

PLANS SURVEY

HODGSON ROAD

FROM RICE ST.

TO NORTH COUNTY LINE

RAMSEY COUNTY PROJECT ~~2107~~

Rd. 9/2 N^o 13 & 1

File N^o 12

28-01-B

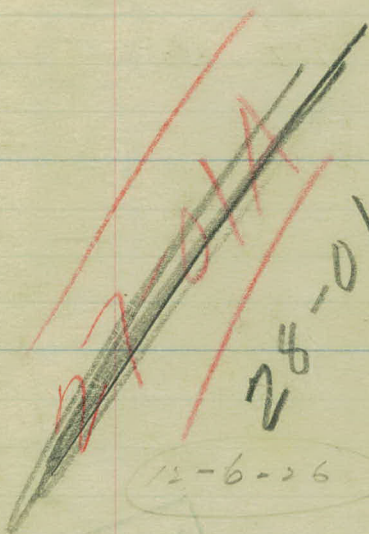
28-01-B

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Dec. 16, 1926

12

Alignment notes on
the Hodgson Rd. (Rd. 7/4 H 13 & 1.)
from Rice St. to the N. Co. line.



28-01B-142

12-6-26

Office of Ramsey Co. Engineer
ST. PAUL, MINN.
12-16-26
12

Sta. Point Lt. Pt.

5760⁴³ P.T. ✓

N. 43°-26' W.

3700 P.I. 43°-58'

x

0710⁶⁵ P.C. ✓

253710⁶⁵ P.O.T. = 0710⁶⁵ P.C.

N. 00°-38' E.

N. 00° 32' E.

252762⁶⁵ P.O.T.

0+10 ⁶⁵

+50 - 1°-34'

1+00 - 3°-34'

+50 - 5°-34'

2+00 - 7°-34'

+50 - 9°-34'

3+00 - 11°-34'

+50 - 13°-34'

4+00 - 15°-34'

+50 - 17°-34'

5+00 - 19°-34'

+50 - 21°-34'

160 ²³ - 21°-59'



Δ - 43°-58'

D. - 8' L.

T. - 289 ³⁵ ✓

L. - 549 ⁵⁸ ✓

R. - 716 ⁶⁸

252+62 ⁶⁵

Rice St.
24' Pavement

63 ²⁵ Tree

P.O.T. on Rice St. Survey

25 ¹⁰ Tree

Sta. Point Lt. Rt.

44+76⁴⁵ P.I.

0°-21'

N. 17°-24' W.

44+50³⁵ P.O.T.

N. 17°-45' W.

20+58⁴⁸ P.T. ✓

18+06¹² P.I.

25°-41'

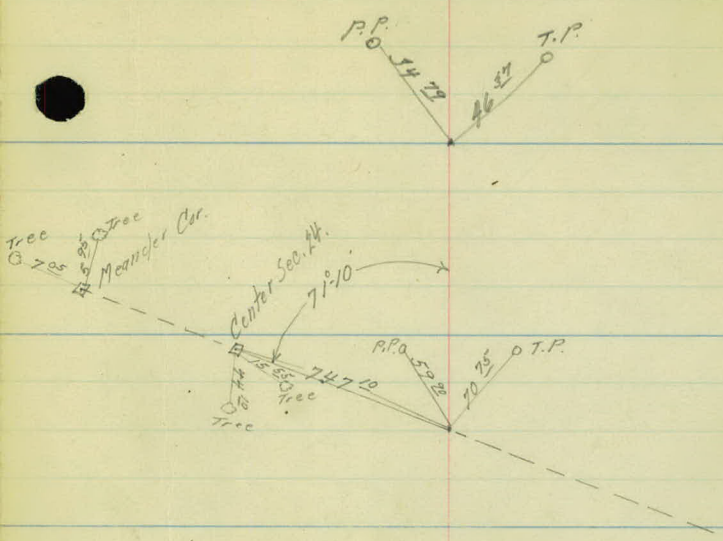
43-52

08-27

X

15+44²² P.C. ✓

N. 45°-26' W.



15 + 44⁸²

- +50 - 0°-08'
- 16 + 00 - 1°-23'
- +50 - 2°-38'
- 17 + 00 - 3°-53'
- +50 - 5°-08'
- 18 + 00 - 6°-23'
- +50 - 7°-38'
- 19 + 00 - 8°-53'
- +50 - 10°-08'
- 20 + 00 - 11°-23'
- +50 - 12°-38'
- +58⁴⁸ - 12°-50'



- Δ - 25°-41'
- D - 5° (L) R
- T - 261⁵⁰ ✓
- L - 513⁶⁶ ✓
- R - 1146²⁸

Sta. Point Lt. Ft.

87+05³⁸ P.T. ✓

N 21° - 48' W.

85+95⁴⁵ P.I. 4° - 24'

x

84+85³⁸ P.C. ✓

N 17° - 24' W.

72+56⁵³ P.O.T. Co. R. of "C."

84785 ³⁸

85700 - 0°-09'

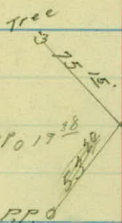
750 - 0°-39'

86100 - 1°-09'

750 - 1°-39'

87100 - 2°-09'

705 ³⁸ - 2°-12'



A - 4°-24'

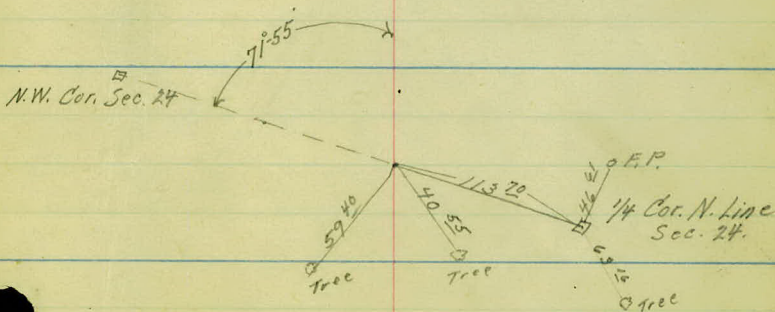
D - 2° L.

T. - 110 ⁰⁷ ✓

L. - 220 ⁰⁰ ✓

R. - 2864 ⁹⁸

71733.9



Sta. Point Lt. Pt.

Equation. ✓

$128 + 25 \frac{93}{2}$ P.T. = $121 + 31 \frac{23}{2}$

✓
N. 00° 00' E

$124 + 32 \frac{5}{2}$ P.I. $41^{\circ} - 14'$

x

$120 + 01 \frac{22}{2}$ P.C. ✓

✓
N. 41° - 14' W.

$102 + 14 \frac{58}{2}$ P.T. ✓

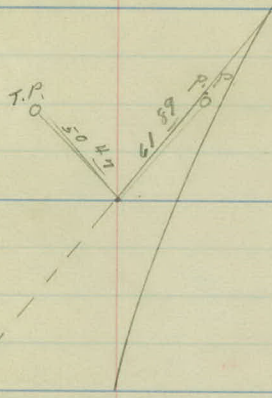
$100 + 22 \frac{9}{2}$ P.I. $19^{\circ} - 16'$

x

$98 + 25 \frac{72}{2}$ P.C. ✓

✓
N. 21° - 48' W.

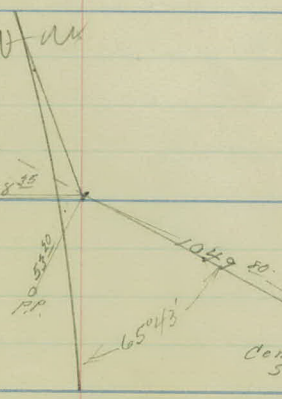
- 120701 ²⁷
- 121700 - 2°-28'
- 122700 - 4°-55'
- 123700 - 7°-28'
- 124700 - 9°-58'
- 125700 - 12°-28'
- 126700 - 14°-58'
- 127700 - 17°-28'
- 128700 - 19°-58'
- 125²⁸ - 20°-57'



- Δ - 41°-14'
- D - 5° R.
- T - 431 ²³ ✓
- L - 824 ⁶⁶ ✓
- R - 1146 ³⁸

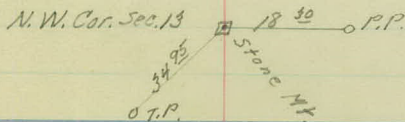
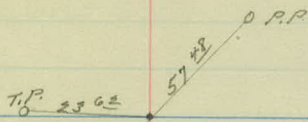
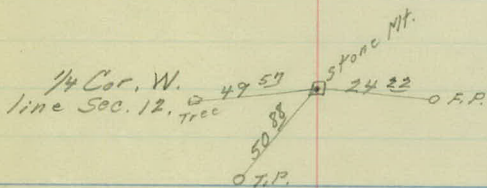
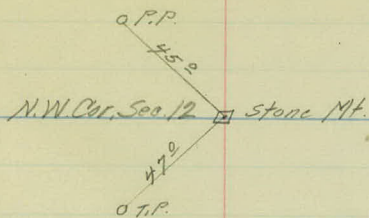
1/4 Cor. W. line Sec. 13

- 98725 ¹²
- 98750 - 0°-56'
- 99700 - 1°-51'
- 99750 - 3°-06'
- 100700 - 4°-21'
- 100750 - 5°-36'
- 101700 - 6°-51'
- 101750 - 8°-06'
- 102700 - 9°-21'
- 114³⁸ - 9°-43'



- Δ - 19°-26'
- D - 5° L.
- T - 196 ²⁸
- L - 388 ⁶⁶
- R - 1146 ²⁸
- Center of Sec. 13.
- Tree
- Tree

Sta.	Point	Ht.	Rt.	
178+58 [±]	P.I.	0°-25'		N00°-11'E. ✓
152+39°	P.I.	0°-15'		N00°-36'E. ✓
146+87 ⁵⁰	P.O.T.			N00°-21'E. ✓
125+94 [±]	P.I.	0°-21'		N00°-00'E. ✓



Sta. Point Lt. Mt.

236+66⁴ P.I. No Co. Line. x

219+00 P.O.T.

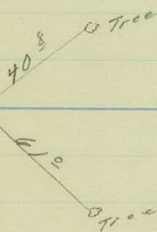
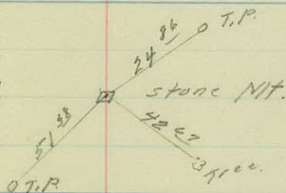
↙
No^o-29' F.

204+97³ P.I.

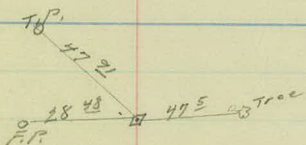
0°-16'

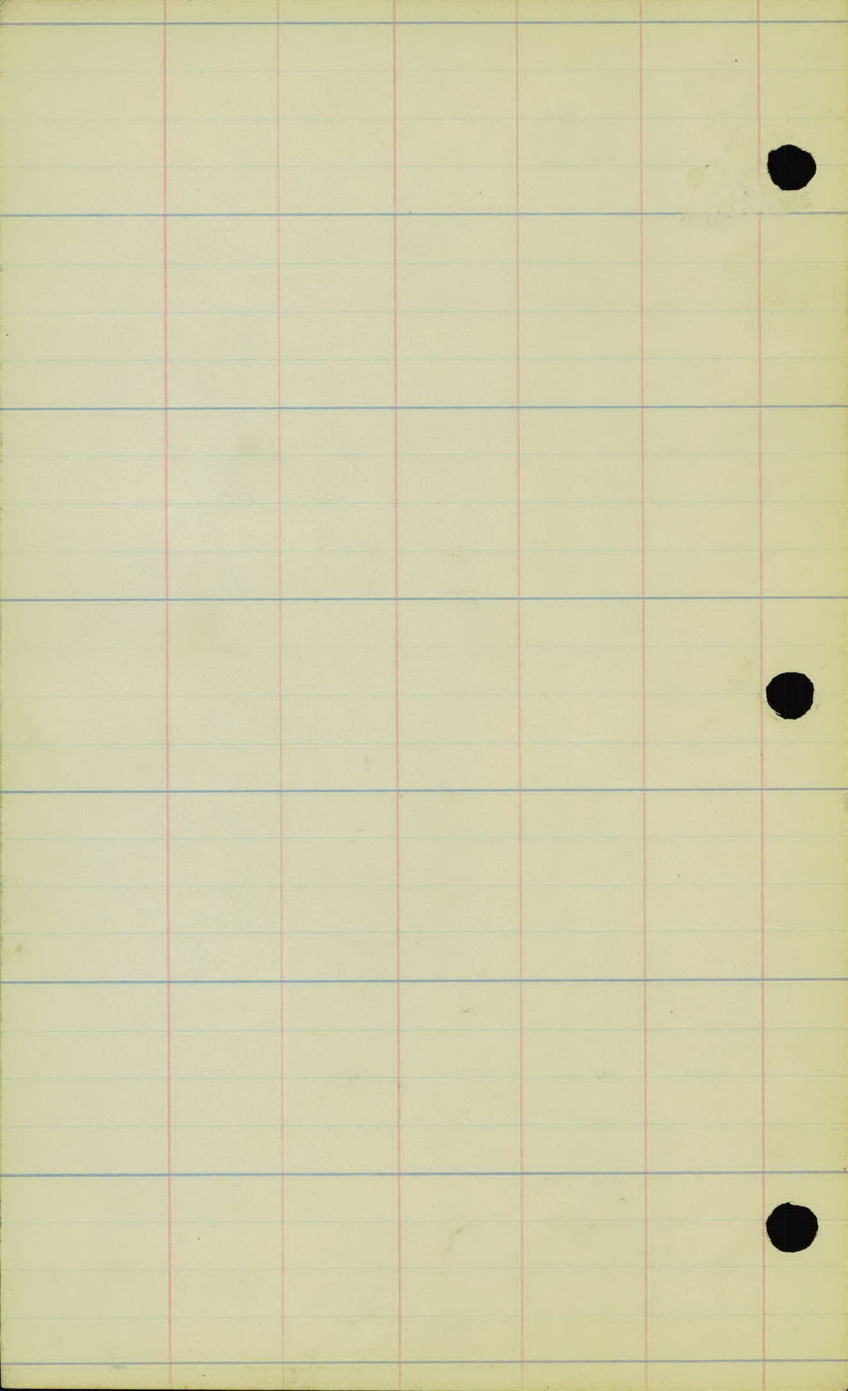
↙
No^o-11' F.

N.W. Cor. Sec. 1



1/4 Cor. W.
line Sec. 1.





Hodgson Rd.

Rd % # 13 & 1.

Art. Topog from Sta.
0+00 to Sta. 236+00.

5

4

3

2

1

0700

Hay field.

SW

Dice St.
24' Pavement.

+15 T.P. E.R.

+95 & ditch.

+85 Triple Tree 15'
+71 -10" T. -20' L.

85
0

+87 T.P. 24' L.

+63 Center Pier Sign 15' L.



11

10

9

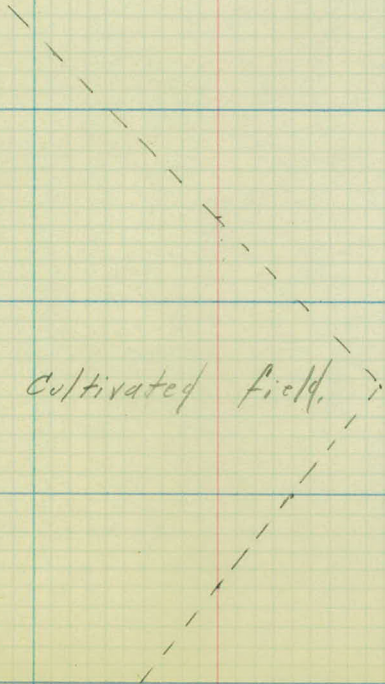
8

7

6

5

Hay
field.



cultivated field.

17

16

15

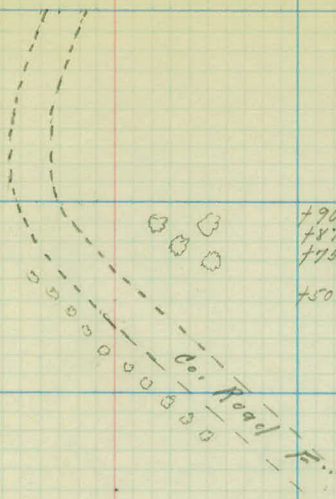
14

13

12

11

11-20-26



+90-24"-T. 20.
+87-24"-T. 14"
+95 T.P. 7 R.
+50 E. Co. Rd. F.

Hay
field,

23

22

21

20

19

18

17

F. 20

F. 20

+06 F. Cor. 20



+93 F. Cor. 21

+90 T.P. 16 R.

Corn Field.

Scattered Oaks.

+28-T.P. 19

+11-12"-T-35

+21-18"-T-1-L.

+81-24"-T-25

+67-T.P.-8-R.

+54-10"-T-10

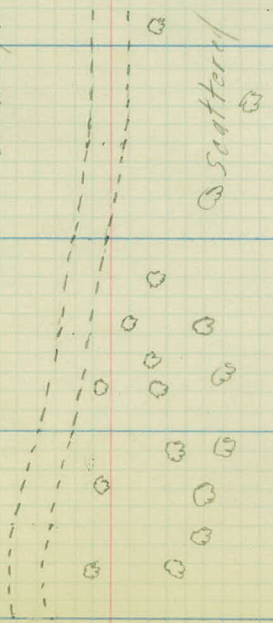
+37-12"-T-23

+22-18"-T-26

+74-18"-T-1-L.

+39 T.P. 20

+24-24"-T-7-L.



29

28

27

26

25

24

23

F. 19

+77 P.P. 17

Cultivated field.

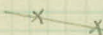
Cultivated field.

+83 T.P. 15

+20 P.P. 14

F. 19

+77 C.F. 19



Corn field.

+56 T.P. 17

+33 F. Cor. 21

+56 P.P. 18

scattered Oaks

Yard.

F. 20

+45 Field Ent

F. 21

+90 T.P. 14

+49 F. Cor. 21

+40 Farm Ent

+31 F. Cor. 20

Farm

+43 T.P. 20 R

35-

34

33

32

31

30

19

+74 P.P. 15'

+46 P.P. 16'

+62 Field Ent.

+99 P.P. 15'

+72 P.P. 17'

+70 F. Cor. 18'

+17 P.P. 17'

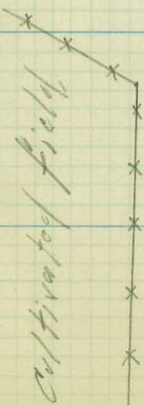
Field.

Hay Field.

+86 T.P. 17-

+54 Farm Rd.
+43 Milk Stand 15'
+22 T.P. 16

+72 T.P. 16



Cultivated Field

+29 T.P. 15'

41

40

39

38

37

36

35

+67 P.P. 16

F. 18

+28 P.P. 17

F. 17

+65 F. Cor. 16

+63 P.P. 15

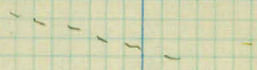
+18 P.P. 16



Woods.



Cultivated field.



+56 T.P. 20

Cultivated field

+72 T.P. 19

+11 T.P. 18



+47 T.P. 17

47

46

45

44

43

42

41

+57 P.P. 17

Woods

Cultivated field.

+83 T.P. 25

+67 P.P. 16 L.

+16 T.P. 24

+58 Farm Ent.
+48 F. Cor. 21



+60 P.P. 17

+60 T.P. 22

F. 30^E

Woods.

Corn field.

+17 P.P. 17

+60 T.P. 21

+35 F. Cor. 19
+12 Farm Ent.
+09 F. Cor. 18



53

52

51

50

49

48

47

F, 21

+21 P.P. 21

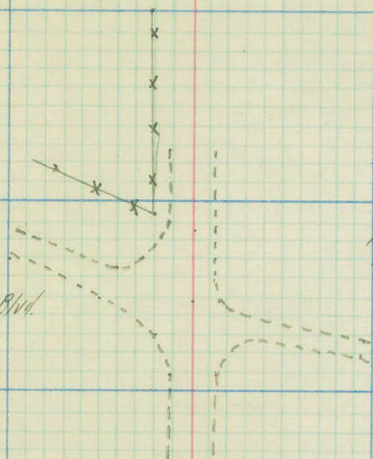
+94 F. Cor. 20

+48 Snail Lake Blvd.

+85 P.P. 15

+57 P.P. 14

+00 P.P. 17



+82 T.P. 24
+70 Iron Mt. Sign St.

Woods

Cultivated field

+14 T.P. 26

+60 T.P. 25

+46 Side Rd. Sign 13

59

58

57

56

55

54

53

+57 F. Cor. 21

+58 P.P. 28
+35 Farm Rd.

+84 P.P. 19

F. 21

+39 P.P. 17

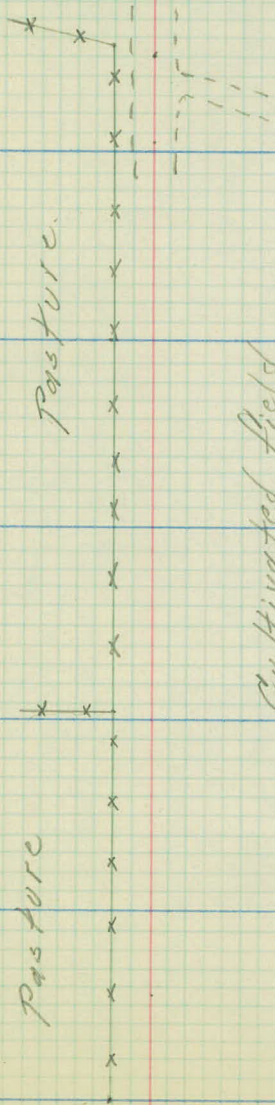
+55 Side W. Sign 13

+04 Cross F. 20

+00 P.P. 17

+63 T.P. P.P. 17h.

+43 T.P. 26



65

64

63

62

61

60

59

F. 17'

+63 P.P. 17

+20 P.P. 17

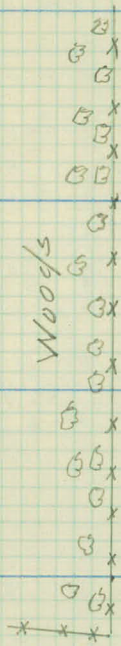
F. 19'

+70 F. Cor. 21
+60 Farm Ent.
+50-6"-T-18
+47-6"-T-18

+76 P.P. 17

+33 P.P. 17

Woods



Pasture.

Woods



F. 20

+69 F. Cor. 20

+02 Mail Box 17'

+86 Farm Ent.

+89-6"-T-19'

71

70

69

68

67

66

65

+00 P.P. 18

+65 P.P. 18

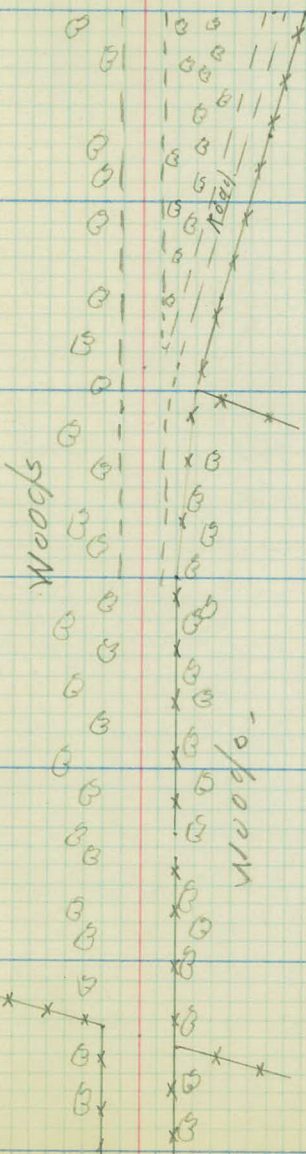
+19 P.P. 18

+77 P.P. 19

+41 P.P. 17

+67 F. Cor. 19

+03 P.P. 17



+50 F. 44

+00 F. 30

+51 F. 21
+47 Cross Mt. Sign 10
+35 F. 20

F. 20

F. 20

+60 Farm Ent

+54 C.F. 19

77

76

75

74

73

72

71

Hodgson Rd.

Rd. 9/2, #13 & 1.

Check Levels from Co. Rd. I.
to Co. Rd. F.

Sta.	+	H.I.	-	Elev.
B.M.	4.92	917.19		912.27
	2.89	915.21	4.87	912.32
	3.74	912.29	6.44	908.55
B.M.			4.05	908.24
	7.15	915.29	4.15	908.14
	10.85	925.12	1.02	914.27
B.M.			8.78	916.34
	8.14	952.24	1.04	924.08
	4.88	951.30	5.82	926.42
B.M.			5.24	926.06
	3.37	929.10	5.57	925.73
	3.64	926.24	6.50	922.60
B.M.			2.41	923.85
	4.05	926.07	4.22	922.04
	7.24	928.07	5.24	920.83
	8.51	930.93	5.45	922.62
B.M.	4.04	929.87	5.10	925.83
	4.30	929.08	5.09	924.78
	6.56	931.52	4.12	924.94
B.M.			4.51	927.01
	4.78	934.25	2.25	929.27
	4.13	932.37	4.01	928.24
B.M.			5.31	929.04 927.08
	4.44	930.62	6.21	926.14
	4.31	929.33	5.60	925.02
	3.01	928.83	3.51	925.82
B.M.			4.03	924.80

Spk. in 12" Oak Rt. Sta. 164+60.

Spk. in T.P. Lt. Sta.

Spk. in 30" Poplar Rt. Sta. 139+12

Spk. in 24" Oak Rt. Sta.

Spk. in 30" Oak, 100' Lt. Sta. 101+00

Spk. in 10" Oak Lt. Sta. 86+78

Spk. in 18" Oak Rt. Sta. 71+30

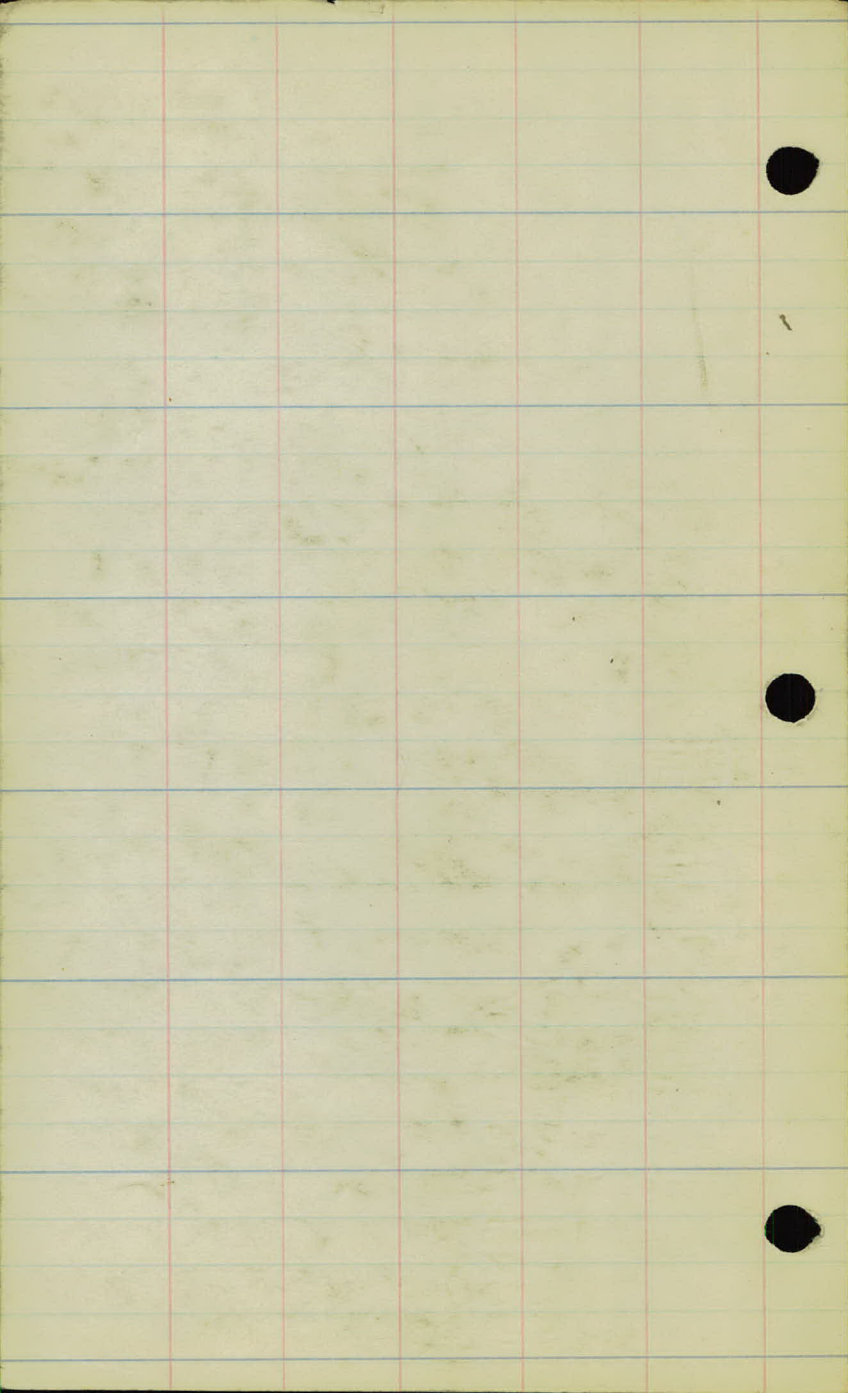
Spk. in 30" Oak Lt. Sta. 47+70

Sta.	+	H.I.	-	Elev.
		928.85		
	3.85	927.13	5.55	923.28
	4.40	926.14	5.59	921.54
	4.81	926.03	4.92	921.22
	4.14	924.65	5.52	920.51
B.M.			2.96	921.69
	3.34	921.07	4.92	917.73
B.M.	2.57	922.44	1.20	919.89
	8.61	927.69	3.36	919.08
	5.85	928.80	4.74	922.95
B.M.			4.88	923.92

Spk. in 18" Oak. H. Sta. 26+50,

Spk. in 18" Oak. H. Sta. 16+34

Spk. in 44" Oak. H. Sta. 0-20



+58 Cross Rd. Sign 17

+18 P.P. 18

Cultivated Field

Cultivated Field

+69 P.P. 18

74

Small Lake

+94 P.P. 18

75



+73 Store 57 1/2

+53 Store 31 1/2

+14 Gasline Pump 22

+11 Hedge Cor. 27

+78 Hedge Cor. 24

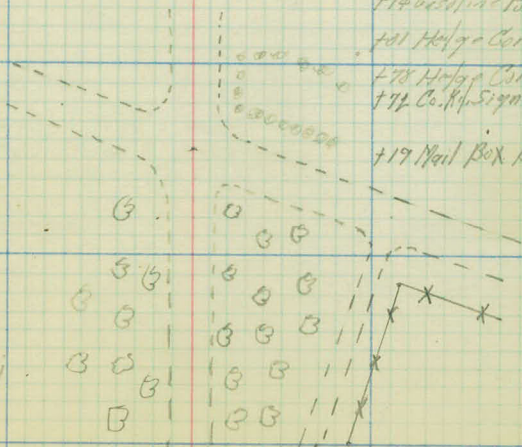
+74 Co. Rd. Sign 24

+19 Mail Box 15

+56 Co. Rd. C.

76

72 704 I. Rd. Sign 21



83

82

81

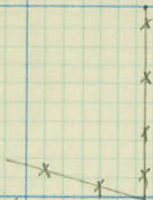
80

79

78

77

F. 36



+99 F. Cor. 36'

+69 P.P. 14'

+30 P.P. 18'

Cultivated Field

+73 P.P. 18'

Cultivated Field

+57 P.P. 18'

89

88

87

86

85

84

83

775 P.P. 20

754 P.P. 19

767 Twin Oaks 22

757 Farm 11h

750 F. 20

744 F. 30

728 C.F. 34

F. 34

795 P.P.

746 P.P. 17

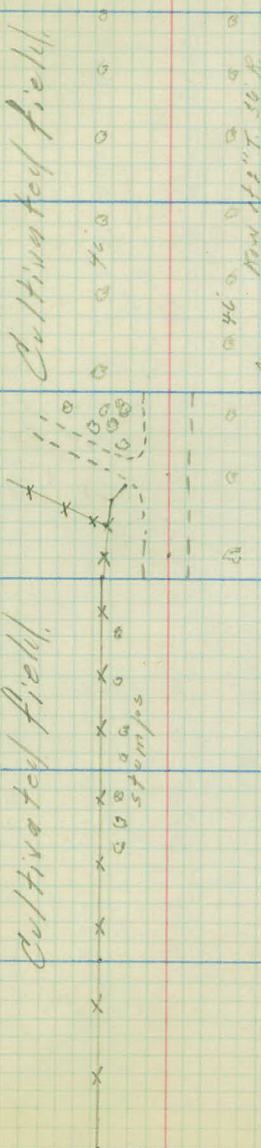
F. 34

708 P.P. 18

Cultivated field.

Cultivated field.

Cultivated field.



95

94

93

92

91

90

89

8 36 16 0

6 0

725 P.P. 21

0 6

0 0

0 0

786 P.P. 21

Cultivated field

Cultivated field

0 0

0 0

0 0

747 P.P. 20

0 6

0 0

0 0

0 0

714 P.P. 20

0 0

0 0

0 0

0 0

101

100

99

98

97

96

95

180-4¹/₂ 7-22

746 P.P. 48

715 F. Co. 25

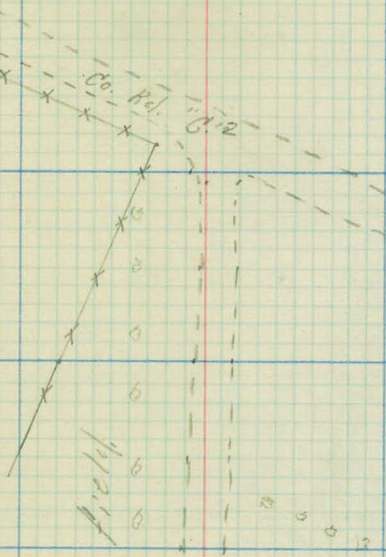
772 P.P. 10

F. 80

750 P.P. 21

705 P.P. 24

743 P.P. 11



Cultivated field

Cultivated

107

106

105

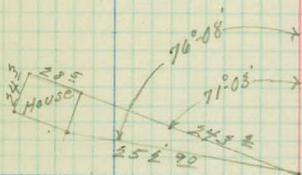
104

103

102

101

Cultivated
field.



Cultivated
field.

11-4^h-17

113

112

111

110

109

108

107

Cultivated
field.

0

0

0

+42-2-T-6

0

Cultivated
field.

0

0

+44-2-T-21

0

0

119

118

117

116

115

114

113

Cultivated
field.



125

124

123

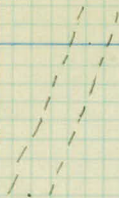
122

121

120

119

759 P.P. 43'



Cultivated
field.

124

123

122

128

127

126

125

+99 T.P. 19.

+06 P.P. 19'

+63 T.P. 18'
+49 Power line
Cross line

+63 P.P. 18'

+89 Power line & line
+81 P.P. 15

+74 F. Cor. 28

+07 T.P. 25

+17 P.P. 13

F. 24

+55 Mod Box 2

+51 F. Cor. 14

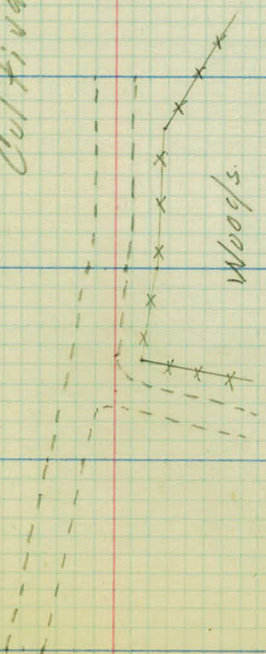
+38 Farm Est.

+89 P.P. 8

Cultivated field.

Cut Over land.

Woods.



130

129

128

127

126

125

124

+96 Farm Rd.
+76 F. Cor. 24
+64 T.P. 23

+56 P.P. 18

+98 T.P. 22
+33 F. Cor. 23
+09 Farm Ent.

+37 Turtle Lake
Sign 15
+16 P.P. 18

+64 Turtle Lake
Sign 18

+83 T.P. 22

+22 P.P. 18

+00 Farm Ent.

+65 T.P. 21

+96 P.P. 19

+21 T.P. 20

+54 P.P. 19

Cultivated field.

Cultivated field.

136

135

134

133

132

131

130

+95 T.P. 20

x

x

x

F. 33

+02 P.P. 22

x

+64 T.P. 24

x

x

Woods.

+80-8: T-10

x

+84 P.P. 15
+75 Farm Ent.

+46 F. Cor. 33
+67 Farm Rd
+50 F. Cor. 33
+49-8-7-16
+37 T.P. 21
F. 33

Cultivated field.

x

x

x

x

+15 T.P. 21

+37 P.P. 15

F. 33

x

x

x

Cultivated field.

F. 33

x

+89 T.P. 22

x

+95 P.P. 17

+09 F. Cor. 34

x

+08 P.P. 34

-x x

142

141

140

139

138

137

136

141 +93 T.P. 23

140 +95 C.F. 33
140 +90 -8"-T-24
140 +85 T.P. 22
140 +75 F. Cor. 33
+69 Farm Hl.
+64 F. Post 33
+56 Farm Hl.
+50 F. Cor. 33
+41 C.F. 33.

Cultivated Field



Cultivated field.

+52 P.P. 19

F. 33

+75 -18"-Stump 23

+58 T.P. 21

+46 -30"-T-32

F. 33

+99 P.P. 20

+16 F. Cor. 33

Woods

+38 T.P. 28

+12 -20"-T-28

F. 33

+92 -18"-T-29

+76 -18"-T-29

+75 -18"-T-29

+20 -14"-T-24

+15 T.P. 20

+13 C.F. 33

+28 F. Cor. 33

+05 Farm Hl.

Woods

+44 P.P. 21

F. 33

F. 33

+97 F. Cor. 33

+98 P.P. 13

+90 F. Cor. 33

+05 P.P. 14

148

147

146

145

144

143

142

154

153

152

151

150

149

148

+35 C.F. 33
+27 T.P. 34
+22 T.P. 20

F. 33



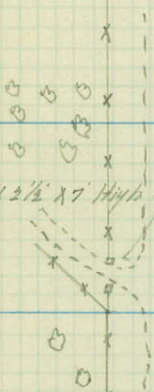
Pasture.

+24 P.P. 17

+92 T.P. 22

2 Stone Pillars 2 1/2 x 2 1/2 x 7 High

+275 F. Cor. 33
+20 P.P. Ext
+13 F. Cor. 33
+27 C.F. 61
+00 C.F. 34



+25 Pri. Road
+12 F. Cor. 23
+07 Mail Box 15

+75 P.P. 17

+64 T.P. 22

Cultivated Field.

+16 F. Cor. 23

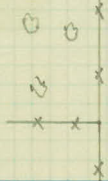
+97 Mail Box 13

+35 P.P. 17

+35 T.P. 23

+30 C.F. 34

F. 34

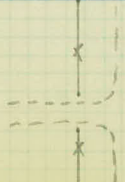


+88 P.P. 18

+48 F. Cor. 34

+37 Farm Rd.
+31 F. Cor. 34

+09 T.P. 24



160

159

158

157

156

155

154

F. 33

+69 T. P. 18'

F. 33

+34 T. P. 18'

F. 33

+13 T. P. 19'

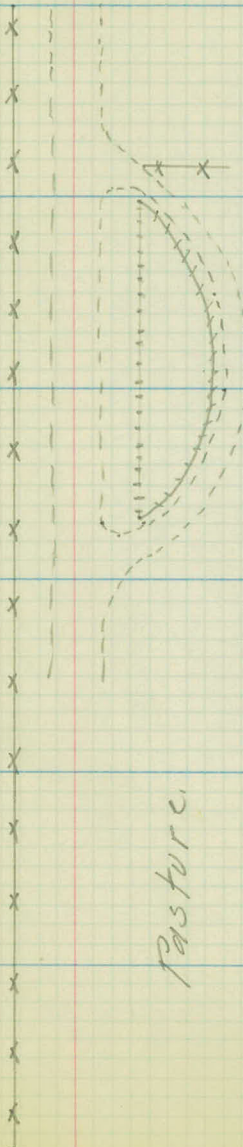
+81 T. P. 19'

F. 33

+54 T. P. 19'

Cultivated field

Pasture



+95-8"-T-27

+96-10"-T-27

+59-6"-T-27

+43-6"-T-27

+30-4"-T-36

+17 C. F. 38

+98. End Hedge 33

+94-10"-T-20

+95-4"-T-28

+63-4"-T-28

+48-4"-T-28

+35 Mail Box 16

+34-4"-T-28

+21 Iron Post 21

+03-4"-T-28

+33 Hedge 33'

+94-6"-T-35

+99-6"-T-27

+65-6"-T-27

+48-8"-T-27

+30-8"-T-27

+15 P. P. 19'

+96-10"-T-27

+70 P. P. 18'

164

165

164

163

162

161

160

F.33
+93 T.P. 18

F.38



+150 F.C. 1.40

F.33

+66 T.P. 18

+83 P.P. 22
+61-20"-T-39

Cultivated field

scrub oaks

+40 T.P. 18

+39 P.P. 21

F.33



+15 T.P. 18

Cultivated field

+92 P.P. 20

F.33

+96 T.P. 18

+42 P.P. 20

+11-10"-T-27

172

171

170

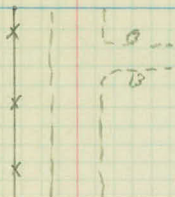
169

168

167

166

F. 32



+82-10" T-32
+75 Farm Ent.
+65-10" T-31

F. 32

+94 T.P. 18

x

+69 P.P. 25

x

+31-18" T-30

x

Cultivated field.

+68 T.P. 18

x

+80 F. Cor. 27

x

+29 P.P. 23

F. 33

x

F. 29

x

+42 T.P. 18

x

Bo99Y
pasture.

F. 33

y

F. 32

y

+84 P.P. 23

+17 T.P. 18

x

F. 33

F. 33

y

+34 P.P. 23

y

x

178

177

176

175

174

173

172

F. 33

X

X

F. 33

F. 33

X

X

F. 33

+89 T.P. 19

X

X

School Grounds

+63 P.P. 23
+34 F. Cor. 33
+32 School Ent.
+30 F. Cor. 33

X

X

+59 F. Cor. 33
+54 School Ent.
+49 F. Cor. 33
+28 P.P. 24

F. 33

X

X

+74 T.P. 19

X

X

Cultivated field

F. 32

X

O

+53 T.P. 19

X

O

F. 33

X

O

+91 P.P. 24

+70-6" T-29

X

O

Cultivated field

+17 T.P. 18

X

O

F. 32

X

O

+62 P.P. 24

+15 T.P. 18

X

O

+16 P.P. 24
+10 School Sign 20

X

O

X

O

X

O

X

O

|

184

183

182

181

180

179

178

6
6
6

+38 P.P. 25'

+68 School Sign 18'
+66 T.P. 21

6
6
6
6

6
6
6
6

Cultivated Field.

Cultivated field.

+64 T.P. 21

+76 P.P. 25

6

6
6
6
6
6
6

+42 T.P. 21

+14 P.P. 25

6
6

6
6

+41 T.P. 20

+05 St. Paul Water Main
& Conc. Main.
About 5' Below Elev.

+90 P.P. 33

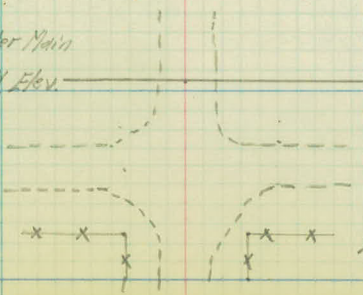
+84 I. Road Sign 25
+81 P.P. 23

+58⁴ Co. N.Y. I.

+25 F. Cor. 33

+07 T.P. 20

+26 F. Cor. 33



190

189

188

187

186

185

184

F. 30

x
x
x
x
x
x
x

+94-8"-Stamp 27

+61-30"-Stamp 24

+11 T.P. 21

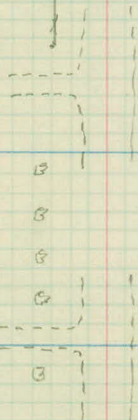
F. 30

+48 P.P. 25

+89 T.P. 21

+55 F. Cor. 30

+36 Farm Ent.



Cultivated field.

+80 P.P. 25

+70 T.P. 21

G
G
G
G
G
G
G

+07 Mail Box 19

+79 Guy Pole 30

+04 Farm Ent.

+67 T.P. 21

+08 P.P. 24

O
G

+12 T.P. 21

196

195

194

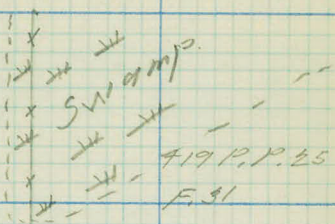
193

192

191

190

+52 T.P. 22



+23 T.P. 22

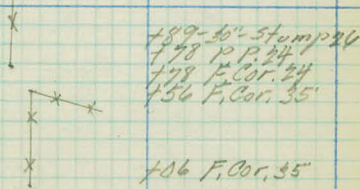
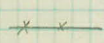
Hay Meadow

F. 31
 +94-6" T-28'
 +65-8" T-28'
 +51 P.P. 24

+92 T.P. 22

F. 30

+80 F. Cor. 32
 +75 Farm Kit
 +72 F. Cor. 31
 +62 T.P. 21



F. 30

+34 T.P. 21

+46-10" Stamp 26
 +36-10" " 30
 +27-10" " 25
 +07-8" " 30
 +16 P.P. 25

502

201

200

199

198

197

194

F. 25

+67 T.P. 20
35 F. Cor. 25
+28 Farm Ent.
+21 F. Cor. 24
F. 23

+45 T.P. 21

F. 25

+21 T.P. 21

F. 24

+97 T.P. 22

F. 25

+74 T.P. 22

+02 F. Cor. 27

F. 33

+96 P.P. 25

F. 33

+31 P.P. 24

F. 32

F. 31

+61 P.P. 25

F. 31

F. 31

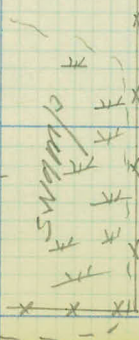
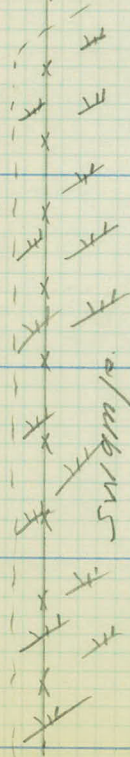
+99 P.P. 25

Pasture.

Swamp

Woods

Swamp



208

207

206

205

204

203

202

F. 29.

+89 T.P. 18.

F. 29.

+66 T.P. 19.
+53 Farm Ent.
+41 F. Cor. 29.
+32 Farm Ent.
+24 F. Cor. 29.

F. 29

+42 T.P. 19

+98 C.F. 26

+15 T.P. 19

F. 26

F. 26

+90 T.P. 20

Cultivated
field

Pasture



SW 1/4

F. 32

+22 P.P. 26

F. 30

+08 F. Cor. 33
+02 Farm Ent.

+95 F. Cor. 32

+57 P.P. 26

+98 C.F. 32

F. 31

+92 P.P. 26

F. 32

214

213

212

211

210

209.

208

F. 30

F. 32

+82 P.P. 26

X X
X X
X X
X X

+90 T.P. 16
+86 F. Cor. 30
+78 Farm Exit
+69 F. Cor. 30
+67 S.W. Drain 25
12" X 40' C.M.
Good Cond.

+95 Nail Box 15

Cultivated field.

F. 30

+18 P.P. 26

F. 32

+63 T.P. 16

X X
X X
X X
X X
X X

Pasture.

F. 31

F. 32

+36 T.P. 17

X X

+25 C.F. 31

+44 P.P. 26

F. 30

X X X

F. 32

Pasture

+12 T.P. 17

X X
X X
X X

+99 C.F. 31

+93 Cross Drain
Double 18" X 34" Vit.
Extend 19' L. & 15' R.
Good Cond.
+50 C.F. 82

+87 C.F. 32
+87 P.P. 27

SWAMP

220

219

218

217

216

215

214

F. 30.

8	0	x	13	0
	0		13	0
8	0	x	0	0

+02 T.P. 17

F. 30

x

x

x

+38 Farm Ent.

+78 P.P. 26

+15 O.F. 31

+07 F. Cor. 24

+00 Farm Ent.

+93 F. Cor. 23

+79 T.P. 16



+28 Farm Ent.

+05 F. Cor. 37

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

x

+60 F. 29

+14 P.P. 26

F. 30.

F. 25

+56 T.P. 14

F. 26

Cultivated field.

Pasture.

F. 30

+32 T.P. 14

F. 28

+47 P.P. 24

F. 32

+10 T.P. 15

x

x

x

x

x

x

226

225

224

223

222

221

220

+14 T.P. 19

+91 T.P. 19

+80 Farm Ent.
+72 F. Cor. 31
+72 T.P. 18

F. 31

+49 T.P. 18

F. 31
+71 F. Cor. 31
+76 Farm Ent.
+71 F. Cor. 31

+28 T.P. 28

Cultivated field

Timber

Row of Cottonwood
Trees 32' L.

Row of Cottonwood
Trees 30' L.

Cultivated field

+76 P.P. 21

+58 T.P. 22

+12 P.P. 26

+68 Mail Box 22
+53 Farm Ent.

+32 P.P. 26

232

231

230

229

228

227

226

F. 24.

+32 Cross Drain 16⁵
+14 T.P. 19
+07 Iron Sign Post 23

+71 P.P. 19.

+05 Cross Drain
24" X 67' V.I.T.
Cand. Fair.
Extends 32' L. & 35' R.

+97 F. Cor. 25.

+75 Pri. Ent.

+75 Cross Drain 17⁵

+49 Wooden Sign
Post 23

F. 79

+96 T.P. 19'

+87 P.P. 19

+73 T.P. 19'

Cultivated Field.

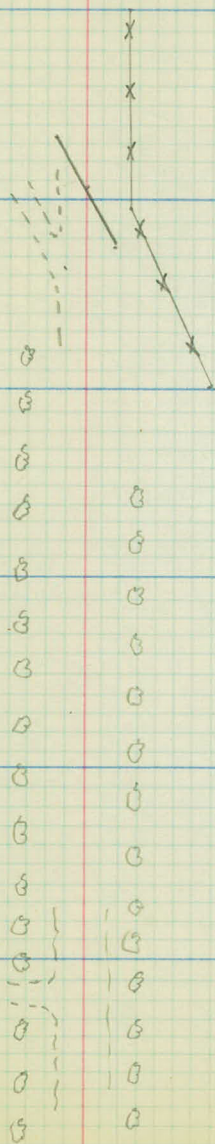
+53 T.P. 19

+83 Ferra Ent.

+33 T.P. 19

+04 P.P. 19

+14 P.P. 21



237

236

235

234

233

232

+66 N. Co. Line

+18 T.P. 21

+04 T.P. 19

+86 Cross Drain
12" x 38' vit
Extends 18' L & 20' R.
Good Cond.

+65 T.P. 19

+31 T.P. 18

Farm Street

Cultivated field.

Cultivated field.

← Drains

+86 P.P. 16
+82 G.V. Pole 19
+81 G. Co. Rd. Sign
+54 T.P. 38
+40 - 8" - T-22
+40 F. Car. 22
+59 Iron Nl. Sign 18
+26 - 8" - T-19
+15 - 6" - T-19
+00 - 8" - T-22

F 21
+04 Nail Box 19'
+92 Nail Box 19'
+91 Nail Box 17'

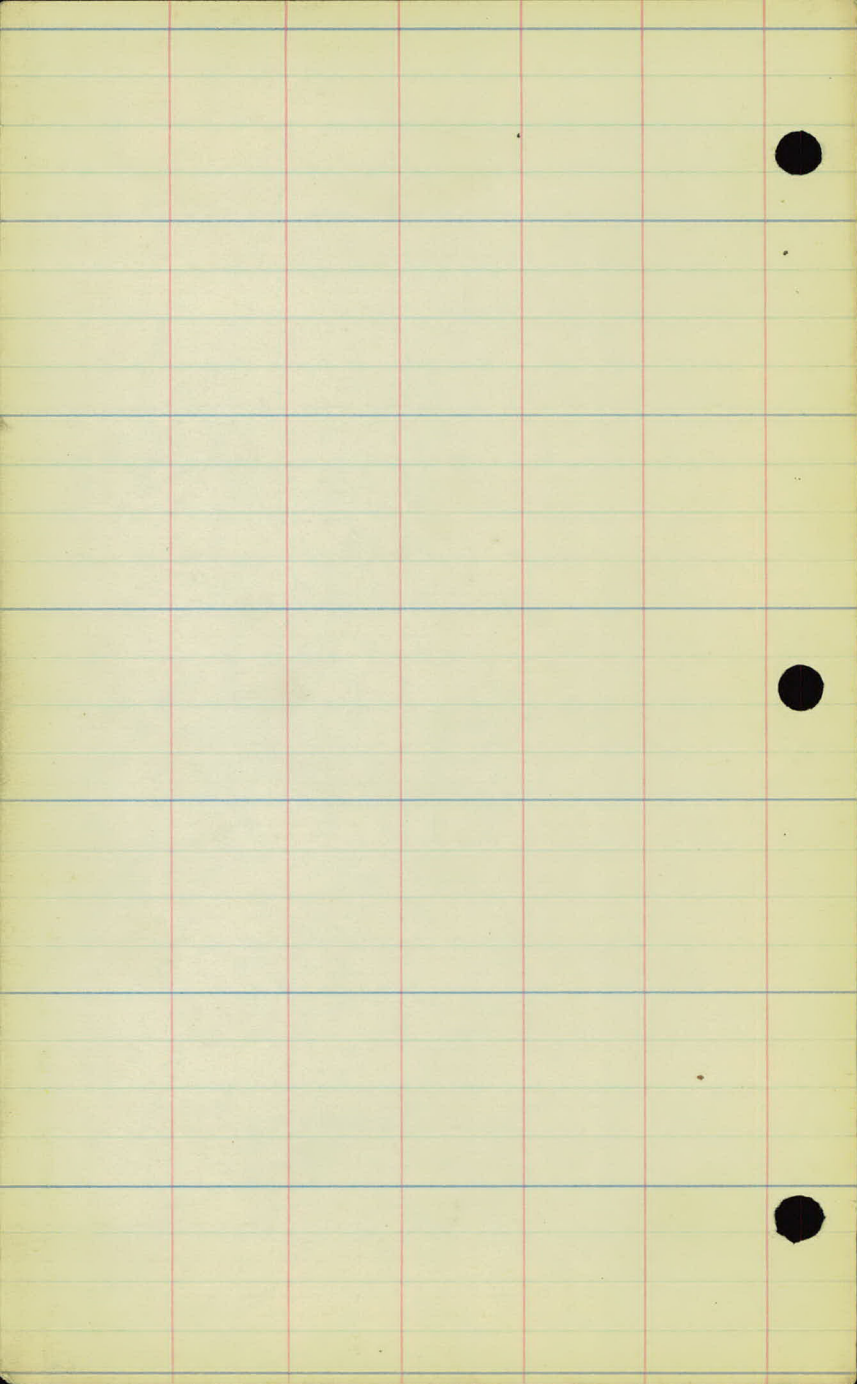
+37 P.P. 17

F 22

F 21

+54 P.P. 18

F 22



Hodgson Road,

13 & 1

LATITUDE & DEPARTURE CHART.

Proj. From Rice Str To No Co. Line

Sta.	Dist.	Deflection		Course	Latitude		Departure		Totals	
		L.	R.		+ N	- S	+ E	- W	Latitude	Departure
0+10 ⁶⁵					289.33			2.69		
	289.35			N00°38'E	289.33			3.20		
3+00		43°58'							289.33	+2.69
	1535.24			N43°26'W	1114.85			105.579		
18+06 ¹²		25°41'							1404.18	-1052.80
	2679.27			N17°45'W	2551.74			816.80		
44+76 ⁴⁵		0°21'							3955.92	1869.60
	4119.0			N17°24'W	3930.51			1231.75		
85+95 ¹²		4°24'							7886.43	3101.35
	1426.69			N21°48'W	1324.67			529.83		
100+22°		19°26'							9211.10	3631.18
	2414.40			N41°14'W	1815.70			1591.40		
124+32 ⁵		41°14'							11026.80	5222.58
125+25.93 ⁰										
121+31.23	894.20			N0°00'E	894.20			0		
125+94 ²		0°21'							11921.00	5222.58
	2644.8			N0°21'E	2644.74			16.16		
152+39°		0°15'							14565.74	5206.42
	2619.4			N0°36'E	2619.27			27.43		
178+58 ⁴		0°25'							17185.01	5178.99
	2638.9			N0°11'E	2638.87			8.44		
204+97 ³		0°16'							19823.88	5170.55
	3169.1			N0°27'E	3169.0			24.88		
236+66 ⁴									22992.88	5145.67

Rd. No. A 13 & 1.1

Hodgson Road.

Center line levels and x
sections from Sta. 0+00 to
Sta. 2+66+00.

Sta.	+	H.I.	-	Rod	Elev.
B.M.	4.88	928.80		923.92	
0-100	On Pavement			9.32	919.48
0-50	"	"		7.98	21.42.
0+00	"	"		5.94	22.86.
0+10 ⁶⁵	"	"		5.64	23.14.
0+50	"	"		5.09	23.71.
1+00	"	"		4.90	23.90.
+41 ⁵	Edge of Pavement			4.94	23.84.
+62					23.6
+79				6.9	21.9.
+95				7.3	21.5.
2+00				7.3	21.5.
+06				7.3	21.5.
+41				1.2	27.6.
T.P.	8.99	932.40	5.39	923.41	27.5
3+00				1.1	31.2
+50				5.2	27.2.
4+00				5.4	27.0.
+50				6.4	26.0.

Spk. in 24" Dpt. Mt. Sta. 0-20.

Lt.

Pt.

4.8	4.5	7.1	7.2	5.7	5.75	5.75	5.7	7.8	7.7	5.3	5.4	
33	31	25	21	17	12	5.66	12	17	22	24	28	33

4.0	4.2	7.2	7.3	5.2	5.19	5.18	5.4	6.8	6.6	5.2	5.1	
33	31	25	20	14	11	5.09	13	18	23	27	29	33

3.1	3.2	7.3	7.2	5.1	4.75	4.94	5.1	6.5	6.5	4.8	
33	29	21	15	11	6.5	4.90	17.5	22	26	31	33

1.3	2.0	6.9	7.0	5.05	5.06	5.4	
33	21	13	4	5.4	4.5	2.8	3.3

1.1	1.6	6.7	6.9	5.3	5.11	5.19	
33	15	4	7.3	2	7	12.5	41

1.2	1.6	7.1	7.0	5.3	5.12	5.18	
33	13	3	7.3	4	9	15	4.5

0.0	7.2	7.0	5.2	5.27	5.32	
33	1.2	12	14	22	27.5	54.5

3.9	5.5	10.4	10.8	9.4	7.09	
33	1.1	2.9	31	40	44	33

4.4	4.8	5.0	6.0	
33	14	5.2	7.4	33

6.8	5.2	6.2	6.6	
33	17	5.4	7.8	33

5.1	5.5	7.0	7.3	
33	20	6.4	1.8	3.9

Sta.	+	H.I.	-	Rod.	Elev.
5+00		922.40 ✓		6.8	25.6
+50				7.0	25.4
6+00				7.6 ✓	24.8
T.P.	1.39	925.63 ✓	8.14	724.24	
7+00				3.1	922.5
8+00				4.1	21.5
9+00				5.0	20.6
10+00				5.9	19.7
11+00				7.4	18.2
+47				7.7	17.9
12+00				6.6 ✓	19.0
T.P.	1.92	921.98 ✓	5.77	719.84	
13+00				3.3	18.5
14+00				4.3	17.5
15+00				5.5	16.3

Lt.

Rt.

$$\begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 6.5 \\ 22 \end{array} \quad 6.8 \quad \begin{array}{r} 7.4 \\ 19 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 18 \end{array} \quad 7.0 \quad \begin{array}{r} 8.3 \\ 23 \end{array} \quad \begin{array}{r} 8.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 7.0 \\ 18 \end{array} \quad 7.4 \quad \begin{array}{r} 8.4 \\ 18 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array}$$

$$\begin{array}{r} 1.3 \\ 33 \end{array} \quad \begin{array}{r} 1.3 \\ 20 \end{array} \quad 3.1 \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 3.4 \\ 20 \end{array} \quad 4.1 \quad \begin{array}{r} 4.4 \\ 24 \end{array} \quad \begin{array}{r} 5.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.5 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 18 \end{array} \quad 5.0 \quad \begin{array}{r} 5.3 \\ 18 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 6.1 \\ 20 \end{array} \quad 5.9 \quad \begin{array}{r} 5.7 \\ 17 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 19 \end{array} \quad 7.4 \quad \begin{array}{r} 7.6 \\ 18 \end{array} \quad \begin{array}{r} 7.7 \\ 33 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 18 \end{array} \quad 7.7 \quad \begin{array}{r} 8.1 \\ 18 \end{array} \quad \begin{array}{r} 8.7 \\ 33 \end{array}$$

$$\begin{array}{r} 5.4 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ 19 \end{array} \quad 6.6 \quad \begin{array}{r} 7.8 \\ 18 \end{array} \quad \begin{array}{r} 8.6 \\ 33 \end{array}$$

$$\begin{array}{r} 2.1 \\ 33 \end{array} \quad \begin{array}{r} 2.6 \\ 18 \end{array} \quad 3.3 \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 2.9 \\ 33 \end{array} \quad \begin{array}{r} 3.1 \\ 19 \end{array} \quad 4.3 \quad \begin{array}{r} 5.2 \\ 19 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 3.8 \\ 33 \end{array} \quad \begin{array}{r} 4.7 \\ 17 \end{array} \quad 5.5 \quad \begin{array}{r} 6.6 \\ 17 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array}$$

Sta.	T	H.I.	-	Red.	Flex.
		921.78			
+50				5.1	916.7.
16 +00				4.2	17.6.
B.M.	1.19	921.06	1.91	919.87	919.87
+30				3.9	17.2.
+35				6.4	14.7.
+50	Q. Road.			6.2	14.9.
+64				6.4	14.5.
+70				4.2	16.9.
17				3.6	17.5.
+50				3.4	17.7.
18				3.2	17.9.
+50				3.0	18.1.
+77				3.0	18.1.
19.				3.4	15.7.
+50				4.4	16.5.

Lt.

Rt.

3.9	4.9		6.5	6.9
<u>33</u>	<u>18</u>	5.1	<u>22</u>	<u>33</u>

→ R. Rd.

3.9	4.0		4.2	5.1	6.4	6.9	7.7	8.0
<u>33</u>	<u>21</u>	4.2	<u>6</u>	<u>12</u>	<u>32</u>	<u>37</u>	<u>39</u>	<u>62</u>

Spk. in 18" Oak Lt. 5.9 16 + 36 → R. Rd.

2.3	3.4		6.5	6.7
<u>33</u>	<u>14</u>	3.9	<u>8</u>	<u>33</u>

→ R. Rd.

2.2	3.5		6.5	7.2
<u>33</u>	<u>11</u>	6.4	<u>18</u>	<u>33</u>

→ R. Rd.

5.5	5.7		4.1	4.8
<u>33</u>	<u>24</u>	6.6	<u>10</u>	<u>33</u>

→ R. Rd.

5.5	5.7	6.6		4.3	4.7
<u>33</u>	<u>31</u>	<u>8</u>	4.2	<u>17</u>	<u>33</u>

→ R. Rd.

5.4	6.4	6.1	3.0		4.4	5.4	5.3
<u>44</u>	<u>33</u>	<u>31</u>	<u>25</u>	3.6	<u>27</u>	<u>30</u>	<u>33</u>

→ R. Rd.

5.5	5.8	3.5		3.7	4.5
<u>42</u>	<u>30</u>	<u>24</u>	3.4	<u>15</u>	<u>33</u>

→ R. Rd.

5.3	5.8	2.7		5.8	4.0	4.6
<u>33</u>	<u>18</u>	<u>14</u>	3.2	<u>14</u>	<u>30</u>	<u>33</u>

→ R. Rd.

5.5	5.1	5.4	3.0		3.7	4.2	4.0
<u>33</u>	<u>21</u>	<u>17</u>	<u>4</u>	3.0	<u>28</u>	<u>30</u>	<u>33</u>

→ R. Rd.

1.2	1.2	5.5	5.0	5.4		3.5	4.2	4.1
<u>40</u>	<u>37</u>	<u>30</u>	<u>17</u>	<u>3</u>	3.0	<u>27</u>	<u>28</u>	<u>33</u>

→ R. Rd.

1.4	5.4	5.0		5.3	3.0	3.5	4.1	3.7
<u>33</u>	<u>25</u>	<u>13</u>	5.4	<u>1</u>	<u>4</u>	<u>26</u>	<u>27</u>	<u>33</u>

→ R. Rd.

1.8	2.1	5.0	4.6		4.9	3.1	3.4	4.0	4.0	3.3	3.6
<u>33</u>	<u>24</u>	<u>19</u>	<u>5</u>	4.4	<u>7</u>	<u>10</u>	<u>18</u>	<u>19</u>	<u>15</u>	<u>24</u>	<u>33</u>

Sta.	T	H.I.	-	Red.	Elev.
20		921.04		4.3	16.8.
+58				4.0	17.1.
+85				4.0	17.1.
21				3.9	17.2.
+20				3.7	17.4.
22				3.3	17.8.
T.P.	6.62	924.46	3.22	917.84	
+77				6.0	18.5.
23				6.0	18.5.
24				5.2	19.3.
25				4.6	19.9.
26				4.4	20.1.
B.M.	3.65	925.34	2.74	921.70	921.69
27				4.8	20.5.
+50				4.8	20.5.

Lt.

Rt.

$\frac{3.2}{33}$	$\frac{3.8}{16}$	$\frac{4.7}{14}$	$\frac{4.3}{2}$	4.3	$\frac{4.6}{15}$	$\frac{5.7}{19}$	$\frac{3.8}{33}$
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$\frac{4.7}{33}$	$\frac{3.8}{24}$	$\frac{3.8}{18}$	$\frac{4.3}{12}$	4.0	$\frac{4.5}{14}$	$\frac{4.0}{18}$	$\frac{4.7}{22}$	$\frac{5.0}{29}$	$\frac{4.3}{33}$
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$\frac{5.9}{33}$	$\frac{4.9}{21}$	$\frac{4.2}{15}$	$\frac{4.3}{12}$	4.0	$\frac{4.4}{15}$	$\frac{2.5}{21}$	$\frac{5.0}{28}$	$\frac{5.1}{33}$
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$\frac{5.9}{33}$	$\frac{5.0}{21}$	$\frac{4.1}{11}$	3.7	$\frac{4.6}{14}$	$\frac{3.5}{19}$	$\frac{5.2}{33}$
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$\frac{5.8}{33}$	$\frac{5.5}{20}$	$\frac{5.1}{14}$	$\frac{4.1}{12}$	3.7	$\frac{4.3}{12}$	$\frac{5.3}{16}$	$\frac{5.3}{33}$
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$\frac{4.1}{33}$	$\frac{4.5}{16}$	$\frac{3.7}{14}$	3.3	$\frac{3.5}{12}$	$\frac{4.2}{23}$	$\frac{4.4}{33}$
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$\frac{5.4}{33}$	$\frac{5.3}{28}$	$\frac{4.2}{22}$	$\frac{6.3}{12}$	6.0	$\frac{6.6}{12}$	$\frac{5.8}{14}$	$\frac{5.8}{33}$
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$\frac{5.2}{33}$	$\frac{4.8}{19}$	$\frac{6.0}{12}$	4.0	$\frac{6.4}{12}$	$\frac{5.4}{13}$	$\frac{5.3}{33}$
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$\frac{5.1}{33}$	$\frac{4.2}{18}$	$\frac{5.5}{15}$	$\frac{5.5}{12}$	5.2	$\frac{5.7}{11}$	$\frac{5.1}{14}$	$\frac{5.8}{33}$
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$\frac{4.5}{33}$	$\frac{4.3}{14}$	$\frac{5.0}{12}$	4.4	$\frac{5.1}{12}$	$\frac{3.1}{16}$	$\frac{2.6}{33}$
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$\frac{3.4}{33}$	$\frac{3.1}{22}$	$\frac{2.3}{14}$	$\frac{4.6}{12}$	4.4	$\frac{4.7}{12}$	$\frac{0.5}{19}$	$\frac{0.5}{33}$
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Sp. in 18" Dull. Lt. Sta. 26 + 50.

$\frac{4.7}{33}$	$\frac{3.8}{14}$	$\frac{5.1}{12}$	4.8	$\frac{5.1}{12}$	$\frac{3.7}{14}$	$\frac{4.2}{33}$
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$\frac{5.8}{33}$	$\frac{5.9}{24}$	$\frac{5.4}{15}$	$\frac{5.2}{12}$	4.8	$\frac{5.1}{12}$	$\frac{4.9}{14}$	$\frac{5.4}{33}$
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Sta.	+	M.I.	-	Pod.	Elev.
28		925.34 ✓		5.0	20.3. ✓
+42				5.0	20.3. ✓
29				4.9	20.4. ✓
30				4.3	21.0. ✓
+34				4.2	21.1. ✓
I.P.	6.07	927.25 ✓	4.16	921.18.	
31				6.0	21.3. ✓
+60				6.1	21.2. ✓
32				6.1	21.2. ✓
+10				6.1	21.2. ✓
+74				6.0	21.3. ✓
33				6.0	21.3. ✓
34				6.1	21.2. ✓
35				6.0	21.3. ✓

Lf.

Rf.

$\frac{6.2}{33}$	$\frac{4.6}{14}$	$\frac{5.2}{12}$	5.0	$\frac{5.2}{12}$	$\frac{5.1}{15}$	$\frac{5.6}{33}$
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$\frac{7.5}{33}$	$\frac{7.5}{22}$	$\frac{7.0}{16}$	$\frac{5.6}{12}$	5.0	$\frac{5.2}{12}$	$\frac{5.8}{14}$	$\frac{7.3}{33}$
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$\frac{8.0}{33}$	$\frac{6.8}{26}$	$\frac{5.1}{22}$	$\frac{4.6}{14}$	$\frac{5.2}{13}$	4.9	$\frac{5.2}{13}$	$\frac{4.3}{17}$	$\frac{5.9}{33}$
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$\frac{5.4}{33}$	$\frac{5.8}{26}$	$\frac{5.4}{14}$	$\frac{4.7}{12}$	4.3	$\frac{4.6}{13}$	$\frac{4.1}{14}$	$\frac{4.0}{33}$
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$\frac{5.9}{33}$	$\frac{3.8}{22}$	$\frac{4.1}{14}$	$\frac{4.6}{12}$	4.2	$\frac{4.4}{12}$	$\frac{4.9}{14}$	$\frac{4.8}{33}$
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$\frac{3.8}{33}$	$\frac{2.5}{27}$	$\frac{2.5}{18}$	$\frac{6.3}{12}$	6.0	$\frac{6.4}{12}$	$\frac{2.3}{20}$	$\frac{3.3}{33}$
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$\frac{1.8}{33}$	$\frac{0.9}{21}$	$\frac{6.3}{12}$	6.1	$\frac{6.5}{12}$	$\frac{2.5}{19}$	$\frac{3.4}{28}$	$\frac{3.4}{33}$
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$\frac{2.8}{33}$	$\frac{2.1}{21}$	$\frac{3.0}{14}$	$\frac{6.3}{12}$	6.1	$\frac{6.3}{12}$	$\frac{3.5}{18}$	$\frac{4.7}{25}$	$\frac{4.9}{33}$
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$\frac{3.0}{33}$	$\frac{3.0}{14}$	$\frac{6.0}{12}$	6.1	$\frac{6.3}{11}$	$\frac{3.8}{18}$	$\frac{5.2}{33}$
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$\frac{4.4}{33}$	$\frac{2.6}{21}$	$\frac{6.3}{12}$	6.0	$\frac{6.0}{10}$	$\frac{4.9}{14}$	$\frac{5.9}{24}$	$\frac{6.7}{33}$
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$\frac{3.6}{33}$	$\frac{1.4}{19}$	$\frac{6.4}{12}$	6.0	$\frac{6.2}{11}$	$\frac{5.3}{14}$	$\frac{6.1}{33}$
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$\frac{4.7}{33}$	$\frac{3.0}{22}$	$\frac{5.1}{14}$	$\frac{6.4}{10}$	6.1	$\frac{6.3}{12}$	$\frac{5.9}{14}$	$\frac{5.4}{22}$	$\frac{6.2}{33}$
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$\frac{5.9}{33}$	$\frac{6.0}{29}$	$\frac{4.6}{22}$	$\frac{6.3}{11}$	6.0	$\frac{6.2}{12}$	$\frac{5.8}{14}$	$\frac{6.0}{23}$	$\frac{6.4}{33}$
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Sta.	+	H. I.	-	Rod	Elev.
		921.25			
36				58	921.5
T.P.	4.88	926.34	5.79	921.46	
37				4.7	21.6.
+63				4.8	21.5.
38				4.8	21.5.
+50				5.0	21.3.
T.P.	5.10	926.51	4.93	921.41	
39				5.3	21.2.
+78				5.3	21.2.
+78	Cross Drain 12" X 34" C.M.				
40				5.3	21.2.
41				5.1	21.4.
42				4.9	21.6.
43				5.0	21.5.
44				4.6	21.9.
T.P.	7.10	929.63	3.98	922.53	
+67				7.4	22.2.

Lt.

Rt.

$\frac{4.4}{33}$ $\frac{3.0}{20}$ $\frac{3.8}{14}$ $\frac{6.1}{11}$ 58 $\frac{6.0}{12}$ $\frac{4.9}{18}$ $\frac{5.5}{24}$ $\frac{5.9}{33}$

$\frac{1.5}{33}$ $\frac{0.8}{21}$ $\frac{1.7}{15}$ $\frac{4.9}{10}$ 4.7 $\frac{5.1}{13}$ $\frac{2.6}{14}$ $\frac{3.6}{24}$ $\frac{4.3}{33}$

$\frac{3.2}{33}$ $\frac{3.2}{21}$ $\frac{5.0}{11}$ 4.8 $\frac{5.0}{12}$ $\frac{5.0}{13}$ $\frac{5.6}{33}$

$\frac{4.4}{33}$ $\frac{4.5}{23}$ $\frac{5.3}{19}$ $\frac{5.1}{10}$ 4.8 $\frac{5.1}{13}$ $\frac{6.3}{33}$

$\frac{6.1}{33}$ $\frac{6.6}{15}$ $\frac{5.6}{13}$ $\frac{5.3}{11}$ 5.0 $\frac{5.2}{12}$ $\frac{6.1}{13}$ $\frac{6.7}{33}$

$\frac{8.4}{33}$ $\frac{8.1}{18}$ $\frac{5.5}{10}$ 5.3 $\frac{5.7}{12}$ $\frac{8.1}{17}$ $\frac{7.4}{23}$ $\frac{7.8}{33}$

$\frac{11.4}{33}$ $\frac{10.4}{21}$ $\frac{5.7}{11}$ 5.3 $\frac{5.7}{13}$ $\frac{8.8}{19}$ $\frac{8.4}{33}$
 Out/let = $\frac{10.3}{15}$ $\frac{9.7}{19}$ = Intake.

$\frac{11.8}{33}$ $\frac{9.8}{17}$ $\frac{5.7}{8}$ 5.3 $\frac{5.4}{12}$ $\frac{8.3}{28}$ $\frac{8.0}{33}$

$\frac{8.5}{33}$ $\frac{7.2}{18}$ $\frac{5.6}{11}$ 5.1 $\frac{5.5}{13}$ $\frac{5.2}{22}$ $\frac{5.9}{33}$

$\frac{7.6}{33}$ $\frac{5.2}{17}$ $\frac{5.4}{11}$ 4.9 $\frac{5.4}{13}$ $\frac{4.5}{33}$

$\frac{7.6}{33}$ $\frac{5.0}{16}$ $\frac{5.5}{12}$ 5.0 $\frac{5.5}{12}$ $\frac{6.2}{19}$ $\frac{5.5}{33}$

$\frac{8.6}{33}$ $\frac{4.3}{22}$ $\frac{4.3}{17}$ $\frac{5.0}{12}$ 4.4 $\frac{5.2}{13}$ $\frac{4.7}{19}$ $\frac{5.2}{33}$

Nail in T.P. Rt. 574 49100

$\frac{7.5}{33}$ $\frac{7.8}{14}$ 7.4 $\frac{7.8}{12}$ $\frac{6.9}{14}$ $\frac{6.3}{33}$

Sta.	T	H.I.	-	Rod	Elev.
		929.63			
45				7.4	22.2.
46				7.1	22.5.
47				6.7	22.9.
48				6.5	23.1.
T.P.	7.20	930.45 ✓	6.38	923.25 ✓	
49				4.0	23.5.
B.M.	5.63	930.43 ✓	5.63	924.82 ✓	924.80
50				6.8	23.6.
+90				6.5	23.9.
51				6.5	23.9.
+40				6.2	24.2.
52				6.2	24.2.
53				5.9	24.5.
54				5.8	24.6.
T.P.	4.68	929.24 ✓	5.85	924.58 ✓	
55				4.9	24.4.

Lt.

Rt.

$\frac{6.1}{33}$	$\frac{4.7}{26}$	$\frac{6.1}{15}$	$\frac{7.6}{13}$	7.4	$\frac{7.5}{12}$	$\frac{5.3}{15}$	$\frac{4.7}{28}$	$\frac{5.2}{33}$
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$\frac{2.9}{33}$	$\frac{2.5}{24}$	$\frac{7.2}{13}$	7.1	$\frac{7.1}{12}$	$\frac{1.4}{21}$	$\frac{1.4}{33}$
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$\frac{0.9}{33}$	$\frac{1.1}{23}$	$\frac{7.0}{12}$	4.7	$\frac{6.9}{12}$	$\frac{1.8}{21}$	$\frac{1.8}{33}$
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$\frac{1.5}{33}$	$\frac{0.8}{19}$	$\frac{6.7}{11}$	6.5	$\frac{6.7}{13}$	$\frac{2.3}{19}$	$\frac{2.3}{33}$
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$\frac{5.6}{33}$	$\frac{5.5}{15}$	$\frac{7.4}{11}$	7.0	$\frac{7.3}{13}$	$\frac{5.5}{14}$	$\frac{5.1}{33}$
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Sp. N. in 30" Oak H. Sta. 49+70.

$\frac{6.7}{33}$	$\frac{7.0}{25}$	$\frac{5.4}{17}$	$\frac{7.3}{11}$	6.8	$\frac{7.5}{14}$	$\frac{5.5}{19}$	$\frac{5.3}{33}$
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$\frac{5.2}{33}$	$\frac{4.8}{14}$	$\frac{6.9}{11}$	6.5	$\frac{6.6}{14}$	$\frac{4.3}{18}$	$\frac{3.4}{28}$	$\frac{3.5}{33}$
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$\frac{4.8}{33}$	$\frac{5.1}{17}$	$\frac{6.8}{11}$	6.5	$\frac{6.6}{13}$	$\frac{3.7}{14}$	$\frac{0.9}{25}$	$\frac{3.3}{31}$	$\frac{3.5}{33}$
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$\frac{6.4}{33}$	$\frac{6.3}{12}$	6.2	$\frac{6.3}{13}$	$\frac{5.8}{33}$
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$\frac{6.7}{33}$	$\frac{6.6}{11}$	6.2	$\frac{6.5}{12}$	$\frac{5.9}{15}$	$\frac{5.3}{33}$
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$\frac{5.8}{33}$	$\frac{5.5}{13}$	$\frac{6.4}{11}$	5.9	$\frac{6.2}{12}$	$\frac{4.4}{17}$	$\frac{4.4}{33}$
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$\frac{6.2}{33}$	$\frac{6.3}{12}$	5.8	$\frac{6.3}{12}$	$\frac{5.8}{13}$	$\frac{5.5}{33}$
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$\frac{4.7}{33}$	$\frac{4.5}{21}$	$\frac{5.6}{14}$	$\frac{5.3}{12}$	4.9	$\frac{5.4}{10}$	$\frac{5.0}{14}$	$\frac{4.6}{33}$
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Sta.	+	H. I. ✓ 929.24	-	Rod	Elev.
56				4.7	24.6.
57				4.6	24.7.
58				4.3	25.0.
59				4.2	25.1.
60				4.0 ✓	25.3.
T.P.	5.09	930.38 ✓	3.97	925.29	
61				4.9	25.5.
62				4.8	25.6.
63				4.8	25.6.
64				4.5	25.9.
65				4.1	26.3.
66				4.2 ✓	26.2.
T.P.	3.56	931.84 ✓	2.08	928.30	
67				5.4	26.5.
68				5.2	26.7.

Lt.

Rt.

$$\frac{5.4}{33} \quad \frac{5.1}{12} \quad 4.7 \quad \frac{5.2}{10} \quad \frac{4.3}{13} \quad \frac{4.1}{33}$$

$$\frac{6.5}{33} \quad \frac{6.0}{15} \quad \frac{5.1}{12} \quad 4.6 \quad \frac{4.9}{11} \quad \frac{4.8}{33}$$

$$\frac{5.5}{33} \quad \frac{4.6}{14} \quad \frac{4.8}{13} \quad 4.3 \quad \frac{4.6}{10} \quad \frac{4.5}{18} \quad \frac{3.5}{15} \quad \frac{4.2}{33}$$

$$\frac{4.0}{33} \quad \frac{4.1}{12} \quad \frac{4.6}{11} \quad 4.2 \quad \frac{4.6}{11} \quad \frac{3.6}{13} \quad \frac{3.0}{33}$$

$$\frac{2.0}{33} \quad \frac{2.2}{13} \quad \frac{4.4}{10} \quad 4.0 \quad \frac{4.4}{11} \quad \frac{2.8}{15} \quad \frac{2.5}{33}$$

$$\frac{3.5}{33} \quad \frac{4.1}{13} \quad \frac{5.2}{11} \quad 4.9 \quad \frac{5.2}{11} \quad \frac{5.3}{33}$$

$$\frac{5.2}{33} \quad \frac{5.1}{11} \quad 4.8 \quad \frac{5.1}{13} \quad \frac{5.3}{33}$$

$$\frac{5.7}{33} \quad \frac{5.2}{11} \quad 4.8 \quad \frac{5.4}{12} \quad \frac{4.6}{14} \quad \frac{5.1}{33}$$

$$\frac{5.3}{33} \quad \frac{5.1}{12} \quad 4.5 \quad \frac{4.8}{11} \quad \frac{4.0}{14} \quad \frac{3.1}{19} \quad \frac{3.6}{33}$$

$$\frac{3.3}{33} \quad \frac{3.3}{15} \quad \frac{4.2}{12} \quad 4.1 \quad \frac{4.5}{12} \quad \frac{3.7}{15} \quad \frac{3.8}{33}$$

$$\frac{3.7}{33} \quad \frac{3.6}{14} \quad \frac{4.6}{12} \quad 4.2 \quad \frac{4.5}{13} \quad \frac{3.4}{15} \quad \frac{3.5}{33}$$

$$\frac{4.2}{33} \quad \frac{4.2}{15} \quad \frac{5.7}{13} \quad 5.4 \quad \frac{5.7}{13} \quad \frac{4.3}{15} \quad \frac{4.4}{33}$$

$$\frac{3.1}{33} \quad \frac{2.9}{14} \quad \frac{5.3}{14} \quad 5.2 \quad \frac{5.7}{12} \quad \frac{3.0}{14} \quad \frac{2.9}{33}$$

Sta.	+	H. I.	-	Rod	Elev.
		931.84			
+72				5.0	926.9.
69				4.9	27.0.
+50				4.6	27.3.
70				4.3	27.6.
B.M.	5.82	932.88	4.72	27.14.	927.22
71				4.5	28.4.
B.M.	5.82	932.88			927.06
72				5.1	27.8.
56534				4.5	28.4.
					Co. Rd. "G"
73				4.6	28.3.
74				4.7	28.2.
75				4.8	28.1.
74				4.6	28.3.
T.P.	5.49	934.10.	4.27	928.61	
77				4.9	29.2.
78				4.7	29.4.

L.

R.

$\frac{3.5}{33}$	$\frac{3.4}{14}$	$\frac{5.0}{14}$	5.0	$\frac{5.3}{11}$	$\frac{3.1}{14}$	$\frac{3.1}{33}$
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$\frac{3.7}{33}$	$\frac{3.6}{15}$	$\frac{5.0}{13}$	4.9	$\frac{5.6}{17}$	$\frac{3.4}{21}$	$\frac{3.2}{33}$
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$\frac{4.0}{33}$	$\frac{3.8}{13}$	$\frac{4.9}{12}$	4.6	$\frac{5.0}{12}$	$\frac{6.0}{32}$	$\frac{3.8}{37}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{4.5}{33}$	$\frac{3.4}{15}$	$\frac{4.5}{12}$	4.3	$\frac{4.6}{11}$	$\frac{4.0}{13}$	$\frac{4.3}{22}$	$\frac{5.9}{18}$	$\frac{6.3}{37}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.3}{33}$	$\frac{4.8}{12}$	4.5	$\frac{4.9}{11}$	$\frac{5.0}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{5.0}{33}$	$\frac{4.9}{13}$	$\frac{5.3}{12}$	5.1	$\frac{5.3}{12}$	$\frac{5.8}{33}$
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$\frac{5.4}{50}$	$\frac{5.1}{29}$	4.5	$\frac{4.8}{22}$	$\frac{4.9}{33}$	$\frac{5.0}{50}$
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$\frac{4.8}{33}$	$\frac{5.0}{30}$	$\frac{5.1}{17}$	$\frac{5.5}{14}$	4.6	$\frac{5.3}{13}$	$\frac{5.3}{24}$	$\frac{5.1}{28}$	$\frac{5.1}{33}$
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$\frac{4.5}{33}$	$\frac{4.6}{18}$	$\frac{5.0}{11}$	4.7	$\frac{5.1}{14}$	$\frac{5.6}{20}$	$\frac{4.9}{24}$	$\frac{4.8}{33}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{6.8}{33}$	$\frac{6.6}{25}$	$\frac{5.5}{11}$	4.8	$\frac{5.4}{13}$	$\frac{6.1}{24}$	$\frac{6.4}{33}$
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$\frac{6.8}{33}$	$\frac{6.0}{24}$	$\frac{5.5}{18}$	$\frac{5.2}{12}$	4.4	$\frac{5.0}{13}$	$\frac{5.0}{19}$	$\frac{5.0}{33}$
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$\frac{6.6}{33}$	$\frac{6.3}{27}$	$\frac{5.6}{20}$	$\frac{5.6}{12}$	4.9	$\frac{5.5}{12}$	$\frac{5.2}{14}$	$\frac{6.2}{24}$	$\frac{5.4}{33}$
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$\frac{5.9}{33}$	$\frac{5.4}{22}$	$\frac{4.9}{14}$	$\frac{5.1}{11}$	4.7	$\frac{5.1}{12}$	$\frac{5.6}{21}$	$\frac{5.1}{25}$	$\frac{4.6}{33}$
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Sta.	T	H.I.	-	Rod	Elev.
		934.10			
79				4.5	29.6
80				4.4	29.5
81				4.8	29.3
82				5.1	29.0
T.P.	3.02	931.07	4.05	928.05	
83				3.3	27.8
84				3.9	27.2
85				4.3	26.8
86				5.4	25.7
+46				5.9	25.2
B.M.	4.07	931.08	4.07	927.00	927.01
87				6.4	24.7
88				7.3	23.8
T.P.	5.24	928.78	7.52	923.54	
89				5.2	23.6
90				4.8	24.0

14.

RT.

$\frac{5.8}{33}$ $\frac{5.7}{28}$ $\frac{4.5}{14}$ $\frac{4.8}{10}$ 4.5 $\frac{4.9}{12}$ $\frac{4.1}{22}$ $\frac{4.2}{33}$

$\frac{5.6}{33}$ $\frac{5.4}{24}$ $\frac{4.8}{13}$ 4.4 $\frac{4.8}{12}$ $\frac{5.0}{24}$ $\frac{4.8}{33}$

$\frac{5.9}{33}$ $\frac{4.5}{17}$ $\frac{5.1}{12}$ 4.8 $\frac{4.9}{12}$ $\frac{4.2}{19}$ $\frac{4.4}{33}$

$\frac{6.3}{33}$ $\frac{5.4}{23}$ $\frac{5.2}{15}$ $\frac{5.8}{14}$ 5.1 $\frac{5.4}{13}$ $\frac{4.7}{19}$ $\frac{4.7}{33}$

$\frac{3.4}{33}$ $\frac{2.5}{18}$ $\frac{3.4}{14}$ 3.3 $\frac{3.3}{12}$ $\frac{2.5}{17}$ $\frac{3.0}{25}$ $\frac{2.9}{33}$

$\frac{3.0}{33}$ $\frac{3.3}{30}$ $\frac{4.0}{28}$ $\frac{4.0}{20}$ $\frac{4.5}{14}$ 3.9 $\frac{4.2}{12}$ $\frac{3.5}{18}$ $\frac{4.3}{24}$ $\frac{4.8}{33}$

$\frac{2.2}{33}$ $\frac{3.0}{30}$ $\frac{3.8}{18}$ $\frac{4.2}{14}$ $\frac{4.7}{13}$ 4.3 $\frac{4.7}{14}$ $\frac{3.5}{19}$ $\frac{4.2}{31}$ $\frac{4.2}{33}$

$\frac{3.1}{33}$ $\frac{2.8}{29}$ $\frac{4.1}{22}$ $\frac{4.6}{12}$ 5.4 $\frac{6.1}{14}$ $\frac{4.3}{24}$ $\frac{4.3}{32}$ $\frac{4.3}{33}$

$\frac{4.5}{33}$ $\frac{4.6}{17}$ $\frac{6.2}{12}$ 5.9 $\frac{6.5}{15}$ $\frac{3.9}{24}$ $\frac{4.0}{33}$

Spk. in 10" Oak. 14. Spg. 86 + 88.

$\frac{7.2}{33}$ $\frac{6.2}{14}$ $\frac{7.0}{12}$ 6.4 $\frac{6.8}{14}$ $\frac{6.0}{21}$ $\frac{6.0}{33}$

$\frac{10.8}{33}$ $\frac{10.6}{29}$ $\frac{8.8}{16}$ $\frac{8.0}{10}$ 7.3 $\frac{7.4}{9}$ $\frac{9.1}{24}$ $\frac{8.9}{33}$

$\frac{7.2}{33}$ $\frac{6.1}{23}$ $\frac{6.1}{19}$ $\frac{6.0}{13}$ 5.2 $\frac{5.9}{13}$ $\frac{6.4}{24}$ $\frac{6.6}{33}$

$\frac{6.5}{33}$ $\frac{5.6}{25}$ $\frac{5.2}{15}$ $\frac{5.5}{14}$ 4.8 $\frac{5.3}{13}$ $\frac{5.4}{20}$ $\frac{5.3}{33}$

Sta.	T	H.I.	-	Proc.	Elev.
		928.78 ✓			
91				4.5	24.3
92				4.5	24.3
93				4.1	24.7
94				3.8	25.0
95				4.0	24.8
T.P.	4.90	929.96	3.72	925.06	
96				5.1	24.9
97				5.0	25.0
98				5.0	25.0
99				4.6	25.4
+50				4.8	25.2
100				4.4	25.6
B.M.	4.91	930.74 ✓	4.11	925.85	925.83
+50				5.5	25.2
+75				3.0	27.7

28.01 B
526.2 ✓

Lt.

Rt

$\frac{4.9}{33}$ $\frac{4.7}{24}$ $\frac{4.6}{18}$ $\frac{5.1}{13}$ 4.5 $\frac{5.1}{14}$ $\frac{5.3}{22}$ $\frac{5.8}{33}$

$\frac{3.7}{33}$ $\frac{3.5}{27}$ $\frac{3.2}{18}$ $\frac{4.8}{11}$ 4.5 $\frac{5.1}{13}$ $\frac{5.6}{21}$ $\frac{5.9}{33}$

$\frac{4.0}{33}$ $\frac{3.5}{30}$ $\frac{3.4}{18}$ $\frac{5.0}{14}$ 4.1 $\frac{4.7}{13}$ $\frac{4.3}{20}$ $\frac{4.6}{33}$

$\frac{3.2}{33}$ $\frac{2.7}{19}$ $\frac{4.4}{14}$ 3.8 $\frac{4.4}{15}$ $\frac{3.6}{20}$ $\frac{3.6}{33}$

$\frac{2.4}{33}$ $\frac{2.0}{30}$ $\frac{2.1}{20}$ $\frac{4.5}{13}$ 4.0 $\frac{4.5}{14}$ $\frac{3.7}{19}$ $\frac{3.6}{33}$

$\frac{4.3}{33}$ $\frac{4.0}{30}$ $\frac{4.4}{22}$ $\frac{3.9}{19}$ $\frac{5.8}{13}$ 5.1 $\frac{5.9}{14}$ $\frac{5.3}{19}$ $\frac{5.7}{33}$

$\frac{5.0}{33}$ $\frac{4.7}{29}$ $\frac{4.2}{18}$ $\frac{5.8}{13}$ 5.0 $\frac{5.4}{13}$ $\frac{5.1}{21}$ $\frac{5.5}{33}$

$\frac{5.2}{33}$ $\frac{4.8}{18}$ $\frac{5.6}{13}$ 5.0 $\frac{5.7}{14}$ $\frac{5.8}{24}$ $\frac{6.2}{33}$

$\frac{4.2}{33}$ $\frac{4.1}{24}$ $\frac{4.1}{14}$ $\frac{5.1}{9}$ 4.6 $\frac{4.7}{12}$ $\frac{5.1}{16}$ $\frac{5.4}{33}$

$\frac{4.0}{33}$ $\frac{3.9}{11}$ $\frac{5.0}{4}$ 4.8 $\frac{4.5}{15}$ $\frac{4.8}{22}$ $\frac{5.1}{33}$

$\frac{3.5}{33}$ $\frac{3.8}{28}$ $\frac{4.4}{22}$ $\frac{4.2}{11}$ $\frac{4.9}{8}$ 4.4 $\frac{4.6}{17}$ $\frac{5.3}{20}$ $\frac{5.3}{33}$

Spk. in 50" Oak 100' Lt. 579, 101+100.

$\frac{5.5}{33}$ $\frac{4.8}{23}$ $\frac{5.0}{8}$ 5.5 $\frac{4.9}{10}$ $\frac{4.5}{22}$ $\frac{4.6}{33}$

$\frac{4.9}{33}$ $\frac{5.5}{25}$ $\frac{4.5}{14}$ 3.0 $\frac{3.2}{6}$ $\frac{4.6}{14}$ $\frac{4.8}{33}$

950.74 ✓

101 25.8 ✓

+50 25.2 ✓

102 24.9 ✓

103 25.8 ✓

104 25.6 ✓

105 25.0 ✓

106 23.8 ✓

4.11 928.93 ✓ 5.92 924.82 ✓

107 22.3 ✓

108 21.8 ✓

109 22.8 ✓

110 24.9 ✓

+47 25.8 ✓

111 24.9 ✓

$\frac{4.2}{33}$ $\frac{3.7}{28}$ $\frac{3.7}{24}$ $\frac{4.5}{14}$ $\frac{4.6}{12}$ 4.9 $\frac{5.2}{17}$ $\frac{5.3}{33}$

$\frac{5.4}{33}$ $\frac{5.4}{12}$ 5.5 $\frac{5.5}{20}$ $\frac{5.8}{33}$

$\frac{5.0}{33}$ $\frac{5.3}{15}$ 5.8 $\frac{6.0}{16}$ $\frac{6.3}{33}$

$\frac{4.6}{33}$ $\frac{4.8}{15}$ 4.9 $\frac{5.3}{18}$ $\frac{5.5}{33}$

$\frac{4.7}{33}$ $\frac{4.9}{17}$ 5.1 $\frac{4.9}{19}$ $\frac{4.8}{33}$

$\frac{4.8}{33}$ $\frac{5.0}{22}$ 5.7 $\frac{6.1}{22}$ $\frac{6.1}{33}$

$\frac{6.4}{33}$ $\frac{6.4}{14}$ 6.9 $\frac{7.3}{19}$ $\frac{7.4}{33}$

$\frac{6.7}{33}$ $\frac{6.8}{15}$ 6.6 $\frac{6.8}{20}$ $\frac{6.7}{33}$

$\frac{6.9}{33}$ $\frac{7.0}{15}$ 7.1 $\frac{6.9}{17}$ $\frac{7.1}{33}$

$\frac{6.2}{33}$ $\frac{6.1}{15}$ 6.1 $\frac{5.9}{18}$ $\frac{5.8}{33}$

$\frac{4.3}{33}$ $\frac{4.1}{18}$ 4.0 $\frac{3.9}{17}$ $\frac{3.7}{33}$

$\frac{3.4}{33}$ $\frac{3.1}{14}$ 3.1 $\frac{3.4}{15}$ $\frac{4.1}{33}$

$\frac{3.4}{33}$ $\frac{3.7}{17}$ 4.0 $\frac{4.8}{18}$ $\frac{5.5}{33}$

✓
728.93

+50

23.4

112

23.2

113

1.59 725.99 ✓ 4.53 724.40 ✓

23.3

114

21.4

115

20.4

116

19.8

117

20.7

118

3.54 724.62 ✓ 4.91 721.08 ✓

20.3

119

20.0

120

19.7

121

19.5

122

19.9

123

20.1

$$\frac{4.8}{33} \quad \frac{5.2}{16} \quad 5.5 \quad \frac{5.8}{16} \quad \frac{6.1}{33}$$

$$\frac{4.9}{33} \quad \frac{5.4}{15} \quad 5.7 \quad \frac{6.0}{14} \quad \frac{6.4}{33}$$

$$\frac{4.3}{33} \quad \frac{5.0}{18} \quad 5.4 \quad \frac{6.1}{18} \quad \frac{6.5}{33}$$

$$\frac{3.5}{33} \quad \frac{4.1}{17} \quad 4.4 \quad \frac{4.7}{14} \quad \frac{4.8}{33}$$

$$\frac{5.3}{33} \quad \frac{5.2}{14} \quad 5.4 \quad \frac{5.7}{17} \quad \frac{5.6}{33}$$

$$\frac{6.1}{33} \quad \frac{6.1}{17} \quad 6.2 \quad \frac{6.3}{16} \quad \frac{6.2}{33}$$

$$\frac{6.0}{33} \quad \frac{5.4}{14} \quad 5.3 \quad \frac{5.6}{14} \quad \frac{5.7}{33}$$

$$\frac{5.7}{33} \quad \frac{5.7}{14} \quad 5.7 \quad \frac{5.5}{14} \quad \frac{5.6}{33}$$

$$\frac{4.8}{33} \quad \frac{4.6}{14} \quad 4.6 \quad \frac{4.3}{14} \quad \frac{4.1}{33}$$

$$\frac{4.8}{33} \quad \frac{4.7}{14} \quad 4.9 \quad \frac{4.5}{18} \quad \frac{4.4}{33}$$

$$\frac{5.1}{33} \quad \frac{5.1}{14} \quad 5.1 \quad \frac{4.7}{18} \quad \frac{4.5}{33}$$

$$\frac{5.0}{33} \quad \frac{4.8}{14} \quad 4.7 \quad \frac{4.5}{21} \quad \frac{4.3}{33}$$

$$\frac{5.1}{33} \quad \frac{4.8}{14} \quad 4.5 \quad \frac{4.1}{17} \quad \frac{3.7}{33}$$

924.62 ✓

124

19.3 ✓

125

19.9 ✓

5.54 926.45 ✓ 5.73 920.89 ✓

+50

20.9 ✓

126

21.9 ✓

+50

21.0 ✓

B.M.

2.83 926.68 ✓ 2.59 923.86 ✓ 924.85 ✓

127

21.3 ✓

128

21.9 ✓

$\frac{128 + 25 \frac{93}{25}}{121 + 31 \frac{25}{25}} =$

21.9 ✓

122

22.0 ✓

123

22.4 ✓

124

22.7 ✓

125

22.7 ✓

4.73 929.24 ✓ 4.17 922.51 ✓

124

22.6 ✓

To here

$\frac{5.2}{33}$	$\frac{5.2}{14}$	5.3	$\frac{5.3}{14}$	5.0
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→ 2 N1.

$\frac{5.7}{50}$	$\frac{3.9}{42}$	$\frac{4.4}{33}$	$\frac{4.9}{29}$	$\frac{5.0}{14}$	4.7	$\frac{4.3}{17}$	$\frac{3.9}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------

→ 2 N1.

$\frac{5.6}{34}$	$\frac{5.6}{29}$	$\frac{5.8}{15}$	5.6	$\frac{5.1}{15}$	$\frac{4.6}{33}$
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→ 2 N1.

$\frac{6.0}{36}$	$\frac{5.4}{25}$	$\frac{5.6}{11}$	$\frac{4.9}{5}$	4.4	$\frac{3.8}{18}$	$\frac{3.4}{28}$	$\frac{3.5}{33}$
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→ 2 N1.

$\frac{4.4}{33}$	$\frac{5.6}{25}$	$\frac{5.0}{14}$	5.5	$\frac{5.4}{4}$	$\frac{4.6}{7}$	$\frac{3.4}{19}$	$\frac{3.4}{33}$
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Spk in 24" Oak N1 579, 126 + 65.

$\frac{4.5}{33}$	$\frac{4.8}{25}$	$\frac{5.5}{20}$	$\frac{5.2}{9}$	5.4	$\frac{5.6}{5}$	$\frac{3.8}{18}$	$\frac{3.9}{33}$
------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------

$\frac{6.0}{33}$	$\frac{5.6}{13}$	4.8	$\frac{5.2}{12}$	$\frac{5.3}{33}$
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$\frac{5.8}{33}$	$\frac{5.5}{13}$	4.8	$\frac{5.1}{15}$	$\frac{5.4}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{5.6}{33}$	$\frac{5.4}{20}$	$\frac{5.1}{12}$	4.7	$\frac{5.1}{11}$	$\frac{4.9}{23}$	$\frac{4.9}{33}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

$\frac{5.6}{33}$	$\frac{5.5}{28}$	$\frac{4.9}{13}$	4.3	$\frac{4.6}{12}$	$\frac{3.8}{20}$	$\frac{4.4}{24}$	$\frac{4.1}{27}$	$\frac{4.0}{33}$
------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{5.3}{33}$	$\frac{4.8}{23}$	$\frac{5.0}{15}$	4.0	$\frac{4.5}{11}$	$\frac{3.8}{21}$	$\frac{4.2}{33}$
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$\frac{4.9}{33}$	$\frac{4.8}{24}$	$\frac{5.0}{14}$	4.0	$\frac{4.4}{13}$	$\frac{3.5}{22}$	$\frac{3.2}{33}$
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$\frac{8.1}{33}$	$\frac{8.2}{24}$	$\frac{7.1}{11}$	6.4	$\frac{7.1}{12}$	$\frac{8.0}{21}$	$\frac{7.8}{33}$
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729.24 ✓

127

22.9 ✓

128

23.4 ✓

129

24.1 ✓

130

24.7 ✓
~~25.7~~

131

25.0 ✓

132

25.6 ✓

133

5.34 731.18 ✓ 3.40 725.84 ✓

25.8 ✓

134

25.9 ✓

135

26.4 ✓

136

26.6 ✓

137

26.4 ✓

138

26.5 ✓

139

B.M.

5.57 731.63 ✓ 5.10 726.08 726.06 ✓

26.3 ✓

$$\frac{7.5}{33} \quad \frac{6.8}{21} \quad \frac{7.6}{18} \quad \frac{6.7}{11} \quad 6.3 \quad \frac{6.7}{9} \quad \frac{8.1}{20} \quad \frac{8.1}{33}$$

$$\frac{7.4}{33} \quad \frac{6.7}{24} \quad \frac{6.2}{11} \quad 5.8 \quad \frac{6.6}{15} \quad \frac{7.5}{18} \quad \frac{7.5}{33}$$

$$\frac{4.4}{33} \quad \frac{3.9}{22} \quad \frac{5.4}{18} \quad \frac{5.6}{12} \quad 5.1 \quad \frac{5.8}{12} \quad \frac{5.8}{15} \quad \frac{5.4}{33}$$

$$\frac{4.3}{33} \quad \frac{4.4}{27} \quad \frac{4.7}{12} \quad 4.5 \quad \frac{5.3}{12} \quad \frac{6.1}{24} \quad \frac{6.2}{33}$$

$$\frac{4.6}{33} \quad \frac{4.4}{20} \quad \frac{4.7}{12} \quad 4.2 \quad \frac{4.6}{10} \quad \frac{3.6}{19} \quad \frac{3.7}{33}$$

$$\frac{2.9}{33} \quad \frac{3.1}{22} \quad \frac{4.3}{13} \quad 3.4 \quad \frac{4.0}{11} \quad \frac{3.5}{17} \quad \frac{3.9}{33}$$

$$\frac{2.1}{33} \quad \frac{2.8}{24} \quad \frac{4.2}{12} \quad 3.4 \quad \frac{4.0}{12} \quad \frac{3.2}{20} \quad \frac{3.8}{33}$$

$$\frac{5.6}{33} \quad \frac{5.9}{19} \quad \frac{5.6}{10} \quad 5.3 \quad \frac{6.0}{13} \quad \frac{6.5}{19} \quad \frac{6.6}{22} \quad \frac{6.3}{24} \quad \frac{6.5}{33}$$

$$\frac{5.7}{33} \quad \frac{5.9}{21} \quad \frac{5.1}{14} \quad \frac{5.4}{11} \quad 4.8 \quad \frac{5.9}{12} \quad \frac{5.7}{21} \quad \frac{4.8}{29} \quad \frac{4.8}{33}$$

$$\frac{4.2}{33} \quad \frac{4.6}{17} \quad \frac{5.5}{13} \quad 4.6 \quad \frac{5.2}{13} \quad \frac{5.5}{33}$$

$$\frac{4.9}{33} \quad \frac{5.3}{14} \quad 4.8 \quad \frac{5.3}{13} \quad \frac{6.0}{19} \quad \frac{6.0}{33}$$

$$\frac{5.5}{33} \quad \frac{5.1}{17} \quad \frac{5.4}{14} \quad 4.7 \quad \frac{5.4}{12} \quad \frac{5.7}{24} \quad \frac{5.9}{33}$$

$$\frac{6.1}{33} \quad \frac{6.0}{24} \quad \frac{5.4}{13} \quad 4.9 \quad \frac{5.6}{13} \quad \frac{6.8}{25} \quad \frac{6.4}{27} \quad \frac{6.3}{33}$$

931.63

140

26.4 ✓

141

26.9 ✓

142

27.2 ✓

143

26.9 ✓

144

27.4 ✓

145

27.5 ✓

3.39 930.93 ✓

4.09

927.54 ✓

146

27.6 ✓

147

27.6 ✓

148

25.4 ✓

149

23.5 ✓

150

21.1 ✓

1.34 922.24 ✓

10.01

920.92 ✓

151

19.1 ✓

152

16.6 ✓

B.M.

0.29 916.63 ✓

5.94

916.32 ✓

916.37 ✓

$$\frac{5.7}{33} \quad \frac{5.8}{19} \quad \frac{5.6}{11} \quad 5.2 \quad \frac{5.8}{12} \quad \frac{6.7}{25} \quad \frac{6.7}{33}$$

$$\frac{5.5}{33} \quad \frac{5.4}{14} \quad \frac{5.4}{12} \quad 4.7 \quad \frac{5.3}{11} \quad \frac{5.7}{22} \quad \frac{5.4}{33}$$

$$\frac{4.2}{33} \quad \frac{4.2}{18} \quad \frac{5.2}{16} \quad \frac{5.0}{13} \quad 4.4 \quad \frac{4.9}{11} \quad \frac{5.2}{24} \quad \frac{4.9}{33}$$

$$\frac{4.1}{33} \quad \frac{4.3}{19} \quad \frac{5.1}{13} \quad 4.7 \quad \frac{5.2}{12} \quad \frac{5.4}{23} \quad \frac{5.1}{33}$$

$$\frac{5.4}{33} \quad \frac{4.9}{13} \quad 4.2 \quad \frac{4.6}{11} \quad \frac{4.8}{23} \quad \frac{4.5}{33}$$

$$\frac{6.2}{33} \quad \frac{6.1}{14} \quad \frac{5.3}{21} \quad \frac{4.4}{13} \quad 4.1 \quad \frac{4.6}{11} \quad \frac{3.9}{17} \quad \frac{3.4}{33}$$

$$\frac{5.1}{33} \quad \frac{3.8}{18} \quad \frac{4.0}{14} \quad 3.3 \quad \frac{3.7}{11} \quad \frac{3.8}{13} \quad \frac{2.6}{19} \quad \frac{2.7}{33}$$

$$\frac{4.6}{33} \quad \frac{3.5}{20} \quad \frac{3.8}{14} \quad 3.3 \quad \frac{3.8}{9} \quad \frac{4.0}{12} \quad \frac{1.9}{21} \quad \frac{2.3}{33}$$

$$\frac{2.5}{33} \quad \frac{2.3}{22} \quad \frac{5.9}{14} \quad 5.5 \quad \frac{5.8}{11} \quad \frac{1.8}{24} \quad \frac{1.9}{33}$$

$$\frac{5.4}{33} \quad \frac{4.8}{22} \quad \frac{8.1}{14} \quad \frac{7.9}{13} \quad 7.4 \quad \frac{7.8}{11} \quad \frac{2.9}{27} \quad \frac{2.9}{33}$$

$$\frac{7.0}{33} \quad \frac{7.4}{29} \quad \frac{7.5}{18} \quad \frac{10.3}{16} \quad \frac{10.2}{12} \quad 9.8 \quad \frac{10.1}{11} \quad \frac{10.5}{13} \quad \frac{6.7}{24} \quad \frac{7.1}{33}$$

$$\frac{4.5}{33} \quad \frac{4.3}{22} \quad \frac{3.6}{10} \quad 3.2 \quad \frac{3.9}{13} \quad \frac{3.7}{29} \quad \frac{3.7}{33}$$

$$\frac{8.2}{33} \quad \frac{7.2}{29} \quad \frac{7.1}{19} \quad \frac{6.2}{14} \quad 5.7 \quad \frac{6.2}{13} \quad \frac{7.1}{17} \quad \frac{7.6}{33}$$

Sta.	T	H.I.	-	Red.	Elev.
		716.63			
+31				0.7	15.9
153				2.5	14.1
154				4.8	12.0
+77				5.2	11.4
155				5.3	11.3
156				5.8	10.8
157				6.5	10.1
T.P.	2.40	712.26	6.77	909.54	
158				2.7	09.7
159				3.5	08.8
160				4.3	08.0
161				5.0	07.3
162				5.5	06.8
163				5.3	07.0

Lt.

Rt.

$\frac{3.7}{33}$	$\frac{2.7}{28}$	$\frac{2.1}{14}$	$\frac{1.1}{12}$	0.7	$\frac{1.3}{13}$	$\frac{2.0}{33}$
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$\frac{5.9}{33}$	$\frac{6.7}{27}$	$\frac{6.6}{22}$	$\frac{2.9}{12}$	2.5	$\frac{3.0}{12}$	$\frac{5.7}{19}$	$\frac{6.0}{25}$	$\frac{6.0}{33}$
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$\frac{5.4}{33}$	$\frac{5.5}{29}$	$\frac{7.5}{23}$	$\frac{7.5}{18}$	$\frac{5.2}{12}$	4.6	$\frac{5.1}{12}$	$\frac{5.9}{16}$	$\frac{8.8}{22}$	$\frac{9.5}{33}$
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$\frac{4.3}{33}$	$\frac{4.9}{24}$	$\frac{6.5}{20}$	$\frac{6.5}{16}$	$\frac{5.5}{11}$	5.2	$\frac{5.7}{13}$	$\frac{7.6}{20}$	$\frac{8.5}{23}$	$\frac{8.5}{33}$
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$\frac{4.0}{33}$	$\frac{4.4}{25}$	$\frac{6.1}{18}$	$\frac{5.9}{11}$	5.3	$\frac{5.9}{12}$	$\frac{7.7}{21}$	$\frac{8.3}{26}$	$\frac{8.6}{33}$
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$\frac{4.8}{33}$	$\frac{4.8}{25}$	$\frac{5.2}{18}$	$\frac{6.3}{11}$	5.8	$\frac{6.2}{13}$	$\frac{6.5}{25}$	$\frac{6.6}{33}$
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$\frac{6.1}{33}$	$\frac{5.8}{24}$	$\frac{6.2}{18}$	$\frac{7.2}{14}$	$\frac{6.8}{12}$	6.5	$\frac{6.7}{12}$	$\frac{6.2}{14}$	$\frac{6.2}{33}$
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$\frac{8.3}{33}$	$\frac{1.0}{21}$	$\frac{3.3}{14}$	$\frac{3.2}{11}$	2.7	$\frac{3.1}{13}$	$\frac{0.3}{25}$	$\frac{0.0}{33}$
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$\frac{3.4}{33}$	$\frac{3.3}{18}$	$\frac{4.4}{14}$	$\frac{4.1}{11}$	3.5	$\frac{3.8}{11}$	$\frac{3.4}{18}$	$\frac{2.5}{23}$	$\frac{2.3}{33}$
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$\frac{6.1}{33}$	$\frac{5.9}{23}$	$\frac{6.4}{18}$	$\frac{5.6}{15}$	$\frac{4.8}{11}$	4.3	$\frac{4.8}{11}$	$\frac{5.2}{14}$	$\frac{5.3}{33}$
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$\frac{6.0}{33}$	$\frac{8.0}{21}$	$\frac{5.5}{12}$	5.0	$\frac{5.6}{11}$	$\frac{8.9}{20}$	$\frac{8.7}{33}$
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$\frac{7.2}{33}$	$\frac{10.1}{27}$	$\frac{9.5}{12}$	$\frac{6.2}{12}$	5.5	$\frac{6.0}{11}$	$\frac{9.4}{20}$	$\frac{10.1}{33}$
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$\frac{7.7}{33}$	$\frac{9.7}{27}$	$\frac{9.7}{21}$	$\frac{7.0}{14}$	$\frac{6.2}{11}$	5.3	$\frac{6.0}{12}$	$\frac{9.4}{22}$	$\frac{10.1}{33}$
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Sta.	+	H.I.	-	Red.	Elev.
164		912.26 ✓		5.1	07.2
	+50			4.9	07.4
13. N1	5.50	913.74 ✓	4.01	908.25 ✓	908.24
165				6.3	07.4
	+50			6.2	07.5
166				6.0	07.7
	+56			5.6	08.1
167				5.5	08.2
168				5.1	08.6
169				4.7	09.0
170				3.8	09.9
171				2.9	10.9
T.P.	8.15	920.04 ✓	1.85	911.89 ✓	
172				8.1	11.9
173				6.9	13.1

$\frac{7.5}{33}$	$\frac{8.0}{20}$	$\frac{5.7}{11}$	5.1	$\frac{5.8}{12}$	$\frac{8.5}{20}$	$\frac{7.3}{33}$
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$\frac{5.0}{33}$	$\frac{6.2}{26}$	$\frac{6.0}{13}$	$\frac{5.3}{11}$	4.9	$\frac{5.6}{13}$	$\frac{7.1}{20}$	$\frac{8.3}{25}$	$\frac{6.2}{37}$	$\frac{6.2}{40}$
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Spk. in 12" Oak. Rt. Sta. 164 + 60.

$\frac{4.3}{33}$	$\frac{4.8}{31}$	$\frac{7.1}{26}$	$\frac{7.4}{16}$	$\frac{6.8}{11}$	6.3	$\frac{7.0}{13}$	$\frac{9.1}{22}$	$\frac{9.1}{30}$	$\frac{6.9}{34}$	$\frac{4.0}{40}$
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$\frac{3.5}{33}$	$\frac{6.7}{22}$	$\frac{7.4}{14}$	$\frac{6.7}{11}$	6.2	$\frac{6.7}{13}$	$\frac{8.3}{22}$	$\frac{8.0}{28}$	$\frac{6.0}{32}$	$\frac{2.2}{40}$
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$\frac{5.0}{33}$	$\frac{5.1}{27}$	$\frac{6.8}{17}$	$\frac{6.5}{11}$	6.0	$\frac{6.6}{13}$	$\frac{8.0}{22}$	$\frac{7.6}{29}$	$\frac{3.6}{34}$
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$\frac{6.2}{33}$	$\frac{6.4}{19}$	$\frac{6.4}{11}$	5.6	$\frac{6.1}{13}$	$\frac{7.1}{20}$	$\frac{6.2}{33}$
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$\frac{4.9}{33}$	$\frac{5.6}{19}$	$\frac{6.5}{13}$	$\frac{5.9}{10}$	5.5	$\frac{6.2}{14}$	$\frac{7.4}{21}$	$\frac{7.6}{33}$
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$\frac{3.6}{33}$	$\frac{4.8}{26}$	$\frac{6.4}{22}$	$\frac{6.6}{14}$	$\frac{5.5}{9}$	5.1	$\frac{6.0}{14}$	$\frac{7.4}{24}$	$\frac{8.5}{27}$	$\frac{9.0}{33}$
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$\frac{3.2}{33}$	$\frac{5.0}{22}$	$\frac{6.0}{18}$	$\frac{5.9}{14}$	$\frac{5.0}{9}$	4.7	$\frac{5.4}{15}$	$\frac{6.2}{20}$	$\frac{10.3}{28}$	$\frac{10.8}{33}$
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$\frac{4.8}{33}$	$\frac{5.8}{26}$	$\frac{6.3}{18}$	$\frac{4.2}{10}$	3.8	$\frac{4.8}{13}$	$\frac{6.1}{19}$	$\frac{7.3}{25}$	$\frac{10.4}{33}$
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$\frac{3.4}{33}$	$\frac{3.9}{22}$	$\frac{3.6}{11}$	2.9	$\frac{3.5}{13}$	$\frac{5.0}{23}$	$\frac{5.6}{24}$	$\frac{6.2}{33}$
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$\frac{6.4}{33}$	$\frac{7.3}{19}$	$\frac{7.2}{14}$	$\frac{8.7}{11}$	8.1	$\frac{8.9}{15}$	$\frac{8.6}{18}$	$\frac{8.4}{24}$	$\frac{8.2}{33}$
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$\frac{3.3}{33}$	$\frac{3.3}{24}$	$\frac{7.4}{19}$	$\frac{7.4}{12}$	4.9	$\frac{7.7}{14}$	$\frac{7.2}{24}$	$\frac{3.1}{34}$
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Sta.	+	H.I.	-	Red.	Elev.
		920.04			
+50				6.5	13.5
174				6.1	13.9
175				6.7	13.3
T.P.	2.07	914.34 ✓	7.77	912.27 ✓	
176				2.0	12.3
177				3.0	11.3
178				3.9	10.4
B.M.	3.45	915.72 ✓	2.08	912.26 ✓	912.27
+58		Co. Road I		5.2	10.5
179				5.3	10.4
+42				5.4	10.3
180				5.4	10.3
181				4.9	10.8
182				6.2	09.5
183				7.6	08.1
T.P.	4.65	911.90 ✓	8.47	907.95 ✓	

0.7	1.3	7.1	7.0		7.1	6.7	1.0
$\frac{33}{33}$	$\frac{29}{29}$	$\frac{23}{23}$	$\frac{11}{11}$	6.5	$\frac{14}{14}$	$\frac{22}{22}$	$\frac{35}{35}$

2.9	3.7	7.1	6.8		6.7	6.9	2.8
$\frac{33}{33}$	$\frac{26}{26}$	$\frac{22}{22}$	$\frac{12}{12}$	6.1	$\frac{12}{12}$	$\frac{21}{21}$	$\frac{35}{35}$

6.2	6.9	7.7	8.0	7.4		7.4	7.5	6.3	6.4
$\frac{33}{33}$	$\frac{24}{24}$	$\frac{23}{23}$	$\frac{17}{17}$	$\frac{12}{12}$	6.7	$\frac{13}{13}$	$\frac{25}{25}$	$\frac{29}{29}$	$\frac{33}{33}$

2.8	3.5	3.5	2.6		2.7	3.6	3.6	2.9
$\frac{33}{33}$	$\frac{27}{27}$	$\frac{18}{18}$	$\frac{12}{12}$	2.0	$\frac{13}{13}$	$\frac{21}{21}$	$\frac{29}{29}$	$\frac{34}{34}$

6.1	6.1	3.6		3.3	4.8	4.8
$\frac{33}{33}$	$\frac{20}{20}$	$\frac{12}{12}$	3.0	$\frac{8}{8}$	$\frac{19}{19}$	$\frac{33}{33}$

6.9	6.5	4.7		4.5	5.0	4.4
$\frac{33}{33}$	$\frac{21}{21}$	$\frac{14}{14}$	3.9	$\frac{14}{14}$	$\frac{23}{23}$	$\frac{33}{33}$

Top of Conc. Step N.E. Cor. of School House.

5.8	5.5	5.2	5.6
$\frac{50}{50}$	$\frac{27}{27}$	$\frac{32}{32}$	$\frac{50}{50}$

6.2	5.9	5.6		5.5	5.8	5.4
$\frac{33}{33}$	$\frac{26}{26}$	$\frac{12}{12}$	5.3	$\frac{10}{10}$	$\frac{14}{14}$	$\frac{33}{33}$

5.6	4.5	5.2	5.7		5.6	5.6	4.4	3.1
$\frac{33}{33}$	$\frac{28}{28}$	$\frac{20}{20}$	$\frac{12}{12}$	5.4	$\frac{11}{11}$	$\frac{19}{19}$	$\frac{28}{28}$	$\frac{33}{33}$

4.8	4.7	5.9	6.5	5.6		5.8	5.7	4.5
$\frac{33}{33}$	$\frac{24}{24}$	$\frac{17}{17}$	$\frac{15}{15}$	$\frac{11}{11}$	5.4	$\frac{10}{10}$	$\frac{25}{25}$	$\frac{33}{33}$

5.3	5.6	6.1	6.1	5.3		5.0	5.4	4.0	4.8
$\frac{33}{33}$	$\frac{17}{17}$	$\frac{14}{14}$	$\frac{14}{14}$	$\frac{11}{11}$	4.7	$\frac{7}{7}$	$\frac{15}{15}$	$\frac{21}{21}$	$\frac{33}{33}$

6.2	5.9	7.4	7.4	6.6		6.6	7.3	6.6	5.3	5.5
$\frac{33}{33}$	$\frac{24}{24}$	$\frac{17}{17}$	$\frac{14}{14}$	$\frac{11}{11}$	6.2	$\frac{11}{11}$	$\frac{14}{14}$	$\frac{18}{18}$	$\frac{31}{31}$	$\frac{33}{33}$

7.7	7.5	9.6	8.8	7.9		8.0	8.7	9.6	9.4	8.7
$\frac{33}{33}$	$\frac{26}{26}$	$\frac{20}{20}$	$\frac{16}{16}$	$\frac{11}{11}$	7.4	$\frac{10}{10}$	$\frac{14}{14}$	$\frac{21}{21}$	$\frac{27}{27}$	$\frac{33}{33}$

Sta.	+	H.I.	-	Red.	Elev.
		911.90			
184				5.1	06.8
185				5.3	06.6
186				5.1	06.8
187				5.1	06.8
	+5.0			5.0	06.9
188				5.0	06.9
189				5.0	06.9
190				5.2	06.7
B.M.	1.05	907.90 ✓	5.05	906.85 ✓	
191				3.3	04.6
	+5.0			4.5	03.4
194				5.8	02.1
193				8.2	899.7
	1.86	899.05 ✓	10.71	897.19 ✓	
194				1.8	97.3

$\frac{7.3}{33}$ $\frac{7.2}{20}$ $\frac{6.8}{18}$ $\frac{5.3}{11}$ 5.1 $\frac{5.5}{7}$ $\frac{7.4}{16}$ $\frac{7.3}{19}$ $\frac{8.0}{33}$

$\frac{5.1}{33}$ $\frac{5.1}{28}$ $\frac{5.9}{23}$ $\frac{6.2}{20}$ $\frac{5.7}{11}$ 5.3 $\frac{5.7}{9}$ $\frac{6.7}{15}$ $\frac{7.6}{17}$ $\frac{7.6}{18}$ $\frac{7.3}{22}$ $\frac{7.3}{33}$

$\frac{6.5}{33}$ $\frac{6.4}{28}$ $\frac{5.4}{9}$ 5.1 $\frac{5.4}{11}$ $\frac{7.0}{19}$ $\frac{7.0}{33}$

$\frac{6.7}{33}$ $\frac{5.7}{25}$ $\frac{5.4}{11}$ 5.1 $\frac{5.3}{9}$ $\frac{6.0}{17}$ $\frac{7.1}{25}$ $\frac{7.4}{33}$

$\frac{4.3}{33}$ $\frac{4.7}{25}$ $\frac{5.2}{13}$ 5.0 $\frac{5.3}{9}$ $\frac{5.4}{13}$ $\frac{5.1}{14}$ $\frac{5.4}{28}$ $\frac{5.4}{33}$

$\frac{1.6}{33}$ $\frac{1.4}{30}$ $\frac{4.6}{22}$ $\frac{5.0}{17}$ $\frac{5.4}{10}$ 5.0 $\frac{5.2}{10}$ $\frac{5.7}{12}$ $\frac{5.7}{13}$ $\frac{5.1}{15}$ $\frac{4.4}{22}$ $\frac{4.4}{33}$

$\frac{1.6}{33}$ $\frac{1.2}{29}$ $\frac{4.1}{21}$ $\frac{5.3}{12}$ 5.0 $\frac{5.2}{8}$ $\frac{5.1}{12}$ $\frac{3.4}{18}$ $\frac{3.5}{33}$

$\frac{3.5}{33}$ $\frac{3.5}{30}$ $\frac{4.7}{24}$ $\frac{4.7}{22}$ $\frac{5.6}{16}$ $\frac{5.7}{11}$ 5.2 $\frac{5.5}{9}$ $\frac{6.0}{22}$ $\frac{6.4}{33}$

Nail in P.P. Rt. Sta. 190+20.

$\frac{3.6}{33}$ $\frac{3.7}{19}$ $\frac{3.7}{17}$ 3.3 $\frac{3.7}{10}$ $\frac{4.1}{13}$ $\frac{3.1}{18}$ $\frac{3.7}{24}$ $\frac{4.5}{33}$

$\frac{5.8}{33}$ $\frac{4.5}{27}$ $\frac{4.6}{24}$ $\frac{4.2}{17}$ $\frac{5.3}{14}$ $\frac{4.8}{8}$ 4.5 $\frac{4.6}{9}$ $\frac{4.8}{12}$ $\frac{3.9}{18}$ $\frac{4.0}{25}$ $\frac{4.5}{33}$

$\frac{7.0}{33}$ $\frac{6.0}{23}$ $\frac{6.4}{17}$ $\frac{6.1}{10}$ 5.8 $\frac{6.2}{9}$ $\frac{5.4}{21}$ $\frac{3.4}{27}$ $\frac{3.2}{33}$

$\frac{11.0}{33}$ $\frac{9.1}{18}$ $\frac{8.3}{10}$ 8.2 $\frac{8.5}{9}$ $\frac{8.5}{16}$ $\frac{8.4}{23}$ $\frac{5.1}{31}$ $\frac{5.0}{33}$

$\frac{7.3}{33}$ $\frac{6.8}{30}$ $\frac{5.3}{21}$ $\frac{3.8}{17}$ $\frac{2.5}{12}$ $\frac{2.1}{9}$ 1.8 $\frac{2.0}{9}$ $\frac{1.4}{21}$ $\frac{2.8}{24}$ $\frac{2.8}{27}$ $\frac{1.0}{31}$ $\frac{1.0}{33}$

Sta.	+	H. I.	-	Red.	Elev.
195		899.05		4.1	95.0
196				4.8	94.3
197				4.8	94.3
198				4.7	94.4
199				4.3	94.8
200				3.3	95.8
T.P.	5.03	900.57	✓ 3.57	895.48	✓
201				4.8	95.7
202				4.7	95.8
203				4.7	95.8
750				4.8	95.7
204				5.0	95.5
T.P.	3.59	897.97	✓ 4.13	894.58	✓
205				3.3	94.7
204				4.1	93.9

$\frac{88}{33}$ $\frac{86}{23}$ $\frac{53}{15}$ $\frac{44}{9}$ 4.1 $\frac{44}{10}$ $\frac{50}{14}$ $\frac{62}{19}$ $\frac{59}{28}$ $\frac{48}{31}$ $\frac{48}{33}$

$\frac{82}{33}$ $\frac{82}{25}$ $\frac{80}{21}$ $\frac{67}{17}$ $\frac{54}{11}$ 4.8 $\frac{51}{9}$ $\frac{57}{12}$ $\frac{71}{13}$ $\frac{76}{33}$

$\frac{85}{33}$ $\frac{82}{22}$ $\frac{66}{18}$ $\frac{53}{10}$ 4.8 $\frac{51}{9}$ $\frac{60}{14}$ $\frac{71}{17}$ $\frac{71}{33}$

$\frac{84}{33}$ $\frac{80}{22}$ $\frac{60}{17}$ $\frac{50}{8}$ 4.7 $\frac{51}{9}$ $\frac{59}{14}$ $\frac{72}{17}$ $\frac{72}{33}$

$\frac{82}{33}$ $\frac{80}{23}$ $\frac{53}{14}$ $\frac{47}{10}$ 4.3 $\frac{46}{9}$ $\frac{51}{16}$ $\frac{72}{24}$ $\frac{75}{33}$

$\frac{37}{33}$ $\frac{47}{24}$ $\frac{44}{14}$ $\frac{36}{10}$ 3.3 $\frac{37}{9}$ $\frac{41}{15}$ $\frac{65}{21}$ $\frac{68}{28}$ $\frac{61}{31}$ $\frac{61}{33}$

$\frac{18}{33}$ $\frac{36}{21}$ $\frac{55}{16}$ $\frac{50}{8}$ 4.8 $\frac{52}{14}$ $\frac{48}{17}$ $\frac{54}{22}$ $\frac{62}{24}$ $\frac{61}{28}$ $\frac{44}{33}$

$\frac{18}{33}$ $\frac{32}{25}$ $\frac{48}{19}$ $\frac{50}{7}$ 4.7 $\frac{52}{11}$ $\frac{47}{22}$ $\frac{24}{30}$ $\frac{24}{33}$

$\frac{31}{33}$ $\frac{41}{28}$ $\frac{45}{21}$ $\frac{52}{16}$ $\frac{51}{9}$ 4.7 $\frac{51}{11}$ $\frac{48}{22}$ $\frac{24}{29}$ $\frac{24}{33}$

$\frac{46}{33}$ $\frac{51}{27}$ $\frac{53}{19}$ $\frac{51}{10}$ 4.8 $\frac{51}{10}$ $\frac{43}{16}$ $\frac{42}{28}$ $\frac{42}{33}$

$\frac{80}{33}$ $\frac{85}{24}$ $\frac{83}{20}$ $\frac{59}{13}$ $\frac{52}{9}$ 5.0 $\frac{55}{19}$ $\frac{62}{15}$ $\frac{83}{20}$ $\frac{88}{24}$ $\frac{82}{33}$

$\frac{63}{33}$ $\frac{63}{28}$ $\frac{75}{24}$ $\frac{71}{21}$ $\frac{51}{14}$ $\frac{36}{9}$ 3.3 $\frac{36}{9}$ $\frac{46}{14}$ $\frac{61}{21}$ $\frac{63}{27}$ $\frac{49}{29}$ $\frac{49}{33}$

$\frac{64}{33}$ $\frac{64}{27}$ $\frac{79}{25}$ $\frac{68}{19}$ $\frac{55}{16}$ $\frac{44}{9}$ 4.1 $\frac{43}{9}$ $\frac{53}{17}$ $\frac{69}{27}$ $\frac{65}{26}$ $\frac{53}{29}$ $\frac{51}{33}$

Sta.	+	H.I.	-	Rod.	Elev.
		897.97			
207				5.1	92.9
208				5.7	92.3
	+	Cross Drain	24" X		
209				5.6	92.4
210				5.4	92.6
13. M.	8.57	901.78 ✓	4.75	893.22 ✓	893.21
211				7.7	94.1
212				6.4	95.4
213				5.5	96.3
214				4.3	97.5
215				2.6	99.2
T.P.	8.27	908.65 ✓	1.40	900.38 ✓	
216				8.1	900.6
217				6.7	02.0
218				5.5	03.2
+17				5.3	03.4

8.9	8.9	8.5	6.9	5.7		5.4	6.8	8.2	8.4
<u>33</u>	<u>29</u>	<u>22</u>	<u>14</u>	<u>10</u>	5.1	<u>10</u>	<u>17</u>	<u>23</u>	<u>33</u>

9.0	8.9	8.5	7.6	6.3		5.9	6.9	8.6	8.8
<u>33</u>	<u>29</u>	<u>21</u>	<u>14</u>	<u>11</u>	5.7	<u>8</u>	<u>13</u>	<u>21</u>	<u>33</u>
				<u>11.5</u>			<u>16.1</u>		

8.4	8.2	7.2	6.1		6.0	8.0	8.2	10.0	10.1	8.4	8.4
<u>33</u>	<u>21</u>	<u>14</u>	<u>10</u>	5.4	<u>9</u>	<u>18</u>	<u>23</u>	<u>26</u>	<u>28</u>	<u>30</u>	<u>33</u>

8.4	8.4	9.0	9.0	8.4	8.3	6.1	5.4		5.4	6.5	7.8	8.5	9.5	9.5	8.5	8.5
<u>33</u>	<u>30</u>	<u>29</u>	<u>28</u>	<u>26</u>	<u>21</u>	<u>16</u>	<u>10</u>	5.4	<u>9</u>	<u>13</u>	<u>19</u>	<u>24</u>	<u>26</u>	<u>27</u>	<u>29</u>	<u>33</u>

S/A. in T.P. 17.5 to 21.0 + 4.0.

7.2	10.1	10.5	8.5	7.9		8.1	9.4	10.2	12.7	12.6	9.7	9.7
<u>33</u>	<u>28</u>	<u>21</u>	<u>17</u>	<u>9</u>	7.7	<u>10</u>	<u>18</u>	<u>23</u>	<u>26</u>	<u>28</u>	<u>30</u>	<u>33</u>

7.5	9.0	10.2	10.0	7.4	6.6		7.0	8.8	12.4	12.5	9.6	9.6
<u>33</u>	<u>30</u>	<u>27</u>	<u>22</u>	<u>17</u>	<u>9</u>	6.4	<u>10</u>	<u>20</u>	<u>25</u>	<u>28</u>	<u>30</u>	<u>33</u>

7.0	6.6	8.4	8.3	6.6	5.7		5.8	7.2	12.3	12.2	8.7	8.7
<u>33</u>	<u>28</u>	<u>25</u>	<u>21</u>	<u>16</u>	<u>9</u>	5.5	<u>10</u>	<u>17</u>	<u>24</u>	<u>27</u>	<u>31</u>	<u>33</u>

8.0	8.3	9.4	9.3	5.0	4.5		4.4	5.6	10.0	10.0
<u>33</u>	<u>27</u>	<u>25</u>	<u>21</u>	<u>16</u>	<u>8</u>	4.3	<u>10</u>	<u>22</u>	<u>22</u>	<u>33</u>

4.4	4.4	6.5	6.6	3.4	2.9		2.8	3.3	6.5	6.7	6.8
<u>33</u>	<u>27</u>	<u>23</u>	<u>20</u>	<u>14</u>	<u>8</u>	2.6	<u>9</u>	<u>21</u>	<u>9</u>	<u>32</u>	<u>33</u>

6.8	6.4	7.7	8.6	8.4		8.5	8.7	7.7	7.2	7.2
<u>33</u>	<u>25</u>	<u>18</u>	<u>15</u>	<u>9</u>	8.1	<u>11</u>	<u>14</u>	<u>17</u>	<u>29</u>	<u>33</u>

4.7	4.2	5.1	6.9	7.0		7.0	6.6	4.8	4.1	4.1
<u>33</u>	<u>24</u>	<u>20</u>	<u>15</u>	<u>9</u>	6.7	<u>9</u>	<u>14</u>	<u>20</u>	<u>29</u>	<u>33</u>

4.0	4.0	5.6	5.8		5.9	5.7	3.4	2.3	2.6
<u>33</u>	<u>22</u>	<u>18</u>	<u>9</u>	5.5	<u>10</u>	<u>13</u>	<u>20</u>	<u>28</u>	<u>33</u>

1.7	1.7	3.8	5.3	5.5		5.5	5.0	4.5	2.3
<u>33</u>	<u>28</u>	<u>24</u>	<u>17</u>	<u>9</u>	5.3	<u>10</u>	<u>17</u>	<u>24</u>	<u>33</u>

Sta.	T	H. I.	-	Rod.	Elev.
		908.65			
219				4.8	03.9.
220				4.7	04.0.
221				4.7	04.0.
222				4.7	04.0.
P.M.	3.49	908.82 ✓	3.32	905.33 ✓	
223				4.8	04.0.
224				4.8	04.0.
225				4.8	04.0.
226				5.0	03.8.
227				4.9	03.9.
228				5.1	03.7. ✓
229				5.2	03.6.
230				5.2	03.6.
T.P.	4.43	907.98 ✓	5.27	903.55 ✓	
231				4.5	03.5.

#15 Cross Drain

$\frac{42}{28}$ $\frac{42}{28}$ $\frac{40}{19}$ $\frac{54}{14}$ $\frac{5.1}{9}$ 4.8 $\frac{5.1}{11}$ $\frac{4.7}{23}$ $\frac{3.7}{26}$ $\frac{3.8}{33}$

$\frac{6.0}{33}$ $\frac{6.0}{28}$ $\frac{5.5}{14}$ $\frac{4.9}{8}$ 4.7 $\frac{5.2}{10}$ $\frac{5.7}{21}$ $\frac{5.8}{33}$

$\frac{5.5}{33}$ $\frac{5.4}{14}$ $\frac{4.9}{9}$ 4.7 $\frac{5.1}{9}$ $\frac{5.7}{21}$ $\frac{5.5}{33}$

$\frac{4.7}{33}$ $\frac{4.7}{30}$ $\frac{5.1}{16}$ $\frac{4.9}{9}$ 4.7 $\frac{5.2}{9}$ $\frac{5.5}{18}$ $\frac{5.7}{28}$ $\frac{5.8}{33}$

Nail in T.P. 1. Sta. 222 + 75.

$\frac{4.1}{32}$ $\frac{4.5}{27}$ $\frac{5.1}{17}$ $\frac{5.1}{10}$ 4.8 $\frac{5.1}{9}$ $\frac{5.0}{15}$ $\frac{4.6}{24}$ $\frac{5.7}{30}$ $\frac{3.7}{33}$

$\frac{2.5}{33}$ $\frac{4.6}{32}$ $\frac{5.1}{9}$ 4.8 $\frac{5.7}{9}$ $\frac{5.1}{15}$ $\frac{3.8}{24}$ $\frac{2.3}{29}$ $\frac{2.2}{33}$

$\frac{3.3}{33}$ $\frac{4.6}{23}$ $\frac{4.9}{17}$ $\frac{5.5}{15}$ $\frac{5.1}{9}$ 4.8 $\frac{5.1}{8}$ $\frac{5.5}{12}$ $\frac{5.4}{15}$ $\frac{4.6}{20}$ $\frac{4.4}{33}$

$\frac{3.0}{33}$ $\frac{4.8}{23}$ $\frac{5.3}{9}$ 5.0 $\frac{5.2}{8}$ $\frac{5.2}{15}$ $\frac{4.4}{21}$ $\frac{4.0}{33}$

$\frac{4.9}{33}$ $\frac{5.4}{14}$ $\frac{5.3}{9}$ 4.9 $\frac{5.2}{9}$ $\frac{5.7}{17}$ $\frac{5.7}{33}$

$\frac{5.5}{33}$ $\frac{6.5}{20}$ $\frac{5.7}{10}$ 5.1 $\frac{5.3}{8}$ $\frac{6.1}{19}$ $\frac{7.4}{25}$ $\frac{7.8}{33}$

$\frac{4.8}{33}$ $\frac{5.8}{21}$ $\frac{5.5}{10}$ 5.2 $\frac{5.5}{9}$ $\frac{6.5}{15}$ $\frac{7.3}{24}$ $\frac{7.4}{33}$

$\frac{4.3}{33}$ $\frac{4.6}{28}$ $\frac{4.6}{18}$ $\frac{5.5}{15}$ $\frac{5.4}{10}$ 5.2 $\frac{5.4}{7}$ $\frac{5.7}{15}$ $\frac{5.7}{23}$ $\frac{6.7}{33}$ $\frac{11.9}{56}$

Bottom of pitch

$\frac{3.7}{33}$ $\frac{4.5}{18}$ $\frac{4.8}{10}$ 4.5 $\frac{4.7}{8}$ $\frac{4.9}{20}$ $\frac{5.7}{26}$ $\frac{5.8}{33}$
 $\frac{10.17}{32}$ $\frac{10.65}{35}$

Sta.	+	H. I.	-	Red.	Elev.
		907.98			
232				4.6	03.4.
233				4.9	03.1.
	+84	Cross Prain			
234				4.8	03.2.
235				4.5	03.8.
236				3.7	04.3.
	+50			3.3	04.7.
	+66 ⁴	No. Co. Line		3.2	04.8.
B.M.			2.17	905.81	✓ 905.84

Bottom of Pitch

$\frac{110}{50}$	$\frac{73}{33}$	$\frac{70}{25}$	$\frac{77}{21}$	$\frac{60}{16}$	$\frac{59}{10}$	4.6	$\frac{4.9}{9}$	$\frac{5.4}{14}$	$\frac{6.9}{24}$	$\frac{7.0}{33}$
------------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----	-----------------	------------------	------------------	------------------

$\frac{9.5}{33}$	$\frac{9.4}{25}$	$\frac{9.4}{22}$	$\frac{6.4}{16}$	$\frac{5.4}{10}$	4.9	$\frac{5.2}{8}$	$\frac{6.4}{14}$	$\frac{8.5}{24}$	$\frac{8.0}{33}$
------------------	------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------

		$\frac{12.2}{78}$					$\frac{12.1}{20}$		
$\frac{10.2}{33}$	$\frac{10.1}{22}$	$\frac{6.3}{16}$	$\frac{5.3}{10}$	4.8	$\frac{5.2}{9}$	$\frac{5.8}{15}$	$\frac{10.0}{23}$	$\frac{9.5}{33}$	

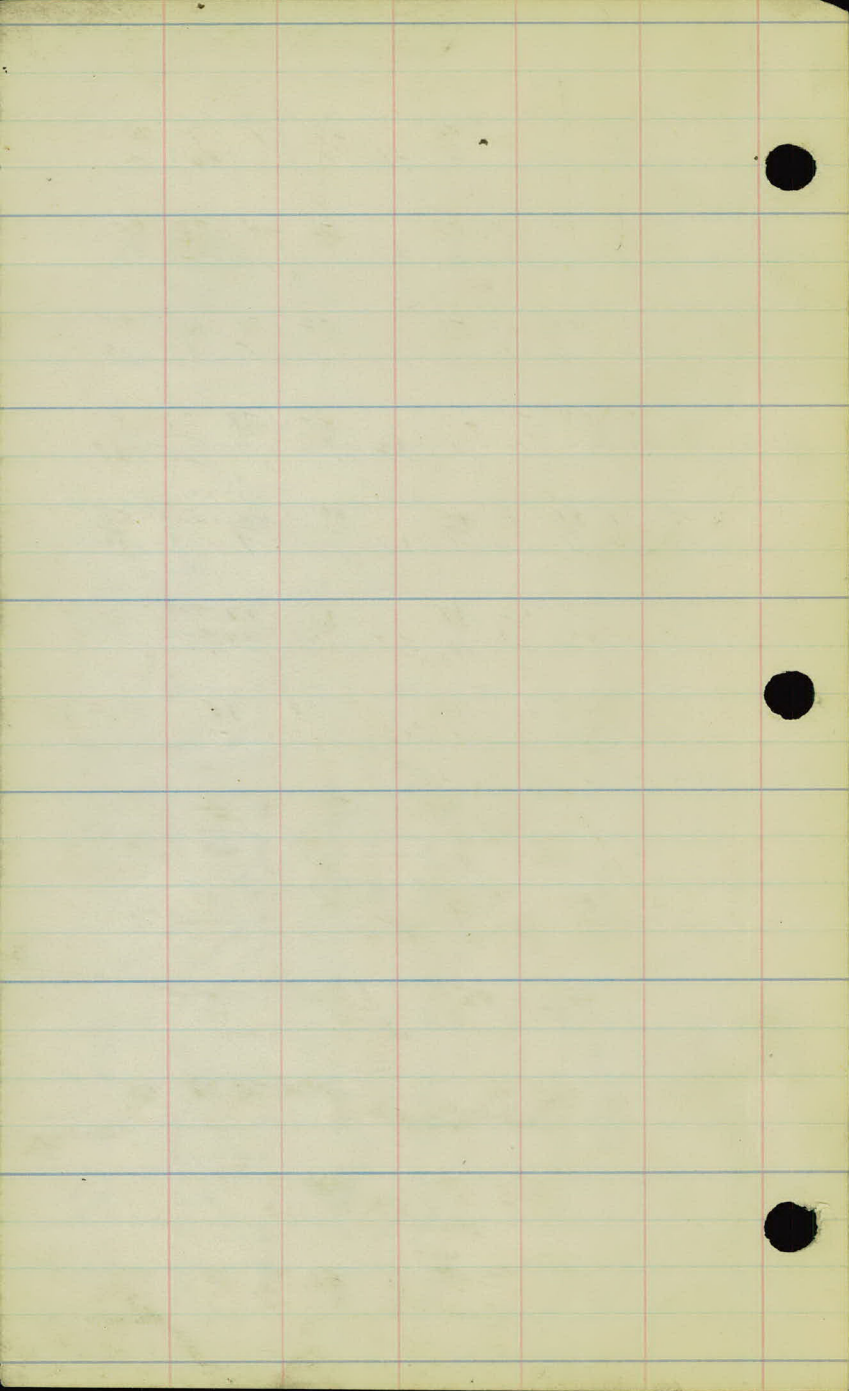
$\frac{8.8}{33}$	$\frac{8.7}{17}$	$\frac{5.5}{10}$	$\frac{4.7}{11}$	4.4	$\frac{4.4}{8}$	$\frac{5.9}{17}$	$\frac{8.7}{25}$	$\frac{8.8}{33}$
------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------

$\frac{4.2}{33}$	$\frac{3.1}{24}$	$\frac{3.1}{20}$	$\frac{4.0}{16}$	$\frac{4.0}{11}$	3.7	$\frac{3.8}{4}$	$\frac{4.0}{17}$	$\frac{5.0}{21}$	$\frac{5.0}{33}$
------------------	------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------

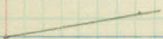
$\frac{3.1}{33}$	$\frac{3.2}{23}$	$\frac{3.9}{18}$	3.3	$\frac{3.8}{13}$	$\frac{3.9}{33}$
------------------	------------------	------------------	-----	------------------	------------------

$\frac{4.0}{50}$	$\frac{3.6}{33}$	3.2	$\frac{3.3}{33}$	$\frac{3.5}{50}$
------------------	------------------	-----	------------------	------------------

Sp. in T.P. 14. 54. 2. 36 + 20



Proj. # 28-01 "B"
Location of Buildings.



102

101

100

99

98

97

+17-2"-T-25 LT

+76-2"-T-22 K.

+98 P.P. 72

+63-2"-T-46

+54-24"-T-60

+50-3-2"-T-81

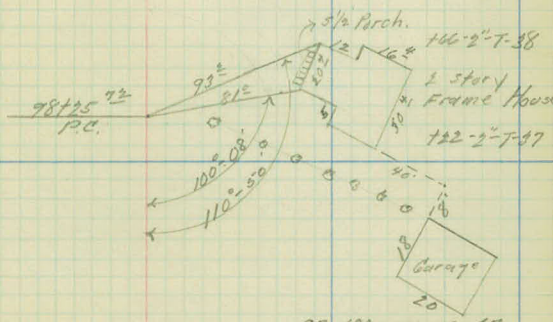
+30-4"-T-78

+19-2"-T-85

+10-24"-T-138

+09-2"-T-40

+82-4"-T-69



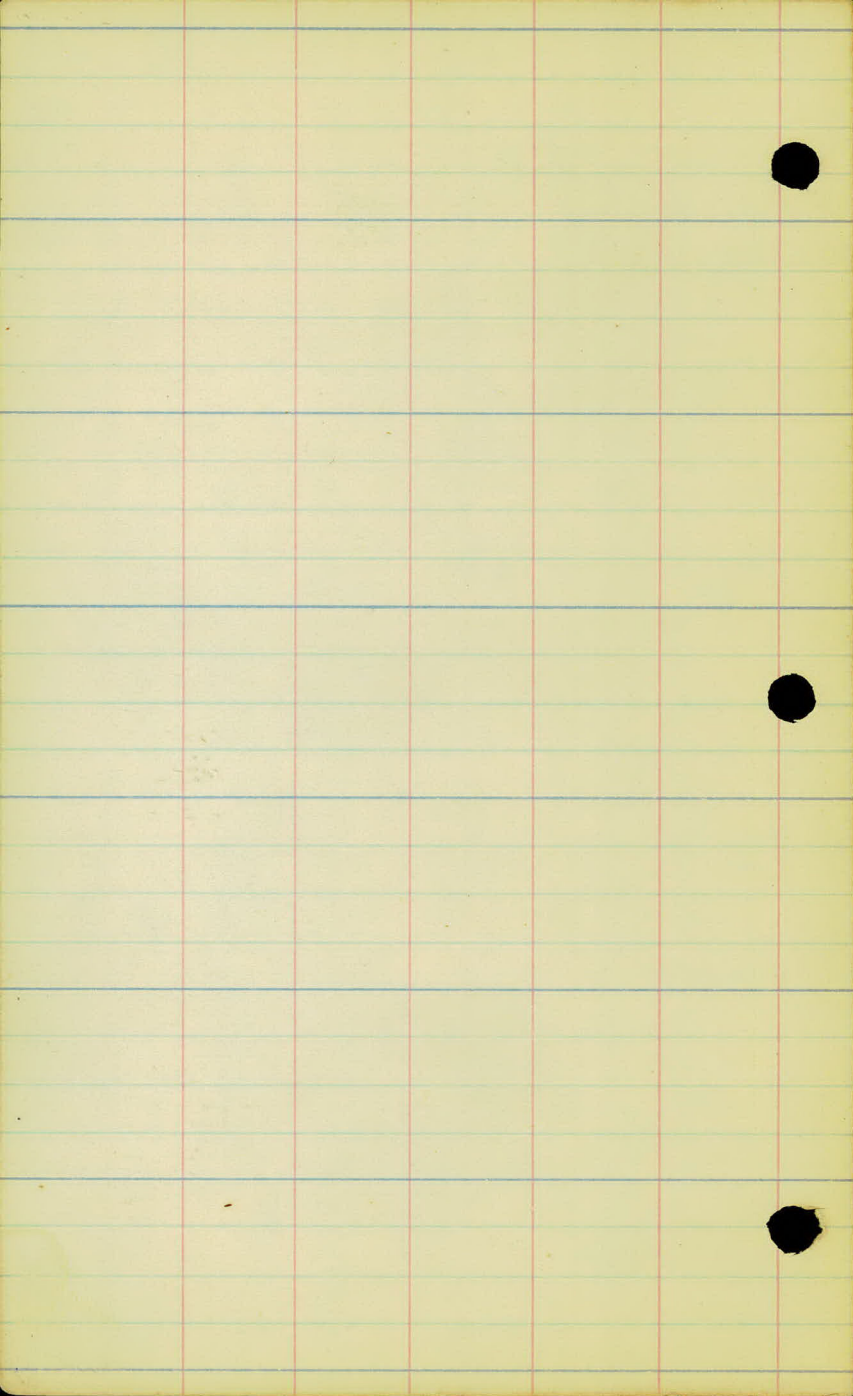
106-2"-T-38

2 story Frame House

+22-2"-T-37

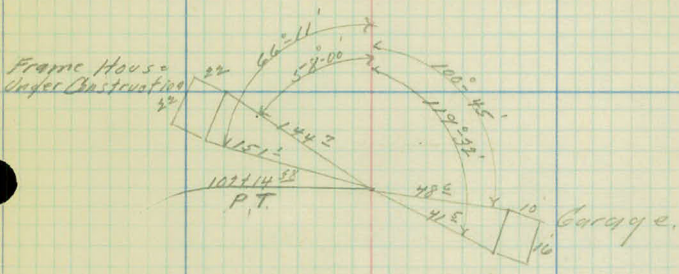
77 180-2"-T-37

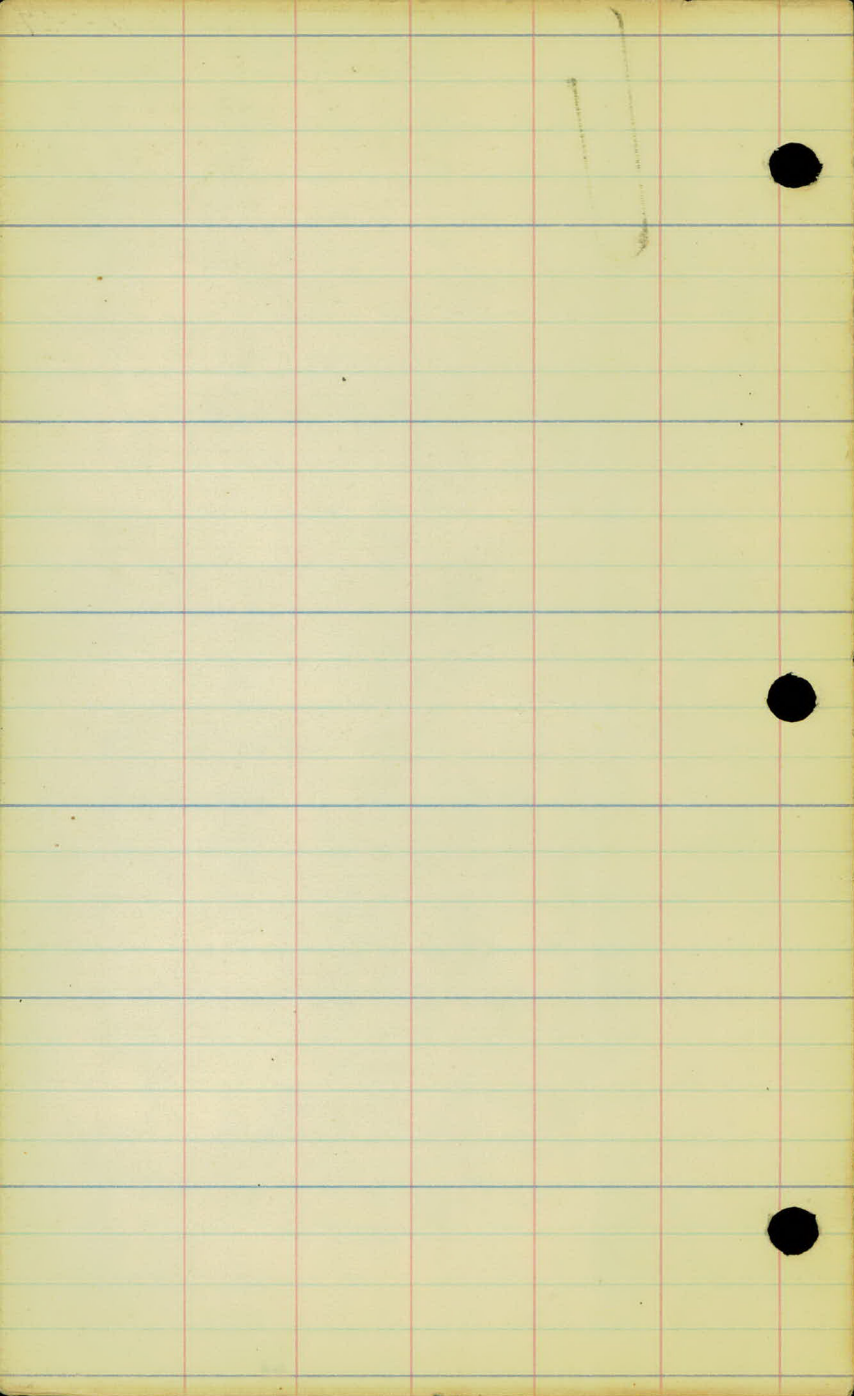
77 144-2"-T-37



10-8-27

1247325 . P.I.





Plans in hand inspection - 3-1-27

O. R. V. K.
W. S. M.
H. Purcell

- ✓ 1+00 to 2+00 - Cl. + Gr. 2 T.
- ✓ 8+00 - F.E. Rt + Lt. - P. 2-15" x 24' C.M.
- ✓ 16 to 21 - Cl. + Gr. 22 T.
- ✓ 22+00 - F.E. Lt. - P. 15" x 24' C.M.
- ✓ 22+00 to 27+00 Cl. + Gr. 18 T.
- ✓ 24+40 - F.E. Rt. + Lt. P. 2-15" x 24' C.M.
- ✓ 19+00 - No culv. req.
- ✓ 29 to 31 - Gr. 6 T.
- ✓ 32+54 - F.E. Rt. + Lt. - No culv. req.
- ✓ G.R. - O.K. 39 to 41
- ✓ 40 to 41 - Cl. 7 T.
- ✓ 41+22 - F.E. Rt. P. 15" x 24'
- ✓ " " Lt. No culv. req.
- ✓ 44+60 - F.E. Lt. - P. 15" x 24' C.M.
- ✓ 45 to 51+50 - Gr. 60 T.
- ✓ Snail Lake Blvd. P. 15" x 30' on Rt
- ✓ 52 to 54 - Gr. 20 T.
- ✓ 58+35 - F.E. Rt. - P. 15" x 24' C.M.
- ✓ 61 to 72+50 Cl. 110 T. - Gr. 153 T
- ✓ 61+60 - F.E. Lt. P. 15" x 24' C.M.
- ✓ 61+86 - " Rt. "
- ✓ 66+60 - " " "
- ✓ 69+00 - " " No culv. req.

- ✓ 73+00 - R. F.E. - No culv. req.
- ✓ 85 to 88 - Cl. 6 T. Gr. 26 T.
- ✓ 86+57 - F.E. - Lt. - P. 15'x24' C.M.
- ✓ 89+00 - No culv. req.
- ✓ 108+00 - " " "
- ✓ 126+38 - F.E. R. - P. 15'x24' C.M.
- ✓ 126+50 to 127+50 - Cl. 6 T. Gr. 10 T.
- ✓ 128+00 - F.E. Lt. P. 15'x24' C.M.
- ✓ EQUATION
121+50 " R. "
- ✓ 122 to 126 - Gr. 4 T.
- ✓ 126+00 - F.E. Lt. No culv. req.
- ✓ 128+07 - " " P. 15'x24' C.M.
- ✓ 129+96 - " " "
- ✓ 132+00 - " R. "
- ✓ 133+67 - " Lt. "
- ✓ 133+75 - " R. "
- ✓ 132 to 139 - Cl. 6 T. Gr. 52 T.
- ✓ 137+03 - F.E. Lt. - P. 15'x24' C.M.
- ✓ 140+56 - " " "
- ✓ 140 to 141 - Cl. + Gr. 2.
- ✓ 142+69 - F.E. Lt. P. 15'x24' C.M.
- ✓ 144+00 " R. "
- ✓ 144+67+79 - F.E. Lt. No culv. req.
- ✓ 145 to 152 - Gr. 25 T.

(27-01)

(2)

- ✓ 148+37 - F.E. Lt. P. 15" x 24' C.M.
- ✓ 151+20 " " "
- ✓ 152+25 " R. "
- ✓ 152+50 to 154+50 - No G.R.
- ✓ 156 to 157 - Cl. + Gr. 4T.
- ✓ 157+20 - F.E. R. P. 15" x 24' C.M.
- ✓ 159+30 - " " "
- ✓ 159+5 to 160+50 - Cl. + Gr. 5T.
- ✓ 161 to 164 - " G.R. O.K.
- ✓ 162+00 - P. 24" P₃
- ✓ 168+50 to 171 G.R. O.K.
- ✓ 171+65 - F.E. R. P. 15" x 24' C.M.
- ✓ 172 to 176 - Cl. + Gr. 23T.
- ✓ 176+54 - R. F.E. - No culv. req.
- ✓ No culv. req. at G. Rd. "I"
- ✓ 186 to 4 - Lt. F.E. No culv. req.
- ✓ 187+30 - F.E. R. " " "
- ✓ 188 to 192 - Gr. 20T.
- ✓ 191+75 - F.E. R. + Lt. P. 2-15" x 24' C.M.
- ~~193 to 194 - Lt. G.R.~~
- ✓ 194 to 196 - Cl. + Gr. 10T.
- ✓ 196+50 - P. 24" P₃
- ✓ 201+20 - F.E. Lt. No culv. req.

✓ 201 to 207 - Gr. 20 T.

✓ 206+00 - F.E. R. P. 15' x 24' CM

✓ 206+50 " " " "

✓ 204 to 215 - No G.R.

✓ 208+99 - Remove culv. P. 20' B.

✓ 212+78 - F.E. L. Remove culv. P. 15' x 24' CM

✓ 215 to 218 - Gr. 4 T.

✓ 218+00 F.E. - L. P. 15' x 24' CM

✓ 219+30 " " R. " " " "

✓ 220+76 " " " No culv. req.

✓ 220+53 " " " " " "

✓ 222+80 " " " " " "

✓ 224+87 " " " " " "

✓ 230+15 " " " " " "

✓ 233+86 - Remove culv. P. 24' B

✓ 236 to 239+60 - Cl. + Gr. 4 T.

Co. Rd. "G"

Road 9/8 # 11.

X sec. from Sta. 92 to Sta. 98.

Clay for Proj 28-01B

Dated 3.2.28
C. H. Hantwell

Crane
H. P.
X. P.
E. F.

Sta.	+	H.I.	-	Rod	Elev.
B.M.	7.52	970.00		962.68	
92+00					63.5
92+60					62.0
93+00					61.2
93+50					60.0
94+00					58.7
	2.86	963.26	760	969.40	
94+50					57.4
95+00					56.3
95+50					55.5
96+00					54.5
96+50					53.2
	2.74	956.03	9.97	953.29	
97+00					51.8
97+35					50.7
T.P.			2.74	953.29	

Lt.

Rt.

①

SpA in T.P. Rt. Sta. 92+85

31	60	60	67	71	69	65	6.9	7.7	6.3	1.3	0.9	1.5	1.0	
30	33	21	16	15	10	6	6.5	9	13	15	19	29	33	50

0.4	0.5	0.5	64	73	91	81	80	8.0	8.0	8.6	6.3	0.3	
50	33	32	29	24	16	11	7	8.0	9	12	14	21	25

64	95	92	91	90	90	91	8.6	
27	21	13	9	8.8	11	16	17	21

76	86	112	105	104	102	104	104	8.7	
28	27	22	16	12	10.0	11	14	18	22

117	117	114	118	119	113	
19	13	10	11.3	12	14	19

6.1	6.1	6.0	6.7	6.2	6.0	2.7	
18	10	5.9	10	14	17	19	21

72	72	74	71	7.1	8.2	8.6	6.9	
20	15	11	9	7.0	10	13	16	19

84	86	81	82	90	101	5.5	
20	15	11	7.8	11	14	17	21

96	96	95	94	99	110	9.1	7.9	
20	14	12	8.8	11	13	16	20	22

104	113	116	107	10.5	11.3	12.2	10.5	
22	21	17	14	10.1	10	14	19	22

50	5.3	46	46	48	52	61	46	3.9	6.5	
25	19	15	4.2	9	13	17	20	24	33	50

56	46	71	65	54	53	5.5	6.0	15.4	15.5	17.9	
50	40	33	21	18	13	5.3	11	16	30	33	50

Nail in T.P. Rt. Sta. 96+65

Sta.	+	H.I.	-	Rod	Elev
B.M.	12.40	975.08		962.68	
92+60					62.0
93+00					61.2
93+50					60.0
94+00					58.7
94+50					57.4
	6.74	971.92	9.90	965.18	
95+00					56.3
95+50					55.5
96+00					54.5
96+50					53.2
	1.56	963.50	10.18	961.74	
97+00					51.8
T.P.			10.01	953.29	953.29

H.

BT

(2)

Sp. N. in T.P. N.T. Sta 92 185.

(13.1)	$\frac{5.1}{31}$	$\frac{2.6}{32}$	$\frac{3.5}{50}$
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$\frac{3.0}{50}$	$\frac{2.6}{33}$	(13.9)	$\frac{4.8}{26}$	$\frac{3.6}{30}$	$\frac{2.0}{34}$	$\frac{3.1}{42}$	$\frac{3.0}{50}$
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$\frac{3.5}{50}$	$\frac{1.9}{35}$	(15.1)	$\frac{5.4}{26}$	$\frac{4.5}{33}$	$\frac{5.7}{41}$	$\frac{6.0}{50}$
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$\frac{8.0}{50}$	$\frac{7.8}{37}$	$\frac{8.0}{32}$	(16.4)	$\frac{8.4}{25}$	$\frac{7.2}{27}$	$\frac{6.6}{33}$	$\frac{7.2}{40}$	$\frac{7.7}{50}$
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$\frac{9.4}{50}$	$\frac{10.1}{40}$	$\frac{11.3}{33}$	$\frac{11.3}{25}$	(17.7)	$\frac{11.7}{22}$	$\frac{10.0}{26}$	$\frac{9.9}{33}$	$\frac{9.9}{28}$	$\frac{10.0}{40}$	$\frac{10.5}{50}$
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$\frac{5.9}{50}$	$\frac{5.9}{41}$	$\frac{6.5}{39}$	$\frac{6.9}{33}$	$\frac{7.3}{30}$	(15.6)	$\frac{7.3}{23}$	$\frac{6.6}{29}$	$\frac{5.0}{37}$	$\frac{5.8}{43}$	$\frac{6.6}{50}$
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$\frac{5.0}{50}$	$\frac{4.4}{44}$	$\frac{4.6}{33}$	(16.4)	$\frac{6.5}{28}$	$\frac{2.6}{33}$	$\frac{3.1}{39}$	$\frac{5.1}{50}$
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$\frac{9.2}{50}$	$\frac{7.7}{34}$	$\frac{8.7}{33}$	(17.4)	$\frac{9.6}{26}$	$\frac{6.8}{33}$	$\frac{7.1}{40}$	$\frac{8.6}{50}$
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$\frac{11.6}{50}$	$\frac{11.1}{44}$	$\frac{10.8}{33}$	(18.7)	$\frac{14.0}{24}$	$\frac{10.1}{33}$	$\frac{9.9}{36}$	$\frac{11.5}{43}$	$\frac{12.1}{50}$
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$\frac{7.3}{50}$	$\frac{6.4}{42}$	$\frac{6.5}{33}$	(11.5)
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