

OFFICE OF  
DARBY COUNTY ENGINEER

# CONSTRUCTION NOTES

EAST CO. LINE ROAD

PROJ. 27-04

FIELD BOOK

3311

10 10 27

"12"

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

*"Copyright, 1895, by Keuffel & Esser Co."*

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

179-60

54-14

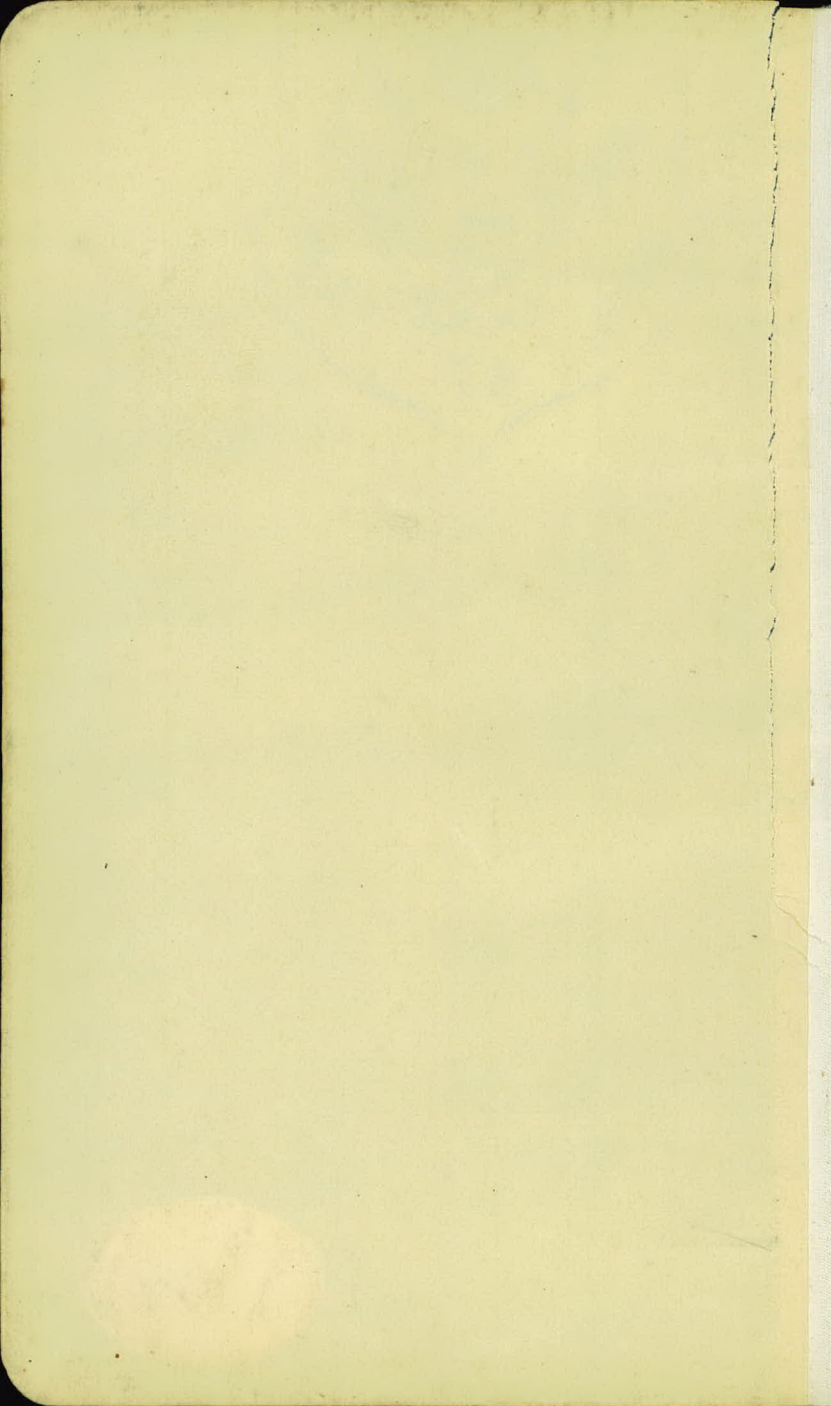
13546

179-60

150-46

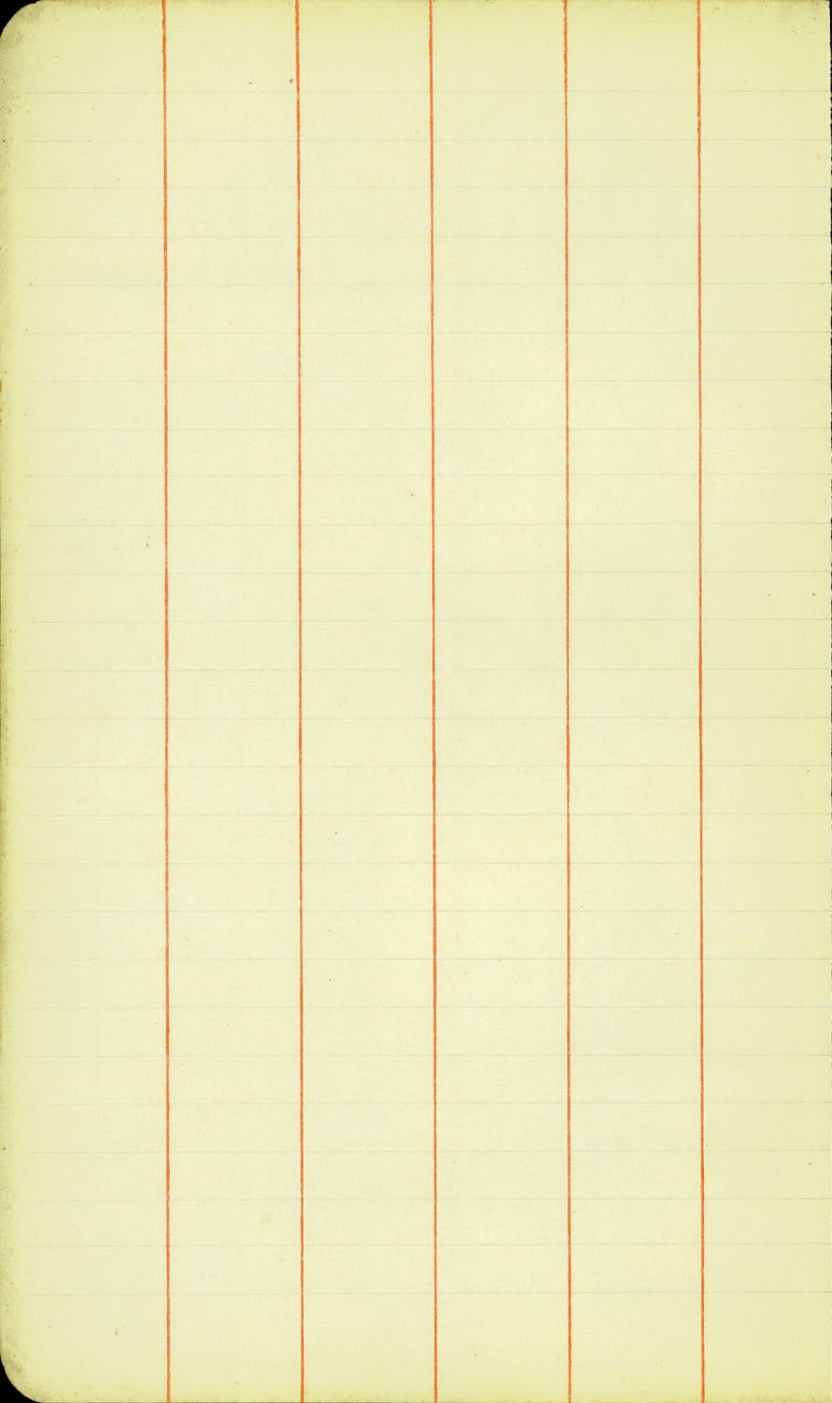
99 14

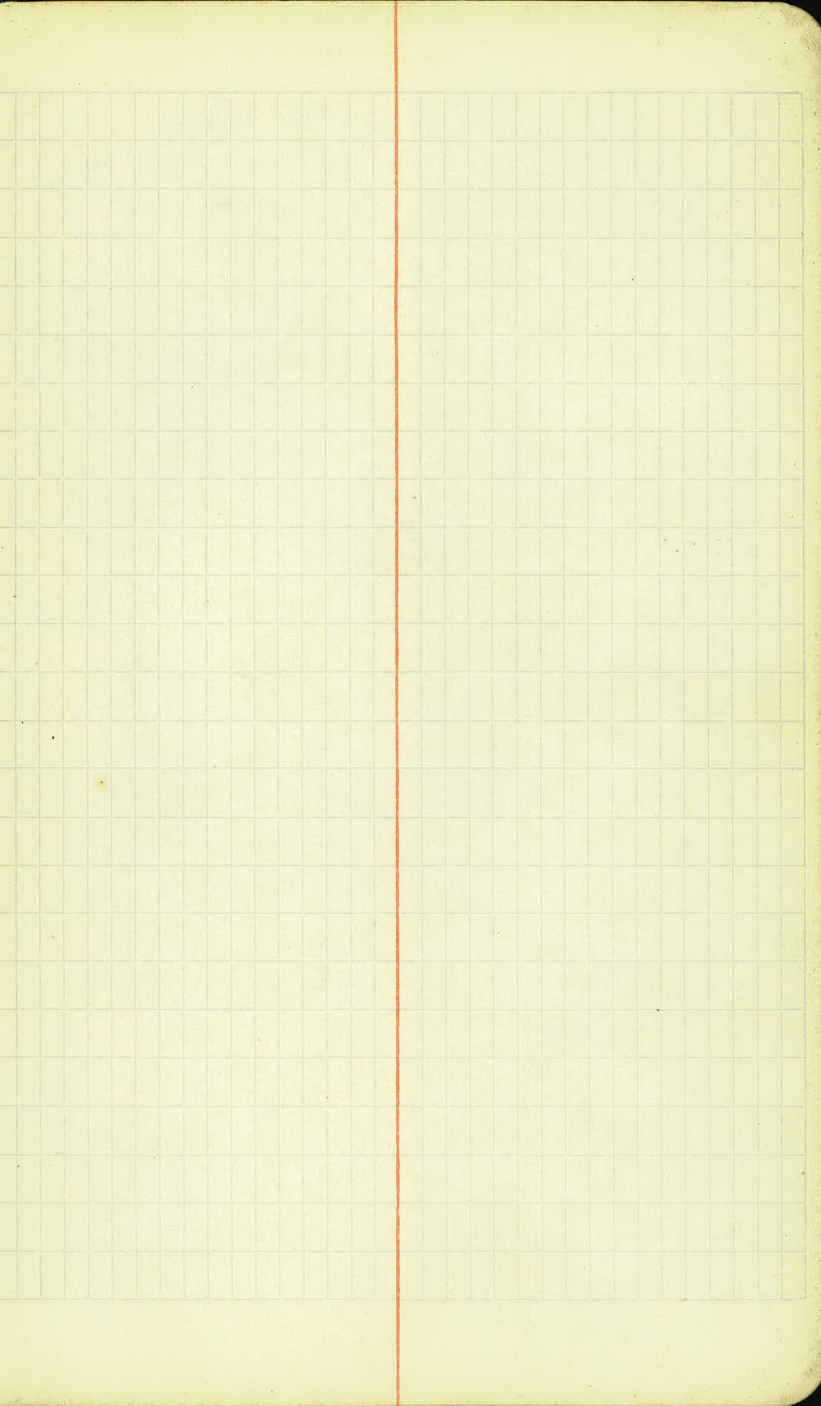




Proj. # 27-04.

Sta	to Sta.	Description.	Page	to Page.
379	503	Alignment.	1	4
379	423 <sup>150</sup>	Original X sections	9	13
404	451	Original X sections	29	38
451	505	Original X sections	15	25
		Original X Sec. Seventh St.	40	





Sta. Point A Lt. A Rt.

400+04<sup>2</sup> P.O.T.

N 10° 29' E

396+39<sup>40</sup> P.I.

0°-09'

389+93<sup>30</sup> P.O.T.

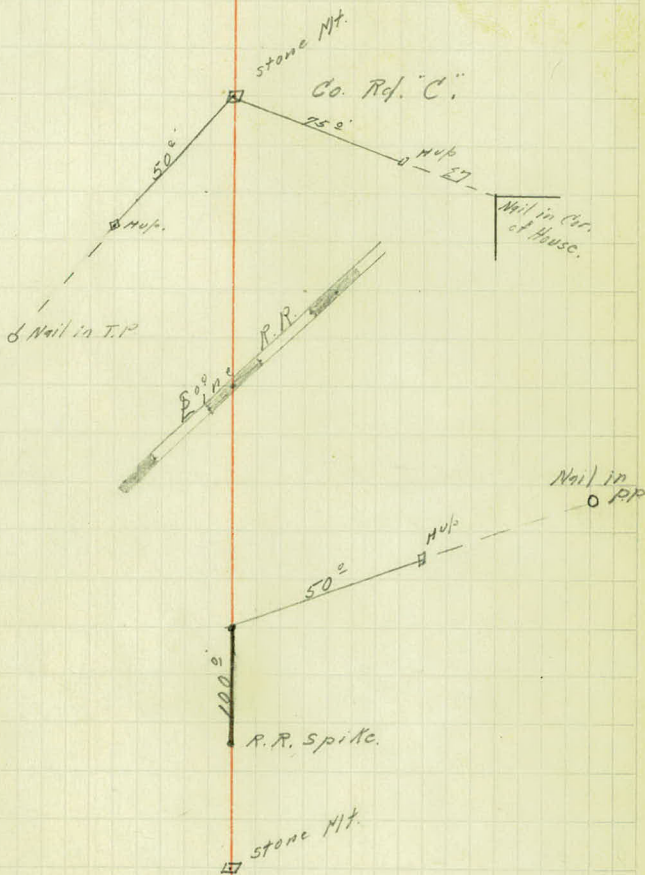
379+08<sup>2</sup> P.O.T. Beginning of Proj' 27-04.

379+00<sup>2</sup> P.O.T.

370+08<sup>5</sup> P.O.T.

6-5-27

Electric Line



Sta.	Point	$\Delta$ Lt.	$\Delta$ Rt.
423 + 30 <sup>79</sup>	P. T.	27° 07'	
423		24° 48 <sup>4</sup>	
150		21° 03 <sup>4</sup>	
422		17° 18 <sup>4</sup>	
421 + 65 <sup>4</sup> 25 05	P. I.	54° 14'	$\Delta$ - 54° 14'
150		13° 33 <sup>4</sup>	D. - 15° L.
421		9° 48 <sup>4</sup>	T. - 196 <sup>16</sup>
150		6° 03 <sup>4</sup>	L. - 361 <sup>55</sup>
420		2° 18 <sup>4</sup>	R. - 383 <sup>00</sup>
419 + 69 <sup>24</sup>	P. C.	0° 00'	

N 23° 31' W

417 + 35 <sup>16</sup>	P. T.		14° 37'
417			12° 30 <sup>4</sup>
150			9° 30 <sup>4</sup>
416 + 16 <sup>3</sup> + 15 <sup>76</sup>	P. I.		29° 14'
416			6° 30 <sup>4</sup>
150			3° 30 <sup>4</sup>
415			0° 30 <sup>4</sup>
414 + 91 <sup>55</sup>	P. C.		0° 00'
			$\Delta$ - 29° 14'
			D. - 12° N.
			T. - 124 <sup>75</sup>
			L. - 243 <sup>61</sup>
			R. - 478 <sup>34</sup>

N 30° 43' E

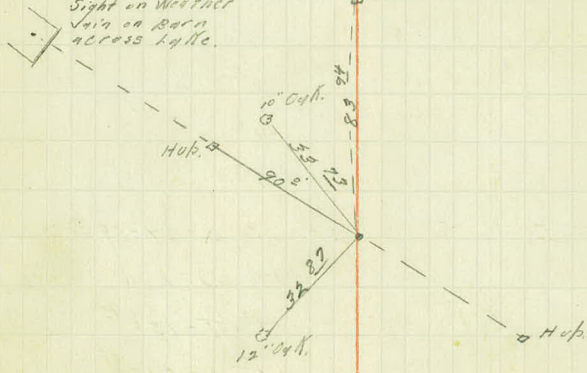
5-5-27

Nail in Corn.  
of Sign Board.



Stone Mt.

Sight on Weather  
Vain on Barn  
across Lytle.



Sta. Point  $\Delta$  Lt.  $\Delta$  Rt.

476+84<sup>2</sup> P. I. 0°-02'

450+46<sup>1</sup> P. I. 0°-02'

429+33<sup>12</sup> P. T.

429

750

428

427+79<sup>2</sup> P. I.

750

427

750

424+21<sup>0</sup> P. C.

12°-29'

11°-09<sup>c</sup>

9°-09<sup>c</sup>

7°-09<sup>c</sup>

24°-58' A-24°58'

5°-09<sup>c</sup> D.-8° R.

3°-09<sup>c</sup> T.-158<sup>70</sup>

1°-09<sup>c</sup> L.-312<sup>08</sup>

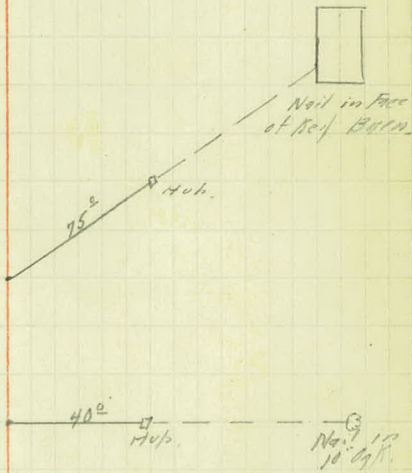
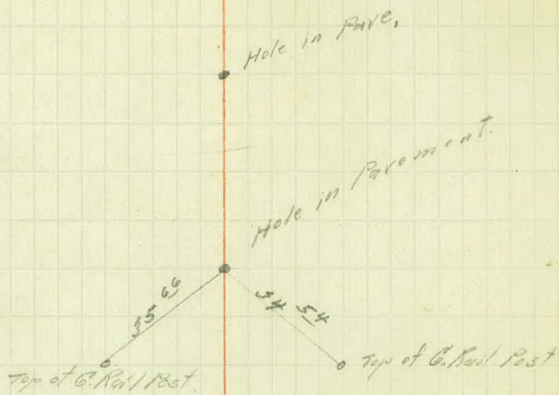
0°-00' R.-716<sup>78</sup>

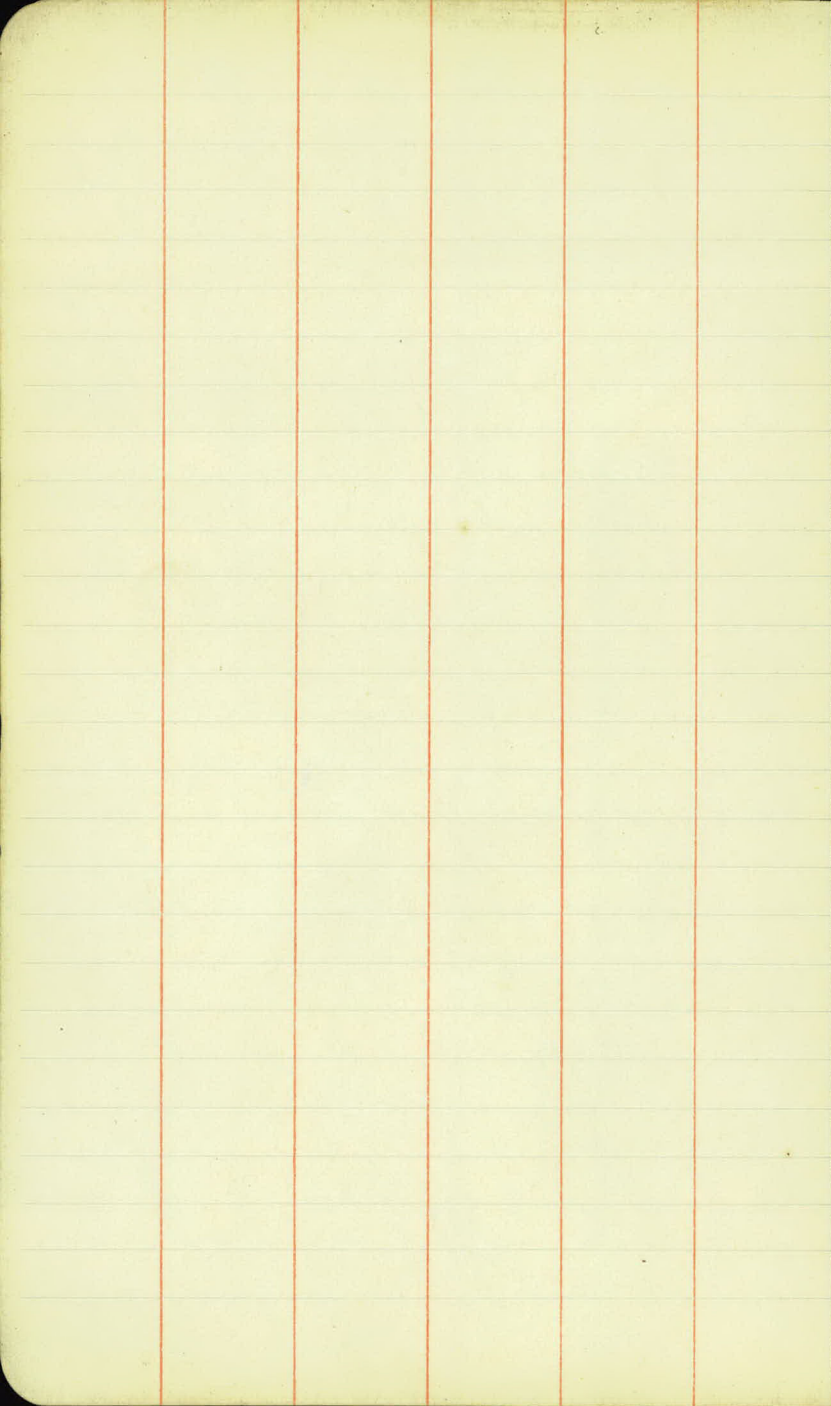
N1027'E.

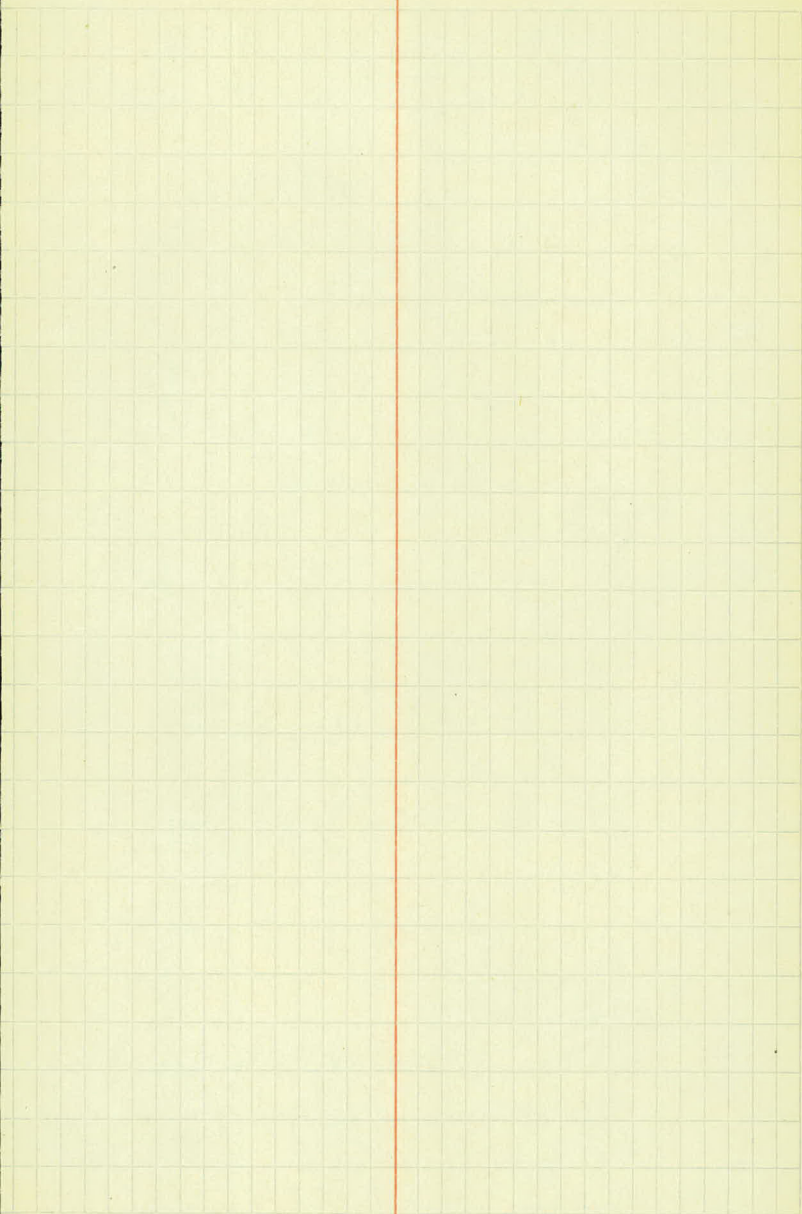


Sta.	Point	$\Delta Lt.$	$\Delta Rt.$
504 + 85 <sup>77</sup>	P. T.		45°-05
+50			41°-30
504			36°-30
+50			31°-30
503 + 23 <sup>7</sup> 12 -	P. I.		A-90°-10
503			26°-30 P.-20° R.
+50			21°-30 T.-288 <sup>76</sup>
502			16°-30 L.-450 <sup>83</sup>
+50			11°-30 R.-587 <sup>74</sup>
501			6°-30
+50			1°-30
94			
500 + 34	P. C.		0°-00
500 + 33 <sup>34</sup>			
489 + 53 <sup>7</sup>	P. O. T.		
484 + 82 <sup>0</sup> + 81 45	P. O. T.		

5-9-27







Sta.	+	H.I.	-	Elev.
B.M.	6.94	1002.38		995.44
	4.34	999.13	7.59	994.79
	5.73	997.94	4.92	994.21
B.M.			5.57	
	4.91	996.17	6.58	991.36
B.M.	5.08	996.25	5.08	991.19
				991.17
B.M.			3.69	992.57
	4.16	998.67	1.74	994.51
	5.53	998.47	5.75	992.92
B.M.			6.41	
	12.09	1009.83	0.73	997.74
	1.00	1008.89	1.94	1007.89
B.M.	7.84	1008.96	7.84	1001.05
				1001.12
B.M.			4.09	1004.87
	0.37	998.80	10.53	998.43
	4.80	997.31	6.29	992.57
	5.41	998.61	4.15	993.20
			3.99	
	10.91	1009.04	0.48	998.13
	6.97	1014.48	1.53	1007.51
B.M.			6.40	1008.08
	7.96	1019.40	3.04	1011.44
	11.17	1029.78	0.79	1018.61
	10.77	1039.84	0.69	1029.09

5-12-26

Spk. in P.P. 65 Lt. Sta. 378+85.

Spk. in T.P. 100 Lt. Sta. 389+85.

Spk. in T.P. N.W. Cor. Co. Rd. C.

Top of Nut on Hyd. N.W. Cor. Co. Rd. C

Spk. in Tree Lt. Sta. 407+15.

Spk. in Twin Oak. Lt. Sta. 416+90.

Spk. in 12" Tree Lt. Sta. 429+90.

1039.86

B.M. 5.61 1039.83 5.61 1034.25 1034.25

B.M. 6.79 1040.62 6.63 1033.23

1.29 1035.31 6.00 1034.02

4.90 1034.64 5.57 1029.74

B.M. 3.97 1030.67

6.72 1035.32 6.04 1028.60

6.93 1038.92 3.33 1031.99

B.M. 3.21 1038.91 3.21 1035.71 1035.70

7.00 1047.76 0.75 1038.16

10.46 1057.74 0.50 1047.26

4.90 1061.80 0.82 1056.90

1.21 1055.32 7.69 1054.11

B.M. 1.34 1047.18 9.48 1045.84

0.61 1036.37 11.42 1035.76

0.45 1024.57 12.45 1023.92

0.22 1013.01 11.58 1012.79

B.M. 6.01 1007.53 11.49 1001.52

B.M. 5.40 1051.18 1045.79

B.M. 9.64 1041.53

B.M. 5.41 1006.90 1001.49

B.M. 4.29 1002.61

Spk. in T.P. Lt. Sta. 450 + 25

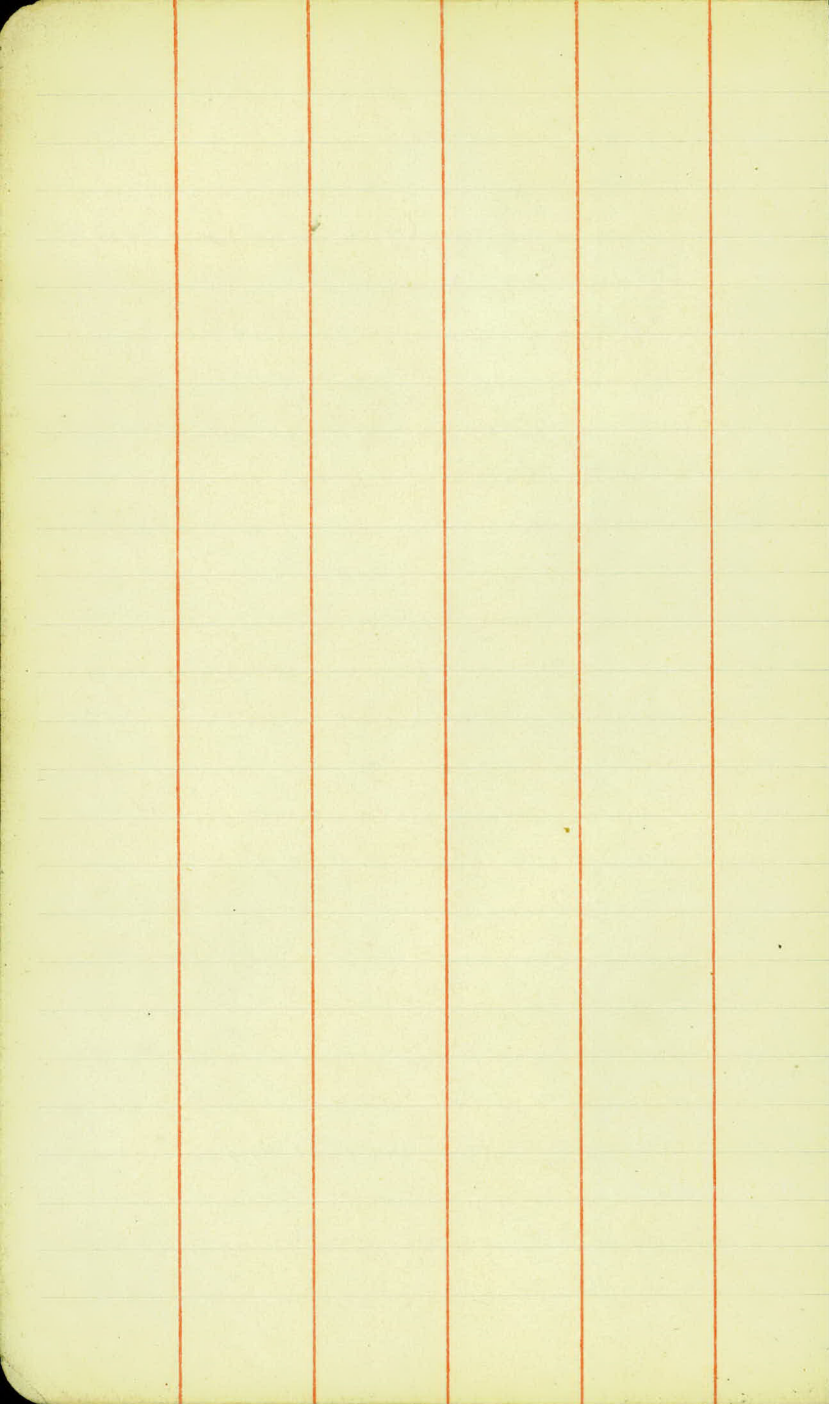
Spk. in 12" Oak 40 Lt. Sta. 462 + 80.

Spk. in 12" Oak 40 Lt. Sta. 476 + 05

Spk. in 8" Oak 33 Mt. Sta. 490 + 93.

Spk. in P.P. Mt. Sta. 492 + 33

Spk. in P.P. N.E. Cor. Int. Co. Rd. F. & E. Co. Line



This image shows a blank ledger page with a grid of 20 columns and 30 rows. A vertical red line runs down the center, dividing the page into two equal halves of 10 columns each. The grid is composed of light gray lines, and the page is otherwise empty of any text or markings.

Sta.	+	H. I.	-	Elev.	Gr. Rod
B.M.	7.74	1003.18		995.44	
379+08				97.0	6.2
T.P.	7.91	1003.35	7.74	995.44	
+18				97.0	6.4
+25				97.0	8.1 6.4
+50				97.0	7.9 6.4
+60				97.0	6.4
380				97.0	7.4 6.4
+46 <sup>1</sup>				97.0	7.0 6.4
+60				97.0	6.4
381				97.0	6.5 6.4
T.P.	7.11	1002.55	7.91	995.44	
+50				96.7	5.9
382				96.2	6.4
+60				95.9	7.3

5-21-27

Spok. in P.P. 65' Lf. 5' Tol. 3.28 7.85  
 7.2 6.8 7.1 6.4 5.7 5.2 4.8 4.5 4.0 0.6/3.3 3.3  
 4.6 4.0 3.9 2.6 1.6 1.0 1.4 9 1.8 8/7.1 3.3

7.2 6.8 7.1 5.6 4.9 4.8 3.5 2.8 2.8  
 4.1 3.5 3.4 1.6 1.0 1.8 3.1 3.3

8.2 8.3 7.2 7.1 6.5 5.4 4.9 4.2 3.6 2.4 2.5  
 5.0 4/5/8.5 40 36 31 22 11 11.0 16 20 8/2.4 3.3  
 4/0.4

6.9 4/7.8 7.9 6.8 5.4 5.2 0/1.7  
 5.0 3/10.1 5.8 1.6 11.0 9 3/14.8

6.0 7.1 7.5 7.6 5.9 5.6 5.3 5.8 2.1 2.0  
 5.0 4.4 3.3 2.4 1.1 1.4 3.9 3.0 3.3

6.5 4/6.6 6.2 6.0 6.4 7.2 6.9 2.8 1.7  
 3.3 2/10.8 1.4 1.4 8 11 17 2.4 3.3

2.5 1/2.5 2.6 6.1 6.1 6.6 6.0 5.8 6.5 6.9 6.4 5/5.5 4.2 4.0  
 3.3 3/7.4.5 3.0 2.6 2.4 1.9 1.2 10.6 9 1.2 3.4 2/11.0 3.2 3.3

2.4 2.6 6.2 6.5 6.0 5.8 6.4 7.6 7.8 5.9 3.3 3.3  
 3.3 3.0 2.4 2.1 1.2 9 1.3 2.4 2.8 2.9 3.3

3.4 5/3.5 3.7 6.4 6.9 5.9 5.7 6.4 5.4 0/2.8 7.6 4.1 2.0 1.7  
 3.3 3/13.0 2.8 2.3 1.8 1.1 10.7 10 1.4 6/2.5 2.3 2.9 3.0 3.3

5.4 1/5.4 5.5 5.5 5.7 5.9 8.0 8.3 7.2 4.1 3.1 0.4  
 3.3 4/10.5 2.2 1.3 10.7 10 1.6 9/2.4 2.5 3.2 3.3 3.3

6.9 5/6.4 6.1 5.7 6.2 8.0 9/8.5 8.2 3.0  
 3.3 2/10.3 1.1 10.7 11 1.5 8/1.7 2.9 3.5

9.8 9.1 4/7.9 7.1 6.5 7.1 8/8.8 8.9 5.2 4.4  
 3.3 2.1 1.6/10.6 1.4 10.8 1.4 8/1.5 2.9 3.4 3.3

Sta.	+	H.I.	-	Elev.	Gr. Rod
		1002.55			
	+85			95.1	7.5
383				95.0	7.0
	+50			94.4	8.2
T.P.	5.41	999.41 <sup>✓</sup>	8.55	994.00 <sup>✓</sup>	
384				94.0	5.4
385				93.6	5.8
	+50			93.6	5.8
386				93.8	5.6
	+50			94.0	5.4
387				94.1	5.3
	+50			94.2	5.2
388				94.1	5.3
	+35			94.0	5.4

5-21-27

$\frac{11.3}{33}$	$\frac{11.1}{24}$	$\frac{10.4}{20}$	$\frac{7.5}{14}$	$\frac{6.8}{17}$	$\frac{7.1}{17}$	$\frac{8.4}{23}$	$\frac{8.5}{33}$
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$\frac{12.7}{33}$	$\frac{12.6}{25}$	$\frac{11.9}{24}$	$\frac{6}{2}$	$\frac{11.4}{-3.8}$	$\frac{11.1}{21}$	$\frac{7.8}{14}$	$\frac{7.1}{10.5}$	$\frac{7.5}{10}$	$\frac{9.8}{17}$	$\frac{4}{-3.2}$	$\frac{9.8}{26}$	$\frac{10.1}{33}$	$\frac{8.8}{33}$
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$\frac{14.0}{33}$	$\frac{8}{5}$	$\frac{13.6}{-5.4}$	$\frac{13.8}{25}$	$\frac{13.1}{24}$	$\frac{12.9}{21}$	$\frac{8.4}{13}$	$\frac{8.0}{10.2}$	$\frac{8.3}{10}$	$\frac{12.6}{17}$	$\frac{2}{5}$	$\frac{13.5}{-5.1}$	$\frac{13.1}{33}$
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$\frac{10.9}{32}$	$\frac{8}{5}$	$\frac{10.8}{-5.4}$	$\frac{11.0}{24}$	$\frac{10.4}{23}$	$\frac{10.4}{21}$	$\frac{6.0}{14}$	$\frac{5.4}{0.0}$	$\frac{5.4}{10}$	$\frac{10.0}{18}$	$\frac{4}{2}$	$\frac{10.1}{-4.7}$	$\frac{10.1}{33}$
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$\frac{10.8}{33}$	$\frac{0}{2}$	$\frac{10.8}{-5.0}$	$\frac{10.4}{23}$	$\frac{10.0}{21}$	$\frac{6.0}{14}$	$\frac{5.7}{10.1}$	$\frac{6.0}{11}$	$\frac{9.4}{16}$	$\frac{10.4}{17}$	$\frac{4}{2}$	$\frac{10.5}{-4.7}$	$\frac{10.2}{33}$
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$\frac{10.0}{33}$	$\frac{9.9}{23}$	$\frac{2}{2}$	$\frac{9.4}{-3.6}$	$\frac{8.9}{19}$	$\frac{5.7}{14}$	$\frac{5.4}{10.4}$	$\frac{5.7}{7}$	$\frac{6.2}{11}$	$\frac{8.0}{13}$	$\frac{9.3}{18}$	$\frac{7.5}{19.2}$	$\frac{47.5}{-3.7}$	$\frac{8.6}{25}$	$\frac{8.6}{33}$
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$\frac{6.8}{33}$	$\frac{8.5}{27}$	$\frac{8.5}{23}$	$\frac{2}{2}$	$\frac{8.2}{-2.6}$	$\frac{8.0}{18}$	$\frac{5.9}{14}$	$\frac{5.1}{10.5}$	$\frac{5.7}{11}$	$\frac{9.0}{18}$	$\frac{0}{2}$	$\frac{9.1}{-3.5}$	$\frac{8.7}{25}$	$\frac{5.6}{28}$	$\frac{5.3}{33}$
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$\frac{2.1}{57}$	$\frac{6.4}{30}$	$\frac{7.1}{25}$	$\frac{2}{8}$	$\frac{7.0}{-1.2}$	$\frac{5.2}{14}$	$\frac{4.9}{10.5}$	$\frac{5.5}{11}$	$\frac{7.5}{17}$	$\frac{7.7}{22}$	$\frac{6.6}{25}$	$\frac{9}{2}$	$\frac{6.8}{-0.6}$	$\frac{4.4}{27}$	$\frac{4.5}{33}$
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$\frac{4.6}{57}$	$\frac{6.3}{33}$	$\frac{7.6}{28}$	$\frac{6}{7}$	$\frac{7.6}{-2.3}$	$\frac{5.3}{14}$	$\frac{4.8}{10.5}$	$\frac{5.4}{13}$	$\frac{6.6}{14}$	$\frac{9.0}{17}$	$\frac{9.0}{18}$	$\frac{6.5}{20}$	$\frac{5.6}{21.6}$	$\frac{47.5}{0.0}$	$\frac{4.8}{33}$
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$\frac{7.2}{33}$	$\frac{7.5}{24}$	$\frac{4}{19}$	$\frac{7.4}{-3.2}$	$\frac{7.0}{17}$	$\frac{5.4}{13}$	$\frac{5.1}{10.1}$	$\frac{5.5}{12}$	$\frac{7.5}{16}$	$\frac{0}{2}$	$\frac{7.7}{-2.5}$	$\frac{7.2}{24}$	$\frac{7.7}{27}$	$\frac{9.3}{27}$	$\frac{7.5}{30}$
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$\frac{7.5}{33}$	$\frac{8}{19}$	$\frac{7.7}{-2.4}$	$\frac{7.5}{18}$	$\frac{5.5}{13}$	$\frac{5.3}{10.1}$	$\frac{5.4}{13}$	$\frac{8.1}{17}$	$\frac{8}{2}$	$\frac{8.7}{-3.4}$	$\frac{9.0}{33}$
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$\frac{6.3}{-0.9}$	$\frac{6.1}{29}$	$\frac{7.1}{28}$	$\frac{6.9}{24}$	$\frac{6.0}{22}$	$\frac{5.8}{20}$	$\frac{6.0}{16}$	$\frac{5.3}{14}$	$\frac{5.0}{10.4}$	$\frac{5.6}{16}$	$\frac{6.2}{19}$	$\frac{3}{2}$	$\frac{6.4}{-1.0}$	$\frac{6.3}{33}$
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Sta.	+	H. I.	-	Elev.	Cr. Rog
		999.41			
	+75			93.9	5.5
389				93.9	5.5
T.P.	4.14	998.22	5.33	994.08	
	+50			93.7	4.5
B.M.			5.25	992.37	
	+79			93.6	4.6
390				93.6	4.6
	+25			93.5	4.7
	+60			93.3	4.9
391				93.2	5.0
	+50			92.9	5.3
392				92.6	5.4
	+50			92.1	6.1
393				91.7	6.5

5-21-27

$\frac{1.6}{34}$	$\frac{5.4}{30}$	$\frac{6.9}{26}$	$\frac{6.8}{19}$	$\frac{5.8}{16}$	$\frac{5.0}{13}$	$\frac{5.7}{14}$	$\frac{6.5}{23}$	$\frac{6.6}{28}$	$\frac{4.0}{27}$	$\frac{3.6}{33}$
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$\frac{5.2}{55}$	$\frac{3.9}{33}$	$\frac{0}{10.5}$	$\frac{5.0}{30}$	$\frac{6.9}{24}$	$\frac{7.2}{21}$	$\frac{6.8}{16}$	$\frac{5.8}{10.5}$	$\frac{5.0}{14}$	$\frac{5.9}{16}$	$\frac{6.6}{22}$	$\frac{6.7}{29}$	$\frac{2.0}{3}$	$\frac{0}{141}$
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$\frac{3.3}{3}$	$\frac{0}{7.2}$	$\frac{5.7}{31}$	$\frac{5.7}{24}$	$\frac{6.4}{15}$	$\frac{5.2}{12}$	$\frac{4.1}{10.7}$	$\frac{5.8}{18}$	$\frac{4.3}{16}$	$\frac{5.8}{24}$	$\frac{5.2}{27}$	$\frac{2.8}{30}$	$\frac{1.9}{3}$	$\frac{0}{12.7}$
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Sp N. in T.P. 100 Lt. 579. 389+85.

$\frac{5.8}{35}$	$\frac{4.5}{12}$	$\frac{4.2}{7}$	$\frac{5.8}{10}$	$\frac{3.9}{18}$	$\frac{5.1}{17}$	$\frac{5.0}{25}$	$\frac{4.3}{27}$	$\frac{4.2}{33}$
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$\frac{7.8}{53}$	$\frac{7.4}{21}$	$\frac{0}{10}$	$\frac{4.6}{20}$	$\frac{4.2}{14}$	$\frac{3.9}{10.7}$	$\frac{4.0}{14}$	$\frac{4.1}{24}$	$\frac{0}{3}$	$\frac{4.5}{10.1}$
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$\frac{7.3}{33}$	$\frac{6.3}{22}$	$\frac{4.4}{12}$	$\frac{5.8}{10}$	$\frac{4.0}{12}$	$\frac{4.9}{15}$	$\frac{5.0}{25}$	$\frac{4.4}{27}$	$\frac{4.5}{33}$
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$\frac{8.2}{59}$	$\frac{0}{2}$	$\frac{0}{-2.5}$	$\frac{7.4}{18}$	$\frac{7.0}{13}$	$\frac{4.5}{11.0}$	$\frac{3.9}{12}$	$\frac{4.3}{15}$	$\frac{5.8}{20}$	$\frac{7.3}{21}$	$\frac{8.4}{22}$	$\frac{2.4}{26}$	$\frac{6.1}{3}$	$\frac{0}{-0.6}$
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$\frac{0}{-1.5}$	$\frac{0}{6.5}$	$\frac{6.4}{28}$	$\frac{6.8}{17}$	$\frac{0}{10}$	$\frac{5.0}{10.7}$	$\frac{4.3}{12}$	$\frac{5.0}{14}$	$\frac{5.9}{23}$	$\frac{6.5}{29}$	$\frac{5.9}{3}$	$\frac{0}{-0.9}$
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$\frac{0}{71.8}$	$\frac{0}{3.5}$	$\frac{3.6}{27}$	$\frac{7.1}{22}$	$\frac{6.9}{17}$	$\frac{6.4}{18}$	$\frac{4.7}{10.4}$	$\frac{5.7}{14}$	$\frac{6.5}{16}$	$\frac{6.8}{24}$	$\frac{5.9}{31}$	$\frac{0}{3}$	$\frac{0}{71.5}$
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$\frac{0}{11.2}$	$\frac{0}{4.4}$	$\frac{5.0}{24}$	$\frac{7.3}{24}$	$\frac{7.3}{18}$	$\frac{5.8}{13}$	$\frac{5.1}{10.5}$	$\frac{6.1}{16}$	$\frac{7.1}{19}$	$\frac{7.2}{23}$	$\frac{6.5}{25}$	$\frac{0}{3}$	$\frac{0}{-0.7}$
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$\frac{0}{10.5}$	$\frac{0}{6.6}$	$\frac{7.0}{21}$	$\frac{8.3}{20}$	$\frac{7.7}{15}$	$\frac{6.3}{13}$	$\frac{5.6}{10.5}$	$\frac{6.5}{17}$	$\frac{8.0}{21}$	$\frac{8.3}{33}$	$\frac{0}{15}$	$\frac{0}{-0.2}$
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$\frac{6.7}{33}$	$\frac{0}{15}$	$\frac{0}{-0.2}$	$\frac{6.5}{10.4}$	$\frac{6.1}{10}$	$\frac{0}{10}$	$\frac{6.5}{19}$	$\frac{6.9}{23}$	$\frac{8.7}{23}$	$\frac{7.2}{33}$
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Sta.	+	M. I.	-	Elev.	Gr. Rod
		798.22			
	+35			71.3	6.9
394				71.4	6.8
T.P.	4.38	996.30	6.50	991.92	
	+50			90.9	5.4
B.M.	5.12	796.29	5.12	991.18	991.18
395				90.9	5.4
	+50			90.9	5.4
396				91.1	5.2
	+20			91.2	5.1
	+39 <sup>4</sup>			91.2	5.1
	+63			91.4	4.9
397				91.4	4.7
	+50			91.9	4.4
398				92.3	4.0

5-23-27

<u>90</u>	<u>89</u>	<u>69</u>	<u>64</u>	<u>68</u>	<u>87</u>	<u>73</u>
33	16	11	10.5	17	22	33

<u>96</u>	<u>0</u>	<u>93</u>	<u>90</u>	<u>70</u>	<u>64</u>	<u>66</u>	<u>68</u>	<u>89</u>	<u>90</u>	<u>101</u>	<u>101</u>	<u>87</u>	<u>85</u>
33	2	-2.5	16	11	10.4	15	18	23	24	35	27	27	33

<u>79</u>	<u>72</u>	<u>2</u>	<u>80</u>	<u>72</u>	<u>53</u>	<u>47</u>	<u>5.1</u>	<u>5.1</u>	<u>66</u>	<u>69</u>	<u>0</u>	<u>68</u>
33	23	2	-2.6	15	10	10.7	15	15	17.7	27	3	-1.4

5/10 N. in T.P. N.W. Cor. Co. Rd "C"

<u>78</u>	<u>4</u>	<u>26</u>	<u>73</u>	<u>54</u>	<u>48</u>	<u>5.3</u>	<u>70</u>	<u>71</u>	<u>0</u>	<u>6.3</u>
33	9	2.2	15	11	10.6	15	19	23	3	-0.9

<u>0</u>	<u>64</u>	<u>58</u>	<u>5.2</u>	<u>6.3</u>	<u>6.3</u>	<u>5.5</u>	<u>4.9</u>	<u>5.5</u>	<u>6.7</u>	<u>4</u>	<u>7.1</u>	<u>7.0</u>	<u>3.8</u>	<u>3.2</u>
3	-1.0	2.8	1.8	1.4	1.5	1.0	10.5	16	18	2	-1.7	26	30	33

<u>0</u>	<u>5.5</u>	<u>46</u>	<u>6.3</u>	<u>5.2</u>	<u>4.8</u>	<u>5.3</u>	<u>4</u>	<u>6.5</u>	<u>6.5</u>	<u>37</u>	<u>29</u>
3	-0.3	1.9	1.6	1.8	10.4	12	2	-1.3	2.7	33	34

<u>60</u>	<u>64</u>	<u>50</u>	<u>47</u>	<u>5.2</u>	<u>6.3</u>
33	28	11		19	33

<u>5.3</u>	<u>5.1</u>	<u>46</u>	<u>48</u>	<u>46</u>
33	20		21	33

<u>7.1</u>	<u>64</u>	<u>5.2</u>	<u>46</u>	<u>5.0</u>	<u>5.8</u>	<u>5.5</u>	<u>5.8</u>
33	18	10	10.3	12	23	164	33

(26A)

<u>8.5</u>	<u>3</u>	<u>80</u>	<u>7.1</u>	<u>5.6</u>	<u>5.1</u>	<u>5.7</u>	<u>7.5</u>	<u>8</u>	<u>7.6</u>	<u>80</u>	<u>44</u>	<u>57</u>
33	2	-3.3	15	11	-0.4	15	19	2	-2.9	28	33	36

<u>10.0</u>	<u>8</u>	<u>9.8</u>	<u>10.2</u>	<u>9.1</u>	<u>5.8</u>	<u>5.0</u>	<u>5.5</u>	<u>80</u>	<u>8</u>	<u>8.5</u>	<u>80</u>
33	2	-5.4	17	17	12	-0.6	13	17	2	-2.9	33

<u>8.3</u>	<u>4</u>	<u>8.6</u>	<u>8.5</u>	<u>5.3</u>	<u>4.6</u>	<u>5.2</u>	<u>8.8</u>	<u>5</u>	<u>7.3</u>	<u>104</u>	<u>10.3</u>	<u>9.8</u>
33	2	-4.6	17	12	-0.4	12	78	2	-5.3	37	30	33

Sta.	T	H.I.	-	F/ev.	Gr. No.
		996.29			
+50				92.7	3.4
399				93.0	3.3
T.P.	5.35	999.25 <sup>✓</sup>	2.39	993.90 <sup>✓</sup>	
+50				93.4	5.9
400				93.7	5.6
+50				93.9	5.4
401				94.1	5.2
402				94.1	5.2
+30				94.0	5.1
403				93.8	5.5
+50				93.6	5.7
T.P.			5.11	993.44	

5-25-27

$\frac{5.0}{33}$	$\frac{4.9}{20}$	$\frac{4}{18} \frac{5.5}{-1.7}$	$\frac{6.1}{14}$	$\frac{6.1}{15}$	$\frac{4.4}{11}$	$\frac{5.7}{10.1}$	$\frac{4.2}{12}$	$\frac{6.2}{17}$	$\frac{2}{2} \frac{6.7}{-3.1}$	$\frac{6.4}{28}$	$\frac{5.4}{31}$	$\frac{5.3}{33}$
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$\frac{2.9}{33}$	$\frac{3}{2} \frac{3.1}{70.2}$	$\frac{3.2}{22}$	$\frac{6.0}{18}$	$\frac{4.0}{13}$	$\frac{3.1}{10.2}$	$\frac{3.7}{12}$	$\frac{5.9}{16}$	$\frac{4}{2} \frac{6.0}{-2.7}$	$\frac{5.8}{23}$	$\frac{2.8}{28}$	$\frac{2.7}{33}$
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$\frac{6.1}{33}$	$\frac{6}{2} \frac{5.4}{00}$	$\frac{6.2}{24}$	$\frac{6.2}{13}$	$\frac{5.5}{10.4}$	$\frac{6.2}{12}$	$\frac{8.1}{15}$	$\frac{8}{19} \frac{8.5}{-2.4}$	$\frac{8.3}{22}$	$\frac{5.3}{26}$	$\frac{5.5}{33}$
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$\frac{5.3}{33}$	$\frac{6}{2} \frac{5.3}{70.3}$	$\frac{5.2}{20}$	$\frac{4.7}{12}$	$\frac{4.8}{10.8}$	$\frac{4.9}{14}$	$\frac{5.4}{24}$	$\frac{3}{2} \frac{5.4}{10.2}$	$\frac{5.6}{33}$
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$\frac{6.8}{33}$	$\frac{5.8}{25}$	$\frac{6.7}{23}$	$\frac{6}{2} \frac{8.9}{-3.5}$	$\frac{9.3}{21}$	$\frac{7.6}{17}$	$\frac{5.1}{12}$	$\frac{4.7}{10.7}$	$\frac{5.3}{12}$	$\frac{6.5}{16}$	$\frac{6.4}{24}$	$\frac{5.8}{25}$	$\frac{5}{2} \frac{5.7}{-0.3}$	$\frac{6.1}{28}$	$\frac{5.0}{33}$
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$\frac{7.0}{30}$	$\frac{6.2}{24}$	$\frac{4}{2} \frac{8.4}{-3.2}$	$\frac{9.4}{21}$	$\frac{9.5}{18}$	$\frac{7.3}{17}$	$\frac{5.1}{13}$	$\frac{4.5}{10.7}$	$\frac{5.2}{13}$	$\frac{6.4}{16}$	$\frac{6.5}{20}$	$\frac{5.5}{22}$	$\frac{3}{2} \frac{5.0}{10.2}$	$\frac{4.6}{33}$
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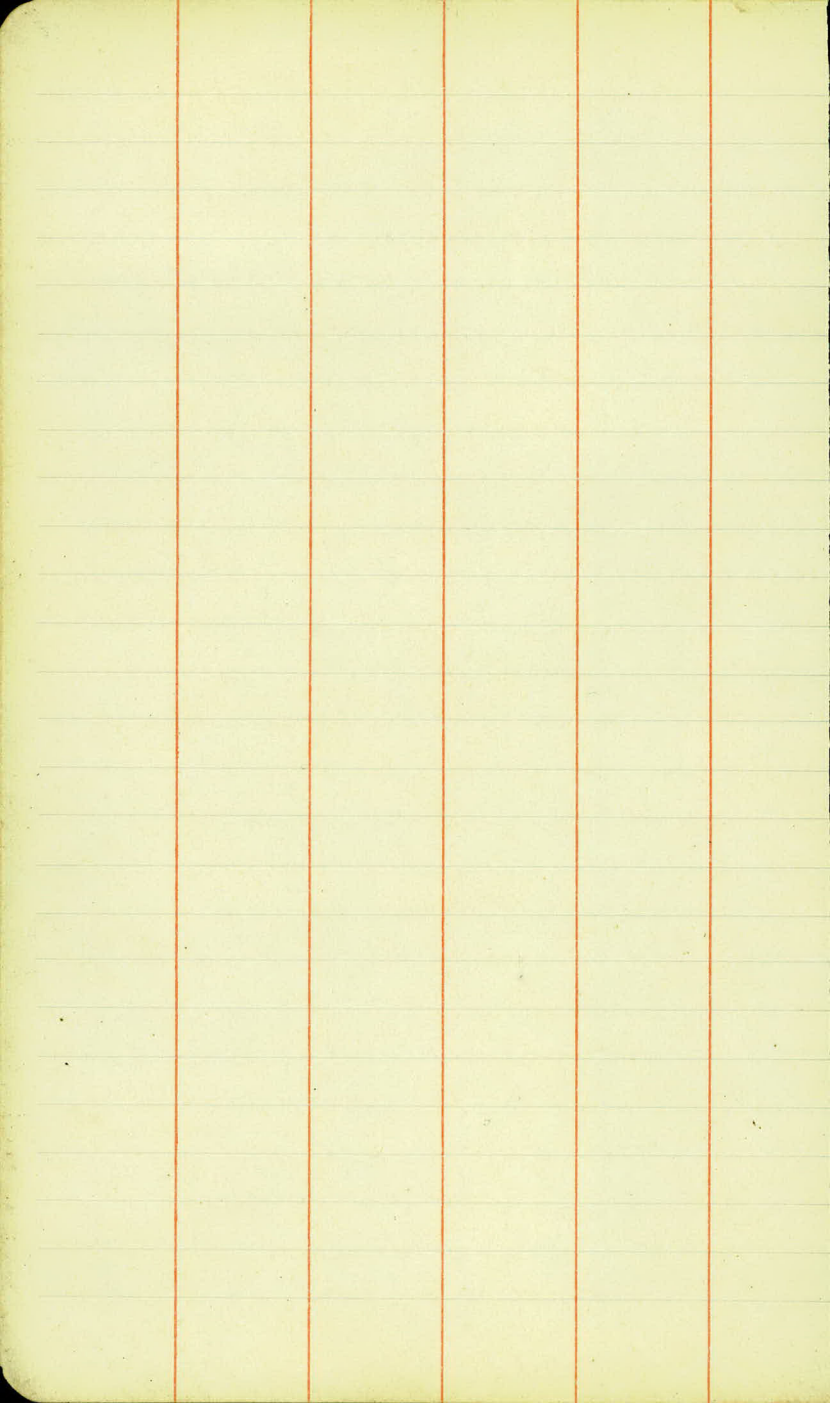
$\frac{7.2}{33}$	$\frac{7.1}{23}$	$\frac{8}{2} \frac{8.6}{-3.4}$	$\frac{8.8}{21}$	$\frac{9.0}{19}$	$\frac{7.8}{17}$	$\frac{5.4}{12}$	$\frac{7.9}{10.3}$	$\frac{5.3}{12}$	$\frac{6.4}{16}$	$\frac{6.4}{29}$	$\frac{5.3}{23}$	$\frac{6}{2} \frac{5.2}{00}$	$\frac{5.0}{33}$
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$\frac{7.5}{33}$	$\frac{7.3}{23}$	$\frac{9.2}{21}$	$\frac{9.2}{19}$	$\frac{8.1}{18}$	$\frac{5.5}{12}$	$\frac{5.0}{12}$	$\frac{5.2}{14}$	$\frac{5.5}{24}$	$\frac{5.5}{33}$
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$\frac{7.3}{33}$	$\frac{7.1}{23}$	$\frac{8}{2} \frac{8.9}{-3.4}$	$\frac{9.1}{21}$	$\frac{8.9}{19}$	$\frac{7.5}{18}$	$\frac{5.8}{13}$	$\frac{5.2}{10.3}$	$\frac{5.6}{13}$	$\frac{6.6}{15}$	$\frac{4}{2} \frac{6.7}{-1.2}$	$\frac{6.9}{33}$
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$\frac{7.1}{33}$	$\frac{7.0}{28}$	$\frac{4}{2} \frac{6.6}{-0.9}$	$\frac{6.2}{20}$	$\frac{5.6}{12}$	$\frac{5.4}{10.3}$	$\frac{6.0}{10}$	$\frac{6.5}{19}$	$\frac{3}{2} \frac{6.8}{-1.1}$	$\frac{6.5}{29}$	$\frac{6.7}{33}$
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Nail in P.P. Lt. Sta 404 + 20.





Sta.	T	H. I.	-	Elev.	Gr. No.
B.M.	10.23	1043.34		1033.11	
451				1035.1	8.2
+50				35.3	8.0
452				35.1	8.2
+50				34.8	8.5
T.P.	4.44	1039.53	8.25	1035.09	
453				34.5	5.0
+50				34.3	5.4
454				34.0	5.5
+50				33.7	5.8
455				33.4	6.1
+40				33.0	6.5
456				32.3	7.2
T.P.	2.77	1035.12	7.18	1032.95	
+50				31.5	3.6

5-24-27

PK in T.P. Lt. Sta. 450 +25  
 $\begin{array}{r} 8.4 \\ 33 \end{array} \begin{array}{r} 8.2 \\ 15 \end{array} \begin{array}{r} 8.0 \\ 10.2 \end{array} \begin{array}{r} 8.4 \\ 14 \end{array} \begin{array}{r} 8.6 \\ 23 \end{array} \begin{array}{r} 7.8 \\ 25 \end{array} \begin{array}{r} 7.0 \\ 3 \end{array} \begin{array}{r} +1.2 \\ 1.2 \end{array}$

$\begin{array}{r} 2.5 \\ 33 \end{array} \begin{array}{r} 2 \\ 2 \end{array} \begin{array}{r} 8.8 \\ -2.8 \end{array} \begin{array}{r} 8.4 \\ 26 \end{array} \begin{array}{r} 8.5 \\ 21 \end{array} \begin{array}{r} 8.3 \\ 15 \end{array} \begin{array}{r} 8.1 \\ -0.1 \end{array} \begin{array}{r} 18.4 \\ 13 \end{array} \begin{array}{r} 8.1 \\ 22 \end{array} \begin{array}{r} 4.0 \\ 28 \end{array} \begin{array}{r} 4.1 \\ 1.59 \end{array}$

$\begin{array}{r} 3.2 \\ 33 \end{array} \begin{array}{r} 0 \\ 2 \end{array} \begin{array}{r} 5.8 \\ 12.4 \end{array} \begin{array}{r} 9.4 \\ 27 \end{array} \begin{array}{r} 7.5 \\ 18 \end{array} \begin{array}{r} 8.8 \\ 15 \end{array} \begin{array}{r} 8.3 \\ -0.1 \end{array} \begin{array}{r} 19.7 \\ 11 \end{array} \begin{array}{r} 8.5 \\ 19 \end{array} \begin{array}{r} 8.8 \\ 20 \end{array} \begin{array}{r} 8.1 \\ 28 \end{array} \begin{array}{r} 5.4 \\ 1.28 \end{array}$

$\begin{array}{r} 10.1 \\ 33 \end{array} \begin{array}{r} 10.1 \\ 27 \end{array} \begin{array}{r} 11.2 \\ 23 \end{array} \begin{array}{r} 10.6 \\ 18 \end{array} \begin{array}{r} 8.9 \\ 14 \end{array} \begin{array}{r} 8.6 \\ -0.1 \end{array} \begin{array}{r} 19.1 \\ 15 \end{array} \begin{array}{r} 6 \\ -2.8 \end{array} \begin{array}{r} 12.2 \\ 27 \end{array} \begin{array}{r} 12.4 \\ 33 \end{array}$

$\begin{array}{r} 8.6 \\ 33 \end{array} \begin{array}{r} 8.5 \\ 26 \end{array} \begin{array}{r} 8.9 \\ -3.9 \end{array} \begin{array}{r} 8.4 \\ 19 \end{array} \begin{array}{r} 5.0 \\ 13 \end{array} \begin{array}{r} 5.1 \\ -0.1 \end{array} \begin{array}{r} 5.4 \\ 14 \end{array} \begin{array}{r} 7.8 \\ 19 \end{array} \begin{array}{r} 4 \\ -2.7 \end{array} \begin{array}{r} 7.7 \\ 25 \end{array} \begin{array}{r} 8.2 \\ 33 \end{array}$

$\begin{array}{r} 4.3 \\ 33 \end{array} \begin{array}{r} 4.4 \\ 27 \end{array} \begin{array}{r} 6 \\ 2 \end{array} \begin{array}{r} 5.2 \\ 00 \end{array} \begin{array}{r} 5.9 \\ 24 \end{array} \begin{array}{r} 6.2 \\ 18 \end{array} \begin{array}{r} 5.4 \\ 15 \end{array} \begin{array}{r} 5.1 \\ 10.1 \end{array} \begin{array}{r} 5.4 \\ 14 \end{array} \begin{array}{r} 8.1 \\ 19 \end{array} \begin{array}{r} 4 \\ -4.2 \end{array} \begin{array}{r} 7.4 \\ 28 \end{array} \begin{array}{r} 10.2 \\ 33 \end{array}$

$\begin{array}{r} 7 \\ 33 \end{array} \begin{array}{r} 6.5 \\ 2 \end{array} \begin{array}{r} 3.7 \\ 27 \end{array} \begin{array}{r} 5.8 \\ 23 \end{array} \begin{array}{r} 6.0 \\ 18 \end{array} \begin{array}{r} 5.2 \\ 15 \end{array} \begin{array}{r} 5.5 \\ 10 \end{array} \begin{array}{r} 5.4 \\ 10.5 \end{array} \begin{array}{r} 5.5 \\ 14 \end{array} \begin{array}{r} 8.0 \\ 20 \end{array} \begin{array}{r} 8.1 \\ 24 \end{array} \begin{array}{r} 7.4 \\ 28 \end{array} \begin{array}{r} 7.5 \\ 33 \end{array}$

$\begin{array}{r} 5.9 \\ 33 \end{array} \begin{array}{r} 6 \\ 2 \end{array} \begin{array}{r} 5.8 \\ 24 \end{array} \begin{array}{r} 6.7 \\ 18 \end{array} \begin{array}{r} 5.6 \\ 15 \end{array} \begin{array}{r} 5.5 \\ 11 \end{array} \begin{array}{r} 5.8 \\ 9 \end{array} \begin{array}{r} 5.5 \\ 10.3 \end{array} \begin{array}{r} 5.7 \\ 15 \end{array} \begin{array}{r} 7.5 \\ 19 \end{array} \begin{array}{r} 7.7 \\ 25 \end{array} \begin{array}{r} 6.3 \\ 29 \end{array} \begin{array}{r} 6.7 \\ 33 \end{array}$

$\begin{array}{r} 6.7 \\ 33 \end{array} \begin{array}{r} 6.2 \\ 27 \end{array} \begin{array}{r} 4 \\ 2 \end{array} \begin{array}{r} 2.3 \\ -1.2 \end{array} \begin{array}{r} 7.0 \\ 19 \end{array} \begin{array}{r} 6.1 \\ 14 \end{array} \begin{array}{r} 6.1 \\ 10 \end{array} \begin{array}{r} 5.8 \\ 10.3 \end{array} \begin{array}{r} 6 \\ 12 \end{array} \begin{array}{r} 5.6 \\ 15 \end{array} \begin{array}{r} 5.9 \\ 14 \end{array} \begin{array}{r} 7.2 \\ 20 \end{array} \begin{array}{r} 7.2 \\ 23 \end{array} \begin{array}{r} 6.7 \\ -0.9 \end{array} \begin{array}{r} 7.0 \\ 28 \end{array} \begin{array}{r} 6.4 \\ 33 \end{array}$

$\begin{array}{r} 6.3 \\ 33 \end{array} \begin{array}{r} 6.5 \\ 27 \end{array} \begin{array}{r} 7.6 \\ 24 \end{array} \begin{array}{r} 4 \\ 2 \end{array} \begin{array}{r} 0.7 \\ -7.3 \end{array} \begin{array}{r} 7.7 \\ 19 \end{array} \begin{array}{r} 6.4 \\ 15 \end{array} \begin{array}{r} 6.4 \\ 10 \end{array} \begin{array}{r} 6.0 \\ 10.5 \end{array} \begin{array}{r} 6.5 \\ 12 \end{array} \begin{array}{r} 6.3 \\ 18 \end{array} \begin{array}{r} 6.9 \\ 21 \end{array} \begin{array}{r} 6.4 \\ 10.1 \end{array} \begin{array}{r} 5.9 \\ 28 \end{array} \begin{array}{r} 0.4 \\ 33 \end{array}$

$\begin{array}{r} 4.4 \\ 33 \end{array} \begin{array}{r} 4.3 \\ 27 \end{array} \begin{array}{r} 1 \\ 2 \end{array} \begin{array}{r} 7.8 \\ -0.6 \end{array} \begin{array}{r} 8.0 \\ 24 \end{array} \begin{array}{r} 8.2 \\ 19 \end{array} \begin{array}{r} 7.1 \\ 14 \end{array} \begin{array}{r} 7.0 \\ 10 \end{array} \begin{array}{r} 6.9 \\ 10.3 \end{array} \begin{array}{r} 7.3 \\ 12 \end{array} \begin{array}{r} 7.1 \\ 16 \end{array} \begin{array}{r} 8.7 \\ 21 \end{array} \begin{array}{r} 8.7 \\ -7.5 \end{array} \begin{array}{r} 8.5 \\ 27 \end{array} \begin{array}{r} 5.9 \\ 33 \end{array}$

$\begin{array}{r} 5.6 \\ 33 \end{array} \begin{array}{r} 5.1 \\ 28 \end{array} \begin{array}{r} 5.8 \\ 24 \end{array} \begin{array}{r} 5.8 \\ 23 \end{array} \begin{array}{r} 3.4 \\ 17 \end{array} \begin{array}{r} 3.7 \\ 11 \end{array} \begin{array}{r} 3.4 \\ -0.2 \end{array} \begin{array}{r} 3.7 \\ 11 \end{array} \begin{array}{r} 3.3 \\ 13 \end{array} \begin{array}{r} 3.6 \\ 10 \end{array} \begin{array}{r} 3.7 \\ 16 \end{array} \begin{array}{r} 7.1 \\ 24 \end{array} \begin{array}{r} 7.4 \\ 33 \end{array}$

Sta	T	H.I.	-	Elev.	Gr. R.
		1035.12.			
457				30.7	4.4.
+50				30.0	5.1.
T.P.	5.26	1035.05.	5.33	1029.99.	
458				29.6	5.5.
+50				29.3	5.8.
459				29.1	6.0.
+50				29.2	5.9.
460				29.4	5.7.
+50				29.7	5.4.
461				30.1	5.0.
+50				30.2	4.9.
462				30.2	4.9.
B.M.	3.65	1034.20.	4.50	1030.55.	
+30				30.1	4.1.

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9.6	<sup>0</sup> / <sub>5</sub> 9.4	9.3	4.8	4.6	4.4	4.5	4.0	4.4	8.0	7.3	7.5
33	24	24	15	11	0	11	12	17	25	28	33

12.2	11.0	6.0	<sup>8</sup> / <sub>5</sub> 5.5	5.0	<sup>5.1</sup> / <sub>5</sub> 5.2	5.0	9.8	9.5
33	24	17	15	10	10	17	27	33

12.4	11.5	2.6	5.3	5.5	5.4	10.0	10.2
33	24	16	10	7	19	25	33

6.8	6.8	7.7	7.4	<sup>2</sup> / <sub>5</sub> 5.9	5.5	<sup>5.1</sup> / <sub>5</sub> 5.7	<sup>0</sup> / <sub>5</sub> 5.1	5.4	7.4	7.7	6.8	7.5
33	28	25	19	11	10	10	17	17	22	25	28	33

4.9	4.9	7.1	<sup>6</sup> / <sub>5</sub> 7.4	7.2	5.8	<sup>6.0</sup> / <sub>5</sub> 6.9	5.5	7.4	7.4	<sup>0</sup> / <sub>5</sub> 7.3	6.6	5.0
33	31	24	24	19	15	10	14	21	23	24	27	33

5.6	<sup>5</sup> / <sub>4</sub> 6.9	6.8	6.0	<sup>5.9</sup> / <sub>5</sub> 6.0	6.1	7.1	7.3	<sup>9</sup> / <sub>4</sub> 7.2	6.8	5.7
33	24	17	15	10	14	20	23	27	27	33

4.5	4.0	<sup>9</sup> / <sub>4</sub> 6.4	6.5	5.8	5.4	5.6	5.6	7.2	<sup>9</sup> / <sub>4</sub> 7.1	6.7	5.7
33	29	24	18	16	10	15	15	19	24	27	33

2.1	1.9	<sup>1</sup> / <sub>5</sub> 5.8	6.1	6.4	<sup>0</sup> / <sub>5</sub> 5.4	5.0	5.2	6.0	5.9	<sup>0</sup> / <sub>5</sub> 5.4	0.0
33	31	24	24	18	10	10	15	17	24	24	33

2.0	6.2	<sup>3</sup> / <sub>5</sub> 6.8	6.6	5.2	4.9	5.0	6.1	<sup>9</sup> / <sub>5</sub> 7	0.2	10.5
33	24	24	19	15	10	15	20	24	33	34

WAVE H.S.

7.4	6.0	7.0	<sup>9</sup> / <sub>5</sub> 6.9	6.8	6.0	5.1	<sup>5.0</sup> / <sub>5</sub> 5.2	5.1	6.4	<sup>4</sup> / <sub>5</sub> 6.6	6.3	5.0	4.9
33	30	28	24	19	16	13	12	17	22	24	26	28	33

7.3	7.5	<sup>4</sup> / <sub>5</sub> 7.6	7.6	7.0	5.7	5.1	5.4	5.4	7.9	7.4
33	29	24	19	17	15	11	17	22	22	33

Sp N. in 18" Ogr. 40' Lt. 579. 462 + 80.

5.7	5.7	6.7	<sup>2</sup> / <sub>5</sub> 6.7	4.8	4.4	4.6	4.5	5.5	5.6	4.7	5.6
33	29	25	24	13	11	11	14	19	21	24	33

Sta.	T	H. I.	-	Elev.	Gr. R.
		1034.20			
463				29.7	4.5
	+50			29.4	4.8
464				29.2	5.0
	+27			29.1	5.1
	+70			29.0	5.2
465				28.9	5.3
T.B.M.			4.95	1029.25	
T.P.	11.69	1045.43	0.46	1033.74	
464				29.2	10.2
	+27			29.1	16.3
	+70			29.0	16.4
T.P.	1.09	1034.41	12.11	1033.32	
T.P.	1.34	1030.59	5.14	1029.25	
446				28.9	1.7
467				29.0	1.4
T.P.	5.45	1034.70	1.34	1029.25	

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$\begin{array}{r} 4.1 \\ 33 \end{array}$ 
 $\begin{array}{r} 4.1 \\ 32 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 27 \end{array}$ 
 $\begin{array}{r} 6.6 \\ 21 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 16 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 13 \end{array}$ 
 $\begin{array}{r} 4.6 \\ -0.1 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 10 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 16 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 2 \end{array}$ 
 $\begin{array}{r} 2.86 \\ -4.1 \end{array}$ 
 $\begin{array}{r} 9.2 \\ 33 \end{array}$

$\begin{array}{r} 3.6 \\ 33 \end{array}$ 
 $\begin{array}{r} 3.6 \\ 32 \end{array}$ 
 $\begin{array}{r} 6.1 \\ 24 \end{array}$ 
 $\begin{array}{r} 6.5 \\ 21 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 4.9 \\ -0.1 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 10.1 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 14 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 18 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 1 \end{array}$ 
 $\begin{array}{r} 4.6.9 \\ -2.1 \end{array}$ 
 $\begin{array}{r} 6.6 \\ 24 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 29 \end{array}$ 
 $\begin{array}{r} 5.8 \\ 33 \end{array}$

$\begin{array}{r} 4.7 \\ 24 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 18 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 15 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 12 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 10.2 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 11 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 15 \end{array}$ 
 $\begin{array}{r} 6.0 \\ 19 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 21 \end{array}$ 
 $\begin{array}{r} 1.2 \\ 32 \end{array}$ 
 $\begin{array}{r} 1.2 \\ 33 \end{array}$

$\begin{array}{r} 4.4 \\ 25 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 19 \end{array}$ 
 $\begin{array}{r} 4.9 \\ 15 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 12 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 10.1 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 11 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 15 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 16 \end{array}$ 
 $\begin{array}{r} 6.4 \\ 19 \end{array}$ 
 $\begin{array}{r} 7.66 \\ -1.5 \end{array}$ 
 $\begin{array}{r} 6.4 \\ 27 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 33 \end{array}$

$\begin{array}{r} 2.7 \\ 33 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 26 \end{array}$ 
 $\begin{array}{r} 7.3 \\ 21 \end{array}$ 
 $\begin{array}{r} 5.7 \\ 14 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 12 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 10.1 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 10 \end{array}$ 
 $\begin{array}{r} 5.7 \\ -0.5 \end{array}$ 
 $\begin{array}{r} 7.0 \\ 24 \end{array}$ 
 $\begin{array}{r} 8.8 \\ 33 \end{array}$

$\begin{array}{r} 7.1 \\ 46 \end{array}$ 
 $\begin{array}{r} 7.9 \\ 34 \end{array}$ 
 $\begin{array}{r} 8.6 \\ 24 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 17 \end{array}$ 
 $\begin{array}{r} 5.2 \\ 10.1 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 14 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 12 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 10.2 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 10 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 12 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 17 \end{array}$ 
 $\begin{array}{r} 9.5 \\ 26 \end{array}$ 
 $\begin{array}{r} 10.4 \\ 33 \end{array}$

$\begin{array}{r} 7.2 \\ 49.5 \end{array}$ 
 $\begin{array}{r} 9.5.6 \\ 4 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 37 \end{array}$

$\begin{array}{r} 9.1.7 \\ 4 \end{array}$ 
 $\begin{array}{r} 1.6 \\ 38 \end{array}$

$\begin{array}{r} 10.7 \\ 49.5 \end{array}$ 
 $\begin{array}{r} 12.2 \\ 40 \end{array}$

$\begin{array}{r} 14.3 \\ 49.5 \end{array}$ 
 $\begin{array}{r} 3.6 \\ -1.9 \end{array}$ 
 $\begin{array}{r} 13.4 \\ 37 \end{array}$ 
 $\begin{array}{r} 9.1 \\ 28 \end{array}$ 
 $\begin{array}{r} 2.7 \\ 16 \end{array}$ 
 $\begin{array}{r} 2.0 \\ -0.3 \end{array}$ 
 $\begin{array}{r} 2.3 \\ 10 \end{array}$ 
 $\begin{array}{r} 2.7 \\ 16 \end{array}$ 
 $\begin{array}{r} 6.2 \\ 22 \end{array}$ 
 $\begin{array}{r} 11.0 \\ -9.3 \end{array}$

$\begin{array}{r} 12.6 \\ 49.5 \end{array}$ 
 $\begin{array}{r} 11.4 \\ 33 \end{array}$ 
 $\begin{array}{r} 3.5 \\ 20 \end{array}$ 
 $\begin{array}{r} 4.2.4 \\ 4 \end{array}$ 
 $\begin{array}{r} 2.4 \\ 15 \end{array}$ 
 $\begin{array}{r} 1.7 \\ -0.1 \end{array}$ 
 $\begin{array}{r} 2.0 \\ 11 \end{array}$ 
 $\begin{array}{r} 1.6 \\ 12 \end{array}$ 
 $\begin{array}{r} 4.2.3 \\ 4 \end{array}$ 
 $\begin{array}{r} 7.9 \\ 27 \end{array}$ 
 $\begin{array}{r} 9.2 \\ 33 \end{array}$

Sta.	T	H. I.	-	Elev.	Gr. Ref.
		1034.70.			
	+45			29.2	5.5.
468				29.4	5.3.
	+33			29.8	4.9.
469				30.0	4.7.
469 +50				30.3	4.4.
T.P.	9.40	1042.28.	1.82	1032.88.	
468				29.4	12.9
468 +33				29.8	12.5
T.P.	3.83	1036.71.	7.40	1032.88.	
470				30.7	6.0.
	+50			31.0	5.7.
471				31.2	5.5.
	+40			31.2	5.5.
472				31.4	5.3.

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5	7.6	7.6	8.2	7.9	6.0	4/6.7	5.4	5.7	5.4	4/5.7	9.0	8.5	9.2
5	40	30	27	22	18	15	10.1	11	12	15	24	28	33

Above H.L.

4.3	5.5	5.0	4.9	5.3	5.1	5.5	6.6	6.0	6.5	10.2
24	17	14	10.4	11	12	15	18	25	20	33

(4.9)

3.9	5.1	4.8	4.7	5.0	4.9	5.4	4.6
23	17	15	10.2	9	10	16	23

(4.7)

8.8	8.1	7.0	6.6	4.7	4.9	4.5	4.7	4.2	5.0	4.8	3.3	2.1	1.5
49.5	40	31	21	15	12	10.2	8	11	15	18	22	12.6	33

(4.4)

4.7	4.5	5.6	5.9	4.9	4.5	4.4	4.6	4.3	4.7	4.3	4.5	5.6	4.5	4.4	4.0
46	2	12	20	17	15	13	12	10.1	10	10	13	15	2	1.9	30

5.1	4.1	3.8
49.5	3	34

3.9	2.2	1.3	1.3	1.7
49.5	4	35	37	40

6	4.8	4.7	7.0	7.1	6.5	6.3	6.0	6.3	6.6	7.4	6.7	7.5
5	4	11.2	27	22	18	17	12	00	11	14	16	2

5.2	6.4	5.8	5.6	5.7	5.8	6.4	6.2	5.0	7.1	5.4
24	17	14	10.1	11	15	17	21	24	2	33

5.1	6.1	5.6	5.3	5.3	3.4	5.0
22	17	15	10.2	14	2	33

5.2	6.1	5.3	5.3	5.2	5.5	6.1	5.8
23	18	15	11	10.3	1	18	24

5.1	5.7	5.3	5.0	5.3	5.0	5.6	4.2	3.5
21	17	15	10.3	11	14	17	25	26

Sta.	+	H. I.	-	Elev.	Gr. Pt.
		1036.71.			
	+24			31.4	5.3
	+63			31.4	5.3
	473			31.4	5.3
	474			31.9	4.8
	+50			32.5	4.2
	T.R.M.		3.49	1033.22	
	T.P.	11.60	1047.69	0.62	1036.09
	470+50			31.0	16.7
	471			31.2	16.5
	471+40			31.2	16.5
	472			31.4	16.3
	472+24			31.4	16.3
	T.P.	4.61	1040.44	11.86	1035.73
	T.P.	7.22	1040.44	7.22	1033.22
	B.M.	4.84	1040.44	4.84	1035.58
					1035.60
					1035.6

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$\frac{78}{93}$	$\frac{90}{27}$	$\frac{5 \times 63}{2 \times 70}$	$\frac{56}{22}$	$\frac{64}{19}$	$\frac{62}{17}$	$\frac{48}{13}$	$\frac{49}{104}$	$\frac{52}{16}$	$\frac{61}{18}$	$\frac{60}{20}$	$\frac{54}{22}$	$\frac{08}{27}$
-----------------	-----------------	-----------------------------------	-----------------	-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{123}{33}$	$\frac{116}{29}$	$\frac{50}{14}$	$\frac{49}{14}$	$\frac{52}{11}$	$\frac{49}{104}$	$\frac{52}{12}$	$\frac{52}{14}$	$\frac{74}{21}$	$\frac{70}{30}$	$\frac{52}{33}$
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$\frac{141}{39}$	$\frac{137}{30}$	$\frac{60}{17}$	$\frac{4 \times 56}{3 \times 05}$	$\frac{50}{103}$	$\frac{52}{121}$	$\frac{52}{00}$	$\frac{53}{23}$	$\frac{83}{28}$	$\frac{81}{31}$	$\frac{78}{31}$	$\frac{61}{33}$
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$\frac{124}{39}$	$\frac{119}{28}$	$\frac{59}{18}$	$\frac{03 \times 9}{1 \times 05}$	$\frac{52}{15}$	$\frac{48}{00}$	$\frac{48}{11}$	$\frac{50}{1 \times 04}$	$\frac{8 \times 2}{22}$	$\frac{87}{27}$	$\frac{87}{27}$	$\frac{77}{33}$
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$\frac{55}{33}$	$\frac{55}{31}$	$\frac{67}{27}$	$\frac{65}{22}$	$\frac{48}{18}$	$\frac{9 \times 44}{5 \times 00}$	$\frac{45}{11}$	$\frac{45}{01}$	$\frac{45}{11}$	$\frac{43}{12}$	$\frac{6 \times 46}{1 \times 04}$	$\frac{68}{21}$	$\frac{74}{26}$	$\frac{68}{27}$	$\frac{82}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------------------------	-----------------	-----------------	-----------------	-----------------	-----------------------------------	-----------------	-----------------	-----------------	-----------------

$\frac{97}{495}$	$\frac{97}{45}$	$\frac{8 \times 108}{5 \times 159}$	$\frac{115}{30}$	$\frac{167}{167}$
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$\frac{64}{495}$	$\frac{7 \times 80}{5 \times 185}$	$\frac{94}{30}$	$\frac{165}{165}$
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$\frac{54}{495}$	$\frac{4 \times 69}{40 \times 196}$	$\frac{86}{32}$	$\frac{165}{3 \times 153}$	$\frac{105}{34}$
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$\frac{126}{495}$	$\frac{105}{43}$	$\frac{9 \times 90}{5 \times 173}$	$\frac{62}{31}$	$\frac{163}{163}$	$\frac{89}{30}$	$\frac{0 \times 8}{3 \times 195}$	$\frac{40}{35}$	$\frac{41}{40}$
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$\frac{163}{163}$	$\frac{0 \times 79}{3 \times 184}$	$\frac{19}{38}$	$\frac{21}{43}$
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Spk. in 12" Oak 40 Lt. Stg. 476 to 5.

Sta.	T	H. I.	-	Elev.	Gr. Rd.
		1040.46.			
475				33.3	7.2
+50				34.3	6.2
474				35.3	5.2
+50				36.3	4.2
+80				36.9	3.6
477				37.3	3.2
T.P.	9.93	1048.96.	1.43	1039.03.	
+50				38.3	10.7
478				39.3	9.7
+60				40.5	8.5
T.P.	6.02	1042.88.	6.10	1042.84.	
479				41.3	7.6
+40				42.1	6.8
480				43.5	5.4

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1.4	$\frac{2}{3} \frac{77}{25}$	$\frac{82}{22}$	$\frac{80}{19}$	$\frac{72}{17}$	$\frac{71}{13}$	$\frac{75}{11}$	$\frac{7.2}{0.0}$	$\frac{9.4}{11.9}$	$\frac{9.5}{-0.3}$	9.9	$\frac{10.1}{27}$	$\frac{71}{28}$	$\frac{97}{33}$
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18	$\frac{2.2}{32}$	$\frac{7.3}{24}$	$\frac{2}{4} \frac{74}{72}$	$\frac{78}{21}$	$\frac{6.5}{17}$	$\frac{66}{12}$	$\frac{6.2}{0.0}$	$\frac{6.6}{11}$	$\frac{6.1}{12.1}$	$\frac{0}{8} \frac{6.2}{0.0}$	$\frac{6.6}{14}$	$\frac{9.2}{22}$	$\frac{9.4}{23}$	$\frac{96}{24}$	$\frac{75}{33}$
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6.0	$\frac{6.0}{32}$	$\frac{9.0}{27}$	$\frac{2}{2} \frac{8.7}{-3.5}$	$\frac{5.7}{15}$	$\frac{5.8}{12}$	$\frac{5.5}{0.3}$	$\frac{5.3}{12}$	$\frac{5.8}{12}$	$\frac{5.5}{12}$	$\frac{9}{11} \frac{5.6}{-0.9}$	$\frac{6.5}{18}$	$\frac{11.0}{24}$	$\frac{12.1}{33}$
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11.2	$\frac{11.1}{30}$	$\frac{10.4}{27}$	$\frac{2}{1} \frac{4.8}{-0.6}$	$\frac{4.8}{12}$	$\frac{4.5}{-0.3}$	$\frac{4.8}{11}$	$\frac{4.9}{16}$	$\frac{6.4}{19}$	$\frac{8.0}{22}$	$\frac{10.2}{25}$	$\frac{0}{8} \frac{10.7}{-6.5}$	$\frac{11.1}{27}$	$\frac{11.2}{33}$
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78	$\frac{71}{33}$	$\frac{41}{21}$	$\frac{3.9}{15}$	$\frac{4.2}{13}$	$\frac{3.7}{12}$	$\frac{3.6}{12}$	$\frac{3.8}{12}$	$\frac{4.1}{18}$	$\frac{5.7}{23}$	$\frac{6.0}{25}$	$\frac{5.0}{27}$	$\frac{5.0}{33}$
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4.9	$\frac{4.3}{33}$	$\frac{5.3}{26}$	$\frac{5.5}{20}$	$\frac{3.6}{14}$	$\frac{3.7}{11}$	$\frac{3.2}{0.0}$	$\frac{3.6}{12}$	$\frac{3.5}{14}$	$\frac{4.5}{19}$	$\frac{4}{2} \frac{4.5}{-1.5}$	$\frac{4.0}{27}$	$\frac{0.9}{33}$
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5.2	$\frac{11.3}{33}$	$\frac{11.7}{25.1}$	$\frac{10.6}{19}$	$\frac{10.8}{15}$	$\frac{10.5}{12}$	$\frac{10.9}{10.2}$	$\frac{10.4}{12}$	$\frac{11.0}{13}$	$\frac{10.2}{18}$	$\frac{0}{3} \frac{10.7}{-7.8}$	$\frac{11.2}{23}$	$\frac{11.2}{33}$
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3.8	$\frac{0}{3} \frac{4.3}{75.4}$	$\frac{7.5}{24}$	$\frac{10.5}{17}$	$\frac{9.5}{16}$	$\frac{9.3}{13}$	$\frac{9.7}{12}$	$\frac{7.3}{10.4}$	$\frac{9.4}{12}$	$\frac{9.9}{17}$	$\frac{9.0}{24}$	$\frac{0}{5} \frac{1.9}{-7.8}$	$\frac{1.4}{34}$
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7.9	$\frac{8.4}{33}$	$\frac{9}{2} \frac{9.9}{-1.4}$	$\frac{9.8}{18}$	$\frac{8.5}{15}$	$\frac{8.1}{10.4}$	$\frac{8.4}{11}$	$\frac{8.0}{14}$	$\frac{9.4}{18}$	$\frac{9.6}{21}$	$\frac{8.5}{24}$	$\frac{0}{3} \frac{3.4}{-2.1}$	$\frac{3.5}{36}$
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15.1	$\frac{7.9}{33}$	$\frac{2}{1} \frac{7.7}{-7.1}$	$\frac{7.6}{12}$	$\frac{7.1}{10.5}$	$\frac{7.2}{13}$	$\frac{7.4}{17}$	$\frac{8.2}{22}$	$\frac{8.5}{22}$	$\frac{4}{2} \frac{8.5}{-0.9}$	$\frac{8.4}{28}$	$\frac{7.6}{30}$	$\frac{7.8}{33}$
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20.0	$\frac{3}{4} \frac{18.9}{-12.1}$	$\frac{6.9}{14}$	$\frac{6.5}{10.3}$	$\frac{6.6}{10}$	$\frac{6.8}{16}$	$\frac{12.0}{24}$	$\frac{12.4}{33}$
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21.0	$\frac{20.8}{46}$	$\frac{0}{3} \frac{16.1}{-10.7}$	$\frac{6.2}{16}$	$\frac{5.7}{12}$	$\frac{5.4}{0.0}$	$\frac{5.5}{10}$	$\frac{5.2}{12}$	$\frac{4}{4} \frac{5.4}{-0.2}$	$\frac{10.0}{25}$	$\frac{10.1}{33}$
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Sta.	T	H. I.	-	Elev.	C. r. M.
		1048.88			
+50				44.7	4.2
T.P.	10.14	1056.56	2.46	1046.42	
481				46.1	10.5
+50				47.5	9.1
482				49.0	7.4
+50				50.7	6.9
483				52.3	4.3
+50				54.1	2.5
T.P.	10.50	1066.17	1.89	1055.67	
484				55.6	10.4
+50				56.7	9.5
485				57.4	8.8
+50				57.7	8.5
486				57.5	8.1

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15.3 135 49 4 44 42 46 41 44 40 41 55 4 59 52 34 29  
 40 32 17 1 02 13 12 10.1 10 11 14 18 2 -17 26 29 33

13.1 11.3 12.4 12.2 10.4 10.2 10.6 10.1 10.3 9.8 10.2 11.5 6 10.8 5.8 40  
 33 24 22 19 16 13 13 10.4 10 11 15 19 2 -03 30 33

11.9 9 10.9 10.2 9 9.1 8.5 8.6 8.2 9.2 8.6 9 3.2  
 33 2 16 19 1 00 10.4 10 14 18 26 3 15.9

11.3 10.1 7.6 7.4 7.9 7.2 7.5 7 6.3 5.7  
 33 23 18 13 12 10.4 12 2 +13 39

11.7 11.5 6.3 6.3 5.9 6.2 5.5  
 33 24 14 11 11 33

9.0 8.3 4.4 4.5 4.7 4.1 4.7 4.5 5 4.6 4.8  
 33 25 17 15 11 10.4 12 13 2 -03 31.5

1.7 3 3.6 4.0 0 2.5 2.3 2.6 2.1 2.7 2.2 7 2.7 2.4  
 33 2 -1.1 20 1 00 14 11 10.4 13 14 2 -02 32

1.0 3.6 3.6 10.4 11.1 10.3 10.5 10.0 10.3 7 9.6 8.3  
 10 3 7.0 33 24 17 10 12 10.4 15 2 11.0 32

3.3 2 2.6 3.4 9.2 9.6 8.7 8.5 9.5 4 7.9 6.5  
 40 5 16.9 34 24 17 13 11.2 14 2 11.6 32.4

3.7 3.1 3 8.4 9.0 7.7 8.0 7.6 7.5 0 6.1 5.1  
 40 04 2 10.2 21 14 12 11.2 15 5 12.7 32

6.4 5.7 8.8 4 9.2 9.1 7.9 7.9 7.7 7.9 5 5.5 4.4  
 40 53 37 2 -0.7 17 13 13 -0.8 16 8 13.0 32.5

8.2 10.6 10.5 9.0 8.7 8.7 8.5 8.5 2 7.2 6.1  
 33 27 19 15 20 1 8.7 23 2 7.5 32

Sta.	+	H. I.	-	Elev.	Gr. Rod
		1066.17.			
	+50			56.9	9.3
487				56.1	10.1
T.P.	3.73	1059.83.	10.07	1056.10.	
	+50			55.3	4.5
488				54.5	5.3
	+50			53.6	6.7
489				52.5	7.3
	+53 <sup>2</sup>			51.1	8.7
490				49.6	10.2
T.P.	6.17	1057.36.	8.64	1051.19.	
	+50			47.7	9.7
491				45.9	11.5
B.M.	3.93	1049.72.	11.57	1045.79.	
	+60			43.3	6.4
492				41.3	7.4

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86	85	11.1	10.9	9.6	9.4	9.6	0/9.3	8.2
33	52	26	22	14	70.1	15	2/00	32

9.3

28	10.5	7/10.6	11.4	10.5	10.4	10.5	10.4	8/9.9	9.6
33	29	2/-7.5	19	16	12	10.2	15	2/10.2	31

10.1

1.3	5.5	9/5.4	5.8	4.8	4.9	4.8	5.2	2/5.1	6.3	6.7	6.4
33	26	2/-1.4	18	15	11	0.9	12	1/-0.6	21	27	32

4.5

0	1.7	5.4	4/6.5	6.5	5.5	5.6	5.5	8/5.7	6.3	11.6	12.3
5	33	28	1/-7.2	19	16	11	00	1/0.4	19	27	33

5.3

2.8	6.7	4/7.4	7.3	5.9	6.1	6.0	6.4	4/6.4	11.9	12.3
33	28	2/-7.2	19	15	11	10.2	12	1/-0.2	26	33

1.2

4.3	6.9	5/7.6	7.7	7.1	6.8	6.8	7.2	4/7.2	8.2
33	28	2/-0.3	17	14	14	10.5	15	2/-0.9	33

7.3

1.3	7/1.2	1.2	8.9	9.6	8.4	8.4	7/7.9	10.4	4/10.4	8.3
40	3/7.5	34	24	18	15	10.3	14	17	2/-1.7	33

8.7

1.2	8/2.0	20	10.3	11.2	9.6	9.9	9.9	10.5	11.6	9/11.6	11.2	9.6	7.9
49.5	8/7.8	32	23	17	14	13	10.3	14	17	2/-1.4	24	29	33

10.0

0	5/2.0	12	9.1	9.4	8.9	8.8	7.5	9.2	9.6	10.7	5/10.7	9.6	10.0
5	3/7.7	34	23	17	15	12	10	10.5	14	16	2/-7.0	29	33

9.7

1.3	8/1.9	1.5	10.8	11.6	11.2	11.3	11.5	11.5	11.7	12.5	12.7	8/12.3	12.1
33	4/7.4	33	23	20	14	12	10.3	13	14	22	2/-0.1	33	

11.5

SPK in 8" OAK 33' Lt. 5+9. 490+93

70.6	6/10.2	2.0	7.4	7.8	6.6	6.5	6.9	7.5	7.5	5/6.7	4.6
49.5	4/7.6	31	23	20	14	0.1	13	15	21	2/-0.3	33

6.4

2/5.5	6.7	6.7	9.4	9.6	9.0	8.8	8.4	8.7	8.6	9.6	9.6	8.2	4/6.3	5.4
4/7.7	40	32	27	21	16	12	00	11	15	18	21	23	2/12.1	33

8.4

Sta.	T	H. I.	-	Elev.	Gr. No.
		1049.72			
f50				38.8	10.9
T.P.	2.68	1042.80.	9.60	1040.12.	
493				36.3	6.5
f50				33.8	9.0
T.P.	5.42	1040.36.	7.84	1034.94.	
494				31.3	9.1
T.P.	2.07	1035.20.	7.23	1033.13.	
f60				28.3	6.9
495				26.3	8.9
T.P.	0.49	1026.65.	9.04	1026.14.	
f17				25.4	1.3
T.P.	0.51	1021.07.	6.09	1020.56.	
496				21.3	-0.2
497				16.4	4.7
f50				14.2	6.9
498				12.2	8.9
T.P.	2.22	1013.94.	9.35	1011.72.	
f50				11.4	3.5

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9.5	9.1	8.3	12.2	12.5	11.4	11.9	10.9	10.1	11.2	11.5	12.9	11.9	8.1	8.2
4	1.8	34	28	18	15	12	0.0	12	17	20	26	33	34	

6.1	2.2	7.2	7.9	9.2	9.1	8.1	6.6	7.5	6.5	6.9	6.8	8.1	9.5	8.2	1.0
94	34	27	24	23	20	19	14	13	0.0	11	15	21	20	24	53

4.1	2.8	1.7	1.7	1.6	1.0	9.0	7.6	8.9	9.5	8.8	10.0	10.1	1.5	5.1	1.8
49	41	57	35	22	19	14	13	10.1	11	13	18	23	32	3	72

5.7	2.2	3.5	8.6	9.9	11.7	11.6	10.5	9.4	8.9	9.6	8.8	9.8	9.7	1.5	1.0
4	1.9	32	25	20	20	17	17	13	10.2	12	13	16	22	31	76

4.6	6.6	3.6	8.2	10.3	10.2	8.1	7.2	6.9	7.4	6.8	8.4	8.7	1.6	5.1
4	70.3	28	22	20	17	17	12	0.0	12	13	18	21	30	148

10.7	9.9	10.1	13.7	13.2	9.6	9.1	9.8	9.5	10.0	9.4	10.9	10.8	8.3	7.1
489	33	25	21	20	18	14	13	0.4	12	13	18	22	25	71.8

5.6	5.4	3.8	2.2	6.1	1.6	1.8	2.3	1.8	2.3	1.9	3.2	4.0	4.0	3.2	3.4
25	23	21	18	1	0.3	14	13	0.5	11	13	20	22	24	27	33

8.4	8.3	8.4	0.0	0.0	0.5	0.5	1.0	0.7	1.4	1.4	1.4	1.4	1.6	1.6
35	33	30	17	14	13	0.7	14	14	32	3	11.6	35		

9.9	9.4	4.8	4.7	4.7	4.7	4.9	4.7	8.1	8.6	7.9	8.8
33	25	17	13	0.0	0.0	11	11	21	23	28	35

10.2	9.3	6.9	6.7	7.0	6.7	7.0	8.1	8.2	5.9	5.7	5.2	6.0
33	24	17	15	12	10.2	13	17	22	24	27	27	33

10.2	11.2	11.8	11.1	8.9	8.4	8.9	8.0	10.8	10.9	10.5	11.2
33	30	26	20	10.5	12	15	17	22	27	33	

4.0	4.0	5.9	6.0	3.3	3.0	3.4	3.0	3.6	3.5	8.3	9.2
33	32	30	21	15	13	12	10.5	12	10.0	24	33

Sta.	+	H. I.	-	Elev.	Gr. R.
		1013.94			
499				08.7	5.2
B.M.	11.50	1013.01	12.43	1001.51	
+50				07.1	5.9
500				05.7	7.3
T.P.	1.49	1005.98	8.52	1004.49	
+50				04.4	1.4
501				03.4	2.6
+54				02.7	3.3
+50				02.5	<del>3.1</del> 3.5
T.P.	3.36	1004.86	4.48	1001.50	
502				01.8	3.1
+50				01.1	3.8
+78				00.7	4.2
503				00.3	4.4
+44				99.5	5.4

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$\frac{4.1}{32} \frac{64}{29} \frac{1}{2} \frac{7.1}{-1.9} \frac{64}{20} \frac{4.5}{14} \frac{7.4}{12} \frac{7.7}{11} \frac{4.5}{10.7} \frac{4.9}{15} \frac{6.4}{21} \frac{2}{2} \frac{6.4}{-1.2} \frac{7.7}{33}$

1.2  
5.2

$\frac{4.0}{28} \frac{7.6}{25} \frac{1}{2} \frac{7.8}{-1.9} \frac{7.8}{22} \frac{7.2}{21} \frac{5.2}{15} \frac{5.1}{12} \frac{5.7}{11} \frac{5.5}{10.7} \frac{5.5}{14} \frac{7.1}{19} \frac{5.9}{-10} \frac{5.1}{27} \frac{5.8}{33}$

5.9

$\frac{2.5}{23} \frac{7.7}{28} \frac{1}{2} \frac{8.1}{-0.8} \frac{8.2}{21} \frac{6.7}{14} \frac{6.7}{12} \frac{7.2}{11} \frac{6.8}{10.5} \frac{7.1}{15} \frac{7.4}{17} \frac{8.2}{19} \frac{8.3}{23} \frac{1}{2} \frac{7.8}{-0.3} \frac{9.4}{35}$

1.3

Approx H.I.

$\frac{1.14}{33} \frac{7.07}{31} \frac{2.7}{27} \frac{2.7}{22} \frac{1.3}{18} \frac{2.1}{14} \frac{1.5}{12} \frac{1.2}{10.4} \frac{1.8}{15} \frac{4.8}{21} \frac{5.4}{24} \frac{4}{2} \frac{2.93}{7.5} \frac{5.0}{33}$

1.6

Approx H.I.

$\frac{1.14}{42} \frac{4.6}{33} \frac{4.9}{29} \frac{2.9}{25} \frac{2.5}{21} \frac{2.5}{8} \frac{2.5}{10.1} \frac{2.9}{8} \frac{5.1}{13} \frac{5.3}{17} \frac{3.5}{18} \frac{2.8}{21} \frac{1}{2} \frac{4.1}{-0.8} \frac{5.0}{33}$

2.6

$\frac{8.0}{50} \frac{7.4}{44} \frac{3.4}{37} \frac{3.3}{32} \frac{2.9}{18} \frac{3.2}{18} \frac{5.9}{4} \frac{5.6}{8} \frac{2.7}{13} \frac{3.3}{24} \frac{3.2}{33}$

3.3

$\frac{1.1}{57} \frac{10.1}{50} \frac{5.5}{46} \frac{4.3}{43} \frac{3.4}{38} \frac{3.1}{26} \frac{3.7}{7} \frac{7.8}{-4.7} \frac{7.5}{4} \frac{4.8}{9} \frac{5.2}{23} \frac{1}{2} \frac{4.7}{-0.8} \frac{4.5}{50}$

3.5

$\frac{10.4}{90} \frac{7.5}{87} \frac{2.5}{73} \frac{2.4}{58} \frac{2.9}{40} \frac{11.6}{20} \frac{12.2}{-7.1} \frac{9.7}{14} \frac{7}{2} \frac{7.7}{-3.6} \frac{5.9}{33}$

3.1

$\frac{2.8}{88} \frac{2.5}{83} \frac{11.5}{66} \frac{12.7}{50} \frac{12.8}{-9.0} \frac{11.1}{25} \frac{9}{2} \frac{10.4}{-5.6} \frac{10.0}{33}$

3.8

$\frac{2.7}{79} \frac{2.5}{76} \frac{12.4}{54} \frac{12.8}{37} \frac{12.5}{21} \frac{12.2}{21} \frac{11.1}{33}$

4.2

$\frac{3.1}{65} \frac{3.2}{59} \frac{11.6}{38} \frac{12.2}{23} \frac{10.0}{-5.4} \frac{10.8}{21} \frac{1}{2} \frac{10.6}{-5.0} \frac{10.7}{33}$

4.6

$\frac{4.2}{28} \frac{4.2}{27} \frac{5.0}{15} \frac{8.5}{8} \frac{5.4}{17} \frac{5.0}{17} \frac{7.5}{33}$

5.4

Sta.	+	H. I.	-	Elev.	Gr. No.
		1004.84.			
	+50			97.5	54.
	+64			99.0	59.
504				98.2	49.
	+50			97.0	
	+85.			95.7	9.
13.M.			3.36	1001.50.	

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(56)

$\frac{4.4}{26}$	$\frac{4.5}{24}$	$\frac{4.9}{19}$	$\frac{9.1}{10}$	$\frac{9.1}{4}$	$\frac{7.8}{-2.2}$	$\frac{5.7}{5}$	$\frac{4.4}{19}$	$\frac{5.9}{28.8}$	$\frac{4}{170.5}$	$\frac{6.1}{33}$	$\frac{6.5}{33}$
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(59)

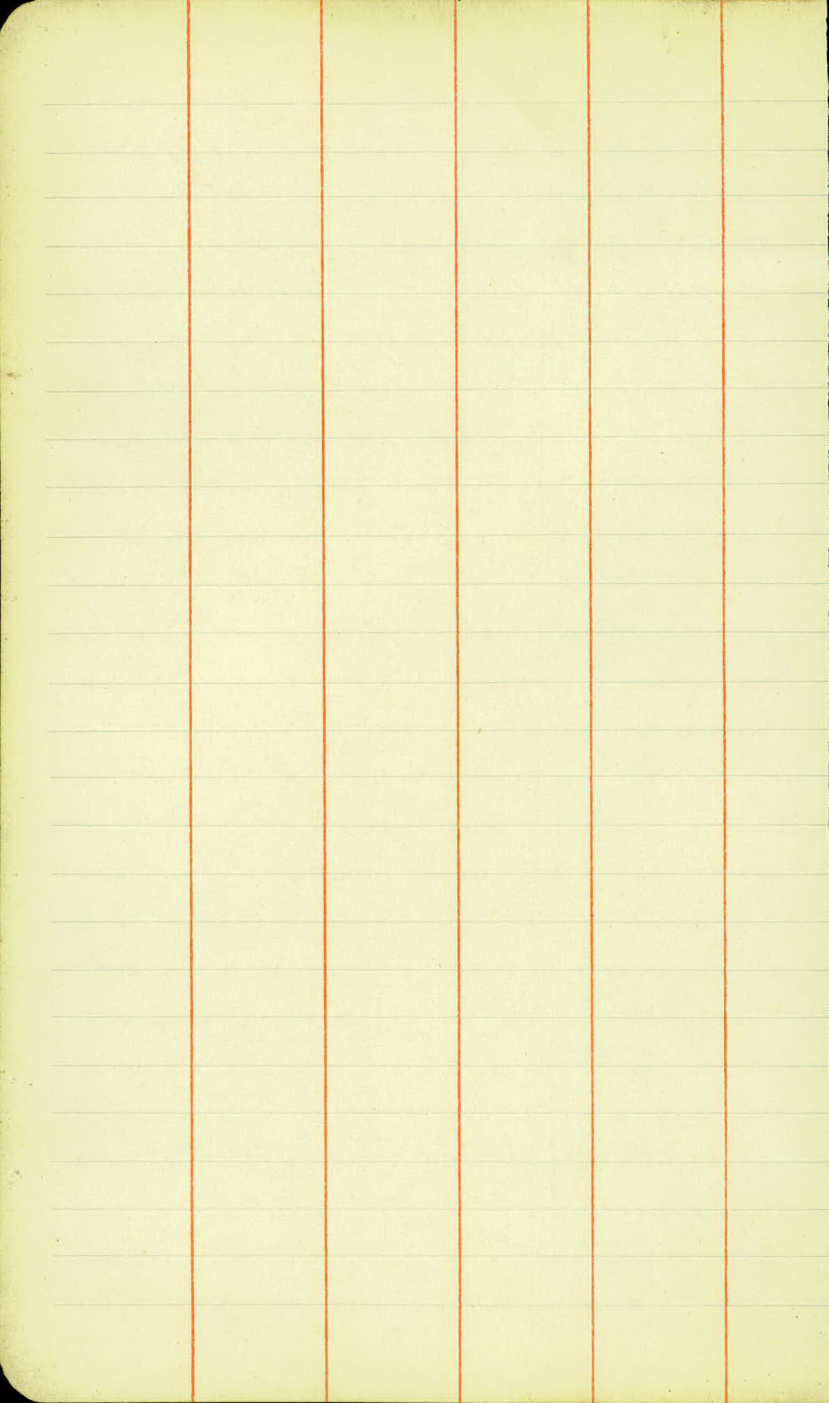
$\frac{4.9}{17}$	$\frac{4.8}{16}$	$\frac{4.7}{11}$	$\frac{9.1}{4}$	$\frac{9.8}{9}$	$\frac{9.2}{7}$	$\frac{6.2}{13}$	$\frac{4.5}{28}$	$\frac{5.4}{33}$
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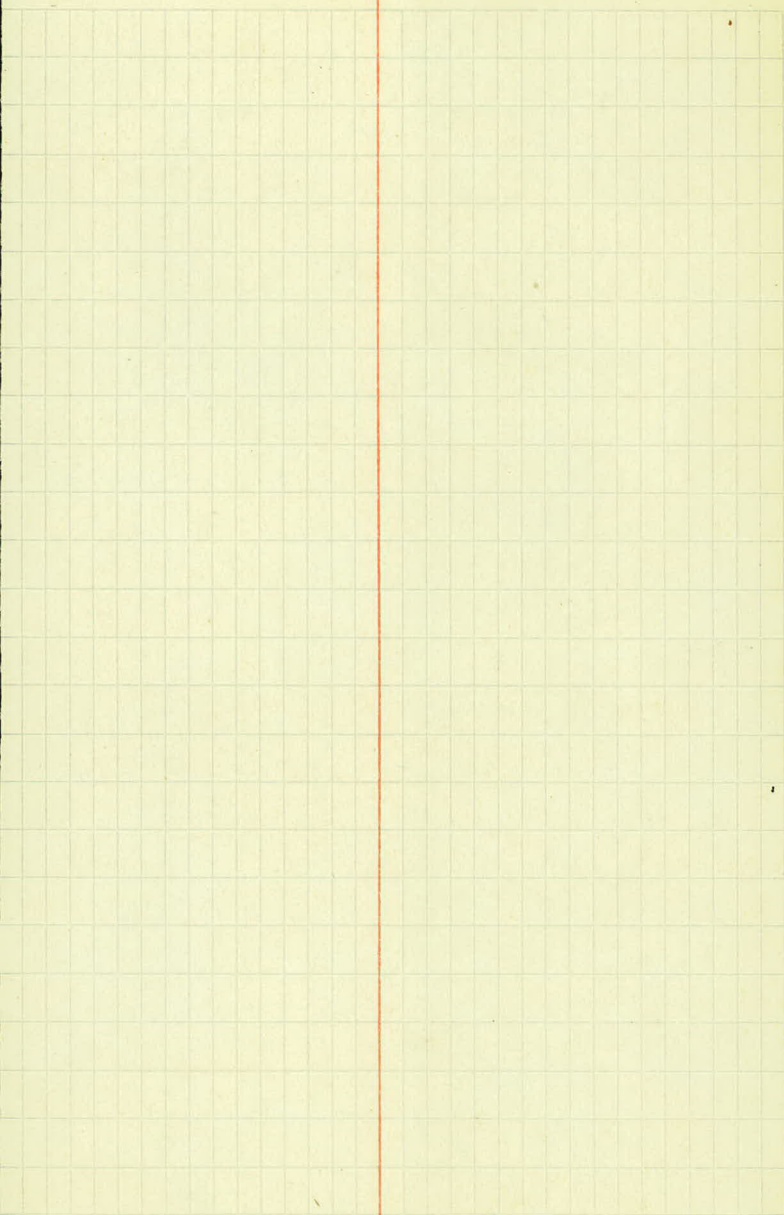
(67)

$\frac{5.9}{4}$	$\frac{5.8}{3}$	$\frac{5.7}{110}$	$\frac{5.9}{3}$	$\frac{9.8}{10}$	$\frac{9.6}{20}$	$\frac{6.4}{26.8}$	$\frac{4}{171.8}$	$\frac{5.6}{33}$	$\frac{5.6}{33}$
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$\frac{7.4}{7}$	$\frac{4.4}{8}$	$\frac{7.5}{13}$	$\frac{7.2}{13}$	$\frac{9.0}{18}$	$\frac{9.0}{27.2}$	$\frac{5.9}{-0.7}$	$\frac{8.9}{33}$
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$\frac{8.5}{9}$	$\frac{8.5}{10}$	$\frac{8.3}{14}$	$\frac{8.4}{14}$	$\frac{11.2}{19}$	$\frac{11.0}{23.2}$	$\frac{4}{171.2}$	$\frac{8.4}{33}$
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Sta.	+	H. I.	-	Elev.	Gr. No.
B.M.	4.51	997.95		993.44	
404				93.5	45
405				93.2	4.8
406				92.9	5.1
+45				95.0	<del>5.0</del>
407				92.9	5.1
+45				93.0	5.0
408				93.5	4.7
T.P.	5.90	998.69	5.16	992.79	
409				94.1	4.9
B.M.			0.61	992.08	
410				95.6	5.1
+50				96.7	2.0
+90				97.7	7.0
T.P.	8.91	1006.54	1.04	997.65	
411				97.9	8.9

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Nail 11 10.10 Lt. Sta. 404 + 20

4.9 5.7 7.6 7.6 5.9 4.7 9.46 4.1 4.7 5.0 8/5.3 5.3  
33 25 24 22 20 14 1/00 10.4 11 15 2/-28 33

5.8 6.0 7.8 7.1 6.5 5.8 7/4.9 4.5 4.6 4.4 7/4.9 6.2 6.2  
33 24 22 21 20 18 1/00 10.5 9 15 1/00 20 33

7.6 6/7.5 7.2 5.7 4.8 5.2 0/5.2 5.6 6.8 7.6 7.8  
33 19/-23 17 15 10.3 10 1/00 17 19 26 33

8.0 8.0 8.6 1.080 7.5 5.3 4.8 8/5.4 5.5 7.4 8.0 8.3  
33 24 22 2/-30 17 14 10.4 1/-29 17 22 26 33

8.2 7.9 8.5 7.4 4/5.4 5.2 4.9 5.2 2/5.2 5.3 7.5 7.9 8.0  
33 25 24 19 1/-03 15 10.2 13 1/-01 18 22 26 33

6.8 0/5.5 4.9 5.3 5.0 0/5.0 5.0 7.1 7.3 7.5  
33 16/-0.5 10.1 9 11 1/00 19 22 26 33

6.7 7.1 7.1 8.8 7.3 5.9 8/5.1 4.7 5.0 0/4.7 4.9 7.1 7.4 7.6  
33 27 24 22 21 18 1/-04 00 10 1/00 17 22 26 33

9.3 9.0 4/8.8 8.8 6.5 5.3 4.8 5.0 9/4.9 5.1 7.8 8.4  
33 27 2/-4.2 22 17 15 0.2 12 1/-03 17 24 33

Top in Tree Lt. Sta. 407 + 15.

10.0 9.9 5.7 5.3 3.8 5.9 7.0 8/7.0 9.6  
26 23 15 -0.2 15 20 23 2/-5.9 33

7.7 9/7.3 9.1 8.7 2.6 2.0 2.5 4/2.3 3.1 7.1 7.8  
33 2/-7.3 28 24 16 0.0 10 1/-03 18 24 33

7.8 6.0 1.6 0.9 1.3 1.1 2.9 5.0 5.1  
33 22 15 11 18 22 24 33

11.4 10.5 6/7.2 8.9 8.5 8.7 3/2.7 12.0 12.1 12.5  
33 25 16/-0.5 14 10.7 13 1/00 23 25 33

Sta.	+	M. I.	-	Elev.	Gr. R.
		1006.54.			
	+35			98.9	7.7
	+40			99.1	7.5
412				1000.9	5.7
	+50			02.5	4.1
413				04.0	2.6
T.P.	8.58	1013.93.	1.61	1004.95.	
	+50			05.6	7.6 7.7
414				07.0	6.0 6.3
	+50			07.7	5.2 5.6
415				07.9	4.7 5.4
	+50			07.8	4.4 5.5
416				07.0	5.4 6.3
	+50			05.7	6.7 7.4
T.P.	11.85	1021.74.	3.24	1010.09.	

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118	111	88	77	74	80	74
53	22	17	10		21	33

11.7	10.6	8.5	7.6	7.3	7.7	7.6	8.3	5.7	4.9
33	22	17	10	10.2	12	11	22	25	33

7.5	4.0	7.0	6.3	5.4	5.6	6.3	6.2	0.6
33	2	13	20	10.3	15	18	22	2.7

4.8	4.5	4.9	4.4	5.8	4.2	3.5
33	2	23	20	10.3	4	17

2.8	3.3	3.1	2.6	2.3	2.4	2.2
33	31	2	15	10.3	7	17

7.5	8.8	9.0	8.4	8.2	7.8	7.6	7.6	7.8
33	31	29	2	21	13	10.1	8	15

5.2	5.4	7.7	7.5	7.1	6.7	6.5	6.6	6.6	6.3
33	31	28	2	22	14	10.2	10	1	19

6.3	2.6	6.0	5.6	5.7	5.6	5.1
33	2	15	0.0	12	15	29

7.0	4.6	6.1	5.3	5.0	7.4	4.5	4.0	1.7	1.0
33	2	21	12	10.4	6	24	24	29	3

7.0	6.1	6.9	6.9	5.3	5.1	5.1	5.6	5.7	5.3	0.0
33	21	24	24	19	15	10.4	14	10.9	20	29

8.2	9.2	8.9	6.0	5.8	5.9	6.2	6.4	5.9	2.0
33	32	27	22	10.4	10.4	13	15	17	25

8.9	7.8	6.9	6.7	6.6	7.2	7.2	7.9	4.7	3.8
40	33	29	2	15	10.4	10	14	17	20

Sta.	+	H. I.	-	Flev.	Gr. N.
		1021.94.			
412				1000.9	21.0
	+50			02.5	19.5
413				04.0	17.9
	+50			05.6	16.3.
414				07.0	14.9.
	+50			07.7	14.2.
415				07.9	14.0.
	+50			07.8	14.1.
416				07.0	14.9.
T.P.	0.07	1010.16.	11.85	1010.09.	
B.M.			9.09	1001.07.	
B.M.			5.35	1004.81.	
417				04.2	52.60.
	+50			02.7	6.9 7.5.

1027

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$$\begin{array}{r} 0 \\ 8 \overline{) 13.4} \\ \underline{3} \\ 7.6 \end{array} \quad \begin{array}{r} 12.1 \\ \underline{34} \end{array}$$

$$\begin{array}{r} 7.5 \\ 31 \overline{) 230} \\ \underline{216} \\ 140 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 6.9} \\ \underline{5} \\ 1.9 \end{array} \quad \begin{array}{r} 6.5 \\ 35 \overline{) 227.5} \\ \underline{210} \\ 17.5 \end{array}$$

$$\begin{array}{r} 0 \\ 8 \overline{) 8.5} \\ \underline{8} \\ .5 \end{array} \quad \begin{array}{r} 5.5 \\ 35 \overline{) 192.5} \\ \underline{175} \\ 17.5 \end{array} \quad \begin{array}{r} 1.5 \\ 40 \overline{) 60} \\ \underline{40} \\ 20 \end{array} \quad \begin{array}{r} 1.9 \\ 50 \overline{) 95} \\ \underline{50} \\ 45 \end{array}$$

$$\begin{array}{r} 6.2 \\ 31 \overline{) 192.2} \\ \underline{186} \\ 6.2 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 3.8} \\ \underline{3} \\ .8 \end{array} \quad \begin{array}{r} 2.1 \\ 35 \overline{) 73.5} \\ \underline{70} \\ 3.5 \end{array} \quad \begin{array}{r} 2.4 \\ 40 \overline{) 96} \\ \underline{80} \\ 16 \end{array}$$

$$\begin{array}{r} 0 \\ 8 \overline{) 3.9} \\ \underline{3} \\ .9 \end{array} \quad \begin{array}{r} 4.3 \\ 36 \overline{) 154.8} \\ \underline{144} \\ 10.8 \end{array} \quad \begin{array}{r} 4.0 \\ 40 \overline{) 160} \\ \underline{160} \\ 0 \end{array}$$

$$\begin{array}{r} 0 \\ 8 \overline{) 9.0} \\ \underline{8} \\ 1.0 \end{array} \quad \begin{array}{r} 5.4 \\ 35 \overline{) 189} \\ \underline{175} \\ 14 \end{array} \quad \begin{array}{r} 5.2 \\ 40 \overline{) 208} \\ \underline{200} \\ 8 \end{array}$$

$$\begin{array}{r} 5.9 \\ 35 \overline{) 206.5} \\ \underline{203} \\ 3.5 \end{array} \quad \begin{array}{r} 5.5 \\ 40 \overline{) 220} \\ \underline{200} \\ 20 \end{array}$$

$$\begin{array}{r} 5.9 \\ 31 \overline{) 182.9} \\ \underline{177} \\ 5.9 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 5.7} \\ \underline{4} \\ 1.7 \end{array} \quad \begin{array}{r} 5.2 \\ 40 \overline{) 208} \\ \underline{200} \\ 8 \end{array}$$

$$\begin{array}{r} 8.3 \\ 26 \overline{) 213.8} \\ \underline{208} \\ 5.8 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 7.6} \\ \underline{6} \\ 1.6 \end{array} \quad \begin{array}{r} 7.3 \\ 40 \overline{) 292} \\ \underline{280} \\ 12 \end{array}$$

Sp. N. in Twin Oak Lt Sta. 466 + 90.

$$\begin{array}{r} 8.1 \\ 43 \overline{) 348.3} \\ \underline{344} \\ 4.3 \end{array} \quad \begin{array}{r} 6.4 \\ 57 \overline{) 364.8} \\ \underline{342} \\ 22.8 \end{array} \quad \begin{array}{r} 5.4 \\ 39 \overline{) 210.6} \\ \underline{205} \\ 5.6 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 5.1} \\ \underline{4} \\ 1.1 \end{array} \quad \begin{array}{r} 5.1 \\ 14 \overline{) 71.4} \\ \underline{70} \\ 1.4 \end{array} \quad \begin{array}{r} 5.9 \\ 10.1 \overline{) 59.61} \\ \underline{59} \\ .61 \end{array} \quad \begin{array}{r} 5.5 \\ 12 \overline{) 66} \\ \underline{60} \\ 6 \end{array} \quad \begin{array}{r} 6.5 \\ 15 \overline{) 97.5} \\ \underline{90} \\ 7.5 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 6.2} \\ \underline{5} \\ 1.2 \end{array} \quad \begin{array}{r} 10.8 \overline{) 86.4} \\ \underline{86} \\ .4 \end{array} \quad \begin{array}{r} 6.1 \\ 20 \overline{) 122} \\ \underline{120} \\ 2 \end{array} \quad \begin{array}{r} 3.0 \\ 23 \overline{) 69} \\ \underline{69} \\ 0 \end{array} \quad \begin{array}{r} 93.1 \\ 8 \overline{) 744.8} \\ \underline{736} \\ 8.8 \end{array} \quad \begin{array}{r} 27 \\ 40 \overline{) 1080} \\ \underline{1040} \\ 40 \end{array}$$

$$\begin{array}{r} 7.3 \\ 37 \overline{) 270.1} \\ \underline{261} \\ 9.1 \end{array} \quad \begin{array}{r} 7.2 \\ 24 \overline{) 172.8} \\ \underline{168} \\ 4.8 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 6.9} \\ \underline{5} \\ 1.9 \end{array} \quad \begin{array}{r} 6.9 \\ 15 \overline{) 103.5} \\ \underline{102} \\ 1.5 \end{array} \quad \begin{array}{r} 7.4 \\ 10.1 \overline{) 74.61} \\ \underline{74} \\ .61 \end{array} \quad \begin{array}{r} 8.0 \\ 13 \overline{) 104} \\ \underline{104} \\ 0 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \overline{) 106.4} \\ \underline{100} \\ 6.4 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 7.5} \\ \underline{6} \\ 1.5 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \overline{) 106.4} \\ \underline{100} \\ 6.4 \end{array} \quad \begin{array}{r} 7.6 \\ 14 \overline{) 106.4} \\ \underline{100} \\ 6.4 \end{array} \quad \begin{array}{r} 8.1 \\ 21 \overline{) 170.1} \\ \underline{168} \\ 2.1 \end{array} \quad \begin{array}{r} 8.5 \\ 22 \overline{) 187} \\ \underline{184} \\ 3 \end{array} \quad \begin{array}{r} 50.0 \\ 25 \overline{) 1250} \\ \underline{1250} \\ 0 \end{array} \quad \begin{array}{r} 0 \\ 8 \overline{) 5.3} \\ \underline{4} \\ 1.3 \end{array} \quad \begin{array}{r} 5.5 \\ 30 \overline{) 165} \\ \underline{150} \\ 15 \end{array}$$

Sta.	T	H.I.	-	Elev	Br. No.
		1010.14			
418				01.2	8.7 9.0.
T.P.	8.88	1009.94.	9.10	1001.06.	
+50				99.7	102.
419				98.2	12.0 11.7.
T.P.	2.77	1000.64.	12.07	997.87.	
418+50				99.7	- 0.9
419				98.2	2.7 2.4
+50				96.3	5.0 4.3.
420				95.4	6.2 5.2.
+50				94.3	7.4 6.5.
421				93.6	8.1 7.0.
T.P.	4.18	997.25.	7.57	993.07.	
+50				93.0	5.4 4.3.
422				92.7	5.7 4.4.
+50				92.6	5.8 4.7.

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$\frac{11.8}{33}$	$\frac{9.6}{30}$	$\frac{9.5}{27}$	$\frac{4}{2} \frac{9.1}{-0.4}$	$\frac{8.2}{24}$	$\frac{8.6}{15}$	$\frac{8.8}{10.2}$	$\frac{99.1}{102}$	$\frac{97}{20}$	$\frac{97}{24}$	$\frac{8.5}{27}$	$\frac{4}{2} \frac{8.1}{7.2}$	$\frac{8.3}{33}$
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$\frac{10.5}{17.5}$	$\frac{2}{1} \frac{10.3}{-0.1}$	$\frac{10.4}{14}$	$\frac{10.2}{0.0}$	$\frac{10.7}{13}$	$\frac{11.0}{15}$	$\frac{10.9}{20}$	$\frac{3.5}{31.3}$	$\frac{0.4}{10.2}$
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$\frac{12.2}{11}$	$\frac{12.0}{-0.3}$	$\frac{12.0}{15}$	$\frac{12.0}{19}$	$\frac{12.6}{20}$	$\frac{12.6}{21}$	$\frac{11.7}{24.3}$	$\frac{0}{10.3}$	$\frac{1.6}{36}$
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$\frac{11.5}{33}$	$\frac{11.3}{30}$	(9)
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$\frac{0}{3} \frac{12.3}{-9.6}$	$\frac{10.8}{23}$	$\frac{5.7}{13}$
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$\frac{11.5}{33}$	$\frac{4}{2} \frac{11.2}{-6.2}$	$\frac{10.8}{22}$	$\frac{9.7}{18}$	$\frac{5.1}{11}$	$\frac{5.0}{8}$	$\frac{5.5}{6}$	$\frac{5.2}{-0.9}$	$\frac{4.7}{12}$	$\frac{4.8}{16}$	$\frac{5.0}{20.4}$	$\frac{4}{2} \frac{4.4}{-0.7}$	$\frac{4.5}{27}$	$\frac{5.7}{33}$
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$\frac{11.6}{33}$	$\frac{4}{2} \frac{11.1}{-4.9}$	$\frac{10.1}{31}$	$\frac{8.1}{17}$	$\frac{6.8}{13}$	$\frac{6.3}{7.1}$	$\frac{5.8}{9}$	$\frac{4}{1} \frac{6.1}{-1.7}$	$\frac{5.7}{21}$	$\frac{5.9}{25}$	$\frac{9.7}{33}$
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$\frac{11.6}{33}$	$\frac{4}{2} \frac{10.6}{-3.2}$	$\frac{9.9}{21}$	$\frac{9.8}{17}$	$\frac{6.6}{-0.3}$	$\frac{7.0}{11}$	$\frac{6.8}{16}$	$\frac{12.5}{27}$	$\frac{2}{1} \frac{2.5}{-7.1}$	$\frac{12.5}{33}$
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$\frac{10.5}{33}$	$\frac{4}{2} \frac{8.9}{-0.8}$	$\frac{7.6}{25}$	$\frac{7.3}{11}$	$\frac{7.3}{-0.9}$	$\frac{7.5}{4}$	$\frac{7.7}{9}$	$\frac{12.6}{19}$	$\frac{4}{1} \frac{4.4}{-2.3}$	$\frac{14.2}{33}$
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$\frac{6.0}{33}$	$\frac{4}{2} \frac{5.0}{10.4}$	$\frac{4.1}{15}$	$\frac{4.5}{-0.2}$	$\frac{4.4}{4}$	$\frac{6.2}{7}$	$\frac{9.1}{14}$	$\frac{2}{1} \frac{10.5}{-7.1}$	$\frac{10.0}{33}$
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$\frac{5.5}{33}$	$\frac{4}{2} \frac{5.4}{-0.3}$	$\frac{4.5}{15}$	$\frac{4.5}{10.1}$	$\frac{4.8}{4}$	$\frac{8.7}{14}$	$\frac{4}{2} \frac{4.4}{-5.7}$	$\frac{9.7}{33}$
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$\frac{6.0}{33}$	$\frac{4}{2} \frac{5.8}{0.0}$	$\frac{4.8}{14}$	$\frac{4.9}{-0.2}$	$\frac{5.1}{7}$	$\frac{7.6}{12}$	$\frac{4}{2} \frac{8.5}{-4.7}$	$\frac{8.8}{33}$
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Sta.		H. I.	-	Elev.	Gr. No.
379.	+	997.25			
423				92.6	5.7 4.7.
+50				92.6	5.3 4.7.
424				92.5	5.1 4.8.
+50				92.5	4.9 4.8.
425				92.4	4.9 4.7.
+50				92.4	4.6 4.9.
T. P.	4.44	996.75	4.94	992.31.	
426				92.3	4.0 4.5.
+50				92.3	3.7 4.5.
427				92.2	3.7 4.4.
+50				92.4	3.5 4.4.
428				92.8	3.1 4.0.
+50				95.7	2.2 3.1.
B. M.	7.58	1100.70	3.63	993.12.	

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$\frac{5.2}{33} \frac{4}{2} \frac{4}{1} \frac{6.6}{79} \frac{5.6}{24} \frac{5.0}{178} \frac{4.7}{10} \frac{4.8}{0.1} \frac{4.7}{4} \frac{5.0}{4} \frac{6.6}{11.2} \frac{2.7}{2} \frac{7.5}{36} \frac{7.7}{33}$

$\frac{5.5}{33} \frac{5.9}{28} \frac{6.6}{27} \frac{4}{2} \frac{6.7}{-13} \frac{6.4}{22} \frac{5.4}{19} \frac{5.1}{15} \frac{4.8}{-0.1} \frac{4.7}{15} \frac{5.7}{9} \frac{6.6}{-2.0} \frac{6.9}{33}$

$\frac{4.9}{33} \frac{4}{2} \frac{4.8}{103} \frac{4.8}{24} \frac{5.8}{20} \frac{5.7}{15} \frac{5.4}{12} \frac{4.9}{-0.1} \frac{5.4}{14} \frac{5.4}{21.8} \frac{6.4}{-1.9} \frac{6.0}{26} \frac{6.1}{33}$

$\frac{4.5}{33} \frac{6}{2} \frac{4.7}{102} \frac{4.9}{17} \frac{5.2}{15} \frac{5.6}{14} \frac{5.3}{7} \frac{5.1}{-0.3} \frac{4.9}{10} \frac{5.1}{15} \frac{5.6}{2} \frac{6.8}{-0.8} \frac{6.8}{28} \frac{6.5}{31} \frac{5.7}{32} \frac{5.7}{33}$

$\frac{5.0}{33} \frac{5.7}{2} \frac{5.1}{-0.2} \frac{4.7}{15} \frac{4.9}{0.0} \frac{4.8}{15} \frac{5.4}{26} \frac{5.7}{2} \frac{5.2}{-0.2} \frac{5.4}{27} \frac{6.5}{33}$

$\frac{8.6}{33} \frac{8.3}{30} \frac{6.8}{22} \frac{4}{1} \frac{5.8}{-1.2} \frac{4.9}{13} \frac{5.2}{9} \frac{5.2}{-0.3} \frac{4.8}{15} \frac{5.4}{24.2} \frac{6}{0} \frac{5.2}{0.0} \frac{5.5}{30} \frac{6.4}{33}$

$\frac{9.0}{33} \frac{3}{2} \frac{0}{-4.0} \frac{7.9}{22} \frac{4.8}{15} \frac{4.5}{0.0} \frac{5.1}{15.4} \frac{5.2}{20} \frac{5.6}{24} \frac{6.5}{2} \frac{7.9}{-0.9} \frac{7.9}{27} \frac{8.2}{33}$

$\frac{5.9}{33} \frac{5.2}{21} \frac{5}{2} \frac{4.7}{-1.0} \frac{4.3}{15} \frac{5.0}{-0.5} \frac{5.9}{13} \frac{5.5}{14} \frac{6.5}{7} \frac{9}{-0.5} \frac{7.4}{26} \frac{10.0}{33}$

$\frac{4.8}{33} \frac{4}{1} \frac{5.0}{-13} \frac{5.0}{15} \frac{6.0}{-1.4} \frac{6.4}{9} \frac{6.7}{14} \frac{7.4}{17} \frac{9.9}{21} \frac{2}{2} \frac{10.8}{-5.1} \frac{11.4}{33}$

$\frac{4.4}{33} \frac{1.8}{0} \frac{5.0}{-1.5} \frac{5.0}{19} \frac{6.3}{-1.9} \frac{7.7}{15} \frac{11.5}{22} \frac{8}{2} \frac{1.9}{-6.4} \frac{12.8}{33}$

$\frac{6.7}{33} \frac{6.5}{30} \frac{4.4}{24} \frac{4}{1} \frac{4.4}{-13} \frac{5.2}{-1.2} \frac{5.8}{10} \frac{5.9}{15} \frac{10.8}{26} \frac{9}{2} \frac{11.1}{-6.0} \frac{11.4}{33}$

$\frac{9.0}{33} \frac{9.0}{31} \frac{7.4}{29} \frac{5.9}{27} \frac{3.6}{23} \frac{6}{1} \frac{3.5}{-1.3} \frac{3.7}{-0.6} \frac{4.9}{14} \frac{6.1}{17} \frac{10.0}{24} \frac{4}{2} \frac{10.4}{-6.2} \frac{10.7}{33}$

Sta.	+	M.I.	-	Elev.	Gr. No.
		1000.70.			
429				74.7	5.0 5.8.
B.M.			6.16	794.54.	
+50				76.3	3.7 4.4.
+74				97.0	3.7
T.P.	8.39	1006.27.	2.82	797.88.	
430				77.7	8.5 8.6.
+50				99.1	7.2.
431				00.5	5.8.
+50				01.8	4.5.
432				03.0	3.3.
+50				04.0	2.9.
T.P.	7.40	1011.70.	1.97	1004.30.	
430+50				99.1	12.6
431				00.5	11.7
431+50				01.8.	9.9

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$\begin{array}{r} 10.5 \\ 33 \end{array}$ 
 $\begin{array}{r} 10.7 \\ 27 \end{array}$ 
 $\begin{array}{r} 4/9.8 \\ -4.8 \end{array}$ 
 $\begin{array}{r} 9.2 \\ 21 \end{array}$ 
 $\begin{array}{r} 6.3 \\ 16 \end{array}$ 
 $\begin{array}{r} 6.1 \\ -0.3 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 13 \end{array}$ 
 $\begin{array}{r} 7.5 \\ 16 \end{array}$ 
 $\begin{array}{r} 12.4 \\ 25 \end{array}$ 
 $\begin{array}{r} 6/13.1 \\ -6.4 \end{array}$ 
 $\begin{array}{r} 13.5 \\ 33 \end{array}$

510 N in 12" Tree Lt. Sta. 429+30

$\begin{array}{r} 1.9 \\ 33 \end{array}$ 
 $\begin{array}{r} 1.9 \\ 31 \end{array}$ 
 $\begin{array}{r} 5.8 \\ 25 \end{array}$ 
 $\begin{array}{r} 9.6 \\ 19 \end{array}$ 
 $\begin{array}{r} 6.2 \\ -2.5 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 15 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 00 \end{array}$ 
 $\begin{array}{r} 5.0 \\ 14 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 1 \end{array}$ 
 $\begin{array}{r} 5.6 \\ -0.2 \end{array}$ 
 $\begin{array}{r} 10.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 10.9 \\ 29 \end{array}$ 
 $\begin{array}{r} 10.9 \\ 33 \end{array}$

Above H.I.

$\begin{array}{r} 11.0 \\ 33 \end{array}$ 
 $\begin{array}{r} 11.0 \\ 32 \end{array}$ 
 $\begin{array}{r} 0.0 \\ 31 \end{array}$ 
 $\begin{array}{r} 5.1 \\ 25 \end{array}$ 
 $\begin{array}{r} 5.3 \\ 19 \end{array}$ 
 $\begin{array}{r} 5.8 \\ 16 \end{array}$ 
 $\begin{array}{r} 3.5 \\ 14 \end{array}$ 
 $\begin{array}{r} 4.4 \\ 14 \end{array}$ 
 $\begin{array}{r} 5.4 \\ 18 \end{array}$ 
 $\begin{array}{r} 7.8 \\ 27 \end{array}$ 
 $\begin{array}{r} 8.3 \\ 33 \end{array}$

$\begin{array}{r} 4.9 \\ 33 \end{array}$ 
 $\begin{array}{r} 9.9 \\ 26 \end{array}$ 
 $\begin{array}{r} 10.5 \\ 22 \end{array}$ 
 $\begin{array}{r} 9.9 \\ 18 \end{array}$ 
 $\begin{array}{r} 4/8.5 \\ 1 \end{array}$ 
 $\begin{array}{r} 8.2 \\ -0.2 \end{array}$ 
 $\begin{array}{r} 8.2 \\ 10.4 \end{array}$ 
 $\begin{array}{r} 8.7 \\ 13 \end{array}$ 
 $\begin{array}{r} 6/9.7 \\ 1 \end{array}$ 
 $\begin{array}{r} 12.9 \\ -0.8 \end{array}$ 
 $\begin{array}{r} 12.9 \\ 33 \end{array}$

$\begin{array}{r} 7.9 \\ 23 \end{array}$ 
 $\begin{array}{r} 8.6 \\ 18 \end{array}$ 
 $\begin{array}{r} 0/7.2 \\ 1 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 10.3 \end{array}$ 
 $\begin{array}{r} 7.5 \\ 14 \end{array}$ 
 $\begin{array}{r} 10.0 \\ 19 \end{array}$ 
 $\begin{array}{r} 6/10.1 \\ 1 \end{array}$ 
 $\begin{array}{r} 9.9 \\ 23 \end{array}$ 
 $\begin{array}{r} 8.5 \\ 26 \end{array}$ 
 $\begin{array}{r} 8.8 \\ 33 \end{array}$

$\begin{array}{r} 5.6 \\ 24 \end{array}$ 
 $\begin{array}{r} 6.7 \\ 18 \end{array}$ 
 $\begin{array}{r} 0/5.8 \\ 1 \end{array}$ 
 $\begin{array}{r} 5.6 \\ 10.2 \end{array}$ 
 $\begin{array}{r} 6.2 \\ 13 \end{array}$ 
 $\begin{array}{r} 8.0 \\ 17 \end{array}$ 
 $\begin{array}{r} 8/8.2 \\ 1 \end{array}$ 
 $\begin{array}{r} 8.5 \\ 23 \end{array}$ 
 $\begin{array}{r} 4.1 \\ 29 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 33 \end{array}$

$\begin{array}{r} 4.7 \\ 22 \end{array}$ 
 $\begin{array}{r} 5.5 \\ 18 \end{array}$ 
 $\begin{array}{r} 0/4.9 \\ 1 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 10.2 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 14 \end{array}$ 
 $\begin{array}{r} 7.0 \\ 19 \end{array}$ 
 $\begin{array}{r} 4/7.2 \\ 1 \end{array}$ 
 $\begin{array}{r} 6.9 \\ 25 \end{array}$ 
 $\begin{array}{r} 4.0 \\ 29 \end{array}$ 
 $\begin{array}{r} 4.2 \\ 33 \end{array}$

$\begin{array}{r} 4.5 \\ 24 \end{array}$ 
 $\begin{array}{r} 4.8 \\ 18 \end{array}$ 
 $\begin{array}{r} 2/3.4 \\ 1 \end{array}$ 
 $\begin{array}{r} 3.2 \\ 10.1 \end{array}$ 
 $\begin{array}{r} 3.6 \\ 13 \end{array}$ 
 $\begin{array}{r} 6.0 \\ 19 \end{array}$ 
 $\begin{array}{r} 4/6.4 \\ 1 \end{array}$ 
 $\begin{array}{r} 6.2 \\ 26 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 29 \end{array}$ 
 $\begin{array}{r} 4.5 \\ 33 \end{array}$

$\begin{array}{r} 3.1 \\ 25 \end{array}$ 
 $\begin{array}{r} 3.6 \\ 19 \end{array}$ 
 $\begin{array}{r} 8/2.3 \\ 1 \end{array}$ 
 $\begin{array}{r} 2.1 \\ 13 \end{array}$ 
 $\begin{array}{r} 1.9 \\ 10.4 \end{array}$ 
 $\begin{array}{r} 2.5 \\ 14 \end{array}$ 
 $\begin{array}{r} 2/5.4 \\ 1 \end{array}$ 
 $\begin{array}{r} 3.3 \\ 26 \end{array}$ 
 $\begin{array}{r} 4.3 \\ 29 \end{array}$ 
 $\begin{array}{r} 4.7 \\ 33 \end{array}$

$\begin{array}{r} 4.9 \\ 33 \end{array}$ 
 $\begin{array}{r} 4.9 \\ 32 \end{array}$

$\begin{array}{r} 1.8 \\ 35 \end{array}$ 
 $\begin{array}{r} 1.8 \\ 33 \end{array}$

$\begin{array}{r} 1.3 \\ 35 \end{array}$ 
 $\begin{array}{r} 1.3 \\ 33 \end{array}$

Sta.	+	H. I.	-	Elev.	Dr. R.
		1011.70.			
432				03.0	8.7
432 + 50				04.0	7.7
433				04.9	6.8
+ 50				05.4	6.1
434				06.2	5.5
+ 50				06.7	5.0
435				07.2	4.5
+ 50				07.4	4.1
436				08.1	3.6
+ 50				08.5	3.2
T.P.	5.65	1014.49.	2.86	1008.84.	
437				08.9	5.4
+ 50				09.3	5.2

6-2-27

$$\begin{array}{r} 4.1 \\ 35 \end{array} \quad \begin{array}{r} 4.1 \\ 35 \end{array}$$

$$\begin{array}{r} 5.3 \\ 35 \end{array} \quad \begin{array}{r} 5.1 \\ 32 \end{array}$$

$$\begin{array}{r} 6.4 \\ 33 \end{array} \begin{array}{r} 8.5 \\ 27 \end{array} \begin{array}{r} 8.4 \\ 18 \end{array} \begin{array}{r} 4 \times \\ 7.1 \\ 15 \end{array} \begin{array}{r} 6.8 \\ 14 \end{array} \begin{array}{r} 6.5 \\ 10.3 \end{array} \begin{array}{r} 4 \times \\ 7.1 \\ 15 \end{array} \begin{array}{r} 8.7 \\ 19 \end{array} \begin{array}{r} 9.5 \\ 24 \end{array} \begin{array}{r} 8.8 \\ 44 \end{array} \begin{array}{r} 7.6 \\ 28 \end{array} \begin{array}{r} 7.8 \\ 38 \end{array}$$

$$\begin{array}{r} 8.8 \\ 33 \end{array} \begin{array}{r} 7.8 \\ 24 \end{array} \begin{array}{r} 8 \times \\ 6.5 \\ 15 \end{array} \begin{array}{r} 6.3 \\ 14 \end{array} \begin{array}{r} 5.7 \\ 10.4 \end{array} \begin{array}{r} 9 \times \\ 6.1 \\ 15 \end{array} \begin{array}{r} 7.1 \\ 18 \end{array} \begin{array}{r} 7.7 \\ 22 \end{array} \begin{array}{r} 4 \times \\ 7.7 \\ 15 \end{array} \begin{array}{r} 7.3 \\ 24 \end{array} \begin{array}{r} 6.1 \\ 28 \end{array} \begin{array}{r} 6.7 \\ 33 \end{array}$$

$$\begin{array}{r} 9.1 \\ 33 \end{array} \begin{array}{r} 8.2 \\ 23 \end{array} \begin{array}{r} 4 \times \\ 7.2 \\ 15 \end{array} \begin{array}{r} 5.6 \\ 14 \end{array} \begin{array}{r} 5.2 \\ 10.3 \end{array} \begin{array}{r} 0 \times \\ 5.5 \\ 15 \end{array} \begin{array}{r} 6.7 \\ 19 \end{array} \begin{array}{r} 2 \times \\ 6.7 \\ 15 \end{array} \begin{array}{r} 6.3 \\ 27 \end{array} \begin{array}{r} 5.2 \\ 30 \end{array} \begin{array}{r} 3.5 \\ 33 \end{array}$$

$$\begin{array}{r} 8.8 \\ 33 \end{array} \begin{array}{r} 6 \times \\ 7.5 \\ 15 \end{array} \begin{array}{r} 5.6 \\ 14 \end{array} \begin{array}{r} 5.3 \\ 13 \end{array} \begin{array}{r} 4.6 \\ 10.4 \end{array} \begin{array}{r} 4.9 \\ 15 \end{array} \begin{array}{r} 6.1 \\ 18 \end{array} \begin{array}{r} 4 \times \\ 5.7 \\ 15 \end{array} \begin{array}{r} 5.5 \\ 24 \end{array} \begin{array}{r} 1.5 \\ 32 \end{array} \begin{array}{r} 1.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.6 \\ 33 \end{array} \begin{array}{r} 2 \times \\ 6.6 \\ 15 \end{array} \begin{array}{r} 4.7 \\ 12 \end{array} \begin{array}{r} 4.3 \\ 10.2 \end{array} \begin{array}{r} 4.5 \\ 14 \end{array} \begin{array}{r} 4.6 \\ 18 \end{array} \begin{array}{r} 6.1 \\ 23 \end{array} \begin{array}{r} 4 \times \\ 5.9 \\ 15 \end{array} \begin{array}{r} 4.3 \\ 28 \end{array} \begin{array}{r} 2.4 \\ 32 \end{array} \begin{array}{r} 2.4 \\ 33 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \begin{array}{r} 4 \times \\ 5.8 \\ 15 \end{array} \begin{array}{r} 5.8 \\ 17 \end{array} \begin{array}{r} 4.3 \\ 13 \end{array} \begin{array}{r} 4.2 \\ 10.1 \end{array} \begin{array}{r} 4.3 \\ 15 \end{array} \begin{array}{r} 5.6 \\ 18 \end{array} \begin{array}{r} 4 \times \\ 5.6 \\ 15 \end{array} \begin{array}{r} 5.3 \\ 27 \end{array} \begin{array}{r} 3.3 \\ 31 \end{array} \begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 7.0 \\ 33 \end{array} \begin{array}{r} 1 \times \\ 6.6 \\ 15 \end{array} \begin{array}{r} 6.5 \\ 19 \end{array} \begin{array}{r} 3.8 \\ 13 \end{array} \begin{array}{r} 3.8 \\ 10.2 \end{array} \begin{array}{r} 4.1 \\ 12 \end{array} \begin{array}{r} 4.1 \\ 15 \end{array} \begin{array}{r} 5.4 \\ 18 \end{array} \begin{array}{r} 5.5 \\ 25 \end{array} \begin{array}{r} 3.4 \\ 30 \end{array} \begin{array}{r} 3.3 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \end{array} \begin{array}{r} 2 \times \\ 4.8 \\ 15 \end{array} \begin{array}{r} 4.7 \\ 19 \end{array} \begin{array}{r} 3.2 \\ 14 \end{array} \begin{array}{r} 3.1 \\ 10.1 \end{array} \begin{array}{r} 3.4 \\ 15 \end{array} \begin{array}{r} 5.1 \\ 19 \end{array} \begin{array}{r} 3 \times \\ 5.0 \\ 15 \end{array} \begin{array}{r} 4.7 \\ 25 \end{array} \begin{array}{r} 2.7 \\ 28 \end{array} \begin{array}{r} 2.1 \\ 33 \end{array}$$

$$\begin{array}{r} 5.4 \\ 33 \end{array} \begin{array}{r} 4.9 \\ 27 \end{array} \begin{array}{r} 7.7 \\ 23 \end{array} \begin{array}{r} 7.3 \\ 20 \end{array} \begin{array}{r} 0 \times \\ 5.6 \\ 15 \end{array} \begin{array}{r} 5.4 \\ 10.2 \end{array} \begin{array}{r} 6.0 \\ 15 \end{array} \begin{array}{r} 7.1 \\ 17 \end{array} \begin{array}{r} 4 \times \\ 7.2 \\ 15 \end{array} \begin{array}{r} 7.0 \\ 27 \end{array} \begin{array}{r} 4.6 \\ 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 33 \end{array} \begin{array}{r} 3.0 \\ 31 \end{array} \begin{array}{r} 7.2 \\ 24 \end{array} \begin{array}{r} 7.2 \\ 20 \end{array} \begin{array}{r} 9 \times \\ 5.2 \\ 15 \end{array} \begin{array}{r} 5.0 \\ 10.2 \end{array} \begin{array}{r} 5.1 \\ 13 \end{array} \begin{array}{r} 6.4 \\ 18 \end{array} \begin{array}{r} 6.2 \\ 23 \end{array} \begin{array}{r} 4 \times \\ 5.6 \\ 15 \end{array} \begin{array}{r} 3.1 \\ 33 \end{array}$$

Sta.	+	H. I.	-	Elev.	Gr. 189
		1014.49			
438				09.7	4.8
	+30			09.9	4.6
	+70			10.3	4.2
439				10.5	4.0
	+70			11.1	3.4
B.M.			6.57	1007.98	
440				11.3	3.2
		8.41	1020.14	2.74	1011.73
	+40			11.7	8.4
441				12.2	7.7
	+50			12.7	7.4
442				13.2	6.9
	+50			13.7	6.4
+43				14.2	5.9

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9	1.9	4.9	4	6.0	6.5	6.6	5.0	4.9	5.3	4.6	7.4	7.4	
33	30	27	4	-1.2	32	19	17	-0.1	15	2	-1.4	30	33

5.4	5.6	6.2	6.3	4.9	5.1	5.1	5.7	7.0	10.2	10.8
33	26	23	20	14	13	16	19	26	33	

8.4	8.0	0	7.2	7.2	5.0	5.2	6.1	8.5	10.3	4	10.4	10.8
33	24	3	-30	20	14	-1.0	16	22	25	2	-6.2	33

8.7	7.6	8	6.9	6.3	5.0	5.0	5.9	10.4	2	1.1	11.6
33	25	2	-29	18	14	7.0	17	26	2	-7.1	33

6.0	6.1	4	4.6	4.2	3.8	4.5	8.0	2	10.0	10.3
33	25	1	7.2	14	-0.4	16	29	2	-6.6	33

1.7	1.7	5.3	5.3	4	3.4	3.2	0	3.7	9.0	10.1
33	29	25	19	0	-0.2	0.0	1	-0.5	28	33

5.4	4.9	10.3	10.3	8	8.8	8.6	8.4	8.7	2	6.1	11.1	11.1	12.4
33	27	23	20	1	-0.4	13	0.0	14	1	-2.1	21	28	33

3	2.7	8.5	8.7	9.6	9.4	8.1	7.9	8.2	9.3	9.7	8.5	0.5	1.0	
3	7.8	26	21	20	18	14	0.0	15	18	21	26	3	14.7	35

10.5	9.1	0	8.9	8.9	7.8	7.4	7.8	9.0	8.0	0.2	2.4	2.4
33	24	1	-13	17	14	0.0	14	18	27	3	7.5	35

3	0.8	8.6	6.8	7.1	6.8	7.1	8.1	8.3	7.5	0.5	5.8	5.8
3	-1.9	17	14	11	10.1	14	17	25	30	3	4.1	35

3	0.7	6.6	7.9	7.6	6.2	6.4	6.2	6.5	7.5	7.5	6.8	0.3	3.9	4.0
3	-0.7	24	24	18	15	11	10.2	13	18	23	27	3	7.5	35

3	0.7	4.5	7.0	7.1	5.7	5.7	6.0	7.0	7.1	6.5	0.2	2.4	2.4
3	7.1	27	24	20	14	10.2	14	18	22	28	3	7.5	35

Sta.	+	H. I.	-	Elev.	Gr. No.
		1020.14			
	+32			14.5	5.6
	+60			14.8	5.5
444				15.4	4.7
	8.32	1023.40	5.04	1015.08	
	+50			16.4	7.0
445				17.7	5.7
	+50			19.3	4.1
	+77			20.3	3.1
T.P.	10.22	1031.87	1.75	1021.65	
446				21.1	10.8
	+50			22.9	9.0
447				24.7	7.2
	+50			26.5	5.4
448				28.1	3.8
T.P.	10.10	1040.02	1.75	1029.92	

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(5.6)

$\frac{2.0}{33}$	$\frac{2.0}{28}$	$\frac{6.2}{21}$	$\frac{5.2}{17}$	$\frac{5.5}{12}$	$\frac{5.3}{-}$	$\frac{5.7}{15}$	$\frac{6.7}{18}$	$\frac{6.9}{24}$	$\frac{6.2}{28}$	$\frac{1.7}{34}$
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$\frac{4.8}{35}$	$\frac{0}{5}$	$\frac{4.8}{10.5}$	$\frac{5.0}{27}$	$\frac{6.4}{24}$	$\frac{6.3}{18}$	$\frac{4.9}{15}$	$\frac{5.0}{10.5}$	$\frac{0}{5}$	$\frac{5.3}{00}$	$\frac{6.0}{19}$	$\frac{6.4}{29}$	$\frac{0}{3}$	$\frac{7.0}{-1.7}$	$\frac{7.2}{35}$
------------------	---------------	--------------------	------------------	------------------	------------------	------------------	--------------------	---------------	------------------	------------------	------------------	---------------	--------------------	------------------

$\frac{9.7}{35}$	$\frac{9.7}{28}$	$\frac{8.7}{23}$	$\frac{0}{9}$	$\frac{5.7}{-1.0}$	$\frac{4.8}{-0.1}$	$\frac{0}{6}$	$\frac{4.7}{-0.5}$	$\frac{5.2}{17}$	$\frac{9.3}{25}$	$\frac{10.0}{28}$	$\frac{10.2}{33}$
------------------	------------------	------------------	---------------	--------------------	--------------------	---------------	--------------------	------------------	------------------	-------------------	-------------------

$\frac{13.0}{33}$	$\frac{12.7}{28}$	$\frac{0}{4}$	$\frac{12.4}{-5.4}$	$\frac{12.3}{24}$	$\frac{8.1}{16}$	$\frac{7.7}{12}$	$\frac{7.5}{-0.5}$	$\frac{7.7}{14}$	$\frac{0}{7}$	$\frac{8.5}{-1.3}$	$\frac{12.6}{26}$	$\frac{13.8}{33}$
-------------------	-------------------	---------------	---------------------	-------------------	------------------	------------------	--------------------	------------------	---------------	--------------------	-------------------	-------------------

$\frac{12.4}{33}$	$\frac{12.2}{28}$	$\frac{6.9}{18}$	$\frac{0}{5}$	$\frac{6.1}{-0.4}$	$\frac{6.2}{11}$	$\frac{5.8}{-0.1}$	$\frac{0}{6}$	$\frac{6.5}{-0.2}$	$\frac{12.5}{27}$	$\frac{13.1}{33}$
-------------------	-------------------	------------------	---------------	--------------------	------------------	--------------------	---------------	--------------------	-------------------	-------------------

$\frac{9.5}{33}$	$\frac{9.9}{27}$	$\frac{0}{6}$	$\frac{4.1}{00}$	$\frac{5.7}{11}$	$\frac{4.1}{10}$	$\frac{5.8}{10.3}$	$\frac{4.5}{12}$	$\frac{5.8}{13}$	$\frac{0}{7}$	$\frac{4.1}{00}$	$\frac{4.5}{18}$	$\frac{10.1}{27}$	$\frac{10.4}{33}$
------------------	------------------	---------------	------------------	------------------	------------------	--------------------	------------------	------------------	---------------	------------------	------------------	-------------------	-------------------

$\frac{5.5}{33}$	$\frac{5.0}{28}$	$\frac{4.8}{19}$	$\frac{2.9}{13}$	$\frac{2.7}{11}$	$\frac{3.1}{10}$	$\frac{2.6}{10.5}$	$\frac{3.0}{12}$	$\frac{2.7}{13}$	$\frac{2.7}{17}$	$\frac{4.0}{21}$	$\frac{4.2}{27}$	$\frac{0}{3}$	$\frac{3.5}{-0.7}$	$\frac{3.5}{33}$
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$\frac{5.9}{35}$	$\frac{0}{3}$	$\frac{5.4}{15.4}$	$\frac{5.0}{30}$	$\frac{11.1}{23}$	$\frac{12.3}{17}$	$\frac{10.8}{13}$	$\frac{10.2}{10.4}$	$\frac{10.6}{12}$	$\frac{10.3}{15}$	$\frac{11.3}{20}$	$\frac{10.9}{25}$	$\frac{0}{3}$	$\frac{3.7}{17.0}$	$\frac{2.8}{34}$	$\frac{2.8}{35}$
------------------	---------------	--------------------	------------------	-------------------	-------------------	-------------------	---------------------	-------------------	-------------------	-------------------	-------------------	---------------	--------------------	------------------	------------------

$\frac{5.4}{35}$	$\frac{0}{6}$	$\frac{5.4}{13.6}$	$\frac{5.2}{27}$	$\frac{9.9}{23}$	$\frac{10.3}{17}$	$\frac{7.0}{14}$	$\frac{8.7}{10.3}$	$\frac{9.0}{17}$	$\frac{9.9}{21}$	$\frac{2.7}{29}$	$\frac{0}{3}$	$\frac{6.1}{12.9}$	$\frac{4.3}{34}$	$\frac{4.3}{35}$
------------------	---------------	--------------------	------------------	------------------	-------------------	------------------	--------------------	------------------	------------------	------------------	---------------	--------------------	------------------	------------------

$\frac{5.2}{33}$	$\frac{0}{3}$	$\frac{5.3}{17.7}$	$\frac{5.4}{22}$	$\frac{8.1}{25}$	$\frac{8.7}{17}$	$\frac{7.0}{13}$	$\frac{7.4}{10}$	$\frac{6.9}{10.3}$	$\frac{0}{6}$	$\frac{7.2}{00}$	$\frac{7.4}{14}$	$\frac{8.4}{20}$	$\frac{8.2}{24}$	$\frac{0}{3}$	$\frac{8.1}{-0.9}$	$\frac{8.1}{35}$
------------------	---------------	--------------------	------------------	------------------	------------------	------------------	------------------	--------------------	---------------	------------------	------------------	------------------	------------------	---------------	--------------------	------------------

$\frac{0}{2}$	$\frac{2.4}{13.0}$	$\frac{2.5}{29}$	$\frac{6.7}{23}$	$\frac{7.0}{16}$	$\frac{5.2}{12}$	$\frac{5.1}{11}$	$\frac{5.5}{9}$	$\frac{5.1}{10.3}$	$\frac{5.6}{12}$	$\frac{5.3}{13}$	$\frac{5.3}{14}$	$\frac{0}{6}$	$\frac{3.4}{01}$	$\frac{7.2}{20}$	$\frac{7.4}{26}$	$\frac{8.3}{33}$
---------------	--------------------	------------------	------------------	------------------	------------------	------------------	-----------------	--------------------	------------------	------------------	------------------	---------------	------------------	------------------	------------------	------------------

$\frac{3.8}{19}$	$\frac{4.3}{15}$	$\frac{3.4}{12}$	$\frac{3.3}{10}$	$\frac{3.7}{9}$	$\frac{3.4}{10.4}$	$\frac{3.7}{14}$	$\frac{4.0}{17}$	$\frac{5.2}{19}$	$\frac{5.7}{24}$	$\frac{6.2}{33}$	$\frac{6.5}{35}$
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Sta.	+	M. I.	-	Elev.	Gr. M.
		1040.02			
	+50			29.8	10.2
449				31.3	8.7
	+45			32.6	7.4
450				33.7	6.3
B.M.			6.91	1033.11	
	+46 <sup>8</sup>			34.5	5.5
	+70			34.7	5.3
B.M.	12.35	1046.48	5.89	1034.13	
448				28.1	18.9
	+50			29.8	16.2
449.				31.3	15.7
B.M.			12.35	1034.13	

6-3-27

5.1	8.0	10.9	11.0	10.2	10.2	10.6	10.3	10.5	11.2	11.7	8.9	8.9
<u>29</u>	<u>24</u>	<u>20</u>	<u>15</u>	<u>12</u>	<u>20</u>	<u>12</u>	<u>14</u>	<u>14</u>	<u>17</u>	<u>24</u>	<u>31</u>	<u>115</u>

9.2	10.0	9.1	8.8	9.1	9.8	9.0	1.9	2.0	1.9	1.9
<u>20</u>	<u>16</u>	<u>13</u>	<u>0.1</u>	<u>15</u>	<u>18</u>	<u>23</u>	<u>31</u>	<u>3</u>	<u>16.8</u>	<u>35</u>

7.0	8.0	6.2	9.2	9.3	7.7	7.6	7.9	8.7	8.2	5.8	8.0	5.1		
<u>35</u>	<u>3</u>	<u>10.4</u>	<u>27</u>	<u>22</u>	<u>17</u>	<u>13</u>	<u>-0.2</u>	<u>16</u>	<u>20</u>	<u>27</u>	<u>32</u>	<u>3</u>	<u>718</u>	<u>35</u>

6.2	8.0	6.1	8.1	8.2	9.0	6.5	6.7	8.0	6.8	
<u>35</u>	<u>5</u>	<u>10.2</u>	<u>23</u>	<u>22</u>	<u>18</u>	<u>16</u>	<u>-0.2</u>	<u>19</u>	<u>3</u>	<u>-0.5</u>

Spk. in T.P. Lt. 5 ft. 450 + 25

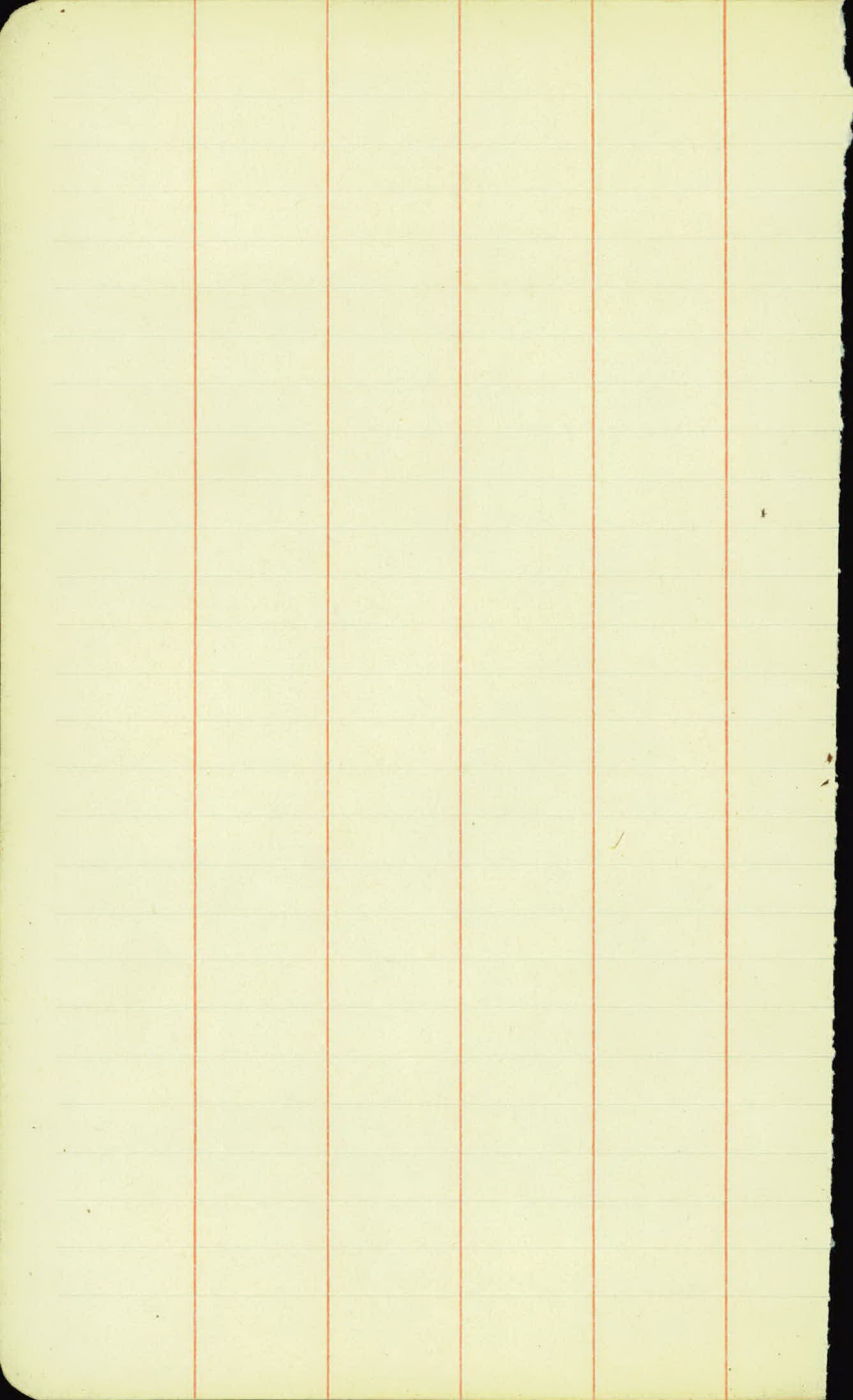
4.4	4.8	5.1	5.4	5.6
<u>33</u>	<u>15</u>		<u>15</u>	<u>33</u>

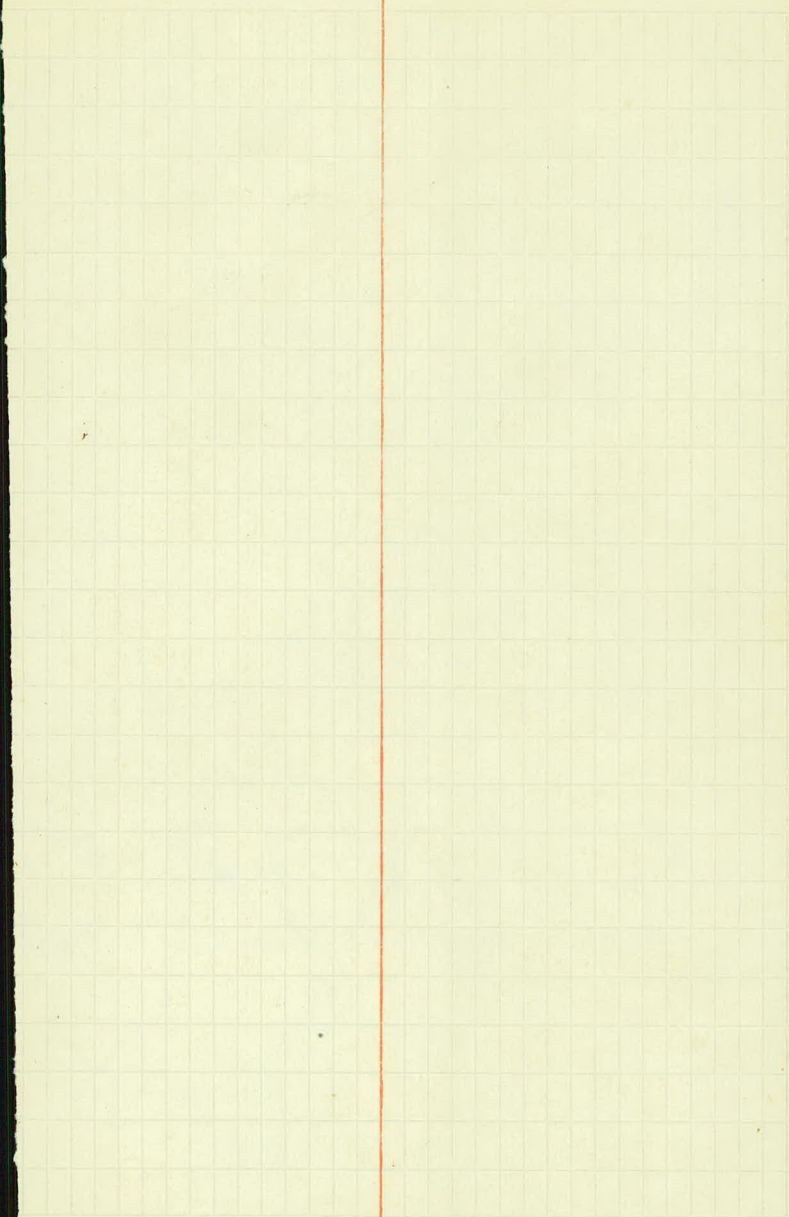
4.9	4.9	4.8	5.2	5.8	3.9	3.8
<u>33</u>	<u>17</u>		<u>15</u>	<u>24</u>	<u>31</u>	<u>33</u>

7.7	8.0	8.5	
<u>495</u>	<u>3</u>	<u>194</u>	<u>30</u>

1.7	8.0	2.9	2.3	
<u>495</u>	<u>4</u>	<u>1148</u>	<u>41</u>	<u>39</u>

5.2	7.0	6.6	5.8	6.4	
<u>495</u>	<u>8</u>	<u>186</u>	<u>36</u>	<u>33</u>	<u>30</u>





Sta.	+	H.I.	-	Elev.
B.M.	9.50	1004.94		995.44 ✓
0+33				01.1
				04.0
0+50				
	7.33	1013.75	0.52	1004.42
0+33				
0+50				
0+75				04.0
1+00				05.5
1+25				07.0
1+50				08.4
1+75				08.6
	1.40	1005.82	9.33	1004.42
2+00			10.51	995.44 ✓

17

18

Sp. N. in P.P. 65 Lt. Sta. 578+85.

57	54	40	3.7
23	9	3.8	12
			21

Road 21 L.

56	28	08	25	2.7	30	1.4
33	19	4	0.9	4	12	19
						23

Road 14 L.

12.6

5.6	5.5
33	43

9.8

5.5	4.9
32	42

104	107	109	101	100	103	7.4	4.2
35	27	19	11	9.8	12	22	31
							40

Road 8 L.

104	96	88	81	8.8	8.8	4.2	5.5
33	24	10	8.3	9	18	22	30
							38

Road 1 L.

105	86	73	71	64	6.6	6.6	2.8	3.3
33	20	12	4	6.8	7	17	25	30
								35

Road 5 R.

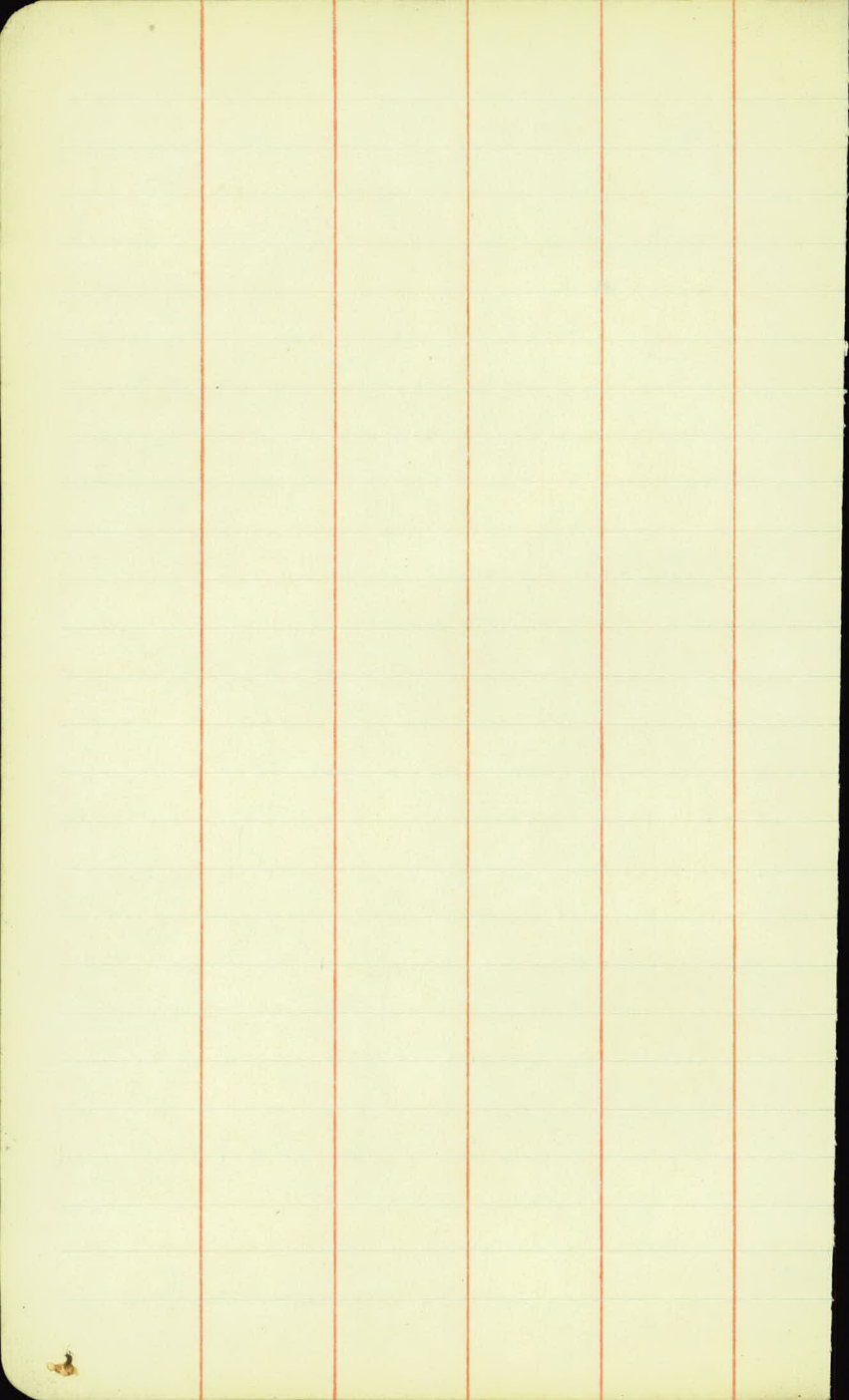
8.9	7.9	6.1	5.0	5.2	2.8
33	20	7	5.4	14	29
					39

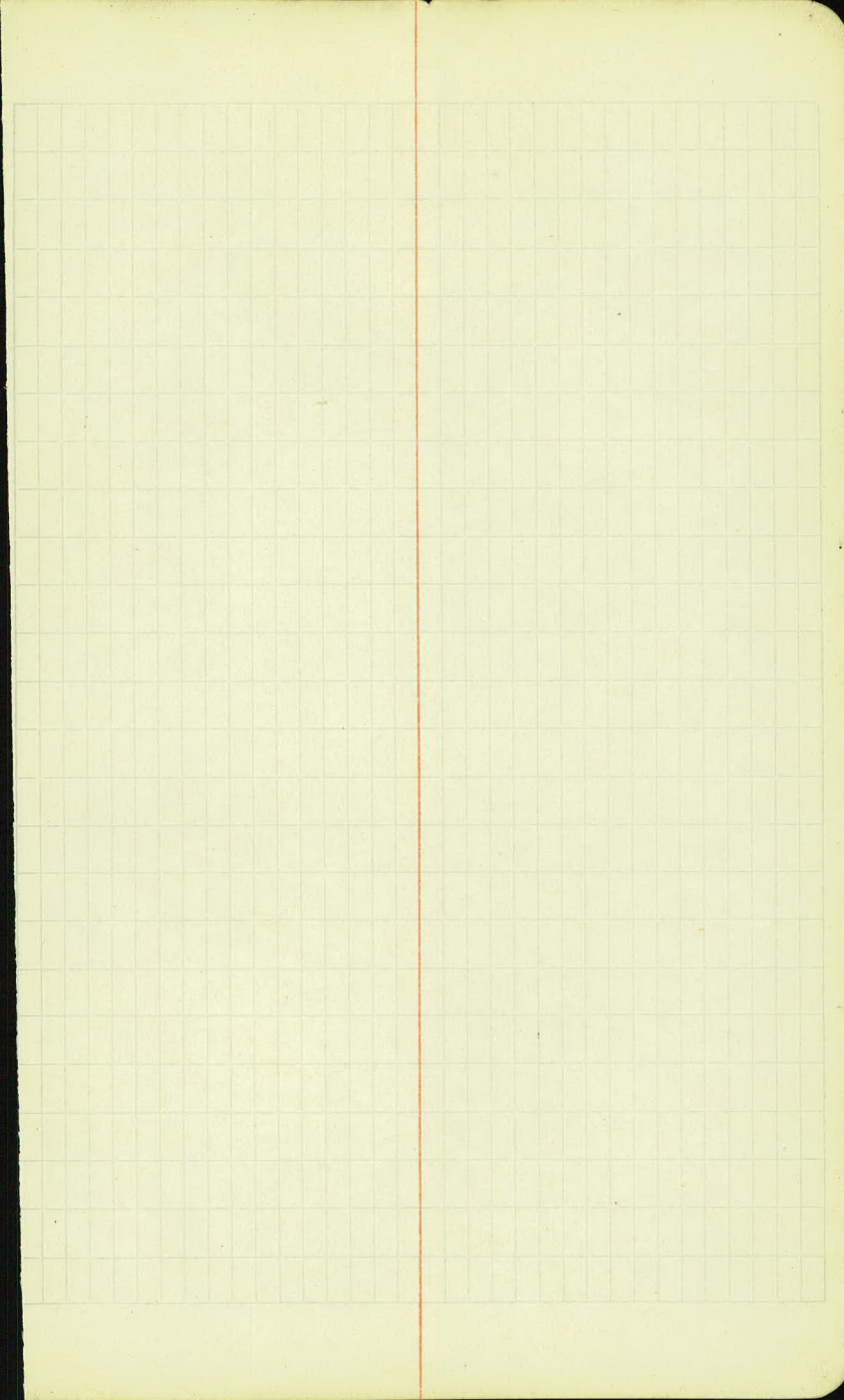
Road 15 R.

8.8	7.3	6.0	4.7	4.8	4.3	4.3	4.0
33	18	8	5.2	10	19	26	30
							50

Road 29 R.

Road 40 R.





	Cross Drains	Elev. Lt.	Elev. Rt.
384738	24" X 48' P <sup>2</sup>	24 989.67	24 989.47
390751	24" X 42' P <sup>3</sup>	21.5 989.28	20.5 989.68
394706	24" X 42' P <sup>2</sup>	21.5 988.00	20.5 988.40
397782	24" X 48' P <sup>2</sup>	24.3 985.30	23.7 985.50
409747	24" X 60' P <sup>3</sup>		
427748	24" X		
444727	<sup>56</sup> 24" X 54' P <sup>3</sup>	27 1007.29	27 1007.79
457775	24" X 54' P <sup>2</sup>	28 1022.14	26 1024.56
466700	24" X 60' P <sup>3</sup>	34 1017.00	32 1018.20
479772	24" X 72' P <sup>2</sup>	1028.38	1035.88

85.47 Intake Co. Rd. C.

Inlet of Co. Rd. C.

84.9	85.4	85.5	Elev. in	Bottom of Pitah	
<u>200</u>	<u>100</u>	<u>50</u>	<u>85.8</u>	<u>85.5</u>	<u>85.1</u>
			<u>00</u>	<u>0.0</u>	<u>50</u>

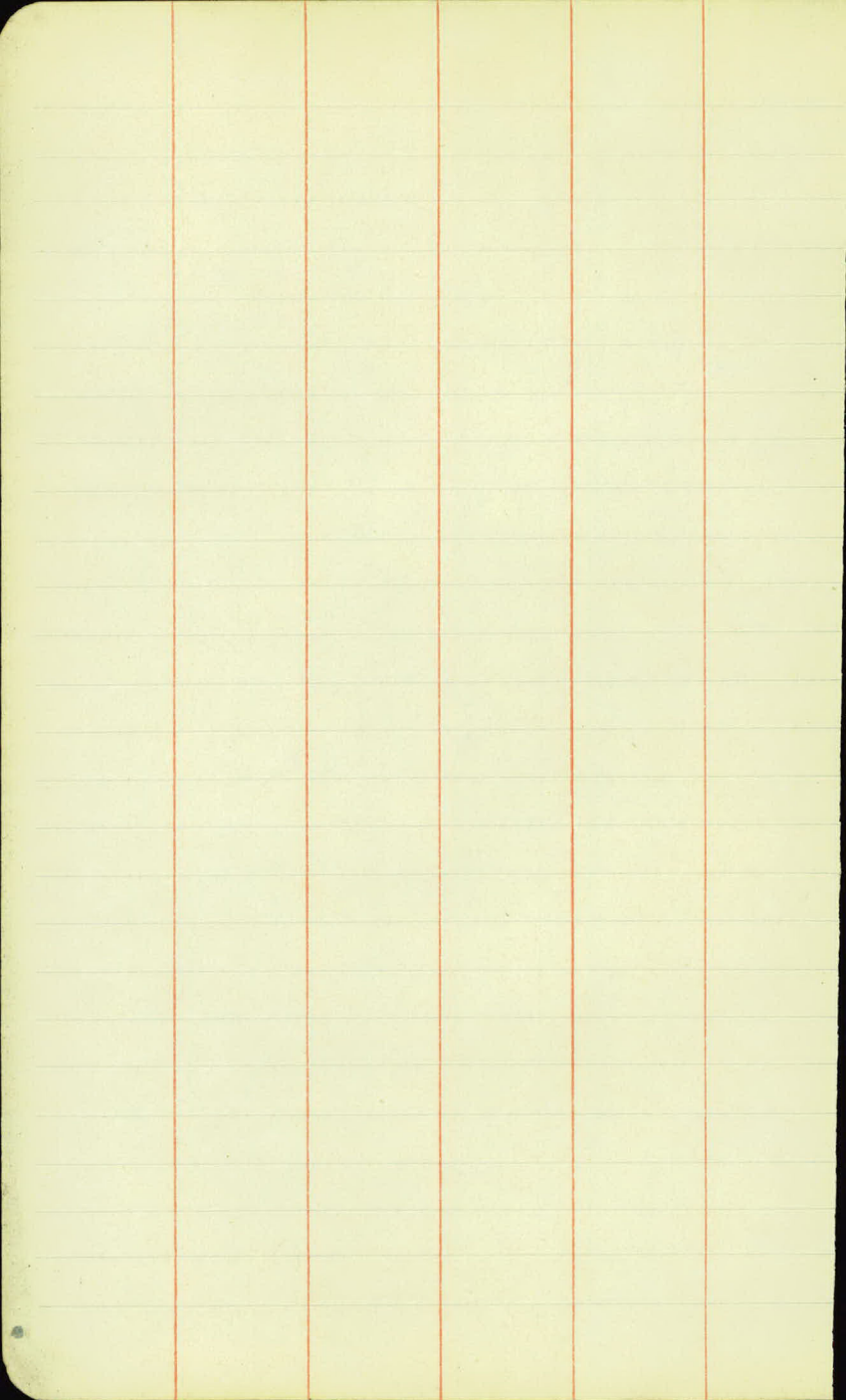
85.42

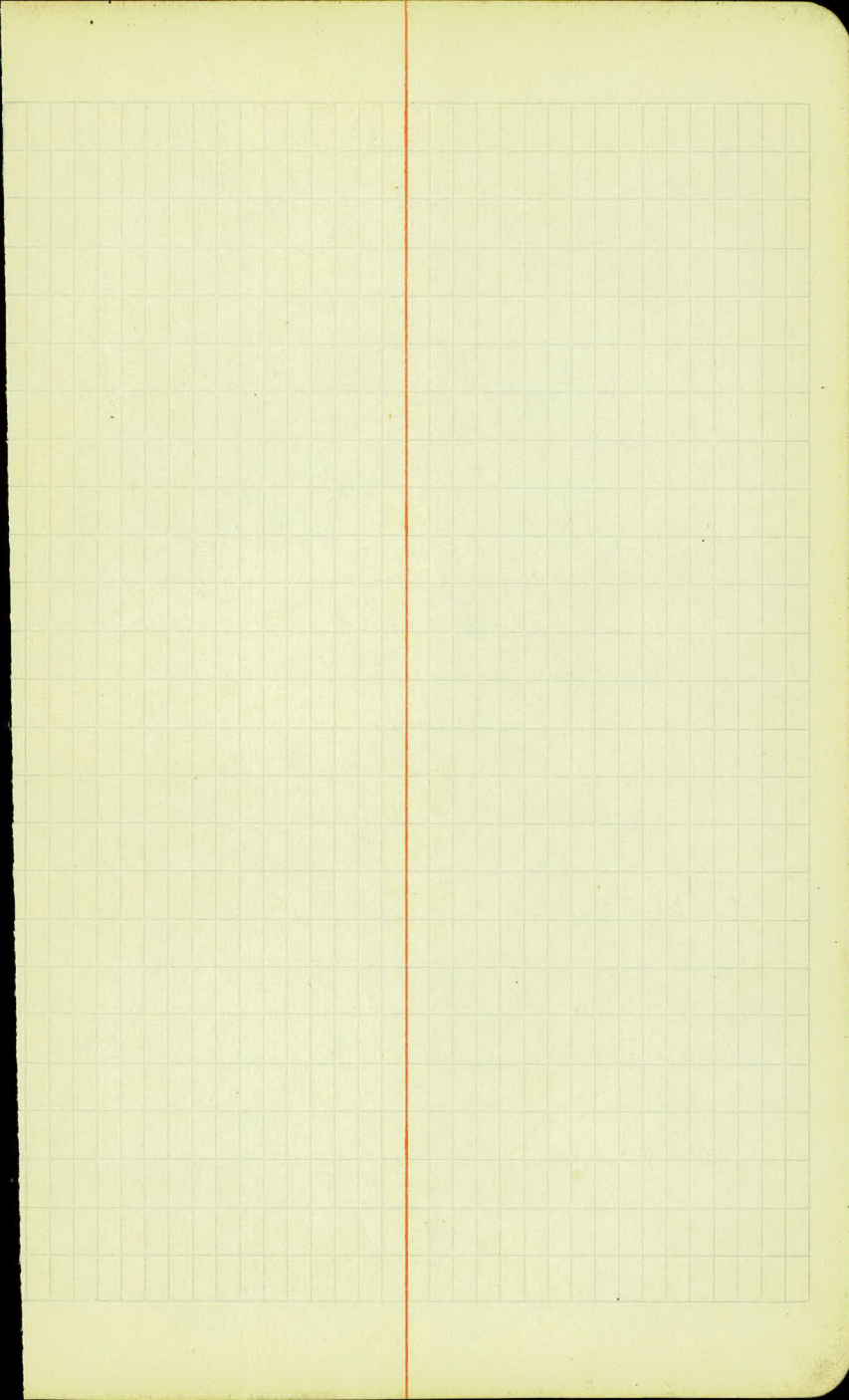
85.42 Bottom of Old Cuts.

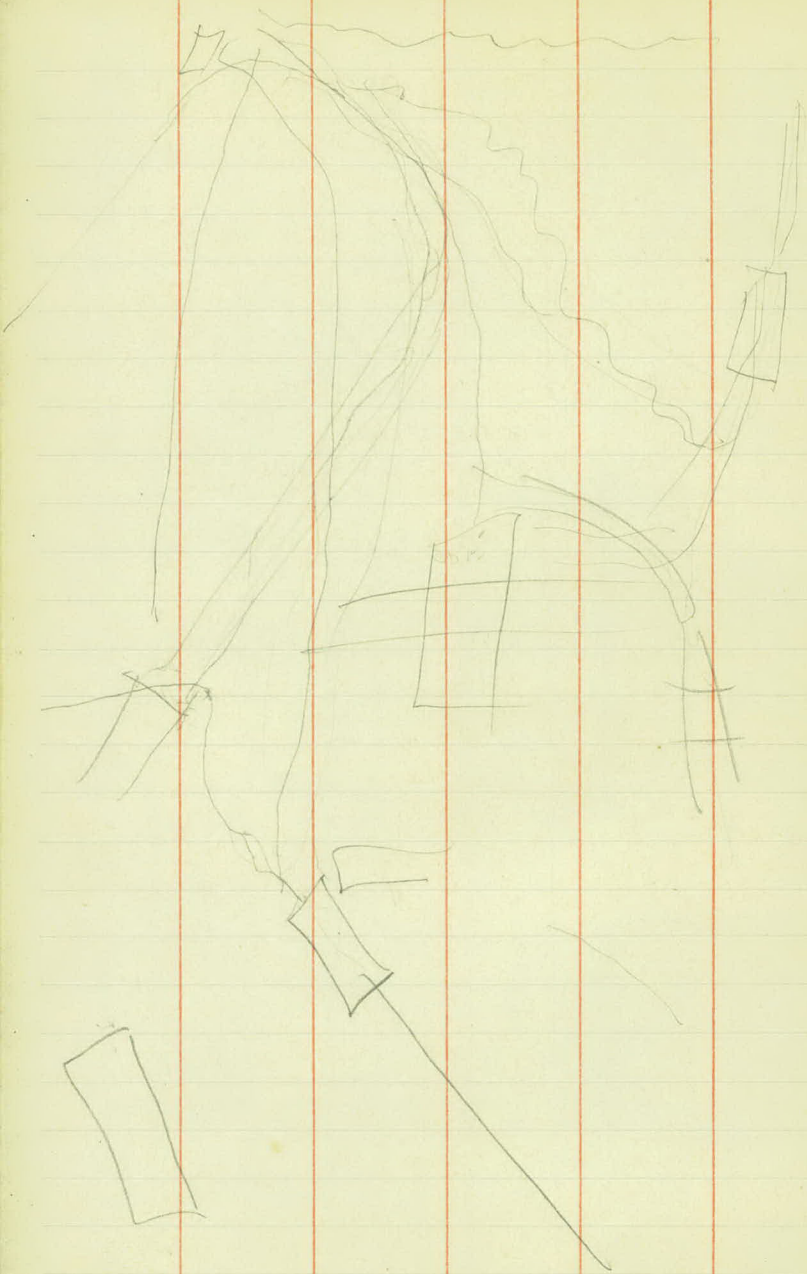
88.24 = Till Drain

87.0 Low spot on Mt.

88.54 Intake of S Drain







# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or I. P.= $23^{\circ} 20'$  to the R. at Station  
542+72.

Ext. in Tab. IV opposite  $23^{\circ} 20'$ =120.87  
 $120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20'$ =1183.1  
 $1183.1 \div 10 = 118.31$ .

Tab. V. correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur.=0.16  
 $118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)  
Ang.  $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 = \text{L. C.}$

$2^{\circ} 19\frac{1}{2}' = \text{def. for sta.}$	542	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}' = \text{ " " "}$	+50	Tan.=	118.47
$7^{\circ} 19\frac{1}{2}' = \text{ " " "}$	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' = \text{ " " "}$	+50	L. C.=	2.33.33
$11^{\circ} 40' = \text{ " " "}$	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3$  (def. for 1 ft. of  $10^{\circ}$  Cur.)= $139.41' =$   
 $2^{\circ} 19\frac{1}{2}'' = \text{def. for sta. 542.}$

Def. for 50 ft.= $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)

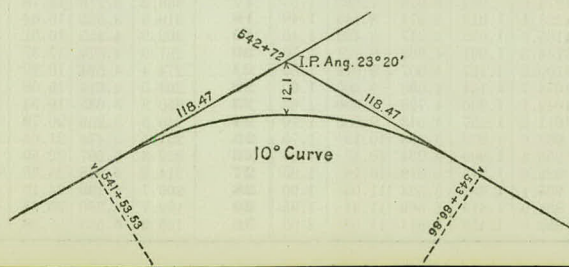


TABLE I. — Minutes in Decimals of a Degree.

<b>1</b>	.0167	<b>11</b>	.1833	<b>21</b>	.3500	<b>31</b>	.5167	<b>41</b>	.6833	<b>51</b>	.8500
<b>2</b>	.0333	<b>12</b>	.2000	<b>22</b>	.3667	<b>32</b>	.5333	<b>42</b>	.7000	<b>52</b>	.8667
<b>3</b>	.0500	<b>13</b>	.2167	<b>23</b>	.3833	<b>33</b>	.5500	<b>43</b>	.7167	<b>53</b>	.8833
<b>4</b>	.0667	<b>14</b>	.2333	<b>24</b>	.4000	<b>34</b>	.5667	<b>44</b>	.7333	<b>54</b>	.9000
<b>5</b>	.0833	<b>15</b>	.2500	<b>25</b>	.4167	<b>35</b>	.5833	<b>45</b>	.7500	<b>55</b>	.9167
<b>6</b>	.1000	<b>16</b>	.2667	<b>26</b>	.4333	<b>36</b>	.6000	<b>46</b>	.7667	<b>56</b>	.9333
<b>7</b>	.1167	<b>17</b>	.2833	<b>27</b>	.4500	<b>37</b>	.6167	<b>47</b>	.7833	<b>57</b>	.9500
<b>8</b>	.1333	<b>18</b>	.3000	<b>28</b>	.4667	<b>38</b>	.6333	<b>48</b>	.8000	<b>58</b>	.9667
<b>9</b>	.1500	<b>19</b>	.3167	<b>29</b>	.4833	<b>39</b>	.6500	<b>49</b>	.8167	<b>59</b>	.9833
<b>10</b>	.1667	<b>20</b>	.3333	<b>30</b>	.5000	<b>40</b>	.6667	<b>50</b>	.8333	<b>60</b>	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	1/8	3-16	1/4	5-16	3/8	1/2	5/8	3/4	7/8
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	
<b>0°</b>	10'	34377.	.036	.145	.291	0.05'	<b>7°</b>	819.0	1.528	6.105	12.21	2.10
	20'	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
	30'	11459.	.109	.436	.873	0.15	30'	764.5	1.637	6.540	13.08	2.25
	40'	8594.4	.145	.582	1.164	0.20	40'	747.9	1.673	6.685	13.37	2.30
	50'	6875.5	.182	.727	1.454	0.25	<b>8</b>	716.8	1.746	6.976	13.95	2.40
<b>1</b>	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50	
	10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
	20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
	30	3819.8	.327	1.309	2.618	0.45	<b>9</b>	637.3	1.965	7.846	15.69	2.70
	40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
	50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
<b>2</b>	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90	
	10	2644.6	.473	1.891	3.781	0.65	<b>10</b>	573.7	2.183	8.716	17.43	3.00
	20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
	30	2292.0	.545	2.181	4.363	0.75	<b>11</b>	521.7	2.402	9.585	19.16	3.30
	40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
	50	2022.4	.618	2.472	4.945	0.85	<b>12</b>	478.3	2.620	10.45	20.91	3.60
<b>3</b>	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75	
	10	1809.6	.691	2.763	5.526	0.95	<b>13</b>	441.7	2.839	11.32	22.64	3.90
	20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
	30	1637.3	.764	3.054	6.108	1.05	<b>14</b>	410.3	3.058	12.18	24.37	4.20
	40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
	50	1495.0	.836	3.345	6.689	1.15	<b>15</b>	383.1	3.277	13.05	26.11	4.50
<b>4</b>	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65	
	10	1375.4	.909	3.635	7.271	1.25	<b>16</b>	359.3	3.496	13.92	27.84	4.80
	20	1322.5	.945	3.718	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
	30	1273.6	.982	3.826	7.852	1.35	<b>17</b>	338.3	3.716	14.78	29.56	5.10
	40	1228.1	1.018	4.071	8.143	1.40	<b>18</b>	319.6	3.935	15.64	31.29	5.40
	50	1185.8	1.055	4.217	8.433	1.45	<b>19</b>	302.9	4.155	16.51	33.01	5.70
<b>5</b>	1146.3	1.091	4.362	8.724	1.50	<b>20</b>	287.9	4.374	17.37	34.73	6.00	
	10	1109.3	1.127	4.507	9.014	1.55	<b>21</b>	274.4	4.594	18.22	36.44	6.30
	20	1074.7	1.164	4.653	9.305	1.60	<b>22</b>	262.0	4.814	19.08	38.16	6.63
	30	1042.1	1.200	4.798	9.596	1.65	<b>23</b>	250.8	5.035	19.94	39.87	6.90
	40	1011.5	1.237	4.943	9.886	1.70	<b>24</b>	240.5	5.255	20.79	41.58	7.20
	50	982.6	1.273	5.088	10.18	1.75	<b>25</b>	231.0	5.476	21.64	43.28	7.50
<b>6</b>	955.4	1.309	5.234	10.47	1.80	<b>26</b>	222.3	5.697	22.50	44.99	7.80	
	10	929.6	1.346	5.379	10.76	1.85	<b>27</b>	214.2	5.918	23.35	46.69	8.10
	20	905.1	1.382	5.524	11.05	1.90	<b>28</b>	206.7	6.139	24.19	48.38	8.40
	30	881.9	1.418	5.669	11.34	1.95	<b>29</b>	199.7	6.360	25.04	50.07	8.70
	40	859.9	1.455	5.814	11.63	2.00	<b>30</b>	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>1°</b>	50.00	.22	<b>11°</b>	551.70	26.50	<b>21°</b>	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
<b>2</b>	100.01	.87	<b>12</b>	602.21	31.56	<b>22</b>	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
<b>3</b>	150.04	1.96	<b>13</b>	652.81	37.07	<b>23</b>	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
<b>4</b>	200.08	3.49	<b>14</b>	703.51	43.03	<b>24</b>	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
<b>5</b>	250.16	5.46	<b>15</b>	754.32	49.44	<b>25</b>	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
<b>6</b>	300.28	7.86	<b>16</b>	805.25	56.31	<b>26</b>	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
<b>7</b>	350.44	10.71	<b>17</b>	856.30	63.63	<b>27</b>	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
<b>8</b>	400.66	13.99	<b>18</b>	907.49	71.42	<b>28</b>	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
<b>9</b>	450.93	17.72	<b>19</b>	958.81	79.67	<b>29</b>	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
<b>10</b>	501.28	21.89	<b>20</b>	1010.3	88.39	<b>30</b>	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>31°</b>	1589.0	216.3	<b>41°</b>	2142.2	387.4	<b>51°</b>	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
<b>32</b>	1643.0	230.9	<b>42</b>	2199.4	407.6	<b>52</b>	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
<b>33</b>	1697.2	246.1	<b>43</b>	2257.0	428.5	<b>53</b>	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
<b>34</b>	1751.7	261.8	<b>44</b>	2314.9	450.0	<b>54</b>	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
<b>35</b>	1806.6	278.1	<b>45</b>	2373.3	472.1	<b>55</b>	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.3	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
<b>36</b>	1861.7	294.9	<b>46</b>	2432.1	494.8	<b>56</b>	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
<b>37</b>	1917.1	312.2	<b>47</b>	2491.3	518.2	<b>57</b>	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
<b>38</b>	1972.9	330.2	<b>48</b>	2551.0	542.2	<b>58</b>	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
<b>39</b>	2029.0	348.6	<b>49</b>	2611.2	566.9	<b>59</b>	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
<b>40</b>	2085.4	367.7	<b>50</b>	2671.8	592.3	<b>60</b>	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>61°</b>	3375.0	920.2	<b>71°</b>	4086.9	1308.2	<b>81°</b>	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
<b>62</b>	3442.7	954.8	<b>72</b>	4162.8	1352.6	<b>82</b>	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1916.7
<b>63</b>	3511.1	990.2	<b>73</b>	4239.7	1398.0	<b>83</b>	5069.2	1926.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1936.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1946.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1956.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1966.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1976.3
<b>64</b>	3580.3	1026.6	<b>74</b>	4317.6	1444.6	<b>84</b>	5159.0	1986.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1996.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2006.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2016.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2027.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2037.4
<b>65</b>	3650.2	1063.9	<b>75</b>	4396.5	1492.4	<b>85</b>	5250.3	2047.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2058.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2068.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2079.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2089.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2099.9
<b>66</b>	3720.9	1102.2	<b>76</b>	4476.5	1541.4	<b>86</b>	5343.0	2109.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2119.6
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2129.6
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2139.6
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2149.7
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2159.8
<b>67</b>	3792.4	1141.4	<b>77</b>	4557.6	1591.6	<b>87</b>	5437.2	2169.9
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2190.5
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2200.9
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2211.3
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2221.8
<b>68</b>	3864.7	1181.6	<b>78</b>	4639.8	1643.0	<b>88</b>	5533.1	2232.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2243.2
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2254.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2264.8
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2275.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2286.4
<b>69</b>	3937.9	1222.7	<b>79</b>	4723.2	1695.8	<b>89</b>	5630.5	2297.3
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2308.2
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2319.1
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2330.1
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2341.1
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2352.1
<b>70</b>	4011.9	1265.0	<b>80</b>	4807.7	1749.9	<b>90</b>	5729.7	2363.1
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2374.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2385.1
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2396.1
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2407.1
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2418.1

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>91°</b>	5830.5	2444.9	<b>101°</b>	6950.6	3278.1	<b>111°</b>	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
<b>92</b>	5933.2	2518.5	<b>102</b>	7075.5	3374.9	<b>112</b>	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
<b>93</b>	6037.8	2594.0	<b>103</b>	7203.2	3474.4	<b>113</b>	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
<b>94</b>	6144.3	2671.6	<b>104</b>	7333.6	3576.8	<b>114</b>	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
<b>95</b>	6252.8	2751.3	<b>105</b>	7467.0	3682.3	<b>115</b>	8992.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
<b>96</b>	6363.4	2833.2	<b>106</b>	7603.5	3791.0	<b>116</b>	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
<b>97</b>	6476.2	2917.3	<b>107</b>	7743.2	3902.9	<b>117</b>	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
<b>98</b>	6591.2	3003.8	<b>108</b>	7886.2	4018.2	<b>118</b>	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
<b>99</b>	6708.6	3092.7	<b>109</b>	8032.7	4137.1	<b>119</b>	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
<b>100</b>	6828.3	3184.1	<b>110</b>	8182.8	4259.7	<b>120</b>	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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For Tangents Add														
ANGLE	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

For Externals Add

ANGLE	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.045	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

## VIII

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

## CURVE FORMULAS.

$$T = R \tan \frac{1}{2} I$$

$$T = 50 \tan \frac{1}{2} I$$

$$\frac{\text{Sin. D}}{\text{Sin. D} = \frac{50}{R}}$$

$$\text{Sin. D} = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot \frac{1}{2} I$$

$$R = 50$$

$$\frac{\text{Sin. D}}{E = R \text{ ex. sec. } \frac{1}{2} I}$$

$$E = T \tan \frac{1}{4} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{\frac{1}{2} I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.—Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt. 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 = B^{\text{se}}$ .

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

## Natural Sines

DEG.	0'	10'	20'	30'	40'	50'	DEG.	0'	10'	20'	30'	40'	50'	DEG.	
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1279	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10

DEG.	60'	50'	40'	30'	20'	10'	DEG.	60'	50'	40'	30'	20'	10'	DEG.
80	9848	9853	9858	9863	9868	9872	9	9868	9872	9				
81	9877	9881	9886	9890	9894	9899	8	9894	9899	8				
82	9903	9907	9911	9914	9918	9922	7	9918	9922	7				
83	9925	9929	9932	9936	9939	9942	6	9939	9942	6				
84	9945	9948	9951	9954	9957	9959	5	9957	9959	5				
85	9962	9964	9967	9969	9971	9974	4	9971	9974	4				
86	9976	9978	9980	9981	9983	9985	3	9983	9985	3				
87	9986	9988	9989	9990	9992	9993	2	9992	9993	2				
88	9994	9995	9996	9997	9997	9998	1	9997	9998	1				
89	9998	9999	9999	9999	I.0000	I.0000	0	I.0000	I.0000	0				

DEG. 60' 50' 40' 30' 20' 10' DEG.

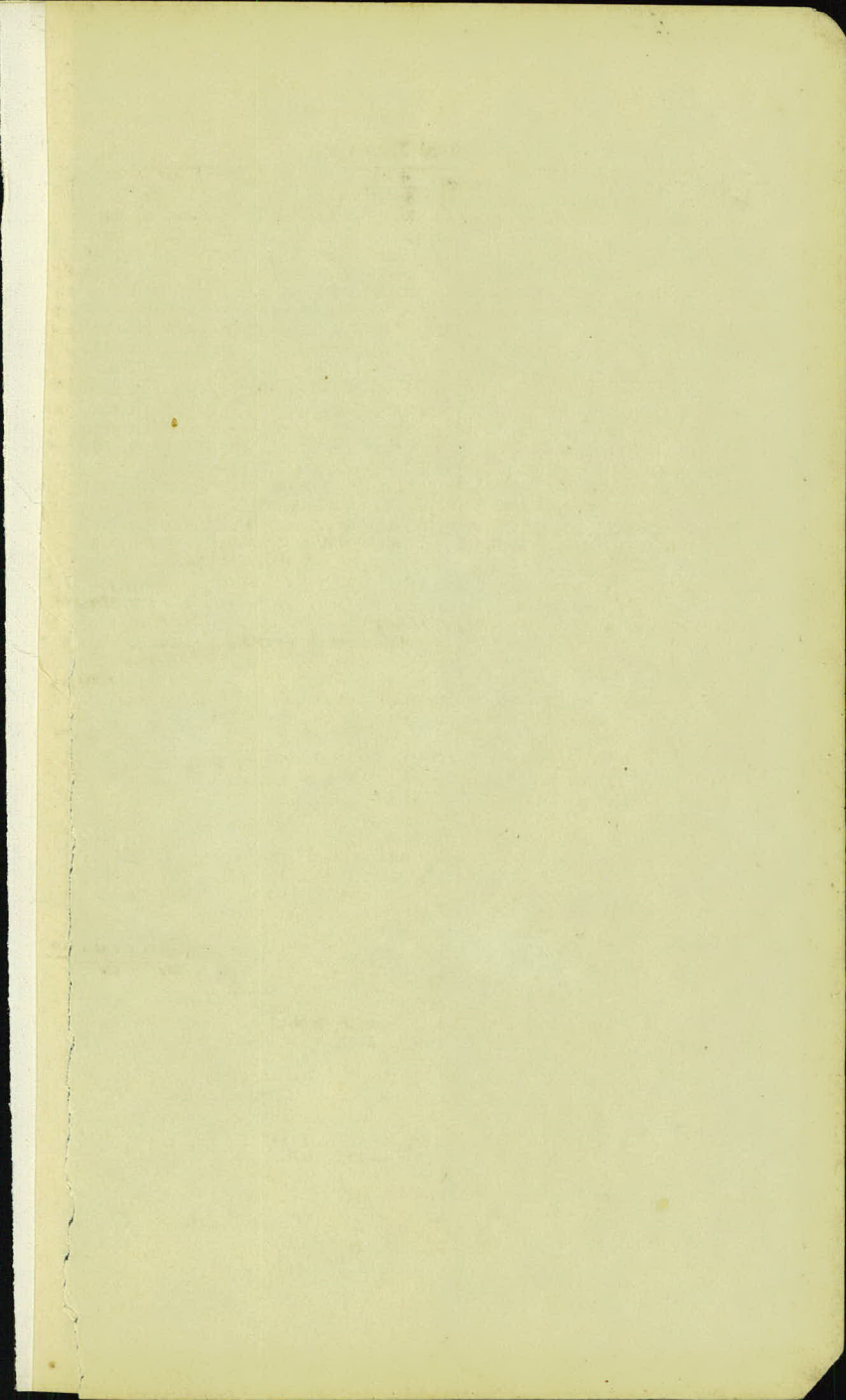
## Natural Cosines

Natural Tangents

deg.	0'	10'	20'	30'	40'	50'	deg.	0'	10'	20'	30'	40'	50'	deg.
0	0000	0029	0058	0087	0116	0145	89	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	1.3270	1.3351	1.3452	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733	34
16	2867	2899	2931	2962	2994	3026	73	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10

deg.	60'	50'	40'	30'	20'	10'	deg.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.865	343.770	0

Natural Cotangents



10000  
8926  

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1096

10000  
3079  

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6921

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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