

Void

PLANS SURVEY

CLEVELAND AVE.

From: County Road "E" - North

Road $\frac{9}{16}$ c No. 5

File No. 12

27-05

Office of Plans & Engineering
ST. PAUL, MINN.

9-8-26

12

Road 9c #5.
Relocation of Cleveland Ave
from Co. Rd. "E" North.

Office of Ramsey Co., Engineer
ST. PAUL, MINN.
9-8-26
~~13~~ 12
Date Filed
File No.

Sta. Point Lt. Rt.

234702⁹ P.O.T.

232711¹² P.T.

230703⁶ P.I. 43°-50

227772²⁹ P.C.

227760¹ P.I.

227750¹ P.I.

227+72⁷³

228 -1°-21⁶
+50 -3°-51⁶

229 -6°-21⁶
+50 -8°-51⁶

230 -11°-21⁶
+50 -13°-51⁶

231 -16°-21⁶
+50 -18°-51⁶

232 -21°-21⁶
+11¹³ -21°-55

Mont.
Co. Rd. E 8
Long Lake Rd.

890 1/2

3mils Sec. line

36° 00' N
 13 44
 49 52
 P.B.
 A-43-50
 D-10° 17.
 T-230 81.
 L-438 53.
 R-573.69.

355.6

8-25-25

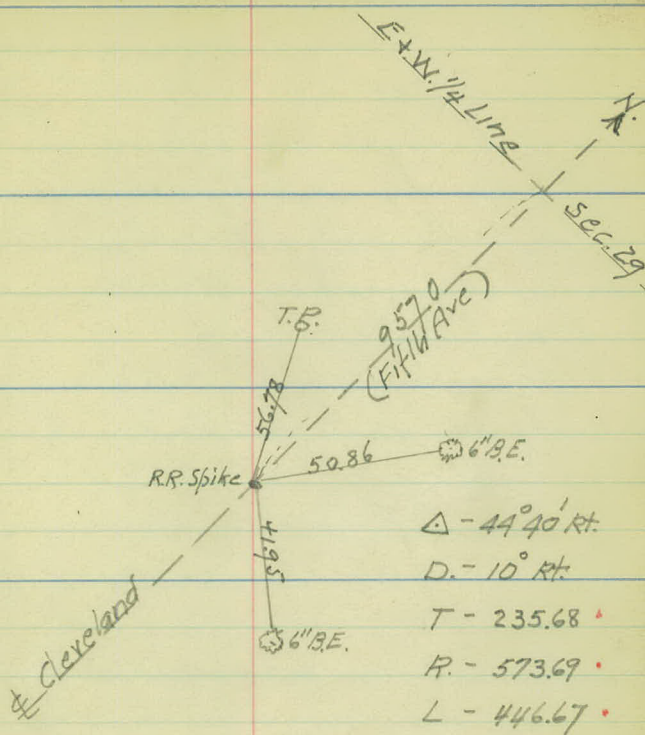
250+6489 P.T.

248+53.9 P.I.

44°40'

246+18.22 P.C.

243+38 P.O.T.



- $\Delta - 44^{\circ} 40' \text{ Rt.}$
- $D. - 10^{\circ} \text{ Rt.}$
- $T - 235.68 \cdot$
- $R - 573.69 \cdot$
- $L - 446.67 \cdot$

264+456 P.I

257+867 P.O.T.

To New Brighton



Iron Sign

AP 235

N.B. Road 10' Pav.

F. Cor. 232

IRON. Rd. Sign.

F. Post

E & W 1/4 line

Sec. 29

16 31

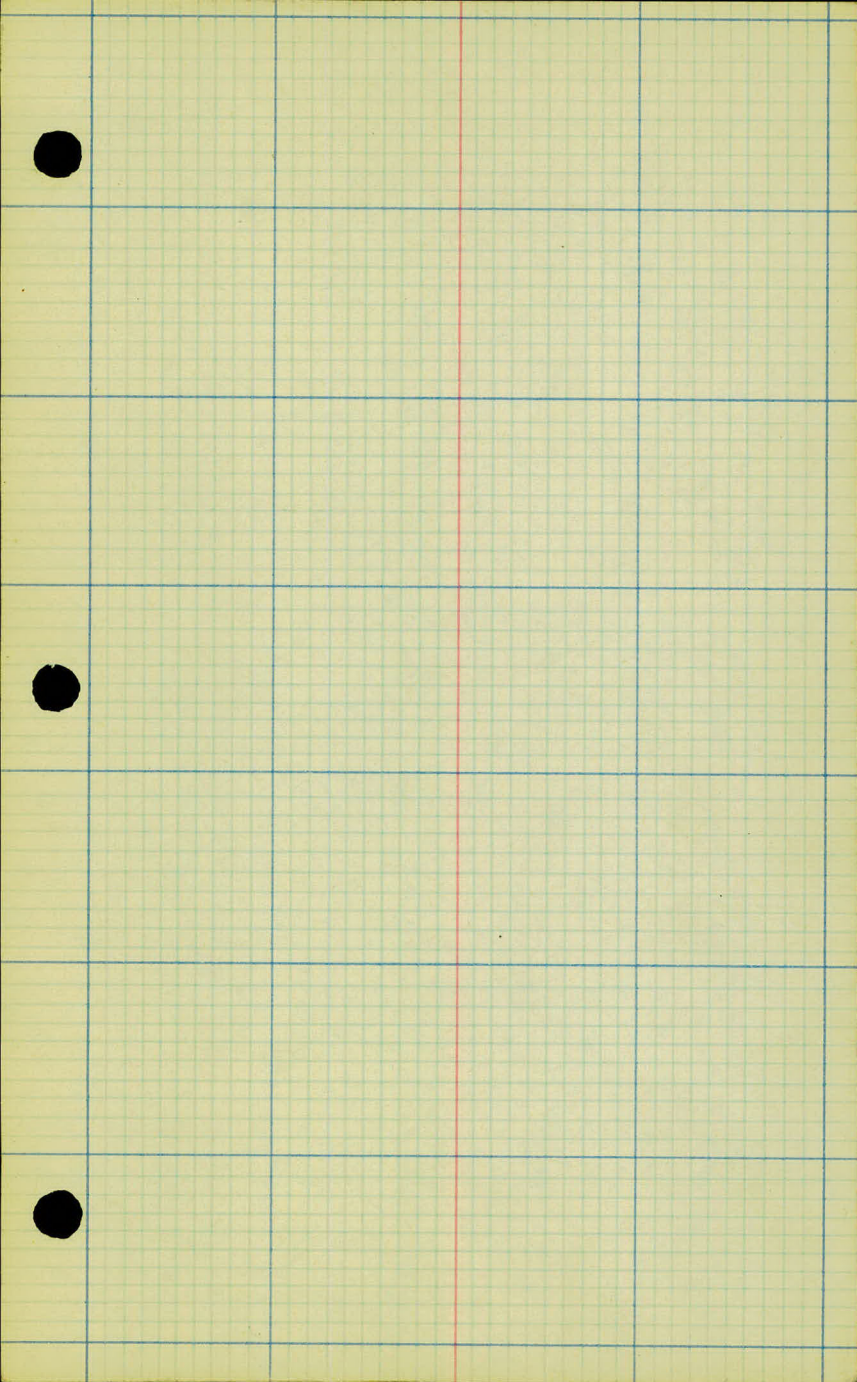
17 15

F. Post.

8-25-25

235+00

230+00



240

239

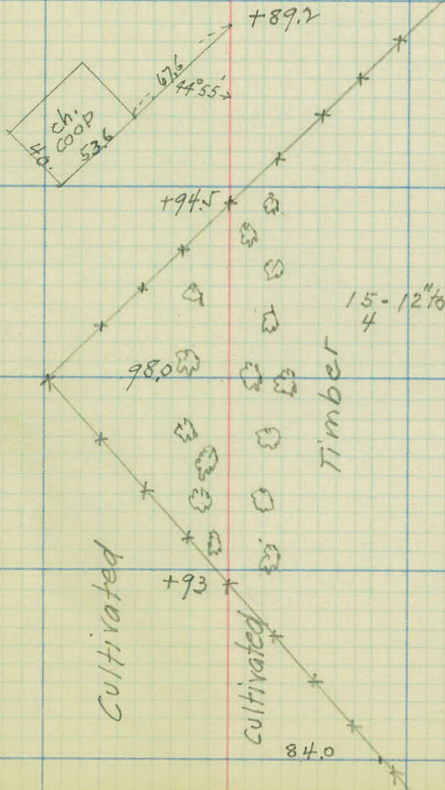
238

237

236

Cultivated

Cultivated



ch. coop
40.
53.6

+89.2

+94.5

+98.0

+93

84.0

15-12" to 20" Oaks
4
11 Stumps

Timber

Cultivated

Cultivated

248

247

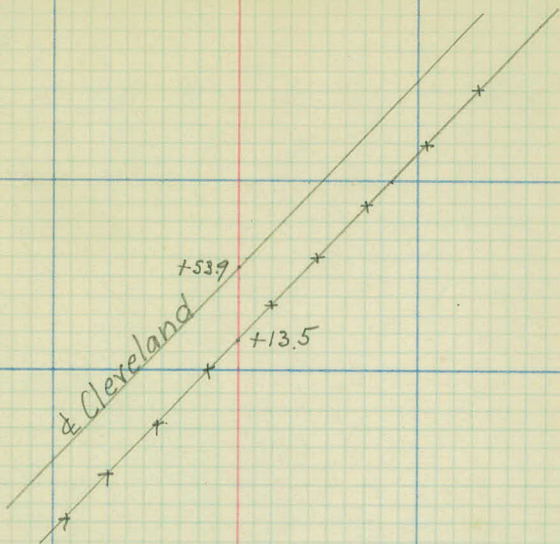
246

245

244

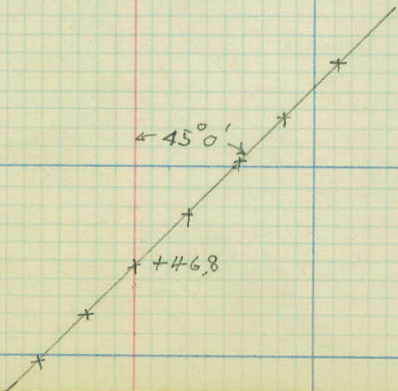
+38 P.O.T.

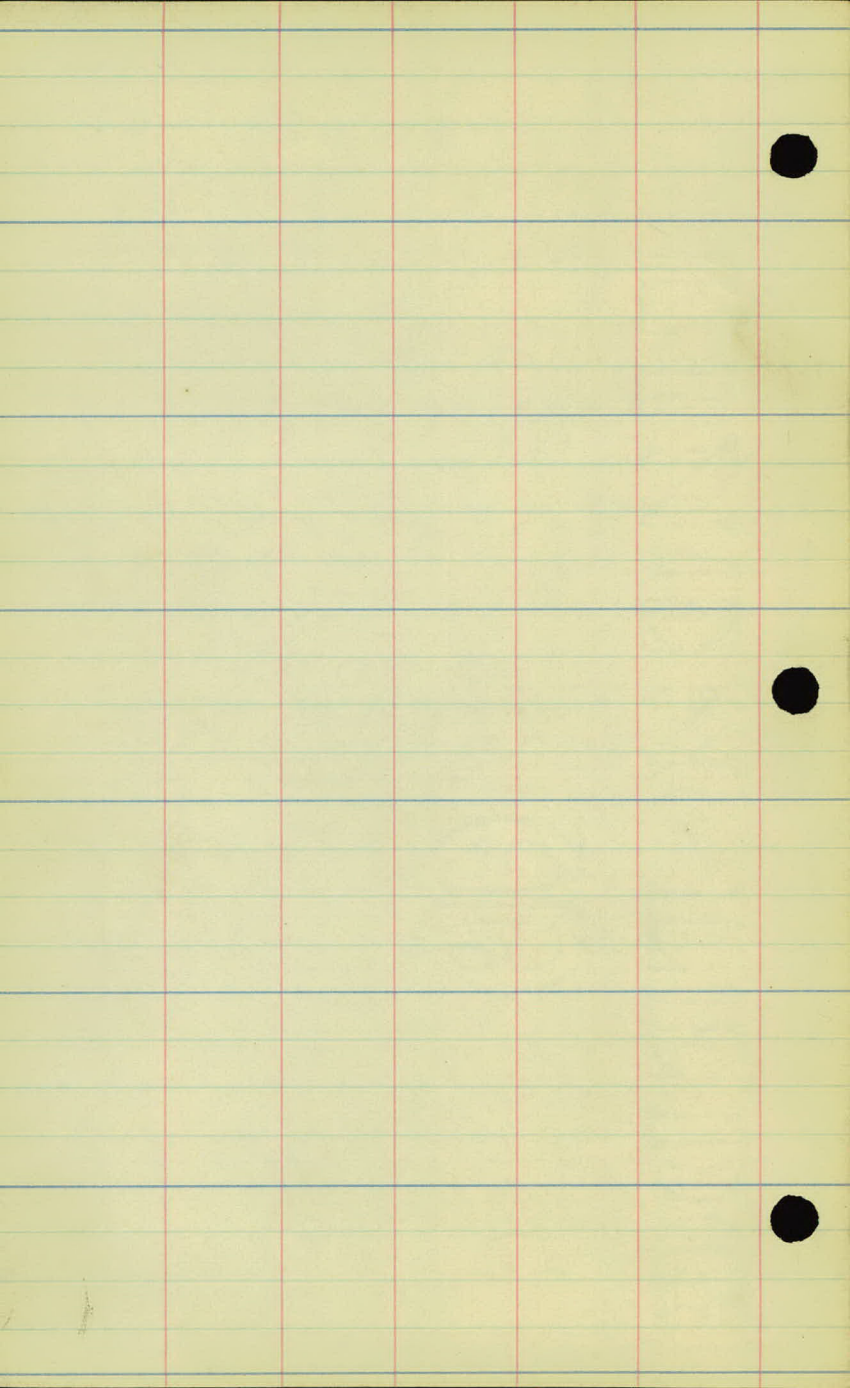
243



Cultivated

Cultivated





Cleveland Ave

Topography

Sta 250+00 to 264+45.6

party
{ Wjsthusen
Skoodjen
{ Bertholme
Messenpura

Received 1-11-27
G. H. K. K. K.

256

255

254

253

252

251+00

250+00

+09 T.P. 27'

F.L. 13

Rd - 12'

Rd. 12.5 F.L.

+52 T.P. 27

Hog Farm

F.L. 13'

+85.4 drive

+10 F.Box 12'
+60 2 drive
+30 F.Cor 30'

+24 T.P. 27'

F.L. 29'

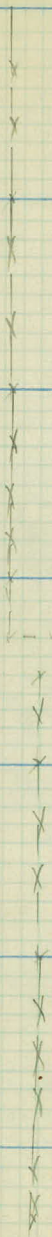
+78 T.P. 26'

#11 Center 2709
F.L. 29'

Pole yard

Cultivated

164.89 - F.L. 28



262

261

260

259

258

257

194 T.P. 17

+83 & drive

F.L. 27

S.W. 21

+22 F. Cor. 24
+08 P.P. 12

+51 T.P. 19

F.L. 29

S.W. 22

+91 P.P. 31 27 6'

+72 F.L. 29

+62 & drive

+87 T.P. 18

+77 P.P. 10

+51 & drive

+12 T.P. 12
Rd. 15

Rd=11

+84 P.P. 10

+82 F.L. 15

S.W. 23.5 Rd. 15
+17 & School Walk 65 W-37

F.L. 16

+75 P.P. 25

+85 P.P. 10

+28 T.P. 18

+54 T.P. 37

+57 Cor School

72'

+19 B. Side W. 23

4' Walk

+87 School yard

+91 F. Cor. 125-175

+16 T.P. 16

F.L. 125

Pole yard
School yard

School yard
School yard

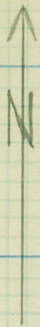
Pole yard

Pole yard
School yard
Pole yard

265+00

264+00

263+00



To New Brighton

Note 300
Construction
Notes for
Correct Radius



20' Pav.

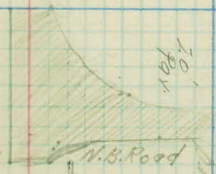
44' 10"

10'
Pav.

+56 P.V. 57.0
+75 S.W. 15-14
+79 S.P.V. 155
+30 S.W. 37
+29 P.P. 4
+25 F.R.W. 22
P.W. 23'

+29 Fl. 30'
+20 Fl. 25'
+15 T.P. 16'
Fl. 25

+22 Pav.
S.W. 18'



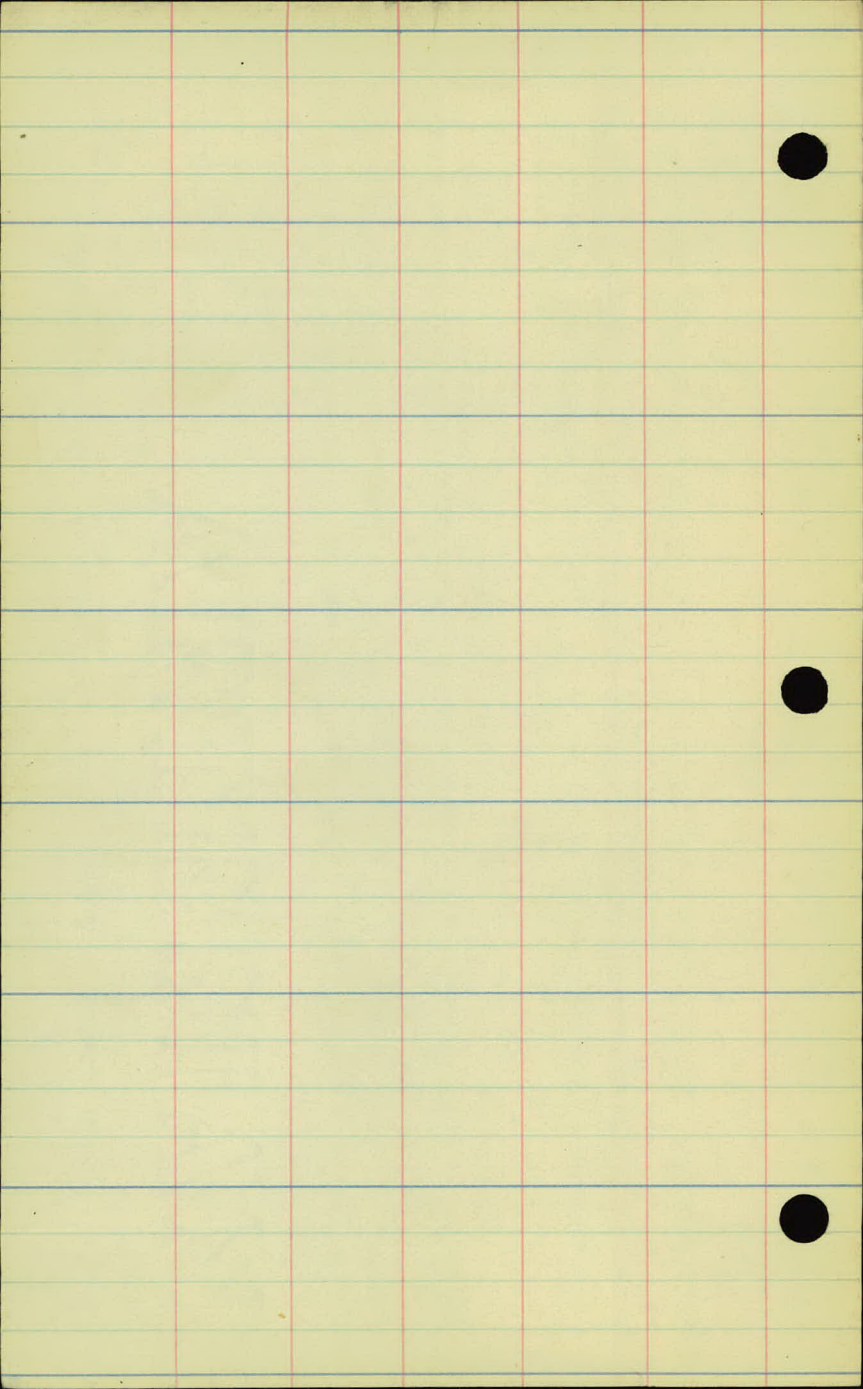
+32 T.P. 27'
+22 P.V. 51
+13 P.R.W. 23
+08 S. Drive
+01 P. Cor 25'

+28 S. Step 26'
S.W. 19'

Pole yard driveway

Side wall

road



Xsections

(27-05)

8-27-26

7.27 942.65[✓]

935.38

227+72.8

P.C. 942.7

228

41.1

+50

38.3

229

34.1

+50

30.5

230

708 941.06[✓] 8.67 933.98[✓]

34.2

+50

34.0

231

34.0

+50

35.0

232+11.12

P.T. 35.9

+50

35.6

233

934.8

Spike in 30" Oak Rt. Sta 230+03

10.1	48	01	00	0.2	5.8	12.7
<u>33</u>	<u>79</u>	<u>77</u>		<u>11</u>	<u>20</u>	<u>33</u>

13.5	12.1	84	20	16	20	7.9	12.8	13.1
<u>33</u>	<u>25</u>	<u>18</u>	<u>70</u>		<u>17</u>	<u>18</u>	<u>28</u>	<u>33</u>

13.9	13.3	4.7	4.4	4.2	4.5	13.3	14.1
<u>33</u>	<u>19</u>	<u>5</u>		<u>6</u>	<u>15</u>	<u>28</u>	<u>33</u>

11.5	12.1	13.6	12.7	8.6	6.5	6.1	6.7	11.3
<u>33</u>	<u>25</u>	<u>20</u>	<u>6</u>		<u>4</u>	<u>15</u>	<u>25</u>	<u>33</u>

9.8	10.0	12.4	12.2	10.0	7.7	7.7	8.2
<u>33</u>	<u>18</u>	<u>8</u>		<u>8</u>	<u>13</u>	<u>26</u>	<u>33</u>

11.1	11.5	10.3	9.0	8.5	8.0	9.3
<u>33</u>	<u>29</u>	<u>13</u>	<u>8</u>		<u>12</u>	<u>33</u>

7.2	6.8	7.1	6.9	7.1
<u>33</u>	<u>14</u>		<u>15</u>	<u>33</u>

6.7	7.0	7.1	7.3	7.7
<u>33</u>	<u>14</u>		<u>15</u>	<u>33</u>

5.7	5.8	6.1	6.6	6.7
<u>33</u>	<u>14</u>		<u>16</u>	<u>33</u>

5.0	5.1	5.2	5.6	5.9
<u>33</u>	<u>18</u>		<u>17</u>	<u>33</u>

5.0	5.2	5.5	5.8	6.4
<u>33</u>	<u>18</u>		<u>15</u>	<u>33</u>

5.6	5.8	6.3	7.0	7.5
<u>33</u>	<u>20</u>		<u>18</u>	<u>33</u>

✓
941.06

233 + 50

935.1

234

35.8

+ 50

35.3

235

2.22

✓
936.62

6.66

✓
934.40

33.8

+ 50

33.0

236

32.6

+ 50

30.7

237

28.5

+ 50

26.5

238

27.1

+ 50

28.5

239

1.99

✓
933.28

5.33

✓
931.29

930.6

$$\begin{array}{r} 47 \\ \hline 33 \end{array} \quad \begin{array}{r} 54 \\ \hline 14 \end{array} \quad 6.0 \quad \begin{array}{r} 72 \\ \hline 15 \end{array} \quad \begin{array}{r} 83 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 41 \\ \hline 33 \end{array} \quad \begin{array}{r} 46 \\ \hline 18 \end{array} \quad 5.3 \quad \begin{array}{r} 68 \\ \hline 20 \end{array} \quad \begin{array}{r} 81 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 42 \\ \hline 33 \end{array} \quad \begin{array}{r} 48 \\ \hline 17 \end{array} \quad 5.8 \quad \begin{array}{r} 73 \\ \hline 15 \end{array} \quad \begin{array}{r} 89 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 57 \\ \hline 33 \end{array} \quad \begin{array}{r} 64 \\ \hline 14 \end{array} \quad 7.3 \quad \begin{array}{r} 86 \\ \hline 15 \end{array} \quad \begin{array}{r} 10.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 17 \\ \hline 33 \end{array} \quad \begin{array}{r} 25 \\ \hline 15 \end{array} \quad 3.6 \quad \begin{array}{r} 50 \\ \hline 13 \end{array} \quad \begin{array}{r} 67 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 25 \\ \hline 33 \end{array} \quad \begin{array}{r} 31 \\ \hline 16 \end{array} \quad 4.0 \quad \begin{array}{r} 57 \\ \hline 18 \end{array} \quad \begin{array}{r} 73 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 44 \\ \hline 33 \end{array} \quad \begin{array}{r} 50 \\ \hline 20 \end{array} \quad 5.9 \quad \begin{array}{r} 71 \\ \hline 15 \end{array} \quad \begin{array}{r} 88 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 61 \\ \hline 33 \end{array} \quad \begin{array}{r} 67 \\ \hline 6 \end{array} \quad 8.1 \quad \begin{array}{r} 89 \\ \hline 16 \end{array} \quad \begin{array}{r} 11.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 75 \\ \hline 33 \end{array} \quad \begin{array}{r} 85 \\ \hline 15 \end{array} \quad 10.1 \quad \begin{array}{r} 119 \\ \hline 15 \end{array} \quad \begin{array}{r} 14.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 70 \\ \hline 33 \end{array} \quad \begin{array}{r} 81 \\ \hline 17 \end{array} \quad 9.5 \quad \begin{array}{r} 113 \\ \hline 15 \end{array} \quad \begin{array}{r} 133 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 57 \\ \hline 33 \end{array} \quad \begin{array}{r} 64 \\ \hline 19 \end{array} \quad 8.1 \quad \begin{array}{r} 10.1 \\ \hline 20 \end{array} \quad \begin{array}{r} 11.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 58 \\ \hline 33 \end{array} \quad \begin{array}{r} 59 \\ \hline 20 \end{array} \quad 6.0 \quad \begin{array}{r} 67 \\ \hline 13 \end{array} \quad \begin{array}{r} 9.4 \\ \hline 33 \end{array}$$

933.28

239 + 50

930.4.

240

30.4.

+ 50

29.6.

241

29.1.

+ 50

29.1.

242

28.9.

+ 50

29.3.

243

6.25 936.13

3.40 929.88

29.1.

+ 50

30.1.

244

28.7.

+ 50

27.4.

245

926.2.

$$\begin{array}{r} 2.0 \\ \hline 33 \end{array} \quad \begin{array}{r} 2.5 \\ \hline 15 \end{array} \quad 2.9 \quad \begin{array}{r} 3.3 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 2.3 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.0 \\ \hline 16 \end{array} \quad 2.9 \quad \begin{array}{r} 3.5 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 2.8 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.2 \\ \hline 14 \end{array} \quad 3.7 \quad \begin{array}{r} 4.3 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.2 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.5 \\ \hline 16 \end{array} \quad 4.2 \quad \begin{array}{r} 4.4 \\ \hline 18 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.7 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.2 \\ \hline 17 \end{array} \quad 4.2 \quad \begin{array}{r} 4.9 \\ \hline 18 \end{array} \quad \begin{array}{r} 5.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.9 \\ \hline 33 \end{array} \quad \begin{array}{r} 4.5 \\ \hline 18 \end{array} \quad 4.4 \quad \begin{array}{r} 4.6 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.6 \\ \hline 17 \end{array} \quad 4.0 \quad \begin{array}{r} 4.3 \\ \hline 15 \end{array} \quad \begin{array}{r} 5.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline 33 \end{array} \quad \begin{array}{r} 3.6 \\ \hline 19 \end{array} \quad \begin{array}{r} 4.0 \\ \hline 12 \end{array} \quad 4.2 \quad \begin{array}{r} 4.1 \\ \hline 16 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline 33 \end{array} \quad \begin{array}{r} 6.0 \\ \hline 20 \end{array} \quad 6.0 \quad \begin{array}{r} 7.1 \\ \hline 15 \end{array} \quad \begin{array}{r} 8.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 7.0 \\ \hline 20 \end{array} \quad 7.4 \quad \begin{array}{r} 8.1 \\ \hline 17 \end{array} \quad \begin{array}{r} 8.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 8.0 \\ \hline 33 \end{array} \quad \begin{array}{r} 8.2 \\ \hline 20 \end{array} \quad 8.7 \quad \begin{array}{r} 8.8 \\ \hline 19 \end{array} \quad \begin{array}{r} 9.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 9.2 \\ \hline 33 \end{array} \quad \begin{array}{r} 9.7 \\ \hline 20 \end{array} \quad 9.9 \quad \begin{array}{r} 10.0 \\ \hline 24 \end{array} \quad \begin{array}{r} 10.2 \\ \hline 33 \end{array}$$

936.13

245 + 50

924.5

245

0.14

926.92

935

926.78

246

22.1

+50

18.9

247

16.2

4.35

919.77

11.30

915.62

+50

15.8

248

13.9

+50

14.9

249

16.1

+25

13.8

+50

14.1

250

14.1

+6409 P.T.

913.5

B.M.

4.38

915.59

L E R

$\frac{11.3}{33}$ $\frac{11.5}{16}$ 11.6 $\frac{11.6}{25}$ $\frac{11.6}{33}$

$\frac{4.8}{33}$ $\frac{4.8}{15}$ 4.8 $\frac{4.8}{15}$ $\frac{4.8}{33}$

$\frac{9.9}{33}$ $\frac{9.0}{16}$ 8.0 $\frac{6.2}{18}$ $\frac{5.9}{33}$

$\frac{12.6}{33}$ $\frac{11.6}{17}$ 10.7 $\frac{9.7}{17}$ $\frac{9.6}{33}$

$\frac{6.9}{33}$ $\frac{6.2}{15}$ 4.2 $\frac{4.2}{16}$ $\frac{3.8}{33}$

$\frac{7.2}{33}$ $\frac{6.9}{15}$ 6.1 $\frac{4.9}{17}$ $\frac{4.1}{33}$

$\frac{6.5}{33}$ $\frac{6.7}{31}$ $\frac{6.6}{28}$ $\frac{5.5}{22}$ $\frac{5.2}{14}$ 5.1 $\frac{4.6}{16}$ $\frac{3.8}{33}$

$\frac{5.3}{33}$ $\frac{5.3}{29}$ $\frac{5.8}{12}$ $\frac{5.6}{0.8}$ $\frac{5.0}{0.4}$ 5.9 $\frac{2.9}{0.6}$ $\frac{2.7}{15}$ $\frac{2.7}{33}$

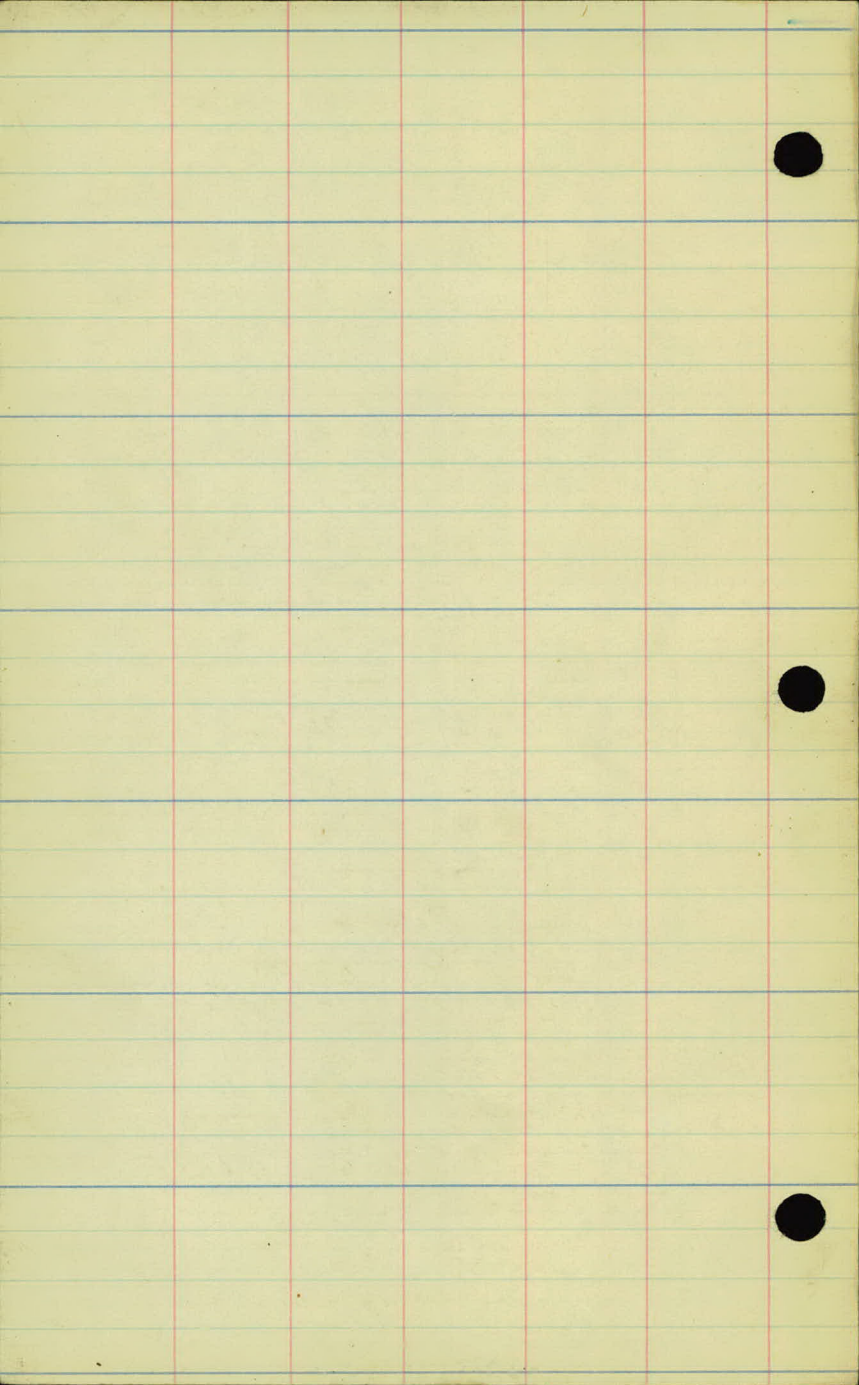
$\frac{5.5}{33}$ $\frac{5.4}{27}$ $\frac{5.4}{17}$ $\frac{5.9}{0.3}$ 6.2 $\frac{2.2}{10}$ $\frac{1.6}{20}$ $\frac{1.5}{33}$

$\frac{5.9}{33}$ $\frac{5.5}{21}$ $\frac{5.5}{11}$ 5.9 $\frac{6.2}{0.3}$ $\frac{5.4}{0.6}$ $\frac{1.5}{1.3}$ $\frac{1.2}{21}$ $\frac{1.4}{33}$

$\frac{1.8}{33}$ $\frac{6.0}{26}$ $\frac{6.5}{21}$ $\frac{5.9}{10}$ 5.9 $\frac{6.0}{0.4}$ $\frac{6.4}{10}$ $\frac{5.9}{15}$ $\frac{0.8}{23}$ $\frac{0.0}{33}$

$\frac{0.0}{33}$ $\frac{0.0}{26}$ $\frac{6.4}{17}$ $\frac{7.1}{13}$ $\frac{6.6}{0.6}$ 6.5 $\frac{6.5}{0.6}$ $\frac{7.0}{14}$ $\frac{6.0}{18}$ $\frac{1.4}{25}$ $\frac{1.0}{33}$

T.P. Sta. 249+00-50'L



1-10-27

Cleveland Ave
Cross sections
Sta. 250+64.89 to 264+45.6

partly
Wilshusen
Kooqun
Berthraime
Messenburg

Station	+	H.I.	-	Elev
B.M	7.78	923.37		915.59
251+00				130
+50				12.3
252+00				11.4
+50				10.7
253+00				10.0
T.P.	0.72	912.48	11.61	911.76
+50				09.0
254+00				8.2
+50				7.4
255+00				06.7
+50				06.3
256+00				05.9
T.P.	4.48	910.27	6.69	905.79
+50				5.6

Lt

Rt

Rt

R.R. SPIKE ON T.P. 50' N. 37. 249+00.

3.4	3.4	10.4	10.6	10.5	10.4	7.2	8.0	8.0
33	27	15	10	10.4	11	15	20	26

3.7	3.8	11.3	11.5	11.5	11.3	8.0	8.5	8.6
33	28	16	10	11.1	11	17	24	28

4.0	4.0	12.0	12.0	12.4	12.4	10.0	4.8	4.9
33	29	15	9	14.0	13	15	22	29

5.0	5.0	13.2	13.1	13.0	13.0	10.4	6.0	6.1
33	29	16	12	12.7	13	17	24	29

5.0	11.7	14.0	13.7	13.7	13.7	11.7	8.0	7.8
33	27	15	11	13.4	11	16	22	28

2.3	1.9	3.3	4.3	3.7	3.4	4.3	4.6	4.0	3.7	1.1
33	25	18	14	10	3.5	10	15	16	18	24

1.5	6.1	5.2	4.3	4.5	10.3
33	23	13	12	12	33

12.4	11.8	7.2	8.6	5.2	14.3
33	24	16	12	5.1	12

15.0	12.8	6.3	6.0	16.3
33	21	12	5.8	12

15.8	15.3	8.5	6.6	6.4	16.8
33	25	15	11	6.2	12

17.2	13.3	7.0	6.6	16.5
33	22	12	6.6	12

16.0	6.0	8.1	6.0	14.7
33	15	12	4.7	12

Station + H. 1 - Elev.

91027

257+00 53

+44 53

+76 53

258+00 53

+50 56

259+00 59

+50 62

260+00 68

+50 77

261+00 85

T.P. 8.50 917.94 * 0.83 909.44.

+50 96

262+00 10.9

1-10-12
 W/1570307
 D.S.
 A.B.
 (M.M.)

140 137 54 5.2 12.2 120
 33 26 12 6.0 7.2 24 33

116 115 53 5.3 12.0 130
 33 26 15 5.0 12 24 33

110 64 54 5.2 10.4 120
 33 29 15 5.0 12 24 33

62 60 53 5.2 7.0 82
 33 22 13 5.0 7.2 19 33

53 51 63 63 58 53 55 92 120
 33 28 26 23 21 14 47 12 18 33

54 53 58 56 50 46 70 10.4
 33 28 24 20 14 11 16 33

5.6 55 55 55 45 45 6.1 9.4
 33 29 26 24 14 4.1 10 15 33

56 50 48 38 35 37 80 75
 33 28 24 14 25 10 23 33

48 38 38 35 3.2 2.6 7.0 6.2
 33 27 24 22 15 2.6 10 2.2 33

38 2.4 2.2 1.8 16.2 2.0 6.6 7.0
 33 26 15 8 10 16 25 33

9.2 9.6 8.7 8.5 13.4 18.7
 33 23 14 13 23 33

7.8 7.0 7.4 7.1 7.5 11.4 12.4
 33 21 13 7.0 10 15 24 33

Station + M. - 12/01

917.94

+50 12.4

263+00 140

T.P. 8.17 924.57 154 916.40

+50 15.8

B.M. 4.62 919.95 919.94

264+00 17.8

+22 18.8

+22 18.8

B.M. 4.62 924.56 919.94

+45.6 End of Survey 19.31

265+45.6

266+45.6

267+45.6

268+45.6

lt. A Rt.

24 46 54 54 58 57 62 64 64
33 28 24 20 12 55 10 17 25 33

no 050 33 27 42 39 38 23
33 32 25 20 12 39 10 18 33

28 85 87 70 91 100 87 46 28
33 25 18 13 88 9 16 17 23 33

T.P.W.

R.R. Spike in T.P. 50' lt. Sta. 249+00 T.P.W.
12 67 67 70 68 70 75 82 70 33 30 98
33 24 18 11 68 10 14 15 17 78 22 29 33

30 56 5.6 5.9 5.8 5.8 5.8 5.8 2.8 2.8
33 12 16 10' 5.8 11 12 22 22 33

P.V.

P.V.

T.P.W.

? 2.0 36 5.6 5.9 5.8 5.8 5.8 2.8 2.8
33 23 10 10 5.8 11 22 33 ?

P.V.

P.V.

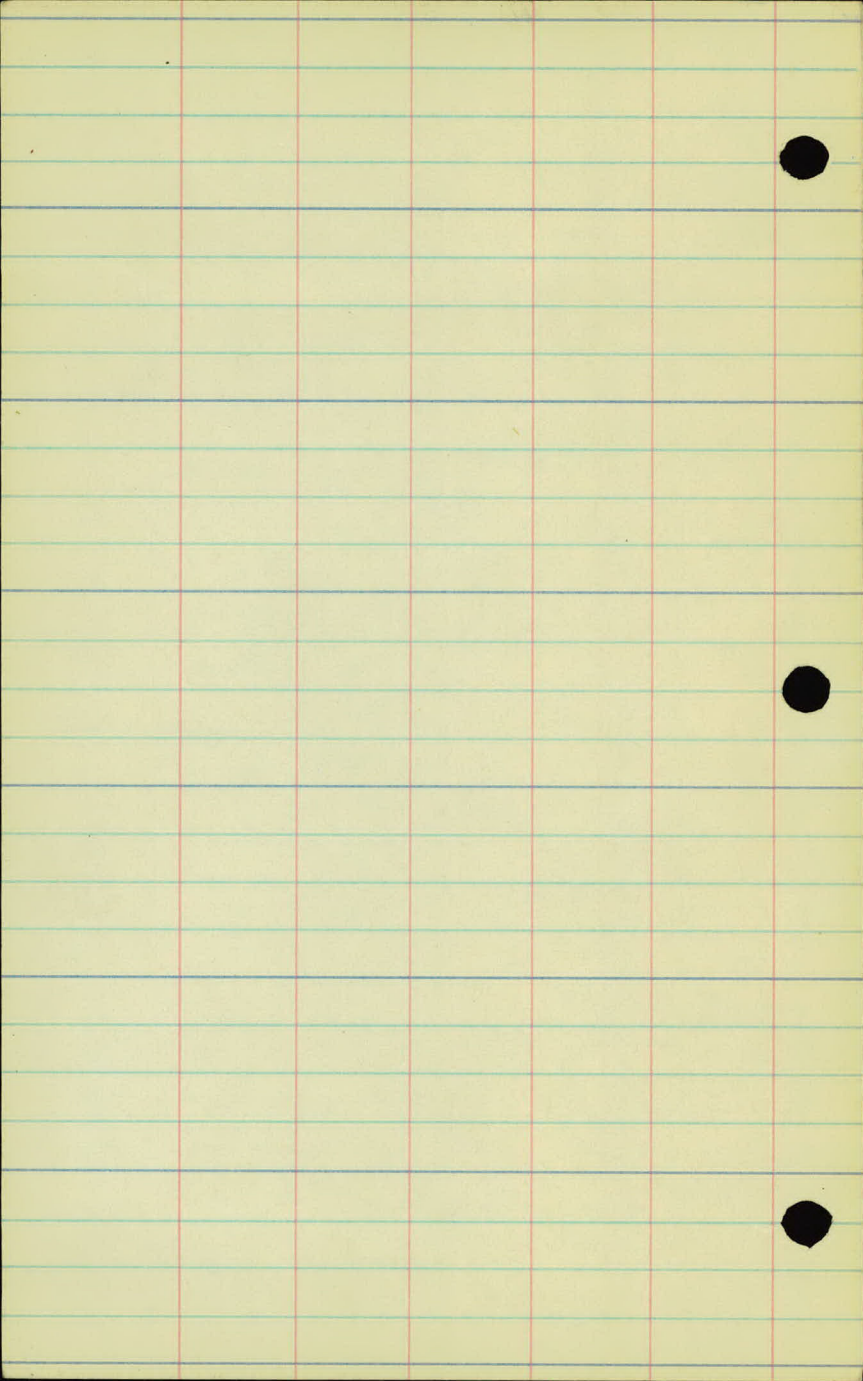
R.R. Spike in T.P. 50' lt. Sta. 249+00
47 P.V. 5.32 P.V. 3.35 2.55
33 10 5.35 200' 300'
P.V. P.V.

P.V.
6.25

P.V.
7.60

P.V.
9.25

P.V.
10.95



1-8-27

Cleveland Ave
& Levels
Sta. 260+64.89 to 264+45 $\frac{1}{2}$

Wilshusen
D.S.
A.B
A.M

Station	+	H.I.	-	Elev.
B.M.	3.07	918.66		915.59
250+64.89			5.2	
251+00			5.6	
+50			6.4	
252+00			7.2	
+50			8.0	
253+00			8.8	
+50			9.6	
254+00			10.6	
+50			11.4	
255+00			12.1	
T.P.	3.64	910.31	11.99	906.67
+50			4.0	
256+00			4.5	

R.R. Spike in T.P. 56' Lt. Sta. 249+00

Station	+	H.I.	-	Elev.
		910.21		
	+50		4.8	
257+00			5.0	
	+50		5.1	
258+00			5.1	
	+50		4.7	
259+00			4.5	
	+50		4.2	
260+00			3.7	
	+50		2.8	
261+00			1.8	
	+50		0.80	
T.P.	12.05	922.99	0.87	909.44
262+00			11.6	
	+50		10.1	



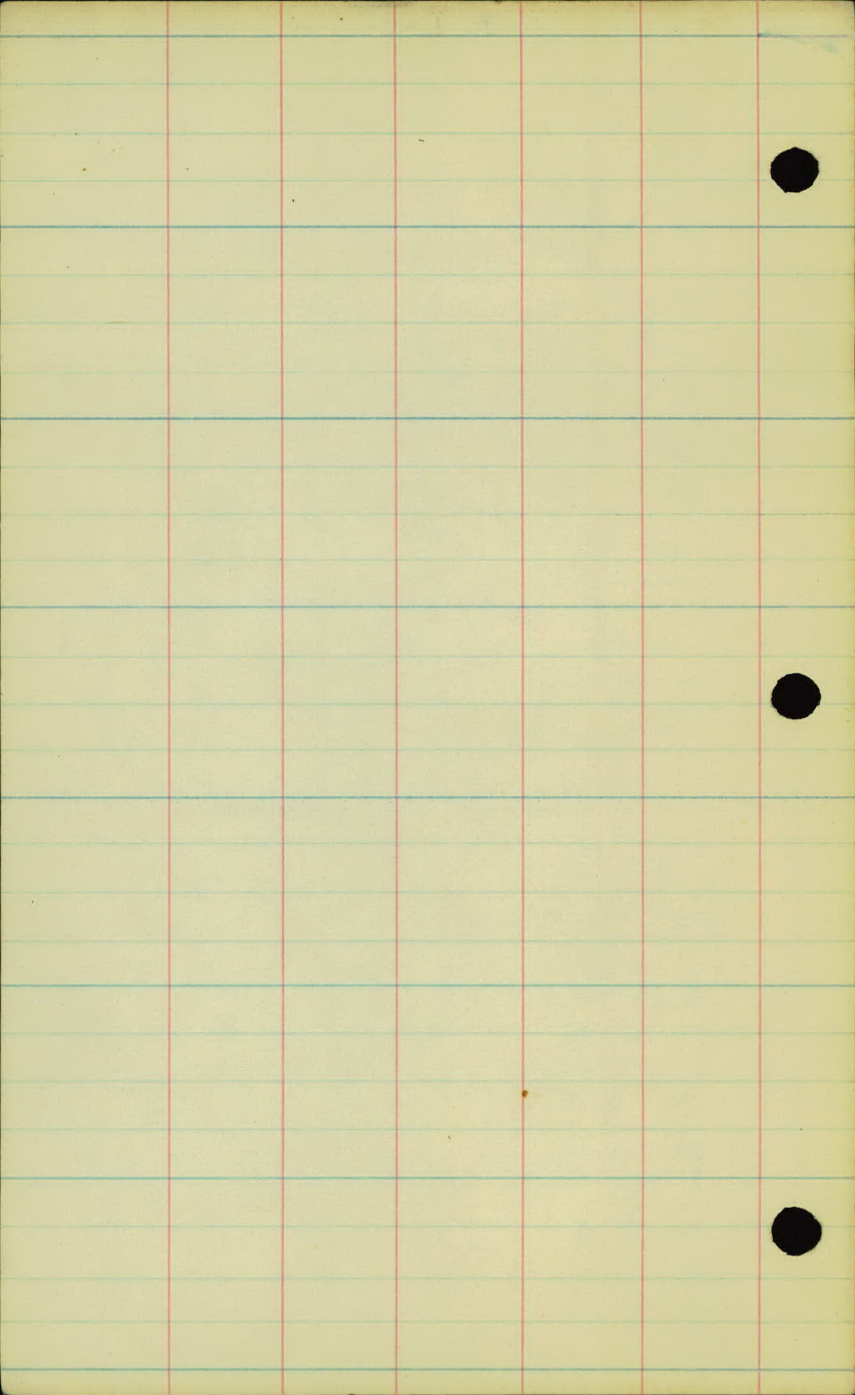
Station	+	H.I.	-	Elev.
		922.49		
263+00			8.5	
+50			6.8	
264+00			4.9	
B.M.			2.55	919.94
+15 5	Edge Pav		4.0	
+45 5			^{Pav} 3.15	
B.M.	4.68	924.62		919.94
264+45 5				
265+00			^{Pav.} 5.84	
266+00			^{Pav.} 7.03	

1-8-27

Wilshusen
Stooglen
Berthigume

R.R. Spike in P.P. 15' H. Sta. 264 + 180

"	"	ant.	rod.	rod. H	"	"
		52	3.5	5.35	4.47	3.47
		100'	50'	16'	100'	200'
		Readings Top	rod.	N.B. Rd.		



2-19-27 FAIR-COLD

A.W. LINDAHL
A.L. PERSONS
W.G. ALEXANDER
E.T. SINCLAIR

PROJ. 27-05
CLEVELAND AVE.

T. 30N., -R. 23W.



13'-0" P.I. (NAIL)

49'-52"

O.P.P.

355.78'

0°-52'

P.I. (NAIL)

NAIL IN WHEEL GUARD

19'-15"

19'-30"

NAIL IN WHEEL GUARD

SEC. 29

SOD LINE BRIDGE

SEC. 28

3 NAILS IN WHEEL GUARD

9.21'

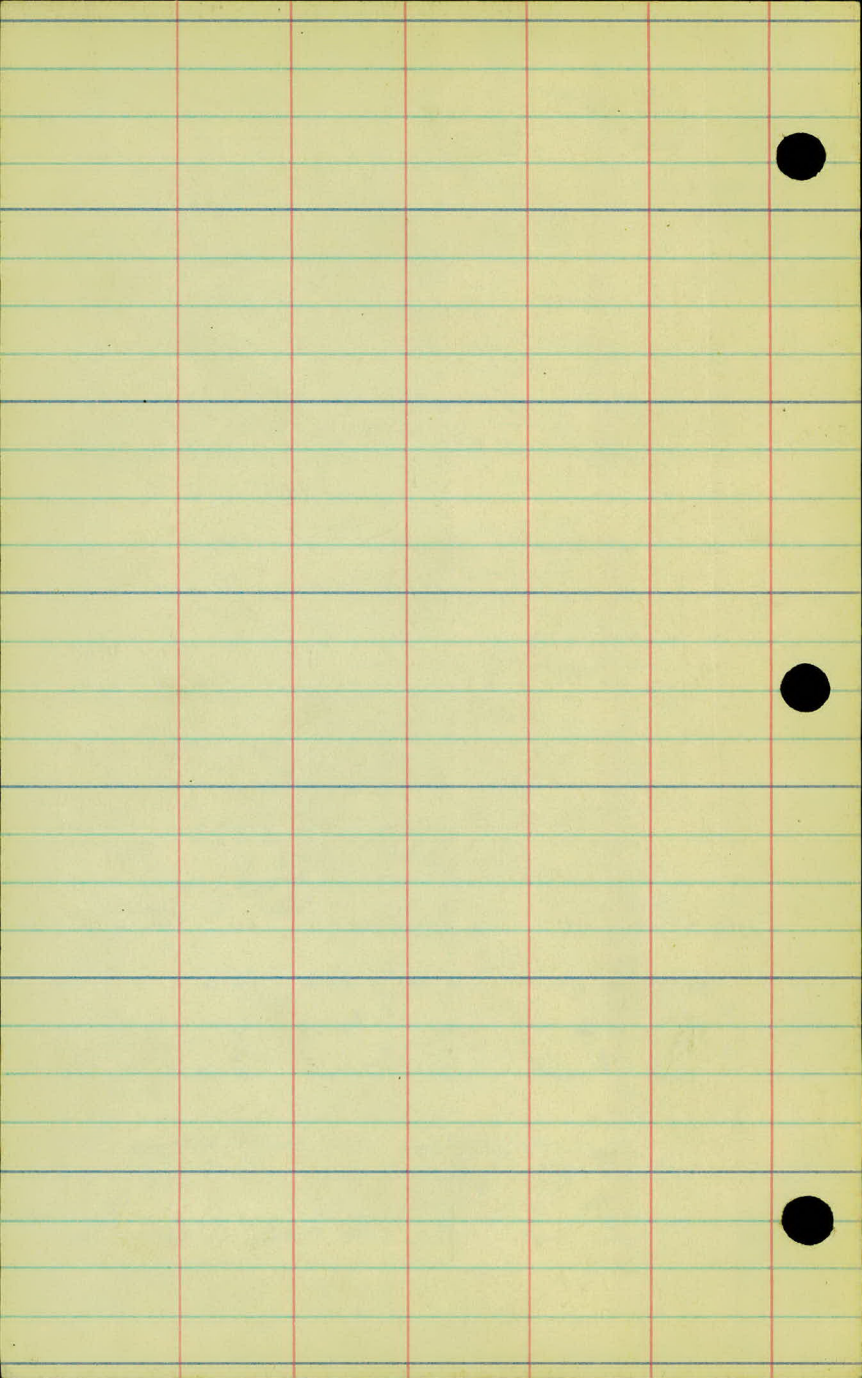
14.61'

3 NAILS IN WHEEL GUARD

SEC. 32

SEC. MONIT. (5 NAILS)

SEC. 33



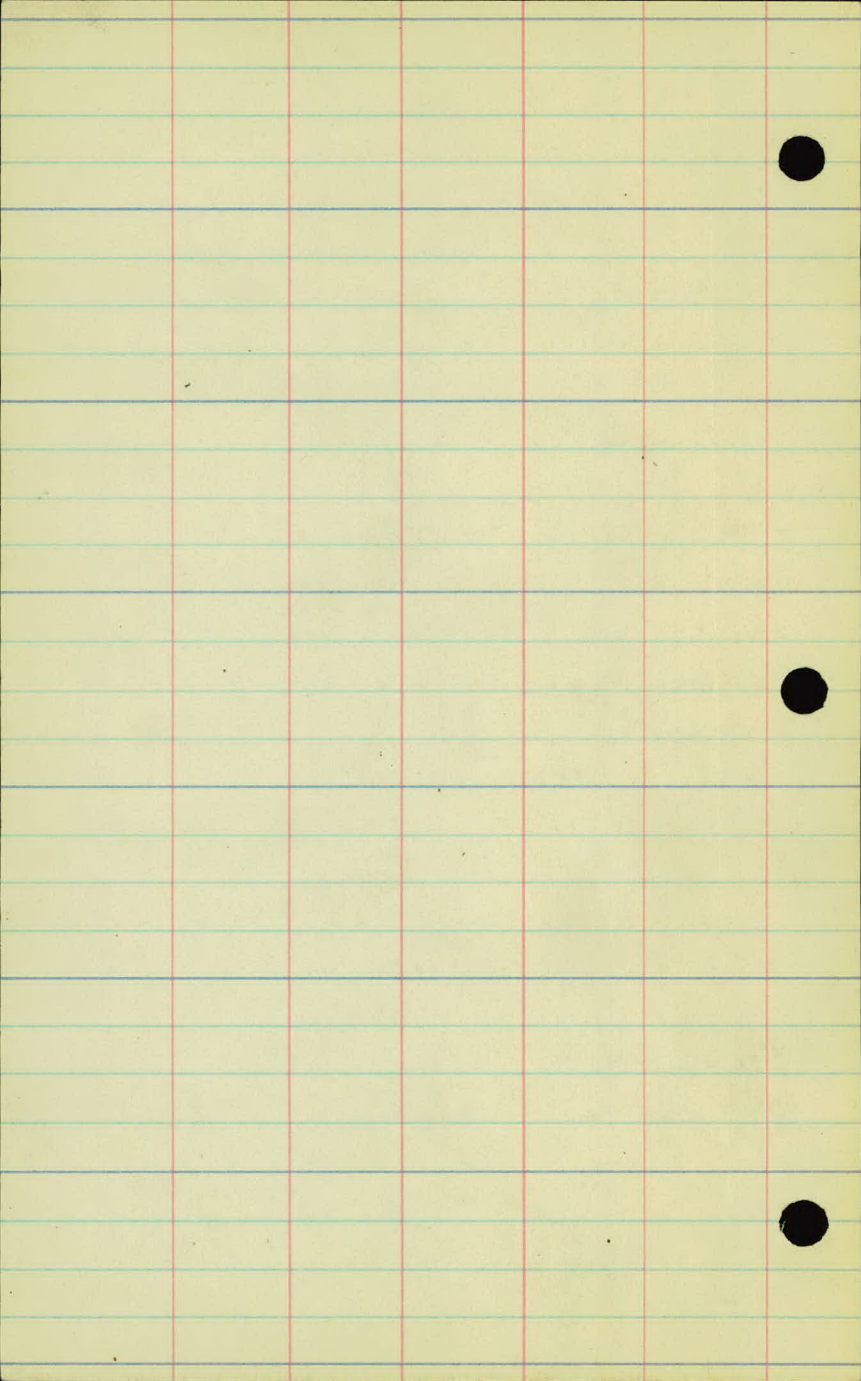
~ PROJ. 27-05 ~

~ CLEVELAND AVENUE ~

Plans in hand inspection - 2-24-27

O.R. Van Krevelen
W.S. Mackintosh
H.J. Goldberg

- ✓ 227+75 to 230+00 - Lt - Remove and replace guard rail.
Rt - Leave guard rail in place
 - ✓ 230+10 - F.E. - Rt - No culv. req.
 - ✓ 237+50 - P. 24" P₃
 - ✓ 237+00 to 239+00 - Cl. 17 trees Gr. 19 Trees
 - ✓ 236+75 to 238+75 - Rt - Guard rail
 - ✓ 238+50 - F.E. - Lt - No culv. req.
 - ✓ 240+00 - F.E. - Rt - P. 15" x 24' C.M.
 - ✓ 248+00 - P. 24" P₃
 - ✓ 246+25 to 248+75 - Lt - Guard rail
 - ✓ 248+80 - F.E. - Rt - P. 15" x 24' C.M.
 - ✓ 249+10 - " - Lt - No culv. req.
 - ✓ 253+60 - " - Rt - P. 15" x 24' C.M.
 - ✓ 253+85 - " - Lt - P. 15" x 24' C.M.
 - ✓ 253+75 to 257+75 - Lt - Guard rail
 - ✓ 253+75 to 258+00 - Rt - " "
- END PROJ. AT 258+00.



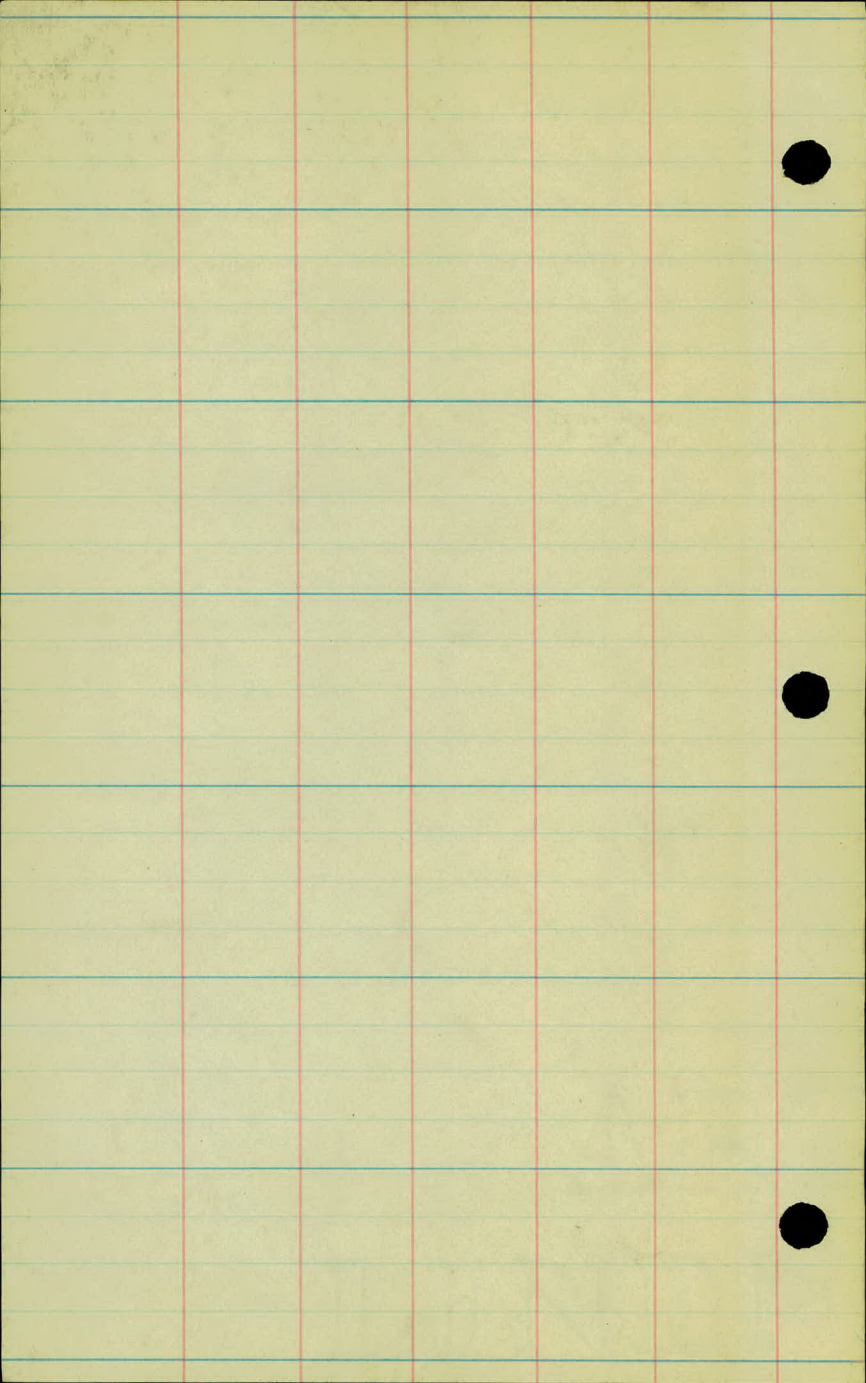
CLEVELAND AVE.

Prop. 27-05.

Plans in hand inspection. 4-26-27

O.R.I.K.
W.S.M.

- ✓ 0+00 to 1+80 - Rt+Lt - Remove + Replace G.R. 351'
- ✓ 2+45 - Rt+Lt - No culv's. req.
- ✓ 2+50 to 4+50 - Cl. 5 Trees Gr. 6 Trees
- ✓ 5+00 - F.E. Rt. - No culv. req.
- ✓ 7+25 - P. 24" P₃
- ✓ 6+75 + 8+00 G.R. Lt
- ✓ 6+75 to 9+75 - G.R. - Rt.
- ✓ 9+00 to 12+00 - Cl. 4 Trees Gr. 6 Trees.
- ✓ 11+73 - F.E. - Rt. + Lt. - No culv's. req.
- ✓ 12+00 to 15+50 - Cl. + Gr. 10 Trees
- ✓ 17+00 to 20+00 G.R. ~~Rt~~ + Lt.
- ✓ 19+00 - P. 24" P₃
- ✓ 20+75 - F.E. Lt. - P. 15' x 24' C.M.
- ✓ 25+75 - F.E. Rt. - No culv. req.
- ✓ 26+29 - " Lt. - " " " "
- ✓ 30+75 - F.E. Rt. - P. 15' x 24' C.M.
- ✓ 31+00 - " Lt. " " " "
- ✓ 31+25 to 35+02 - G.R. - Rt. + Lt.



U2496