

LOCATION SURVEY

S.T.H. N^o 52

Connection at Fort Snelling

CO. PROJ N^o

FILE N^o 7

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 4/9/26

File No. 7

ST. H. # 52 Connection
At Fort Snelling

Alignment Notes
Sta 981+57 To 1079+23⁶⁴

Austin }
Skoglan } Party
Fritz }
JanKoski }
Alexander }

3/22 To 3/29 - 1926

Station

Ang. ht [±] Ang. Rt.

1005+00 P.O.T.

989+78⁰ Meet 10' Rt.

988+87⁰ P.T. ✓

N 65° 25' E. ✓

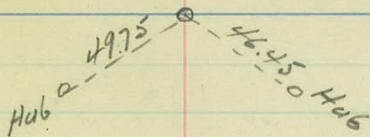
985+35⁰ P.I.

36° 30'

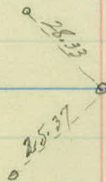
981+57⁰ P.C. Beg. Proj. ✓

959+13.6 P.O.T. - State Notes

N 28° 55' E. ✓



10° Govt. Mont.



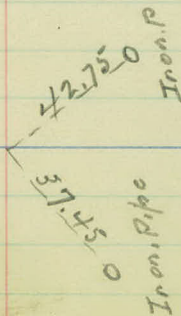
5° Curve Rt.

$\Delta = 36^{\circ}30'$

Rad = 1146.28 ✓

Tang = 377.99 ✓

Length = 730.00 ✓



Station

^E
Ang. ht Ang. Rt.

1053+05.6 P.O.T

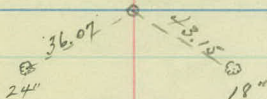
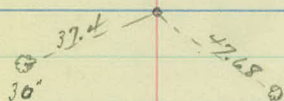
1036+21.6 P.O.T.

N.14°00'E ✓

1023+52.25 P.T. ✓

1021+93.9 P.I. 51025'

1020+09.4 P.C. ✓



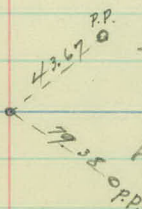
15° Curve. 4t.

$$\Delta = 51^{\circ} 25'$$

$$\text{Rad} = 383.07 \checkmark$$

$$\text{Tang} = 184.43 \checkmark$$

$$\text{Length} = 342.78 \checkmark$$



Station

Ang. ht. ^{ft.} Ang. Pt

1075+72.61 P.T. ✓

N. 80° 15' E.

1074+67.5 P.I.

44° 42'

1073+49.4 P.C. ✓

1069+38.8 P.O.T

N. 35° 33' E.

1061+27.94 P.T. ✓

1058+61.85 P.I.

21° 33'

1055+89.19 P.C. ✓

Sta - Def

$$1073+49'' = 0^\circ 00'$$

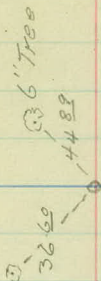
$$1074+00 = 5^\circ 05'$$

$$+50 - 10^\circ 05'$$

$$1075+00 = 15^\circ 05'$$

$$+50 - 20^\circ 05'$$

$$1075+72'' = 22^\circ 21'$$



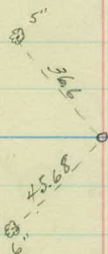
20° Curve Rt.

$$\Delta = 44042'$$

$$Rad = 287.94 \checkmark$$

$$Tang = 118.39 \checkmark$$

$$Length = 223.50 \checkmark$$



Sta Def

$$1055+89.19 = 0^\circ 00'$$

$$1056+00 = 0^\circ 13'$$

$$1057+00 = 2^\circ 13'$$

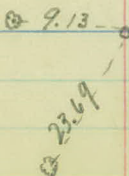
$$1058+00 = 4^\circ 13'$$

$$1059+00 = 6^\circ 13'$$

$$1060+00 = 8^\circ 13'$$

$$1061+00 = 10^\circ 13'$$

$$+27.94 = 10^\circ 46\frac{1}{2}'$$



4° Curve, Rt.

$$\Delta = 21^\circ 33'$$

$$Rad = 1432.69 \checkmark$$

$$Tang = 272.66 \checkmark$$

$$Length = 538.75 \checkmark$$

Station

Aug. Ht. [±] Aug. Rt.

$$1079+23^{\text{let}} = 12+34.35 \text{ (Proj. 25-58)}$$

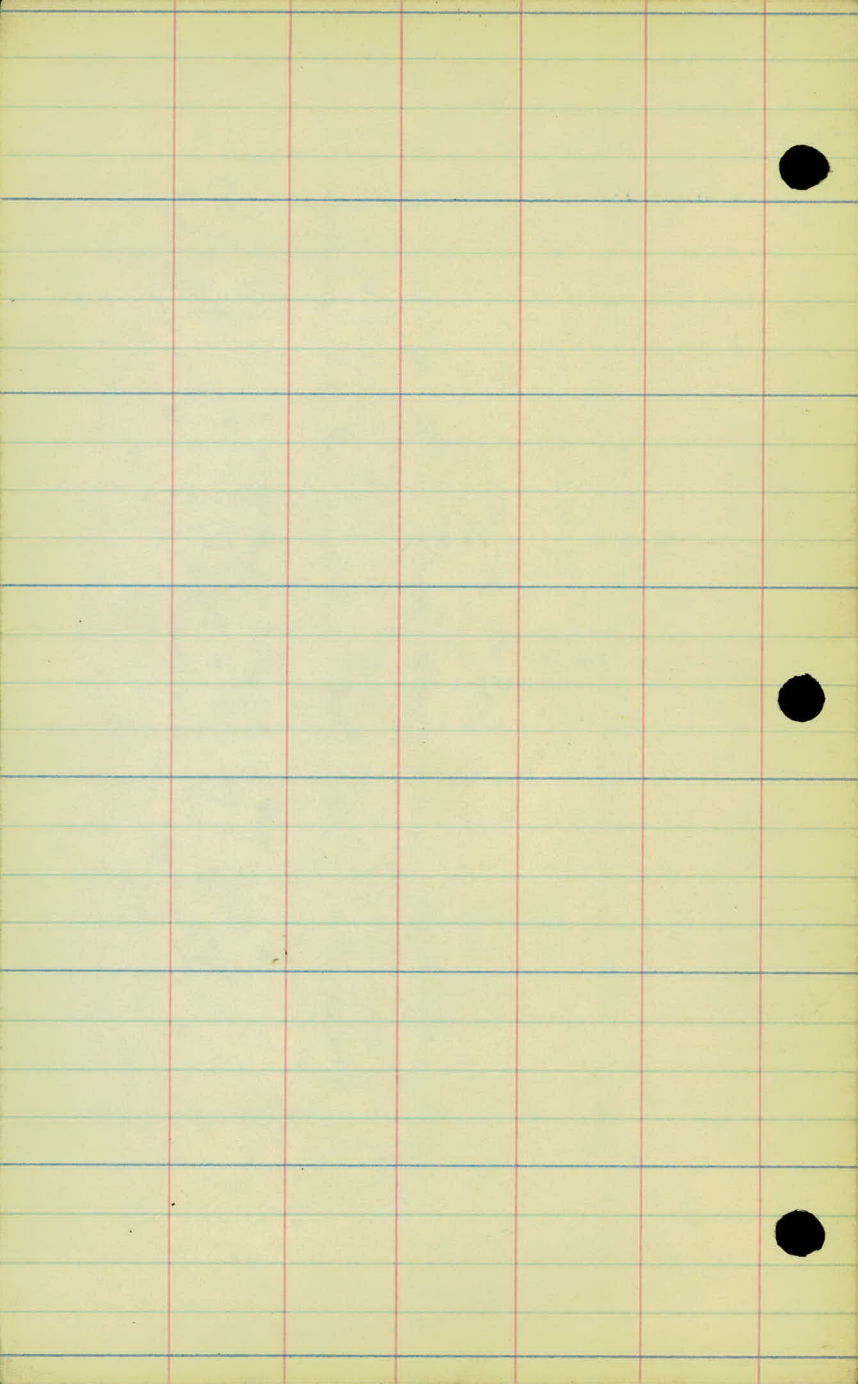
1078+529 } Edge Mpls. Pav.
1078+26 } $\frac{1}{2}$ M.Phs. Pav.

1078+00 Edge M.Phs. Pav

← To. St. Paul

← Proj. - 25-58

52028 →



ST.H. #52 Connection
At. Font Snelling.

4 levels

Sta 981+57 To 1079+234

Station	+	H.I.	-	Red.	Elev.
B.M.	8.06	821.72			813.66
T.P.	7.09	828.44	0.37	821.35	
981+57	P.C.			5.9	822.5
982+00				5.7	22.7
+50				5.5	22.9
983+00				5.2	23.2
+57				5.4	23.0
+77				6.7	21.7
+85				4.7	23.7
984+00				4.7	23.7
+50				5.1	23.3
985+00				6.8	21.6
+50				8.7	19.7
986+00				10.8	17.6
T.P.	3.67	821.97	10.14	818.30	
+50				3.6	18.4
987+00				2.4	19.6
+50				3.7	18.3
988+00				4.5	17.5
+50				6.3	15.7
989+00				7.4	14.6
+50				8.3	13.7
990+00				8.0	14.0
+50				8.0	14.0
991+00				7.3	14.7
T.P.	0.26	815.42	6.81	815.16	
B.M.					813.66

3-25-26

Spike, in 40" Cottonwood 100' Rt. Sta (991+50 state)

Sp. in 40" Tree. 350' ht. St. 990+75 = (991+50 state)

Station	+	H.I	-	Rod	Elev
		815.42			
991+50				2.2	813.2
992+00				3.2	12.2
+50				3.7	11.7
993+00				5.0	10.4
+46				6.3	09.1
+54				6.3	09.1
+56				8.2	07.2
+58.5				8.2	07.2
+61.5				6.2	09.2
+74				6.5	08.9
+81				5.4	10.0
994+00				4.8	10.6
+48				4.0	11.4
+50				5.2	10.2
995+00				3.8	11.6
+27				4.0	11.4
+32				5.0	10.4
+50				4.2	11.2
996+00				3.5	11.9
+50				3.4	12.0
997+00				2.8	12.6
T.P.	3.23	816.42	2.23	813.19	
998+00				5.2	11.2
+50				3.9	12.5
+36				3.8	12.6

Ditch Bottom

✓✓ ✓✓

Station	+	H.I.	-	Rod	Elev.
		816.42			
999+00				4.9	811.5
1000+00				4.9	11.5
1001+00				4.6	11.8
1002+00				4.8	11.6
1003+00				5.3	11.1
1004+00				4.9	11.5
T.P.	4.50	816.57	4.35	812.07	
1005+00				5.1	11.5
1006+00				6.4	10.2
1007+00				5.5	11.1
B.M.				4.04	812.53
					CA 812.54
1008+00				5.0	11.6
1009+00				5.2	11.4
1010+00				4.8	11.8
T.P.	4.40	816.91	4.06	812.51	
1011+00				5.0	11.9
+50				5.7	11.2
1012+00				5.3	11.6
1013+00				4.3	12.6
1014+00				4.6	12.3
1015+00				4.2	12.7
1016+00				3.2	13.7
1017+00				2.0	14.9
T.P.	4.72	820.35	1.28	815.63	
+25				4.9	15.5

Sp. in 12" OAK 50' ht. Sta. 1007+60

Station	+	H.I.	-	Rod.	Elev
		820.35			
1019+00				5.7	814.7
1019+00				5.4	15.0
+38				4.6	15.8
+47				3.0	17.4
+50				5.0	15.4
+63				5.5	14.9
+69				3.8	16.6
+91				4.0	15.4
+94				6.8	13.6
+96				6.8	13.6
+97				4.8	15.6
1020+00				4.8	15.6
+07				4.2	16.0
+34.5				4.8	15.6
+37				5.7	14.7
+38				5.7	14.7
+42.5				4.5	15.9
+50				4.8	15.6
1021+00				5.1	15.3
+04				5.0	15.4
+15				3.8	16.6
+23				5.8	14.6
+24				5.8	14.6
+28				5.2	15.2
+50				5.4	15.0
B.M.	2.49	818.03	4.81	815.54	CA. 815.56

Ditch Bottom

vv vv

$\frac{1}{2}$ Road

Ditch Bottom

vv vv

Station	+	H.I.	-	Rod	Elev.
		818.03			
1022 +00				3.7	814.3
+50				5.1	12.9
1023 +00				6.8	11.2
+50				6.9	11.1
1024 +00				6.6	11.4
1025 +00				6.4	11.6
1026 +00				6.0	12.0
T.P.	7.00	818.70	6.33	811.70	
1027 +00				6.0	12.7
1028 +00				5.6	13.1
1029 +00				5.1	13.6
1030 +00				4.6	14.1
B.M.				0.58	818.12
1031 +00				4.1	14.6
1032 +00				3.7	15.0
T.P.	7.52	822.30	3.92	814.78	
1033 +00				6.4	15.9
1034 +00				5.5	16.8
1035 +00				5.1	17.2
1036 +00				4.7	17.6
+50				4.8	17.5
1037 +00				5.2	17.1
1038 +00				6.6	15.7
T.P.	3.13	818.39	7.04	815.26	
1039 +00				3.5	14.9

Mac

Top. Hydrant 125' Rt. Sta 1030+45

Station	+	H.I.	-	Rod.	Elev.	
		818.39				
1040+00				4.2	814.2	
1041+00				5.0	13.4	
1042+00				5.3	13.1	
1043+00				5.6	12.8	
1044+00				5.7	12.7	
B.M.				0.17	818.22	check 818.22
1045+00				5.7	12.7	
T.P.	5.17	818.41	5.15	813.24		
1046+00				5.7	12.7	
1047+00				5.5	12.9	
1048+00				5.3	13.1	
1049+00				5.0	13.4	
1050+00				4.6	13.8	
1051+00				4.1	14.3	
1052+00				3.7	14.7	
T.P.	7.50	821.84	4.07	814.84		
1053+00				6.4	15.4	
1054+00				5.8	16.0	
+50				5.4	16.4	
B.M.				1.81	820.03	check 820.05
1055+00				5.1	16.7	
1056+00				5.4	16.4	
+40				5.6	16.2	
1057+00				5.9	15.9	
1058+00				6.5	15.3	
T.P.	5.73	821.88	5.69	816.15		

Top Hydrant. 125' Rt. Stn 1044+00

Top Hydrant. 25' Rt. Stn 1054+50

Station	+	H.I.	-	Rod	Elev.
		821.88			
1059	+00			6.5	815.4
1060	+00			6.0	15.9
1061	+00			5.5	16.4
1062	+00			5.1	16.8
1063	+00			4.6	17.3
1064	+00			4.0	17.9
1065	+00			3.5	18.4
T.P.		6.17 . 825.53	2.52	819.36	
1066	+00			6.7	18.8
1067	+00			6.0	19.5
1068	+00			5.4	20.1
1069	+00			4.8	20.7
	+50			4.6	20.9
1070	+00			4.6	20.9
	+50			5.0	20.5
B.M.				1.59	823.94
					CXeck 82396
1071	+00			5.5	20.0
T.P.		2.45 822.27	5.71	819.82	
1072	+00			3.4	18.9
1073	+00			4.5	17.8
B.M.		3.86 821.51	4.62	817.65	
	+50			4.3	17.2
1074	+00			5.0	16.5
	+43			5.7	15.8
	+43			5.25	16.26
	+50			5.25	16.26

Top. Hydrant. 30' Rt. Sta. 1070+70

Top. Hydrant. 60' ht. Sta. 1075+60

Top. Curb
on sidewalk

Station + H.I. - Rod Elev.

821.51

1075+00 5.0 816.5

+50 4.8 16.7

1076+00 5.1 16.4

+61 6.1 15.4

1077+00 7.4 14.1

+50 9.4 12.1

+70 10.0 11.5

T.P. 4.42 814.27 11.66 809.85

1078+00 6.52 807.75

+26 6.63 807.64

+52.9 7.17 807.10

B.M. 5.61 { 808.66 =
113.28

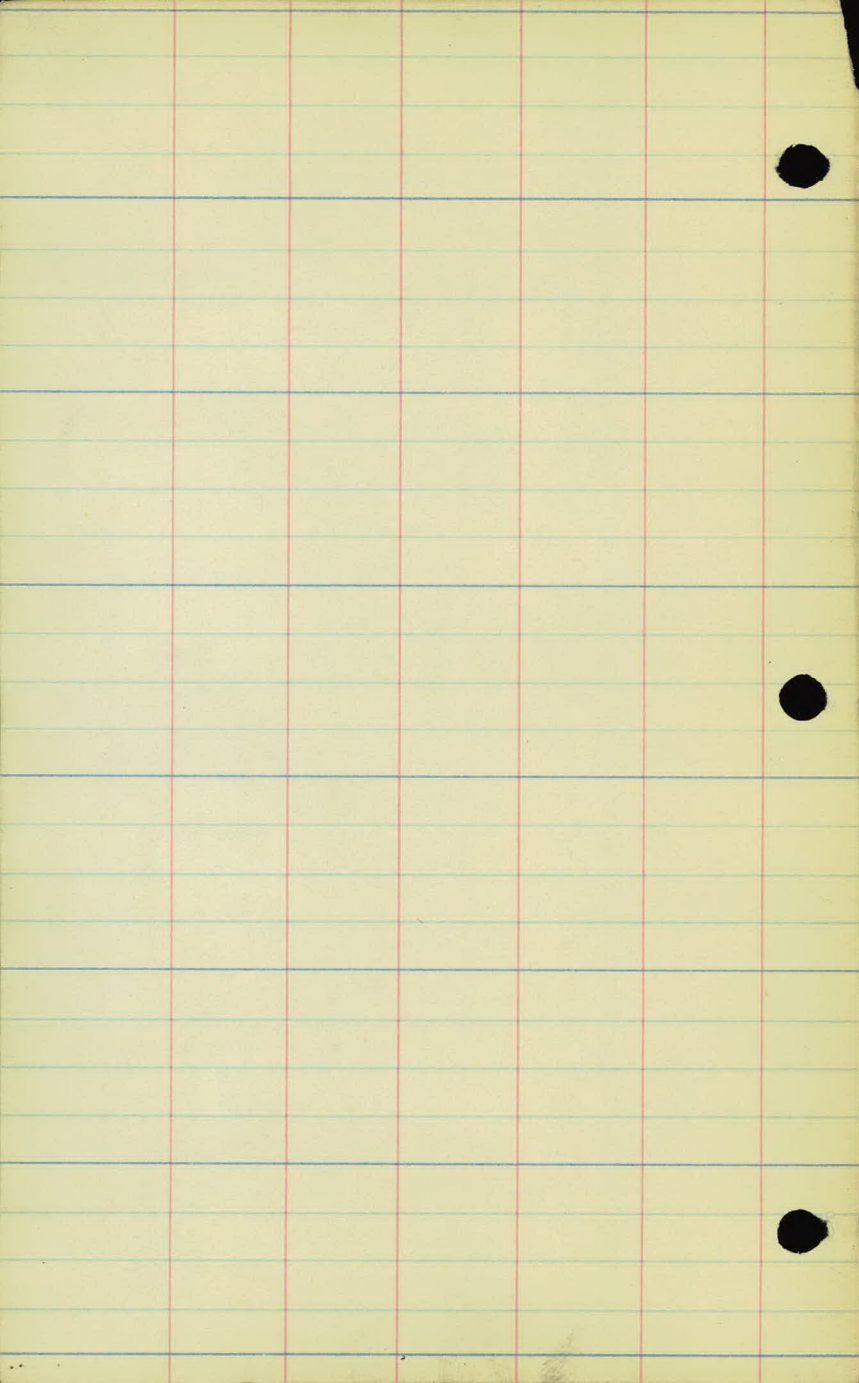
CX80868

Edge. Pav

h "

Edge. Pav

Spike in 30' Tree. 102' Rt. Sta 11+62 } Proj. 25-58



St. H. #52 Connection
At. Fort Snelling.

X-Sections

Sta 981+57-1079+2364

Station	+	H.I.	-	Rod	Elev.
B.M.	9.24	822.90			813.66
T.P.	5.93	825.22	0.61	822.29	
981+57	P.C.			56	226.
982+00				57	225.
+50				54	228.
983+00				50	232.
+50				52	230.
+75				66	216.
984+00				45	237.
985+00				66	216.
986+00				106	176.
+50				100	182.
987+00				87	195.
T.P.	0.43	820.62	8.03	820.19	
+50				24	182.

Sp. in 40 Cottonwood. 350 ft. stop 990+75 = { state. }
 991+50

$\frac{6.7}{50}$ $\frac{6.2}{20}$ $\frac{7.3}{19}$ $\frac{7.3}{18}$ $\frac{6.0}{14}$ 5.6 $\frac{5.8}{14}$ $\frac{7.6}{19}$ $\frac{7.6}{20}$ $\frac{6.3}{22}$ $\frac{6.6}{38}$ $\frac{6.5}{50}$

$\frac{5.7}{50}$ $\frac{6.1}{21}$ $\frac{7.0}{19}$ $\frac{7.0}{18}$ $\frac{6.0}{16}$ 5.7 $\frac{6.1}{15}$ $\frac{8.0}{19}$ $\frac{8.0}{20}$ $\frac{6.6}{22}$ $\frac{6.6}{40}$ $\frac{6.6}{50}$

$\frac{5.7}{50}$ $\frac{5.6}{35}$ $\frac{6.0}{24}$ $\frac{7.2}{22}$ $\frac{7.2}{21}$ $\frac{5.7}{18}$ $\frac{5.5}{10}$ 5.4 $\frac{5.8}{13}$ $\frac{7.3}{16}$ $\frac{7.3}{17}$ $\frac{5.5}{18}$ $\frac{6.0}{50}$

$\frac{5.5}{50}$ $\frac{5.0}{31}$ $\frac{7.0}{28}$ $\frac{5.5}{26}$ $\frac{4.8}{9.0}$ 5.0 $\frac{5.2}{8.0}$ $\frac{6.8}{11}$ $\frac{6.8}{12}$ $\frac{5.2}{14}$ $\frac{5.3}{50}$

$\frac{4.6}{50}$ $\frac{5.0}{28}$ $\frac{6.8}{35}$ $\frac{5.3}{32}$ $\frac{4.8}{15}$ 5.2 $\frac{5.4}{1.5}$ $\frac{6.6}{5.0}$ $\frac{6.6}{6.0}$ $\frac{4.7}{7.0}$ $\frac{5.4}{50}$

$\frac{4.7}{50}$ $\frac{5.0}{43}$ $\frac{7.0}{41}$ $\frac{5.3}{37}$ $\frac{5.0}{20}$ $\frac{5.3}{4.0}$ 6.6 $\frac{4.7}{2.0}$ $\frac{5.0}{30}$ $\frac{5.6}{50}$

$\frac{4.8}{50}$ $\frac{5.1}{48}$ $\frac{7.1}{45}$ $\frac{5.3}{42}$ $\frac{4.8}{26}$ $\frac{5.3}{10}$ $\frac{6.5}{6.0}$ $\frac{4.6}{4.0}$ 4.5 $\frac{5.2}{19}$ $\frac{5.8}{50}$

$\frac{5.9}{56}$ $\frac{6.0}{50}$ $\frac{6.1}{42}$ $\frac{6.4}{38}$ $\frac{7.3}{34}$ $\frac{5.7}{33}$ $\frac{5.6}{21}$ $\frac{6.2}{14}$ 6.6 $\frac{7.8}{25}$ $\frac{8.4}{50}$

$\frac{9.4}{50}$ $\frac{10.2}{36}$ $\frac{10.2}{23}$ 10.6 $\frac{10.4}{25}$ $\frac{10.2}{50}$

$\frac{10.6}{50}$ $\frac{10.7}{23}$ 10.0 $\frac{10.0}{25}$ $\frac{10.0}{50}$

$\frac{9.0}{50}$ $\frac{9.0}{17}$ $\frac{9.4}{6.0}$ 8.7 $\frac{9.0}{25}$ $\frac{9.1}{50}$

$\frac{1.8}{50}$ $\frac{1.6}{25}$ $\frac{1.8}{1.0}$ 2.4 $\frac{1.7}{8.0}$ $\frac{1.7}{25}$ $\frac{1.7}{50}$

Station + H.I. - Rod. Elev.

820.62

988+00

817.3

989+00

14.6

990+00

13.9

991+00

14.6

992+00

12.2

993+00

10.2

T.P. 6.47 917.42 9.67 910.95

+50

09.3

994+00

10.4

+67

11.0

995+00

11.5

+50

11.1

996+00

11.8

ht.

K

ht.

$$\frac{4.5}{50} \quad \frac{3.5}{27} \quad \frac{2.8}{10} \quad 3.3 \quad \frac{3.3}{6.0} \quad \frac{4.0}{7.0} \quad \frac{3.8}{14} \quad \frac{2.8}{19} \quad \frac{2.8}{50}$$

$$\frac{6.7}{50} \quad \frac{6.4}{25} \quad 6.0 \quad \frac{6.2}{24} \quad \frac{6.0}{50}$$

$$\frac{7.0}{50} \quad \frac{6.8}{25} \quad 6.7 \quad \frac{6.5}{25} \quad \frac{6.3}{50}$$

$$\frac{7.3}{50} \quad \frac{6.5}{25} \quad 6.0 \quad \frac{6.8}{25} \quad \frac{6.7}{50}$$

$$\frac{8.2}{50} \quad \frac{8.0}{21} \quad 8.4 \quad \frac{7.7}{8.0} \quad \frac{8.2}{9.0} \quad \frac{8.2}{13} \quad \frac{7.6}{15} \quad \frac{9.1}{50}$$

$$\frac{10.0}{50} \quad \frac{10.7}{30} \quad \frac{10.8}{14} \quad 10.4 \quad \frac{10.2}{25} \quad \frac{10.6}{50}$$

$$\frac{9.2}{50} \quad \frac{9.2}{40} \quad \frac{8.4}{27} \quad 8.1 \quad \frac{8.7}{25} \quad \frac{9.0}{50}$$

$$\frac{7.5}{50} \quad \frac{8.5}{46} \quad \frac{8.6}{38} \quad \frac{7.6}{35} \quad \frac{7.3}{17} \quad \frac{8.0}{14} \quad \frac{8.2}{8.0} \quad 7.0 \quad \frac{7.0}{25} \quad \frac{6.6}{50}$$

$$\frac{7.0}{50} \quad \frac{6.7}{44} \quad \frac{8.1}{36} \quad \frac{7.5}{31} \quad \frac{7.0}{29} \quad \frac{5.5}{23} \quad \frac{5.2}{8.0} \quad \frac{5.8}{5.0} \quad 6.4 \quad \frac{6.0}{4.0} \quad \frac{5.8}{21} \quad \frac{6.0}{50}$$

$$\frac{6.2}{50} \quad \frac{6.4}{35} \quad \frac{7.6}{22} \quad \frac{7.6}{17} \quad \frac{6.7}{14} \quad 5.9 \quad \frac{5.9}{22} \quad \frac{5.9}{50}$$

$$\frac{5.6}{50} \quad \frac{6.0}{38} \quad \frac{5.7}{20} \quad 6.3 \quad \frac{6.8}{3.0} \quad \frac{6.8}{8.0} \quad \frac{5.8}{11} \quad \frac{5.8}{29} \quad \frac{5.8}{50}$$

$$\frac{4.8}{50} \quad \frac{5.3}{41} \quad \frac{5.3}{23} \quad 5.6 \quad \frac{6.0}{22} \quad \frac{5.7}{38} \quad \frac{5.8}{50}$$

Station + H.I. - Rod Elev

817.42

997+00 12.6

998+00 11.2

999+00 11.4

1000+00 11.4

T.P. 4.09 816.39 5.12 812.50

1001+00 11.8

1002+00 11.5

1003+00 11.1

1004+00 11.5

1005+00 11.4

1006+00 10.1

1007+00 11.0

B.M. 3.99 816.52 3.93 812.46 812.53

1008+00 11.5

Ht

4

TR4

$\frac{5.0}{50}$	$\frac{4.9}{25}$	4.8	$\frac{5.4}{20}$	$\frac{5.8}{35}$	$\frac{6.4}{42}$	$\frac{6.1}{50}$
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$\frac{5.4}{50}$	$\frac{5.6}{27}$	6.2	$\frac{6.4}{25}$	$\frac{6.8}{50}$
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$\frac{5.1}{50}$	$\frac{5.6}{25}$	6.0	$\frac{6.3}{27}$	$\frac{6.6}{50}$
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$\frac{5.6}{50}$	$\frac{6.0}{22}$	6.0	$\frac{6.4}{25}$	$\frac{6.5}{50}$
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$\frac{4.5}{50}$	$\frac{4.5}{25}$	4.6	$\frac{4.8}{30}$	$\frac{4.8}{50}$ ✓
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$\frac{4.7}{50}$	$\frac{4.7}{25}$	4.9	$\frac{5.1}{25}$	$\frac{5.1}{50}$ ✓
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$\frac{5.0}{50}$	$\frac{5.2}{25}$	5.3	$\frac{5.6}{25}$	$\frac{5.3}{50}$
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$\frac{5.1}{50}$	$\frac{5.0}{25}$	4.9	$\frac{5.0}{25}$	$\frac{5.0}{50}$
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$\frac{5.2}{50}$	$\frac{5.2}{22}$	5.0	$\frac{5.6}{28}$	$\frac{5.6}{50}$
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$\frac{6.0}{50}$	$\frac{6.2}{25}$	6.3	$\frac{6.6}{30}$	$\frac{6.5}{50}$
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$\frac{5.2}{50}$	$\frac{5.1}{25}$	5.4	$\frac{5.8}{27}$	$\frac{5.5}{50}$
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Sp. in 12" Oak 50' Ht Sta 1007+60

$\frac{5.4}{50}$	$\frac{5.0}{25}$	5.0	$\frac{5.2}{27}$	$\frac{5.4}{50}$
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Station	+	H.I.	-	Rod.	Elev
		816.52			
1009+00					11.5.
1010+00					11.7.
1011+00					12.0.
+50					11.3.
1012+00					11.6.
1013+00					12.6.
1014+00					12.2.
1015+00					12.7.
T.P.	6.17	819.73	2.96	813.56	
1016+00					13.7.
1017+00					14.9.
1018+00					14.6.
1019+00					14.9.

51.

2

77

$$\frac{5.1}{50} \quad \frac{4.8}{30} \quad 5.0 \quad \frac{5.2}{20} \quad \frac{5.0}{50} \quad |$$

$$\frac{6.0}{50} \quad \frac{5.3}{30} \quad 4.8 \quad \frac{4.8}{25} \quad \frac{4.7}{50} \quad |$$

$$\frac{4.8}{50} \quad \frac{4.7}{25} \quad 4.5 \quad \frac{4.5}{25} \quad \frac{4.7}{50} \quad |$$

$$\frac{4.9}{50} \quad \frac{5.1}{27} \quad 5.2 \quad \frac{4.8}{22} \quad \frac{4.5}{50} \quad |$$

$$\frac{5.1}{50} \quad \frac{5.4}{22} \quad 4.9 \quad \frac{4.4}{30} \quad \frac{3.8}{50} \quad |$$

$$\frac{5.0}{50} \quad \frac{4.4}{25} \quad 3.9 \quad \frac{3.5}{27} \quad \frac{3.4}{50} \quad |$$

$$\frac{4.5}{50} \quad \frac{4.5}{25} \quad 4.3 \quad \frac{3.7}{25} \quad \frac{3.8}{50} \quad |$$

$$\frac{4.8}{50} \quad \frac{4.0}{23} \quad 3.8 \quad \frac{3.3}{20} \quad \frac{3.3}{25} \quad \frac{2.5}{50} \quad |$$

$$\frac{6.8}{50} \quad \frac{6.4}{25} \quad 6.0 \quad \frac{5.8}{25} \quad \frac{6.0}{50} \quad |$$

$$\frac{5.3}{50} \quad \frac{4.7}{25} \quad 4.8 \quad \frac{4.6}{12} \quad \frac{4.8}{24} \quad \frac{5.7}{37} \quad \frac{5.8}{50} \quad |$$

$$\frac{4.3}{50} \quad \frac{4.5}{32} \quad \frac{4.3}{10} \quad 5.1 \quad \frac{5.4}{22} \quad \frac{5.5}{50} \quad |$$

$$\frac{5.4}{50} \quad \frac{4.9}{20} \quad 4.8 \quad \frac{4.3}{13} \quad \frac{4.0}{26} \quad \frac{6.0}{29} \quad \frac{6.8}{31} \quad \frac{5.7}{33} \quad \frac{4.2}{34} \quad |$$

$$\left. \begin{array}{l} 4.9 \\ 5.0 \end{array} \right\}$$

Station	+	H.I.	-	Red Elev.
		819.73		
1019+32				15.8-
+45				17.3-
+58				14.9-
+69				16.5.
1020+00				15.4-
+50				15.5-
1021+00				15.4-
B.M.	3.62	819.16	4.17	815.56
+50				815.54
+50				15.0-
1022+00				14.3.
+50				13.1-
1023+00				11.5.
+50				11.1-

H.

K

KA

$$\frac{5.0}{50} \quad \frac{4.4}{25} \quad 3.9 \quad \frac{2.3}{8.0} \quad \frac{3.5}{10} \quad \frac{5.7}{11} \quad \frac{6.4}{14} \quad \frac{4.0}{15} \quad \frac{3.3}{21} \quad \frac{4.0}{30} \quad \frac{4.5}{50}$$

$$\frac{4.8}{50} \quad \frac{4.0}{22} \quad \frac{4.3}{12} \quad 2.4 \quad \frac{2.7}{1.5} \quad \frac{6.0}{5.0} \quad \frac{6.0}{7.0} \quad \frac{3.4}{7.0} \quad \frac{3.8}{18} \quad \frac{3.7}{31} \quad \frac{4.6}{50}$$

$$\frac{4.4}{50} \quad \frac{3.9}{25} \quad \frac{3.3}{12} \quad 4.8 \quad \frac{4.6}{2.5} \quad \frac{3.2}{4.0} \quad \frac{3.8}{23} \quad \frac{4.3}{50}$$

$$\frac{4.3}{50} \quad \frac{4.1}{37} \quad \frac{3.4}{18} \quad \frac{2.5}{12} \quad \frac{3.3}{9.0} \quad \frac{6.0}{6.0} \quad \frac{6.0}{4.0} \quad \frac{3.6}{2.0} \quad 3.2 \quad \frac{3.8}{25} \quad \frac{4.3}{50}$$

$$\frac{4.7}{50} \quad \frac{4.2}{43} \quad \frac{4.1}{25} \quad 4.3 \quad \frac{4.3}{23} \quad \frac{4.9}{50}$$

$$\frac{4.7}{50} \quad \frac{4.4}{27} \quad 4.2 \quad \frac{4.4}{26} \quad \frac{4.2}{50}$$

$$\frac{5.5}{50} \quad \frac{4.6}{30} \quad 4.3 \quad \frac{4.4}{10} \quad \frac{4.6}{27} \quad \frac{4.6}{50}$$

$$\frac{4.0}{20} \quad \frac{3.2}{16} \quad \frac{4.0}{14} \quad \frac{4.1}{12} \quad \frac{5.0}{10} \quad \frac{5.0}{9.0} \quad \frac{4.1}{7.0} \quad 4.2 \quad \frac{4.3}{18} \quad \frac{4.6}{19} \quad \frac{3.4}{21} \quad \frac{3.1}{33} \quad \frac{3.5}{26} \quad \frac{4.0}{50}$$

$$\frac{6.6}{50} \quad \frac{6.5}{38} \quad \frac{5.9}{32} \quad \frac{4.4}{26} \quad \frac{6.2}{22} \quad \frac{6.2}{20} \quad \frac{5.1}{16} \quad 4.9 \quad \frac{5.2}{8.0} \quad \frac{5.6}{10} \quad \frac{5.8}{12} \quad \frac{4.0}{17} \quad \frac{3.4}{24} \quad \frac{3.8}{50}$$

$$\frac{8.8}{50} \quad \frac{9.1}{34} \quad \frac{7.7}{32} \quad \frac{7.6}{20} \quad \frac{6.5}{15} \quad 6.1 \quad \frac{5.9}{9.0} \quad \frac{6.8}{12} \quad \frac{6.8}{13} \quad \frac{3.8}{18} \quad \frac{5.1}{23} \quad \frac{4.5}{20} \quad \frac{5.5}{22} \quad \frac{4.5}{50}$$

$$\frac{8.8}{40} \quad \frac{9.2}{28} \quad \frac{9.0}{16.2} \quad \frac{8.5}{16.2} \quad 7.7 \quad \frac{7.5}{25} \quad \frac{6.8}{39} \quad \frac{6.8}{50}$$

$$\frac{9.6}{42} \quad \frac{8.1}{41} \quad \frac{9.3}{19.6} \quad \frac{8.6}{19.6} \quad 8.1 \quad \frac{8.5}{19.7} \quad \frac{8.1}{19.7} \quad \frac{8.1}{38}$$

Station + H.I. - Rod. Elev

819.16

1024+00 11.5.

1025+00 11.7.

1026+00 12.1.

T.P. 7.15 819.03 7.28 811.88

1027+00 12.6.

1028+00 13.1.

1029+00 13.6.

1030+00 14.1.

B.M. 0.89 818.14 818.12

1031+00 14.5.

1032+00 15.0.

1033+00 15.8.

T.P. 7.50 822.60 3.93 815.10

1034+00 16.7.

1035+00 17.2.

Ht. - 2 R4

S. Walk C
 $\frac{7.5}{42.6}$ $\frac{8.1}{19.5}$ $\frac{8.5}{19.5}$ 7.7 $\frac{8.5}{19.6}$ $\frac{8.1}{19.6}$ $\frac{7.9}{20.6}$ $\frac{8.1}{33}$ ✓

S.W C
 $\frac{7.2}{42.6}$ $\frac{7.7}{19.4}$ $\frac{8.2}{19.4}$ 7.5 $\frac{8.2}{19.6}$ $\frac{7.8}{19.6}$ $\frac{7.6}{33}$ ✓

S.W C
 $\frac{6.9}{42.5}$ $\frac{7.5}{19.4}$ $\frac{8.0}{19.4}$ 7.1 $\frac{7.9}{19.6}$ $\frac{7.2}{19.6}$ $\frac{7.1}{33}$ ✓

S.W C
 $\frac{6.2}{42.5}$ $\frac{6.7}{19.6}$ $\frac{7.2}{19.6}$ 6.4 $\frac{7.2}{19.5}$ $\frac{6.7}{19.5}$ $\frac{6.2}{33}$ ✓

S.W C
 $\frac{5.6}{42.5}$ $\frac{6.2}{19.5}$ $\frac{6.6}{19.5}$ 5.9 $\frac{6.6}{19.4}$ $\frac{6.2}{19.4}$ $\frac{5.8}{33}$ ✓

S.W C
 $\frac{5.0}{42.7}$ $\frac{5.5}{19.5}$ $\frac{6.0}{19.5}$ 5.4 $\frac{6.0}{19.5}$ $\frac{5.6}{19.5}$ $\frac{5.5}{33}$ ✓

S.W C
 $\frac{4.5}{42.7}$ $\frac{5.0}{19.7}$ $\frac{5.5}{19.7}$ 4.9 $\frac{5.5}{19.4}$ $\frac{5.0}{19.4}$ $\frac{4.6}{33}$ ✓

Top. Hyd }
 1030+45 }

S.W C
 $\frac{4.1}{42.6}$ $\frac{4.6}{19.5}$ $\frac{5.0}{19.5}$ 4.8 $\frac{5.0}{19.5}$ $\frac{4.7}{19.5}$ $\frac{4.5}{33}$ ✓

S.W C
 $\frac{3.6}{42.5}$ $\frac{4.2}{19.5}$ $\frac{4.6}{19.5}$ 4.0 $\frac{4.6}{19.5}$ $\frac{4.2}{19.5}$ $\frac{4.1}{33}$ ✓

S.W C
 $\frac{2.8}{42.6}$ $\frac{3.3}{19.5}$ $\frac{3.7}{19.5}$ 3.2 $\frac{3.3}{19.5}$ $\frac{3.2}{19.5}$ $\frac{3.2}{33}$ ✓

Driveway
 $\frac{5.4}{42.7}$ $\frac{6.2}{19.5}$ 5.7 $\frac{6.4}{19.4}$ $\frac{6.0}{19.4}$ $\frac{5.8}{33}$ ✓

S.W C
 $\frac{5.0}{42.7}$ $\frac{5.4}{19.5}$ $\frac{5.8}{19.5}$ 5.4 $\frac{5.9}{19.4}$ $\frac{5.4}{19.4}$ $\frac{5.2}{33}$ ✓

Station	+	H.I.	-	Rod Elev
		822.60		
1036+00				17.6
1037+00				17.1
1038+00				15.8
1039+00				15.0
T.P.	3.44	817.98	8.06	814.54
1040+00				14.2
1041+00				13.5
1042+00				13.2
1043+00				12.8
1044+00				12.7
T.P.	6.02	818.64	5.36	812.62
B.M.	0.68	818.90		0.42 818.22
1045+00				12.7
1046+00				12.7

ht ♀ RT

S.W c
 $\frac{4.7}{42.5}$ $\frac{5.2}{19.5}$ $\frac{5.5}{19.5}$ 5.0 $\frac{5.6}{19.3}$ $\frac{5.2}{19.3}$ $\frac{5.1}{33}$

S.W. c
 $\frac{5.0}{42.7}$ $\frac{5.5}{19.7}$ $\frac{6.0}{19.7}$ 5.5 $\frac{6.0}{19.3}$ $\frac{5.6}{19.3}$ $\frac{5.7}{33}$

S.W c
 $\frac{6.5}{42.6}$ $\frac{7.0}{19.6}$ $\frac{7.3}{19.6}$ 6.8 $\frac{7.4}{19.4}$ $\frac{7.0}{19.4}$ $\frac{6.7}{33}$

S.W c
 $\frac{7.3}{42.5}$ $\frac{7.9}{19.5}$ $\frac{8.2}{19.5}$ 7.6 $\frac{8.1}{19.5}$ $\frac{7.7}{19.5}$ $\frac{7.6}{33}$

W c
 $\frac{3.4}{42.6}$ $\frac{3.9}{19.8}$ $\frac{4.3}{19.8}$ 3.9 $\frac{4.3}{19.5}$ $\frac{3.9}{19.5}$ $\frac{3.5}{33}$ ✓

W c
 $\frac{4.0}{42.5}$ $\frac{4.5}{19.4}$ $\frac{4.9}{19.4}$ 4.5 $\frac{4.9}{19.5}$ $\frac{4.5}{19.5}$ $\frac{4.0}{33}$ ✓

W c
 $\frac{4.6}{42.5}$ $\frac{5.0}{19.5}$ $\frac{5.4}{19.5}$ 4.8 $\frac{5.4}{19.5}$ $\frac{5.0}{19.5}$ $\frac{4.4}{33}$ ✓

W c
 $\frac{4.8}{42.4}$ $\frac{5.4}{19.6}$ $\frac{5.8}{19.6}$ 5.2 $\frac{5.7}{19.5}$ $\frac{5.3}{19.5}$ $\frac{5.0}{33}$ ✓

W c
 $\frac{5.0}{42.5}$ $\frac{5.6}{19.5}$ $\frac{6.0}{19.5}$ 5.3 $\frac{6.0}{19.5}$ $\frac{5.6}{33}$ DRIVEWAY RT ✓

W c
 $\frac{5.9}{42.7}$ $\frac{6.4}{19.6}$ $\frac{6.8}{19.6}$ 6.2 $\frac{6.8}{19.5}$ $\frac{6.4}{19.5}$ $\frac{6.1}{33}$ ✓

W c
 $\frac{5.8}{42.5}$ $\frac{6.2}{19.6}$ $\frac{6.7}{19.6}$ 6.2 $\frac{6.7}{19.6}$ $\frac{6.3}{19.6}$ $\frac{5.7}{33}$ ✓

Station	+	H.I.	-	Rod. Elev.
		818.90		
1047+00				130.
1048+00				131.
T.P.	6.93	820.14	5.69	813.21
1049+00				134.
1050+00				138.
1051+00				144.
1052+00				147.
1053+00				155.
1054+00				161.
B.M.				0.07 819.07
T.P.	3.85	820.15	3.84	816.30
1055+00				168.
1056+00				165.
1057+00				160.

820.07

ht

4

RT

S.W.	c			c			
$\frac{5.4}{42.6}$	$\frac{6.1}{19.6}$	$\frac{6.5}{19.6}$	5.9	$\frac{6.5}{19.5}$	$\frac{6.1}{19.5}$	$\frac{5.7}{33}$	✓

	c			c			
$\frac{5.4}{42.7}$	$\frac{5.9}{19.7}$	$\frac{6.3}{19.7}$	5.8	$\frac{6.2}{19.8}$	$\frac{5.8}{19.8}$	$\frac{5.5}{33}$	✓

	c			c			
$\frac{6.3}{42.8}$	$\frac{6.8}{19.7}$	$\frac{7.3}{19.7}$	6.7	$\frac{7.2}{19.8}$	$\frac{6.8}{19.8}$	$\frac{6.5}{33}$	✓

S.W.	c			c			
$\frac{6.0}{42.7}$	$\frac{6.4}{19.7}$	$\frac{6.8}{19.7}$	6.3	$\frac{6.8}{19.9}$	$\frac{6.4}{19.9}$	$\frac{6.0}{33}$	✓

Rood. ht	$\frac{5.6}{33}$	$\frac{6.2}{18}$	5.7	$\frac{6.4}{19.9}$	$\frac{6.0}{19.9}$	$\frac{5.4}{42.5}$	✓
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	c			c			S.W.
$\frac{4.8}{33}$	$\frac{5.4}{19.8}$	$\frac{5.7}{19.8}$	5.4	$\frac{5.8}{19.9}$	$\frac{5.3}{19.9}$	$\frac{4.7}{42.3}$	✓

	c			c			S.W.
$\frac{4.2}{33}$	$\frac{4.7}{19.8}$	$\frac{5.1}{19.8}$	4.6	$\frac{5.1}{19.8}$	$\frac{4.7}{19.8}$	$\frac{3.8}{42.3}$	✓

	c			c			S.W.
$\frac{3.8}{33}$	$\frac{4.1}{19.7}$	$\frac{4.5}{19.7}$	4.0	$\frac{4.5}{19.8}$	$\frac{4.1}{19.8}$	$\frac{3.1}{42.3}$	✓

	c			c			S.W.	
$\frac{3.3}{33}$	$\frac{3.5}{19.6}$	$\frac{3.9}{19.6}$	3.2	$\frac{3.8}{19.9}$	$\frac{3.7}{25}$	$\frac{3.4}{25}$	$\frac{3.0}{42}$	Rood. ✓

	c			c			S.W.	
$\frac{3.1}{33}$	$\frac{4.0}{19.7}$	$\frac{4.4}{19.7}$	3.7	$\frac{4.0}{20}$	$\frac{4.0}{25}$	$\frac{3.7}{25}$	$\frac{3.4}{41.8}$	Rood. ✓

	S.W.							
$\frac{4.0}{33}$	$\frac{4.1}{23.2}$	$\frac{4.9}{19}$	4.2	$\frac{4.7}{17}$	$\frac{4.5}{19}$	$\frac{4.6}{20.6}$	$\frac{4.0}{38.2}$	✓

Station	+	H.I.	-	Rod Elev
		820.15		
1058+00				15.5
1059+00				15.4
1060+00				16.0
1061+00				16.6
1062+00				16.8
T.P.	7.26	823.93	3.46	816.67
1063+00				17.3
1064+00				17.9
1065+00				18.3
1066+00				18.9
1067+00				19.6
1068+00				20.1
1069+00				20.7
T.P.	4.14	824.61	3.46	820.47

ht. ♀ Rt.

$$\frac{5.3}{33} \quad \frac{4.4}{21.0} \quad \frac{5.3}{18.5} \quad \frac{5.4}{17.5} \quad 4.7 \quad \frac{5.1}{15.6} \quad \frac{5.0}{18} \quad \frac{4.6}{19.5} \quad \frac{S.W.}{4.4} \quad 30.5$$

$$\frac{5.0}{33} \quad \frac{4.6}{18.0} \quad \frac{5.3}{15.8} \quad \frac{5.3}{14.4} \quad \frac{5.0}{13.0} \quad 4.8 \quad \frac{5.2}{15} \quad \frac{5.2}{15.7} \quad \frac{4.7}{17.4} \quad \frac{S.W.}{4.5} \quad 23.0 \quad \checkmark$$

$$\frac{4.5}{33} \quad \frac{3.8}{17.5} \quad \frac{4.4}{15.5} \quad \frac{4.6}{14} \quad 4.2 \quad \frac{4.7}{14.5} \quad \frac{4.7}{16} \quad \frac{4.2}{17.4} \quad \frac{S.W.}{4.2} \quad \checkmark$$

$$\frac{4.0}{33} \quad \frac{3.3}{17.0} \quad \frac{4.1}{14.2} \quad 3.6 \quad \frac{4.1}{15.2} \quad \frac{3.6}{15.2} \quad \frac{C+S.W.}{3.6} \quad \checkmark$$

$$\frac{4.0}{33.0} \quad \frac{3.0}{17.3} \quad \frac{3.6}{15.2} \quad \frac{3.7}{13} \quad 3.4 \quad \frac{3.8}{15.0} \quad \frac{3.3}{15.0} \quad \frac{C+S.W.}{3.3} \quad \checkmark$$

$$\frac{6.8}{33} \quad \frac{6.2}{18.5} \quad \frac{6.7}{15.8} \quad \frac{6.8}{13} \quad 6.6 \quad \frac{7.0}{15} \quad \frac{6.6}{15.0} \quad \frac{C+S.W.}{6.6} \quad \checkmark$$

$$\frac{6.8}{33} \quad \frac{5.8}{17.3} \quad \frac{6.2}{15.6} \quad \frac{6.3}{14.5} \quad 6.0 \quad \frac{6.5}{15} \quad \frac{6.0}{15} \quad \frac{C+S.W.}{6.0} \quad \checkmark$$

$$\frac{5.9}{33} \quad \frac{5.3}{17} \quad \frac{5.8}{15} \quad \frac{5.8}{13.0} \quad 5.6 \quad \frac{6.0}{15.0} \quad \frac{5.5}{15.0} \quad \frac{C+S.W.}{5.5} \quad \checkmark$$

$$\frac{5.2}{33} \quad \frac{4.9}{18.5} \quad \frac{5.4}{12.5} \quad 5.0 \quad \frac{5.5}{15} \quad \frac{5.1}{15} \quad \frac{C+S.W.}{5.1} \quad \checkmark$$

$$\frac{4.5}{33} \quad \frac{4.3}{17} \quad \frac{4.7}{12.5} \quad 4.3 \quad \frac{4.7}{15} \quad \frac{4.4}{15} \quad \frac{C+S.W.}{4.4} \quad \checkmark$$

$$\frac{3.8}{33} \quad \frac{3.5}{23.6} \quad \frac{3.6}{17} \quad \frac{4.0}{14.8} \quad \frac{4.2}{12.5} \quad 3.8 \quad \frac{4.2}{15} \quad \frac{3.8}{15} \quad \frac{C+S.W.}{3.8} \quad \checkmark$$

$$\frac{3.2}{33} \quad \frac{3.2}{26} \quad \frac{3.3}{16.8} \quad \frac{3.6}{15.3} \quad \frac{3.6}{13.5} \quad 3.2 \quad \frac{3.6}{15} \quad \frac{3.2}{15} \quad \frac{C+S.W.}{3.2} \quad \checkmark$$

Station	+	H.I.	-	Rod Elev	
		824.61			
1070+00				20.9	
B.M.			0.62	823.99	823.96
1071+00				20.0	
1072+00				18.9	
1073+00				17.8	
+50				17.2	
1074+00				16.6	
+50				16.3	
B.M.	2.06	819.76	6.91	817.70	check 817.68
1075+00				16.5	
+50				16.8	
1076+00				16.4	
1077+00				14.2	
+50				12.2	

51

4

Rt.

$\frac{2.7}{33}$	$\frac{3.5}{17}$	$\frac{4.0}{15.4}$	$\frac{4.1}{13.6}$	3.7	$\frac{4.1}{15}$	$\frac{3.5}{18}$	✓
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C+S.W

$\frac{3.9}{33}$	$\frac{3.9}{25}$	$\frac{4.2}{23.5}$	$\frac{4.0}{17.3}$	$\frac{4.8}{14.5}$	4.6	$\frac{4.8}{15}$	$\frac{4.3}{15}$	✓
------------------	------------------	--------------------	--------------------	--------------------	-----	------------------	------------------	---

C+S.W

$\frac{5.0}{33}$	$\frac{5.0}{25.5}$	$\frac{5.2}{24.5}$	$\frac{5.2}{17.3}$	$\frac{6.0}{14.5}$	5.7	$\frac{6.0}{15}$	$\frac{5.5}{15}$	✓
------------------	--------------------	--------------------	--------------------	--------------------	-----	------------------	------------------	---

C+S.W

$\frac{6.0}{33}$	$\frac{6.0}{28}$	$\frac{6.5}{24.3}$	$\frac{6.5}{16.5}$	$\frac{7.1}{14.4}$	6.8	$\frac{7.2}{15.2}$	$\frac{6.7}{15.2}$	$\frac{6.6}{21}$	$\frac{6.3}{23}$	$\frac{6.2}{33}$
------------------	------------------	--------------------	--------------------	--------------------	-----	--------------------	--------------------	------------------	------------------	------------------

C+S.W

$\frac{6.7}{33}$	$\frac{7.2}{17}$	$\frac{7.7}{15}$	7.4	$\frac{7.8}{15.2}$	$\frac{7.4}{15.2}$	$\frac{7.2}{21}$	$\frac{6.8}{24}$	$\frac{6.7}{33}$
------------------	------------------	------------------	-----	--------------------	--------------------	------------------	------------------	------------------

C+S.W

$\frac{7.3}{33}$	$\frac{7.7}{24}$	$\frac{7.7}{21.3}$	$\frac{8.3}{18.7}$	$\frac{8.0}{4.6}$	8.0	$\frac{8.3}{10.7}$	$\frac{7.8}{10.7}$	$\frac{7.8}{16.5}$	$\frac{7.3}{17.5}$	$\frac{7.2}{33}$	✓
------------------	------------------	--------------------	--------------------	-------------------	-----	--------------------	--------------------	--------------------	--------------------	------------------	---

4 Rd

C+W

$\frac{9.0}{33}$	$\frac{8.6}{17}$	$\frac{8.8}{2.6}$	$\frac{8.8}{2.6}$	8.3	$\frac{8.3}{3.3}$	$\frac{7.9}{7.0}$	$\frac{7.2}{33}$	✓
------------------	------------------	-------------------	-------------------	-----	-------------------	-------------------	------------------	---

4 Rd

2 W

$\frac{4.7}{59.5}$	$\frac{4.9}{33}$	$\frac{4.4}{33}$	$\frac{4.2}{25}$	$\frac{3.7}{18}$	3.3	$\frac{2.5}{33}$	✓
--------------------	------------------	------------------	------------------	------------------	-----	------------------	---

4 Rd

C

$\frac{3.8}{33}$	3.0	$\frac{2.5}{33}$
------------------	-----	------------------

$\frac{4.3}{33}$	3.4	$\frac{2.8}{33}$
------------------	-----	------------------

$\frac{5.7}{33}$	5.6	$\frac{6.2}{28}$	$\frac{5.9}{33}$
------------------	-----	------------------	------------------

2 M.D.H.S Fav

$\frac{9.8}{75}$	$\frac{10.4}{50}$	$\frac{9.8}{50}$	$\frac{7.4}{39}$	7.6	$\frac{7.6}{18}$	$\frac{8.2}{34}$	$\frac{7.9}{43}$	$\frac{8.4}{48}$	$\frac{8.3}{60}$	} 4 Rd.
								$\frac{9.2}{92}$	$\frac{8.6}{74}$	

Station	+	H.I.	-	Rod. Elev
		819.76		
1077+69				11.6
T.P.	2.53	812.58	9.71	810.05
1078+00		Edge. P.O.V.		07.8
	+26	1/2 P.O.V.		07.7
B.M.			3.88	808.70
				808.68

At.

±

Rd.

MPHS. Pov.

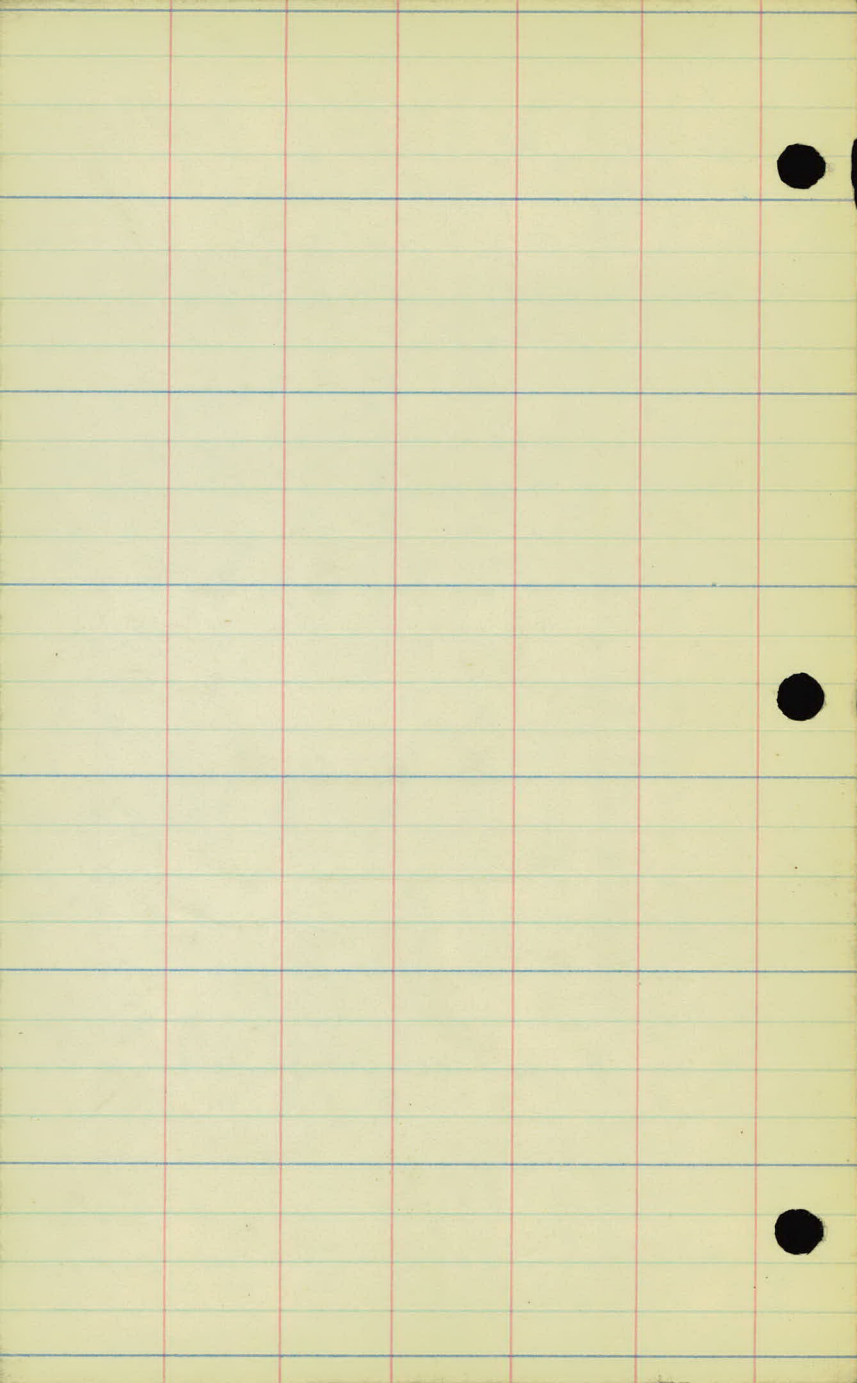
10.5	11.0	10.4	9.0	8.3	8.2	9.0	10.0	10.0	9.5	9.5
52.5	28.6	28.6	20	7.5		76	29	42.5	58	70

Top. Corb		± Pov.	± Rd	T.R.		T.R.
3.5	41	41	4.8	4.2	4.8	4.7
47	47	24	16.5	46	54.5	55
						62

Edge. Pov

4.8	4.9	5.5	4.9	5.8	5.2	5.2
23.7		24.7	24.7	38	46	50

Spike in 30" Tree 102' ht. Sta 11+62 (Proj. 25.58)

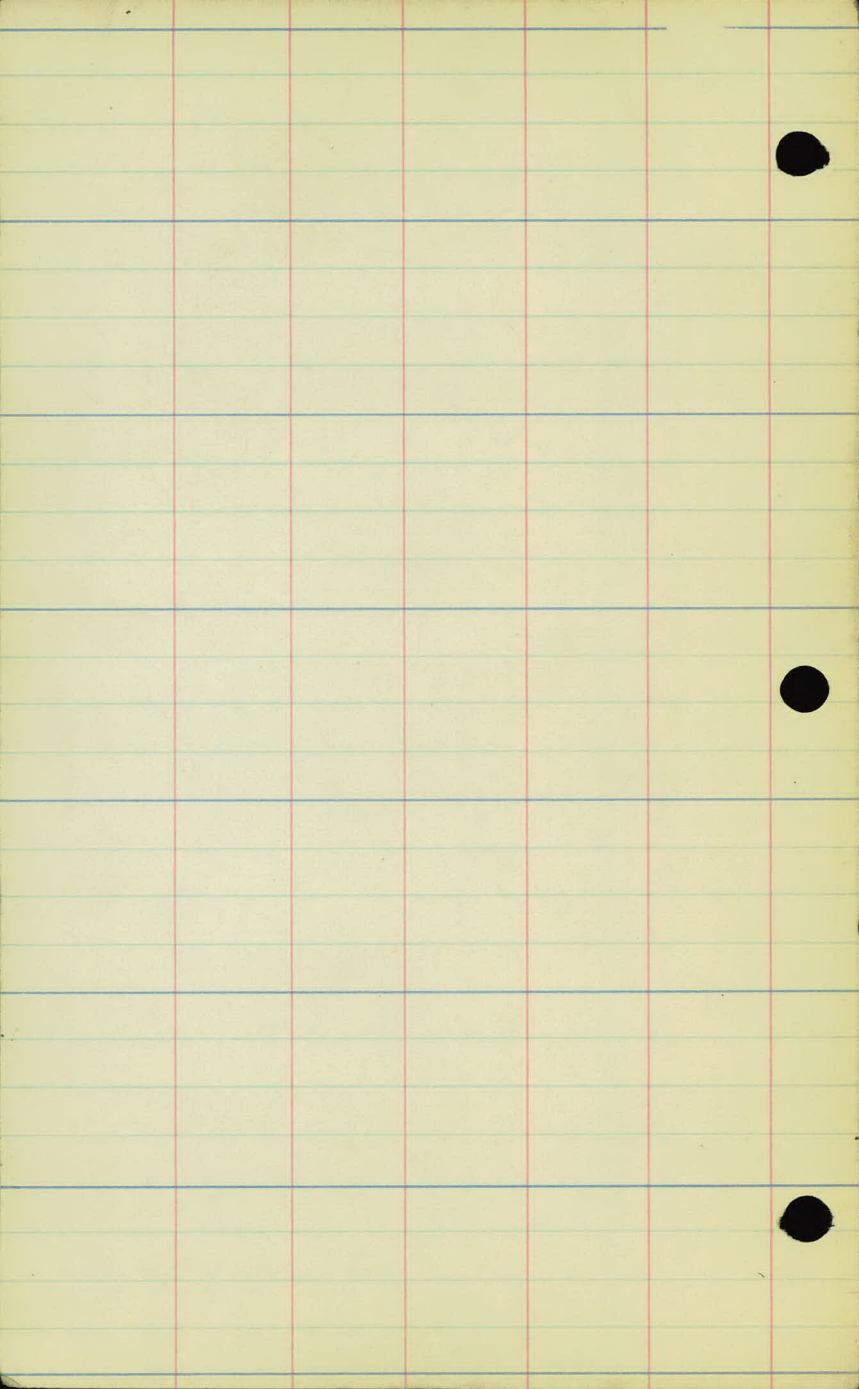


St. H. #52 Connection
At. Font Snelling

Artificial Topography
Sta 981+57 To 1099+23~~54~~

Austin }
Skoglan } Party
Fritz }
Jan Koski }
Alexander }

3/22 To 3/29 - 1926



3-29-76

Rd 10' R1

986

+ 37 Rd X 199

987

Rd 91'

986

Rd 55

985

Rd 25

984

Rd 8' Ht.

983

Rd 00

982

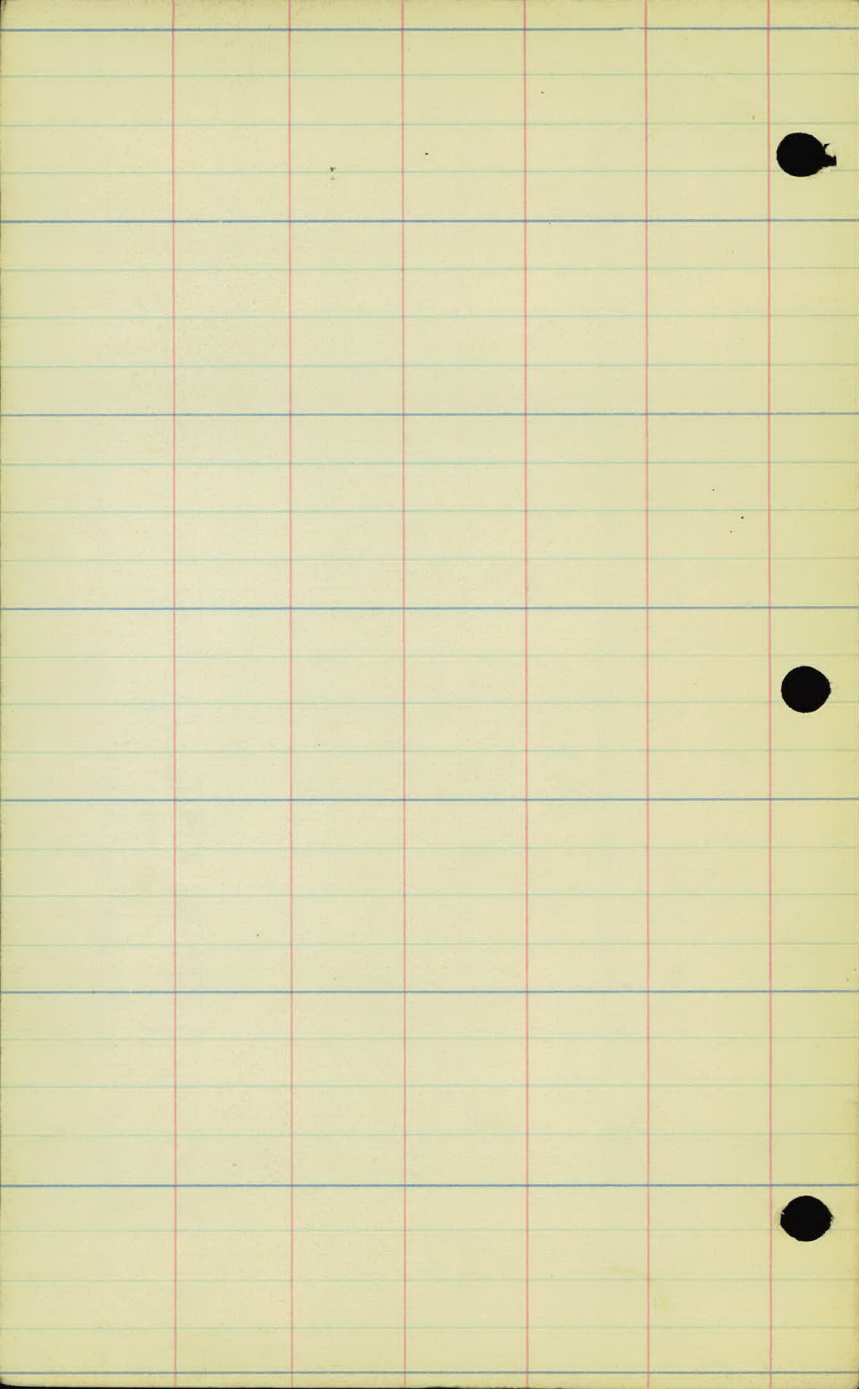
undeveloped hand

undeveloped hand

ST. H. # 52

26
55

981



Rd 9' Rt

995

+65 Rd Xing

Rd 11' Lt

994

15" X 19" V.P.

8'

+57 Ditch line

+36 Rd 20'

Rd 19'

993

Rd 3' Lt

+70 Rd Xing

Meadow hand

Meadow hand

992

Road

Rd 8'

991

+25 Rd Xing

Rd 22

990

+78 Cont. Mont 10' Rt

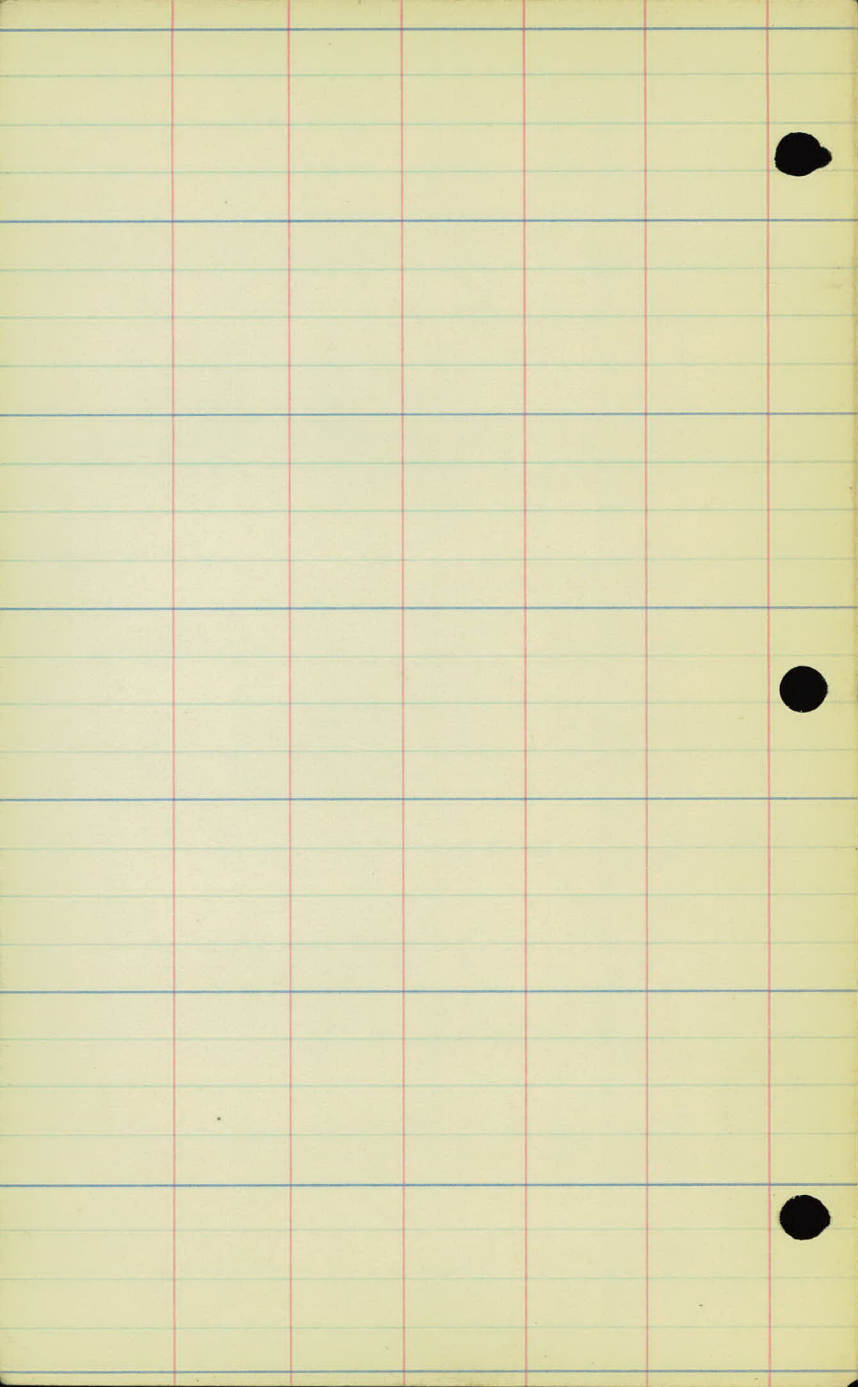
+80 Fe. Xing

Meadow hand

Rd 17'

989

988



Meadow hand

Meadow hand

Meadow hand.

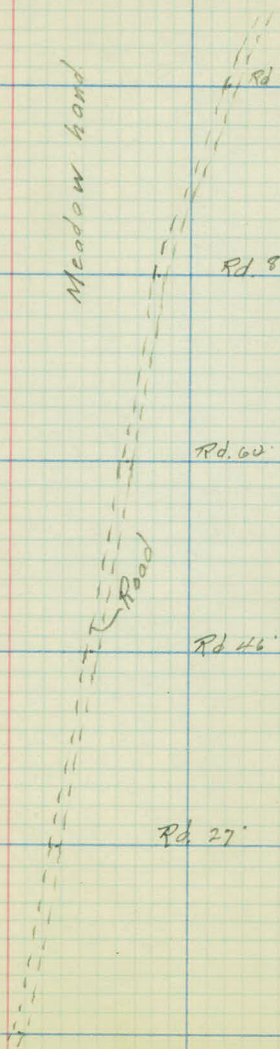
Rd 120 1000

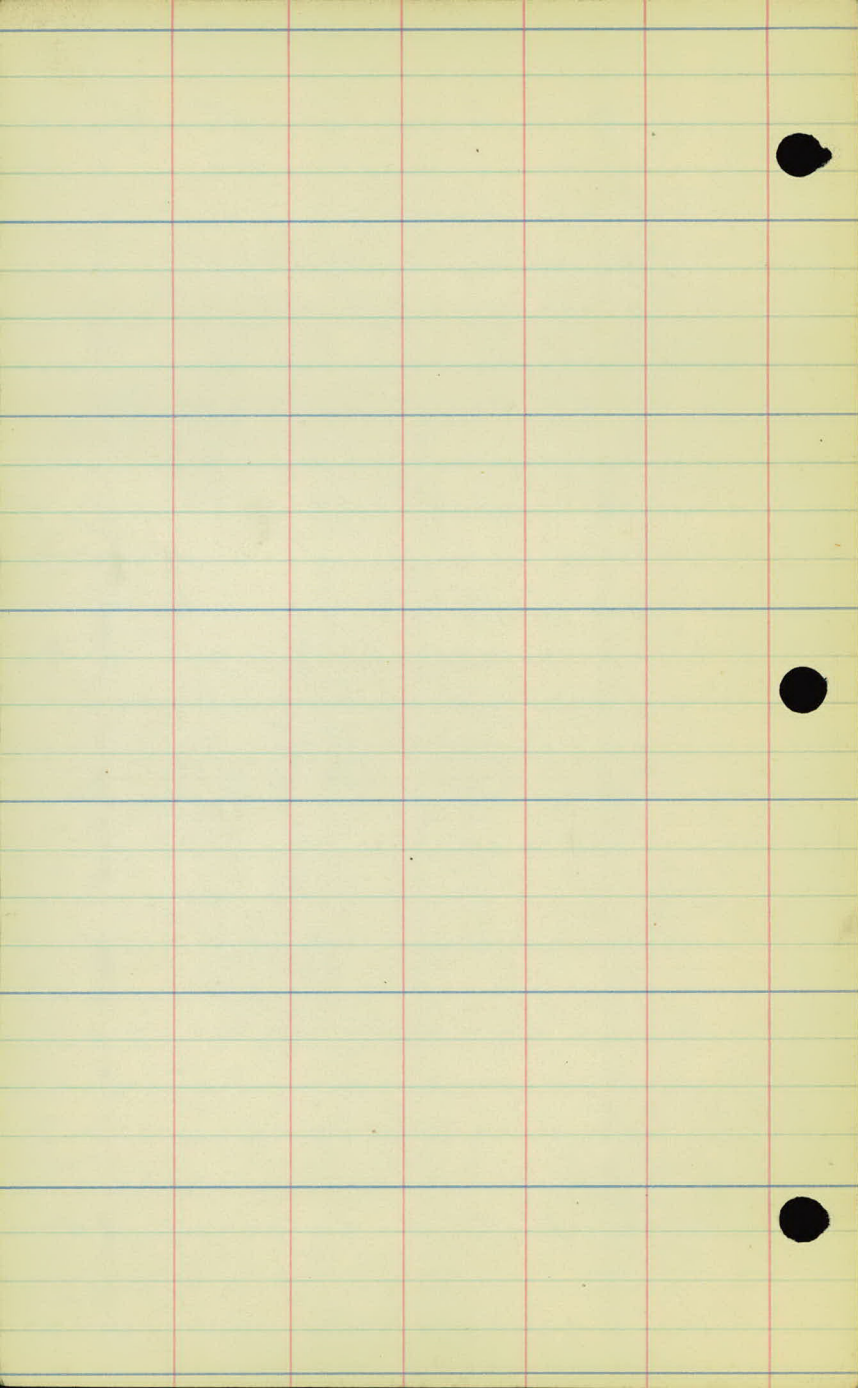
Rd. 82 999

Rd. 60 998

Rd 46 997

Rd 27 996





1009

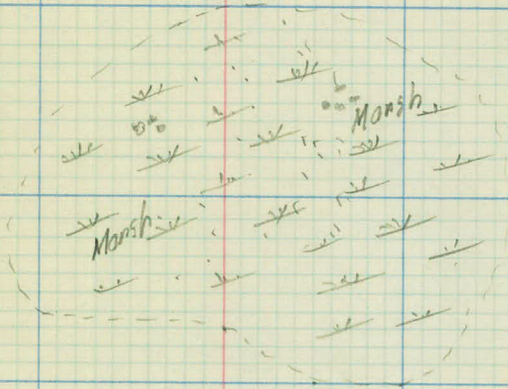
162-8" @ 15'

Meadow land

Meadow land

1008

1007



1006

1005

Meadow land

Meadow land

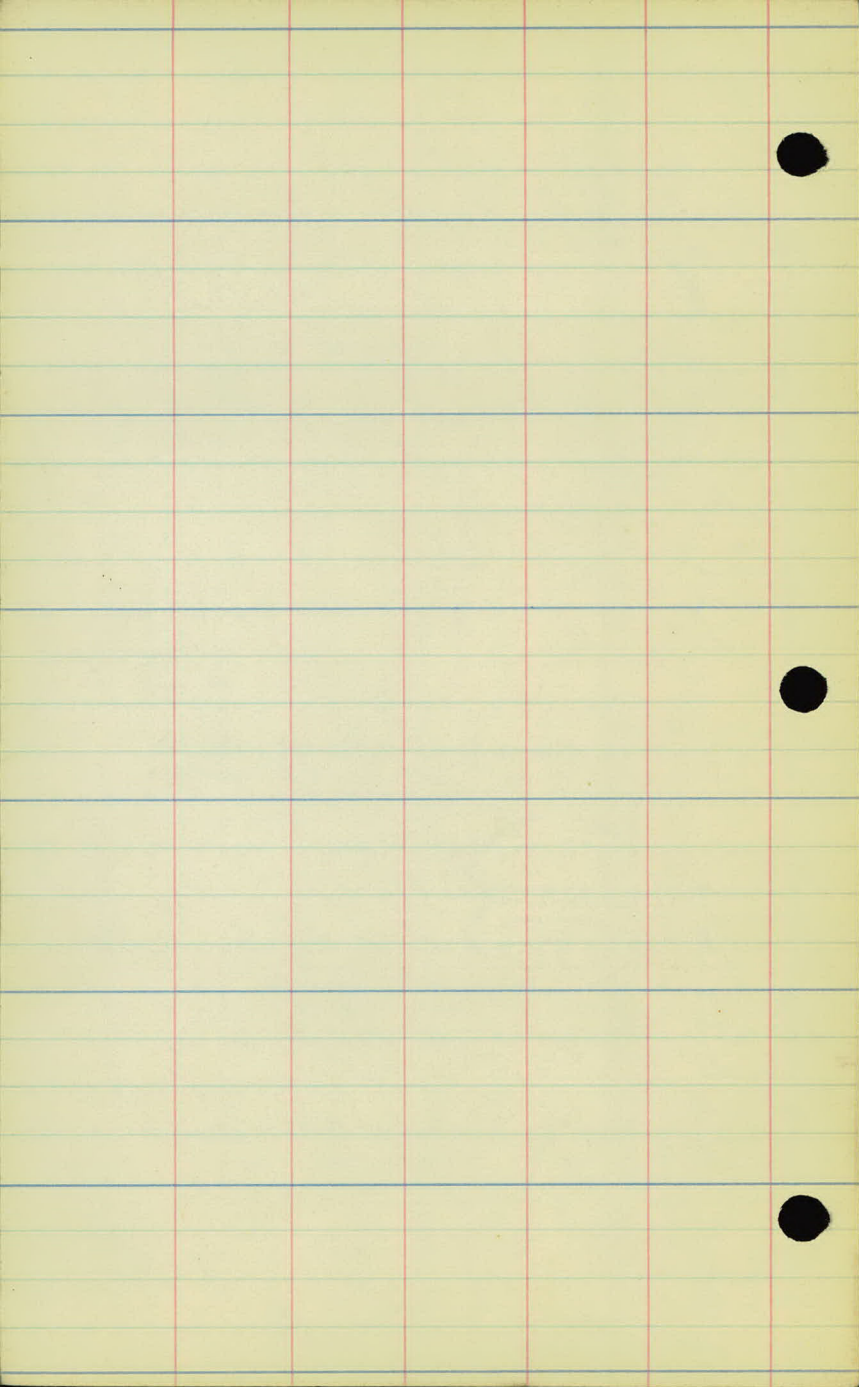
1004

1003

+71-4" @ 20'

+27-4" @ 27'

1002



1016

1015

Meadow hand

Meadow hand

1014

+63-14" @ 27'

1013

+48-(2) 8" @ 11' + 20'

1012

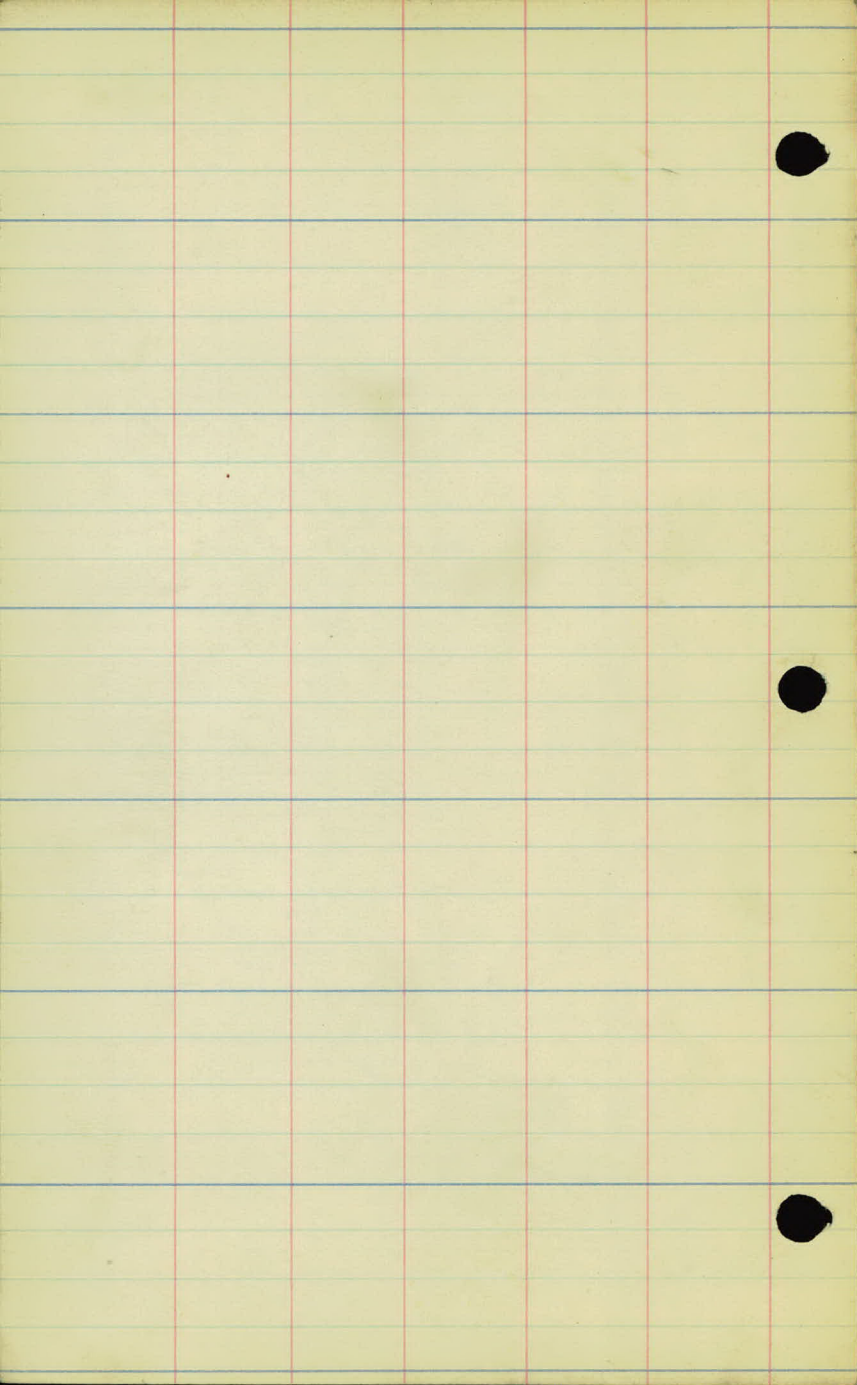
Meadow hand

Meadow hand

1011

1010

1009



+75 Rd Xing

+24 -3" @ 20'
+105 -2" @ 19'
Rd 4' ht - 24' wide

+81 -2" @ 19'
+72 Rd Xing
+58 -2" @ 15'

Rd 3.5
+91 ht. P. 23

Rd 4.5
+30 -4" @ 13'

+12 -3" @ 9' 1022
+86 -5" @ 12'
+75 -4" @ 14'
+62 -4" @ 15'
+60 Manhole 22' R1
Rd 6'

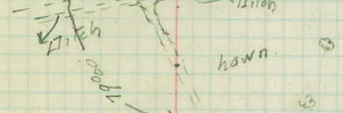
Rd. 26' - 22' wide 1021

+07 Rd - 17' wide

+88 Ditch 14' ht.

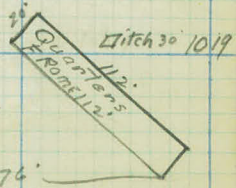
+55 Ditch Xing

+97 -8" @ 21' 1020



+07

95



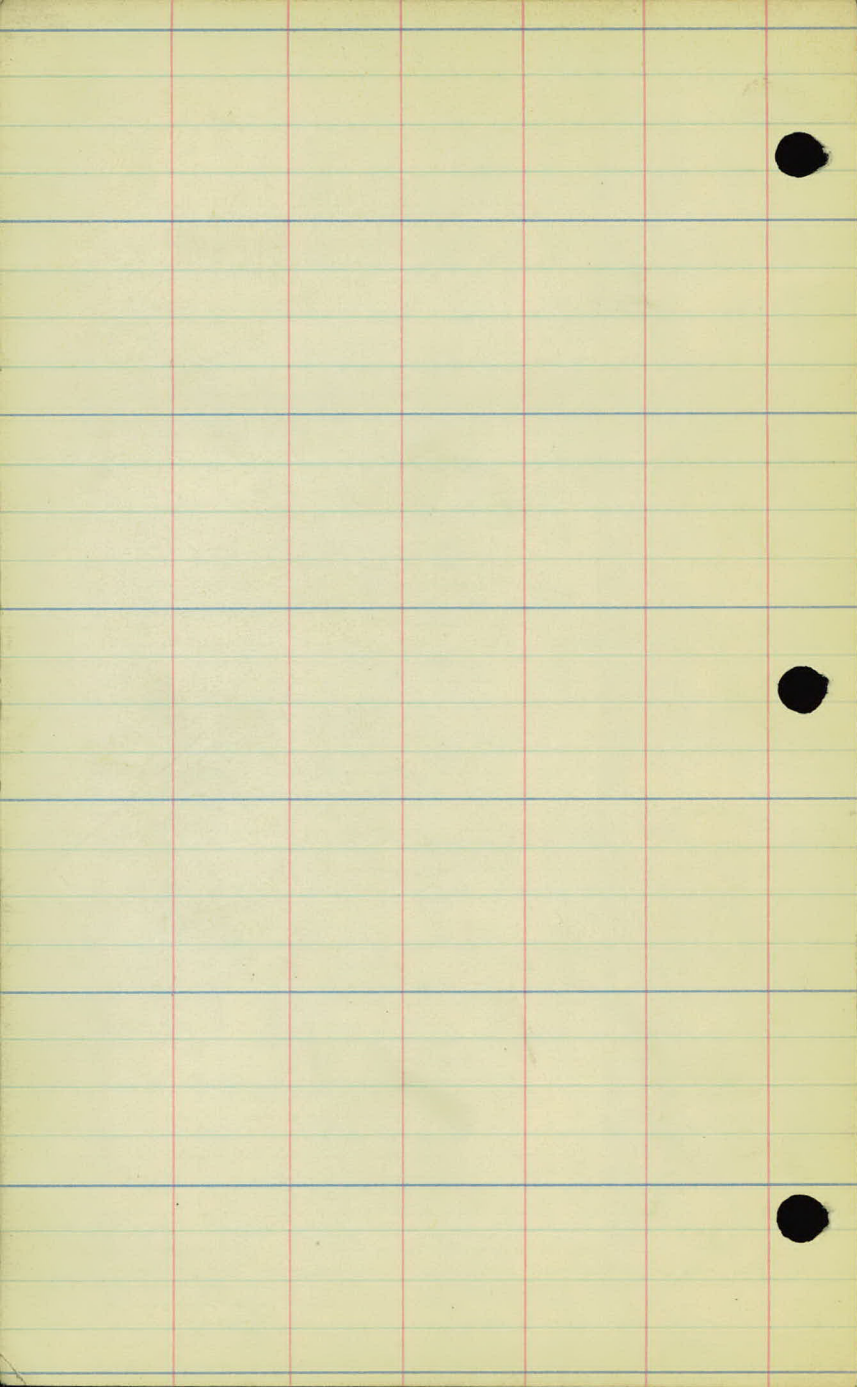
+85

176'

Ditch 55 1018

Undeveloped land

Undeveloped land

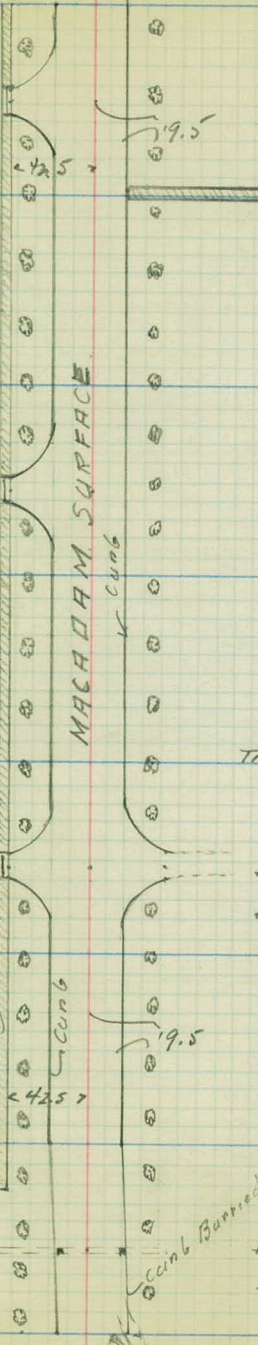


Tree 35

Tree line 35.5

+52 Drive ht 13' Wide
22' Rad

+78 ht. P. 21' R1



<42.5>

19.5

+02 Walk 6' wide 1029

+46 Drive ht 12.6 Wide
22' Rad

1028

1027

Tree line 35

MACADAM SURFACE

Tree line 36' 1026

+47.5 Drive 13' wide
22' Rad

+47.5 Drive 13' wide
22' Rad.
+26 Rd. Sign 22'

1025

6' Con. Side Walk

Curb

19.5

<42.5>

1024

+78 Beg. side Walk 4'
6' wide

Curb Barrier

+45.5 Catch Basin 18'

+45.5 Catch Basin 18' 193

+03 - 40' 32'

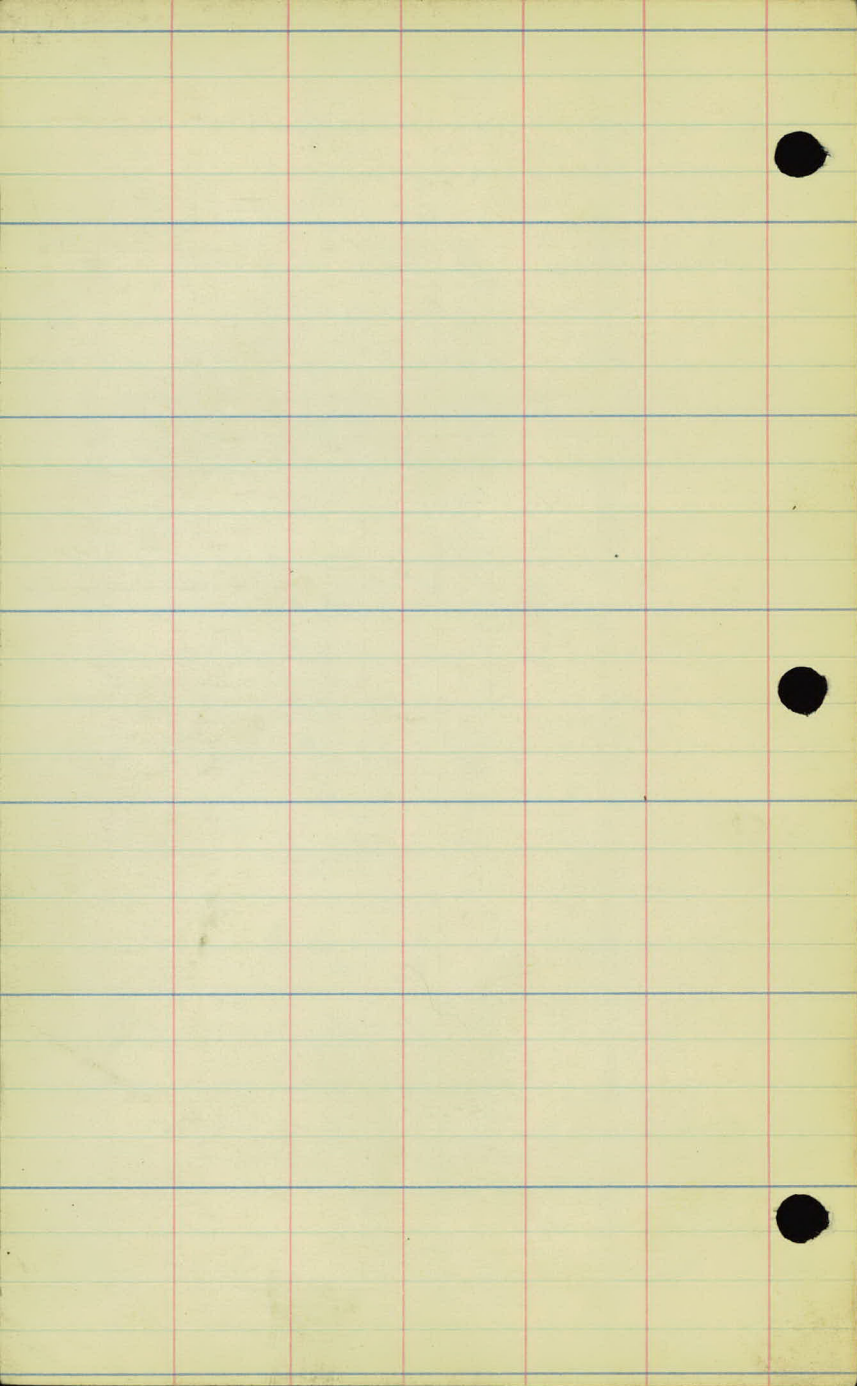
+21 37'

+03 Rd. Sign 19'

Curb 16.2 Beg

Rd 28'

1023



+53 1/2 Drive - 13' wide
22' Rad



19.5

42.5

+73 1/2 Rd
15' - 32' Wide

1036

Tree line 35

Tree line 35 1035

+67 H.P. 21' Rd

+66 1/2 Drive 13' wide
22' Rad

1032

+52.5 1/2 Drive 13' wide
22' Rad

+26 - 6' Walk

10 33

19.5

10 32

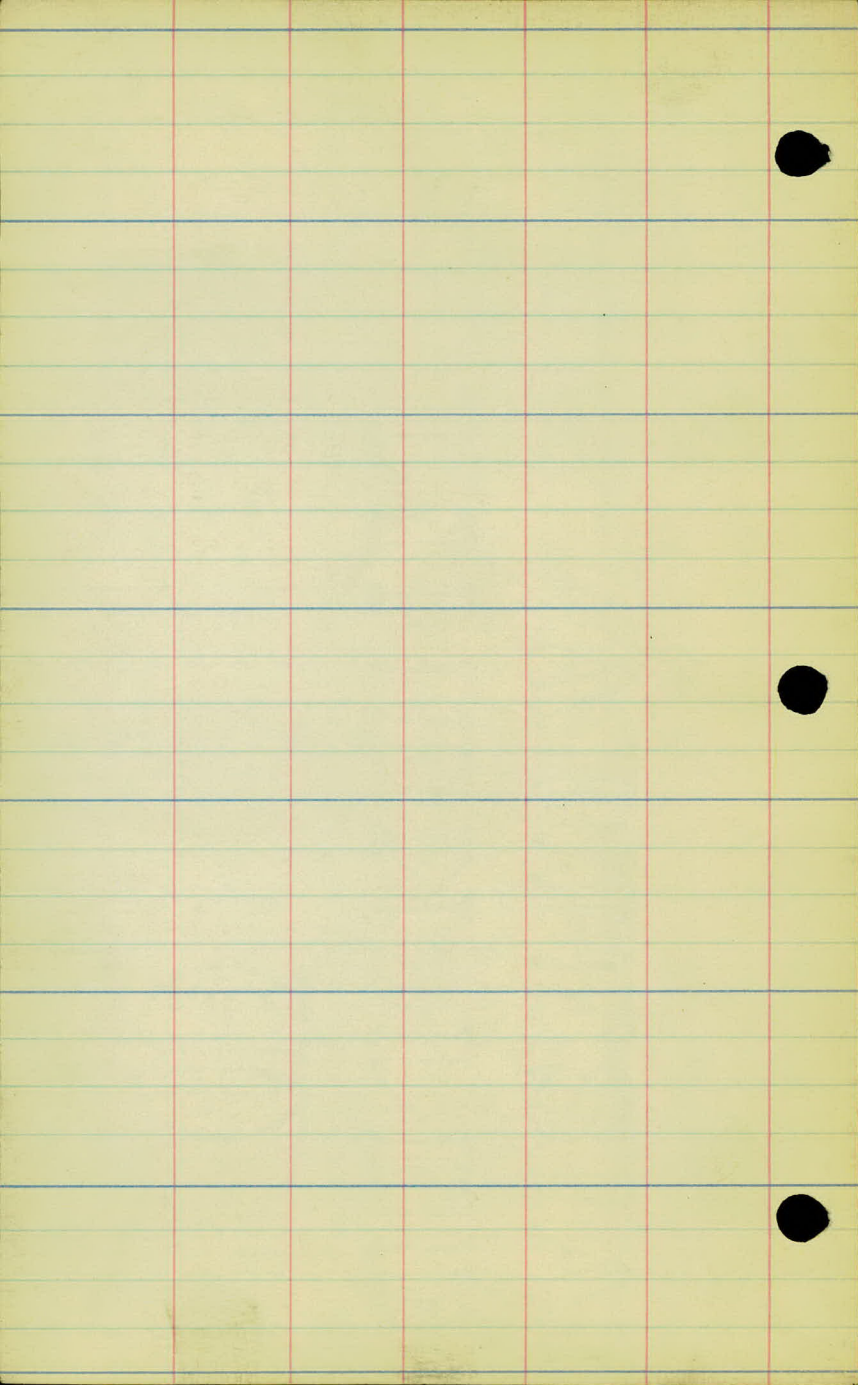
+52 1/2 Drive 13' wide
22' Rad

+13.5 1/2 Walk 4' wide

+13 1/2 Walk 4' wide

10 31

42.5



1044

+78-4' Walk

+98 & Drive
13-25' wide
+78-4' Walk

1043

+52 & Drive 13' Wide
22' Rad.

1042

+52-6' Walk

6' CON. WALK

Macadam Pfl

1041

+54 & Drive - 13' wide
22' Rad.

CONG 19.5

Tree line 35'

Tree line 35' 1040

+54 H.P. 21' R!

1039

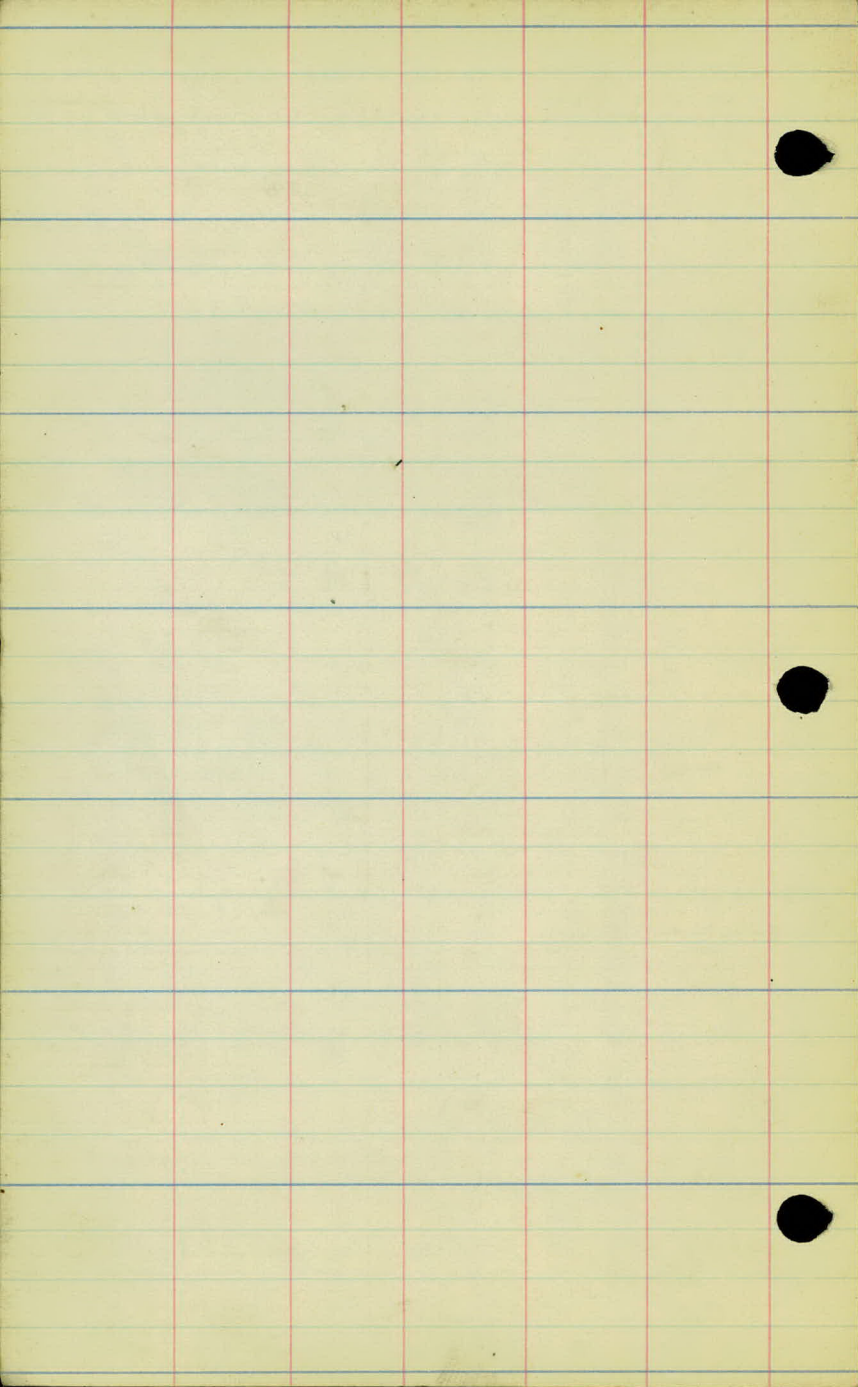
+53- & Drive 13' Wide
22' Rad.

1038

42.5

+54.5 Walk 6' Wide

1037



+56 End Walk
+57 - Rd Sign 21.5
+77-6' Walk
+53.5' Drive 12.5W
22' Rod

Tree line 35'

+53.5' Drive 13'W
22' Rod

+53' Drive 13' wide
22' Rod

Tree line 35'

+54' Drive 18'
22' Rod

+18 Catch Basin 18.5

, 400' Rd



Macadam Rd

42.5

42.5

1051

+77-6' Walk
+096' P. 21.5
+35' Beg. Walk
+35-6' Walk

Tree line 35' 1050

+17.4' walk 50' P1
1048

+09-6' Walk 1046

tree line 35' 1045

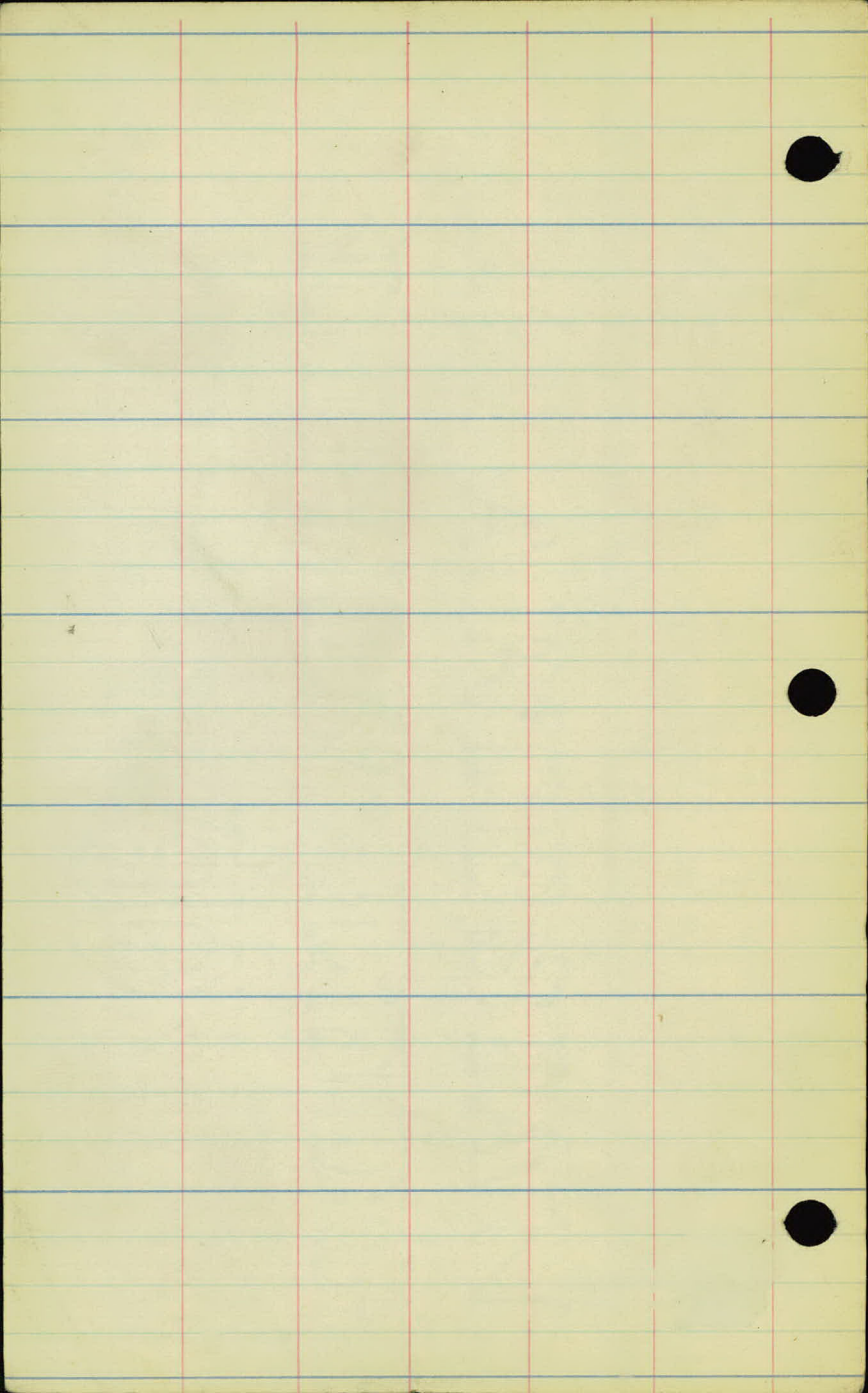
+42' P. 21'

+18 C. Basin 18.5

1044

1049

1047



5' Walk 30.5 1058

5' Con. Walk

+36-32" @ 25' (End)

+405-12" @ 30.5

5' Side Walk 38 1057

Tree line 36

+92 Rd 5.99 24
+94 Catch Basin 19'
+72 1/2 Road 44
Rod 30
+98 End Curve
+65 1/2 Rd

+45 Lt. P 22' R L

+41.5 End Curve
22' Rod

+17 1/2 Drive 16.5

Walk 41.5 1056

Tree line 34'

Macadam Rd

22' Rod
+14 1/2 Drive 42'

Tree line 36 1055

+32-4' Walk 20'

1054

+51.5 1/2 Drive
22' Rod

1053

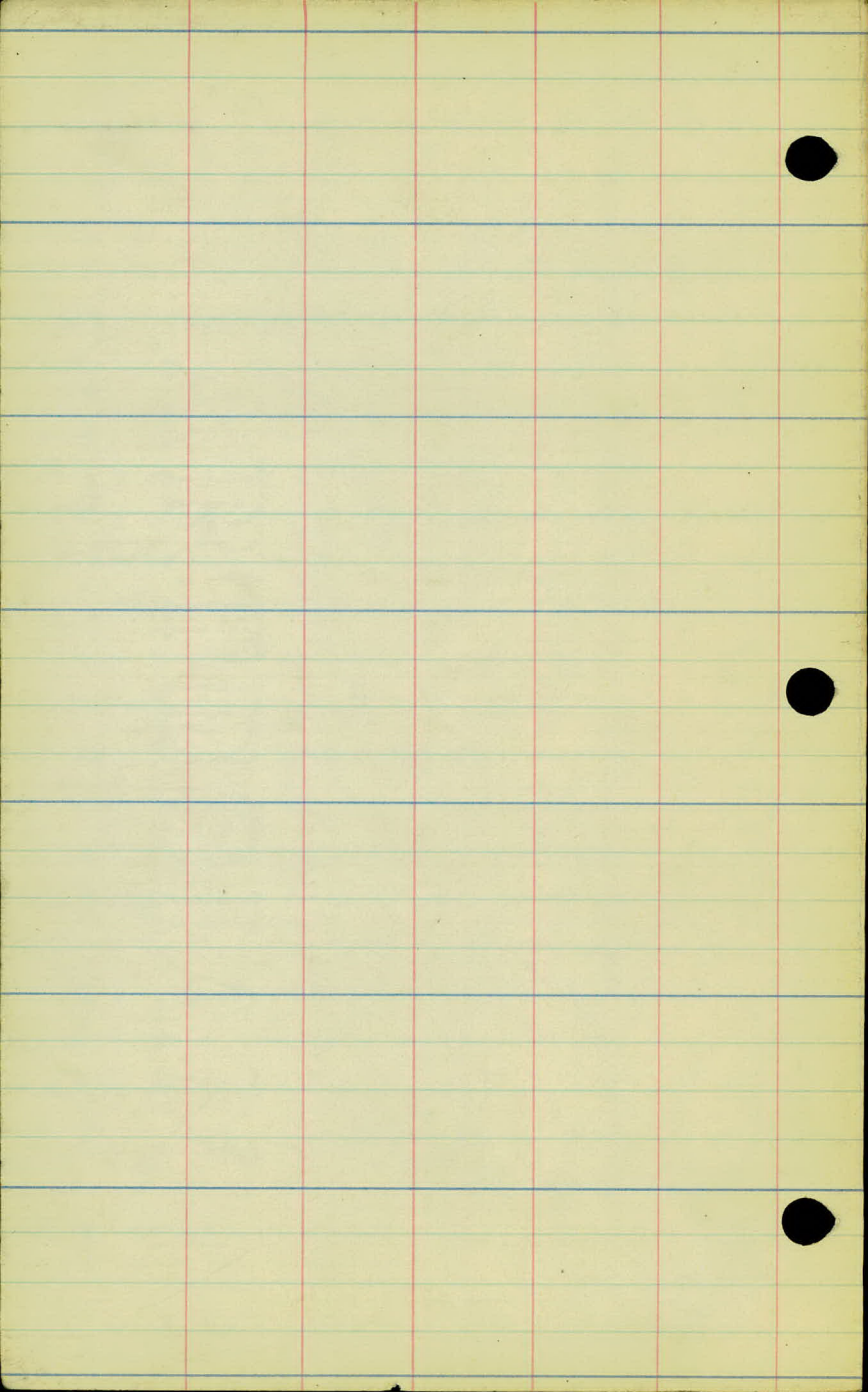
+42.5

19.5 19.5

1052

+51 P.P. 21.5

1051



Tree line 32.2

1065

1062

1063

1062

1061

1060

1059

1058

Tree line 53

Tree line 32

58.5 Catch Basin 16'

Macodoms Rd

15' Face. Curb

5' Con. Walk

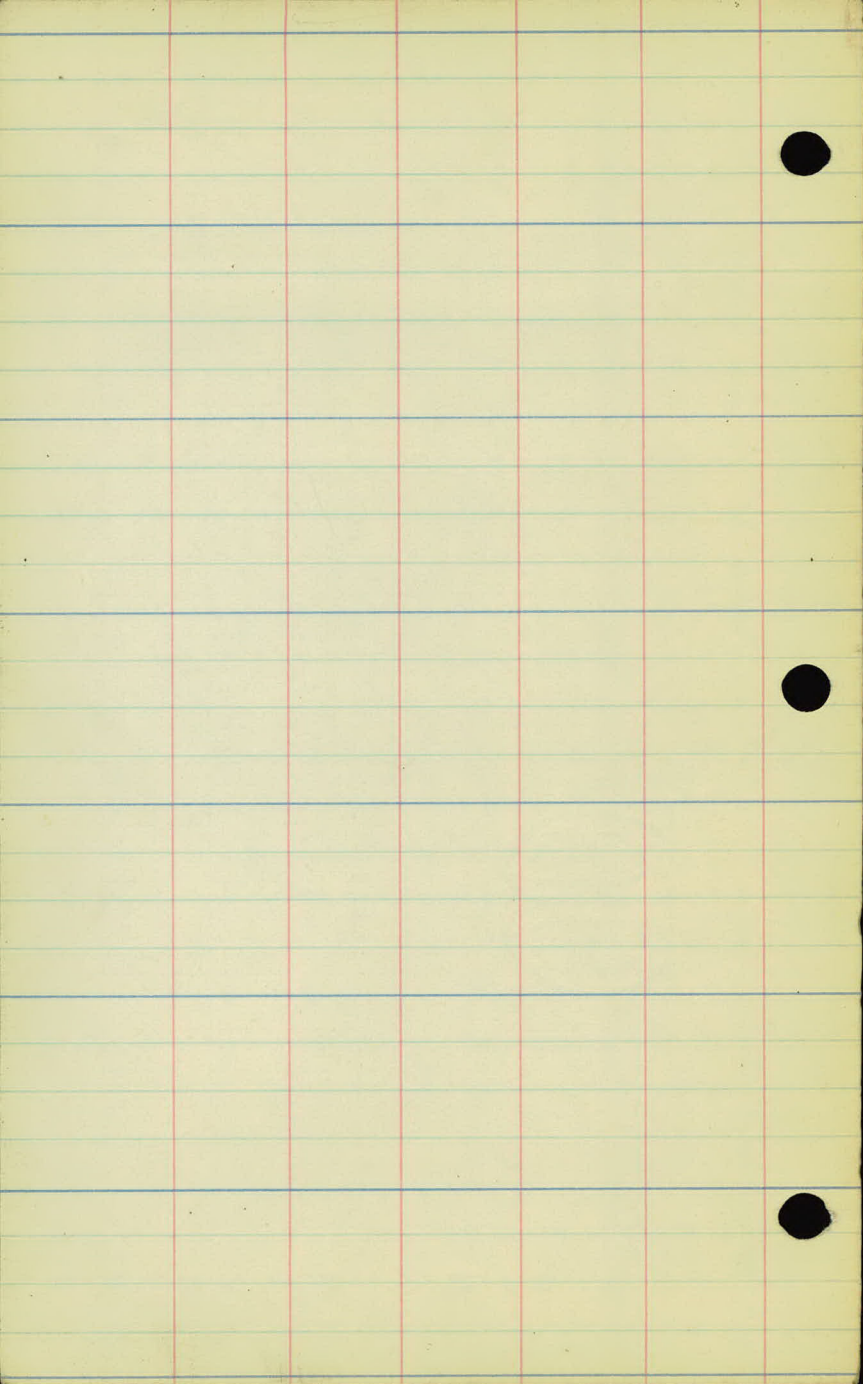
6" Curb

+66 ft. P. 21.5

+10.5 Beg. Curb 16.5
5' Walk, 17.4

5' Walk 23' ft.

+55.5 C. Basin 19'



1072

1071

1070

1069

1068

1067

1066

1065

Tree line S25

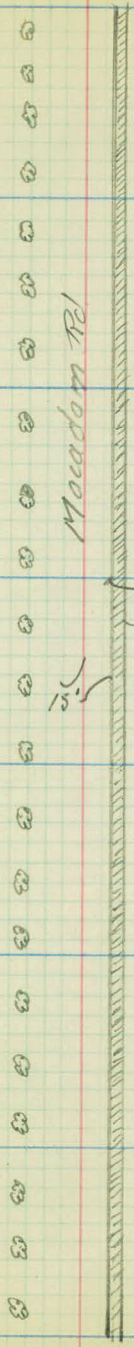
Macadam Rd

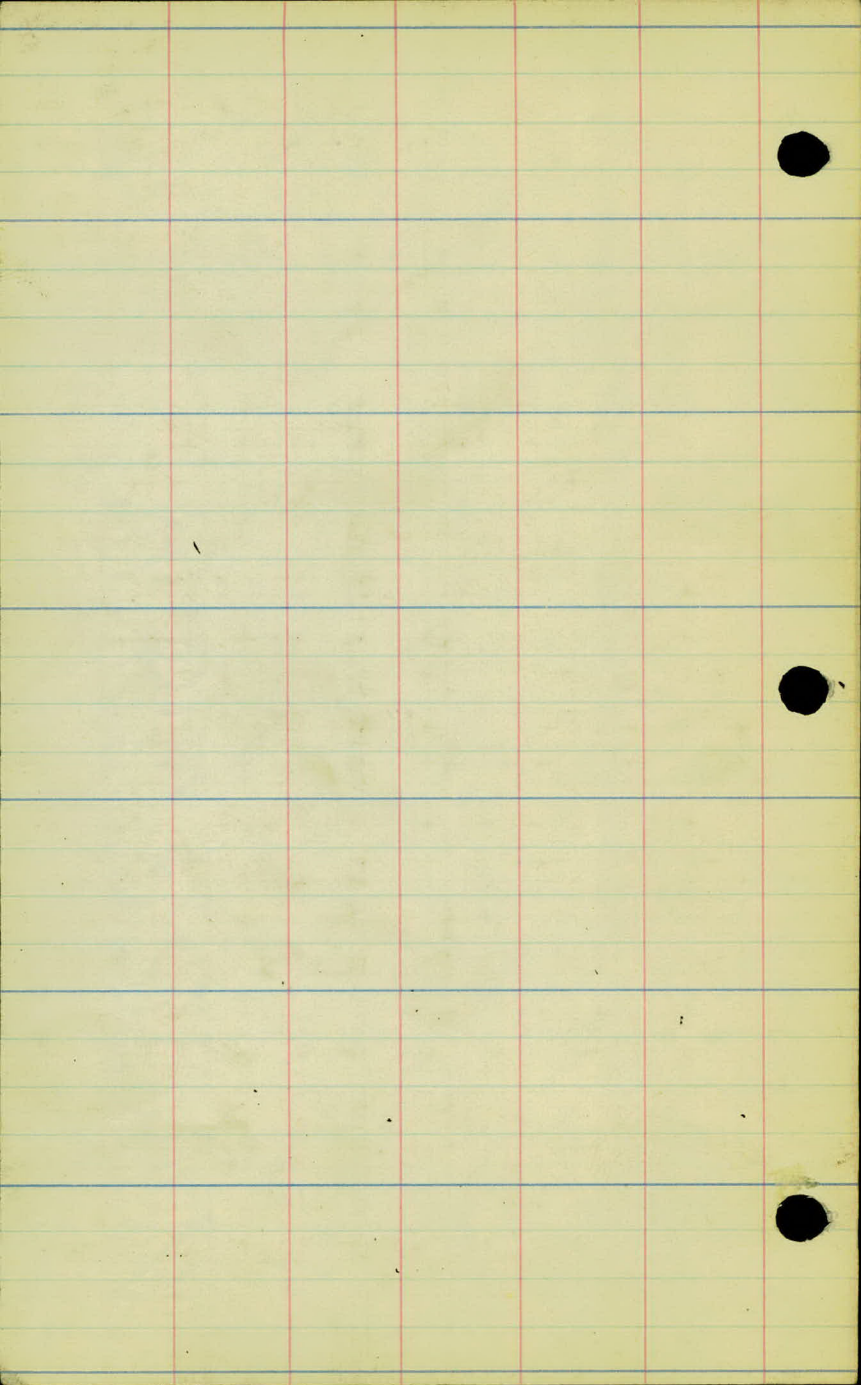
6" curb

5' con. sidewalk

5'

155 ft. R 22'





3-29-26

1079

+52.9 Edge. Pav

+26 1/2 MPHS. Pav

+96 P.P. 1' H

+60 Edge. Pav

1078

+92 End. Curb Rod 6.5

+50 MPHS. Curb hinge 78

+46-30" @ 2'

+29-24" @ 50'

Rd. 6.4

+43-12" @ 24'

+31 - Twin 12" @ 8.5

+24-30" @ 45'

1077

+75-16" @ 30'

hawn

+20

127.2

26' 24" @

+80

90'



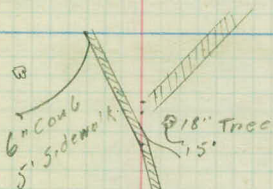
1076

+20-18" @ 21.7

Curb. hinge 30'

+18-10" @ 36.0

1075



+66 1/2 Ho. Walk 4.5

+60 Int. Edge Walk

+43 Int. Curb

Curb 10.9

1074

+50 Tree hinge 32'

+49-20" @ 32.5

+36.5 Walk. 4.5 W

+31 Hyd. 76.5

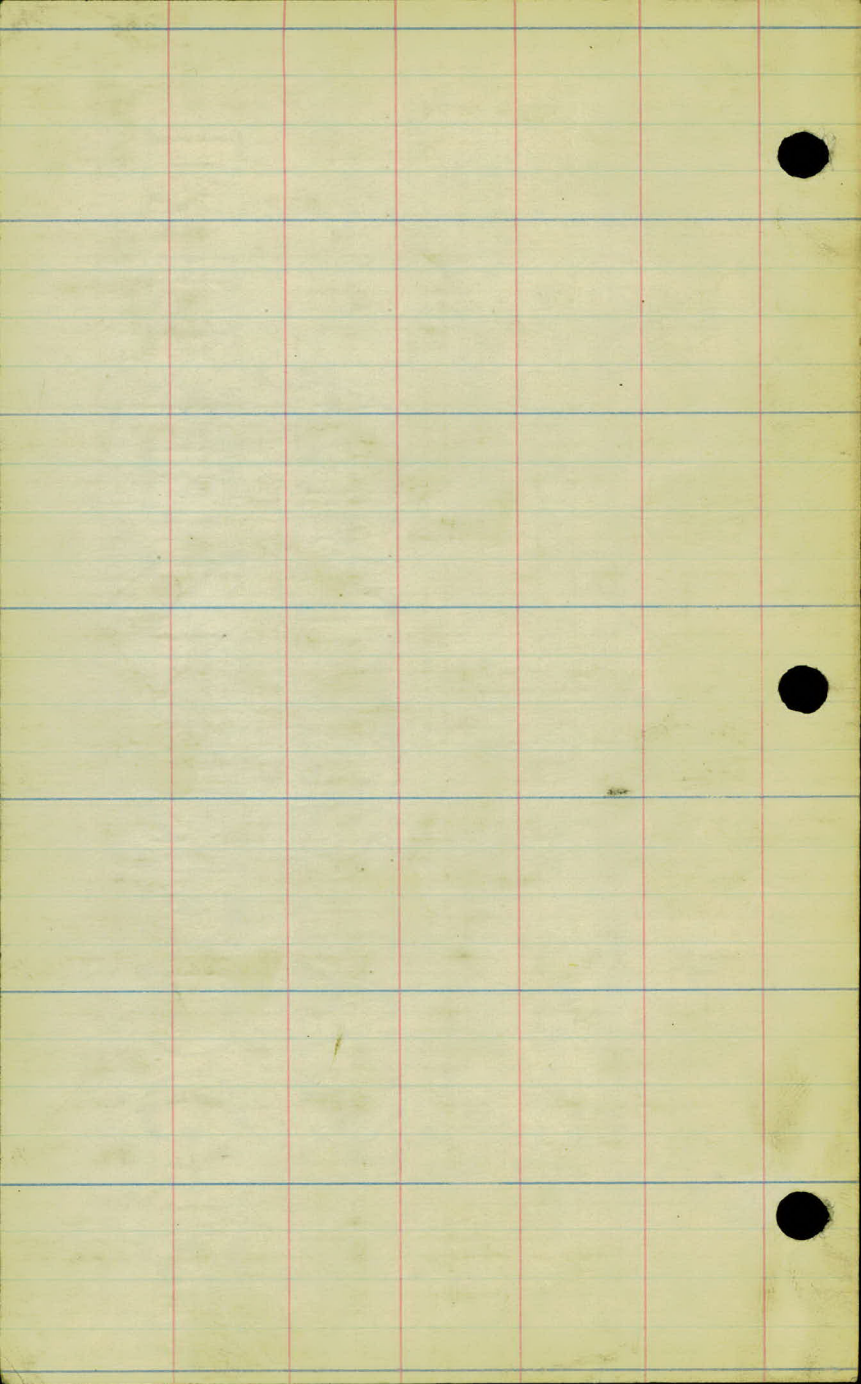
+00-16" @ 33'

1073

+85 H.P. 22

6" Curb
5' side Walk

1072



Rd 9/c # 98

Alignment on Fort
Snelling Connection from S.T.H. 52.

2

Station

Ang. ht.

Ang. Rt.

N. 33° 59' E.

1043+279 P.T.

1041+30 P.I.

20° 00'

1039+279 P.C.

1032+71.7 P.O.T.

N. 13° 59' E.

1031+46⁷⁴ P.T.

1030+54⁸ P.O.S.T.

1026+70.15 P.I. 51° 26'

1021+93⁹ P.O.S.T. = Old P.I.

1021+18⁰⁹ P.C.

N. 65° 25' E.

Sta. - Def.

1039+27.9 - 0°00'

1040+00 - 1°48'

1041+00 - 4°18'

1042+00 - 6°48'

1043+00 - 9°18'

1043+27.9 - 10°00'

Tack in Tie

Tack P. 44.80

Tack in Tie

5° Curve Rt.

 $\Delta = 20^{\circ}00'$

Rad = 1146.28

Tang = 202.12

Length = 400.00

Sta. - Def.

1021+18.07 - 0°00'

1022+00 - 2°03'

1023+00 - 4°33'

1024+00 - 7°03'

1025+00 - 9°33'

1026+00 - 12°03'

1027+00 - 14°33'

1028+00 - 17°03'

1029+00 - 19°33'

1030+00 - 22°03'

1031+00 - 24°33'

1031+46.74 - 25°43'

5° Curve Lt.

 $\Delta = 51^{\circ}26'$

Rad = 1146.28

Tang = 552.083

Length = 1028.67

Tack P. 0 - 57.65

50.48 - 57.6'

Station

Ang. ht. Ang. Rt.

N. 28° 57' E.

1062+68³⁵ P.T.

1061+25⁰ P.I.

14° 25'

1059+80⁰² P.C.

1058+00 P.O.T

N. 14° 32' E.

1051+58⁴⁵ P.T.

1049+65⁹ P.I. 19° 27'

1047+69⁴⁵ P.C.

N. 33° 59' E.

Sta - Def

1059+80⁰⁰ - 0°00'

1060+00 - 0°30'

+ 25 = 1°12'

+ 50 = 1°45'

+ 75 = 2°22½'

1061+00 - 3°00'

+ 50 = 4°15'

1062+00 - 5°30'

+ 50 = 6°45'

1062+68³⁵ - 7°12½'

Twin 04H.

40 25

62 05
12 04H

5° Curve. Rt.

 $\Delta = 14°25'$

Rad = 1146.28

Tang = 144.98

Length = 288.33

19" Box Eff. H.

73 58

63 45
24 04H

Sta - Def

1047+69⁴⁵ - 0°00'

1048+00 - 0°46'

+ 50 = 2°01'

1049+00 - 3°16'

+ 50 = 4°31'

1050+00 - 5°46'

+ 50 = 7°01'

1051+00 - 8°16'

+ 38.45 = 9°43½'

Twin 04H.

34 58

12 25
8 04H

5° Curve. Lt.

 $\Delta = 19°27'$

Rad = 1146.28

Tang = 196.45

Length = 389.00

Station

Ang. ht. Ang. Rt.

N. 28° 47' E.

1075+08³² P.T. = 01+75²⁷ On Pike Island Survey

1073+79²⁵ P.I. = 03+03¹⁰ Beg. of Map. Pike Island Survey.
10° 18'

1072+50⁸² P.C.

1070+80⁵⁵ P.O.T

N. 18° 29' E.

1070+30⁴⁵ P.T.

1069+00 P.I. 10° 28'

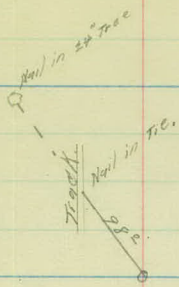
1067+68⁷⁸ P.C.

N. 28° 57' E.

1066+12⁰ P.O.T

Sta. - Def

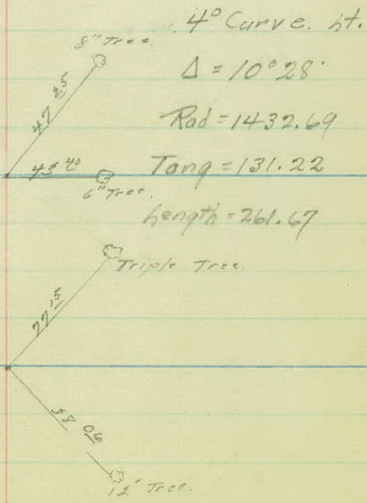
- 1072+50⁸² - 0°00'
- 1073+00 - 0°59'
- +50 - 1°59'
- 1074+00 - 2°59'
- +50 - 3°59'
- 1075+00 - 4°59'
- +08³² - 5°09'



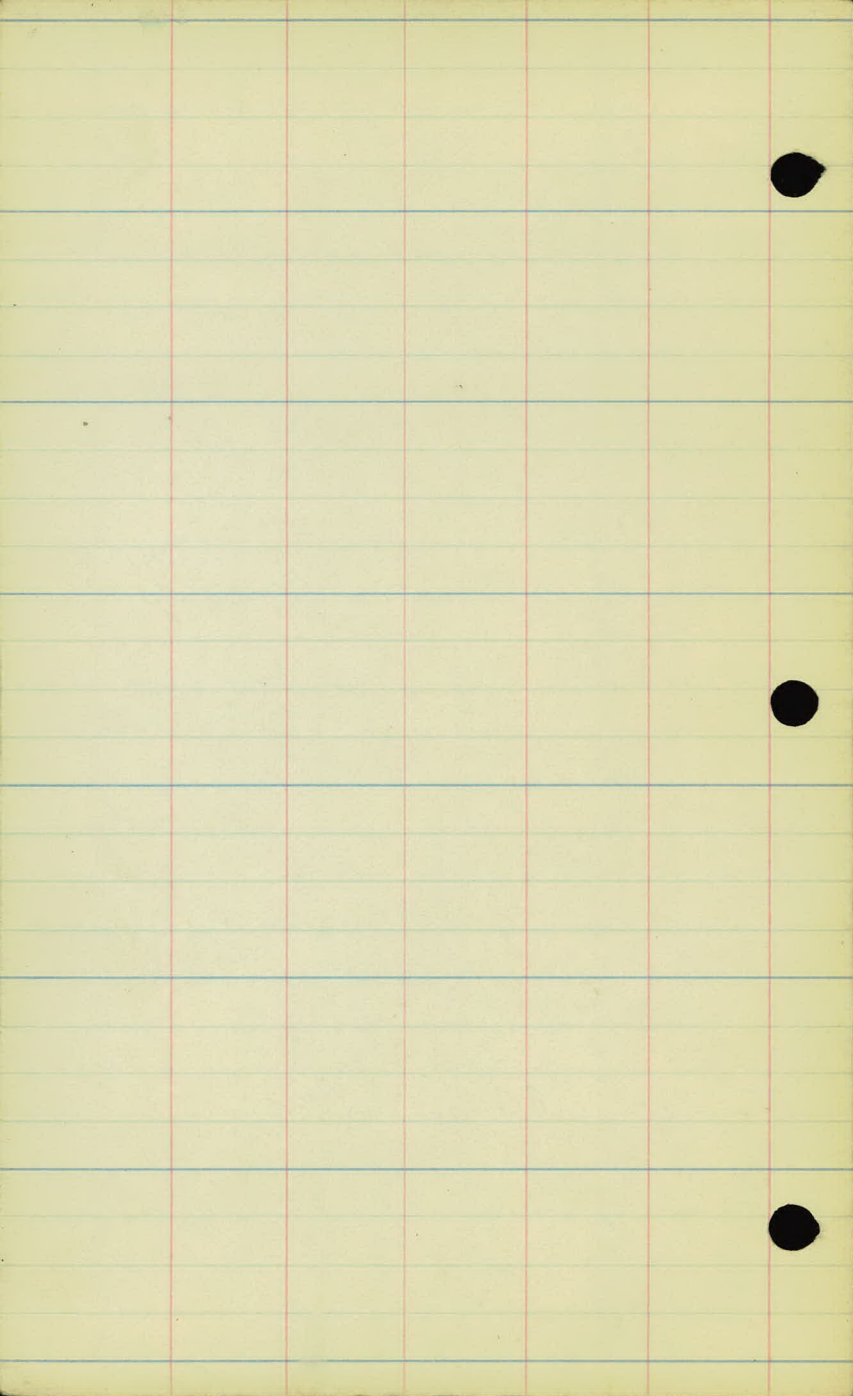
4° Curve. Rt.
 $\Delta = 10^{\circ}18'$
 Rad = 1432.69
 Tang = 129.13
 Length = 257.50

Sta. - Def

- 1067+68¹⁸ - 0°00'
- 1068+00 - 0°37½'
- +50 - 1°37½'
- 1069+00 - 2°37½'
- +50 - 3°37½'
- 1070+00 - 4°37½'
- +30⁴⁵ - 5°14'



4° Curve. Rt.
 $\Delta = 10^{\circ}28'$
 Rad = 1432.69
 Tang = 131.22
 Length = 261.67



FORT SHELING
ADDITIONAL TOPOG. ON STATE LINE
S.T.H. #52

Station

Ang. Mt. ^h Ang. Rd.

1068+05¹ P.T.

1066+63³ P.I. 62°46'

1064+53² P.C. = 1065+83²

Sta. - Elev

1064+83.2 - 0°00'

1065+00 - 1°38'

+50 - 6°30³/₄'1066+00 - 11°23¹/₄'+50 - 16°15³/₄'1067+00 - 21°08¹/₄'+50 - 26°00³/₄'1068+00 - 30°53¹/₄'

+05.1 - 31°23'

19°30' Curve Rt.

 $\Delta = 62°46'$

Rad. = 295.3

Tang = 180.1

Length = 321.9

Station

Flag. ht. ⁴ Flag. Rt.

1091+42.3 = 0+00 Proj 25-58

1086+24.5 P.T.

1083+48.2 P.I. 16°42'

1080+67.8 P.C.

1078+96.9 P.T.

1076+57.0 P.I. 4°48'

1074+16.9 P.C. = 1074+17.4

Sta. Def

1080+67.8 - 0°00'

1081+00 - 0°29'

1082+00 - 1°59'

1083+00 - 3°29'

1084+00 - 4°59'

1085+00 - 6°29'

1086+00 - 7°59'

+245 - 8°21'

3° Curve ht.

 $\Delta = 16°42'$

Rad = 1910.08

Tang = 280.4

Length = 556.7

1074+16.9 - 0°00'

1075+00 - 0°25'

1076+00 - 0°55'

1077+00 - 1°25'

1078+00 - 1°55'

1078+96.9 - 2°24'

1° Curve ht.

 $\Delta = 4°48'$

Rad = 5729.7

Tang = 240.1

Length = 480.0

Additional Topog. on
State Line - S.T.H. #52

Ft. Snelling
#52

To St. Paul
Sem. Tong

10' Chrs

62' 0" 6
5' 6" 6
6' 6" 6
6' 6" 6
6' 6" 6

110° 30'

50'

10' Chrs

29.1'

3.75'

23'

34'

Paved Xing

12'

50'

30'

29.1'

32'

10' Rod

10' Rod

13' Rod

12.6 x 25.3

67.2

470

283

28.0

18.0

170

16.4

106500 Sem. Tong

P.I. for Pavement

1066

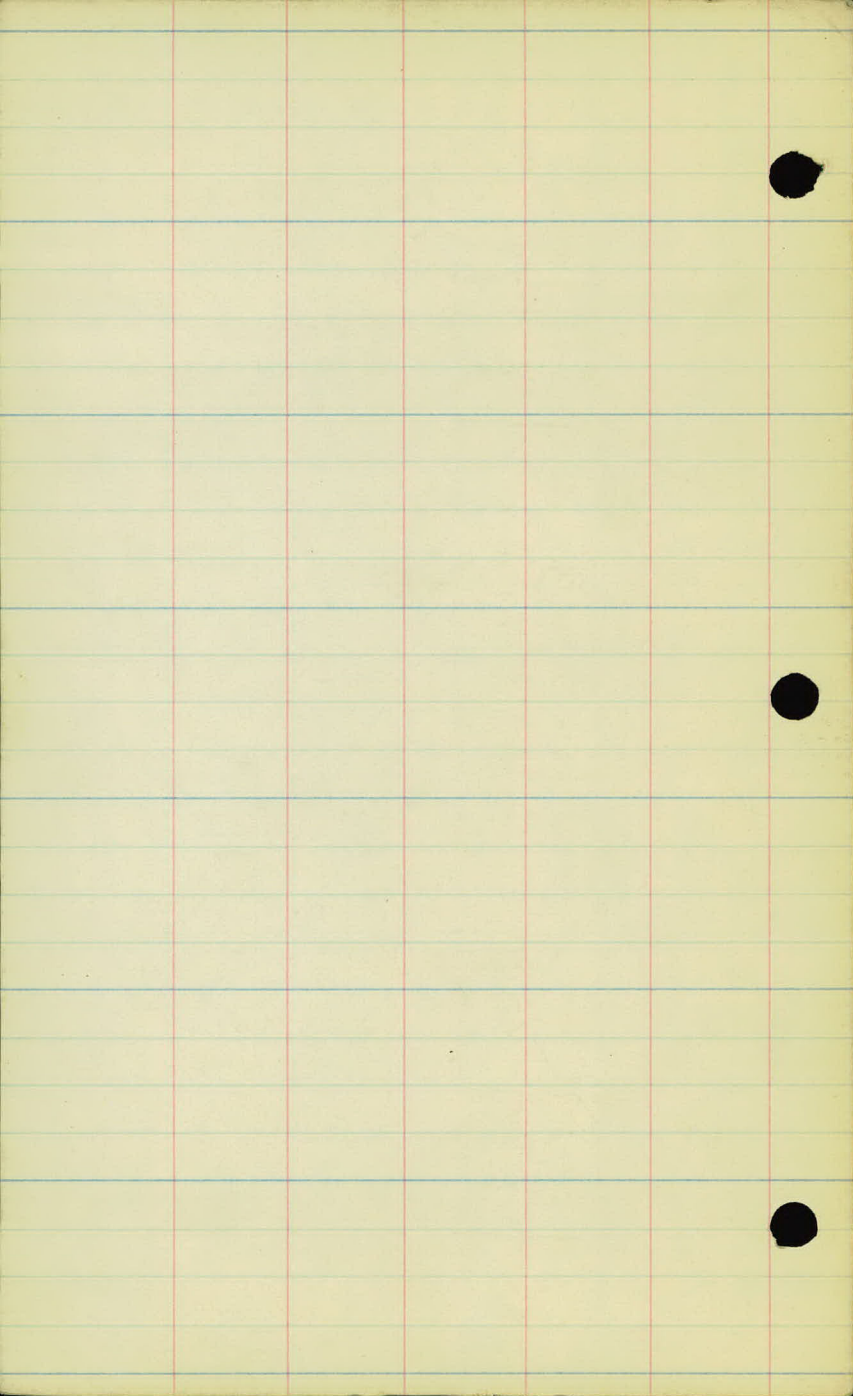
Tong

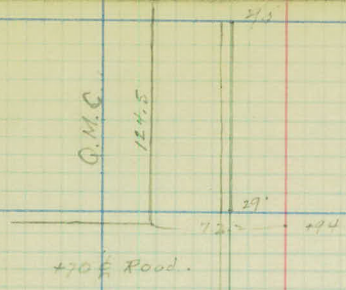
1066

1066

1066

1066





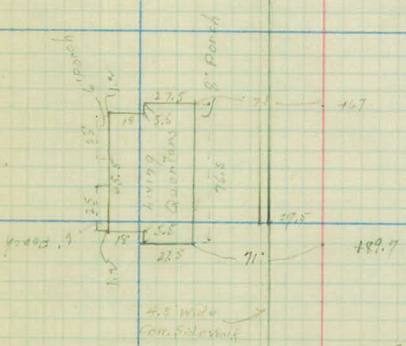
1004

28.0

1005

1000

1041



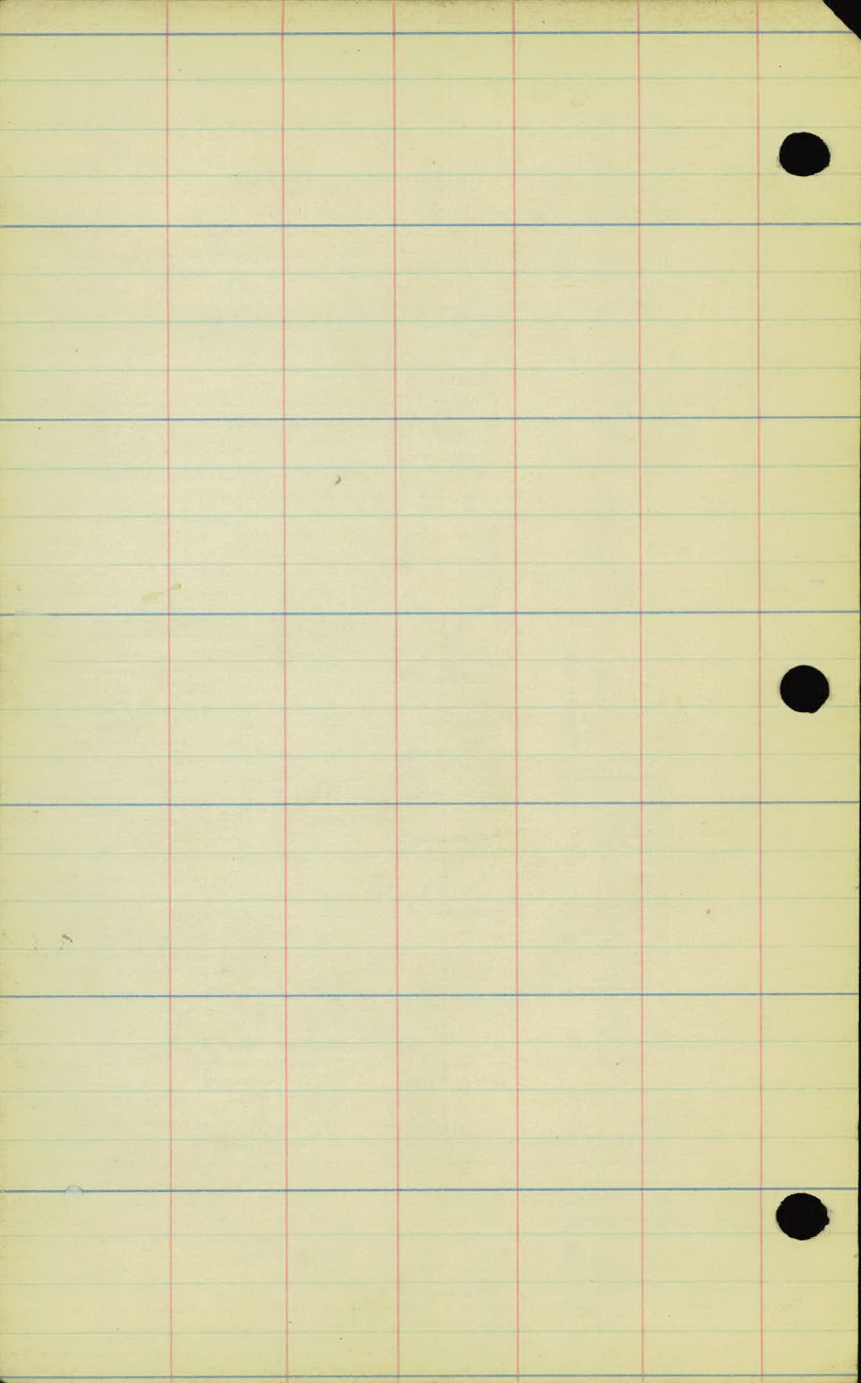
1040

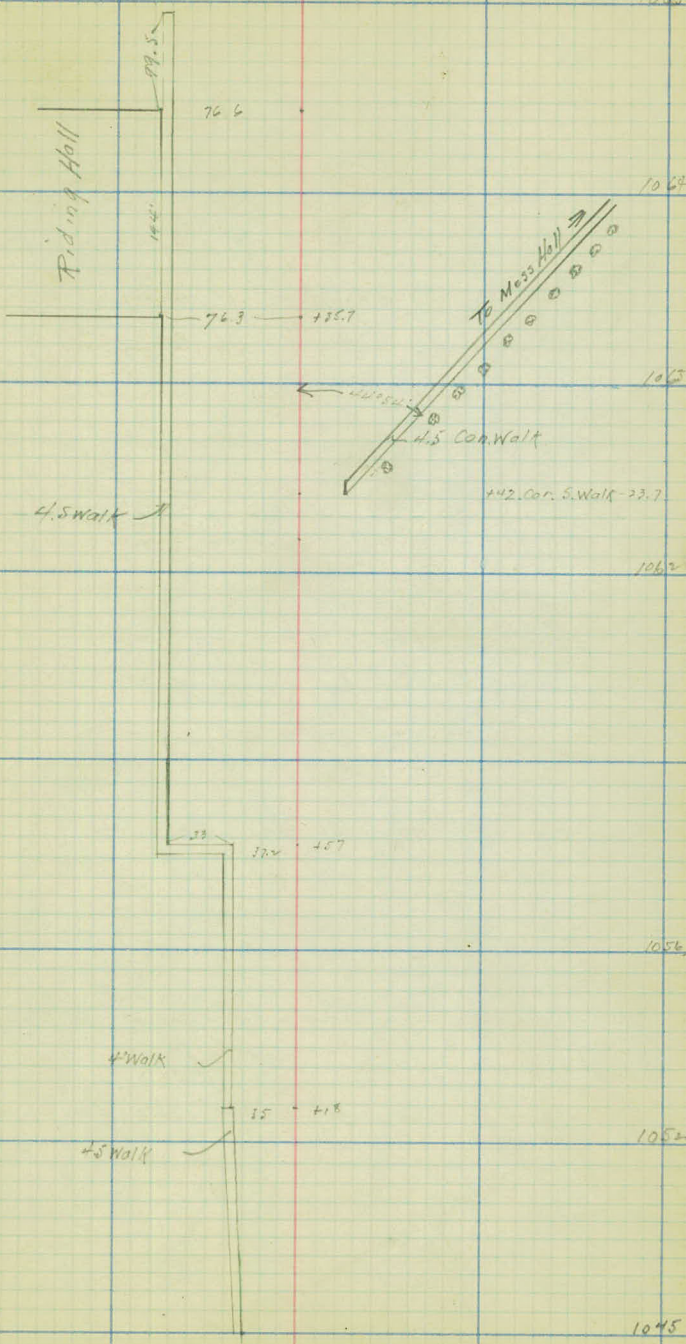
+32 Hyd. 27'
 +19 Inside Con Wall 30'



+36 Edge Brick 7 1/2\"/>
 +21 Edge Brick 7 1/2\"/>
 10 3/4

10 3/4





Riding Hall

To Mess Hall

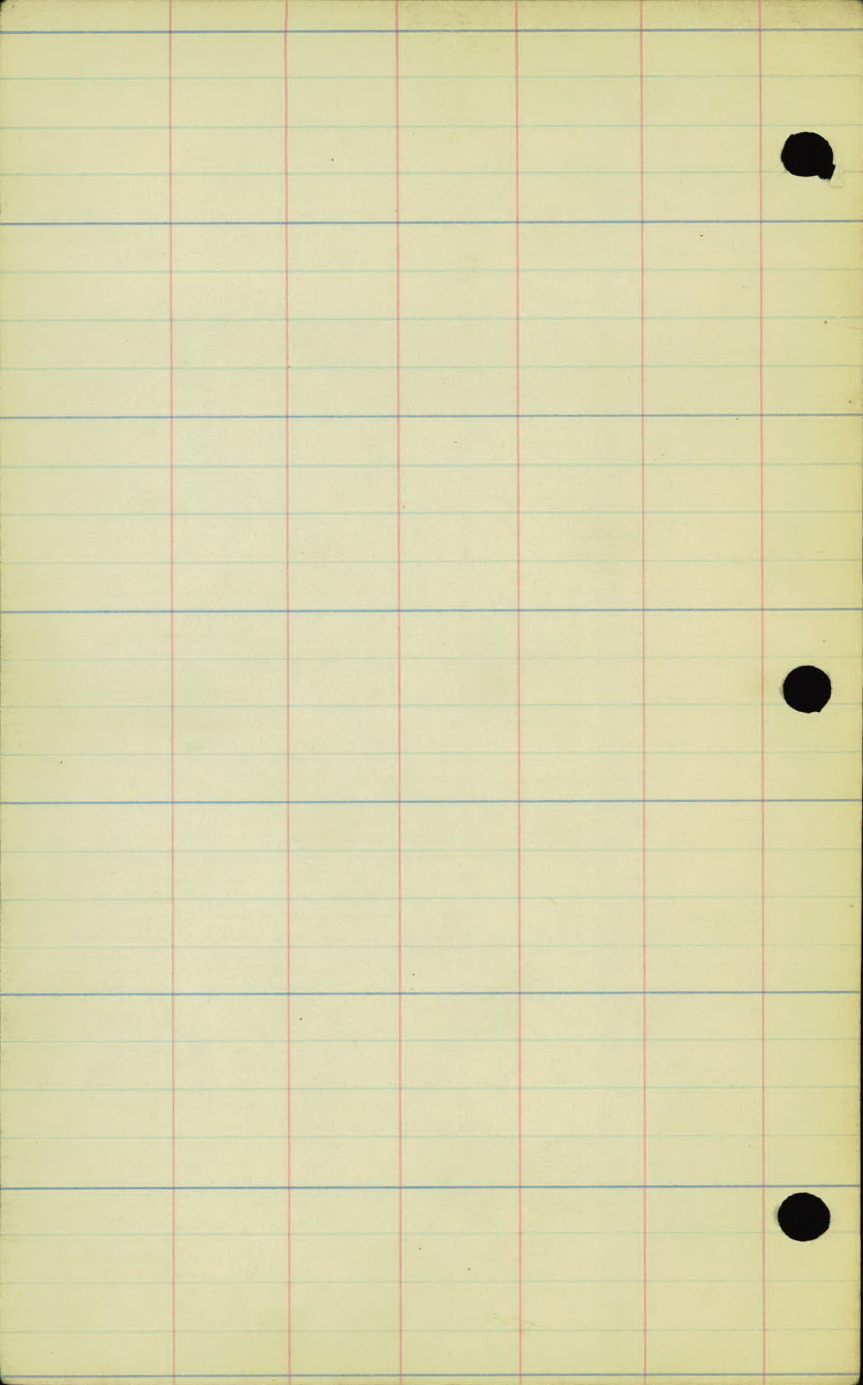
4.5 Walk

4.5 Car. Walk

4.8 Car. S. Walk 73.7

4.8 Walk

4.5 Walk



Brick Stable Shack.

Tn. 2.65-12.65 Corb. 46 Pav. 35.5 1079
+94. P.P. 25.5

+54 Trol. P. 18.6

+58 Trol. P. 25.5
+44. 30" @ 26

Brick

5' x 8' 1/2



(Tn. 2.65-12.65) { Pav. 35.7
Curb 45.8 1069

+76 Hqd. 22.5

+94-30" @ 25.5

+40 Trol. P. 18.5

+68-18" @ 26

+44-20" @ 26
+37 Trol. P. 25.5
+19-14" @ 27.5

Tn. 2.65 Tn. 12.65 Pav. 45.3 1068

+95-24" @ 29.5

+68 Fa. Cor. 22
+60-12" x 73" C.M.P

+43 Trol. P. 27

+27 Trol. P. 19

+07 P.P. 103.5 1067
Rl. 19

+57 Trol. P. 10

+30 Rd. 100
+29-20" @ 168
+17-20" @ 74

Rd. 88'-20" wide 1066
+99-16" @ 27

+77-24" @ 34
+68-20" @ 107
+56-P.P. 25
+43-12" @ 40

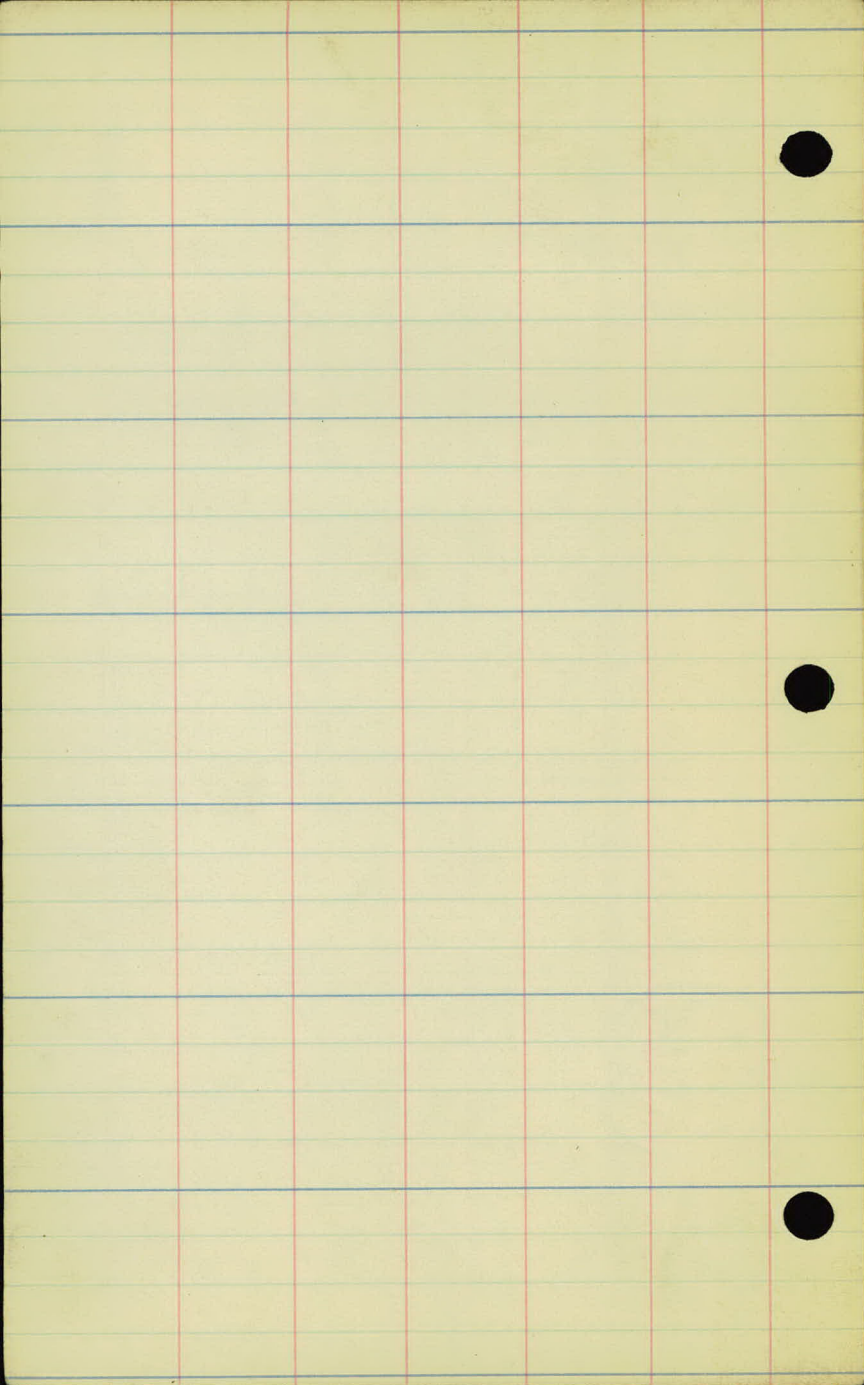
+26 G. P. 17

+16-24" @ 43
+02-16" @ 75 1065

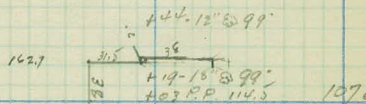
+61 P.P. 32

+39-8" @ 46

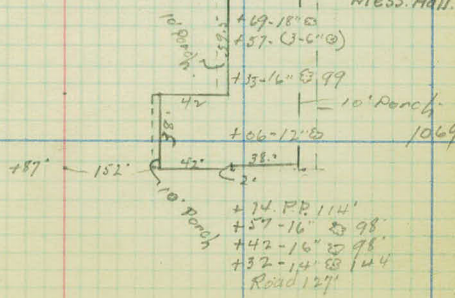
+15-30" @ 48 1064



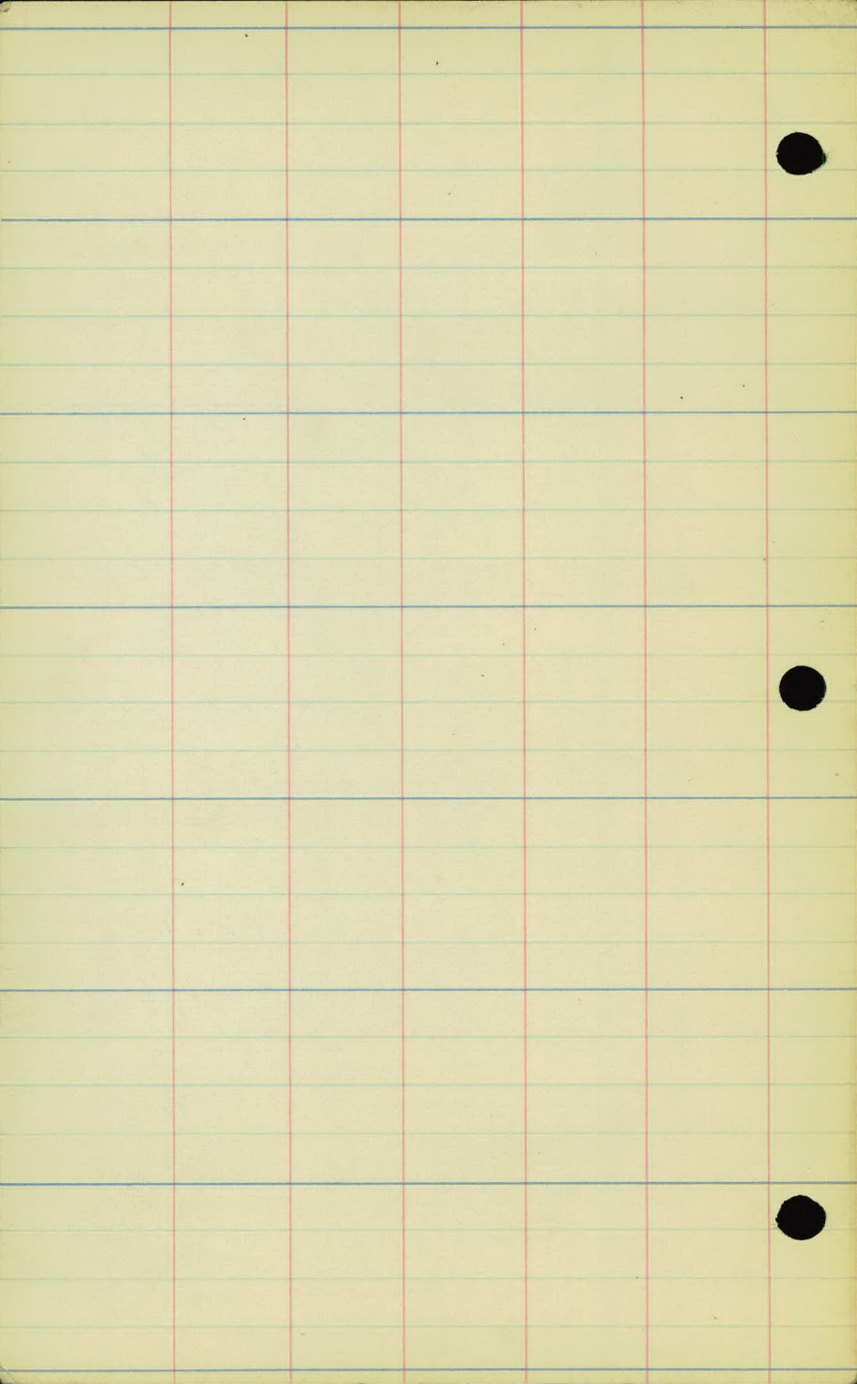
1071



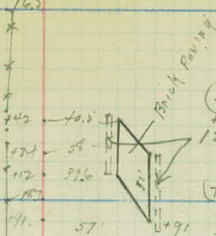
Brick Mess. Hall.



1068



+137 Ent. 19' u. d.
Fc 18.7



+66-18" @ 27'
 +55 Tool. P. 30'
 (+50 Tr. 44.7 - 54.7)
 +47 End Col. 36
 12' x 34' C.M.P.
 +16-18" @ 27'
 +12 Col. 34.6
 (Tr. 43.4 - 53.0)

1076

+139 Tool. P. 18.5

(Tr. 39.6 - 49.6) (Curb 131)
 +50-15" @ 26'
 +38 Tool. P. 27.3
 +34-15" @ 25.5
 +18-18" @ 26'

1075

+112 Tool. P. 18'

(Tr. 34.00) +91 Tool. P. 59.8

(Tr. 24.1 - 34.1)

+23 Tool. P. 40.0

Brick Stable Shoot

+102
+99 Tool. P. 17.7



(+50 Tr. 6.6 - 16.6) (Curb 81.5) (Fb. 35.9)

+19-12" @ 25.5
 +13 Tool. P. 22.0
 (Curb 60.5 Fb. 35.9)
 +95-24" @ 25

1073

+101 Tool. P. 18'

(Tr. 3.2 - 13.2) +70-15" @ 25.5
 +64-24" @ 26'

+59 Hyd. 22.5

+51 Entrance 17.5

(Tr. 2.65 - 12.65) +19-12" @ 25.5
 +107 Tool. P. 25.5
 Pav. 49 (Width 35.8)
 +74-24" @ 26'

1072

+80 Tool. P. 18.5

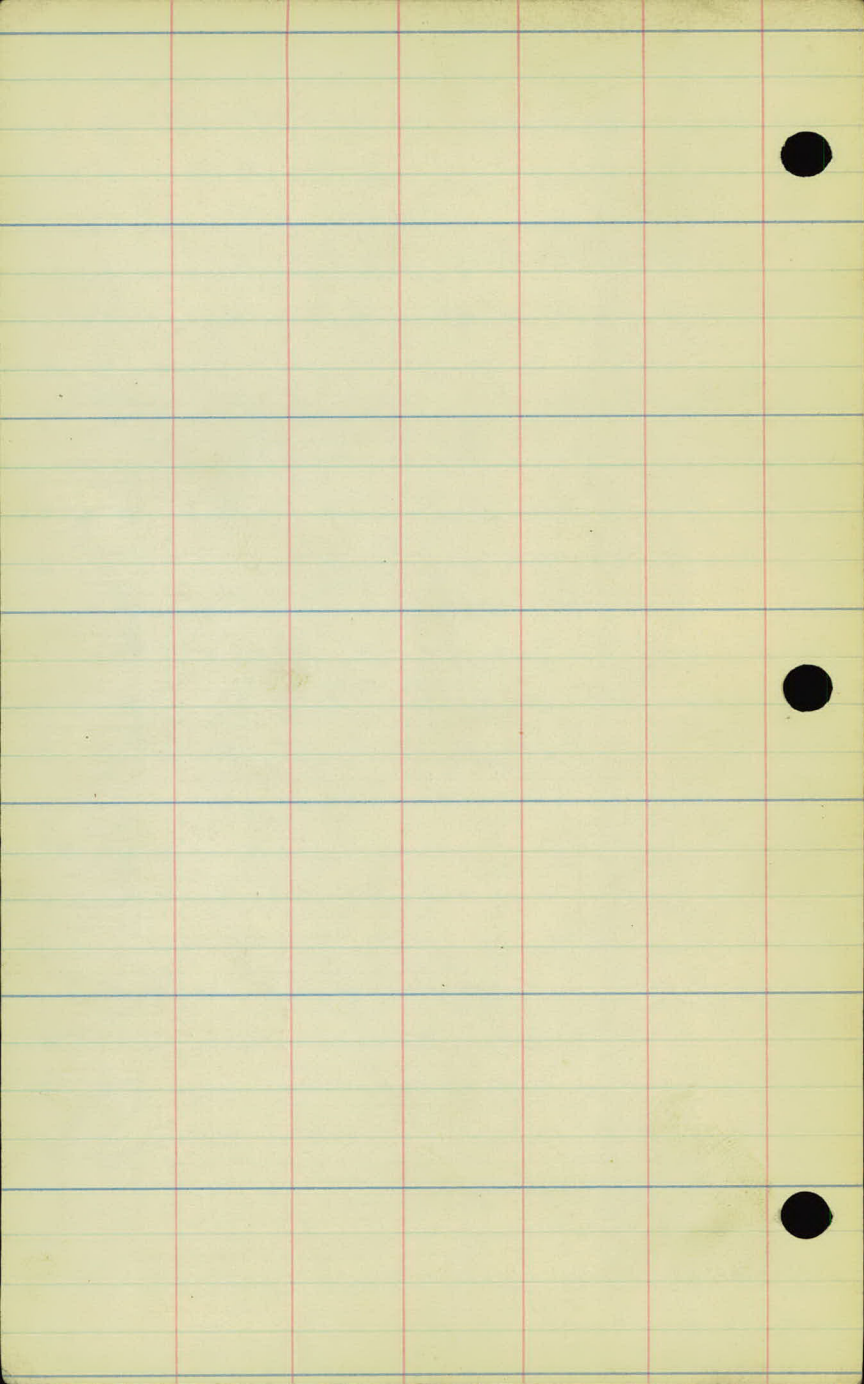
+44-30" @ 25.5

Pav. 46 (Width 35.8) 1071

+102 Beg. Fa. 19.5

+80 Tool. P. 24.5
 770-10" @ 25.5

1070



+98-Tool, P. 24.5
 +77-12" @ 21'
 +54-12" @ 23.5
 +71-30" @ 27'

+45-18" @ 21.5

+53-15" @ 21'

+28-18" @ 20.5

+52-12" @ 20'

+27-15" @ 19.5

+03-12" @ 19'

+81-20" @ 18.5

+90 1/2 Drive

+71 P.P. 16.5

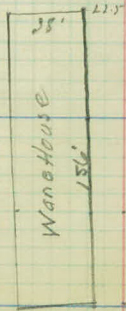
+06-15" @ 22.5

+93-11" @ 26'

+02-15" @ 15.5

+01 Bldg. 16.6

+58



60.5



6' walk

70

64.2

14.1

30

75

+10

11.5

(Track - 6.25-18.25)

1064

+50 Tool. P. 14.8

(Track 23'-53')

1063

+92 Tool. P. 11.6

Track 31.75

+51-30" @ 19.2

+23-24" @ 20'

+17 Hyd. 21.5

Track 39.85

1062

+87 Tool. P. 28'

(+50 Track 46.85)

+53-20" @ 22.5'

Track 53'

1061

+65-30" @ 24'

168 1/2 Road

Track 61'

1060

+91-24" @ 26.5

+57-38" @ 21'

+35 Hyd. 29'

+24-16" @ 27'

(Track 60.2)

1079

+79-Tool. P. 43.2

+66-20" @ 27.2

+16-24" @ 27.5

1078

+91-20" @ 27'

+66-6" @ 27'

+61 Tool. P. 35'

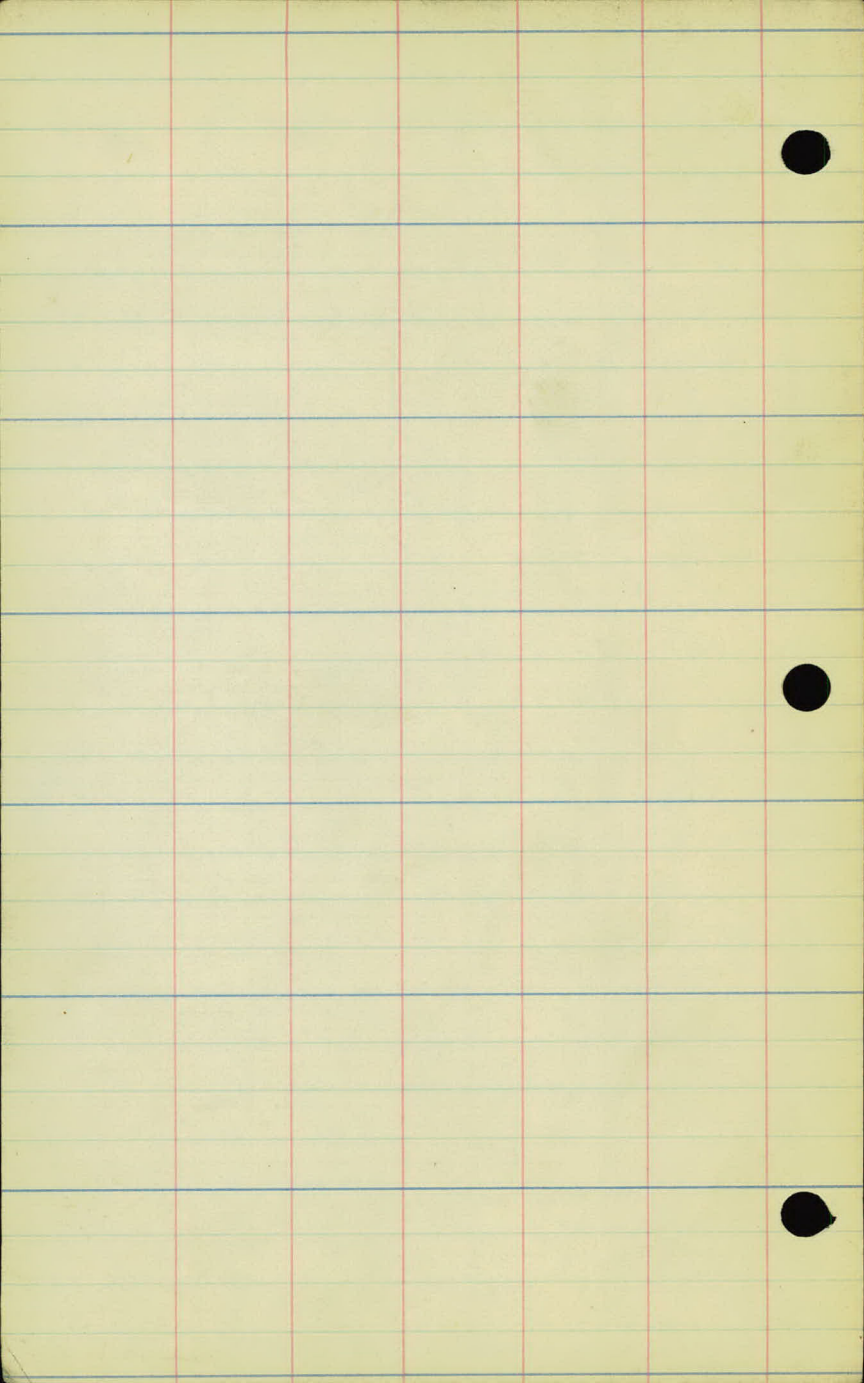
(Tr. 49.55-59.55)

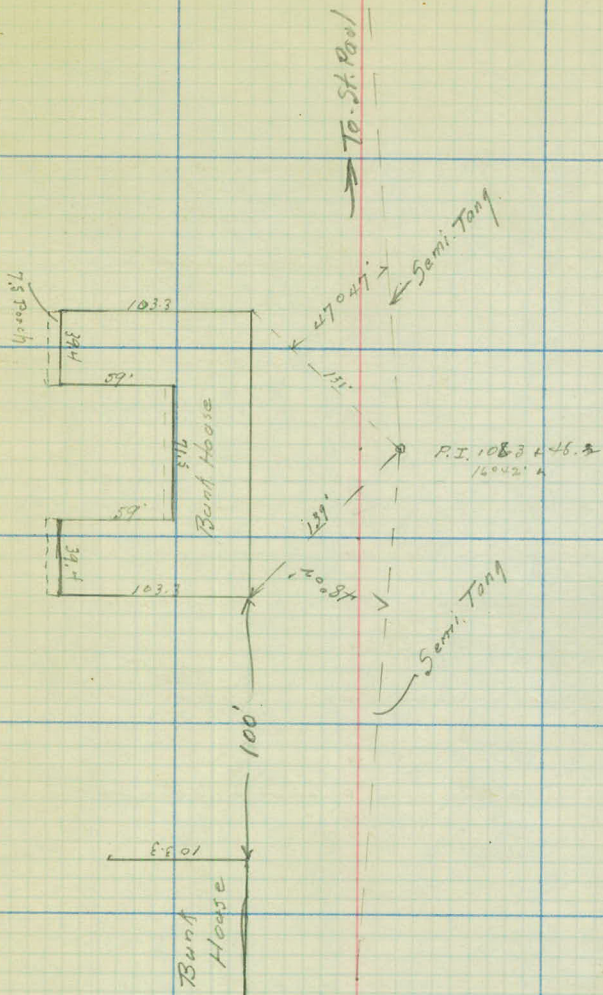
+40-20" @ 26.5

+16-24" @ 26.5

Tr. 49.5 - 57.5

1077





+10-12' @ 35
+00 Trolly P. 33

+97-15' @ 35

+31 @ 110

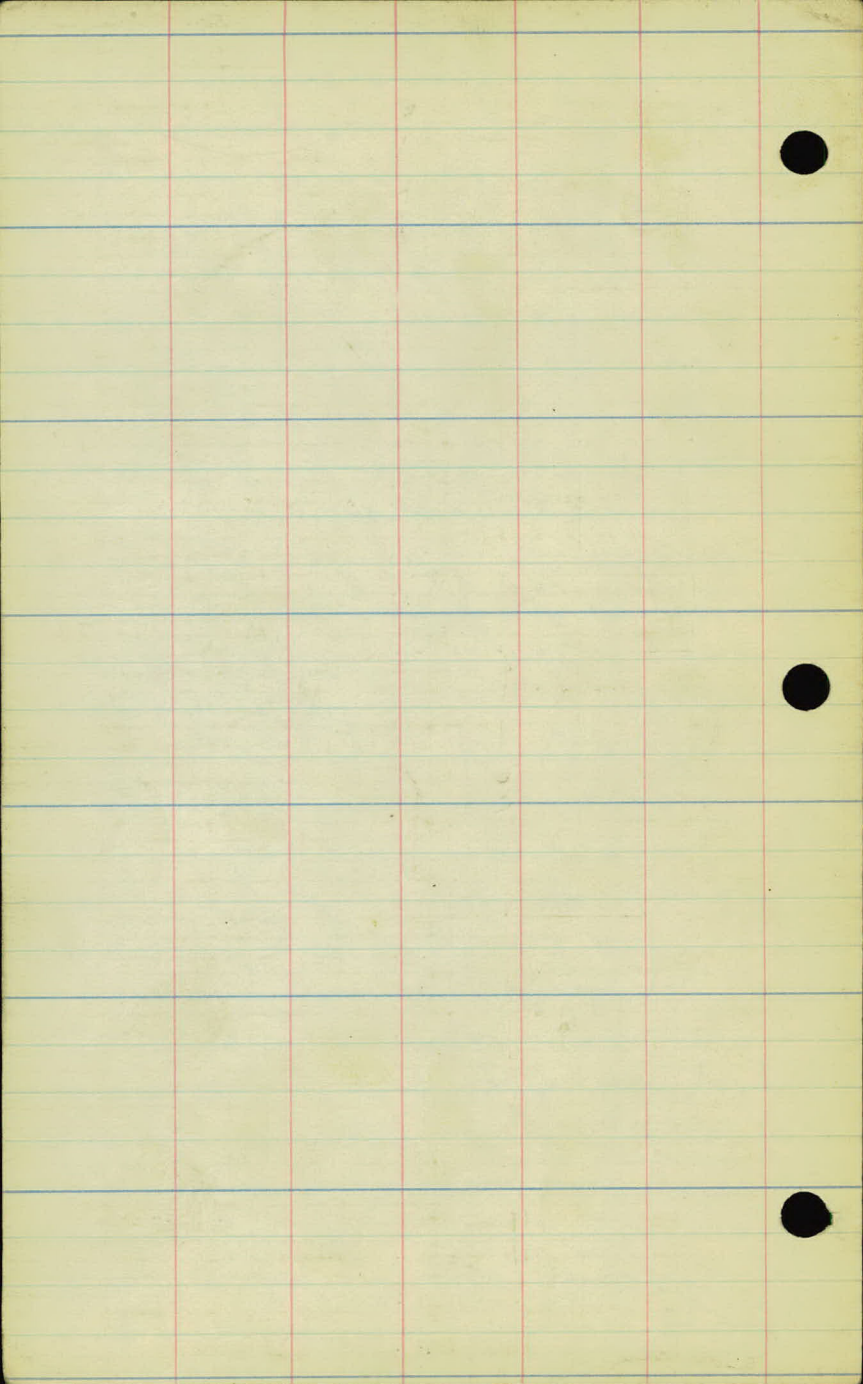
+04-15' @ 24

Track 0.85
55.6

+15 Trolly P. 22.5
Track 9.2
1085

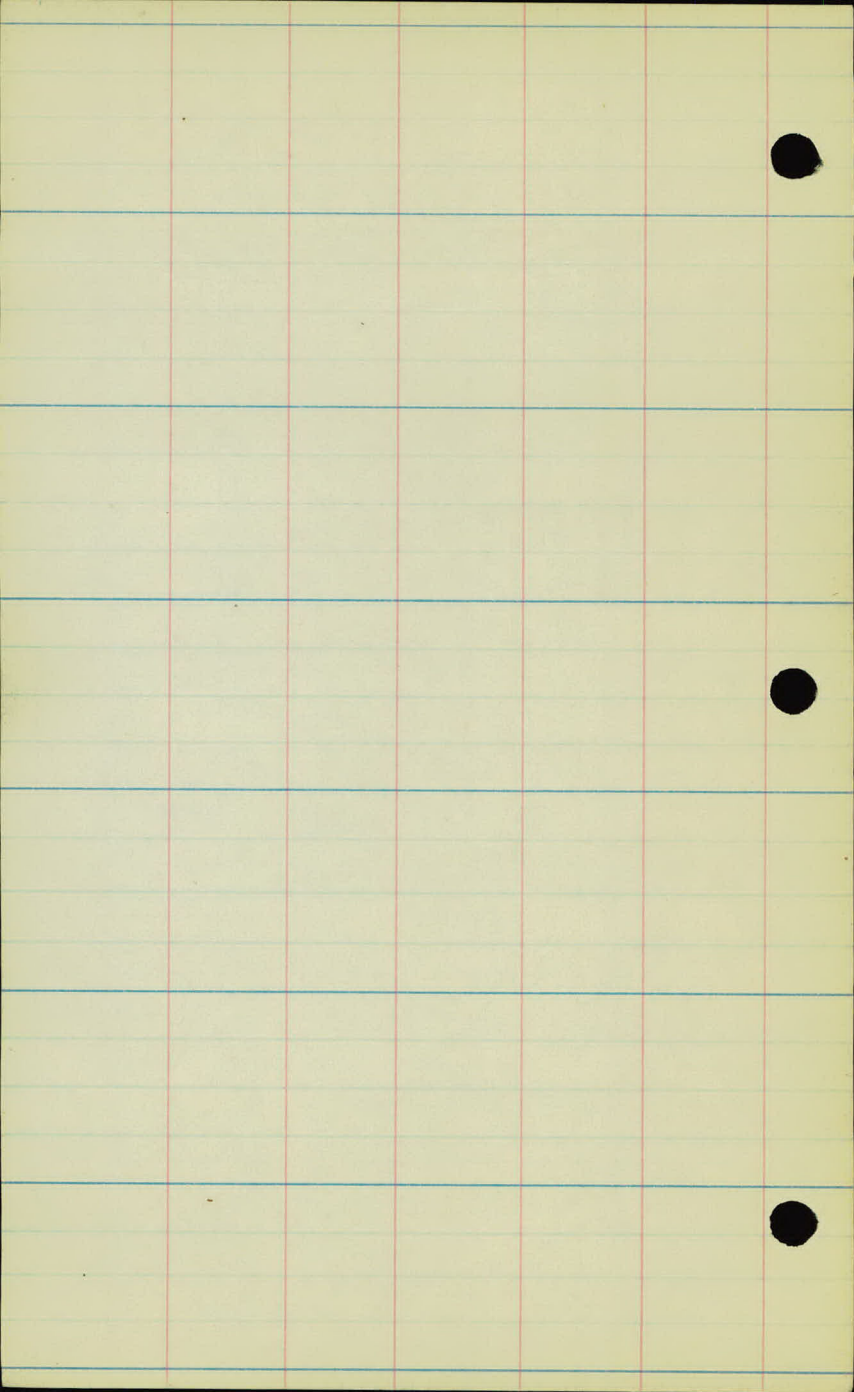
+76-24' @ 34.5

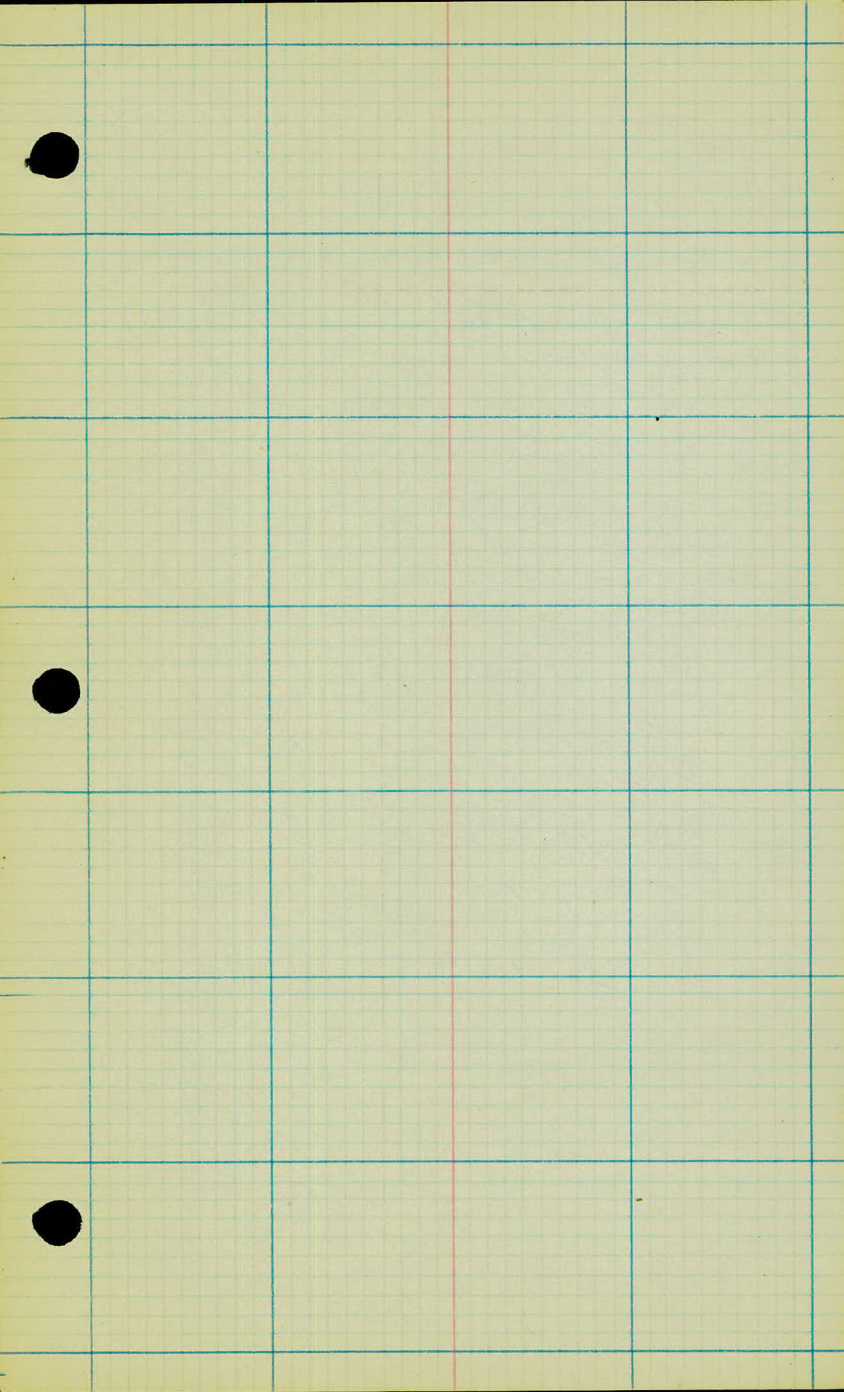
1084



Ref. 9/c H 98

Art. Topog on Fort
Snelling Connection.





1024

1025

1024

1023

1022

1021

5/19/20

W 8
34
8157

157 Q. Pitch.

Cultivated field

Ditch

187 pole 9'

122 Q. Nd

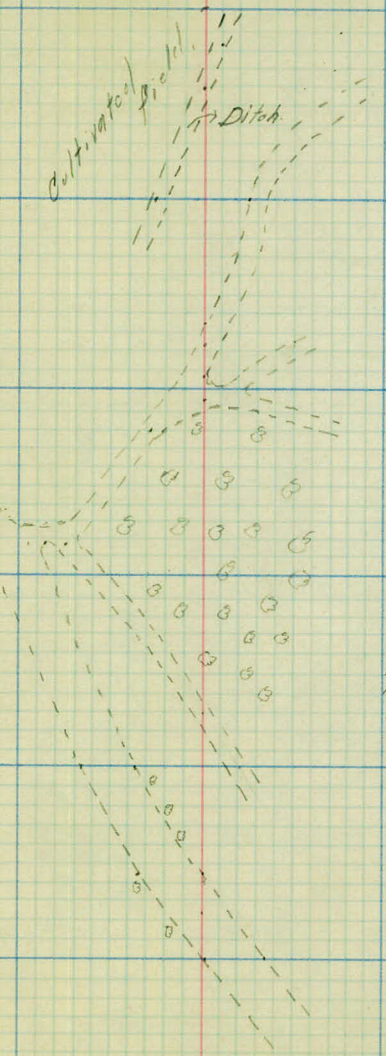
190 Q. Nd.

107 P.P.

136 T.P. 24
136 P.M. 18
129 Q. Nd.

144 Man Hole 7'

123 Q. Nd.



1032

1031

1030

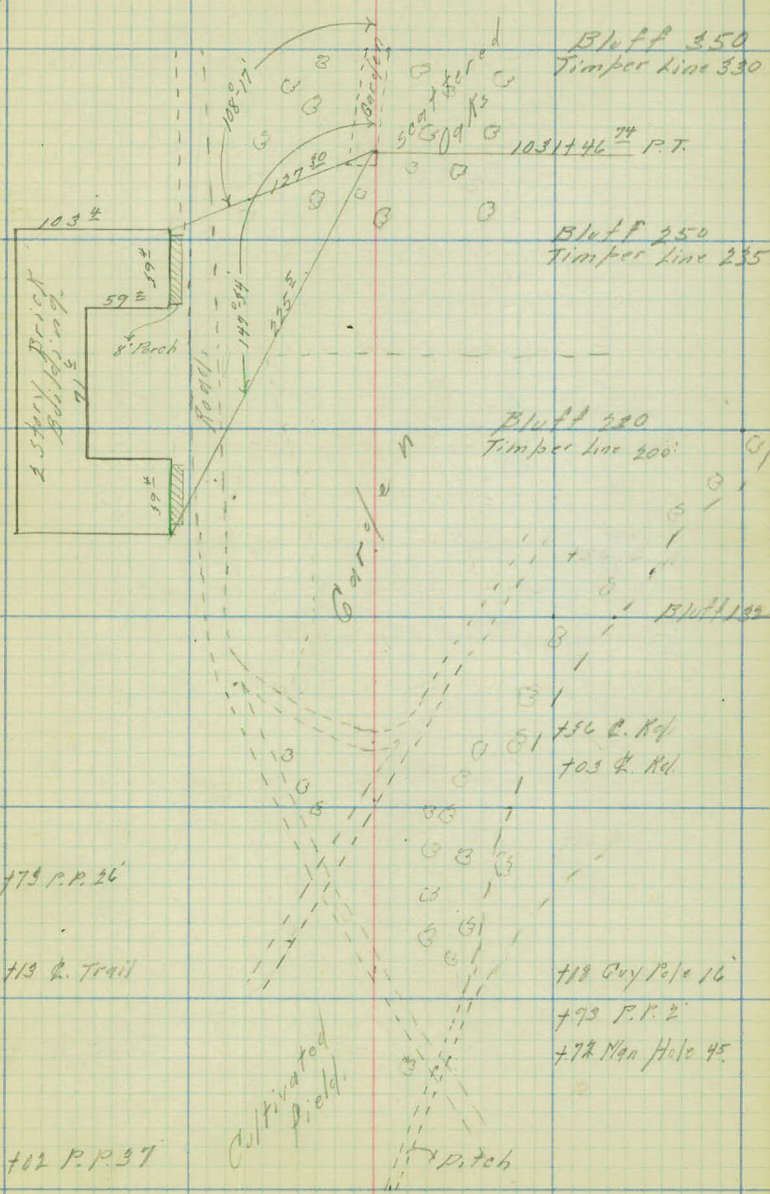
1029

1028

1027

1024

5/19/25



Bluff 350
Timber line 330

1031146 P.T.

Bluff 250
Timber line 235

Bluff 220
Timber line 200

Bluff 190

156 Q. Rd
103 Q. Rd

179 P.P. 26

113 Q. Trail

102 P.P. 37

118 Guy Pole 16

173 P.P. 2

172 Man Hole 45

Cultivated field

Pitch

1038

1037

1036

1035

1034

1033

1032

5/17/22

700 ft. Track 35 1/2

Garden

Bluff 450
Timber line 180

G

G

G

G

Bluff 415
Timber line 315

G

Bluff 450
Timber line 290

G

Garden

Bluff 450
Timber line 290

Reach

Timber

Garden

Bluff 475
Timber line 300

G

G

G

Bluff 475
Timber line 300

G

G

G

G

G

G

G

437 Rec. of Tr 35 1/2

1044

1043

1042

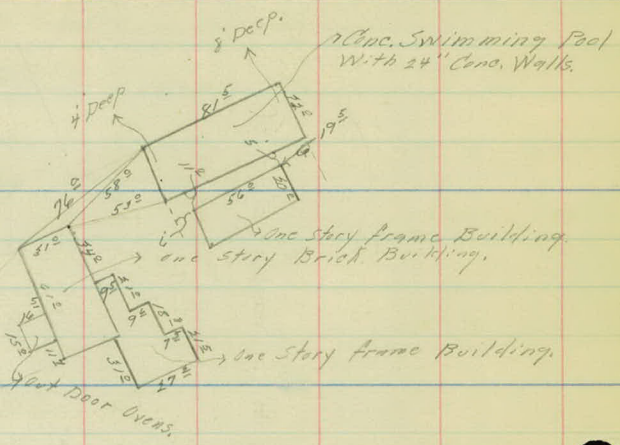
1043 + 27²⁰

1041

1040

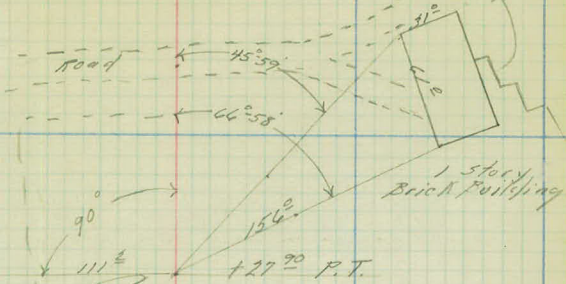
1039

1038



5/17/02

See opposite page



(44)

(43)

+27² H. Tract.
111²⁰ H.

+27²⁰ P.T.

Bluff 275
Timber line 275

(42)

Bluff 360
Timber line 360

(41)

Bluff 390
Timber line 250

(40)

Bluff 400
Timber line 250

+27² Q. Tr. 35

(39)

Bluff 400
Timber line 150

(1030)

Road
Garden

1050

1049

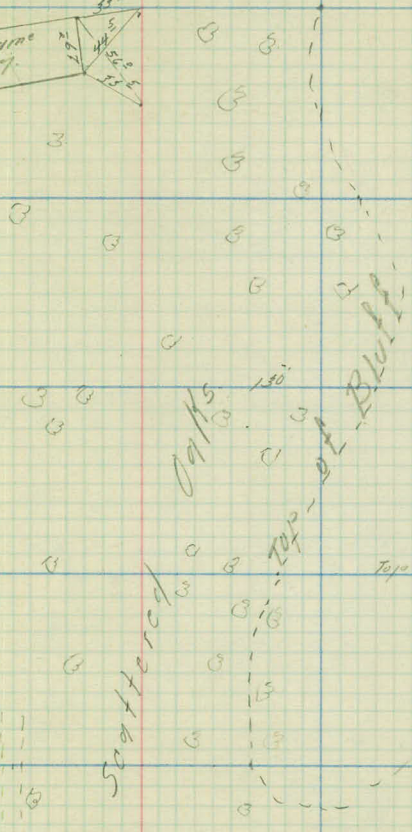
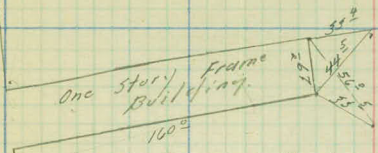
1048

1047

1046

1045

1044



Scattered

Top of Bluff

Top of Bluff

Bluff

Bluff 225
Timber line 225

150 E. Trail

128 E. Trail

107 P.F. 29
Bluff 150
Timber line 250

1054

1055

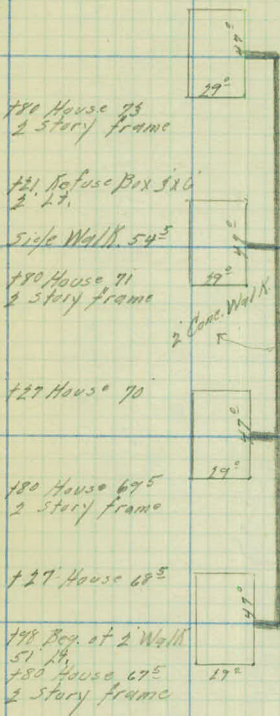
1054

1053

1052

1051

1050



180 House 75
2 story frame

121 Refuse Box 3x6
2 ft.

Side Walk 54"

180 House 71
2 story frame

2 Conc. Walk
↑

127 House 70

180 House 695
2 story frame

127 House 685

178 Box at 2 Walk
51 ft.
180 House 675
2 story frame

181 Refuse Box 3x6
5 ft.

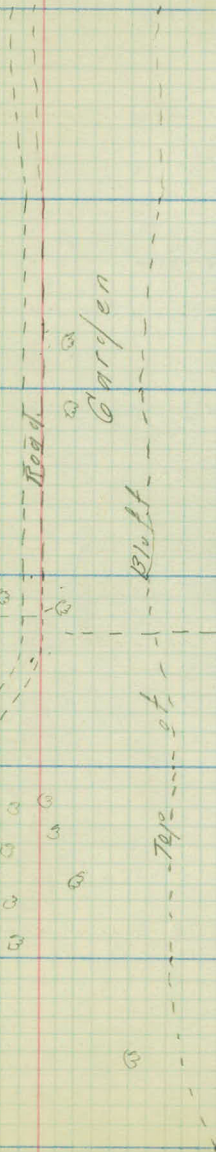
144 Refuse Box 3x6
1 ft.

141 Refuse Box 3x6
1 ft.

190 Refuse Box 3x6
2 ft.

106 Refuse Box 3x6
1 ft.

149 Refuse Box 3x6
2 ft.



Garden

Road

Bluff

Tape of

1062

1061

1060

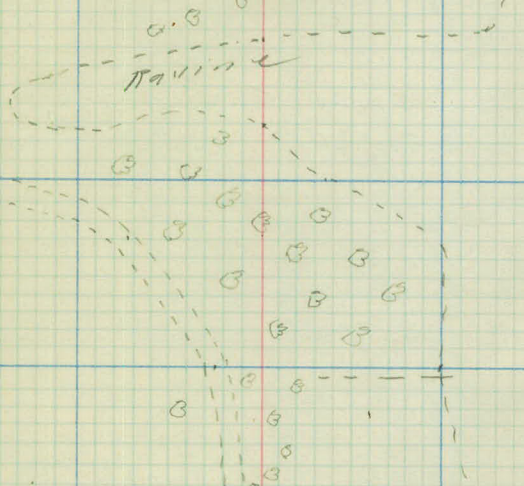
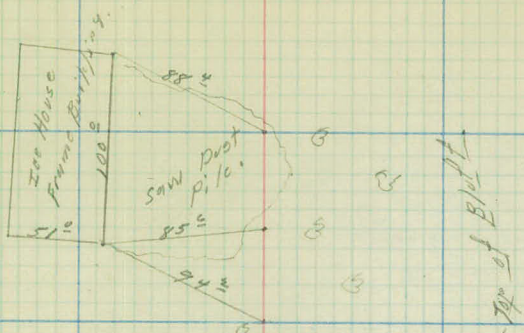
1059

1058

1057

1056

5/17/21



#27 House 76'
 104 End of 2' Side Walk 60'

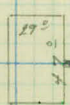
#80 House 77'

#27 House 76'
 102 Refuse Box 56' x 4' Side Walk 58'

#80 House 75' ± 5 story frame

#80 Refuse Box 56' on E.

Top of Bluff



Garden

1068

1067

1066

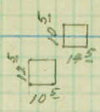
1065

1064

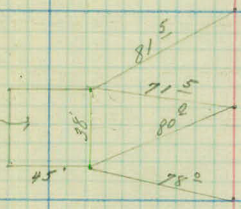
1063

1062

174 Shed/52'
185 Shed/51'

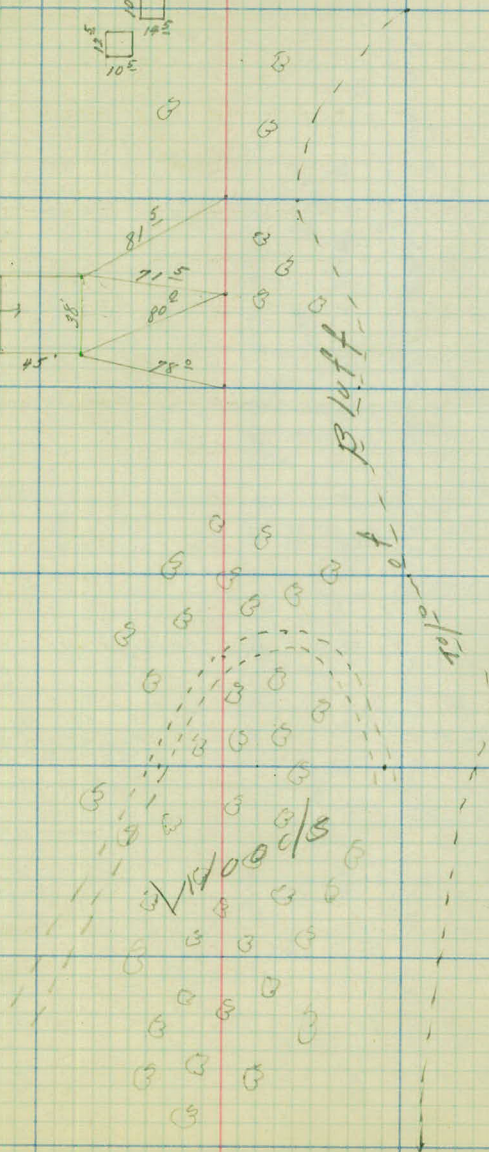


Water Tower



148 E. Road

Bluff



1074

1073

1072

1071

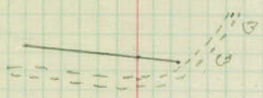
1070

1069

1068

5/19/40

117 E. Pitch

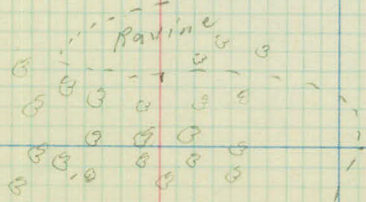


128 Cross Drain
 125 Cross Drain 24
 171.6' Vit.

3
 3 3

Cultivated Field

Top of Bluff



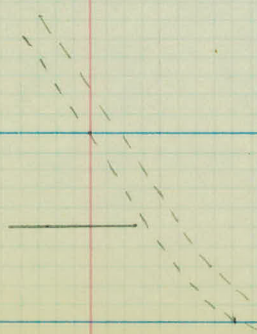
1077

1076

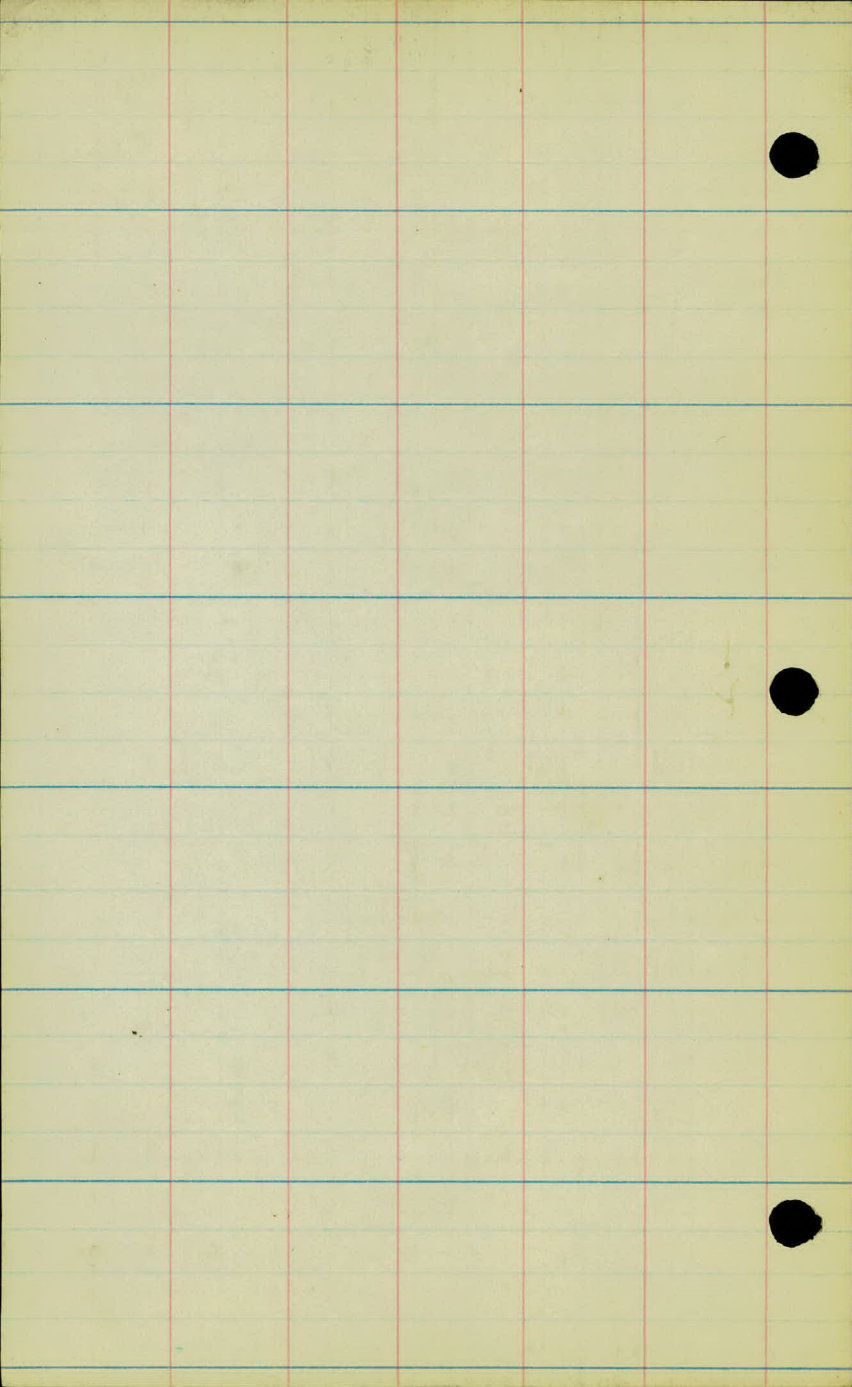
1075

1074

5/19/26



150 Cross Proj. 24'
P.H. 6 Vit.



Ref. 9/6 H 98

Center line levels and
X sections on Fort Snelling
Connection.

Sta.	+	H.I.	-	Red.	Elev.
B.M.	4.22	819.74		815.54	
1021+23	Q. Road			4.4	815.2.
+45				5.0	14.8.
+47				4.0	15.8.
1022				4.3	15.5.
+28	Q. Trail			4.9	14.9.
+38				4.8	15.0.
+48				4.4	15.2.
+74				8.8	11.0.
+81				8.3	11.5.
1023				9.7	10.1.
+22				11.0	08.8.
+28				9.8	10.0.
T.P.	0.93	812.76	7.93	811.83	
+65					06.5
+77				5.7	07.1.
+80				3.7	09.1.
+92	Q. Trail			3.8	09.0.
1024				3.7	09.1.
+50				4.4	08.2.
1025				4.4	08.2.

Lt.

Rt.

Spk. in P.P. 100 Rt. Sta. 1021+65

5.3	4.5	3.1	5.2	4.7		5.0	4.0	4.9
<u>50</u>	<u>30</u>	<u>18</u>	<u>15</u>	<u>11</u>	4.6	<u>14</u>	<u>17</u>	<u>50</u>

→ R.R.

5.0	4.1	4.7	5.6	4.6	4.6		4.0	4.6	4.6
<u>50</u>	<u>40</u>	<u>35</u>	<u>32</u>	<u>26</u>	<u>17</u>	5.0	<u>1</u>	<u>23</u>	<u>50</u>

→ R.R.

5.6	5.9	6.4	4.7	4.2					
<u>50</u>	<u>38</u>	<u>32</u>	<u>27</u>	<u>14</u>	4.3				

→ R. Trail

4.5		4.6	5.1	4.8					
<u>15</u>		<u>24</u>	<u>45</u>	<u>50</u>					

815.7 - Elev
of Top of
7th St. Sta. 1021+60.

7.0	4.4	5.2	5.0		4.4	4.9	10.0	10.3	
<u>50</u>	<u>45</u>	<u>30</u>	<u>15</u>	4.8	<u>11</u>	<u>33</u>	<u>42</u>	<u>50</u>	

→ R. Road.

11.1	4.6	5.3	5.1		9.3	10.9	11.0	9.7	9.3	10.9
<u>71</u>	<u>50</u>	<u>35</u>	<u>15</u>	4.4	<u>8</u>	<u>18</u>	<u>29</u>	<u>35</u>	<u>44</u>	<u>50</u>

→ R. Road.

6.2	6.0	6.4	5.3	4.7		9.7	9.9	8.8	11.2	
<u>50</u>	<u>41</u>	<u>36</u>	<u>24</u>	<u>10</u>	8.8	<u>17</u>	<u>29</u>	<u>44</u>	<u>50</u>	

6.7	5.0	9.1	7.5	9.2		9.3	9.1			
<u>50</u>	<u>33</u>	<u>20</u>	<u>15</u>	<u>9</u>	9.7	<u>27</u>	<u>50</u>			

7.5	9.2	10.0		9.5	12.0	10.8	10.8	11.0		
<u>50</u>	<u>33</u>	<u>14</u>	9.8	<u>4</u>	<u>7</u>	<u>19</u>	<u>35</u>	<u>50</u>		

→ R.R.

2.0	2.7	2.8	2.8	5.7		4.9	3.5	4.9	5.0	4.1
<u>50</u>	<u>46</u>	<u>36</u>	<u>29</u>	<u>15</u>	6.3	<u>8</u>	<u>18</u>	<u>24</u>	<u>34</u>	<u>50</u>

→ Bottom of Ditch

7.6	3.3	3.3	3.7	3.9	3.2	3.6		3.3	3.7	4.6	4.5
<u>74</u>	<u>54</u>	<u>50</u>	<u>35</u>	<u>21</u>	<u>16</u>	<u>11</u>	3.7	<u>19</u>	<u>30</u>	<u>39</u>	<u>50</u>

→ Bottom of Ditch.

3.8	7.7	7.7	4.0	3.8	4.9	4.5		4.7	4.4	4.1	5.3	5.4
<u>57</u>	<u>47</u>	<u>43</u>	<u>37</u>	<u>29</u>	<u>22</u>	<u>12</u>	4.6	<u>11</u>	<u>15</u>	<u>27</u>	<u>38</u>	<u>50</u>

→ Bottom of Ditch

4.7	4.2	8.5	8.5	4.6		4.1	3.9	4.2	4.2			
<u>50</u>	<u>34</u>	<u>25</u>	<u>13</u>	<u>16</u>	4.6	<u>13</u>	<u>50</u>	<u>44</u>	<u>50</u>			

Sta.	+	H.I.	-	Rod.	Elev.
		812.76			
+39				5.2	807.6
+59				9.1	03.7
+71				6.4	06.4
1026				7.0	05.8
T.P.	7.15	811.32	8.59	804.17	
+50				6.3	05.0
1027				5.0	06.3
+05				6.1	05.2
+14	Q. Trail			5.9	05.4
+50				4.4	06.9
B.M.				1.95	809.57
1028				4.1	07.2
+35	Q. Road.			4.1	07.2
+50				3.7	07.6
1029				4.4	06.9
T.P.	8.23	815.74	3.81	807.51	
1030				7.4	08.3
+50				6.5	09.2

Bottom of Ditch Pt.

5.2 5.1 8.7 8.7 5.1 4.0 3.4
50 16 8 6 5.2 21 37 50

Bottom of Ditch

5.0 6.6 5.9 7.1 7.1 5.2 6.1 4.8 4.1
50 15 7 1 9.1 1 9 22 40 50

Bottom of Ditch

5.2 6.8 9.0 9.0 6.2 4.8 4.6
50 8 6.4 5 7 14 44 50

Bottom of Ditch

5.2 6.5 7.3 9.3 9.5 8.3 5.8
50 14 7.0 7 13 14 21 50

Bottom of Ditch

3.7 4.3 7.5 9.7 9.2 9.2 9.0 8.5
50 30 6.3 18 31 32 34 43 50

Bottom of Ditch

Q. Rd.

50 37 5.1 50 6.7 6.9 7.1 12.4 12.4
64 50 14 5.0 4 5 18 38 50 52

Q. Rd.

3.6 3.7 3.5 4.9 7.0 8.0
50 29 8 4.4 22 46 50

Spk. in 12" Co. N 40 Lt. Sta. 1028100 Q. Rd.

3.3 3.2 3.8 4.3 4.1 4.4 7.7 6.2
50 40 30 14 2 4.1 15 32 50

Q. Rd.

3.6 3.7 4.6 5.3 5.4
50 35 3.7 24 37 50

Above H.I.

Q. Road.

70.9 70.5 70.5 00 2.9 4.7 5.4
79 50 44 38 32 4.4 28 50

5.9 6.8 7.9 8.2
50 39 7.4 30 50

Q. Road.

15 1.6 4.7 7.6 8.2
100 70 50 6.5 30 50

802.8 = E/10
70% of Max H/10
45 ft. Sta. 1026 + 74.

Sta.	T.	H.I.	-	Prod.	Elev.
		815.74			
1031				7.0	808.7.
105				7.0	08.7.
107				5.7	10.0.
1032				4.5	11.2.
137				4.0	11.7.
1033				3.9	11.8.
1034				3.8	11.9.
1035				3.4	12.3.
T.P.	5.04	817.77	3.01	812.73	
1034				4.8	15.0.
1037				4.7	13.1.
1038				6.6	11.2.
1039				6.0	11.8.
1040				6.4	11.4.
1041				6.1	11.7.
T.P.	1.98	816.47	3.28	814.49	

		LT										RT
2.4	3.2	5.4	5.8	7.1				6.9				7.4
<u>75</u>	<u>50</u>	<u>25</u>	<u>18</u>	<u>10</u>	7.0			<u>23</u>				<u>50</u>

		5.1	5.5					7.1	7.7
		<u>44</u>	<u>28</u>	5.7				<u>32</u>	<u>50</u>

22 1/2

2.5	2.7	3.5	3.8	5.9				5.4	6.2
<u>105</u>	<u>94</u>	<u>85</u>	<u>50</u>	<u>15</u>	4.5			<u>25</u>	<u>50</u>

Top of Rail

3.4	2.9	2.8	3.2					4.7	5.7
<u>50</u>	<u>57.8</u>	<u>33</u>	<u>22</u>	4.0				<u>37</u>	<u>50</u>

T.R.

3.3	4.2	3.5	3.1	3.1	3.6	3.4				4.3	4.8
<u>50</u>	<u>45</u>	<u>47</u>	<u>37.8</u>	<u>33</u>	<u>51</u>	<u>19</u>	3.9			<u>31</u>	<u>50</u>

5.5	3.5	4.4	4.4	3.4	2.9	2.9	3.3					3.8	4.2
<u>50</u>	<u>47</u>	<u>44</u>	<u>43</u>	<u>40</u>	<u>37.8</u>	<u>33</u>	<u>30</u>	3.8				<u>24</u>	<u>50</u>

2.8	2.8	4.1	4.1	3.2	2.7	2.8	3.3					3.6	4.1
<u>50</u>	<u>48</u>	<u>44</u>	<u>40</u>	<u>37.8</u>	<u>33</u>	<u>30</u>	3.4					<u>22</u>	<u>50</u>

5.0	5.7	5.7	5.2	4.6	4.6	5.0	4.9					5.0	6.4	6.8
<u>50</u>	<u>45</u>	<u>43</u>	<u>40</u>	<u>37.8</u>	<u>33</u>	<u>31</u>	<u>19</u>	4.8				<u>23</u>	<u>33</u>	<u>50</u>

T.R.

4.9	5.7	5.1	4.5	4.5	5.0	4.5						5.2	6.2	6.2	6.2
<u>50</u>	<u>43</u>	<u>40</u>	<u>37.8</u>	<u>33</u>	<u>24</u>	<u>15</u>	4.7					<u>14</u>	<u>24</u>	<u>39</u>	<u>50</u>

4.9	4.5	4.5	4.9	6.4						6.6	6.6
<u>50</u>	<u>37.8</u>	<u>33</u>	<u>31</u>	<u>22</u>	6.4					<u>24</u>	<u>50</u>

T.R.

4.5	4.1	4.1	4.6	5.5						5.4	6.0
<u>50</u>	<u>37.8</u>	<u>33</u>	<u>27</u>	<u>22</u>	6.0					<u>21</u>	<u>50</u>

4.6	3.7	3.7	4.7	6.2						6.4	6.1
<u>50</u>	<u>41</u>	<u>37</u>	<u>31</u>	<u>22</u>	6.4					<u>28</u>	<u>50</u>

T.R.

3.9	3.9	4.4	5.6	6.4						5.4	5.2
<u>52</u>	<u>47</u>	<u>43</u>	<u>34</u>	<u>17</u>	6.1					<u>34</u>	<u>50</u>

Sta.	+	H.F.	-	Ref.	Elev
		816.47			
1042				5.8	810.7.
1043				4.3	12.2 <u>14.2</u>
1044				5.4	11.1.
+13				4.4	11.9.
+28	Q. Ref.			5.2	11.3.
+35				5.4	11.1.
+50				6.4	10.1.
T.P.	4.76	817.28	3.95	812.52	
1045				8.7	08.4.
+50				8.7	08.4.
1046				5.9	11.4.
1047				4.2	13.1.
1048				1.9	16.0.
T.P.	5.07	821.84	0.51	816.77	
+50				4.5	17.3.
1049				4.6	17.2.
+50				5.7	16.1.

Lt.

Rt.

$\frac{5.9}{30}$	$\frac{6.0}{23}$	5.8	$\frac{5.7}{27}$	$\frac{5.5}{50}$
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T.R.

$\frac{2.6}{108}$	$\frac{2.5}{103}$	$\frac{3.1}{100}$	$\frac{4.5}{89}$	$\frac{4.5}{50}$	$\frac{4.9}{30}$	4.3	$\frac{4.3}{12}$	$\frac{5.0}{50}$
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$\frac{4.3}{50}$	$\frac{4.4}{25}$	5.4	$\frac{5.7}{24}$	$\frac{5.9}{50}$
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$\frac{5.0}{50}$	$\frac{5.4}{25}$	5.4	$\frac{5.6}{21}$	$\frac{5.6}{50}$
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→ 2. R/L

$\frac{6.3}{50}$	$\frac{7.1}{27}$	$\frac{8.4}{12}$	8.9	$\frac{11.0}{25}$	$\frac{8.8}{50}$
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$\frac{5.6}{50}$	$\frac{6.0}{34}$	$\frac{8.0}{14}$	8.9	$\frac{10.3}{24}$	$\frac{11.7}{39}$	$\frac{11.2}{50}$
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$\frac{4.2}{50}$	$\frac{5.0}{20}$	$\frac{6.1}{12}$	5.9	$\frac{7.4}{26}$	$\frac{9.2}{43}$	$\frac{10.0}{50}$
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$\frac{2.3}{50}$	$\frac{3.5}{21}$	4.2	$\frac{5.0}{9}$	$\frac{4.8}{15}$	$\frac{8.3}{50}$
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$\frac{1.4}{50}$	$\frac{1.5}{22}$	1.3	$\frac{2.3}{30}$	$\frac{1.4}{50}$
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$\frac{4.8}{50}$	$\frac{4.8}{19}$	4.5	$\frac{5.0}{28}$	$\frac{5.5}{50}$
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$\frac{3.8}{50}$	$\frac{3.8}{24}$	4.4	$\frac{6.0}{19}$	$\frac{7.0}{30}$
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$\frac{4.2}{50}$	$\frac{3.7}{38}$	$\frac{4.9}{18}$	5.7	$\frac{6.6}{11}$	$\frac{7.5}{32}$	$\frac{7.4}{50}$
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Sta.	T	H.I.	-	Red.	Elev.
		821.84			
1050				5.8	816.0.
750				6.5	15.3.
1051				6.3	15.5.
B.M.	1.03	819.50	3.37	918.47	
1052				4.1	15.4.
754				4.5	15.0.
1053				5.5	14.0.
1054				8.6	10.9.
T.P.	4.28	814.72	7.06	810.44	
1055				6.2	08.5.
1056				8.3	06.4.
753				7.4	07.3.
1057				7.4	07.1.
1058				4.9	09.8.
T.P.	5.32	815.17	4.87	809.85	
750				5.5	09.7.

H. $\frac{4.4}{50}$ $\frac{4.7}{45}$ $\frac{5.5}{11}$ 5.8 7.5 $\frac{9.0}{19}$ $\frac{11.0}{39}$ $\frac{11.0}{50}$ RT

818.0 = Elev of foundation Building in H.

$\frac{3.8}{50}$ $\frac{4.9}{34}$ $\frac{6.6}{7}$ 6.5 $\frac{9.3}{27}$ $\frac{11.7}{50}$

$\frac{4.4}{50}$ $\frac{5.5}{32}$ 6.3 $\frac{8.7}{25}$ $\frac{11.8}{50}$

SPK in 18" dia. 40 H. Sta. 1051760

$\frac{1.5}{50}$ $\frac{1.9}{34}$ $\frac{2.9}{14}$ 4.1 $\frac{4.4}{10}$ $\frac{6.5}{32}$ $\frac{8.8}{50}$

$\frac{1.8}{50}$ $\frac{2.9}{14}$ $\frac{4.3}{10}$ 4.5 $\frac{5.0}{9}$ $\frac{7.3}{25}$ $\frac{9.6}{50}$

814.15 = Elev. of top of foundation House on Lt. 1052180

$\frac{2.1}{50}$ $\frac{3.0}{31}$ $\frac{3.7}{15}$ $\frac{5.4}{9}$ 5.5 $\frac{6.9}{9}$ $\frac{9.4}{30}$ $\frac{12.1}{50}$

816.9 = Elev. of foundation House on Lt. 1053180.

$\frac{4.6}{50}$ $\frac{6.0}{33}$ $\frac{6.7}{16}$ $\frac{8.0}{11}$ 8.4 $\frac{9.5}{5}$ $\frac{12.5}{27}$ $\frac{16.0}{50}$

815.2 Elev. foundation House on Lt. 1054180.

$\frac{1.5}{50}$ $\frac{3.0}{37}$ $\frac{3.8}{20}$ $\frac{5.7}{13}$ 6.2 $\frac{8.4}{13}$ $\frac{11.0}{34}$ $\frac{13.6}{50}$

814.4 = Elev. foundation House Lt. 1055180.

$\frac{3.4}{50}$ $\frac{4.5}{34}$ $\frac{5.1}{22}$ $\frac{6.4}{14}$ $\frac{6.6}{2}$ 8.3 $\frac{9.8}{12}$ $\frac{15.4}{50}$

$\frac{3.7}{50}$ $\frac{5.1}{21}$ $\frac{6.5}{14}$ 7.4 $\frac{8.9}{7}$ $\frac{16.5}{17}$ $\frac{15.7}{50}$

814.7 Elev. foundation House Lt. 1056180.

$\frac{3.3}{50}$ $\frac{4.5}{27}$ $\frac{5.7}{13}$ 7.6 $\frac{11.7}{14}$ $\frac{16.0}{50}$

814.5 = Elev. foundation House Lt. 1057180.

$\frac{0.7}{50}$ $\frac{2.9}{35}$ $\frac{4.4}{17}$ 4.9 $\frac{7.2}{17}$ $\frac{9.2}{38}$ $\frac{10.6}{50}$

$\frac{1.1}{50}$ $\frac{2.7}{16}$ $\frac{4.0}{11}$ $\frac{4.5}{7}$ 5.5 $\frac{8.5}{24}$ $\frac{11.4}{50}$

Sta.	T	H. I.	-	Roof	Elev.
		815.17			
1059				7.1	808.1.
P.M.				5.43	809.54
780				12.5	02.7.
T.P.	5.23	807.91	12.49	802.68	
1060				7.4	800.3.
730				11.7	796.2.
752				28.6	779.3.
773				9.0	798.9.
782				7.4	800.5.
1061				6.1	01.8.
T.P.	9.95	816.32	1.54	806.37	
750				10.9	05.4.
1062				9.4	06.7.
739				14.7	801.4.
T.P.	5.84	809.48	12.70	803.42	
1063				10.4	798.9.

Lt. $\frac{1.7}{50}$ $\frac{3.6}{30}$ $\frac{4.4}{24}$ $\frac{5.0}{18}$ 7.1 $\frac{9.0}{18}$ $\frac{11.8}{39}$ $\frac{14.0}{50}$

510 N. in 12°04N 50 Lt. 514, 1059+94

$\frac{6.2}{50}$ $\frac{6.8}{41}$ $\frac{9.8}{18}$ 12.5 $\frac{20.3}{39}$ $\frac{23.0}{50}$

$\frac{0.4}{50}$ $\frac{1.8}{33}$ $\frac{4.2}{18}$ 7.4 $\frac{10.9}{17}$ $\frac{16.5}{39}$ $\frac{25.1}{50}$

$\frac{3.0}{50}$ $\frac{4.8}{33}$ $\frac{8.0}{14}$ 11.7 $\frac{34.1}{19}$ $\frac{39.2}{40}$ $\frac{44.7}{63}$ $\frac{50.5}{82}$ $\frac{53.2}{100}$

$\frac{21.7}{50}$ $\frac{24.3}{38}$ $\frac{26.3}{25}$ $\frac{27.0}{15}$ 28.6 $\frac{24.2}{16}$ $\frac{22.2}{31}$ $\frac{28.6}{50}$ $\frac{35.3}{70}$

$\frac{3.5}{50}$ $\frac{8.2}{37}$ $\frac{9.4}{27}$ $\frac{12.8}{10}$ $\frac{9.0}{4}$ 9.0 $\frac{10.7}{18}$ $\frac{15.4}{34}$ $\frac{14.9}{50}$

$\frac{2.4}{50}$ $\frac{4.8}{24}$ $\frac{6.4}{10}$ 7.4 $\frac{10.6}{23}$ $\frac{12.4}{38}$ $\frac{14.0}{50}$

$\frac{0.0}{50}$ $\frac{0.9}{41}$ $\frac{2.6}{19}$ $\frac{5.0}{8}$ 6.1 $\frac{7.9}{17}$ $\frac{11.7}{50}$

$\frac{4.5}{50}$ $\frac{4.5}{32}$ $\frac{5.3}{27}$ $\frac{8.9}{7}$ 10.9 $\frac{12.8}{13}$ $\frac{15.8}{18}$ $\frac{16.6}{43}$ $\frac{17.7}{50}$

$\frac{4.0}{50}$ $\frac{5.3}{24}$ $\frac{4.7}{17}$ $\frac{7.1}{4}$ 7.4 $\frac{12.2}{7}$ $\frac{15.3}{23}$ $\frac{18.5}{34}$ $\frac{18.0}{46}$ $\frac{21.8}{50}$

$\frac{4.2}{50}$ $\frac{4.8}{41}$ $\frac{7.2}{34}$ $\frac{9.4}{24}$ $\frac{12.6}{11}$ 14.9 $\frac{16.0}{19}$ $\frac{20.7}{34}$ $\frac{22.6}{50}$

$\frac{2.6}{50}$ $\frac{7.1}{18}$ 10.4 $\frac{13.5}{20}$ $\frac{18.1}{50}$

Sta.	T	H.I.	-	Red.	Elev.
		809.48			
f30				12.2	797.3
1044				11.7	97.8
f31				12.4	96.9
f40				13.8	95.7
f48	H. Road			15.4	94.1
f50				15.5	94.0
f63				15.8	93.7
1045				14.0	95.5
f30				10.7	798.8
T. P.	8.01	814.73	2.74	806.72	
f50				14.2	800.5
1064				10.8	03.9
f50				8.5	06.2
1067				7.3	07.4
T. P.	5.47	814.97	5.23	809.50	
f83				6.6	08.4
B. M.				9.73	805.24
1048				9.0	06.0

17. $\frac{5.0}{50}$ $\frac{6.7}{37}$ $\frac{9.7}{17}$ $\frac{12.2}{12.2}$ $\frac{19.7}{28}$ $\frac{17.7}{50}$ R.H.
 ↗ 2. Road.

$\frac{7.1}{50}$ $\frac{7.7}{45}$ $\frac{8.1}{34}$ $\frac{8.3}{29}$ $\frac{9.7}{17}$ $\frac{11.7}{11.7}$ $\frac{14.7}{28}$ $\frac{16.0}{40}$ $\frac{17.7}{50}$

↗ 2. Rd.
 $\frac{7.9}{50}$ $\frac{7.4}{30}$ $\frac{12.7}{18}$ $\frac{13.8}{7}$ $\frac{13.8}{13.8}$ $\frac{14.3}{14}$ $\frac{16.7}{33}$ $\frac{17.3}{50}$

↗ 2. Rd. ↗ 2. Rd.
 $\frac{7.3}{50}$ $\frac{11.3}{25}$ $\frac{13.1}{21}$ $\frac{15.1}{4}$ $\frac{15.8}{15.8}$ $\frac{17.3}{8}$ $\frac{18.4}{17}$ $\frac{20.7}{34}$ $\frac{22.3}{50}$ $\frac{22.3}{55}$

$\frac{6.1}{50}$ $\frac{8.6}{34}$ $\frac{11.4}{11}$ $\frac{13.3}{7}$ $\frac{14.0}{14.0}$ $\frac{16.0}{12}$ $\frac{21.0}{47}$ $\frac{20.5}{50}$

$\frac{3.2}{50}$ $\frac{6.8}{43}$ $\frac{6.8}{29}$ $\frac{7.6}{15}$ $\frac{10.7}{10.7}$ $\frac{12.5}{18}$ $\frac{14.4}{39}$ $\frac{18.5}{50}$

$\frac{11.0}{46}$ $\frac{11.0}{46}$ $\frac{10.0}{33}$ $\frac{11.2}{16}$ $\frac{14.2}{14.2}$ $\frac{17.3}{19}$ $\frac{22.5}{50}$

$\frac{7.4}{50}$ $\frac{9.6}{47}$ $\frac{11.5}{25}$ $\frac{8.9}{18}$ $\frac{9.7}{8}$ $\frac{10.8}{10.8}$ $\frac{15.5}{29}$ $\frac{19.8}{50}$

$\frac{1.5}{30}$ $\frac{5.5}{21}$ $\frac{8.5}{8.5}$ $\frac{13.2}{29}$ $\frac{17.3}{50}$

$\frac{1.6}{50}$ $\frac{4.4}{27}$ $\frac{5.8}{7}$ $\frac{7.3}{7.3}$ $\frac{13.2}{18}$ $\frac{15.8}{50}$

Nail in tree \$ 106.7 + 54

$\frac{0.6}{50}$ $\frac{2.4}{31}$ $\frac{6.4}{6.4}$ $\frac{9.3}{15}$ $\frac{12.0}{41}$ $\frac{13.3}{50}$

Spk. in 12" tree 35 ft. 54. 106.7 + 50.

$\frac{1.2}{50}$ $\frac{3.2}{30}$ $\frac{6.0}{13}$ $\frac{9.0}{9.0}$ $\frac{14.3}{24}$ $\frac{17.3}{50}$

Sta.	T	H.I.	-	Red.	Elev.
		814.97			
+09				6.7	808.3.
+50				7.1	07.9.
1069				9.3	05.7.
T.P.	4.05	809.33	7.69	805.28	
+32				6.3	803.0.
+54				14.0	795.3.
+61				13.9	95.4.
+64				13.9	795.4.
+84				5.1	804.2.
1070				5.0	04.3.
T.P.	10.50	818.11	1.72	807.61	
+54				7.3	10.8.
1071				5.8	12.3.
1072				6.4	11.7.
+50				7.5	10.4.
T.P.	2.95	813.74	7.30	810.81	
+65				5.2	08.6.
1073				5.5	08.3.
+15				6.7	07.1.
+15				7.8	06.0.

Lt $\frac{1.2}{50}$ $\frac{3.3}{24}$ 6.7 $\frac{10.6}{25}$ $\frac{14.6}{50}$ Rt.

$\frac{0.3}{50}$ $\frac{0.4}{44}$ $\frac{4.0}{23}$ 7.1 $\frac{12.2}{30}$ $\frac{14.6}{50}$

$\frac{6.6}{50}$ $\frac{8.3}{19}$ 7.3 $\frac{10.2}{18}$ $\frac{12.1}{41}$ $\frac{13.2}{50}$

$\frac{4.6}{50}$ $\frac{5.9}{24}$ 6.3 $\frac{5.4}{9}$ $\frac{6.7}{28}$ $\frac{8.4}{50}$

$\frac{6.8}{50}$ $\frac{11.1}{28}$ 13.9 $\frac{16.1}{22}$ $\frac{20.6}{38}$ $\frac{24.0}{50}$

$\frac{5.1}{50}$ $\frac{4.0}{19}$ 5.1 $\frac{8.5}{31}$ $\frac{10.7}{43}$ $\frac{13.9}{50}$

$\frac{3.8}{50}$ $\frac{3.6}{31}$ 5.0 $\frac{9.3}{34}$ $\frac{11.3}{50}$

$\frac{3.4}{50}$ $\frac{4.9}{25}$ 7.3 $\frac{9.5}{25}$ $\frac{12.7}{50}$

$\frac{2.3}{50}$ $\frac{4.0}{25}$ 5.8 $\frac{8.9}{30}$ $\frac{12.0}{50}$

$\frac{2.6}{50}$ $\frac{4.4}{25}$ 6.4 $\frac{8.3}{32}$ $\frac{10.6}{50}$

$\frac{5.5}{50}$ $\frac{6.8}{30}$ 7.5 $\frac{8.9}{20}$ $\frac{11.1}{50}$

5.2
 $\frac{1.4}{50}$ $\frac{3.4}{22}$ 5.5 $\frac{7.6}{22}$ $\frac{9.9}{50}$

Sta.	+	H.I.	-	Red.	Elev.
		813.76			
+19				7.7	806.1.
+24				5.9	07.9.
+50				5.2	08.6.
1074				5.9	07.9.
+50				6.7	07.1.
+88				7.9	05.9.
+77				9.3	04.5.
1075				10.6	03.2.
³² +08				10.1	03.7.
+14	♀. Road.			9.9	04.1.
+30				8.7	05.1.
B.M.			5.15	808.61	808.66 =
					113.28

5/24/26

Lt.

Rt.

Bottom of Ditch.

Bottom of Ditch.

$\frac{3.4}{50}$

$\frac{13.4}{50}$

803.1 = Outlet Elev. of Cross Drain Rt. 1073 + 28.

$\frac{2.3}{50}$ $\frac{4.3}{15}$ 5.2 6.4 8.5 $\frac{10.1}{44}$ $\frac{13.8}{50}$

$\frac{2.2}{50}$ $\frac{3.7}{29}$ 5.9 $\frac{8.8}{25}$ $\frac{11.2}{50}$

802.7 Outlet Elev. Cross Drain Rt. Sta. 1074 + 50. \nearrow Q. Road.

$\frac{2.7}{50}$ $\frac{4.9}{28}$ 6.7 8.5 9.9 14.4 $\frac{14.2}{40}$ $\frac{14.3}{50}$

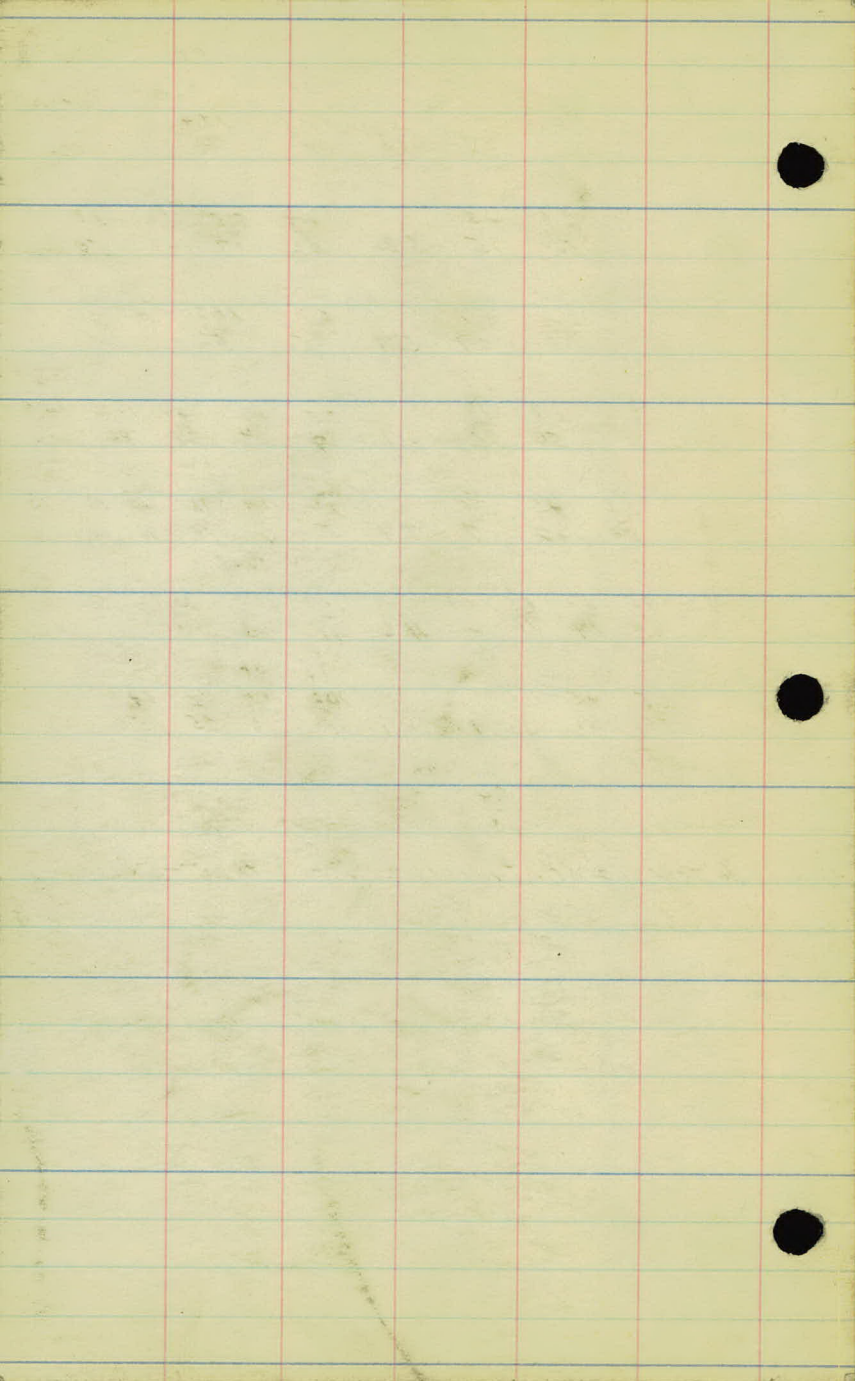
$\frac{2.2}{50}$ $\frac{4.5}{42}$ $\frac{5.6}{17}$ 7.9 9.4 11.4 11.6 11.8 12.7 $\frac{13.3}{50}$

$\frac{2.5}{50}$ $\frac{4.5}{43}$ $\frac{4.9}{29}$ $\frac{6.8}{10}$ $\frac{10.1}{4}$ 10.6 $\frac{10.8}{11}$ $\frac{11.0}{23}$ $\frac{13.7}{50}$

$\frac{2.5}{50}$ $\frac{4.5}{41}$ $\frac{6.6}{13}$ $\frac{9.6}{9}$ 10.1 $\frac{10.2}{5}$ $\frac{10.4}{14}$ $\frac{11.2}{25}$ $\frac{14.0}{50}$

$\frac{8.4}{13}$

Spk. in 50" Tree 102' Rt. Sta. 1166 Proj. #25-58.



2-9-28

RE-X-SECTIONS

PROJ. 27-52

STA. 1032+00 - 1039+00

E
GRADE G.P.

B.M.	1.95	819.00		817.05		
1032					813.3	5.7
1033					812.7	6.3
1034					812.1	6.9
	4.37	816.68	6.67	812.31		
1035					811.6	5.1
+50	INTERSECTION OF DRAW AND ROAD				811.4	5.3
	4.30	816.61	4.37	812.31		
1036					811.2	5.4
1037					811.1	5.5
1038					811.0	5.6
1039					811.0	5.6
+54	Q. of Pitch. A - 104°-47' 6" Back Tangent.				811.04	5.6
	6.54	818.85	4.30	812.31		
B.M.			1.80	817.05		

LT

E

RT

Spr. in 12" Tree 168 47 57 10 29 30. 811.5

56	57	56	69	70	54	0.3	59	72	75	66	70	64	60
100	95	21	18	15	12	5.4	15	17	21	23	54	100	150

811.8							811.4							
64	67	69	67	78	72	62	0.5	61	74	78	62	66	72	65
100	75	30	21	19	15	12	5.2	15	18	21	24	50	100	150

810.8							810.5							
81	83	76	92	92	82	70	0.3	69	83	85	75	77	76	70
100	49	23	21	17	15	12	6.4	14	17	20	23	39	100	150

810.8							809.8							
58	64	67	72	70	50	0.3	49	67	66	58	58	59	52	54
100	46	24	17	14	12	4.8	15	18	21	23	57	71	100	150

809.1							809.8							↗ Draw		
58	63	60	66	76	76	54	0.2	53	69	69	68	69	67	60	63	54
100	49	39	20	18	16	12	5.1	15	18	21	28	36	59	70	100	150

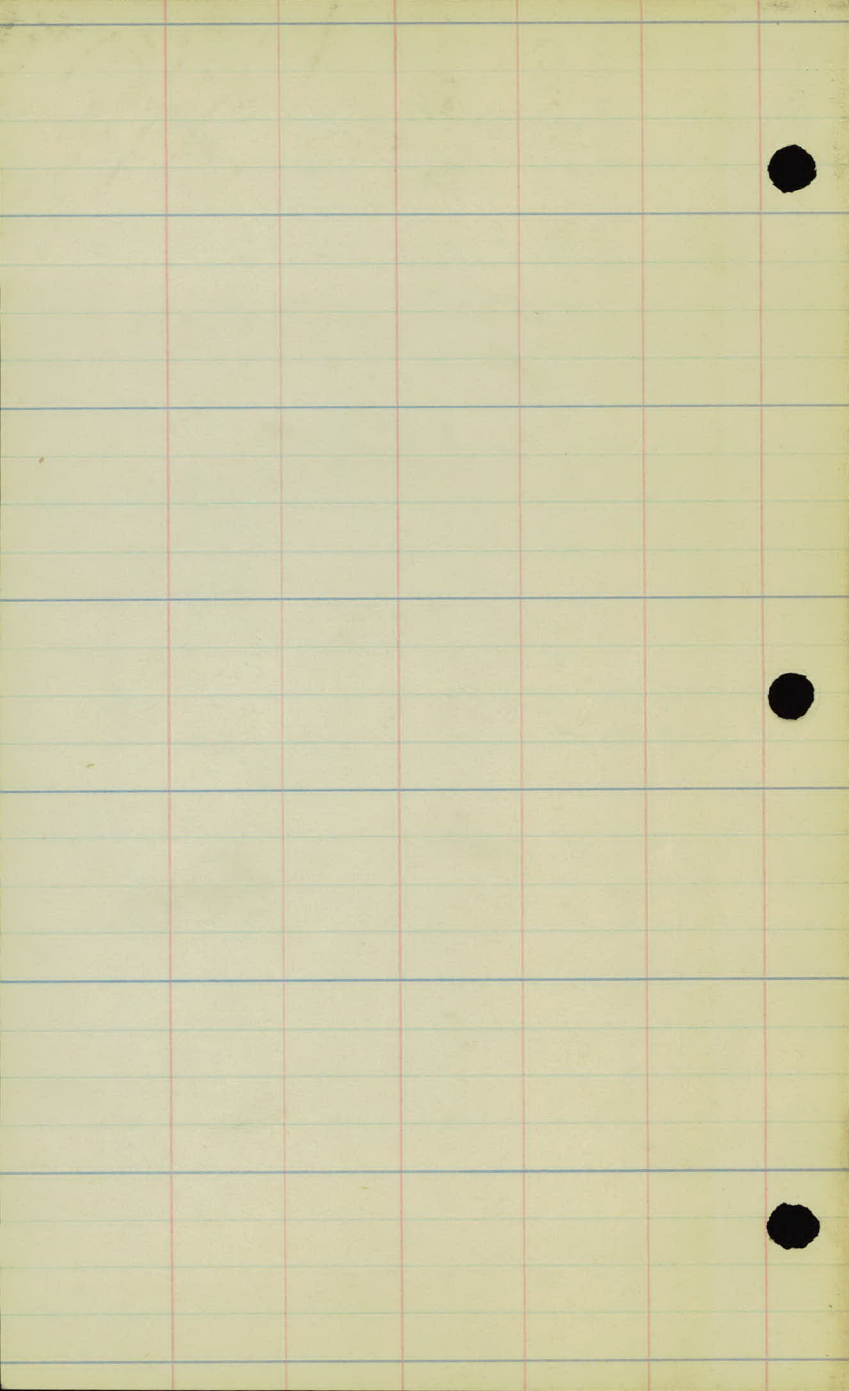
809.6							809.6							↗ Draw			
60	60	55	59	64	70	54	0.2	54	70	70	61	65	69	73	67	63	63
100	57	36	23	19	16	13	5.2	15	18	20	23	45	63	76	91	100	150

808.8							809.4							↗ Draw			
56	62	62	57	61	72	78	52	0.5	54	65	72	65	68	63	73	78	73
100	69	46	32	22	19	14	12	5.0	15	18	21	28	40	100	137	150	170

809.2							809.3							↗ top of Ice ↗ Draw				
51	59	57	74	71	51	0.4	53	72	73	60	57	63	66	70	74	85	87	88
100	52	22	19	14	11	5.0	14	18	21	25	52	100	142	200	215	230	255	266

808.9							809.6							↗ Draw				
57	60	64	77	52	54	0.9	53	68	70	66	67	68	66	67	66	85	85	89
100	59	22	19	16	12	5.4	13	17	21	25	59	100	150	200	219	250	277	300

809.7							↗ Draw						
0.6	53	55	69	68	66	68	74	76	77	79	77		
5.0	12	16	18	37	50	100	150	200	250	300	350		



02500