PLANS SURVEY

COUNTY RD. "G"

From Cleveland Ave. to Rice St.
Road & C Nos 1&11

RAMSEY CO. PROJ. 27-11
File No 12

1/6/27
12

132+10.80
105+65.70
26+45.10

Cross Section

CO. RD. "G"

Rd. 9/c # 11 & 1.

From Cleveland Ave

To Centerville Road

X Sections & Center line

Levels from Sta. 0+00 to 53+00.

For Alignment see

Road Map Notes for

S.T.H. 96.

	+	H.I	−	Rod	Elev.
B.M.	3.66	917.95			914.29
0 + 00				914.5	
+ 15				14.6	
+ 50				14.5	
1 + 00				14.4	
2 + 00				13.6	
3 + 00				11.5	
4 + 00				08.9	
+ 50				07.4	
T.P.	1.90	908.67	11.18	906.77	906.77
5 + 00				06.1	
6 + 00				03.9	
7 + 00				03.5	
+ 65				04.0	
T.P.	6.74	910.31	5.10	903.57	903.57
8 + 00				04.0	

9-17-26

Lt. ℄ Rt.

U.S. Gov. B.M. Lt Sta 0+00

		3.2/100	3.4/50	3.5	4.0/50	4.5/100		
		4.3/33	3.6/15	3.4	3.6/17	4.7/33		
	3.8/33	4.5/15	3.8/12	3.5	4.5/13	5.4/17	5.1/19	5.6/33
3.9/33	4.1/19	4.4/15	4.0/13	3.6	4.5/12	5.1/15	6.2/33	
4.1/33	4.5/18	5.0/13	4.8/11	4.4	4.9/12	5.3/14	4.7/17	4.3/33
		5.5/33	6.6/11	6.5	6.9/11	7.9/16	8.0/19	4.0/33
	11.0/33	10.2/13	9.5/10	9.1	9.6/13	10.6/18	10.5/19	7.1/33
	13.0/33	12.5/19	11.2/11	10.6	11.2/12	11.9/15	11.9/17	11.4/33
4.6/33	4.9/19	4.4/16	4.2/13	3.1/10	3.6	3.0/12	5.8/19	5.5/21	5.8/33
6.4/33	6.8/25	7.5/18	5.0/12	4.8	5.4/13	8.8/21	9.9/26	10.1/33	
	11.1/33	10.6/17	5.8/11	5.2	5.6/14	9.2/21	9.5/25	9.1/33	
10.6/33	9.6/21	9.1/16	5.0/8	4.7	4.9/15	7.3/23	6.2/25	5.2/33	
Nail in T.P. Rt. Rt. 606+66								
10.7/33	9.3/21	8.6/15	7.6/12	6.6/8	6.8	6.6/15	9.2/22	9.1/23	7.3/26	5.3/33

	+	H.I.	−	Rod	Elev
		910.31			
8+32				04.1	
9+00				04.4	
+35				04.7	
10 +00				05.2	
11 +00				05.4	
12 +00				05.3	
+25				05.1	
13 +00				04.4	
14 +00				03.6	
B.M	3.84	908.47	5.46	904.65	904.63
+35				03.4	
15 +00				03.1	
+65				02.6	
16 +00				02.4	

10.6	9.5	7.2	6.5			6.6	7.5	8.4	6.3	4.0				
33	18	12	8	6.2		15	18	22	27	33				
12.1	10.4	5.4	6.3			6.0	7.6	7.6	6.6	4.4				
33	20	14	8	5.9		15	21	23	24	33				
10.3	9.3	8.7	7.4	7.3	5.9		5.7	6.0	6.7	5.9	4.7			
33	20	13	12	11	8	5.6	15	19	21	22	33			
6.0	5.3	5.0	5.6	5.3			5.4	5.9	5.3	4.3	4.0			
33	20	13	10	8	5.1		16	18	21	22	33			
2.3	2.6	5.2	5.1				5.0	5.3	4.7	3.6	3.4			
33	16	13	9	4.9			16	19	21	23	33			
5.7	4.7	5.6	5.4				5.3	5.6	3.6	3.7				
33	12	9	8	5.0			15	17	22	33				
8.2	7.0	6.1	5.7				5.6	5.9	5.0	5.4				
33	18	11	8	5.2			16	18	20	33				
12.8	12.2	10.3	7.4	6.4			6.1	6.8	7.8	7.5				
33	21	15	9	7	5.9		17	21	22	33				
9.4	9.0	7.7	7.0				6.9	6.7	7.2					
33	16	10	8	6.7			15	19	33					
Sp. in T.P. Rt. Sta 14+90														
5.3	5.4	5.9	5.4	5.3			5.3	5.2	5.6	5.6				
33	20	13	10	9	5.1		14	18	20	33				
1.2	2.2	6.2	6.5	5.9			5.6	5.8	4.8	3.9	4.5			
33	18	14	10	9	5.4		14	17	20	22	33			
1.6	0.5	6.5	7.0	6.2			6.0	6.2	2.4	2.6				
33	21	15	12	9	5.9		14	16	28	33				
2.4	1.4	6.3	6.9	6.5			6.3	6.5	6.0	5.8	4.4	5.0		
33	22	16	11	9	6.1		14	16	17	20	24	33		

	+	H.I	−	Rod.	Elev.
		908.47 ✓			
16 + 13				902.3	
+ 45				01.9	
17 + 00				01.3	
18 + 00				99.9	
T.P.	3.38	901.36 ✓	10.49	897.98 ✓	
19 + 00				98.2	
20 + 00				96.7	
21 + 00				96.4	
22 + 00				96.5	
23 + 00				97.1	
24 + 00				98.0	
T.P.	10.83	909.54 ✓	2.65	898.71 ✓	
25 + 00				99.9	
+ 32				900.9	

9-17-26

3.2/33	2.5/21	7.0/16	7.3/11	6.6/9	6.2	6.5/14	6.7/16	6.2/18	7.4/33
7.5/33	7.6/20	8.1/16	7.1/13	6.8/9	6.6	7.0/14	6.7/19	8.6/23	9.2/33
9.1/33	8.7/23	8.7/17	7.6/9		7.2	7.6/14	9.3/21	8.9/33	
9.4/33	10.3/22	10.8/17	8.7/9		8.6	8.9/12	9.5/17	13.4/28	13.7/33
4.2/33	4.7/27	5.7/20	5.4/17	3.4/10	3.2	3.5/13	6.0/21	7.5/33	
5.5/33	6.7/21	5.9/14	4.9/11		4.9	4.9/12	8.5/17	7.8/23	8.3/33
8.1/33	8.4/23	7.8/18	7.2/15	5.3/12	5.0	5.3/11	6.1/14	9.5/20	10.3/33
8.8/33	8.9/19	6.7/11	5.1/11		4.9	5.2/10	6.4/13	10.1/20	10.7/33
9.5/33	9.5/24	8.9/20	4.6/12		4.3	4.7/10	5.3/12	10.1/20	10.6/33
8.8/33	8.9/25	8.3/22	4.6/16	3.5/12	3.4	3.6/10	9.7/21	10.3/33	
10.9/33									
12.0/27	13.6/24	13.6/21	11.6/16	9.8/11	9.6	10.1/11	12.6/18	13.2/33	
8.0/33	8.2/28	12.8/22	12.4/20	9.6/15	8.9/11	8.6	9.2/11	10.7/18	10.6/33

	+		−		
		909.54			
25+49				901.5	
26+00				03.3	
	30.38 28.46 1.92				
+25				04.1	
+32				04.4	
+44.15				04.9	
B.M	8.66	913.70	4.50	905.04	905.04
+60				05.4	
+70				05.7	
27+00				06.8	
+60				08.9	
28+00				10.6	
T.P	12.03	924.59	1.14	912.56	
+50				12.6	
29+00				14.3	
B.M.			6.97	917.62 = 917.44	

9.8 10.3 12.7 12.9 9.9 8.4 8.0 8.3 9.7 8.1 9.6
33 26 22 20 16 12 10 17 19 33

11.6 12.0 11.5 7.1 6.7 6.2 6.4 7.8 10.8 11.5
33 25 21 15 11 12 16 20 33

11.1 10.8 10.2 6.2 5.7 5.4 5.7 6.2 10.0 10.5
33 26 23 17 10 11 16 23 33

6.3 6.7 5.3 5.1 5.6 6.6 10.3 9.7
33 22 10 12 16 22 33

5.3 5.2 5.0 4.6 5.2 6.7 8.0
33 16 9 8 20 33

Sp. in T.P. Lt. Sta. 26+25

11.1 9.8 8.4 8.3 8.1 13.8 13.2
42 30 8 12 20 33

13.5 13.0 9.5 8.2 8.0 8.5 13.1 13.1
33 27 20 9 12 20 33

13.9 13.3 8.0 7.8 6.9 7.2 7.8 10.2 11.2
33 21 14 8 11 15 19 33

7.0 8.0 7.8 5.8 5.0 4.8 5.0 5.3 6.5 5.4 5.2
33 27 19 14 7 9 13 19 24 33

1.7 2.2 3.9 3.9 3.3 3.1 3.3 4.0 4.2 4.2 1.2 0.7
38 21 18 11 6 8 13 15 20 24 33

5.4 5.8 13.0 12.2 12.0 12.3 12.6 6.6 5.5
33 26 17 7 10 19 25 33

3.0 3.6 11.0 10.6 10.3 10.5 13.5 8.5 4.1 3.3
33 27 18 12 9 15 20 26 33

Sp.K. in P.P. Lt. Sta. 28+44
Sp.K. in P.P. 200' Lt. Sta. 375+00 Proj #26-62

Sta	+	HI 924.59	−	Elev
29+50				915.9
30+00				17.7
+50				19.1
+70				19.5
31+00				20.2
+50				20.8
32+00				21.5
+40				21.9
33+00				22.4
+35				22.4
+75				22.8
34+00				22.9
T.P. 31+00	8.74	933.04	0.27	924.32

2.8/33 4.2/24 6.5/22 9.0/16 8.9/8 9.7 9.0/12 9.0/15 5.6/20 4.1/33

5.9/33 6.4/20 6.8/16 6.9 7.1/8 8.2/14 9.0/17 7.7/21 7.0/33

7.1/33 5.8/22 5.6/9 5.5 5.7/11 6.0/33

10.1/33 0.0/31 4.7/18 5.2/10 5.1 5.4/10 5.8/33

4.4/16 4.8/10 4.4 4.7/8 5.4/14 5.4/26 6.6/30 6.9/33

3.5/15 4.1/11 3.8 4.2/13 4.7/15 4.8/21 5.2/27 5.3/33

2.8/20 3.1/11 3.1 3.3/9 4.0/15 3.2/22

2.1/22 2.8/11 2.7 2.9/10 3.2/14 3.1/28 1.8/24

0.7/26 1.4/17 2.4/12 2.2 2.5/9 2.9/14 2.7/21

1.9/27 1.7/20 2.3/12 2.2 2.6/10 3.5/17 3.0/20 3.8/28 4.3/33

1.5/26 1.7/18 2.3/12 1.8 2.5/11 2.7/16 5.9/22 6.8/28 7.5/33

2.1/22 2.1/12 1.7 2.8/13 4.2/17 7.2/21 9.3/33

5.2/33 7.1/23

Sta	+	HI	−	Elev	
		933.06			
32+00					21.5
+40					21.9
33+00					22.4
T.P.	12.27	944.60	0.73	932.33	
31+50					20.8
32+00					21.5
+40					21.9
33+00					22.4
+35					22.4
+75					22.8
T.P.	0.24	933.69	1.15	933.45	
34+00					22.9
T.P.	4.80	927.67	10.82	922.87	
+25				923.0	
+75				923.0	

LT RT

11.6

4.0/30 3.6/33

11.2

18/31 12/39

10.7

8.9/25 8.8/33

23.8

11.1/33

23.1

5.5/44

22.7

5.4/43

22.2

5.7/42

22.2

5.4/45 8.8/38

21.8

8.7/41 13/34

10.8

2.7/36 3.7/31

1.5/33 4.3/26 5.7/23 5.0/13 4.7 5.3/11 4.6/15 11.7/21 14.3/33

4.7/33 6.4/31 6.9/26 5.6/19 5.0/14 4.7 5.4/12 12.8/22 14.7/33

St	+	H I	-	E
		922.67		
35+00				923.0
T. P	6.72	929.39	5.00	922.67
+ 50				23.1
36+00				23.4
+ 50				23.9
B.M.			5.10	924.29 = 924.26
37+00				24.2
+ 54				24.7
38+00				25.0
+ 35				25.3
39+00				25.4
+60				25.6
40+00				25.6
T. P.	11.26	940.51	0.14	929.25

Lt Ct Rt

6.8/33 7.5/31 6.9/23 5.4/19 4.6/8 4.7 5.4/11 13.0/21 14.8/33

nail in TP Pt sta 35+25

10.3/33 11.0/27 9.9/23 7.6/17 6.6/13 6.3 7.2/12 14.2/22 15.3/33

10.5/33 11.4/27 10.8/22 7.2/16 6.4/13 6.0 6.6/12 11.8/20 12.6/33

9.1/33 10.3/26 10.1/21 6.6/15 5.9/12 5.5 5.8/11 6.8/15 10.2/21 11.2/33

SPK in TP 15' Rt 34+36+65

9.7/33 9.0/22 5.8/15 5.4/11 5.2 5.8/13 9.7/19 10.1/33

4.3/33 3.8/22 5.0/19 5.0/11 4.7 5.1/11 6.2/17 6.3/33

2.7/19 4.1/12 4.4 4.8/12 4.8/25 3.4/33

2.2/19 4.1/11 4.1 4.7/13 4.7/21 2.9/33

2.5/19 4.1/12 4.0 4.4/11 4.7/15 6.4/16 10.4/33

2.0/33 2.9/23 3.8/12 3.8 4.5/12 12.2/23 14.1/33

1.8/33 3.8/12 3.8 4.3/12 12.3/24 13.9/33

STA.	+	HI	−	ELEV.	
		940.51			
38+00					25.0
T.P.	6.41	946.28	0.64	939.87	
+ 35					25.3
39+00					25.4
T.P.	1.29	934.42	13.15	933.13	
T.P.	5.46	931.32	8.56	925.86	
40+50					925.9
41+00					26.2
+ 50					26.6
42+00					26.8
+ 70					27.0
43+00					27.0
T.P.	7.03	934.94	3.41	927.91	
43					27.0
+ 50					27.4
+ 51	Cross Drain.				
44					28.0

Lt Rt

15.5

4.5/33 4.2/27

5.8/33 6.2/30 (15.2)

8.6/33 9.6/30 (15.1)

4.0/33 5.4/12 5.4 6.2/12 12.2/22 14.2/33

3.0/33 5.0/12 5.1 5.7/12 10.3/21 12.4/33

3.2/33 4.9/13 4.7 5.4/12 10.5/33

3.6/33 4.3/25 5.6/20 5.6/16 5.1/13 4.5 4.7/12 4.6/16 4.0/18 6.5/33

10.0/33 8.6/22 5.4/18 4.6/12 4.3 5.0/12 8.3/33

10.4/33 9.9/23 5.3/16 4.9/12 4.3 4.9/12 8.9/22 9.5/33

NAIL IN T.P. STA 43+25. 15' Rt.

14.1/33 13.5/24 8.8/15 7.9 8.2/12 12.6/23 13.2/33

14.6/33 14.1/27 8.4/13 7.7/11 7.5 8.0/13 13.2/24 13.7/33

Interlace = 14.9/33

14.4/33 14.3/24 7.7/14 7.2/7 6.9 7.1/8 7.8/15 12.6/23 13.4/33

Sta.	+	H.I.	−	Rod	Elev.
		934.94			
45				4.2	30.7
46				1.2	33.7
	11.02	945.83	0.13	934.81	
+30				11.1	34.7
+67				10.0	35.8
47				8.9	36.9
+75				6.3	39.5
48				5.4	40.4
+75				3.9	41.9
49				3.3	42.5
	7.50	954.20	1.13	944.70	
47+75					39.5
48					40.4
48+75					41.9
49					42.5
	5.88	950.58	7.50	944.70	

12-21-26

$\frac{11.4}{33}$ $\frac{10.7}{24}$ $\frac{4.8}{14}$ $\frac{4.4}{11}$ 4.2 $\frac{4.5}{10}$ $\frac{4.7}{12}$ $\frac{9.4}{24}$ $\frac{9.6}{31}$ $\frac{9.2}{33}$

$\frac{4.6}{33}$ $\frac{3.1}{23}$ $\frac{1.7}{14}$ 1.2 $\frac{1.3}{11}$ $\frac{0.9}{15}$ $\frac{1.7}{30}$ $\frac{0.6}{33}$

$\frac{15.0}{33}$ $\frac{12.0}{19}$ $\frac{11.4}{11}$ 11.1 $\frac{11.3}{12}$ $\frac{11.3}{17}$ $\frac{5.9}{24}$ $\frac{6.6}{33}$

$\frac{12.9}{33}$ $\frac{10.4}{14}$ $\frac{10.2}{12}$ 10.0 $\frac{10.2}{12}$ $\frac{10.4}{16}$ $\frac{4.5}{24}$ $\frac{3.6}{33}$

$\frac{8.4}{33}$ $\frac{6.7}{20}$ $\frac{9.0}{15}$ $\frac{9.0}{12}$ 8.9 $\frac{9.1}{10}$ $\frac{9.5}{15}$ $\frac{8.8}{19}$ $\frac{3.3}{27}$ $\frac{2.6}{33}$

$\frac{5.0}{19}$ $\frac{6.0}{16}$ $\frac{6.8}{14}$ $\frac{6.6}{10}$ 6.3 $\frac{6.6}{11}$ $\frac{7.5}{13}$ $\frac{7.4}{18}$ $\frac{5.1}{23}$

$\frac{5.4}{17}$ $\frac{5.9}{12}$ $\frac{5.7}{10}$ 5.4 $\frac{5.8}{12}$ $\frac{6.3}{15}$ $\frac{6.3}{19}$ $\frac{4.3}{25}$

$\frac{3.9}{16}$ $\frac{4.3}{14}$ $\frac{4.0}{10}$ 3.9 $\frac{4.3}{13}$ $\frac{4.6}{17}$ $\frac{4.3}{20}$ $\frac{2.7}{24}$ $\frac{2.0}{33}$

$\frac{2.0}{19}$ $\frac{3.0}{14}$ 3.3 $\frac{3.9}{13}$ $\frac{3.9}{16}$ $\frac{3.1}{30}$ $\frac{3.1}{33}$

$\frac{4.6}{43}$ $\frac{4.1}{33}$ $\frac{3.8}{28}$ 12.7 $\frac{4.9}{33}$ $\frac{3.7}{44}$

$\frac{4.5}{43}$ $\frac{3.3}{28}$ 11.8 $\frac{5.6}{34}$ $\frac{4.3}{43}$

$\frac{6.5}{39}$ $\frac{5.2}{24}$ 10.3

$\frac{8.3}{43}$ 9.7

Sta.	+	H.I. 950.58	−	Rod	Elev.
+50				7.2	43.4
50				6.6	44.0
+72				6.0	44.6
51				5.7	44.9
+50				5.0	45.6
52				4.3	46.3
+26				3.6	47.0
+42				3.2	47.4
+66.88	Center of Snelling Ave.			2.5	48.1
B.M.				3.61	946.97

12-22-46

10.0/33	9.4/23	7.7/13	7.2	7.6/12	8.0/18	8.2/33
10.0/33	9.3/22	7.2/12	6.6	6.9/11	6.7/18	5.2/28	5.0/33
9.3/33	8.8/20	6.6/12	6.0	6.5/12	6.0/17	5.2/33
8.0/33	8.2/20	6.2/12	5.7	6.2/11	6.9/14	7.4/25	7.4/33
7.0/33	6.7/19	5.8/12	5.0	4.7/12	7.6/18	9.3/33
7.4/33	6.4/18	4.5/13	4.3	4.6/13	9.9/21	11.6/33
8.2/33	6.9/24	4.0/19	3.6	4.8/18	9.8/27	11.7/33
7.8/40	6.9/41	3.7/32	3.6/13	3.4	3.4/21	3.9/28	10.7/33
		2.9/50	4.7/18	4.5	3.7/24	5.4/50

Spk. in P.P. Rt. Sta. 52+45.

Co. Rd. "C"
Rd. %c. # 11-1
Center line levels from
Sta. 53+00 to Sta. 212+00.

Stg.	+	H.I.	−	Rod.	Elev.
B.M.	11.54	958.51 ✓		946.97	
53				9.30	949.2
54				5.4	53.1
55				1.5	57.0
T.P.	11.67	969.92 ✓	0.26	958.25 ✓	
56				8.8	61.1
57				5.3	64.6
58				1.3	68.6
T.P.	11.74	981.37 ✓	0.29	969.63 ✓	
59				8.9	72.5
60				5.3	76.1
61				1.5	79.9
T.P.	11.67	992.67 ✓	0.37	981.00 ✓	
62				9.0	83.7
63				6.8	85.9
64				5.1	87.6
65				4.8	87.9
66				5.0	87.7
B.M.	1.20	989.32 ✓	4.55	988.12 ✓	
67				3.3	86.0
68				5.5	83.8
69				7.8	81.5
70				10.7	78.6
T.P.	0.70	978.14 ✓	11.88	977.44 ✓	
71				2.3	75.8
72				5.6	72.5
73				8.8	69.3

12-27-24

STA.	+	HI	−	Rod	ELEV.
		978.14			
74				11.8	966.3
T.P	0.76	966.31	12.59	965.55 ✓	
75				2.6	63.7
76				5.5	60.8
77				8.2	58.1
78				10.7	55.6
79				13.1	53.2
B.M.	8.39	962.47 ✓	12.21	954.10 ✓	
80				8.7	53.8
81				5.5	57.0
82.		✓		2.0	60.5
T.P	10.58	972.21	0.86	961.63 ✓	
83				7.8	64.4
84				4.5	67.7
85				0.9	71.3
T.P.	4.68	976.72 ✓	0.17	972.04 ✓	
86				3.6	73.1
87				3.4	73.3
88				4.5	72.2
89				6.5	70.2
90				8.8	67.9
91				11.0	65.7
T.P.	2.07	967.30 ✓	11.49	965.23 ✓	
92				3.9	63.4
93		✓		6.1 ✓	61.2
B.M.	4.59	967.27	4.59	962.71	962.68

12-58-2.6

Sp K. in P.P. Int. of Co. Rd. "B" & Hamline Ave.

SPK. IN T.P. RT. STA. 92+85

STA.	+	H.I.	−	Rod	ELEV.
		967.27			
94				8.7	958.6
95				11.0	956.3
T.P.	0.54	955.74	11.53	956.28	
96				1.9	53.8
97				4.5	51.2
98				7.1	48.6
99				9.5	46.2
100				10.9	44.8
T.P.	8.10	953.26	11.12	945.16	
101				7.9	45.4
102				7.6	45.7
103				6.7	46.6
104				5.5	47.8
105				3.8	49.5
B.M.	4.59	957.52	0.33	952.93	952.93
106				6.1	51.4
107				5.7	52.2
108				5.1	52.4
109				5.1	52.4
110				5.1	52.4
111				6.1	51.4
T.P.	1.06	952.81	5.77	951.75	
112				5.2	47.6
113				9.5	43.3
T.P.	0.31	941.10	12.08	940.73	
114				2.2	38.9

12-29-26

SPK. IN So. Side of T.P. 35' RT OF STA. 105+94

Sta.	+	Hi.	-	Rod	ELEV.
		941.10			
115				6.8	934.3
116				11.2	29.9
T.P.	0.29	929.22	12.17	928.93	
117				4.1	25.1
B.M.	8.98	929.20	8.98	920.24	920.22
118				8.8	20.4
T.P.	0.89	917.16	12.97	916.83	
119				1.8	15.4
120				7.0	10.2
121				11.7	05.5
T.P.	0.26	905.62	11.80	905.36	
122				3.9	901.7
123				7.6	898.0
124				11.0	94.6
T.P.	9.07	897.35	11.34	894.28	
125				4.5	92.9
126				5.0	92.4
127				4.9	92.5
128				4.5	92.9
129				2.7	94.7
T.P.	9.76	905.08	2.03	895.32	
130				7.8	97.3
131				5.3	899.8
132				2.2	902.9
B.M.	8.69	910.04	9.70	901.38	901.35

12-29-26

Spike in Stump 45' Rt Sta. 1177+60

Spike in T.P. 17' Lt. Sta 1191+00

STA.	+	H.I.	−	Rod.	ELEV.
		910.04			
133+00				4.3	905.74
134				1.6	908.44
T.P.	6.73	916.18	0.59	909.45	
135				5.6	910.58
136				5.1	911.08
137				5.2	910.98
138				4.9	911.28
139				5.4	910.78
140				5.7	910.48
T.P.	3.86	914.32	5.72	910.46	
141				3.8	910.52
142				4.4	909.92
143				5.7	908.62
144				6.3	908.02
145				6.8	907.52
B.M.	1.23	907.43	8.13	906.19	906.20
146				2.2	905.23
147				4.3	903.13
148				5.4	902.03
149				5.0	902.43
150				5.4	902.03
T.P.	2.76	905.59	4.60	902.83	
151				4.5	901.1
152				4.5	901.1
153				5.0	900.6
154				5.1	900.5

1-3-27

SPK. IN T.P. LT. of STA. 145+97 (LAKE, IMP. #57)

STA.	+	H.I.	−	Rod	ELEV.
		905.59			900.7
155				4.9	900.7
156				4.5	901.1
157				4.9	900.7 900.6
T.P.	1.97	902.68	4.88	900.71	
158				3.2	899.5
159				5.2	897.5
160				5.7	897.0
161				4.7	898.0
B.M.	10.16	911.46	1.38	901.30	
162				10.5	901.0
163				6.7	904.8
164				2.5	909.0
T.P.	10.81	921.87	0.40	911.06	
165				8.7	913.2
166				4.5	917.4
167				2.5	919.4
168				2.7	919.2
169				4.3	917.6
T.P	1.30	918.96	4.21	917.66	
170				4.1	914.9
171				7.4	911.6
172		908.83		10.7	908.3
T.P.	1.82	908.84	11.95	907.01	
173				3.2	905.6
174				5.3	903.5

1-3-27.

SPK. IN T.P. LT. of STA. 1/61+93

STA.	+	H.I. 908.84	−	Rod.	EL
175				4.0	904.8
B.M.	10.75	915.94	3.65	905.19	905.23
176				8.0	907.9
177				4.1	911.8
T.P.	9.87	925.32	0.49	915.45	
178				9.7	915.6
179				6.9	918.4
180				3.6	921.7
T.P.	8.72	932.67	1.37	923.95	924.7
181				8.0	924.6
182				5.6	927.1
183				5.2	927.5
B.M.			5.68	926.99	=927.06
184				4.8	927.9
B.M.	5.60	933.02	5.26	927.41	927.42
185				5.5	27.5
186				5.2	27.8
187				5.1	27.9
188				5.1	27.9
189				4.7	28.3
190				4.7	28.3
191				4.8	28.2
T.P.	7.21	935.35	4.88	928.14	
192				7.1	28.3
193				6.3	29.1

1-3-27.

SPK. IN T.P. 15' LT. of STA. 175+20

Spk. in 12" Oak Rt. Sta. 71+30 On. Hodgson Rd.
Proj. # 27-01 A.

SPK. IN 15" OAK LT. 02 STA. 185+17

Sta.	+	H.I. 935.35	−	Rod.	Elev
194				5.0	930.4
195				4.4	31.0
196				3.2	32.2
197				2.1	33.3
T.P.	4.86	937.94	2.27	933.08	
198				5.0	32.9
199				5.2	32.7
B.M.			3.34	934.60	
200				4.9	33.0
201				6.1	31.8
202				7.7	30.2
203				10.8	27.1
T.P.	0.78	927.44	11.28	926.66	
204				3.5	23.9
205				6.4	21.0
206				9.7	17.7
207				12.6	14.8
T.P.	0.13	916.80	10.77	916.67	
208				4.6	12.2
209				7.2	09.6
210				9.9	06.9
211				12.8	04.0
+01 45	End of Proj.			17.8	04.0
B.M.			8.82	907.98	908.00
+50				12.6	04.2
212				11.3	05.5

1-5-27

Spk. in Tree Lt. Stg. 199+85.

Spk. in Tree Lt. Stg. 209+20.

Co. Rd. "C"

Rd. % # 11 & 1.

X Sections from Sta. 53+00 to 211+01.

Stg.		Elev.
53		949.2
	+50 -2.1	951.0
54		953.1
		955.5
	+60 -1.5	951.6
55		957.0
	+50 +2.0	959.0
56		961.1
	+50 +1.9	963.0
57		964.6
	+75 -1.1	967.5
58		968.6
	+50 +2.1	970.7
59		972.5

					-0.8	-1.3	-7.8		
			-2.6	-1.1	-0.4	15	23	33	
			33	21	17				
				-5.2	-5.0	-0.1	-0.6	-7.8	-8.1
				33	19	11	15	25	33
			-0.1	-0.2	-2.3	-1.9	-0.3	-0.5	-4.4	-5.2
			33	31	24	19	12	14	24	33
		+0.7	+1.7	-1.8	-1.4	-0.3	-0.3	-2.1	-3.0	+0.5
		33	31	23	18	14	14	20	27	33
	+2.6	-1.3	-1.3	-0.9	-0.4	+0.2	-1.8	-1.4	+3.1	+3.1
	33	28	22	16	13	15	21	27	33	35
	+1.8	-0.4	-2.2	-1.4	-0.2	-0.6	-1.8	-2.3	+2.9	
	33	30	27	20	14	15	21	25	33	
	+1.0	+0.8	-1.7	-1.6	-0.4	-0.8	-1.5	-2.2	-0.6	-1.0
	33	30	24	18	12	15	18	25	27	33
	-1.1	-1.0	-1.4	-1.4	-0.6	-0.4	-2.7	-3.0		
	33	28	24	20	13	14	21	33		
		-1.0	-1.0	-0.3	-0.3	-2.5	-3.3		
		33	19	12	15	22	33		
	+0.1	+0.2	-0.7	-1.0	-0.3	-0.4	-1.4	-2.1		
	33	24	21	17	13	16	21	33		
	+4.0	+4.4	-1.0	-1.1	-0.3	-0.3	-0.3	-1.3		
	33	28	22	17	13	15	19	33		
+10.5	+10.5	+1.5	-1.1	-0.9	-0.5	-0.5	-0.8	-0.4	+5.2	+2.0
40	38	28	20	17	14	14	19	24	28	33
+10.2	+10.2	+8.0	+1.7	-0.7	-1.2	-0.3	-0.1	-1.0	-0.4	+7.3	+7.3
42	39	34	28	19	17	13	16	19	23	31	33

Sta.		Elev.
+50	-1.8	974.3.
60		976.1.
+50	+1.7	977.8.
61		979.7.
+50	+1.9	981.8.
62		983.7.
+50	+1.4	985.1.
63		985.9.
+50	+1.0	986.9.
64		987.6.
+50	+0.3	987.9.
65		987.9.
+50	+0.1	988.0.

					+7.0	
					33	
+5.5	+6.1	+0.8	-1.0	-1.1	-0.9	-0.3
33	28	22	19	16	14	12
-0.3	-0.7	-1.4	-1.4	+0.3	+6.3	
16	18	19	20	22	27	
+4.0	+4.2	-0.8	-0.5			
33	23	14	13			
-0.3	-1.3	-1.1	-0.8	+2.8	+3.2	
14	17	19	22	25	33	
+5.0	+5.0	-0.3	-0.8			
33	24	15	13			
-0.5	-0.1	+1.9	+1.6			
14	18	22	33			
+6.7	+6.9	-0.6	-0.6			
33	25	17	13			
-0.4	-0.1	+5.3	+4.7			
12	17	23	33			
+7.7	+8.4	+0.6	-0.3			
33	24	16	11			
-0.1	+0.8	+7.8	+7.0			
13	17	25	33			
+5.0	+5.1	+0.9	-0.5	-0.7		
33	25	20	17	13		
-0.7	+0.7	+2.3	+1.9			
12	16	20	33			
+2.7	+2.7	-0.4	-0.8			
33	32	19	14			
-0.8	-0.9	-0.7				
12	20	33				
+2.7	+2.5	+0.8	-0.9			
33	22	19	13			
-0.5	+0.2	-0.3				
14	21	33				
+1.2	+0.9	+0.4	-0.2			
33	19	15	11			
-0.4	-0.5	+0.1	-0.1			
11	15	18	33			
	+1.1	+0.5	-0.1			
	33	14	12			
-0.5	+0.1	+1.0	+0.6	+0.5		
12	14	19	23	33		
	+0.5	+0.5	-0.1			
	33	17	11			
-0.2	+0.3	+1.5	+2.2			
10	15	18	33			
	+0.4	+0.8	+0.1			
	33	17	13			
+0.1	+1.0	+1.4	+3.7			
12	15	20	43			
	-0.5	-1.4	-0.6			
	33	19	13			
-0.3	0.0	+1.0				
12	15	33				

Sta.		Elev.
66		987.7
	+50 -0.9	986.8.
67		986.0.
	+50 -1.0	985.0.
68		983.8.
	+50 -1.2	982.6.
69		981.5.
	+50 -1.3	980.2.
70		978.6.
	+50 -1.2	977.4.
71		975.8.
	+50 -1.7	974.1.
72		72.5.

-0.5	-1.3	-0.6
33	18	13

-0.7	-1.3	-1.1
12	19	33

+0.3	-0.7	-0.1
50	19	12

-0.2	0.0	+0.2	+0.7
12	18	24	33

+0.8	+0.4	-1.3	-0.9	-0.4
33	24	22	17	12

-0.5	-0.2	+1.8	+2.3
12	18	24	33

+1.2	+0.7	-0.8	-0.4
33	23	19	14

-0.4	+2.3	+2.7
14	23	33

+1.8	+1.6	-0.5	-0.2
33	20	17	11

-0.2	+0.8	+1.4
13	20	33

-0.9	-1.2	-0.8
33	16	12

0.0	-0.9	-0.8
13	19	33

-0.3	-0.8	-0.6
33	17	12

-0.5	-1.3	-0.9
12	16	33

-0.7	-0.5	-0.4
33	17	12

-0.6	-0.9	-0.6
12	15	33

0.0	+0.2	-0.8
33	17	14

-0.2	-0.6	+0.1	+0.2
11	15	21	33

+1.1	+3.2	-1.0
33	19	14

-0.3	+1.9	+2.7	+3.5
11	16	23	33

+3.0	+4.0	-1.1	-0.2
33	22	15	9

-0.5	+4.7	+5.8
13	21	33

+3.7	+4.4	-1.0	-0.2
33	22	15	12

-0.4	-0.8	+3.0	+4.3	+4.3
12	16	22	27	33

+1.7	+1.3	0.0	-0.2
33	20	17	12

-0.3	-0.6	-0.9	+0.8	+1.7
11	14	18	24	33

Sta.		Elev.
		971.6
+30	+2.3	
73		969.3
74		966.5
+50	-1.4	964.9
75		963.7
+50	-1.6	962.1
76		960.8
+60	-1.6	959.2
77		958.1
+50	+1.3	956.9
78		955.6
+50	-1.7	953.9
79		953.2

12-27-26

-0.1	-0.6	-1.7	-1.0	+0.7	-1.7	-1.4	-0.7	-0.3	
11	14	17	23	33	33	22	17	12	
-0.7	-1.4	-4.6	-5.3	-5.5	-6.0	-5.0	-0.6		
13	15	20	26	33	33	23	14		
-0.6	-2.6	-3.5	-2.5		-3.3	-2.4	-0.3		
12	16	24	33		33	25	13		
-0.5	-1.7	-2.8	-1.6		-3.8	-2.1	-0.2		
12	15	25	33		33	20	14		
-0.4	-1.8	-3.3	+0.2		-6.8	-6.0	-5.1	-0.8	
12	15	22	33		33	27	21	13	
-0.4	-1.2	-3.0	-0.9		-6.3	-3.7	-0.9	+0.1	
12	17	23	33		33	21	17	13	
-0.8	-2.4	-2.1	-0.4		-4.9	-3.1	-0.5		
13	18	25	33		33	21	12		
-0.5	-1.5	-1.5	-1.1		-6.0	-4.7	-4.3	-2.1	-0.7
12	17	28	33		33	25	21	19	12
-0.7	-1.1	-1.5			-1.8	-2.0	-2.1	-0.4	
13	17	33			33	23	18	13	
-0.6	-0.4	-1.3	-1.0		+1.2	0.0	-0.7	-0.7	
13	15	25	33		33	22	01	14	
-0.5	-0.3	-0.1	+0.7		+1.6	+0.7	-0.3	-0.3	
11	15	25	33		33	25	21	13	
-0.5	-0.9	-0.2	+1.0		+0.8	-0.3	-1.0	+0.1	
14	17	23	33		33	24	19	14	
-0.1	0.0	-0.5			-1.7	-0.1	-0.5		
14	24	33			33	24	15		

Sta.		Elev.
79		953.2
+19	0.2 Center of Hamline Ave.	953.0
+34	-0.1	953.1
+45	0.0	953.1
80		953.8
		955.5
+50	+1.7	955.7
81		957.0
+50	+1.6	958.6
82		960.5
+50	+1.8	962.3
+87	-0.4	964.0
83		964.4
+50	+1.8	966.2
84		967.7

$\frac{-1.2}{50.}$	$\frac{+0.5}{50}$
$\frac{-1.5}{33}$ $\frac{-0.9}{24}$	$\frac{-0.2}{17}$ $\frac{+0.2}{33}$
$\frac{-6.0}{33}$ $\frac{-2.8}{28}$ $\frac{-0.7}{18}$	$\frac{-0.1}{13}$ $\frac{-0.4}{21}$ $\frac{-0.6}{28}$ $\frac{-3.7}{33}$
$\frac{-0.8}{33}$ $\frac{-0.8}{27}$ $\frac{-0.3}{16}$	$\frac{-0.3}{11}$ $\frac{-0.4}{18}$ $\frac{-3.4}{33}$
$\frac{-2.0}{33}$ $\frac{-1.2}{26}$ $\frac{-0.4}{15}$	$\frac{-0.4}{13}$ $\frac{-1.1}{20}$ $\frac{-2.2}{33}$
$\frac{-1.3}{33}$ $\frac{-1.3}{31}$ $\frac{-0.2}{26}$ $\frac{-0.1}{15}$	$\frac{-0.6}{10}$ $\frac{-2.8}{18}$ $\frac{-4.3}{33}$
$\frac{+0.9}{33}$ $\frac{-1.0}{30}$ $\frac{-1.1}{18}$ $\frac{-0.3}{14}$	$\frac{-0.3}{9}$ $\frac{-0.3}{16}$ $\frac{-0.9}{25}$ $\frac{-1.5}{33}$
$\frac{+5.2}{38}$ $\frac{+5.2}{35}$ $\frac{+1.1}{30}$ $\frac{-0.1}{27}$ $\frac{-1.4}{18}$ $\frac{-0.5}{14}$	$\frac{-0.2}{12}$ $\frac{-1.0}{19}$ $\frac{-0.6}{25}$ $\frac{+5.0}{31}$ $\frac{+5.0}{33}$
$\frac{+3.7}{35}$ $\frac{+3.7}{32}$ $\frac{-0.9}{28}$ $\frac{-1.7}{20}$ $\frac{-0.4}{14}$	$\frac{-0.1}{9}$ $\frac{-0.7}{12}$ $\frac{-0.1}{15}$ $\frac{+7.2}{33}$ $\frac{+7.2}{35}$
$\frac{+4.5}{33}$ $\frac{+4.5}{31}$ $\frac{-0.7}{25}$ $\frac{-1.2}{18}$ $\frac{-0.7}{14}$	$\frac{-0.3}{9}$ $\frac{-0.6}{11}$ $\frac{+2.1}{23}$ $\frac{+6.7}{29}$ $\frac{+10.1}{32}$ $\frac{+10.4}{35}$
$\frac{+6.7}{33}$ $\frac{+6.6}{31}$ $\frac{+4.7}{30}$ $\frac{-0.5}{23}$ $\frac{-1.0}{17}$ $\frac{-0.5}{13}$	$\frac{0.0}{9}$ $\frac{+0.3}{12}$ $\frac{+4.3}{25}$ $\frac{+4.3}{33}$
$\frac{+3.3}{33}$ $\frac{+4.8}{30}$ $\frac{+4.3}{28}$ $\frac{+3.4}{26}$ $\frac{+0.6}{20}$ $\frac{-0.3}{13}$	$\frac{-0.3}{8}$ $\frac{+1.2}{20}$ $\frac{+5.5}{26}$ $\frac{+7.6}{33}$
$\frac{-0.6}{33}$ $\frac{+0.2}{25}$ $\frac{-0.9}{17}$ $\frac{-0.4}{13}$	$\frac{-0.5}{8}$ $\frac{-0.7}{12}$ $\frac{+0.1}{19}$ $\frac{+2.3}{33}$

Sta.		Elev.
	+50	969.9
85	-1.4	971.3
	+24 -1.0	972.1
	+54 -0.4	972.9
86		973.1
	+48 +0.2	973.3
87		973.3
	+60 +0.8	973.0
88		972.2
89		970.2
	+50 -1.1	969.1
90		967.9
	+50 -1.2	966.7

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+1.6	+0.5	-0.9	-0.2		-0.5	-0.8	+0.6		
33	26	17	12		8	19	33		
+1.9	+0.6	-0.8	-1.1	-0.4	-0.4	-1.1	+1.5	+3.7	+5.4
33	24	22	14	12	8	11	19	27	33
									+10.3
									35
+3.3	+2.0	-0.8	-0.6	-0.3	-0.2	-0.4	+0.6	+2.6	0.0 +10.1
33	30	22	14	10	9	11	14	26	31 33
+4.7	+4.6	+0.9	-0.2	-0.3	-0.4	-0.4	-0.5	+0.3	+0.5
33	23	20	17	15	11	11	27	31	33
	+6.2	+5.8	-0.6	-0.2		-0.2	-0.1	-2.6	-3.6
	33	25	17	11		11	21	30	33
+7.8	+6.2	+5.6	+1.7	+0.1	-0.2	-0.7	+7.7	+7.4	
33	29	22	19	17	13	11	22	33	
+9.1	+9.1	+5.8	+1.3	+0.4	-0.3	-0.2	+0.2	+9.5	+9.2
33	31	26	19	16	12	9	13	24	33
	-1.4	-1.4	+0.2	0.0		-0.3	-0.3	0.0	
	33	28	19	12		10	16	33	
	-2.1	-2.1	-0.9	-0.2		-0.6	-2.2	+1.9	+1.7
	33	29	21	14		11	15	26	33
		+0.9	-0.3	-0.4		0.0	-3.4	-4.8	-5.0
		33	18	12		10	22	29	33
	+3.5	+3.5	+2.7	0.0	-0.3	-0.3	+0.5	-3.0	-3.6 -3.9
	33	29	18	15	12	11	17	25	29 33
	+4.2	+4.8	+4.6	-0.5	-0.2	-0.2	+2.8	+2.0	+0.3 -0.5
	33	24	18	14	11	13	16	24	30 33
		+2.3	+3.1	-0.5	-0.3	-0.6	-0.1	+3.7	+3.5 +1.9 +3.2
		33	18	14	11	11	19	18	23 27 33

Sta.			Elev.
91			965.7
92			963.4
	+50	+1.0	962.4
93			961.2
	+50	-1.2	960.0
94			958.6
	+50	-1.2	957.4
95			956.3
	+50	-0.9	955.4
96			54.4 953.8
	+50	-1.1	53.2 952.6
97			51.8 951.2
	+31	-0.9	50.9 950.3

+4.6 +4.6 +5.2 -0.3 33 25 20 14	+0.1 +4.2 +4.9 +4.2 +4.2 12 18 25 31 33
+1.7 +1.5 +1.7 -0.8 33 25 18 15	-1.0 +5.2 +5.4 +5.2 12 19 30 33
+6.1 +5.0 -0.2 33 21 14	-0.2 +0.5 +6.7 +7.1 +8.8 +7.5 11 18 24 31 36 40
+11.3 +11.3 +10.4 +2.0 0.0 -0.4 36 31 28 23 19 13	-0.3 -0.2 +0.6 +5.7 +9.0 +12.0 +14. 8 14 20 25 26 34 40
+12.6 +13.1 +0.7 +0.1 -0.2 40 33 21 17 12	-0.5 0.0 +4.4 +10.4 +7.7 10 20 24 27 40
+8.4 +8.5 +8.1 +1.8 -0.1 -0.4 40 31 28 21 18 14	-0.4 +0.3 +9.5 +9.6 11 20 30 40
+6.0 +6.0 +6.3 -0.4 -0.3 33 31 24 19 14	-0.5 -0.1 +0.3 +3.9 +7.7 +7.8 11 18 20 22 24 38
+8.6 +7.0 +3.5 +0.9 -0.1 33 27 22 18 15	-0.5 +0.1 +2.8 +10.5 +10.5 11 19 22 33 40
+12.0 +12.0 +4.0 -0.5 -0.5 40 34 25 19 13	-0.5 -1.1 -0.7 +14.2 +13.1 10 13 17 33 40
+9.2 +10.0 +7.0 -1.0 -0.3 40 34 28 17 12	-0.6 -1.0 -1.1 +5.0 +10.5 +10.5 11 14 18 25 33 40
+7.7 +7.7 +4.6 -1.2 -0.4 34 33 27 21 13	-0.6 -1.4 -1.1 +1.2 +4.8 +8.4 +8.4 11 15 20 24 25 31 34
+4.3 +4.3 +2.0 -0.2 -0.6 35 33 28 23 15	-0.5 -0.9 -2.6 11 20 33
+0.8 +0.2 0.0 33 24 15	-0.4 -8.7 -10.0 -10.2 14 28 33 35

Sta.			Elev.
98			49.2 948.6
99			46.8 946.2
100			45.4 944.8
101			945.4.
102			945.7.
103			946.6.
104			947.8.
+50	+0.8		948.6.
105			949.5.
+65.7	Center of Lexington Ave		951.4.
106		0.0	951.4.
107			952.2.
+50	0.0		952.2.

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-11.0	-10.1	-0.5	-0.2
41	34	17	15
-11.5	-9.4	-0.5	
40	30	16	
-11.7	-10.6	-0.7	-0.3
37	31	17	14
-11.8	-10.4	-1.0	-0.3
36	30	17	14
-11.0	-9.7	-1.4	-0.5
35	30	17	13
-10.5	-9.5	-7.7	-0.8	-0.1
40	33	26	17	14
	-2.7	-1.7	-0.8	
	33	18	13	
+0.8	+0.9	-1.0	-0.3	
33	21	17	11	
0.0	-0.4	-1.0	-0.4	
33	19	17	11	
		-1.0		
		50		
+1.3	+0.5	0.0	-0.3	
33	28	21	14	
+1.0	+0.9	0.0	-0.1	-0.1
33	28	21	17	12
	0.0	+0.1	0.0	
	33	19	13	

-0.3	-1.0	-11.8	-13.3
10	14	33	38
-0.1	-0.6	-11.0	-13.3
10	14	30	40
-0.1	-0.4	-9.6	-10.8
13	15	31	40
+0.3	+0.2	-10.1	-10.7
11	15	31	40
+0.2	+0.2	-6.5	-7.2	-7.4
12	13	24	31	33
0.0	0.0	-5.6	-7.5	-5.7
11	16	25	30	40
-0.1	-1.4	-1.4		
10	15	33		
-0.2	-1.5	-0.9	+1.2	+1.4
10	14	18	27	33
-0.1	-1.0	-1.2	-1.2	
11	16	24	33	
	-0.3			
	50			
+0.1	-0.4	-0.6	+0.6	+1.3
12	16	20	22	33
-0.3	+0.3	+1.4	+1.9	
10	15	21	33	
-0.1	+0.9	+1.9	+2.6	
10	17	28	33	

Sta.		Elev.
108		952.4.
+50	+0.4	952.8.
109		952.4.
110		952.4.
+65	-0.2	952.2.
111		951.4.
+50	-1.8	949.6.
112		947.6.
+50	-2.3	945.3.
113		943.3.
+50	-2.1	941.2.
114		938.9.
+50	-2.3	936.6.

11-30-26

					-0.3	+0.5	+1.3		
					11	17	33		
		-0.5	-0.2	-0.2					
		33	23	13					
					-0.1	+0.1			
					14	33			
		-0.7	-0.5	-0.5					
		33	22	13					
					-0.4	-0.7	-0.6		
					9	14	33		
		-0.7	-0.3	0.0					
		33	22	14					
					-0.2	-0.9	-1.3	-0.8	
					11	18	23	33	
		-2.2	-2.1	-0.7					
		33	20	14					
					-0.2	-1.8	-1.5	+3.3	+4.4
					10	15	17	21	33
+1.9	+2.0	-0.1	-1.5	-1.5	-0.6				
33	30	26	23	17	14				
					-0.3	-1.5	-0.6	+10.2	+10.2
					10	14	17	29	35
+3.7	+3.7	+2.4	-1.2	-1.1	-0.3				
35	33	30	23	18	13				
					+0.2	-1.8	-1.3	+16.4	+17.2
					11	14	20	41	45
+6.0	+6.0	+4.4	-0.6	-1.3	-0.3				
35	33	30	24	17	13				
					-0.7	-1.9	-0.9	+22.4	+22.4
					11	13	20	47	55
									+24.0
									55
+7.9	+7.9	+7.0	-1.0	-5.4	-0.3				
36	33	30	21	17	14				
					-0.7	-1.4	-0.7	+4.1	+8.7	+13.0	+14.6
					10	13	18	26	39	40	51
+9.5	+9.5	+6.7	-0.8	-1.1	-0.2				
38	35	32	20	18	14				
					-0.7	-2.1	-0.5	+1.6	+5.4	+10.8	+10.0	+19.4
					11	14	19	20	28	32	46	50
+9.7	+9.7	+7.7	-0.4	-1.7	-0.2				
40	37	32	22	17	14				
					-0.4	-1.7	-0.6	+1.8	+6.5	+15.4	+15.4
					10	13	17	20	30	40	45
+11.2	+11.4	+8.3	-1.3	-1.4	-0.3	-0.4			
45	37	33	20	17	15	13			
					-0.3	-1.6	-1.0	+11.8	+12.0
					11	14	21	35	38
+9.0	+9.0	+6.3	-0.9	-1.0	-0.6				
38	35	33	22	14	14				
					-0.8	-1.5	-1.4	+11.1	+11.1
					14	15	23	36	40
+6.5	+6.5	+4.3	-1.3	-1.4	-0.8	-0.5			
40	34	32	24	21	14	13			

Sta.	Elev.
115	934.3
+50 -21	932.2
116	929.9
+50 -22	927.7
117	925.1
+42 -21	923.0
118	920.4
119	915.4
120	910.2
121	905.5
122	901.7
123	898.0
124	894.6

+6.8	+4.8	+1.4	-0.9	-1.1	-0.5	-0.6	-2.0	-0.9	+0.4	+7.9	+8.0
37	35	29	25	20	15	11	14	20	23	33	35
+9.0	+9.0	+7.3	+1.1	-1.7	-0.5	-0.3	-1.6	-1.6	+0.4	+6.0	+6.8
37	35	34	27	23	16	10	13	17	22	30	35
+9.0	+8.8	+5.5	+2.2	-1.5	-0.5	-0.5	-1.0	-0.2	+2.1	+7.6	+7.3
40	36	33	28	22	16	10	14	20	23	30	35
+6.2	+5.8	+2.9	-1.2	-0.8		-0.3	-1.2	-1.0	+5.7	+5.2	
40	33	29	22	15		10	14	17	25	33	
+2.0	+0.7	-0.4	-1.6	-0.8	-0.2	-0.2	-1.2	+2.7	+3.0	+3.0	
33	30	29	24	19	16	12	15	18	22	33	
	-2.1	-2.1	-1.3	-0.4		0.0	-0.2	-0.8	-0.9	-1.0	
	33	33	22	17		10	14	18	27	33	
	-8.4	-8.2	-1.0	-0.2		-0.2	-8.1	-8.6			
	35	33	21	19		13	28	35			
		-15.0	-14.4	-0.2		-0.1	-18.1	-19.3			
		48	42	18		11	37	46			
		-15.6	-14.8	-0.3		+0.1	-16.2	-18.0			
		50	41	15		11	42	50			
		-12.6	-11.6	-11.0	-0.1	+0.1	-15.8	-17.0			
		50	38	36	14	12	38	50			
			-7.5	-10.8	-0.3	-0.3	-14.0	-14.2			
			50	30	15	12	33	50			
			-8.2	-7.2	+0.1	-0.6	-9.3	-11.6			
			30	30	14	15	31	50			
			-5.4	-5.4	-4.2	-0.6	-0.3	-4.0	-4.4	-6.1	-8
			33	31	20	13	11	18	24	33	40

Sta.		Elev.
125		892.9
126		892.4
127		892.5
+50	+0.3	892.8
128		892.9
+50	+0.6	893.5
129		894.7
+50	+1.4	896.1
130		897.3
+50	+1.0	898.3 898.0
131		899.8
+50	+1.7	901.5
132		902.9

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				-0.7	-4.5	-4.8	-4.8
				11	17	21	33
				-0.6	-3.8	-4.0	-4.2
				11	17	25	33
				-0.6	-3.2	-3.7	-3.7
				12	17	24	33
				-0.6	-2.6	-3.2	-3.2
				12	18	26	33
				-0.3	-2.9	-3.0	-3.0
				11	16	24	33
				-0.8	-3.3	-3.2	-3.2
				11	16	27	33
				-0.3	-2.5	-3.9	-3.9
				10	18	27	33
				-0.7	-4.5	-5.0	-5.0
				12	18	26	33
				-0.8	-4.0	-6.3	-6.1
				11	15	23	33
				-0.4	-6.6	-7.2	-7.2
				10	21	27	33
				-0.3	-4.6	-5.8	-6.6
				10	18	24	33
				-0.4	-2.8	-4.2	-4.6
				12	19	24	33
				-0.2	+0.2	-1.6	
				12	17	33	

		-3.7	-3.8	-0.8			
		33	18	13			
		-0.7	-2.1	-2.6	-0.3		
		33	25	17	12		
+0.8	+0.3	-1.5	-1.7	-0.6			
33	23	20	15	12			
+1.0	+0.1	-1.0	-1.2	-0.5			
33	20	18	15	12			
	-1.3	-1.7	-1.8	-0.5			
	33	27	18	12			
		-2.1	-2.6	-0.8			
		33	16	13			
		-1.9	-1.5	-0.6			
		33	17	12			
		+1.6	-1.1	-0.6			
		33	20	13			
	-0.1	-0.8	-0.5	-0.1			
	33	27	19	13			
		+0.7	-0.3	0.0			
		33	23	14			
		+0.7	+0.2	-0.1			
		33	21	13			
		+0.7	+0.5	-0.2			
		33	19	13			
	+4.9	+4.6	+1.0	-0.2			
	33	29	17	12			

Sta.		Elev.
+30	-2.0	903.7.
133		905.7.
134		908.4.
135		910.6
136		911.1.
137		911.0.
138		911.3.
+50	-0.1	911.2.
139		910.8.
140		910.5.
+50	-0.1	910.4.
141		910.5.
+50	-0.1	910.4.

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+7.3	+7.1	+0.6	-0.1	-0.2	+1.0	-0.4	
33	26	16	13	12	15	33	
+7.9	+7.0	+2.1	-0.2	0.0	+1.6	+0.2	
33	26	16	12	12	16	33	
+6.0	+5.9	+4.8	+1.4	-0.5	-0.2	-0.4	-2.1
33	27	24	19	14	13	17	33
+6.0	+6.2	+5.6	+3.4	+0.4	-0.2	0.0	-1.5
33	28	26	25	19	16	17	33
+4.7	+4.7	+0.6	-0.4	-0.4	-0.6	-3.2	
33	22	18	14	13	18	33	
+2.9	+1.9	+0.2	-0.4	-0.4	-2.3	-5.4	
33	20	18	14	10	16	33	
+2.7	+1.8	-0.2		0.0	-0.4	-0.9	
33	18	14		11	16	33	
+1.7	+1.4	+1.0	-0.7	-0.1	-0.6	-1.5	-1.8
33	20	18	16	10	15	21	33
+1.4	+1.1	-0.5		-0.4	-1.9	-3.4	
33	19	16		11	18	33	
-1.6	-1.0	-0.4		-0.4	-2.1	-2.8	
33	19	15		11	17	33	
-0.7	-1.5	-1.1	-0.3	-0.3	-3.5	-4.1	
33	22	16	14	10	17	33	
+1.1	+0.8	+0.1	-1.1	-0.5	-0.3	-2.6	-3.5
33	24	19	17	14	10	14	33
+1.8	+1.2	-0.7	-0.7	-0.4	-0.3	-0.9	-4.1
33	32	19	16		10	14	33

Sta.		Elev.
142		909.9 910.0
+50	+0.7	909.3
143		908.6
144		908.0
+50	-0.3	907.7
145		907.5
+50	-1.0	906.5
146		905.2
+50	+1.1	904.2
147		903.1
+50	+0.8	902.8
148		902.0
+50	-0.1	901.9

+1.6 +0.3 -0.6 -0.7 -0.5 33 20 18 17 15	-0.3 -1.3 -2.5 11 15 33
+0.3 -0.8 -1.0 -0.5 33 19 18 14	-0.5 -1.5 -1.8 -3.4 10 14 19 33
+1.6 +0.8 -0.9 -0.9 -0.3 33 20 15 15 15	-0.3 -2.9 -3.5 10 17 33
+3.6 +3.6 -0.7 -0.9 -0.5 33 31 24 19 17	-0.6 -1.3 -1.4 -1.9 -2.4 10 14 19 22 33
+4.2 +3.0 -0.8 -0.8 -0.5 33 30 24 19 16	-0.5 -0.7 -0.9 10 17 33
+3.3 +3.3 +0.9 -1.0 -1.2 -0.5 33 31 28 23 19 17	-0.3 -0.2 +1.0 +1.0 9 13 17 33
+3.0 -1.2 -1.3 -0.6 33 23 20 17	-0.1 +0.4 +1.3 12 30 33
-0.4 -0.3 -1.4 -1.0 -0.5 33 27 23 19 16	-0.4 -0.3 +0.6 10 13 33
-4.3 -3.3 -1.7 -1.0 -0.4 34 32 26 20 13	-0.5 -2.1 -2.7 -3.1 9 16 22 33
-3.9 -2.1 -1.4 -0.5 33 21 19 16	-0.4 -2.1 -3.2 -3.6 10 14 21 33
-3.2 -2.9 -0.7 33 19 14	-0.3 -2.9 -3.4 10 17 33
-3.3 -3.0 -2.6 -0.3 33 24 20 14	-0.5 -2.8 -2.4 -2.2 10 16 23 33
-2.3 -2.4 -0.3 33 21 14	-0.3 -2.2 -2.5 9 14 33

Sta.		Elev.
149		902.4
+50	00	902.4
150		902.0
+50	-0.5	901.5
151		901.1
152		901.1
153		900.6
154		900.5
+50	+0.2	900.7
155		900.7 900.6
+50	+0.2	900.9 900.8
156		901.1
+50	-0.2	900.9

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+1.5 +1.4 -0.6 -0.4 33 21 19 14	-0.3 -0.5 -1.2 10 13 33
+2.6 +2.5 -0.2 33 21 14	-0.6 -0.6 -0.2 10 14 33
+1.7 +1.3 -0.9 -0.2 33 22 17 14	-0.7 -0.5 -1.1 10 14 33
+0.8 +0.5 -0.2 -0.9 -0.3 33 20 19 17 14	-0.5 -1.6 -3.6 10 14 33
-0.4 +0.2 -0.6 -0.4 33 23 19 15	-0.8 -3.2 -4.7 10 17 33
-0.4 -1.3 -1.4 -0.6 33 22 18 15	-0.5 -1.9 -2.4 10 16 33
-4.4 -3.9 -0.8 33 20 13	-0.8 -4.0 -4.0 10 14 33
-3.1 -4.6 -0.6 33 19 13	-0.5 -2.0 -2.7 -4.1 11 16 19 33
+2.7 +1.4 +0.2 -0.6 33 24 18 14	-0.8 -1.1 -2.0 12 17 33
+8.5 +7.4 +1.9 0.0 -0.4 33 29 23 19 16	-0.8 -1.3 +0.2 14 15 33
+11.8 +11.1 +9.0 +2.8 +0.3 -0.1 40 34 33 24 19 14	-0.4 -0.8 +1.2 +2.3 14 15 20 33
+11.9 +9.5 +8.9 +0.5 -0.2 -0.6 40 35 33 21 17 15	-0.6 -1.5 -1.0 +1.1 +2.5 11 13 14 21 33
+10.0 +9.9 +6.3 +1.5 +0.3 -0.4 35 33 31 29 19 15	-0.6 -1.4 +0.6 +1.0 +1.1 14 15 19 30 33

Sta.		Elev.
157		900.7 900.0
+50	-0.4	900.3 900.2
158		899.5
159		897.5
160		897.0
161		898.0
162		901.0
+50	-2.0	902.8
163		904.8
+50	+1.8	906.6
164		909.0
+50	-1.9	911.3
165		913.2

12-31-26

-0.3	-1.2	-1.6	-1.1	-2.3
11	13	16	21	33
-0.3	-1.5	-4.1	-5.2	
12	17	22	33	
-0.6	-1.2	-4.6		
13	21	33		
-0.5	-2.8	-2.4		
14	20	33		
-0.8	-2.7	-1.8		
14	19	33		
-0.3	-2.7	-2.7	-2.1	
11	17	24	33	
-0.4	-3.3	-3.5	-5.4	-4.2 -2.7 3.1
12	18	24	28	30 33 38
-0.4	-4.0	-4.2		
12	20	33		
-0.6	-4.7	-5.6		
12	23	33		
-0.6	-1.0	-1.0	-2.7	-3.1
13	14	19	29	33
-0.3	-1.1	-0.1	-0.1	
11	15	28	33	
-0.7	-1.4	-1.5	+0.4	+2.6 +3.1
12	15	18	22	27 33
-0.4	-1.4	-0.6	+3.4	+3.4
12	15	20	28	33

+0.1	+5.5	+1.8	+0.1	-0.3
33	24	22	18	12
+0.6	0.0	-0.1		
33	24	16		
-2.3	-2.6	-0.4		
33	20	12		
-1.0	-1.8	-0.3		
33	18	12		
-0.8	-1.7	-0.3		
33	17	11		
-1.8	-2.3	-0.5		
33	19	12		
-3.0	-3.1	-0.7		
33	21	14		
-4.2	-4.1	-0.8	-0.3	
33	24	18	14	
-4.1	-1.5	-0.6	-0.4	
33	20	18	14	
+1.2	+0.0	-1.3	-1.4	-0.5
33	30	27	19	13
+0.6	-0.9	-1.5	-0.4	
33	28	18	14	
+3.0	+0.5	-0.7	-1.1	-0.7
33	29	25	17	13
+2.2	+1.5	0.0	-0.9	-0.7
33	25	20	17	13

Sta.		Elev.
	+50 -2.1	915.3
166		917.4
	+50 -0.8	918.6
167		919.4
	+50 +0.4	919.8
168		917.2
	+50 -0.6	918.4
169		917.4
	+50 -1.0	16.6 916.0
170		914.9
	+50 +1.8	913.4
171		911.4
	+50 -1.7	909.9

+1.7	+1.9	-0.4	-1.1	-0.5	-0.4	-0.9	+0.4	+3.1	+2.8
33	27	20	17	13	11	14	19	24	33
+2.2	+2.6	-0.8	-0.7	-0.6	-0.5	-0.6	+0.5	+2.4	+2.1
33	26	22	18	14	7	13	18	23	30
+3.1	+3.9	-0.2	-0.2		-0.4	-0.3	+0.8	+2.5	-2.7
33	23	16	12		12	14	20	23	33
+3.5	+4.1	+0.4	-0.4		-0.6	+0.5	+3.4	+3.3	
33	23	18	13		13	17	24	33	
+3.6	+4.1	+4.7	+0.6	-0.4	-0.4	+0.7	+5.0	+5.1	
33	28	22	16	13	12	17	23	33	
+3.6	+4.2	-0.1	-0.2		-0.4	+0.7	+5.0	+5.4	
33	20	15	11		12	17	22	33	
+2.1	+2.7	-0.2	-0.4		-0.6	0.0	+3.3	+3.5	
33	20	13	11		11	15	19	33	
+1.8	+2.1	0.0	0.0		-0.5	-0.7	+2.3	+2.5	
33	20	16	11		11	15	19	33	
+2.4	+2.9	-0.7	-0.7		+0.2	+0.7	+1.7		
33	21	15	13		11	20	33		
+4.5	+5.1	0.0	-0.2		-0.4	-0.3	+4.4	+4.5	
33	24	17	12		11	15	22	33	
+4.0	+3.9	+4.4	-0.9	-0.3	-0.2	-0.4	+5.3	+5.5	
33	29	24	16	13	12	14	23	33	
+2.5	+2.9	-0.5	-0.2		-0.3	-0.1	+2.3	+5.0	+5.3
33	21	14	10		13	18	22	24	33
	-2.4	+0.1	-0.3		-0.4	+0.2	+1.5	+3.9	+3.9
	33	17	12		12	20	24	29	33

Sta.		Elev.
172		908.3
+50	-0.8	907.5
173		905.6
174		903.5
+40	-0.1	903.4
175		904.8
176		907.9
+50	-2.0	908 907.0
177		911.8
+50	+2.1	913.9
178		915.6
179		918.4
180		921.7

-6.1	-5.7	-4.9	-0.2	-0.3	-0.7	-0.6	+0.3
33	23	18	11	15	19	27	33
-7.0	-6.9	-5.6	-0.3	-0.5	-4.5	-4.5	
33	24	19	11	15	26	33	
-5.8	-5.8	-4.8	-0.2	-0.3	-4.7	-5.2	-5.6
33	25	19	12	15	23	27	33
-4.5	-4.5	-3.8	-0.2	-0.2	-4.4	-4.4	
33	27	19	12	13	19	33	
	-4.2	-3.9	-0.1	-0.1	-3.9	-4.8	
	33	19	12	12	18	33	
	-5.3	-5.2	-0.4	-0.2	-5.2	-5.7	-5.7
	33	20	11	12	21	26	33
	-6.0	-5.1	-0.2	-0.5	-6.3	-6.9	-7.4
	33	22	13	13	23	26	33
	-3.8	-2.5	-0.3	-0.2	-3.8	-6.4	
	33	19	12	13	24	33	
	+0.5	+1.5	-0.2	-0.2	-0.4	-0.6	+0.5	-0.2
	33	22	17	12	11	16	18	33
+0.8	+2.1	-0.2	-0.2	-0.4	-0.3	+4.9	+3.6	+3.6
33	24	19	12	11	14	21	27	33
+0.2	+1.2	-0.3	-0.3	-0.2	-0.4	+5.3	+4.7	
34	23	19	13	10	14	24	33	
-1.2	-0.4	-0.4	-0.4	-0.3	+0.2	+5.7	+5.1	+4.6
33	24	19	13	10	14	21	26	33
-0.5	+0.7	+0.1	-0.3	-0.2	-0.1	+4.2	+3.0	+1.5
33	21	19	14	9	12	17	26	33

57a		E/c 4.
181		24.7 924.6
182		927.1.
183		927.5.
765	to Center of Hedgson Rd.	928.4.
184		927.9.
185		927.5.
186		927.8.
187		927.9.
188		927.9.
189		928.3.
190		928.3.
191		928.2.
192		928.3.

+1.8 +2.2 -0.6 -0.3 33 23 18 12	-0.4 +0.2 +2.8 +2.9 +1.5 10 13 16 20 33
+1.9 +1.8 +0.5 -0.6 33 24 20 15	-0.5 -1.2 +1.8 +0.8 +0.5 11 14 18 27 33
+0.8 +0.6 -0.7 -0.4 33 22 18 12	-0.2 -0.2 +2.8 +2.9 11 15 20 33
-0.2 50	-0.7 50
-0.4 -0.3 -0.6 33 17 12	-0.2 -0.3 -0.2 -0.5 11 15 20 33
-1.2 -1.3 -0.6 33 16 11	-0.7 -1.9 -2.4 -1.4 13 17 24 33
-0.3 -0.5 -0.6 -0.4 33 26 17 12	-0.2 -2.4 -2.9 -0.4 13 19 25 33
-0.4 -0.4 -0.5 33 17 11	-0.3 -2.1 -1.7 -0.9 -0.9 13 19 28 31 33
-0.8 -0.7 -0.7 -0.5 33 24 17 12	-0.3 -2.3 -2.6 -1.7 -1.9 11 18 23 28 33
-1.2 -1.1 -0.7 33 17 13	-0.6 -2.4 -2.3 -1.0 -1.0 13 19 26 30 33
-1.2 -1.2 -0.6 33 17 12	-0.4 -2.0 -2.0 -0.6 0.0 13 17 27 33 36
-1.8 -1.7 -0.6 33 17 12	-1.4 -3.3 -2.8 -1.3 11 21 28 33
-1.7 -1.3 -0.4 33 17 12	-0.4 -2.1 -2.6 -1.6 13 17 27 33

Sta.		Elev.
193		929.1.
194		930.4.
195		931.0.
196		932.2.
197		933.3.
198		932.9.
199		932.7.
200		933.0.
+50	-0.4	932.6.
201		931.8.
202		930.2.
+50	-1.6	928.6.
203		927.1.

+0.4 -1.0 -0.8 32 18 13	-0.4 -1.6 -1.6 13 17 33
+2.2 +0.3 -0.5 33 21 14	-0.3 -1.0 -1.0 -0.3 +0.2 14 18 24 28 33
+1.3 -0.8 -0.6 33 20 14	-0.1 -1.5 -1.3 14 19 33
+1.5 +1.5 -0.2 -0.3 33 31 22 11	-0.3 -1.7 -1.6 -0.9 -0.9 15 19 23 27 33
+1.7 +0.5 -0.5 33 22 13	-0.3 -1.5 -1.3 -0.1 -0.4 14 17 24 28 33
+0.4 +0.4 -0.6 -1.0 -0.3 33 28 24 17 11	-0.8 -1.9 -1.9 -1.1 13 22 28 33
-0.7 -0.7 -1.4 -0.7 33 27 18 14	-0.5 -1.0 -2.1 14 17 33
+2.0 +1.6 +0.2 -0.1 33 23 14 13	-0.1 +0.6 -0.8 14 18 33
+3.5 +2.9 +0.3 -0.2 33 21 15 12	-0.2 +0.7 +0.5 14 19 33
+4.4 +4.9 +4.5 +1.5 -0.4 33 31 23 14 12	-0.1 +1.7 +2.3 +2.3 14 18 25 33
+5.7 +4.7 +2.0 -0.3 33 23 17 14	-0.4 +1.1 +2.2 +2.0 14 19 23 33
+4.9 +4.1 +1.2 -0.4 33 25 17 12	-0.5 -0.1 +1.3 +1.5 14 17 24 33
+2.0 +1.4 +0.5 -0.4 33 24 17 14	-0.7 -1.0 -0.7 13 27 33

Stg.			Elev.
	+50 +16		925.5.
204			923.9.
205			921.0.
206			917.7.
207			914.8.
208			912.2.
209			909.6.
210			906.9.
	+44 -1.2		905.7.
	+64 -0.4		905.0.
211			904.0.
	+01.25 00	@ Rice St.	904.0.

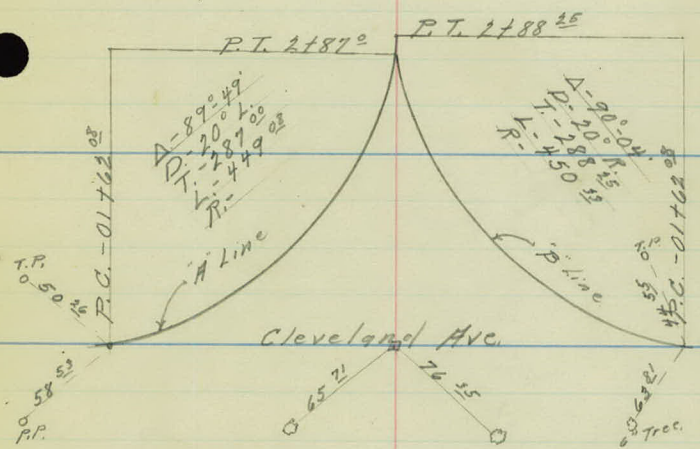
Co. Rd. "C"
Rd. % # 11 & 1
Allignment on Double
Connection at Cleveland Ave
& Co. Rd. "C."

26744[15] P.I.

11-20-26

Mounds View Rd.

Co. Rd. "C"



"B" Line

Co. Rd. "C"
Rd. 9/c # 11 & 1.
X sections & & Levels
on "B" Line.

Sta.	+	H.I.	−	Rod.	Elev.
B.M.	5.37	919.66		914.29	
-2+00				8.6	
-1+62.03				8.1	
-1+50				8.0	
-1+00				7.5	
-0+53				7.1	
-0+28				8.7	
-0+11				6.7	
0+00				6.5	
0+50				6.6	
1+00				7.7	
1+50				7.0	
2+00				6.3	
2+50				6.7	
2+88.25				7.8	
B.M.			5.37	914.29	

11-20-26

"B" Line

Pt.

13.2/33	8.4/21	8.1	8.1/20	9.3/27	9.6/34	8.3/39		
12.4/33	8.8/22	8.0	7.9/20	9.3/27	9.6/34	8.1/40		
7.3/30	7.5	7.4/13	8.8/20	9.4/30	7.5/30	7.5/40		
6.8/44	6.8/20	7.1	8.6/7	9.0/17	6.9/22	6.6/40		
6.9/40	6.7/35	6.8/15	8.2/4	8.7	9.2/6	6.9/10	6.7/25	6.7/40
6.3/30	6.4/30	7.7/22	8.4/14	6.4/7	6.5	6.6/22	7.0/40	
6.4/40	6.1/36	6.6	6.5/23	6.4/40				
7.5/40	8.1/22	7.7	6.4/21	5.8/40				
5.3/40	5.6/29	6.2/20	6.6/11	7.0	6.0/23	5.1/40		
5.6/40	5.9/33	6.0/18	6.3	6.1/14	5.1/32	5.1/40		
5.1/40	5.6/24	6.4/22	6.9/8	6.9	7.2/17	5.7/30	5.2/40	
5.7/40	7.8/17	7.8	8.5/17	7.5/24	4.8/35	4.6/40		

A Line

Co Rd. 6"
Rd. % # 11 & 1.
X sections & & Levels.
on "A" Line.

(A)

Sta.	+	H.I.	−	Rod	Elev
B.M.	5.37	919.66		914.29	
-2+00				4.5	15.2
-1+62.8	-2+37.92			4.4	15.3
-1+50	-2+50			4.4	15.3
-1+00	-1+00			4.5	15.2
-0+55	-1+45			4.5	15.2
-0+28	-1+72			6.8	12.9
-0-13	-1+87			5.5	14.2
0+00				5.6	14.1
0+50				6.2	13.5
1+00				5.6	14.1
1+50				5.3	14.4
2+00				6.5	13.2
2+50				6.8	12.9
2+87.0				7.8	11.9
B.M.			5.37	914.29	

12-20-26

"A" Line

U. S. Gov. B.M. 60 Rt. Sta. 0+75

Lt.					Rt.		
6.6	6.9	6.7	4.4		4.1	6.6	7.2
40	38	27	21	4.4	27	30	37
6.5	6.9	6.9	4.5		4.2	6.5	7.0
40	37	28	21	4.4	22	29	38
5.6	5.6	6.7	6.6	4.5	4.4	6.6	7.2
40	34	32	22	14 4.5	29	34	43
5.7	5.1	6.8	6.5		4.5	4.3	
40	20	18	8	4.5	25	43	
5.8	5.3	7.0			6.2	4.6	4.6
40	9	5	6.8		5	12	39
6.0	4.9				5.6	6.9	6.5	4.8	5.0
40	18	5.4			8	12	22	31	50
6.2	6.5				5.9	5.7			
40	24	6.2			27	40			
6.0	5.9				5.6	5.6			
40	24	5.6			28	40			
5.7	5.7				5.3	5.6	5.4	5.4
40	24	5.3			13	18	27	38
5.5	5.6	6.0			6.0	6.6	6.1	6.1
40	29	10	6.5		15	28	34	40
5.3	6.1	6.3	7.2		6.8	6.9	5.4	5.4
40	34	20	11	6.8	3	23	36	40
5.7	7.8				8.5	7.5	4.8	4.6
40	17	7.8			17	24	35	40

Co. Rd. "C"
Rd. 9/c # 11.
Alignment on connection
at Co. Rd. "C" & Hodgson.

Pros. 27-11

Received 1-8-27
C. Van Kleeck

Sta.	Point	Lt	Rt

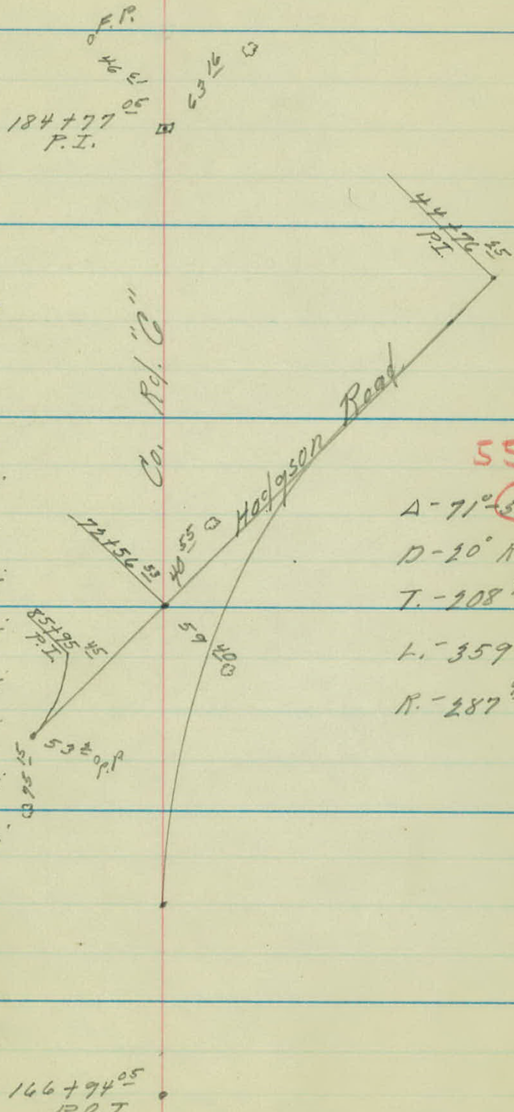
185+14.09 P.T. = 70+47.60 On Hodgson Rd.

183+63.35 P.I. 71°-54

181+54.42 P.C.

1-7-27

6 Trees



181+54.43	
182+00	−4°−33.5′
182+50	−9°−33.5′
183+00	−14°−33.5
183+50	−19°−33.5′
184+00	−24°−33.5′
184+50	−29°−33.5
185+00	−34°−33.5
185+14.09	−35°−58′

55

Δ − 71°−56′
D − 20° R.
T. − 208.93
L. − 359.67
R. − 287.94

Co. Rd. "C"

Rd. %. # 11.

Center line levels and cross sections on connection of Co Rd. "C" & Hodgson.

Sta.	+	H.I.	−	Rod.	Elev.
B.M.	5.72	933.13		927.41	
181+54 47	P.C.			7.0	926.1
182				6.2	26.9
+38				6.4	26.7
+59				4.1	29.0
183				3.9	29.2
+25				4.5	28.6
+50				5.1	28.0
184				6.1	27.0
+50				6.1	27.0
185				5.8	27.3
+14 09	P.T.			5.4	27.5
B.M.			6.14	926.99 =	927.04

1-7-27

Lt. Rt.

Spk. in 15" Oak. Lt. Sta. 185+17 On Co. Rd. "C"

5.0 4.8 6.6 7.2 7.5 5.9 6.5
33 23 19 12 7.0 13 17 33

¢ Rd.

4.2 4.4 5.9 6.1 6.6 4.4 6.1
33 28 25 7 6.2 10 14 33

¢ Rd.

5.5 6.0 5.7 4.4 5.5 5.7
35 27 14 6.4 6 24 33

¢ Rd.

6.0 5.8 5.7 6.0 5.2 5.7
35 22 15 5 4.1 21 33

¢ Rd.

5.8 5.3 4.9 4.9 4.8 5.3
42 25 19 4 3.9 9 33

¢ Rd.

5.0 5.5 4.8 4.8 3.8 5.0 5.4
61 41 31 21 8 4.5 17 33

¢ Rd.

5.1 5.5 4.7 5.5 4.9 5.3 5.6
57 42 38 15 12 5.1 20 33

¢ Rd.

5.8 5.5 6.1 5.3 6.3 6.5
39 25 8 6.1 8 18 33

¢ Rd.

6.7 6.4 5.8 6.6 6.6 7.2
33 24 11 4.1 13 27 35

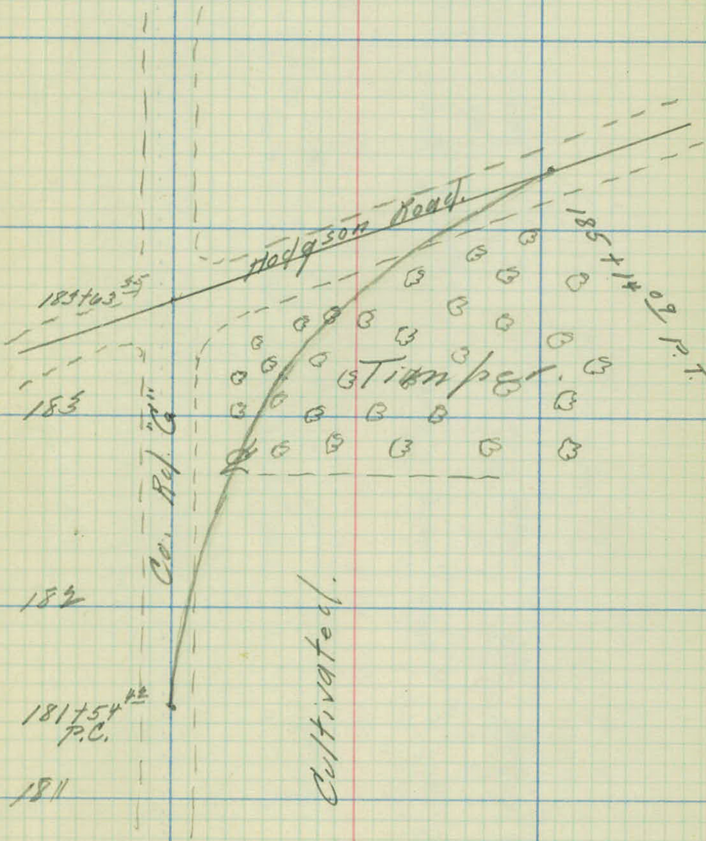
¢ Rd.

5.6 5.8 6.5 6.8 5.8 4.1 5.6 7.0 6.7
39 27 23 15 1 5.8 13 17 28 33

6.1 6.0 6.3 6.0 6.5 6.3
33 27 14 5.6 12 20 33

Spk. in 12" Oak. Rt. Sta. 71+30. On Hodgson Rd.

1-7-27


183+63 55
183
182
181+54 42
P.C.
181
Hodgson Road
Timber
Cultivated
185+14 09 P.T.

& LEVELS

CROSS-SECTIONS

CO. RD. "G"

INTERSECTION OF CO. RD. "G" & RICE ST.

Received 2-19-27

File with Co. Rd. "G" Pros 27-11

STA.	B.S.	H.I.	F.S.	ROD	ELEV.
B.M.	4.65	912.65 ✓			908.00
211+01.3				8.70	903.95
+16				8.60	904.05
+50				8.40	904.25
212+00				7.20	905.45
+30				5.90	906.75
+65				4.70	907.95
213+00				4.90	907.75
213+50				5.10	907.55
214+00				4.90	907.75
215+00				4.00	908.65

2-18-27

⊼ A.W.L.
A.L.P.
W.G.A.
E.T.S.

CLEAR-COLD

LEFT RIGHT

SPIKE IN TREE LEFT OF STA. 109+20

— — — — 7.1/33 6.5/14 6.1 6.1/12 6.2/50 5.0/100 3.3/150 2.90/170 3.10/192 EDGE PAVE

— — — — 6.9/33 6.6/16 6.0 6.2/12 6.6/28 6.0/100 5.2/130 3.1/142 3.2/160 EDGE —

— — 12.7/33 12.6/30 6.6/18 5.8/12 5.7 6.0/12 10.7/25 9.1/70 2.7/90 3.2/103 EDGE 4.6/145 EDGE

— — — 14.0/33 13.2/27 4.9/10 4.5 4.6/11 10.7/23 10.3/29 2.6/46 2.8/54 EDGE 4.3/87 EDGE

— — — 13.4/33 12.7/26 4.1/10 3.3 3.1/14 2.3/24 2.6/33 EDGE 3.9/64 EDGE — —

— — — 12.3/33 12.1/27 2.3/9 2.0 2.5/15 EDGE 3.9/40 EDGE — — — —

— — — 10.8/33 10.1/27 1.7/12 2.3 2.6/7 EDGE 3.8/28 EDGE — — — —

— — 8.7/33 8.0/27 1.8/16 2.0/8 EDGE 2.5 3.4/15 EDGE 2.8/21 4.6/26 4.0/33 — —

— — 5.3/27 5.3/24 1.7/16 1.9/12 EDGE 2.3 2.7/11 EDGE 2.4/15 4.8/20 4.8/23 3.2/28 3.2/33 —

— — — — 1.4/16 1.4/11 EDGE 1.5 1.6/9 EDGE 1.5/15 2.7/18 2.7/21 +2.5/33 — —

Co. Rd. "C"
Rd. Jc. # 11
Test Holes on Co. Rd. "C"
from the Hodgson Rd. to Hamline Ave.

Cut # 5

3rd Sta. From Mt. E.

Sounding # 1 Lt. Stg
0 to 7 Sand.

1st Sta E. Mt.

Sounding # 2 Lt. Stg.
0 to 7 Sand.
7 to 9 Gravel.

Soundings in Cut # 1

Sounding # 1 Rt. Sta. 181+50
0' to 7' Sand.

sounding # 2 Rt. Sta. 180+00
0' to 8' Sand.

sounding # 3 Rt. Sta 178+00
0' to 8' Sand.

3-3-27

Soundings in Cut #2.

Sounding # 1 Rt. Sta. 171 +00
0' to 7' Sand.

Sounding #2 Lt. Sta. 171 +50
0' to 6' Sand.

Sounding #3 Rt. Sta. 168 +00
0' to 7' Sand.

Sounding # 4 Lt. Sta. 167 +50
0' to 9' Sand.

Sounding #5 Rt. Sta 165+00
0' to 7' Sand.

Sounding # 6 Lt. Sta. 165+00
0' to 5' Sand.

Cut # 4.

Sounding #1 Lt. Sta. 114+00
0' to 3' Clay & Gravel

Sounding #2 Rt. 114+00.
0' to 3' Clay & Gravel.

Sounding #3 Lt. Sta. 113+00
0' to 4' Clay & Gravel

Sounding #4 Lt. Sta. 108+00.
0' to 10' Clay & Gravel.

Sounding #5 Rt. Sta. 108+00
0' to 4' Clay

Sounding #6 Rt. Sta. 112+00 ✓
0' to 4' Clay.

3-2-27

Cut # 5.

Sounding # 1 Rt. Sta. 95+00

0' to 5' Clay.

~ PROJECT 27-11 ~

~ COUNTY ROAD "G" ~

Plans in hand inspection. 2-24-27

O.R. Vankrevelen
W.S. Mackintosh
H.J. Goldberg

✓ 0-30 - P. 18" R_3 along ditch of Cleveland Ave.

✓ 2+80 - F.E. ~~Lt~~ - P. 15"X 24' C.M.

✓ 7+00 - No culv. req.

✓ 11+00 to 13+00 Lt. - Cl. 11 trees Gr. 12 trees

✓ 13+21 - Remove culv. None req.

✓ 16+20 - F.E. Rt. - P. 15"X24' C.M.

✓ 16+92 - " Lt. - P. 15"X24' C.M.

✓ 19+98 - No culv. req. Hand ditch on Lt. to culv. at 23+29.

✓ 20+50 to 26+25 - Lt. - G.R.

✓ 20+00 to 25+00 - Rt. - G.R.

✓ 23+29 - Remove culv. P. 24" R_3

✓ 25+13 - F.E. - Abandon.

✓ 24+50 to 26+00 Rt. - Cl. 10 trees Gr. 13 trees.

✓ 26+42 - F.E. Rt. - Remove culv. P. 15"X24' C.M.

✓ 27+00 to 28+00 Lt. - Cl. & Gr. 2 trees

? Show Anoka Cut-off.

✓ 33+50 to 37+25 Rt. - G.R.

✓ 35+79 - Remove culv. - P. 24" R_3.

✓ 37+80 - F.E. Rt. - No culv. req.

✓ 38+75 to 41+50 Rt. - G.R.

✓ 42+30 - F.E. Rt & Lt. - No culv's. req.

✓ 42+25 to 45+75 - Lt. - G.R. (o.v.)

✓ 42+50 to 45+50 Rt. - G.R.

✓ 43+51 - Remove culv. - P. 24" P_3.

✓ 46+03 - F.E. Rt. - Abandon.

✓ 49+50 - F.E. Lt. - No culv. req.

✓ 51+50 to 52+25 Rt. - G.R.

✓ 52+32 - Culv. O.K.

✓ 52+70 - Lt. - Culv. O.K.

✓ 53+00 to 54+00 Rt. & Lt. - G.R.

✓ 58+00 - F.E. - Rt. - P. 15"X24' C.M.

✓ 61+50 to 64+50 - Cl. & Gr. 10 trees.

✓ 66+55 - F.E. - Rt. & Lt. - Remove on Lt. - P. 2 - 15"X24' C.M.

✓ 68+31 - F.E. Rt. - Remove culv. P. 15"X24' C.M.

✓ 74+20 - F.E. - Lt. - No culv. req.

✓ 74+50 to 77+00 Lt. - G.R.

✓ 78+97 - Remove culv. P. 24" P_3.

✓ 79+54 - " " . P. 24' P_3.

✓ 80+00 - F.E. Rt. - No culv. req.

✓ 84+70 - F.E. Lt. - Rep. 12"X24' C.M. from 78+97.

✓ 87+82 - F.E. Rt. & Lt. - No culv. req.

✓ 88+00 to 89+00 Rt. - Cl. & Gr. 4 trees.

✓ 89+00 to 90+00 Lt. - " " " 11 trees.

✓ 93+00 to 94+00 - " " " 6 " .

✓ 97+07 - F.E. Rt. - Remove culv. P. 15"X24' C.M.

✓ 97+20 - F.E. Lt. - P. 15"X24' C.M.

✓ 97+00 to 104+00 Rt. - G.R.

✓ 97+50 to 104+00 Lt. - "

✓ 99+00 to 103+00 - Cl. 11 trees.

(Proj. 27-11)

✓ 100+63 - Remove culv. - P. 24" P_3.

✓ No culv's. req. at Lexington.

✓ 108+56 - F.E. Rt. - No culv. req.

✓ 116+00 to 117+00 - Rt. - Gr. 12 trees.

✓ 117+45 to 123+85 Rt. - Remove & replace G.R.

✓ 125+75 - Inp. 12"x30' (?) - Remove - P. 24" P_3.

✓ 126+20 - F.E. Lt. - Rep. 12"x27' C.M. from 129+16.

✓ 129+16 - F.E. Lt. - Remove culv. P. 15"x24' C.M.

✓ 129+00 to 131+00 Lt. - Cl. & Gr. 11 trees.

✓ 129+00 to 131+50 Rt. - G.R.

✓ 132+00 - F.E. Rt. - P. 15"x24' C.M.

✓ 137+81 - F.E. Lt. - No culv. req.

✓ 139+00 - F.E. Rt. - " " "

✓ 143+75 - F.E. Lt. - P. 15"x24' C.M.

✓ 144+61 - F.E. Rt. - No culv. req.

✓ 145+45 - F.E. Rt. - P. 15"x24' C.M.

✓ 147+79 - Remove culv. - P. 24" P_3.

✓ 149+16 - F.E. Rt. - No culv. req.

✓ 151+33 - F.E. Lt. - P. 15"x24' C.M.

✓ 153+00 - P. 24" P_3. H.D. 50 cu yd. on Rt.

✓ 157+00 to 158+00 - Cl. & Gr. 5 trees.

✓ 157+45 - F.E. Lt. - Rep. 12"x24' C.M. from 163+65.

✓ Raise grade from about 158+00 to 162+00 so as to have about 1.5' fill over old road.

✓ 160+83 - Remove culv. P. 24" P_3.

✓ 158+00 to 160+83 - H.D. on Lt.

✓ 163+65 - Road Rt. - Remove culv. - P. 15"x30' C.M.

(over)

✓ 164+00 to 165+00 - Cl. & Gr. 2 trees.

✓ 166+62 - F.E. Rt. - No culv. req.

✓ 168+00 to 169+00 - Cl. 3 trees Gr. 5 trees.

✓ 168+81 - F.E. Lt. - Rep. 12" x 24' C.M. from 174+18.

✓ 169+50 - F.E. Rt. - Remove & replace.

✓ 171+75 to 176+50 - Lt. - G.R.

✓ 172+25 to 176+50 - Rt. - "

✓ 174+18 - Remove culv. P. 24" B.

✓ 175+65 - Leave culv. in place and cover.

✓ 176+00 to 182+00 - Cl. 1 Tree - Gr. 35 trees.

✓ Curve from "G" on to Hodgson - Cl. & Gr. 33 trees.

✓ 184+90 - F.E. Lt. - Remove & rep.

✓ 184+00 to 185+00 - Cl. & Gr. 3 trees.

✓ 184+90 - F.E. Rt. - No culv. req.

✓ 185+00 to 187+00 - Cl. & Gr. 3 trees.

✓ 188+00 - No culv. req.

✓ 192+50 - F.E. Rt. - No culv. req.

✓ 197+25 - F.E. Rt. - " " "

✓ 197+00 to 201+00 - Cl. 8 trees Gr. 18 trees.

✓ 203+50 to 211+00 - Cl. 16 " Gr. 5 "

✓ 203+75 to 209+55 - Remove G.R. on Rt.

✓ 203+50 to 210+50 - Rt. & Lt. - G.R.

✓ 24" B to be placed on skew from about 210+70 on Rt. to 211+50 on Lt.