

PLANS SURVEY

EAST AVE.

From Co. Rd. A to No. St. Paul Road.

Sta. 0+00 to 47+70.40

County Proj. 27-75

Road % N^o 75

File N^o 12

3-7-27

12

PROJ. 27-75

Alignment.

East Ave.

From Co. Rd. 4. to No St. Paul Road

From Sta. 0+00 to 47+70.4

Received 2-26-27
C. J. [Signature]

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed

3-7-27

File No.

17

Station	Point	Δ Lt.	Δ Rt.	Calc. Bearing	Magn Bearing
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76+40.7	P.I.	0°40' Lt.			
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13+48 ⁸⁰	P.O.T.				
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0+00					
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2-11-27

H.A. Wisbuser

D.S.

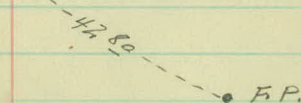
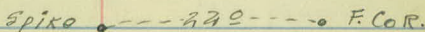
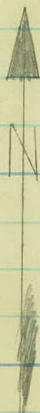
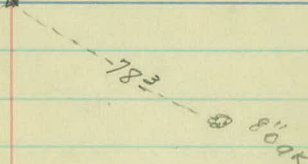
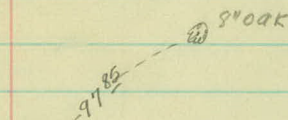
A.B.

F.M.

cold. Windy

N.E. 1/4 Sec 13

Stone Mont.

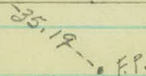
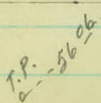
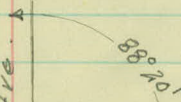


East Ave.

S.W. Cor. 13

Stone Mont.

Co. Rd. A.



Station Point A Lt. A Rt. Cal. Bearing Mag. Bearing

47+70.4

End of Project.

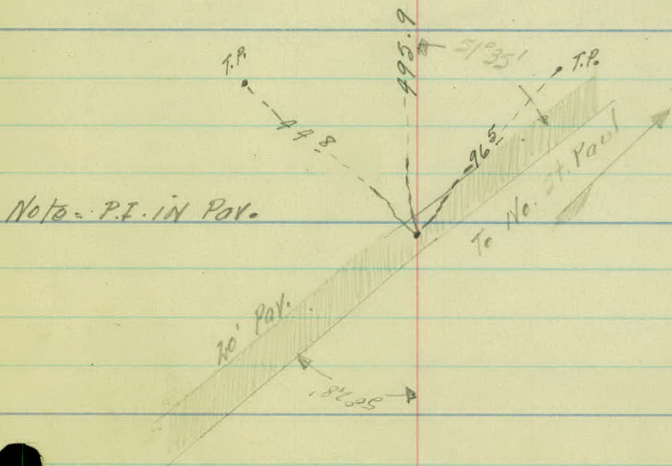
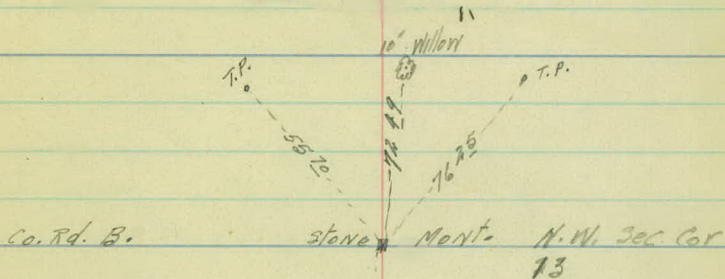
26 40.7
21 29.7
4 95.9

2625.4

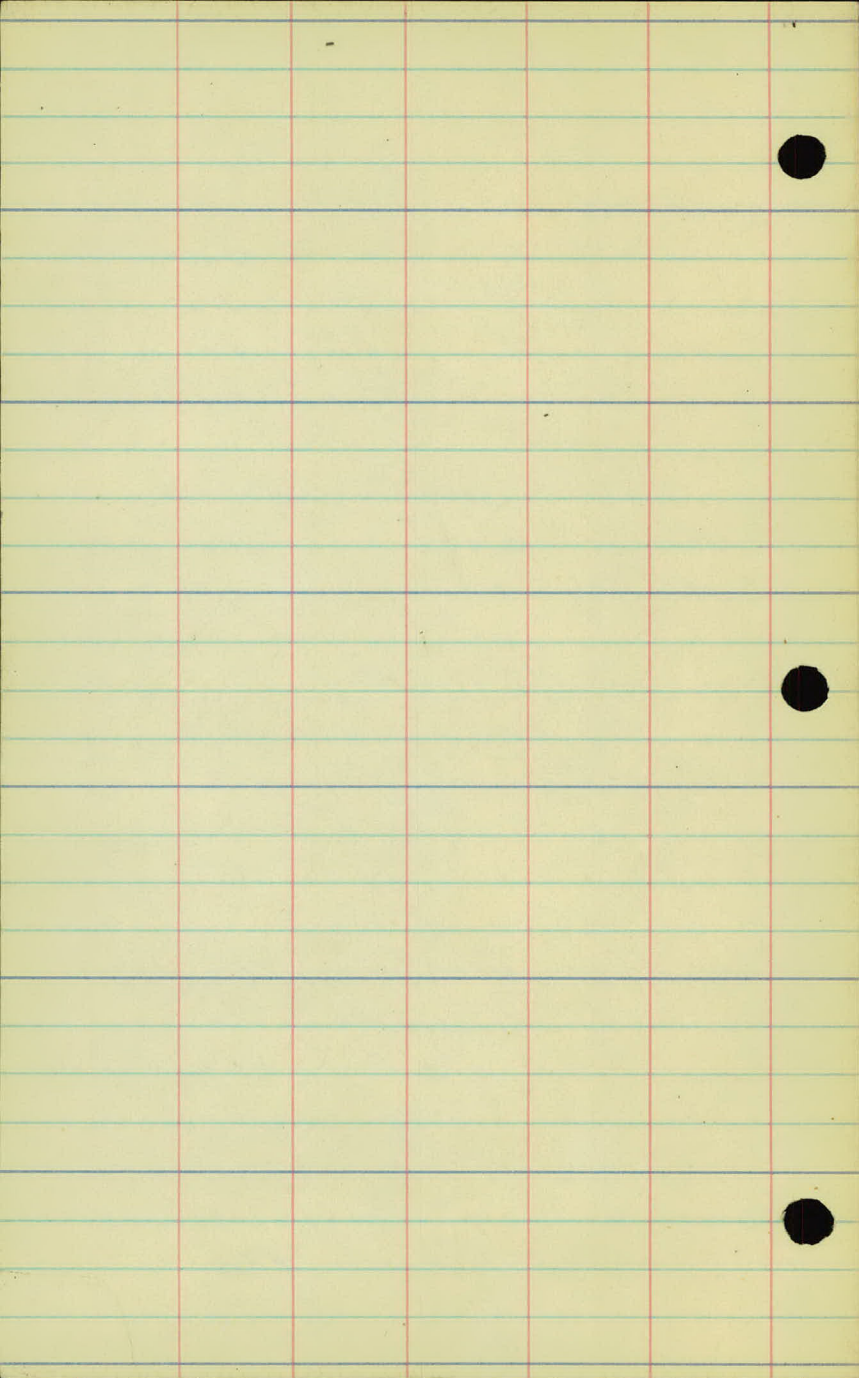
2-11-27

H.A. Wilhousan
D.S.
P.B.
A.M.

Cold-Windy



Note - P.I. IN Pav.



Topography
East Ave.
From Co. Rd. H. to No. St. Paul Rd.
From Sta 0+00 to 47+70.4

Road bed
Lt. Rt.

6+00

5+00

9' 8'

4+00

3+00

2+00

1+00

8' 10'

+7 1/2

30' X 12" C.M.
Cross drain

0+00

Road bed
Lt. Rt.

13+00

12+00

11+00

10+00

7' 5'

+67 $\frac{1}{2}$ drive Lt.

9+00

8+00

7+00

12' 11'

Cultivated

Cultivated

Cultivated

X X X F.V.E. Cor 22'

F. 24'

F. 25'

F. 22'

F. 19'

+76 M. by 9'

F. 20'

F. 23'

+76 Tree 15'

F. 15'

150 E. Orchard 27'

Roost
360' x 51.9' x 50'

orchard

164 Bldg Orchard 30'

154 F.P. 22'



Meadow

Meadow

roadbed
Lt. Rt.

20+00

5'

7'

19+00

18+00

17+00

+94 $\frac{1}{2}$ drive Rt.

16+00

15+00

7'

7'

14+00

Cultivated

Cultivated

Cultivated

Orchard

Orchard

Waste land

orchard 35'

+96 orchard 32' and 52'

orchard 49'

+80 orchard 30'

+64 B. Orchard 20'



Roadbed
Ht. Rt.

27+00

+37

Road Rt
Not graded
20' x 15" CM. 20'

26+00

25+00

9'

9'

24+00

23+00

22+00

7'

8'

21+00

x x x x

104 F. Cor. 20'

x

Golf Course

x

15 72'

x

x

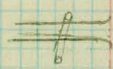
x x x x

153 F. Cor. 25'

147 Cult. 20'

127 Cult. 18'

Cultivated



102 M. 24' 7"

170 F. 24'

Cultivated

Waste lands & Woodland

Cultivated

124 R. Orchard 35'

Roadbed
Lt Rt.

32+00

33+00

34+00

7' 8'

31+00

130 $\frac{1}{2}$ FE Lt.

30+00

8' 7'

29+00

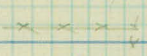
28+00

10' 6'

+81 Tree 30'

+88 F Cor. 16'
F 16'

yard



F 17'

y

F 18'

x

Golf Course

+87 Tree 19'
+25 Tree 20'

+82-2 Trees 22'

+60 Tree 29'
+44 Tree 31'

+25-2 Trees 18'

feature



+74 F Cor. 22'



o

+72 Tree 27'

+75 2 Trees 28'

Collected



Golf Course

Roadbed
14' Rt.

4100

4000

+04

4 CROSS CULV
33x24' C.M.

3900

9'

9'

+96

3800

3700

3600

10'

9'

+65

4 FE HT.

22' x 12' C.M.

3500

+12 T.P. 20'

Cultivated

E Meadow
+92 T.P. 21'

lots
Golf Course Property
+76 +85

+55 across E
of fourth Ave



Meadow

+60 E Orchard 20

+09 T.P. 22'

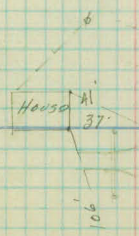
+57 T.P. 2A P.P.
+36 B. Orchard 33

+18 Car. House 37'

+99 Car. House 37'
30 x 18'

+20 E. Coll.

Yard



+50 Tree 20'

+06 N. pr. 9'

+96 Tree 23

+20 Street
+16 Tree 23

+06 Tree 20

Golf Course

Road bed
Lt Rt.

48+00

47+00

191
E of cross culv.
31' x 15" C.M. 12' Lt 19' Rt.

46+00

45+00

9' 12'

44+00

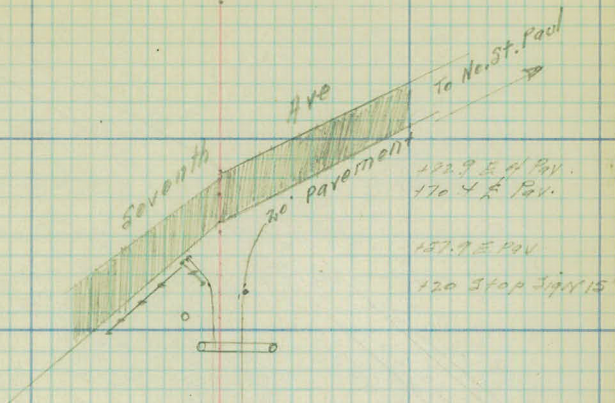
783
E F.E. Rt.

43+00

42+00

10' 10'

134 G.R. 21
124 G.R. 9
109 T.P. 18'



122.9 E of Pav.
170.4 S of Pav.

157.9 E of Pav.
120 Stop Sign 15'

157 T.P. 18'

lots
167 Lot Iron 33

110 T.P. 18'
E of Cult.

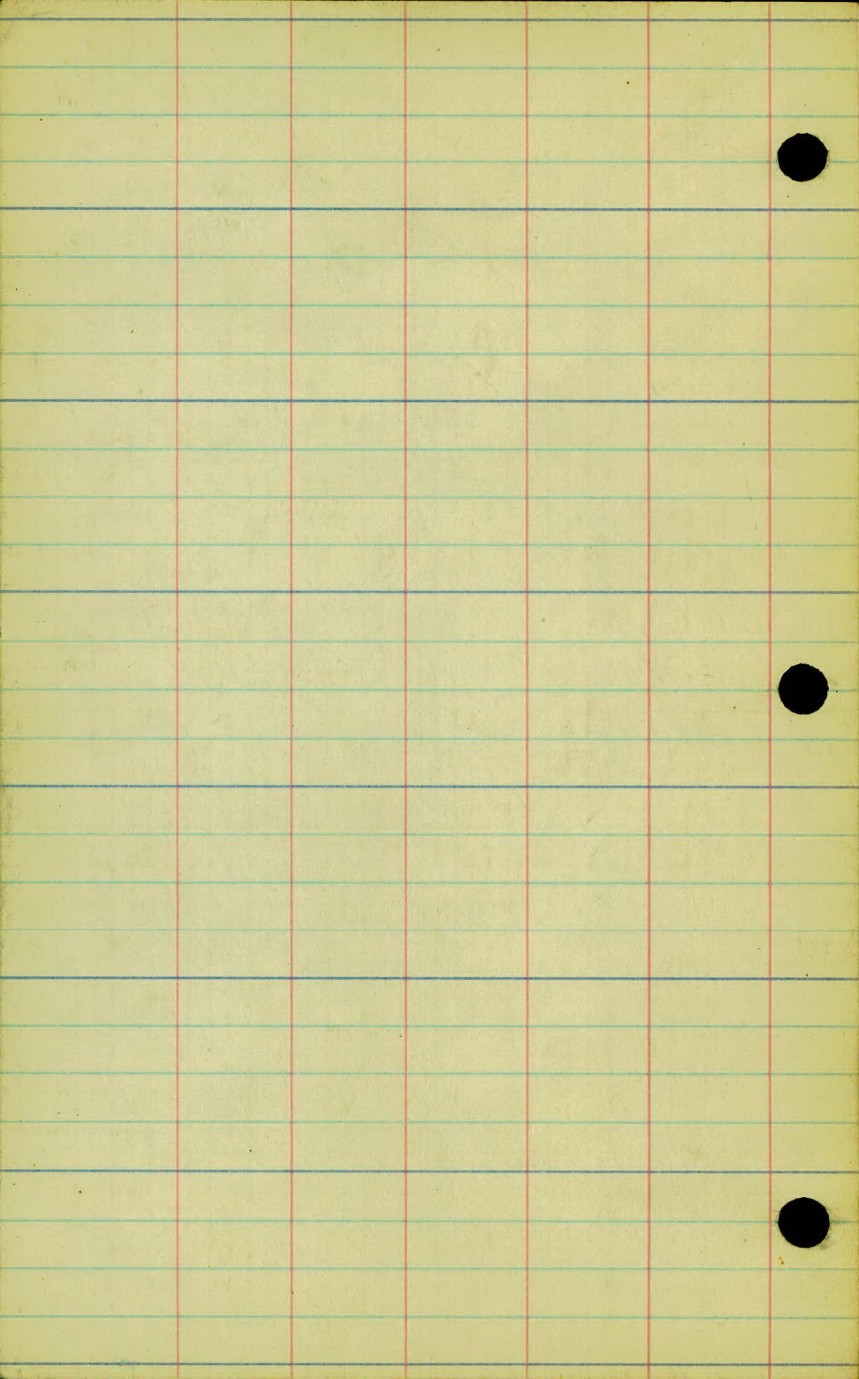
Meadow

lots

100 T.P. 18'

Cultivated

lots



Cross sections.

East Ave.

From Co. Rd. A to No. St. Paul Road

From Sta. 0+00 to 47+70.4

Station	Top - Elev.
0+00	10 20.9 .
+10	20.6 .
+23	20.1 .
+50	19.6 -
1+00	19.0 .
+50	18.9 .
2+00	19.4 .
+50	19.6 .
+75	19.6 .
3+00	19.3 .
+50	18.5 .
+75	17.3 18.3
4+00	16.5 .

sandy clay

2

Lt.

±

Rt.

		27	28	28		30	32	34	
L.O		33	19	5	2.9	12	25	33	L.O

	24	35	33	30		34	36	37	38
	33	26	20	11	3.3	6	16	26	33

L.O

	46	46	42	40	35		43	23	27
	33	29	26	20	9	3.6	6	19	33

	75	80	70	47		45	5.6	85	84	86
	33	26	16	9	4.2	4	8	13	16	33

L.O

	88	88	86	53		51	8.7	85	8.7
	33	25	15	6	4.8	5	16	23	23

L.O

	83	85	90	85	55		5.4	80	8.2	86	83
	33	22	19	16	9	4.9	9	14	20	26	33

L.O

	78	75	68	64	55	48		48	46	43	20
	33	28	25	19	11	9	4.4	9	15	19	33

	43	98	92	94	90		90	93	94	94	80	3.8	24
	33	19	14	11	5	9.0	3	8	11	16	21	27	33

L.O

	84	82	76	90		84	84	82	28	2.2
	33	19	15	10	9.0	15	17	20	29	33

	58	52	97	94		97	8.7	8.7	8.2	32	2.7
	33	21	15	10	9.3	11	15	17	20	28	33

	52	64	106	103	102		105	101	10.4	98	9.5
	33	21	14	10	5	10.1	11	12	14	24	33

	50	65	110	113		117	115	116	105	114	116
	33	21	14	9	11.2	9	12	14	16	23	33

R.O

	1.8	34	72	68	67		70	13	68	62	6.7	75	48
	3.3	19	14	9	5	6.6	9	10	11	14	16	22	33

Station + or - Elev. Soil

+50 15.7

5+00 15.3

+50 15.3

6+00 15.6

+50 16.3

7+00 17.7

+50 19.5

8+00 22.2

+40 23.9

9+00 25.6

+50 26.4

10+00 26.3

+50 25.6

2-17-27 L Rt Windy. cold.

76 78 82 82 76 80 10.4 11.4 11.7
 L.O. 33 28 18 12 6 75 7 16 26 33

9.4 100 98 74 70 6.9 100 10.5
 L.O. 33 22 16 12 9 6.4 7 15 33

L.O

103 103 92 81 70 6.8 7.7 100 106 10.7
 33 22 13 12 10 6.5 8 9 12 35 33
25

101 100 95 8.7 70 6.5 7.1 95 10.2 10.3
 L.O. 33 30 16 14 9 6.1 7 9 18 22 22

L.O

96 96 95 6.2 8.7 6.4 9.0 9.8 10.8 10.4
 33 24 17 10 3.4 9 10 12 17 24 33

8.2 6.8 4.7 4.5 7.7 8.0 8.2
 33 17 12 4.0 7 13 17 33

35 37 3.4 2.8 2.4 2.5 2.1 3.4 3.6
 33 27 18 14 4.2 7 11 14 29 33

52 50 73 9.7 9.7 9.3 9.5 100 100 90 8.2 4.2 50
 33 23 21 16 14 6 9.2 8 11 13 14 17 21 33

3.1 3.5 3.5 8.3 7.2 7.2 7.5 8.0 8.0 7.0 4.0 3.5 3.6
 33 23 21 15 5 4 7.4 10 11 13 14 19 20 33

2-18-27

3.8 3.8 4.2 6.4 5.8 6.2 3.8 4.2 4.4
 33 27 21 15 5 5.9 11 17 25 33 Cold

3.7 3.2 3.2 5.2 5.2 5.3 5.7 4.8 3.5 4.2
 33 21 18 9 6 5.2 5 9 13 16 33

50 48 50 5.6 5.6 5.4 5.3 5.7 5.7 5.0 4.9 4.0 3.5
 33 21 17 13 10 9 5.3 5 8 12 13 16 17 33

70 6.4 6.4 6.4 6.0 6.0 6.4 5.2 3.5 3.5
 33 22 22 13 8 6 8 12 7 14 33

Station	+ 0 V.	Elev.	Soil
11+00		24.9.	
	+50	24.4.	
12+00		24.1.	
	+50	23.8.	
13+00		23.5.	
	+50	22.8.	
14+00		21.7	
		<u>26.7</u>	
	+50	20.5.	
15+00		18.9.	
	+50	16.6.	
16+00		14.4	
		<u>14.3</u>	
	+50	11.7.	
17+00		09.0.	

2-18-27 Lt.

Wilshusen

D.S.

4.B.

A.M.

Rt.

Cold.

10	$\frac{82}{33}$	$\frac{81}{28}$	$\frac{84}{18}$	$\frac{84}{14}$	$\frac{71}{9}$	66	$\frac{65}{6}$	$\frac{78}{11}$	$\frac{65}{15}$	$\frac{64}{21}$	$\frac{54}{33}$	10
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$\frac{82}{33}$	$\frac{82}{28}$	$\frac{85}{17}$	$\frac{85}{11}$	$\frac{85}{10}$	$\frac{75}{9}$	72	$\frac{75}{7}$	$\frac{82}{14}$	$\frac{80}{19}$	$\frac{80}{29}$	$\frac{80}{33}$
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10	$\frac{82}{2}$	$\frac{85}{24}$	$\frac{85}{18}$	$\frac{85}{12}$	$\frac{85}{8}$	$\frac{72}{6}$	75	$\frac{75}{2}$	$\frac{78}{7}$	$\frac{76}{13}$	$\frac{85}{17}$	$\frac{85}{33}$	10
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$\frac{83}{33}$	$\frac{82}{26}$	$\frac{85}{17}$	$\frac{81}{9}$	$\frac{78}{7}$	7.8	$\frac{7.8}{4}$	$\frac{7.7}{9}$	$\frac{80}{12}$	$\frac{8.8}{22}$	$\frac{9.1}{33}$
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$\frac{84}{33}$	$\frac{84}{26}$	$\frac{84}{14}$	$\frac{88}{13}$	$\frac{88}{9}$	$\frac{82}{8}$	8.2	$\frac{82}{10}$	$\frac{85}{12}$	$\frac{90}{16}$	$\frac{98}{20}$	$\frac{104}{32}$
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$\frac{84}{33}$	$\frac{84}{15}$	$\frac{87}{14}$	$\frac{88}{9}$	$\frac{82}{7}$	$\frac{87}{5}$	8.8	$\frac{90}{13}$	$\frac{94}{14}$	$\frac{94}{15}$	$\frac{86}{16}$	$\frac{86}{28}$	$\frac{88}{33}$
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$\frac{75}{33}$	$\frac{84}{14}$	$\frac{100}{13}$	$\frac{102}{8}$	$\frac{98}{5}$	$\frac{98}{3}$	9.8	$\frac{9.8}{7}$	$\frac{102}{15}$	$\frac{8.8}{18}$	$\frac{85}{27}$	$\frac{90}{33}$
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$\frac{98}{33}$	$\frac{100}{23}$	$\frac{100}{16}$	$\frac{116}{13}$	$\frac{114}{8}$	$\frac{110}{4}$	11.0	$\frac{112}{5}$	$\frac{113}{9}$	$\frac{117}{13}$	$\frac{102}{14}$	$\frac{98}{22}$	$\frac{100}{33}$
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$\frac{25}{33}$	$\frac{30}{16}$	$\frac{40}{15}$	$\frac{44}{11}$	$\frac{36}{8}$	3.4	6	$\frac{34}{9}$	$\frac{36}{13}$	$\frac{40}{14}$	$\frac{26}{21}$	$\frac{22}{23}$	$\frac{27}{33}$
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$\frac{54}{33}$	$\frac{54}{16}$	$\frac{65}{14}$	$\frac{66}{10}$	$\frac{57}{7}$	5.7	$\frac{5.8}{7}$	$\frac{61}{12}$	$\frac{63}{13}$	$\frac{54}{14}$	$\frac{5.3}{23}$	$\frac{47}{33}$
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$\frac{78}{33}$	$\frac{78}{16}$	$\frac{82}{13}$	$\frac{84}{9}$	8.0	$\frac{81}{7}$	$\frac{86}{11}$	$\frac{86}{13}$	$\frac{74}{14}$	$\frac{70}{33}$
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$\frac{104}{33}$	$\frac{106}{16}$	$\frac{116}{13}$	$\frac{117}{11}$	$\frac{107}{8}$	10.6	$\frac{10.8}{8}$	$\frac{114}{13}$	$\frac{102}{14}$	$\frac{10.4}{24}$	$\frac{10.4}{33}$
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$\frac{27}{33}$ $\frac{35}{33}$ $\frac{43}{11}$ $\frac{35}{12}$ $\frac{35}{4}$ 3.4 $\frac{35}{3}$ $\frac{39}{7}$ $\frac{38}{15}$ $\frac{36}{15}$ $\frac{38}{33}$

Station + or - Elev. Soil

+50 96.7

18+00 94.5

+50 92.3

19+00 99.9

+50 97.4

20+00 94.8

+40 92.7

21+00 90.1

+50 88.5

22+00 87.1

+50 85.6

23+00 84.5

+50 83.3

+50 84.3

lean

hard

Waldhusen
 D.S. ✓
 H.B.
 H.M.
 Lt. Rt. clear. cold

2-18-27

43 54 64 70 65 58 60 65 60 61 59
 33 17 16 12 9 7 58 7 13 14 24 33 40

63 22 87 90 80 83 88 90 82 82 86
 23 17 15 9 8 80 10 11 13 14 19 33

94 100 115 115 105 108 110 105 105 107
 33 16 13 11 9 102 10 11 16 18 33

30 32 43 44 32 31 33 38 30 28 26
 33 16 15 12 8 31 4 10 12 12 21 33

42 50 68 58 55 59 64 65 50 48 44
 33 16 13 9 6 55 11 13 15 16 21 33

64 67 22 22 85 81 82 84 92 72 55
 33 27 17 14 30 5 82 7 12 14 15 33
 10

74 85 103 107 100 105 115 102 95
 33 18 15 10 8 10.3 11 15 17 33

15 27 37 40 33 35 43 47 47
 33 18 17 12 9 3.2 10 13 27 33

44 55 64 60 55 51 55 68 77 79
 33 17 15 13 10 7 4.8 11 13 20 33

33 40 44 43 34 32 41 56 57 57
 33 18 17 14 11 3.1 8 11 13 18 33

L.O.

57 57 57 57 55 50 48 65 65
 33 25 20 16 12 10 4.4 10 13 33

78 77 75 65 62 75 76 74
 33 18 14 10 56 10 13 19 33

90 90 90 82 75 90 95 100 105 ditch
 33 28 26 14 11 6.8 10 12 15 26 28 29 30
 120
 120
 30
 C. d. 105
 31 102/30

Station	Top -	Elev.	Soil
24+00		82.2	
	+50	81.4	
25+00		80.7	
	+50	78.8	
26+00		77.3	
	+27	76.5	
	+37	76.3	
	+47	75.9	
27+00		74.8	
	+40	75.6	
28+00		72.4	
	+50	72.0	
29+00		72.4	

Lt.

H. W. Johnson
D.S.
R.B.
A.M. Rt.

clear cold

2-18-27

100 98 97 84 87 10.8 115 117 123 133
33 17 13 10 9 11 14 23 24 25

120 120
26 23

90 100 100 96 90 92 120 123
33 24 18 14 11 87 6 12 33

100 12 28 30 70 72 66 65 90 75 88 96 100
33 27 23 17 14 13 7 4 6.4 9 14 21 29 32

26 50 55 72 90 82 82 86 85 10.4
33 26 21 17 14 5 82 8 12 21 32

78 85 92 98 107 105 100 9.8 11.0 120 117 12.6
33 27 22 17 16 13 10 5 8 15 22 32

25 25 24 30 27 30 32 3.4 37 65 65 53
33 18 13 9 6 2.0 5 10 15 20 23 24 25

ditch

5.3 8
32

2.8 33 38 37 36 31 3.2 35 26 3.6
33 27 16 12 10 5 4 12 20 33

33 47 42 43 35 35 3.8 4.0 5.6 31 5.3 5.7 5.4
33 24 17 13 10 7 3.4 7 14 20 21 23 28 33

ditch

4.3 47 62 66 50 57 51 4.8 5.0 6.2 6.7 7.0 7.0 5.2
33 26 24 20 16 15 11 4.6 5 10 16 17 18 20

ditch

4.3
33

7.4 7.5 2.7 7.6 6.2 5.7 6.0 6.4 7.6 7.9 5.7 4.5
33 29 20 14 11 6 5.8 5 11 12 16 20 33

9.3 9.2 8.5 7.0 7.4 9.7 10.0 10.5
33 17 13 8 7.1 6 12 16 33

7.7 7.8 8.5 8.5 7.5 7.8 8.8 11.0 11.5 11.7 12.0
33 27 19 13 8 7.4 6 9 14 17 24 33

6.4 5.0 10.2 10.8 11.0 10.5 11.5 12.0 13.3 15.0 16.3 16.3
33 27 20 15 10 4 10.7 7 6 11 18 26 27

Station	tor -	Elev.	Soil
	+25	72.4 .	
		72.6	
	+55	(72.7)	
		72.7	
	+75	(71.1)	
30+00		72.4 .	
	+25	72.1 .	
	+75	71.1 .	
31+00		70.5 .	
		69.4	
	+50	(69.7)	
32+00		68.1 .	
	+50	67.5 .	
33+00		67.2 .	
	+50	67.5 .	
34+00		68.2 .	

4.

H.A. Wilshusen
D.S.
P.B.
H.M. Rt.

clear. cold.

2-18-27

$\frac{25}{33}$ $\frac{40}{22}$ $\frac{66}{18}$ $\frac{80}{17}$ $\frac{107}{11}$ $\frac{100}{6}$ 10.5 11.2 13.8 16.0 16.4

$\frac{57}{33}$ $\frac{45}{26}$ $\frac{35}{18}$ $\frac{78}{15}$ $\frac{105}{11}$ $\frac{104}{8}$ 10.5 $\frac{10.8}{8}$ $\frac{11}{13}$ $\frac{12.2}{18}$ 13.7 15.6 33

$\frac{72}{33}$ $\frac{58}{21}$ $\frac{104}{15}$ $\frac{107}{11}$ $\frac{102}{7}$ 10.5 $\frac{10.6}{8}$ $\frac{12}{11}$ $\frac{11.7}{23}$ 13.3 33

$\frac{75}{33}$ $\frac{27}{16}$ $\frac{107}{8}$ 10.7 $\frac{10.7}{9}$ $\frac{68}{13}$ $\frac{7.4}{21}$ 12.7 33

$\frac{87}{33}$ $\frac{70}{19}$ $\frac{66}{16}$ $\frac{80}{13}$ $\frac{80}{7}$ $\frac{80}{5}$ 7.9 $\frac{8.1}{8}$ $\frac{40}{14}$ $\frac{44}{24}$ 6.6 33

$\frac{98}{33}$ $\frac{86}{20}$ $\frac{82}{16}$ $\frac{94}{14}$ $\frac{90}{9}$ 8.9 $\frac{90}{8}$ $\frac{65}{15}$ $\frac{5.8}{16}$ 4.5 4.5 33

$\frac{108}{33}$ $\frac{100}{21}$ $\frac{75}{15}$ $\frac{101}{13}$ $\frac{98}{10}$ $\frac{94}{7}$ 9.5 $\frac{96}{7}$ $\frac{94}{12}$ $\frac{78}{15}$ 6.6 6.0 33

$\frac{120}{33}$ $\frac{124}{27}$ $\frac{120}{17}$ $\frac{118}{12}$ $\frac{112}{10}$ $\frac{107}{8}$ 10.6 $\frac{10.5}{7}$ $\frac{10.6}{10}$ $\frac{11.2}{17}$ 10.4 33

$\frac{64}{33}$ $\frac{66}{21}$ $\frac{67}{13}$ $\frac{49}{7}$ 4.8 $\frac{5.1}{6}$ $\frac{5.7}{11}$ $\frac{6.3}{16}$ $\frac{5.8}{27}$ 5.4 33

$\frac{78}{33}$ $\frac{82}{18}$ $\frac{77}{13}$ $\frac{56}{8}$ 5.4 $\frac{5.7}{9}$ $\frac{7.2}{12}$ $\frac{6.5}{22}$ 33

$\frac{54}{33}$ $\frac{90}{20}$ $\frac{87}{15}$ $\frac{60}{9}$ 5.7 $\frac{6.4}{9}$ $\frac{8.4}{14}$ $\frac{7.8}{16}$ 7.4 33

$\frac{80}{33}$ $\frac{60}{21}$ $\frac{74}{13}$ $\frac{58}{10}$ $\frac{54}{6}$ 5.5 $\frac{5.5}{9}$ $\frac{6.8}{13}$ $\frac{6.7}{22}$ 6.0 33

$\frac{55}{33}$ $\frac{40}{14}$ $\frac{50}{13}$ $\frac{60}{10}$ 4.8 $\frac{50}{11}$ $\frac{57}{19}$ $\frac{55}{31}$

Station	Hor-	Elev.	Soil
175		68.4	
+55		68.1	
+90		67.8	
35+00		67.5	
+50		66.9	
36+00		66.3	
+50		64.9	
37+00		64.1	
		<u>62.1</u>	
+50		63.1	
38+00		62.1	
+25		61.6	
+75		60.7	

2-19-27 17.

Milwaukee
25
4.8
4.11

R.T.

100	92	80	93	97	96	98	96	86	82	45	12	1.0
33	27	16	11	7	4	96	9	13	15	20	21	33

B.P.T.

97	88	96	100	98	100	90	65	22	18	1.0
33	16	13	9	98	6	11	15	23	27	41

B.P.T.

112	106	97	103	103	102	103	96	80	50	35	26
33	26	15	13	7	102	7	10	15	16	24	33

B.P.T.

117	116	110	106	105	105	84	72	73	
33	21	17	12	10.5	5	9	13	14	33

2-23-27

40	33	40	42	41	35	45	
33	16	12	3	4.4	10	12	30

42	42	45	49	47	36	45	6.2	
33	25	15	10	4.9	8	10	16	33

46	48	64	60	59	62	55	60	64	76
33	22	15	10	5.9	8	11	13	17	33

64	65	62	70	75	70	73	72	95	80	75	82	
33	24	20	14	12	8	7.0	7	12	16	19	22	33

75	72	73	81	81	85	83	80	85	85	76	90	
33	21	17	13	10	8.1	8	10	12	15	18	21	33

96	96	85	95	90	92	100	10.8	102	10.8	
33	17	15	12	8	8.9	7	10	12	19	33

102	102	96	100	10.8	11.2	12.0	
33	13	10	9.6	8	11	13	33

112	105	105	107	12.0	133	137	
33	16	10	10.5	8	13	24	33

Station	+ or -	Elev.		Soil
39+00		60.3.		
+35		60.0.	59.9	
40+00		59.7.	59.6	✓
+50		60.0.	59.9	
			6	
41+00		60.1.	60.0	
		59.8		
+50		(59.9)	59.7	
42+00		60.1.	60.0	
+50		59.6.	59.5	
43+00		59.1.	59.0	
+28	↕ -05	58.6.	58.5	
+50		58.0.	57.9	
+50		57.7.	57.6	
44+00		57.6.	57.5	

clay

Gravel

2-23-27 Lt.

W. Wilhozen
0.5
#8 Rt.
8.71.

$\frac{130}{33}$ $\frac{12.2}{16}$ $\frac{10.8}{8}$ 11.0 $\frac{11.3}{8}$ $\frac{12.7}{14}$ $\frac{15.5}{17}$ $\frac{13.8}{38}$

$\frac{9.8}{33}$ $\frac{9.5}{19}$ $\frac{8.6}{13}$ $\frac{6.5}{8}$ 6.5 $\frac{7.0}{9}$ $\frac{8.5}{13}$ $\frac{8.2}{19}$ $\frac{7.5}{28}$ $\frac{7.0}{33}$

$\frac{8.5}{33}$ $\frac{9.0}{19}$ $\frac{9.0}{13}$ $\frac{7.0}{8}$ 6.7 $\frac{7.0}{16}$ $\frac{8.5}{12}$ $\frac{8.5}{18}$ $\frac{8.5}{23}$ $\frac{7.5}{24}$ $\frac{6.2}{33}$

$\frac{8.0}{33}$ $\frac{7.8}{26}$ $\frac{8.4}{22}$ $\frac{7.8}{15}$ $\frac{7.0}{9}$ $\frac{5.6}{6}$ 6.4 $\frac{6.4}{11}$ $\frac{7.7}{14}$ $\frac{7.6}{18}$ $\frac{7.3}{23}$ $\frac{5.5}{30}$ $\frac{5.4}{33}$

$\frac{8.2}{33}$ $\frac{7.8}{17}$ $\frac{7.7}{12}$ $\frac{6.8}{7}$ 6.4 $\frac{6.5}{4}$ $\frac{6.7}{9}$ $\frac{7.7}{15}$ $\frac{7.0}{16}$ $\frac{6.2}{20}$ $\frac{4.8}{33}$

$\frac{7.8}{33}$ $\frac{6.6}{14}$ $\frac{7.6}{13}$ $\frac{7.6}{11}$ $\frac{6.6}{7}$ 6.7 $\frac{6.6}{8}$ $\frac{7.0}{11}$ $\frac{7.0}{12}$ $\frac{5.6}{14}$ $\frac{3.5}{16}$ $\frac{2.5}{26}$ $\frac{1.5}{33}$

$\frac{8.2}{33}$ $\frac{7.0}{15}$ $\frac{9.0}{14}$ $\frac{9.0}{12}$ $\frac{8.4}{10}$ 8.2 $\frac{8.0}{16}$ $\frac{7.5}{13}$ $\frac{4.2}{17}$ $\frac{3.5}{27}$ $\frac{3.2}{33}$

$\frac{8.0}{33}$ $\frac{8.4}{17}$ $\frac{9.4}{14}$ $\frac{8.8}{11}$ 8.6 $\frac{8.8}{11}$ $\frac{9.2}{13}$ $\frac{8.5}{16}$ $\frac{7.5}{18}$ $\frac{7.0}{33}$

$\frac{8.2}{33}$ $\frac{8.2}{17}$ $\frac{9.7}{15}$ $\frac{9.7}{13}$ $\frac{9.2}{11}$ 9.2 $\frac{9.2}{11}$ $\frac{9.6}{13}$ $\frac{9.4}{14}$ $\frac{8.0}{17}$ $\frac{7.2}{19}$ $\frac{6.2}{25}$ $\frac{6.5}{33}$

$\frac{7.0}{33}$ $\frac{7.2}{18}$ $\frac{10.4}{15}$ $\frac{10.4}{13}$ $\frac{9.8}{10}$ 9.7 $\frac{9.8}{11}$ $\frac{10.2}{12}$ $\frac{10.2}{13}$ $\frac{9.0}{15}$ $\frac{6.6}{18}$ $\frac{7.4}{33}$

$\frac{7.4}{33}$ $\frac{8.7}{18}$ $\frac{10.7}{15}$ $\frac{10.4}{12}$ $\frac{10.2}{9}$ 10.7 $\frac{10.5}{10}$ $\frac{10.7}{13}$ $\frac{10.4}{14}$ $\frac{9.6}{17}$ $\frac{10.0}{33}$

$\frac{11.8}{33}$ $\frac{12.8}{21}$ $\frac{12.2}{14}$ $\frac{10.8}{11}$ 10.6 $\frac{10.8}{11}$ $\frac{11.0}{16}$ $\frac{11.0}{33}$

$\frac{6.4}{33}$ $\frac{6.6}{25}$ $\frac{6.7}{14}$ $\frac{4.7}{9}$ 3.8 $\frac{3.9}{9}$ $\frac{5.4}{12}$ $\frac{5.4}{14}$ $\frac{4.6}{28}$ $\frac{4.2}{33}$

Station	top-	Elev.	Soil
+50		56.1	57.0
45+00		57.3	57.2
+50		56.8	56.7
46+00		56.5	56.4
+50		56.0	55.9
47+00		56.4	56.3
+22		56.8	56.7
+60	Edge	58.6 Pav.	58.5
47+70 ±		58.67	58.7

2/23/27 Lt.

Wichuson
D.S. RT Fair. Warm
A.M.

$\begin{array}{r} 70 \\ 23 \end{array}$ $\begin{array}{r} 66 \\ 14 \end{array}$ $\begin{array}{r} 44 \\ 9 \end{array}$ $\begin{array}{r} 43 \\ 4.3 \end{array}$ $\begin{array}{r} 42 \\ 10 \end{array}$ $\begin{array}{r} 56 \\ 15 \end{array}$ $\begin{array}{r} 54 \\ 22 \end{array}$ $\begin{array}{r} 46 \\ 30 \end{array}$ $\begin{array}{r} 36 \\ 31 \end{array}$ $\begin{array}{r} 33 \\ 33 \end{array}$

$\begin{array}{r} 68 \\ 28 \end{array}$ $\begin{array}{r} 68 \\ 27 \end{array}$ $\begin{array}{r} 64 \\ 13 \end{array}$ $\begin{array}{r} 43 \\ 9 \end{array}$ $\begin{array}{r} 42 \\ 4.2 \end{array}$ $\begin{array}{r} 41 \\ 10 \end{array}$ $\begin{array}{r} 56 \\ 15 \end{array}$ $\begin{array}{r} 58 \\ 23 \end{array}$ $\begin{array}{r} 46 \\ 30 \end{array}$ $\begin{array}{r} 35 \\ 31 \end{array}$ $\begin{array}{r} 32 \\ 33 \end{array}$

$\begin{array}{r} 66 \\ 22 \end{array}$ $\begin{array}{r} 62 \\ 12 \end{array}$ $\begin{array}{r} 47 \\ 9 \end{array}$ $\begin{array}{r} 46 \\ 4.6 \end{array}$ $\begin{array}{r} 46 \\ 10 \end{array}$ $\begin{array}{r} 60 \\ 15 \end{array}$ $\begin{array}{r} 58 \\ 22 \end{array}$ $\begin{array}{r} 54 \\ 29 \end{array}$ $\begin{array}{r} 44 \\ 30 \end{array}$ $\begin{array}{r} 41 \\ 33 \end{array}$

$\begin{array}{r} 78 \\ 38 \end{array}$ $\begin{array}{r} 72 \\ 20 \end{array}$ $\begin{array}{r} 65 \\ 11 \end{array}$ $\begin{array}{r} 50 \\ 7 \end{array}$ $\begin{array}{r} 49 \\ 4.9 \end{array}$ $\begin{array}{r} 60 \\ 11 \end{array}$ $\begin{array}{r} 60 \\ 15 \end{array}$ $\begin{array}{r} 56 \\ 22 \end{array}$ $\begin{array}{r} 56 \\ 28 \end{array}$ $\begin{array}{r} 41 \\ 13 \end{array}$ $\begin{array}{r} 38 \\ 30 \end{array}$ $\begin{array}{r} 38 \\ 33 \end{array}$

$\begin{array}{r} 83 \\ 38 \end{array}$ $\begin{array}{r} 84 \\ 18 \end{array}$ $\begin{array}{r} 55 \\ 7 \end{array}$ $\begin{array}{r} 53 \\ 5.3 \end{array}$ $\begin{array}{r} 58 \\ 11 \end{array}$ $\begin{array}{r} 66 \\ 16 \end{array}$ $\begin{array}{r} 65 \\ 22 \end{array}$ $\begin{array}{r} 60 \\ 30 \end{array}$ $\begin{array}{r} 58 \\ 22 \end{array}$

$\begin{array}{r} 84 \\ 32 \end{array}$ $\begin{array}{r} 84 \\ 18 \end{array}$ $\begin{array}{r} 80 \\ 11 \end{array}$ $\begin{array}{r} 53 \\ 6 \end{array}$ $\begin{array}{r} 50 \\ 5.0 \end{array}$ $\begin{array}{r} 48 \\ 4 \end{array}$ $\begin{array}{r} 50 \\ 13 \end{array}$ $\begin{array}{r} 64 \\ 19 \end{array}$ $\begin{array}{r} 64 \\ 33 \end{array}$

$\begin{array}{r} 35 \\ 34 \end{array}$ $\begin{array}{r} 78 \\ 24 \end{array}$ $\begin{array}{r} 74 \\ 15 \end{array}$ $\begin{array}{r} 47 \\ 7 \end{array}$ $\begin{array}{r} 47 \\ 4.7 \end{array}$ $\begin{array}{r} 45 \\ 4 \end{array}$ $\begin{array}{r} 43 \\ 13 \end{array}$ $\begin{array}{r} 62 \\ 20 \end{array}$ $\begin{array}{r} 62 \\ 33 \end{array}$

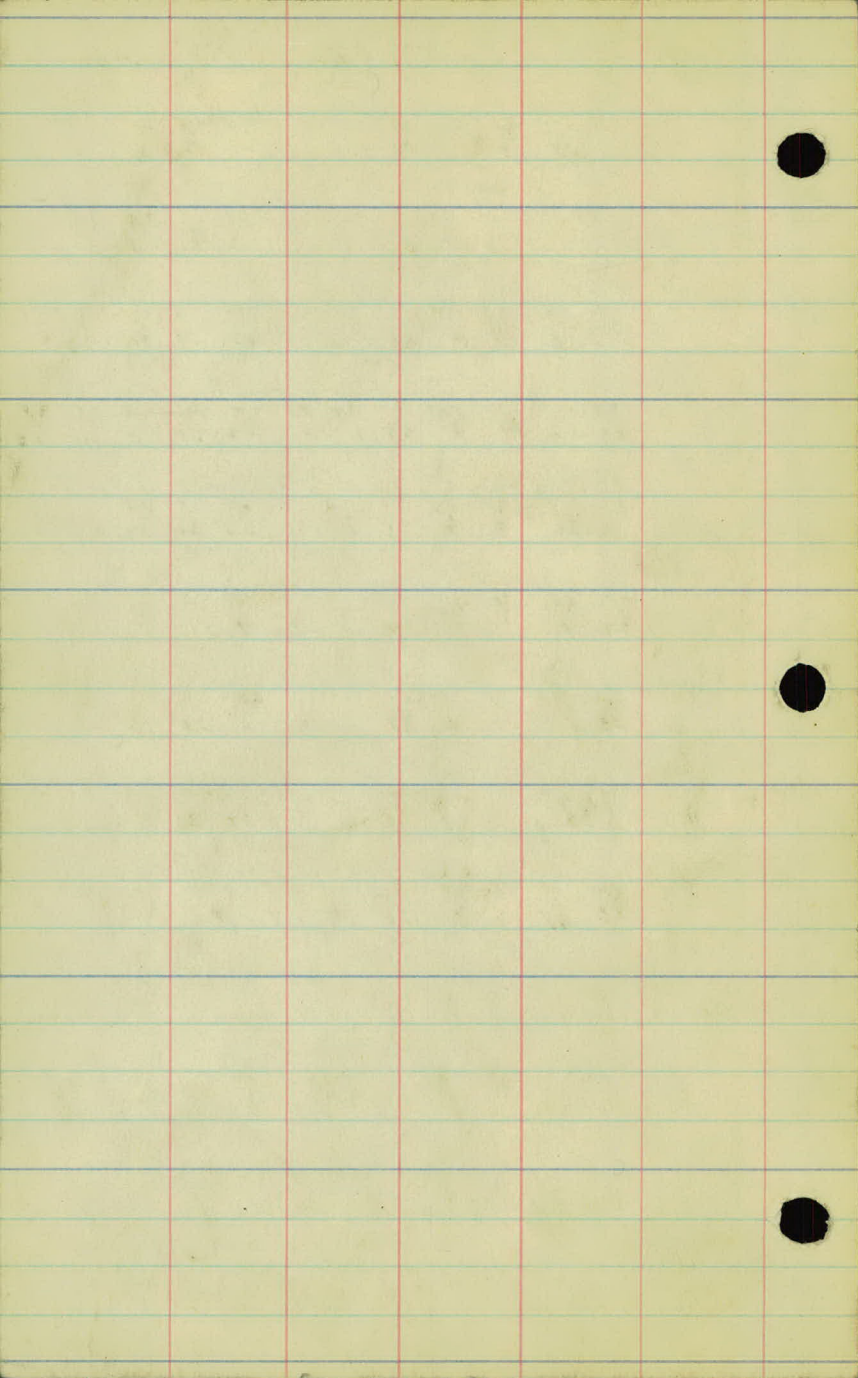
K.POV PAU.

$\begin{array}{r} 32 \\ 33 \end{array}$ $\begin{array}{r} 31 \\ 30 \end{array}$ $\begin{array}{r} 29 \\ 14 \end{array}$ $\begin{array}{r} 28 \\ 2.8 \end{array}$ $\begin{array}{r} 27 \\ 5 \end{array}$ $\begin{array}{r} 24 \\ 20 \end{array}$ $\begin{array}{r} 50 \\ 27 \end{array}$ $\begin{array}{r} 42 \\ 33 \end{array}$

K.POV

K.POV

$\begin{array}{r} 42 \\ 33 \end{array}$ $\begin{array}{r} 38 \\ 27 \end{array}$ $\begin{array}{r} 30 \\ 22 \end{array}$ $\begin{array}{r} 28 \\ 15 \end{array}$ $\begin{array}{r} 28 \\ 2.6 \end{array}$ $\begin{array}{r} 25 \\ 16 \end{array}$ $\begin{array}{r} 75 \\ 25 \end{array}$ $\begin{array}{r} 47 \\ 38 \end{array}$



2-16-27

W.L. Wisnason cloudy - cold
D.S.
F.S.
A.M.

Spike in 8" oak 50' N. Stg. 27+80

Station	B.2.	H.1.	F.S.	Red.	Elev.
		172.26			
+50				5.8	67.5
33+00				6.1	67.2
+50				5.8	67.5
34+00				5.1	68.2
+25				4.9	68.4
+55				5.2	68.1
+80				5.5	67.8
35+00				5.8	67.5
+25				6.2	67.1
+50				6.9	66.9
36+00				7.0	66.3
+50				8.4	64.9
37+00				9.2	64.1 63.7
+50				10.2	63.1
38+00				11.2	62.1
+25				11.9	61.6
+75				12.6	60.7
39+00				13.0	60.3
T.P.	<u>3.2</u>	<u>965.1</u> <u>965.18</u>	11.60		961.66
+35				5.2	59.9 60.0 59.6
40+00				5.5	59.7 59.9
+50				5.2	60.0
41+00				5.1	60.0 60.1
+50				5.4	59.7 59.8
43+00				5.1	60.0 60.1
+50				5.6	59.5 59.6

2-16-27

W.L. Nicholson cloudy-cool

6.5
7.8
P.M.

Station	B.S.	I.S.	Red.	Elev.
		965.14		59.0
		(45.18)		59.1
13+00			71	57.9
+50			72	58.0
+83			73	57.6
14+00			75	57.7
+20			76	57.5
				57.6
45+00			81	(26.1) 57.0
+50	23.40	982.87	79	57.2
	4.21	1869		57.3
B.M.	1869	96518.0	84	56.8 56.7
	check # 2.11	(1.27)		963.70 ✓
46+00			87	56.4
+50			92	56.5
				55.9
47+00			88	56.0
+22				56.3
+87.9			94	56.4
+78				56.7
+82.9			66	56.8
100 ft			295	58.5
Rec "				58.6
300 "			640	58.67
5+50				58.7
				58.8
T.P.	10.75	969.44	76	57.6
				54.6
100 "			76	56.5
200 "			76	56.6
300 "			71	56.0
400 "			71	56.1
				56.0
				56.1
				6.43
100 "			90	758.69 ✓
200 "			67	60.4
300 "			40	67.7
400 "			0.70	65.4
				68.5

2-16-27

Wishusen cloudy-cold

D.S.

F.B.

A.M.

Spike in 18" oak 90 ft. Sta. 41+42

Edge of Pavement.

1/2 of Pavement

Edge of " " "

1/2 of Seventh Ave Top of Pavement

" " " " " "

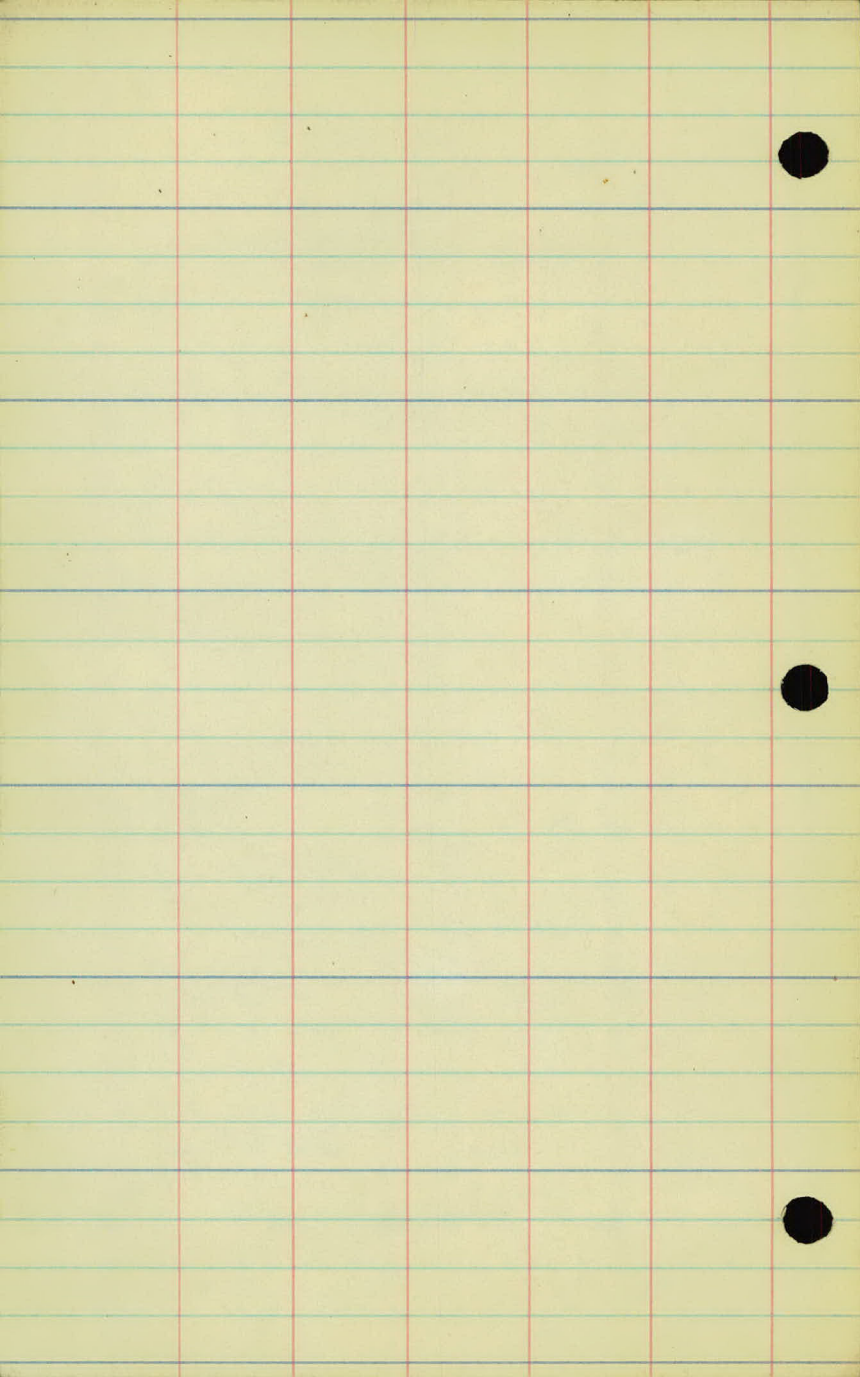
" " " " " "

Top of pavement 1/2 7th Ave

" " "

" " "

" " "



C. Hoffman
72 18

Check levels
East Ave

From the Int of Frost
Ave and White Bear Ave
top of Mont.

Station	B.S.	I.I.	F.S.	Elev.
B.M.	9.76	976.63		966.87
T.P.	4.73	969.81	11.55	965.08
T.P.	12.56	974.82	7.55	962.26
T.P.	8.82	982.58	1.06	973.76
T.P.	8.00	990.06	0.52	982.06
T.P.	2.95	991.79	2.22	997.52
T.P.	2.57	997.51	6.85	998.92
T.P.	11.10	998.39	0.22	997.29
T.P.	0.19	999.1	11.47	996.92
T.P.	0.31	976.67	10.23	976.16
T.P.	6.36	968.02	12.02	963.16
T.P.	9.16	967.99	6.39	957.63
B.M.			3.77	963.72
T.P.	7.43	968.41	6.51	960.90
T.P.	7.20	975.36	0.35	968.06
T.P.	11.35	984.93	1.78	973.58
B.M.			8.21	976.72
T.P.	13.16	996.97	1.12	983.81
T.P.	13.21	1009.11	1.07	995.90
T.P.	13.21	1021.79	0.53	1008.58
T.P.	9.27	1029.44	1.62	1020.17
B.M.			6.10	1023.34
T.P.	0.09	1023.74	5.79	1023.65
T.P.	4.88	1024.29	4.33	1019.41
B.M.			4.39	1019.90

2014-27

Snow-cold

Top of Stone Mont. White Bear Ave
and Co. Rd 17th

71.79	967.49
<u>64.65</u>	<u>914</u>
7.14	976.63 CHK H.L.W

Spike in 8" oak 90' RT 27+42

26.08	967.49
<u>864</u>	<u>1749</u>
1174	984.93 CH.H.L.W

Spike in 8" oak 50' RT 57+30

48.85	984.93
<u>434</u>	<u>44.51</u>
44.51	1029.44 CHECK H.L.W.

rail in P.P. 50' RT 13+48

10.12	1029.44
<u>497</u>	<u>8.15</u>
515	1024.29 CHK H.W.

Spk. in 10" oak 70' RT 37+50

Station	B.S.	I.I.	F.S.	Elev.	
			1024.29		
T.P.	2.50	1022.05	4.74	1019.55	
T.P.	8.68	1030.11	0.56	1021.49	11.12 5.30
B.M.			6.75	1023.36	5.82
T.P.	0.66	1021.66	9.11	1021.00	1030.11 CK H.L.W.
T.P.	0.09	1010.62	11.13	1010.53	
T.P.	0.15	997.47	13.30	997.32	
T.P.	0.52	985.94	12.05	985.42	
B.M.			9.28	976.66	976.72
T.P.	1.71	975.43	12.22	972.72	
T.P.	0.51	969.20	6.74	968.69	
B.M.			5.50	963.70	963.72
T.P.	0.09	963.49	5.80	963.40	
T.P.	12.15	975.53	0.11	963.38	
T.P.	11.51	986.01	1.03	974.50	
T.P.	11.44	997.16	0.29	985.73	
T.P.	2.43	975.74	3.85	993.31	
T.P.	2.97	990.85	7.86	987.88	
T.P.	6.85	976.74	5.96	984.89	
T.P.	2.93	990.13	3.94	987.80	
T.P.	0.08	979.20	11.61	979.12	
T.P.	0.27	969.22	10.25	968.95	
T.P.	10.78	971.62	8.38	960.84	
T.P.	3.61	975.07	0.16	971.46	
B.M.			8.24	966.85	

2-14-27

W. L. ...
L. ...
A. ...
A. ...

Spike in F.P. 50' Rt. Sta. 13+48

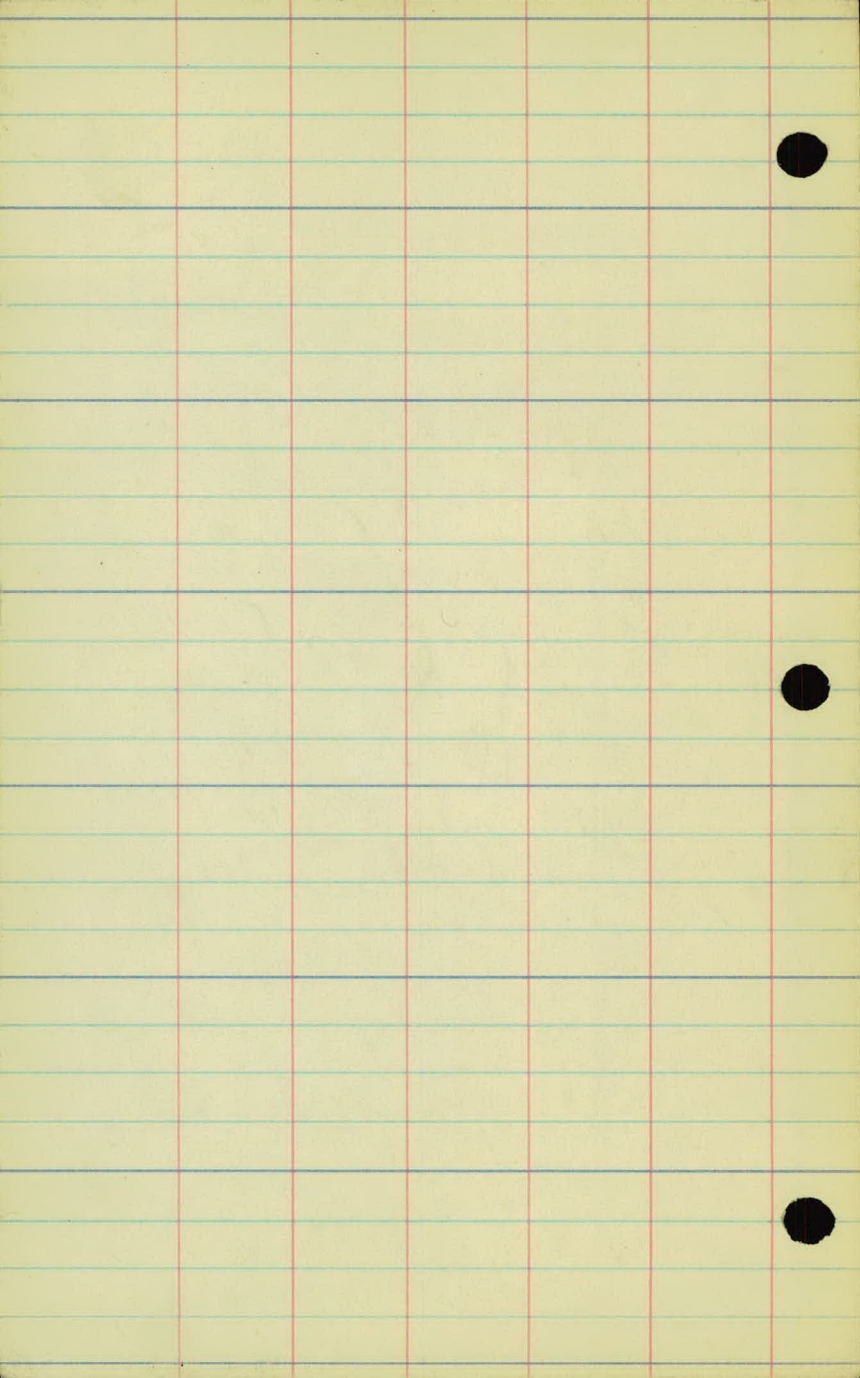
45.69	1030.11	
<u>1.22</u>	<u>44.77</u>	
44.17	985.94	check W.

Spike in 8" oak 50' Rt Sta. 27+30

18.96	985.94	
<u>2.22</u>	<u>16.74</u>	
16.74	969.20	check W.

Spike in 18" oak 90' Lt Sta. 42+42

Top of Mont. Cor. Co. Rd. A. and
White Bear Ave.



Culverts
East Ave
Sta. 0+00 to 47+70.4

station	H.P.	outlet	inlet	present. Cul. Cond.
0+73	1025.79	12.5	10.7	30'x12" C.M. good
39+04	965.17	$\frac{8.5}{17.5}$	$\frac{7.7}{12.5}$	33'x12" C.M. good
46+91.2	961.34	$\frac{8.6}{17.1}$	$\frac{7.6}{17.1}$	31'x12" C.M. good
44+03	965.90	$\frac{11.02}{12}$	$\frac{10.22}{12}$	24'x12" C.M. good

2-16-27

Wichusa
D.S.
P.B.
F.M.

cloudy cold

$\frac{127}{150}$ $\frac{103}{100}$ $\frac{104}{50}$

$\frac{110}{50}$ $\frac{106}{100}$ $\frac{103}{150}$

Drains to Lt.

$\frac{74}{100}$ $\frac{93}{100}$ $\frac{93}{50}$

$\frac{72}{50}$ $\frac{72}{100}$ $\frac{70}{150}$

Drains to Lt.

$\frac{86}{50}$

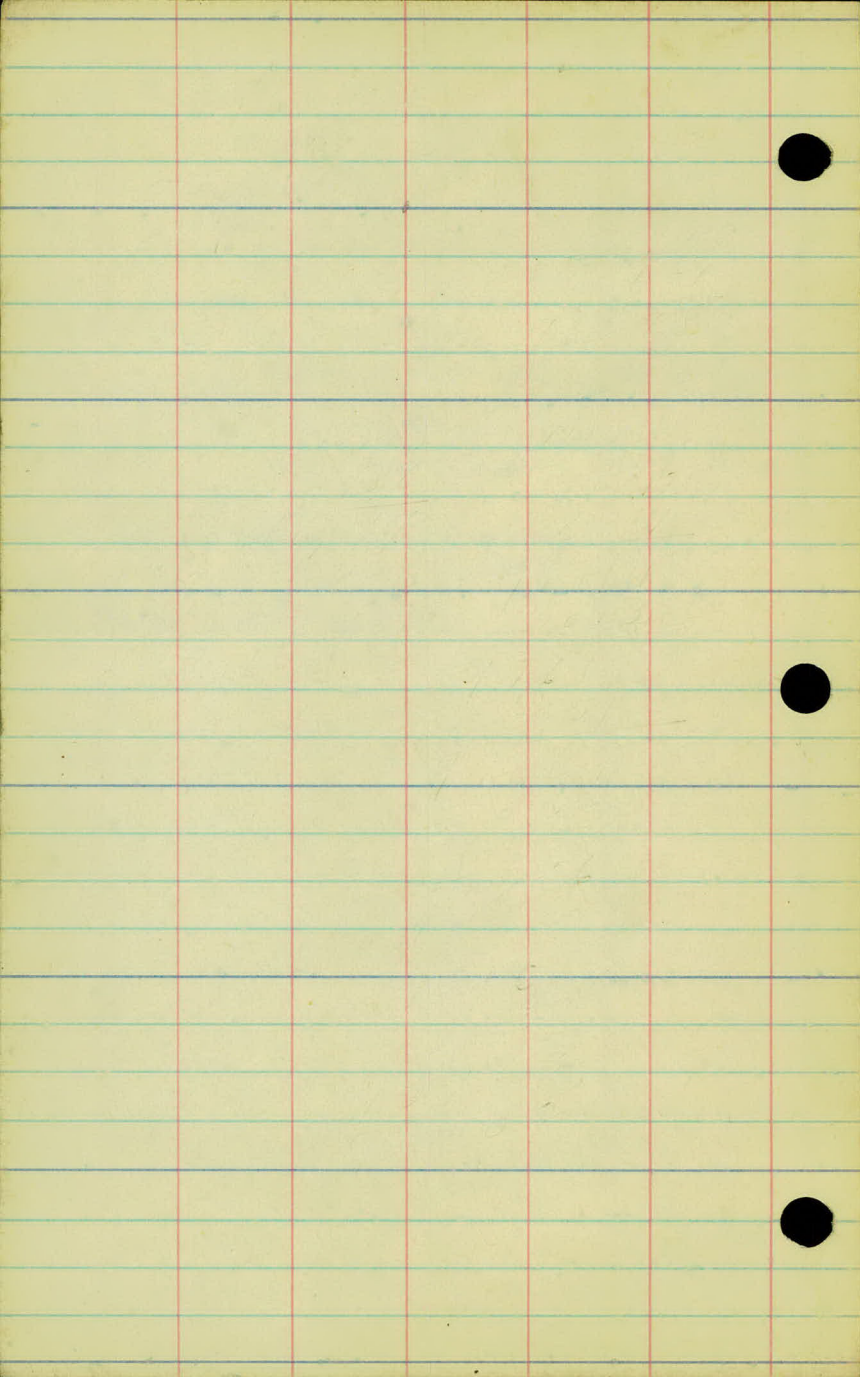
$\frac{66}{50}$ $\frac{67}{100}$ $\frac{46}{150}$

RUNS along toe Seventh Ave slope
Drains to Lt.

$\frac{120}{100}$ $\frac{113}{50}$

$\frac{88}{50}$ $\frac{65}{100}$ $\frac{32}{150}$

Drains to Lt.



A Line Levels
East Ave
From Co. Rd Ave to No. St Paul.
Road
From Sta. 0+00 to 47+70.4.

Station BS H.I. F.S. Rod. Elev.

B.M. 5.89 1025.79 1019.90

0+00			4.9	20.9
100' Rt.			5.5	20.3
200' "			4.5	21.3
300' "			3.8	22.0
400'			1.7	24.1
500'			0.50	25.5
100' Lt.			4.0	21.8
200' "			3.7	22.1
300' "			2.8	23.0
400' "			1.6	24.2
500' "			1.3	24.5

East Ave. Right

- 100'			5.7	20.1
- 200'			4.8	21.0
- 300'			2.2	21.6
- 400'			4.0	19.8
- 500'			6.2	19.6
0+00			4.9	20.9
+ 10			5.2	20.6
+ 25			3.7	20.1
+ 50			6.2	19.6
1+00			6.8	19.0
+ 50			6.9	18.9
2+00			6.4	19.4
+ 50			6.3	19.6

2-16-27

cloudy. cold

Spike in 10" oak 70 ft 59 0-50

Station	B.S.	H.I.	I.S.	Red.	Elev.
		1022.79			
+75				6.2	19.6
2+00				6.3	19.3
+50				7.3	18.5
+75				8.5	17.3
					18.3
2+00				9.3	16.5
T.P.	10.97	1026.93	9.83		1015.96
+50				11.2	15.7
3+00				11.6	15.3
+50				11.6	15.3
4+00				11.3	15.6
+50				10.6	16.3
7+00				9.2	17.7
+30				7.4	19.5
8+00				4.7	22.2
+40				3.0	23.9
9+00				1.3	25.6
T.P.	376	1029.28	0.91		1026.02
+50				2.9	21.4
10+00				3.0	26.3
+50				3.7	25.6
11+00				4.4	24.9
+50				4.7	24.4
12+00				5.2	24.1
+50				5.5	23.8
13+00				5.8	23.5
+50				6.5	22.8

2-16-27

J. L. WILSON

D. S.

H. B.

R. M.

Cloudy - Cold

2600	3.3	4.1	5.5	Ref.	51.0
		1029.28			
B.M.			5.71		1023.27
1400	14.23	14.2577		7.6	21.7
	10.74	3.29			26.7
+50	3.29	1029.28		8.8	20.5
		CHECK H.W.			
1500				10.4	18.9
+50				12.7	16.6
T.P.	0.78	1018.65	12.91		1016.87
1600				3.3	14.4
+50				6.0	11.7
1700				8.7	09.0
+50				11.0	06.7
1800				13.3	04.5
T.P.	0.23	1008.17	12.71		1005.94
+50				2.7	02.3
1900				6.3	99.9
+50				2.8	97.4
2000				11.4	94.8
T.P.	0.60	995.19	11.62		994.55
+50				3.5	92.7
2100				3.1	90.1
+50				6.7	88.5
2200				8.1	87.1
+50				9.6	85.6
2300				10.7	84.5
+50				11.9	83.3
					84.3
2400				13.0	82.2

2-16-27

H. Wilshusen blood field

25

28

17.11

Nail in F.P. 50' RT sta. 13+48

Station	2.8	4.6	5.2	Rad.	El. G.
		995.15			
T.P.	1.66	983.87	12.71		982.21
+50				2.5	81.4
+100				3.2	80.7
+150				5.1	78.8
+200				6.6	77.3
+22				7.4	76.5
+37				7.6	76.3
+47				8.0	75.9
+100				7.1	74.8
+160	48.68 327	1029.28 4541		10.3	73.6
B.M.	45.41	983.87	7.14		976.73
	CK. H. X. W.				
+100				11.5	72.4
+30				11.7	72.0
+80				11.8	72.1
+100				11.5	72.4
+25				11.5	72.4
+55				11.8	72.6
+75				11.7	72.7
+100				11.5	72.4
T.P.	2.99	972.76	11.60		972.27
+25				11.7	72.1
+75				11.7	71.1
+100				11.8	70.5
+85				11.6	69.7
+75				11.6	68.7
+100				11.7	68.1

X Sections & slope stakes

East Ave

0+00 to 47+69.9

File with
Proj 27-75

Sta.	+	H.I.	-	Elev	Gr. Rd
B.m.	2.10	1022.84		1020.74	

0+00				20.2	2.6
------	--	--	--	------	-----

+10				20.1	2.7
-----	--	--	--	------	-----

+25				20.0	2.8
-----	--	--	--	------	-----

+50				19.8	3.0
-----	--	--	--	------	-----

1+00				19.4	3.4
------	--	--	--	------	-----

+50				19.0	3.8
-----	--	--	--	------	-----

2+00				18.6	4.2
------	--	--	--	------	-----

+50				18.2	4.6
-----	--	--	--	------	-----

T.P	7.31	1028.05	3.15	1019.69	
-----	------	---------	------	---------	--

3+00				17.8	10.2
------	--	--	--	------	------

+50				17.4	10.6
-----	--	--	--	------	------

Top of monument 0 + 00

$$\frac{1.9}{33}$$

$$\frac{2.1}{0}$$

$$\frac{2.5}{33}$$

$$\frac{2.2}{33}$$

$$\frac{2.4}{0}$$

$$\frac{2.9}{33}$$

$$\frac{2.8}{33}$$

$$\frac{3.0}{20}$$

$$\frac{3.0}{0.10}$$

$$\frac{3.6}{6}$$

$$\frac{4.2}{9}$$

$$\frac{5.7}{13.5}$$

$$\frac{4.8}{15.5}$$

$$\frac{4.7}{33}$$

$$\frac{3.0}{33}$$

$$\frac{3.2}{26}$$

$$\frac{3.8}{18}$$

$$\frac{4.0}{12.5}$$

$$\frac{3.6}{F0.6}$$

$$\frac{4.1}{5}$$

$$\frac{5.2}{9}$$

$$\frac{7.6}{14}$$

$$\frac{8.3}{18.5}$$

$$\frac{8.1}{F5.1}$$

$$\frac{8.0}{33}$$

$$\frac{5.2}{33}$$

$$\frac{8.1}{F4.7}$$

$$\frac{8.3}{17}$$

$$\frac{5.1}{9}$$

$$\frac{4.5}{F1.1}$$

$$\frac{5.2}{8}$$

$$\frac{8.2}{15}$$

$$\frac{8.2}{F4.8}$$

$$\frac{8.0}{33}$$

$$\frac{7.9}{33}$$

$$\frac{7.8}{F4.0}$$

$$\frac{8.1}{14}$$

$$\frac{5.1}{9}$$

$$\frac{4.3}{F0.5}$$

$$\frac{4.7}{8.5}$$

$$\frac{7.0}{18}$$

$$\frac{7.4}{F3.6}$$

$$\frac{7.2}{33}$$

$$\frac{6.5}{33}$$

$$\frac{6.2}{0.00}$$

$$\frac{5.8}{20}$$

$$\frac{5.6}{17}$$

$$\frac{4.5}{10}$$

$$\frac{3.5}{C0.7}$$

$$\frac{4.2}{11}$$

$$\frac{3.2}{12.5}$$

$$\frac{3.5}{2.0}$$

$$\frac{2.6}{25.6}$$

$$\frac{2.1}{C1.1}$$

$$33$$

$$\frac{6.0}{C0.6}$$

$$\frac{3.2}{C1.4}$$

$$\frac{-2.7}{C1.3}$$

$$33$$

$$\frac{6.5}{C3.7}$$

$$\frac{5.3}{2.6}$$

$$\frac{9.8}{16}$$

$$\frac{8.6}{C1.6}$$

$$\frac{9.1}{9}$$

$$\frac{8.1}{15}$$

$$\frac{7.7}{20}$$

$$\frac{7.6}{2.9}$$

$$\frac{2.1}{C8.1}$$

$$33$$

$$\frac{4.7}{C3.9}$$

$$\frac{5.1}{2.9}$$

$$\frac{10.1}{18}$$

$$\frac{9.8}{C0.8}$$

$$\frac{10.4}{10}$$

$$\frac{9.6}{12}$$

$$\frac{9.4}{15}$$

$$\frac{8.6}{19}$$

$$\frac{8.6}{1.9}$$

$$\frac{9.3}{23.5}$$

$$\frac{C1.0}{33}$$

$$\begin{array}{r} 65 \\ C44 \\ \hline 33 \end{array} \quad \begin{array}{r} 8.4 \\ 22 \\ \hline 20 \end{array} \quad \begin{array}{r} 8.4 \\ 20 \\ \hline 20 \end{array} \quad \begin{array}{r} 11.7 \\ 14 \\ \hline 14 \end{array} \quad \begin{array}{r} 11.4 \\ F0.5 \\ \hline 10 \end{array} \quad \begin{array}{r} 12.1 \\ 10 \\ \hline 13 \end{array} \quad \begin{array}{r} 10.9 \\ 13 \\ \hline 16 \end{array} \quad \begin{array}{r} 11.0 \\ 16 \\ \hline 18 \end{array} \quad \begin{array}{r} 11.7 \\ 18 \\ \hline 20.1 \\ 33 \end{array}$$

$$\begin{array}{r} 3.7 \\ EC0.9 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.4 \\ 24 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.2 \\ F1.6 \\ \hline 9 \end{array} \quad \begin{array}{r} 4.6 \\ 9 \\ \hline 15 \end{array} \quad \begin{array}{r} 6.4 \\ 15 \\ \hline 20 \end{array} \quad \begin{array}{r} 6.9 \\ 20 \\ \hline F5.6 \\ 32.5 \end{array} \quad \begin{array}{r} 8.1 \\ F5.6 \\ \hline 32.5 \end{array}$$

$$\begin{array}{r} 8.3 \\ F5.8 \\ \hline 33 \end{array} \quad \begin{array}{r} 8.0 \\ 17 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.9 \\ F2.4 \\ \hline 9 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \\ \hline 15 \end{array} \quad \begin{array}{r} 6.3 \\ 15 \\ \hline F6.6 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ F6.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 8.3 \\ F6.0 \\ \hline 33 \end{array} \quad \begin{array}{r} 8.9 \\ 18 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.9 \\ F2.6 \\ \hline 9 \end{array} \quad \begin{array}{r} 5.2 \\ 9 \\ \hline 16 \end{array} \quad \begin{array}{r} 8.2 \\ 16 \\ \hline F6.9 \\ 33 \end{array} \quad \begin{array}{r} 9.2 \\ F6.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 7.8 \\ F5.9 \\ \hline 33 \end{array} \quad \begin{array}{r} 7.8 \\ 19 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \\ \hline 13 \end{array} \quad \begin{array}{r} 4.6 \\ F2.7 \\ \hline 9 \end{array} \quad \begin{array}{r} 4.9 \\ 9 \\ \hline 17 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \\ \hline F6.0 \\ 33 \end{array} \quad \begin{array}{r} 7.9 \\ F6.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 7.3 \\ F6.1 \\ \hline 33 \end{array} \quad \begin{array}{r} 7.4 \\ 19 \\ \hline 14 \end{array} \quad \begin{array}{r} 4.4 \\ 14 \\ \hline 14 \end{array} \quad \begin{array}{r} 3.7 \\ F2.5 \\ \hline 9 \end{array} \quad \begin{array}{r} 4.1 \\ 9 \\ \hline 16 \end{array} \quad \begin{array}{r} 7.2 \\ 16 \\ \hline 22 \end{array} \quad \begin{array}{r} 8.2 \\ 22 \\ \hline F9.3 \\ 33 \end{array} \quad \begin{array}{r} 8.5 \\ F9.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 13.9 \\ 33 \\ \hline 33 \end{array} \quad \begin{array}{r} 12.6 \\ F5.0 \\ \hline 31.3 \end{array} \quad \begin{array}{r} 12.8 \\ 17 \\ \hline 14 \end{array} \quad \begin{array}{r} 11.1 \\ 14 \\ \hline 14 \end{array} \quad \begin{array}{r} 10.3 \\ F1.7 \\ \hline 9 \end{array} \quad \begin{array}{r} 10.9 \\ 9 \\ \hline 16 \end{array} \quad \begin{array}{r} 13.7 \\ 16 \\ \hline F5.8 \\ 33 \end{array} \quad \begin{array}{r} 14.4 \\ F5.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 9.7 \\ 33 \\ \hline 33 \end{array} \quad \begin{array}{r} 9.4 \\ 25 \\ \hline 21 \end{array} \quad \begin{array}{r} 9.3 \\ F1.7 \\ \hline 21 \end{array} \quad \begin{array}{r} 8.7 \\ 15 \\ \hline 15 \end{array} \quad \begin{array}{r} 8.4 \\ F0.8 \\ \hline 9 \end{array} \quad \begin{array}{r} 8.8 \\ 9 \\ \hline 10 \end{array} \quad \begin{array}{r} 8.1 \\ 10 \\ \hline 15 \end{array} \quad \begin{array}{r} 8.4 \\ 15 \\ \hline F0.8 \\ 19.7 \end{array} \quad \begin{array}{r} 9.2 \\ 25 \\ \hline 20.0 \\ 33 \end{array} \quad \begin{array}{r} 9.6 \\ 33 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 1.6 \\ C4.9 \\ \hline 33 \end{array} \quad \begin{array}{r} 2.0 \\ 28 \\ \hline 23 \end{array} \quad \begin{array}{r} 1.1 \\ 23 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.3 \\ 19 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.9 \\ 15 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.9 \\ C0.8 \\ \hline 12.5 \end{array} \quad \begin{array}{r} 6.0 \\ 12.5 \\ \hline 17 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \\ \hline 21 \end{array} \quad \begin{array}{r} 0.5 \\ 21 \\ \hline C5.0 \\ 33 \end{array} \quad \begin{array}{r} 1.5 \\ C5.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ C0.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.2 \\ 22 \\ \hline 16 \end{array} \quad \begin{array}{r} 2.1 \\ C1.8 \\ \hline 15 \end{array} \quad \begin{array}{r} 7.5 \\ 15 \\ \hline 19 \end{array} \quad \begin{array}{r} 3.0 \\ 19 \\ \hline C5.2 \\ 33 \end{array} \quad \begin{array}{r} 3.7 \\ C5.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ C4.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.7 \\ 21 \\ \hline 16 \end{array} \quad \begin{array}{r} 6.0 \\ 16 \\ \hline C2.3 \end{array} \quad \begin{array}{r} 5.6 \\ C2.3 \\ \hline 14 \end{array} \quad \begin{array}{r} 6.1 \\ 14 \\ \hline 18 \end{array} \quad \begin{array}{r} 3.4 \\ 18 \\ \hline C3.6 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ C3.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.6 \\ C3.0 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.6 \\ 27 \\ \hline 18 \end{array} \quad \begin{array}{r} 5.1 \\ 18 \\ \hline C2.2 \end{array} \quad \begin{array}{r} 4.9 \\ C2.2 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.5 \\ 13 \\ \hline 17 \end{array} \quad \begin{array}{r} 3.0 \\ 17 \\ \hline C3.3 \\ 33 \end{array} \quad \begin{array}{r} 3.8 \\ C3.3 \\ \hline 33 \end{array}$$

Sta + H.I. - Elev Gr

1031.26

10+00 2417 6.6

+50 2510 6.3

11+00 2510 6.3

+50 2418 6.5

12+00 24.3 7.0

+50 23.6 7.7

PK. BM. 1023.24

5.5.5

1028.79

8.00

1023.24
1023.26

13+00

22.7 6.1

B.M.

5.20

1028.44

1023.24

+50

21.7 6.7

14+00

20.5 7.9

+50

19.2 9.2

15+00

17.7 10.7

+50

16.0 12.4

$\frac{4.7}{19}$ $\frac{4.7}{16}$ $\frac{5.1}{11}$ $\frac{5.0}{16}$ $\frac{5.6}{13}$ $\frac{5.8}{17}$ $\frac{4.2}{24}$
33 33

$\frac{6.7}{16}$ $\frac{5.9}{17}$ $\frac{6.1}{11}$ $\frac{5.9}{16}$ $\frac{6.1}{13}$ $\frac{3.9}{18}$ 32
33 33

$\frac{7.8}{10.5}$ $\frac{7.5}{15}$ $\frac{7.1}{10}$ $\frac{6.5}{12}$ $\frac{6.7}{13}$ $\frac{6.1}{18}$ $\frac{5.1}{12}$
33 33

$\frac{8.1}{10.4}$ $\frac{7.8}{15}$ $\frac{7.6}{8}$ $\frac{7.0}{10.5}$ $\frac{7.2}{11}$ $\frac{7.7}{20}$ $\frac{7.4}{11}$
33 33

$\frac{7.8}{11.2}$ $\frac{7.9}{16}$ $\frac{8.3}{14}$ $\frac{7.9}{8}$ $\frac{7.4}{10.4}$ $\frac{7.5}{12}$ $\frac{8.2}{29}$ $\frac{8.4}{10.6}$
33 33

$\frac{7.9}{11.8}$ $\frac{8.1}{16}$ $\frac{7.8}{7}$ $\frac{7.6}{10.1}$ $\frac{7.8}{13}$ $\frac{8.6}{25}$ $\frac{8.7}{11.0}$
33 33

$\frac{5.3}{10.8}$ $\frac{5.8}{16}$ $\frac{5.8}{10}$ $\frac{5.4}{10.7}$ $\frac{6.0}{13}$ $\frac{7.3}{22}$ $\frac{7.6}{10.5}$
33 33

$\frac{4.3}{2.4}$ $\frac{5.1}{11}$ $\frac{5.8}{9}$ $\frac{5.6}{11.1}$ $\frac{6.0}{15}$ $\frac{5.6}{16}$ $\frac{5.7}{11.0}$
33 33

$\frac{4.7}{3.2}$ $\frac{5.4}{17}$ $\frac{5.9}{11}$ $\frac{7.1}{9}$ $\frac{6.8}{11.1}$ $\frac{7.2}{14}$ $\frac{5.6}{19}$ $\frac{5.7}{2.2}$
33 33

$\frac{6.7}{11.5}$ $\frac{7.3}{16}$ $\frac{7.7}{11}$ $\frac{8.6}{9}$ $\frac{8.1}{11}$ $\frac{8.5}{13}$ $\frac{6.9}{17}$ $\frac{6.3}{27}$ $\frac{6.9}{2.3}$
33 33

$\frac{9.0}{1.8}$ $\frac{9.5}{15}$ $\frac{9.8}{12}$ $\frac{10.4}{10}$ $\frac{9.7}{11.0}$ $\frac{10.1}{14}$ $\frac{8.9}{16}$ $\frac{8.9}{21}$ $\frac{8.8}{1.9}$
33 33

$\frac{11.6}{10.8}$ $\frac{12.2}{12}$ $\frac{12.7}{11}$ $\frac{12.1}{10.3}$ $\frac{12.6}{14}$ $\frac{11.5}{16}$ $\frac{11.4}{21}$ $\frac{11.1}{28}$ $\frac{11.5}{2.9}$
33 33

Sta. + H.I. - Elev G.R.

1028.44

1.55 1016.94 13.05 1015.39

16+00 14.1 2.8

+50 12.1 4.8

17+00 09.9 7.0

+50 07.6 9.3

T.P. 2.45 1008.94 10.45 1006.49

18+00 05.3 3.6

+50 03.0 5.9

19+00 00.7 8.2

+50 98.5 10.4

T.P. 3.35 1000.34 11.95 996.99

20+00 96.1 4.2

+40 94.5 5.8

T.P. 2.22 993.84 8.72 991.62

21+00 92.0 1.8

+50 90.1 3.7

Sta.	+	HI	-	Elev	Giv.
		993.84			
22+00				88.3	5.5
+50				86.7	7.1
	5.38	988.74	10.48	983.36	
23+00				85.2	3.5
+50				83.8	4.9
24+00				82.5	6.2
+50				81.2	7.5
25+00				79.9	8.8
+50				78.7	10.0
26+00				77.5	11.2
CK. B.M.			12.06	976.68	976.93
B. m.	2.73	979.46		976.73	
26+27				76.9	2.4

$\frac{7.7}{33}$	$\frac{7.5}{F20}$ 22.	$\frac{7.6}{12}$	$\frac{7.8}{8.5}$	$\frac{7.4}{F19}$	$\frac{7.7}{12}$	$\frac{9.1}{17}$	$\frac{9.5}{F40}$ 28	$\frac{9.4}{33}$
$\frac{9.7}{33}$	$\frac{9.5}{F24}$ 23.2	$\frac{9.1}{17.5}$	$\frac{8.8}{12}$	$\frac{9.0}{8}$	$\frac{8.7}{F16}$	$\frac{9.4}{16}$	$\frac{9.9}{22}$	$\frac{10.2}{F31}$ 25.3
$\frac{6.2}{33}$	$\frac{5.9}{F24}$ 23.2	$\frac{5.8}{22}$	$\frac{5.1}{13}$	$\frac{5.3}{11}$	$\frac{5.9}{F15}$	$\frac{5.5}{10.5}$	$\frac{6.1}{16}$	$\frac{6.0}{F2.5}$ 23.5
$\frac{7.1}{33}$	$\frac{7.0}{F21}$ 22.3	$\frac{6.9}{18}$	$\frac{6.5}{12}$	$\frac{6.0}{F11}$	$\frac{6.4}{11}$	$\frac{7.7}{14}$	$\frac{8.2}{19}$	$\frac{8.9}{F40}$ 28
$\frac{7.7}{F0.5}$ 33	$\frac{7.7}{23}$	$\frac{7.3}{11}$	$\frac{7.1}{F0.9}$	$\frac{7.7}{10}$	$\frac{10.0}{17}$	$\frac{11.0}{F.48}$ 30.4	$\frac{11.0}{33}$	
$\frac{7.4}{C0.1}$ 33	$\frac{7.7}{19}$	$\frac{7.9}{15}$	$\frac{8.1}{17}$	$\frac{7.8}{F0.3}$	$\frac{8.5}{11}$	$\frac{10.6}{16}$	$\frac{11.3}{F38}$ 27.4	$\frac{11.7}{33}$
$\frac{2.4}{C6.4}$ 33	$\frac{2.5}{25}$	$\frac{9.3}{14}$	$\frac{8.6}{C0.2}$	$\frac{9.0}{12}$	$\frac{10.9}{21.4}$	$\frac{11.0}{F2.2}$ 22.6	$\frac{11.8}{33}$	
$\frac{5.0}{C5.0}$ 33	$\frac{5.6}{20}$	$\frac{11.1}{13}$	$\frac{10.3}{F0.7}$	$\frac{10.0}{15}$	$\frac{10.0}{19}$	$\frac{11.1}{F0.9}$ 22	$\frac{11.4}{24}$	$\frac{12.1}{33}$
$\frac{10.1}{C1.1}$ 33	$\frac{10.3}{25}$	$\frac{11.5}{19}$	$\frac{12.1}{16}$	$\frac{12.2}{F1.0}$	$\frac{12.5}{12}$	$\frac{13.9}{17}$	$\frac{14.3}{F3.1}$ 20.3	$\frac{14.6}{33}$

S. Pike in 10" oak 50' R- 26 + 70

" " 10" " 50' R- 26 + 70

$\frac{3.0}{F0.4}$ 23	$\frac{3.5}{18}$	$\frac{4.1}{12}$	$\frac{3.7}{F0.7}$	$\frac{3.8}{20}$	$\frac{3.9}{33}$	$\frac{3.8}{50}$
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+ H.I - Eleo Gr
979.46

26+47 76.5 3.0

27+00 75.5 4.0

+40 75.0 4.6

28+00 73.9 5.4

+50 73.3 6.2

29+00 72.7 6.8

T.P 8.29 980.86 6.89 972.57

+25 72.4 8.5

+55 72.1 8.8

+75 71.9 9.0

30+00 71.7 9.2

+25 71.4 9.5

+75 70.9 10.0

$$\frac{3.7}{\frac{21.3}{33}} \quad \frac{4.2}{28} \quad \frac{4.2}{19} \quad \frac{4.8}{14} \quad \frac{4.3}{F1.3} \quad \frac{4.4}{18} \quad \frac{5.0}{F2.0} \quad \frac{5.5}{22} \quad \frac{5.5}{33}$$

$$\frac{4.7}{\frac{24.3}{33}} \quad \frac{4.4}{27} \quad \frac{5.8}{15} \quad \frac{5.6}{F1.6} \quad \frac{5.7}{9} \quad \frac{6.1}{14} \quad \frac{5.7}{20} \quad \frac{5.1}{\frac{20.9}{33}}$$

$$\frac{7.6}{33} \quad \frac{7.5}{\frac{F3.0}{20}} \quad \frac{6.7}{16} \quad \frac{6.2}{1.7} \quad \frac{6.8}{11} \quad \frac{6.6}{19} \quad \frac{5.1}{\frac{21.4}{33}}$$

$$\frac{9.1}{33} \quad \frac{9.0}{\frac{F2.6}{26.8}} \quad \frac{7.8}{16} \quad \frac{7.4}{F2.0} \quad \frac{7.9}{8} \quad \frac{9.8}{15} \quad \frac{10.4}{25} \quad \frac{10.4}{F5.0} \quad \frac{10.3}{31} \quad \frac{10.3}{33}$$

$$\frac{8.0}{\frac{21.0}{33}} \quad \frac{8.4}{23} \quad \frac{8.1}{12} \quad \frac{7.8}{F1.6} \quad \frac{8.3}{8} \quad \frac{11.2}{16} \quad \frac{12.0}{25} \quad \frac{12.1}{\frac{F5.9}{33}}$$

$$\frac{2.8}{\frac{C4.0}{33}} \quad \frac{3.6}{29} \quad \frac{6.2}{19} \quad \frac{7.4}{12.5} \quad \frac{7.2}{F0.4} \quad \frac{8.1}{9} \quad \frac{11.2}{18.5} \quad \frac{13.0}{27} \quad \frac{13.2}{\frac{F6.4}{33}}$$

$$\frac{0.14}{\frac{C8.1}{33}} \quad \frac{1.7}{22.5} \quad \frac{8.4}{12} \quad \frac{8.4}{C0.1} \quad \frac{9.0}{10.5} \quad \frac{11.8}{20} \quad \frac{13.3}{27} \quad \frac{14.4}{\frac{F5.9}{33}}$$

$$\frac{3.2}{\frac{C5.6}{33}} \quad \frac{2.6}{28} \quad \frac{1.8}{20} \quad \frac{8.5}{11} \quad \frac{8.3}{C0.5} \quad \frac{8.4}{13} \quad \frac{10.0}{22} \quad \frac{10.8}{\frac{50.8}{22}} \quad \frac{11.3}{33}$$

$$\frac{5.2}{\frac{C4.8}{33}} \quad \frac{4.1}{20} \quad \frac{8.2}{13} \quad \frac{8.7}{11} \quad \frac{8.3}{C0.7} \quad \frac{8.7}{10} \quad \frac{7.3}{13} \quad \frac{9.5}{2.5} \quad \frac{10.7}{\frac{20.3}{33}}$$

$$\frac{7.4}{\frac{E1.3}{33}} \quad \frac{7.1}{25} \quad \frac{5.7}{16} \quad \frac{8.1}{11} \quad \frac{8.5}{C0.7} \quad \frac{8.8}{9} \quad \frac{4.8}{14} \quad \frac{7.2}{22} \quad \frac{10.0}{\frac{21.2}{33}}$$

$$\frac{9.2}{\frac{C0.3}{33}} \quad \frac{7.4}{24} \quad \frac{8.0}{18} \quad \frac{9.3}{12} \quad \frac{9.0}{C0.5} \quad \frac{9.4}{11} \quad \frac{5.1}{16} \quad \frac{6.7}{\frac{C2.8}{33}}$$

$$\frac{10.7}{\frac{F1.3}{33}} \quad \frac{10.8}{23} \quad \frac{9.5}{17} \quad \frac{10.5}{13} \quad \frac{10.0}{60} \quad \frac{10.1}{11} \quad \frac{6.8}{17} \quad \frac{5.9}{\frac{C4.1}{33}}$$

+ H.I - Elev G.R.

980.86

T.P. 6.24 978.28 8.82 972.04

31+00 70.7 7.6

+60 70.1 8.2

T.P. 4.12 971.56 10.84 967.44

32+00 69.7 1.9

+50 69.2 2.4

33+00 68.7 2.9

+50 68.2 3.4

34+00 67.6 4.0

T.P. 7.84 975.65 3.75 967.81

+55 67.0 8.6

35+00 66.5 9.1

+50 65.9 9.7

36+00 65.2 10.4

T.P. 2.72 966.88 11.49 964.16

+50 64.6 2.3

$$\frac{9.2}{33} \quad \frac{8.5}{20} \quad \frac{8.7}{13} \quad \frac{8.0}{F0.4} \quad \frac{8.4}{15} \quad \frac{5.6}{17} \quad \frac{4.6}{C3.0}$$

$$\frac{11.2}{33} \quad \frac{11.2}{F3.0} \quad \frac{11.2}{23} \quad \frac{10.8}{16} \quad \frac{10.2}{11} \quad \frac{9.5}{F0.3} \quad \frac{10.0}{11} \quad \frac{10.6}{13} \quad \frac{10.2}{24} \quad \frac{9.2}{B1.0}$$

$$\frac{5.2}{33} \quad \frac{5.4}{F3.0} \quad \frac{5.4}{20.0} \quad \frac{5.4}{19} \quad \frac{4.4}{10} \quad \frac{3.8}{F1.9} \quad \frac{4.5}{11} \quad \frac{5.2}{16} \quad \frac{4.9}{26} \quad \frac{4.8}{F2.9} \quad \frac{4.2}{24.4} \quad \frac{4.2}{33}$$

$$\frac{6.9}{33} \quad \frac{7.1}{F4.7} \quad \frac{7.3}{22} \quad \frac{7.1}{14} \quad \frac{5.2}{10} \quad \frac{4.7}{F2.3} \quad \frac{5.3}{10} \quad \frac{6.4}{16} \quad \frac{5.9}{F3.0} \quad \frac{5.4}{26.0} \quad \frac{5.4}{33}$$

$$\frac{7.2}{33} \quad \frac{7.1}{F4.2} \quad \frac{7.2}{14} \quad \frac{5.4}{9} \quad \frac{5.0}{F2.1} \quad \frac{5.8}{11} \quad \frac{6.8}{16} \quad \frac{6.4}{28} \quad \frac{6.5}{F3.6} \quad \frac{6.3}{26.0} \quad \frac{6.3}{33}$$

$$\frac{6.9}{33} \quad \frac{6.9}{F3.5} \quad \frac{6.9}{26.0} \quad \frac{6.9}{23} \quad \frac{6.6}{15} \quad \frac{5.0}{16} \quad \frac{4.4}{F1.0} \quad \frac{4.9}{12} \quad \frac{5.6}{16} \quad \frac{5.3}{19} \quad \frac{4.0}{D1.4} \quad \frac{4.0}{23}$$

$$\frac{4.3}{11.7} \quad \frac{3.9}{23} \quad \frac{5.3}{18} \quad \frac{3.8}{13} \quad \frac{4.0}{10} \quad \frac{3.7}{C0.3} \quad \frac{4.1}{11} \quad \frac{3.7}{16} \quad \frac{4.2}{25} \quad \frac{3.5}{C0.9} \quad \frac{3.5}{33}$$

$$\frac{8.1}{C0.5} \quad \frac{7.6}{20} \quad \frac{6.8}{15} \quad \frac{8.2}{11} \quad \frac{7.8}{C0.8} \quad \frac{8.1}{12} \quad \frac{6.8}{16} \quad \frac{4.4}{22} \quad \frac{3.4}{C3.2} \quad \frac{3.4}{33}$$

$$\frac{9.8}{11.3} \quad \frac{9.9}{20} \quad \frac{8.7}{14} \quad \frac{9.5}{11} \quad \frac{8.5}{C0.6} \quad \frac{8.7}{10} \quad \frac{6.5}{12} \quad \frac{5.6}{19} \quad \frac{5.7}{C4.4} \quad \frac{5.7}{33}$$

$$\frac{9.0}{C0.7} \quad \frac{8.6}{21.0} \quad \frac{8.2}{16} \quad \frac{9.4}{12} \quad \frac{9.1}{C0.6} \quad \frac{9.4}{10} \quad \frac{8.2}{13} \quad \frac{9.0}{C0.9} \quad \frac{9.0}{33}$$

$$\frac{9.1}{C1.3} \quad \frac{9.3}{15} \quad \frac{9.8}{10} \quad \frac{9.7}{C0.7} \quad \frac{10.1}{10} \quad \frac{8.7}{12} \quad \frac{9.6}{21} \quad \frac{10.7}{1.7} \quad \frac{10.7}{33}$$

$$\frac{0.8}{C1.5} \quad \frac{0.9}{28} \quad \frac{1.1}{17} \quad \frac{2.2}{14} \quad \frac{2.2}{C0.1} \quad \frac{2.6}{9} \quad \frac{1.5}{11} \quad \frac{2.2}{18} \quad \frac{3.1}{28} \quad \frac{3.6}{D0.7} \quad \frac{3.6}{33}$$

	+	H.I	-	Elev	G.S.
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966.88

37+00

63.9 3.0

+50

63.2 3.7

38+00

62.5 4.4

T.P.

2.45 964.41 5.22 961.66

+50

61.8 2.3

39+00

61.3 2.8

+35

60.9 3.2

40+00

60.3 3.8

+50

59.9 4.2

41+00

59.5 4.6

T.P.

8.87. 968.03 4.95 959.16

+50

59.2 8.8

42+00

58.9 9.1

+50

58.6 9.4

$$\frac{2.4}{\frac{60.6}{33}} \quad \frac{2.2}{17} \quad \frac{3.6}{12} \quad \frac{3.2}{\frac{80.2}{33}} \quad \frac{3.6}{9} \quad \frac{3.1}{12} \quad \frac{3.8}{18} \quad \frac{3.3}{22} \quad \frac{3.9}{\frac{81.1}{33}}$$

$$\frac{3.6}{\frac{60.1}{33}} \quad \frac{3.3}{17} \quad \frac{4.5}{12} \quad \frac{4.2}{\frac{80.3}{33}} \quad \frac{4.6}{9} \quad \frac{4.0}{12} \quad \frac{4.6}{17} \quad \frac{3.9}{22} \quad \frac{4.6}{\frac{81.1}{33}}$$

$$\frac{6.2}{\frac{80.2}{33}} \quad \frac{6.1}{25} \quad \frac{5.5}{16} \quad \frac{5.3}{\frac{81.1}{33}} \quad \frac{5.8}{11} \quad \frac{6.7}{16} \quad \frac{6.3}{21} \quad \frac{6.4}{\frac{82.0}{22}} \quad \frac{6.7}{33}$$

$$\frac{5.1}{33} \quad \frac{5.1}{29} \quad \frac{4.8}{\frac{85.50}{25 \cdot 15}} \quad \frac{3.9}{11} \quad \frac{3.6}{\frac{81.3}{33}} \quad \frac{4.2}{10} \quad \frac{5.4}{13} \quad \frac{5.9}{20} \quad \frac{6.1}{\frac{83.8}{27.4}} \quad \frac{6.4}{33}$$

$$\frac{4.5}{33} \quad \frac{8.4}{\frac{83.6}{26.9}} \quad \frac{6.7}{19} \quad \frac{5.5}{15} \quad \frac{4.7}{11} \quad \frac{4.4}{\frac{81.6}{33}} \quad \frac{5.0}{10} \quad \frac{6.7}{16} \quad \frac{6.8}{\frac{84.0}{28}} \quad \frac{6.6}{33}$$

$$\frac{8.0}{33} \quad \frac{7.9}{\frac{84.7}{30.1}} \quad \frac{7.8}{23} \quad \frac{7.3}{19} \quad \frac{8.0}{16} \quad \frac{5.3}{11} \quad \frac{4.8}{\frac{81.6}{33}} \quad \frac{5.2}{11} \quad \frac{6.4}{16} \quad \frac{6.3}{20} \quad \frac{5.2}{\frac{82.0}{33}}$$

$$\frac{6.1}{33} \quad \frac{6.2}{\frac{82.4}{22.2}} \quad \frac{6.7}{20} \quad \frac{7.0}{15} \quad \frac{5.5}{10} \quad \frac{4.8}{\frac{81.0}{33}} \quad \frac{5.0}{11} \quad \frac{6.3}{16} \quad \frac{6.3}{21} \quad \frac{5.0}{20} \quad \frac{4.3}{30} \quad \frac{4.1}{\frac{81.7}{33}}$$

$$\frac{6.0}{\frac{80.2}{35}} \quad \frac{5.8}{26} \quad \frac{6.2}{\frac{82.0}{22}} \quad \frac{5.0}{11} \quad \frac{4.5}{\frac{80.3}{33}} \quad \frac{4.8}{12} \quad \frac{5.6}{19} \quad \frac{4.4}{26} \quad \frac{3.9}{\frac{60.3}{33}}$$

$$\frac{6.3}{\frac{80.3}{33}} \quad \frac{5.8}{15} \quad \frac{5.1}{10} \quad \frac{4.6}{20} \quad \frac{5.1}{12} \quad \frac{5.3}{15} \quad \frac{4.9}{18} \quad \frac{4.8}{23} \quad \frac{2.8}{29} \quad \frac{3.2}{\frac{81.4}{33}}$$

$$\frac{9.5}{\frac{81.3}{33}} \quad \frac{9.1}{24} \quad \frac{8.9}{19} \quad \frac{8.7}{14} \quad \frac{9.0}{12} \quad \frac{8.6}{\frac{80.2}{33}} \quad \frac{9.1}{12} \quad \frac{4.9}{19} \quad \frac{5.8}{22} \quad \frac{4.4}{27} \quad \frac{3.7}{\frac{85.1}{33}}$$

$$\frac{8.3}{\frac{80.8}{33}} \quad \frac{8.0}{23} \quad \frac{7.3}{16} \quad \frac{8.8}{12} \quad \frac{8.3}{\frac{80.8}{33}} \quad \frac{8.6}{12} \quad \frac{4.3}{18} \quad \frac{3.9}{27} \quad \frac{3.8}{\frac{85.3}{33}}$$

$$\frac{8.7}{\frac{80.9}{33}} \quad \frac{8.8}{26} \quad \frac{8.9}{17} \quad \frac{9.5}{14} \quad \frac{9.1}{11} \quad \frac{8.8}{\frac{80.6}{33}} \quad \frac{9.5}{13} \quad \frac{8.7}{19} \quad \frac{7.5}{20} \quad \frac{7.4}{25} \quad \frac{6.6}{28} \quad \frac{7.2}{\frac{82.4}{33}}$$

Sfa. + H.I. - Elev. Gr. Rod
968.03

43+00 58.3 9.7

+50 58.0 10.0

T.P. 6.28 963.53 10.78 957.25
44+00 57.7 5.8

+50 57.6 5.9

45+00 57.5 6.0

+50 57.5 6.0

46+00 57.5 6.0

+50 57.7 5.8

47+00 57.9 5.6

+22 58.0 5.5

+60 58.5 5.0

B.M. 4.57 963.53 4.57 958.96

$$\frac{9.8}{60.9} \frac{8.2}{17} \frac{9.5}{14} \frac{9.8}{11} \frac{9.4}{60.3} \frac{9.8}{11} \frac{9.6}{15} \frac{7.5}{20} \frac{6.5}{26} \frac{6.9}{21.9} \\ 33$$

$$\frac{7.7}{62.3} \frac{8.0}{31} \frac{7.8}{27} \frac{8.4}{23} \frac{9.0}{18} \frac{10.5}{14} \frac{10.4}{F0.4} \frac{10.8}{13} \frac{10.2}{16} \frac{9.8}{21} \frac{10.0}{25} \frac{10.4}{11.6} \\ 33$$

$$\frac{9.0}{33} \frac{9.0}{F4.2} \frac{9.0}{20.6} \frac{8.7}{19} \frac{7.0}{15} \frac{7.0}{11} \frac{6.6}{F0.8} \frac{6.9}{12} \frac{7.9}{10} \frac{7.8}{25} \frac{6.9}{50.9} \\ 33$$

$$\frac{9.6}{33} \frac{9.4}{F5.6} \frac{9.3}{26.5} \frac{7.4}{15} \frac{6.8}{10} \frac{6.8}{F0.9} \frac{7.1}{13} \frac{8.0}{17} \frac{7.4}{29} \frac{6.8}{0.19} \\ 33$$

$$\frac{9.4}{33} \frac{9.1}{F3.1} \frac{8.6}{25.3} \frac{7.4}{17} \frac{7.4}{11} \frac{6.7}{F0.7} \frac{7.1}{12} \frac{8.0}{16} \frac{8.0}{F2.0} \frac{7.9}{22} \frac{6.1}{0.14} \\ 33$$

$$\frac{9.3}{33} \frac{9.0}{F3.0} \frac{8.7}{25} \frac{7.8}{15} \frac{7.8}{11} \frac{7.2}{F1.2} \frac{7.6}{12} \frac{8.5}{15.5} \frac{8.5}{F2.5} \frac{8.4}{23.5} \frac{6.9}{0.11} \\ 33$$

$$\frac{9.9}{33} \frac{9.8}{F3.8} \frac{9.6}{24.4} \frac{9.1}{21} \frac{8.2}{13.5} \frac{8.2}{11} \frac{7.2}{F1.5} \frac{7.7}{14} \frac{8.6}{18} \frac{8.6}{F2.6} \frac{8.4}{23.8} \frac{6.6}{0.14} \\ 33$$

$$\frac{11.5}{F5.7} \frac{11.2}{24} \frac{10.1}{14} \frac{8.9}{10} \frac{8.1}{F2.3} \frac{8.2}{12} \frac{9.1}{17} \frac{9.0}{F3.2} \frac{8.9}{25.6} \frac{8.5}{28} \\ 33$$

$$\frac{11.4}{F5.8} \frac{10.6}{13} \frac{8.3}{8} \frac{7.8}{F1.8} \frac{7.6}{14} \frac{9.3}{22} \frac{9.4}{F3.8} \frac{9.2}{27.4} \\ 33$$

$$\frac{6.9}{33} \frac{6.0}{31} \frac{8.1}{F2.6} \frac{9.6}{23.8} \frac{7.3}{18} \frac{7.3}{10} \frac{7.7}{F1.7} \frac{7.3}{17} \frac{8.8}{22} \frac{8.8}{F3.3} \frac{9.0}{25.9} \\ 33$$

$$\frac{5.6}{33} \frac{5.5}{22} \frac{5.2}{F0.2} \frac{5.4}{15} \frac{6.0}{22} \frac{6.0}{25} \frac{7.0}{33}$$

Spike in T.P. 42' West Sta 47+70.4

+ HI - Elev
963.53

5.44 964.77 4.20 959.33 ✓

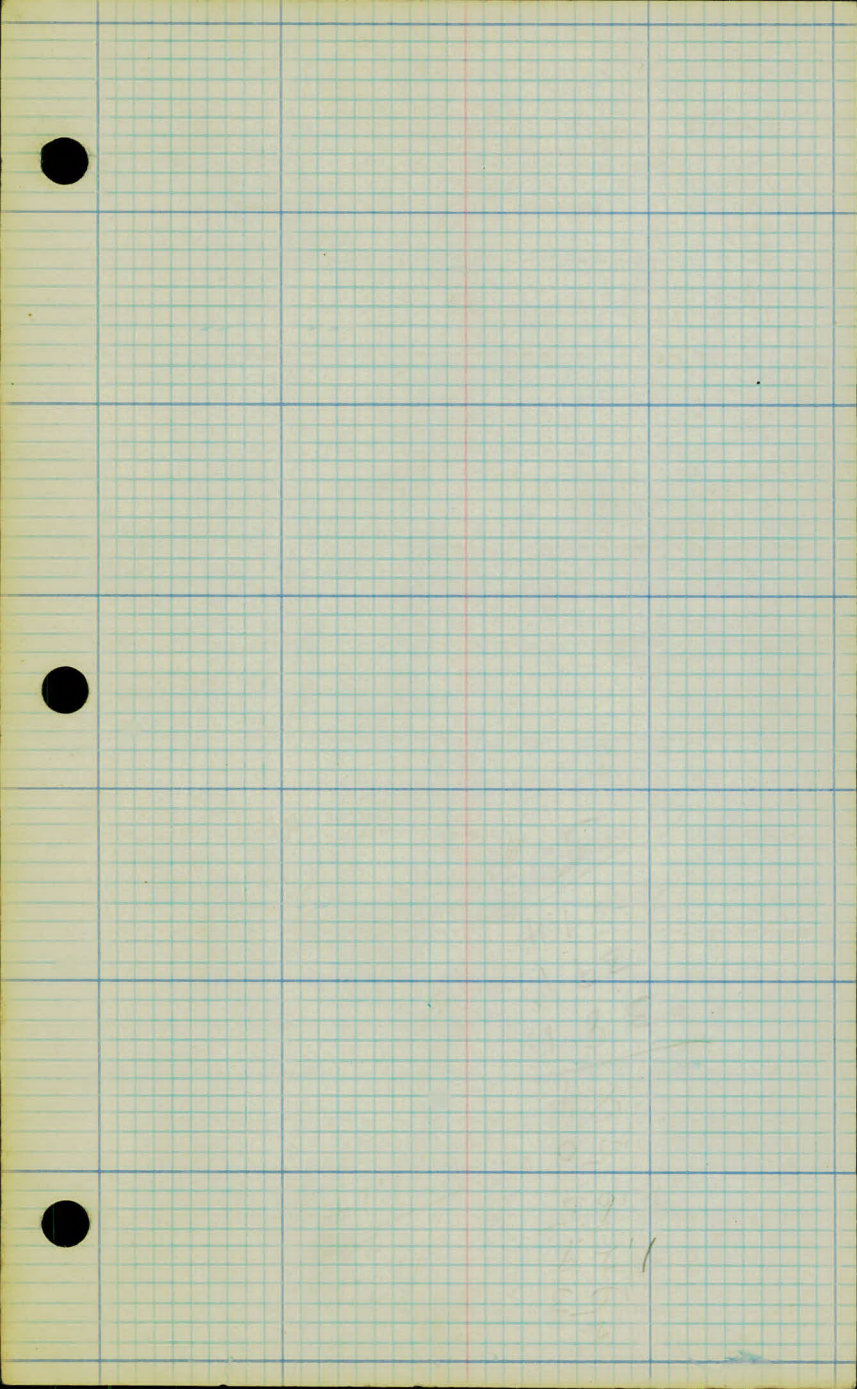
8.89 972.83 0.83 963.94 ✓

5.48 977.21 1.10 971.73

CK. B.M.

0.45 976.76 976.73 ✓

SPike in 10' oak 50' R-Sta 26+70



6+00

5+00

4+00

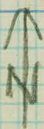
3+00

2+00

1+00

0+00

Mon. P.I. Larpenteur + East



Na. 1/4 R. P.

39.85



23.45

Na. 1/4 R. P.

13+48.8 P.O.T.

13+00

12+00

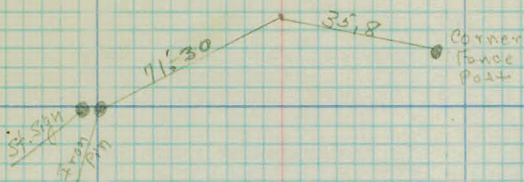
11+00

10+00

9+00

8+00

7+00



20+00

19+00

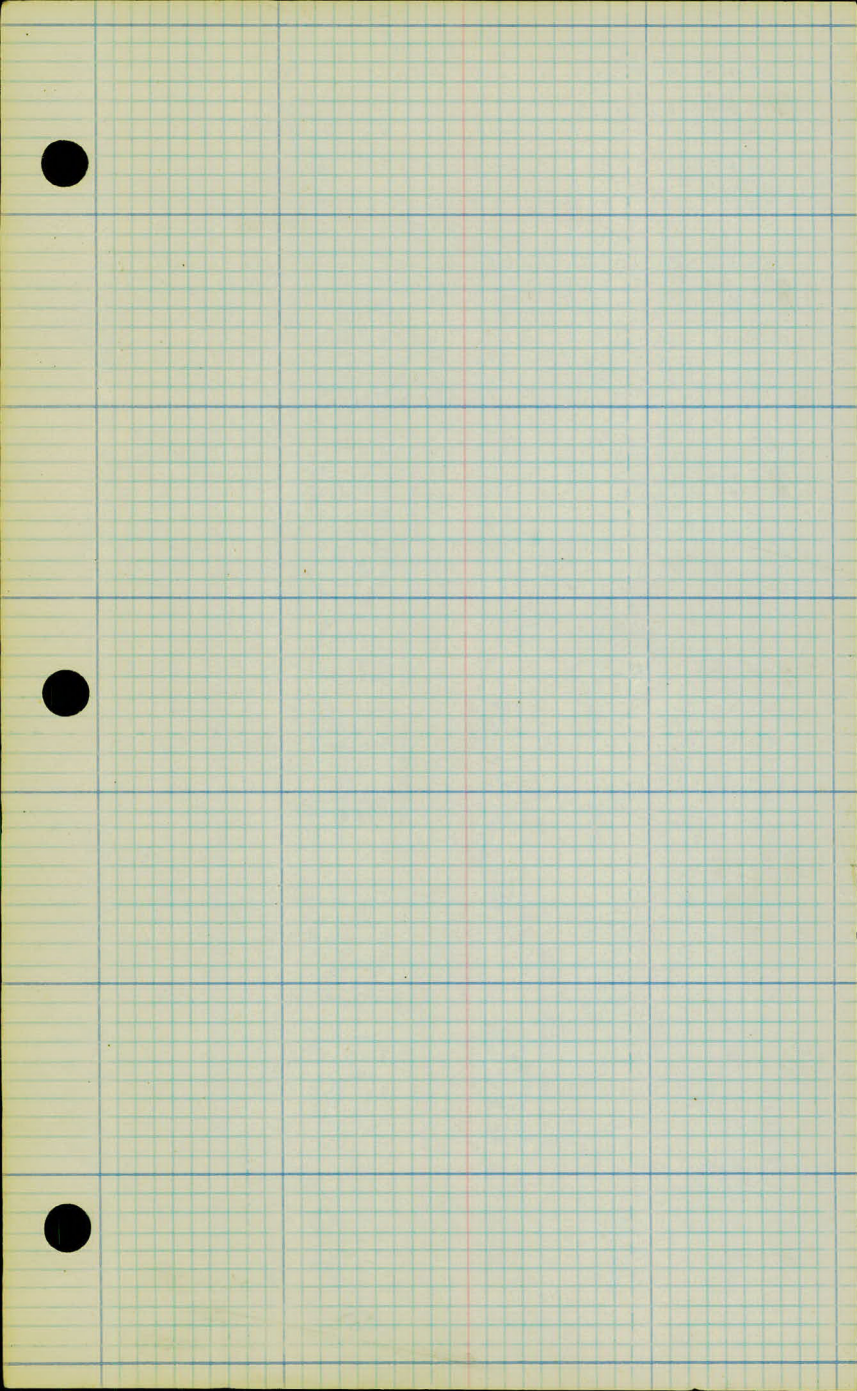
18+00

17+00

16+00

15+00

14+00



27+00

.+40.9

26+00

25+00

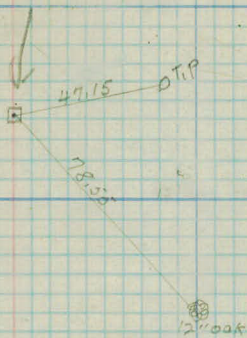
24+00

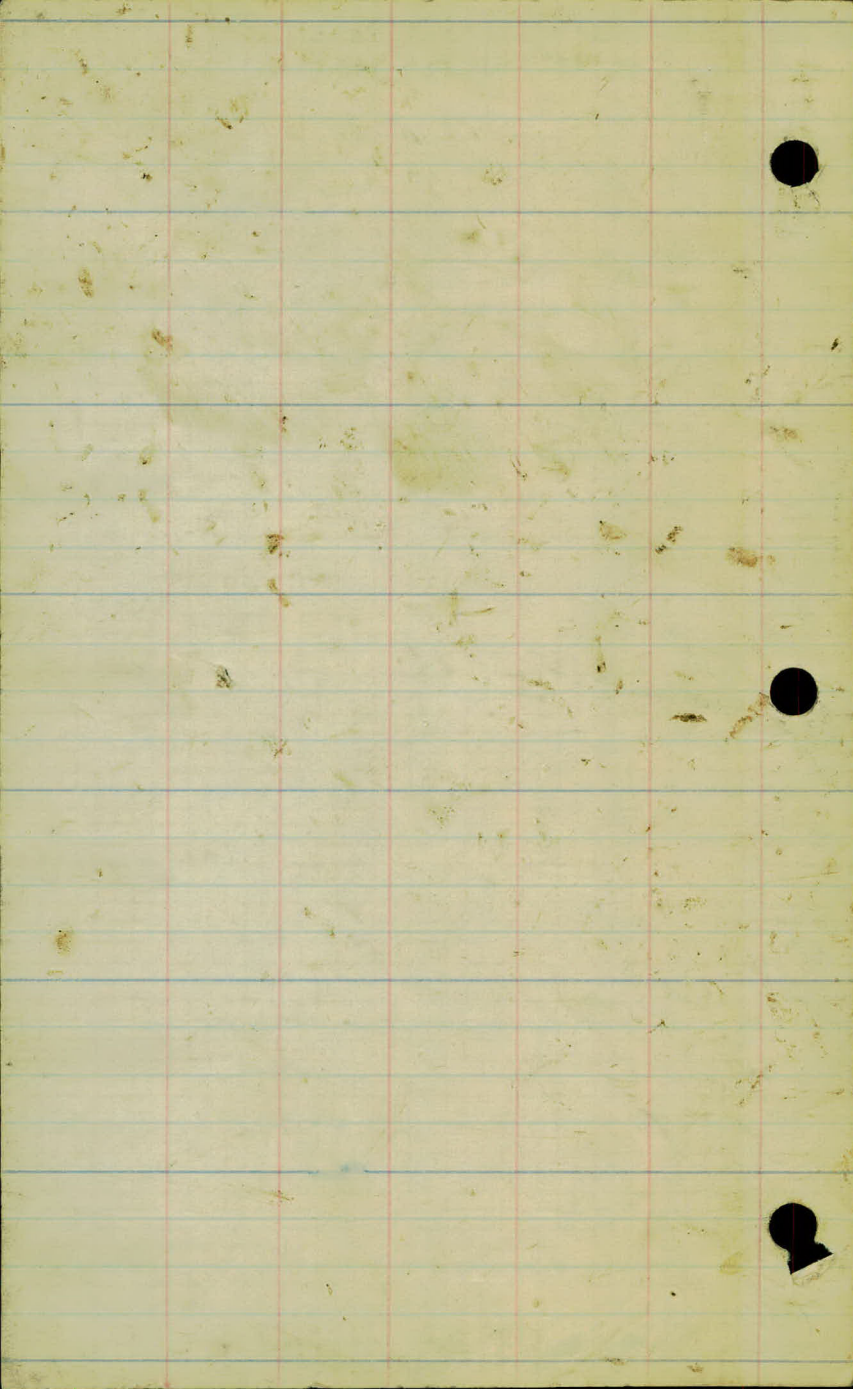
23+00

22+00

21+00

Monument is tipped
to north





U 2502