

PLANS SURVEY

EAST COUNTY LINE

From N. St. Paul Rd. to County Road "E"

RAMSEY COUNTY PROJ. 27-04

Road $\frac{3}{4}$ N^o 4

File N^o 12

1/4/27

12

EAST COUNTY LIND ROAD

From No. St. Paul Road to Co. Road E

PROJ. - 27-04

INDEX

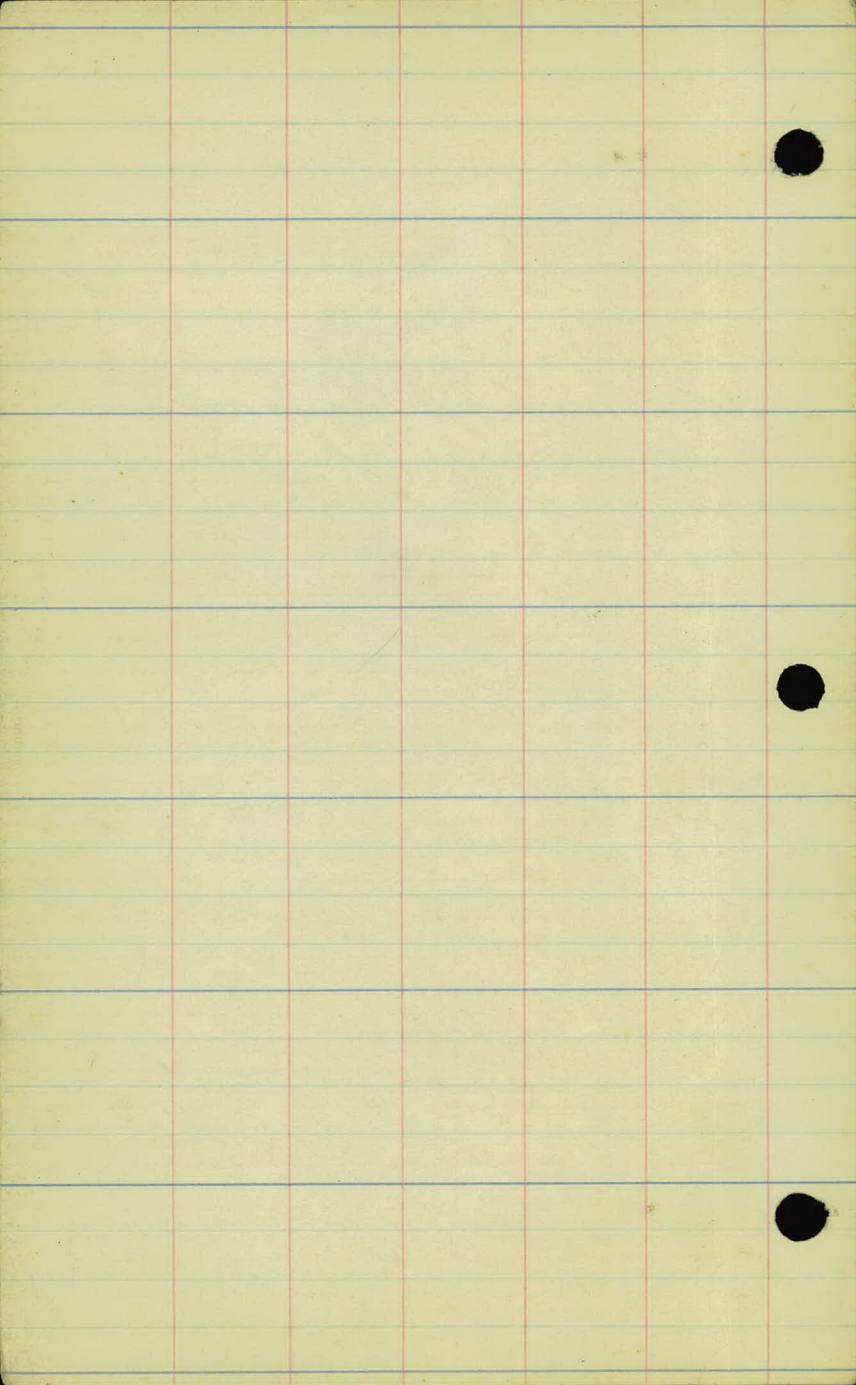
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December 27, 1926
Wm. Carlsoff

Division of Highways
State of Michigan
Date Filed
File No. 1-4-27
12
ENGINEER

27-04

12-9-26
KDC



Alignment.

station 379 - station 503+23.7

Station	Point	Lt.	A	Rt.	Bear.
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389+93 Σ	P.O.T.				
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379+00 $^{\circ}$	P.O.T.				
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N. 0° 55' 44"

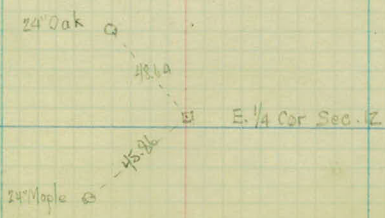
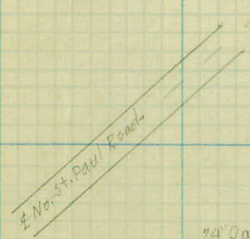
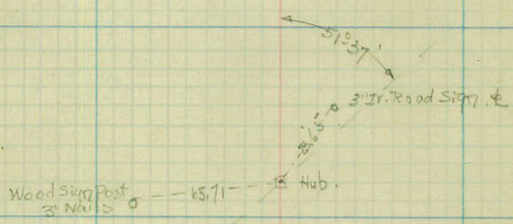
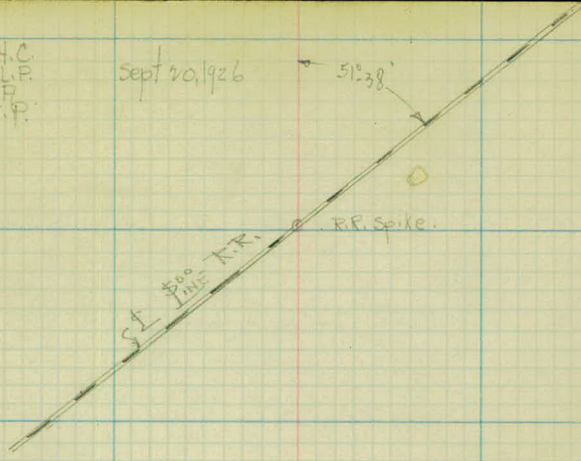
370+08 Σ					
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^A
(Road Map Stationing)

□

W.H.C.
F.L.P.
W.P.P.
H.T.P.

Sept 20, 1926



E. 1/4 Cor Sec. 2

Station	Point	Lt. Δ Rt.	Bear.
417 35.16	P.T.	14° 37'	N. 30° 15' E.
417		12° 30.4'	12° C.B.
+50		9° 30.4'	Δ 29° 14'
416		6° 30.4'	P.I. 416 + 163
+50		3° 30.4'	T. 124.75
415		0° 30.4'	L. 243.61
414 + 91.55	P.C.	0° 00'	R. 478.34

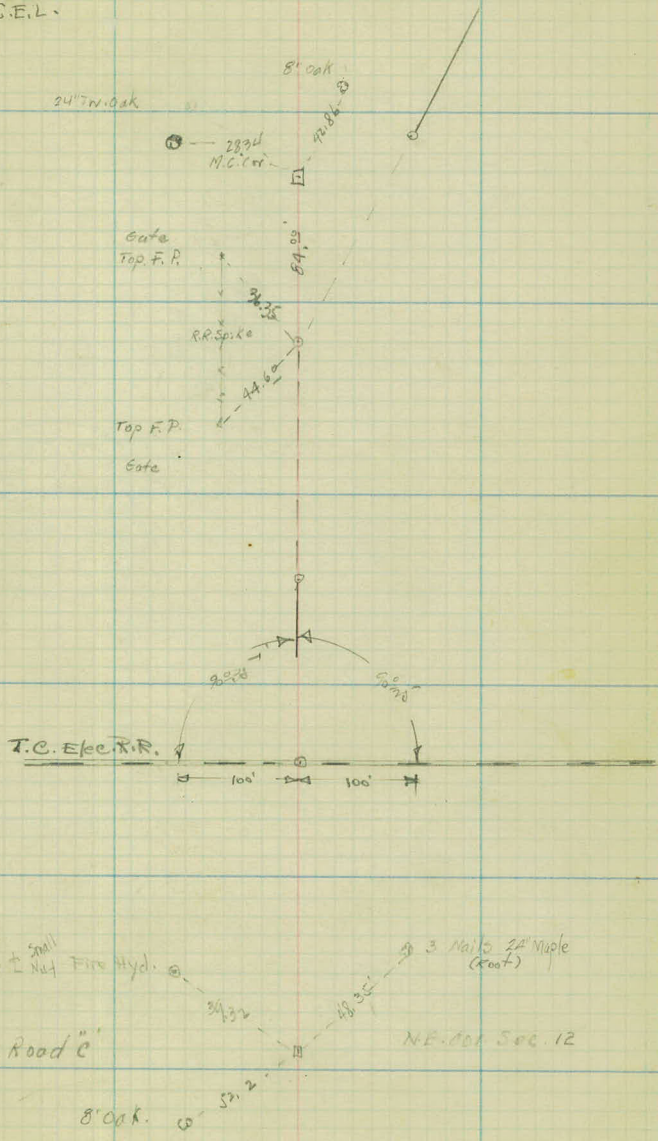
400 + 04.9 P.O.T.

396 + 39.4 P.I. 17017.

N. 12° 01' E.
N. 0° 53' E.

W.H.C.
A.B.
A.L.
R.R.
C.E.L.

Nov. 23, 1926



Station Point Lt. Δ Rt. Year.

429+93.08 P.T. 12°29'

N. 0°09' E. 11

429 11°09.6

8° C. Pt

+50 9°09.6

Δ 29°58'

428 7°09.6

P.I. 427+79.7

+50 5°09.6

T. 158.70

427 3°09.6

L. 312.08

+50 1°09.6

R. 716.78

426+21.20 P.C. 0°00'

N. 23°59' W. 1

423+30.79 P.T. 27°07'

1

423 24°48.4

15° C. Lt.

+50 21°03.4

Δ 54°14'

422 17°18.4

P.I. 421+65.4

+50 13°33.4

T. 196.16

421 9°48.4

L. 361.55

+50 6°03.4

R. 383.06

420 2°18.9'

419+69.24 P.C. 0°00'

N. 30°15' E. 1

33.10

38.03

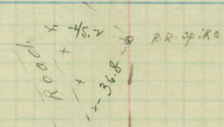
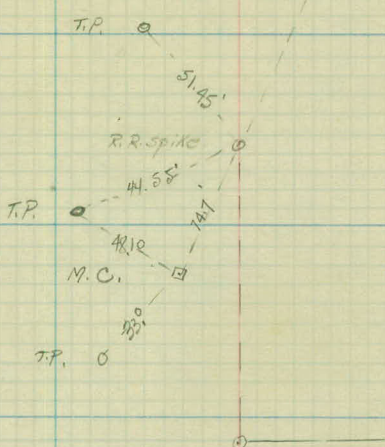
27.01

20.87

30.54

30.54

5
NOV. 24, 1926



Station Point Lt. & Rt. Bear.

503+23.10 Int. of Pavements.

489+53.7 P.O.T.

484+82.00 P.O.T.

476+84.7 P.I. Mont. 0°-02'

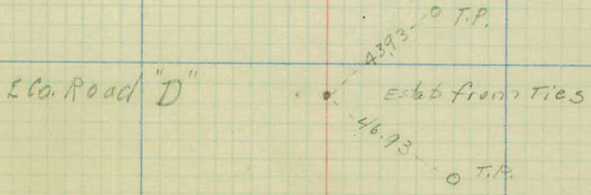
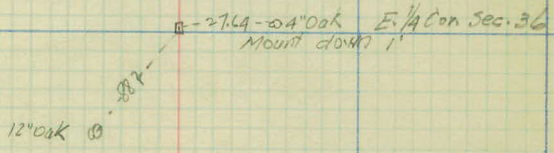
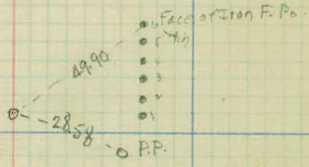
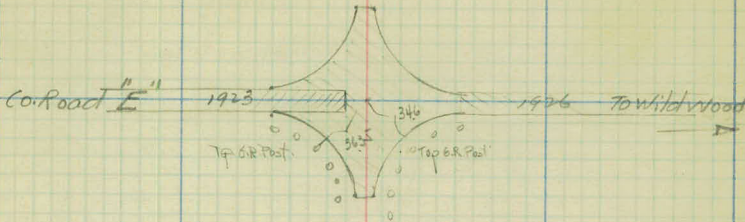
450+46.8 P.I.

0°-02'

N. 0°-59' E.

N. 1°-01' E.

N. 0°-59' E.



station

Point

Lt. & Rt.

Bear-

Levels.

W
Λ
0
H

Station	+	H.I.	-	Elev.
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Bench Levels

B.M.	4.94	996.11.		991.17
T.P.	6.47	998.89.	3.69	992.42.
✓	4.32	998.88.	4.33	994.56.
✓	5.96	1003.02.	1.82	997.06
B.M.	6.23	1002.27.	7.58	995.44

Levels

377			2.5	99.8.
+50			2.8	99.5.
378			3.2	99.1.
+40			3.9	98.9.
+60			4.1	98.2.
+80			4.0	98.3.
379			4.0	98.3.
+07.3			3.9	98.4.
+18			3.9	98.4.
380			4.8	97.5.
381			4.6	97.7.
382			5.4	96.9.
383			6.8	95.5.
T.P.	3.33	999.27.	6.33	995.94.
384			5.3	94.0.
385			5.5	93.8.
386			5.0	94.3.
387			4.6	94.7.

Station	T	H.I	-	Elev.
		999.27.		
388			5.0	94.3.
389			4.8	94.5.
T.P.	3.32	997.60.	4.99	994.28.
389+903			3.36	94.28 ⁴
+935			-	-
+96.7			3.32	94.28.
390			3.3	94.3.
391			3.7	93.9.
392			4.5	93.1.
393			5.5	92.1.
394			5.8	91.8.
395			6.1	91.5.
T.P.	4.24	995.80.	6.04	991.56.
396			4.3	91.5.
+39.4			4.0	91.8.
B.M.	6.75	997.92 ^r	4.63	991.17.
397			6.6	91.3.
398			6.2	91.7.
399			4.7	93.2.
400			3.5	94.4.
T.P.	4.70	999.75 ^r	3.37	994.55.
			4.86	94.39.
400+049			4.7	94.6.
			4.94	94.51.
401			4.6	94.7.

Top of South Rail

± ¹⁰⁰ ~~Line~~ R.R.

Top of North Rail

± County Road "C"

L.I.B.M #23 - Spike in T.P. N.E. Cor. Co. Road "C"

Top of South Rail

± Elec. R.R.

Top of North Rail

Sta	+	H.I	-	Elev.
		999.25		
402			4.9	994.4
403			5.1	94.2
T.P.	3.28	997.94 ✓	4.59	994.66 ✓
404			4.0	93.9
405			4.2	93.7
406			4.8	93.1
407			4.8	93.1
408			4.6	93.3
409			4.0	93.9
410			2.4	95.5
T.P.	11.43	1006.94 ✓	2.43	995.51 ✓
411			8.8	998.1
412			5.7	1001.2
413			2.7	04.2
T.P.	5.96	1012.56 ✓	0.34	1006.60 ✓
414			5.7	06.9
415			4.2	08.4
+50			4.2	08.4
416			5.1	07.5
+50			6.4	06.2
417			8.2	04.4
+35			9.3	03.3
B.M.	2.43	1003.55 ✓	11.44	1001.12 ✓
418			2.0	01.5
+50			3.6	1000.0

PC.

RR Spike T.P. 34 Lt. Sta. 417+90

Station	+	HI	-	Elev.
		1003.55 ✓		
419			5.5	998.1
	+69.2		8.1	95.5
420			9.0	94.6
	+50		9.4	94.2
421			10.1	93.4
	+50		10.5	93.1
T.P.	4.12	997.23 ✓	10.44	993.11 ✓
422			4.2	93.0 ✓
	+50		4.7	92.5
423			4.7	92.5
	+30.8		4.7	92.5
424			4.7	92.5
425			4.8	92.4
			13.35	983.88
426			4.8	92.4
	+50		5.2	92.0
427			6.3	90.9
	+50		6.6	90.6
428			5.5	91.7
	+50		4.0	93.2
429			2.5	94.7
	+33.08		1.3	95.9
B.M.	11.77	1004.97 ✓	4.03	993.20 ✓
430			6.8	98.2

P.C.

Top Ice Silver Lake.

P.T.

R.R. in T.P. 28' Lt 429+18

station	+	H.I	-	Elev.
		1004.97 ✓		
431			4.2	1000.8
432			1.7	03.3
T.P.	8.40	1012.71 ✓	0.66	1004.31 ✓
433			7.4	05.3
434			6.0	06.7
435			5.2	07.5
436			4.6	08.1
437			3.5	09.2
438			3.0	09.7
439			3.0	09.7
T.P.	9.74	1019.47 ✓	2.98	1009.73 ✓
B.M.	11.40	1019.47 ✓	11.40	1008.07 ✓
440			8.0	11.5
441			7.1	12.4
442			6.0	13.5
443			4.8	14.7
444			4.0	15.5
445			1.7	17.8
T.P.	12.80	1031.53 ✓	0.74	1018.73 ✓
446			9.7	21.8
447			6.3	25.2
448			2.9	28.6
449			0.2	31.3
T.P.	9.11	1040.22 ✓	0.42	1031.11 ✓
B.M.	6.00	1040.22 ✓	6.00	1034.22 ✓

R.R. in T.P. 28' Lt. Sta. 439+10

R.R. in T.P. 28' Lt. Sta. 449+63

Station	+	H.I	-	Elev.
		1040.22 ✓		
450			6.5	1033.7
+46.8			5.1	35.1
451			4.8	35.4
452			5.1	35.1
453			5.6	34.6
454			5.7	34.5
455			6.3	33.9
T.P.	0.63	1035.74 ✓	5.11	1035.11 ✓
456			3.0	32.7
457			4.8	30.9
458			5.9	29.8
459			6.2	29.5
460			6.0	29.7
T.P.	4.86	1034.57 ✓	6.03	1029.71 ✓
461			4.3	30.3
462			4.5	30.1
463			4.8	29.8
464			5.0	29.6
465			5.4	29.2
466			5.8	28.8
467			5.4	29.2
B.M.	6.75	1035.45 ✓	5.87	1028.70 ✓
468			5.6	29.9
469			5.0	30.5

P.R. spite in 12" oak 33' Lt. Sta. 467 + 50

Station	+	H.I	-	Elev.
		1035.45 ✓		
470			4.5	1031.0
471			3.8	31.7
472			3.5	32.0
473			3.5	32.0
T.P.	9.39	1041.30 ✓	3.54	1031.91 ✓
474			9.3	32.0
475			7.8	33.5
476			6.2	35.1
B.M.	5.60	1041.30 ✓	5.60	1035.70 ✓
+84.7			4.3	37.0
477			3.9	37.4
478			1.5	39.8
T.P.	11.90	1052.39 ✓	0.81	1040.49 ✓
479			10.5	41.9
480			8.7	43.7
481			5.8	46.6
482			2.9	49.5
T.P.	11.62	1063.37 ✓	0.64	1051.75 ✓
483			10.8	52.6
484			7.2	56.2
+50			5.4	58.0
485			4.7	58.7
+50			4.8	58.6
486			5.7	57.7

R.R Spike in 12" oak 40' Lt. Sta. 476+05

Station	+	H.I	-	E lev.
		1063.37 ✓		
487			7.3	1056.1
488			8.7	54.7
489			10.2	53.2
T.P.	0.71	1054.00 ✓	10.08	1053.29 ✓
	+53.7		2.4	51.6
490			4.0	50.0
491			7.7	46.3
B.M.	8.13	1054.00 ✓	8.13	1045.87 ✓
492			12.5	41.5
T.P.	0.22	1041.42 ✓	12.80	1041.20 ✓
493			4.8	36.6
494			9.7	31.7
T.P.	0.43	1028.85 ✓	13.00	1028.42 ✓
495			2.7	26.2
496			8.1	20.8
497			12.2	16.7
T.P.	0.26	1016.43 ✓	12.68	1016.17 ✓
498			3.6	12.8 ✓
499			6.8	09.6
500			10.0	06.4
501			12.6	03.8
T.P.	4.15	1007.93 ✓	12.65	1003.78 ✓
B.M.	6.34	1007.93 ✓	6.34	1001.59 ✓
502			5.3	02.6

R.R. Spike in 8" Oak 33' Rt. Sta. 490193

R.R. Spike 8" Oak 40' Rt. Sta. 500170

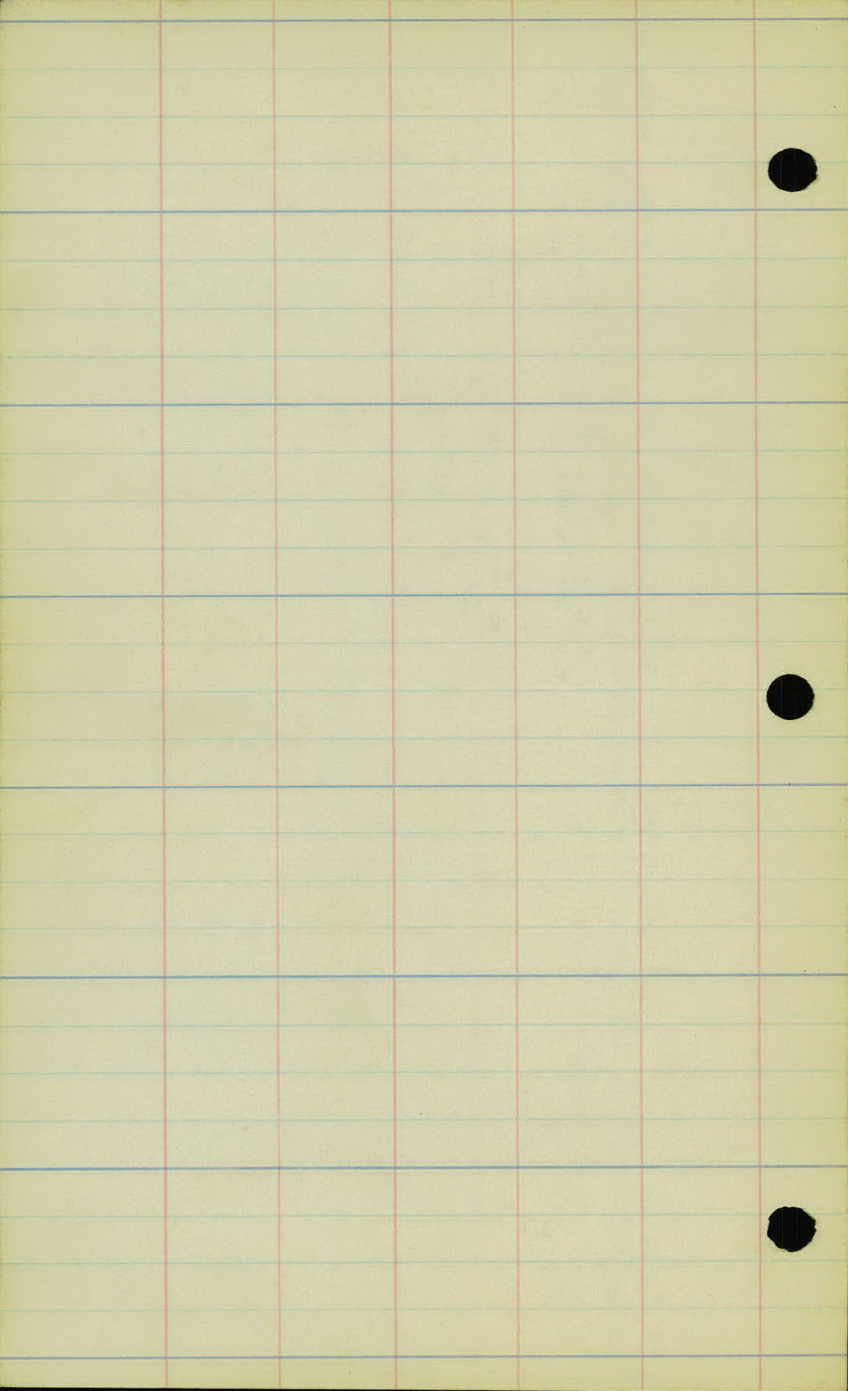
Station	+	H.I	-	Elev.
		1007.93		
502+73.7			5.62	1002.31
503+00			5.45	1002.48
503+23.7			5.40	1002.53
B.M.			1.96	1005.97

Top and base Pavement

✓ Pavement

✓ ✓ of Co. Road "E"

R.R. Spike in Top of Stump 50' N. and 100' W. of Co. Rd "E"
E. Co. Line Road. (This B.M. was used on Proj 7551)



check Levels.

	+	H.I	-	Elev.
B.M.	8.14	999.31		991.17
T.P.	3.11	997.77	4.65	994.66
✓	12.54	1008.57	1.74	996.03
B.M.	1.92	1003.04	7.45	1001.12
T.P.	3.00	997.00	9.04	994.00
B.M.	12.96	1006.19	3.77	993.23
T.P.	7.09	1012.99	0.29	1005.90
B.M.	9.86	1017.92	4.93	1008.06
T.P.	12.86	1030.72	0.56	1017.36
✓	9.84	1039.90	0.16	1030.06
B.M.	5.70	1039.90	5.70	1034.20
T.P.	0.56	1035.64	4.82	1035.08
✓	3.58	1034.37	4.85	1030.79
B.M.	6.59	1035.27	5.69	1028.68
T.P.	7.03	1038.98	3.32	1031.95
B.M.	3.29	1038.98	3.29	1035.69
T.P.	9.01	1047.49	0.50	1038.48
✓	13.02	1060.75	0.26	1047.23
✓	1.56	1057.32	4.49	1055.76
B.M.	11.48	1057.32	11.48	1045.84
T.P.	0.34	1044.64	13.02	1044.30
✓	0.12	1032.16	12.60	1032.04
✓	0.14	1019.33	12.97	1019.19
✓	1.16	1009.79	10.70	1008.63
B.M.	8.21	1009.79	8.21	1001.58
for each B.M.			3.83	1005.96

153.11

138.32

$$\begin{array}{r} 153.11 \\ - 100.32 \\ \hline 52.79 \\ \hline 14.79 \end{array}$$

L.I. B.M. #23

R.R. spike in T.P. N.E. Cor. Co. Rd. C¹

R.R. spike in T.P. 34' Lt. Sta. 417+90

R.R. spike in T.P. 28' Lt. Sta. 429+18

R.R. spike in T.P. 28' Lt. Sta. 439+10

R.R. spike in T.P. 28' Lt. Sta. 449+62

R.R. spike in 12" Oak 33' Lt. Sta. 467+50

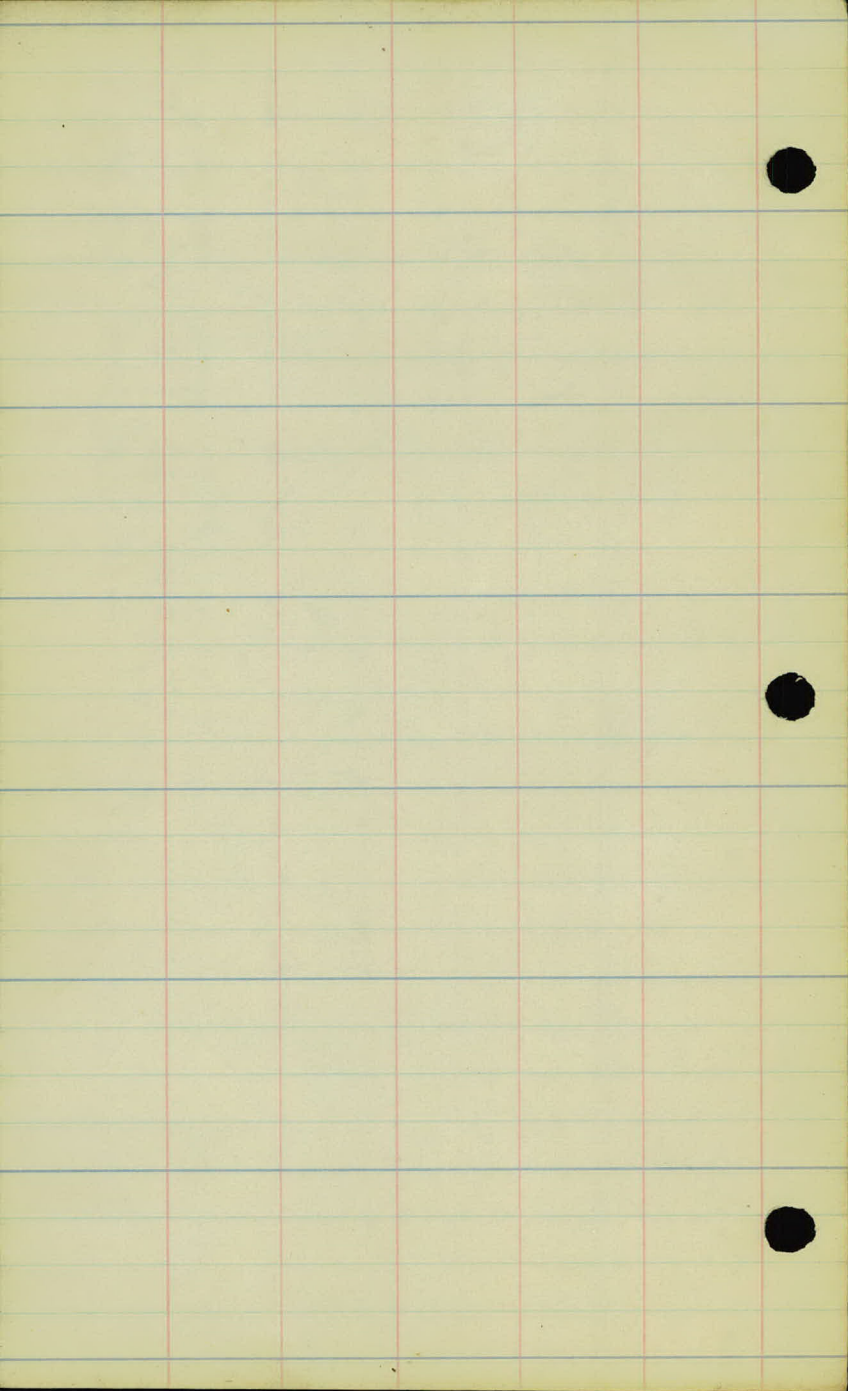
R.R. spike in 12" Oak 40' Lt. Sta. 476+05

R.R. spike in 8" Oak 33' Lt. Sta. 490+93

R.R. spike in 8" Oak 30' Rt. Sta. 500+70

R.R. spike Top Stump 30' N. and 100' W. of Co. Rd. E.

This B.M. was used on Proj 25-51



X-Sections.

station

Elev.

320+60

+02

997.7

380

97.5

+60

+03

97.8

+18

98.4

+073

98.4

379

98.3

+80

98.3

+60

98.2

+40

98.4

378

99.1

+50

99.5

377+00

999.8

W.H.C.
A.L.P.
P.R.
C.L.

Lt.

E

Rt.

40

Dec. 1926

73.1	73.1	-04	-07	01	85	-04	-20	-20	-04	+26	25
33	30	23	21	11		9	14	22	28	30	33

-06				-03	87	-03	-13	-10	+3.2	+4.2
33				15		8	11	20	26	33

-20	-20	-03	00		84	+04		+40	
33	26	16	7			15		33	

Top of curb	-18.1	-21	-03		77	+07	+1.4	+24	
	32.5	32.5	10			14	18	33	

-20	-23		07		73	+10		+20	
37.5	37.5		10.9			20		33	

-20	-23	-17	-26		78	+02		+24	
42.0	42.0	13.7	8			12		35	

-24	-28	E. edge Pav. =	1.01	-06	-02	88	-03	+1.5	+5.0	+2.0
54.5	54.5	2.5	18	10			13	28	34	37

Top of curb
Middle Pavement
E. Edge Pavement

-13	-10	-06	00		80	-02	-06	+06	+40	+8.8
40	29	17	8			10	18	25	33	35

-21	-13	-05	00		77	-0.6	+06	+3.5	+2.0
58.5	26	16	6			12	28	33	35

-1.25	-3.2	-2.9	-1.6	00	79	-0.8	-1.4	-0.6	+2.1
107	70	36	22	5		10	15	25	34

-28	-20	-05			67	-0.8	-1.6	+1.6	+1.7
33	25	13				12	15	23	33

-41	-41	-40	-40	-07	64	0.0	+20	+20	
33	28	25	23	15		19	21	33	

station Elev

386+50 +0.2 94.5

386+00 94.3

+50 +0.3 94.1

385+00 93.8

384+00 94.0

+50 -0.8 94.7

383 95.5

+85 +0.3 95.8

+60 +0.4 96.2

382+00 96.9

+50 -0.2 97.5

381+00 97.7

41.

E

rt.

41

$$\frac{+25}{37} \quad \frac{-20}{29} \quad \frac{-24}{21} \quad \frac{-0.4}{15} \quad 41$$

$$\frac{-0.6}{11} \quad \frac{-40}{20} \quad \frac{+0.5}{29} \quad \frac{+0.5}{33}$$

$$\frac{-10}{33} \quad \frac{-2.3}{27} \quad \frac{-2.2}{21} \quad \frac{-0.7}{14} \quad 43$$

$$\frac{-0.6}{11} \quad \frac{-40}{18} \quad \frac{-3.9}{24} \quad \frac{-4.6}{28} \quad \frac{-4.6}{32}$$

$$\frac{5.0}{33} \quad \frac{-4.6}{23} \quad \frac{-0.4}{14} \quad 46$$

$$\frac{-0.8}{11} \quad \frac{-3.9}{17} \quad \frac{-40}{23} \quad \frac{-3.2}{25} \quad \frac{-2.9}{33}$$

$$\frac{-5.6}{33} \quad \frac{-5.5}{24} \quad \frac{-0.3}{14} \quad 47$$

$$\frac{-0.2}{10} \quad \frac{-50}{20} \quad \frac{-4.7}{33}$$

$$\frac{-5.8}{33} \quad \frac{-5.6}{25} \quad \frac{-0.3}{13} \quad 47$$

$$\frac{-0.3}{10} \quad \frac{-4.7}{19} \quad \frac{-4.8}{33}$$

$$\frac{-5.8}{33} \quad \frac{5.6}{26} \quad \frac{-0.5}{13} \quad 40$$

$$\frac{-0.3}{11} \quad \frac{-4.9}{17} \quad \frac{-5.2}{33}$$

$$\frac{-5.5}{33} \quad \frac{-5.3}{26} \quad \frac{-0.5}{14} \quad 42$$

$$\frac{-0.4}{11} \quad \frac{-2.7}{18} \quad \frac{-3.2}{33}$$

$$\frac{-4.6}{33} \quad \frac{-4.3}{26} \quad \frac{-0.7}{14} \quad 27$$

$$\frac{-0.3}{11} \quad \frac{-1.6}{24} \quad \frac{-1.6}{33}$$

$$\frac{-3.2}{33} \quad \frac{-2.7}{25} \quad \frac{-0.7}{14} \quad 25$$

$$\frac{-0.5}{13} \quad \frac{-2.5}{19} \quad \frac{-2.4}{26} \quad \frac{-0.1}{33}$$

$$\frac{-1.2}{33} \quad \frac{-10}{18} \quad \frac{-0.3}{11} \quad 72$$

$$\frac{-0.5}{11} \quad \frac{-2.5}{17} \quad \frac{-2.2}{24} \quad \frac{+3.0}{36}$$

$$\frac{0.0}{33} \quad \frac{-0.3}{14} \quad 27$$

$$\frac{-0.7}{10} \quad \frac{-2.7}{17} \quad \frac{-2.7}{22} \quad \frac{+3.0}{33}$$

$$\frac{+21}{33} \quad \frac{+21}{28} \quad \frac{-0.4}{24} \quad \frac{-0.9}{20} \quad \frac{-0.3}{13} \quad 35$$

$$\frac{-0.5}{10} \quad \frac{-2.7}{15} \quad \frac{-2.7}{22} \quad \frac{+3.7}{31} \quad \frac{+3.7}{33}$$

station

Elev.

391+00

993.9

+60

-0.1

94.3

+75

+0.1

94.4

390

+

-

94.3

+79

+0.1

94.4

+50

0.0

94.5

389+00

+

-

94.5

+25

0.0

94.5

+35

+0.1

94.6

388+00

94.3

+50

-0.3

94.4

387+00

94.7

Lt.

Z

Rt.

42

$$\begin{array}{r} -2.7 \\ 33 \end{array} \quad \begin{array}{r} -2.2 \\ 28 \end{array} \quad \begin{array}{r} 2.7 \\ 24 \end{array} \quad \begin{array}{r} -1.2 \\ 18 \end{array} \quad \begin{array}{r} -0.6 \\ 13 \end{array}$$

47

$$\begin{array}{r} -0.6 \\ 13 \end{array} \quad \begin{array}{r} -1.7 \\ 15 \end{array} \quad \begin{array}{r} -3.0 \\ 26 \end{array} \quad \begin{array}{r} -1.7 \\ 33 \end{array}$$

$$\begin{array}{r} -4.2 \\ 33 \end{array} \quad \begin{array}{r} -3.0 \\ 18 \end{array} \quad \begin{array}{r} -0.3 \\ 12 \end{array}$$

39

$$\begin{array}{r} -0.3 \\ 12 \end{array} \quad \begin{array}{r} -1.7 \\ 15 \end{array} \quad \begin{array}{r} -2.0 \\ 33 \end{array}$$

$$\begin{array}{r} -4.0 \\ 33 \end{array} \quad \begin{array}{r} -2.8 \\ 20 \end{array} \quad \begin{array}{r} -0.3 \\ 13 \end{array}$$

37

$$\begin{array}{r} 0.0 \\ 11 \end{array} \quad \begin{array}{r} -0.8 \\ 14 \end{array} \quad \begin{array}{r} -0.9 \\ 20 \end{array} \quad \begin{array}{r} -0.3 \\ 28 \end{array} \quad \begin{array}{r} -0.5 \\ 33 \end{array}$$

$$\begin{array}{r} -3.8 \\ 33 \end{array} \quad \begin{array}{r} -3.2 \\ 21 \end{array} \quad \begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 12 \end{array}$$

39

$$\begin{array}{r} 0.0 \\ 14 \end{array} \quad \begin{array}{r} -0.2 \\ 23 \end{array} \quad \begin{array}{r} -0.7 \\ 33 \end{array}$$

$$\begin{array}{r} -1.4 \\ 33 \end{array} \quad \begin{array}{r} -0.8 \\ 15 \end{array} \quad \begin{array}{r} 0.0 \\ 9 \end{array}$$

37

$$\begin{array}{r} 0.0 \\ 13 \end{array} \quad \begin{array}{r} -0.9 \\ 15 \end{array} \quad \begin{array}{r} -1.2 \\ 25 \end{array} \quad \begin{array}{r} -0.5 \\ 27 \end{array} \quad \begin{array}{r} -0.5 \\ 33 \end{array}$$

$$\begin{array}{r} -1.9 \\ 33 \end{array} \quad \begin{array}{r} -1.4 \\ 17 \end{array} \quad \begin{array}{r} -0.2 \\ 12 \end{array}$$

38

$$\begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -1.9 \\ 16 \end{array} \quad \begin{array}{r} 1.5 \\ 23 \end{array} \quad \begin{array}{r} 1.0 \\ 27 \end{array} \quad \begin{array}{r} +2.0 \\ 33 \end{array}$$

$$\begin{array}{r} +2.0 \\ 36 \end{array} \quad \begin{array}{r} -2.0 \\ 30 \end{array} \quad \begin{array}{r} -1.3 \\ 18 \end{array} \quad \begin{array}{r} -0.3 \\ 14 \end{array}$$

33

$$\begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} -1.5 \\ 15 \end{array} \quad \begin{array}{r} 1.7 \\ 21 \end{array} \quad \begin{array}{r} +3.0 \\ 29 \end{array} \quad \begin{array}{r} +3.5 \\ 33 \end{array}$$

$$\begin{array}{r} +3.6 \\ 36 \end{array} \quad \begin{array}{r} -1.5 \\ 28 \end{array} \quad \begin{array}{r} -1.8 \\ 20 \end{array} \quad \begin{array}{r} -0.3 \\ 14 \end{array}$$

33

$$\begin{array}{r} -0.6 \\ 14 \end{array} \quad \begin{array}{r} -1.5 \\ 16 \end{array} \quad \begin{array}{r} -1.6 \\ 22 \end{array} \quad \begin{array}{r} +1.2 \\ 27 \end{array} \quad \begin{array}{r} +1.8 \\ 33 \end{array}$$

$$\begin{array}{r} -1.2 \\ 33 \end{array} \quad \begin{array}{r} -2.0 \\ 28 \end{array} \quad \begin{array}{r} -2.0 \\ 26 \end{array} \quad \begin{array}{r} -0.9 \\ 22 \end{array} \quad \begin{array}{r} -0.7 \\ 15 \end{array} \quad \begin{array}{r} -0.2 \\ 14 \end{array}$$

27

$$\begin{array}{r} -0.8 \\ 15 \end{array} \quad \begin{array}{r} -1.3 \\ 18 \end{array} \quad \begin{array}{r} -1.2 \\ 33 \end{array}$$

$$\begin{array}{r} -2.8 \\ 33 \end{array} \quad \begin{array}{r} -2.5 \\ 19 \end{array} \quad \begin{array}{r} -0.4 \\ 13 \end{array}$$

33

$$\begin{array}{r} -0.4 \\ 12 \end{array} \quad \begin{array}{r} -2.3 \\ 18 \end{array} \quad \begin{array}{r} -2.6 \\ 33 \end{array}$$

$$\begin{array}{r} -2.2 \\ 33 \end{array} \quad \begin{array}{r} -2.1 \\ 18 \end{array} \quad \begin{array}{r} -0.2 \\ 13 \end{array}$$

33

$$\begin{array}{r} -0.3 \\ 11 \end{array} \quad \begin{array}{r} -2.4 \\ 16 \end{array} \quad \begin{array}{r} -2.8 \\ 33 \end{array}$$

$$\begin{array}{r} +0.4 \\ 38 \end{array} \quad \begin{array}{r} -2.7 \\ 31 \end{array} \quad \begin{array}{r} -2.7 \\ 21 \end{array} \quad \begin{array}{r} -0.4 \\ 14 \end{array}$$

40

$$\begin{array}{r} -0.7 \\ 13 \end{array} \quad \begin{array}{r} -1.1 \\ 17 \end{array} \quad \begin{array}{r} -1.3 \\ 21 \end{array} \quad \begin{array}{r} 0.0 \\ 29 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array}$$

Station

Elev.

396+39A

91.8 Z.C.R. 0

+20

+0.1

91.6

396

91.5

+50

-0.1

91.4

395

91.5

+50

-0.3

91.5

394

91.8

+35

-0.3

91.8

393+00

92.1

+50

-0.4

92.7

392+00

93.1

391+50

+0.4

93.5

4

5

6

43

$$\frac{-0.6}{33}$$

$$\frac{-0.4}{15}$$

43

$$\frac{-0.1}{15}$$

$$\frac{-0.1}{33}$$

$$\frac{-1.4}{33}$$

$$\frac{-1.6}{25}$$

$$\frac{-0.5}{12}$$

44

$$\frac{-0.4}{17}$$

$$\frac{-1.6}{33}$$

$$\frac{-0.8}{33}$$

$$\frac{0.0}{20}$$

$$\frac{-1.6}{17}$$

$$\frac{-0.7}{12}$$

45

$$\frac{-0.4}{10}$$

$$\frac{1.8}{26}$$

$$\frac{+2.0}{33}$$

$$\frac{-1.5}{33}$$

$$\frac{-0.4}{19}$$

$$\frac{-1.5}{16}$$

$$\frac{-0.8}{11}$$

46

$$\frac{-0.5}{15}$$

$$\frac{-1.9}{20}$$

$$\frac{-2.1}{27}$$

$$\frac{+1.2}{31}$$

$$\frac{-1.2}{33}$$

$$\frac{-3.0}{33}$$

$$\frac{-2.7}{17}$$

$$\frac{-0.4}{11}$$

45

$$\frac{-0.5}{16}$$

$$\frac{-2.3}{21}$$

$$\frac{-1.2}{33}$$

$$\frac{-3.3}{33}$$

$$\frac{-2.8}{17}$$

$$\frac{-0.6}{11}$$

46

$$\frac{-0.4}{16}$$

$$\frac{-2.1}{21}$$

$$\frac{-2.0}{33}$$

$$\frac{-3.3}{33}$$

$$\frac{-2.6}{16}$$

$$\frac{-0.6}{11}$$

43

$$\frac{-0.5}{18}$$

$$\frac{-2.1}{22}$$

$$\frac{-2.2}{33}$$

$$\frac{-2.7}{33}$$

$$\frac{-2.5}{16}$$

$$\frac{-0.5}{11}$$

43

$$\frac{-0.4}{17}$$

$$\frac{-2.4}{23}$$

$$\frac{-2.9}{33}$$

$$\frac{-0.7}{33}$$

$$\frac{-0.7}{17}$$

40

$$\frac{-0.7}{17}$$

$$\frac{-2.5}{13}$$

$$\frac{-3.2}{33}$$

$$\frac{-0.8}{33}$$

$$\frac{-2.6}{22}$$

$$\frac{-2.5}{18}$$

$$\frac{-1.0}{13}$$

45

$$\frac{-0.4}{15}$$

$$\frac{-2.4}{21}$$

$$\frac{-2.8}{33}$$

$$\frac{+1.2}{33}$$

$$\frac{+0.2}{28}$$

$$\frac{-2.2}{24}$$

$$\frac{-3.3}{19}$$

$$\frac{-0.8}{14}$$

51

$$\frac{-0.9}{15}$$

$$\frac{-2.0}{19}$$

$$\frac{-2.2}{24}$$

$$\frac{-1.4}{25}$$

$$\frac{-1.2}{33}$$

$$\frac{+1.3}{33}$$

$$\frac{+1.3}{28}$$

$$\frac{-2.3}{22}$$

$$\frac{-2.0}{18}$$

$$\frac{-0.5}{13}$$

47

$$\frac{-0.7}{14}$$

$$\frac{-1.7}{17}$$

$$\frac{-2.1}{26}$$

$$\frac{-1.1}{33}$$

station

Elev.

400 +50

-0.1

994.6

+0.9

+0.2

94.7

Edge Ties

+0.3

94.51

North Rail

+0.5

994.39

South Rail

400 +00

94.4

- Edge Ties

+50

+0.5

93.7

399

93.2

+50

+0.9

92.6

398 +00

91.7

+50

+0.1

91.4

397

91.3

396 +63

+0.4

91.7

LT.						RT.
$\frac{-2.0}{33}$	$\frac{-1.1}{26}$	$\frac{-4.6}{22}$	$\frac{-4.7}{19}$	$\frac{-0.3}{13}$	12	$\frac{-0.5}{12}$ $\frac{1.4}{16}$ $\frac{-2.0}{23}$ $\frac{-0.7}{25}$ $\frac{-0.3}{33}$
$\frac{-0.5}{33}$				$\frac{-0.1}{15}$	4.1	$\frac{-0.1}{14}$ $\frac{-0.6}{38}$
$\frac{+0.7}{33}$					12.4	Rails $\frac{-0.18}{33}$
$\frac{+8.5}{33}$		Top			13.7	Rail $\frac{-0.70}{38}$
$\frac{-0.3}{38}$				$\frac{0.0}{12}$	4.4	$\frac{0.0}{12}$ $\frac{-0.5}{38}$
$\frac{-0.6}{33}$				$\frac{-0.5}{11}$	5.0	$\frac{-0.7}{12}$ $\frac{-2.7}{16}$ $\frac{-2.9}{23}$ $\frac{+0.2}{27}$ $\frac{+0.1}{33}$
$\frac{0.0}{33}$	$\frac{-0.3}{21}$	$\frac{-3.2}{19}$	$\frac{-3.2}{18}$	$\frac{-1.0}{12}$	5.5	$\frac{-0.7}{12}$ $\frac{-3.0}{17}$ $\frac{-2.8}{25}$ $\frac{+0.7}{29}$ $\frac{+0.2}{33}$
$\frac{-1.3}{33}$	$\frac{-1.3}{19}$	$\frac{-2.7}{15}$	$\frac{-0.7}{12}$		3.4	$\frac{-0.6}{13}$ $\frac{-2.4}{17}$ $\frac{-3.0}{23}$ $\frac{-2.6}{30}$ $\frac{-1.7}{33}$
$\frac{-4.1}{33}$		$\frac{-4.0}{19}$	$\frac{-0.7}{12}$		4.8	$\frac{-0.6}{13}$ $\frac{4.2}{18}$ $\frac{-0.7}{33}$
$\frac{4.6}{33}$		$\frac{-2.0}{18}$	$\frac{-0.7}{11}$		4.7	$\frac{-0.5}{12}$ $\frac{-3.0}{17}$ $\frac{-2.4}{24}$ $\frac{-3.0}{38}$
$\frac{-3.3}{33}$		$\frac{-2.3}{16}$	$\frac{-0.6}{11}$		4.6	$\frac{-0.8}{15}$ $\frac{-2.5}{21}$ $\frac{-2.7}{31}$ $\frac{-0.5}{36}$
$\frac{-2.4}{33}$		$\frac{-1.7}{19}$	$\frac{-0.4}{11}$		4.4	$\frac{-0.4}{14}$ $\frac{-1.6}{33}$

back 4.1

station Elev.

409 99.9

408 93.3

405 -0.2 93.1

407 93.1

406 93.1

405 93.7

404 93.9

450 -0.2 94.0

403 94.2

430 -0.1 94.3

402 94.4

401 94.7

station Elev.

414+50 +0.9 1007.8

414+00 1006.9

+50 +1.6 05.8

413+00 04.2

+50 +1.6 02.8

412+00 1001.2

+40 -1.2 1000.0

+35 +1.1 99.2

411+00 98.1

410+90 +1.1 97.9

+50 +1.3 96.8

410 95.5

H. 2 RH.

$$\begin{array}{r} -07 \\ 33 \end{array} \quad \begin{array}{r} -07 \\ 26 \end{array} \quad \begin{array}{r} -04 \\ 17 \end{array} \quad 13 \quad \begin{array}{r} -02 \\ 70 \end{array} \quad \begin{array}{r} 00 \\ 16 \end{array} \quad \begin{array}{r} -06+04+08 \\ 19 \end{array} \quad \begin{array}{r} +08 \\ 22 \end{array} \quad \begin{array}{r} +08 \\ 31 \end{array} \quad \begin{array}{r} +21 \\ 33 \end{array} \quad \begin{array}{r} +21 \\ 40 \end{array}$$

$$\begin{array}{r} +11 \\ 33 \end{array} \quad \begin{array}{r} +11 \\ 37 \end{array} \quad \begin{array}{r} -12 \\ 28 \end{array} \quad \begin{array}{r} -14 \\ 28 \end{array} \quad \begin{array}{r} -06 \\ 22 \end{array} \quad 62 \quad \begin{array}{r} -02 \\ 12 \end{array} \quad \begin{array}{r} 00 \\ 19 \end{array} \quad \begin{array}{r} +12 \\ 28 \end{array} \quad \begin{array}{r} +112 \\ 34 \end{array} \quad \begin{array}{r} +112 \\ 40 \end{array}$$

$$\begin{array}{r} +05 \\ 33 \end{array} \quad \begin{array}{r} -12 \\ 31 \end{array} \quad \begin{array}{r} -10 \\ 28 \end{array} \quad \begin{array}{r} -06 \\ 22 \end{array} \quad 73 \quad \begin{array}{r} -01 \\ 12 \end{array} \quad \begin{array}{r} -04 \\ 16 \end{array} \quad \begin{array}{r} +12 \\ 28 \end{array} \quad \begin{array}{r} +144 \\ 37 \end{array} \quad \begin{array}{r} +144 \\ 45 \end{array}$$

$$\begin{array}{r} -09 \\ 33 \end{array} \quad \begin{array}{r} -03 \\ 20 \end{array} \quad 68 \quad \begin{array}{r} 00 \\ 13 \end{array} \quad \begin{array}{r} -01 \\ 15 \end{array} \quad \begin{array}{r} +06 \\ 17 \end{array} \quad \begin{array}{r} +108 \\ 34 \end{array} \quad \begin{array}{r} +120 \\ 45 \end{array}$$

$$\begin{array}{r} -10 \\ 33 \end{array} \quad \begin{array}{r} -04 \\ 20 \end{array} \quad 123 \quad \begin{array}{r} 00 \\ 11 \end{array} \quad \begin{array}{r} +05 \\ 17 \end{array} \quad \begin{array}{r} +128 \\ 33 \end{array} \quad \begin{array}{r} +120 \\ 40 \end{array}$$

$$\begin{array}{r} -21 \\ 33 \end{array} \quad \begin{array}{r} -10 \\ 27 \end{array} \quad \begin{array}{r} -09 \\ 19 \end{array} \quad 14 \quad \begin{array}{r} -01 \\ 16 \end{array} \quad \begin{array}{r} -09 \\ 21 \end{array} \quad \begin{array}{r} +85 \\ 34 \end{array} \quad \begin{array}{r} +87 \\ 40 \end{array}$$

$$\begin{array}{r} -31 \\ 33 \end{array} \quad \begin{array}{r} -05 \\ 16 \end{array} \quad 121 \quad \begin{array}{r} -03 \\ 15 \end{array} \quad \begin{array}{r} -12 \\ 21 \end{array} \quad \begin{array}{r} +57 \\ 33 \end{array}$$

$$\begin{array}{r} -46 \\ 33 \end{array} \quad \begin{array}{r} -35 \\ 22 \end{array} \quad \begin{array}{r} -07 \\ 76 \end{array} \quad 23 \quad \begin{array}{r} -04 \\ 16 \end{array} \quad \begin{array}{r} -02 \\ 33 \end{array}$$

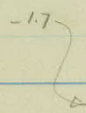
$$\begin{array}{r} -28 \\ 33 \end{array} \quad \begin{array}{r} -20 \\ 25 \end{array} \quad \begin{array}{r} -05 \\ 14 \end{array} \quad 24 \quad \begin{array}{r} -02 \\ 17 \end{array} \quad \begin{array}{r} -38 \\ 23 \end{array} \quad \begin{array}{r} -38 \\ 33 \end{array}$$

$$\begin{array}{r} -21 \\ 33 \end{array} \quad \begin{array}{r} -52 \\ 22 \end{array} \quad \begin{array}{r} -07 \\ 14 \end{array} \quad 37 \quad \begin{array}{r} -02 \\ 12 \end{array} \quad \begin{array}{r} -03 \\ 19 \end{array} \quad \begin{array}{r} -40 \\ 26 \end{array} \quad \begin{array}{r} -43 \\ 33 \end{array}$$

$$\begin{array}{r} -76 \\ 33 \end{array} \quad \begin{array}{r} -65 \\ 76 \end{array} \quad \begin{array}{r} -04 \\ 13 \end{array} \quad 62 \quad \begin{array}{r} -04 \\ 10 \end{array} \quad \begin{array}{r} -06 \\ 17 \end{array} \quad \begin{array}{r} -52 \\ 76 \end{array} \quad \begin{array}{r} -53 \\ 33 \end{array}$$

$$\begin{array}{r} -127 \\ 33 \end{array} \quad \begin{array}{r} -65 \\ 24 \end{array} \quad \begin{array}{r} -03 \\ 15 \end{array} \quad 61 \quad \begin{array}{r} -03 \\ 12 \end{array} \quad \begin{array}{r} -57 \\ 26 \end{array} \quad \begin{array}{r} -62 \\ 33 \end{array}$$

Station	Elev.
420 +50	94.2
420	94.6
+69	95.5
419	98.1
+50	1000.0 99.8
418	01.5
+35	03.3
417	04.4
+50	06.2
416+00	07.5
+50	08.4
415+00	08.4



H. Z H.

$\frac{-5.2}{33}$ $\frac{-3.2}{22}$ $\frac{-1.0}{16}$ 40 $\frac{-0.1}{15}$ $\frac{-5.1}{27}$ $\frac{-5.9}{33}$

$\frac{-5.4}{33}$ $\frac{-3.8}{21}$ $\frac{-0.1}{12}$ $\frac{-0.5}{10}$ 36 $\frac{+0.4}{7}$ $\frac{+0.4}{24}$ $\frac{-3.6}{34}$

$\frac{6.7}{33}$ $\frac{-5.7}{22}$ $\frac{+0.3}{10}$ 27 $\frac{+0.7}{9}$ $\frac{+0.5}{22}$ $\frac{+0.7}{27}$ $\frac{-0.7}{33}$ $\frac{-0.4}{39}$ $\frac{0.0}{42}$

$\frac{-8.5}{33}$ $\frac{-7.5}{24}$ $\frac{-0.1}{11}$ 11.1 $\frac{0.0}{18}$ $\frac{+0.2}{24}$ $\frac{+6.0}{31}$ $\frac{+10.3}{38}$

$\frac{-9.5}{33}$ $\frac{0.0}{17}$ 9.3 $\frac{-0.5}{14}$ $\frac{-1.0}{19}$ $\frac{+2.0}{32}$ $\frac{+6.4}{33}$

$\frac{-0.7}{33}$ $\frac{-0.7}{27}$ $\frac{-0.1}{24}$ 7.2 $\frac{-0.7}{19}$ $\frac{-0.9}{23}$ $\frac{+0.7}{27}$ $\frac{+0.4}{33}$

$\frac{+0.1}{33}$ 5.8 $\frac{-0.0}{17}$ $\frac{-1.2}{19}$ $\frac{-1.2}{21}$ $\frac{+2.8}{26}$ $\frac{+2.7}{33}$

$\frac{0.0}{33}$ $\frac{+0.2}{23}$ 4.5 $\frac{+0.2}{16}$ $\frac{-0.2}{20}$ $\frac{+3.0}{24}$ $\frac{+3.0}{33}$

$\frac{+1.6}{47}$ $\frac{-1.1}{36}$ $\frac{+0.4}{28}$ $\frac{+0.6}{12}$ 7.0 $\frac{+0.7}{12}$ $\frac{-0.7}{14}$ $\frac{-0.7}{16}$ $\frac{+3.5}{21}$ $\frac{+9.0}{33}$

$\frac{-2.2}{33}$ $\frac{-3.2}{32}$ $\frac{-2.1}{29}$ $\frac{0.0}{23}$ 5.6 $\frac{-0.1}{13}$ $\frac{-0.4}{17}$ $\frac{+4.1}{24}$ $\frac{+6.0}{26}$ $\frac{+3.0}{40}$

$\frac{-1.7}{33}$ $\frac{-1.0}{27}$ $\frac{-2.0}{26}$ $\frac{-0.1}{19}$ 1.8 $\frac{-0.6}{19}$ $\frac{+4.8}{28}$ $\frac{+7.1}{31}$ $\frac{+7.2}{40}$

$\frac{-0.3}{33}$ $\frac{-1.6}{26}$ $\frac{-0.6}{19}$ 4.3 $\frac{0.0}{13}$ $\frac{+0.2}{15}$ $\frac{+3.8}{34}$ $\frac{+2.2}{36}$ $\frac{+8.5}{40}$

station

E/ov

+76+50

92.0

476

92.1

+65

-0.1

92.3

475

92.4

+50

-0.2

92.3

424

92.5

+30.8

92.5

473

92.5

+50

92.5

422

93.0

+50

93.1

421

93.4

L. R. H.

$-\frac{3.3}{33}$	$\frac{0.0}{29}$	$+\frac{0.6}{16}$	51	$-\frac{0.7}{18}$	$-\frac{4.7}{27}$	$-\frac{5.2}{33}$				
$-\frac{4.5}{33}$	$-\frac{3.4}{23}$	$-\frac{0.3}{14}$	44	$-\frac{0.7}{15}$	$-\frac{0.7}{24}$	$-\frac{3.3}{29}$	$-\frac{3.8}{33}$			
$-\frac{4.2}{33}$	$-\frac{2.7}{18}$	$\frac{0.0}{6}$	50	$+\frac{0.3}{9}$	$-\frac{0.2}{19}$	$-\frac{0.4}{25}$	$-\frac{2.0}{33}$			
$-\frac{0.4}{33}$		$\frac{0.0}{5}$	50	$+\frac{0.3}{12}$	$-\frac{0.5}{30}$	$+\frac{1.8}{33}$				
$+\frac{0.7}{33}$	$+\frac{0.1}{15}$	$-\frac{0.6}{14}$	$-\frac{0.5}{9}$	$-\frac{0.2}{6}$	53	$+\frac{0.2}{8}$	$-\frac{0.4}{25}$	$-\frac{1.4}{28}$	$-\frac{1.4}{30}$	$-\frac{0.7}{33}$
$\frac{0.0}{33}$	$\frac{0.0}{24}$	$-\frac{1.0}{20}$	$-\frac{1.0}{17}$	$-\frac{0.5}{13}$	46	$-\frac{0.4}{21}$	$-\frac{1.1}{23}$	$-\frac{1.1}{33}$		
$-\frac{0.7}{33}$	$-\frac{1.6}{25}$	$-\frac{0.4}{21}$	$+\frac{0.1}{7}$	46	$-\frac{0.2}{9}$	$-\frac{1.3}{14}$	$-\frac{2.4}{33}$			
$-\frac{0.3}{33}$	$-\frac{1.6}{29}$	$-\frac{1.5}{16}$	$-\frac{0.6}{23}$	$+\frac{0.1}{10}$	51	$-\frac{0.5}{6}$	$-\frac{1.8}{10}$	$-\frac{3.0}{26}$	$-\frac{3.9}{33}$	
$-\frac{1.3}{33}$	$-\frac{0.8}{28}$	$+\frac{0.2}{11}$	46	$\frac{0.0}{6}$	$-\frac{3.0}{13}$	$-\frac{3.8}{33}$				
$-\frac{1.5}{33}$	$-\frac{0.7}{27}$	$+\frac{0.1}{13}$	51	$-\frac{0.6}{5}$	$-\frac{4.4}{14}$	$-\frac{5.3}{33}$				
$-\frac{2.0}{33}$	$\frac{0.0}{28}$	$+\frac{0.1}{11}$	51	$-\frac{0.0}{4}$	$-\frac{5.0}{16}$	$-\frac{6.1}{33}$				
$-\frac{3.1}{33}$	$-\frac{0.2}{24}$	$-\frac{0.1}{13}$	47	$-\frac{0.1}{8}$	$-\frac{5.1}{21}$	$-\frac{6.6}{33}$				

Station

Elev.

1132

1003.3

+50

+1.2

99.0

1131

1000.8

+50

+14

99.6

1130

98.2

+76

-0.8

91.4

+33.08

95.9

1129

94.7

+50

93.2

1128

91.7

+50

90.6

1127

90.9

H.

R

A.

$$\frac{+4.1}{33}$$

$$\frac{-1.4}{25} \quad \frac{-1.7}{19} \quad \frac{-0.1}{15}$$

38

$$\frac{-0.5}{14}$$

$$\frac{-3.0}{19}$$

$$\frac{-3.1}{25}$$

$$\frac{-1.2}{30}$$

$$\frac{-1.3}{33}$$

$$\frac{+8.8}{33}$$

$$\frac{-0.5}{23}$$

$$\frac{-1.2}{18}$$

$$\frac{-0.1}{15}$$

50

$$\frac{-0.3}{13}$$

$$\frac{-2.5}{18}$$

$$\frac{-2.7}{24}$$

$$\frac{+0.8}{31}$$

$$\frac{+0.2}{33}$$

$$\frac{+9.4}{33}$$

$$\frac{-0.4}{23}$$

$$\frac{-1.2}{18}$$

$$\frac{-0.3}{15}$$

62

$$\frac{-0.5}{13}$$

$$\frac{-2.4}{18}$$

$$\frac{-3.0}{23}$$

$$\frac{+1.5}{30}$$

$$\frac{+1.2}{33}$$

$$\frac{+8.0}{33}$$

$$\frac{-1.2}{22}$$

$$\frac{-2.0}{19}$$

$$\frac{-0.3}{15}$$

75

$$\frac{-0.5}{14}$$

$$\frac{-2.8}{19}$$

$$\frac{-3.2}{23}$$

$$\frac{-1.5}{26}$$

$$\frac{-1.7}{33}$$

$$\frac{+3.3}{33}$$

$$\frac{-2.0}{25}$$

$$\frac{-2.1}{20}$$

$$\frac{-0.2}{16}$$

89

$$\frac{-0.5}{14}$$

$$\frac{-4.4}{33}$$

$$\frac{+4.5}{33}$$

$$\frac{-2.0}{26}$$

$$\frac{-2.0}{21}$$

$$\frac{-0.1}{17}$$

97

$$\frac{-0.6}{12}$$

$$\frac{-4.3}{22}$$

$$\frac{-5.2}{33}$$

$$\frac{-2.0}{33}$$

$$\frac{-2.0}{23}$$

$$\frac{-0.1}{15}$$

1

15

$$\frac{-0.5}{12}$$

$$\frac{-0.7}{17}$$

$$\frac{-6.5}{30}$$

$$\frac{-6.8}{33}$$

$$\frac{-4.2}{33}$$

$$\frac{-4.8}{28}$$

$$\frac{-3.1}{23}$$

$$\frac{0.0}{16}$$

21

$$\frac{-1.0}{15}$$

$$\frac{-6.4}{25}$$

$$\frac{-7.0}{33}$$

$$\frac{-2.6}{26}$$

$$\frac{-5.2}{31}$$

$$\frac{-5.2}{30}$$

$$\frac{+0.2}{19}$$

42

$$\frac{-1.1}{14}$$

$$\frac{-6.4}{24}$$

$$\frac{-6.8}{33}$$

$$\frac{-1.2}{44}$$

$$\frac{-2.5}{41}$$

$$\frac{-2.5}{39}$$

$$\frac{-1.1}{23}$$

$$\frac{-1.8}{31}$$

$$\frac{+0.8}{26}$$

56

$$\frac{-0.8}{16}$$

$$\frac{-5.2}{26}$$

$$\frac{-5.5}{33}$$

$$\frac{-1.8}{33}$$

57

$$\frac{-1.2}{13}$$

$$\frac{-5.2}{23}$$

$$\frac{-5.2}{33}$$

$$\frac{+1.2}{33}$$

$$\frac{+0.7}{26}$$

64

$$\frac{-0.7}{14}$$

$$\frac{-3.6}{21}$$

$$\frac{-5.1}{33}$$

stations

Elev.

438

09.7

+50

+0.4

09.6

437

09.2

+50

+0.6

08.7

436

08.1

+50

+0.2

07.7

435

07.5

+50

+0.5

07.2

434

06.7

+50

+0.8

06.1

433 +00

05.3

432 +50

-0.8

04.5

A. E R.

$$\begin{matrix} +3.0 & +2.8 & -1.4 & -1.1 & -0.1 \\ \hline 33 & 30 & 24 & 20 & 15 \end{matrix}$$

30

$$\begin{matrix} -0.4 \\ \hline 16 \end{matrix}$$

$$\begin{matrix} -2.8 \\ \hline 33 \end{matrix}$$

$$\begin{matrix} +2.1 & -2.0 & -2.2 & -0.2 \\ \hline 33 & 25 & 21 & 16 \end{matrix}$$

31

$$\begin{matrix} 0.0 & -1.2 & -1.1 & +0.9 \\ \hline 12 & 18 & 24 & 33 \end{matrix}$$

$$\begin{matrix} 0.0 & +0.4 & -2.1 & 2.1 & -0.2 \\ \hline 33 & 27 & 23 & 20 & 15 \end{matrix}$$

32

$$\begin{matrix} -0.5 & -1.8 & -1.8 & +1.1 \\ \hline 15 & 19 & 26 & 33 \end{matrix}$$

$$\begin{matrix} -2.1 & -1.7 & 0.0 \\ \hline 33 & 20 & 14 \end{matrix}$$

33

$$\begin{matrix} -0.2 & -2.0 & -1.6 & +0.5 & +1.0 \\ \hline 15 & 20 & 24 & 29 & 33 \end{matrix}$$

$$\begin{matrix} -2.4 & -2.1 & -0.1 \\ \hline 33 & 23 & 14 \end{matrix}$$

34

$$\begin{matrix} -0.4 & -1.8 & -1.8 & +0.5 & +0.6 \\ \hline 15 & 18 & 24 & 30 & 33 \end{matrix}$$

$$\begin{matrix} 2.4 & -1.7 & -0.2 \\ \hline 33 & 18 & 14 \end{matrix}$$

35

$$\begin{matrix} -0.2 & -1.6 & -1.4 & +0.9 & +0.1 \\ \hline 14 & 19 & 27 & 31 & 33 \end{matrix}$$

$$\begin{matrix} -2.4 & 2.0 & -0.4 \\ \hline 33 & 17 & 12 \end{matrix}$$

37

$$\begin{matrix} -0.2 & -1.5 & -1.4 & +1.8 & +1.8 \\ \hline 14 & 18 & 25 & 32 & 33 \end{matrix}$$

$$\begin{matrix} -1.6 & -2.3 & -0.4 \\ \hline 33 & 19 & 13 \end{matrix}$$

36

$$\begin{matrix} -0.1 & -1.2 & -1.0 & +3.3 & +3.3 \\ \hline 14 & 17 & 26 & 32 & 33 \end{matrix}$$

$$\begin{matrix} -2.2 & -2.0 & -0.3 \\ \hline 33 & 19 & 14 \end{matrix}$$

41

$$\begin{matrix} -0.2 & -1.4 & -1.4 & +2.0 & +1.1 \\ \hline 14 & 19 & 25 & 32 & 33 \end{matrix}$$

$$\begin{matrix} -3.0 & & -0.4 \\ \hline 33 & & 14 \end{matrix}$$

66

$$\begin{matrix} -0.2 & -1.8 & -1.8 & -0.4 & -0.9 \\ \hline 15 & 21 & 25 & 29 & 33 \end{matrix}$$

$$\begin{matrix} +0.2 & -2.0 & -2.0 & -0.3 \\ \hline 33 & 21 & 19 & 15 \end{matrix}$$

74

$$\begin{matrix} -0.3 & -2.3 & -2.1 & -1.1 & -1.3 \\ \hline 14 & 20 & 24 & 28 & 33 \end{matrix}$$

$$\begin{matrix} -1.4 & -1.6 & -1.8 & -0.1 \\ \hline 33 & 16 & 20 & 16 \end{matrix}$$

87

$$\begin{matrix} -0.6 & -3.3 & -3.4 & -2.4 & -2.8 \\ \hline 14 & 20 & 26 & 28 & 33 \end{matrix}$$

station		Elev.
443+32	+0.4	10 15.1
	↙	
443	+	14.7
	↘	
+50	-0.6	14.1
442		13.5
		12.9
+50	+0.5	12.0
	↙	
441	+	12.4
	↘	11.5
+40	+0.5	12.0
440	+	11.5
+70	+1.2	10.9
439	+	09.7
+70	+0.2	09.9
438+30	+0.1	10 10.0

H. Z Pt.

$$\begin{array}{r} +3.2 \\ 33 \end{array} \quad \begin{array}{r} +3.2 \\ 29 \end{array} \quad \begin{array}{r} -0.5 \\ 24 \end{array} \quad \begin{array}{r} -0.7 \\ 20 \end{array} \quad \begin{array}{r} 0.0 \\ 16 \end{array}$$

69

$$\begin{array}{r} -0.2 \\ 14 \end{array} \quad \begin{array}{r} -1.4 \\ 19 \end{array} \quad \begin{array}{r} -1.0 \\ 28 \end{array} \quad \begin{array}{r} +3.6 \\ 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ 33 \end{array} \quad \begin{array}{r} +1.2 \\ 28 \end{array} \quad \begin{array}{r} -1.2 \\ 25 \end{array} \quad \begin{array}{r} -1.4 \\ 20 \end{array} \quad \begin{array}{r} -0.0 \\ 16 \end{array}$$

73

$$\begin{array}{r} -0.3 \\ 14 \end{array} \quad \begin{array}{r} -1.3 \\ 19 \end{array} \quad \begin{array}{r} -0.9 \\ 28 \end{array} \quad \begin{array}{r} +2.9 \\ 33 \end{array}$$

$$\begin{array}{r} -0.9 \\ 33 \end{array} \quad \begin{array}{r} -0.3 \\ 26 \end{array} \quad \begin{array}{r} -1.5 \\ 25 \end{array} \quad \begin{array}{r} -1.3 \\ 18 \end{array} \quad \begin{array}{r} -0.1 \\ 15 \end{array}$$

79

$$\begin{array}{r} -0.1 \\ 13 \end{array} \quad \begin{array}{r} -1.2 \\ 18 \end{array} \quad \begin{array}{r} -0.7 \\ 28 \end{array} \quad \begin{array}{r} +2.2 \\ 33 \end{array}$$

$$\begin{array}{r} -2.1 \\ 33 \end{array} \quad \begin{array}{r} -1.7 \\ 19 \end{array} \quad \begin{array}{r} -0.2 \\ 15 \end{array}$$

21

$$\begin{array}{r} -0.3 \\ 14 \end{array} \quad \begin{array}{r} -1.4 \\ 20 \end{array} \quad \begin{array}{r} -1.0 \\ 30 \end{array} \quad \begin{array}{r} +0.9 \\ 33 \end{array}$$

$$\begin{array}{r} -2.6 \\ 33 \end{array} \quad \begin{array}{r} -1.5 \\ 17 \end{array} \quad \begin{array}{r} -0.3 \\ 14 \end{array}$$

38

$$\begin{array}{r} -0.1 \\ 14 \end{array} \quad \begin{array}{r} -1.6 \\ 19 \end{array} \quad \begin{array}{r} -0.6 \\ 27 \end{array} \quad \begin{array}{r} +5.0 \\ 33 \end{array}$$

$$\begin{array}{r} -1.5 \\ 33 \end{array} \quad \begin{array}{r} -0.8 \\ 22 \end{array} \quad \begin{array}{r} -1.2 \\ 20 \end{array} \quad \begin{array}{r} -1.5 \\ 18 \end{array} \quad \begin{array}{r} -0.1 \\ 15 \end{array}$$

43

$$\begin{array}{r} -0.2 \\ 15 \end{array} \quad \begin{array}{r} -1.5 \\ 20 \end{array} \quad \begin{array}{r} -0.4 \\ 27 \end{array} \quad \begin{array}{r} +6.8 \\ 35 \end{array}$$

$$\begin{array}{r} +3.2 \\ 33 \end{array} \quad \begin{array}{r} +3.2 \\ 29 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -2.1 \\ 20 \end{array} \quad \begin{array}{r} 0.0 \\ 15 \end{array}$$

47

$$\begin{array}{r} -0.4 \\ 14 \end{array} \quad \begin{array}{r} -2.6 \\ 21 \end{array} \quad \begin{array}{r} -2.8 \\ 25 \end{array} \quad \begin{array}{r} -2.2 \\ 27 \end{array} \quad \begin{array}{r} -3.7 \\ 33 \end{array}$$

$$\begin{array}{r} +0.9 \\ 33 \end{array} \quad \begin{array}{r} +0.9 \\ 30 \end{array} \quad \begin{array}{r} -2.2 \\ 24 \end{array} \quad \begin{array}{r} -2.4 \\ 21 \end{array} \quad \begin{array}{r} -0.1 \\ 15 \end{array}$$

52

$$\begin{array}{r} -0.6 \\ 16 \end{array} \quad \begin{array}{r} -5.5 \\ 26 \end{array} \quad \begin{array}{r} -7.0 \\ 33 \end{array}$$

$$\begin{array}{r} -2.2 \\ 33 \end{array} \quad \begin{array}{r} -2.3 \\ 24 \end{array} \quad \begin{array}{r} -0.1 \\ 15 \end{array}$$

58

$$\begin{array}{r} -0.7 \\ 15 \end{array} \quad \begin{array}{r} -6.0 \\ 28 \end{array} \quad \begin{array}{r} -6.5 \\ 33 \end{array}$$

$$\begin{array}{r} -3.5 \\ 33 \end{array} \quad \begin{array}{r} -3.2 \\ 27 \end{array} \quad \begin{array}{r} +0.2 \\ 16 \end{array}$$

70

$$\begin{array}{r} -0.8 \\ 17 \end{array} \quad \begin{array}{r} -5.6 \\ 28 \end{array} \quad \begin{array}{r} -5.6 \\ 33 \end{array}$$

$$\begin{array}{r} -2.8 \\ 33 \end{array} \quad \begin{array}{r} -2.8 \\ 24 \end{array} \quad \begin{array}{r} +0.2 \\ 16 \end{array}$$

72

$$\begin{array}{r} -0.5 \\ 15 \end{array} \quad \begin{array}{r} -5.0 \\ 25 \end{array} \quad \begin{array}{r} -5.4 \\ 33 \end{array}$$

$$\begin{array}{r} -0.2 \\ 33 \end{array} \quad \begin{array}{r} -1.0 \\ 25 \end{array} \quad \begin{array}{r} -1.2 \\ 20 \end{array} \quad \begin{array}{r} +0.2 \\ 17 \end{array}$$

71

$$\begin{array}{r} -0.6 \\ 16 \end{array} \quad \begin{array}{r} -4.8 \\ 24 \end{array} \quad \begin{array}{r} -5.6 \\ 33 \end{array}$$

station

Elev.

449+50 +1.4 30.0

448 28.6

+50 +1.8 27.0

447 25.2

+50 +1.6 23.4

446 21.8

+77 +1.1 21.1

+50 +2.2 20.0

445 17.8

+50 +0.6 16.1

444+00 15.5

443+60 -0.1 15.4

Lt. Z Kt.

$\frac{+146}{39}$	$\frac{+114}{36}$	$\frac{+50}{30}$	$\frac{-07}{21}$	$\frac{-09}{16}$	$\frac{00}{12}$	101	$\frac{03}{15}$	$\frac{-15}{19}$	$\frac{-15}{24}$	$\frac{+15}{31}$	$\frac{+15}{33}$
-------------------	-------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------

$\frac{+9.8}{33}$	$\frac{+14}{31}$	$\frac{-09}{18}$	$\frac{-09}{16}$	$\frac{00}{13}$	115	$\frac{-04}{16}$	$\frac{-20}{21}$	$\frac{-23}{26}$	$\frac{-20}{28}$	$\frac{-30}{33}$
-------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------

$\frac{+30}{33}$	$\frac{+28}{30}$	$\frac{-16}{23}$	$\frac{-19}{17}$	$\frac{-01}{13}$	55	$\frac{-03}{18}$	$\frac{-2.7}{20}$	$\frac{-3.2}{33}$
------------------	------------------	------------------	------------------	------------------	----	------------------	-------------------	-------------------

$\frac{+14}{33}$	$\frac{+15}{24}$	$\frac{-14}{25}$	$\frac{-17}{17}$	$\frac{-02}{13}$	73	$\frac{-04}{16}$	$\frac{-15}{21}$	$\frac{-11}{33}$
------------------	------------------	------------------	------------------	------------------	----	------------------	------------------	------------------

$\frac{+31}{33}$	$\frac{+36}{30}$	$\frac{-15}{23}$	$\frac{-17}{18}$	$\frac{-02}{14}$	91	$\frac{-03}{17}$	$\frac{-1.3}{20}$	$\frac{-0.6}{28}$	$\frac{+9}{33}$
------------------	------------------	------------------	------------------	------------------	----	------------------	-------------------	-------------------	-----------------

$\frac{+47}{33}$	$\frac{+53}{30}$	$\frac{-14}{21}$	$\frac{-20}{17}$	$\frac{-03}{12}$	107	$\frac{-02}{17}$	$\frac{-1.0}{21}$	$\frac{-0.8}{24}$	$\frac{+7.4}{35}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	-------------------	-------------------	-------------------

$\frac{-25}{33}$	$\frac{-20}{18}$	$\frac{-03}{13}$	09	$\frac{-02}{18}$	$\frac{-1.3}{21}$	$\frac{-1.7}{27}$	$\frac{-1.7}{33}$
------------------	------------------	------------------	----	------------------	-------------------	-------------------	-------------------

$\frac{-6.4}{33}$	$\frac{-6.2}{29}$	$\frac{-02}{16}$	20	$\frac{-05}{17}$	$\frac{-6.6}{29}$	$\frac{-6.8}{33}$
-------------------	-------------------	------------------	----	------------------	-------------------	-------------------

$\frac{-6.7}{33}$	$\frac{-6.1}{28}$	$\frac{-03}{16}$	42	$\frac{-06}{17}$	$\frac{-5.8}{28}$	$\frac{-7.1}{33}$
-------------------	-------------------	------------------	----	------------------	-------------------	-------------------

$\frac{-5.5}{33}$	$\frac{-5.1}{26}$	$\frac{-04}{16}$	51	$\frac{-03}{15}$	$\frac{-6.0}{28}$	$\frac{-5.8}{33}$
-------------------	-------------------	------------------	----	------------------	-------------------	-------------------

$\frac{-4.7}{33}$	$\frac{-4.0}{23}$	$\frac{-03}{16}$	65	$\frac{-02}{16}$	$\frac{-4.1}{26}$	$\frac{-5.2}{33}$
-------------------	-------------------	------------------	----	------------------	-------------------	-------------------

$\frac{01}{33}$	$\frac{00}{27}$	$\frac{-1.2}{20}$	$\frac{-1.3}{19}$	$\frac{00}{15}$	64	$\frac{-03}{16}$	$\frac{-1.4}{33}$
-----------------	-----------------	-------------------	-------------------	-----------------	----	------------------	-------------------

station

E lev.

454

10 345

+50

+0.1

347

453

346

+50

-0.3

348

452

351

+50

-0.0

354

451

354

+70

+0.3

354

+46.8

35.1

450

33.7

+45

+1.1

32.4

449+00

31.3

L. d Rt.

$$\begin{array}{r} +16 \\ 33 \end{array} \quad \begin{array}{r} +12 \\ 28 \end{array} \quad \begin{array}{r} -04 \\ 23 \end{array} \quad \begin{array}{r} -07 \\ 19 \end{array} \quad \begin{array}{r} 00 \\ 15 \end{array}$$

56

$$\begin{array}{r} -03 \\ 15 \end{array} \quad \begin{array}{r} -7.7 \\ 20 \end{array} \quad \begin{array}{r} -7.8 \\ 24 \end{array} \quad \begin{array}{r} -21.21 \\ 28 \end{array} \quad \begin{array}{r} -21 \\ 33 \end{array}$$

$$\begin{array}{r} +0.8 \\ 33 \end{array} \quad \begin{array}{r} +08 \\ 28 \end{array} \quad \begin{array}{r} -0.8 \\ 25 \end{array} \quad \begin{array}{r} -11 \\ 19 \end{array} \quad \begin{array}{r} -0.2 \\ 15 \end{array}$$

57

$$\begin{array}{r} -05 \\ 14 \end{array} \quad \begin{array}{r} -4.0 \\ 21 \end{array} \quad \begin{array}{r} -5.1 \\ 33 \end{array}$$

$$\begin{array}{r} -8.5 \\ 33 \end{array} \quad \begin{array}{r} -3.2 \\ 19 \end{array} \quad \begin{array}{r} 00 \\ 14 \end{array}$$

58

$$\begin{array}{r} -04 \\ 14 \end{array} \quad \begin{array}{r} -2.7 \\ 19 \end{array} \quad \begin{array}{r} -3.2 \\ 33 \end{array}$$

$$\begin{array}{r} +13 \\ 33 \end{array} \quad \begin{array}{r} +15 \\ 29 \end{array} \quad \begin{array}{r} -22 \\ 25 \end{array} \quad \begin{array}{r} -21 \\ 19 \end{array} \quad \begin{array}{r} 00 \\ 15 \end{array}$$

59

$$\begin{array}{r} -02 \\ 15 \end{array} \quad \begin{array}{r} -2.8 \\ 21 \end{array} \quad \begin{array}{r} -3.8 \\ 33 \end{array}$$

$$\begin{array}{r} +21 \\ 33 \end{array} \quad \begin{array}{r} +21 \\ 31 \end{array} \quad \begin{array}{r} -13 \\ 27 \end{array} \quad \begin{array}{r} -12 \\ 18 \end{array} \quad \begin{array}{r} -03 \\ 15 \end{array}$$

49

$$\begin{array}{r} -03 \\ 11 \end{array} \quad \begin{array}{r} +01 \\ 19 \end{array} \quad \begin{array}{r} +01 \\ 33 \end{array}$$

$$\begin{array}{r} +17 \\ 33 \end{array} \quad \begin{array}{r} -05 \\ 26 \end{array} \quad \begin{array}{r} -01 \\ 18 \end{array}$$

47

$$\begin{array}{r} -03 \\ 15 \end{array} \quad \begin{array}{r} +02 \\ 23 \end{array} \quad \begin{array}{r} +41 \\ 29 \end{array} \quad \begin{array}{r} +40 \\ 33 \end{array}$$

$$\begin{array}{r} -03 \\ 33 \end{array}$$

47

$$\begin{array}{r} -02 \\ 14 \end{array} \quad \begin{array}{r} -07 \\ 17 \end{array} \quad \begin{array}{r} -0.8+0.8 \\ 22 \end{array} \quad \begin{array}{r} +11 \\ 29 \end{array} \quad \begin{array}{r} +11 \\ 33 \end{array}$$

$$\begin{array}{r} -01 \\ 33 \end{array}$$

47

$$\begin{array}{r} -05 \\ 17 \end{array} \quad \begin{array}{r} -09 \\ 26 \end{array} \quad \begin{array}{r} +07 \\ 26 \end{array} \quad \begin{array}{r} +11 \\ 33 \end{array}$$

$$\begin{array}{r} +05 \\ 33 \end{array}$$

50

$$\begin{array}{r} -06 \\ 33 \end{array}$$

$$\begin{array}{r} +05 \\ 33 \end{array} \quad \begin{array}{r} +05 \\ 25 \end{array} \quad \begin{array}{r} -17 \\ 21 \end{array} \quad \begin{array}{r} -17 \\ 18 \end{array} \quad \begin{array}{r} -04 \\ 14 \end{array}$$

64

$$\begin{array}{r} -01 \\ 19 \end{array} \quad \begin{array}{r} 00 \\ 33 \end{array}$$

$$\begin{array}{r} +07 \\ 33 \end{array} \quad \begin{array}{r} +11 \\ 28 \end{array} \quad \begin{array}{r} -16 \\ 23 \end{array} \quad \begin{array}{r} -17 \\ 18 \end{array} \quad \begin{array}{r} 00 \\ 14 \end{array}$$

76

$$\begin{array}{r} -01 \\ 14 \end{array} \quad \begin{array}{r} -11 \\ 18 \end{array} \quad \begin{array}{r} -08 \\ 25 \end{array} \quad \begin{array}{r} +22 \\ 33 \end{array}$$

$$\begin{array}{r} +92 \\ 33 \end{array} \quad \begin{array}{r} +81 \\ 31 \end{array} \quad \begin{array}{r} -05 \\ 20 \end{array} \quad \begin{array}{r} -13 \\ 16 \end{array} \quad \begin{array}{r} -02 \\ 12 \end{array}$$

87

$$\begin{array}{r} -04 \\ 15 \end{array} \quad \begin{array}{r} -06 \\ 22 \end{array} \quad \begin{array}{r} +7.0 \\ 32 \end{array} \quad \begin{array}{r} +7.0 \\ 33 \end{array}$$

station		Elev.
460		29.7
+50	-0.2	29.5
459		29.5
+50	-0.2	29.6
458		29.8
+50	-0.6	30.3
457		30.9
+50	-0.9	31.8
456+00		32.7
+40	-0.3	33.6
455+00		33.9
454+50	+0.2	34.1

4. 2 27.

$\frac{+1.2}{33}$	$\frac{+1.6}{29}$	$\frac{-0.8}{25}$	$\frac{-1.0}{19}$	$\frac{-0.1}{15}$	52	$\frac{0.0}{14}$	$\frac{-1.7}{19}$	$\frac{-1.4}{27}$	$\frac{+1.5}{33}$
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$\frac{+0.3}{33}$	$\frac{-1.1}{27}$	$\frac{-1.1}{20}$	$\frac{-0.3}{15}$	54	$\frac{-0.1}{15}$	$\frac{-1.4}{20}$	$\frac{-1.2}{27}$	$\frac{+2.0}{33}$
-------------------	-------------------	-------------------	-------------------	----	-------------------	-------------------	-------------------	-------------------

$\frac{+0.9}{33}$	$\frac{+0.9}{33}$	$\frac{-1.5}{26}$	$\frac{-1.5}{19}$	$\frac{-0.1}{15}$	46	$\frac{0.0}{16}$	$\frac{-1.6}{21}$	$\frac{-1.1}{27}$	$\frac{+3.0}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	----	------------------	-------------------	-------------------	-------------------

$\frac{-1.0}{33}$	$\frac{-1.0}{29}$	$\frac{-2.2}{26}$	$\frac{-1.8}{19}$	$\frac{-0.4}{15}$	95	$\frac{+0.4}{16}$	$\frac{-2.8}{22}$	$\frac{-1.9}{25}$	$\frac{-1.0}{29}$	$\frac{-1.4}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	----	-------------------	-------------------	-------------------	-------------------	-------------------

$\frac{-6.9}{33}$	$\frac{-6.1}{26}$	$\frac{-0.5}{15}$	93	$\frac{+0.2}{17}$	$\frac{-4.4}{27}$	$\frac{-4.7}{33}$
-------------------	-------------------	-------------------	----	-------------------	-------------------	-------------------

$\frac{-6.1}{33}$	$\frac{-6.0}{26}$	$\frac{-0.5}{17}$	89	$\frac{0.8}{16}$	$\frac{-4.5}{27}$	$\frac{-4.2}{33}$
-------------------	-------------------	-------------------	----	------------------	-------------------	-------------------

$\frac{-5.1}{33}$	$\frac{-4.5}{24}$	$\frac{-2.4}{16}$	33	$\frac{+0.1}{17}$	$\frac{-3.4}{25}$	$\frac{+1.1}{33}$
-------------------	-------------------	-------------------	----	-------------------	-------------------	-------------------

$\frac{-2.0}{33}$	$\frac{-1.7}{28}$	$\frac{-2.4}{26}$	$\frac{-1.2}{20}$	$\frac{-0.4}{17}$	3	$\frac{-0.3}{16}$	$\frac{-3.3}{23}$	$\frac{-4.0}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	---	-------------------	-------------------	-------------------

$\frac{+2.6}{33}$	$\frac{+2.6}{30}$	$\frac{-0.8}{26}$	$\frac{-1.0}{18}$	$\frac{0.0}{16}$	64	$\frac{-0.2}{17}$	$\frac{-1.8}{21}$	$\frac{-1.6}{28}$	$\frac{+0.7}{33}$
-------------------	-------------------	-------------------	-------------------	------------------	----	-------------------	-------------------	-------------------	-------------------

$\frac{-0.1}{33}$	$\frac{-0.5}{24}$	$\frac{-1.7}{26}$	$\frac{-1.1}{18}$	$\frac{-0.2}{15}$	56	$\frac{0.0}{18}$	$\frac{-0.7}{20}$	$\frac{-0.2}{26}$	$\frac{+2.0}{36}$
-------------------	-------------------	-------------------	-------------------	-------------------	----	------------------	-------------------	-------------------	-------------------

$\frac{-1.1}{33}$	$\frac{-0.4}{27}$	$\frac{+3}{25}$	$\frac{-0.8}{18}$	$\frac{-0.1}{15}$	58	$\frac{0.0}{16}$	$\frac{-1.0}{19}$	$\frac{0.0}{27}$	$\frac{+3.2}{30}$
-------------------	-------------------	-----------------	-------------------	-------------------	----	------------------	-------------------	------------------	-------------------

$\frac{-0.8}{33}$	$\frac{-0.2}{27}$	$\frac{-1.0}{24}$	$\frac{+3}{18}$	$\frac{0.0}{14}$	51	$\frac{0.0}{14}$	$\frac{-1.8}{20}$	$\frac{-2.0}{25}$	$\frac{-0.6}{28}$	$\frac{-0.6}{33}$
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Station Elev.

466 1028.8

465 29.2

+70 -0.1 } 29.3

+27 -0.2 } 29.4

464 29.6

+50 -0.2 } 29.6

463 29.8

+30 +0.1 } 30.2

462+00 30.1

+50 0.0 } 30.3

461 30.3

460+50 -0.1 } 30.2

LY

Q

FX

$$\frac{-1.8}{34}$$

$$\frac{-1.8}{17}$$

54

$$\frac{-0.3}{15}$$

$$\frac{-1.0}{30}$$

$$\frac{-1.2}{33}$$

$$\frac{-2.1}{33}$$

$$\frac{-3.3}{28}$$

$$\frac{-0.2}{17}$$

56

$$\frac{0.0}{15}$$

$$\frac{-5.0}{28}$$

$$\frac{-5.2}{33}$$

$$\frac{+3.0}{33}$$

$$\frac{-1.7}{26}$$

$$\frac{-1.0}{20}$$

$$\frac{-0.4}{16}$$

56

$$\frac{-0.4}{15}$$

$$\frac{-3.0}{26}$$

$$\frac{-3.2}{33}$$

$$\frac{+14.5}{27}$$

$$\frac{+0.2}{24}$$

$$\frac{-0.7}{18}$$

$$\frac{0.0}{15}$$

55

$$\frac{-0.1}{15}$$

$$\frac{-1.5}{20}$$

$$\frac{-1.5}{27}$$

$$\frac{+0.9}{33}$$

$$\frac{+11.8}{31}$$

$$\frac{-0.5}{23}$$

$$\frac{-1.1}{18}$$

$$\frac{-0.1}{15}$$

53

$$\frac{-0.1}{14}$$

$$\frac{-1.2}{19}$$

$$\frac{-0.9}{24}$$

$$\frac{+3.3}{33}$$

$$\frac{+1.2}{33}$$

$$\frac{-1.3}{28}$$

$$\frac{-1.6}{21}$$

$$\frac{-0.2}{16}$$

53

$$\frac{-0.1}{13}$$

$$\frac{-2.2}{18}$$

$$\frac{-2.0}{24}$$

$$\frac{+0.2-0.8}{19 \quad 33}$$

$$\frac{+0.4}{33}$$

$$\frac{+0.4}{32}$$

$$\frac{-2.2}{28}$$

$$\frac{-1.8}{20}$$

$$\frac{-0.1}{15}$$

54

$$\frac{-0.4}{14}$$

$$\frac{-3.9}{23}$$

$$\frac{-4.6}{33}$$

$$\frac{-1.4}{33}$$

$$\frac{-1.5}{28}$$

$$\frac{-2.3}{24}$$

$$\frac{-2.2}{19}$$

$$\frac{-0.4}{14}$$

56

$$\frac{0.0}{15}$$

$$\frac{-1.4}{20}$$

$$\frac{-0.6}{33}$$

$$\frac{-2.1}{33}$$

$$\frac{-2.1}{19}$$

$$\frac{-0.3}{14}$$

47

$$\frac{-0.1}{16}$$

$$\frac{-2.7}{23}$$

$$\frac{-2.5}{33}$$

$$\frac{-0.6}{33}$$

$$\frac{-2.1}{28}$$

$$\frac{-1.7}{18}$$

$$\frac{-0.3}{14}$$

47

$$\frac{-0.1}{15}$$

$$\frac{-1.4}{27}$$

$$\frac{-1.4}{25}$$

$$\frac{+0.2}{28}$$

$$\frac{+0.2}{33}$$

$$\frac{+3.0}{33}$$

$$\frac{-1.3}{26}$$

$$\frac{-1.5}{19}$$

$$\frac{-0.1}{14}$$

47

$$\frac{0.0}{15}$$

$$\frac{-1.0}{19}$$

$$\frac{-0.4}{27}$$

$$\frac{+5.8}{35}$$

$$\frac{+3.3}{33}$$

$$\frac{-0.8}{26}$$

$$\frac{-1.3}{19}$$

$$\frac{0.0}{15}$$

47

$$\frac{0.0}{14}$$

$$\frac{-0.9}{18}$$

$$\frac{-0.1}{25}$$

$$\frac{+5.4}{23}$$

station

Elev.

+16

+0.1

1032.1

472

↓

32.0

+40

0.0

31.7

471

↓

↓

31.7

+50

-0.3

31.4

470+00

31.0

469+50

+0.2

30.7

469

↓

30.5

+33

+0.3

30.2

468

↓

29.9

+45

+0.4

29.6

467

↓

29.2

Lt.

L

Rt.

$$\begin{array}{cccc|c|cccc} +4.9 & -1.0 & -1.2 & -0.1 & 75 & 0.0 & -0.5 & +0.1 & +2.6 \\ \hline 33 & 23 & 19 & 15 & & 14 & 17 & 23 & 25 \end{array}$$

$$\begin{array}{cccc|c|cccc} +5.7 & -1.1 & -1.3 & 0.0 & 87 & 3.0 & -0.4 & 0.0 & +7.8 \\ \hline 34 & 24 & 19 & 13 & & 15 & 18 & 22 & 34 \end{array}$$

$$\begin{array}{cccc|c|cccc} -1.6 & -1.4 & -2.1 & -2.0 & 100 & -0.2 & -1.1 & -0.3 & +1.9 \\ \hline 33 & 29 & 26 & 21 & & 15 & 19 & 28 & 33 \end{array}$$

$$\begin{array}{cccc|c|cccc} -4.2 & & -3.3 & -0.1 & 119 & 0.0 & -1.9 & -1.9 & -1.2 & -1.2 \\ \hline 33 & & 22 & 15 & & 15 & 23 & 26 & 28 & 30 \end{array}$$

$$\begin{array}{ccc|c|ccc} -6.1 & -6.4 & -0.1 & 57 & -0.3 & -6.0 & -6.2 \\ \hline 33 & 29 & 15 & & 15 & 26 & 33 \end{array}$$

$$\begin{array}{ccc|c|cc} -0.2 & -2.1 & -2.2 & 67 & 0.0 & -6.4 \\ \hline 33 & 28 & 23 & & 15 & 33 \end{array}$$

$$\begin{array}{ccc|c|cc} +4.2 & -1.2 & -1.5 & 75 & 0.0 & -2.2 & -2.8 \\ \hline 33 & 26 & 21 & & 15 & 21 & 33 \end{array}$$

$$\begin{array}{ccc|c|cccc} +5.5 & -0.8 & -1.1 & 82 & -0.3 & -1.1 & -2.0 & -2.8 & -2.5 \\ \hline 33 & 25 & 21 & & 15 & 22 & 26 & 28 & 33 \end{array}$$

$$\begin{array}{ccc|c|cccc} -1.5 & +1.5 & -2.6 & -2.6 & 41 & -0.1 & -2.2 & -2.1 & -2.1 \\ \hline 33 & 31 & 28 & 23 & & 15 & 22 & 28 & 33 \end{array}$$

$$\begin{array}{ccc|c|cccc} -7.1 & -7.4 & & -0.4 & 4 & -0.2 & -4.1 & -3.3 & -3.0 \\ \hline 33 & 30 & & 15 & & 15 & 22 & 31 & 33 \end{array}$$

$$\begin{array}{ccc|c|cccc} -9.0 & & & -0.5 & 08 & -0.1 & -2.1 & -2.6 & -0.7 \\ \hline 33 & & & 15 & & 15 & 22 & 31 & 33 \end{array}$$

$$\begin{array}{ccc|c|cccc} -7.4 & & & 0.0 & 17 & -0.1 & -2.5 & -2.0 & +1.7 \\ \hline 33 & & & 17 & & 17 & 22 & 29 & 33 \end{array}$$

station

Elev.

484+50 +1.8 1058.0

484 56.2

+50 +2.0 54.6

483 52.6

482 49.5

+50 +1.7 48.3

481 46.6

+50 +1.3 45.0

480 43.7

+40 +0.6 42.5

479 41.9

478+60 -1.0 40.9

H L H.

$\frac{+60}{35}$	$\frac{-07}{26}$	$\frac{-14}{19}$	$\frac{-03}{15}$	56	$\frac{00}{14}$	$\frac{-02}{20}$	$\frac{+03}{28}$	$\frac{+18}{33}$
------------------	------------------	------------------	------------------	----	-----------------	------------------	------------------	------------------

$\frac{+6.2}{33}$	$\frac{-07}{24}$	$\frac{-09}{18}$	$\frac{00}{14}$	76	$\frac{-01}{15}$	$\frac{+06}{28}$	$\frac{+18}{33}$
-------------------	------------------	------------------	-----------------	----	------------------	------------------	------------------

$\frac{+01}{33}$	$\frac{00}{28}$	$\frac{-19}{24}$	$\frac{-18}{19}$	$\frac{-04}{15}$	37	$\frac{-02}{14}$	$\frac{-02}{33}$
------------------	-----------------	------------------	------------------	------------------	----	------------------	------------------

$\frac{-49}{33}$	$\frac{-08}{18}$	$\frac{-04}{12}$	57	$\frac{00}{15}$	$\frac{-06}{33}$
------------------	------------------	------------------	----	-----------------	------------------

$\frac{-4.4}{33}$	$\frac{-04}{19}$	$\frac{-04}{14}$	88	$\frac{00}{14}$	$\frac{+1.5}{33}$
-------------------	------------------	------------------	----	-----------------	-------------------

$\frac{-3.6}{33}$	$\frac{-20}{22}$	$\frac{-07}{15}$	100	$\frac{+02}{14}$	$\frac{-07}{18}$	$\frac{-03}{26}$	$\frac{+49}{34}$
-------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{-23}{33}$	$\frac{-13}{28}$	$\frac{-24}{23}$	$\frac{-28}{21}$	$\frac{-01}{15}$	117	$\frac{+03}{14}$	$\frac{-11}{19}$	$\frac{00}{26}$	$\frac{+50}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	-----------------	------------------

$\frac{-9.2}{33}$	$\frac{-02}{14}$	21	$\frac{-02}{14}$	$\frac{-14}{21}$	$\frac{-16}{26}$	$\frac{+08}{31}$	$\frac{+08}{33}$
-------------------	------------------	----	------------------	------------------	------------------	------------------	------------------

$\frac{-15.0}{40}$	$\frac{-06}{14}$	37	$\frac{+03}{15}$	$\frac{-4.6}{26}$	$\frac{-4.5}{33}$
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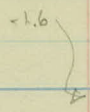
$\frac{-128}{33}$	$\frac{-02}{16}$	56	$\frac{-01}{15}$	$\frac{-5.6}{27}$	$\frac{-5.8}{33}$
-------------------	------------------	----	------------------	-------------------	-------------------

$\frac{-7.5}{33}$	$\frac{-07}{18}$	51	$\frac{00}{15}$	$\frac{-11}{23}$	$\frac{-13}{27}$	$\frac{-04}{33}$
-------------------	------------------	----	-----------------	------------------	------------------	------------------

$\frac{00}{33}$	$\frac{00}{32}$	$\frac{-16}{24}$	$\frac{-16}{19}$	$\frac{-03}{14}$	68	$\frac{00}{14}$	$\frac{-11}{18}$	$\frac{-06}{25}$	$\frac{+48}{34}$
-----------------	-----------------	------------------	------------------	------------------	----	-----------------	------------------	------------------	------------------

Station ELEV.

+50 10484



490 50.0

+53.7 51.6

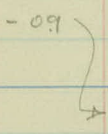
489 53.2

+50 54.1



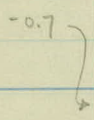
488 54.7

+50 55.2



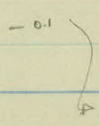
487 56.1

+50 57.0



486 57.7

+50 58.6



485 58.7

	L1	L2	R1						
$\frac{+7.8}{34}$	$\frac{-0.3}{24}$	$\frac{-0.3}{19}$	$\frac{+0.2}{15}$	110	$\frac{-0.5}{14}$	$\frac{-1.5}{18}$	$\frac{-1.5}{24}$	$\frac{-0.1}{29}$	$\frac{-0.9}{33}$
$\frac{+7.8}{33}$	$\frac{-1.2}{23}$	$\frac{-1.2}{18}$	$\frac{+0.4}{14}$	94	$\frac{-0.4}{15}$	$\frac{-1.6}{19}$	$\frac{-1.7}{24}$	$\frac{+0.4}{29}$	$\frac{0.0}{33}$
$\frac{+7.1}{34}$	$\frac{-0.6}{25}$	$\frac{-1.2}{19}$	$\frac{0.0}{15}$	78	$\frac{-0.6}{14}$	$\frac{-2.2}{19}$	$\frac{-2.2}{24}$	$\frac{0.0}{31}$	$\frac{0.0}{33}$
$\frac{+3.4}{33}$	$\frac{-0.8}{16}$	$\frac{-1.3}{20}$	$\frac{0.0}{15}$	63	$\frac{-0.3}{15}$		$\frac{-1.2}{33}$		
$\frac{+3.0}{33}$	$\frac{-1.3}{28}$	$\frac{-1.4}{21}$	$\frac{-0.1}{16}$	51	$\frac{-0.5}{16}$	$\frac{-6.2}{18}$	$\frac{-6.5}{33}$		
$\frac{+3.6}{34}$	$\frac{-0.9}{25}$	$\frac{-1.3}{21}$	$\frac{+0.2}{15}$	48	$\frac{0.0}{16}$	$\frac{-6.8}{30}$	$\frac{-6.6}{33}$		
$\frac{+3.4}{33}$	$\frac{-0.6}{27}$	$\frac{-1.0}{20}$	$\frac{0.0}{15}$	86	$\frac{-0.2}{15}$	$\frac{-2.6}{27}$	$\frac{-2.3}{33}$		
$\frac{+2.8}{33}$	$\frac{-1.0}{28}$	$\frac{-1.4}{21}$	$\frac{-0.1}{16}$	77	$\frac{0.0}{15}$			$\frac{+0.4}{33}$	
$\frac{+1.0}{33}$	$\frac{-1.8}{26}$	$\frac{-1.8}{20}$	$\frac{-0.2}{14}$	63	$\frac{-0.1}{16}$	$\frac{+0.2}{28}$	$\frac{+1.0}{33}$		
$\frac{+0.4}{33}$	$\frac{-2.6}{27}$	$\frac{-1.8}{20}$	$\frac{-0.2}{15}$	61	$\frac{-0.1}{15}$	$\frac{+0.5}{26}$	$\frac{+2.3}{33}$		
$\frac{+1.6}{33}$	$\frac{+1.6}{32}$	$\frac{-1.4}{20}$	$\frac{-1.5}{19}$	12	$\frac{-0.2}{15}$	$\frac{+0.5}{28}$	$\frac{+3.8}{33}$		
$\frac{+4.7}{33}$	$\frac{-1.0}{27}$	$\frac{-1.0}{19}$	$\frac{-0.1}{16}$	51	$\frac{+0.2}{15}$	$\frac{+0.9}{18}$	$\frac{+2.6}{33}$		

Station ELEV.

497+00 1016.7

496 20.8

+17 -0.9 25.3

495 26.2

+60 -3.2 28.5

494 31.7

+50 +2.4 34.1

493 36.6

+50 -2.5 39.0

492 41.5

+60 +2.0 43.5

491 46.3

4

2

171

$$\begin{array}{r} -5.1 \\ 33 \end{array} \quad \begin{array}{r} -5.0 \\ 28 \end{array} \quad \begin{array}{r} -0.1 \\ 17 \end{array} \quad 61$$

$$\begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} -4.0 \\ 23 \end{array} \quad \begin{array}{r} -3.9 \\ 26 \end{array} \quad \begin{array}{r} -3.3 \\ 28 \end{array} \quad \begin{array}{r} -4.1 \\ 33 \end{array}$$

$$\begin{array}{r} -8.0 \\ 33 \end{array} \quad \begin{array}{r} -0.1 \\ 16 \end{array} \quad 19$$

$$\begin{array}{r} -0.5 \\ 15 \end{array} \quad \begin{array}{r} -10.9 \\ 34 \end{array}$$

$$\begin{array}{r} -2.6 \\ 33 \end{array} \quad \begin{array}{r} -1.9 \\ 28 \end{array} \quad \begin{array}{r} -2.0 \\ 26 \end{array} \quad \begin{array}{r} -2.0 \\ 23 \end{array} \quad \begin{array}{r} -0.2 \\ 17 \end{array} \quad 20$$

$$\begin{array}{r} -0.4 \\ 14 \end{array} \quad \begin{array}{r} -2.0 \\ 20 \end{array} \quad \begin{array}{r} -2.0 \\ 23 \end{array} \quad \begin{array}{r} -1.1 \\ 26 \end{array} \quad \begin{array}{r} -0.4 \\ 33 \end{array}$$

$$\begin{array}{r} -0.3 \\ 33 \end{array} \quad \begin{array}{r} -0.5 \\ 25 \end{array} \quad \begin{array}{r} -1.9 \\ 21 \end{array} \quad \begin{array}{r} -1.6 \\ 19 \end{array} \quad \begin{array}{r} 0.0 \\ 16 \end{array} \quad 11$$

$$\begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} -1.7 \\ 20 \end{array} \quad \begin{array}{r} -1.7 \\ 22 \end{array} \quad \begin{array}{r} +2.6 \\ 29 \end{array} \quad \begin{array}{r} +3.0 \\ 33 \end{array}$$

$$\begin{array}{r} +2.1 \\ 33 \end{array} \quad \begin{array}{r} +3.4 \\ 29 \end{array} \quad \begin{array}{r} -2.0 \\ 21 \end{array} \quad \begin{array}{r} -2.0 \\ 19 \end{array} \quad \begin{array}{r} -0.3 \\ 14 \end{array} \quad 19$$

$$\begin{array}{r} -0.3 \\ 14 \end{array} \quad \begin{array}{r} -1.5 \\ 18 \end{array} \quad \begin{array}{r} -1.5 \\ 21 \end{array} \quad \begin{array}{r} +4.9 \\ 27 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} +5.1 \\ 33 \end{array} \quad \begin{array}{r} -1.8 \\ 20 \end{array} \quad \begin{array}{r} -1.8 \\ 18 \end{array} \quad \begin{array}{r} -0.6 \\ 15 \end{array} \quad 77$$

$$\begin{array}{r} -0.3 \\ 14 \end{array} \quad \begin{array}{r} -0.9 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 21 \end{array} \quad \begin{array}{r} +7.6 \\ 32 \end{array} \quad \begin{array}{r} +7.7 \\ 33 \end{array}$$

$$\begin{array}{r} +8.1 \\ 34 \end{array} \quad \begin{array}{r} -2.7 \\ 26 \end{array} \quad \begin{array}{r} -2.1 \\ 22 \end{array} \quad \begin{array}{r} -0.4 \\ 16 \end{array} \quad 73$$

$$\begin{array}{r} 0.0 \\ 14 \end{array} \quad \begin{array}{r} -1.0 \\ 18 \end{array} \quad \begin{array}{r} -1.3 \\ 22 \end{array} \quad \begin{array}{r} +7.3 \\ 33 \end{array}$$

$$\begin{array}{r} -4.0 \\ 34 \end{array} \quad \begin{array}{r} -3.3 \\ 28 \end{array} \quad \begin{array}{r} -3.3 \\ 23 \end{array} \quad \begin{array}{r} -0.5 \\ 15 \end{array} \quad 119$$

$$\begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} -1.5 \\ 20 \end{array} \quad \begin{array}{r} -1.5 \\ 28 \end{array} \quad \begin{array}{r} +4.7 \\ 34 \end{array}$$

$$\begin{array}{r} +2.8 \\ 33 \end{array} \quad \begin{array}{r} -1.6 \\ 26 \end{array} \quad \begin{array}{r} -1.5 \\ 21 \end{array} \quad \begin{array}{r} -0.3 \\ 15 \end{array} \quad 87$$

$$\begin{array}{r} -0.3 \\ 15 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -1.6 \\ 24 \end{array} \quad \begin{array}{r} +2.7 \\ 33 \end{array}$$

$$\begin{array}{r} +1.8 \\ 33 \end{array} \quad \begin{array}{r} -1.1 \\ 26 \end{array} \quad \begin{array}{r} -1.1 \\ 21 \end{array} \quad \begin{array}{r} -0.1 \\ 18 \end{array} \quad 68$$

$$\begin{array}{r} 0.0 \\ 15 \end{array} \quad \begin{array}{r} -0.9 \\ 18 \end{array} \quad \begin{array}{r} -0.9 \\ 20 \end{array} \quad \begin{array}{r} +2.7 \\ 33 \end{array}$$

$$\begin{array}{r} +5.1 \\ 33 \end{array} \quad \begin{array}{r} +5.2 \\ 32 \end{array} \quad \begin{array}{r} -2.0 \\ 22 \end{array} \quad \begin{array}{r} -2.0 \\ 20 \end{array} \quad \begin{array}{r} -0.1 \\ 14 \end{array} \quad 48$$

$$\begin{array}{r} -0.1 \\ 14 \end{array} \quad \begin{array}{r} -1.0 \\ 18 \end{array} \quad \begin{array}{r} -1.0 \\ 23 \end{array} \quad \begin{array}{r} +1.3 \\ 33 \end{array}$$

$$\begin{array}{r} +9.8 \\ 34 \end{array} \quad \begin{array}{r} -0.6 \\ 27 \end{array} \quad \begin{array}{r} -0.6 \\ 18 \end{array} \quad \begin{array}{r} +0.1 \\ 14 \end{array} \quad 121$$

$$\begin{array}{r} -1.2 \\ 14 \end{array} \quad \begin{array}{r} -1.6 \\ 18 \end{array} \quad \begin{array}{r} -1.6 \\ 22 \end{array} \quad \begin{array}{r} -1.2 \\ 25 \end{array} \quad \begin{array}{r} -0.8 \\ 33 \end{array}$$

station

E/ev

Fin. Dec. 8, 1976

W.H.C.

A.L.P.

W.F.

E.T.S.

503 + 73.7

1002.53

+10

+0.02

1002.50

503 + 00

1002.48

502 + 73.7

1002.53

.31

502

02.6

+1.6

+0.5

03.1

501

03.8

+50

-1.5

04.9

500

06.4

+50

-1.6

08.0

499

09.6

+50

+1.5

11.1

498

12.8

497 + 50

+1.6

14.4

H

Z

pt

$$\begin{array}{r} +0.08 \\ \hline 5.00 \\ -0.22 \\ \hline 4.78 \\ -7.0 \\ \hline 5.0 \\ -9.2 \\ \hline 5.0 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 4.5 \\ -0.1 \\ \hline 4.4 \\ -0.1 \\ \hline 4.3 \end{array} \quad \begin{array}{r} -0.21 \\ \hline 19.5 \\ -0.1 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 4.87 \\ \hline 4.85 \\ \hline 4.81 \\ \hline 5.05 \\ -0.22 \\ \hline 10.0 \\ -0.2 \\ \hline 15 \\ -8.0 \\ \hline 28 \\ -9.7 \\ \hline 50 \end{array} \quad \begin{array}{r} -0.21 \\ \hline 50 \\ 0.0 \\ \hline 46.0 \\ -0.37 \\ \hline 19.5 \\ -0.2 \\ \hline 27 \\ -8.0 \\ \hline 28 \\ -9.7 \\ \hline 50 \end{array} \quad \begin{array}{r} -0.91 \\ \hline 100.0 \\ -0.4 \\ \hline 75 \\ -8.2 \\ \hline 56 \\ -8.0 \\ \hline 70 \\ -9.7 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -9.2 \\ \hline 33 \\ -9.0 \\ \hline 30 \\ -0.1 \\ \hline 15 \\ -0.16 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 4.6 \\ -0.6 \\ \hline 11 \\ -8.4 \\ \hline 28 \\ 10.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} -1.8 \\ \hline 33 \\ -14 \\ \hline 31 \\ -3.1 \\ \hline 76 \\ -3.3 \\ \hline 73 \\ -0.2 \\ \hline 16 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 75 \\ -3.9 \\ \hline 22 \\ -4.0 \\ \hline 75 \\ -1.2 \\ \hline 30 \\ -1.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +5.6 \\ \hline 33 \\ -3.0 \\ \hline 24 \\ -2.8 \\ \hline 20 \\ -0.2 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 100 \\ -0.5 \\ \hline 75 \\ -2.8 \\ \hline 22 \\ -2.9 \\ \hline 26 \\ 0.0 \\ \hline 28 \\ -0.4 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +2.3 \\ \hline 83 \\ -1.6 \\ \hline 75 \\ -1.0 \\ \hline 21 \\ 0.0 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 90 \\ -0.6 \\ \hline 14 \\ -4.5 \\ \hline 22 \\ -7.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +4.5 \\ \hline 33 \\ -1.0 \\ \hline 29 \\ -1.4 \\ \hline 20 \\ 0.0 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 75 \\ -0.4 \\ \hline 16 \\ -1.5 \\ \hline 19 \\ -1.6 \\ \hline 21 \\ -0.4 \\ \hline 24 \\ -2.5 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +3.8 \\ \hline 33 \\ -2.4 \\ \hline 25 \\ -1.8 \\ \hline 20 \\ 0.0 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 58 \\ -0.6 \\ \hline 15 \\ -2.0 \\ \hline 19 \\ -1.8 \\ \hline 24 \\ -2.1 \\ \hline 28 \\ -0.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 33 \\ -2.2 \\ \hline 29 \\ -2.0 \\ \hline 21 \\ 0.0 \\ \hline 15 \end{array}$$

$$\begin{array}{r} 44 \\ -0.5 \\ \hline 15 \\ -2.2 \\ \hline 22 \\ -3.2 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.2 \\ \hline 33 \\ -1.2 \\ \hline 32 \\ -3.1 \\ \hline 29 \\ -2.9 \\ \hline 22 \\ 0.0 \\ \hline 15 \end{array}$$

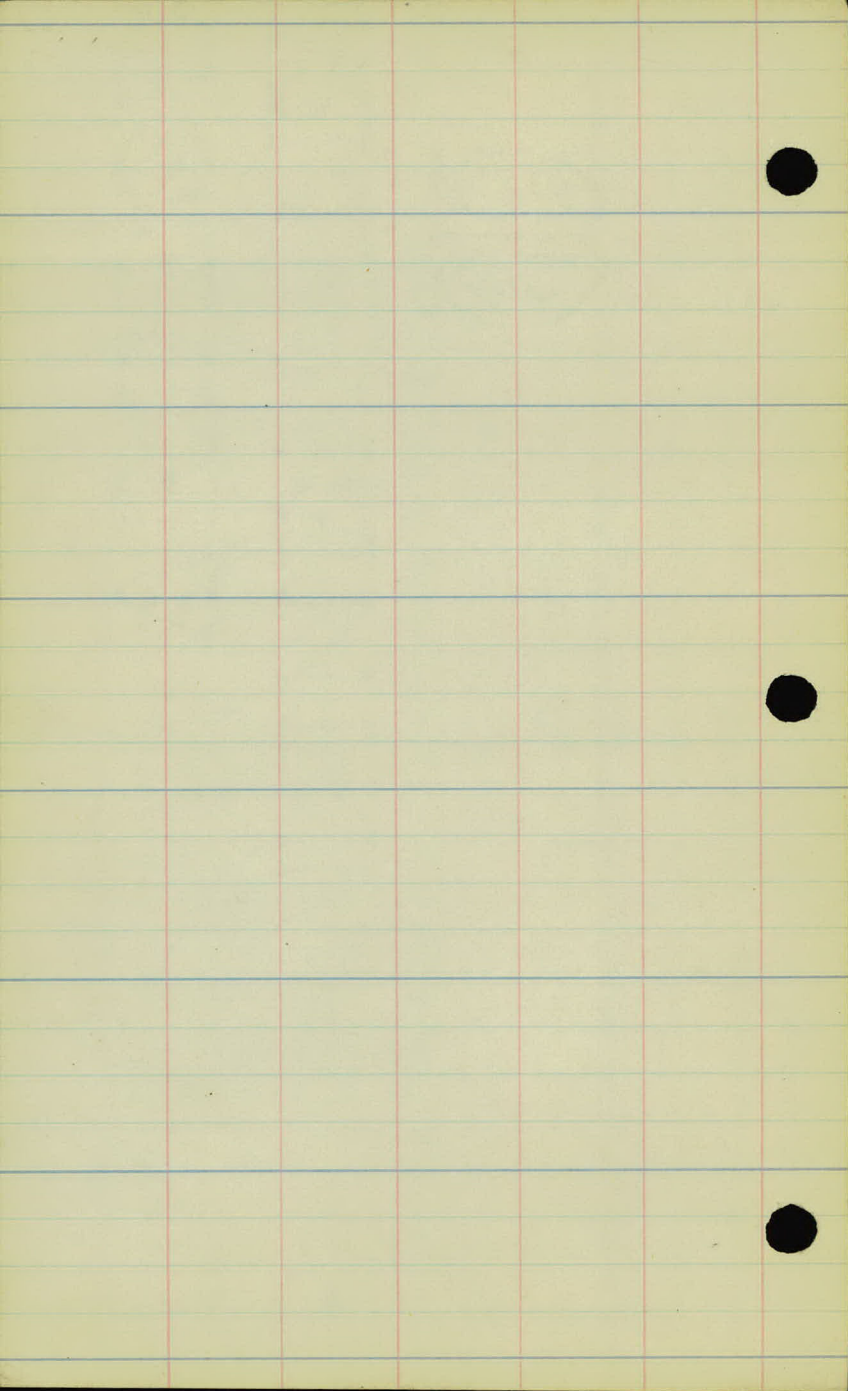
$$\begin{array}{r} 21 \\ -0.6 \\ \hline 15 \\ -5.4 \\ \hline 24 \\ -6.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -1.5 \\ \hline 33 \\ -2.9 \\ \hline 30 \\ -2.8 \\ \hline 20 \\ -0.4 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 18 \\ -0.6 \\ \hline 14 \\ -2.5 \\ \hline 20 \\ -2.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} -3.4 \\ \hline 33 \\ -2.3 \\ \hline 23 \\ 0.0 \\ \hline 17 \end{array}$$

$$\begin{array}{r} 82 \\ -0.5 \\ \hline 16 \\ -1.5 \\ \hline 19 \\ -1.7 \\ \hline 22 \\ +0.1 \\ \hline 75 \\ +4 \\ \hline 78 \\ +0.8 \\ \hline 33 \end{array}$$



Drainage.

Station	Culv. Kind.	Rec'd Culv.
384+38	12" x 38.5 Vit 15' Rt. - 22.5 Lt.	18" P.3
390+51	10" x 35' Vit 15.5 Rt. - 20' Lt.	24" P.3.
394+06	12" x 35' C.M. & Vit. 19' Rt. - 16' Lt.	18" P.3
397+71	15" x 43' Vit 16.4 Rt. - 15.6 Lt.	24" P.3
409+47	12" x 46.5 Vit. 28' Rt. - 18.5 Lt.	24" P.3
438+69	12" x 45' Vit. 22' Rt. - 23' Lt.	24" P.3
444+27	10" x 53' Vit 26' Rt. - 27' Lt.	18" P.3
457+75	12" x 54' Vit 27' Rt. - 27' Lt.	18" P.3
469+38	10" x 38' Vit 17.5' Rt. - 19.5 Lt.	24" P.3

W.H.C.
D.L.P.
W.R.
E.T.S.

Dec. 9 1926

65

Inv. Elev. 988.7

Drains Left.

Inv. Elev. 989.3

Drains Left.

Inv. Elev. 988.3

Drains Left.

Inv. Elev. 986.5

Drains Left.

Inv. Elev. 989.1

Drains Left.

Inv. Elev. 1006.2

Drains Right.

Inv. Elev. 1010.3

Drains Right.

Inv. Elev. 1023.6

Drains Left.

Inv. Elev. 1028.2

Drains Left.

Station	Culv. Kind.	Rec. and Culv.
---------	-------------	----------------

473+67	12" x 54.5' Vit. 23.5 Rt. - 31' Lt.	24" P.3
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479+72	12" x 70' Vit 30' Rt. - 40' Lt.	24" P.3
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496+30	15" x 67' Vit. 34' Rt - 33' Lt.	24" P.3
--------	------------------------------------	---------

Dec. 9, 1926

Inv. Elev. 1027.9

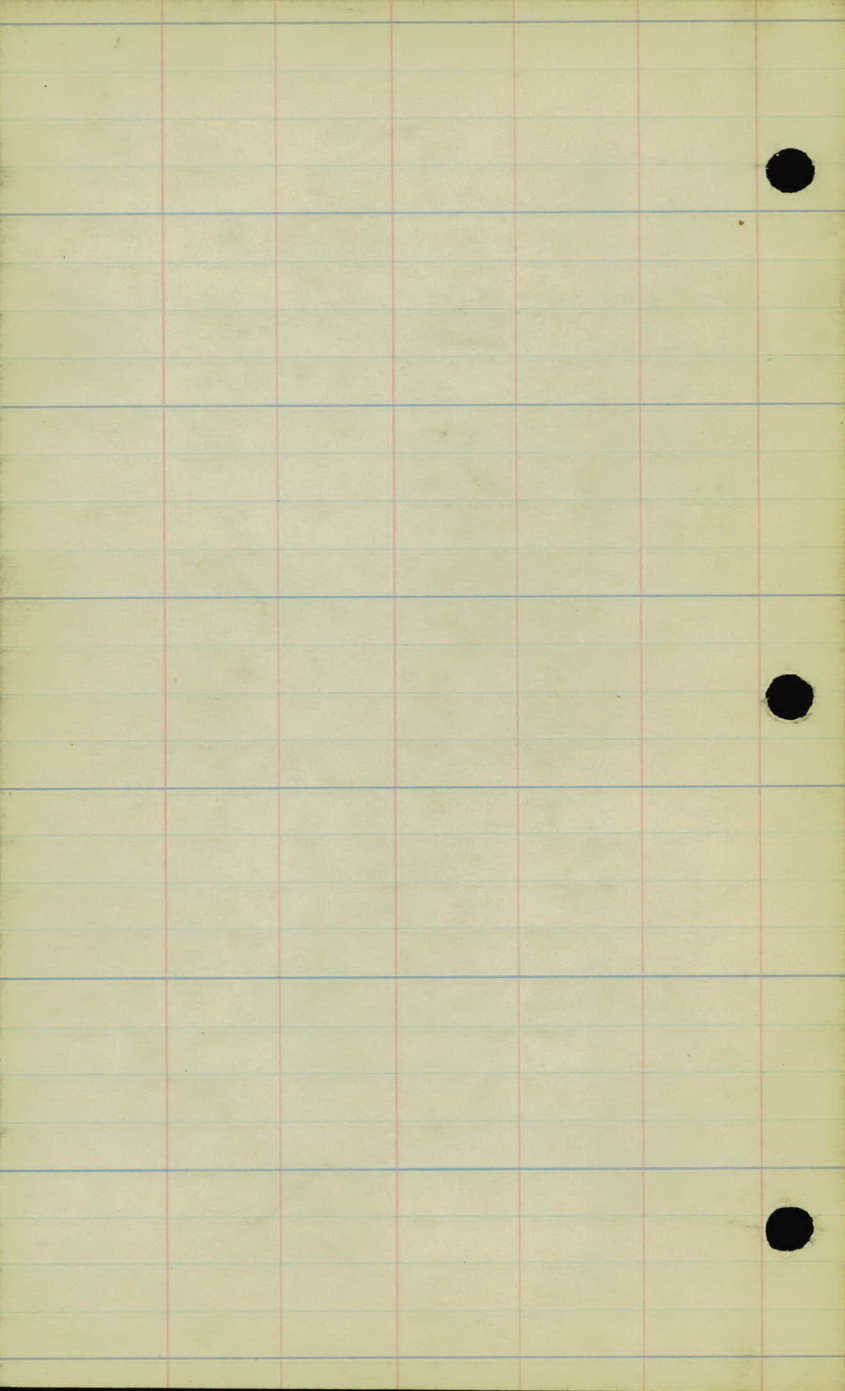
Drains, Left.

Inv. Elev. 1035.2

Drains Left.

Inv. Elev. 1010.2

Drains. Right.



Topography.

station 377 to station 303+73.7

~~27-04~~

383

+78 - E F. Ent Rd.

382

+57 E F. Ent Rd.

381

+04 E 12th Ave.

380

+30 Int Road Rd.

379

378

!

377

Note:
 Dash line indicates
 Shoulder of Roadway.
 Road is Grave N'ed
 thru-out.

+51- 1 Culv. 10'x35' Vit.

+45- R.R. Tel Line Xing.

390

+93.5 1 PINE RR

82' Planking (not full planked)

389

+20- 1 F. Ent Rt.

388

387

+65 1 F. Ent Rt.

386

385

+38. 12" x 38⁵ V.T.

384

+85-G.P.-21'

+84-F. Cor. 34
+86-P.P. 18'

+79-B.F. 30'
+15-E.F. 42'

+58-Wood X-219, 20'

Pine T.R.

R.O.W.

+87-G.P.-31'

+61-T.P. 31'
+38-P.P. 28'

+46-F. Cor. 39'

R.P.

+49-F. Cor. 37'

F-16'

+45-T.P. 34'
+29-14" Maple 34'

F-22'

+15-R.R. X-5117 14'
+10-T.P. 21'

Posture

10' x 24" C.M. 1 V 4 ft
15' x 20'

+73-24 Maple 34'
+13-E. Tree 34'

+24-P.P. 28'
+11-R.R. X-1954 13'
New.

F-13'

+18-T.P. 25'
Full-De Row Maples 25'

225
15'

+25-T.P. 24'

9

390

389

388

387

386

385

384

+71

culv. - 14' x 43' V.P.

397

+394 I Co. Road "C"

396

395

+06- dculv 12' x 35' C.M. + V.P.

394

+09- d Street #.

393

392

391

Low Land

Ditch

Ditch

+01-6' Oak 17'
 +84-27 R.R. 17'
 +76-P.P. 26
 +66-27 R.R. 20
 +61 Fiveyd 53'
 +57-12' Oak 24'

+94-6' Oak 16'
 +72-6' Maple 16'
 +54-P.P. 28'
 +48-6' Oak 18'
 +27-A' Maple 20

397

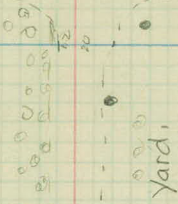
+25-14' Oak 18'

+91-P.P. 19'
 +98-New R.R. 16'
 +72-6' Maple 35'

70 Lake DeMontreville.

+12-P.P. 39'
 +15-P.P. 28'

396



+71-7' P.P. 19'

+33-8' Oak 32'

395

New
 +70-R.R. 14 Sq. 14

Platted Land

+23-R.P. 20

34

394

+92-8' W Oak 30
 +84-10' Oak 31
 +71-6' Oak 29'

+48-P.P. 28

+41-8' Oak 28'

+12-X-Road 14 Sq. 14'

393

+92-T.P. 20'

Yard

+09-14' Oak 30

+34-8' Oak 28'
 +76-10' Oak 30
 +03-8' W Oak 29'

392

~~+91-8' Oak 28'~~

+69-10' Oak 30'

+90-16' Oak 30

+24-72' Oak 31

+21-T.P. 20'

391

404

+69 - $\frac{1}{2}$ 19th Ave N.E.

403

+30 E F. ENT RT.

402

401

+049 E Elec. R.R. (no Planks)
(Paved Tarvia)

400

399

+25 - E F. ENT RT.

398

106 - 8" Maple 33

+93 - E. C. 22
+93 - I. S. 29

+93 - B. C. 21

+36 - Row Maple 33

+87 - R.P. King 14
(new)

+63 - Maple 24
+42 - 6" Oak 24
+95 - E.P. 24
+31 - 10" Maple 25
+13 - E. C. 24
+19 - Xing Signal 14

+77 - R.P. King 14 (new)
+61 - Cor. Ho.

+37 - Ho. 33
+23 - E.P. 22
+16 - (3) - 10" Maple 29

+86 - Cor. Ho. 14
+93 - 12" Maple 24
+67 - Cor. Ho. 23
+20 - 8" Maple 24
+33 - P.P. 26

Ditch

15' canopy
Culv.

see X-sec.
Ditch

Ditch

10'

10'

10'

10'

10'

12'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

+68 - R.P. 12

+66 - R.P. 11

+87 - F. Cor. 18
+53 - 14" Oak 31
+53 - F. Cor. 21
+50 - P.P. 17

+28 - P.P. 28

+87 - R.P. 13
+74 - 8" Oak 22
+69 - F. Cor. 22
+69 - 10" Oak 22

+40 - B. F. 19

+21 - Cor. Ho. 23
+16 - 8" Oak 28
+01 - 10" Oak 22

+83 - 8" Oak 29
+76 - 10" Oak 24
+69 - Cor. Ho. 24
+59 - P.P. 28
+57 - P.P. 13

+55 - 12" Oak 30
+42 - P.P. 28
+87 - P.P. 16
+25 - P.P. King 20

+84 - R.P. King 24
+77 - P.P. 15
+73 - Xing Signal 12
+44 - 8" Oak 29
+3 - 6" Oak 23
+27 - P.P. 28
+15 - 6" Oak 31
+2 - 6" Oak 31
+0 - 4" Trv. 31

+82 - 10" Tw. Oak 31
+13 - 5" Oak 24

+35 - P.P. 16
20' x 16" C.M.
+17 - E. C. 23

104

103

104

101

100

399

398

orchard

strubs

Yard

Yard



+71 1/2 Dive Lt.

+30 - 2 F. Ent Rt.

+05 1/2 F. Ent Lt.

411

410

+47 - 12" X 40.5 Vit + G.M.

+16 - 1/2 F. Ent Lt.

409.

408

+44 1/2 20th Ave N.E. Lt.

407

406

405

+33-12" oak 38'
+19-F. cor. 34'

+96-E.F. 34'

+75-F. cor. 34'

+18-30" oak 29'
+18-F. cor. 34'

+68-30" maple 29'
+46-30" maple 33'

+70-F. cor. 33'
+70-Arch. 19'
+63-Tr. Sq. 29'

20" x 40" Vit.
+21-B. cul. v. 23'

+31-14" Maple 30'
+13-20" Maple 29'

+99-12" Maple 29'
+81-Group Maple 23'

Marsh

Marsh

Pasture

See X-580
Ditch

+90-P.R. 75'
+44-10" oak 25'
+40-Corn Wall 23'
12" x 20" c. 24'
+13-F. cor. 26'
+13-8" oak 17'

+95-P.R. 17'

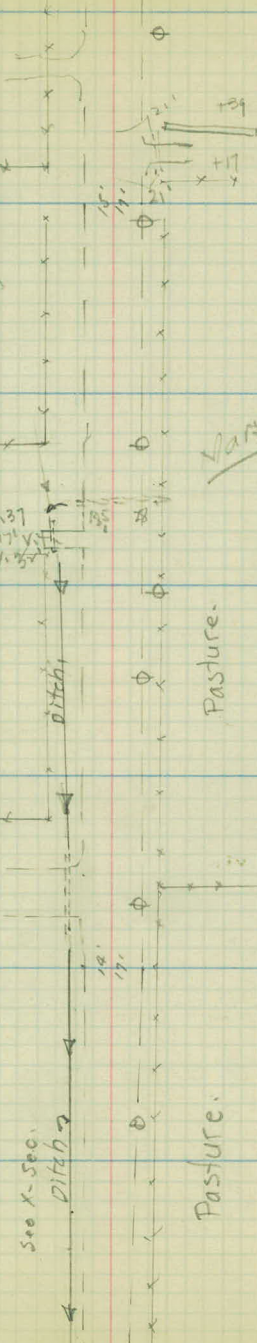
+76-P.R. 16'

+99-P.R. 75'

+53-P.R. 15'

+45-F. cor. 24'
+35-P.P. 4'

+68-P.P. 13'
+64-P.P. 28'



48

47

187-2 F. Ent Rt

145- Drive Lt.

46

103- 1/2 Drive Lt.

45

153 1/2 Ent Lt.

44

130 1/2 Drive Lt.

43

42

+94-8' Oak 19'
+76-8' Oak 20'
+34-8' Oak 27'
+28-12' Oak 30'

+86-R.P. 21'
+40-F. Cor. 37'

+39-T.P. 34'

Shoulder Line of Road

Orchard

418

+60-G.P. 38'
+50-F. 43'

12' x 16' C.M.

+69-R.P. 10'
+62-R.P. 11'

+34'

417

+49-T.P. 24'

Platted Land

+90-R.P. 23'

416

+67-G.P. 28'
+67-F. 31'
+67-F. 34'
+61-R.P. 34'
+45-E.P. 34'

Platted Land

Orchard

+67-R.P. 25'
+45-R.P. 26'

415

+50-B.F. 33'

Dist. from Shoulder of Road

414

+18-F. Cor. 33'

+6-R.P. 23'

413

+23-R.P. 19'

412

428

424

199. 2 F. ENT. RT.

420

422

421

420

419

+78-10" oak 18'
 +11-12" oak 26'
 +6-12" oak 9'

+92-12" oak 12'
 +57-8" TW oak 25'

+101-8" oak 29'

+26-8" oak 21'
 +20-8" oak 24'
 +73-8" oak 33'

+20-6" oak 26'
 +71-8" oak 35'

+88-20" TW Wil 28'
 +76-24" cot 28'

+32-30" cot 19'

+63-18" oak 13'
 +57-14" oak 13'

+02-8" TW Birch 17'

Silver Lake sea stadia next p. for shore line loc.



+02 F 38

F 38'

+07 P.P. 20'
 +00 F 32'

F 25'

+40 F 17'

F 13'

+00 F 13'

+34 P.P. 11'
 F 15'

+02 F 16

F 21'

+07-24 20'
 NW-Lake Elm 15'
 +52 F 29'

F 37'

432

431

By + stadia to locate shore
of Silver Lake

($\square = P.C. 42621$)

	By	Dist stadia
430	Byg. Fence	259° 00' 100'
	Lake shore	250° 00' 106'
	" "	214° 00' 100'
429	" "	195° 00' 170'
	" "	182° 00' 240'
	" "	175° 00' 360'
	" "	177° 00' 460'
428	" "	181° 00' 620'
	" "	185° 00' 700'
	" "	192° 00' 800'

427

426

F-33'

F-34'

15

+70-T.P. 28'

+43-T.P. 29'

+11-T.P. 28'
F-34'

+13-T.P. 28'
F-35

+54-20' W 11 23'

+22-G.P. 28'

+12-T.P. 29'

F-46'

+44-G.P. 20'

+76 Lake Side 21'

Timber

56

Cattle Pass

Cultivated

+13-P.P. 28'
F-34'

+83-A F-34'

+67-A F-27'

F-25'

+50-F-20'

+20-F. cor 60'

+12-P.P. 28'

F-24'

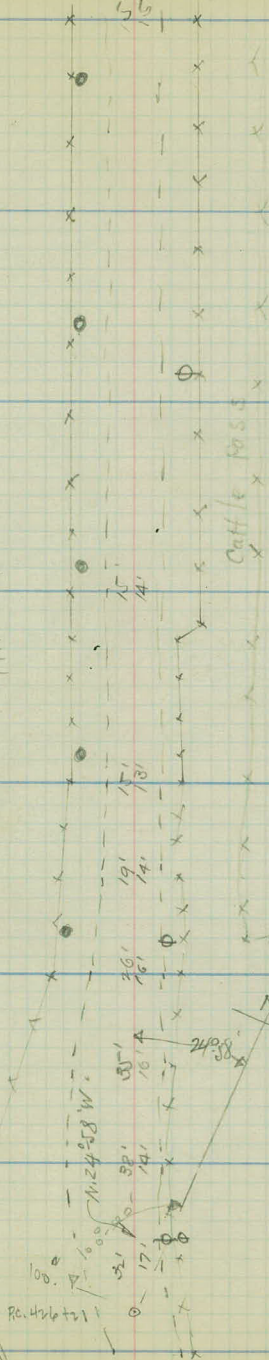
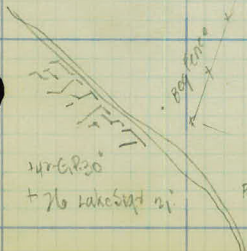
+50-F-21'

F-20'

+19-AP 16'
+51-P.P. 24'
+50-F-20'

Re. 426 221

N. 24° 58' W.



439

+69

12" x 45' V.P.

438

437

436

435

+81 - 2 FEET RT.

+73 - Road Lt

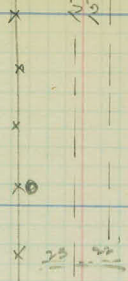
434

433

F-33'

16

+10 T.P. 28'



+81-T.P. 28'

Pasture.

+89-P.P. 28'

+74-T.P. 28'

cultivated.

+84-P.cor. 24'

+73-T.P. 25'

+99-F. cor. 32'
+86-10' Oak 22'

+56-10' Oak 16
+55-8' Oak 13

+41-F. cor. 34'

+96-T.P. 28'

timber.

cattle pass

+89-B.F. 32'
+74-F. P. 33'
+57-P.P. 28'

435

438

437

436

431

434

433

446

+17- High Ten. Power Xing.

445

+27 10" X 53' V.P.

444

443

442

441

440

453

452

+86-2 F. ENTRY

451

+46.8 2 co. Road "D"

450

449

448

447

F-29'

18

+75-A.F. 28'

453

F-23'

+52

+04 F.B. 4

+63-8" Oak 30'

F-51'

+40-6" Oak 30'

451

+23-2" Rd. 5g. 28'
+21-R. Oak 30'
+21-R. Oak 30'
+08-G.P. 24'

+21-T.P. 4'
+70-R. King 38'

+26-T.P. 4'
+02 R.P. 28'

400

+63-T.P. 28'

F-22'

447

+85-T.P. 29'

Pasture.

+71-T.P. 28'

Cultivated.

cultivated.

cultivated.

bird.

caulifl.



460

459

458

+75 12" x 54" V.P.

457

456

455

+85 - FENT. RY.

454

467

466

465

464

463

462

461

+50-F. 37
+49-12" oak 37

Timber.

cultivated.

F-78'

+60-F. cor. 34'
+59-F. cor. 37'
+49-10" Will. 30
+44-(5)-8" Will. 27'

F-35'

17'
13'

F-36'

+77-P.P. 78'

cultivated.

+82-F. cor. 33

Timber.

+85-6" oak +7'

+37-12" oak 30

+51-P.P. 78

474

+67

12" X 54.5' V.P.

473

472

+07

± FRONT RT

471

470

+38

10" X 38' V.P.

469

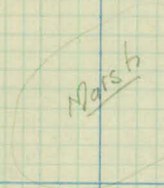
468

F-30

F-29' 21

Timber

Pasture



31' 23.6'

Willows

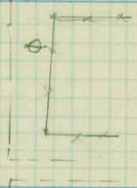
+60-Floor 60

474

473

F-33'

Yard



+95-Floor 30

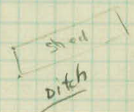
+78-P.R. 28'

+32-Floor 34

472

471

F-30



+38-cor. Shed 27 1/2'

+33-cor. Shed 30 1/2'

+95-F. cor. 41

470

+35 195-205 +41

F-32'

F-19'

Timber

Cultivated

+77-P.P. 28'

469

468

+80 - E.F. Ent L.

+70 - E.F. Ent R.

481

480

tr 12" x 70' V.P.

479

478

477

+247 Mont. (below grade 1 ft.)

476

475

+180- RR 28'
+179- cor. F. 33'
+179- cor. conc. 6/11/1932

+160- 8" oak 30'
+145- 10" oak 27'
+141- 10" oak 27'
+119- 24" Pop 29'
+101- 4" O 24'

+192- 10" Pop 29'
+176- 6" Oak 33'
+162- 24" Pop 29'
+153- 6" Tree 29'
+134- 10" Tree 29'
+111- 30" Pop 29'

+193- 12" Will 29'
+173- 12" T. Will 29'

+153- 8" will. 30'

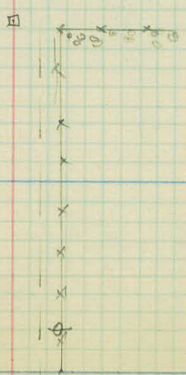
+190- 24" Pop. 26'

cultivated.

cultivated

+162- P.P. 28'

+148- F. cor. 33'



+120- F. cor. 27'
Row small Oaks

+120- P.P. 28'

488

487

+58 - Int of Road to Cemetery

486

485

484

483

+10 - d Drive to Cemetery

482

Cultivated.

+89- F. Cor. 32'

+12- RR 28
+100- F. Cor. 33 - 2 Post
+100- F. Cor. 46

+86- F. Cor. 58

+76- F. 46

+42- Cone Post 32'

+58

F- 32'

+75- P.P. 28

Cemetery.

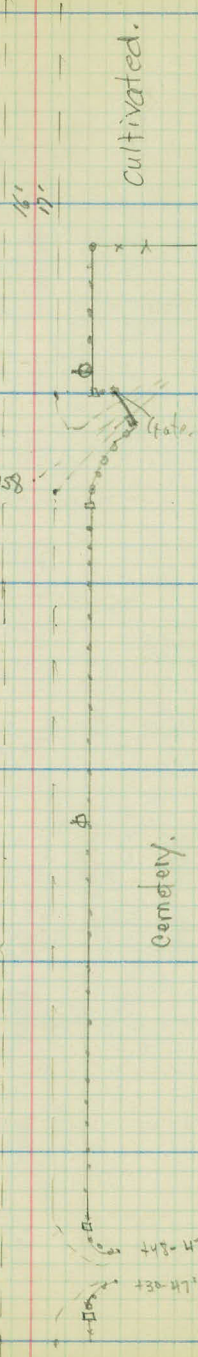
cultivated.

+62- F- 33
+61- Cone Blk P. 32'

+48- 47

+38- 47'

+12- Cone Blk Post
F- 32'
32'



495

494

493

+ 25 = 2 F. ENT. RT. & J.

492

491

490

489

Pasture.

+70 F. Oak 35

+15 0

+13-R.P. 78

495

cultivated.

444

492

+12 X 16' C.M.
+18

+35

+11 0
+17

+12 X 16' C.M.

+36-R.P. 28

+48-10" oak 25

492

cultivated.

+10 X 16' C.M.
+32

Yard

- +75 6" Oak 24
- +70-16" oak 28
- +57-10" oak 24
- +43-12" T.W. oak 23
- +32-6" oak 21
- +28-8" oak 24
- +26-6" oak 26
- +09-6" oak 24

491

+95-10" oak 30

+94-8" oak 28

+99-8" oak 16

490

+73.7 - Bay Pavc:
50 wide
46 Radius Lt. & Rt.

Cont'd next page

502

501

500

175 R.F. ENT 171

499

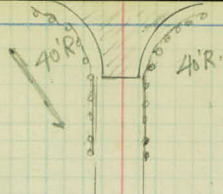
498

497

+30 15" x 67' V.P.

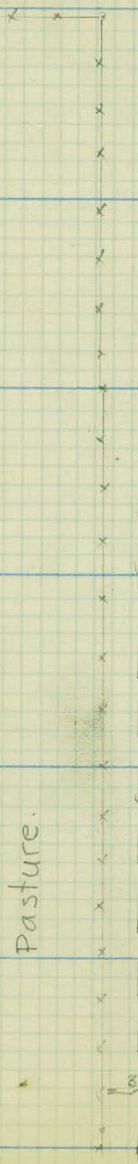
496

G.R. 27
 +92-Bill Road 138
 +75-Δ G.R. 135
 +43-Bill Road 31'
 +43-A G.R. 138
 +34-B G.R. 147



G.R. 25
 +30-Δ G.R. 134
 +40-A G.R. 134
 +32-B G.R. 147

+98 F. Cor. 36'



⊕

+27-P.P. 78'

F-35'



cultivated.

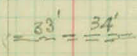
+66-10" Oak 26'
 +44-12" Oak 25'
 +34-14" Oak 25'
 +03-12" Oak 23'

198. ^{sign} cross Road 15'
 New

+15-P.P. 28'

Pasture.

— +60-Land Line.

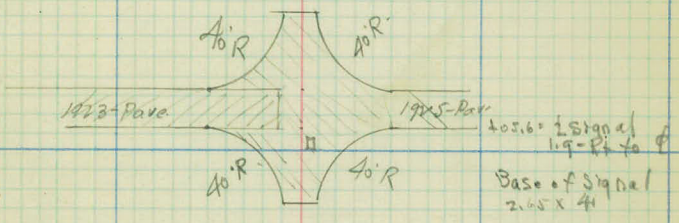


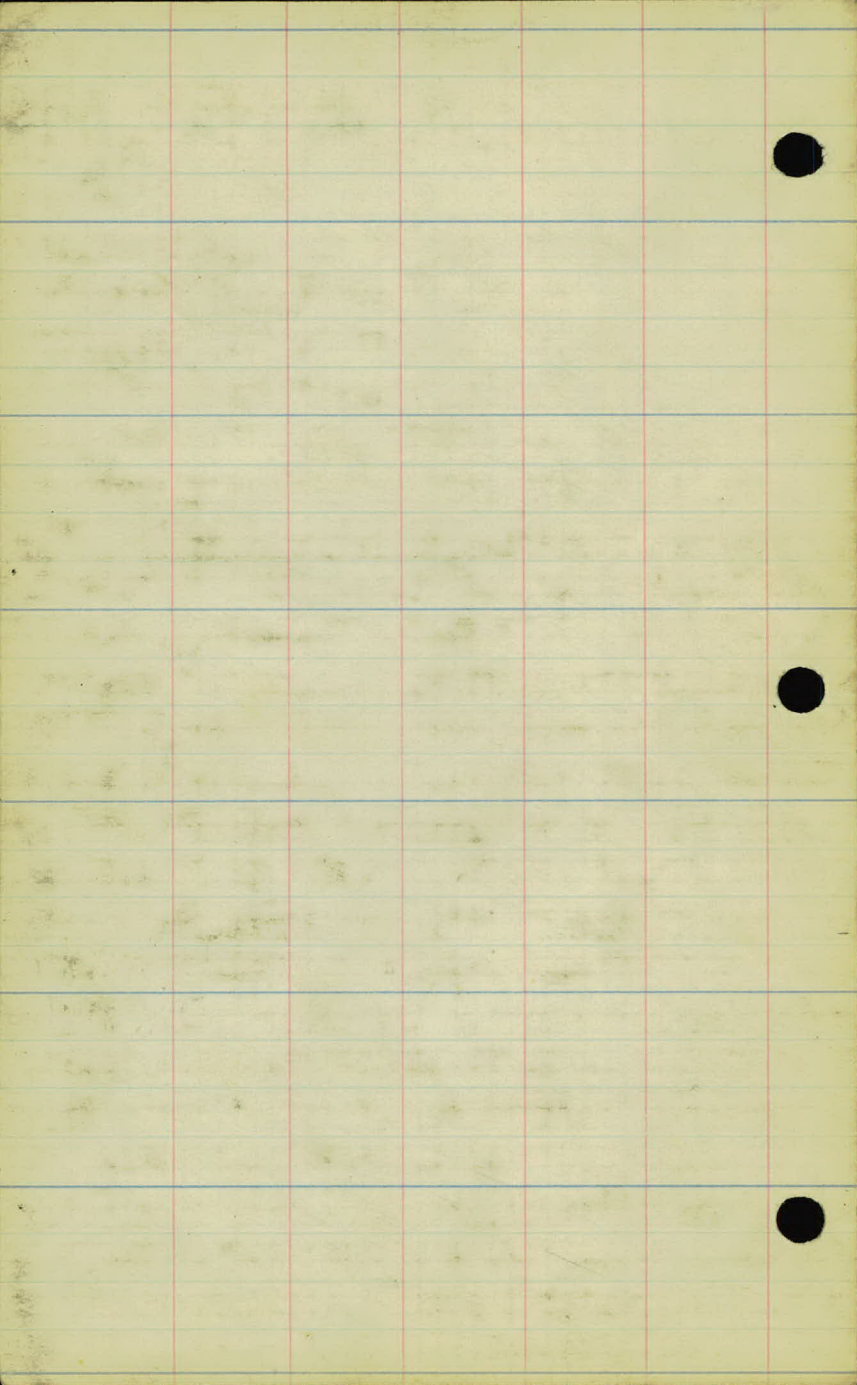
F-33'

504

173.7 † Co. Rd E, Parc.

503





Alignment
E. County Line Road.
Connection to Co. Rd. E.

Pros. 27-04

1-7-27

Wilshusen
Stooglen
Berthiaume
Messenburg

Received 1-8-27
C. P. Hanfswiler

Station Point ang. Lt. ang. Rt. Bear.

504+85.77	P.T.	45° 05'
+50		41° 30'
504+00		36° 30'
+50		31° 30'
503+23.70	P.I.	90° 10'
503+00		26° 30'
+50		21° 30'
502+00		16° 30'
+50		11° 30'
501+00		6° 30'
+50		1° 30'
500+34.94	P.C.	0° - 00'

N 0° - 59' E

489+53.7 P.O.T

$$P.I. = 503 + 23.7$$

$$\Delta = 90^\circ 10' \text{ Rt.}$$

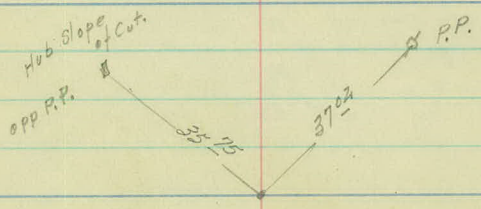
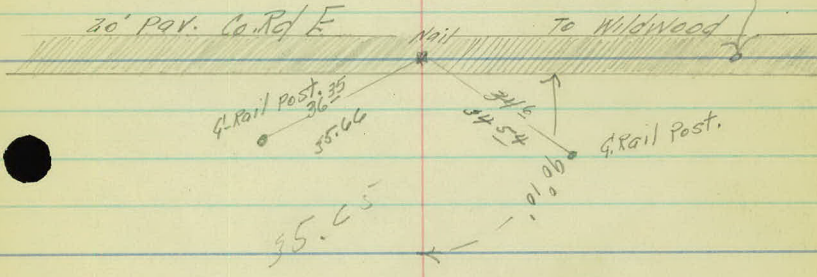
$$D = 20^\circ \text{ Curve}$$

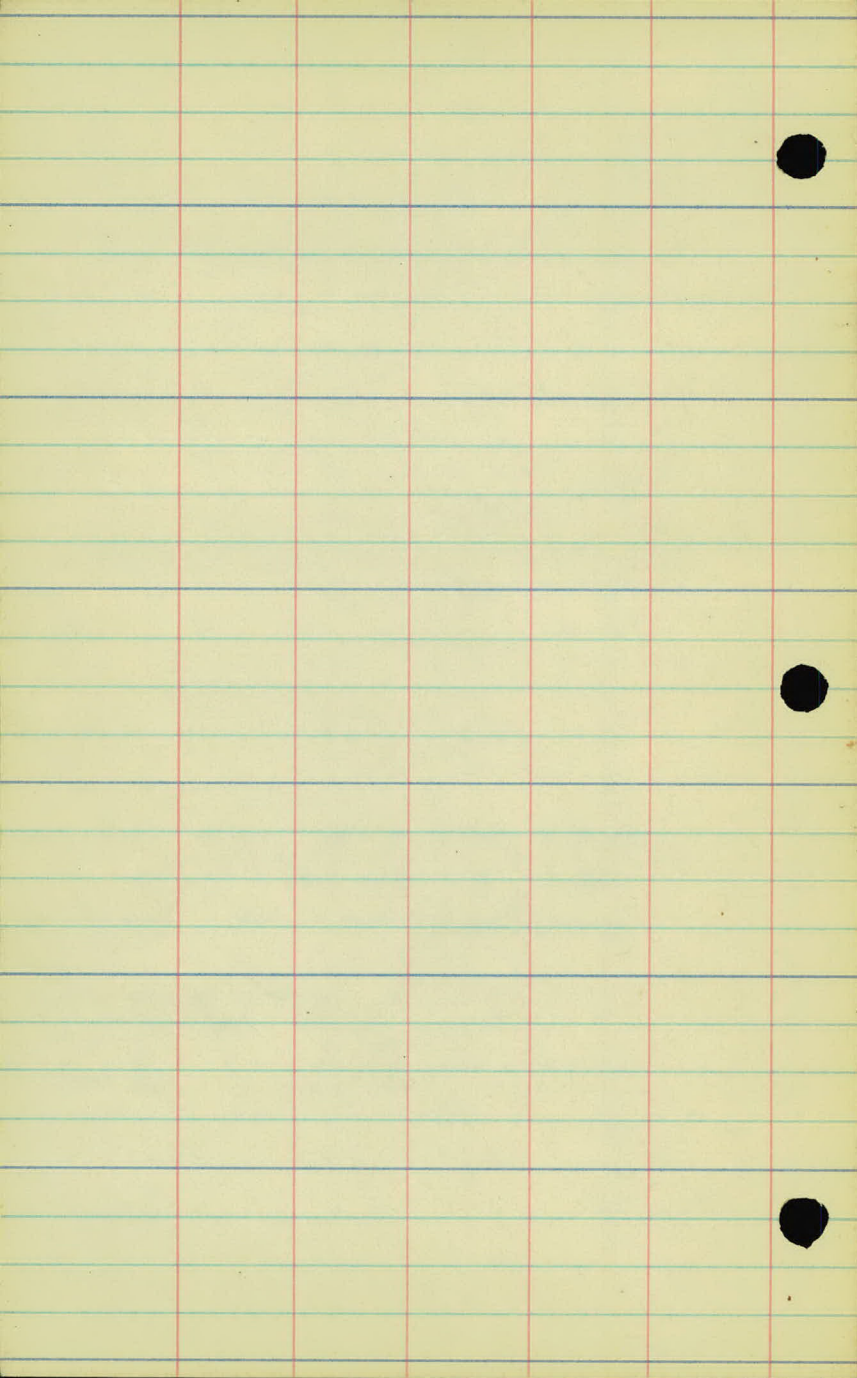
$$TAN = 288.76$$

$$h.c. = 450.83$$

$$Rad. = 287.94$$

$\frac{1}{2}$ of Pav





East County Live Road
Connection to Co. Rd. E
E Levels

1-7-27

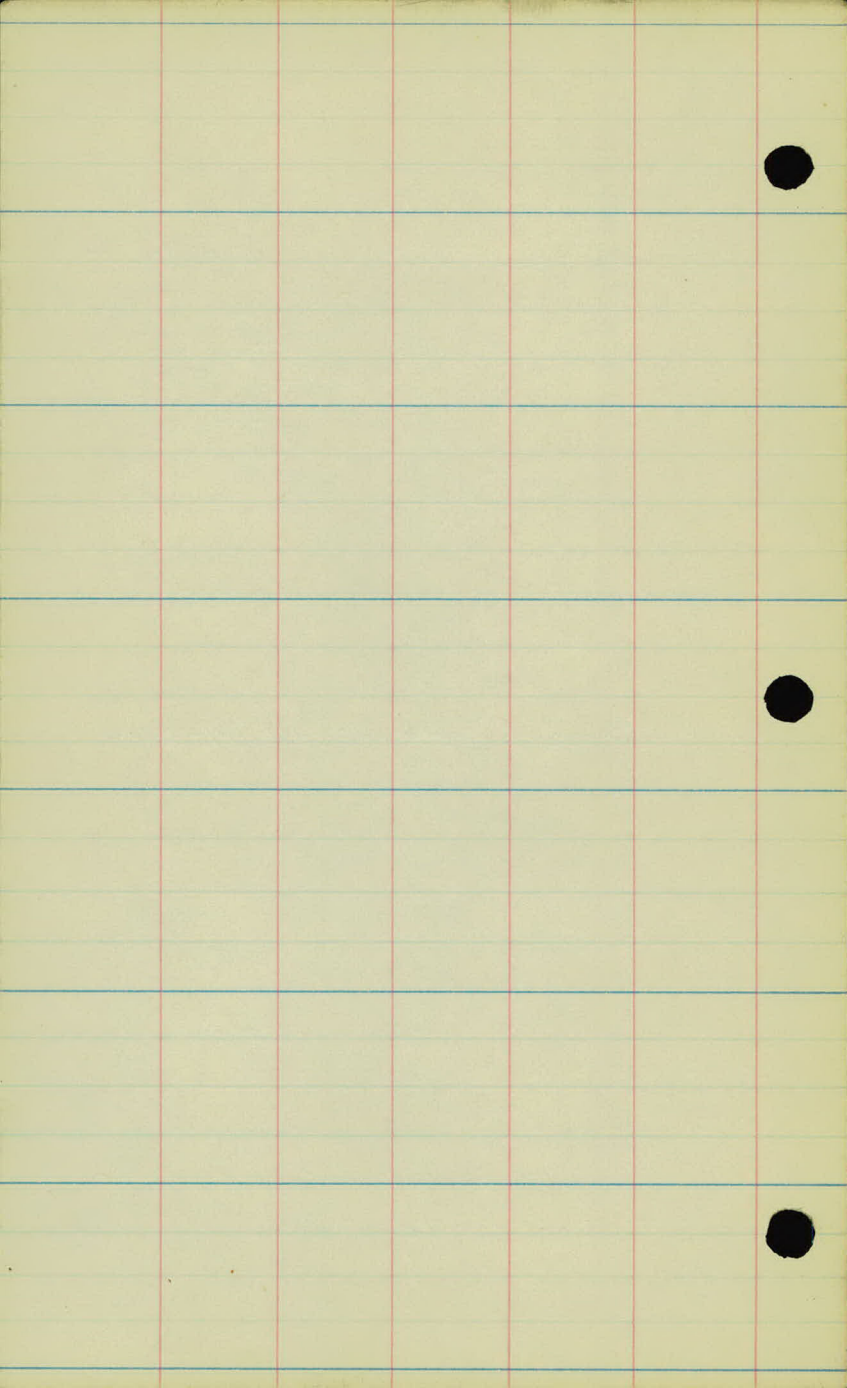
Wishuseo
atocglun
Berthiaume
Massenburg

Station	+	H.I.	-	Elev.
B.M.	4.61	1006.70		1001.59
500+34.94			0.90	05.30
+50			1.4	04.80
501+00			2.6	03.60
+34			3.2	02.00
+50			8.0	98.70
+60			9.2	97.00
502+00			13.2	93.00
+50			13.7	92.50
+78			13.5	92.70
503+00			11.0	95.70
+44			6.5	99.70
+50			8.8	97.40

R.R. Spike in 8" OAK 40' Rt. Sta. 500+70

Station	+	H.I.	-	Elev.
		1006.20		
166			11.0	94.90
+94			6.7	97.50
504+00			6.8	97.40
+12			Edge Inv. 7.3	98.90
+50			POV. 8.52	97.68
504+85.77	P.T.		POV. 9.62	96.58
B.M.			4.61	

R.R. SPIKE IN 8" OAK 40' RT. STA. 500+70



colg =

1-7-27

Wilshusen
D.S.
A.B.
H.M.

Cross Sections

E. Co. line and C. Rd E

Connection

Sta. 500+34.64 to 504+86.77

Station	+	H.I.	-	Elev.
B. M.	4.61	1006.20		1001.59

500+34.94 05.3

+50 04.8

501+00 03.6

+34 03.0

+50 98.2

502+00 93.0

250 92.5

+98 92.9

503+00 95.2

+34 99.7

+50 97.4

14.

4

1-7-27 Rt.

R.R. Spike in 8" O9K 40' Rt. 879. 500+70

$\frac{103}{33}$	$\frac{27}{27}$	$\frac{27}{22}$	$\frac{0.70}{16}$	990	$\frac{14}{15}$	$\frac{46}{23}$	$\frac{66}{30}$	$\frac{74}{23}$
------------------	-----------------	-----------------	-------------------	-----	-----------------	-----------------	-----------------	-----------------

$\frac{103}{33}$	$\frac{103}{32}$	$\frac{27}{27}$	$\frac{27}{22}$	$\frac{12}{15}$	1.4	$\frac{17}{15}$	$\frac{80}{33}$
------------------	------------------	-----------------	-----------------	-----------------	-----	-----------------	-----------------

$\frac{50}{33}$	$\frac{50}{31}$	$\frac{76}{24}$	4.6	$\frac{2.6}{8}$	$\frac{47}{14}$	$\frac{53}{18}$	$\frac{30}{21}$	$\frac{53}{33}$
-----------------	-----------------	-----------------	-----	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{39}{33}$	$\frac{30}{20}$	37.5	$\frac{5.5}{8}$	$\frac{5.4}{13}$	$\frac{26}{13}$	$\frac{33}{23}$
-----------------	-----------------	------	-----------------	------------------	-----------------	-----------------

$\frac{35}{33}$	$\frac{33}{28}$	$\frac{37}{10}$	80	$\frac{46}{6}$	$\frac{42}{9}$	$\frac{42}{33}$
-----------------	-----------------	-----------------	----	----------------	----------------	-----------------

$\frac{6.0}{33}$	$\frac{12.5}{21}$	13.2	$\frac{11.8}{11}$	$\frac{7.0}{23}$
------------------	-------------------	------	-------------------	------------------

$\frac{14.5}{33}$	$\frac{13.3}{17}$	13.7	$\frac{12.2}{21}$	$\frac{11.5}{23}$
-------------------	-------------------	------	-------------------	-------------------

$\frac{14.0}{33}$	$\frac{13.7}{19}$	13.5	$\frac{13.0}{18}$	$\frac{12.4}{33}$
-------------------	-------------------	------	-------------------	-------------------

$\frac{12.7}{33}$	$\frac{11.4}{9}$	11.0	$\frac{11.7}{22}$	$\frac{11.5}{23}$
-------------------	------------------	------	-------------------	-------------------

$\frac{4.8}{33}$	$\frac{5.1}{28}$	$\frac{7.0}{10}$	6.5	$\frac{5.5}{17}$	$\frac{7.2}{33}$
------------------	------------------	------------------	-----	------------------	------------------

PAV. F.PAV.

$\frac{53.5}{33}$	$\frac{54}{24}$	$\frac{53}{20}$	$\frac{10.5}{7}$	8.8	$\frac{6.8}{5}$	$\frac{5.5}{25}$	$\frac{6.3}{33}$
-------------------	-----------------	-----------------	------------------	-----	-----------------	------------------	------------------

Station	+	H.I.	-	Elev.
		1006.70	✓	
	+66			95.72
	+94			99.5
	504+00			99.4
	+12			98.9
	+50			97.68
	504+85 ⁷⁷	P.T		96.58
	505+00			
	+50			
	506+00			
B.M.		4.61		1001.59 ✓

Lt. Lt. Rt. 1-7-27

Pay. E.Pay
5.55 5.7 5.8 10.8 7.7 5.8 6.0
33 18 13 7 11.0 12 27 33

E.Pay E.Pay
6.3 6.55 6.65 6.75 7.4 7.2 7.4 7.0
33 28 15 5 6.7 12 20 27 33

E.Pay E.Pay
6.3 6.6 7.0 6.8 6.8 11.5 11.2 7.5 7.2
33 27 3 6.8 3 15 24 27 33

E.Pay Pay.
6.6 6.85 11.4 11.0 5.2 5.2
33 25 7.3 19 27 30 33

14.5 E.Pay E.Pay
8.3 8.42 Pay. 8.48 8.5 11.0 10.8 10.5
33 19 13 8.52 8 13 22 25 27 33

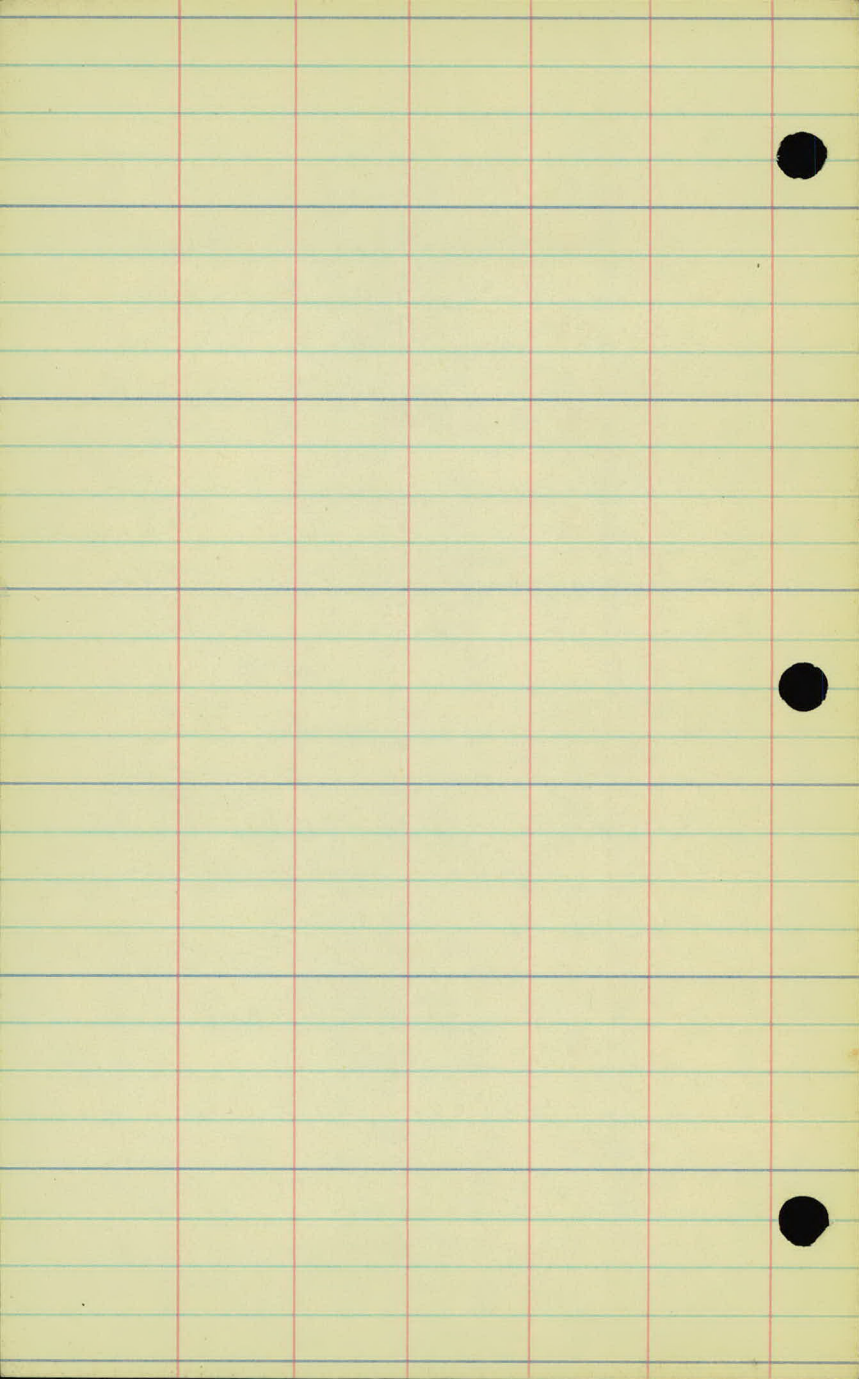
Pay. Pay.
15.0 14.5 9.7 9.64 Pay. 9.55 9.5 12.5 12.0 9.0 9.2
33 27 15 10 9.62 10 14 21 23 28 32

Pay.
10.08

Pay.
11.38

Pay.
12.42

R. R. Spike 10. 8" OAK 40' Rt. Sta. 500+70



1-7-27

E. County Line Road
connection to Co. Road E

Topography
sta. 500+34.94 to 504+85.17

1-7-27

{Wilshusen
Stoggen
Bertharine
Messenburg

505+00

504+00

503+00

502+00

501+00

500+00

+15.77 Pav-10'

+50 Pav-12.9

Edge Pav. 2' ^{1/2} Edge Pav. 3'

+50 edge Pav 26'

+52 G. Rail 21

+46 G. Rail 21

+40 G. Rail 21

+34 G. Rail 23

+33 G. Rail 21

G. Rail 6.4

+12 INT Pav.

+15.77 Pav-10'

+30 Pav-7.5

+49-K G.R-12'

+99 INT G. Rail

Cultivated

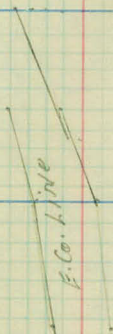
Shoulder,
Rd -2.8'

Sh
Rd 4.2' +50 Rd. 10'

134 Rd 27'

Rd 24'

+35 Rd. 16'



Cultivated

+34 RR 13

INT

+34 Sh. Line

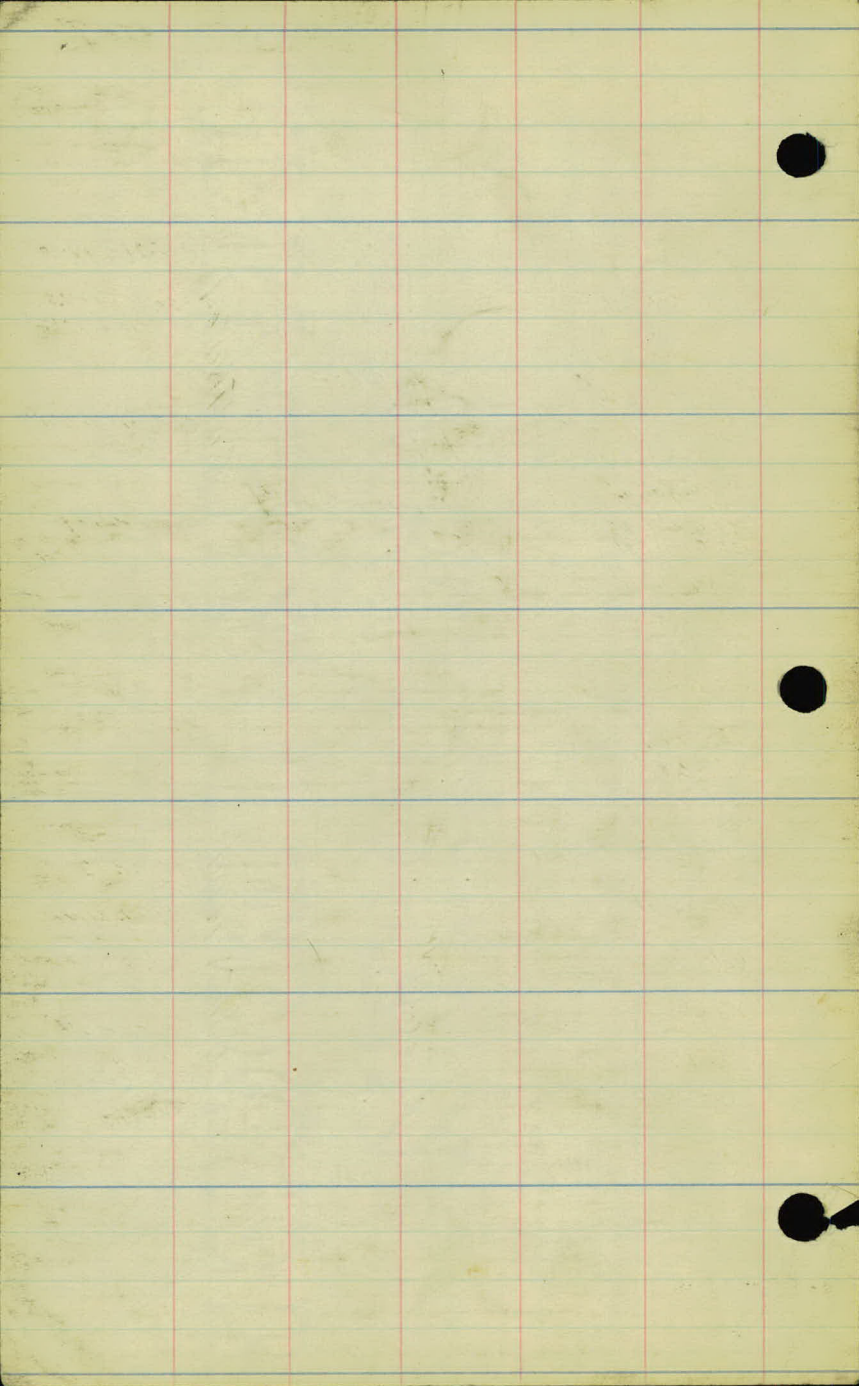
Rd. 8'

+10 Tree 24'

+42 Tree 24'

+35 Rd 15'

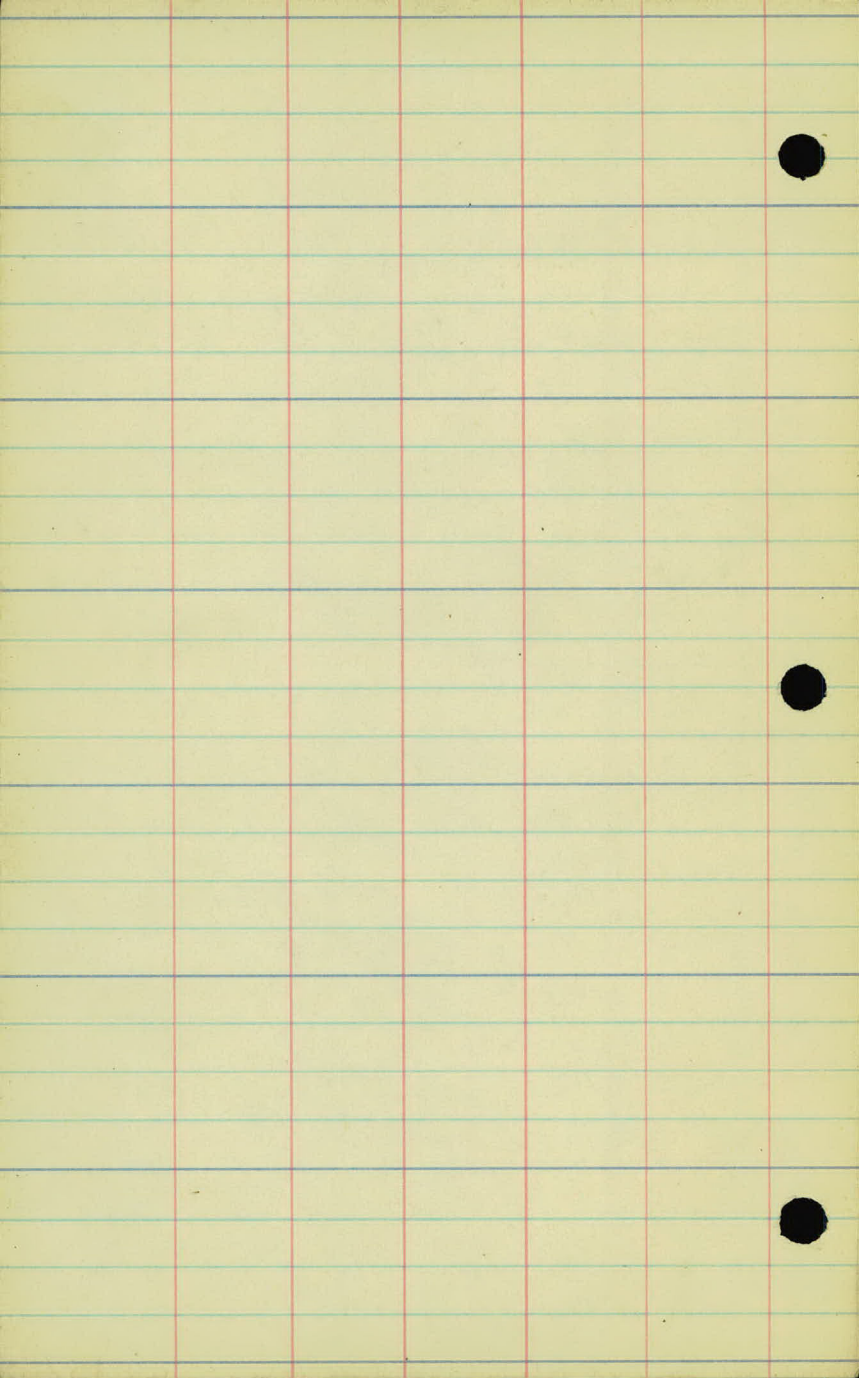
+35-24'



Proj' #27-04

X sections extended on
the left at Int. E. Co. line
& Co. Rd. E.

Received 3-5-27
O. H. H. H. H. H.



Sta.

3-4-27

LT.

④

A.M.
F.F.
E.M.

501+90

$$\frac{+7.7}{43} \quad \frac{+7.9}{29} \quad \frac{+0.1}{13} \quad \frac{+0.1}{10} \quad 9.3$$

502+00

$$\frac{+9.3}{48} \quad \frac{+8.9}{34} \quad \frac{+0.1}{22} \quad \frac{0.0}{11} \quad 11.0$$

502+50

$$\frac{+10.1}{100} \quad \frac{+10.0}{79} \quad \frac{+2.2}{66} \quad \frac{+1.4}{62} \quad \frac{+0.1}{50} \quad \frac{-0.4}{48} \quad \frac{-0.4}{25} \quad 11.8$$

502+(65)78

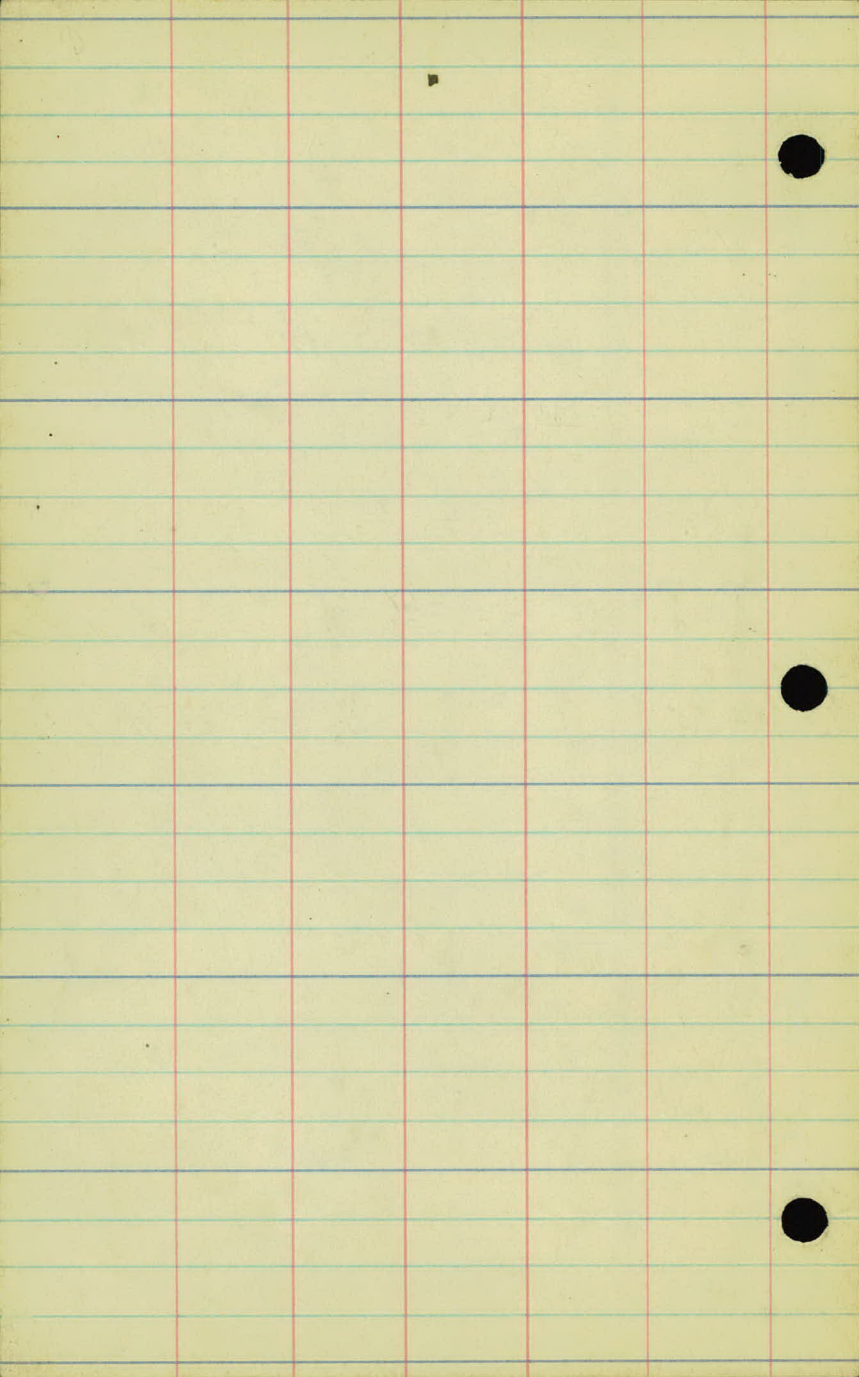
$$\frac{+10.2}{133} \quad \frac{9.8}{83} \quad \frac{+1.1}{66} \quad \frac{-0.7}{50} \quad \frac{-0.3}{30} \quad 11.8$$

503+00

$$\frac{+7.1}{77} \quad \frac{+6.9}{57} \quad \frac{-0.7}{31} \quad \frac{-1.8}{36} \quad \frac{-1.8}{24} \quad \frac{-0.8}{16} \quad 9.2$$

503+95

$$\frac{+1.4}{42} \quad \frac{+1.3}{90} \quad \frac{-2.3}{23} \quad \frac{-0.5}{11} \quad 4.4$$



~ PROJECT 27-04 ~

~ EAST COUNTY LINE ~

PLANS IN HAND INSPECTION - 2-28-27

O. R. Van Krevelen
W. J. Mackintosh
C. W. Sookup.

- ✓ ✓ 379+50 - Road Rt. - No culv. req.
- ✓ ✓ 12th Ave. on Lt. - " " "
- ✓ ✓ 380+70 - F.E. - Rt. - P. 15" x 24" C.M.
- ✓ ✓ 380+70⁵⁹ - Walk on Lt. - Rep. 12" x 10" C.M. from 394+06
- ✓ ✓ 380+70⁵⁹ - Remove steps on Lt.
- ✓ ✓ 380 to 384 - Cl. 17 T. Gr. 20 T.
- ✓ ✓ 381+57 - F.E. - Lt. P. 15" x 24" C.M.
- ✓ ✓ 382+76 - F.E. - Rt. - Remove culv. - P. 15" x 24" C.M.
- ✓ ✓ 383+00 - F.E. - Lt. - P. 15" x 24" C.M.
- ✓ ✓ 384+38 - Remove culv. P. 24" P₃.
- ✓ ✓ 386+65 - F.E. - Rt. - P. 15" x 24" C.M.
- ✓ ✓ 388+20 - " " - " "
- ✓ ✓ 390+51 - Remove culv. - P. 24" P₃.
- ✓ ✓ 391+40 - F.E. - Lt. - No culv. req.
- ✓ ✓ 391 to 393 - Cl. & Gr. 9 T.
- ✓ ✓ 391+80 - F.E. - Rt. - P. 15" x 24" C.M.
- ✓ ✓ 392+60 - Walk on Rt. - Rep. 12" x 10" C.M. from 394+06
- ✓ ✓ 393+09 - Road Lt. - P. 15" x 30" C.M.
- ✓ ✓ 394+06 - Remove culv. P. 24" P₃.
- ✓ ✓ 395 to 403 - Cl. & Gr. 40 T.
- ✓ ✓ 395+50 - Walk on Rt. - Rep. 12" x 10" C.M. from 394+06
- ✓ ✓ No culv's. req. at Co. Rd. "C."
- ✓ ✓ 397+71 - Remove culv. P. 24" P₃. H.P. on Lt. 30 C.Y.

(over)

- ✓ 398+25 - F.E. Rt. - Remove culv. - P. 15" X 24' C.M.
- ✓ 399+70 - Lt. - Leave culv. in place.
- ✓ 401+60 to 402+20 - Move hedge.
- ✓ 402+30 - F.E. Rt. - P. 15" X 24' C.M.
- ✓ 19th Ave. Remove + rep. culv. on Lt. - Rt. - P. 15" X 24' C.M.
- ✓ 406 to 407 - Cl. + Gr. 4 T.
- ✓ 20th Ave. Lt. - Remove culv. - P. 15" X 30' C.M.
- ✓ 409+26 - F.E. - Lt. - P. 15" X 24' C.M.
- ✓ 409+47 - Remove culv. P. 24" P₃
- ✓ 411+05 - F.E. Lt. - P. 15" X 24' C.M.
- ✓ 411+30 - F.E. Rt. - Remove culv. P. 15" X 24' C.M.
- ✓ 411 to 412 - Cl. + Gr. 2 T.
- ✓ 411+43 - Remove wall.
- ✓ 411+71 - F.E. - Lt. - P. 15" X 24' C.M.
- ✓ 413+30 " " "
- ✓ 414+53 " " "
- ✓ 415+03 " " No culv. req.
- ✓ 416+45 " " P. 15" X 24' C.M.
- ✓ 416+87 " Rt. "
- ✓ 418 to 422+88 Cl. 10 Gr. 3 T.
- ✓ 422+88 to 426 - Cl. 22 T. Gr. 17 T.
- ✓ 422+70 - F.E. Lt. - No culv. req.
- ✓ 423+49 - " Rt. - " " "
- ✓ 427+30 - P. 24" P₃
- ✓ 428 to 429 - Cl. 2 T.
- ✓ 434+81 - F.E. - Rt. + Lt. - P. 15" X 24' C.M. on Rt. - No culv. req. on Lt.
- ✓ 434 to 435 - Cl. + Gr. 3 T.
- ✓ 438+69 - Leave culv. - No culv. req.
- ✓ 444+27 - Remove culv. - P. 24" P₃

(27.04)

(2)

- ✓ ✓ Co. Road "D" - No culv's. req.
- ✓ ✓ 451 to 452 - Cl. + Gr. 21T.
- ✓ ✓ 451 + 86 - F.E. Rt. - No culv. req.
- ✓ ✓ 454 + 85 - " " - " " "
- ✓ ✓ 454 + 85 " Lt. - P. 15" x 24' C.M.
- ✓ ✓ 457 + 75 - Remove culv. P. 24" P₃
- ✓ ✓ 462 to 466 - Cl. 9T. Gr. 8T.
- ✓ ✓ 466 + 00 - P. 24" P₃
- ✓ ✓ 467 + 38 - Leave culv. - No culv. req.
- ✓ ✓ 467 + 50 to 473 + 50 - Cl. + Gr. 60T.
- ✓ ✓ 471 + 02 - F.E. Rt. - P. 15" x 24' C.M.
- ✓ ✓ 473 + 67 - Remove culv. P. 24" P₃
- ✓ ✓ 476 to 477 - Cl. + Gr. 4T.
- ✓ ✓ 479 to 482 - Cl. 18T. Gr. 6T.
- ✓ ✓ 479 + 72 - Remove culv. P. 24" P₃
- ✓ ✓ 481 + 70 - F.E. Lt. - No culv. req.
- ✓ ✓ 481 + 70 - " Rt. - P. 15" x 24' C.M.
- ✓ ✓ 482 + 40 - " " - " "
- ✓ ✓ 486 + 58 - " " - " "
- ✓ ✓ 491 + 32 - Walk Rt. - Remove culv. - Rep. 12" x 10' C.M. From 492 + 25.
- ✓ ✓ 490 to 492 - Cl. + Gr. 13T.
- ✓ ✓ 492 + 25 - F.E. Rt. + Lt. - ^{Remove culv's} P. - 2 - 15" x 24' C.M.
- ✓ ✓ 496 + 30 - Leave culv. No culv. req.
- ✓ ✓ 499 + 25 - F.E. Rt. - " " "
- ✓ ✓ 500 to 501 - Cl. + Gr. 4T.

Remove all G.R. at int. of Proj. and Wildwood Road - 300' - Replace on Lt. of tangent of curve on E. Co. line road - 150'

Fill intersection complete.

(over)

Guard Rail

- ✓✓ 382 to 386 - G.R. O.K.
✓ 397 to 398150 G.R. - No.
✓✓ 408 " 411 " " - O.K.
✓ 415 " 416 No.
✓✓ 417+75 " 420+75 O.K.
✓✓ 419 to 423 O.K.
✓✓ 425+50 to 429+00 - O.K. Lt.
✓✓ 426+00 to 430+00 - O.K. R!
✓✓ 438 to 440 - O.K.
✓✓ 443 to 445 O.K.
✓✓ 456 to 458 O.K.
✓✓ 464 to 467 - O.K.
✓✓ 472 to 474 O.K.
✓✓ 476+50 to 477 - O.K.
? ✓ 476 to 477 O.K.
✓✓ 479 to 480 O.K.
✓✓ 478 to 480 O.K.
✓✓ 487 to 489 O.K.
✓✓ 495 to 497 O.K.
✓✓ 501 to 503 O.K.

U 2495