

X

PLANS SURVEY

RICE STREET

From Co. Rd. "A" to Co. Rd. "A2"
Ramsey Co. Proj N^o 28-01A

Road ^o/_c N^o 1
File N^o 11



Office of Ramsey Co. Engineer
ST. PAUL, MINN.
Date Filed _____
File No. 11

Proj. # 28-01^A

Rice St.

Alignment from Carpenter Ave.
to Co Road A^E.

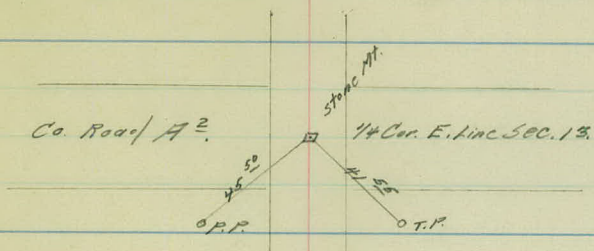
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ST. PAUL, MINN.
Date Filed 11-1-27
File No. 11

Sta. Point Δ Lt Δ Rt.

26 + 32^e P.O.T.

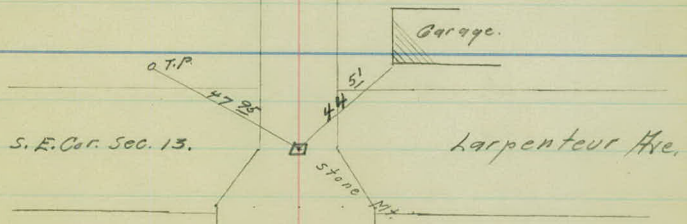
N. 00° - 00' E.

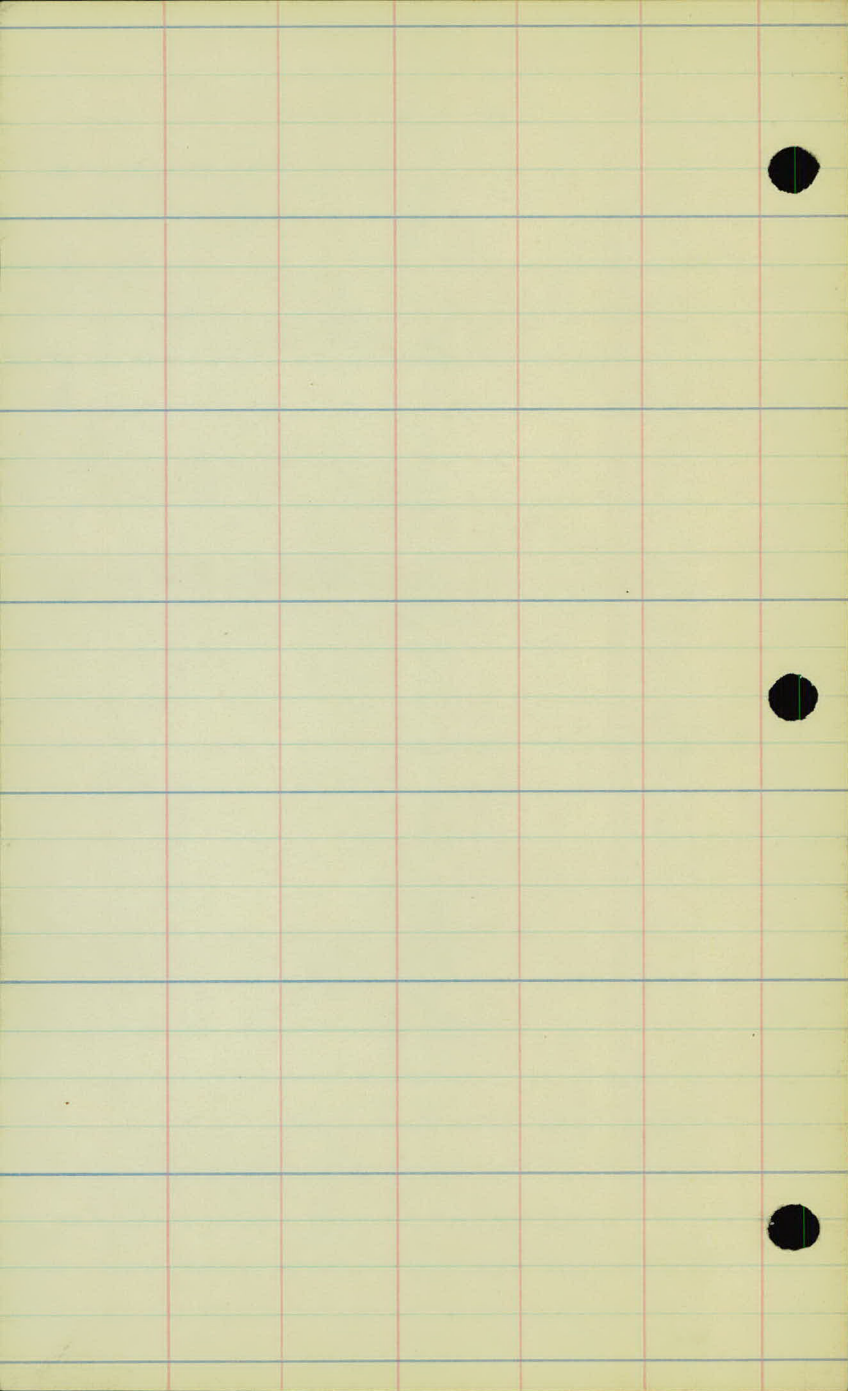
0 + 00



24'

Rice St.





Proj. # 28-01[#]

Rice St.

Art. Topog. from Sta. 0+00
to Sta. 27+00.

Sta.

Lt. Rt.
Edge of Pav.

2+00

12²

11⁸

1+00

12

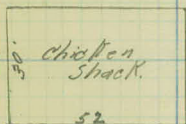
12

0+00

-100

100 T.P. 21

+63 Bldg 48^E



+33 Bldg 47

+50 P.P. 19
+44 P.P. 19

+29 P.P. 20

+22 I. H. / Sign 21

-01 Pave 12L. & 12R.

-16 End Nipple Gutter

1² X 6 X 14

-30 End of Curb

-38 Catch Basin

-48^E Pave 5L & 5R

-56 Hyd 25

-89 P.P. 24

Curb 33'

One Course Conc. 4" Wide.

+50 End of Well 50

+51 4" Conc. Steps 5 Wdg

+14 Mail Box 22

+10 Stone Wall 35
2' High.

+95 T.P. 22

+70 Bldg 39²

+70 Cor. Walk 27



+59 4" Gas Pumps 28

+30 Bldg 38²

+24 Cor. Conc. Walk 26

5" X 10" X 32"
Wooden Header L. & R.

-52 End of Curb 23

-40 Nipple 5

-42 Catch Basin

-54 T.P. 26

-53 Pave 10L & 10R.

Opening
in Curb 14 & 14



Curb 23'

7+00

12¹

11²

6+00

12⁴

11²

5+00

12⁶

11⁴

4+00

12

12

3+00

12²

11²

2+00

+00 F. 38

From Sta. 6 to
Sta. 7 several small
Patches W. & N.E.

+72 F. 31

+29 P.P. 19

F. 34

+14 Willow 34

+14 " 28

+12 " 34

+12 Willow 21

+08 P.P. 19

+35 2' x 2' Patch Mt

+41 F. 36

+30 F. 29

+00 F. 64

+81 P.P. 19

+72 P.P. 19

+50 F. 90

+07 Side Rd Sign 16

+06 F. Cor. 83

+68 P.P. 19

Pasture



SWamp.

+88 Pldg. 53²

+55 T.P. 21

+40-2' x 4' Patch Mt.
+67 Prii. Eat.

+61 T.P. 21

+51 Mail Box 20

+11-24" T- 35

+25 Side Rd Sign 16

+24 T.P. 21

+28 Post Hole 4'
1' x 1'

+04 T.P. 21

scattered logs

12700

12⁷

12⁵

11700

12³

12²

10700

12⁰

12⁰

9700

12²

11²

8700

11²

12²

7700

+74 - 18" Water Main

+60 - 36" Water Main 58

+34 Cross Drain
5' x 3' x 61 Conc. Box
With Miring Walls.
Extends 30 L. & 31 R.
+31 P.P. 17

+63 Cross Drain
36" x 64" C.I.P.
Extends 29 R. & 35 L.

+44 T.P. 21

+77 Sule R. / Sign 17

+45 End of Willows

+11 P.P. 20
Willows 30

+12 T.P. 23

SWAMP

SWAMP

+93 P.P. 19

+93 T.P. 22

+48 Beg. of Row
of Willows 33

+64 Beg. of Row
of Willows 33

+70 P.P. 18
+67 L.P. Sign 25

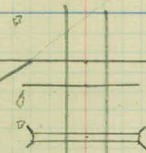
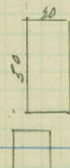
+74 T.P. 21

+36 McCarrons
+44 F. 71

Chicken Shack

+18 Bldg. 44²
+09 Bldg. 33⁴

SWAMP



17+00

12⁰

12⁰

16+00

11⁸

12²

15+00

11²

12⁴

14+00

12⁰

12²

13+00

12⁰

12

12+00

McCarrons Beach

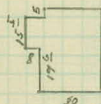
+11 P.P. 18

+15 T.P. 19

+65-24" T-36

Chicken Shack.

+11 Bldg. 36



+91 P.P. 18

Ent. to McCarrons Beach:

+58 T.P. 20

+98 1/2 Sign 18

+12 Side Drain 30⁵
15" X 60

+86 End of Willows

+72 P.P. 19

+60-12" T-27

+52-12" T-24

+23 T.P. 20

+50 P.P. 20

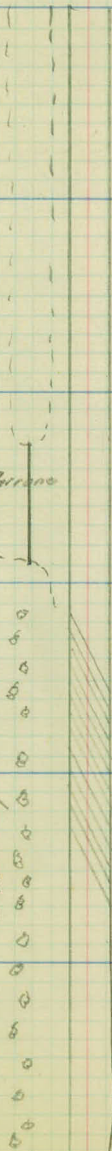
Swamp

Swamp

+40 Mail Box 26

+34-12" T-31

+15 Rd To
Filtration Plant.



22+00

11⁸

12³

21+00

12³

11⁸

20+00

12⁰

12⁰

19+00

12⁰

11⁷

18+00

12⁴

11⁰

17+00

+92 P.P. 19

+83 Surface Drain
+73 P.P. 20

+46 Cross Drain
Double 24" X (59) P.P.
60
Extend 29 L. & 50 R.

+78 Side Drain 31
15" X 60 C.M.

+52 P.P. 19

+65 Cross Drain
5' X 5' X 55 Conc. Box
With Wing Walls
Extends 25 R. & 24 L.

+31 P.P. 19

Swamp

McCormick Beach

This End Covered

Hay Meadow

+90 T.P. 21

+34 T.P. 21

+12 Row Row of
Willows 50
+03 Field Ent.
+03 Side Drain 38
30" X 20 C.M.

+26 Surface Drain
12" X 72 C.M.

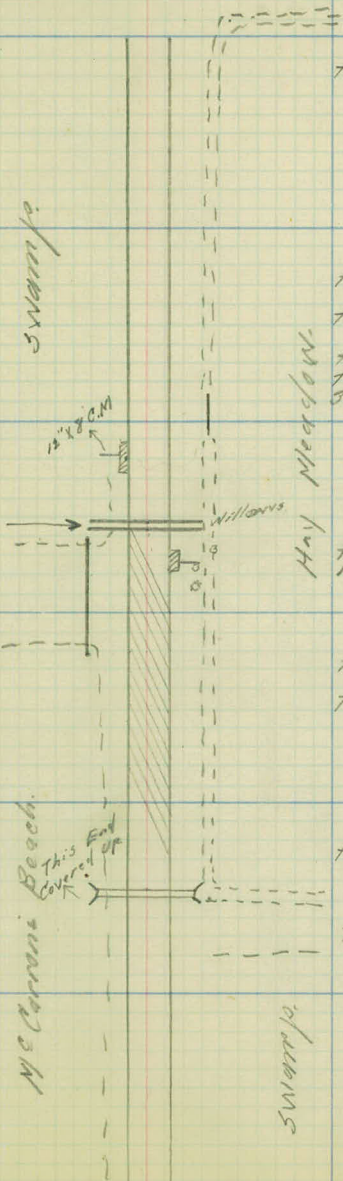
+89 T.P. 20

+80-5' X 3 Patch

+50-5' X 10 Patch Rt.

+29 T.P. 19

Swamp



27+00

132

13⁵

10⁵

26+00

13³

10⁷

25+00

13⁰

11⁰

24+00

12⁰

11⁵

23+00

11²

12³

22+00

+59 Side Pavin 28
8" x 9" V.t.



+99 Filling Sta. 45

+11 Side Pavin 24⁵
15" x 9" Cone Culv.

+91 P.P. 20

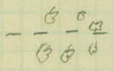
+51 P.P. 20

+62 Ent Sunset Park

+55 Side Pavin 28^E
18" x 54" C.M.

+33 P.P. 19

+08 P.P. 19



SWAMP

Co. Rd A²

130 ft. curve.

SWAMP

+91 T.P. 19

+56 Co. Rd/ Sign 27

+52 Side Pavin 22
15" x 40" P²

+03 F. Cor. 71

+95 T.P. 19

+52 F. Cor. 38

F. 35

+62 T.P. 19
+58 F. 27

+98 F. Cor. 27^E

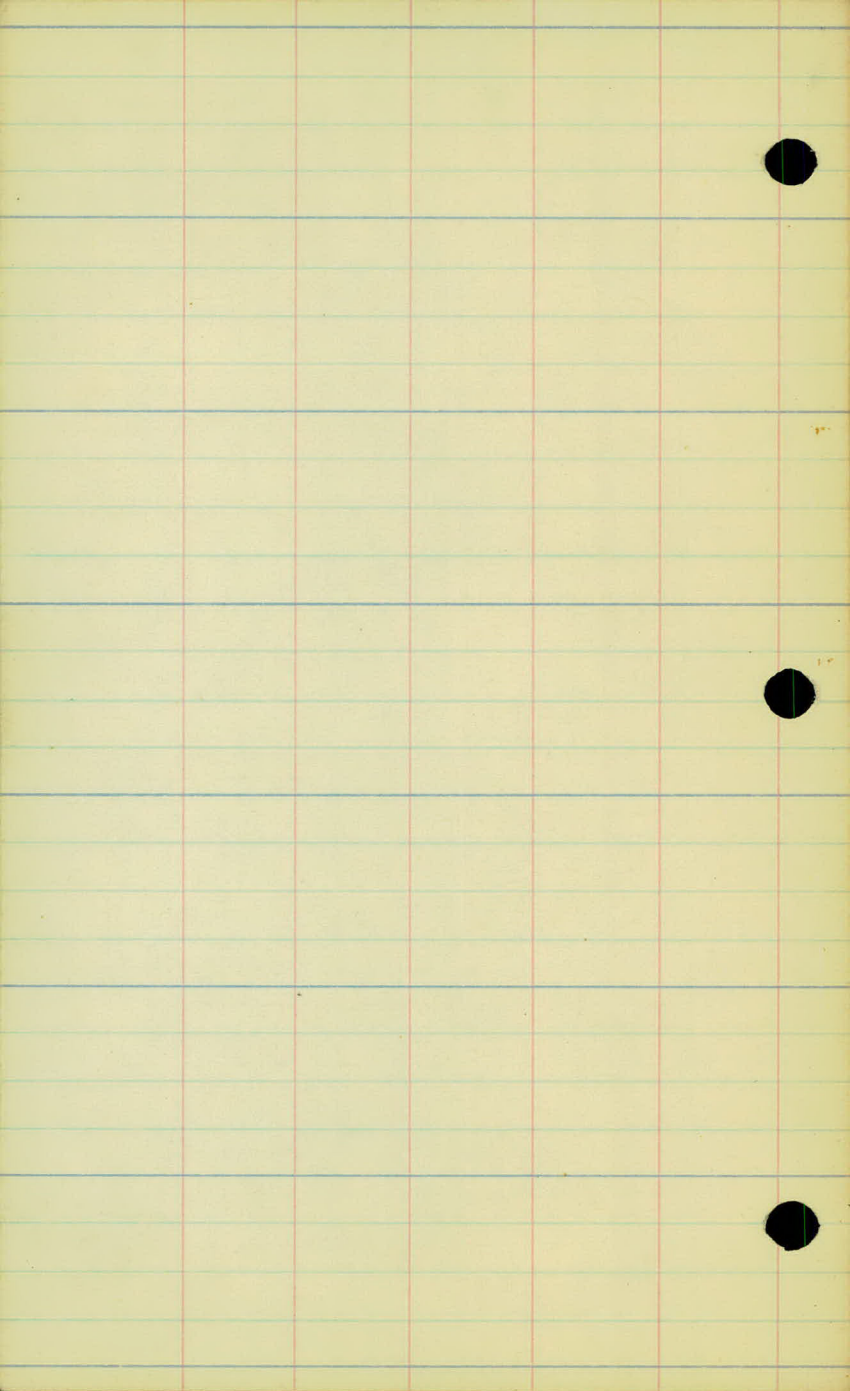
+98 - 24" T- 23

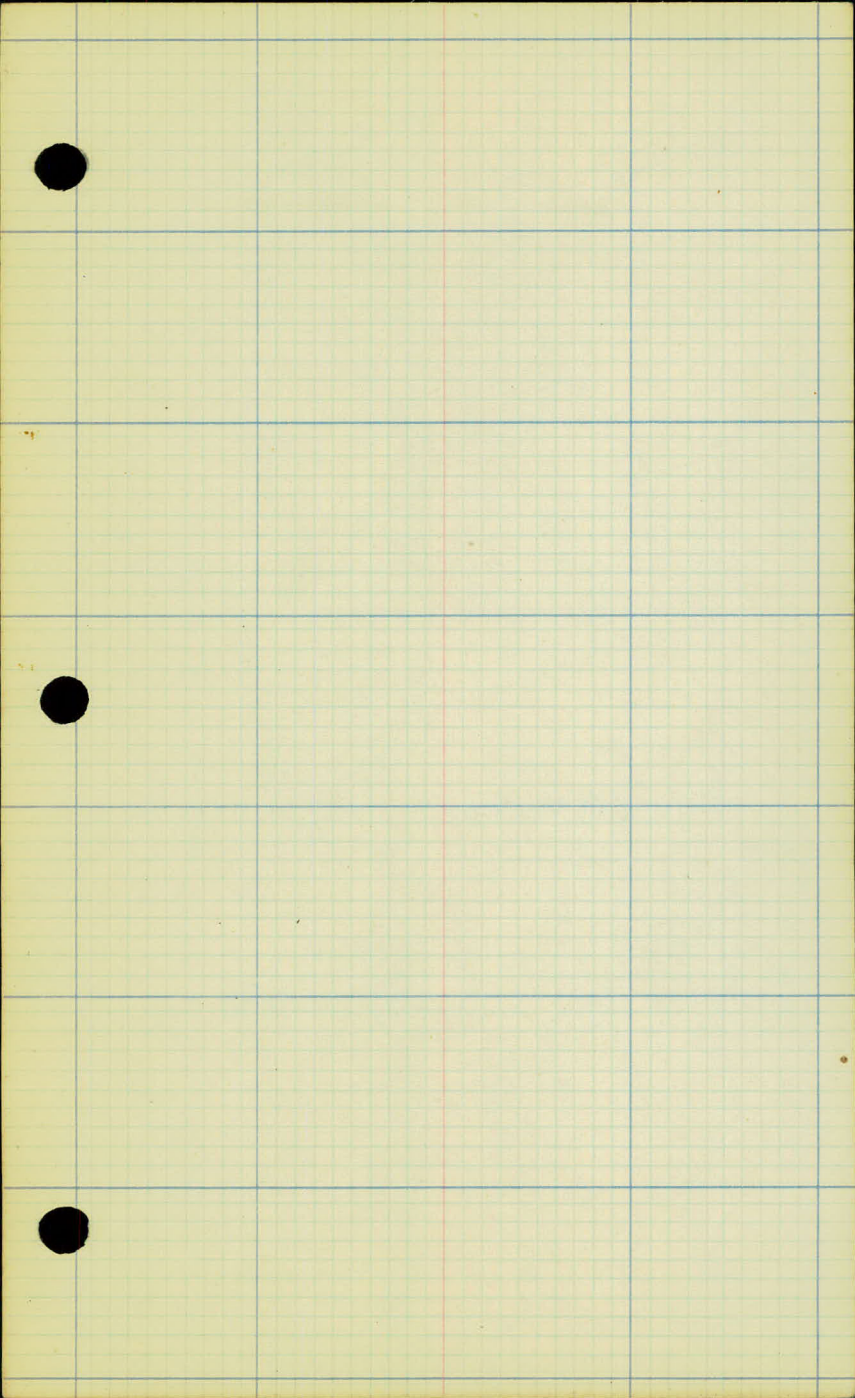
+70 Side Rd/ Sign 1C

+00 Ent of Willows 27

+33 T.P. 21

+13 Guy Pole 25

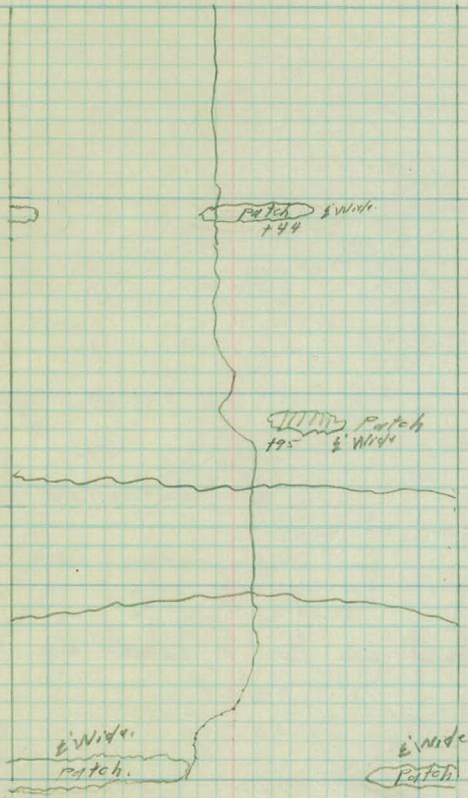




2700

1700

0700

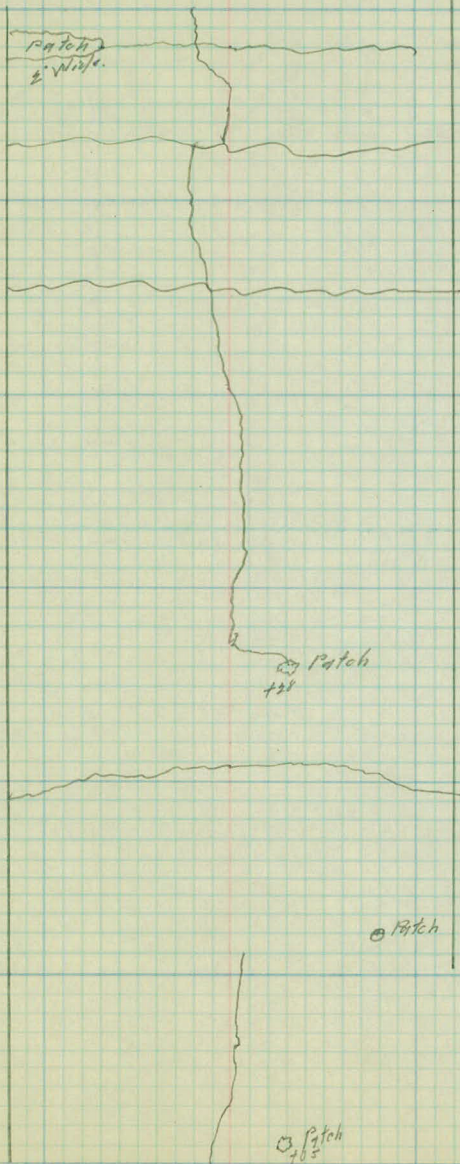


500

400

300

200

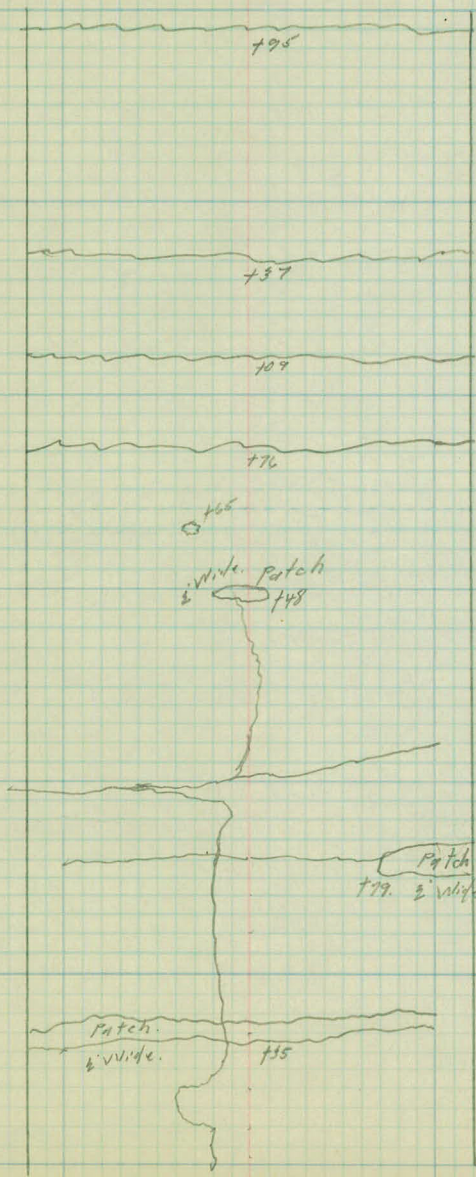


8+00

7+00

6+00

5+00

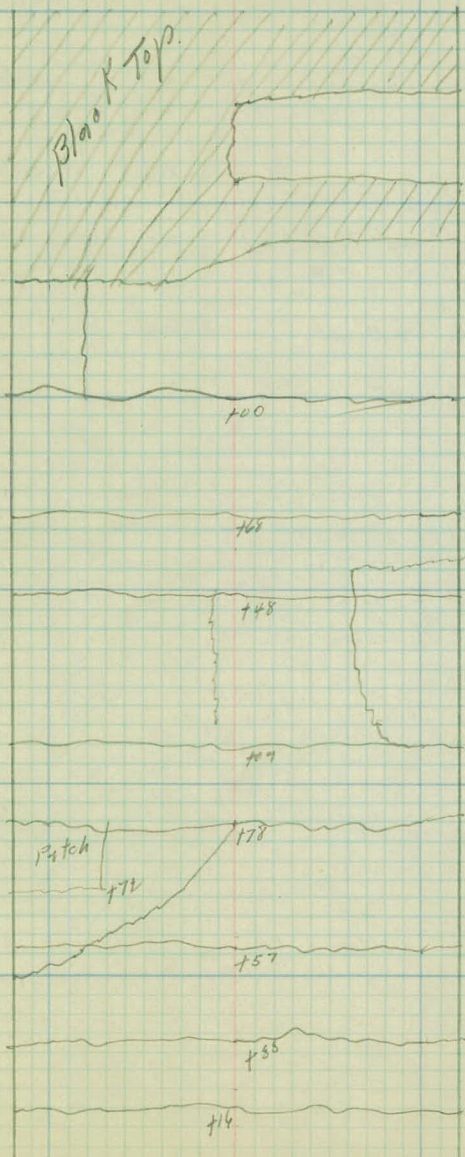


11+00

10+00

7+00

8+00

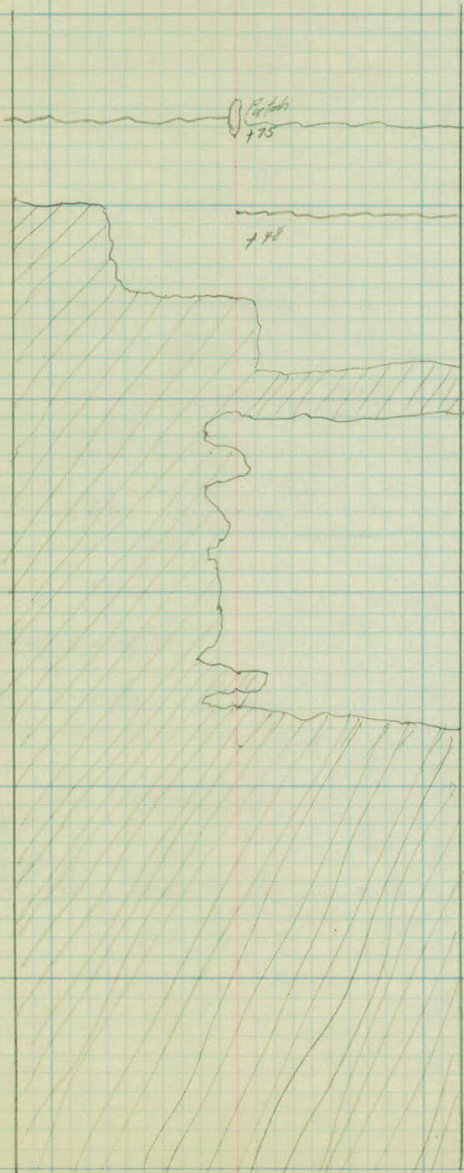


14700

13700

12700

11700

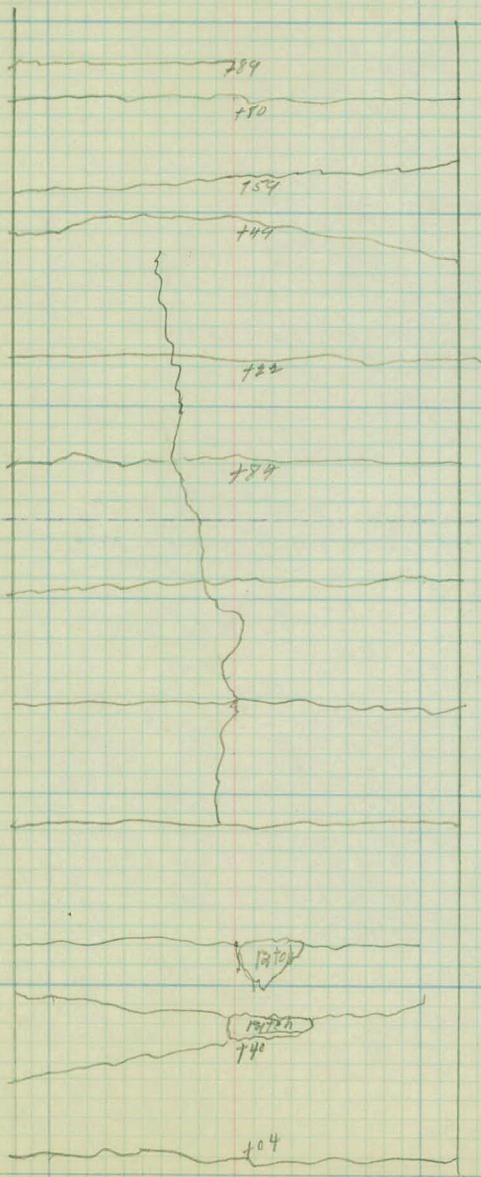


17700

16700

15700

14700

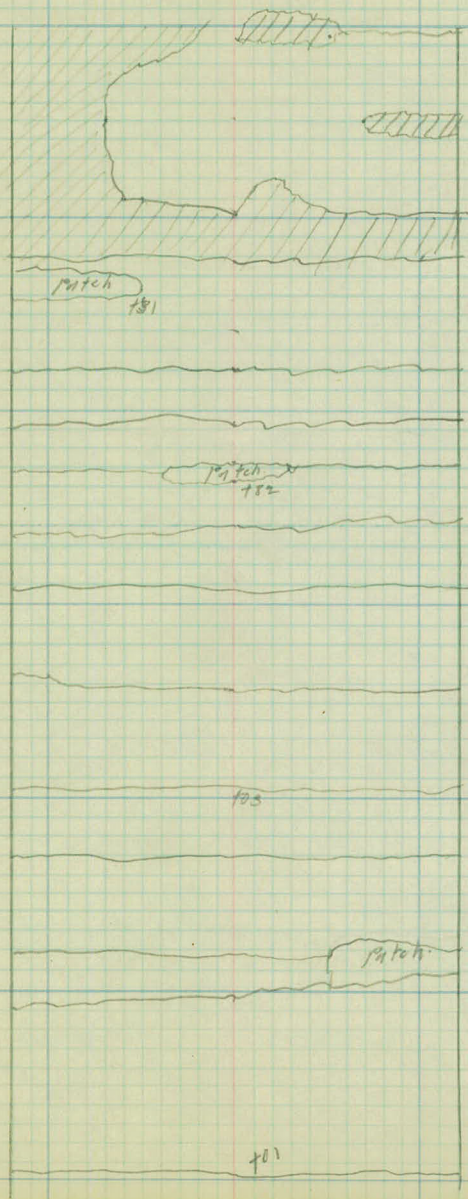


20+00

19+00

18+00

17+00



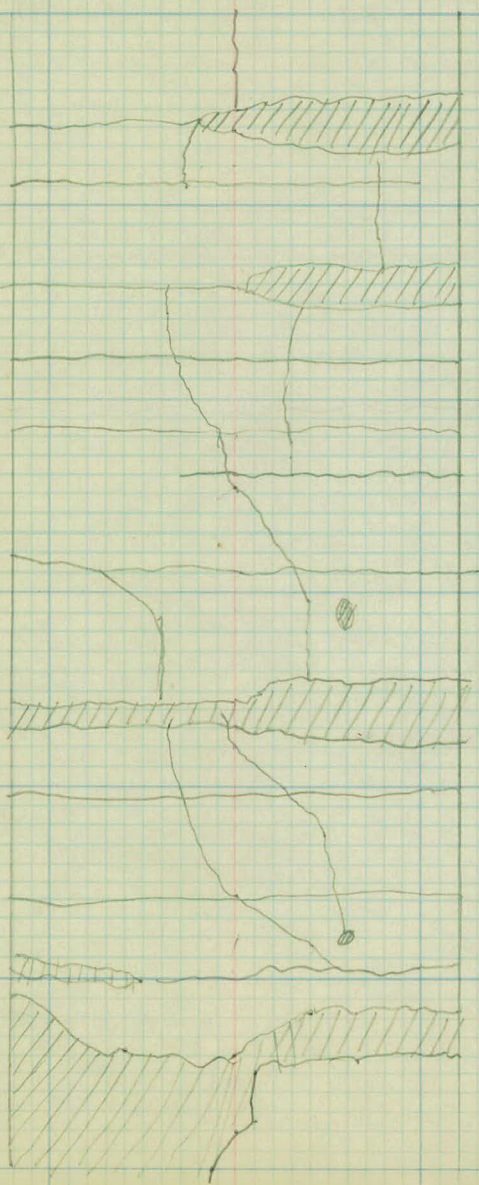
£3+00

£2+00

£1+00

£0+00

10-31-27



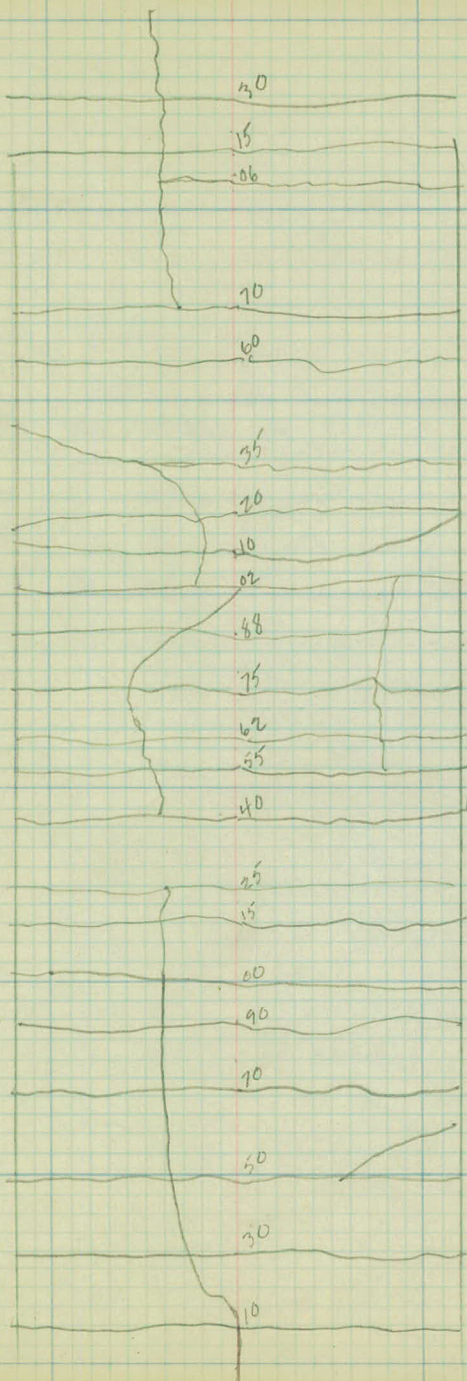
26700

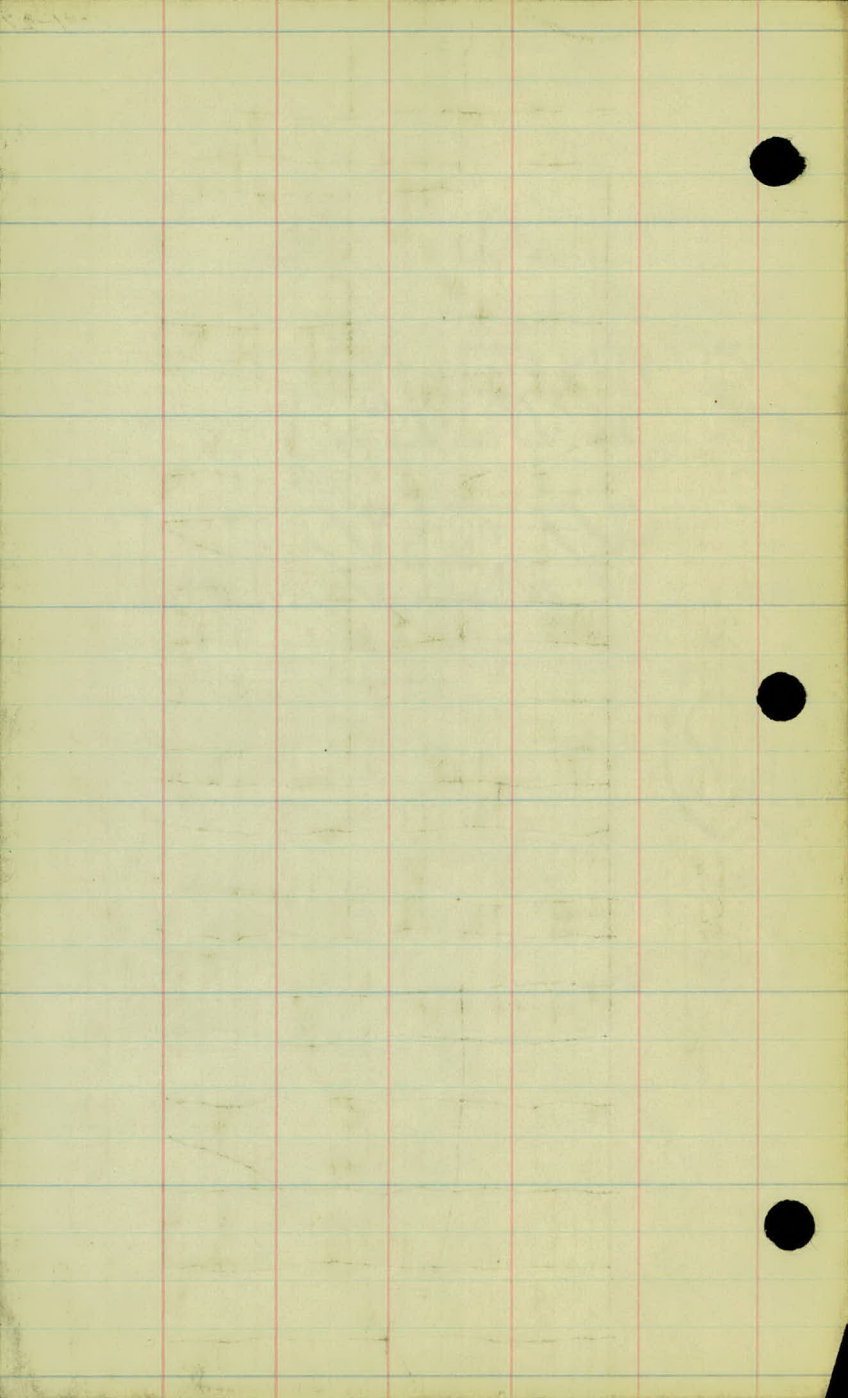
25100

24100

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23100





RICE ST.
SOUNDINGS
From Larpenieur to Co. Rd A2

PROJ 28-01A

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed

File No. 11

Sounding	Location	Depth	Kind of Material
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No. 1	15' Rt. Sta. 7+78	0 - 1.5'	Clay
		1.5 - 2'	Crushed Rock
		2' - 9'	Sand
		9' - 11'	Clay
		11' - 11.5'	Peat
		11.5 -	Sand

No. 2	15' Lt. Sta. 7+78	0 - 1'	Clay
		1' - 2'	Crushed Rock
		2' - 10'	Sand
		10' - 12'	Clay
		12' -	Sand

No. 3	15' Lt. Sta. 8+00	0' - 1'	Clay
		1' - 9'	Sand
		9' - 10'	Black Bog
		10' - 11'	Clay
		11' - 12'	Peat
		12' -	Sand

No. 4	15' Lt. Sta. 9+00	0 - 0.5'	Clay
		0.5' - 3'	Sand
		3' - 6'	" (Red)
		6' - 12'	Sand
		12' - 15'	Clay (Very Wet)
		15' - 21'	Black Bog
		21' -	Clay Very Wet

9-29-1927

Cloudy & Cold

Pavement in Fair Cond.

Party

{ Goldberg
Smith
Celiski

Pavement in Fair Cond.

Pavement in Fair Cond.

Soundings unnecessary below last layer
of Sand because Pav. in Fair Cond.

Pavement on Lt. in Poor Cond.

Clay assumed below 21'

Sounding	Location	Depth	Kind of Material
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No. 5	15' Rt. Sta. 9+50	0-1'	Clay
		1'-10'	Sand
		10'-12'	Clay (Very Wet)
		12'-	" " "

No. 6	15' Lt. Sta. 10+00	0-1'	Clay
		1'-1.5'	Crushed Rock
		1.5'-10'	Sand
		10'-12'	Clay (Very Wet)
		12'-	" " "

No. 7	31' Lt. Sta. 10+00	0-8'	Clay (Very Wet)
		8'-	" " "

No. 8	33' Rt. Sta. 9+50	0-11'	Clay (Very Wet)
		11'-	" " "

No. 9	33' Lt. Sta. 9+00	0-2'	Sand
		2'-9'	Bag Black
		9'-11'	Clay (Very Wet)
		11'-	" " "

No. 10	15' Rt. Sta. 10+00	0-11'	Sand
		11-17	Clay (Very Wet)
		17'-	" " "

9-30-27

Cloudy & Cold

Pavement on Lt. in Poor Cond.

Clay assumed below 12' [Party

Pavement on Lt. in Poor Cond.

{ Goldberg
Smith
Celiski
Braun

Clay assumed below 12'

Clay assumed below 8'

Clay assumed below 11'

Clay assumed below 11'

Clay assumed below 17'

Sounding	Location	Depth	Kind of Material
----------	----------	-------	------------------

No. 11	15' Rt. Sta. 10+50	0-2'	Sand
		2'-3'	Crushed Rock
		3'-8'	Sand
		8-14'	Clay (Very Wet)
		14'-	" " "

No. 12	32' Rt. Sta. 10+00	0-6'	Sand
		6'-17'	Clay (Very Wet)
		17'-	" " "

No. 13	31' Rt. Sta. 10+50	0-21'	Clay
		21'-23'	Peat
		23-24'	Clay (Very Wet)
		24'-	" " "

No. 14	15' Lt. Sta. 10+50	0-3'	Clay
		3'-4'	Crushed Rock
		4'-7'	Sand
		7-11	Clay
		11-13	Sand
		13-23	Clay (Very Wet)
		23'-	" " "

Pavement on Lt. in Poor Cond.

Clay assumed below 14'

Clay assumed below 17'

Pavement on Lt. in Poor Cond.

Clay assumed below 24'

Clay assumed below 23'

Sounding Location Depth Kind of Matil

No. 15 15' Lt. Sta. 11400 0-4' Clay
 4-5' Crushed Rock
 5-8' Clay
 8-17' Sand (Wet)
 17-20' Clay (Very Wet)
 (Assumed) 20' - " " "
 2 Men forced 1/2" Pipe down to 21'
 10# hammer " " " " 30'

No. 16 15' Lt. Sta. 11450 0-3' Sand
 3-10' Clay
 10-18' Sand (Wet)
 18-28' Clay (Very Wet)
 2 Men forced 1/2" Pipe down to 27'
 10# hammer " " " " 36'

No. 17 32' Lt. Sta. 10450 0-3' Clay
 3-14' Sand (Wet)
 14-18' Clay (Wet)
 18-22' Sand (Very Wet)
 22-29' Clay (" " "
 2 Men forced 1/2" Pipe down to 32'
 10# hammer " 1/2" " " 36'

10-1-27

Cloudy & Cool

Pavement on Lt. in Poor Cond.

Material too wet to adhere to auger
below this depth
At this depth pipe broke

Pavement on Lt. in Poor Cond.

Material too wet to adhere to auger below
this depth
Pipe broke at this depth

Material too wet to adhere to auger below
this depth

Pipe broke at this depth

10-3-27

cloudy & Cool

Material too wet to adhere to auger
below this depth

" " " " " " " "

Rate of penetration is 1.5" per drop
of 80# wt. dropped 3'

Between 35' & 48' Penetration is 0.5"

Pavement in Poor Condition Lt.

Material too wet to adhere to auger
below this depth

10-4-27

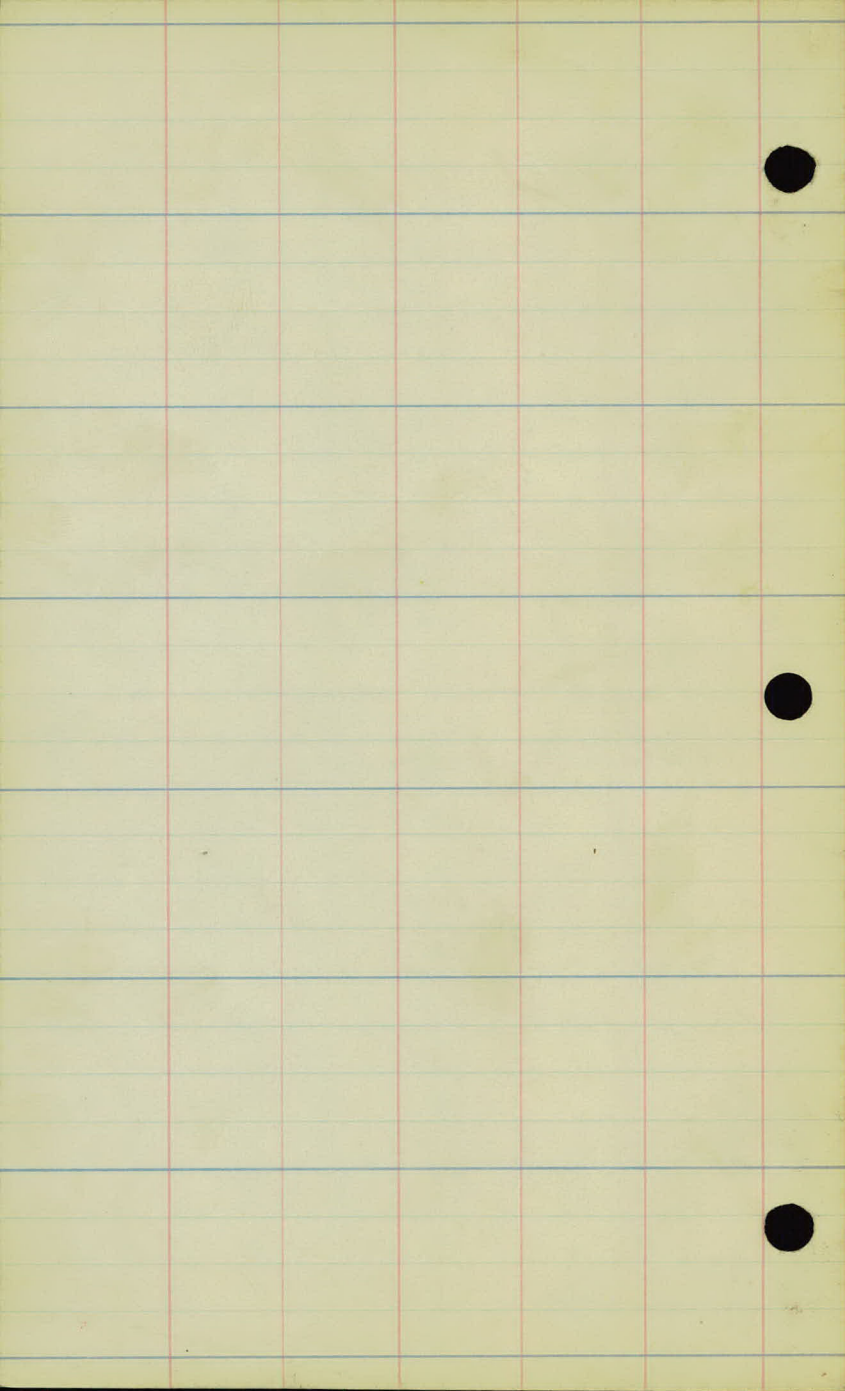
Cloudy & Cold

Pavement on Lt. in Poor Cond.

Material too wet to adhere to auger below
this depth

Pipe broke at this depth

Material too wet to adhere to auger
below this depth.





Sounding Location Depth Kind of Material

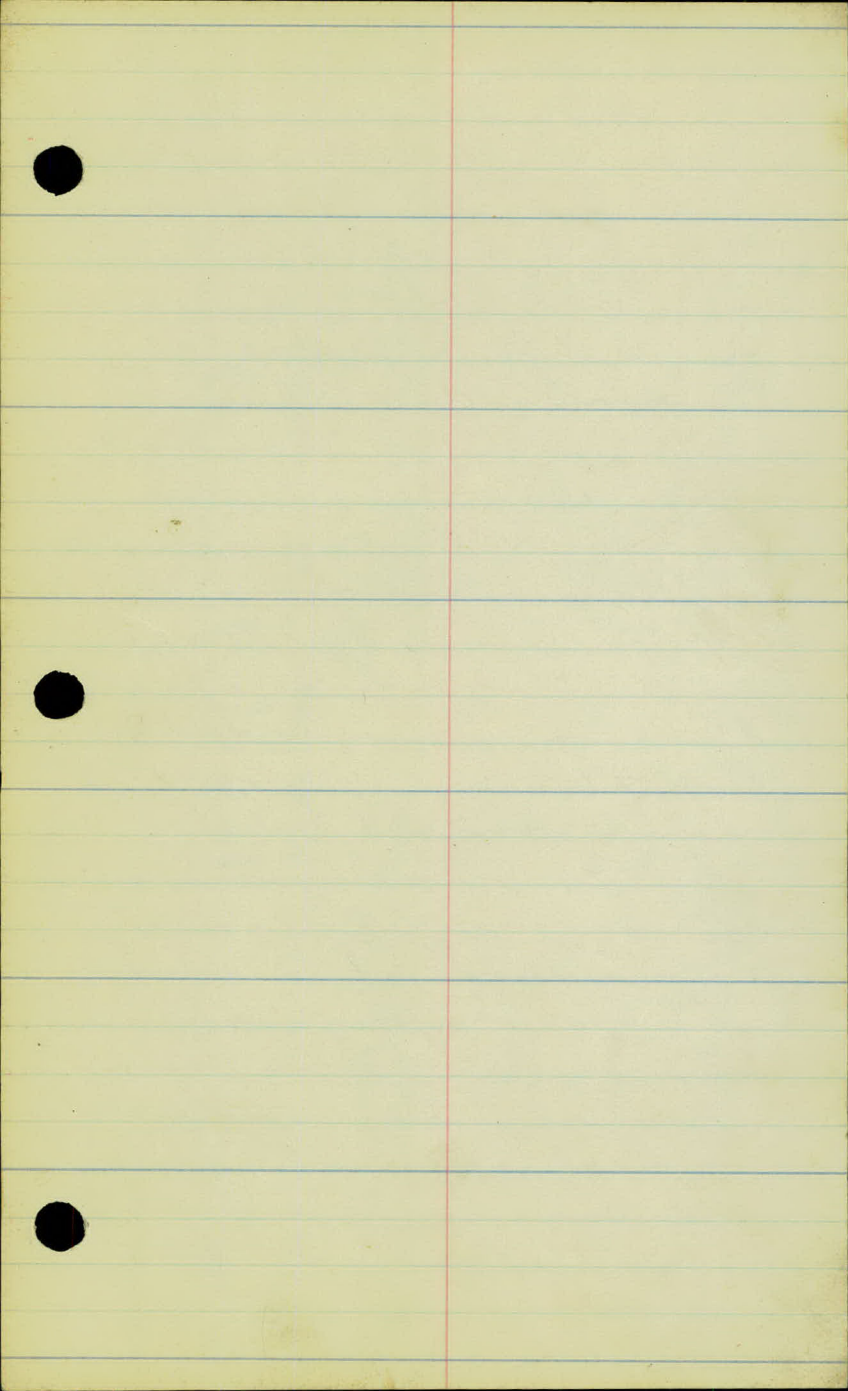
Note: Altho Soundings Nos. 20, 22 & 25 have already been taken, we have again taken soundings at the same stations with better equipment, thus making the previous soundings void.

No. 20 15' Rt. Sta. 11+50 0-10' Clay
10'-39' Wet sand
39'-43' Peat
43'-45' Quicksand ↗
(Mostly water) ↘

80# hammer forced 2" pipe down 42'
Penetration at 35' = 1.5" per drop of 3'
" at 42' = 0.25" " " " "

No. 22 15' Lt. Sta. 12+50 0-13' Wet Sand
13'-20' .. Clay
20-43' Quicksand

80# hammer forced 2" pipe down to 41'
Penetration at 41' = 0.25" per drop of 3'
" .. 30' = 2" " " " "



Pavement in poor Condition

Stone or some other solid object prevented soundings below 24'

Sounding	Location	Depth	Kind of Mat'rl
----------	----------	-------	----------------

No. 28	15' Rt. Sta. 21+50	0-17'	Sand
		17-25'	Clay
		25-27'	Black Bog
		27-30'	Peat
		30-34'	Black Bog
		34-37'	Clay
		37-42'	Quicksand

80# hammer forced 2" pipe down 42'
 Penetration at 42' = 0.25" per drop of 3"
 " " 36 = 2 " " " "

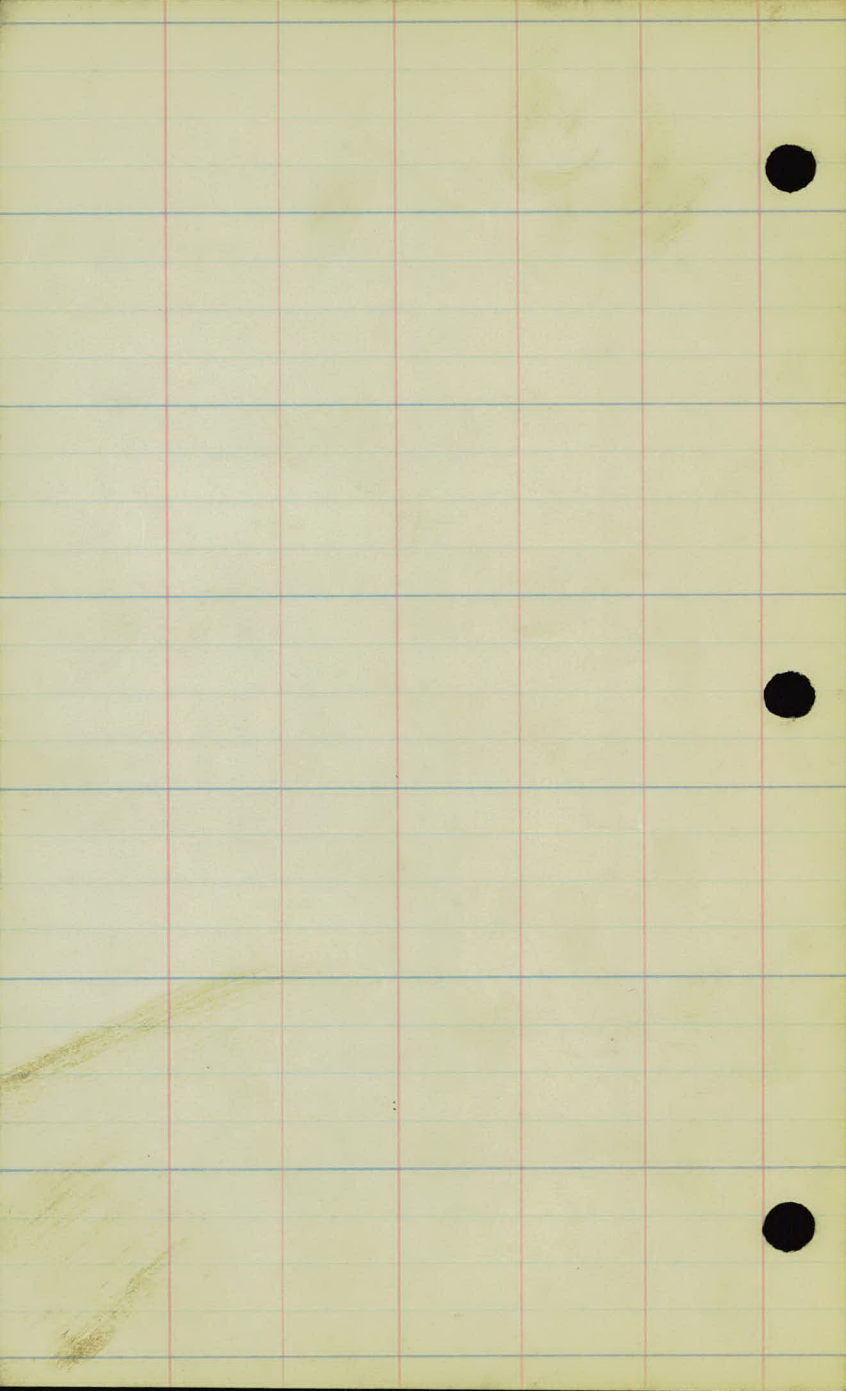
No. 29	60' Rt. Sta. 21+50	Elev. = 5.3' lower than $\frac{1}{2}$ of Rice St.	
		0-32'	Bog
		32-39'	Peat
		39-41'	Clay
		41-43'	Quicksand

80# hammer forced 2" pipe down 42'
 Penetration at 42' = 0.25" per drop of 3"
 " " 30 = 1 " " " "

No. 30	15' Rt. Sta. 22+00	0-12'	Sand
		12-27'	clay
		27-31'	Peat
		31-38'	Clay
		38-39'	Quicksand

Pavement on Rt. in poor Cond.

Pavement on Rt. in poor Cond.



Proj. # 28-01^A

Rice St.

X sections from sta.
0+00 to sta. 26+50.

Sta.	+	H. I.	-	Rod.	Elev
B.M.	5.14	870.57		865.23	
- 1.00				1.90	67.47
- 50				4.11	66.26
- 25					65.58
0 + 00					64.99
0 + 25					64.52
0 + 50					63.96
0 + 75					63.33
1 + 00					62.84
T.P.				1.31	869.06
1 + 25					61.99
T.P.	1.40	866.65	5.14	865.23	
1 + 50					61.63
1 + 75					61.05
2 + 00					60.60
2 + 25					60.07

Spk in Arc. light Pole Int. Larp. & Rice St. # B.

3.7 3.1 3.4 4.5 5.6 5.22 4.87 4.8 4.87 5.16 5.0 5.0 4.7 4.6
 60 50 41 22 23 21 10 4.77 10 21 24 38 50 60

6.5 6.7 7.0 6.5 5.3 5.38 5.37 5.14 5.41 5.47 5.1 5.0 5.3 5.3
 60 50 40 27 18 12 6 5.38 6 12 18 33 50 60

(59) on side walk
7.3 6.3 5.5 6.0 5.5 5.94 5.87 5.90 6.00 5.4 4.77 4.75
 60 50 41 32 19 12 6 5.85 6 12 25 27 60

(64)
8.2 7.1 6.5 6.48 6.45 6.46 6.52 5.8 4.75 4.64
 60 50 26 12 6 6.41 6 12 26 26 32 Blvd.

(7.0)
8.5 8.4 8.2 7.4 7.10 7.07 7.08 7.11 6.4 5.2 5.3 6.6 5.4
 60 50 40 27 12 6 7.04 6 12 24 35 44 50 60

(7.5)
8.0 8.0 7.7 7.62 7.56 7.58 7.63 7.2 6.2 4.0 3.7 3.2
 60 50 26 12 6 7.53 6 12 20 27 35 50 60

On Step

(8.4) Above HE + 5.4
6.5
8.3 8.3 8.1 8.0 8.19 8.15 8.14 8.26 7.9 7.0 4.8 4.4 4.2 4.7 4.53
 60 50 41 29 12 6 8.38 6 12 24 33 33 36 42 50 60

(5.0)
4.6 4.7 5.15 4.99 5.05 5.14 4.9 4.2 3.2 1.2 0.9
 Blvd. 48 24 12 6 5.00 6 12 18 25 33 33 37

(5.6)
4.7 4.7 5.2 5.5 5.67 5.58 5.63 5.67 5.4 4.2 0.3
 60 50 32 23 12 6 5.58 6 12 30 30 36

(6.0)
5.5 5.7 5.9 6.3 6.0 6.15 6.07 6.08 6.14 5.7 4.6 1.1
 60 50 40 34 18 12 6 6.03 6 12 21 27 35

(6.6)
0.2 5.7 6.8 6.6 6.65 6.60 6.63 6.71 6.6 5.6 4.0 0.6
 45 37 29 20 12 6 6.56 6 12 19 27 32 35

Sta	+	H.I.	-	Rod	Elev.
		866.63			
2+50					859.61
2+75					59.07
3+00					58.59
3+25					58.10
3+50					57.45
3+75					56.89
4+00					56.40
4+25					55.87
T.P.			11.48	855.15	
T.P.	10.69	879.75		869.06	
1+50		879.75 59.6 820.1			
1+75					
2+25					
2+50					

$\frac{22}{37} \frac{5.5}{31} \frac{6.5}{30} \frac{70}{28} \frac{76}{22} \frac{71}{20} \frac{70.5}{12} \frac{700}{6}$ (7.0) $\frac{7.09}{7.02} \frac{7.18}{6} \frac{90}{12} \frac{7.1}{16} \frac{6.5}{22} \frac{0.4}{28} \frac{0.4}{36}$

$\frac{22}{37} \frac{5.2}{33} \frac{7.6}{27} \frac{80}{21} \frac{76}{18} \frac{76.2}{12} \frac{7.56}{6}$ (7.6) $\frac{7.64}{7.56} \frac{7.71}{6} \frac{81}{12} \frac{7.7}{12} \frac{7.7}{14} \frac{6.6}{20} \frac{0.9}{28} \frac{0.9}{37}$

$\frac{1.9}{3.5} \frac{3.6}{32} \frac{7.7}{16} \frac{86}{24} \frac{8.7}{21} \frac{8.3}{19} \frac{8.1}{15} \frac{8.4}{12} \frac{8.18}{12} \frac{8.09}{6}$ (8.0) $\frac{8.07}{8.04} \frac{8.18}{6} \frac{8.5}{12} \frac{8.2}{12} \frac{8.3}{14} \frac{7.4}{22} \frac{3.9}{29} \frac{1.0}{34} \frac{1.0}{38}$

$\frac{1.0}{3.7} \frac{8.3}{26} \frac{9.8}{22} \frac{7.6}{18} \frac{9.1}{17} \frac{8.7}{14} \frac{90}{12} \frac{8.74}{12} \frac{8.64}{6}$ (8.6) $\frac{8.69}{8.63} \frac{8.75}{6} \frac{90}{12} \frac{8.7}{12} \frac{90}{14} \frac{8.6}{20} \frac{2.0}{26} \frac{2.0}{38}$

$\frac{6.2}{3.8} \frac{8.6}{3.4} \frac{10.3}{2.7} \frac{9.9}{20} \frac{9.3}{18} \frac{9.4}{12} \frac{9.31}{12} \frac{9.32}{6}$ (9.2) $\frac{9.23}{9.18} \frac{9.24}{6} \frac{9.4}{12} \frac{9.1}{12} \frac{90}{14} \frac{9.6}{18} \frac{9.7}{21} \frac{8.6}{2.7} \frac{0.6}{3.2} \frac{0.6}{40}$

$\frac{4.5}{4.1} \frac{7.8}{3.5} \frac{10.8}{3.2} \frac{10.7}{20} \frac{9.9}{18} \frac{9.87}{12} \frac{9.72}{6}$ (9.7) $\frac{9.79}{9.74} \frac{9.85}{6} \frac{9.9}{12} \frac{10.4}{20} \frac{10.1}{22} \frac{9.6}{31} \frac{6.5}{3.4} \frac{2.5}{3.6} \frac{2.5}{4.3}$

$\frac{3.9}{40} \frac{7.4}{3.7} \frac{11.3}{30} \frac{11.3}{21} \frac{10.3}{18} \frac{10.32}{12} \frac{10.25}{6}$ (10.2) $\frac{10.29}{10.23} \frac{10.35}{6} \frac{10.3}{12} \frac{10.8}{18} \frac{8.8}{31} \frac{5.4}{3.4} \frac{3.1}{40} \frac{40}{41} \frac{6.4}{50} \frac{6.4}{60}$

→ Above H.F.

$\frac{40.8}{60} \frac{12}{4.5} \frac{2.4}{4.2} \frac{4.8}{3.8} \frac{11.9}{2.8} \frac{12.0}{21} \frac{110}{12} \frac{10.7}{15} \frac{110}{12} \frac{10.80}{12} \frac{10.79}{6}$ (10.8) $\frac{10.81}{10.76} \frac{10.91}{6} \frac{11.1}{12} \frac{10.7}{12} \frac{10.9}{20} \frac{11.7}{23} \frac{11.8}{28} \frac{11.5}{3.4} \frac{15.1}{3.8}$

On Stop.

$\frac{10.1}{4.3} \frac{8.2}{5.3} \frac{3.8}{6.4} \frac{3.8}{70}$ (18.1)

$\frac{6.5}{4.3} \frac{5.2}{50} \frac{4.4}{60} \frac{3.9}{70}$ (18.1)

$\frac{6.8}{70} \frac{6.1}{60} \frac{6.1}{50}$ (19.7)

$\frac{6.1}{50}$ (20.1)

Sta + H.I. - Rod Elev

879.75
5.77

2+75

3+00

3+25

3+50

3+75

4+00

T.P. 9.94 885.92 5.77 875.98

2+00

2+25

2+50

2+75

3+00

3+25

3+50

$$\frac{65}{50}$$

20.7

$$\frac{26}{50} \quad \frac{65}{45}$$

21.2

$$\frac{22}{50}$$

21.6

$$\frac{13}{62} \quad \frac{94}{50}$$

22.3

$$\frac{37}{61} \quad \frac{73}{50}$$

22.9

$$\frac{16}{60} \quad \frac{100}{50}$$

23.4

25.2

$$\frac{8.8}{47} \quad \frac{6.2}{52} \quad \frac{3.8}{54} \quad \frac{5.8}{65}$$

25.8

$$\frac{12.9}{92} \quad \frac{7.2}{50} \quad \frac{4.8}{52} \quad \frac{5.4}{65} \quad \frac{6.0}{75}$$

26.3

$$\frac{4.8}{50} \quad \frac{4.2}{60} \quad \frac{4.3}{75}$$

26.8

$$\frac{12.4}{44} \quad \frac{7.8}{50} \quad \frac{4.4}{54} \quad \frac{3.5}{65} \quad \frac{2.0}{75}$$

27.3

$$\frac{11.2}{45} \quad \frac{7.5}{50} \quad \frac{4.2}{55} \quad \frac{2.8}{65} \quad \frac{2.0}{75}$$

27.9

$$\frac{13.0}{48} \quad \frac{10.2}{52} \quad \frac{2.9}{56} \quad \frac{2.7}{70} \quad \frac{2.5}{75}$$

28.4

$$\frac{5.4}{57} \quad \frac{5.1}{70} \quad \frac{5.3}{75}$$

Sta.	+	H.I.	-	Rod	Elev.
		885.92			
3+75					
4+00					
T.P.	11.29	896.24	0.97	884.95	
3+75					
T.P.	8.74	904.40	0.58	895.64	
2+50					
2+75					
3+00					
3+25					
3+50					
T.P.	0.50	896.14	8.74	895.64	
T.P.	1.11	886.05	11.22	884.94	
T.P.	0.57	873.79	12.83	873.22	
T.P.	2.61	864.61	11.79	862.00	
T.P.	1.99	857.41	9.48	855.13	855.15
4+50					855.30
4+75					54.76
5+00					54.09

(29.0) $\frac{13.5}{57}$ $\frac{13.4}{70}$ $\frac{13.7}{75}$

$\frac{4.8}{80}$ $\frac{5.8}{70}$ (29.5)

$\frac{4.4}{100}$ $\frac{4.7}{91}$ $\frac{5.3}{82}$ $\frac{9.5}{74}$ (39.3)

$\frac{2.0}{100}$ $\frac{18.7}{90}$ $\frac{13.8}{80}$ $\frac{17.0}{71}$ (44.8)

$\frac{6.3}{108}$ $\frac{6.5}{95}$ $\frac{6.7}{83}$ $\frac{12.0}{80}$ (45.3)

4406 F23

$\frac{5.8}{104}$ $\frac{5.6}{96}$ $\frac{5.2}{83}$ $\frac{6.6}{77}$ $\frac{9.8}{74}$ (46.8)

$\frac{2.5}{110}$ $\frac{2.6}{95}$ $\frac{3.2}{82}$ $\frac{12.0}{69}$ (46.4)

$\frac{6.0}{110}$ $\frac{5.8}{100}$ $\frac{6.3}{90}$ (46.9)

Along H.I.

$\frac{7.0}{60}$ $\frac{0.3}{50}$ $\frac{1.3}{37}$ $\frac{1.9}{34}$ $\frac{3.0}{32}$ $\frac{2.8}{31}$ $\frac{2.1}{18}$ $\frac{1.9}{14}$ $\frac{2.1}{12}$ $\frac{18.6}{12}$ $\frac{18.3}{6}$ (1.8) $\frac{1.91}{6}$ $\frac{1.99}{12}$ $\frac{2.3}{12}$ $\frac{2.0}{14}$ $\frac{2.5}{22}$ $\frac{2.5}{30}$ $\frac{8.0}{40}$ $\frac{9.8}{50}$ $\frac{10.0}{60}$

(2A) $\frac{4.4}{60}$ $\frac{4.8}{50}$ $\frac{4.8}{41}$ $\frac{3.2}{35}$ $\frac{3.5}{20}$ $\frac{2.6}{17}$ $\frac{2.57}{12}$ $\frac{2.95}{6}$ $\frac{2.45}{6}$ $\frac{2.57}{12}$ $\frac{2.2}{14}$ $\frac{2.5}{18}$ $\frac{2.4}{25}$ $\frac{4.4}{29}$ $\frac{6.7}{40}$ $\frac{9.7}{50}$ $\frac{11.1}{60}$

$\frac{6.6}{60}$ $\frac{6.0}{50}$ $\frac{5.0}{37}$ $\frac{4.4}{35}$ $\frac{4.2}{32}$ $\frac{4.2}{24}$ $\frac{3.0}{18}$ $\frac{3.0}{15}$ $\frac{3.17}{12.5}$ $\frac{3.10}{6}$ (3.1) $\frac{3.06}{6}$ $\frac{3.12}{11.5}$ $\frac{3.2}{13}$ $\frac{3.0}{18}$ $\frac{4.2}{22}$ $\frac{7.6}{29}$ $\frac{10.9}{39}$ $\frac{13.4}{50}$ $\frac{14.6}{60}$

Sta.	+	H. I. ✓	-	Ref	Elev.
		857.14			
5+25					853.45
5+50					52.92
5+75					52.36
6+00					51.89
T.P.	3.06	854.70 ✓	5.50	851.64 ✓	
6+25					51.48
6+50					51.06
6+75					50.64
7+00					50.20
7+25					49.77
7+50					49.32
7+75					48.83
T.P.	1.72	849.73 ✓	6.69	848.01 ✓	<u>49.83</u>
8+00					48.39
8+25					47.91

$\begin{array}{r} 72 \ 68 \ 52 \ 45 \ 38 \ 35 \ 30 \ 27 \\ 60 \ 50 \ 39 \ 21 \ 19 \ 16 \ 12^E \ 6 \end{array}$
3.7
 $\begin{array}{r} 3.73 \ 3.76 \ 3.6 \ 3.4 \ 6.6 \ 10.7 \ 18.1 \ 140 \ 150 \\ 6 \ 11^E \ 18 \ 24 \ 31 \ 37 \ 45 \ 50 \ 60 \end{array}$

$\begin{array}{r} 82 \ 76 \ 68 \ 65 \ 57 \ 56 \ 42 \ 434 \ 424 \\ 60 \ 50 \ 38 \ 35 \ 31 \ 24 \ 20 \ 12^E \ 6 \end{array}$
4.2
 $\begin{array}{r} 4.28 \ 4.34 \ 4.4 \ 6.2 \ 7.3 \ 11.5 \ 12.4 \ 13.0 \\ 6 \ 11^E \ 17 \ 24 \ 29 \ 40 \ 50 \ 60 \end{array}$

$\begin{array}{r} 87 \ 82 \ 79 \ 73 \ 67 \ 62 \ 50 \ 492 \ 480 \\ 60 \ 50 \ 47 \ 35 \ 31 \ 24 \ 21 \ 12^E \ 6 \end{array}$
4.8
 $\begin{array}{r} 4.85 \ 4.92 \ 5.4 \ 11.3 \ 13.4 \ 14.3 \\ 6 \ 11^E \ 22 \ 39 \ 47 \ 60 \end{array}$

2.3R

$\begin{array}{r} 88 \ 88 \ 82 \ 75 \ 67 \ 52 \ 534 \ 526 \\ 60 \ 50 \ 48 \ 33 \ 24 \ 17 \ 12^E \ 6 \end{array}$
5.3
 $\begin{array}{r} 5.28 \ 5.38 \ 5.7 \ 11.0 \ 14.4 \ 15.8 \ 18.3 \ 18.5 \\ 6 \ 11^E \ 21 \ 30 \ 46 \ 50 \ 55 \ 60 \end{array}$

$\begin{array}{r} 61 \ 64 \ 53 \ 45 \ 35 \ 328 \ 322 \\ 60 \ 50 \ 31 \ 22 \ 20 \ 12^E \ 6 \end{array}$
3.2
 $\begin{array}{r} 3.29 \ 3.39 \ 3.7 \ 5.3 \ 3.2 \ 6.8 \ 12.3 \ 15.0 \ 16.5 \\ 6 \ 11^E \ 12 \ 16 \ 17 \ 25 \ 34 \ 50 \ 60 \end{array}$

$\begin{array}{r} 60 \ 61 \ 65 \ 65 \ 58 \ 57 \ 39 \ 366 \ 363 \\ 60 \ 50 \ 40 \ 32 \ 30 \ 27 \ 21 \ 12^E \ 6 \end{array}$
3.6
 $\begin{array}{r} 3.68 \ 3.79 \ 3.9 \ 3.7 \ 12.6 \ 15.3 \ 17.1 \\ 6 \ 11^E \ 12 \ 20 \ 34 \ 50 \ 60 \end{array}$

$\begin{array}{r} 62 \ 63 \ 59 \ 53 \ 45 \ 413 \ 406 \\ 60 \ 50 \ 40 \ 32 \ 18 \ 12^E \ 6 \end{array}$
4.1
 $\begin{array}{r} 4.15 \ 4.24 \ 4.9 \ 7.2 \ 7.2 \ 11.2 \ 15.2 \ 17.4 \\ 6 \ 11^E \ 28 \ 38 \ 36 \ 50 \ 60 \ 70 \end{array}$

$\begin{array}{r} 66 \ 63 \ 61 \ 66 \ 65 \ 53 \ 454 \ 450 \\ 60 \ 50 \ 37 \ 35 \ 33 \ 29 \ 12 \ 6 \end{array}$
4.5
 $\begin{array}{r} 4.57 \ 4.67 \ 4.5 \ 4.4 \ 4.7 \\ 6 \ 12 \ 15 \ 21 \ 33 \ \text{RND} \end{array}$

$\begin{array}{r} 72 \ 71 \ 70 \ 58 \ 501 \ 496 \\ 60 \ 50 \ 45 \ 28 \ 12 \ 6 \end{array}$
4.9
 $\begin{array}{r} 5.01 \ 5.12 \ 4.8 \ 4.7 \ 4.7 \\ 6 \ 12 \ 26 \ 37 \ 45 \ \text{RND} \end{array}$

$\begin{array}{r} 70 \ 75 \ 71 \ 53 \ 545 \ 539 \\ 60 \ 50 \ 45 \ 18 \ 12 \ 6 \end{array}$
5.4
 $\begin{array}{r} 5.40 \ 5.14 \ 5.2 \ 4.9 \ 5.2 \\ 6 \ 12 \ 27 \ 40 \ 45 \ \text{RND} \end{array}$

$\begin{array}{r} 87 \ 78 \ 100 \ 118 \ 103 \ 58 \ 596 \ 589 \\ 60 \ 50 \ 43 \ 38 \ 27 \ 16 \ 12 \ 6 \end{array}$
5.9
 $\begin{array}{r} 5.95 \ 6.01 \ 5.7 \ 5.2 \\ 6 \ 12 \ 27 \ 45 \end{array}$

5.87

$\begin{array}{r} 95 \ 91 \ 80 \ 64 \ 16 \ 12 \ 137 \ 132 \\ 60 \ 50 \ 37 \ 29 \ 19 \ 16 \ 12 \ 6 \end{array}$
1.3
 $\begin{array}{r} 1.42 \ 1.52 \ 1.3 \ 0.9 \ 0.9 \ 11.8 \ 12.0 \\ 6 \ 12 \ 14 \ 19 \ 35 \ 50 \ 60 \end{array}$

$\begin{array}{r} 110 \ 106 \ 105 \ 70 \ 19 \ 500 \ 486 \\ 60 \ 50 \ 44 \ 27 \ 17 \ 12 \ 6 \end{array}$
1.8
 $\begin{array}{r} 1.88 \ 1.95 \ 1.7 \ 2.0 \ 11.4 \ 12.7 \ 13.4 \\ 6 \ 12 \ 18 \ 23 \ 39 \ 50 \ 60 \end{array}$

Sta.	T	H.I. ✓	-	Rod	Elev.
8+50		849.73			847.37
8+75					46.74
9+00					46.20
T.P.	2.17	847.87 ✓	4.05	845.68 ✓	
9+25					45.81
9+50					45.51
9+75					45.13
10+00					44.70
T.P.	3.16	847.67 ✓	3.36	844.51 ✓	
10+25					44.27
10+50					44.05
10+75					43.71
11+00					43.28
11+25					42.90
11+34					Cross Drain
11+50					42.80
11+63					Cross Drain

13.0 13.1 11.4 9.2 3.1 2.5 2.68 2.45 (2.4) 2.36 2.43 2.6 2.5 9.6 12.1 13.0 13.5 14.0
60 50 40 31 18 15 14 4 2.36 6 12 12 19 26 39 45 50 60

14.5 14.0 13.5 12.0 3.2 3.37 3.12 (3.0) 3.04 3.10 3.3 2.9 3.1 2.1 12.9 13.5 14.5
60 50 43 34 18 12 6 2.99 6 12 12 14 18 26 44 50 60

15.5 15.0 14.8 11.8 3.7 3.77 3.61 (3.5) 3.59 3.74 3.6 6.5 12.9 13.4 14.5 15.0
60 50 43 32 17 12 6 3.53 6 12 18 22 33 35 50 60

12.1 12.5 11.8 10.7 6.3 2.1 2.25 2.13 (2.1) 2.15 2.34 2.3 1.1 11.7 12.9 13.3 14.0
60 50 38 33 25 18 12 6 2.06 6 12 17 33 35 46 50 60

13.0 12.4 11.7 10.2 6.7 2.5 2.4 2.7 2.51 2.34 (2.4) 2.42 2.60 2.6 10.4 11.7 12.7 13.2
60 50 43 34 24 18 14 12 12 6 2.36 6 12 18 31 39 50 60

13.7 13.3 11.7 8.6 3.3 2.95 2.80 (2.7) 2.76 2.84 2.7 9.9 11.8 12.8
60 45 34 28 18 12 4 2.74 6 12 18 25 38 60

14.0 13.7 12.7 11.7 3.7 3.49 3.24 (3.2) 3.19 3.28 3.3 6.9 11.0 11.7 12.5 12.9
60 40 33 31 19 12 6 3.17 6 12 18 23 32 36 50 60

Nail in P.P. pt. 3.4. 16 + 4.5 (3.4) 3.44 3.60 3.8 6.4 11.5 12.6 13.0 13.0
60 50 41 31 24 19 12 6 3.40 6 12 19 22 32 42 50 60

13.0 12.8 12.9 11.4 7.7 4.3 4.24 3.70 (3.6) 3.63 3.95 4.2 4.0 6.7 11.4 13.5 14.0
60 50 42 31 26 19 12 6 3.62 6 12 12 18 22 31 40 60

14.0 13.7 13.3 11.4 8.8 4.8 4.66 4.04 (4.0) 3.96 4.30 4.3 6.5 11.4 12.1 12.8 13.0
60 50 40 31 26 19 12 6 3.96 6 12 18 22 29 38 50 60

14.0 13.7 13.3 11.4 8.7 5.0 5.12 4.61 (4.4) 4.38 4.67 4.8 7.5 11.4 13.5 13.5 14.0
60 50 40 29 24 17 12 6 4.39 6 12 18 24 30 40 50 60

11.2 11.4 12.2 11.4 8.1 5.7 5.23 4.95 (4.8) 4.84 4.99 5.0 6.0 8.6 10.9 11.4 13.3 14.0
60 50 41 30 23 19 12 6 4.77 6 13 18 22 26 31 32 50 60

12.0 11.4 10.8 11.0 11.7 5.7 5.4 5.74 5.15 (4.9) 4.83 5.18 5.3 9.0 10.6 11.5 12.0
60 54 49 51 24 18 14 11.2 6 4.87 6 13.2 19 25 36 47 60
13.04 35 15.27 29

Sta.	+	H. I. ✓	-	Rod	Elev
		847.67			
11+75					842.67
				9.5	Top of 36" Water Main Lt.
				<u>32</u>	
12+00				10.0	Top of 18" Water Main Lt.
				<u>32</u>	42.68
12+25					42.87
12+50					42.99
T.P.	57.11	848.01 ✓	4.77	842.90 ✓	
12+75					43.03
13+00					42.90
13+25					42.79
13+50					42.79
13+75					42.85
14+00					43.02
14+25					43.20
14+50					43.20
14+75					43.25

W.F.
140 13.3 11.4 9.9 6.9 5.6 5.65 5.18 (5.0) 5.00 5.19 6.0 6.9 8.3 9.8 11.5 11.0
 60 50 34 33 23 20 13 6 5.00 6 13 27 32 33 40 50 60

W.F.
13.6 13.4 13.4 12.5 11.4 8.3 5.5 5.51 5.10 (5.0) 5.05 5.39 5.8 6.2 7.0
 60 50 40 34 27 33 17 13 6 4.99 6 12.5 25 40 60

W.F.
15.0 14.0 11.4 8.3 5.8 5.35 4.85 (4.8) 4.94 5.26 5.0 5.5 5.9 6.3 6.5
 60 37 28 21 16 12 5 4.80 6 11 14 25 36 50 60

W.F.
14.0 13.7 11.4 10.7 8.7 5.9 6.3 5.43 4.77 (4.8) 4.73 5.06 4.9 5.6 5.9 9.5 11.1 11.1 10.2
 60 40 27 26 22 17 13 12 6 4.68 6 12 13 19 24 32 44 50 60

W.F.
13.0 13.3 14.3 14.3 11.8 9.1 5.8 5.3 5.30 5.10 (5.0) 5.02 5.44 5.2 5.6 8.2 10.6 11.3 11.7 10.4
 60 45 42 34 28 24 18 13 12 4 4.98 6 12 13 20 25 27 41 50 60

W.F.
11.8 11.2 11.7 11.5 13.3 11.7 9.0 5.9 5.35 5.74 5.35 (5.1) 5.12 5.43 5.3 5.2 6.4 9.0 10.3 11.5 11.7 11.1
 60 50 42 40 36 29 23 17 13 12 6 5.11 6 12 14 17 21 24 27 34 50 60

W.F.
12.0 12.1 12.6 11.8 9.2 6.0 5.25 5.33 (5.2) 5.22 5.30 5.2 5.4 11.7 12.4 11.7 12.2 11.5
 60 45 40 30 21 16 12 6 5.22 6 12 13 19 28 35 40 50 60

W.F.
13.0 12.6 13.1 11.8 6.3 5.9 6.16 5.47 (5.2) 5.20 5.33 5.3 6.9 11.7 12.6 12.5 13.0
 60 50 40 29 18 13 12 6 5.22 6 12 18 23 29 38 50 60

W.F.
12.8 13.0 11.8 8.4 5.6 5.5 5.61 5.30 (5.2) 5.19 5.31 5.4 6.9 11.3 11.7 11.6 11.9
 60 34 27 21 17 13 12 6 5.14 6 12 19 25 34 40 50 60

W.F.
10.7 11.5 11.2 10.7 5.3 5.35 5.05 (5.0) 5.04 5.15 5.4 10.9 11.2 11.3 11.1
 60 44 35 26 17 12 6 4.99 6 12 18 28 36 50 60

W.F.
8.7 8.3 6.2 4.9 4.8 5.00 4.87 (4.8) 4.84 4.96 5.3 9.0 9.7 9.7
 60 50 43 35 23 12 6 4.81 6 12 19 24 31 60

W.F.
4.9 4.8 4.7 4.7 4.74 4.86 (4.8) 4.85 4.92 4.7 5.1 8.2 8.8 8.6 8.9
 60 50 31 12 12 6 4.81 6 12 15 20 26 37 50 60

W.F.
4.8 4.7 5.0 4.9 4.91 4.77 (4.8) 4.86 4.95 5.1 6.5 7.8 8.0 8.3
 60 50 34 25 12 6 4.74 6 12 17 21 27 50 60

Sta.	+	H. I.	-	Rod	Elev.
15+00		848.01 ✓			843.32
15+25					43.43
15+50					43.57
B.M.	4.54	848.82 ✓	3.73	844.28 ✓	
15+75					43.72
16+00					43.86
16+25					44.00
16+50					44.09
16+75					44.16
17+00					44.20
17+25					44.17
17+50					44.08
17+55	Cross Drain				
17+75					43.95
18+00					43.82

4.8 5.0 5.1 6.7 6.7 4.7 4.5 4.76 4.71 (4.7) 4.77 4.90 5.2 5.0 5.4 5.6 5.9
6.0 5.0 3.6 3.2 2.8 2.5 1.7 1.2 6 4.69 6 1.2 1.2 1.8 3.0 3.0 6.0

4.7 4.7 5.0 6.6 6.5 4.9 4.65 4.61 (4.6) 4.66 4.74 4.8 4.6
6.0 5.0 3.5 3.1 2.6 2.3 1.2 4 4.58 6 1.2 2.3 3.6 1.14

4.7 4.6 4.5 6.1 6.1 5.0 4.7 4.54 4.43 (4.4) 4.49 4.55 4.5 4.5
6.0 5.0 3.5 3.0 2.5 2.3 1.1 1.1 6 4.44 6 1.3 2.2 3.7 1.14

SpK in P.P. Lt. Stop 16+11 (5.1)
5.3 5.2 5.1 6.7 6.6 5.3 5.22 5.17 (5.1) 5.15 5.22 5.2 4.9 5.6 6.1
6.0 5.0 3.4 3.0 2.4 2.3 1.1 6 5.10 6 1.3 2.5 3.0 5.0 6.0

5.5 5.5 5.1 7.0 6.7 5.3 5.14 5.05 (5.0) 4.98 4.98 4.8 5.3 6.2
6.0 5.0 3.5 3.1 2.4 2.4 1.2 6 4.96 6 1.2 2.9 5.0 6.0

old cellar

5.4 5.2 6.5 6.5 5.3 5.07 4.90 (4.8) 4.80 4.80 4.7 3.9 5.0 7.4 8.3
6.0 3.4 3.1 3.6 2.3 1.2 6 4.82 6 1.2 2.1 2.7 3.5 3.7 6.0

5.6 5.6 5.3 6.6 6.4 5.3 5.0 4.84 (4.7) 4.68 4.68 4.6 3.7 2.7 3.3 6.6 8.0 5.0
6.0 5.0 2.6 3.1 2.4 2.3 1.2 6 4.78 6 1.2 3.0 2.8 3.2 4.5 5.0 5.5 6.0
 36

5.5 5.3 5.3 6.3 6.4 5.4 4.9 4.76 (4.7) 4.66 4.68 5.0 6.1 7.0 7.6
6.0 4.7 3.4 3.1 2.6 2.4 1.2 6 4.66 6 1.2 2.6 3.7 5.0 6.0

5.2 5.2 6.8 6.3 5.3 4.82 4.69 (4.6) 4.63 4.67 4.5 4.2 4.8 7.0 8.1 8.4
6.0 3.6 3.1 2.6 2.4 1.2 6 4.62 6 1.2 1.7 2.2 3.3 3.9 5.0 6.0

5.3 5.1 5.1 6.4 6.4 5.1 4.75 4.68 (4.7) 4.68 4.74 4.5 5.0 5.6 6.6 7.9 8.6 9.1 9.3
6.0 3.0 3.5 3.4 2.4 2.4 1.2 6 4.65 6 1.2 1.6 2.1 2.3 3.1 3.9 4.6 5.0 6.0

(4.7)
5.2 5.4 6.7 6.7 5.2 4.9 4.90 4.81 (4.7) 4.82 4.92 4.6 5.3 4.8 10.5 10.6 10.0 9.9
6.0 3.4 3.3 2.7 2.4 1.7 1.2 6 4.74 6 1.2 1.4 2.0 2.5 3.2 4.0 5.0 6.0
 12.05
 28

5.5 5.5 5.8 7.4 7.2 5.5 5.01 4.92 (4.9) 4.91 5.00 5.4 10.6 11.8 12.1 9.2 10.1 10.2
6.0 5.0 3.6 3.3 2.7 2.4 1.2 6 4.87 6 1.2 2.0 2.9 3.0 3.2 3.4 5.0 6.0

5.8 6.0 6.0 7.5 7.5 5.7 5.18 5.08 (5.0) 5.03 5.10 5.4 10.3 11.7 12.0 10.1 10.4 9.9 10.3
6.0 5.0 3.6 3.3 2.7 2.3 1.2 6 5.00 6 1.2 1.8 3.0 3.1 3.3 3.4 4.0 5.0 6.0

Sta.	+	H.I. ✓	-	Rod.	Elev
18+25		848.82			843.70
18+50					43.57
T.P.	3.63	848.49 ✓	3.96	844.86 ✓	
18+75					43.46
19+00					43.39
19+25					43.31
19+46	Cross Drain				
19+50					43.27
19+75					43.58
20+00					43.59
20+25					43.17
20+50					43.42
20+75					44.10
21+00					44.33
21+25					44.68

$\frac{110}{60} \frac{104}{45}$
6.2 6.3 6.1 8.1 7.8 6.0 5.35 5.20 (5.1) 5.18 5.28 5.0 11.6 10.5 11.6 12.1 10.9 9.7
60 50 37 33 27 23 12 6 5.12 6 12 21 25 31 32 33 34 36
10.7 10.5 10.6
20 50 42

6.6 6.6 6.4 8.4 8.6 6.4 5.49 5.31 (5.2) 5.30 5.37 5.4 6.1 10.8 11.7 12.0 10.5 9.7
60 50 37 33 28 24 12 6 5.25 6 12 16 21 31 31 33 34 35

Nail in P.P. Lt. Star, 18+50 (5.0)
6.3 6.3 6.0 8.1 8.2 5.8 5.4 5.22 5.05 (5.0) 5.09 5.26 5.5 7.7 9.8 11.2 11.8 9.9 10.4 10.4 10.4
60 50 35 33 29 26 18 12 6 5.03 6 11.5 19 26 30 31 33 34 43 50 60

6.5 6.5 6.4 5.5 5.19 5.09 (5.1) 5.25 5.49 6.0 8.9 9.6 11.1 11.1 7.5 10.1 10.3
60 50 39 28 12 6 5.10 6 12 20 25 29 30 32 34 50 60

6.9 6.9 6.8 5.8 5.31 5.14 (5.2) 5.39 5.64 5.8 5.7 10.9 11.1 9.7 10.1 10.1
60 50 40 25 12 6 5.18 6 11.0 21 30 31 33 35 50 60
11.90 10.5

9.5 9.7 9.9 10.7 10.9 5.5 5.1 5.39 5.19 (5.2) 5.39 5.50 5.0 5.4 10.7 11.5 11.6 10.3 10.2 10.3
60 50 41 36 32 21 13 12 6 5.22 6 12 13 20 30 31 34 36 50 60

9.8 9.6 10.4 11.0 10.8 6.1 5.3 5.6 5.29 5.08 (4.9) 5.06 5.30 5.0 5.5 10.6 11.7 10.9 10.4 10.3
60 50 38 36 29 20 14 13 12 6 4.91 6 12 13 18 28 36 44 50 60

9.7 9.8 10.5 10.8 10.7 9.9 6.2 5.5 5.76 5.21 (4.9) 4.95 5.01 5.0 10.8 10.9 9.4 8.9 9.7
60 50 40 37 32 26 19 13 11 6 4.90 6 12 19 30 39 44 50 60

9.6 9.6 10.9 10.6 5.2 5.4 5.70 5.52 (5.3) 5.10 5.02 5.5 10.6 11.0 10.3 10.3 9.7 9.1
60 50 40 31 17 13 12 6 5.32 6 12 20 29 34 36 45 50 60

9.6 9.8 10.9 10.9 10.8 5.9 5.2 5.72 5.39 (5.1) 4.87 4.75 5.1 10.6 11.0 10.8 10.3 9.9 9.0
60 50 42 41 30 20 13 12 6 5.07 6 12 20 29 30 34 35 50 60

9.4 9.5 10.3 10.8 10.8 10.1 5.1 5.15 4.22 (4.4) 4.32 4.49 5.0 9.1 10.0 10.4 11.0 10.5 10.2 9.5 9.0
60 50 39 38 32 28 21 12 6 4.39 6 12 21 23 32 33 35 38 42 50 60

9.4 9.3 10.3 10.5 10.4 9.7 4.9 4.5 4.72 4.36 (4.2) 4.50 4.52 4.3 4.3 8.7 9.8 10.3 10.8 10.4 10.0 9.6 9.2
60 50 39 37 32 29 20 14 12 6 4.16 6 12 13 18 27 33 34 40 45 47 50 60

9.1 9.1 9.8 10.0 9.9 4.4 4.0 4.20 3.95 (3.8) 4.15 4.37 4.9 2.3 10.0 11.0 10.0 9.7
60 50 40 37 30 20 13 12 6 3.81 6 12 18 25 41 45 56 60

Sta. + H.I. ✓ - Rod Elev.

848.49

21+50 844.92

21+75 45.25

22+00 45.92

22+25 46.71

T.P. 6.53 852.78 ✓ 2.24 846.25 ✓

22+50 47.70

22+75 48.77

23+00 49.73

23+25 50.73

23+50 51.75

23+75 52.58

T.P. 7.57 859.86 ✓ 0.49 852.29 ✓

24+00 53.51

24+25 54.44

24+50 55.36

T.P. 9.94 866.19 ✓ 3.61 856.25 ✓

87 90 93 97 93 4.1 3.6 3.73 3.57 3.6 3.76 4.16 3.8 3.6 8.7 10.4 11.1 10.4 9.7
60 50 43 36 30 22 15 12 6 3.57 6 12 13 19 27 34 41 51 60

85 75 89 86 3.4 2.7 3.12 3.16 3.7 3.72 3.67 3.3 3.7 10.3 11.4 10.4 9.9 9.8
60 50 37 31 19 14 12 6 3.24 6 12 15 22 29 39 46 48 60

82 82 80 82 7.6 2.8 2.2 2.60 2.42 3.6 2.72 2.91 2.9 7.3 9.1 9.9 10.4 9.8
60 50 40 33 28 21 14 12 6 2.57 6 12 18 24 31 42 49 60

74 73 74 7.5 6.7 1.4 1.4 1.57 1.61 1.8 2.05 2.30 2.0 1.8 6.4 8.7 9.6 9.8 9.9
60 50 38 31 27 19 13 12 6 1.78 6 12 13 17 24 32 40 53 60

10.9 10.7 10.4 9.6 5.2 4.85 4.95 5.29 5.71 5.5 5.7 10.4 12.7 14.0 14.0
60 50 34 26 20 12 6 5.08 6 12 14 17 25 34 50 60

93 87 91 86 4.5 3.81 3.88 4.32 4.66 4.4 8.3 9.4 12.2 13.2 13.5 13.7
60 50 34 26 20 12 6 4.01 6 12 17 23 26 31 40 50 60

4.9 5.5 5.9 7.1 6.9 5.3 3.2 3.3 2.94 2.79 3.22 3.45 3.2 3.9 7.9 12.6 13.1 13.1 13.2
60 50 35 34 27 24 19 12 12 6 3.05 6 12 13 18 25 33 41 50 60

2.6 2.7 2.8 3.7 5.5 5.5 4.9 3.7 1.9 2.02 2.04 2.19 2.34 2.2 2.6 6.8 9.2 11.0 12.0 12.1
60 50 44 39 32 31 22 22 14 12 6 2.05 6 12 13 18 24 31 37 50 60

0.9 0.3 1.2 1.1 1.15 1.05 1.0 1.09 1.19 1.0 1.1 5.2 6.8 9.2 10.4 10.5
60 50 34 15 12 6 1.03 6 12 12 18 24 26 31 50 60

0.5 0.6 0.5 0.3 0.44 0.29 0.20 0.25 0.1 0.0 6.4 6.9 7.9 8.9
60 50 32 14 12 6 0.20 6 11 13 18 24 38 50 60

8.3 8.6 8.8 8.8 6.6 6.4 6.58 6.41 6.4 6.40 6.46 6.3 6.5 10.4 10.9 10.1 11.7 13.3 13.8 14.9
60 50 40 26 19 14 13 6 6.35 6 11 14 19 23 26 27 35 44 50 60

1.7 3.2 5.8 6.8 6.8 5.9 5.3 5.47 5.44 5.4 5.38 5.57 5.9 8.4 8.6 6.9 8.0 9.5 11.1 12.2
4.6 3.3 2.3 2.2 2.1 2.1 1.4 1.2 6 5.42 6 7.1 18 20 23 24 34 42 50 60

0.5 1.0 4.0 4.2 4.9 4.3 4.57 4.50 4.5 4.53 4.64 4.50 4.8 6.7 6.7 3.6 3.2 5.8 7.8
3.5 2.9 2.6 2.3 2.2 2.1 1.2 4 4.50 6 7.1 13 17 20 21 24 32 45 60

Sta.	+	H.I. ✓	-	Rod	Elev.
		866.19 55 86			
24+25					
24+50					
24+75					856.29
25+00					57.16
25+25					58.09
25+50					59.14
25+75					60.16
26+00					61.19
T.P.	13.11	878.68 ✓ 59 86	0.62	865.57 ✓	
24+50					
24+75					
25+00					
25+25					
25+50					

$$\begin{array}{r} 5.2 \quad 6.9 \\ \hline 60 \quad 50 \end{array}$$

16.8

$$\begin{array}{r} 0.0 \quad 1.3 \quad 4.5 \\ \hline 50 \quad 47 \quad 39 \end{array}$$

10.8

$$\begin{array}{r} 3.7 \quad 9.5 \quad 10.1 \quad 10.6 \quad 10.6 \quad 10.0 \quad 10.02 \quad 9.96 \\ \hline 40 \quad 32 \quad 24 \quad 22 \quad 21 \quad 20 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} 9.94 \quad 10.1 \quad 9.9 \quad 10.8 \quad 11.9 \quad 11.95 \quad 1.46 \quad 5.6 \quad 6.3 \quad 6.8 \\ \hline 7.90 \quad 6 \quad 11 \quad 17 \quad 20 \quad 22 \quad 23 \quad 28 \quad 31 \quad 40 \quad 50 \quad 60 \end{array}$$

9.9

$$\begin{array}{r} 2.9 \quad 7.6 \quad 9.5 \quad 9.9 \quad 9.9 \quad 9.3 \quad 9.15 \quad 9.09 \\ \hline 38 \quad 27 \quad 24 \quad 23 \quad 22 \quad 21 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} 9.09 \quad 9.17 \quad 9.2 \quad 10.1 \quad 10.7 \quad 8.0 \\ \hline 9.03 \quad 6 \quad 11 \quad 17 \quad 19 \quad 23 \quad 24 \end{array}$$

9.0

$$\begin{array}{r} 2.4 \quad 6.6 \quad 8.6 \quad 9.2 \quad 8.1 \quad 7.9 \quad 8.12 \quad 8.09 \\ \hline 36 \quad 28 \quad 25 \quad 21 \quad 19 \quad 14 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} 8.15 \quad 8.23 \quad 8.3 \quad 8.6 \quad 10.0 \quad 6.6 \\ \hline 8.10 \quad 6 \quad 11 \quad 20 \quad 21 \quad 24 \quad 26 \end{array}$$

8.10

$$\begin{array}{r} 2.7 \quad 3.4 \quad 7.1 \quad 7.6 \quad 8.5 \quad 8.5 \quad 7.0 \quad 6.9 \quad 7.16 \quad 7.09 \\ \hline 35 \quad 31 \quad 25 \quad 23 \quad 22 \quad 21 \quad 19 \quad 14 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} 7.07 \quad 7.12 \quad 7.0 \quad 8.4 \quad 9.0 \quad 5.3 \quad 1.3 \\ \hline 7.05 \quad 6 \quad 11 \quad 17 \quad 20 \quad 24 \quad 28 \quad 33 \end{array}$$

7.1

$$\begin{array}{r} 0.0 \quad 1.1 \quad 2.1 \quad 6.1 \quad 7.4 \quad 7.4 \quad 5.9 \quad 5.8 \quad 6.07 \quad 6.02 \\ \hline 41 \quad 37 \quad 30 \quad 24 \quad 22 \quad 21 \quad 19 \quad 14 \quad 13 \quad 6 \end{array} \quad \begin{array}{r} 6.04 \quad 6.13 \quad 6.0 \quad 6.0 \quad 7.9 \quad 7.8 \quad 3.0 \quad 2.7 \quad 1.4 \\ \hline 6.03 \quad 6 \quad 11 \quad 12 \quad 13 \quad 19 \quad 23 \quad 28 \quad 39 \quad 47 \end{array}$$

6.0

$$\begin{array}{r} 0.1 \quad 1.1 \quad 2.0 \quad 6.8 \quad 6.8 \quad 5.1 \quad 5.07 \quad 5.01 \\ \hline 46 \quad 38 \quad 30 \quad 24 \quad 22 \quad 19 \quad 13 \quad 7 \end{array} \quad \begin{array}{r} 5.10 \quad 5.18 \quad 4.8 \quad 4.8 \quad 7.2 \quad 7.1 \quad 3.0 \quad 3.4 \quad 2.9 \quad 1.2 \\ \hline 5.00 \quad 5 \quad 10 \quad 14 \quad 19 \quad 20 \quad 25 \quad 28 \quad 43 \quad 50 \quad 64 \end{array}$$

5.0

$$\begin{array}{r} 8.5 \quad 9.5 \quad 12.8 \\ \hline 70 \quad 60 \quad 50 \end{array}$$

23.3

$$\begin{array}{r} 5.8 \quad 5.8 \quad 4.0 \\ \hline 68 \quad 60 \quad 55 \end{array}$$

22.4

$$\begin{array}{r} 4.2 \quad 3.4 \quad 1.4 \quad 0.6 \\ \hline 70 \quad 65 \quad 60 \quad 55 \end{array}$$

21.5

$$\begin{array}{r} 10.7 \quad 11.4 \quad 12.5 \\ \hline 35 \quad 50 \quad 60 \end{array}$$

$$\begin{array}{r} 2.9 \quad 2.9 \quad 3.4 \\ \hline 70 \quad 60 \quad 53 \end{array}$$

20.6

$$\begin{array}{r} 9.1 \quad 10.2 \quad 11.5 \quad 12.7 \\ \hline 37 \quad 41 \quad 50 \quad 60 \end{array}$$

19.5

$$\begin{array}{r} 4.3 \quad 3.7 \quad 3.1 \quad 3.5 \quad 3.8 \\ \hline 70 \quad 67 \quad 63 \quad 60 \quad 49 \end{array}$$

$$\begin{array}{r} 8.1 \quad 9.4 \quad 9.8 \quad 11.2 \\ \hline 38 \quad 45 \quad 50 \quad 60 \end{array}$$

Sta.	+	H. I.	-	Rod	Elev.
		878.68			
25+75					
26+00					
	4.14	869.71	13.11	865.57	
26+25					862.11
26+32					862.31
26+50					63.05
B.M.			7.87	261.84	

18.5

<u>4.8</u>	<u>4.8</u>	<u>4.2</u>	<u>4.7</u>	<u>8.5</u>	<u>9.7</u>
70	60	54	49	50	60

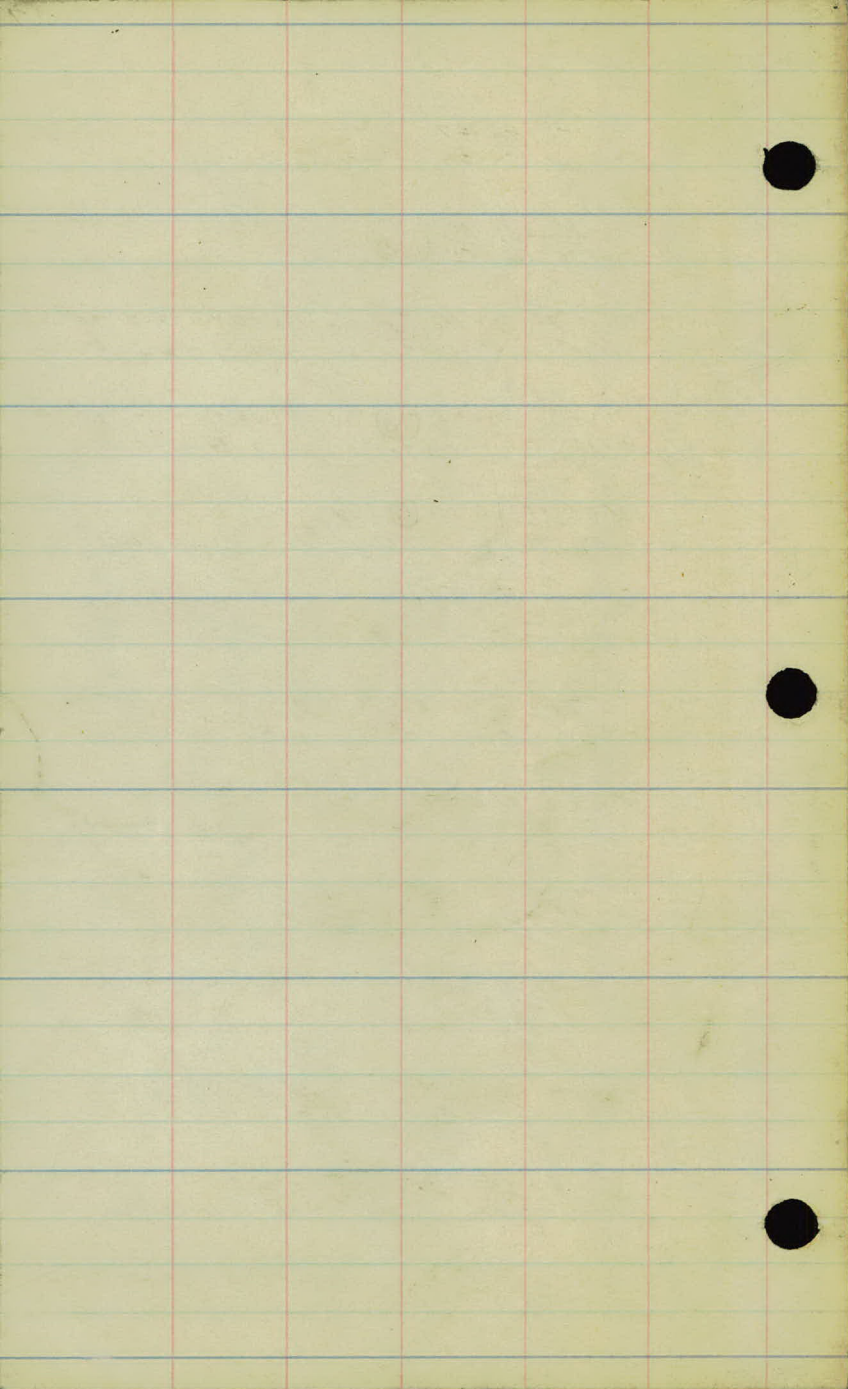
<u>9.1</u>	<u>8.8</u>	<u>9.0</u>	17.5
70	60	52	

<u>3.4</u>	<u>4.5</u>	<u>5.6</u>	<u>6.6</u>	<u>7.5</u>	<u>7.69</u>	<u>7.65</u>	7.6	<u>7.65</u>	<u>7.75</u>	<u>7.6</u>	<u>7.4</u>	<u>7.3</u>	<u>7.1</u>	<u>7.0</u>
60	50	38	28	18	15 ^s	6	7.60	6	10 ^s	11	21	52	50	60

<u>5.0</u>	<u>5.9</u>	<u>6.3</u>	<u>7.2</u>	<u>7.3</u>	<u>7.49</u>	<u>7.40</u>	7.4	<u>7.42</u>	<u>7.49</u>	<u>7.3</u>	<u>7.2</u>	<u>7.1</u>	<u>7.0</u>	<u>7.0</u>
60	45	34	25	15	15 ^s	6	7.40	6	10 ^s	11	24	36	50	60

<u>5.9</u>	<u>6.2</u>	<u>6.1</u>	<u>6.5</u>	<u>6.84</u>	<u>6.74</u>	6.7	<u>6.70</u>	<u>6.77</u>	<u>7.2</u>	<u>8.6</u>	<u>8.6</u>	<u>8.1</u>	<u>8.1</u>	<u>8.0</u>
60	50	37	24	15 ^s	6	6.66	6	10 ^s	20	21	27	38	50	60

SpN in Arc Light Pole 17. Sta. 25+91.



U 2506