

PLANS SURVEY

LARPENTEUR AVE.

From Rice St. to McMenemy St.
Sta. 0+00 to Sta. 50+67.2

RAMSEY COUNTY PROJ. 27-50

Road N^o 50
File N^o 12

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed... 6-22-26

File No. 12

Road #50
Lanpentaer Ave.
Rice St. To McMenemy.
Sta-0+00 To 50+67.2
Alignment.

27-50

Lt Rt

26+00 P.O.T.

N 89°-57'E

S. 90°-03'E

142¹⁵
24+40.9 Mont P.I.

0°12'

X

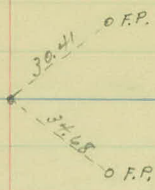
17+62.9 P.O.T.

N 89°-45'E

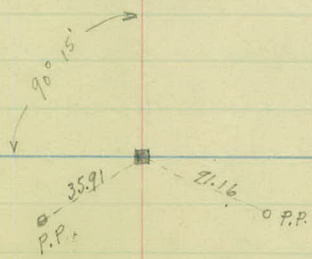
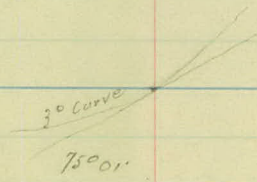
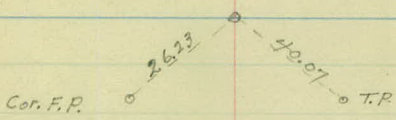
S. 90°-15'E

6+56.5 P.O.T. & 500 Track

0+00 Beg. Proj - & Rice St. Pav.

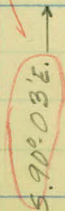


↳ Corthand. St



50+67² Mont. $\frac{1}{2}$

N 89° 57' E



5.90° 03' E.

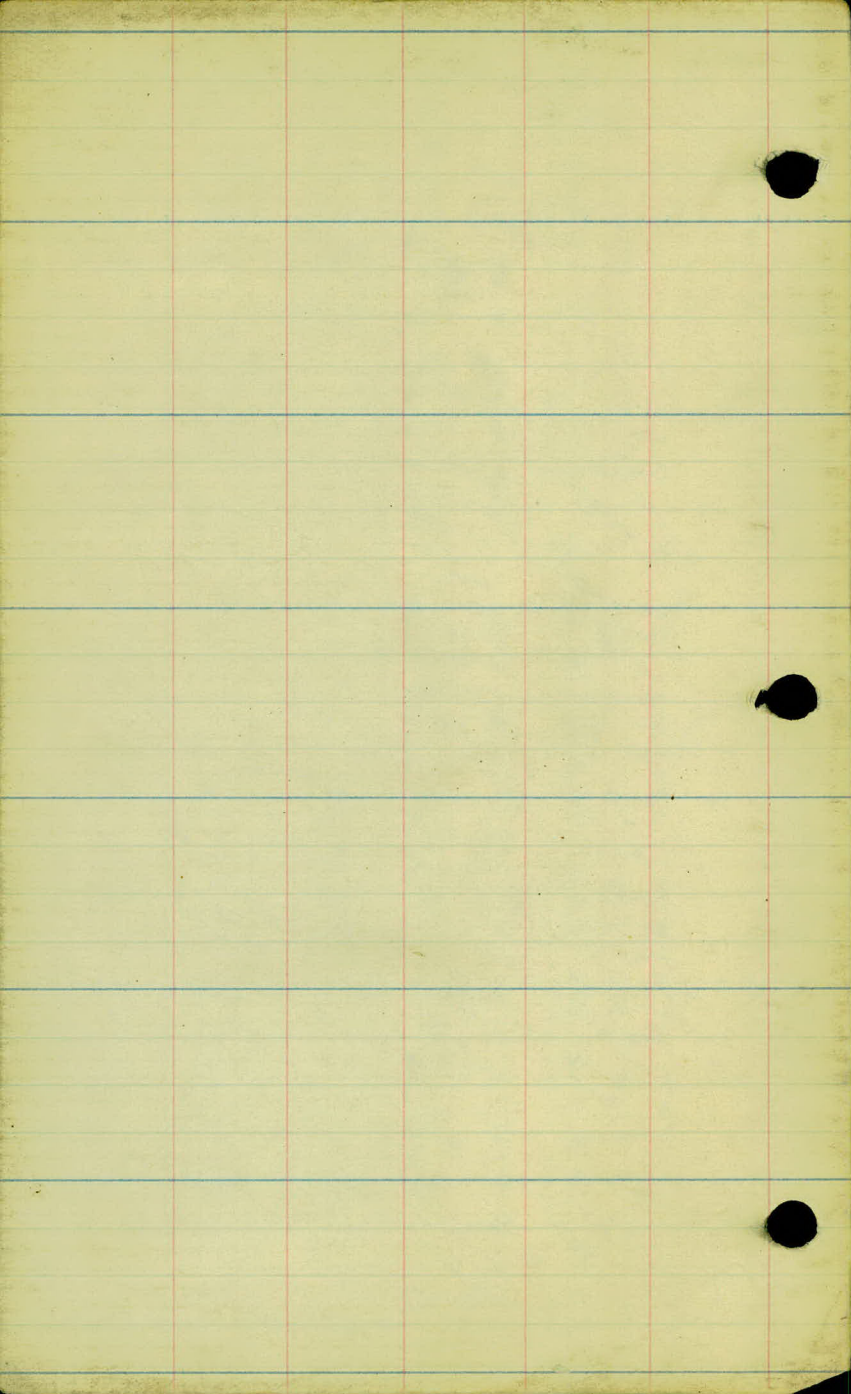
Dipe. Lt P. hamp + Rice West
865.23.

50 + 167.2
24 + 40.9

26 + 26.3

18

□ hamp 2626.37
T.P. 66.46
G.P. 50.14
42.21 G.P.



Topography:

$\frac{8}{5}$
Rd. ht Rd. Rt

150

00

2.0

2.0

1.5

2.0

2.0

+98-36" x 51.3' G.M.P. ← 25 26.2 +100
 +64 T.P. 19.5 (+95.5 - 36" x 49.4' Iron Pipe)
 +97 23 24.4 497
 +87-P.P. 17.5
 +816-P.P. 13.5

+101 T.P. 20' 64 32 5400

+10 T.P. 20 28 4200

+69 M.B. 15.5
 +53 K. Drive
 Pasture
 +39 P.P. 19.5
 Fe. 24.5 3400

+52 P.P. Danger Sign 15.5
 +40 T.P. 20'
 Cultivated
 +19 Fe. Cor. 24'
 +38 P.P. 19.5 2400

+108 M.B. 16
 +97 T.P. 20
 +62 Drive
 Garage
 +44 29.5
 30'
 6" Walk
 Cultivated land
 +99 P.P. 20' 1400

0+12 Edge. Pav.
 +26 24
 6.5 Walk
 24
 30.3
 9"
 6" Cont
 0+00

Rd. Lt. ^R Rd. Rt.

3.0

2.0

00

2.0

1.0

00

2.0

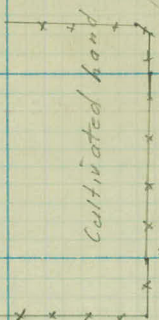
2.0

39'

12400

160 1/2 Road

+25 Fc. Cor. 30.5
+21 Fc. 21.5



+37 P.P. 18.5 (End)
←

12400

+63 T.P. 20'

+70 Fc. Cor. 25

+31 T.P. 20'
+20 (2 M.B. 18.5)
Power line Xing +20
+17 P.P. 31

100 1/2 St.

39'

40'

Cultivated hand.

+02 P.P. 18

11400

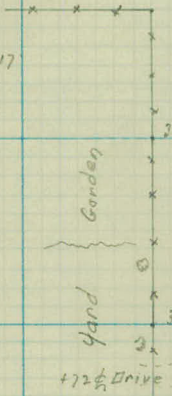
+56 R.R. Danger Sign 21.5
+51 Fc. Cor. 43

100 1/2 St.

10400

+69 Fc. Cor. 30'

+48 Hyd. 20'
+48 Valve Box 17
Water



+67 P.P. 17.5
31 --- x x x 150

9400

+91 T.P. 20'

+91 M.B. 18.5
+88 T.P. 19.5

+72 1/2 Drive

+39 P.P. 17.84

8400

Waste land.

+02 T.P. 20'
+00 Fc. Cor. 30'



+11 - P.P. 16.5
+09 - G.P. 17'
+11 Fc. Cor. 30.5

7400

+67 R.R. Xing. P. 16.7

+31 Valve Box 15.5
+13 R.R. T.P. 35'

+45 R.R. Xing. P. 13'



6400

£ £
Rd. left Rd. Pt.

8.0

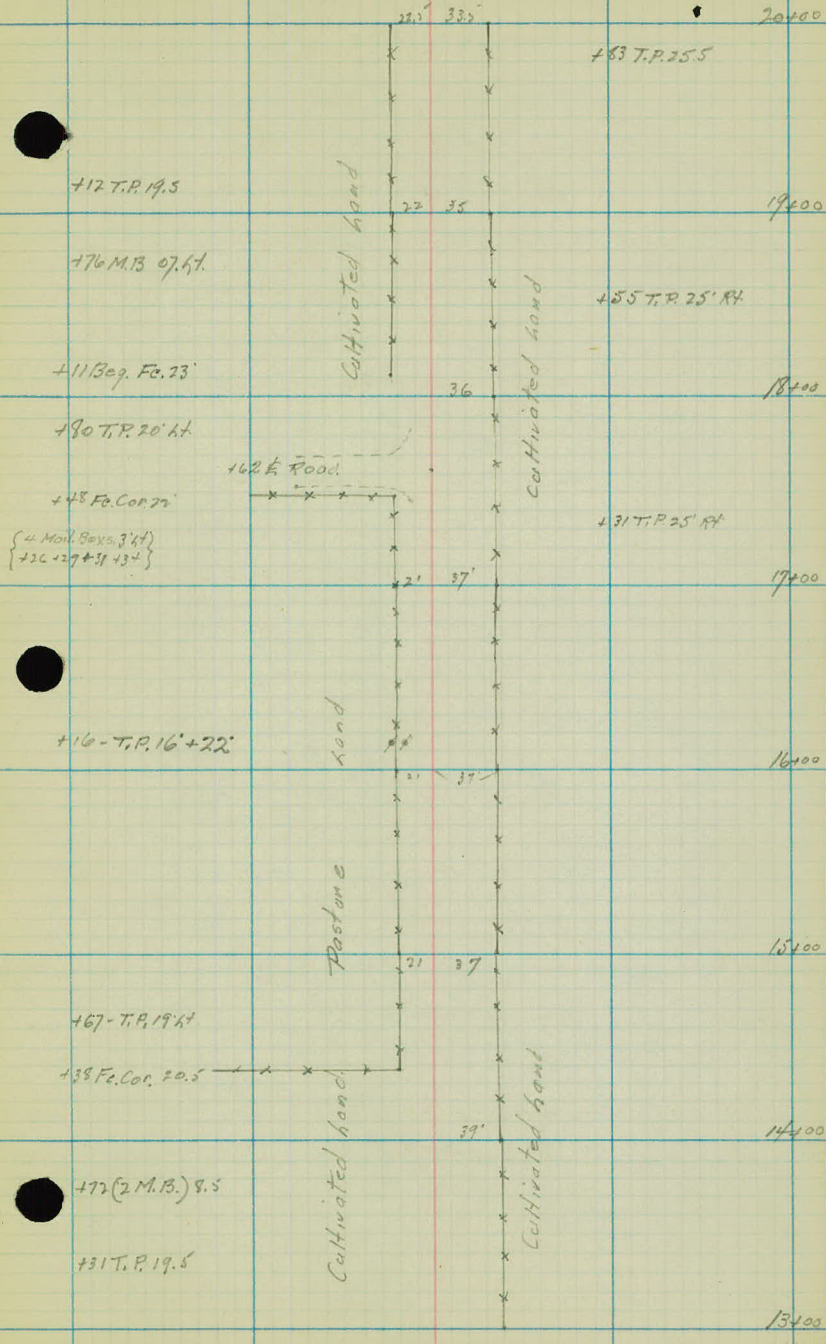
8.0

8.0

3.5

4.0

5.0



+12 T.P. 19.5

+76 M.B. 07.67

+113 eq. Fc. 23'

+90 T.P. 20' 1/2

+48 Fc. Cor. 22'

{ 4 Mail Boxes 3' 1/2 }
 { +26 +27 +31 +32 }

+16 - T.P. 16' + 22'

+67 - T.P. 19' 1/2

+38 Fc. Cor. 20.5'

+72 (2 M.B.) 8.5

+31 T.P. 19.5

Cultivated land

Cultivated land

Pasture land

Cultivated land

Cultivated land

162 E Road

+83 T.P. 25.5

+55 T.P. 25' 1/2

+31 T.P. 25' 1/2

20400

19400

18400

17400

16400

15400

14400

13400

22' 33'

22' 35'

36'

21' 37'

21' 37'

21' 37'

39'

±

Rd. H. Rd. 74

00

2.0

6.0

7.0

10.0

12.0

9.5

+87 T.P. 19'

27+00

+51+22.5 T.P.

+23 1/2 F.E.

+52 1/2 F.E.

26+00

25+00

{ +4 M.B. 09 +72 Fe. Cor. 25
+47-+69+71+72

+40.9 1/2 Cont hand. st

+66 Fe. Cor. 25

+40.9 1/2 Cont hand. st.

+02 T.P. 18.5

+00 Rd. Sign 30.5

24+00

+84 M.B. 07.

+76 T.P. 24'

+36 Fe. Cor. 26'

+12 Fe. 28.5
+07 Fe. 31

+86 T.P. 19.5



Cultivated hand

23+00

+50 T.P. 24.5

29

33

End Fence

22+00

+60 T.P. 20'

+70 Beg. Fe. 30

+07 Fe. 24' End

+20 T.P. 25'

23

34

21+00

+39 T.P. 18.5

20+00

Cultivated hand

Cultivated hand

Rd. At. ^h Rd. Rt

30

30

2.0

1.0

3.0

4.0

3.0

1.0

F-31

34+00

33+00

+29 T.P. 21

32+00

+12 T.P. 19.5

31+00

Posture land

Box hand.

176 Fe. Cor. 27'

30+00

+74 T.P. 18

+56 — +67 $\frac{1}{2}$ FE

29+00

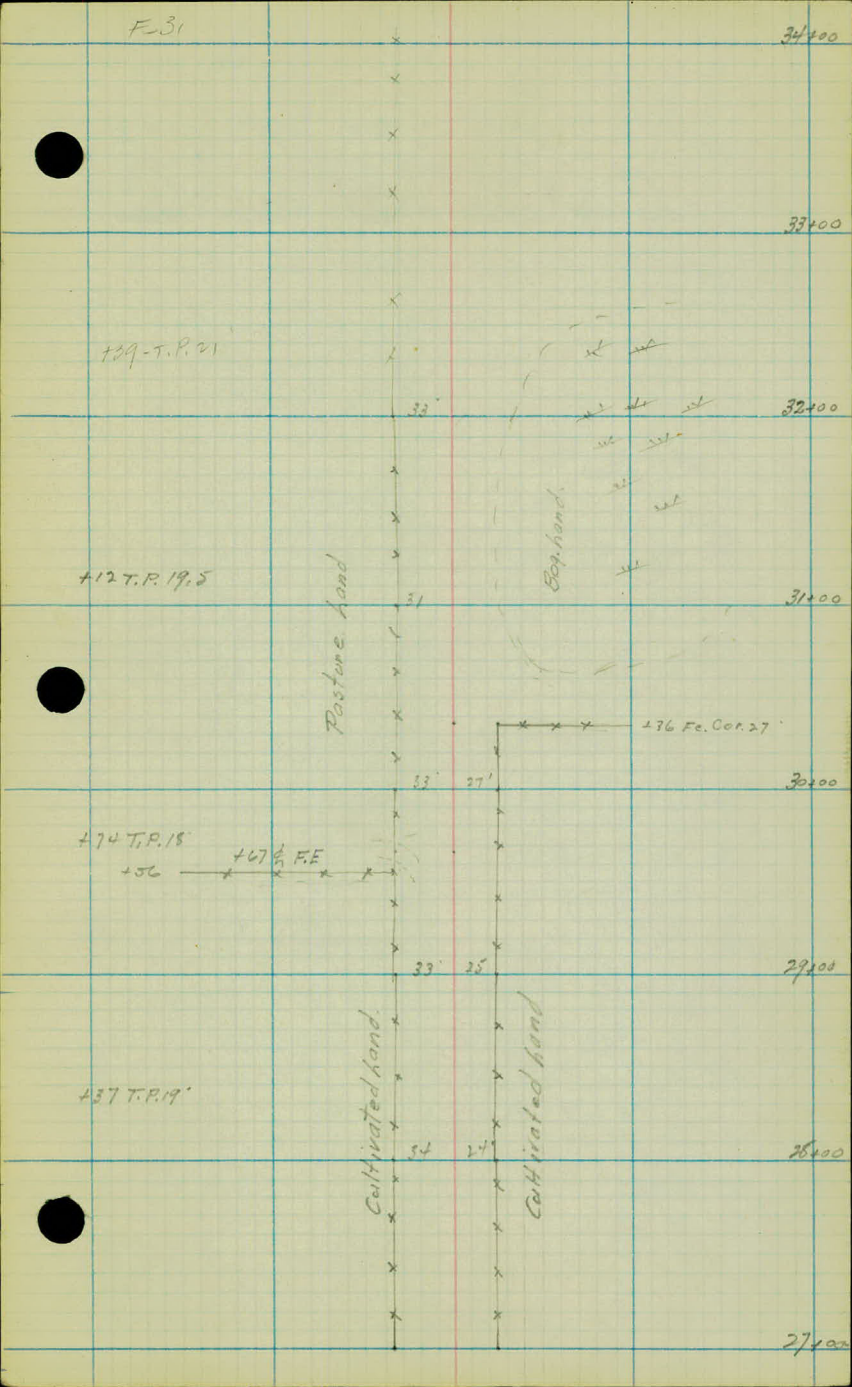
+37 T.P. 19'

Cultivated land.

Cultivated land

28+00

27+00



Rel. H. ⁵ Rel. R.

5.0

5.0

5.0

5.0

3.0

2.0

4.0

+106-T.P. 20'

40200

+120-E.F. 33'

cultivated

x
x

37100

+70-T.P. 23'
+70-T.P. 17'

cult.

38400

+58-E.Cot. 34'

x x x

+70

x
x
x
x

F 33'

37100

+90-T.P. 19'

+62 Δ F-31'
+52 Δ F-24'

x x

Pasture

F 19'

Pot Hole

x
x
x

Pot Hole
90 Willow
60 Bluffs
48'

+09-41' W. 1/2 25'

36400

+55 Δ F 33

x
x

Platted Property

+08-T.P. 20'

35100

+05-T.P. 19'

x

34100

Rt. Lt. R.A. Rt
8.0

5.0

2.0

17.0

12.0

43421 R.F. ENT LT.

8.0

2.0

E13

48400

+77- Bag Row Will 32'
+69- T.P. 21'

x
7
+
+

+19- 10" Will 32'
F-32'

+20- B.F. 12'

47400

Meadow

+40- T.P. 22'
+04- 12" Will 30'
F-30'

46400

+60- 10" Will. 30' x
+40- F.C.M. 30' x x x
+17- B.F. 30' x
+15- T.P. 20' x

45400

+06- Mississippi St.
44400

+94- T.P. 21'

43400

+69- T.P. 20'

Rubbery

+36- Group Will 28'

42400

+39- T.P. 19'

41400

Rd. L. ² Rd. R

+67.2 E Mc Menemy Road.

10.0

11.0

48481

18" X 34' V: T

5100

+80-Shoulder.

+672 Mon.

+58-Shoulder.

+52-Shoulder.

+32-F. Cor. 34' x x x
+16-T.P. 24'
F-35
+09-E. Willow 37

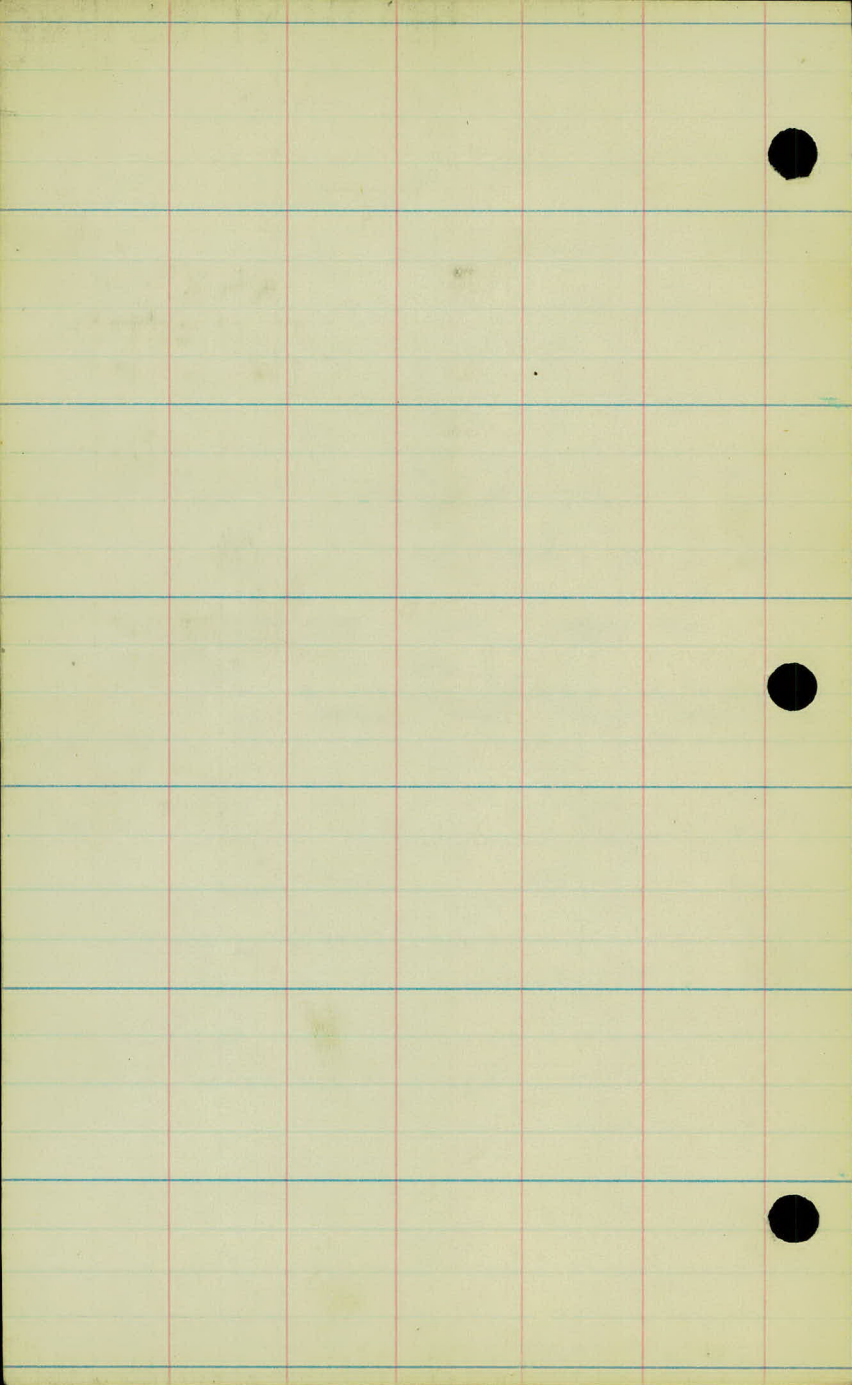
+35-F. Cor 16'
+20-G.P.B. 1'
F-13' 5000

Tree Line 37'
F-35
+96-T.P. 22'

+66-Group Will 12'
+56-Group Will 6'
+52-10' Will 8'
+48-20' Will 9'
+05-7" Tw. Will 8'
+02-6" Will 6' 4900
+8-8" Will 7'

8" 14" Willows
30' Marsh.

4600



LEVELS.

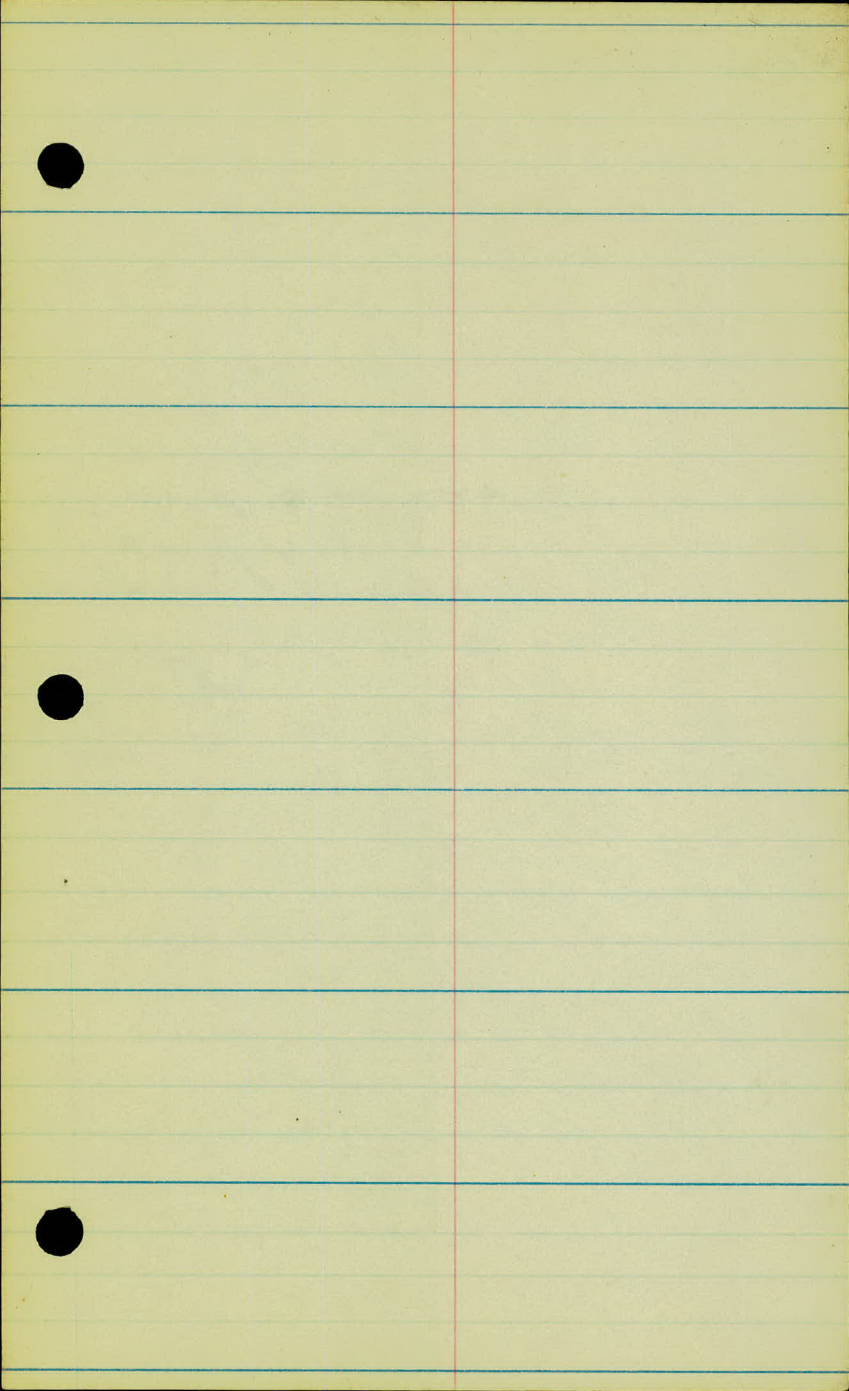
station

+

H.I

-

Elev.



station

+

H.I

-

Elev.



station

+

H.I

-

Elev.



station

+

H.I

-

Elev.

Road # 50.

Larpentuer Ave.

Rice St. to N^a Menemij St.

Sta. 0+00 to 50+67.2

X. Sections.

Sta.	T	H.I.	-	Prod.	Elev.
B.M.	2.88	848.11		845.23	
0+00				3.12	64.99
+12				3.23	64.88
+22				2.4	65.5
+27				2.5	65.6
+50				2.9	65.2
1+00				3.9	64.2
+40				4.8	63.3
2+00				6.4	61.7
+50				7.6	60.5
3+00				8.9	59.2
J.P.	0.91	858.82	10.20	857.91	
+58				1.8	57.0
4+00				3.0	55.8
+56				4.7	54.1

$\frac{3.77}{33}$ 3.12 $\frac{2.35}{33}$

$\frac{3.86}{33}$ 3.23 $\frac{2.45}{33}$

$\frac{3.6}{33}$ $\frac{3.5}{22}$ 2.4 $\frac{2.2}{15}$ $\frac{2.75}{31}$ $\frac{2.75}{33}$
on Side Walk on Pavo.

$\frac{2.4}{33}$ $\frac{2.5}{24}$ $\frac{3.5}{23}$ 2.5 $\frac{2.1}{13}$ $\frac{2.8}{29}$ $\frac{2.0}{31}$ $\frac{2.0}{33}$
on Side Walk Above H.I.

✓ $\frac{2.5}{30}$ $\frac{2.5}{24}$ $\frac{3.3}{24}$ $\frac{3.0}{13}$ 2.9 $\frac{2.9}{14}$ $\frac{3.3}{22}$ $\frac{1.7}{28}$ $\frac{1.2}{31}$ $\frac{10.4}{33}$
on Side Walk Above H.I.

✓ $\frac{2.7}{30}$ $\frac{2.8}{24}$ $\frac{3.6}{10}$ 3.9 $\frac{4.1}{14}$ $\frac{3.6}{14}$ $\frac{3.3}{19}$ $\frac{1.1}{27}$ $\frac{1.5.6}{33}$

1 $\frac{4.7}{30}$ $\frac{5.0}{19}$ $\frac{4.5}{13}$ $\frac{5.0}{10}$ 4.8 $\frac{5.2}{14}$ $\frac{4.8}{15}$ $\frac{4.2}{20}$ $\frac{2.2}{27}$ $\frac{2.1}{33}$

✓ $\frac{5.9}{33}$ $\frac{6.8}{27}$ $\frac{6.9}{20}$ $\frac{6.1}{12}$ $\frac{6.4}{11}$ 6.4 $\frac{6.8}{13}$ $\frac{6.6}{14}$ $\frac{7.5}{33}$

✓ $\frac{7.8}{33}$ $\frac{8.7}{31}$ $\frac{8.7}{25}$ $\frac{7.7}{13}$ $\frac{7.8}{11}$ 7.4 $\frac{8.2}{13}$ $\frac{7.8}{14}$ $\frac{8.7}{23}$ $\frac{9.2}{25}$ $\frac{9.8}{30}$ $\frac{10.6}{33}$

✓ $\frac{8.9}{33}$ $\frac{9.8}{30}$ $\frac{10.0}{21}$ $\frac{9.0}{11}$ $\frac{9.3}{10}$ 8.9 $\frac{9.5}{12}$ $\frac{9.3}{13}$ $\frac{10.2}{22}$ $\frac{10.5}{30}$ $\frac{12.0}{36}$

✓ Above H.I.
 $\frac{10.1}{33}$ $\frac{0.8}{25}$ $\frac{1.6}{21}$ $\frac{1.4}{13}$ $\frac{2.2}{9}$ 1.8 $\frac{1.8}{7}$ $\frac{2.4}{12}$ $\frac{2.1}{14}$ $\frac{2.8}{19}$ $\frac{2.6}{22}$ $\frac{1.9}{25}$ $\frac{2.3}{30}$ $\frac{4.3}{40}$

Above H.I.

$\frac{12.5}{33}$ $\frac{12.5}{31}$ $\frac{0.9}{25}$ $\frac{2.2}{21}$ $\frac{2.9}{18}$ $\frac{2.9}{14}$ $\frac{3.9}{11}$ $\frac{3.2}{10}$ 3.0 $\frac{3.0}{8}$ $\frac{3.5}{13}$ $\frac{3.7}{18}$ $\frac{4.3}{21}$ $\frac{4.2}{23}$ $\frac{3.5}{25}$ $\frac{3.2}{27}$ $\frac{4.6}{41}$

Above H.I.

$\frac{13.1}{40}$ $\frac{13.1}{38}$ $\frac{4.8}{21}$ $\frac{5.4}{16}$ $\frac{4.7}{11}$ 4.7 $\frac{4.7}{6}$ $\frac{5.3}{14}$ $\frac{5.6}{20}$ $\frac{6.5}{23}$ $\frac{6.5}{25}$ $\frac{4.5}{28}$ $\frac{3.8}{33}$

Sta.	+	H.I.	-	Rod.	Elev.
		858.82			
5+00				6.8	852.0 ✓
+38				8.4	50.4 ✓
T.P.	2.56	850.96 ✓	10.42	848.40 ✓	
+57				1.3	49.7 ✓
+95 ^E	Cross Drain				
+98	Cross Drain				
6+00				3.1	47.9 ✓
+30				4.0	47.0 ✓
+45				4.6	46.4 ✓
+	Top of Rail			4.73	46.23 ✓
+	Top of Rail			5.05	45.91 ✓
+75				4.8	46.2 ✓
7+00				3.8	47.2 ✓
+12				3.2	847.8 ✓

$\frac{1.2}{40}$	$\frac{1.3}{37}$	$\frac{6.6}{26}$	$\frac{6.8}{19}$	$\frac{7.1}{11}$	6.8	$\frac{7.2}{13}$	$\frac{7.7}{20}$	$\frac{8.5}{22}$	$\frac{8.5}{25}$	$\frac{4.3}{33}$	$\frac{4.4}{35}$
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$\frac{8.1}{33}$	$\frac{8.7}{34}$	$\frac{7.2}{29}$	$\frac{12.0}{26}$	$\frac{8.4}{24}$	$\frac{8.2}{13}$	$\frac{8.6}{12}$	8.4	$\frac{8.9}{10}$	$\frac{9.2}{15}$	$\frac{12.4}{21}$	$\frac{12.3}{23}$	$\frac{8.2}{28}$	$\frac{8.2}{33}$
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$\frac{6.1}{33}$	$\frac{5.7}{28}$	$\frac{1.2}{23}$	$\frac{6.1}{13}$	$\frac{1.5}{12}$	1.3	$\frac{1.5}{10}$	$\frac{5.4}{21}$	$\frac{7.0}{28}$	$\frac{7.5}{33}$
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Invert
Bottom of Ditch - 17.7
75

180
25
168
25

180
24
18.1 = Bottom of Ditch
75

165
24

$\frac{12.1}{33}$	$\frac{12.4}{25}$	$\frac{3.2}{11}$	3.1	$\frac{3.6}{4}$	$\frac{12.7}{25}$	$\frac{13.9}{33}$
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$\frac{6.5}{33}$	$\frac{5.7}{31}$	$\frac{4.3}{20}$	$\frac{3.9}{11}$	4.0	$\frac{4.2}{4}$	$\frac{10.1}{18}$	$\frac{11.3}{33}$
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$\frac{5.4}{33}$	$\frac{4.7}{10}$	4.6	$\frac{4.5}{9}$	$\frac{5.7}{19}$	$\frac{6.8}{28}$	$\frac{8.5}{33}$
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$\frac{5.22}{100}$	$\frac{4.91}{50}$	4.73	$\frac{4.84}{50}$	$\frac{5.05}{100}$
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$\frac{5.54}{100}$	$\frac{5.27}{50}$	5.05	$\frac{5.13}{50}$	$\frac{5.35}{100}$
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$\frac{5.1}{33}$	$\frac{4.2}{27}$	$\frac{4.6}{15}$	4.8	$\frac{4.9}{21}$	$\frac{5.2}{33}$
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$\frac{5.4}{33}$	$\frac{4.7}{21}$	$\frac{4.1}{17}$	3.8	$\frac{4.0}{8}$	$\frac{6.9}{20}$	$\frac{4.9}{33}$
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$\frac{5.2}{33}$	$\frac{4.6}{29}$	$\frac{3.9}{18}$	3.2	$\frac{3.8}{7}$	$\frac{6.9}{21}$	$\frac{7.3}{30}$	$\frac{4.3}{33}$
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Std.	+	H.I.	-	Red.	Elev.
		850.94			
+20				2.9	48.1
T.P.	10.94	860.72	1.20	849.74	
+75				10.3	50.4
8+00				9.3	51.4
+50				7.5	53.2
9+00				6.4	54.3
+64				5.6	55.1
+84				5.5	55.2
10+00				5.2	55.5
B.M.			2.92	857.80	
+15				4.5	56.2
+43				3.4	57.3
T.P.	9.54	869.65	0.61	860.11	
+50				11.9	59.8
11+00				8.9	60.8
+41				6.3	63.4

Above H.I.

$\frac{10.6}{33}$	$\frac{10.6}{30}$	$\frac{2.9}{34}$	$\frac{3.7}{18}$	✓	$\frac{3.4}{12}$	$\frac{6.8}{23}$	$\frac{7.4}{33}$
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$\frac{8.7}{33}$	$\frac{9.0}{30}$	$\frac{10.7}{15}$	✓	$\frac{10.9}{11}$	$\frac{11.9}{15}$	$\frac{12.2}{22}$	$\frac{14.5}{30}$	$\frac{15.0}{33}$
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$\frac{8.1}{33}$	$\frac{8.2}{30}$	$\frac{9.8}{14}$	$\frac{9.3}{9.3}$	✓	$\frac{9.6}{10}$	$\frac{8.8}{12}$	$\frac{9.6}{15}$	$\frac{9.6}{18}$	$\frac{7.5}{21}$	$\frac{7.6}{25}$	$\frac{10.0}{33}$
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$\frac{6.7}{33}$	$\frac{6.9}{30}$	$\frac{7.6}{27}$	$\frac{7.5}{7.5}$	✓	$\frac{8.0}{11}$	$\frac{7.4}{12}$	$\frac{7.0}{14}$	$\frac{3.9}{25}$	$\frac{2.6}{30}$	$\frac{3.5}{33}$
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$\frac{5.9}{33}$	$\frac{5.9}{30}$	$\frac{6.0}{17}$	$\frac{6.5}{15}$	✓	$\frac{6.7}{10}$	$\frac{5.7}{12}$	$\frac{5.0}{14}$	$\frac{0.0}{23}$	$\frac{10.5}{33}$
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Above H.I.
Above H.I.

$\frac{5.0}{33}$	$\frac{5.5}{27}$	$\frac{5.4}{5.4}$	$\frac{5.7}{11}$	$\frac{0.0}{20}$	$\frac{75.2}{30}$	$\frac{75.7}{33}$
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$\frac{5.6}{33}$	$\frac{4.9}{30}$	$\frac{5.5}{5.5}$	$\frac{6.4}{13}$	$\frac{7.5}{33}$
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$\frac{4.9}{33}$	$\frac{4.5}{14}$	$\frac{5.2}{5.2}$	$\frac{5.6}{19}$	$\frac{6.2}{23}$	$\frac{6.0}{33}$
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Top of Hycl. $\frac{12.5}{4.2}$ $\frac{9.7}{3.5}$ $\frac{4.8}{4.5}$ ✓

$\frac{4.2}{33}$	$\frac{3.5}{22}$	$\frac{4.5}{17}$	$\frac{4.5}{4.5}$	$\frac{4.9}{18}$	$\frac{5.0}{22}$	$\frac{5.1}{25}$	$\frac{4.4}{28}$	$\frac{4.6}{33}$
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$\frac{5.8}{33}$	$\frac{2.5}{23}$	$\frac{0.0}{20}$	$\frac{2.1}{14}$	$\frac{3.6}{13}$	$\frac{3.4}{3.4}$	$\frac{3.3}{13}$	$\frac{4.1}{18}$	$\frac{2.9}{19}$	$\frac{1.5}{31}$	$\frac{0.3}{33}$
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$\frac{5.3}{33}$	$\frac{4.7}{23}$	$\frac{10.8}{12}$	$\frac{12.3}{11}$	$\frac{11.9}{11.9}$	$\frac{11.7}{12}$	$\frac{12.7}{18}$	$\frac{11.3}{19}$	$\frac{8.6}{32}$	$\frac{4.0}{40}$	$\frac{2.0}{42}$	$\frac{2.0}{45}$
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$\frac{3.3}{33}$	$\frac{3.4}{19}$	$\frac{5.3}{17}$	$\frac{7.2}{12}$	$\frac{9.3}{9}$	$\frac{8.9}{8.9}$	$\frac{8.9}{11}$	$\frac{10.4}{17}$	$\frac{8.9}{20}$	$\frac{7.1}{25}$	$\frac{6.3}{33}$
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$\frac{2.7}{33}$	$\frac{2.6}{24}$	$\frac{3.3}{14}$	$\frac{5.0}{11}$	$\frac{6.5}{10}$	$\frac{6.3}{6.3}$	$\frac{6.7}{20}$	$\frac{6.1}{22}$	$\frac{5.8}{33}$	$\frac{3.2}{34}$
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Sta.	T	H.I.	-	Roof	Elev.
		869.65			
	+61			5.0	864.7 ✓
12				3.4 ✓	66.3 ✓
B.M.	11.47	880.17 ✓	0.95	868.70	
	+60			12.1	68.1 ✓
13				10.8	69.4 ✓
	+50			8.7	71.5 ✓
14				6.4	73.6 ✓
T.P.	11.94	888.94 ✓	3.19	876.98 ✓	
	+50			12.7	76.2 ✓
15				9.5	79.4 ✓
	+50			6.9	82.0 ✓
14				5.0 ✓	83.9 ✓
T.P.	4.60	891.09 ✓	4.45	884.49	
	+50			6.2	84.9 ✓
17				5.4	85.7 ✓
+62	Q. Rd. Road on Lt.			4.4	886.7 ✓

6/17/26

$\frac{2.0}{33}$	$\frac{23}{24}$	$\frac{2.6}{14}$	$\frac{4.2}{14}$	$\frac{4.6}{10}$	$\frac{5.2}{9}$	5.0	$\frac{5.5}{20}$	$\frac{4.4}{22}$	$\frac{3.6}{25}$	$\frac{3.6}{33}$
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$\frac{1.9}{33}$	$\frac{1.5}{24}$	$\frac{1.9}{18}$	$\frac{3.4}{17}$	3.4	$\frac{5.8}{14}$	$\frac{4.7}{18}$	$\frac{5.4}{33}$
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spk in P.P. Lt. Sta. 12+40

$\frac{13.4}{33}$	$\frac{13.9}{9}$	$\frac{12.3}{5}$	12.1	$\frac{13.0}{19}$	$\frac{14.2}{33}$
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$\frac{13.4}{33}$	$\frac{11.9}{13}$	$\frac{11.1}{5}$	10.8	$\frac{10.9}{19}$	$\frac{12.2}{33}$
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$\frac{11.2}{33}$	$\frac{9.2}{12}$	8.7	$\frac{8.9}{19}$	$\frac{8.4}{20}$	$\frac{8.0}{33}$
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$\frac{6.4}{33}$	$\frac{5.1}{13}$	$\frac{5.2}{12}$	$\frac{6.6}{8}$	6.6	$\frac{6.3}{15}$	$\frac{6.5}{21}$	$\frac{3.0}{24}$	$\frac{2.5}{33}$
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$\frac{10.8}{33}$	$\frac{10.4}{22}$	$\frac{9.8}{14}$	$\frac{11.6}{10}$	$\frac{12.1}{8}$	$\frac{12.9}{7}$	12.7	$\frac{12.8}{13}$	$\frac{13.1}{20}$	$\frac{11.8}{21}$	$\frac{7.0}{25}$	$\frac{6.0}{33}$
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$\frac{8.5}{33}$	$\frac{8.1}{22}$	$\frac{6.7}{6}$	$\frac{9.3}{4}$	9.5	$\frac{9.7}{13}$	$\frac{10.3}{21}$	$\frac{4.7}{29}$	$\frac{3.4}{33}$
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$\frac{7.9}{33}$	$\frac{7.4}{24}$	$\frac{5.5}{6}$	$\frac{6.6}{4}$	6.9	$\frac{6.9}{17}$	$\frac{7.5}{20}$	$\frac{3.7}{23}$	$\frac{2.7}{33}$
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$\frac{7.3}{33}$	$\frac{6.3}{23}$	$\frac{3.9}{7}$	$\frac{5.2}{6}$	5.0	$\frac{4.8}{14}$	$\frac{5.1}{21}$	$\frac{1.9}{23}$	$\frac{1.3}{33}$
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$\frac{10.8}{33}$	$\frac{9.5}{23}$	$\frac{7.6}{10}$	$\frac{6.9}{7}$	6.2	$\frac{6.0}{13}$	$\frac{6.2}{22}$	$\frac{3.4}{23}$	$\frac{2.2}{33}$
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$\frac{8.8}{33}$	$\frac{8.4}{28}$	$\frac{8.1}{24}$	$\frac{7.1}{20}$	$\frac{4.9}{5}$	$\frac{5.4}{4}$	5.4	$\frac{5.1}{13}$	$\frac{5.3}{22}$	$\frac{1.5}{30}$	$\frac{1.4}{33}$
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$\frac{5.3}{30}$	$\frac{4.8}{44}$	$\frac{4.0}{8}$	4.4
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Sta.	+	H.I.	-	Rod.	Elev.
		891.09			
	+74			4.3	86.8 ✓
	+77			4.4	86.7 ✓
18				4.7	86.4 ✓
	+50			5.6	85.5 ✓
19				8.0	83.1 ✓
	+30			9.9	81.2 ✓
20				13.2 ✓	77.9 ✓
T.P.	1.67	880.89 ✓	11.87	879.22	
	+22			3.7	77.2 ✓
	+72			5.9	75.0 ✓
21				8.0	72.9 ✓
	+47			6.8	74.1 ✓
22				5.8	75.1 ✓
	+34			1.9 ✓	878.0 ✓
T.P.	11.94	892.48 ✓	0.37	880.52	

Above H.I.

$\frac{4.1}{33}$ $\frac{3.7}{15}$ $\frac{4.3}{4.3}$ $\frac{4.2}{21}$ $\frac{12.4}{31}$ $\frac{7.0}{35}$

Above H.I.

$\frac{1.8}{33}$ $\frac{1.2}{24}$ $\frac{1.4}{17}$ $\frac{3.7}{12}$ $\frac{4.4}{4.4}$ $\frac{4.0}{19}$ $\frac{12.9}{22}$ $\frac{7.3}{33}$ $\frac{7.3}{36}$

Above H.I.

$\frac{3.7}{33}$ $\frac{3.6}{24}$ $\frac{3.6}{7}$ $\frac{4.2}{4}$ $\frac{4.7}{4.7}$ $\frac{4.4}{13}$ $\frac{4.8}{20}$ $\frac{7.5}{29}$ $\frac{7.3}{33}$

Above H.I.

$\frac{10.2}{33}$ $\frac{10.6}{27}$ $\frac{10.0}{24}$ $\frac{9.0}{22}$ $\frac{7.0}{15}$ $\frac{5.4}{6}$ $\frac{5.4}{5.4}$ $\frac{5.5}{15}$ $\frac{6.2}{21}$ $\frac{4.8}{24}$ $\frac{4.1}{27}$ $\frac{2.4}{33}$ $\frac{0.4}{34}$ $\frac{11.5}{38}$

Above H.I.

$\frac{12.1}{33}$ $\frac{12.0}{26}$ $\frac{11.0}{15}$ $\frac{7.7}{23}$ $\frac{7.9}{14}$ $\frac{7.0}{10}$ $\frac{7.4}{4}$ $\frac{8.0}{3}$ $\frac{8.0}{8.0}$ $\frac{7.6}{16}$ $\frac{8.3}{20}$ $\frac{7.1}{23}$ $\frac{6.8}{25}$ $\frac{0.0}{33}$ $\frac{7.7}{38}$

$\frac{16.3}{33}$ $\frac{16.3}{26}$ $\frac{15.3}{25}$ $\frac{14.3}{27}$ $\frac{13.2}{16}$ $\frac{9.5}{4}$ $\frac{9.9}{3}$ $\frac{9.9}{9.9}$ $\frac{9.4}{14}$ $\frac{9.9}{21}$ $\frac{8.4}{24}$ $\frac{1.5}{33}$ $\frac{0.2}{37}$

$\frac{20.0}{33}$ $\frac{19.8}{25}$ $\frac{18.5}{24}$ $\frac{15.6}{7}$ $\frac{13.5}{1}$ $\frac{13.2}{13.2}$ $\frac{12.7}{14}$ $\frac{13.0}{21}$ $\frac{12.6}{23}$ $\frac{10.7}{26}$ $\frac{9.1}{29}$ $\frac{6.6}{35}$

Above H.I.

$\frac{11.9}{33}$ $\frac{11.8}{27}$ $\frac{10.3}{25}$ $\frac{6.6}{6}$ $\frac{3.7}{3.7}$ $\frac{3.3}{15}$ $\frac{3.5}{22}$ $\frac{1.6}{25}$ $\frac{7.0.5}{29}$ $\frac{7.2.2}{35}$

$\frac{16.1}{33}$ $\frac{16.2}{28}$ $\frac{14.6}{27}$ $\frac{13.0}{21}$ $\frac{7.8}{3}$ $\frac{5.9}{5.9}$ $\frac{4.5}{3}$ $\frac{4.0}{21}$ $\frac{4.5}{23}$ $\frac{3.9}{28}$ $\frac{3.1}{35}$

$\frac{18.4}{33}$ $\frac{18.6}{29}$ $\frac{17.2}{27}$ $\frac{15.1}{18}$ $\frac{13.0}{10}$ $\frac{8.0}{8.0}$ $\frac{4.7}{4}$ $\frac{4.5}{12}$ $\frac{4.8}{21}$ $\frac{8.9}{28}$ $\frac{9.9}{35}$

$\frac{23.1}{39}$ $\frac{21.6}{31}$ $\frac{20.2}{28}$ $\frac{18.5}{23}$ $\frac{14.3}{10}$ $\frac{6.8}{6.8}$ $\frac{4.6}{3}$ $\frac{4.4}{11}$ $\frac{4.6}{18}$ $\frac{7.7}{23}$ $\frac{8.3}{29}$ $\frac{7.5}{33}$

$\frac{18.7}{34}$ $\frac{18.7}{33}$ $\frac{16.3}{29}$ $\frac{15.1}{24}$ $\frac{12.8}{11}$ $\frac{5.8}{5.8}$ $\frac{3.9}{3}$ $\frac{3.8}{11}$ $\frac{4.3}{19}$ $\frac{8.2}{25}$ $\frac{9.4}{33}$

$\frac{14.6}{34}$ $\frac{13.5}{28}$ $\frac{12.3}{22}$ $\frac{10.5}{11}$ $\frac{2.9}{2.9}$ $\frac{2.6}{10}$ $\frac{3.0}{18}$ $\frac{6.7}{24}$ $\frac{7.8}{33}$

Sta.	+	H. I.	-	Red.	Elev.
		892.48			
23				11.4	881.1 ✓
	+50			8.4	84.1 ✓
	+83			6.9	85.6 ✓
24				6.1	86.1 ✓
	+41	q. Cortland St.		3.7	88.8 ✓
	+63			3.4 ✓	88.9 ✓
B.M.	8.89	897.68	3.69	888.79	
	+84			2.2	89.5 ✓
25				7.7	90.0 ✓
	+62			6.3	91.4 ✓
26				4.8	90.9 ✓
	+60			7.9	89.8 ✓
27				9.1	88.6 ✓
	+50			11.1	886.6 ✓
	1.05	887.28	11.45	886.23	

<u>218</u>	<u>209</u>	<u>113</u>	<u>112</u>		<u>11.5</u>	<u>11.2</u>	<u>9.6</u>	<u>9.6</u>
33	25	7	4	11.4	17	23	29	33

<u>10.9</u>	<u>9.1</u>	<u>8.0</u>	<u>8.8</u>		<u>8.4</u>	<u>8.7</u>	<u>7.2</u>	<u>6.6</u>	<u>5.6</u>
33	20	4	4	8.4	11	18	28	33	36

<u>27</u>	<u>7.6</u>	<u>6.7</u>	<u>6.1</u>	<u>7.0</u>		<u>7.0</u>	<u>7.3</u>	<u>7.0</u>	<u>5.7</u>	<u>1.6</u>	<u>0.7</u>
33	30	25	7	5	6.9	14	18	28	31	35	40

<u>7.6</u>	<u>7.1</u>	<u>6.2</u>	<u>6.1</u>	<u>6.3</u>		<u>6.0</u>	<u>6.5</u>	<u>5.7</u>	<u>4.3</u>
33	29	25	18	7	6.1	9	23	28	41

<u>15.1</u>	<u>11.3</u>	<u>8.9</u>	<u>4.4</u>		<u>4.6</u>	<u>5.6</u>
100	75	50	7	3.7	5.0	100

<u>6.9</u>	<u>6.0</u>	<u>3.6</u>	<u>3.9</u>		<u>3.6</u>	<u>4.0</u>	<u>4.2</u>
33	24	10	6	3.6	11	15	33

<u>11.4</u>	<u>11.2</u>	<u>10.5</u>	<u>9.4</u>	<u>8.3</u>	<u>8.3</u>		<u>8.2</u>	<u>8.3</u>	<u>7.5</u>	<u>6.6</u>	<u>3.7</u>	<u>2.3</u>	<u>1.5</u>
33	31	27	21	13	5	8.2	8	14	16	18	21	24	33

<u>9.8</u>	<u>9.3</u>	<u>8.5</u>	<u>8.0</u>	<u>8.0</u>		<u>7.6</u>	<u>7.9</u>	<u>6.7</u>	<u>2.5</u>	<u>1.3</u>	<u>0.4</u>
33	28	24	18	8	7.7	9	13	14	23	30	33

<u>4.4</u>	<u>4.9</u>	<u>5.7</u>	<u>6.6</u>	<u>6.6</u>		<u>6.3</u>	<u>6.7</u>	<u>6.3</u>	<u>5.4</u>	<u>2.9</u>	<u>3.0</u>
33	24	21	15	11	6.3	8	14	17	24	31	33

<u>6.1</u>	<u>6.4</u>	<u>7.4</u>	<u>7.1</u>	<u>7.3</u>		<u>6.9</u>	<u>7.0</u>	<u>6.5</u>	<u>6.1</u>	<u>5.2</u>	<u>3.5</u>	<u>2.7</u>
35	33	32	13	10	6.8	11	17	19	22	24	29	33

<u>4.7</u>	<u>4.7</u>	<u>6.7</u>	<u>8.0</u>	<u>7.7</u>	<u>8.1</u>		<u>8.3</u>	<u>7.9</u>	<u>5.4</u>	<u>4.9</u>	<u>3.9</u>	<u>3.0</u>	<u>0.5</u>	<u>0.3</u>
33	32	27	23	12	11	7.9	9	14	19	20	22	25	30	33

Above HI

<u>6.9</u>	<u>7.2</u>	<u>8.9</u>	<u>9.3</u>		<u>9.5</u>	<u>8.8</u>	<u>8.6</u>	<u>2.6</u>	<u>1.6</u>	<u>1.0</u>	<u>1.8</u>
33	30	25	13	9.1	9	11	13	22	27	31	34

<u>9.9</u>	<u>10.0</u>	<u>11.4</u>	<u>11.5</u>		<u>11.5</u>	<u>10.7</u>	<u>10.4</u>	<u>3.8</u>	<u>3.1</u>	<u>1.1</u>	<u>1.5</u>
33	27	23	17	11.1	9	10	11	23	26	31	33

Sta.	+	H.I. 887.28	-	Rod	Elev.
28				3.2	884.1 ✓
	+50			5.8	81.5 ✓
29				8.5	78.8 ✓
	+60			12.3	75.0 74.9 ✓
T.P.	0.65	875.42 ✓	12.51	874.77 ✓	
30				2.1	73.3 ✓
31				5.9	69.5 ✓
32				8.7	66.7 ✓
	+28			9.9	65.5 ✓
	+70			10.8	64.6 ✓
33				11.9	63.5 ✓
	+40			13.4	62.0 ✓
T.P.	1.05	864.28 ✓	12.19	863.23 ✓	
	+75			4.3	60.0 ✓
34				5.5	858.8 ✓

Above H.I.

$\frac{5.2}{33}$	$\frac{3.1}{18}$	$\frac{5.4}{17}$	$\frac{3.2}{10}$	$\frac{3.2}{3.2}$	$\frac{3.6}{7}$	$\frac{3.2}{8}$	$\frac{0.0}{15}$	$\frac{+2.5}{21}$	$\frac{+4.1}{26}$	$\frac{+6.7}{32}$	$\frac{+6.6}{35}$
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Above H.I.

$\frac{6.8}{33}$	$\frac{5.3}{23}$	$\frac{6.6}{18}$	$\frac{5.8}{5.8}$	$\frac{6.1}{6}$	$\frac{5.0}{8}$	$\frac{+3.7}{22}$	$\frac{+4.2}{25}$	$\frac{+5.0}{27}$	$\frac{+7.2}{33}$	$\frac{+6.6}{35}$
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Above H.I.

$\frac{8.7}{33}$	$\frac{8.0}{29}$	$\frac{8.0}{27}$	$\frac{9.8}{24}$	$\frac{9.7}{20}$	$\frac{8.4}{6}$	$\frac{8.5}{8.5}$	$\frac{9.2}{7}$	$\frac{7.7}{8}$	$\frac{6.4}{11}$	$\frac{4.4}{14}$	$\frac{0.2}{22}$	$\frac{+0.8}{29}$	$\frac{+2.8}{32}$	$\frac{+2.3}{35}$
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$\frac{13.3}{33}$	$\frac{12.8}{21}$	$\frac{12.0}{15}$	$\frac{12.3}{12.3}$	$\frac{12.5}{4}$	$\frac{11.7}{7}$	$\frac{11.8}{10}$	$\frac{12.3}{13}$	$\frac{11.0}{18}$	$\frac{10.8}{26}$	$\frac{10.7}{33}$
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$\frac{6.1}{33}$	$\frac{5.8}{19}$	$\frac{2.2}{13}$	$\frac{2.3}{12}$	$\frac{2.1}{2.1}$	$\frac{2.2}{7}$	$\frac{4.7}{13}$	$\frac{5.8}{30}$	$\frac{5.3}{33}$
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$\frac{9.8}{33}$	$\frac{9.3}{14}$	$\frac{6.0}{9}$	$\frac{5.9}{5.9}$	$\frac{6.3}{8}$	$\frac{7.6}{18}$	$\frac{12.1}{33}$
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$\frac{7.5}{33}$	$\frac{7.7}{31}$	$\frac{8.9}{13}$	$\frac{8.3}{10}$	$\frac{8.9}{8}$	$\frac{8.7}{8.7}$	$\frac{8.8}{12}$	$\frac{11.3}{17}$	$\frac{12.7}{33}$
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$\frac{4.7}{33}$	$\frac{6.0}{14}$	$\frac{9.8}{8}$	$\frac{9.9}{9.9}$	$\frac{9.6}{4}$	$\frac{9.7}{14}$	$\frac{8.7}{17}$	$\frac{10.7}{33}$
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Above H.I.

$\frac{+2.4}{40}$	$\frac{+2.0}{23}$	$\frac{9.1}{15}$	$\frac{10.8}{8}$	$\frac{10.8}{10.8}$	$\frac{10.8}{12}$	$\frac{10.0}{14}$	$\frac{4.6}{25}$	$\frac{3.0}{27}$	$\frac{4.0}{33}$
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$\frac{70.5}{40}$	$\frac{70.7}{24}$	$\frac{3.5}{18}$	$\frac{10.5}{9}$	$\frac{12.1}{8}$	$\frac{11.9}{11.9}$	$\frac{12.0}{12}$	$\frac{11.0}{14}$	$\frac{9.9}{30}$	$\frac{6.5}{30}$	$\frac{0.4}{37}$	$\frac{0.5}{40}$
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Above H.I.

$\frac{70.2}{40}$	$\frac{70.1}{25}$	$\frac{6.2}{19}$	$\frac{13.4}{9}$	$\frac{13.4}{13.4}$	$\frac{13.8}{12}$	$\frac{5.8}{25}$	$\frac{2.6}{28}$	$\frac{0.3}{33}$	$\frac{0.0}{40}$
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Above H.I.

Above H.I.

$\frac{70.0}{35}$	$\frac{70.8}{24}$	$\frac{7.4}{21}$	$\frac{10}{14}$	$\frac{3.4}{12}$	$\frac{2.8}{10}$	$\frac{4.3}{4.3}$	$\frac{4.3}{12}$	$\frac{1.1}{17}$	$\frac{7.4}{24}$	$\frac{713.6}{35}$	$\frac{713.6}{37}$	$\frac{718.4}{45}$
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Above H.I.

Above H.I.

$\frac{71.8}{33}$	$\frac{71.6}{22}$	$\frac{4.5}{14}$	$\frac{6.2}{11}$	$\frac{5.5}{5.5}$	$\frac{5.8}{13}$	$\frac{1.3}{19}$	$\frac{7.2}{29}$	$\frac{7.8}{39}$
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Sta.	T	H.I.	-	Pod.	Elev.
		864.28			
+36				7.4	56.9 ✓
+76				9.3	55.0 ✓
35				10.6	53.7 ✓
B.M.	4.29	856.31	12.24	852.02	
36				5.0	51.3 ✓
37				2.1	54.7 ✓
	7.80	859.82	4.29	852.02	
+20				4.7	55.1 ✓
	9.44	866.01	3.25	856.57	
+50				10.1	55.9 ✓
38				8.6	57.4 ✓
+50				8.2	57.8 ✓
39				8.3	57.7 ✓
+50				8.5	57.5 ✓
40				7.6	58.4 ✓
+50				7.3	858.7 ✓

$\frac{6.2}{33}$ $\frac{7.1}{12}$ $\frac{7.7}{11}$ 7.4 $\frac{7.7}{13}$ $\frac{6.6}{14}$ $\frac{7.0}{18}$ $\frac{6.1}{27}$ $\frac{4.8}{32}$ $\frac{3.9}{37}$

$\frac{8.9}{33}$ $\frac{10.0}{21}$ $\frac{10.0}{9}$ 9.3 $\frac{9.3}{12}$ $\frac{9.2}{14}$ $\frac{7.0}{18}$ $\frac{11.1}{29}$ $\frac{10.0}{35}$

$\frac{11.2}{33}$ $\frac{12.6}{21}$ $\frac{12.8}{14}$ $\frac{12.2}{9}$ $\frac{11.1}{7}$ 10.6 $\frac{10.4}{12}$ $\frac{15.7}{21}$ $\frac{16.3}{33}$

Nail in P.P. H. 579. 35 + 0.9.

$\frac{15.7}{33}$ $\frac{12.4}{20}$ $\frac{11.7}{19}$ $\frac{11.0}{17}$ $\frac{9.4}{11}$ $\frac{5.5}{5}$ 5.0 $\frac{5.3}{11}$ $\frac{7.9}{14}$ $\frac{12.5}{20}$ $\frac{15.7}{33}$

$\frac{5.0}{33}$ $\frac{3.9}{27}$ $\frac{4.6}{14}$ $\frac{3.0}{12}$ $\frac{1.7}{4}$ $\frac{2.4}{5}$ 2.1 $\frac{3.6}{13}$ $\frac{3.1}{14}$ $\frac{4.1}{20}$ $\frac{3.6}{33}$

$\frac{2.3}{33}$ $\frac{2.7}{21}$ $\frac{4.9}{14}$ $\frac{4.3}{7}$ $\frac{5.0}{6}$ 4.7 $\frac{5.3}{13}$ $\frac{5.8}{18}$ $\frac{6.1}{25}$ $\frac{6.2}{26}$ $\frac{6.3}{33}$

$\frac{3.5}{33}$ $\frac{2.8}{22}$ $\frac{9.9}{13}$ $\frac{10.6}{9}$ $\frac{10.3}{5}$ 10.1 $\frac{10.8}{14}$ $\frac{11.1}{19}$ $\frac{11.0}{25}$ $\frac{12.7}{33}$

$\frac{1.5}{34}$ $\frac{1.0}{22}$ $\frac{8.8}{10}$ $\frac{9.0}{4}$ 8.4 $\frac{9.1}{15}$ $\frac{8.0}{22}$ $\frac{9.1}{26}$ $\frac{10.6}{30}$ $\frac{11.9}{34}$

$\frac{3.4}{33}$ $\frac{2.9}{17}$ $\frac{8.1}{8}$ $\frac{8.6}{4}$ 8.2 $\frac{8.3}{15}$ $\frac{8.5}{17}$ $\frac{5.9}{23}$ $\frac{7.7}{29}$ $\frac{8.9}{33}$

$\frac{10.6}{33}$ $\frac{10.3}{15}$ $\frac{9.1}{4}$ $\frac{8.3}{5}$ 8.3 $\frac{8.5}{17}$ $\frac{6.9}{22}$ $\frac{6.1}{26}$ $\frac{6.2}{33}$

$\frac{13.3}{33}$ $\frac{14.7}{25}$ $\frac{13.6}{17}$ $\frac{12.0}{10}$ $\frac{10.5}{4}$ $\frac{9.3}{4}$ $\frac{8.6}{2}$ 8.5 $\frac{8.2}{17}$ $\frac{5.9}{27}$ $\frac{5.2}{33}$

$\frac{12.3}{33}$ $\frac{11.1}{23}$ $\frac{10.5}{14}$ $\frac{8.7}{8}$ $\frac{7.7}{5}$ $\frac{7.9}{3}$ 7.4 $\frac{7.5}{14}$ $\frac{6.9}{18}$ $\frac{2.5}{26}$ $\frac{2.9}{33}$

$\frac{11.4}{33}$ $\frac{11.7}{31}$ $\frac{10.3}{21}$ $\frac{9.0}{14}$ $\frac{7.0}{8}$ $\frac{7.3}{4}$ 7.3 $\frac{7.5}{15}$ $\frac{6.8}{17}$ $\frac{7.3}{26}$ $\frac{4.2}{32}$ $\frac{4.8}{33}$

Sta.	T	H. I.	-	Red.	Elev.
		866.01			
41				8.2	857.8 ✓
+31				9.1	56.9 ✓
+67				10.1	55.9 ✓
	6.35	860.74	11.62	854.37	
42				6.2	54.5 ✓
+60				8.4	52.3 ✓
43				8.5	52.2 ✓
+37				8.2	52.5 ✓
+68				6.8	53.9 ✓
44				4.9	55.8 ✓
+65				5.5	57.2 ✓
45				1.2	859.5 ✓
	9.97	869.52	1.39	859.35	
43+48					
44					

$$\begin{array}{r} 72 \\ 33 \end{array} \frac{65}{28} \frac{5.5}{23} \frac{6.2}{18} \frac{6.9}{15} \frac{7.4}{10} \frac{8.1}{8} \quad \frac{8.3}{14} \frac{7.7}{17} \frac{4.4}{23} \frac{6.6}{33}$$

$$\frac{1.2}{33} \frac{1.8}{32} \frac{2.0}{29} \frac{3.3}{25} \frac{5.3}{21} \frac{8.3}{14} \frac{9.1}{10} \quad \frac{9.0}{7} \quad \frac{9.1}{9.1} \quad \frac{9.3}{13} \frac{8.9}{16} \frac{6.4}{21} \frac{7.5}{26} \frac{9.6}{33}$$

$$\frac{0.1}{33} \frac{0.0}{29} \frac{0.8}{23} \frac{9.1}{10} \frac{10.1}{6} \quad \frac{10.1}{10.1} \quad \frac{10.3}{12} \frac{10.0}{15} \frac{10.1}{19} \frac{14.8}{33}$$

$$\frac{0.8}{33} \frac{2.8}{24} \frac{5.3}{15} \frac{5.8}{11} \frac{6.3}{7} \quad \frac{6.2}{6.2} \quad \frac{6.6}{11} \frac{7.9}{14} \frac{11.0}{20} \frac{13.6}{33}$$

$$\frac{7.1}{33} \frac{9.1}{29} \frac{11.7}{17} \frac{8.8}{8} \frac{8.6}{5} \quad \frac{8.4}{8.4} \quad \frac{8.0}{11} \frac{10.3}{14} \frac{12.3}{19} \frac{14.0}{27} \frac{15.3}{33}$$

$$\frac{8.5}{33} \frac{9.7}{30} \frac{10.0}{22} \frac{10.4}{16} \frac{10.1}{10} \frac{8.1}{5} \frac{8.6}{4} \quad \frac{8.5}{8.5} \quad \frac{9.0}{15} \frac{10.0}{18} \frac{11.1}{25} \frac{10.5}{33}$$

$$\frac{6.2}{33} \frac{7.0}{23} \frac{7.8}{15} \frac{8.1}{4} \quad \frac{8.2}{8.2} \quad \frac{8.3}{18} \frac{8.0}{20} \frac{8.6}{23} \frac{9.2}{33}$$

$$\frac{5.6}{7} \quad 6.8 \quad \frac{7.7}{21} \quad \frac{8.3}{33}$$

$$\frac{3.3}{6} \quad 4.9 \quad \frac{5.7}{3} \quad \frac{6.3}{4} \quad \frac{6.1}{13} \quad \frac{6.7}{24} \quad \frac{6.1}{27} \quad \frac{6.8}{33}$$

$$\frac{1.5}{4} \quad 3.5 \quad \frac{4.5}{6} \quad \frac{4.4}{16} \quad \frac{5.3}{27} \quad \frac{6.7}{33}$$

$$1.3 \quad \frac{3.0}{7} \quad \frac{2.9}{18} \quad \frac{3.4}{26} \quad \frac{3.0}{33}$$

$$\frac{7.9}{33} \quad \frac{9.2}{17} \quad 15.4$$

$$\frac{3.5}{36} \quad \frac{5.9}{15} \quad 13.5$$

Sta.		H. I.	-	Prod.	27ev.
		869.32			
44	+65				
45					
45	+47			10.2	859.1 ✓
46				10.7	58.6 ✓
	+42			11.3	58.0 ✓
47				12.3	57.0 ✓
	+50			13.1	56.2 ✓
	3.09	860.03 ✓	12.38	856.94 ✓	
48				4.9	55.1 ✓
	+50			5.4	54.6 ✓
49				5.3	54.7 ✓
	9.14	864.80 ✓	4.39	855.64 ✓	
50				9.3	55.5 ✓
	+23			7.1	57.7 ✓
167 ²	Q. M. Menomy St.			6.1	858.7 ✓
B.M.			5.84	858.94 ✓	

Above H.I.

$$\begin{array}{r} 12.5 \\ 33 \end{array} \quad \begin{array}{r} 0.5 \\ 30 \end{array} \quad \begin{array}{r} 2.4 \\ 10 \end{array} \quad 12.1$$

Above H.I.

$$\begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 0.0 \\ 19 \end{array} \quad \begin{array}{r} 0.8 \\ 17 \end{array} \quad \begin{array}{r} 2.7 \\ 7 \end{array} \quad 9.8$$

$$\begin{array}{r} 11.0 \\ 33 \end{array} \quad \begin{array}{r} 9.7 \\ 23 \end{array} \quad \begin{array}{r} 7.5 \\ 12 \end{array} \quad \begin{array}{r} 8.7 \\ 7 \end{array} \quad \begin{array}{r} 9.7 \\ 4 \end{array} \quad 10.2 \quad \begin{array}{r} 9.7 \\ 13 \end{array} \quad \begin{array}{r} 10.2 \\ 22 \end{array} \quad \begin{array}{r} 9.6 \\ 24 \end{array} \quad \begin{array}{r} 8.4 \\ 34 \end{array}$$

$$\begin{array}{r} 11.9 \\ 33 \end{array} \quad \begin{array}{r} 13.1 \\ 19 \end{array} \quad \begin{array}{r} 11.5 \\ 13 \end{array} \quad \begin{array}{r} 11.0 \\ 7 \end{array} \quad 10.7 \quad \begin{array}{r} 10.7 \\ 12 \end{array} \quad \begin{array}{r} 9.9 \\ 16 \end{array} \quad \begin{array}{r} 8.7 \\ 23 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 14.1 \\ 33 \end{array} \quad \begin{array}{r} 13.1 \\ 24 \end{array} \quad \begin{array}{r} 11.6 \\ 19 \end{array} \quad \begin{array}{r} 11.9 \\ 15 \end{array} \quad \begin{array}{r} 11.5 \\ 12 \end{array} \quad 11.3 \quad \begin{array}{r} 11.5 \\ 8 \end{array} \quad \begin{array}{r} 11.0 \\ 12 \end{array} \quad \begin{array}{r} 9.2 \\ 19 \end{array} \quad \begin{array}{r} 5.7 \\ 26 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array}$$

$$\begin{array}{r} 7.1 \\ 35 \end{array} \quad \begin{array}{r} 12.2 \\ 30 \end{array} \quad \begin{array}{r} 12.3 \\ 22 \end{array} \quad \begin{array}{r} 12.7 \\ 19 \end{array} \quad \begin{array}{r} 12.3 \\ 16 \end{array} \quad 12.3 \quad \begin{array}{r} 12.5 \\ 4 \end{array} \quad \begin{array}{r} 12.0 \\ 9 \end{array} \quad \begin{array}{r} 10.5 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 31 \end{array} \quad \begin{array}{r} 2.9 \\ 36 \end{array}$$

$$\begin{array}{r} 13.0 \\ 33 \end{array} \quad \begin{array}{r} 12.9 \\ 23 \end{array} \quad \begin{array}{r} 13.2 \\ 19 \end{array} \quad \begin{array}{r} 13.0 \\ 16 \end{array} \quad 13.1 \quad \begin{array}{r} 13.4 \\ 4 \end{array} \quad \begin{array}{r} 13.1 \\ 8 \end{array} \quad \begin{array}{r} 12.9 \\ 13 \end{array} \quad \begin{array}{r} 10.6 \\ 25 \end{array} \quad \begin{array}{r} 8.8 \\ 29 \end{array} \quad \begin{array}{r} 8.6 \\ 33 \end{array}$$

$$\begin{array}{r} 5.6 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 31 \end{array} \quad \begin{array}{r} 4.3 \\ 24 \end{array} \quad \begin{array}{r} 4.4 \\ 19 \end{array} \quad \begin{array}{r} 4.4 \\ 11 \end{array} \quad 4.9 \quad \begin{array}{r} 5.9 \\ 6 \end{array} \quad \begin{array}{r} 6.9 \\ 16 \end{array} \quad \begin{array}{r} 6.5 \\ 29 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.9 \\ 33 \end{array} \quad \begin{array}{r} 4.9 \\ 24 \end{array} \quad \begin{array}{r} 4.7 \\ 19 \end{array} \quad \begin{array}{r} 4.5 \\ 12 \end{array} \quad 5.4 \quad \begin{array}{r} 7.2 \\ 7 \end{array} \quad \begin{array}{r} 8.0 \\ 11 \end{array} \quad \begin{array}{r} 8.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.5 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 24 \end{array} \quad \begin{array}{r} 4.7 \\ 19 \end{array} \quad \begin{array}{r} 4.4 \\ 11 \end{array} \quad 5.3 \quad \begin{array}{r} 7.3 \\ 4 \end{array} \quad \begin{array}{r} 9.0 \\ 10 \end{array} \quad \begin{array}{r} 8.2 \\ 33 \end{array}$$

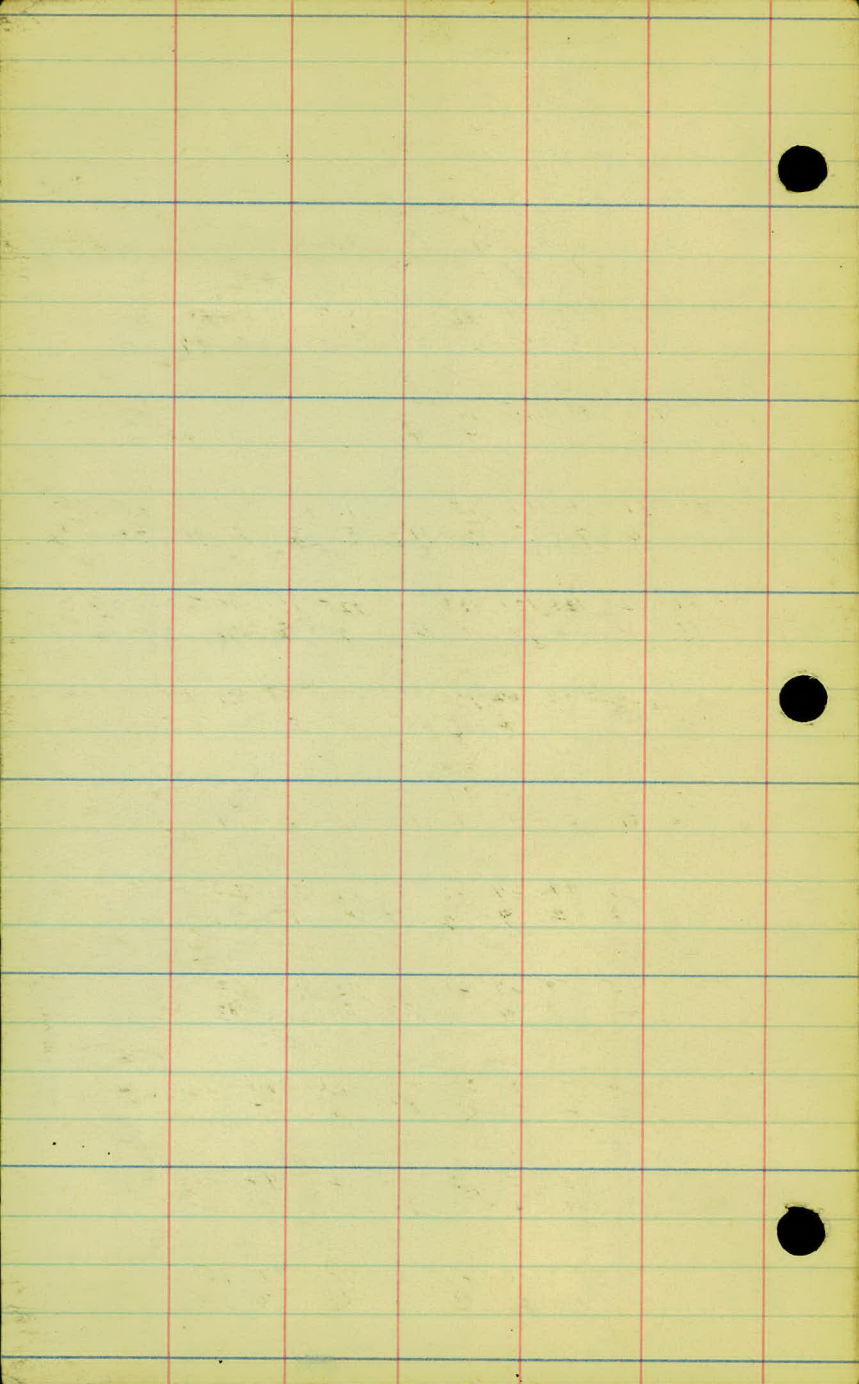
$$\begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 8.3 \\ 25 \end{array} \quad \begin{array}{r} 8.4 \\ 20 \end{array} \quad \begin{array}{r} 8.2 \\ 14 \end{array} \quad \begin{array}{r} 8.3 \\ 5 \end{array} \quad \begin{array}{r} 12.7 \\ 33 \end{array} \quad 9.3 \quad \begin{array}{r} 10.6 \\ 4 \end{array} \quad \begin{array}{r} 11.4 \\ 15 \end{array}$$

$$\begin{array}{r} 12.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 7.3 \\ 29 \end{array} \quad \begin{array}{r} 7.5 \\ 23 \end{array} \quad \begin{array}{r} 7.2 \\ 15 \end{array} \quad 7.1 \quad \begin{array}{r} 7.2 \\ 8 \end{array} \quad \begin{array}{r} 7.2 \\ 33 \end{array}$$

$$\begin{array}{r} 2.0 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array} \quad 6.1 \quad \begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 7.9 \\ 50 \end{array} \quad \begin{array}{r} 9.5 \\ 100 \end{array}$$

Sp. N. in 36 tree, 65 ft. Sp. 50 + 28.



check levels.

Sta	+	H.T	-	Elev.
B.M.	1.31	860.27		858.96
T.P.	1.50	859.97	1.80	858.47
T.P.	4.68	861.89	2.76	857.21
T.P.	12.71	868.79	5.81	856.08
T.P.	11.46	880.07	0.18	868.61
T.P.	12.79	892.73	0.13	879.94
T.B.M.	0.69	889.48	3.94	888.79
T.P.	6.28	889.58	7.18	882.30
T.P.	1.02	876.70	12.90	875.68
B.M.	8.05	876.70	8.05	868.65
T.P.	1.58	865.14	3.14	863.56
T.P.	0.46	858.21	7.39	857.75
T.P.	10.31	859.51	9.01	849.20
T.P.	10.66	870.11	0.06	859.45
B.M.			4.93	865.18 865.23

R.R. spike in 36" Co. Honwood. 65' Lt. Sta. 50178

Top Mon. S.E. cor.

R.R. spike in R.R. Lt. Sta. 12+

Top Fire Hyd Lt. Sta.

Larpenbur & Rice L.I.M. #B.

858.97

857.66

1.31

~~858.97~~

180

857.17

1.50

858.67

2.70

855.91

4.68

~~851.23~~

860.39

5.81

834.78

12.21

827.99

.18

827.31

~ Proj. 27-50 ~

~ LARPENTEUR AVENUE ~

Plans in hand inspection - 2-25-27

A.R. Van Krevelen
W. S. Mackintosh
A. O. Wilson

- ✓ 0+00 to 1+62 - Lt. - No ditch section.
- ✓ 2+70 - F.E. - Rt. - P. 15" x 24" C.M.
- ✓ 3+45 - " - Lt. - Imp. 12" x 16" V.P. - Remove - P. 15" x 24" C.M.
- ✓ 4+30 - Lt. - Walk to house - Rep. 12" x 8" V.P.
- ✓ 5+00 to 6+00 - Rt. - Cl. 1 tree.
- ✓ 5+98 - Extend double culv. with 36" C.M.
- ✓ 5+50 to 6+25 - Rt. & Lt. - Guard rail
- ✓ 7+00 to 7+60 - Rt. - Guard rail
- ✓ 7+72 - F.E. - Lt. - Imp. 12" x 20" C.M. - Remove & replace
- ✓ 8+00 - Walk - Lt. - " 12" x 10" C.M. - " " "
- ✓ About 9+70 Fire Hydrant on Lt. (Look in topoq. notes).
- ✓ No culv's. required at SYLVAN ST.
- ✓ 12+60 - F.E. - Lt. - Imp. 10" x 30" C.M. - Remove - P. 15" x 24" C.M.
- ✓ 13+00 - F.E. - Rt. - P. 15" x 24" C.M.
- ✓ 17+62 - F.E. - Lt. - No culv. req.
- ✓ 18+50 to 23+25 - Lt. - Guard rail
- ✓ 20+50 to 23+00 - Rt. - " "
- ✓ 21+00 - P. 24" P₃.
- ✓ No culverts req. at COURTLAND ST.
- ✓ 25+25 - F.E. - Lt. - No culv. req.
- ✓ 25+52 - " " - Rt. - " " "

(over)

- ✓ 29+67 - F.E. - Lt. - P. 15' X 24' C.M.
- ✓ 36+00 - P. 24" P₃.
- ✓ 34+75 to 37+00 - Rt. & Lt. - Guard rail
- ✓ 35+50 to 36+50 - Cl. 4 trees.
- 43+00 - P. 24" P₃
- 43+21 - F.E. - Lt. - P. 15' X 24' C.M.
- 42+00 to 43+00 - Cl. 6 trees
- 41+50 to 43+75 - Rt. - Guard rail
- No culv's. req. at Mississippi St.
- 48+81 - Remove culv. P. 24" P₃.
- 49+00 to 50+00 - Cl. 8 trees.

U 2499