matrix} 4.8 \\ 18 \end{matrix}$     $\begin{matrix} 4.7 \\ 11 \end{matrix}$     $\begin{matrix} 5.4 \\ 25 \end{matrix}$     $\begin{matrix} 6.1 \\ 30 \end{matrix}$     $\begin{matrix} 6.5 \\ 31 \end{matrix}$     $\begin{matrix} 6.2 \\ 33 \end{matrix}$     $\begin{matrix} 5.1 \\ 19.4 \end{matrix}$     $\begin{matrix} 5.4 \\ 23.9 \end{matrix}$    D.C. 0.6

36.0  
2.3

		H.I.	-	Grado Cir. Rd	
5+0	+	906.61			
15+94				02.6	4.0
16				02.6	4.0
+07				02.6	4.0
+20				02.6	4.0
17				02.7	3.9
B.M.	3.57	906.49	3.57	903.04	902.92
18				03.4	3.1
T.P.	9.95	916.05	0.39	906.10	
19				05.1	11.0
+50				06.25	9.8
20				07.4	8.7
+50				08.6	7.5
T.P.	7.80	918.73	5.12	910.93	
21				09.5	9.2
+50				10.7	8.0
22				11.8	6.9

4

4

pt Carley 10  
Wilson  
Hauser

$\frac{5.2}{33}$   $\frac{4.7}{33}$   $\frac{4.1}{33}$

(4.0)

E ROAD.

$\frac{5.0}{33}$   $\frac{4.7}{33}$   $\frac{4.0}{17}$   $\frac{4.0}{33}$  E.F.E.

(4.0)

$\frac{5.0}{33}$   $\frac{4.8}{33}$   $\frac{4.2}{14}$   $\frac{4.0}{33}$

(4.0)

F2.0  
(6.0)  
19.0

$\frac{6.6}{33}$   $\frac{5.9}{23}$   $\frac{5.6}{14}$   $\frac{4.0}{33}$   $\frac{5.2}{18}$   $\frac{5.6}{17}$   $\frac{6.1}{28}$   $\frac{6.1}{33}$

F2.0  
(6.0)  
22.0

F3.0  
(6.9)  
21.0

$\frac{6.8}{33}$   $\frac{6.7}{21}$   $\frac{6.6}{13}$   $\frac{5.8}{8}$   $\frac{5.4}{33}$   $\frac{5.0}{16}$   $\frac{6.2}{11}$   $\frac{6.1}{22}$   $\frac{6.0}{33}$

(3.9)

F2.2  
(6.1)  
19.4

Spt 112.30" tr. 40' pt. Sta. 17+10

F3.3  
(6.4)  
21.6

$\frac{6.7}{33}$   $\frac{6.3}{17}$   $\frac{4.7}{9}$   $\frac{4.5}{33}$   $\frac{4.6}{5}$   $\frac{5.2}{19}$   $\frac{4.9}{18}$   $\frac{4.3}{33}$

(3.1)

126.04  
(4.7)  
23.6

F2.0  
(1.30)  
19.0

$\frac{15.9}{33}$   $\frac{13.8}{25}$   $\frac{13.0}{17}$   $\frac{11.9}{11}$   $\frac{11.4}{33}$   $\frac{11.5}{4}$   $\frac{12.2}{6}$   $\frac{11.9}{12}$   $\frac{9.9}{15}$   $\frac{9.9}{33}$

(1.0)

C.116  
(9.2)  
28.4

C0.2  
(9.6)  
26.3

$\frac{10.3}{33}$   $\frac{9.3}{17}$   $\frac{9.5}{12}$   $\frac{9.2}{33}$   $\frac{9.2}{12}$   $\frac{10.2}{16}$   $\frac{8.9}{19}$   $\frac{8.5}{17}$   $\frac{6.2}{20}$   $\frac{5.1}{33}$

(1.1)

C.446  
(5.2)  
32.9

C2.2  
(6.5)  
29.3

$\frac{7.9}{33}$   $\frac{6.9}{19}$   $\frac{7.2}{13}$   $\frac{7.3}{33}$   $\frac{7.4}{11}$   $\frac{8.0}{13}$   $\frac{6.8}{17}$   $\frac{6.2}{13}$   $\frac{3.5}{18}$   $\frac{2.7}{33}$

(1.1)

C.6.0  
(2.7)  
33.0

C3.2  
(4.3)  
30.8

$\frac{4.3}{33}$   $\frac{4.2}{17}$   $\frac{5.4}{13}$   $\frac{5.4}{11}$   $\frac{5.7}{33}$   $\frac{7.4}{5}$   $\frac{7.1}{10}$   $\frac{1.7}{16}$   $\frac{0.9}{33}$

(1.5)

C.166  
(0.9)  
33

C.4.2  
(5.9)  
32.3

$\frac{5.0}{33}$   $\frac{5.2}{18}$   $\frac{6.2}{14}$   $\frac{6.6}{11}$   $\frac{7.8}{33}$   $\frac{8.8}{14}$   $\frac{8.7}{12}$   $\frac{1.8}{19}$   $\frac{1.4}{33}$

(9.2)

C.7.8  
(1.4)  
33.0

C.3.2  
(4.8)  
30.8

$\frac{5.9}{33}$   $\frac{4.6}{27}$   $\frac{5.1}{14}$   $\frac{5.3}{33}$   $\frac{4.9}{12}$   $\frac{5.0}{16}$   $\frac{6.9}{19}$   $\frac{3.1}{15}$   $\frac{2.7}{33}$

(8.0)

C.5.5  
(2.5)  
33

C0.8  
(6.1)  
28.2

$\frac{6.3}{33}$   $\frac{6.2}{25}$   $\frac{5.6}{13}$   $\frac{5.4}{33}$   $\frac{5.1}{12}$   $\frac{4.6}{13}$   $\frac{6.2}{11}$   $\frac{5.3}{14}$   $\frac{4.9}{33}$

(6.9)

C.2.0  
(4.9)  
29.0

Sta		H.I.		Grade	Gr. Rd	
23		918.73.		14.1.	4.6	
	+50			15.25.	3.5	
24				16.4.	2.3	
	T.P.	11.42	929.00.	1.15	917.58.	
25				18.7.	10.3	
26				21.0.	8.0	
27				23.3.	5.7	
	B.M.	7.33	928.91.	4.33	924.67	924.58
28				25.3.	3.6	
	T.P.	8.49	933.07.	7.33	924.58.	
	+50			26.1	7.0.	
29				26.8	6.3.	
	+50			27.3	5.8.	
30				27.8	5.3.	
31				28.3	4.8.	
	+50			28.4	4.7.	
32				28.5	4.6.	

RT

D.C. 1.2  
5.4  
24.8

5.5/33 5.4/25 5.2/12 5.1/35 5.8/06 5.9/18 6.0/33

D.C. 0.6  
6.0  
23.9

D.C. 1.4  
4.2  
24.5

D.C. 1.4  
2.9  
25.1

4.4/33 4.4/14 4.6/33 4.5/3 5.5/10 5.5/33  
2.6/33 3.3/14 4.0/11 3.7/4 3.7/10 4.3/10 4.5/24 4.4/33

F2.0  
4.3  
19

F2.0  
12.3  
19.0

11.7/33 11.9/13 12.5/11 12.3/10.2 11.9/8 12.3/14 12.3/33

F2.0  
12.3  
19.0

D.C. 0.5  
9.5  
23.8

F1.5  
9.5  
21.0

9.5/33 9.5/14 10.1/12 10.1/8.0 10.2/2 9.7/4 10.0/24 9.5/33

F1.6  
9.6  
18.2

D.C. 1.0  
6.7  
24.5

6.9/33 6.7/16 6.9/13 7.1/5.7 6.6/2 7.5/8 7.4/23 7.2/33

F1.6  
7.3  
21.4

D.C. 0.4  
7.3  
23.6

Spk. 1.2 T.P. 20' RT

5+4 27+40  
3.0/24.6  
3.1/33 3.9/14 2.7/10.2 1.9/4 3.1/10 2.6/19 2.2/33

C1.6  
2.0  
28.4

S.M.  
6.4  
26.6

Quit work here 6-21-28

7.0  
7.0/33 6.4/27 6.7/24 6.0/14 5.8/19 5.6/5.6 5.7/14 5.1/5 6.1/10 4.9/13 3.8/27 3.8/33

C1.3  
3.8  
30.8

D.C. 1.0  
7.3  
24.5

F1.0  
7.3  
19.0

7.7/33 7.5/29 6.9/15 5.6/17 5.2/5.2 5.2/6 4.7/8 5.5/12 4.4/14 2.9/30 2.8/33

C3.6  
2.7  
30.4

D.C. 1.4  
7.4  
23.6

F1.4  
7.2  
20.6

8.2/32 7.2/24 6.5/14 5.3/18 4.7/6.3 4.7/8 4.9/12 4.9/16 2.7/29 2.9/33

C2.8  
3.0  
30.2

D.C. 1.0  
6.7  
23.9

F1.0  
6.3  
19.0

7.0/33 6.8/27 6.2/18 6.4/12 5.1/18 4.6/4.6 4.8/19 3.2/18 2.4/30 2.4/33

C3.0  
2.3  
30.5

C.O.S  
6.0  
24.2

F0.8  
5.6  
18.2

6.3/33 5.5/20 5.6/15 6.4/11 5.7/8 5.3/5.3 5.6/19 5.0/11 3.7/22 3.4/33

C1.2  
5.6  
27.8

pitch  
6.7  
23.0

6.9/33 7.0/28 5.9/16 7.3/11 6.5/6 6.3/4.7 6.5/10 6.1/15 4.4/23 4.5/31

C1.0  
4.7  
26.0

F3.0  
7.6  
21.0

8.1/33 7.3/20 7.7/12 7.1/5 7.0/4.6 6.9/8 7.7/13 7.9/19 6.2/31

F2.4  
7.0  
19.8

Sta	+	H.I.	-	Grade	Gr. Rd
		933.07 ✓			
	+50			28.6	4.5.
33				28.7	4.4.
	T.P.	9.13	936.16 ✓	6.04	927.03
	+50			28.8	7.4.
34				28.9	<u>7.2</u> 7.3
	+50			29.0	7.2.
35				29.0	7.2.
36				29.0	7.2.
	+50			28.9	7.3.
37				28.8	7.4.
	+50			28.7	7.5.
38				28.5	7.7.
	+50			28.3	7.9.
	T.P.	6.89	933.08 ✓	9.97	926.19

Cloudy - Windy

6-26-28

±

±

RT

Carley 12  
Wilson  
Wheeler

F3.0 (7.5) 21.0	8.2/33	7.9/23	7.6/17	7.8/11	7.2/8	(4.5) 6.8	7.5/12	6.6/17	6.2/33	F2.0 (6.6) 19.0
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F2.0 (6.4) 19.0	8.0/33	6.9/15	7.0/11	6.6/6	(4.0) 6.2	6.2/9	5.3/14	4.3/22	4.8/29	4.3/32	0.0 (4.4) 26.0
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F2.5 (9.9) 20.0	11.0/33	9.8/18	9.7/10	9.9/7	(7.0) 8.5	8.7/9	8.1/13	7.0/24	7.3/28	6.6/32	C0.2 (7.2) 26.3
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D.C.0.6 (8.6) 23.8	F1.3 (8.5) 20.2	9.2/33	8.0/18	8.7/11	7.7/8	(7.3) 7.4	7.4/9	6.5/14	5.9/20	5.4/32	C1.4 (5.8) 28.1
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0.0 (7.2) 26.0	7.5/33	6.8/21	5.7/16	6.9/11	5.8/7	(7.2) 5.8	6.9/9	5.8/14	5.1/19	5.3/32	C1.6 (5.6) 28.4
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C1.0 (6.2) 27.0	6.2/33	4.8/16	5.7/10	4.4/6	(7.0) 4.6	4.9/9	5.5/13	4.5/19	4.9/32	C2.2 (5.0) 29.3
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C0.2 (7.0) 26.3	7.2/33	6.1/19	7.2/19	6.5/5	(7.1) 6.4	6.5/10	5.7/18	6.9/25	5.8/33	C1.2 (6.0) 27.8
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D.C.0.6 (7.7) 28.4	F0.2 (7.5) 15.4	7.9/33	7.2/18	8.9/12	7.4/5	(7.3) 7.1	7.2/9	7.5/14	6.7/20	6.9/33	C0.2 (7.1) 26.3
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0.0 (7.4) 26.0	7.6/33	6.4/20	7.4/19	7.3/6	(7.6) 6.9	6.9/7	6.5/9	7.2/13	6.5/22	6.9/33	C0.4 (7.0) 26.6
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D.C.1.6 (7.9) 25.4	8.4/33	6.2/21	7.9/16	6.5/7	(7.5) 6.4	6.2/7	5.9/25	5.8/33	C1.4 (6.1) 28.1
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0.0 (7.2) 26.0	8.7/33	7.8/25	5.9/15	6.9/7	(7.1) 6.1	6.9/6	5.5/8	5.9/13	3.7/16	2.9/33	C4.6 (3.1) 32.9
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0.0 (7.9) 26.0	9.0/33	7.5/24	6.0/20	5.9/7	(7.9) 6.1	5.8/6	5.1/12	7.3/14	6.6/18	2.4/25	1.9/33
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Nail in T.P.

Quit here 6-26-28

Sta	+	H.I	-	Grade	Gr. Rd	
		933.08				
39				28.1	5.0	
	+50			27.9	5.2	
40				27.7	5.4	
41				27.3	5.8	
42				26.9	6.2	
	+50			26.7	6.4	
	B.M.	4.71	933.12	4.71	928.37	928.41
43				26.5	6.6	
	+50			26.3	6.8	
44				26.1	7.0	
	+50			25.9	7.2	
	T.P.	4.49	929.90	7.71	925.41	
45				25.7	4.2	
46				25.3	4.6	
	+50			25.1	4.8	

Four-Way Lt.

RT

Carley 13  
Wilson  
Wheeler

DC.14  
5.6  
25.1

6.6/33 4.6/21 5.3/10 5.7/6 5.4/7 5.6/17 3.3/17 3.5/33

5.0

5.16  
3.4  
28.4

F4.0  
9.2  
23.0

10.3/33 7.9/17 8.2/14 7.7/10 7.5/17 7.3/17 7.0/33

6.2

F2.0  
7.2  
19.0

F4.8  
10.2  
24.6

11.1/33 9.9/19 9.5/10 9.0/7 9.1/14 8.2/26 8.0/33

5.4

F2.8  
8.2  
20.6

FS.4  
11.2  
25.8

11.4/33 10.6/14 10.9/7 10.6/8 10.7/16 11.6/33 11.4/33

5.8

FS.6  
11.4  
26.2

F2.2  
8.4  
19.4

8.4/33 7.8/12 9.3/6 9.4/8 9.3/15 9.2/20 10.9/33

6.2

F3.2  
9.4  
21.4

0.6.17  
6.7  
55

6.7/33 6.7/20 7.1/16 6.5/19 7.9/14 8.3/8 8.0/18 7.4/17 8.4/33

6.8

F1.2  
7.6  
19.8

DC.1.0  
7.4  
24.5

Spk. in 24" oak 35" Lt. 5" 42" 75"

4.9  
28.5

4.9/33 4.9/12 5.8/7 6.4/6.6 6.2/11 6.4/20 6.7/26 5.9/33

6.6

0.0  
6.6  
26.0

C2.8  
4.0  
30.2

4.2/33 4.5/12 4.8/5 4.9/11 5.1/22 5.2/33 5.5/33

6.8

5.16  
5.2  
27.4

C1.8  
5.2  
28.7

5.1/33 5.4/12 5.8/5 6.1/12 6.6/25 6.4/33 6.8/33

7.0

C.0.6  
6.4  
26.9

C1.0  
6.2  
27.5

F0.4  
7.6  
16.6

6.0/33 7.3/12 7.4/12 7.5/18 7.6/33 8.8/33

7.2

DC.1.0  
8.2  
24.5

C.0.4  
3.8  
26.6

3.9/33 3.8/6 4.6/15 4.9/26 5.2/33 5.3/33

4.2

F0.6  
4.8  
17.4

DC.1.2  
5.0  
24.8

C1.6  
3.0  
28.4

2.9/33 3.4/11 4.4/13 4.7/33 4.7/33 4.7/33 4.6/12 4.7/21 4.5/33

4.6

0.0  
4.6  
26.0

C.0.4  
7.4  
26.6

C1.6  
3.2  
28.4

579	+	H.1	-	Grade	G.R.
		929.90			
47				24.8	5.1
	+40			24.6	5.3
48				24.2	5.7
49				23.0	6.9
50				22.9	7.0
	T.P.	5106	769	922.21	
	+50	927.27		22.5	7.8
51				22.1	5.2
	+50			21.7	5.6
52				21.2	6.1
	+50			20.8	6.5
53				20.4	6.9
	+70			19.7	7.6

LT      E      RT

$\frac{5.1}{260}^{0.0}$	$\frac{5.1}{33}$	$\frac{5.1}{33}$	$\frac{5.1}{13}$	$\frac{4.6}{21}$	$\frac{4.3}{33}$	$\frac{4.3}{27.2}^{00.8}$
$\frac{5.9}{25.1}^{DC.1.4}$ $\frac{5.9}{17.4}^{FO.6}$	$\frac{6.0}{18}$	$\frac{6.0}{18}$	$\frac{6.1}{33}$	$\frac{5.7}{6}$	$\frac{6.0}{12}$	$\frac{5.0}{25}$ $\frac{5.4}{27}$ $\frac{5.1}{33}$ $\frac{5.3}{26}^{0.0}$
$\frac{6.5}{24.8}^{DC.1.2}$ $\frac{6.5}{18.2}^{FA.8}$	$\frac{6.5}{33}$	$\frac{7.2}{7}$	$\frac{6.8}{7}$	$\frac{7.1}{12}$	$\frac{6.6}{15}$ $\frac{6.5}{33}$	$\frac{6.7}{19.0}^{F1.0}$ $\frac{6.9}{24.2}^{12.00.8}$
$\frac{7.9}{24.5}^{DC.1.0}$ $\frac{7.9}{19.0}^{F1.0}$	$\frac{7.8}{33}$	$\frac{8.0}{33}$	$\frac{8.0}{9}$	$\frac{8.4}{18}$	$\frac{8.6}{26}$ $\frac{8.6}{33}$	$\frac{8.5}{21.4}^{F1.6}$ $\frac{8.5}{23.6}^{12.00.4}$
$\frac{8.0}{24.5}^{DC.1.0}$ $\frac{8.0}{19.0}^{F1.0}$	$\frac{8.0}{33}$	$\frac{8.2}{33}$	$\frac{7.9}{9}$	$\frac{8.6}{17}$	$\frac{8.0}{21}$ $\frac{8.6}{29}$ $\frac{8.6}{33}$	$\frac{8.0}{19.0}^{F1.0}$ $\frac{8.2}{24.2}^{12.00.8}$
$\frac{6.6}{19.0}^{F2.0}$	$\frac{6.8}{33}$	$\frac{6.6}{19}$	$\frac{6.5}{33}$	$\frac{5.9}{10}$	$\frac{6.4}{24}$ $\frac{6.0}{28}$ $\frac{6.0}{33}$	$\frac{6.2}{20.6}^{F1.4}$ $\frac{6.2}{23.9}^{12.00.6}$
$\frac{6.6}{23.9}^{DC.0.6}$ $\frac{6.6}{20.6}^{F1.4}$	$\frac{6.5}{33}$	$\frac{6.8}{14}$	$\frac{6.4}{14}$	$\frac{7.4}{24}$	$\frac{7.5}{33}$	$\frac{7.2}{23.0}^{F2.0}$
$\frac{5.0}{26.9}^{00.6}$	$\frac{4.9}{33}$	$\frac{5.1}{17}$	$\frac{6.1}{33}$	$\frac{5.6}{7}$	$\frac{5.8}{18}$ $\frac{6.9}{26}$ $\frac{7.0}{33}$	$\frac{5.8}{15.8}^{FO.2}$ $\frac{6.6}{24.5}^{D.C.1.0}$
$\frac{4.5}{28.4}^{01.6}$	$\frac{4.6}{33}$	$\frac{4.3}{19}$ $\frac{5.0}{14}$	$\frac{4.8}{33}$	$\frac{4.9}{10}$	$\frac{5.6}{24}$ $\frac{4.2}{33}$	$\frac{4.9}{27.8}^{01.2}$
	$\frac{5.1}{33}$	$\frac{4.6}{19}$ $\frac{5.0}{18}$	$\frac{4.7}{33}$	$\frac{4.7}{6}$	$\frac{3.5}{7}$ $\frac{4.1}{16}$ $\frac{3.6}{25}$ $\frac{4.6}{33}$	
$\frac{5.5}{28.1}^{01.4}$	$\frac{5.7}{33}$	$\frac{5.2}{11}$ $\frac{5.6}{10}$	$\frac{5.4}{33}$	$\frac{5.9}{5}$	$\frac{4.6}{6}$ $\frac{4.5}{16}$ $\frac{3.8}{22}$ $\frac{3.4}{33}$	$\frac{3.5}{31.1}^{03.4}$
	$\frac{6.9}{33}$	$\frac{7.4}{10}$ $\frac{8.4}{8}$	$\frac{7.8}{33}$	$\frac{8.4}{7}$	$\frac{7.1}{9}$ $\frac{6.9}{14}$ $\frac{6.9}{22}$ $\frac{6.2}{27}$ $\frac{6.8}{52}$	

Sta	+	H.I.	-	Grade	Gr. Pt
		927.27			
54				19.4	7.9
	+50			19.0	8.3
55				18.6	8.7
	B.M.	4.30	920.17	11.39	915.88
	B.M.			1.65	918.52
56				17.6	2.6
	+50			17.2	3.0
57				16.8	3.4
58				15.9	4.3
	+50			15.4	4.8
59				14.8	5.4
	+50			14.2	6.0
60				13.6	6.6
	T.P.	2.15	917.44	4.88	915.29
	+50			12.7	4.7

Lt      ±      Rt

DC.1.8 $\frac{8.1}{25.7}$		$\frac{8.1}{33}$	$\frac{8.4}{10}$	$\frac{9.4}{8}$	$\frac{9.1}{1}$	$\frac{9.5}{7}$	$\frac{8.3}{8}$	$\frac{9.5}{13}$	$\frac{7.6}{23}$	$\frac{8.1}{32}$	CO.4 $\frac{7.5}{26.6}$
F2.2 $\frac{10.5}{19.4}$	$\frac{10.3}{33}$	$\frac{10.2}{20}$	$\frac{10.8}{8}$	$\frac{11.2}{5}$	$\frac{10.9}{1}$	$\frac{11.0}{8}$	$\frac{10.4}{11}$	$\frac{10.9}{19}$	$\frac{10.4}{24}$	$\frac{10.3}{32}$	F2.2 $\frac{10.9}{20.2}$
F3.5 $\frac{12.2}{22.0}$		$\frac{12.2}{33}$	$\frac{12.3}{6}$	$\frac{11.9}{2}$	$\frac{12.0}{1}$	$\frac{11.9}{10}$	$\frac{12.8}{20}$	$\frac{13.9}{25}$	$\frac{12.7}{28}$	$\frac{12.5}{32}$	F4.0 $\frac{12.7}{23.0}$

Spt in 18" el in 35' Lt Sta 54+05

											F2.2 $\frac{4.8}{19.4}$
F2.0 $\frac{7.6}{19.0}$		$\frac{4.5}{33}$	$\frac{5.0}{1}$	$\frac{4.8}{14}$	$\frac{5.1}{17}$	$\frac{4.7}{26}$	$\frac{4.1}{32}$				
	$\frac{3.8}{33}$	$\frac{4.2}{15}$	$\frac{4.4}{1}$	$\frac{3.9}{7}$	$\frac{4.2}{14}$	$\frac{3.6}{18}$	$\frac{3.4}{28}$	$\frac{3.4}{33}$			

DC.0.4 $\frac{5.0}{23.6}$	F1.6 $\frac{5.0}{21.4}$		$\frac{5.0}{33}$	$\frac{5.0}{3}$	$\frac{4.9}{1}$	$\frac{4.4}{6}$	$\frac{5.1}{14}$	$\frac{4.3}{16}$	$\frac{3.9}{27}$	$\frac{3.8}{32}$	F4.8 $\frac{4.2}{18.2}$	DC.1.4 $\frac{4.0}{25.1}$
DC.0.6 $\frac{5.7}{23.9}$	F1.4 $\frac{5.7}{20.4}$		$\frac{5.4}{33}$	$\frac{6.0}{16}$	$\frac{5.4}{6}$	$\frac{4.9}{1}$	$\frac{5.7}{9}$	$\frac{6.0}{16}$	$\frac{5.8}{33}$		F1.6 $\frac{5.9}{21.4}$	DC.0.4 $\frac{5.9}{23.6}$

$\frac{5.4}{33}$	$\frac{5.8}{24}$	$\frac{6.3}{12}$	$\frac{5.8}{9}$	$\frac{5.3}{1}$	$\frac{5.7}{5}$	$\frac{6.8}{10}$	$\frac{6.7}{14}$	$\frac{6.7}{33}$
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DC.0.8 $\frac{6.6}{24.2}$	F1.2 $\frac{6.6}{19.8}$		$\frac{6.9}{33}$	$\frac{6.5}{18}$	$\frac{5.7}{10}$	$\frac{5.4}{1}$	$\frac{6.2}{7}$	$\frac{5.9}{13}$	$\frac{6.5}{17}$	$\frac{6.0}{20}$	$\frac{6.0}{33}$	DC.1.4 $\frac{6.0}{25.1}$
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$\frac{5.4}{33}$	$\frac{5.8}{11}$	$\frac{5.3}{1}$	$\frac{5.8}{5}$	$\frac{5.3}{8}$	$\frac{5.5}{14}$	$\frac{6.5}{17}$	$\frac{5.1}{20}$	$\frac{4.7}{25}$	$\frac{4.5}{33}$
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C1.0 $\frac{5.6}{27.5}$		$\frac{5.6}{33}$	$\frac{5.6}{23}$	$\frac{5.7}{11}$	$\frac{5.5}{1}$	$\frac{5.7}{14}$	$\frac{5.7}{14}$	$\frac{6.8}{17}$	$\frac{5.7}{20}$	$\frac{5.8}{29}$	$\frac{5.8}{33}$	C0.8 $\frac{5.8}{27.2}$
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Top of stake beside T.P.Rt sta. 60+12

$\frac{1.6}{33}$	$\frac{1.9}{24}$	$\frac{2.5}{19}$	$\frac{2.5}{1}$	$\frac{2.7}{12}$	$\frac{1.8}{8}$	$\frac{4.0}{15}$	$\frac{2.0}{19}$	$\frac{2.1}{33}$
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Sta	+	H.I.	-	Grade	Cr. Rd.
		917.44			
61				11.8	5.6
	+50			10.9	6.5
62				10.2	7.2
63				09.0	8.4
	+50			08.5	8.9
64			-	08.1	9.3
	T.P.	4.51	913.65	8.30	909.14
	+50			07.8	5.9
65			-0.3 +0.3	07.6	6.4 5.8 6.1
	+50		-0.5 +0.5	07.5	6.7 6.2 5.7
66			-0.9 +0.8	07.5	7.1 6.2 5.4
	+50		-1.2 +0.9	07.6	7.3 6.1 5.2
67			-1.2 +0.9	07.6	7.3 6.1 5.2

6-28-28 Cloudy-cool Carley 16  
 Lt. E Rt. Wilson  
 Wheeler

C18 (56) C3.4  
 $\frac{3.8}{28.7}$  3.8/33 3.7/21 4.2/14 4.6/10 4.9/3 4.0/4 4.4/4 3.3/7 3.3/11 4.5/14 2.1/20 2.3/33  $\frac{2.2}{31.1}$

0608 F12 (65) C12  
 $\frac{7.7}{24.2}$   $\frac{7.7}{19.8}$  8.2/33 7.8/26 7.6/11 7.7/9 7.3/7 7.4/5 6.7/6 6.0/18 5.3/21 5.1/33  $\frac{5.3}{27.8}$

F3.4 (70) F20  
 $\frac{10.6}{21.8}$  10.5/33 10.5/16 9.9/8 9.1/3 9.3/4 9.5/4 9.3/6 8.9/17 9.2/27 8.7/33  $\frac{9.2}{23.0}$

F3.4 (48) F4.0  
 $\frac{11.8}{21.8}$  11.2/33 11.8/17 12.4/14 11.9/6 11.4/6 11.5/4 12.2/9 12.1/19 12.9/27 12.7/33  $\frac{12.4}{23.0}$

F4.4 (59) F5.0  
 $\frac{13.3}{23.8}$  13.3/28 13.1/14 12.9/6 11.8/6 12.3/6 13.6/11 14.0/21 14.0/33  $\frac{13.9}{25.0}$

F3.4 (93) F3.0  
 $\frac{12.7}{21.8}$  12.7/33 12.7/13 11.8/8 11.5/6 11.9/6 12.6/10 12.3/13 12.4/23 12.2/30  $\frac{12.3}{21.0}$

C14 (59) C12  
 $\frac{4.5}{28.1}$  4.3/33 4.6/22 5.1/14 5.6/6 6.2/4 5.9/4 6.4/10 5.6/13 4.9/24 4.6/33  $\frac{4.7}{27.8}$

C2.6 (61) C10  
 $\frac{3.8}{29.9}$  3.6/33 4.0/21 4.5/18 4.8/15 5.2/4 5.0/4 4.7/3 5.5/12 5.6/23 4.8/28  $\frac{4.8}{27.5}$

C3.8 (62) F0.4 D.C.1.6  
 $\frac{2.9}{32.7}$  2.9/33 3.6/20 4.2/14 4.9/12 5.5/11 5.2/16 5.2/16 5.6/11 6.0/24 6.2/30 6.1/166  $\frac{6.1}{25.4}$

V.3.0 (120) F0.8 D.C.1.2  
 $\frac{2.5}{35.9}$  2.2/40 3.8/15 5.4/2 6.5/2 6.2/8 6.6/14 6.1/17 6.2/28  $\frac{6.2}{18.2}$   $\frac{6.2}{24.8}$

C4.0 (61) F3.6  
 $\frac{7.3}{36.0}$  3.1/40 5.1/13 5.9/7 6.5/7 7.1/5 8.7/9 8.4/15 9.0/22 8.1/24 8.2/34  $\frac{8.8}{22.2}$

C1.8 (61) F5.6  
 $\frac{5.2}{32.1}$  4.8/40 6.8/15 8.1/7 8.0/5 9.5/20 10.8/23 10.6/31 10.9/35  $\frac{10.8}{26.2}$

Sta.	+	H.I.	-	Grade	Gr. Rd.	
579		913.65				
+50			-1.2	+0.9	07.7	7.2 6.0
68			-1.2	+0.9	07.7	7.2 6.0
+50			-1.2	+0.9	07.8	7.1 5.9
69			-1.2	+0.9	07.8	7.1 5.9
T.P.	5.85	914.66	4.84		908.81	
+50			-1.2	+0.9	07.8	8.1 6.9
70			-1.2	+0.9	07.8	8.1 6.9
+50			-0.8	+0.7	07.7	8.2 7.0
71			-0.4	+0.4	07.6	7.5 7.1
+50			-0.2	+0.2	07.5	7.4 7.2
T.P.	5.74	911.64	8.76		905.90	
72					07.4	4.2
73					07.0	4.6
+50					06.8	4.8

Lt.      ♀      Pt.

4.0	$\frac{6.0}{31.8}$	$\frac{5.4}{40}$	$\frac{6.9}{21}$	$\frac{6.0}{8.4}$	$\frac{10.9}{33}$					$\frac{10.3}{25.4}$				
4.0	$\frac{6.8}{30.6}$	$\frac{6.3}{40}$	$\frac{7.9}{17}$	$\frac{6.0}{9.0}$	$\frac{11.5}{45}$					$\frac{10.3}{25.4}$				
4.0	$\frac{5.3}{32.7}$	$\frac{5.3}{40}$	$\frac{5.8}{15}$	$\frac{6.9}{7.0}$	$\frac{7.9}{16}$	$\frac{7.8}{10}$	$\frac{8.4}{22}$	$\frac{9.9}{40}$		$\frac{8.2}{21.4}$				
4.0	$\frac{1.1}{39.0}$	$\frac{1.0}{40}$	$\frac{2.2}{23}$	$\frac{5.9}{5.6}$	$\frac{6.6}{12}$	$\frac{9.3}{25}$	$\frac{9.2}{32}$	$\frac{9.4}{37}$		$\frac{8.4}{21.8}$				
4.0	$\frac{1.0}{40}$	$\frac{1.0}{40}$	$\frac{1.5}{28}$	$\frac{6.9}{4.3}$	$\frac{6.5}{6.5}$	$\frac{7.6}{3}$	$\frac{7.4}{11}$	$\frac{8.2}{20}$	$\frac{9.8}{40}$	$\frac{8.1}{19.2}$				
3.5	$\frac{2.3}{38.2}$	$\frac{2.5}{40}$	$\frac{2.1}{30}$	$\frac{2.7}{21}$	$\frac{4.2}{13}$	$\frac{5.0}{10}$	$\frac{5.0}{4}$	$\frac{3.9}{7}$	$\frac{4.0}{12}$	$\frac{6.4}{29}$	$\frac{7.9}{40}$	$\frac{5.8}{26.3}$		
7.0	$\frac{6.2}{30.0}$	$\frac{6.4}{33}$	$\frac{6.1}{23}$	$\frac{6.5}{15}$	$\frac{7.0}{14}$	$\frac{6.6}{8}$	$\frac{6.8}{11}$	$\frac{6.0}{6}$	$\frac{5.0}{6}$	$\frac{5.1}{26}$	$\frac{5.6}{34}$	$\frac{5.1}{27.5}$		
7.6.0.4	$\frac{9.1}{23.6}$	$\frac{8.7}{19.8}$	$\frac{9.4}{33}$	$\frac{8.7}{22}$	$\frac{8.7}{14}$	$\frac{8.3}{6}$	$\frac{8.9}{7}$	$\frac{8.3}{7}$	$\frac{7.3}{33}$	$\frac{7.9}{19.8}$	$\frac{7.7}{24.5}$	$\frac{10.6}{11.0}$		
4.2	$\frac{11.6}{23.4}$	$\frac{11.9}{33}$	$\frac{11.9}{30}$	$\frac{11.5}{22}$	$\frac{10.7}{17}$	$\frac{9.4}{13}$	$\frac{9.2}{17}$	$\frac{9.3}{7}$	$\frac{9.8}{2}$	$\frac{9.7}{6}$	$\frac{8.9}{8}$	$\frac{9.0}{18}$	$\frac{8.2}{33}$	$\frac{9.0}{19.0}$
4.2.4	$\frac{6.6}{19.8}$	$\frac{7.1}{33}$	$\frac{6.8}{23}$	$\frac{6.5}{20}$	$\frac{6.5}{16}$	$\frac{5.7}{17}$	$\frac{5.7}{7}$	$\frac{5.8}{7}$	$\frac{5.7}{14}$	$\frac{4.3}{33}$	$\frac{5.2}{19.0}$	$\frac{4.6}{25.4}$	$\frac{11.0}{11.6}$	
2.4	$\frac{7.6}{33}$	$\frac{7.6}{30}$	$\frac{6.9}{19}$	$\frac{6.2}{16}$	$\frac{6.1}{12}$	$\frac{5.6}{5}$	$\frac{5.2}{7}$	$\frac{6.0}{2}$	$\frac{5.7}{3}$	$\frac{5.3}{9}$	$\frac{5.2}{12}$	$\frac{4.2}{33}$	$\frac{4.6}{26}$	
		$\frac{6.4}{33}$	$\frac{5.4}{18}$	$\frac{4.8}{15}$	$\frac{5.0}{11}$	$\frac{5.0}{5}$	$\frac{5.1}{2}$	$\frac{4.8}{6}$	$\frac{4.0}{10}$	$\frac{3.3}{33}$				

Sta	+	H.I.	-	Grade	Gr. Rd
		911.64			
B.M.	660	911.67	6.60	905.04	905.07
74				06.6	5.1
	+50			06.4	5.3
75				06.3	5.4
	+50			06.2	5.5
76				06.1	5.6
	+50			06.1	5.6
77			+0.3 -0.3	06.1	5.3 5.9 5.6
	+50		+0.5 -0.5	06.2	5.0 5.5 6.0
	T.P.	7.45 911.46	7.66	904.01	
78			+0.7 -0.9	06.3	4.5 6.1 5.2
	+50		+0.9 -1.2	06.4	4.2 6.3 5.1
79			+0.9 -1.2	06.6	4.0 4.9 6.0

Lt      Rt

Spk. in 12" oak 200' Lt 579 73 + 95										C2.8	
$\frac{5.9}{24.8}$	$\frac{6.8}{33}$	$\frac{6.2}{27}$	$\frac{5.2}{18}$	$\frac{4.2}{4}$	$\frac{4.3}{5.1}$	$\frac{4.8}{14}$	$\frac{2.9}{18}$	$\frac{2.5}{33}$	$\frac{2.3}{30.2}$		
	$\frac{6.3}{33}$	$\frac{5.6}{26}$	$\frac{4.2}{13}$	$\frac{4.5}{5.3}$	$\frac{5.1}{10}$	$\frac{4.9}{15}$	$\frac{2.9}{22}$	$\frac{2.2}{27}$	$\frac{1.5}{33}$		
$\frac{C0.6}{4.8}$	$\frac{5.3}{33}$	$\frac{4.6}{25}$	$\frac{6.3}{17}$	$\frac{5.6}{10}$	$\frac{5.6}{5.4}$	$\frac{5.7}{11}$	$\frac{5.1}{21}$	$\frac{1.7}{33}$	$\frac{1.4}{32.0}$	C4.0	
	$\frac{6.9}{33}$	$\frac{5.9}{23}$	$\frac{7.0}{17}$	$\frac{6.3}{19}$	$\frac{6.0}{5.8}$	$\frac{6.0}{7}$	$\frac{6.2}{12}$	$\frac{6.2}{15}$	$\frac{5.7}{20}$	$\frac{5.3}{26}$	$\frac{3.3}{32}$
$\frac{F2.6}{8.4}$		$\frac{9.2}{33}$	$\frac{8.3}{23}$	$\frac{7.4}{18}$	$\frac{7.1}{5.6}$	$\frac{7.3}{14}$	$\frac{6.6}{16}$	$\frac{5.2}{16}$	$\frac{4.7}{19}$	$\frac{4.2}{33}$	C0.8
$\frac{F4.0}{9.6}$	$\frac{9.6}{33}$	$\frac{9.6}{24}$	$\frac{9.1}{10}$	$\frac{8.2}{17}$	$\frac{7.9}{5.6}$	$\frac{8.4}{17}$	$\frac{6.7}{19}$	$\frac{5.8}{33}$	$\frac{6.8}{19.8}$	$\frac{6.6}{24.8}$	DC1.0
$\frac{F4.6}{9.9}$	$\frac{9.9}{33}$	$\frac{10.0}{26}$	$\frac{9.9}{18}$	$\frac{8.4}{17}$	$\frac{8.3}{5.6}$	$\frac{8.4}{8}$	$\frac{9.0}{10}$	$\frac{8.5}{16}$	$\frac{7.4}{33}$	$\frac{8.1}{19.5}$	F2.2
$\frac{F4.8}{9.8}$		$\frac{9.7}{33}$	$\frac{9.7}{25}$	$\frac{9.3}{19}$	$\frac{8.4}{6}$	$\frac{8.2}{5.5}$	$\frac{8.3}{17}$	$\frac{7.9}{33}$	$\frac{8.2}{19.4}$	$\frac{8.2}{19.4}$	F2.2
$\frac{F3.0}{7.5}$		$\frac{7.7}{33}$	$\frac{7.7}{25}$	$\frac{7.4}{19}$	$\frac{7.1}{5.2}$	$\frac{7.1}{10}$	$\frac{6.4}{15}$	$\frac{6.6}{33}$	$\frac{6.7}{19.9}$	$\frac{6.9}{27.3}$	DC1.2
$\frac{F2.6}{6.8}$	$\frac{5.8}{33}$	$\frac{5.7}{26}$	$\frac{6.7}{21}$	$\frac{5.7}{17}$	$\frac{6.1}{14}$	$\frac{6.0}{5.1}$	$\frac{5.8}{14}$	$\frac{5.1}{18}$	$\frac{5.1}{33}$	$\frac{5.1}{31.8}$	C1.2
$\frac{6.1.0}{5.0}$	$\frac{5.0}{33}$	$\frac{5.4}{27}$	$\frac{5.2}{15}$	$\frac{4.5}{10}$	$\frac{4.8}{4.9}$	$\frac{4.9}{16}$	$\frac{5.3}{16}$	$\frac{5.3}{33}$	$\frac{5.3}{31.2}$	$\frac{5.3}{31.2}$	C0.8

W.2.5

W.4.0

W.4.0

Sta.	+	H.I.	-	Grade	Gr. Rd.
		911.46			
	+50		+0.9 -1.2	06.8	3.8' 4.7' 5.9'
80			+0.9 -1.2	07.0	3.6' 4.5' 5.7'
	+50		+0.9 -1.2	07.2	3.4' 4.3' 5.5'
81			+0.9 -1.2	07.4	3.2' 4.1' 5.3'
	+50		+0.9 -1.2	07.6	3.0' 3.9' 5.1'
82			+0.8 -1.1	07.7	3.0' 3.8' 4.9'
	+44.5 P.T.		+0.6 -0.7	07.7	3.2' 3.8' 4.5'
	T.P. 6.42	912.78	4.10	907.36	
83			+0.5 -0.5	07.6	5.7' 6.7' 6.2'
	+50		+0.2 -0.2	07.5	6.1' 6.3' 6.5'
84				07.2	6.6'
	+50			07.0	6.8'
	T.P. 3.87	909.29	8.36	905.42	
	B.M. 5.93	910 .01	5.17	904.12	
85				06.6	3.4

LT

~~RT~~

RT

0.0  
(3.8)  
26.0

3.4/33

3.9/11

(4.7)  
4.1

3.9/16

4.3/33

C2.6  
(4.3)  
33

W4.0

D.C.0.4  
(5.2)  
23.6

F1.4  
(5.0)  
20.6

5.3/33

5.5/29

5.0/13

(4.5)  
5.0

5.5/33

C0.2  
(5.5)  
30.3

W.4.0

F3.4  
(6.8)  
21.8

6.3/33

6.9/25

6.6/15

(4.3)  
6.4

6.6/12

6.3/33

D.C.1.0  
(6.5)  
28.5

W.4.0

F3.8  
(7.0)  
22.6

5.7/33

7.1/20

5.9/18

5.8/19

6.1/6

(4.1)  
6.2

6.6/17

6.4/33

D.C.1.0  
(6.3)  
28.5

W.4.0

F2.6  
(5.6)  
20.2

6.1/33

5.9/25

5.4/18

6.5/2

(3.9)  
6.8

6.3/3

5.7/13

6.2/33

F0.8  
(5.9)  
22.2

D.C.1.0  
(6.1)  
28.5

W.4.0

F2.6  
(5.6)  
20.2

4.4/33

4.4/29

5.6/22

5.0/14

5.6/13

(3.3)  
5.3

6.2/7

5.7/12

5.4/18

5.2/33

F0.4  
(5.3)  
24.6

D.C.1.6  
(5.3)  
29.4

W.4.0

F2.2  
(4.2)

2.4/33

2.4/25

3.1/22

4.8/17

4.5/11

4.8/10

(3.3)  
4.6

5.0/17

5.8/14

5.5/16

5.5/33

(5.5)  
21.0

D.C.1.0  
(5.5)  
26.5

W.2.0

Nail in T.P. RT of sta, 82+51 Quit here 6-28-28

(29.5)  
+2.5

33/3.3

25/3.0

20/5.6

16/6.1

11/5.7

5.8

8/6.0

13/6.7

16/6.3

23/6.8

33/9.0

(25.5)  
-0.1

(25.5)  
D+1.9

(31)  
+3.3

33/3.0

24/2.7

21/5.3

15/5.1

10/4.8

5.0

7/5.2

12/6.0

14/5.3

22/5.8

26/4.8

33/5.3

(28.5)  
+1.7

(30.5)  
+3.1

33/3.7

28/3.2

24/3.1

20/4.7

16/5.2

10/4.7

4.7

8/4.7

12/5.8

16/5.5

23/4.9

33/4.8

(28.5)  
+1.8

(28)  
+1.4

33/5.3

29/5.5

25/4.6

23/6.6

17/6.6

11/6.2

6.4

7/6.0

18/6.3

33/6.2

(27)  
+0.6

904.08 Spk in 30" C.P. - 25' RT. 89+00

(26)  
+2.0

(18.7)  
-0.9

33/3.7

28/3.5

20/3.9

17/4.7

11/4.0

4.0

7/4.1

18/3.7

33/3.9

(17)  
-0.5

(25.5)  
D+1.6

Sta.	B.S.	I.I.	F.S.	Grade	Gr. Rd.
85+50		910.01		06.1	3.9
86				05.7	4.3
+40				05.3	4.7
+50				05.1	4.9
87				04.6	5.4
+25				04.3	5.7
+50				04.0	6.0
88				03.4	6.6
+50				02.9	7.1
89				02.3	7.7
T.P.	2.17	903.66	8.52	901.49	
+50				01.7	2.0
90				01.3	2.4
+50				01.1	2.6
+75				01.0	2.7
91				01.0	2.7
+50				01.1	2.6

$\frac{24}{D+0.7}$	$\frac{20.5}{-1.4}$	$\frac{33}{5.2}$	$\frac{26}{5.3}$	$\frac{20}{5.2}$	$\frac{17}{6.0}$	$\frac{9}{4.9}$	4.8	$\frac{9}{5.3}$	$\frac{13}{6.0}$	$\frac{17}{5.7}$	$\frac{26}{5.6}$	$\frac{33}{5.0}$	$\frac{21.5}{-1.6}$	$\frac{24}{D+0.5}$
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$\frac{19.5}{-2.3}$	$\frac{33}{6.0}$	$\frac{23}{6.4}$	$\frac{18}{6.6}$	$\frac{12}{5.6}$	5.0	$\frac{9}{5.3}$	$\frac{13}{6.5}$	$\frac{21}{6.1}$	$\frac{33}{5.4}$	$\frac{22}{-1.7}$	$\frac{23.5}{D+0.4}$
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$\frac{33}{5.9}$	$\frac{27}{5.8}$	$\frac{24}{5.3}$	$\frac{19}{6.4}$	$\frac{16}{6.5}$	$\frac{7}{5.2}$	5.0	$\frac{8}{5.3}$	$\frac{13}{6.2}$	$\frac{24}{6.0}$	$\frac{33}{5.6}$
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$\frac{25}{-1.3}$	$\frac{18.5}{-0.9}$	$\frac{33}{5.7}$	$\frac{26}{5.5}$	$\frac{17}{6.3}$	$\frac{16}{7.4}$	$\frac{14}{6.2}$	$\frac{8}{5.2}$	4.9	$\frac{9}{5.2}$	$\frac{12}{6.2}$	$\frac{16}{6.3}$	$\frac{18}{5.8}$	$\frac{33}{5.3}$	$\frac{18}{-0.8}$	$\frac{25}{D+1.5}$
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$\frac{27.5}{+1.0}$	$\frac{33}{4.8}$	$\frac{20}{4.5}$	$\frac{16}{7.5}$	$\frac{11}{5.6}$	$\frac{8}{4.4}$	$\frac{7}{5.0}$	4.9	$\frac{9}{5.2}$	$\frac{13}{6.4}$	$\frac{18}{3.8}$	$\frac{33}{4.0}$	$\frac{29}{+1.9}$
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$\frac{33}{4.9}$	$\frac{20}{4.8}$	$\frac{16}{7.5}$	$\frac{14}{7.7}$	$\frac{8}{4.6}$	5.0	$\frac{8}{5.2}$	$\frac{11}{6.1}$	$\frac{18}{3.3}$	$\frac{24}{3.0}$	$\frac{33}{3.9}$
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$\frac{28}{+1.5}$	$\frac{33}{4.9}$	$\frac{30}{4.8}$	$\frac{21}{5.2}$	$\frac{17}{7.9}$	$\frac{14}{7.8}$	$\frac{8}{5.0}$	5.3	$\frac{8}{5.5}$	$\frac{12}{6.6}$	$\frac{16}{4.2}$	$\frac{24}{3.7}$	$\frac{33}{4.3}$	$\frac{29.5}{+2.2}$
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$\frac{27}{+0.8}$	$\frac{33}{5.6}$	$\frac{27}{5.8}$	$\frac{23}{5.9}$	$\frac{18}{8.6}$	$\frac{15}{8.5}$	$\frac{10}{6.2}$	6.3	$\frac{8}{6.5}$	$\frac{12}{7.4}$	$\frac{16}{5.2}$	$\frac{24}{4.9}$	$\frac{32}{5.1}$	$\frac{28.5}{+1.7}$
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$\frac{25}{D+1.4}$	$\frac{20}{-1.3}$	$\frac{33}{7.9}$	$\frac{21}{7.4}$	$\frac{18}{9.3}$	$\frac{15}{9.4}$	$\frac{11}{7.6}$	7.6	$\frac{8}{7.4}$	$\frac{11}{8.4}$	$\frac{14}{8.1}$	$\frac{18}{6.2}$	$\frac{33}{5.9}$	$\frac{28}{+1.2}$
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$\frac{23.5}{D+0.2}$	$\frac{21.5}{-1.6}$	$\frac{33}{10.0}$	$\frac{21}{9.2}$	$\frac{19}{9.6}$	$\frac{17}{9.7}$	$\frac{12}{8.6}$	9.0	$\frac{11}{9.3}$	$\frac{17}{9.0}$	$\frac{20}{7.8}$	$\frac{33}{7.8}$	$\frac{18.5}{-0.8}$	$\frac{26}{D+2.1}$
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$\frac{5}{0.2}$	$\frac{22.5}{-1.8}$	$\frac{33}{4.1}$	$\frac{20}{3.6}$	$\frac{18}{4.3}$	$\frac{16}{4.3}$	$\frac{11}{3.2}$	$\frac{8}{3.8}$	3.7	$\frac{14}{4.1}$	$\frac{22}{3.9}$	$\frac{33}{3.5}$	$\frac{19}{-2.1}$
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$\frac{21}{-2.8}$	$\frac{33}{5.0}$	$\frac{26}{4.9}$	$\frac{18}{5.4}$	$\frac{11}{5.0}$	4.7	$\frac{11}{4.9}$	$\frac{22}{5.4}$	$\frac{24}{6.3}$	$\frac{33}{6.3}$	$\frac{20.5}{-2.7}$
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$\frac{24.5}{-4.6}$	$\frac{33}{7.3}$	$\frac{28}{7.3}$	$\frac{9}{6.3}$	$\frac{6}{5.1}$	5.1	$\frac{7}{5.0}$	$\frac{12}{5.7}$	$\frac{24}{6.7}$	$\frac{33}{6.3}$	$\frac{22.5}{-3.7}$
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$\frac{33}{8.7}$	$\frac{15}{9.0}$	$\frac{12}{5.9}$	$\frac{6}{4.9}$	5.1	$\frac{7}{4.8}$	$\frac{14}{7.5}$	$\frac{16}{7.1}$	$\frac{33}{7.0}$
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$\frac{25}{-5.0}$	$\frac{33}{7.9}$	$\frac{25}{7.7}$	$\frac{13}{7.2}$	$\frac{7}{5.0}$	5.1	$\frac{7}{4.9}$	$\frac{12}{6.7}$	$\frac{17}{7.8}$	$\frac{20}{6.6}$	$\frac{25}{6.0}$	$\frac{33}{6.5}$	$\frac{22.5}{-3.7}$
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$\frac{21.5}{-3.3}$	$\frac{33}{5.7}$	$\frac{27}{5.6}$	$\frac{20}{5.8}$	$\frac{13}{4.9}$	4.6	$\frac{6}{4.5}$	$\frac{15}{7.3}$	$\frac{16}{7.2}$	$\frac{19}{5.9}$	$\frac{33}{6.3}$	$\frac{21}{-3.0}$
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Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
92		903.66		01.3	2.4
T.P.	5.47	906.67	2.46	901.20	
+50				01.5	5.2
+75				01.6	5.1
93				01.7	5.0
+50				01.9	4.8
94				02.1	4.6
+50				02.3	4.4
95				02.5	4.2
T.P.	7.27	908.74	5.20	901.47	
+50				02.7	6.0
96				02.9	5.8
+50				03.1	5.6
T.P.	9.58	917.29	1.03	907.71	
97				03.3	14.0
+30				03.4	13.9
+50				03.5	13.8
98				03.7	13.6

$$\begin{array}{cccccccccccc} \textcircled{24.5} & \textcircled{20} & 33 & 21 & 9 & & 5 & 12 & 19 & 30 & \textcircled{20.5} \\ \textcircled{D+1.1} & -1.3 & 3.3 & 3.6 & 3.5 & 3.7 & 3.5 & 4.4 & 5.2 & 5.1 & -2.8 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{29.5} & 33 & 22 & 16 & 9 & & 5 & 15 & 18 & 29 & 33 & \textcircled{23} \\ +2.1 & 2.8 & 4.0 & 6.1 & 5.5 & 5.6 & 5.4 & 7.5 & 9.2 & 8.6 & 7.6 & -3.9 \end{array}$$

$$\begin{array}{cccccccccccc} & 33 & 23 & 17 & 9 & & 6 & 13 & 18 & 26 & 33 & \\ & 1.9 & 3.1 & 5.5 & 4.9 & 5.0 & 4.8 & 8.2 & 9.3 & 8.2 & 6.7 & \\ \textcircled{29.5} & 33 & 28 & 21 & 9 & & 7 & 11 & 15 & 22 & 33 & \textcircled{21.5} \\ +2.4 & 2.4 & 2.8 & 4.0 & 5.8 & 5.0 & 5.0 & 6.6 & 9.1 & 8.3 & 6.0 & -3.2 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{25} & \textcircled{21} & 33 & 25 & 22 & 19 & 10 & & 11 & 15 & 17 & 33 & \textcircled{20} \\ \textcircled{D+1.3} & -1.5 & 5.4 & 5.5 & 6.1 & 6.2 & 5.7 & 5.9 & 6.9 & 9.0 & 7.9 & 6.0 & -2.4 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{23.5} & 33 & 28 & 18 & 12 & & 3 & 8 & 12 & 18 & 33 & \textcircled{21.5} \\ -4.3 & 9.3 & 8.9 & 6.2 & 6.1 & 5.7 & 6.4 & 8.2 & 9.5 & 8.4 & 6.8 & -3.2 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{24} & 33 & 28 & 20 & 14 & & 8 & 11 & 23 & 33 & \textcircled{23.5} \\ -4.5 & 9.4 & 8.8 & 8.7 & 5.9 & 6.0 & 8.5 & 9.0 & 8.7 & 8.8 & -4.3 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{21} & 33 & 19 & 17 & 13 & & 7 & 21 & 33 & \textcircled{23} \\ -2.9 & 7.3 & 6.9 & 6.3 & 5.8 & 6.1 & 7.8 & 8.3 & 8.7 & 8.7 & -4.1 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{18} & 33 & 26 & 23 & 14 & 8 & & 4 & 20 & 33 & \textcircled{19.5} \\ -1.5 & 9.7 & 7.4 & 7.9 & 7.1 & 7.1 & 7.7 & 8.3 & 8.3 & 8.9 & -2.3 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{5.5} & 33 & 30 & 26 & 22 & 20 & 15 & 9 & & 9 & 17 & 33 & \textcircled{19} & \textcircled{24} \\ \textcircled{0.4} & 4.5 & 4.7 & 6.2 & 6.5 & 5.4 & 5.6 & 5.5 & 6.0 & 6.6 & 6.6 & 7.8 & -1.0 & \textcircled{D+0.6} \\ \textcircled{5.5} & & & & & & & & & & & & & \end{array}$$

$\textcircled{D+1.6}$

$$\begin{array}{cccccccccccc} \textcircled{6.5} & 40 & 33 & 29 & 26 & 22 & 20 & 9 & & 8 & 17 & 33 & \textcircled{26} \\ \textcircled{3.8} & 1.7 & 1.8 & 1.9 & 3.3 & 3.5 & 3.0 & 3.2 & 3.6 & 4.9 & 4.9 & 6.0 & 0.0 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{38.5} & 40 & 30 & 24 & 22 & 10 & & 14 & 33 & \textcircled{30} \\ +8.3 & 5.8 & 6.2 & 10.5 & 9.8 & 9.4 & 10.1 & 9.8 & 11.3 & +2.8 \end{array}$$

$$\begin{array}{cccccccccccc} 40 & 31 & 27 & 23 & 19 & 10 & & 8 & 18 & 33 \\ 2.3 & 2.7 & 7.8 & 9.6 & 8.9 & 8.5 & 8.8 & 8.1 & 8.0 & 9.3 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{40} & 40 & 35 & 27 & 22 & 19 & 10 & & 10 & 18 & 33 & \textcircled{33} \\ +12.0 & 1.8 & 1.8 & 6.0 & 9.2 & 8.7 & 8.5 & 8.8 & 7.6 & 7.2 & 8.5 & +5.3 \end{array}$$

$$\begin{array}{cccccccccccc} \textcircled{37} & 40 & 34 & 29 & 21 & 9 & & 7 & 15 & 33 & \textcircled{31} \\ +7.2 & 6.0 & 6.4 & 6.9 & 10.5 & 9.8 & 10.2 & 9.9 & 8.9 & 10.3 & +3.4 \end{array}$$

Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
98+50		917.29		03.9	13.4
T.P.	2.90	908.7A	11.45	905.84	
99				04.1	4.6
+25				04.2	4.5
+50				04.4	4.3
100				04.7	4.0
+50				05.1	3.6
101				05.6	3.1
T.P.	8.68	914.12	3.30	905.44	
+50				06.2	2.9
102				06.9	2.2
+50				07.7	6.4
103				08.6	5.5
+50				09.6	4.5
104				10.6	3.5
+50				11.7	2.4

$$\begin{pmatrix} 28 \\ +1.3 \end{pmatrix} \begin{matrix} 40 & 33 & 23 & 18 & 10 \\ 11.7 & 11.9 & 12.6 & 12.1 & 12.2 \end{matrix} \begin{matrix} 16 & 33 \\ 12.0 & 12.4 \end{matrix} \begin{pmatrix} 29.5 \\ +1.0 \end{pmatrix}$$

$$\begin{pmatrix} 18 \\ -1.4 \end{pmatrix} \begin{matrix} 33 & 20 & 14 \\ 7.1 & 6.8 & 4.7 \end{matrix} 5.0 \begin{matrix} 6 & 20 & 33 \\ 6.5 & 6.3 & 6.0 \end{matrix} \begin{pmatrix} 21.5 \\ -1.6 \end{pmatrix} \begin{pmatrix} 23.5 \\ D+0.4 \end{pmatrix}$$

$$\begin{matrix} 33 & 21 & 14 \\ 7.5 & 7.5 & 5.2 \end{matrix} 5.2 \begin{matrix} 3 & 19 & 33 \\ 6.8 & 7.4 & 7.1 \end{matrix}$$

$$\begin{pmatrix} 21 \\ -3.0 \end{pmatrix} \begin{matrix} 33 & 21 & 14 & 8 \\ 7.4 & 7.2 & 5.3 & 5.1 \end{matrix} 5.1 \begin{matrix} 5 & 20 & 33 \\ 6.0 & 5.5 & 5.3 \end{matrix} \begin{pmatrix} 20 \\ -1.2 \end{pmatrix} \begin{pmatrix} 24.5 \\ D+0.9 \end{pmatrix}$$

$$\begin{pmatrix} 18 \\ -1.6 \end{pmatrix} \begin{matrix} 33 & 24 & 22 & 15 & 8 \\ 5.8 & 5.7 & 6.7 & 4.7 & 4.5 \end{matrix} 4.7 \begin{matrix} 8 & 23 & 33 \\ 4.5 & 4.3 & 4.0 \end{matrix} \begin{pmatrix} 17 \\ -0.5 \end{pmatrix} \begin{pmatrix} 25.5 \\ D+1.7 \end{pmatrix}$$

$$\begin{pmatrix} 21 \\ -3.0 \end{pmatrix} \begin{matrix} 33 & 24 & 22 & 17 & 8 \\ 5.7 & 5.8 & 6.7 & 5.1 & 4.4 \end{matrix} 4.6 \begin{matrix} 7 & 21 & 33 \\ 5.1 & 4.6 & 4.4 \end{matrix} \begin{pmatrix} 19 \\ -1.0 \end{pmatrix} \begin{pmatrix} 24.5 \\ D+1.1 \end{pmatrix}$$

$$\begin{pmatrix} 21 \\ -2.9 \end{pmatrix} \begin{matrix} 33 & 23 & 19 & 9 \\ 6.9 & 6.5 & 5.6 & 4.8 \end{matrix} 5.3 \begin{matrix} 6 & 9 & 23 & 33 \\ 5.9 & 5.4 & 5.7 & 5.6 \end{matrix} \begin{pmatrix} 20 \\ -2.6 \end{pmatrix}$$

Jpk. in P.P. - 30' Lt. 101 + 25

$$\begin{pmatrix} 19 \\ -2.1 \end{pmatrix} \begin{matrix} 33 & 24 & 16 \\ 10.4 & 10.5 & 10.1 \end{matrix} 10.7 \begin{matrix} 7 & 18 & 33 \\ 10.9 & 11.7 & 11.9 \end{matrix} \begin{pmatrix} 23 \\ -4.0 \end{pmatrix}$$

$$\begin{pmatrix} 18.5 \\ -1.7 \end{pmatrix} \begin{matrix} 33 & 30 & 29 & 17 \\ 7.9 & 8.5 & 9.1 & 8.9 \end{matrix} 9.1 \begin{matrix} 8 & 18 & 33 \\ 9.3 & 9.2 & 9.7 \end{matrix} \begin{pmatrix} 19 \\ -2.1 \end{pmatrix}$$

$$\begin{pmatrix} 24.5 \\ D+0.9 \end{pmatrix} \begin{pmatrix} 18 \\ -0.9 \end{pmatrix} \begin{matrix} 33 & 29 & 24 & 11 \\ 6.4 & 8.3 & 7.5 & 7.0 \end{matrix} 7.2 \begin{matrix} 7 & 8 & 14 & 18 & 33 \\ 7.2 & 6.7 & 6.3 & 6.7 & 6.9 \end{matrix} \begin{pmatrix} 25.5 \\ -0.4 \end{pmatrix} \begin{pmatrix} 25.5 \\ D+1.6 \end{pmatrix}$$

$$\begin{pmatrix} 5.5 \\ +1.7 \end{pmatrix} \begin{pmatrix} 25.5 \\ -0.3 \end{pmatrix} \begin{matrix} 33 & 30 & 25 & 21 & 11 \\ 6.1 & 6.7 & 5.7 & 5.4 & 5.3 \end{matrix} 5.0 \begin{matrix} 5 & 9 & 20 & 33 \\ 4.7 & 4.8 & 4.6 & 4.9 \end{matrix} \begin{pmatrix} 27 \\ +0.6 \end{pmatrix}$$

$$\begin{pmatrix} 26 \\ D+1.9 \end{pmatrix} \begin{pmatrix} 26 \\ -0.1 \end{pmatrix} \begin{matrix} 33 & 32 & 29 & 21 & 10 \\ 5.3 & 5.5 & 4.7 & 4.7 & 4.5 \end{matrix} 3.8 \begin{matrix} 8 & 19 & 33 \\ 3.7 & 3.5 & 3.4 \end{matrix} \begin{pmatrix} 28 \\ +1.2 \end{pmatrix}$$

$$\begin{pmatrix} 25 \\ D+1.2 \end{pmatrix} \begin{pmatrix} 19.5 \\ -1.1 \end{pmatrix} \begin{matrix} 33 & 29 & 20 & 10 \\ 4.8 & 4.4 & 4.6 & 4.5 \end{matrix} 4.0 \begin{matrix} 5 & 6 & 20 & 33 \\ 4.1 & 3.7 & 2.8 & 2.4 \end{matrix} \begin{pmatrix} 29.5 \\ +1.0 \end{pmatrix}$$

$$\begin{pmatrix} 18 \\ -1.6 \end{pmatrix} \begin{matrix} 33 & 20 & 10 \\ 4.3 & 4.1 & 3.8 \end{matrix} 3.6 \begin{matrix} 4 & 13 & 33 \\ 3.4 & 3.3 & 2.4 \end{matrix} \begin{pmatrix} 18 \\ -0.7 \end{pmatrix} \begin{pmatrix} 25.5 \\ D+1.8 \end{pmatrix}$$

Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
105		914.12		12.8	1.3
T.P.	5.90	917.47	2.55	911.57	
B.M.	4.32	919.48	4.32	913.15	
+50				13.9	3.6
106				15.0	2.5
T.P.	9.17	923.98	2.67	914.81	
+50				16.1	2.9
107				17.2	6.8
+50				18.1	5.9
108				18.6	5.4
+50			+0.0 -0.0	18.7	5.3
109			+0.2 -0.2	18.4	5.4 5.6
+50			+0.5 -0.5	18.0	5.5 3.5 6.0 4.0
T.P.	8.42	925.51	6.89	917.09	
110			+0.7 -0.8	17.8	2.0 2.7
+50			+0.9 -1.2	17.9	4.7 7.6

$\frac{18.5}{-1.7}$   $\frac{33}{2.8}$   $\frac{23}{3.4}$   $\frac{18}{3.0}$   $\frac{11}{3.0}$  2.5  $\frac{6}{2.7}$   $\frac{13}{2.4}$   $\frac{27}{1.5}$   $\frac{33}{1.3}$   $\frac{18}{-0.7}$   $\frac{25.5}{D+1.7}$

9/13.16 S.E. Cor. Conc. Porch - 75' Lt. 104+85

$\frac{24.5}{D+1.1}$   $\frac{20.5}{-1.4}$   $\frac{33}{4.3}$   $\frac{23}{4.5}$   $\frac{22}{5.1}$   $\frac{18}{5.0}$   $\frac{9}{4.6}$  5.2  $\frac{6}{5.6}$   $\frac{22}{4.8}$   $\frac{33}{4.7}$   $\frac{20}{-1.3}$   $\frac{24}{D+0.7}$

$\frac{25.5}{D+1.7}$   $\frac{18}{-0.7}$   $\frac{33}{2.8}$   $\frac{18}{3.2}$   $\frac{14}{2.8}$   $\frac{8}{2.7}$  3.3  $\frac{5}{3.8}$   $\frac{17}{3.3}$   $\frac{33}{2.8}$   $\frac{18}{-0.7}$   $\frac{25.5}{D+1.6}$

$\frac{26.5}{+0.3}$   $\frac{33}{7.6}$   $\frac{18}{7.5}$   $\frac{8}{7.2}$  7.5  $\frac{8}{8.3}$   $\frac{21}{7.6}$   $\frac{33}{7.7}$   $\frac{26.5}{+0.3}$

$\frac{28.5}{+1.8}$   $\frac{33}{5.1}$   $\frac{16}{5.2}$   $\frac{9}{5.3}$  5.4  $\frac{10}{5.8}$   $\frac{21}{5.9}$   $\frac{33}{5.9}$   $\frac{29.5}{+1.0}$

$\frac{29.5}{+1.1}$   $\frac{33}{4.8}$   $\frac{18}{4.7}$   $\frac{9}{4.3}$  4.4  $\frac{8}{4.6}$   $\frac{15}{4.8}$   $\frac{27}{4.3}$   $\frac{33}{4.5}$   $\frac{28.5}{+1.6}$

$\frac{26}{0.0}$   $\frac{33}{5.5}$   $\frac{24}{5.4}$   $\frac{15}{5.1}$   $\frac{9}{4.5}$  4.5  $\frac{8}{4.5}$   $\frac{16}{4.4}$   $\frac{33}{4.1}$   $\frac{28}{+1.3}$

$\frac{24.5}{D+1.0}$   $\frac{18}{-0.7}$   $\frac{33}{6.1}$   $\frac{28}{6.3}$   $\frac{17}{6.0}$   $\frac{9}{5.3}$  5.3  $\frac{8}{5.2}$   $\frac{15}{6.1}$   $\frac{23}{5.1}$   $\frac{20}{5.0}$   $\frac{33}{5.1}$   $\frac{26.5}{+0.3}$

$\frac{18.5}{-1.7}$   $\frac{33}{7.6}$   $\frac{22}{9.3}$   $\frac{14}{6.8}$   $\frac{9}{6.5}$  6.1  $\frac{7}{6.2}$   $\frac{14}{6.8}$   $\frac{22}{6.4}$   $\frac{33}{6.3}$   $\frac{18.5}{-0.7}$   $\frac{25}{D+1.4}$

$\frac{24.5}{-4.7}$   $\frac{33}{8.7}$   $\frac{28}{8.2}$   $\frac{17}{8.1}$   $\frac{7}{7.2}$  6.4  $\frac{7}{6.5}$   $\frac{11}{7.0}$   $\frac{20}{6.7}$   $\frac{33}{6.4}$   $\frac{20}{-2.4}$

Y.  
0.0

Y. in P.P. Lt. 110+

$\frac{22}{-3.5}$   $\frac{33}{11.2}$   $\frac{24}{10.6}$   $\frac{12}{9.8}$   $\frac{6}{8.8}$  8.3  $\frac{8}{8.3}$   $\frac{16}{8.9}$   $\frac{26}{8.9}$   $\frac{33}{8.7}$   $\frac{18}{-0.3}$   $\frac{27}{D+1.6}$

1.8

$\frac{20}{-2.5}$   $\frac{33}{9.3}$   $\frac{26}{9.4}$   $\frac{15}{9.3}$   $\frac{11}{8.6}$  8.3  $\frac{3}{8.2}$   $\frac{10}{9.5}$   $\frac{20}{9.6}$   $\frac{33}{9.2}$   $\frac{21.5}{-0.7}$   $\frac{29}{D+1.6}$

3.7

Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
110 + 92		925.51			
111			+0.9   -1.2	18.2	6.4 7.3
+50			+0.9   -1.2	18.7	5.9 5.9 6.8
112			+0.9   -1.2	19.4	5.2 6.1
+20				19.7	5.8
+40				20.1	5.4
+50			+0.9   -1.2	20.3	4.3 5.2
113			+0.9   -1.2	21.4	3.2 4.1
+53.46			+0.7   -0.8	22.8	2.0 2.7
B.M.			4.63	920.88	

Section Unnecessary

$\frac{17.5}{-1.3}$	$\frac{33}{8.5}$	$\frac{28}{8.4}$	$\frac{18}{7.7}$	$\frac{13}{7.8}$	$\frac{9}{8.4}$	9.2	$\frac{12}{9.4}$	$\frac{25}{9.5}$	$\frac{33}{9.4}$	$\frac{22.5}{-0.9}$	$\frac{28}{D+1.0}$	1%	3.7
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$\frac{18}{-1.6}$	$\frac{33}{7.1}$	$\frac{28}{7.2}$	$\frac{24}{7.8}$	$\frac{22}{7.2}$	$\frac{9}{7.6}$	$\frac{6}{8.0}$	7.6	$\frac{11}{7.6}$	$\frac{18}{8.1}$	$\frac{33}{8.5}$	$\frac{19.5}{-0.2}$	$\frac{29}{D+1.5}$	3.7
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$\frac{19}{-2.1}$	$\frac{33}{5.3}$	$\frac{28}{5.3}$	$\frac{22}{7.0}$	$\frac{16}{7.2}$	$\frac{12}{5.9}$	5.6	$\frac{13}{5.7}$	$\frac{24}{5.8}$	$\frac{33}{6.4}$	$\frac{31}{+1.0}$	3.7
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$\frac{33}{4.7}$	$\frac{16}{5.0}$	$\frac{11}{6.4}$	$\frac{5}{6.8}$	4.6	$\frac{18}{4.6}$	$\frac{33}{5.0}$	
$\frac{33}{4.5}$	$\frac{17}{4.5}$	$\frac{7}{4.6}$	6.4	$\frac{4}{6.5}$	$\frac{10}{3.6}$	$\frac{24}{3.9}$	$\frac{33}{4.2}$

$\frac{26}{0.0}$	$\frac{33}{4.3}$	$\frac{18}{4.2}$	$\frac{4}{4.4}$	5.1	$\frac{4}{6.3}$	$\frac{9}{6.4}$	$\frac{15}{3.3}$	$\frac{25}{3.6}$	$\frac{33}{3.8}$	$\frac{33}{+2.6}$	3.7
------------------	------------------	------------------	-----------------	-----	-----------------	-----------------	------------------	------------------	------------------	-------------------	-----

Used a 4.6 Gr.Rd.

$\frac{19}{3.4}$	$\frac{10}{3.4}$	3.4	$\frac{12}{3.5}$	$\frac{17}{5.5}$	$\frac{22}{5.9}$	$\frac{26}{3.7}$	$\frac{33}{3.8}$	$\frac{31}{+1.0}$	3.7
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2.4	$\frac{12}{2.6}$	$\frac{18}{2.7}$	$\frac{25}{5.1}$	$\frac{28}{4.9}$	$\frac{31}{2.3}$	$\frac{33}{2.2}$	1.8
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920.86 Spk. in 30" Box Elder N.E. Cor. Intersection.

Culv. - Sta. 90+75 - (36" x 52' P.3.)

B.M.	0.85	904.93.		904.08	
T.P.	4.46	903.45.	5.94	898.99.	
90+75				01.0	2.5
No. End.				894.6	8.9
So. End				894.2	9.3

Culv. - Sta. 101+00 - (24" x 36' P.3.)

T.P.	2.93	908.37.		905.44	
101+00				05.6	2.8
No. End				01.8	6.6
So. End				01.6	6.8

Culv. - Sta. 110+13 - (24" x 42' P.3.)

T.P.	5.24	922.33.		917.09	
110+13				19.8	4.5
No. End				13.9	8.4
So. End				14.3	8.0

Culv. - Sta. 77+00 (36" x 48' P.3.)

B.M.	4.63	909.70.		905.07	
77+00				06.1	3.6
W. End				901.7	8.0
E. End				902.1	7.6

Spt. in 30" C.M. - 25' Rt. - 89+00

$$\frac{26}{8.9}$$

$$\frac{26}{9.3}$$

Blue Top 2.0' Above.

" " 3.0' "

Spt. in P.P. - 30' Lt. 101+25

$$\frac{33}{6.6}$$

Blue Top 1.0' Above

" " 2.0' "

Spt. in P.P. - Lt. 110+

$$\frac{33}{8.4} \quad \frac{21}{8.2} \quad \frac{13}{7.6} \quad \frac{8}{5.7} \quad 5.1 \quad \frac{10}{5.2} \quad \frac{15}{5.7} \quad \frac{21}{5.7} \quad \frac{33}{5.5}$$

Blue Top 2.0' Above (110+19 - Inp. 12" x 22' C.M.)

" " 4.0' "

Spt. in 12" Oak - 200' Lt. 73+95

Blue Top to Grade

" " 2.0' Above.

Culv. 32+00 - (24" x 36' P3)

B.M.	8.47	933.05.	924.58	
32+00			28.5	4.6
No. End			25.5	7.6
So. End.			25.7	7.4

Culv. 9+10 - (24" x 42' P3)

B.M.	3.85	906.77.	902.92.	
T.P.	4.52	904.99.	6.30	900.47.
9+10			02.9	2.1
No. End			98.6	6.4
So. End			98.6	6.4

Spk. in T.P. - 20' Rt. 27+40

$$\frac{19}{-2.0}$$

$$\frac{21}{-3.1}$$

Blue Top to Grade

" " 1.0' Above.

Spk. in 30" Tree - 40' Rt. 17+10

$$\frac{100}{6.4}$$

$$\frac{21}{6.2}$$

$$\frac{21}{6.4}$$

$$\frac{100}{6.3}$$

Blue Top to Grade

" " " "

Σ 129<sup>2</sup>

0 + 00

9-19-29

□ HUB.

105° 00'

HUB □

30'

□ HUB.

65°

HUB □

□ NAIL IN 10" OAK.

B.M.	5.46	105.46 ✓	100.00
0+00			
0+07			
0+21			
0+40			
0+60			93.7
0+75			93.5
1+00			93.4
1+10			92.7
1+21			100.7
1+38			100.4
1+55			01.0
1+74			93.2

7-19-28

SPIN IN 30" OAK 10 RT. STA. 0-30.

<u>70.1</u>	<u>98</u>	<u>96</u>	<u>87</u>		<u>46</u>	<u>2.7</u>	<u>2.5</u>	<u>4.3</u>	<u>5.0</u>	<u>4.4</u>
42	32	17	10	5.8	9	13	30	45	58	70

<u>100</u>	<u>92</u>	<u>93</u>	<u>68</u>		<u>2.1</u>	<u>1.5</u>	<u>2.2</u>	<u>3.9</u>	<u>3.5</u>
45	37	17	9	4.6	13	30	42	50	70

<u>115</u>	<u>112</u>	<u>96</u>	<u>93</u>	<u>64</u>	<u>104</u>		<u>10.7</u>	<u>10.2</u>	<u>7.4</u>	<u>2.2</u>	<u>1.8</u>	<u>1.8</u>
60	52	48	26	14	7	11.0	15	30	38	50	64	70

<u>11.0</u>	<u>87</u>	<u>87</u>	<u>97</u>	<u>10.7</u>	<u>11.7</u>		<u>10.5</u>	<u>11.5</u>	<u>11.5</u>	<u>8.6</u>	<u>7.3</u>	<u>7.13</u>	<u>7.2.0</u>
60	54	44	40	21	7	9.8	14	23	30	36	45	61	70

<u>101</u>	<u>8.0</u>	<u>80</u>	<u>112</u>	<u>11.7</u>		<u>11.5</u>	<u>12.7</u>	<u>11.9</u>	<u>13.4</u>	<u>12.7</u>	<u>8.1</u>	<u>6.9</u>	<u>7.18</u>	<u>7.28</u>
60	55	42	46	26	11.8	14	16	30	32	34	41	51	70	80

<u>10.6</u>	<u>7.6</u>	<u>80</u>	<u>12.1</u>	<u>12.5</u>	<u>12.4</u>		<u>12.4</u>	<u>12.3</u>	<u>13.6</u>	<u>11.8</u>	<u>8.5</u>	<u>7.9</u>	<u>5.9</u>	<u>4.1</u>	<u>7.54</u>	<u>7.24</u>
66	58	45	37	31	14	12.0	8	20	32	36	30	38	46	52	63	70

<u>10.4</u>	<u>9.4</u>	<u>80</u>	<u>13.8</u>	<u>12.8</u>	<u>12.8</u>		<u>12.2</u>	<u>12.2</u>	<u>9.2</u>	<u>8.5</u>	<u>7.6</u>	<u>5.7</u>	<u>7.50</u>	<u>7.12</u>
70	55	49	41	32	19	12.1	4	14	23	30	44	52	64	72

<u>10.2</u>	<u>8.4</u>	<u>12.2</u>	<u>11.9</u>	<u>12.7</u>	<u>12.3</u>		<u>9.8</u>	<u>8.3</u>	<u>8.1</u>	<u>6.7</u>	<u>7.0</u>	<u>8.1</u>	<u>7.2</u>	<u>4.4</u>	<u>7.2.2</u>	<u>7.04</u>
66	53	45	29	21	5	12.8	8	17	21	24	30	33	48	54	64	74

<u>9.4</u>	<u>9.3</u>	<u>8.1</u>	<u>13.1</u>	<u>12.8</u>	<u>11.9</u>	<u>12.6</u>	<u>12.6</u>	<u>7.8</u>		<u>4.8</u>	<u>6.6</u>	<u>6.5</u>	<u>8.2</u>	<u>8.3</u>	<u>7.2</u>	<u>1.0</u>	<u>7.1.6</u>	<u>7.07</u>
0	60	53	46	36	30	23	13	6	4.8	6	13	23	30	42	49	57	64	73

<u>9.9</u>	<u>8.6</u>	<u>9.4</u>	<u>12.9</u>	<u>12.8</u>	<u>12.1</u>	<u>12.8</u>	<u>12.5</u>	<u>5.6</u>		<u>6.2</u>	<u>6.9</u>	<u>8.3</u>	<u>7.9</u>	<u>3.4</u>	<u>1.5</u>	<u>0.8</u>	<u>7.2.4</u>	<u>0.0</u>
66	55	50	43	38	32	27	12	4	5.1	8	16	22	30	40	46	50	57	70

<u>9.8</u>	<u>7.7</u>	<u>11.7</u>	<u>11.9</u>	<u>12.1</u>	<u>5.2</u>		<u>4.5</u>	<u>7.0</u>	<u>7.8</u>	<u>6.7</u>	<u>3.4</u>	<u>0.0</u>	<u>7.4.2</u>	<u>7.1.1</u>
52	56	50	37	22	11	4.5	7	12	22	28	35	39	45	64

<u>9.5</u>	<u>7.1</u>	<u>11.4</u>	<u>12.5</u>	<u>12.4</u>		<u>11.1</u>	<u>7.9</u>	<u>5.8</u>	<u>4.5</u>	<u>7.0.7</u>	<u>7.0.8</u>	<u>0.6</u>
61	53	47	32	16	12.3	15	30	40	46	54	61	70

2+00

105.46 ✓

10.56

111.02 ✓

5.00

94.1 ✓

100.46 ✓

2+21

2+30

B.M.

11.02

100.00 ✓

9-17-28

$\frac{91}{60}$	$\frac{5.7}{48}$	$\frac{9.3}{47}$	$\frac{11.0}{45}$	$\frac{11.9}{36}$	$\frac{12.0}{24}$	$\frac{12.7}{11}$		$\frac{11.2}{9}$	$\frac{10.0}{15}$	$\frac{8.0}{30}$	$\frac{6.1}{35}$	$\frac{1.0}{44}$	$\frac{10.6}{48}$	$\frac{0.0}{55}$
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$\frac{11.4}{45}$	$\frac{9.3}{40}$	$\frac{8.8}{35}$	$\frac{9.1}{25}$	$\frac{6.2}{12}$		$\frac{4.4}{14}$	$\frac{4.5}{14}$	$\frac{3.6}{30}$	$\frac{3.2}{40}$	$\frac{4.6}{48}$	$\frac{6.8}{51}$
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$\frac{11.0}{24}$	$\frac{8.0}{14}$		$5.9$	$\frac{5.2}{15}$	$\frac{4.2}{30}$	$\frac{5.3}{40}$
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B.M. 4.57 914.49 ✓ 909.92

0 +00

0 +50

1

+50

2

+50

3

+15

+50

4

+50

5

1.97

908.07 ✓

7.39

05.9 ✓

906.10 ✓

7-26-28

$$\begin{array}{r} \frac{8.7}{33} \quad \frac{8.7}{23} \quad \frac{9.3}{22} \quad \frac{7.6}{15} \quad \textcircled{4.0} \quad \frac{8.8}{17} \quad \frac{9.3}{25} \quad \frac{7.3}{27} \quad \frac{6.9}{33} \end{array}$$

$$\begin{array}{r} \frac{9.4}{33} \quad \frac{8.8}{23} \quad \frac{7.4}{22} \quad \frac{7.4}{20} \quad \frac{6.9}{15} \quad \textcircled{4.1} \quad \frac{8.6}{19} \quad \frac{10.1}{29} \quad \frac{5.9}{35} \quad \frac{6.0}{37} \end{array}$$

$$\begin{array}{r} \frac{9.6}{33} \quad \frac{8.5}{30} \quad \frac{8.4}{28} \quad \frac{7.4}{25} \quad \frac{6.8}{15} \quad \textcircled{7.1} \quad \frac{8.7}{19} \quad \frac{9.9}{29} \quad \frac{6.1}{34} \quad \frac{6.1}{40} \end{array}$$

$$\begin{array}{r} \frac{8.7}{33} \quad \frac{9.1}{30} \quad \frac{9.5}{23} \quad \frac{6.5}{15} \quad \textcircled{7.1} \quad \frac{8.6}{20} \quad \frac{9.8}{28} \quad \frac{4.9}{35} \quad \frac{4.8}{40} \end{array}$$

$$\begin{array}{r} \frac{6.2}{33} \quad \frac{5.9}{28} \quad \frac{8.0}{24} \quad \frac{6.2}{15} \quad \textcircled{7.1} \quad \frac{8.4}{19} \quad \frac{9.9}{29} \quad \frac{3.4}{37} \quad \frac{3.5}{40} \end{array}$$

$$\begin{array}{r} \frac{6.1}{33} \quad \frac{5.5}{26} \quad \frac{7.3}{22} \quad \frac{6.3}{15} \quad \textcircled{6.9} \quad \frac{8.3}{19} \quad \frac{10.4}{29} \quad \frac{3.7}{37} \quad \frac{3.7}{40} \end{array}$$

$$\begin{array}{r} \frac{7.4}{33} \quad \frac{7.6}{23} \quad \frac{8.0}{22} \quad \frac{7.9}{20} \quad \frac{6.6}{15} \quad \textcircled{7.0} \quad \frac{8.4}{20} \quad \frac{10.0}{29} \quad \frac{5.2}{35} \quad \frac{5.2}{40} \end{array}$$

$$\begin{array}{r} \frac{7.1}{33} \quad \frac{7.4}{26} \quad \frac{8.1}{25} \quad \frac{8.1}{22} \quad \frac{6.3}{15} \quad \textcircled{7.0} \quad \frac{8.5}{19} \quad \frac{10.1}{28} \quad \frac{5.2}{35} \quad \frac{5.4}{40} \end{array}$$

$$\begin{array}{r} \frac{7.6}{33} \quad \frac{7.5}{29} \quad \frac{7.0}{24} \quad \frac{6.6}{15} \quad \textcircled{1.5} \quad \frac{8.6}{19} \quad \frac{10.0}{27} \quad \frac{5.4}{33} \quad \frac{5.5}{40} \end{array}$$

$$\begin{array}{r} \frac{6.2}{33} \quad \frac{7.4}{25} \quad \frac{8.6}{29} \quad \frac{8.6}{20} \quad \frac{7.3}{15} \quad \textcircled{1.7} \quad \frac{9.1}{19} \quad \frac{10.2}{28} \quad \frac{7.3}{32} \quad \frac{7.1}{40} \end{array}$$

$$\begin{array}{r} \frac{6.8}{33} \quad \frac{7.8}{25} \quad \frac{7.7}{22} \quad \frac{8.0}{15} \quad \textcircled{4.1} \quad \frac{9.3}{16} \quad \frac{11.1}{25} \quad \frac{10.4}{27} \quad \frac{9.4}{28} \quad \frac{10.2}{33} \end{array}$$

$$\begin{array}{r} \frac{9.2}{33} \quad \frac{9.7}{23} \quad \frac{10.5}{24} \quad \frac{8.7}{15} \quad \textcircled{5.1} \quad \frac{9.4}{15} \quad \frac{12.4}{23} \quad \frac{13.0}{33} \end{array}$$

908.07 ✓

750

05.4

6

04.8

7

04.2

750

03.9

8

03.4

9

02.4

713 CROSS PRAIN 24" X 36 P<sup>3</sup>

10

01.9

11

01.6

12

02.1 ✓

5.68

907.33 ✓

6.42

901.65 ✓

750

01.7

13

02.0



907.33 ✓

14

01.9

15

02.1

+86

02.4

+94

02.5

16

02.5

+07

02.4

+20

02.4

17

02.8 ✓

13.141

4.42

907.34 ✓

4.42

902.91 ✓

902.92

18

03.4

19

04.9 ✓

13.54

918.05 ✓

2.23

904.51 ✓

+50

05.9

20

06.9

9-26-28

$\frac{5.3}{33}$	$\frac{5.8}{28}$	$\frac{7.1}{26}$	$\frac{7.1}{24}$	$\frac{5.6}{15}$	(4.9)	$\frac{5.2}{15}$	$\frac{7.3}{22}$	$\frac{7.5}{30}$	$\frac{8.1}{31}$	$\frac{8.1}{33}$
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$\frac{7.4}{29}$	$\frac{7.5}{22}$	$\frac{5.5}{15}$	(4.6)	$\frac{5.3}{15}$	$\frac{7.6}{20}$	$\frac{7.7}{30}$	$\frac{8.3}{31}$	$\frac{8.1}{33}$
------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------	------------------

$\frac{7.2}{33}$	$\frac{6.5}{23}$	$\frac{6.4}{22}$	$\frac{5.0}{16}$	(4.7)	$\frac{5.2}{15}$	$\frac{5.8}{18}$	$\frac{6.6}{33}$
------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{5.6}{33}$	$\frac{5.0}{29}$	$\frac{5.0}{17}$	(4.7)	$\frac{5.3}{15}$	$\frac{5.1}{33}$
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$\frac{5.6}{33}$	$\frac{5.0}{26}$	$\frac{4.8}{15}$	(4.7)	$\frac{5.1}{15}$	$\frac{4.7}{33}$
------------------	------------------	------------------	-------	------------------	------------------

$\frac{5.5}{33}$	$\frac{4.9}{27}$	$\frac{4.7}{15}$	(4.7)	$\frac{5.0}{16}$	$\frac{5.0}{29}$	$\frac{5.0}{33}$
------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{7.6}{33}$	$\frac{6.9}{21}$	$\frac{4.7}{15}$	(4.7)	$\frac{5.0}{15}$	$\frac{6.6}{20}$	$\frac{6.6}{29}$	$\frac{7.8}{30}$	$\frac{7.1}{33}$
------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------	------------------

$\frac{7.6}{33}$	$\frac{7.5}{23}$	$\frac{7.3}{20}$	$\frac{5.0}{15}$	(4.6)	$\frac{4.8}{15}$	$\frac{7.0}{20}$	$\frac{6.8}{33}$
------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{7.6}{33}$	$\frac{7.6}{23}$	$\frac{7.2}{21}$	$\frac{4.2}{15}$	(3.9)	$\frac{4.2}{15}$	$\frac{5.6}{20}$	$\frac{5.1}{33}$
------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{5.3}{33}$	$\frac{4.6}{19}$	$\frac{2.6}{15}$	(2.2)	$\frac{2.4}{15}$	$\frac{4.6}{23}$	$\frac{0.6}{29}$	$\frac{0.0}{33}$
------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------

$\frac{12.3}{33}$	(11.9)	$\frac{14.2}{22}$	$\frac{14.1}{20}$	$\frac{12.6}{15}$	(11.8)	$\frac{12.4}{15}$	$\frac{14.2}{21}$	$\frac{14.2}{24}$	$\frac{7.0}{33}$	$\frac{6.5}{40}$
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$\frac{8.9}{33}$	$\frac{8.5}{27}$	$\frac{13.3}{23}$	$\frac{13.3}{20}$	$\frac{11.5}{15}$	(10.7)	$\frac{11.4}{15}$	$\frac{13.5}{19}$	$\frac{13.5}{21}$	$\frac{4.6}{33}$	$\frac{4.3}{40}$
------------------	------------------	-------------------	-------------------	-------------------	--------	-------------------	-------------------	-------------------	------------------	------------------

918.05 ✓

750

08.0

21

09.2

750

10.4

22

11.7

23

13.9

750

15.0

24

16.3 ✓

11.51

928.81 ✓

0.75

917.30 ✓

25

18.2

26

20.8

27

22.8

28

25.2 ✓

5.06

932.55 ✓

1.32

927.49 ✓

750

25.9

9-26-28

$\frac{6.4}{33}$	$\frac{6.6}{30}$	$\frac{12.4}{24}$	$\frac{12.2}{20}$	$\frac{10.6}{15}$	(9.5)	$\frac{10.5}{15}$	$\frac{12.3}{20}$	$\frac{12.3}{22}$	$\frac{2.9}{33}$	$\frac{3.0}{40}$
------------------	------------------	-------------------	-------------------	-------------------	-------	-------------------	-------------------	-------------------	------------------	------------------

$\frac{4.6}{33}$	$\frac{4.5}{32}$	$\frac{10.9}{23}$	$\frac{10.9}{20}$	$\frac{9.7}{15}$	(4.6)	$\frac{9.5}{15}$	$\frac{10.9}{18}$	$\frac{10.9}{20}$	$\frac{0.7}{33}$	$\frac{0.7}{35}$
------------------	------------------	-------------------	-------------------	------------------	-------	------------------	-------------------	-------------------	------------------	------------------

$\frac{4.5}{33}$	$\frac{4.4}{30}$	$\frac{9.9}{23}$	$\frac{9.6}{19}$	$\frac{8.2}{15}$	(7.5)	$\frac{8.3}{15}$	$\frac{9.7}{19}$	$\frac{9.7}{21}$	$\frac{1.9}{33}$	$\frac{1.8}{35}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------	------------------

$\frac{5.9}{33}$	$\frac{5.7}{26}$	$\frac{8.6}{23}$	$\frac{8.5}{20}$	$\frac{6.6}{15}$	(6.3)	$\frac{6.8}{15}$	$\frac{8.4}{1.9}$	$\frac{8.6}{22}$	$\frac{4.3}{30}$	$\frac{4.4}{33}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	-------------------	------------------	------------------	------------------

$\frac{4.9}{33}$	$\frac{4.9}{24}$	$\frac{6.5}{23}$	$\frac{4.5}{15}$	(4.0)	$\frac{4.3}{15}$	$\frac{5.6}{21}$	$\frac{5.6}{23}$	$\frac{5.4}{24}$	$\frac{5.5}{29}$	$\frac{5.5}{33}$
------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{3.7}{33}$	$\frac{3.8}{24}$	$\frac{4.7}{22}$	$\frac{4.7}{21}$	$\frac{3.4}{15}$	(2.4)	$\frac{3.2}{15}$	$\frac{4.8}{19}$	$\frac{5.0}{33}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{2.1}{33}$	$\frac{2.4}{24}$	$\frac{3.6}{23}$	$\frac{3.6}{21}$	$\frac{2.1}{15}$	(1.7)	$\frac{2.0}{15}$	$\frac{3.6}{19}$	$\frac{4.0}{33}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{11.5}{33}$	$\frac{11.6}{25}$	$\frac{12.5}{24}$	$\frac{10.9}{15}$	(10.1)	$\frac{10.6}{15}$	$\frac{12.2}{20}$	$\frac{12.1}{33}$
-------------------	-------------------	-------------------	-------------------	--------	-------------------	-------------------	-------------------

$\frac{9.5}{33}$	$\frac{9.5}{25}$	$\frac{10.6}{24}$	$\frac{10.5}{22}$	$\frac{8.3}{15}$	(7.8)	$\frac{8.3}{15}$	$\frac{9.4}{19}$	$\frac{9.4}{33}$
------------------	------------------	-------------------	-------------------	------------------	-------	------------------	------------------	------------------

$\frac{6.9}{33}$	$\frac{6.7}{25}$	$\frac{7.9}{24}$	$\frac{7.9}{22}$	$\frac{6.0}{15}$	(5.5)	$\frac{6.0}{15}$	$\frac{7.7}{22}$	$\frac{7.2}{23}$	$\frac{7.1}{33}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------

$\frac{3.0}{33}$	$\frac{3.1}{27}$	$\frac{5.4}{23}$	$\frac{5.4}{21}$	$\frac{4.0}{15}$	(3.5)	$\frac{3.9}{15}$	$\frac{5.6}{21}$	$\frac{2.0}{28}$	$\frac{2.1}{33}$
------------------	------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------

$\frac{6.6}{33}$	$\frac{6.0}{24}$	$\frac{8.6}{22}$	$\frac{7.1}{15}$	(6.5)	$\frac{6.9}{15}$	$\frac{8.5}{21}$	$\frac{3.4}{28}$	$\frac{3.4}{33}$
------------------	------------------	------------------	------------------	-------	------------------	------------------	------------------	------------------

932.55 ✓

29

26.7

+50

27.0

30

27.4

31

28.1

+50

28.2

32

28.6

+50

28.5

33

28.8

+50

28.8

34

29.1

+50

29.0

35

29.1 ✓

4.84

933.72 ✓

3.67

929.89 ✓



933.72 ✓

36

28.9

+50

28.8

37

28.3

+50

28.4

38

28.1

+50

28.0

39

28.1

+50

27.8

40

27.3 ✓

3.05

930.73 ✓

6.04

927.68 ✓

41

27.0

42

26.9

+50

26.8

9-26-28

$\frac{47}{33}$	$\frac{47}{27}$	$\frac{69}{24}$	$\frac{49}{15}$	(47)	$\frac{50}{15}$	$\frac{70}{23}$	$\frac{57}{28}$	$\frac{38}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{54}{33}$	$\frac{50}{27}$	$\frac{75}{23}$	$\frac{53}{15}$	(48)	$\frac{54}{15}$	$\frac{68}{23}$	$\frac{49}{26}$	$\frac{46}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{55}{33}$	$\frac{50}{27}$	$\frac{75}{24}$	$\frac{51}{15}$	(49)	$\frac{53}{15}$	$\frac{71}{24}$	$\frac{46}{27}$	$\frac{45}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{62}{33}$	$\frac{64}{26}$	$\frac{76}{24}$	$\frac{59}{15}$	(50)	$\frac{55}{15}$	$\frac{71}{23}$	$\frac{35}{28}$	$\frac{33}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{63}{33}$	$\frac{56}{26}$	$\frac{76}{23}$	$\frac{60}{15}$	(51)	$\frac{59}{15}$	$\frac{72}{23}$	$\frac{05}{33}$	$\frac{05}{35}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{71}{33}$	$\frac{59}{24}$	$\frac{76}{33}$	$\frac{59}{15}$	(52)	$\frac{61}{15}$	$\frac{71}{21}$	$\frac{70.4}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-------------------

$\frac{76}{33}$	$\frac{60}{26}$	$\frac{80}{23}$	$\frac{59}{15}$	(53)	$\frac{62}{15}$	$\frac{77}{22}$	$\frac{77}{24}$	$\frac{40}{29}$	$\frac{3.9}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{108}{33}$	$\frac{91}{21}$	$\frac{62}{15}$	(54)	$\frac{65}{15}$	$\frac{78}{20}$	$\frac{80}{27}$	$\frac{76}{33}$
------------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{118}{33}$	$\frac{108}{23}$	$\frac{62}{15}$	(55)	$\frac{66}{15}$	$\frac{8.9}{21}$	$\frac{8.9}{27}$	$\frac{9.3}{33}$
------------------	------------------	-----------------	------	-----------------	------------------	------------------	------------------

$\frac{91}{33}$	$\frac{89}{26}$	$\frac{37}{15}$	(56)	$\frac{41}{15}$	$\frac{9.1}{27}$	$\frac{8.8}{33}$
-----------------	-----------------	-----------------	------	-----------------	------------------	------------------

$\frac{62}{33}$	$\frac{62}{26}$	$\frac{61}{21}$	$\frac{43}{15}$	(57)	$\frac{42}{15}$	$\frac{71}{21}$	$\frac{7.7}{33}$
-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	------------------

$\frac{44}{33}$	$\frac{45}{25}$	$\frac{5.8}{23}$	$\frac{43}{15}$	(58)	$\frac{46}{15}$	$\frac{6.3}{22}$	$\frac{5.4}{24}$	$\frac{5.9}{33}$
-----------------	-----------------	------------------	-----------------	------	-----------------	------------------	------------------	------------------

930.73 ✓

43

26.5

+50

26.3

44

26.0

+50

26.3

45

25.9

46

25.5

+50

25.2

47

24.8

+40

24.9

48

24.4 ✓

2.50

926.67

6.54

924.17 ✓

49

23.4

50

23.1

9-26-28

$$\frac{2.7}{33} \quad \frac{2.4}{30} \quad \frac{6.0}{23} \quad \frac{4.5}{15} \quad \textcircled{4.2} \quad \frac{4.6}{15} \quad \frac{6.4}{22} \quad \frac{7.3}{25} \quad \frac{4.2}{33}$$

$$\frac{1.6}{33} \quad \frac{1.6}{31} \quad \frac{6.3}{24} \quad \frac{5.0}{15} \quad \textcircled{4.4} \quad \frac{4.8}{14} \quad \frac{6.1}{19} \quad \frac{6.1}{22} \quad \frac{2.9}{28} \quad \frac{3.0}{33}$$

$$\frac{2.7}{33} \quad \frac{2.8}{28} \quad \frac{6.6}{23} \quad \frac{5.3}{15} \quad \textcircled{4.6} \quad \frac{4.8}{15} \quad \frac{6.4}{23} \quad \frac{4.3}{28} \quad \frac{4.5}{33}$$

$$\frac{3.9}{33} \quad \frac{3.7}{28} \quad \frac{6.4}{23} \quad \frac{4.8}{15} \quad \textcircled{4.8} \quad \frac{4.9}{14} \quad \frac{6.8}{24} \quad \frac{6.1}{26} \quad \frac{6.5}{33}$$

$$\frac{4.8}{33} \quad \frac{4.7}{27} \quad \frac{6.5}{23} \quad \frac{5.4}{15} \quad \textcircled{5.0} \quad \frac{5.4}{15} \quad \frac{7.0}{24} \quad \frac{6.0}{26} \quad \frac{6.0}{33}$$

$$\frac{3.7}{33} \quad \frac{3.8}{28} \quad \frac{7.3}{24} \quad \frac{5.8}{15} \quad \textcircled{5.4} \quad \frac{5.6}{15} \quad \frac{7.2}{24} \quad \frac{5.9}{26} \quad \frac{5.6}{33}$$

$$\frac{4.0}{33} \quad \frac{4.0}{28} \quad \frac{7.5}{23} \quad \frac{6.1}{15} \quad \textcircled{5.6} \quad \frac{5.8}{15} \quad \frac{7.4}{22} \quad \frac{5.0}{27} \quad \frac{5.4}{33}$$

$$\frac{5.8}{33} \quad \frac{5.7}{26} \quad \frac{7.9}{22} \quad \frac{6.4}{15} \quad \textcircled{5.9} \quad \frac{6.2}{15} \quad \frac{7.6}{23} \quad \frac{5.3}{27} \quad \frac{5.0}{33}$$

$$\frac{6.8}{33} \quad \frac{6.7}{25} \quad \frac{8.3}{23} \quad \frac{6.6}{15} \quad \textcircled{6.1} \quad \frac{6.6}{15} \quad \frac{8.1}{23} \quad \frac{6.6}{24} \quad \frac{5.9}{33}$$

$$\frac{7.7}{33} \quad \frac{7.3}{26} \quad \frac{8.9}{22} \quad \frac{7.0}{15} \quad \textcircled{6.5} \quad \frac{6.7}{15} \quad \frac{8.8}{23} \quad \frac{7.8}{24} \quad \frac{7.4}{33}$$

$$\frac{4.6}{33} \quad \frac{4.6}{25} \quad \frac{5.6}{23} \quad \frac{3.7}{33} \quad \textcircled{3.7} \quad \frac{3.5}{15} \quad \frac{6.0}{22} \quad \frac{5.5}{24} \quad \frac{5.7}{33}$$

$$\frac{4.8}{33} \quad \frac{4.7}{25} \quad \frac{5.8}{23} \quad \frac{4.0}{15} \quad \textcircled{3.8} \quad \frac{4.3}{15} \quad \frac{6.0}{22} \quad \frac{5.1}{24} \quad \frac{5.1}{33}$$

✓  
926.67

+50

22.5

51

22.0

+50

21.7

52

21.2

+50

21.0

53

20.7

+70

19.6

54

19.2

+50

18.9

4.05

922.02 ✓

8.70

917.90 ✓

B.M.

0.83

919.35 ✓

3.52

918.49

918.52

55

18.2

+ 43 CROSS PRAIN 24" X 44 P<sup>3</sup>

7-26-28

$$\begin{array}{r} 60 \\ 33 \end{array} \quad \begin{array}{r} 60 \\ 24 \end{array} \quad \begin{array}{r} 65 \\ 23 \end{array} \quad \begin{array}{r} 47 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 4.2 \end{array} \quad \begin{array}{r} 4.7 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 23 \end{array} \quad \begin{array}{r} 5.8 \\ 24 \end{array} \quad \begin{array}{r} 5.5 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \quad \begin{array}{r} 61 \\ 25 \end{array} \quad \begin{array}{r} 6.9 \\ 24 \end{array} \quad \begin{array}{r} 5.1 \\ 15 \end{array} \quad \begin{array}{r} 4.5 \\ 4.7 \end{array} \quad \begin{array}{r} 4.9 \\ 15 \end{array} \quad \begin{array}{r} 6.4 \\ 19 \end{array} \quad \begin{array}{r} 6.8 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 26 \end{array} \quad \begin{array}{r} 6.7 \\ 33 \end{array}$$

$$\begin{array}{r} 46 \\ 33 \end{array} \quad \begin{array}{r} 45 \\ 26 \end{array} \quad \begin{array}{r} 72 \\ 23 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 5.0 \\ 5.0 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 72 \\ 23 \end{array} \quad \begin{array}{r} 6.2 \\ 25 \end{array} \quad \begin{array}{r} 61 \\ 27 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array}$$

$$\begin{array}{r} 41 \\ 33 \end{array} \quad \begin{array}{r} 40 \\ 28 \end{array} \quad \begin{array}{r} 77 \\ 24 \end{array} \quad \begin{array}{r} 5.7 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 5.5 \end{array} \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad \begin{array}{r} 7.6 \\ 23 \end{array} \quad \begin{array}{r} 4.3 \\ 28 \end{array} \quad \begin{array}{r} 4.0 \\ 30 \end{array} \quad \begin{array}{r} 3.5 \\ 33 \end{array}$$

$$\begin{array}{r} 4.7 \\ 33 \end{array} \quad \begin{array}{r} 4.8 \\ 29 \end{array} \quad \begin{array}{r} 80 \\ 24 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 5.9 \\ 5.7 \end{array} \quad \begin{array}{r} 6.2 \\ 15 \end{array} \quad \begin{array}{r} 8.2 \\ 23 \end{array} \quad \begin{array}{r} 2.9 \\ 28 \end{array} \quad \begin{array}{r} 3.0 \\ 33 \end{array}$$

$$\begin{array}{r} 51 \\ 33 \end{array} \quad \begin{array}{r} 50 \\ 28 \end{array} \quad \begin{array}{r} 81 \\ 24 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 6.0 \end{array} \quad \begin{array}{r} 6.5 \\ 15 \end{array} \quad \begin{array}{r} 8.8 \\ 23 \end{array} \quad \begin{array}{r} 2.9 \\ 30 \end{array} \quad \begin{array}{r} 2.9 \\ 33 \end{array}$$

$$\begin{array}{r} 66 \\ 33 \end{array} \quad \begin{array}{r} 64 \\ 27 \end{array} \quad \begin{array}{r} 90 \\ 22 \end{array} \quad \begin{array}{r} 7.5 \\ 15 \end{array} \quad \begin{array}{r} 7.0 \\ 7.1 \end{array} \quad \begin{array}{r} 7.5 \\ 14 \end{array} \quad \begin{array}{r} 9.5 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 27 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array}$$

$$\begin{array}{r} 76 \\ 33 \end{array} \quad \begin{array}{r} 74 \\ 25 \end{array} \quad \begin{array}{r} 95 \\ 22 \end{array} \quad \begin{array}{r} 7.6 \\ 15 \end{array} \quad \begin{array}{r} 7.3 \\ 7.5 \end{array} \quad \begin{array}{r} 7.8 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 23 \end{array} \quad \begin{array}{r} 6.7 \\ 27 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array}$$

$$\begin{array}{r} 96 \\ 33 \end{array} \quad \begin{array}{r} 98 \\ 25 \end{array} \quad \begin{array}{r} 106 \\ 23 \end{array} \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 7.7 \\ 7.8 \end{array} \quad \begin{array}{r} 8.3 \\ 15 \end{array} \quad \begin{array}{r} 10.6 \\ 23 \end{array} \quad \begin{array}{r} 10.0 \\ 25 \end{array} \quad \begin{array}{r} 9.7 \\ 33 \end{array}$$

$$\int \begin{array}{r} 44 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 21 \end{array} \quad \begin{array}{r} 1.7 \\ 15 \end{array} \quad \begin{array}{r} 0.8 \\ 1.1 \end{array} \quad \begin{array}{r} 1.4 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 24 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 5.80 \\ 22 \end{array}$$

$$\begin{array}{r} 6.06 \\ 32 \end{array}$$

919.35 ✓

56		17.5
	+50	16.8
57		16.6
58		15.6
	+50	15.1
59		14.5
	+50	14.1
60		13.1
	+50	12.3
61		11.7
	+50	11.0
62		10.3

9-27-28

$\frac{58}{33}$	$\frac{5.8}{19}$	$\frac{2.4}{15}$	$\frac{1.4}{1.9}$	$\frac{2.4}{15}$	$\frac{4.7}{23}$	$\frac{4.7}{25}$	$\frac{5.8}{26}$	$\frac{5.3}{33}$
-----------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{29}{33}$	$\frac{30}{23}$	$\frac{4.2}{22}$	$\frac{2.8}{15}$	$\frac{2.2}{26}$	$\frac{2.7}{15}$	$\frac{4.5}{22}$	$\frac{4.5}{25}$	$\frac{2.7}{27}$	$\frac{2.7}{33}$
-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.1}{33}$	$\frac{4.2}{24}$	$\frac{5.2}{23}$	$\frac{3.4}{15}$	$\frac{2.6}{28}$	$\frac{3.2}{15}$	$\frac{4.7}{23}$	$\frac{4.8}{27}$	$\frac{3.2}{28}$	$\frac{3.2}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.7}{33}$	$\frac{4.9}{24}$	$\frac{6.0}{23}$	$\frac{4.2}{15}$	$\frac{2.7}{3.8}$	$\frac{4.1}{15}$	$\frac{5.7}{21}$	$\frac{5.9}{25}$	$\frac{5.0}{27}$	$\frac{4.9}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.4}{33}$	$\frac{5.3}{24}$	$\frac{6.3}{22}$	$\frac{4.9}{15}$	$\frac{4.0}{4.3}$	$\frac{4.6}{15}$	$\frac{6.5}{25}$	$\frac{5.9}{27}$	$\frac{5.8}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{5.0}{33}$	$\frac{5.7}{24}$	$\frac{6.5}{22}$	$\frac{5.2}{15}$	$\frac{4.6}{4.9}$	$\frac{5.4}{15}$	$\frac{6.8}{24}$	$\frac{5.1}{27}$	$\frac{5.0}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{4.8}{33}$	$\frac{4.8}{26}$	$\frac{7.3}{23}$	$\frac{5.8}{15}$	$\frac{4.2}{5.3}$	$\frac{5.6}{16}$	$\frac{6.9}{23}$	$\frac{3.9}{27}$	$\frac{3.9}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{4.8}{33}$	$\frac{4.8}{27}$	$\frac{7.9}{23}$	$\frac{6.5}{15}$	$\frac{5.4}{6.3}$	$\frac{6.5}{16}$	$\frac{7.6}{23}$	$\frac{5.0}{28}$	$\frac{4.9}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{3.6}{33}$	$\frac{3.7}{28}$	$\frac{8.9}{22}$	$\frac{7.3}{16}$	$\frac{6.7}{7.1}$	$\frac{7.2}{16}$	$\frac{8.6}{23}$	$\frac{4.1}{29}$	$\frac{4.1}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{5.8}{33}$	$\frac{5.6}{29}$	$\frac{9.4}{23}$	$\frac{8.1}{15}$	$\frac{7.6}{7.7}$	$\frac{7.5}{15}$	$\frac{9.3}{23}$	$\frac{4.0}{30}$	$\frac{4.0}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{10.1}{33}$	$\frac{9.6}{25}$	$\frac{11.7}{23}$	$\frac{9.1}{15}$	$\frac{4.3}{8.4}$	$\frac{8.7}{15}$	$\frac{9.8}{23}$	$\frac{7.2}{26}$	$\frac{6.8}{33}$
-------------------	------------------	-------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{12.6}{33}$	$\frac{12.1}{22}$	$\frac{9.9}{15}$	$\frac{9.2}{7.1}$	$\frac{9.2}{9.4}$	$\frac{10.6}{15}$	$\frac{10.8}{22}$	$\frac{10.8}{33}$
-------------------	-------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------

919.35 ✓

63

08.9 ✓

3.79

912.99

10.65

908.70

+50

09.2

64

07.8

+50

07.3

65

07.6

+50

07.5

66

+50

67

+50

68

+50

6.08

914.17 ✓

4.38

909.71 ✓

9-27-28

$\frac{18.3}{33}$	$\frac{13.5}{23}$	$\frac{11.1}{15}$	(104)	$\frac{10.9}{15}$	$\frac{14.3}{23}$	$\frac{14.5}{33}$
-------------------	-------------------	-------------------	-------	-------------------	-------------------	-------------------

$\frac{8.3}{33}$	$\frac{8.3}{25}$	$\frac{4.6}{15}$	(40)	$\frac{4.7}{15}$	$\frac{9.0}{25}$	$\frac{8.7}{33}$
------------------	------------------	------------------	------	------------------	------------------	------------------

$\frac{7.7}{33}$	$\frac{7.7}{26}$	$\frac{8.2}{25}$	$\frac{5.1}{15}$	(44)	$\frac{5.0}{15}$	$\frac{7.0}{22}$	$\frac{7.1}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------

$\frac{3.4}{33}$	$\frac{3.6}{31}$	$\frac{7.9}{25}$	$\frac{5.7}{15}$	(47)	$\frac{4.8}{15}$	$\frac{6.1}{24}$	$\frac{3.4}{27}$	$\frac{3.4}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------

$\frac{2.5}{33}$	$\frac{2.5}{30}$	$\frac{7.5}{24}$	$\frac{5.6}{15}$	(49)	$\frac{4.9}{15}$	$\frac{6.2}{20}$	$\frac{3.8}{27}$	$\frac{3.8}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------

$\frac{1.6}{35}$	$\frac{1.9}{33}$	$\frac{7.3}{27}$	$\frac{6.2}{18}$	(50)	$\frac{4.9}{15}$	$\frac{6.6}{23}$	$\frac{5.0}{25}$	$\frac{5.1}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------

$\frac{1.4}{38}$	$\frac{1.4}{36}$	$\frac{7.1}{29}$	$\frac{6.5}{19}$	(50)	$\frac{4.8}{15}$	$\frac{6.9}{22}$	$\frac{5.3}{25}$	$\frac{5.3}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------

$\frac{2.0}{37}$	$\frac{2.0}{35}$	$\frac{7.4}{30}$	$\frac{6.6}{19}$	(49)	$\frac{4.5}{15}$	$\frac{7.2}{23}$	$\frac{2.1}{28}$	$\frac{7.1}{39}$	$\frac{6.8}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{4.1}{36}$	$\frac{4.4}{33}$	$\frac{7.8}{28}$	$\frac{6.7}{20}$	(49)	$\frac{4.8}{15}$	$\frac{9.6}{29}$	$\frac{9.8}{34}$	$\frac{10.5}{36}$	$\frac{10.6}{40}$	$\frac{10.3}{41}$	$\frac{10.3}{42}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{4.6}{35}$	$\frac{5.0}{32}$	$\frac{7.6}{29}$	$\frac{6.8}{19}$	(48)	$\frac{5.0}{15}$	$\frac{7.4}{24}$	$\frac{9.5}{31}$	$\frac{9.6}{32}$	$\frac{10.6}{34}$	$\frac{11.7}{43}$	$\frac{10.8}{44}$	$\frac{11.1}{46}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{5.5}{33}$	$\frac{5.6}{31}$	$\frac{7.7}{29}$	$\frac{7.0}{19}$	(48)	$\frac{5.0}{15}$	$\frac{9.3}{27}$	$\frac{9.8}{32}$	$\frac{10.4}{34}$	$\frac{11.2}{41}$	$\frac{10.3}{42}$	$\frac{10.5}{45}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------

$\frac{4.4}{33}$	$\frac{4.4}{32}$	$\frac{7.6}{29}$	$\frac{6.7}{19}$	(47)	$\frac{4.7}{15}$	$\frac{7.3}{29}$	$\frac{7.7}{27}$	$\frac{8.6}{30}$	$\frac{8.9}{35}$	$\frac{8.4}{36}$	$\frac{8.6}{38}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

914.19 ✓

69

+50

70

+50

71

+50

72

73

+50

4.10

910.91 ✓

7.58 ✓

916.61 ✓

74

B.M.

5.65

910.72 ✓

5.65 ✓

905.06 ✓

905.07 ✓

+50

75

9-27-28

$$\begin{array}{r} \times \\ \begin{array}{r} 1.6 \\ 40 \end{array} \begin{array}{r} 1.6 \\ 89 \end{array} \begin{array}{r} 9.4 \\ 28 \end{array} \begin{array}{r} 8.0 \\ 16 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.4} \\ 6.8 \end{array} \begin{array}{r} 6.3 \\ 15 \end{array} \begin{array}{r} 9.4 \\ 22 \end{array} \begin{array}{r} 9.6 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 0.5 \\ 41 \end{array} \begin{array}{r} 0.5 \\ 40 \end{array} \begin{array}{r} 9.6 \\ 31 \end{array} \begin{array}{r} 8.0 \\ 19 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.4} \\ 6.4 \end{array} \begin{array}{r} 6.0 \\ 15 \end{array} \begin{array}{r} 7.6 \\ 21 \end{array} \begin{array}{r} 8.2 \\ 25 \end{array} \begin{array}{r} 8.5 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 2.0 \\ 40 \end{array} \begin{array}{r} 1.9 \\ 38 \end{array} \begin{array}{r} 9.1 \\ 30 \end{array} \begin{array}{r} 8.1 \\ 19 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.4} \\ 6.3 \end{array} \begin{array}{r} 5.9 \\ 15 \end{array} \begin{array}{r} 7.2 \\ 21 \end{array} \begin{array}{r} 4.9 \\ 25 \end{array} \begin{array}{r} 6.1 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 6.0 \\ 33 \end{array} \begin{array}{r} 5.7 \\ 30 \end{array} \begin{array}{r} 9.5 \\ 26 \end{array} \begin{array}{r} 8.2 \\ 18 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.5} \\ 6.4 \end{array} \begin{array}{r} 6.2 \\ 15 \end{array} \begin{array}{r} 7.5 \\ 23 \end{array} \begin{array}{r} 4.7 \\ 27 \end{array} \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 2.1 \\ 33 \end{array} \begin{array}{r} 8.8 \\ 24 \end{array} \begin{array}{r} 9.8 \\ 22 \end{array} \begin{array}{r} 8.1 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.6} \\ 7.1 \end{array} \begin{array}{r} 6.4 \\ 15 \end{array} \begin{array}{r} 8.1 \\ 23 \end{array} \begin{array}{r} 7.2 \\ 25 \end{array} \begin{array}{r} 6.9 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 11.4 \\ 33 \end{array} \begin{array}{r} 11.1 \\ 27 \end{array} \begin{array}{r} 7.5 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.7} \\ 6.9 \end{array} \begin{array}{r} 7.0 \\ 15 \end{array} \begin{array}{r} 8.8 \\ 23 \end{array} \begin{array}{r} 8.1 \\ 24 \end{array} \begin{array}{r} 7.7 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 9.6 \\ 33 \end{array} \begin{array}{r} 9.4 \\ 23 \end{array} \begin{array}{r} 7.3 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{6.8} \\ 7.0 \end{array} \begin{array}{r} 7.2 \\ 15 \end{array} \begin{array}{r} 8.7 \\ 20 \end{array} \begin{array}{r} 7.2 \\ 26 \end{array} \begin{array}{r} 6.9 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 10.1 \\ 33 \end{array} \begin{array}{r} 9.5 \\ 21 \end{array} \begin{array}{r} 7.2 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{7.2} \\ 7.0 \end{array} \begin{array}{r} 7.2 \\ 15 \end{array} \begin{array}{r} 9.0 \\ 23 \end{array} \begin{array}{r} 7.0 \\ 26 \end{array} \begin{array}{r} 6.6 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 8.8 \\ 33 \end{array} \begin{array}{r} 8.5 \\ 25 \end{array} \begin{array}{r} 9.4 \\ 23 \end{array} \begin{array}{r} 7.8 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{7.4} \\ 6.9 \end{array} \begin{array}{r} 6.9 \\ 15 \end{array} \begin{array}{r} 9.0 \\ 22 \end{array} \begin{array}{r} 5.8 \\ 27 \end{array} \begin{array}{r} 5.9 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 6.0 \\ 33 \end{array} \begin{array}{r} 5.1 \\ 24 \end{array} \begin{array}{r} 5.8 \\ 22 \end{array} \begin{array}{r} 5.8 \\ 20 \end{array} \begin{array}{r} 4.2 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{4.1} \\ 3.6 \end{array} \begin{array}{r} 3.9 \\ 15 \end{array} \begin{array}{r} 5.4 \\ 23 \end{array} \begin{array}{r} 1.3 \\ 31 \end{array} \begin{array}{r} 1.5 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 5.5 \\ 33 \end{array} \begin{array}{r} 4.9 \\ 26 \end{array} \begin{array}{r} 6.1 \\ 23 \end{array} \begin{array}{r} 4.1 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{4.3} \\ 3.7 \end{array} \begin{array}{r} 4.3 \\ 16 \end{array} \begin{array}{r} 5.6 \\ 23 \end{array} \begin{array}{r} 1.2 \\ 30 \end{array} \begin{array}{r} 1.0 \\ 33 \end{array}$$

$$\begin{array}{r} \times \\ \begin{array}{r} 4.6 \\ 33 \end{array} \begin{array}{r} 3.9 \\ 26 \end{array} \begin{array}{r} 6.7 \\ 22 \end{array} \begin{array}{r} 4.8 \\ 15 \end{array} \end{array} \quad \begin{array}{c} \textcircled{4.4} \\ 4.2 \end{array} \begin{array}{r} 4.5 \\ 16 \end{array} \begin{array}{r} 5.9 \\ 24 \end{array} \begin{array}{r} 0.6 \\ 32 \end{array} \begin{array}{r} 0.6 \\ 33 \end{array}$$

710.72 ✓

+50

76

+50

77

77

CROSS DRAIN 36" X 48" N<sup>3</sup>

+50

78

+50

79

+50

3.61

912.00 ✓

2.33

908.39 ✓

80

+50

9-27-28

5.6	5.0	6.4	4.9	4.5	4.8	6.3	2.3	2.1
33	26	23	15	4.6	15	23	29	33

8.3	7.3	4.7	4.6	4.8	6.6	3.8	3.3
33	23	15	4.7	15	23	27	33

8.8	8.8	8.4	4.8	4.6	5.0	6.7	7.1	5.7	5.4
33	28	23	15	4.8	15	20	25	27	33

9.2	8.4	4.7	4.6	4.7	8.3	8.3	7.0	6.7
33	25	15	4.7	14	24	27	28	33

9.35  
35

8.80  
23

9.2	8.8	4.5	4.5	5.2	7.7	7.8	7.1	6.9
33	25	15	4.5	15	20	26	27	33

7.3	6.8	4.0	4.4	5.5	6.8	7.1	6.0	5.8
33	22	15	4.5	15	22	26	27	33

5.4	5.2	6.5	5.8	3.6	4.3	5.3	6.9	7.1	4.4	4.6	4.6
36	34	31	23	15	4.1	19	26	29	32	33	40

4.7	4.6	6.4	5.9	3.3	4.1	5.6	7.2	7.2	4.5	4.6
35	33	30	27	15	3.7	19	26	29	34	40

3.1	2.9	5.2	5.1	2.9	3.9	5.2	6.5	6.6	3.6	3.8
35	33	28	26	15	3.5	18	25	29	33	40

5.6	5.8	6.6	6.5	4.2	5.0	6.1	7.4	7.5	6.1	6.1
40	33	31	26	15	4.8	18	25	28	30	40

6.9	7.4	4.2	4.4	6.3	7.4	7.6	6.8	6.7
33	22	15	5.0	17	23	26	28	35

912.00 ✓

81

+50

82

+44<sup>5</sup>

83

+50

84

+50

2.87 909.39 ✓ 5.48 906.52 ✓

85

+50

86

+40

$\frac{60}{53}$	$\frac{67}{27}$	$\frac{70}{22}$	$\frac{37}{15}$	$\frac{46}{50}$	$\frac{64}{18}$	$\frac{70}{23}$	$\frac{74}{25}$	$\frac{68}{29}$	$\frac{68}{40}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{67}{53}$	$\frac{62}{27}$	$\frac{39}{20}$	$\frac{37}{15}$	$\frac{44}{48}$	$\frac{61}{21}$	$\frac{68}{24}$	$\frac{70}{28}$	$\frac{69}{29}$	$\frac{67}{34}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{52}{33}$	$\frac{45}{28}$	$\frac{54}{23}$	$\frac{60}{20}$	$\frac{41}{15}$	$\frac{43}{45}$	$\frac{57}{21}$	$\frac{69}{25}$	$\frac{71}{28}$	$\frac{57}{30}$	$\frac{52}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{32}{33}$	$\frac{37}{24}$	$\frac{58}{21}$	$\frac{58}{19}$	$\frac{47}{15}$	$\frac{45}{48}$	$\frac{61}{18}$	$\frac{71}{23}$	$\frac{72}{24}$	$\frac{65}{26}$	$\frac{63}{40}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{14}{33}$	$\frac{14}{30}$	$\frac{64}{19}$	$\frac{64}{18}$	$\frac{50}{15}$	$\frac{44}{49}$	$\frac{54}{15}$	$\frac{67}{20}$	$\frac{47}{23}$	$\frac{50}{26}$	$\frac{52}{38}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{11}{33}$	$\frac{10}{31}$	$\frac{64}{23}$	$\frac{62}{20}$	$\frac{49}{15}$	$\frac{45}{50}$	$\frac{51}{15}$	$\frac{63}{22}$	$\frac{32}{28}$	$\frac{34}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{17}{33}$	$\frac{17}{30}$	$\frac{68}{23}$	$\frac{68}{19}$	$\frac{50}{15}$	$\frac{48}{52}$	$\frac{53}{15}$	$\frac{67}{24}$	$\frac{30}{28}$	$\frac{28}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{35}{33}$	$\frac{35}{30}$	$\frac{73}{23}$	$\frac{46}{15}$	$\frac{50}{52}$	$\frac{57}{16}$	$\frac{70}{21}$	$\frac{70}{24}$	$\frac{44}{27}$	$\frac{44}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{32}{33}$	$\frac{28}{26}$	$\frac{50}{22}$	$\frac{50}{20}$	$\frac{34}{15}$	$\frac{28}{34}$	$\frac{32}{15}$	$\frac{48}{19}$	$\frac{50}{24}$	$\frac{31}{26}$	$\frac{34}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{46}{33}$	$\frac{44}{24}$	$\frac{57}{21}$	$\frac{57}{20}$	$\frac{45}{15}$	$\frac{33}{38}$	$\frac{37}{15}$	$\frac{47}{19}$	$\frac{47}{28}$	$\frac{43}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{53}{33}$	$\frac{56}{24}$	$\frac{63}{22}$	$\frac{62}{19}$	$\frac{48}{15}$	$\frac{37}{42}$	$\frac{43}{15}$	$\frac{56}{19}$	$\frac{59}{23}$	$\frac{51}{29}$	$\frac{47}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{54}{33}$	$\frac{49}{25}$	$\frac{64}{22}$	$\frac{64}{19}$	$\frac{50}{15}$	$\frac{41}{44}$	$\frac{48}{15}$	$\frac{55}{17}$	$\frac{53}{26}$	$\frac{49}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

909.37 ✓

+50

87

+25

+50

88

+50

89

B.M.

1.72

90600 ✓

5.26

904.13 ✓

904.08

+50

90

+50

994 CROSS BATHIN 36" X 52" ✓

+75

9-27-28

$$\begin{array}{r} 5.0 \\ 33 \end{array} \quad \begin{array}{r} 4.8 \\ 27 \end{array} \quad \begin{array}{r} 6.4 \\ 22 \end{array} \quad \begin{array}{r} 6.4 \\ 19 \end{array} \quad \begin{array}{r} 4.9 \\ 15 \end{array} \quad \begin{array}{r} 4.3 \\ 4.4 \end{array} \quad \begin{array}{r} 5.0 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 20 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 4.1 \\ 33 \end{array} \quad \begin{array}{r} 3.8 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 22 \end{array} \quad \begin{array}{r} 6.8 \\ 19 \end{array} \quad \begin{array}{r} 5.3 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 4.9 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 18 \end{array} \quad \begin{array}{r} 3.2 \\ 20 \end{array} \quad \begin{array}{r} 2.9 \\ 30 \end{array} \quad \begin{array}{r} 3.3 \\ 33 \end{array}$$

$$\begin{array}{r} 4.3 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 30 \end{array} \quad \begin{array}{r} 7.3 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 20 \end{array} \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 5.3 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 6.4 \\ 18 \end{array} \quad \begin{array}{r} 2.6 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 28 \end{array} \quad \begin{array}{r} 7.6 \\ 23 \end{array} \quad \begin{array}{r} 7.6 \\ 20 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 5.4 \\ 5.7 \end{array} \quad \begin{array}{r} 5.9 \\ 15 \end{array} \quad \begin{array}{r} 6.7 \\ 18 \end{array} \quad \begin{array}{r} 3.1 \\ 20 \end{array} \quad \begin{array}{r} 3.1 \\ 30 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 27 \end{array} \quad \begin{array}{r} 8.2 \\ 22 \end{array} \quad \begin{array}{r} 8.2 \\ 18 \end{array} \quad \begin{array}{r} 6.8 \\ 15 \end{array} \quad \begin{array}{r} 6.0 \\ 6.6 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 7.6 \\ 18 \end{array} \quad \begin{array}{r} 4.4 \\ 22 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.4 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 24 \end{array} \quad \begin{array}{r} 8.8 \\ 22 \end{array} \quad \begin{array}{r} 8.8 \\ 19 \end{array} \quad \begin{array}{r} 7.3 \\ 16 \end{array} \quad \begin{array}{r} 6.5 \\ 7.2 \end{array} \quad \begin{array}{r} 7.7 \\ 15 \end{array} \quad \begin{array}{r} 8.8 \\ 17 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 9.3 \\ 33 \end{array} \quad \begin{array}{r} 8.8 \\ 28 \end{array} \quad \begin{array}{r} 9.2 \\ 22 \end{array} \quad \begin{array}{r} 7.5 \\ 15 \end{array} \quad \begin{array}{r} 7.1 \\ 7.7 \end{array} \quad \begin{array}{r} 8.1 \\ 15 \end{array} \quad \begin{array}{r} 9.1 \\ 18 \end{array} \quad \begin{array}{r} 7.2 \\ 20 \end{array} \quad \begin{array}{r} 7.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.5 \\ 33 \end{array} \quad \begin{array}{r} 6.2 \\ 24 \end{array} \quad \begin{array}{r} 6.4 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 16 \end{array} \quad \begin{array}{r} 4.3 \\ 5.1 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 26 \end{array} \quad \begin{array}{r} 6.1 \\ 32 \end{array}$$

$$\begin{array}{r} 7.4 \\ 33 \end{array} \quad \begin{array}{r} 7.4 \\ 23 \end{array} \quad \begin{array}{r} 7.1 \\ 19 \end{array} \quad \begin{array}{r} 5.3 \\ 15 \end{array} \quad \begin{array}{r} 4.7 \\ 5.4 \end{array} \quad \begin{array}{r} 5.2 \\ 15 \end{array} \quad \begin{array}{r} 6.3 \\ 25 \end{array} \quad \begin{array}{r} 6.5 \\ 28 \end{array} \quad \begin{array}{r} 6.8 \\ 33 \end{array}$$

$$\begin{array}{r} 9.9 \\ 33 \end{array} \quad \begin{array}{r} 9.3 \\ 24 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 4.9 \\ 5.5 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 8.4 \\ 22 \end{array} \quad \begin{array}{r} 8.9 \\ 25 \end{array} \quad \begin{array}{r} 8.6 \\ 33 \end{array}$$

$$\frac{11.35}{26}$$

$$\frac{11.5}{26}$$

$$\begin{array}{r} 11.4 \\ 33 \end{array} \quad \begin{array}{r} 11.4 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 16 \end{array} \quad \begin{array}{r} 5.0 \\ 5.4 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 11.3 \\ 26 \end{array} \quad \begin{array}{r} 11.4 \\ 33 \end{array}$$

906.00 ✓

91

+50

92

+50

+75

93

+50

94

+50

95

+50

96

13.50

716.37 ✓

9.13

02.87

7-27-25

$\frac{10.4}{33}$	$\frac{10.3}{27}$	$\frac{9.9}{24}$	$\frac{5.6}{15}$	$\frac{5.0}{5.4}$	$\frac{5.3}{15}$	$\frac{8.3}{23}$	$\frac{9.0}{25}$	$\frac{9.1}{27}$	$\frac{8.6}{28}$	$\frac{8.8}{33}$
-------------------	-------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.1}{33}$	$\frac{8.1}{23}$	$\frac{5.1}{16}$	$\frac{4.9}{4.8}$	$\frac{5.1}{15}$	$\frac{7.9}{23}$	$\frac{8.7}{25}$	$\frac{8.1}{27}$	$\frac{8.0}{28}$	$\frac{8.5}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{5.1}{33}$	$\frac{5.3}{24}$	$\frac{6.9}{23}$	$\frac{5.2}{15}$	$\frac{4.7}{4.6}$	$\frac{4.6}{15}$	$\frac{9.0}{26}$	$\frac{7.8}{28}$	$\frac{7.4}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------

$\frac{1.9}{33}$	$\frac{2.3}{30}$	$\frac{6.5}{24}$	$\frac{6.5}{20}$	$\frac{4.7}{16}$	$\frac{4.5}{4.4}$	$\frac{5.0}{15}$	$\frac{8.4}{24}$	$\frac{9.1}{26}$	$\frac{9.1}{28}$	$\frac{7.9}{29}$	$\frac{6.9}{33}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{1.2}{33}$	$\frac{1.4}{30}$	$\frac{6.6}{23}$	$\frac{6.4}{21}$	$\frac{4.2}{16}$	$\frac{4.4}{4.3}$	$\frac{4.6}{15}$	$\frac{8.6}{25}$	$\frac{8.6}{27}$	$\frac{6.5}{30}$	$\frac{6.0}{33}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{1.8}{33}$	$\frac{2.0}{28}$	$\frac{5.8}{23}$	$\frac{5.8}{19}$	$\frac{4.4}{15}$	$\frac{4.3}{4.1}$	$\frac{4.1}{15}$	$\frac{8.5}{26}$	$\frac{8.5}{28}$	$\frac{6.1}{30}$	$\frac{5.6}{33}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.7}{33}$	$\frac{4.8}{25}$	$\frac{5.6}{24}$	$\frac{4.2}{15}$	$\frac{4.1}{4.0}$	$\frac{4.2}{16}$	$\frac{6.1}{28}$	$\frac{8.1}{26}$	$\frac{5.4}{31}$	$\frac{5.4}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.6}{33}$	$\frac{8.2}{25}$	$\frac{4.2}{15}$	$\frac{4.2}{4.2}$	$\frac{4.2}{15}$	$\frac{6.5}{22}$	$\frac{8.3}{27}$	$\frac{6.3}{31}$	$\frac{6.3}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{8.7}{33}$	$\frac{7.0}{25}$	$\frac{4.2}{15}$	$\frac{3.7}{3.9}$	$\frac{4.2}{16}$	$\frac{7.6}{24}$	$\frac{8.8}{27}$	$\frac{8.8}{29}$	$\frac{8.1}{30}$	$\frac{8.1}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.3}{33}$	$\frac{6.4}{22}$	$\frac{3.8}{15}$	$\frac{3.6}{3.6}$	$\frac{3.8}{15}$	$\frac{7.4}{23}$	$\frac{8.0}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{4.9}{33}$	$\frac{4.7}{26}$	$\frac{5.1}{21}$	$\frac{3.6}{15}$	$\frac{3.3}{3.2}$	$\frac{3.8}{15}$	$\frac{5.1}{20}$	$\frac{6.1}{33}$
------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{2.1}{33}$	$\frac{2.1}{30}$	$\frac{3.5}{26}$	$\frac{4.9}{24}$	$\frac{3.3}{15}$	$\frac{3.1}{3.1}$	$\frac{3.1}{15}$	$\frac{4.1}{18}$	$\frac{4.7}{21}$	$\frac{4.5}{25}$	$\frac{5.2}{33}$
------------------	------------------	------------------	------------------	------------------	-------------------	------------------	------------------	------------------	------------------	------------------

916.37 ✓

+50

97

+30

+50

98

+50

7.00

913.11 ✓

12.26

904.11 ✓

99

+25

+50

100

+50

101

9-27-28

$\frac{77}{34}$	$\frac{96}{32}$	$\frac{158}{23}$	$\frac{134}{15}$	<b>(133)</b>	$\frac{137}{15}$	$\frac{150}{17}$	$\frac{150}{21}$	$\frac{129}{24}$	$\frac{135}{33}$
-----------------	-----------------	------------------	------------------	--------------	------------------	------------------	------------------	------------------	------------------

$\frac{51}{40}$	$\frac{50}{36}$	$\frac{146}{24}$	$\frac{135}{15}$	<b>(131)</b>	$\frac{134}{15}$	$\frac{147}{22}$	$\frac{103}{31}$	$\frac{105}{33}$
-----------------	-----------------	------------------	------------------	--------------	------------------	------------------	------------------	------------------

$\frac{17}{40}$	$\frac{19}{39}$	$\frac{147}{22}$	$\frac{132}{15}$	<b>(130)</b>	$\frac{134}{15}$	$\frac{149}{22}$	$\frac{84}{32}$	$\frac{86}{34}$
-----------------	-----------------	------------------	------------------	--------------	------------------	------------------	-----------------	-----------------

$\frac{10}{42}$	$\frac{0.9}{41}$	$\frac{145}{23}$	$\frac{131}{15}$	<b>(129)</b>	$\frac{133}{15}$	$\frac{147}{22}$	$\frac{75}{32}$	$\frac{79}{33}$
-----------------	------------------	------------------	------------------	--------------	------------------	------------------	-----------------	-----------------

$\frac{57}{38}$	$\frac{56}{37}$	$\frac{145}{24}$	<b>(145)</b>	$\frac{130}{15}$	<b>(124)</b>	$\frac{129}{15}$	$\frac{147}{23}$	$\frac{93}{31}$	$\frac{94}{33}$
-----------------	-----------------	------------------	--------------	------------------	--------------	------------------	------------------	-----------------	-----------------

$\frac{107}{36}$	$\frac{110}{33}$	$\frac{142}{25}$	$\frac{139}{19}$	$\frac{125}{19}$	<b>(125)</b>	$\frac{124}{15}$	$\frac{137}{22}$	$\frac{116}{27}$	$\frac{116}{33}$
------------------	------------------	------------------	------------------	------------------	--------------	------------------	------------------	------------------	------------------

$\frac{115}{33}$	$\frac{113}{26}$	$\frac{112}{22}$	$\frac{92}{15}$	<b>(90)</b>	$\frac{88}{16}$	$\frac{103}{23}$	$\frac{102}{33}$
------------------	------------------	------------------	-----------------	-------------	-----------------	------------------	------------------

$\frac{121}{33}$	$\frac{122}{27}$	$\frac{116}{22}$	$\frac{91}{15}$	<b>(87)</b>	$\frac{87}{15}$	$\frac{110}{23}$	$\frac{116}{33}$
------------------	------------------	------------------	-----------------	-------------	-----------------	------------------	------------------

$\frac{118}{33}$	$\frac{117}{21}$	$\frac{89}{15}$	<b>(87)</b>	$\frac{85}{16}$	$\frac{103}{23}$	$\frac{98}{25}$	$\frac{97}{33}$
------------------	------------------	-----------------	-------------	-----------------	------------------	-----------------	-----------------

$\frac{102}{33}$	$\frac{101}{24}$	$\frac{107}{22}$	$\frac{85}{15}$	<b>(84)</b>	$\frac{80}{15}$	$\frac{95}{23}$	$\frac{86}{25}$	$\frac{83}{33}$
------------------	------------------	------------------	-----------------	-------------	-----------------	-----------------	-----------------	-----------------

$\frac{100}{33}$	$\frac{101}{25}$	$\frac{109}{21}$	$\frac{80}{15}$	<b>(80)</b>	$\frac{79}{15}$	$\frac{96}{23}$	$\frac{88}{25}$	$\frac{88}{33}$
------------------	------------------	------------------	-----------------	-------------	-----------------	-----------------	-----------------	-----------------

$\frac{112}{33}$	$\frac{108}{21}$	$\frac{76}{15}$	<b>(85)</b>	$\frac{78}{15}$	$\frac{110}{23}$	$\frac{110}{26}$	$\frac{101}{28}$	$\frac{99}{33}$
------------------	------------------	-----------------	-------------	-----------------	------------------	------------------	------------------	-----------------

913.11 ✓

101

CROSS DRAIN

24" X 42' P<sup>3</sup>

+50

102

+50

103

+50

104

+50

105

9.55

922.32 ✓

0.34

912.77 ✓

+50

104

+50

9-27-29

$$\frac{11.07}{21}$$

$$\frac{12.27}{21}$$

$\frac{95}{33}$	$\frac{91}{26}$	$\frac{71}{15}$	(69)	$\frac{72}{15}$	$\frac{10.5}{23}$	$\frac{11.9}{33}$
-----------------	-----------------	-----------------	------	-----------------	-------------------	-------------------

$\frac{67}{33}$	$\frac{67}{32}$	$\frac{80}{27}$	$\frac{82}{23}$	$\frac{75}{17}$	$\frac{63}{15}$	(67)	$\frac{6.6}{15}$	$\frac{8.3}{21}$	$\frac{8.7}{24}$	$\frac{8.4}{25}$	$\frac{8.7}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{49}{33}$	$\frac{72}{27}$	$\frac{66}{24}$	$\frac{72}{22}$	$\frac{56}{15}$	(54)	$\frac{5.8}{15}$	$\frac{7.5}{24}$	$\frac{5.8}{27}$	$\frac{6.1}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	------	------------------	------------------	------------------	------------------

$\frac{49}{33}$	$\frac{49}{26}$	$\frac{65}{23}$	$\frac{44}{15}$	(45)	$\frac{4.5}{15}$	$\frac{6.0}{24}$	$\frac{3.8}{27}$	$\frac{3.9}{33}$
-----------------	-----------------	-----------------	-----------------	------	------------------	------------------	------------------	------------------

$\frac{3.7}{34}$	$\frac{4.4}{32}$	$\frac{3.6}{26}$	$\frac{5.3}{25}$	$\frac{3.6}{15}$	(35)	$\frac{3.2}{30}$	$\frac{4.5}{15}$	$\frac{4.4}{19}$	$\frac{2.1}{24}$	$\frac{2.1}{27}$
------------------	------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{3.8}{33}$	$\frac{3.4}{25}$	$\frac{4.3}{23}$	$\frac{4.2}{21}$	$\frac{2.6}{15}$	(25)	$\frac{2.6}{22}$	$\frac{4.4}{15}$	$\frac{4.4}{17}$	$\frac{1.5}{23}$	$\frac{1.4}{27}$	$\frac{1.4}{33}$
------------------	------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{3.5}{33}$	$\frac{3.3}{21}$	$\frac{1.8}{15}$	(14)	$\frac{1.9}{1.5}$	$\frac{3.4}{15}$	$\frac{3.4}{19}$	$\frac{1.6}{21}$	$\frac{1.3}{25}$	$\frac{1.3}{33}$
------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{1.8}{33}$	$\frac{2.1}{25}$	$\frac{2.8}{23}$	$\frac{0.7}{15}$	(07)	$\frac{0.9}{0.6}$	$\frac{2.6}{15}$	$\frac{2.6}{17}$	$\frac{0.5}{21}$	$\frac{0.3}{25}$	$\frac{0.3}{33}$
------------------	------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{9.2}{33}$	$\frac{9.4}{26}$	$\frac{10.6}{25}$	$\frac{9.1}{16}$	(48)	$\frac{9.0}{8.6}$	$\frac{10.7}{15}$	$\frac{11.0}{19}$	$\frac{9.7}{23}$	$\frac{9.5}{26}$	$\frac{9.5}{33}$
------------------	------------------	-------------------	------------------	------	-------------------	-------------------	-------------------	------------------	------------------	------------------

$\frac{7.7}{33}$	$\frac{7.5}{26}$	$\frac{9.0}{23}$	$\frac{7.7}{15}$	(73)	$\frac{7.8}{7.5}$	$\frac{9.4}{15}$	$\frac{7.5}{19}$	$\frac{7.7}{23}$	$\frac{7.7}{27}$	$\frac{7.8}{33}$
------------------	------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

$\frac{6.0}{33}$	$\frac{6.2}{27}$	$\frac{8.2}{24}$	$\frac{6.7}{15}$	(67)	$\frac{6.8}{6.5}$	$\frac{7.6}{15}$	$\frac{7.8}{19}$	$\frac{6.0}{28}$	$\frac{6.1}{28}$	$\frac{6.1}{33}$
------------------	------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

922.32 ✓

107

+50

108

+50

109

+50

110

110 + 11 CROSS DRAIN 24" R 40' P<sup>2</sup>

8.44 725.48 ✓ 5.28 917.04 ✓

+50

111

+50

112

9-27-28

$\frac{3.6}{33}$	$\frac{3.5}{29}$	$\frac{6.9}{24}$	$\frac{5.5}{15}$	(51)	$\frac{5.9}{15}$	$\frac{6.6}{18}$	$\frac{6.6}{23}$	$\frac{4.3}{28}$	$\frac{4.5}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{3.2}{33}$	$\frac{3.2}{27}$	$\frac{6.3}{23}$	$\frac{5.1}{15}$	(37)	$\frac{5.0}{15}$	$\frac{6.0}{20}$	$\frac{6.1}{28}$	$\frac{2.7}{29}$	$\frac{3.0}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{3.9}{33}$	$\frac{3.8}{26}$	$\frac{6.3}{22}$	$\frac{4.9}{15}$	(37)	$\frac{4.6}{15}$	$\frac{5.5}{21}$	$\frac{5.7}{25}$	$\frac{2.5}{30}$	$\frac{2.5}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{4.6}{33}$	$\frac{4.6}{24}$	$\frac{5.9}{22}$	$\frac{4.4}{15}$	(30)	$\frac{4.3}{15}$	$\frac{5.7}{21}$	$\frac{5.9}{28}$	$\frac{3.5}{29}$	$\frac{3.8}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{5.7}{33}$	$\frac{5.7}{24}$	$\frac{6.2}{22}$	$\frac{4.7}{15}$	(39)	$\frac{4.4}{15}$	$\frac{6.7}{21}$	$\frac{6.8}{28}$	$\frac{5.0}{27}$	$\frac{4.9}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{6.7}{33}$	$\frac{6.7}{23}$	$\frac{6.4}{21}$	$\frac{4.7}{15}$	(43)	$\frac{4.8}{15}$	$\frac{7.1}{22}$	$\frac{7.3}{25}$	$\frac{5.0}{28}$	$\frac{5.0}{33}$
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	------------------

$\frac{8.2}{33}$	$\frac{7.4}{25}$	$\frac{6.8}{21}$	$\frac{4.8}{15}$	(45)	$\frac{5.4}{17}$	$\frac{7.5}{23}$	$\frac{7.7}{27}$	$\frac{5.0}{29}$	
------------------	------------------	------------------	------------------	------	------------------	------------------	------------------	------------------	--

$$\frac{8.36}{20}$$

$$\frac{8.06}{20}$$

NAIP in P.C. LT. STA 110+40

$\frac{7.5}{33}$	$\frac{7.2}{17}$	$\frac{7.7}{12}$	(76)	$\frac{8.9}{8.0}$	$\frac{10.7}{19}$	$\frac{7.2}{30}$	$\frac{7.2}{33}$	$\frac{7.2}{36}$
------------------	------------------	------------------	------	-------------------	-------------------	------------------	------------------	------------------

$\frac{8.3}{33}$	$\frac{8.5}{28}$	$\frac{7.0}{20}$	(73)	$\frac{8.7}{7.7}$	$\frac{7.9}{19}$	$\frac{10.3}{24}$	$\frac{7.4}{31}$	$\frac{7.4}{33}$	$\frac{7.4}{36}$
------------------	------------------	------------------	------	-------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{6.9}{50}$	$\frac{6.3}{40}$	$\frac{6.2}{20}$	(68)	$\frac{8.3}{6.7}$	$\frac{7.2}{19}$	$\frac{7.6}{25}$	$\frac{8.5}{30}$	$\frac{8.5}{33}$	$\frac{8.5}{36}$
------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

↗ NAIP

$\frac{5.1}{48}$	$\frac{5.2}{36}$	$\frac{5.5}{26}$	$\frac{5.4}{19}$	(61)	$\frac{7.3}{5.8}$	$\frac{8.3}{19}$	$\frac{8.5}{24}$	$\frac{6.5}{29}$	$\frac{7.0}{34}$	$\frac{7.0}{35}$
------------------	------------------	------------------	------------------	------	-------------------	------------------	------------------	------------------	------------------	------------------

925.48 ✓

+20

+40

+50

113

+33

B.M.

4.64

920.84 ✓

920.84

9-28-25

725-46

$\frac{47}{33}$	$\frac{49}{22}$	$\frac{49}{12}$	(54)	$\frac{70}{20}$	$\frac{78}{24}$	$\frac{81}{28}$	$\frac{52}{34}$	$\frac{58}{36}$
-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------	-----------------

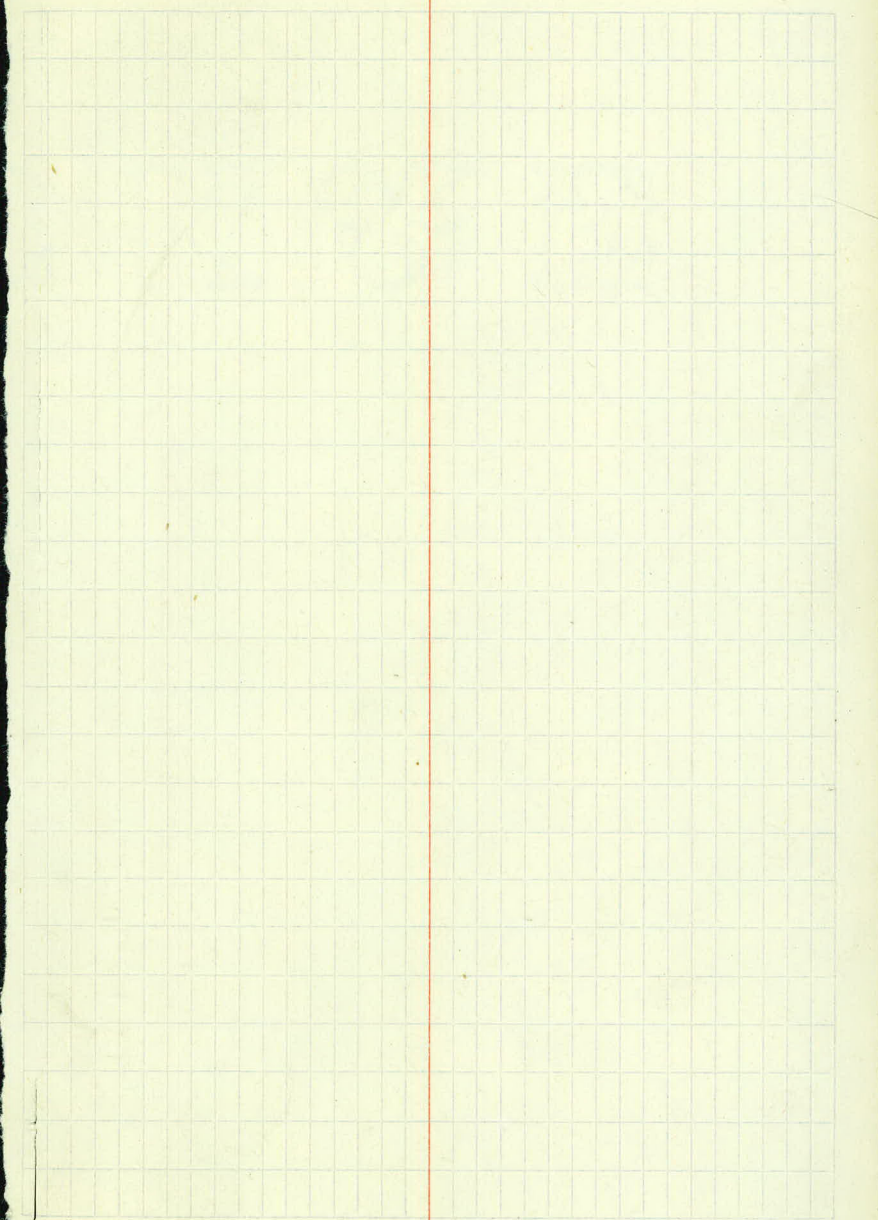
$\frac{44}{24}$	$\frac{46}{12}$	(54)	$\frac{62}{20}$	$\frac{74}{25}$	$\frac{76}{28}$	$\frac{42}{35}$	$\frac{43}{39}$
-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{44}{33}$	$\frac{42}{20}$	$\frac{43}{9}$	(52)	$\frac{60}{20}$	$\frac{72}{25}$	$\frac{74}{28}$	$\frac{39}{35}$	$\frac{41}{40}$
-----------------	-----------------	----------------	------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{56}{19}$	(41)	$\frac{44}{18}$	$\frac{61}{22}$	$\frac{63}{26}$	$\frac{37}{31}$	$\frac{39}{35}$
-----------------	------	-----------------	-----------------	-----------------	-----------------	-----------------

(27)	$\frac{27}{11}$	$\frac{27}{19}$	$\frac{51}{26}$	$\frac{22}{33}$	$\frac{21}{36}$
------	-----------------	-----------------	-----------------	-----------------	-----------------

		EMB	EXC.
108722	FIELD ENT. RT.	4	
103780	FIELD ENT. RT.	9	
103778	FARM ENT. LT.	6	
91799	FIELD ENT. RT.	7	
91794	FARM ENT. LT.	4	
71763	FIELD ENT. LT.	8	
89729	FARM ENT. RT.	9	
88781	FIELD ENT. LT.	9	
82792	FIELD ENT. RT.	2	
82713	FIELD ENT. LT.	3	
81750	APPROACH.	12	
74754	FARM ENT. LT.	3	
74754	FIELD ENT. RT.	4	4
44766	FARM ENT. LT.	4	
23799	P. LINE ROAD LT.	4	
23740	P. LINE ROAD RT.	5	
19709	FARM ENT. RT.	6	4



6 x

5 x

4 x

3 x

2 x

1 ✓

0 + 00

9-28-38

+98 T.P. 28

19 P.P. 28

+72 T.P. 28

12

11

10

9

8

7

6

9-28-28

+150 T.P. 28

+1 P.P. 28

+99 T.P. 28

+08 P.P. 28

+63 T.P. 28

+34 T.P. 28

+11 P.P. 28

18

17

16

15

14

13

12

9-28-28

+12 P.P. 28

+53 T.P. 28

+01 SIDE ROAD  
 +01 SIDE DRAIN 23  
 NEW 15" X 30' C.M.

+01 FARM INT.  
 +01 SIDE DRAIN 30  
 OLD 12" X 32' C.M.

+77 T.P. 28

+78 T.P. 28

+62 P.P. 28

+85 T.P. 28

+94 P.P. 27

+59 T.P. 28

24

23

22

21

20

19

18

9-28-28

+71 T.P. 28

+16 P.P. 28

+ 99 B.W.E.R. LINE ROAD.  
 + 99 SIDE DRAIN 22  
 NEW 15" X 24" C.M.

+ 40 P. LINE ROAD  
 + 40 SIDE DRAIN 22  
 NEW 15" X 24" C.M.  
 + 25 T.P. 28

+78 P.P. 28

+29 T.P. 28

+00 T.P. 28

+96 P.P. 28

+09 FARM ENT.  
 +09 SIDE DRAIN 22  
 NEW 15" X 24" C.M.

+76 T.P. 28

+55 P.P. 28

30

29

28

27

26

25

24

9-28-28

F. 31

+96 T.P. 28

+51 P.P. 28

+67 T.P. 28

+01 F. CA 30

+45 T.P. 28

+81 P.P. 28

+21 T.P. 28

+97 P.P. 28

+90 T.P. 28

36

35

34

33

32

31

30



42

41

40

39

38

37

36

9-28-28

F. 37

+2 P.P. 28

+15 T.P. 28

+44 P.P. 28

+88 T.P. 28

+15 X. F. 35

+71 T.P. 28

F. 35

+47 P.P. 28

+45 T.P. 28

+20 T.P. 28

48

47

46

45

44

43

42

9-28-28

F. 36

39 P.P. 28

+48 T.P. 28

43 P.P. 28

+24 T.P. 28

60 FARM ENT.  
66 SIDE DRAIN 22  
VIEW 15" X 24" C.M.

F. 36

+97 T.P. 28

45 P.P. 28

+68 T.P. 28

+43 T.P. 28

54

53

52

51

50

49

48

9-28-28

F. 33

+82 T.P. 28

+22 P.P. 28

+59 T.P. 28

+29 P.P. 28

+32 T.P. 28

+03 T.P. 28

F. 34

+37 P.P. 28

+76 T.P. 28

60

59

58

57

56

55

54



70

66

65

64

63

62

61

60

9-28-28

F. 29

X

X

X

+34 T.P. 24

X

+29 T.P. 24

X

X

X

X

X

F. 30

X

X

+83 T.P. 24

X

X

X

X

+58 T.P. 28

X

X

X

X

X

+35 T.P. 28

X

X

X

+16 T.P. 27

X

F. 31

+29 P.P. 34

+48 P.P. 28

+42 P.P. 28

72

71

70

69

68

67

66

9-28-28

+88 F. Cor 27.

+83 P.P. 27



+85 T.P. 26

+35 P.P. 31

+35 G. Pole 20

+17 P.P. 33

+84 G. Pole 23

+15 P.P. 33

+15 G. Pole 29

+45 F.S.C.

+45 T.P. 31



78

77

76

75

74

73

72

9-28-28

177 F. 26

159 P.P. 29

180 T.P. 28

159 T.P. 28

F. 26

160 P.P. 28

115 T.P. 28

154 FARM ENT.

154 FIELD ENT.  
154 SIDE DRAIN EE  
NEW 15" X 24" CUMI

184 P.P. 28

184 T.P. 27

F. 25

161 T.P. 27

84

83

82

81

80

79

78

9-28-28

+93 T.P. 28

+42 P.P. 25

+72 FIELD ENT

+64 T.P. 28

+13 FIELD ENT.

+86 P.P. 23

+91 P.P. 23

+96 P.P. 35

+20 F. CAR 49

90

89

88

87

86

85

84

9-28-28

F. 26

+91 F. COR. 28

+81 FIELD ENT.

+81 SIDE DRAIN 28

1.0 24" X 20 IRON PIPE

+64 P.P. 24

+78 P.P. 24

+73 P.P. 24

+29 FARM ENT.  
+29 SIDE DRAIN 20  
NEW 15" X 24 C.M.

+64 T.P. 28

+48 T.P. 28

+51 T.P. 29

+19 T.P. 28

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25

94

95

94

93

92

91

90

9-28-28

F. 31

F. 34

444 P.P. 21

F. 35

468 F. COR. 29

458 P.P. 12

413 P.P. 23

400 F. 30  
499 FIELD ENT.  
199 SIDE DRAIN #6  
NEW 15" X 24 CM

494 FARM ENT.  
494 SIDE DRAIN #3  
NEW 15" X 24 CM.  
487 F. COR. 28  
468 FIELD ENT.  
468 SIDE DRAIN #3  
NEW 15" X 24 CM.

482 X. F. 26

471 F. 32

465 F. 23

412 P.P. 25

F. 34

102

101

100

99

98

97

96

F. 35

F. 33

426 P.P. 26

F. 34

F. 33

428 T.P. 26

428 X. F. 33 B.

450 F. 35

450 F. 34

F. 38

F. 34

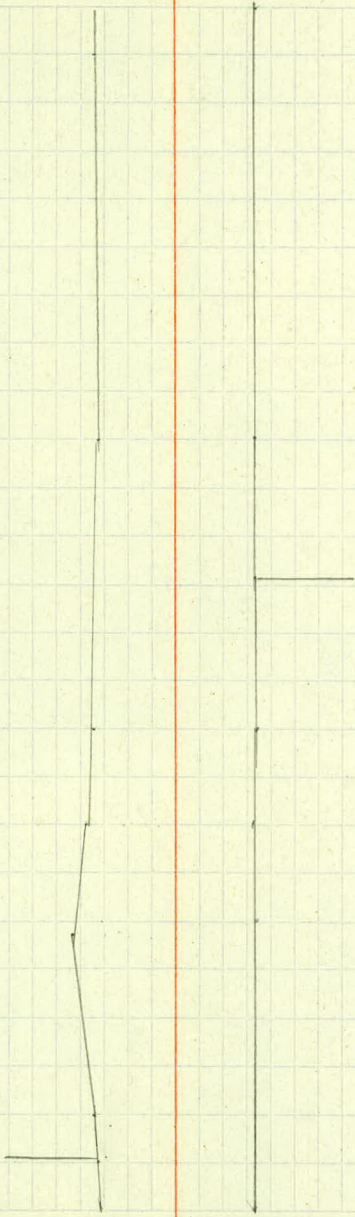
435 F. 43

435 P.P. 24

450 F. 35

440 F. 34

440 X. F.



108

107

106

105

104

103

102

9-28-28

+76 P.P. 30



+85 X.F. 28

+85 T.P. 29

+78 FARM ENT  
+78 SIDE DRAIN 23  
NEW 15' X 24' C.M.  
+21 F.COR 37  
+14 P.P. 28



+80 F.I.D. ENT.  
+80 SIDE DRAIN 22  
NEW 15' X 24' C.M.

+69 F.COR 33



114

113

112

111

110

109

108

68

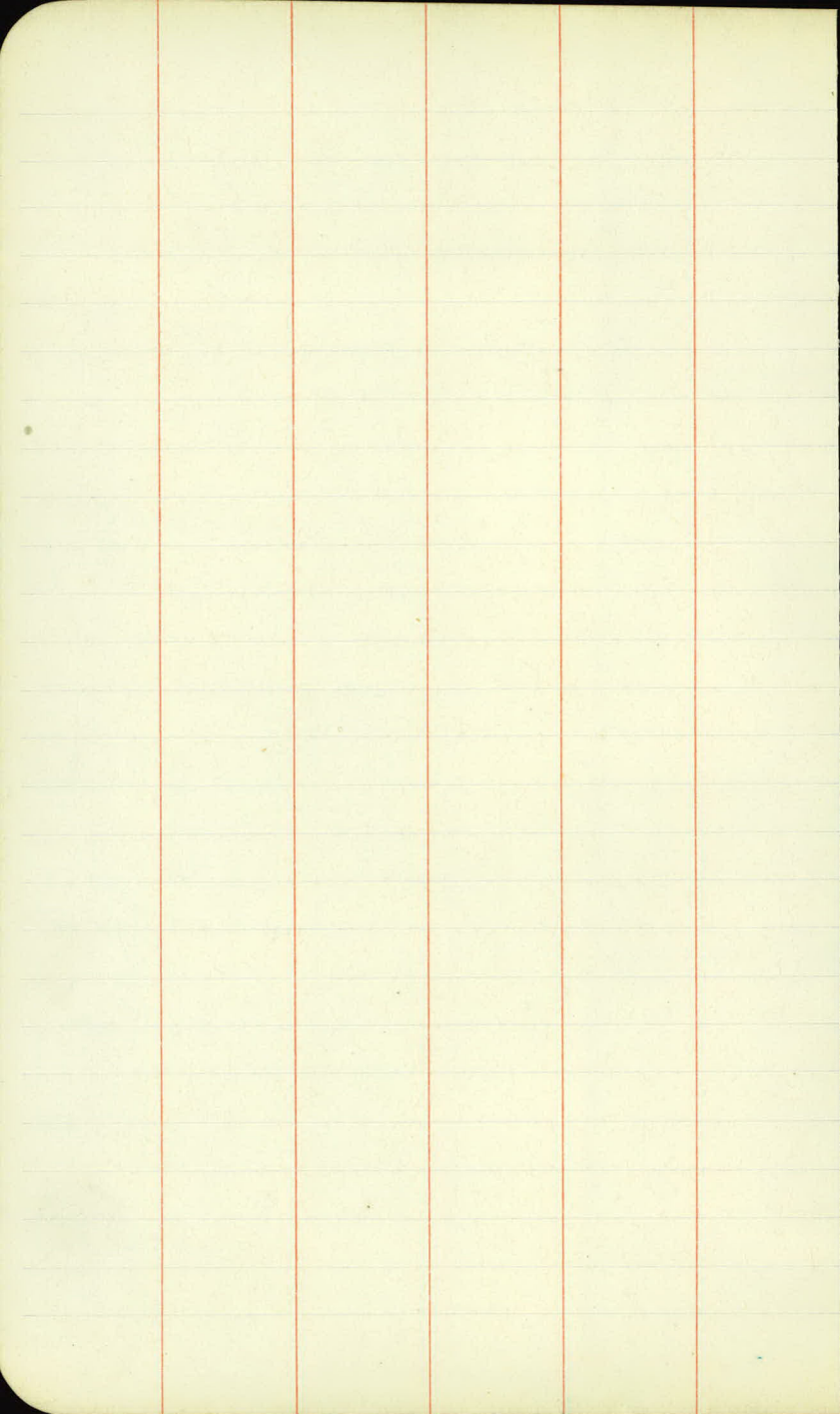
9-28-28

+83 FIELD ENT.  
+83 SIDE DRAIN 25  
OLD 18" 1/16 CM

+25 P.P. 35

+61 P.P. 30

+62 FIELD ENT.



The image shows a page from a notebook with a grid of 20 columns and 30 rows. A vertical red line runs down the center of the page, between the 10th and 11th columns. The grid is composed of light blue lines. The page is otherwise blank, with the number '69' written in the top right corner.

B.M.  
0+40  
0+60

0.46

100.46 ✓

100.00

0+75

1+00

1+10

1+21

1+38

1+55

1+74

2+00

2+21

0.46 100.00 ✓

10-29-28

SAME AS ORIGINAL.

$\frac{31}{42}$	$\frac{53}{40}$	$\frac{63}{38}$	$\frac{63}{31}$	$\frac{72}{24}$	$\frac{72}{16}$	$\frac{77}{5}$	$\frac{77}{5}$	(6.4)	$\frac{78}{20}$	$\frac{73}{23}$	$\frac{70}{30}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	-------	-----------------	-----------------	-----------------

$\frac{50}{45}$	$\frac{72}{40}$	$\frac{77}{36}$	$\frac{83}{20}$	$\frac{81}{8}$	(7.0)	$\frac{77}{10}$	$\frac{74}{21}$
-----------------	-----------------	-----------------	-----------------	----------------	-------	-----------------	-----------------

$\frac{80}{43}$	$\frac{77}{38}$	$\frac{80}{30}$	$\frac{80}{26}$	$\frac{85}{22}$	$\frac{88}{16}$	$\frac{92}{9}$	(7.1)	$\frac{86}{11}$	$\frac{71}{15}$	$\frac{61}{20}$	$\frac{42}{25}$	$\frac{27}{41}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{40}{45}$	$\frac{80}{39}$	$\frac{84}{38}$	$\frac{87}{27}$	$\frac{85}{10}$	(7.8)	$\frac{56}{15}$	$\frac{36}{20}$	$\frac{36}{27}$	$\frac{32}{38}$
-----------------	-----------------	-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------	-----------------

$\frac{38}{53}$	$\frac{68}{48}$	$\frac{77}{40}$	$\frac{84}{36}$	$\frac{80}{17}$	(40.2)	$\frac{54}{8}$	$\frac{43}{18}$	$\frac{34}{24}$	$\frac{31}{31}$	$\frac{33}{39}$
-----------------	-----------------	-----------------	-----------------	-----------------	--------	----------------	-----------------	-----------------	-----------------	-----------------

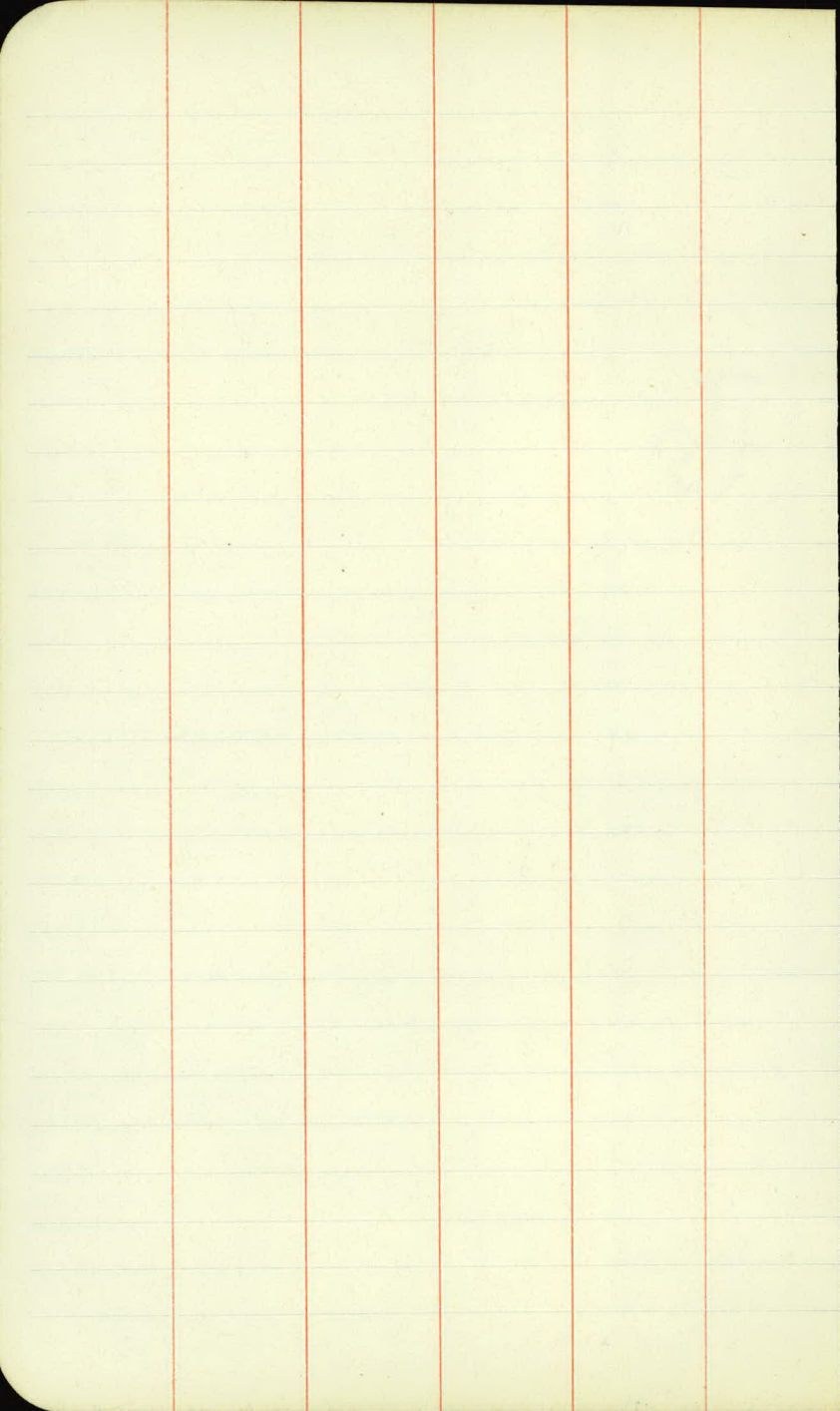
$\frac{75}{45}$	$\frac{81}{43}$	$\frac{83}{35}$	$\frac{88}{27}$	$\frac{87}{16}$	$\frac{67}{13}$	(01)	$\frac{46}{9}$	$\frac{45}{14}$	$\frac{31}{18}$	$\frac{30}{30}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------	----------------	-----------------	-----------------	-----------------

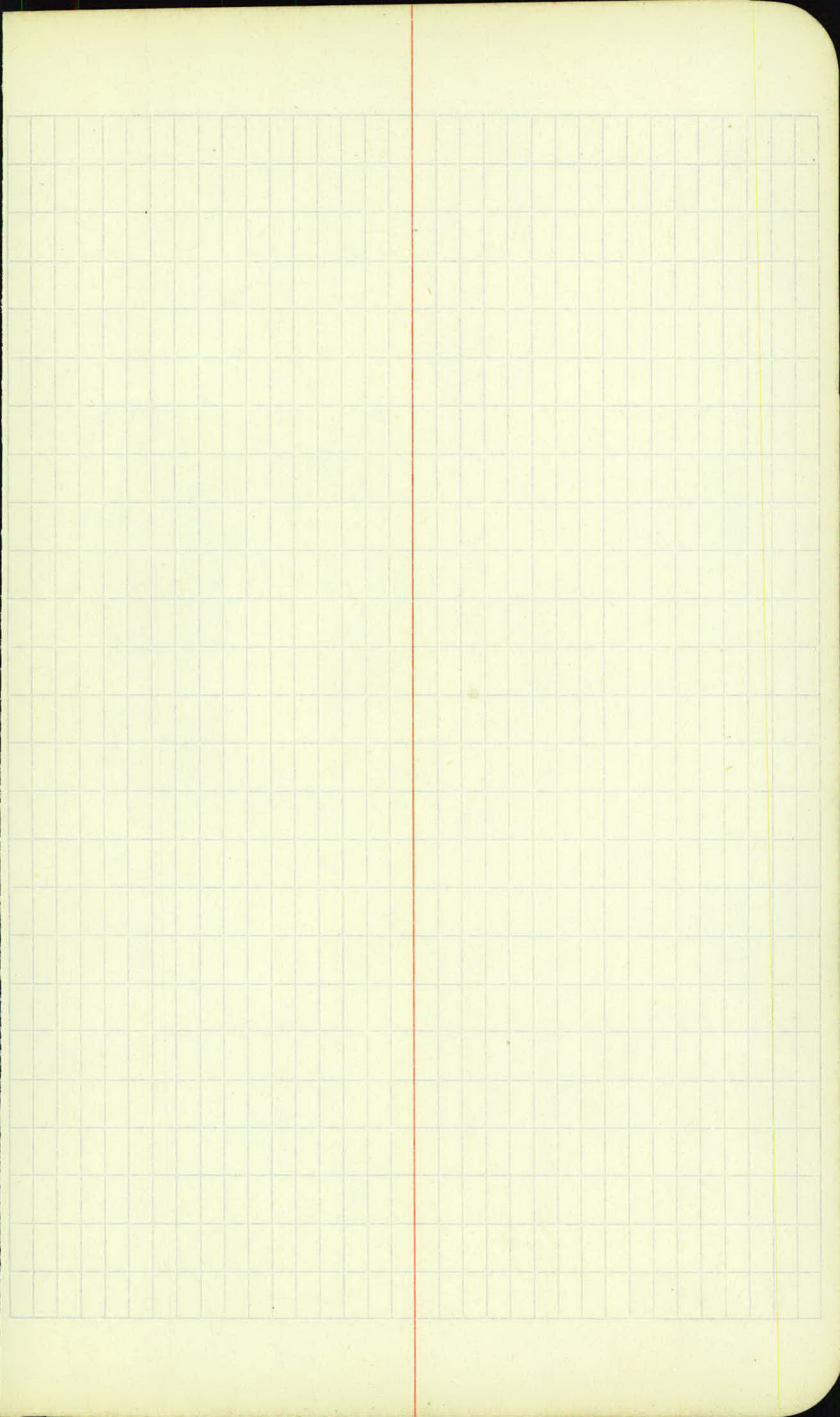
$\frac{71}{50}$	$\frac{76}{44}$	$\frac{83}{33}$	$\frac{82}{22}$	$\frac{58}{13}$	(10.5)	$\frac{50}{9}$	$\frac{45}{15}$	$\frac{28}{17}$	$\frac{21}{26}$
-----------------	-----------------	-----------------	-----------------	-----------------	--------	----------------	-----------------	-----------------	-----------------

$\frac{58}{47}$	$\frac{63}{47}$	$\frac{71}{45}$	$\frac{82}{33}$	$\frac{75}{20}$	(13)	$\frac{72}{10}$	$\frac{60}{15}$	$\frac{54}{25}$	$\frac{44}{27}$	$\frac{28}{27}$	$\frac{18}{35}$
-----------------	-----------------	-----------------	-----------------	-----------------	------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{51}{43}$	$\frac{74}{32}$	$\frac{85}{22}$	(6.4)	$\frac{59}{10}$	$\frac{49}{15}$	$\frac{30}{30}$
-----------------	-----------------	-----------------	-------	-----------------	-----------------	-----------------

SAME AS ORIGINAL.





$$\begin{array}{r} 15.06 \\ \underline{\quad 6} \\ 90.36 \end{array}$$

1030'

# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or I. P.= $23^{\circ} 20'$  to the R. at Station  
542+72.

Ext. in Tab. IV opposite  $23^{\circ} 20'$ =120.87  
 $120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20'$ =1183.1  
 $1183.1 \div 10 = 118.31$ .

Tab. V. correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur.=0.16  
 $118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)  
Ang.  $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333$ =L. C.

$2^{\circ} 19\frac{1}{2}'$ =def. for sta.	542	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}'$ = " " "	+50	Tan.=	1.18.47
$7^{\circ} 19\frac{1}{2}'$ = " " "	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}'$ = " " "	+50	L. C.=	2.33.33
$11^{\circ} 40'$ = " " "	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3'$  (def. for 1 ft. of  $10^{\circ}$  Cur.) =  $139.41'$  =  
 $2^{\circ} 19\frac{1}{2}'$ =def. for sta. 542.

Def. for 50 ft.= $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)

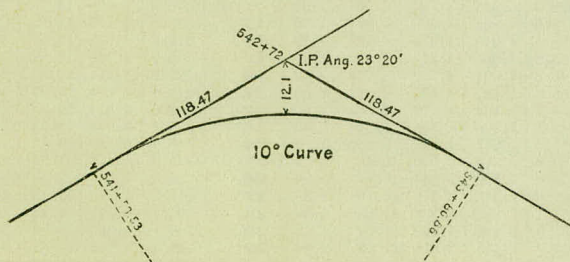


TABLE I. — Minutes in Decimals of a Degree.

<b>1</b>	.0167	<b>11'</b>	.1833	<b>21'</b>	.3500	<b>31'</b>	.5167	<b>41'</b>	.6833	<b>51'</b>	.8500
<b>2</b>	.0333	<b>12</b>	.2000	<b>22</b>	.3667	<b>32</b>	.5333	<b>42</b>	.7000	<b>52</b>	.8667
<b>3</b>	.0500	<b>13</b>	.2167	<b>23</b>	.3833	<b>33</b>	.5500	<b>43</b>	.7167	<b>53</b>	.8833
<b>4</b>	.0667	<b>14</b>	.2333	<b>24</b>	.4000	<b>34</b>	.5667	<b>44</b>	.7333	<b>54</b>	.9000
<b>5</b>	.0833	<b>15</b>	.2500	<b>25</b>	.4167	<b>35</b>	.5833	<b>45</b>	.7500	<b>55</b>	.9167
<b>6</b>	.1000	<b>16</b>	.2667	<b>26</b>	.4333	<b>36</b>	.6000	<b>46</b>	.7667	<b>56</b>	.9333
<b>7</b>	.1167	<b>17</b>	.2833	<b>27</b>	.4500	<b>37</b>	.6167	<b>47</b>	.7833	<b>57</b>	.9500
<b>8</b>	.1333	<b>18</b>	.3000	<b>28</b>	.4667	<b>38</b>	.6333	<b>48</b>	.8000	<b>58</b>	.9667
<b>9</b>	.1500	<b>19</b>	.3167	<b>29</b>	.4833	<b>39</b>	.6500	<b>49</b>	.8167	<b>59</b>	.9833
<b>10</b>	.1667	<b>20</b>	.3333	<b>30</b>	.5000	<b>40</b>	.6667	<b>50</b>	.8333	<b>60</b>	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	<sup>1</sup> / <sub>8</sub>	3-16	<sup>1</sup> / <sub>4</sub>	5-16	<sup>3</sup> / <sub>8</sub>	<sup>1</sup> / <sub>2</sub>	<sup>5</sup> / <sub>8</sub>	<sup>3</sup> / <sub>4</sub>	<sup>7</sup> / <sub>8</sub>
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
<b>0° 10'</b>	34377.	.036	.145	.291	0.05'	<b>7°</b>	819.0	1.528	6.105	12.21	2.10'
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	<b>8</b>	716.8	1.746	6.976	13.95	2.40
<b>1</b>	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	<b>9</b>	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
<b>2</b>	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	<b>10</b>	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2292.0	.545	2.181	4.363	0.75	<b>11</b>	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	<b>12</b>	478.3	2.620	10.45	20.91	3.60
<b>3</b>	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	<b>13</b>	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	<b>14</b>	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	<b>15</b>	383.1	3.277	13.05	26.11	4.50
<b>4</b>	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	<b>16</b>	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.781	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	<b>17</b>	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	<b>18</b>	319.6	3.935	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	<b>19</b>	302.9	4.155	16.51	33.01	5.70
<b>5</b>	1146.3	1.091	4.362	8.724	1.50	<b>20</b>	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	<b>21</b>	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	<b>22</b>	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	<b>23</b>	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	<b>24</b>	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	<b>25</b>	231.0	5.476	21.64	43.28	7.50
<b>6</b>	955.4	1.309	5.234	10.47	1.80	<b>26</b>	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	<b>27</b>	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	<b>28</b>	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	<b>29</b>	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	<b>30</b>	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>1°</b>	50.00	.22	<b>11°</b>	551.70	26.50	<b>21°</b>	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
<b>2</b>	100.01	.87	<b>12</b>	602.21	31.56	<b>22</b>	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
<b>3</b>	150.04	1.96	<b>13</b>	652.81	37.07	<b>23</b>	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
<b>4</b>	200.08	3.49	<b>14</b>	703.51	43.03	<b>24</b>	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
<b>5</b>	250.16	5.46	<b>15</b>	754.32	49.44	<b>25</b>	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
<b>6</b>	300.28	7.86	<b>16</b>	805.25	56.31	<b>26</b>	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
<b>7</b>	350.44	10.71	<b>17</b>	856.30	63.63	<b>27</b>	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
<b>8</b>	400.66	13.99	<b>18</b>	907.49	71.42	<b>28</b>	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
<b>9</b>	450.93	17.72	<b>19</b>	958.81	79.67	<b>29</b>	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
<b>10</b>	501.28	21.89	<b>20</b>	1010.3	88.39	<b>30</b>	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

## IV

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>31°</b>	1589.0	216.3	<b>41°</b>	2142.2	387.4	<b>51°</b>	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
<b>32</b>	1643.0	230.9	<b>42</b>	2199.4	407.6	<b>52</b>	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
<b>33</b>	1697.2	246.1	<b>43</b>	2257.0	428.5	<b>53</b>	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
<b>34</b>	1751.7	261.8	<b>44</b>	2314.9	450.0	<b>54</b>	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
<b>35</b>	1806.6	278.1	<b>45</b>	2373.3	472.1	<b>55</b>	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.4	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
<b>36</b>	1861.7	294.9	<b>46</b>	2432.1	494.8	<b>56</b>	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
<b>37</b>	1917.1	312.2	<b>47</b>	2491.3	518.2	<b>57</b>	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
<b>38</b>	1972.9	330.2	<b>48</b>	2551.0	542.2	<b>58</b>	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
<b>39</b>	2029.0	348.6	<b>49</b>	2611.2	566.9	<b>59</b>	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
<b>40</b>	2085.4	367.7	<b>50</b>	2671.8	592.3	<b>60</b>	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>61°</b>	3375.0	920.2	<b>71°</b>	4086.9	1308.2	<b>81°</b>	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
<b>62</b>	3442.7	954.8	<b>72</b>	4162.8	1352.6	<b>82</b>	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
<b>63</b>	3511.1	990.2	<b>73</b>	4239.7	1398.0	<b>83</b>	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
<b>64</b>	3580.3	1026.6	<b>74</b>	4317.6	1444.6	<b>84</b>	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
<b>65</b>	3650.2	1063.9	<b>75</b>	4396.5	1492.4	<b>85</b>	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
<b>66</b>	3720.9	1102.2	<b>76</b>	4476.5	1541.4	<b>86</b>	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
<b>67</b>	3792.4	1141.4	<b>77</b>	4557.6	1591.6	<b>87</b>	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
<b>68</b>	3864.7	1181.6	<b>78</b>	4639.8	1643.0	<b>88</b>	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
<b>69</b>	3937.9	1222.7	<b>79</b>	4723.2	1695.8	<b>89</b>	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
<b>70</b>	4011.9	1265.0	<b>80</b>	4807.7	1749.9	<b>90</b>	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>91°</b>	5830.5	2444.9	<b>101°</b>	6950.6	3278.1	<b>111°</b>	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
<b>92</b>	5933.2	2518.5	<b>102</b>	7075.5	3374.9	<b>112</b>	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
<b>93</b>	6037.8	2594.0	<b>103</b>	7203.2	3474.4	<b>113</b>	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
<b>94</b>	6144.3	2671.6	<b>104</b>	7333.6	3576.8	<b>114</b>	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
<b>95</b>	6252.8	2751.3	<b>105</b>	7467.0	3682.3	<b>115</b>	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
<b>96</b>	6363.4	2833.2	<b>106</b>	7603.5	3791.0	<b>116</b>	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
<b>97</b>	6476.2	2917.3	<b>107</b>	7742.2	3902.9	<b>117</b>	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
<b>98</b>	6591.2	3003.8	<b>108</b>	7886.2	4018.2	<b>118</b>	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
<b>99</b>	6708.6	3092.7	<b>109</b>	8032.7	4137.1	<b>119</b>	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
<b>100</b>	6828.3	3184.1	<b>110</b>	8182.8	4259.7	<b>120</b>	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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For Tangents Add															
ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°		.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°		.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°		.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°		.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°		.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°		.11	.22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°		.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°		.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°		.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°		.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°		.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°		.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°		.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°		.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°		.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°		.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°		.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°		.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.49	4.98	5.38	5.83
100°		.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

## For Externals Add

ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°		.001	.003	.004	.005	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°		.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°		.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°		.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°		.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°		.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°		.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°		.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°		.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°		.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°		.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°		.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°		.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°		.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°		.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°		.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°		.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°		.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°		.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

## CURVE FORMULAS.

$T = R \tan \frac{1}{2} I$	$R = T \cot. \frac{1}{2} I$	Chord def. = $\frac{\text{chord}^2}{R}$
$T = \frac{50 \tan. \frac{1}{2} I}{\text{Sin. D}}$	$R = 50$	No. chords = $\frac{\frac{1}{2} I}{D}$
$\text{Sin. D} = \frac{50}{R}$	$\text{Sin. D}$	Tan. def. = $\frac{1}{2}$ chord def.
$\text{Sin. D} = \frac{50 \tan. \frac{1}{2} I}{T}$	$E = R \text{ ex. sec. } \frac{1}{2} I$	
	$E = T \tan \frac{1}{4} I$	

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES. — Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

## Natural Sines

DEG.	0'	10'	20'	30'	40'	50'	DEG.	DEG.	0'	10'	20'	30'	40'	50'	DEG.
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1276	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	DEG.	60'	50'	40'	30'	20'	10'	DEG.

DEG.	0'	10'	20'	30'	40'	50'	DEG.
80	9848	9853	9858	9863	9868	9872	9
81	9877	9881	9886	9890	9894	9899	8
82	9903	9907	9911	9914	9918	9922	7
83	9925	9929	9932	9936	9939	9942	6
84	9945	9948	9951	9954	9957	9959	5
85	9962	9964	9967	9969	9971	9974	4
86	9976	9978	9980	9981	9983	9985	3
87	9986	9988	9989	9990	9992	9993	2
88	9994	9995	9996	9997	9997	9998	1
89	9998	9999	9999	9999	I.0000	I.0000	0
DEG.	60'	50'	40'	30'	20'	10'	DEG.

## Natural Cosines

Natural Tangents

DEG.	0'	10'	20'	30'	40'	50'	DEG.	DEG.	0'	10'	20'	30'	40'	50'	DEG.
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8667	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
DEG.	60'	50'	40'	30'	20'	10'	DEG.	DEG.	60'	50'	40'	30'	20'	10'	DEG.

DEG.	0'	10'	20'	30'	40'	50'	DEG.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.77	0
DEG.	60'	50'	40'	30'	20'	10'	DEG.

Natural Cotangents

$$51.29$$

$$60 \overline{) 308.34} \quad 5.14$$

$$\begin{array}{r} 300 \\ \hline 83 \\ 60 \\ \hline 234 \\ 1067 \\ \hline 6 \end{array}$$

$$53.46$$

$$60 \overline{) 3207.6} \quad 5.342$$

$$\begin{array}{r} 300 \\ \hline 207 \\ 1804 \\ \hline 276 \\ \hline 6 \end{array}$$

$$60 \overline{) 267.0} \quad 4.45$$

$$\begin{array}{r} 240 \\ \hline 270 \\ \hline 240 \\ \hline 300 \end{array}$$

$$\begin{array}{r} 12 \\ \hline 20 \\ \hline 340 \\ \hline 51 \\ \hline 9 \\ \hline 3 \end{array}$$

$$60 \overline{) 64.03} \quad 1.067$$

$$\begin{array}{r} 60 \\ \hline 403 \\ 360 \\ \hline 430 \\ 420 \\ \hline 1070 + 39.54 \end{array}$$

$$4 + 54.60$$

$$43065 + 84.94$$

$$1070 + 39.54$$

$$44.5$$

$$60 \overline{) 267.0} \quad 4.45$$

$$\begin{array}{r} 240 \\ \hline 270 \\ \hline 240 \end{array}$$

$$41.40$$

$$4.27$$

$$46.07$$

39.54

$$\begin{array}{r}
 39.54 \\
 \underline{\phantom{39.54}6} \\
 60 \overline{) 237.24} \quad (3.954) \quad 65 + 84.94 \\
 \underline{180} \\
 572 \\
 \underline{540} \\
 324 \\
 \underline{300} \\
 2499
 \end{array}$$

$$\begin{array}{r}
 9 \quad 4546 \\
 \underline{\phantom{9 \quad 4546}6} \\
 70 + 39.54
 \end{array}$$

$$\begin{array}{r}
 \phantom{60} \overline{\phantom{238.14}6} \\
 60 \overline{) 238.14} \quad (3.969)
 \end{array}$$

$$\begin{array}{r}
 180 \\
 \underline{581} \\
 540 \\
 \underline{414} \\
 360 \\
 \underline{54} \quad 4
 \end{array}$$

$$\begin{array}{r}
 1030' \\
 \underline{52} \\
 42
 \end{array}$$

$$60 \overline{) 246}$$

$$\begin{array}{r}
 15.06 \\
 \underline{\phantom{15.06}6} \\
 60 \overline{) 90.36} \quad (1.506) \\
 \underline{60} \\
 303 \\
 \underline{300} \\
 36
 \end{array}$$

05-8'

181  
51  
711

927.84  
9.04  
931.88

92312  
2.05  
92107

915.60  
665  
977.25  
2.79  
921.46  
9.41  
930.87  
52  
930.35  
9.61

918.20  
90  
0

93999  
964  
920.35  
52  
930.87  
8.03  
922.84  
9.04

73.61  
638  
9902  
28.0  
97  
922.95  
520  
917.75  
738

931.88  
10.62  
921.26  
188  
923.12  
205

925.13  
152  
923.61  
152

921.07  
198  
923.05  
3.65  
919.40  
9.55  
929.95

925.13

$$\begin{array}{r}
 918.70 \\
 9.93 \\
 \hline
 928.13 \\
 4.22 \\
 \hline
 923.91 \\
 2.02 \\
 \hline
 925.93 \\
 4.88 \\
 \hline
 921.01 \\
 4.88 \\
 \hline
 925.93 \\
 7.70 \\
 \hline
 918.73 \\
 4.83 \\
 \hline
 923.00 \\
 1.32 \\
 \hline
 917.74
 \end{array}$$

$$\begin{array}{r}
 363 + 54.8 \\
 337 + 15.39 \\
 \hline
 26739.41
 \end{array}$$

$$\begin{array}{r}
 28100.6 \\
 4 + 53.33 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 234627 \\
 29133 \\
 \hline
 \end{array}$$

$$\begin{array}{r}
 96137.57 \\
 \hline
 \end{array}$$

$$263827$$

$$\begin{array}{r}
 152 \\
 23 \\
 \hline
 225
 \end{array}$$

291.10  
 1.43  
 292.53

8.45  
 5813.6  
 291.10  
 5930.5  
 5813.6  
 16.9  
 41.90  
 45.07

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.  
 R.

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