

LINE REVISIONS

ANOKA CUTOFF

From
St. Paul
to

Anoka

RAMSEY CO. PROJ. 26-62

Road $\frac{1}{2}$ c N^o 93

FILE N^o 5

6-8-26

5

Anoka Connection

Line change

station 171+64.8 to 194+75.7

Station	Point	Lt. Δ	Rt.	Bear.
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194+75.7	P.T.	22°-05'		
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+50		20°-48'		
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194		18°-18'		
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+50		15°-48'		10°-C. Lt.
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193		13°-18'		Δ 44°-10'
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+50		10°-48'		P.T. 192+66.78
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192		8°-18'		T. 232.75'
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+50		5°-48'		L. 441.67'
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191		3°-18'		R. 573.69'
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+50		0°-48'		
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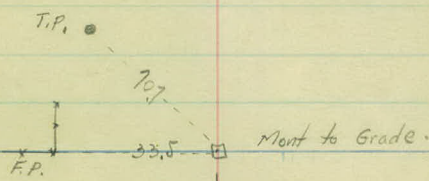
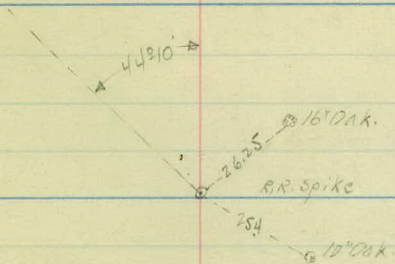
190+34 ⁰⁰	P.O.	0°-00'		
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171+64.8	P.I. Mount	0°-35'		
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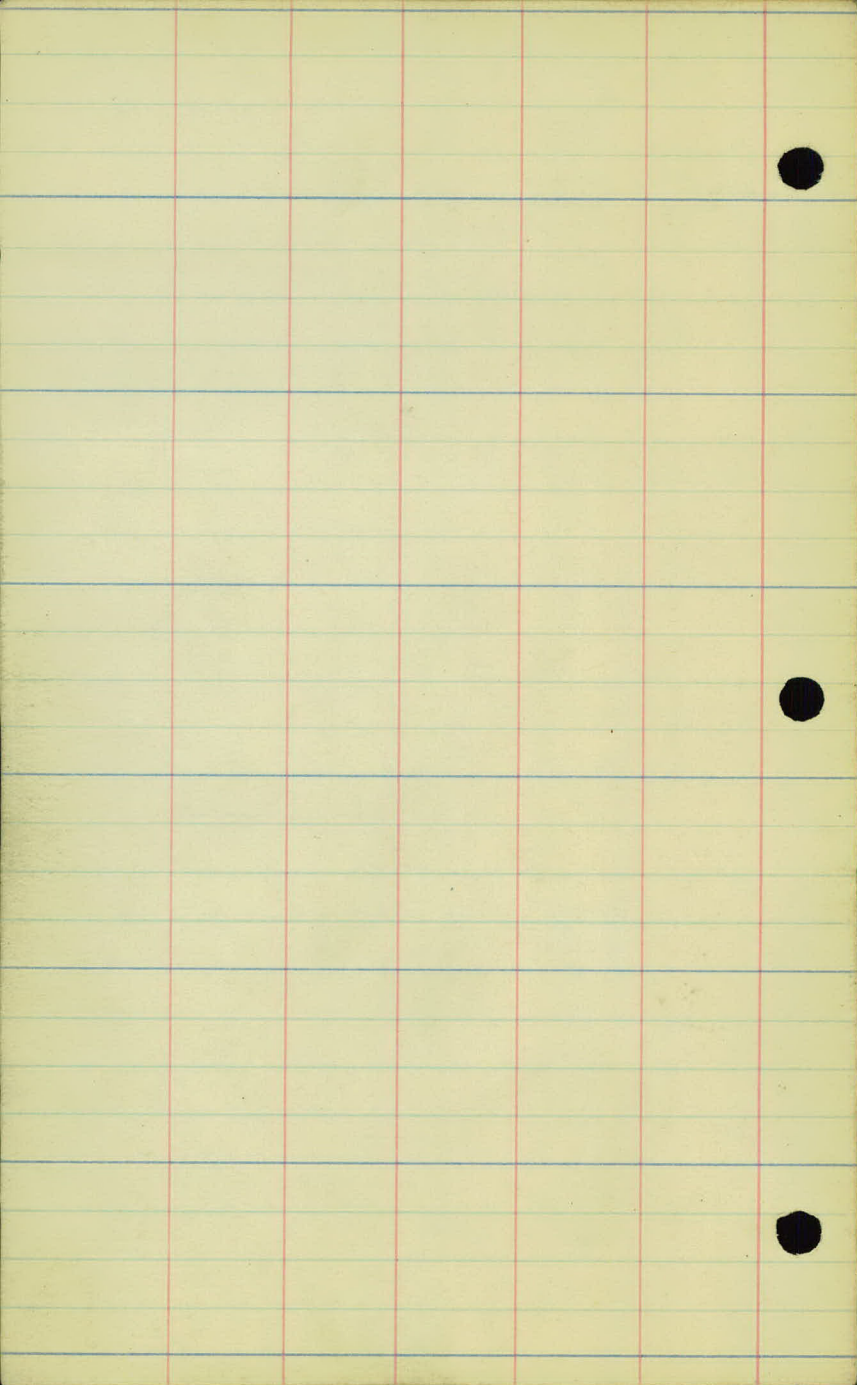
Mon.

TO R-24

W.H.C. 2
A.L.P.
M.G. Mar. 23, 1926
H.B.



Mont & Co. Rd "C"



Topography

Line change

Anoka Connection.

173

172

+73 - Field Ent Rt.

+64.8 Mont.

171

K-31'
 +95 - P.P. 16'
 +73 - 2" Tree 26'

shdr 12' 18'

+72 - 2" Tree 31'

+32 - 2" Tree 18'
 +11 - 16" Oak 34'
 +01 - P.P. 29'
 F-32'
 +46 - 2" Tree 29'

Pasture.

Cultivated

+40 - T.P. 18'
 +21 - 2" Tree 31'

+93 - 4" Tree 30'

+55 - 2" Tree 29'

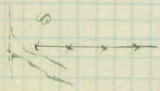
+55 - 2" Tree 30'

+32 - P.P. 18'

+14 - 2" Tree 30'

+15 - 2" Tree 30'

+82 - 4" Tree 30'
 +73 - F. Cor.
 +66 - F. Cor. 34'
 +65 - P.P.



+93 - T.P. 17'
 +32 - 4" Tree 30'
 +66 - FLITIC - 28' E.Y.W.

W.H.C.
 A.L.P.
 M.G.
 H.B.

Mar 23, 1926

180

179

178-

177

176

175

174

+92 - P.R. 20'

+10 - 2" Tree 20'

+34 - 3" Tree 20'
+16 - P.R. 12'

+58 - P.P. 21'

+23 - 3" Tree 22'
+09 - E.F. 25'

+84 - 2" Tree 22'
+53 - 2" Oak 35'
+52 - P.P. 13'
+46 - 2" Tree 22'
+34 - P.P. 22'

+01 - 4" Tree 23'
F-26

+63 - 4" Tree 24'

+23 - P.P. 14'
+19 - 2" Tree 24'
+03 - P.P. 24'
F-27

+81 - 2" Tree 24'

+40 - 3" Tree 25'
+08 - 1" Tree 25'
F-29'

+72 - P.P. 26'
+66 - 3" Tree 26'
+62 - P.P. 15'

+23 - 2" Tree 27'
F-30'

+88 - 2" Tree 28'

+49 - 4" Tree 27'
+35 - P.P. 27'

+07 - 4" Tree 28'

+74 - 3" Tree 37'
+73 - T.P. 23'

+85 - 3" Tree

+96 - 2" Tree

+59 - 2" Tree

+81 - T.P. 22'
+23 - 1" Tree 25'

+84 - 2" Tree 30'

+46 - 1" Tree 34'

+03 - 1" Tree 34'

+91 - T.P. 22'

+65 - 4" Tree 34'

+21 - 2" Tree 33'

+82 - 4" Tree 33'

+40 - 4" Tree 33'
+33 - T.P. 20'
+08 - 2" Tree

+64 - 3" Tree

+24 - 2" Tree 33'

+38 - T.P. 19'
+66 - 2" Tree 27'

+49 - 4" Tree

+09 - 2" Tree 32'

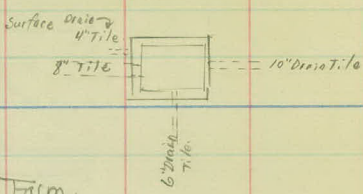


Pasture

Cultivated

+37 - 1/2 Road Rt.

187



+34 - 1/2 Drive to Dairy Farm.

+01 - Field Ent Rt.

186

185

184

183

182

181

+94-8" Tree 35'

+64-6" Tree 16'

+27-6" Tree 15'

+06-4" Man Hole 3' x 3' (45 H.)
conc. frame cover

+88-6" Tree 15'

+77 Hedge 9'
+83 Hedge 9'
+47 Hedge 25' (Cumbrey)

+05-1" Tree 16'

+75-4" Tree 16'

+40-4" Tree 17'

+11-3" Tree

+78-3" Tree 17'

+47-2" Tree

+10-2" Tree 18'

+84-4" Tree 11'

+54-7" Tree

+57-1" Tree 15'

+23-2" Tree 18'
+18-P.P. 18'

+90-2" Tree 14'
+84-P.P. 10'
+54-2" Tree 20'

+09-3" Tree 20'

LAWN.

LAWN.

Tel. Line -
New York
Power.

S.P. & L.I. Co.

New York Power Co.

Lst. P. & L.I. Co.

CULTIVATED.

Shrubs
LAWN.

+62-T.P. 13
+60-B. Dynamometer
F. 33

+60
New York Power Co.

+89-P.P. 41
+94-M.O. 21

+01-T.P. 27'
+86-1" Tree 41'
+83-M.O. 21'
+81-P.P. 27'

+48-3" Tree 40'

+28-T.P. 27'
+12-3" Tree 40'

+80-P.P. 41'

+77-2" Tree 40'

+46-12" Tree 40'

+17-P.P. 15'
+12-2" 40'

+97-T.P. 25'

+78-12" Tree
+63-P.P. 40'

+45-8" Tree 40'

+06-1" Tree 40'

+73-2" Tree 40'

+53-P.P. 39'

+54-T.P. 25'

+52-P.P. 25'
+37-1" Tree 40'

+78-2" Tree 40'

+62-3" Tree 39'

+24-3" Tree
+12-T.P. 24'

+91-2" Tree

+50-4" Tree 31'

+12-3" Tree 31'



+75.1 P.T.

194

193

192

191

+41 - \angle Drive to Homes. 100 - 55 $\frac{1}{2}$ Lt. E. Ed. Conc. 4' Walk.

190

189

+91 - \angle Drive to Estate.

188

+50 - F. 19

+20 - F. 68, 15

F-14'

+84 - 14" Oak 28
+84 - 14" Oak 20
+68 - 10" Oak 28
+51 - 24" Oak 26

+20 - 12" Oak 32

+18 - 10" Oak 24

+13 - 14" Oak 22

F-1'

+92 - 24" Oak 15

+77 - 12" Oak 29

+69 - 10" Oak 27

+50 - 8" Oak 17

+41 - 10" Oak 15

+32 - 4" Oak 20

+28 - 8" Tr. Oak 20

+08 - 14" Oak 3

F. E. W.

+93 - 6" Oak 21

+68 - 10" Oak 30

+47 - 16" Oak 26

+44 - N.E. Cor. 10, 60

+36 - 10" Oak 10

+32 - E. Ed. Walk 476

+27 - 20" Oak 10

+27 - 6" Tree 10

+98 - 8" Oak 13

+67 - P. 97

+59 - Hedge

+30 - Hedge 30

+27 - Hedge 17

+22 - Hedge 9

+19 - 12" Oak 12

+04 - 12" Oak 13

+25 - Hedge 20 - 206

+92 - 10" Oak 12

+90 - 10" Oak 10

+73 - 4" Oak 12

+65 - 2" Oak 13

+45 - 6" Tr. Tree 17

+42 - P. P. 10

+17 - 2" Tree 21

+12 - 8" Tree 17

+04 - 2" Ev. Green 37

+93 - 6" Conc. 6' Walk

+82 - 2" Ev. Green 37

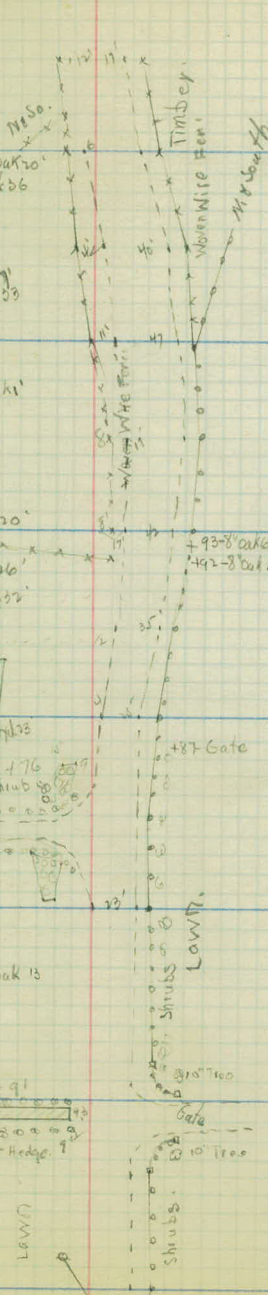
+82 - 2" Ev. Green 22

+64 - 3" Tree 16

+24 - 1" Tree 16

+16 - P. P. 11

Timber



+50 - F. 27'

F-35'

+50 - F. 50

+98 - F. Cor. 53'

+81 - 24" Oak 2'

+22 - 12" Oak 10

F-57'

+88 - F. Cor. 8'

+87 - P. P. 9

+70 - 8" Oak 2'

+50 - F. 42.5

+48 - 2" Tree 4'

F-343

+93 - 1" Ev. Green 316

+84 - 3" Ev. Green 305

+50 - F. 312

+34 - F. 31.2

F-31.3

+18 - Arc. F. 32

+14 - M. B. X 30

+02 - B. F. 46

+81 - E. F. 46

+64 - Arc. F. 325

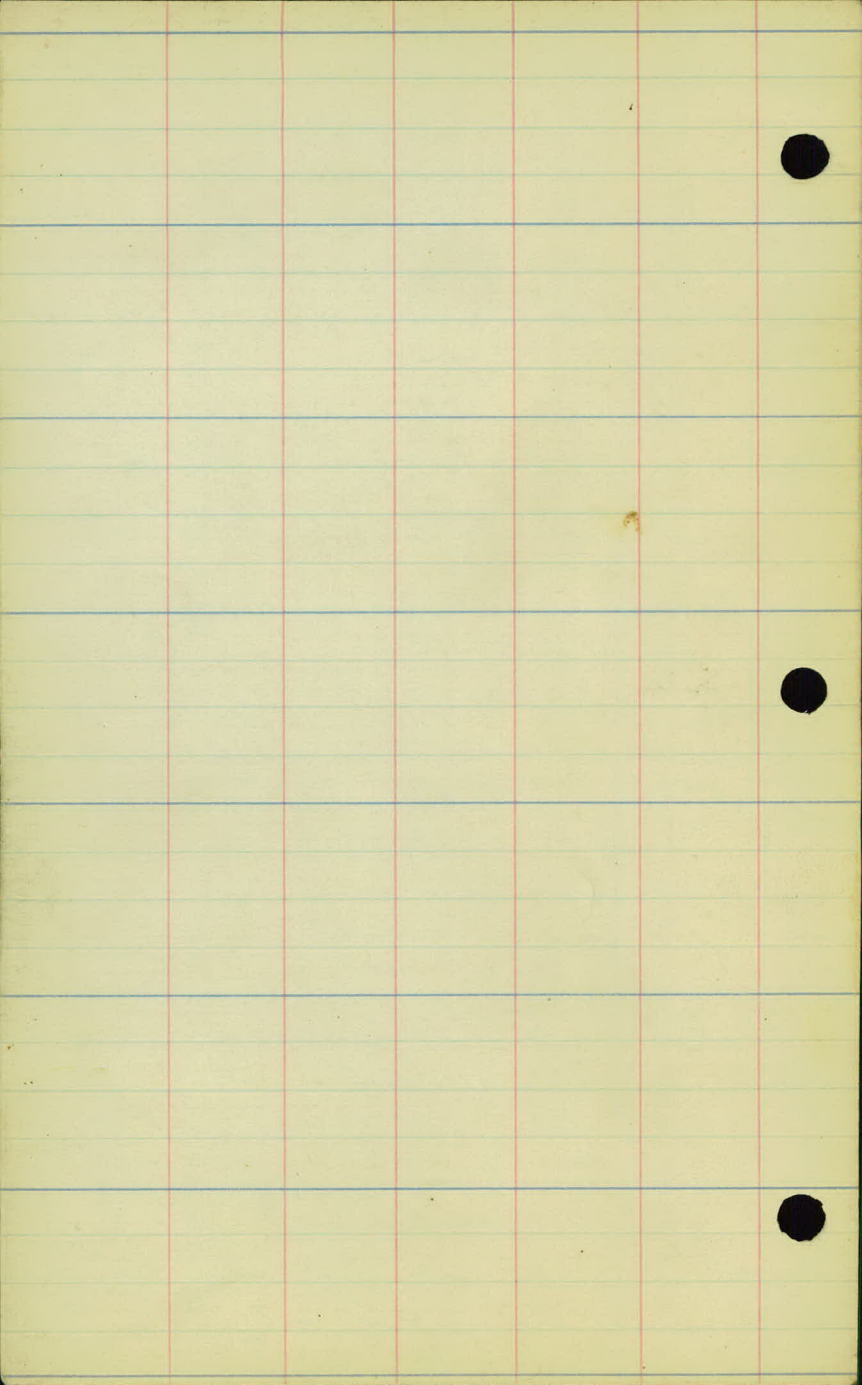
+87 - Hedge 9'

LAWN

LAWN

GATE

SHRUBS



TOPOGRAPHY

4/20/26

8

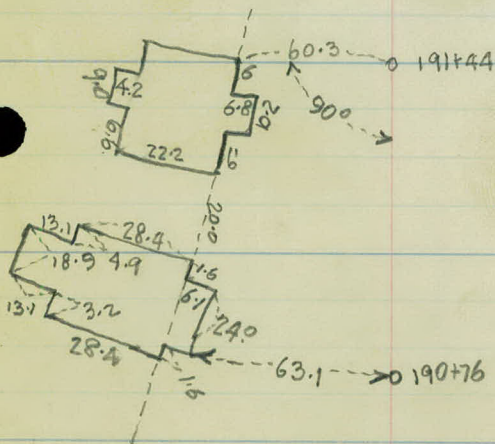
HACKNEY BLDGS

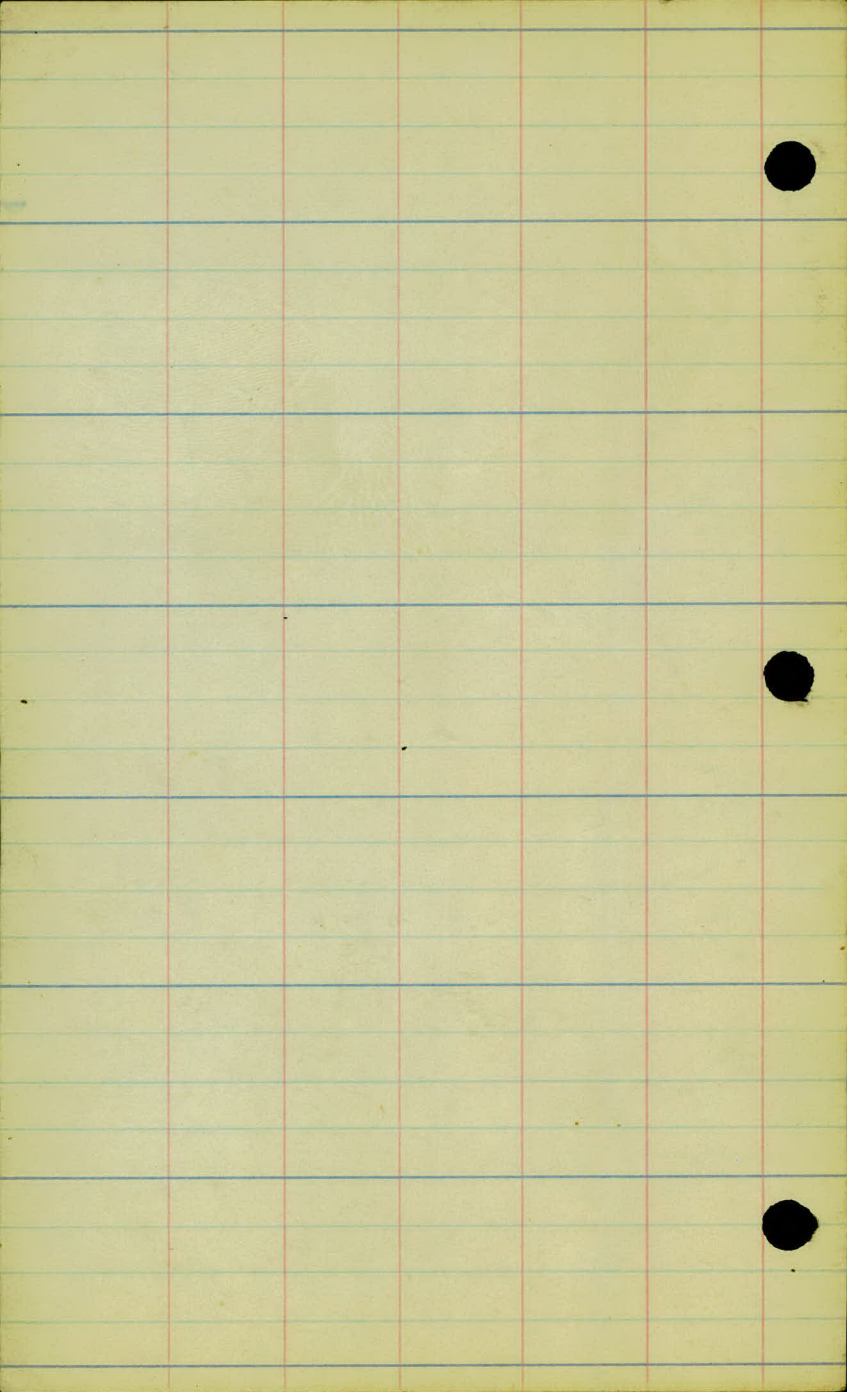
PRB

ANORA CUTOFF

C.W.S.

PROJ-26-62A





2 Levels & X-Sections

Ano ka Line change.

station	+	H.I	-	Elev.
B.M.	1.43	923.33 ✓		921.90
171400				914.7
171465				915.08 Top Mon.
172				915.5
+56				16.5
173				16.9
174				18.7
175				19.1
T.P.	1.55	921.71 ✓	3.17	920.16 ✓
176				17.7
+50				17.1
177				16.7
+50				16.2
178				16.0

Lt. L Rt. W.H.G. A.L.P. M.G. #.B 3-23-26
R.R. Spike in 16" Oak 34' Lt. 173+1

$\frac{9.0}{50}$	$\frac{9.1}{20}$	$\frac{9.0}{12}$	86	$\frac{8.9}{11}$	$\frac{9.1}{16}$	$\frac{10.1}{17}$	$\frac{10.1}{50}$					
$\frac{8.4}{50}$	$\frac{9.1}{34}$	$\frac{8.8}{18}$	$\frac{8.5}{15}$	$\frac{8.5}{12}$	$\frac{8.9}{25}$	$\frac{10.1}{50}$						
$\frac{9.0}{50}$	$\frac{9.1}{33}$	$\frac{9.6}{19}$	$\frac{8.7}{17}$	$\frac{8.1}{12}$	78	$\frac{8.0}{14}$	$\frac{9.5}{15}$	$\frac{9.7}{21}$	$\frac{10.5}{22}$	$\frac{10.1}{27}$	$\frac{9.1}{29}$	$\frac{8.2}{50}$

$\frac{4.5}{50}$	$\frac{4.5}{33}$	$\frac{5.0}{25}$	$\frac{8.0}{18}$	$\frac{7.3}{13}$	68	$\frac{7.2}{15}$	$\frac{8.9}{22}$	$\frac{8.8}{26}$	$\frac{6.4}{29}$	$\frac{6.0}{40}$	$\frac{6.0}{50}$
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$\frac{3.2}{50}$	$\frac{3.2}{30}$	$\frac{4.1}{20}$	$\frac{6.6}{17}$	$\frac{6.1}{10}$	64	$\frac{6.7}{12}$	$\frac{6.8}{17}$	$\frac{7.5}{20}$	$\frac{7.5}{27}$	$\frac{5.7}{50}$	$\frac{4.8}{35}$	$\frac{5.4}{41}$	$\frac{5.4}{50}$
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$\frac{3.2}{50}$	$\frac{3.2}{18}$	$\frac{5.1}{16}$	$\frac{5.5}{13}$	$\frac{5.0}{11}$	46	$\frac{5.2}{17}$	$\frac{5.6}{19}$	$\frac{5.7}{21}$	$\frac{4.3}{25}$	$\frac{2.8}{36}$	$\frac{3.0}{50}$
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$\frac{3.3}{50}$	$\frac{3.4}{17}$	$\frac{5.0}{15}$	$\frac{5.1}{13}$	$\frac{4.7}{12}$	42	$\frac{4.4}{16}$	$\frac{4.8}{21}$	$\frac{4.6}{23}$	$\frac{3.5}{26}$	$\frac{2.5}{37}$	$\frac{3.3}{41}$	$\frac{3.3}{50}$
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Nail in T.P. 14' Rt. 174+88

$\frac{1.6}{50}$	$\frac{2.4}{29}$	$\frac{3.0}{18}$	$\frac{5.0}{13}$	$\frac{4.5}{10}$	40	$\frac{4.2}{19}$	$\frac{5.2}{21}$	$\frac{4.7}{38}$	$\frac{5.4}{41}$	$\frac{5.5}{50}$
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$\frac{3.9}{50}$	$\frac{4.8}{28}$	$\frac{5.1}{14}$	$\frac{4.7}{10}$	46	$\frac{5.2}{19}$	$\frac{7.3}{23}$	$\frac{7.0}{34}$	$\frac{6.6}{39}$	$\frac{6.9}{50}$
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$\frac{4.8}{50}$	$\frac{5.4}{27}$	$\frac{6.0}{14}$	$\frac{5.2}{11}$	50	$\frac{5.4}{18}$	$\frac{7.1}{24}$	$\frac{8.6}{27}$	$\frac{8.7}{31}$	$\frac{7.2}{33}$	$\frac{7.1}{40}$
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$\frac{5.6}{50}$	$\frac{7.0}{27}$	$\frac{7.7}{13}$	$\frac{6.0}{10}$	55	$\frac{6.0}{19}$	$\frac{9.0}{24}$		$\frac{10.3}{50}$		
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$\frac{6.3}{50}$	$\frac{8.3}{27}$	$\frac{8.3}{13}$	$\frac{6.3}{10}$	57	$\frac{6.1}{18}$	$\frac{8.9}{23}$	$\frac{8.7}{35}$	$\frac{8.2}{40}$	$\frac{8.2}{50}$
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station	+	H.I	-	Elev.
		921.71		
178+50				15.8
179				16.0
+50				16.5
180				16.4
T.R	3.23	920.37	4.57	917.14
+50				15.8
181				14.9
+60				14.2
182				13.5
183				12.7
+67				12.0
184				11.9
T.R	3.65	915.73	8.29	912.08
+50				12.8

Lt.

2

Rt.

(Rain)

11

 $\frac{74}{50}$ $\frac{73}{38}$ $\frac{78}{26}$ $\frac{73}{12}$ $\frac{63}{11}$

59

 $\frac{63}{21}$ $\frac{80}{26}$ $\frac{82}{29}$ $\frac{56}{35}$ $\frac{56}{44}$ $\frac{57}{50}$
 $\frac{92}{50}$ $\frac{84}{35}$ $\frac{71}{27}$ $\frac{63}{15}$ $\frac{68}{13}$ $\frac{61}{10}$

57

 $\frac{62}{21}$ $\frac{71}{24}$ $\frac{72}{28}$ $\frac{38}{38}$ $\frac{33}{50}$
 $\frac{66}{50}$ $\frac{56}{32}$ $\frac{44}{17}$ $\frac{63}{12}$ $\frac{54}{10}$

52

 $\frac{55}{22}$ $\frac{67}{25}$ $\frac{67}{29}$ $\frac{51}{36}$ $\frac{46}{48}$ $\frac{13}{50}$
 $\frac{62}{50}$ $\frac{52}{21}$ $\frac{64}{13}$ $\frac{56}{9}$

53

 $\frac{57}{21}$ $\frac{67}{26}$ $\frac{15}{37}$ $\frac{205}{50}$

Nail in P.P.

Lt. 180+20

 $\frac{80}{50}$ $\frac{83}{40}$ $\frac{69}{26}$ $\frac{59}{12}$ $\frac{48}{10}$

46

 $\frac{47}{22}$ $\frac{60}{25}$ $\frac{58}{29}$ $\frac{70}{37}$ $\frac{33}{43}$ $\frac{28}{50}$

Eot

 $\frac{87}{50}$ $\frac{89}{38}$ $\frac{67}{11}$ $\frac{60}{9}$

55

 $\frac{52}{10}$ $\frac{54}{24}$ $\frac{73}{28}$ $\frac{71}{33}$ $\frac{58}{34}$ $\frac{55}{50}$
 $\frac{108}{50}$ $\frac{84}{10}$ $\frac{66}{7}$

62

 $\frac{60}{10}$ $\frac{63}{21}$ $\frac{84}{27}$ $\frac{83}{32}$ $\frac{71}{34}$ $\frac{72}{44}$ $\frac{77}{50}$
 $\frac{112}{50}$ $\frac{111}{37}$ $\frac{98}{12}$ $\frac{71}{5}$

69

 $\frac{66}{9}$ $\frac{72}{24}$ $\frac{86}{27}$ $\frac{88}{31}$ $\frac{70}{35}$ $\frac{84}{50}$
 $\frac{125}{50}$ $\frac{120}{12}$ $\frac{82}{3}$

77

 $\frac{75}{12}$ $\frac{80}{23}$ $\frac{86}{29}$ $\frac{100}{38}$ $\frac{100}{50}$
 $\frac{125}{50}$ $\frac{124}{12}$ $\frac{88}{3}$

84

 $\frac{81}{12}$ $\frac{86}{23}$ $\frac{105}{29}$ $\frac{108}{23}$ $\frac{106}{50}$
 $\frac{109}{50}$ $\frac{115}{12}$ $\frac{89}{4}$

85

 $\frac{81}{10}$ $\frac{85}{23}$ $\frac{99}{27}$ $\frac{94}{42}$ $\frac{96}{50}$
 $\frac{54}{50}$ $\frac{53}{11}$ $\frac{40}{4}$

39

 $\frac{36}{13}$ $\frac{38}{25}$ $\frac{50}{27}$ $\frac{48}{31}$ $\frac{24}{34}$ $\frac{31}{50}$

Station	+	H.I	-	Elev.
		915.73		
185				11.9
186				11.1
+50				11.1
187				10.1
B.M.	4.96	915.73	4.96	910.77
+40				10.0
188				10.0
+50				10.5
189				11.9
+50				11.7
190				11.4
T.P.	6.14	918.82	3.05	912.68
+50				13.4
191				14.3

Lt.

2

Rt.

CRD

$\frac{4.2}{50}$	$\frac{5.2}{30}$	$\frac{5.2}{11}$	$\frac{4.0}{4}$	38	$\frac{3.5}{12}$	$\frac{3.9}{22}$	$\frac{3.4}{25}$	$\frac{4.3}{28}$	$\frac{4.0}{31}$	$\frac{1.4}{35}$	$\frac{2.3}{50}$
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$\frac{5.6}{50}$	$\frac{5.3}{14}$	$\frac{4.6}{7}$	46	$\frac{4.2}{12}$	$\frac{4.3}{23}$	$\frac{4.3}{28}$	$\frac{5.8}{29}$	$\frac{5.7}{32}$	$\frac{2.6}{44}$	$\frac{2.9}{50}$
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$\frac{6.7}{50}$		$\frac{5.4}{15}$	46	$\frac{4.6}{12}$	$\frac{5.2}{21}$	$\frac{7.2}{28}$	$\frac{7.1}{32}$	$\frac{3.5}{36}$	$\frac{3.7}{50}$
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$\frac{6.9}{50}$	$\frac{2.1}{13}$	$\frac{5.7}{4}$	56	$\frac{5.2}{70}$	$\frac{5.9}{26}$	$\frac{7.5}{30}$	$\frac{6.5}{36}$	$\frac{6.6}{50}$
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Spike in T.P. 50' Rt Sta. 187450

$\frac{6.7}{50}$	$\frac{6.2}{8}$	$\frac{5.9}{4}$	57	$\frac{5.1}{16}$	$\frac{5.4}{20}$	$\frac{5.2}{50}$	L Road Rt.
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$\frac{6.3}{33}$	$\frac{6.1}{6}$	57	$\frac{5.4}{12}$	$\frac{5.8}{22}$	$\frac{6.1}{33}$
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$\frac{5.3}{33}$	52	$\frac{4.7}{13}$	$\frac{5.2}{24}$	$\frac{4.6}{33}$
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$\frac{4.7}{33}$	$\frac{3.3}{8}$	$\frac{3.9}{5}$	38	$\frac{3.4}{12}$	$\frac{3.5}{22}$	$\frac{3.8}{33}$
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$\frac{3.8}{33}$	$\frac{3.2}{9}$	$\frac{3.8}{6}$	40	$\frac{3.4}{18}$	$\frac{4.0}{24}$	$\frac{3.8}{33}$
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$\frac{5.1}{33}$	$\frac{5.0}{9}$	43	$\frac{3.5}{13}$	$\frac{4.1}{24}$	$\frac{4.3}{33}$
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$\frac{4.8}{33}$	$\frac{5.2}{10}$	54	$\frac{5.6}{14}$	$\frac{6.1}{23}$	$\frac{6.0}{33}$
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$\frac{2.0}{33}$	$\frac{2.0}{22}$	$\frac{2.8}{6}$	45	$\frac{5.1}{4}$	$\frac{4.5}{17}$	$\frac{4.9}{27}$	$\frac{5.0}{34}$
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Station	+	H.I	-	Elev.
		918.82		
191+21				15.4
+70				12.9
192				10.0
+50				12.4
193				15.1
193+50				11.5
194				11.3
+50				10.4
B.M.				2.05 910.77 ✓

SEE R-19

Lt.

2

Rt.

2 RQ

$\frac{2.1}{33}$

3.4

$\frac{5.0}{7}$

$\frac{4.6}{20}$

$\frac{5.0}{30}$

$\frac{5.0}{35}$

$\frac{7.0}{50}$

$\frac{6.4}{33}$

5.9

$\frac{5.9}{13}$

$\frac{5.0}{29}$

$\frac{5.6}{40}$

$\frac{8.5}{40}$

$\frac{9.0}{28}$

8.8

$\frac{8.3}{12}$

$\frac{5.8}{18}$

$\frac{5.1}{32}$

$\frac{5.9}{50}$

$\frac{6.1}{50}$

$\frac{6.4}{26}$

6.4

$\frac{6.2}{10}$

$\frac{6.8}{12}$

$\frac{6.7}{15}$

$\frac{6.0}{18}$

$\frac{5.0}{36}$

$\frac{5.2}{50}$

$\frac{3.2}{50}$

$\frac{3.0}{28}$

3.7

$\frac{6.5}{5}$

$\frac{6.7}{8}$

$\frac{6.3}{11}$

$\frac{5.7}{29}$

$\frac{6.5}{50}$

$\frac{2.8}{50}$

$\frac{2.8}{30}$

$\frac{3.6}{8}$

$\frac{7.3}{4}$

7.3

$\frac{6.9}{5}$

$\frac{6.4}{24}$

$\frac{7.0}{40}$

$\frac{7.9}{42}$

$\frac{7.6}{45}$

$\frac{4.8}{49}$

$\frac{4.8}{50}$

$\frac{3.2}{50}$

$\frac{5.0}{14}$

$\frac{7.9}{10}$

$\frac{8.4}{7}$

$\frac{7.9}{6}$

7.5

$\frac{7.4}{15}$

$\frac{7.8}{26}$

$\frac{8.6}{28}$

$\frac{8.6}{31}$

$\frac{6.2}{35}$

$\frac{6.2}{50}$

$\frac{6.0}{50}$

$\frac{7.6}{19}$

$\frac{9.2}{17}$

$\frac{9.3}{15}$

$\frac{8.8}{13}$

8.4

$\frac{8.9}{17}$

$\frac{10.0}{19}$

$\frac{10.0}{21}$

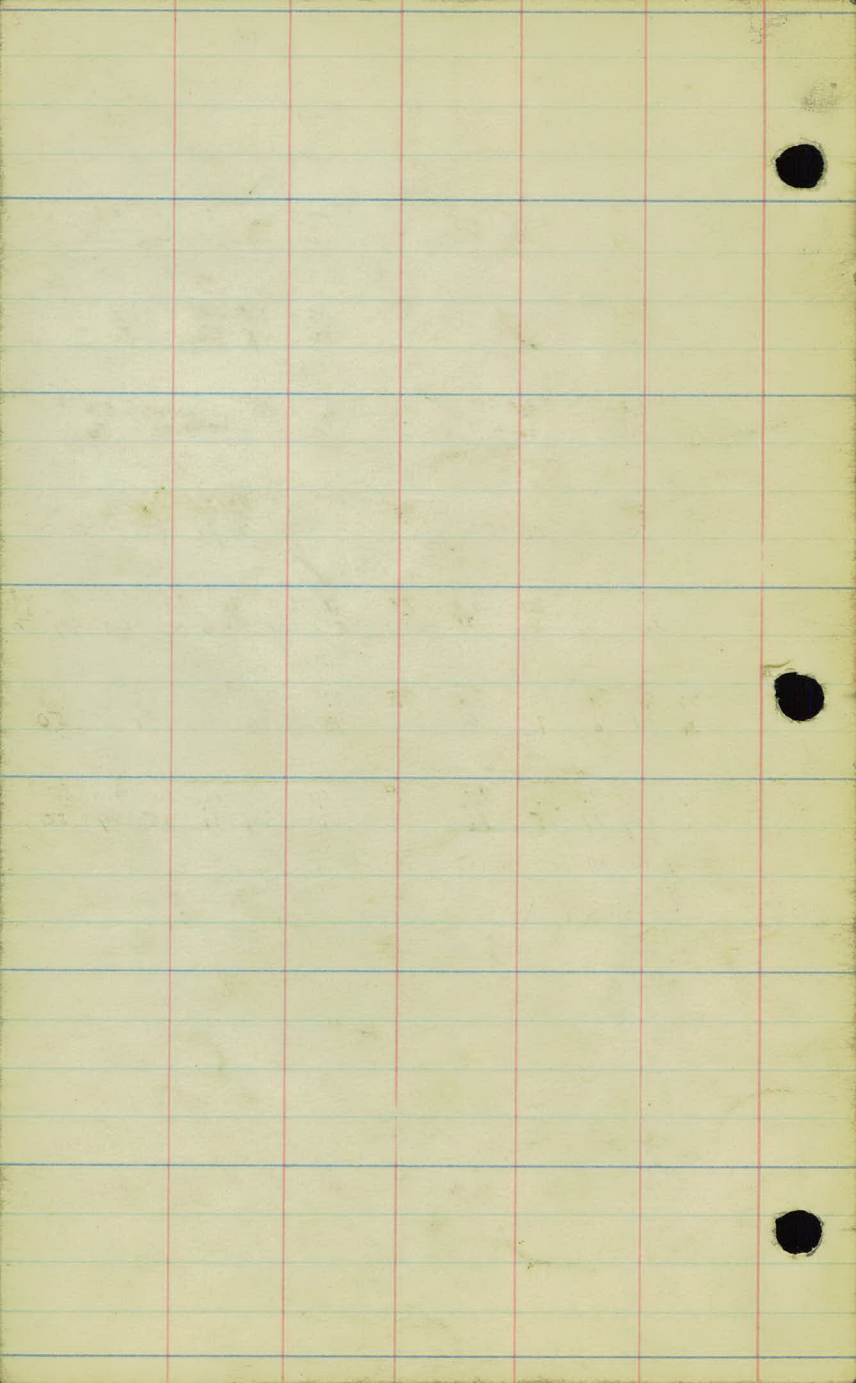
$\frac{8.0}{25}$

$\frac{7.0}{29}$

$\frac{7.0}{50}$

Spike in T.P. 50 Rt. Sta. 187+50

5



Anella line Change
Sta 189-194

194 + 4.77 P.T. = 194 + 49.5

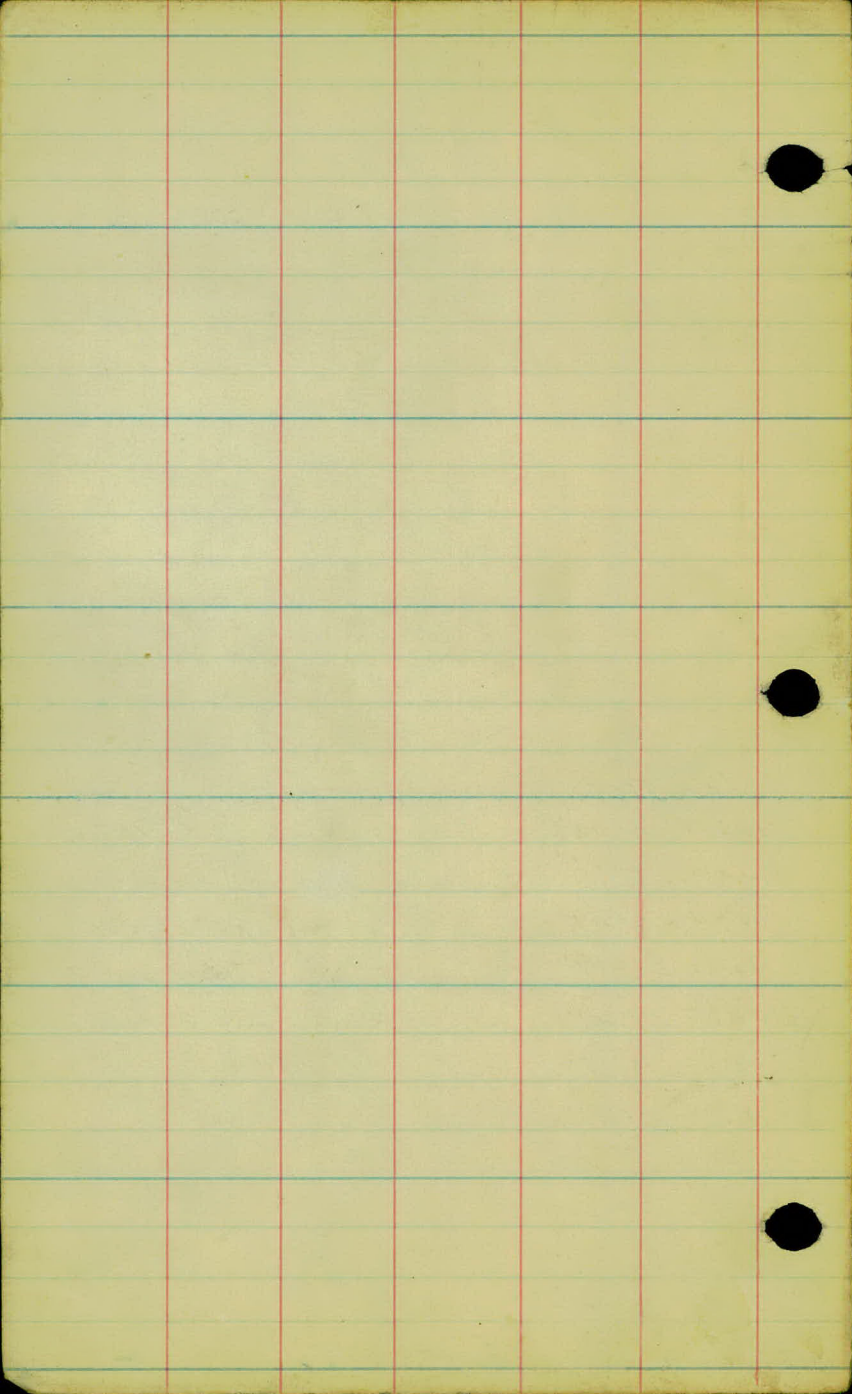
192 + 30.51 P.I. 440 44'

189 + 94.44 P.C.

Sta. - Elev.

~~189+94.44 - 0000'~~
~~190+00 - 0°17'~~
~~+50 - 2047'~~
~~191+00 - 5°17'~~
~~+50 - 7047'~~
~~192+00 - 10°17'~~
~~+50 - 12047'~~
~~193+00 - 15°17'~~
~~+50 - 17047'~~
~~194+00 - 20°17'~~
~~+41.77 - 22°22'~~

10° Curve h eff.
 $\Delta = 44°44'$
 Rad = 573.69
 Tang = 236.07
 Length = 447.33



Line change

3-3-26

Station	+	H.I	-	Rod	Elev
BM.	1.59	923.49.			921.90
171 + 22.0					15.0
+ 50					15.1
172 + 00					15.9
+ 42					16.5
173 + 00					17.2
174 + 00					19.0
175 + 00					18.9
T.P.	4.95	922.85.	5.59	917.90	
176 + 00					17.6
177 + 00					16.6
+ 60					16.1
178 + 00					15.9
179 + 00					16.2

$\frac{8.4}{50.0}$ $\frac{9.6}{17.5}$ $\frac{9.0}{14.0}$ $\frac{9.5}{8.5}$ $\frac{8.8}{14.0}$ $\frac{10.0}{17.5}$ $\frac{11.4}{20.0}$ $\frac{10.6}{31.0}$ $\frac{10.5}{50.0}$

$\frac{8.5}{50.0}$ $\frac{9.0}{32.0}$ $\frac{10.0}{19.0}$ $\frac{8.6}{14.0}$ 8.4 $\frac{9.0}{12.0}$ $\frac{10.0}{23.0}$ $\frac{9.6}{50.0}$

$\frac{8.4}{50.0}$ $\frac{8.6}{38.0}$ $\frac{8.6}{33.0}$ $\frac{9.0}{25.0}$ $\frac{9.0}{18.0}$ $\frac{8.2}{15.0}$ 7.6 $\frac{8.0}{14.0}$ $\frac{9.7}{16.5}$ $\frac{9.4}{20.0}$ $\frac{10.2}{24.0}$ $\frac{8.5}{27.0}$ $\frac{7.6}{34.0}$ $\frac{7.6}{38.0}$
 $\frac{7.6}{50.0}$

$\frac{4.5}{50.0}$ $\frac{4.8}{36.0}$ $\frac{5.0}{28.0}$ $\frac{6.4}{24.0}$ $\frac{8.2}{18.0}$ $\frac{7.5}{15.0}$ 7.0 $\frac{7.2}{14.0}$ $\frac{8.8}{20.5}$ $\frac{8.8}{25.0}$ $\frac{6.5}{27.0}$ $\frac{5.5}{34.0}$ $\frac{6.2}{39.0}$ $\frac{6.0}{50.0}$

$\frac{2.8}{50.0}$ $\frac{2.6}{37.0}$ $\frac{3.0}{30.0}$ $\frac{3.5}{21.0}$ $\frac{7.0}{16.0}$ $\frac{6.4}{13.0}$ 6.3 $\frac{6.6}{15.0}$ $\frac{7.3}{18.0}$ $\frac{7.3}{25.0}$ $\frac{5.5}{28.0}$ $\frac{4.8}{34.0}$ $\frac{5.0}{50.0}$

$\frac{3.5}{50.0}$ $\frac{3.5}{37.0}$ $\frac{3.5}{31.0}$ $\frac{3.5}{20.0}$ $\frac{5.5}{16.0}$ $\frac{5.0}{13.0}$ 4.5 $\frac{5.0}{14.0}$ $\frac{5.4}{16.0}$ $\frac{5.4}{19.0}$ $\frac{4.2}{22.0}$ $\frac{3.7}{28.0}$ $\frac{2.8}{32.0}$
 $\frac{2.8}{50.0}$ $\frac{3.2}{37.0}$

$\frac{2.2}{50}$ $\frac{2.2}{33}$ $\frac{2.6}{26}$ $\frac{5.6}{18}$ $\frac{5.6}{15}$ $\frac{5.0}{11.0}$ 4.6 $\frac{4.6}{15}$ $\frac{4.6}{17}$ $\frac{3.8}{22}$ $\frac{7.2}{29}$ $\frac{2.8}{33}$ $\frac{3.4}{36}$ $\frac{4.0}{50}$

$\frac{3.6}{50}$ $\frac{3.8}{42}$ $\frac{4.0}{33}$ $\frac{4.7}{24}$ $\frac{5.0}{21}$ $\frac{6.2}{17}$ $\frac{5.7}{15}$ 5.3 $\frac{5.6}{14}$ $\frac{6.4}{16}$ $\frac{6.8}{18}$ $\frac{6.4}{20}$ $\frac{6.6}{31}$ $\frac{7.2}{50}$

$\frac{4.3}{50}$ $\frac{6.5}{39}$ $\frac{7.0}{33}$ $\frac{7.0}{24}$ $\frac{7.5}{21}$ $\frac{7.1}{19}$ $\frac{6.5}{16}$ 6.3 $\frac{6.8}{13}$ $\frac{7.4}{15}$ $\frac{9.6}{20}$ $\frac{10.3}{24}$ $\frac{9.6}{28}$ $\frac{8.6}{33}$ $\frac{10.0}{37}$ $\frac{11.5}{50}$

$\frac{9.0}{50}$ $\frac{9.0}{38}$ $\frac{9.2}{33}$ $\frac{9.6}{28}$ $\frac{9.6}{23}$ $\frac{9.0}{20}$ $\frac{7.2}{15}$ 6.6 $\frac{7.2}{13}$ $\frac{11.0}{20}$ $\frac{11.7}{50}$

$\frac{9.0}{50}$ $\frac{9.0}{37}$ $\frac{9.2}{25}$ $\frac{9.2}{20}$ $\frac{7.4}{15}$ 7.0 $\frac{7.4}{18}$ $\frac{9.7}{18}$ $\frac{9.4}{25}$ $\frac{9.0}{30}$ $\frac{8.4}{33}$ $\frac{6.5}{36}$ $\frac{8.0}{38}$
 $\frac{9.0}{50}$

$\frac{7.5}{50}$ $\frac{7.7}{36}$ $\frac{6.8}{23}$ $\frac{7.6}{22}$ $\frac{7.6}{20}$ $\frac{7.1}{16}$ 6.7 $\frac{7.1}{13.0}$ $\frac{8.2}{18}$ $\frac{7.2}{22}$ $\frac{6.8}{31}$ $\frac{3.2}{33}$ $\frac{3.7}{50}$

Station	+	H.I.	-	Rod	Elev.
		922.55			
179+50					16.6
180+00					16.4
181+00					14.9
182+00					13.7
T.P.	2.92	916.70	9.07	913.78	
183+00					12.7
184+00					12.3
185+00					12.2
186+00					11.4
+50					10.8
187+00					10.5
+26					10.5
B.M.				5.93	910.91
188+00					10.4
T.P.	8.80	921.28	4.22	912.48	

$\frac{7.4}{50}$	$\frac{6.0}{34}$	$\frac{5.7}{26}$	$\frac{6.7}{21}$	$\frac{6.5}{16}$	6.3	$\frac{6.6}{13}$	$\frac{7.8}{19}$	$\frac{6.7}{23}$	$\frac{1.6}{31}$	$\frac{2.6}{41}$	$\frac{3.0}{50}$
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$\frac{8.4}{50}$	$\frac{7.6}{38}$	$\frac{7.3}{26}$	$\frac{7.6}{23}$	$\frac{6.8}{19}$	$\frac{6.9}{15}$	6.5	$\frac{6.9}{12}$	$\frac{8.1}{19}$	$\frac{4.7}{24}$	$\frac{3.1}{28}$	$\frac{3.8}{38}$	$\frac{4.4}{50}$
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$\frac{11.8}{50}$	$\frac{10.6}{36}$	$\frac{9.4}{21}$	$\frac{8.3}{17}$	8.0	$\frac{8.3}{12}$	$\frac{10.3}{20}$	$\frac{5.6}{25}$	$\frac{8.4}{32}$	$\frac{8.8}{36}$	$\frac{9.1}{50}$
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$\frac{14.3}{50}$	$\frac{14.0}{35}$	$\frac{13.0}{21.0}$	$\frac{10.0}{15}$	$\frac{9.3}{8.0}$	9.2	$\frac{9.8}{13}$	$\frac{11.1}{15}$	$\frac{11.7}{23.0}$	$\frac{10.4}{31}$	$\frac{11.0}{37}$	$\frac{11.4}{50}$
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$\frac{9.5}{50}$	$\frac{8.4}{19}$	$\frac{4.6}{14.0}$	$\frac{3.9}{7.0}$	4.0	$\frac{4.6}{11.0}$	$\frac{5.4}{17}$	$\frac{7.0}{22}$	$\frac{7.6}{26}$	$\frac{6.4}{33}$	$\frac{6.2}{50}$
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$\frac{7.1}{50}$	$\frac{7.0}{28}$	$\frac{6.5}{21}$	$\frac{5.1}{16}$	$\frac{4.4}{7.0}$	4.4	$\frac{7.7}{12}$	$\frac{6.0}{17}$	$\frac{6.3}{19}$	$\frac{5.8}{21}$	$\frac{5.0}{31}$	$\frac{5.5}{35}$	$\frac{5.0}{50}$
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$\frac{6.4}{50}$	$\frac{5.9}{21}$	$\frac{4.8}{16}$	$\frac{4.7}{8.0}$	4.5	$\frac{4.5}{12}$	$\frac{5.4}{15}$	$\frac{4.0}{19}$	$\frac{2.4}{21}$	$\frac{2.2}{30}$	$\frac{3.3}{37}$	$\frac{4.0}{50}$
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$\frac{6.4}{50.0}$	$\frac{5.8}{21}$	$\frac{5.3}{13}$	5.3	$\frac{5.4}{12}$	$\frac{7.4}{17}$	$\frac{4.2}{20}$	$\frac{3.6}{24}$	$\frac{3.5}{33}$	$\frac{3.6}{50}$
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$\frac{8.0}{50}$	$\frac{7.8}{36}$	$\frac{7.0}{20}$	$\frac{6.3}{17}$	5.9	$\frac{6.3}{11}$	$\frac{8.3}{15}$	$\frac{8.3}{19}$	$\frac{5.5}{23}$	$\frac{5.2}{31}$	$\frac{5.2}{50}$
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$\frac{5.2}{50}$	$\frac{7.4}{21}$	$\frac{6.7}{18}$	$\frac{6.4}{13}$	$\frac{6.2}{7.0}$	6.2	$\frac{6.9}{13}$	$\frac{6.7}{18}$	$\frac{7.3}{30}$	$\frac{7.4}{50}$
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$\frac{7.8}{50}$	$\frac{7.3}{21}$	$\frac{6.7}{18}$	$\frac{6.3}{12}$	$\frac{6.1}{5.0}$	6.2	$\frac{6.0}{21}$	$\frac{6.0}{50}$
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Nail in T.P. 35' R4. Sta 186+45

$\frac{7.0}{50}$	$\frac{6.6}{19}$	$\frac{6.2}{13.0}$	6.3	$\frac{6.8}{6.0}$	$\frac{6.5}{14}$	$\frac{7.0}{34}$	$\frac{7.0}{50}$
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T.P. on Gate. Post. R. Sta 187+51

	+	H.I.	-	Rod	Elev.
	8.78	921.26	4.22	912.48	

189+00					12.0
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x 190+00					12.4
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+46					13.8
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191+00					14.2
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+50					13.8
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192+00					13.5
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+50					13.2
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193+00					12.9
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T.P.	3.88	918.23	6.91	914.35	
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+50					12.2
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194+00					11.5
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FROM R-13

195+00					09.5
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T.P.	0.92	907.98	11.17	907.06	
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196+00					06.0
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67

4

Rt.

19

$$\frac{9.5}{50.0} \frac{8.5}{25.0} \frac{8.8}{20.0} 8.8 \frac{8.8}{15.0} \frac{8.2}{17.0} \frac{7.6}{24.0} \frac{7.4}{50.0}$$

$$\frac{10.2}{50.0} \frac{9.8}{27.0} \frac{8.7}{16.0} \frac{8.6}{7.0} 8.9 \frac{9.3}{6.0} \frac{9.6}{18.0} \frac{9.3}{13.0} \frac{9.6}{50.0}$$

$$\frac{5.6}{50.0} \frac{5.6}{38.0} \frac{6.1}{29.0} \frac{7.3}{25.0} \frac{7.4}{15.0} 7.5 \frac{8.5}{9.0} \frac{7.8}{12.0} \frac{9.2}{50.0}$$

$$\frac{5.2}{50.0} \frac{5.2}{33.0} \frac{5.5}{26.0} \frac{6.7}{21.0} \frac{7.2}{18.0} 7.1 \frac{7.4}{7.0} \frac{7.5}{10.0} \frac{7.0}{12.0} \frac{8.5}{50.0}$$

$$\frac{8.5}{50.0} \frac{7.7}{28.0} \frac{8.0}{16.0} 7.5 \frac{7.7}{12.0} \frac{7.8}{15.0} \frac{7.3}{17.0} \frac{8.0}{50.0}$$

$$\frac{11.7}{50.0} \frac{11.0}{14.0} \frac{10.8}{13.0} \frac{8.3}{9.0} 7.8 \frac{7.4}{7.0} \frac{7.7}{16.0} \frac{8.4}{23.0} \frac{8.6}{25.0} \frac{9.1}{22.0} \frac{8.8}{58.0}$$

$$\frac{8.3}{50.0} \frac{8.3}{25.0} \frac{8.5}{16.0} \frac{9.2}{12.0} \frac{8.4}{8.0} 8.1 \frac{7.1}{17.0} \frac{8.0}{35.0} \frac{8.1}{50.0}$$

$$\frac{5.3}{50.0} \frac{5.8}{21.0} \frac{9.0}{15.0} \frac{9.2}{14.0} \frac{8.6}{10.0} 8.4 \frac{8.0}{13.0} \frac{8.4}{24.0} \frac{8.8}{30.0} \frac{8.5}{32.0} \frac{7.2}{34.0} \frac{7.7}{45.0} \frac{8.4}{50.0}$$

$$\frac{4.3}{50.0} \frac{2.8}{22.0} \frac{6.6}{16.0} \frac{6.5}{12.0} \frac{6.2}{9.0} 6.0 \frac{6.0}{11.0} \frac{6.4}{27.0} \frac{6.8}{28.0} \frac{6.5}{32.0} \frac{4.4}{35.0} \frac{4.4}{50.0}$$

$$\frac{2.8}{50.0} \frac{4.2}{19.0} \frac{7.8}{15.0} \frac{7.8}{12.0} \frac{7.0}{8.0} 6.7 \frac{6.6}{10.0} \frac{7.1}{22.0} \frac{7.8}{24.0} \frac{7.6}{27.0} \frac{5.0}{31.0} \frac{5.0}{50.0}$$

$$\frac{7.8}{50.0} \frac{8.0}{24.0} \frac{9.6}{23.0} \frac{10.0}{21.0} \frac{9.0}{18.0} 8.7 \frac{9.4}{10.0} \frac{11.0}{14.0} \frac{10.7}{17.0} \frac{8.7}{20.0} \frac{11.2}{50.0}$$

$$\frac{5.3}{50.0} \frac{4.6}{38.0} \frac{3.7}{35.0} \frac{1.5}{29.0} \frac{1.5}{15.0} 2.0 \frac{2.2}{7.0} \frac{8.6}{10.0} \frac{9.5}{14.0} \frac{12.0}{50.0}$$

+ H.I. - Rod ELEV.

907.98

197+00

04.8.

198+00

05.0.

199+00

06.0.

T.P. 9.05 916.37. 0.66 907.32.

200+00

08.1.

201+00

09.9.

+60

09.6.

202+00

08.9.

B.M. 2.80 913.57.

B.M. 2.71 916.28. 913.57

150

08.0.

203+00

07.6.

204+00

05.9.

+50

04.7.

T.P. 7.39 912.08. 11.59 904.69.

205+00

02.6.

H

K

RH

20

$\frac{4.5}{50.0}$	$\frac{4.8}{36.0}$	$\frac{5.0}{32.0}$	$\frac{3.2}{27.0}$	3.2	$\frac{3.3}{3.0}$	$\frac{8.6}{12.0}$	$\frac{11.7}{15.0}$	$\frac{12.6}{50.0}$
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$\frac{5.5}{50.0}$	$\frac{5.6}{27.0}$	$\frac{5.6}{22.0}$	$\frac{3.2}{18.0}$	3.0	$\frac{3.3}{11.0}$	$\frac{7.4}{18.0}$	$\frac{8.3}{21.0}$	$\frac{8.2}{31.0}$	$\frac{7.5}{50.0}$
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$\frac{5.7}{50.0}$	$\frac{6.0}{33.0}$	$\frac{5.7}{19.0}$	$\frac{3.4}{13.0}$	2.0	$\frac{3.0}{10.0}$	$\frac{2.4}{14.0}$	$\frac{5.5}{24.0}$	$\frac{5.2}{32.0}$	$\frac{4.2}{50.0}$
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$\frac{4.2}{50.0}$	$\frac{5.2}{28.0}$	$\frac{7.8}{25.0}$	$\frac{9.1}{21.0}$	$\frac{8.8}{18.0}$	$\frac{8.4}{14.0}$	8.3	$\frac{8.6}{17.0}$	$\frac{9.0}{20.0}$	$\frac{9.0}{22.0}$	$\frac{7.6}{25.0}$	$\frac{6.4}{35.0}$	$\frac{5.8}{50.0}$
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$\frac{2.6}{50.0}$	$\frac{1.8}{34.0}$	$\frac{5.4}{28.0}$	$\frac{6.7}{25.0}$	$\frac{6.5}{22.0}$	$\frac{6.7}{19.0}$	$\frac{6.4}{7.0}$	6.5	$\frac{6.8}{13.0}$	$\frac{7.3}{15.0}$	$\frac{7.5}{18.0}$	$\frac{7.1}{21.0}$	$\frac{5.2}{26.0}$	$\frac{4.6}{32.0}$	$\frac{4.1}{50.0}$
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$\frac{3.8}{50.0}$	$\frac{3.5}{34.0}$	$\frac{7.6}{28.0}$	$\frac{7.0}{23.0}$	$\frac{6.7}{9.0}$	6.8	$\frac{6.8}{12.0}$	$\frac{7.5}{15.0}$	$\frac{3.7}{26.0}$	$\frac{3.0}{32.0}$	$\frac{2.5}{56.0}$
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$\frac{4.6}{50.0}$	$\frac{4.7}{35.0}$	$\frac{6.8}{31.0}$	$\frac{8.2}{27.0}$	$\frac{8.3}{24.0}$	$\frac{7.8}{21.0}$	$\frac{7.7}{17.0}$	7.5	$\frac{7.6}{10.0}$	$\frac{8.0}{12.0}$	$\frac{8.2}{14.0}$	$\frac{7.4}{19.0}$	$\frac{5.3}{23.0}$	$\frac{3.5}{28.0}$	$\frac{2.8}{50.0}$
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202 + 50 = 12" Oak - RIGHT.

$\frac{4.2}{50}$	$\frac{4.2}{37}$	$\frac{9.2}{26}$	$\frac{9.0}{22}$	$\frac{8.5}{16}$	8.3	$\frac{9.1}{10}$	$\frac{9.0}{12}$	$\frac{8.5}{18}$	$\frac{5.7}{24}$	$\frac{4.0}{28}$	$\frac{3.3}{50}$
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$\frac{2.7}{50}$	$\frac{3.0}{34}$	$\frac{8.8}{26}$	$\frac{9.6}{24}$	$\frac{9.7}{21}$	$\frac{9.2}{19}$	$\frac{9.0}{14}$	9.7	$\frac{8.7}{13}$	$\frac{9.3}{15}$	$\frac{10.0}{16}$	$\frac{10.0}{18}$	$\frac{4.8}{23}$	$\frac{4.7}{33}$	$\frac{4.0}{50}$
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$\frac{2.4}{50.0}$	$\frac{3.0}{34}$	$\frac{3.6}{27}$	$\frac{4.3}{19}$	$\frac{4.0}{16}$	$\frac{10.7}{13}$	10.4	$\frac{10.3}{8}$	$\frac{10.8}{20}$	$\frac{11.3}{21}$	$\frac{11.5}{25}$	$\frac{10.8}{28}$	$\frac{7.5}{36}$	$\frac{7.1}{50}$
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$\frac{4.5}{50}$	$\frac{6.0}{31}$	$\frac{7.0}{16}$	$\frac{12.0}{11}$	$\frac{11.7}{7}$	11.6	$\frac{12.0}{14}$	$\frac{12.0}{26}$	$\frac{12.6}{28}$	$\frac{12.2}{34}$	$\frac{11.0}{36}$	$\frac{10.2}{50}$
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$\frac{4.0}{36}$	$\frac{5.3}{34}$	$\frac{6.4}{24}$	$\frac{6.5}{23}$	$\frac{8.0}{13}$	$\frac{8.5}{7}$	$\frac{10.7}{2}$	9.5	$\frac{9.0}{2}$	$\frac{9.4}{32}$	$\frac{11.4}{37}$	$\frac{11.4}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	-----	-----------------	------------------	-------------------	-------------------

3/4. + H.I. - Elov

912.08

150

900.5

206+00

897.3

T.P. 369 904.57. 11.20 900.88.

150

895.4

207+00

93.4

T.P. 5.75 900.22. 10.10 894.47.

150

90.3

208+00

88.0

+19.87 M.W.C.

208+9.39 P.T.

87.9

T.P. 182 895.30. 6.74 899.48.

B.M. 6.11 899.19. 889.20

SEE B-7

32	58	72	90	113	120	108	105	112	150
<u>50</u>	<u>36</u>	<u>29</u>	<u>19</u>	<u>8</u>	<u>7</u>	<u>10</u>	<u>28</u>	<u>43</u>	<u>50</u>

50	70	105	110	130	150	148	118	115	116
<u>50</u>	<u>37</u>	<u>27</u>	<u>19</u>	<u>9</u>	<u>148</u>	<u>8</u>	<u>17</u>	<u>19</u>	<u>37</u>

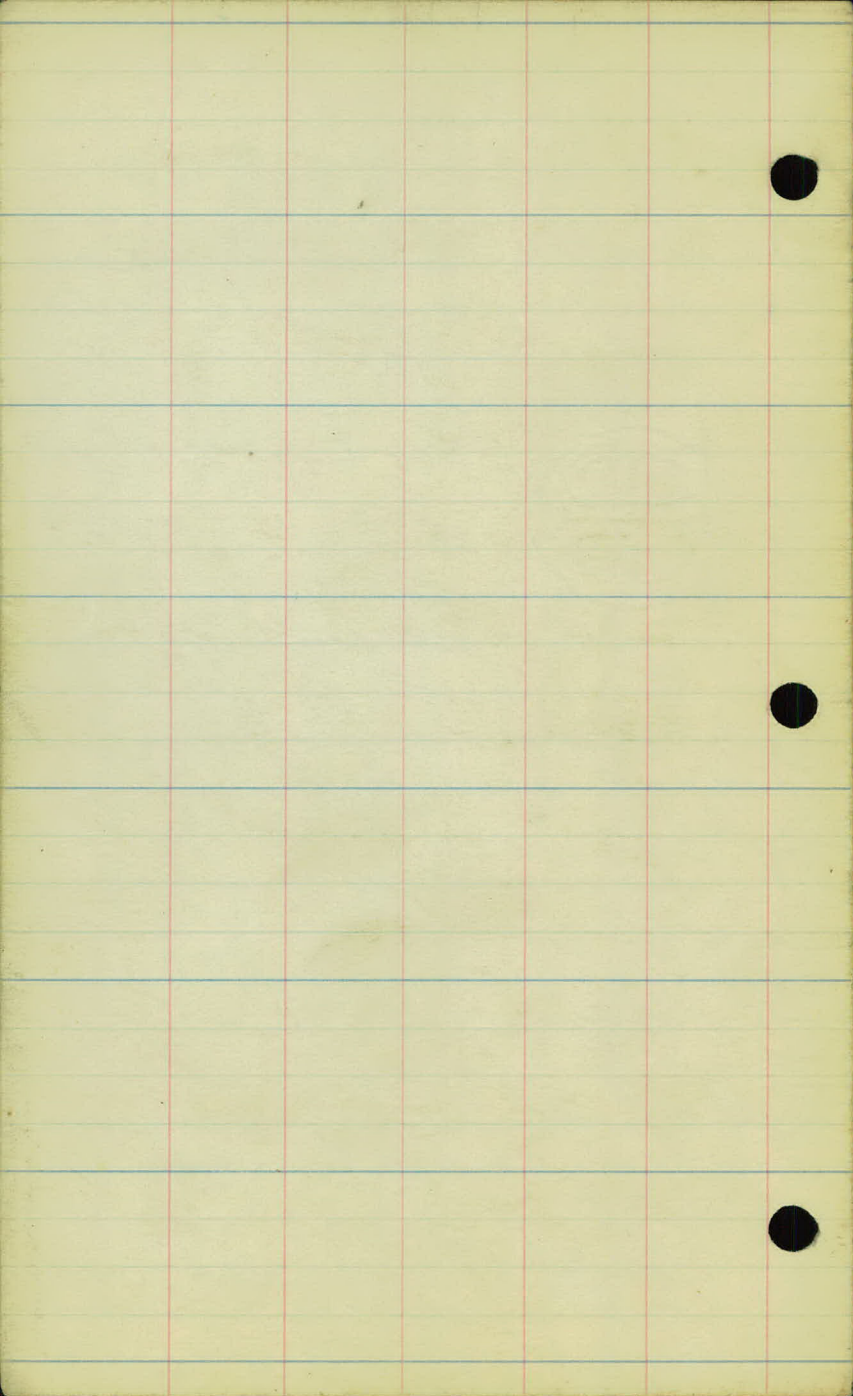
12	58	70	86	92	87	52	46	46
<u>50</u>	<u>20</u>	<u>15</u>	<u>7</u>	<u>92</u>	<u>12</u>	<u>21</u>	<u>30</u>	<u>46</u>

105	111	115	110	100	92	55	68
<u>50</u>	<u>7</u>	<u>112</u>	<u>16</u>	<u>24</u>	<u>30</u>	<u>34</u>	<u>40</u>

100	103	106	92	75	55	37	11
<u>50</u>	<u>50</u>	<u>14</u>	<u>4</u>	<u>19</u>	<u>37</u>	<u>44</u>	<u>50</u>

120	120	114	100	72	47
<u>50</u>	<u>34</u>	<u>122</u>	<u>17</u>	<u>21</u>	<u>45</u>

125	127	118	115	92	89
<u>50</u>	<u>26</u>	<u>123</u>	<u>21</u>	<u>37</u>	<u>47</u>



Анока Connection

Live Change

Station

Ang. ht. Ang. Rt.

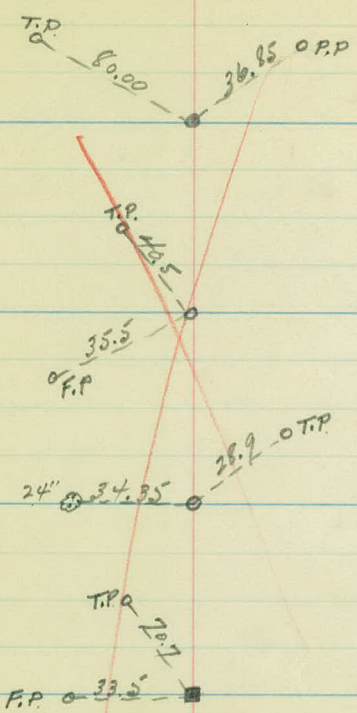
183+02.15 P.O.T

175+11.0 P.O.T

173+00.23 P.O.T = Old P.I

171+49.8 Mont.

171+22.0 = P.C. Sta 172+00.37 Original hinc.



Station Ang. ht. Ang. Rt

208+19.87 P.T.

205+49.25 P.I. 44°45'

198+24.82 P.C.

FROM R-2

193+71.1 P.T.

192+30.51 P.I. 44°42'

190+72.88 P.C.

TO ALIGN. - 5 24

Sta - Def

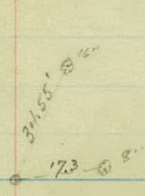
- 198224.32 - 0°00'
- 199+00 - 10°42'
- 200+00 - 3°57'
- 201+00 - 6°12'
- 202+00 - 8°27'
- 203+00 - 10°42'
- 204+00 - 12°57'
- 205+00 - 15°12'
- 206+00 - 17°27'
- 207+00 - 19°42'
- 208+00 - 21°57'
- +19.87 - 22°24'



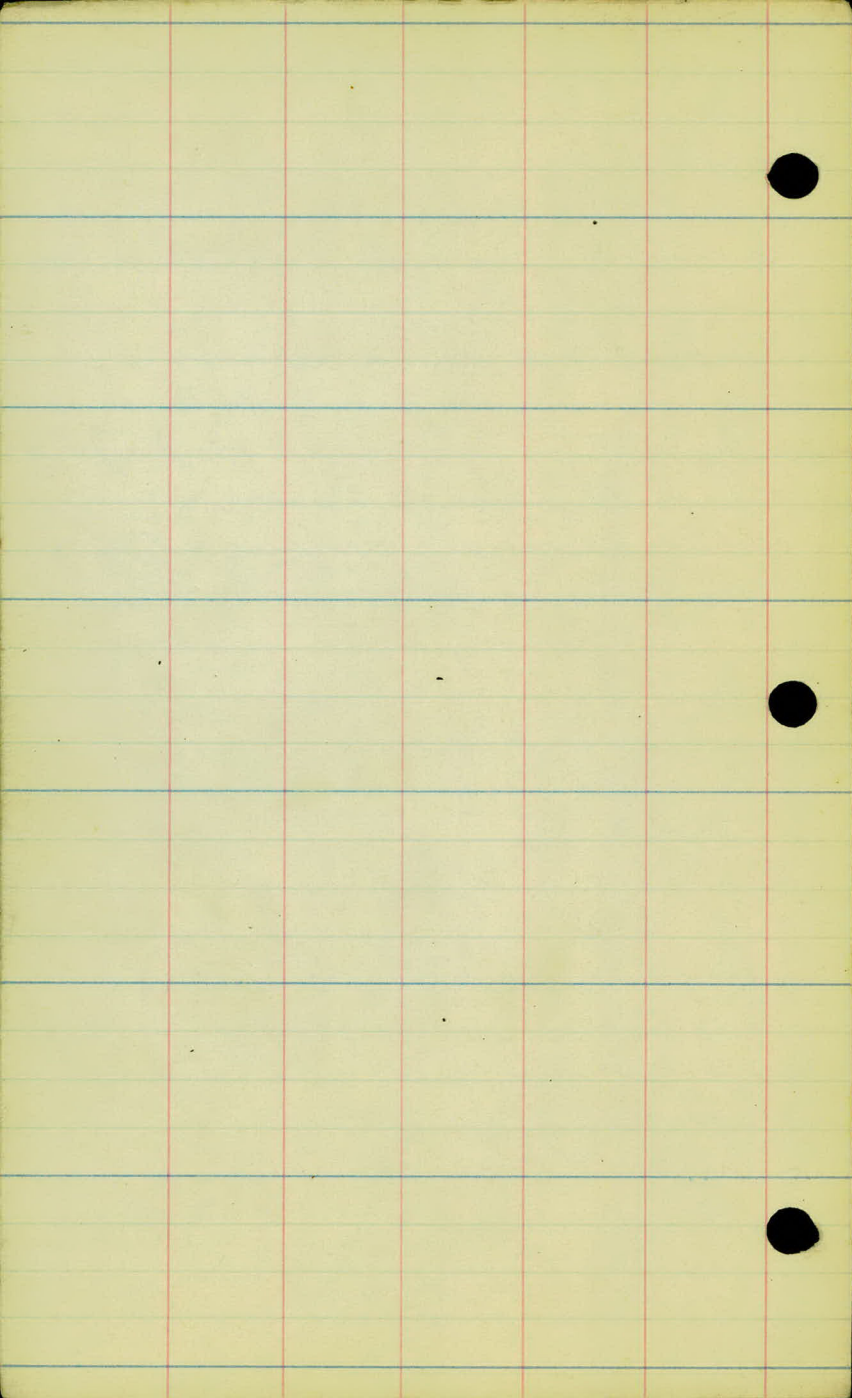
4°30' Curve Rt.
 $\Delta = 440.48'$
 Rad = 1293.57
 Tang = 524.93
 Length = 997.77.

Sta - Def

- 190472.86 - 0°00'
- 191+00 - 2°02'
- +50 - 5°47'
- 192+00 - 9°32'
- +50 - 13°17'
- 193+00 - 17°02'
- +50 - 20°47'
- +71.1 - 22°22'



15° Curve Lt.
 $\Delta = 440.44'$
 Rad = 383.07
 Tang = 157.63
 Length = 298.22.



+97-2" @ 30'
+60 P.P. 18.5

+58-2" @ 30'

+17-2" @ 30'

+85 P.P. 30'
+80-2" @ 30.5'

+42-2" @ 31'

+18 P.P. 18'

+99-2" @ 30'

+67-3" @ 30'
+58 F. line
+50 F. Cor. 24'
+49 P.P. 31'

33.2

33.5

34

Posture C

+94-2" @ 30'

+56-2" @ 30'

+25 T.P. 16'
+16-2" @ 30'

+78-5" @ 31'

+40-2" @ 31'

+99-2" @ 30'

+78 T.P. 16'
+68-4" @ 30.5'
+50 F. Cor. 16.5'

F.C. 16.5

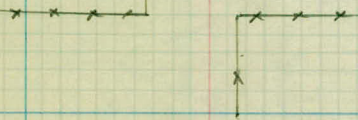
174
25

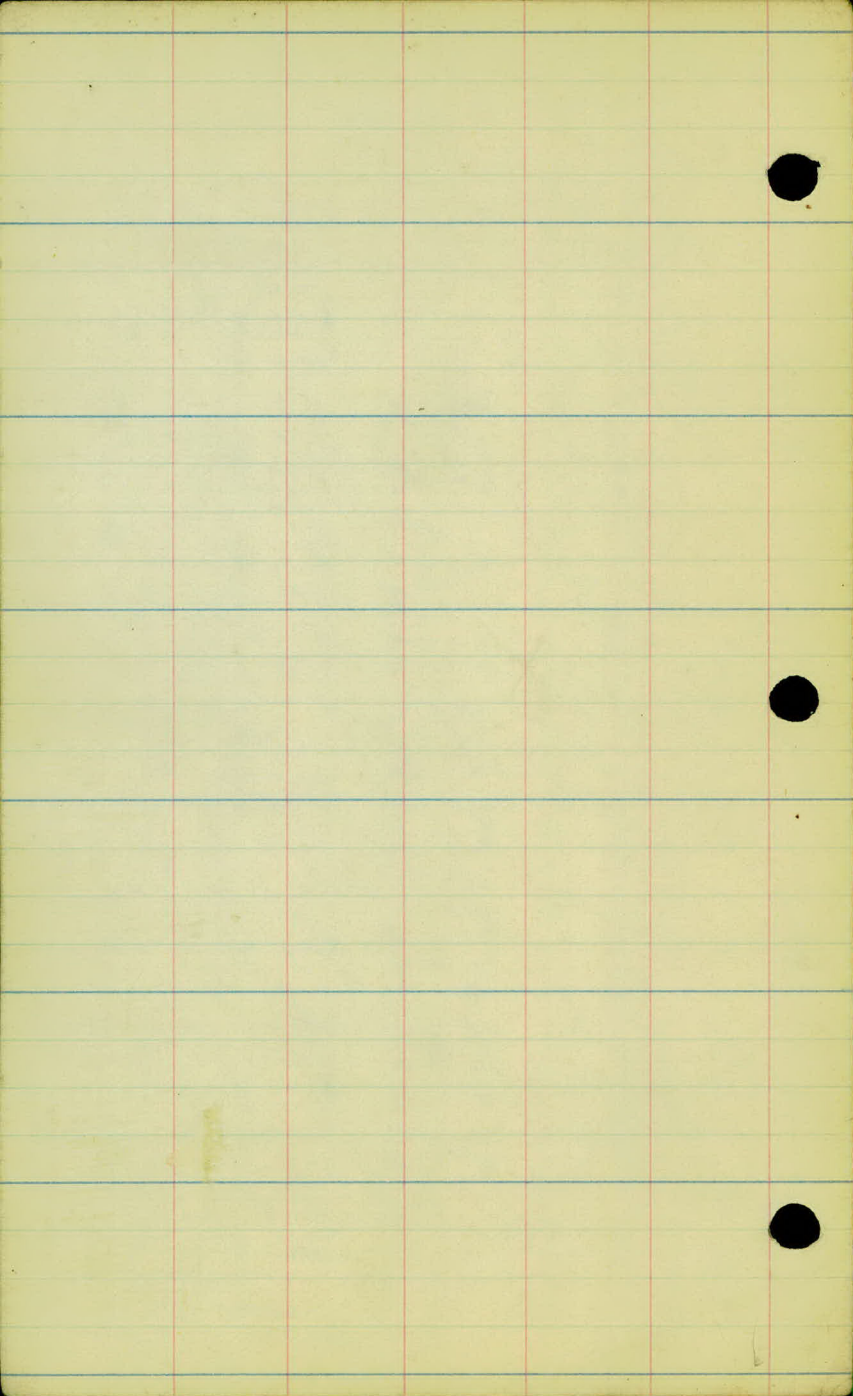
173

172

171

Calibrated





161
26

+94-2" @ 29'
+76 P.P. 29'
+55-2" @ 29'

+97-2" @ 28'
+55-2" @ 28'
+57 T.P. 14'

+19-2" @ 29'
+01 P.P. 20.5

+19-2" @ 28'

180

+44 P.P. 28.5

+44-2" @ 28'

+08-2" @ 29'
+93 End. P.

+17 T.P. 14.5
+07-2" @ 28'

179

+69-2" @ 29'
+37 P.P. 20
+31-2" @ 29'
+20 P.P. 29'

33
Y
Y
X
33

+68-2" @ 28'
+29-2" @ 29'

178

+86-4" @ 29'

Y

+59-2" @ 29'
+75 T.P. 15'

+48-3" @ 29'

Y

+49-4" @ 29'

+08 P.P. 19.5
+05-2" @ 30'

X

Cultivated

35

+05-2" @ 30'

177

+88 P.P. 29'

Y

+66-2" @ 30'

X

+66-2" @ 30'

+25-2" @ 30'

X

+25-2" @ 30'
+17 T.P. 15.5

33.5

176

+99-2" @ 30'
+57 P.P. 30'
+51-2" @ 30'
+47 P.P. 19'

Y

+97-2" @ 30'

Y

+48-2" @ 30'

X

+09-2" @ 30'

33.5

+10-2" @ 29'

175

+71-2" @ 30'

Y

+73 T.P. 15.5
+71-2" @ 30'

X

+56-2" @ 30'
+20 P.P. 30'

X

+38-2" @ 30'

174

33.5

Pasture. Road

4
P. 4 P. 1

7

P.P. 27.5

+49-6" @ 30.5

+41-6" @ 30

+73-4" @ 30

+42-5" @ 30
+36

+90-2" @ 30

+60-4" @ 30

+24-3" @ 30

+97-2" @ 30

+63 @ 2' 30

+37-2" @ 30

+96-2" @ 30

+67-2" @ 30

+37 P.P. 29

+41-2" @ 29

+07-2" @ 29
+03-P.P. 28.5

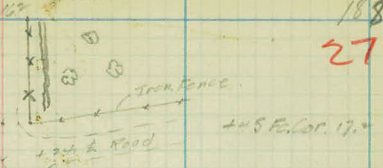
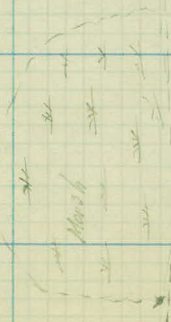
+94-2" @ 29
+69 P.P. 28

+37-2" @ 29

60W4

Helpo

+13 & Drive



+56 T.P. 11.5
 +74 M. 85.5 +74 P.P. 25.5
 +69 1" @ 25
 +66 P.P. 12
 +68 M.R. 5.5
 +38-2" @ 22
 +13 T.P. 17

+77-2" @ 27
 153 F.E
 +64 P.P. 27
 +61-2" @ 27
 +30-16" @ 26

+02 P.P. 12.5
 +95-2" @ 26
 +53 T.P. 17
 +64-16" @ 27
 +49 P.P. 28
 +51-12" @ 27

+92-2" @ 28
 +57-2" @ 28
 +59 P.P. 29
 +39 P.P. 14
 +36 P.P. 14
 +25-2" @ 28

+85-2" @ 28
 +48-2" @ 28
 +10-2" @ 28

+97 T.P. 14 P.P.
 +76-2" @ 28
 +54 Slow Sign 27
 +35-3" @ 28

Cultivated land

188
27

187

186

185

184

183

182

181

Rd. 47. & Rd. 74

4.0

00

4.0

4.0

6.0

10

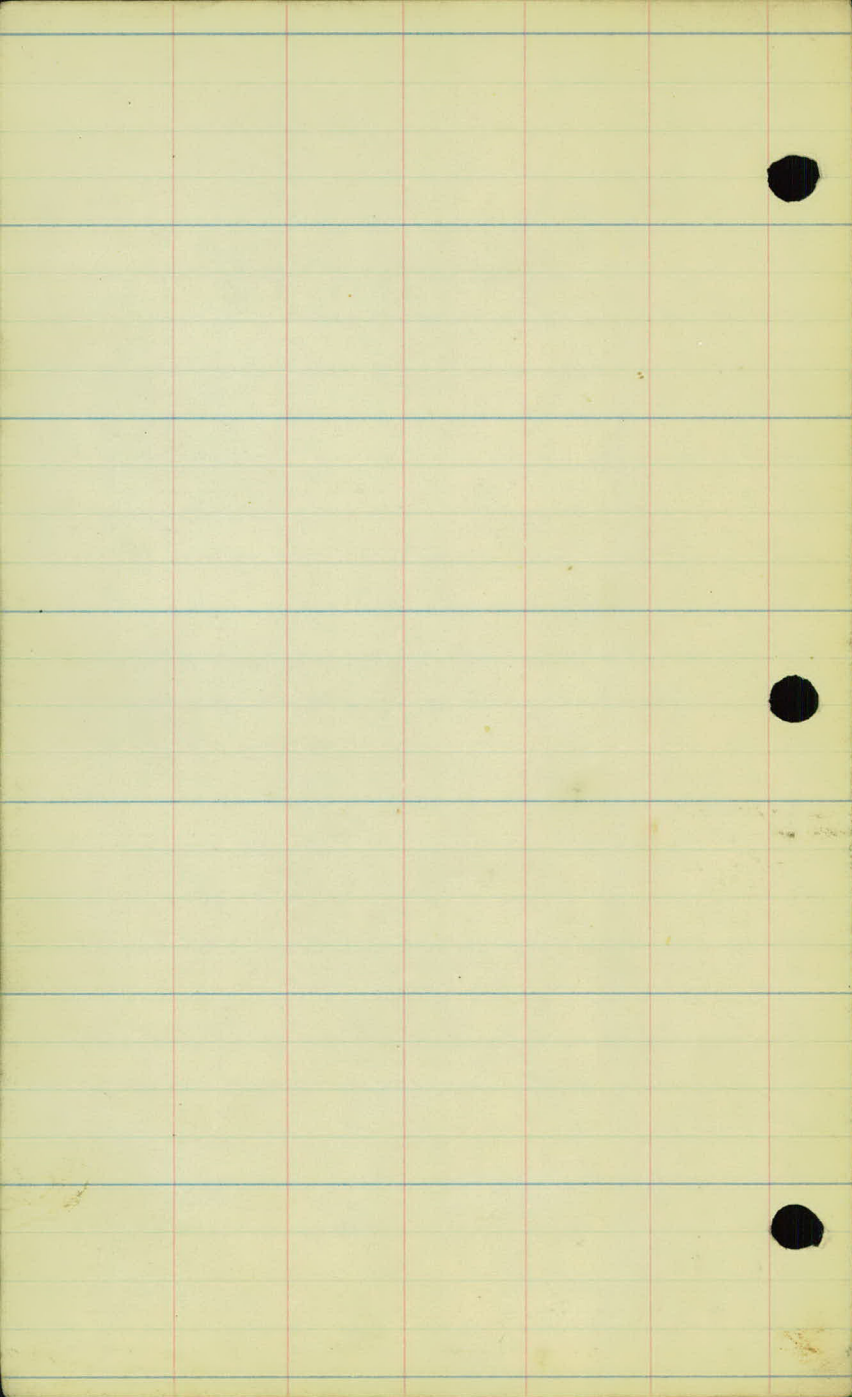
8.0

00

5.5

5

7.



+09 T.P. 22'
FL. 35.5 S.L. 21

+58 C. Hedge 33
+47 1/2 Drive
+32 FL 32
+37.5 drain 155-21 1/2
+24 - R.P. 19' C.V.

FL. 32' - S.L. 13 201

+60 Δ FL. 33'

FL. 27' S.L. 14'

+66 R.P. 23'
FL. 36 S.L. 16' 200

+73 - T.P. 16

+82 1/2 drive
+72 1/2 drive
12" C.V.
+62.5 drain 20 1/2 3/5

+29 - R.P. 22'
FL. 24' S.L. 13

FL. 35.5 S.L. 19'

+71 - T.P. 23'

+77 - G.P. 20'

+34 + Fence 37

FL. 29 S.L. 18

+15 Steel fence 30'
S.L. 12 198

+94 G.P. 25'

Cult. and yard

FL. 36 - S.L. 26

S.L. 4' 197

+10 - 41' Cul
FL. 47 Rd. 28

+42 @ 24-30'
+37 @ 20'
+23 @ 25'
12" C.V. + drain
+10 C.V. 185
315' 196
Rd 2

40 35'
+40 29

Woods

FL. 24

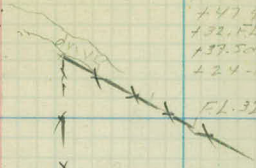
+36 - E.F. 36

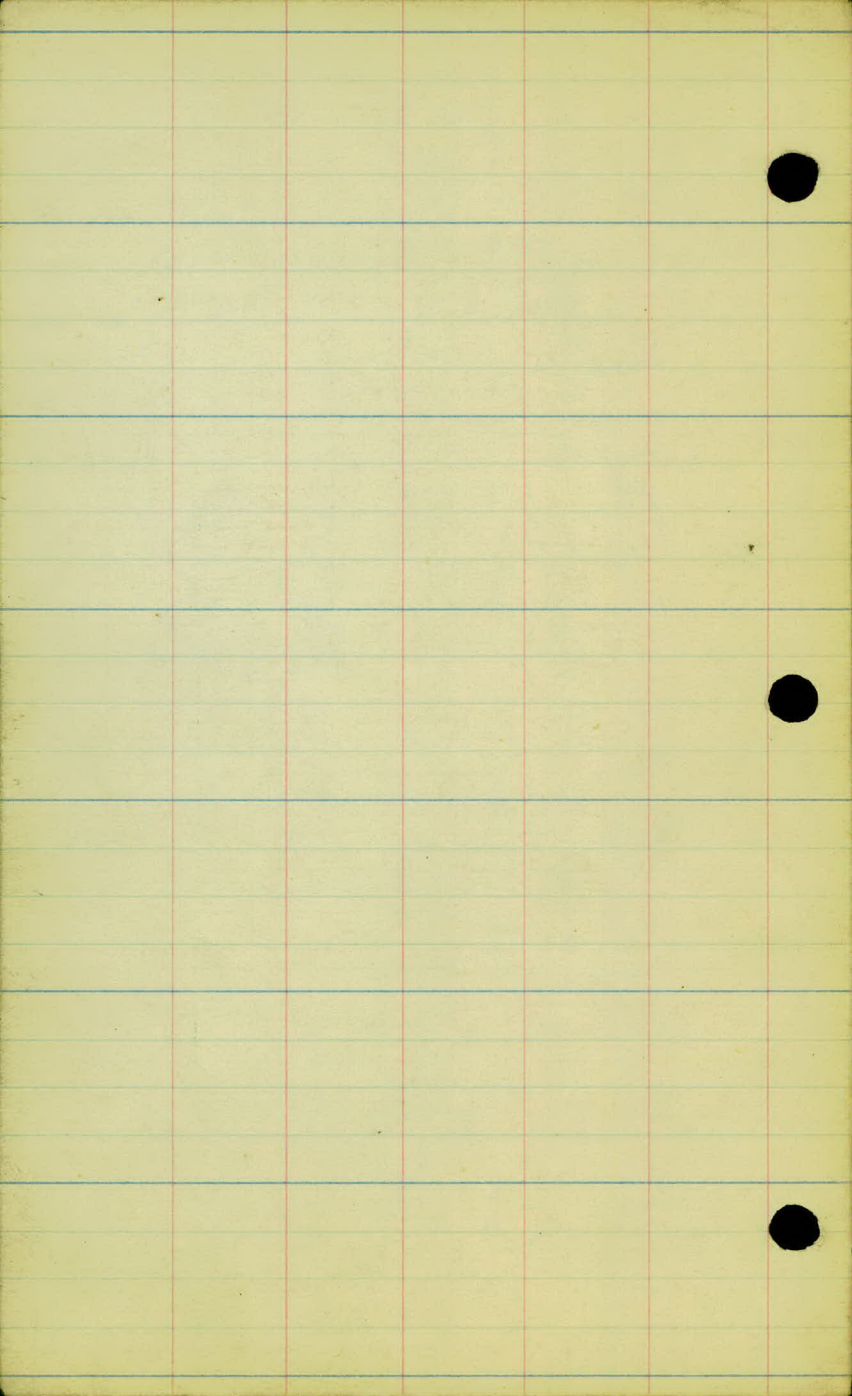
FL. 22 195

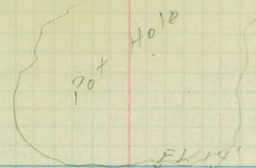
Pasture

Bush

X X X X X







+19-FL. 17-FL. 47'
FL. 45' 208

+72 T.P. 47'

FL. 4'

Pasture

+17 int. FL

Run Way

FL. 28-51-42 207
S.L. 23'

+50 FL. 17-51-28
S.L. 61'

FL. 21'

+120 T.P. 32'
+110 P.P. 55'
S.L. 19' 206
S.L. 9'

Cattle Runway

FL. +39 104

S.L. 3'

FL. 7'-FL. 36

Pasture

Meadow

S.L. 32' 205

+85 P.P. 33'

+33 T.P. 9'

+134 M. br 26
+21 S. drive 28'
+32 S. drain 39'
+104 Tree 39' 208
+107 S. drive 39' 207
S.L. 30 204

S.L. 11' FL. 29

150 S.L. 17'

+173 P.P. 25'

150 S.L. 15'

FL. 33 S.L. 19

Pasture

Gulf and Yard

S.L. 13' 203

+93 S. drive
+86 S. drain 15' 204
cm

+700
+19 T.P. 195

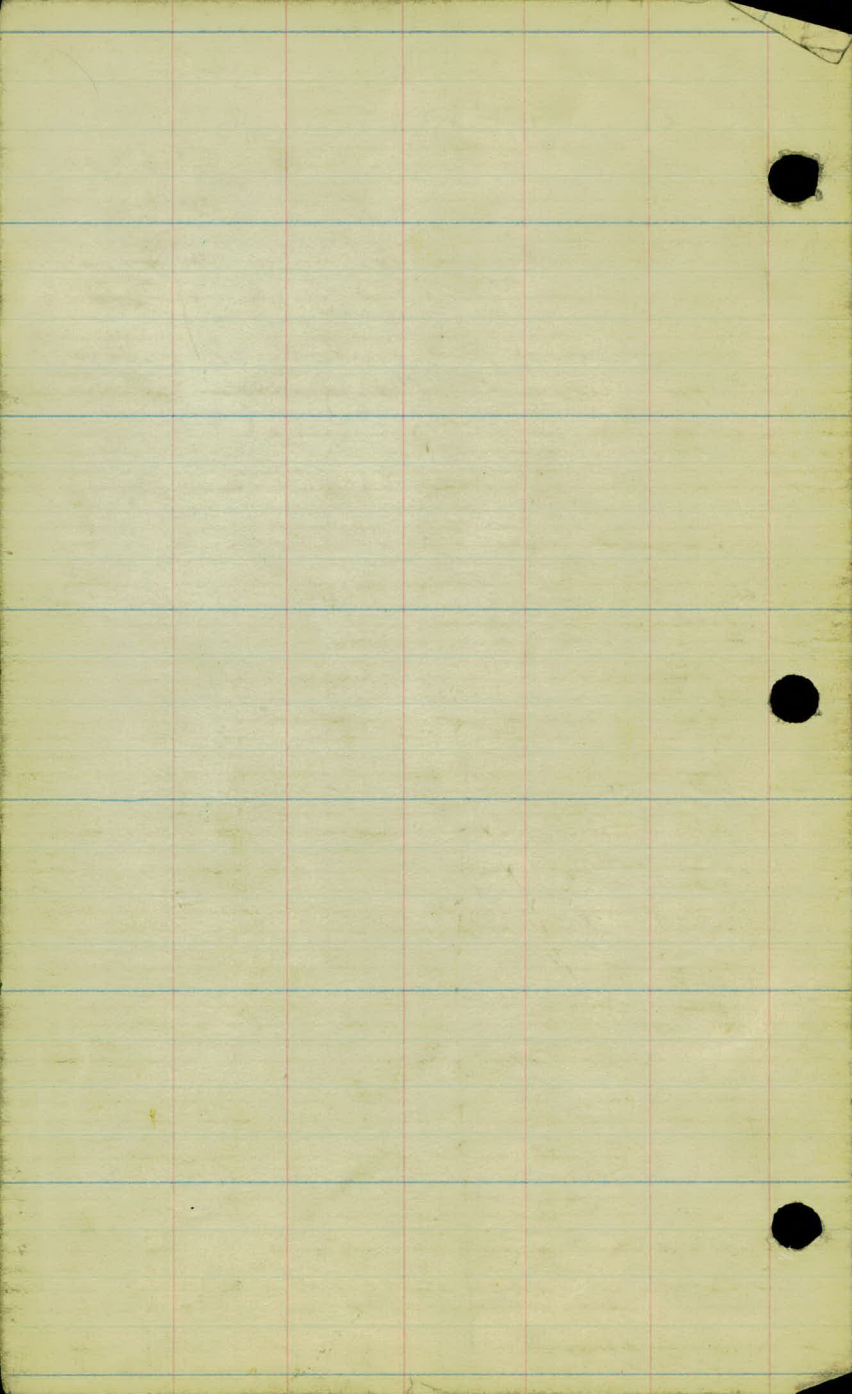
+76 P.P. 18
+31 Tree 24
+23 E.o. H. 196.3
+28 + FL. 25

FL. 1/5 S.L. 21

Cult. Pasture

Gulf

S.L. 10' H. 199.31 202



Proj # 26-62.
Line Revision from
Sta. 259+13⁰⁰ to Sta. 351+59

Crane
McIntyre
Bertram
Frankc.

Sta. Point Lt. Rt.

247+89³⁵ P.O.T.

247+74⁰⁰ P.O.T.

N. 10° 35' W.

262+86³⁷ P.T.

261+00 P.I.

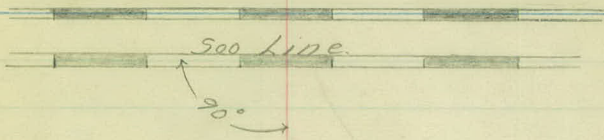
7°-28'

x

259+13⁰⁴ P.C.

P.O.T.

N. 18° 05' W.



257+13⁹³
 260 - 0°-52'
 261 - 1°-52'
 262 - 2°-52'
 286³⁷ - 4°-44'

A - 7°-28'
 D - 2° 1/2'
 T - 184 ⁹⁶
 L - 373 ³⁵
 R - 2864 ⁹³

Sta. Point Lt. 187.

278+17²³ P.O.T.

N 49° 55' W.

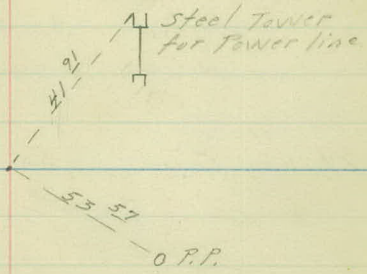
277+90²³ P.T.

274+13²⁵ P.I. 39° 20'

*

270+03⁵⁷ P.C.

N 10° 35' W.



270+03⁵⁷

- 271 - 2°-25'
- 272 - 4°-55'
- 273 - 7°-25'
- 274 - 9°-55'
- 275 - 12°-25'
- 274 - 14°-55'
- 277 - 17°-25'
- +90²³ - 19°-40'

- A - 39°-20'
- D - 5° 14'
- T - 409⁶⁸ ✓
- L - 786⁴⁶ ✓
- R - 1146²⁸

Sta. Point Lt. Rt.

298783²¹ P.T.

N. 18° - 50' E

292792³⁵ P.I.

68° - 45'

x

291724⁶⁵ P.O.S.T.

285708²¹ P.C.

N. 49° - 55' W

285-108²¹

286 - 2°-18'

287 - 4°-48'

288 - 7°-18'

P.O.C. 289 - 9°-48'

290 - 12°-18'

291 - 14°-48'

292 - 17°-18'

293 - 19°-48'

294 - 22°-18'

295 - 24°-48'

296 - 27°-18'

297 - 29°-48'

298 - 32°-18'

183²¹ - 34°-22⁵'

A - 68°-45'

D - 5°-11'

T - 784¹⁴

L - 1375⁰⁰

R - 1146²⁸

Sta. Point Lt. Rt.

310+52⁰² P.T.

18'
N. 7° - 58' W.

307+95⁴⁰ P.I. 26°-08'

X

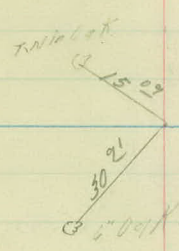
305+29³⁶ P.C.

N. 14° - 50' E.

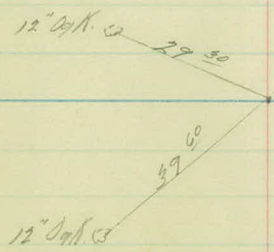
303+36¹⁰ P.O.T.

305729⁰⁴

- 306 - 1°-46'
- 307 - 4°-16'
- 308 - 6°-46'
- 309 - 9°-16'
- 310 - 11°-46'
- 152⁰² - 13°-04'



- A - 26°-08'
- D - 5°-~~17~~' ✓
- T - 266⁰⁴
- L - 522⁶⁶ ✓
- R - 1146²⁸



Sta Point Lt Rt

329+01⁹⁰ P.T.

N00°-09'E
~~N 00° 09' E~~

327+15⁹⁰ P.T.

7°-27'

X

325+29⁴⁰ P.C.

318+60 P.O.T

18°
N 7°
~~54° W~~

312+43⁹⁰ P.O.T

325 + 27⁴⁰

326 - 0°-42⁴

327 - 1°-42⁴

328 - 2°-42⁴

329 - 3°-42⁴

+ 01⁹⁰ - 3°-42⁴

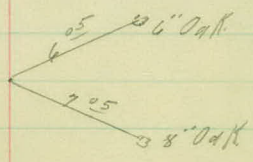
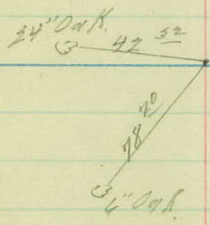
Δ - 7°-27'

D - 2°-11'

T - 186⁵⁰ ✓

L - 372⁵⁰ ✓

R - 2864⁹⁵



Sta. Point Lt. Rt.

TO ALIGN-12

374+11⁹² P.O.T.

Egva.

351+73³⁰ P.O.T.

351+59⁴¹ =

351+40⁴⁵ P.T.

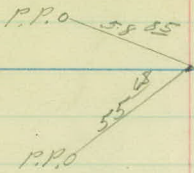
347+70⁶⁰ P.I. 38-31

343+70¹² P.C.

333+00 P.O.T.

N 38° 22' W
N. 38° - 30' W.

N 00° 09' E
N. 00° - 14' E.



343 + 70¹²

344 - 0°-45'

345 - 3°-15'

346 - 5°-45'

347 - 8°-15'

348 - 10°-45'

349 - 13°-15'

350 - 15°-45'

351 - 18°-15'

142⁴⁵ - 19°-15'

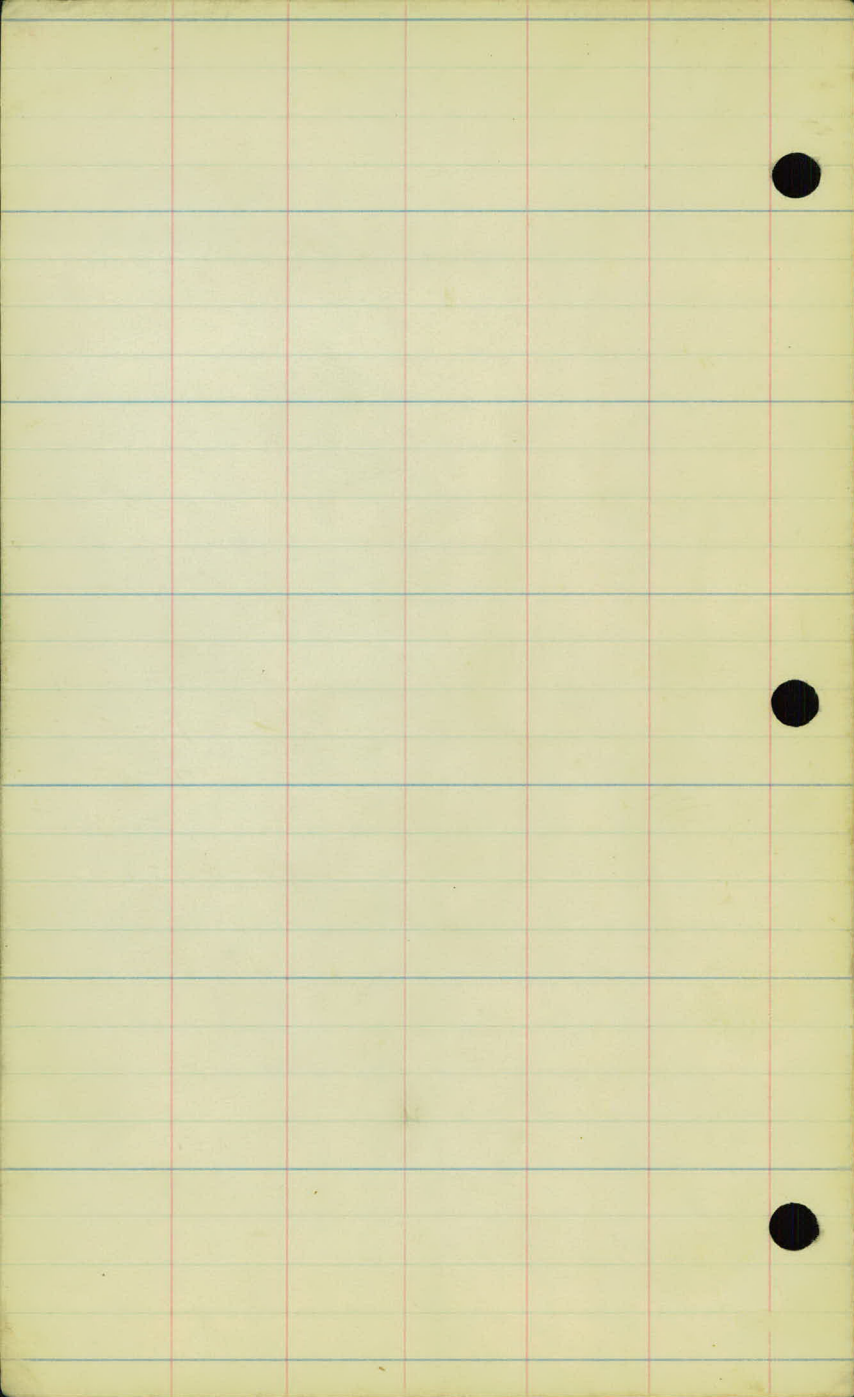
A - 38°-51'

D - 5°-11'

T - 400⁴⁸ ✓

L - 770³⁵ ✓

R - 1146²⁸



Proj. #46-62
Center line levels and
X sections from Sta. 259+36 to
Sta. 351+59th.

FROM B-19

Sta.	t	H. I.	-	Mod.	Flex.
B.M.	0.49	941.45	✓	940.96	✓
T.P.	0.51	929.67	✓	12.29	929.16 ✓
T.P.	3.94	921.53	✓	12.08	917.59 ✓
259+34				6.5	915.0
+50				5.0	16.5
260				3.3	18.2
T.P.	4.51	924.32	✓	1.72	919.81 ✓
+50				2.8	21.5
+75				1.0	23.3
261				1.8	22.5
+60				4.8	19.5
262				8.7	15.4
T.P.	4.71	918.64	✓	10.37	913.95 ✓
+50				9.9	10.8
263				12.8	05.9
T.P.	1.07	908.01	✓	11.72	906.94 ✓
+45				5.5	02.5
264				4.3	03.7
+36				4.8	03.2

Spk in 15" Oak 40 Lt. Stq. 254 + 85.

MT.

10.3	82		4.2	3.2
<u>50</u>	<u>33</u>	5.0	<u>2.3</u>	<u>50</u>

Above H.I.

11.5	49		1.4	+0.7
<u>50</u>	<u>14</u>	3.3	<u>2.5</u>	<u>50</u>

Above H.I.

13.6	93	4.7		+1.4	+4.4
<u>50</u>	<u>35</u>	<u>15</u>	2.8	<u>3.2</u>	<u>50</u>

Above H.I.

12.4	84		+3.2	+6.6
<u>50</u>	<u>28</u>	1.8	<u>2.8</u>	<u>50</u>

Above H.I.

14.5	12.0	6.0		1.6	+1.3
<u>50</u>	<u>39</u>	<u>10</u>	4.8	<u>3.2</u>	<u>50</u>

Above H.I.

17.3	14.2	11.9		3.8	+0.8
<u>50</u>	<u>35</u>	<u>17</u>	8.7	<u>3.8</u>	<u>50</u>

Above H.I.

18.7	15.0	7.9		6.0	1.3	+1.0
<u>50</u>	<u>32</u>	<u>21</u>	7.9	<u>7.4</u>	<u>34</u>	<u>50</u>

25.3	22.6	15.7		10.5	4.7
<u>50</u>	<u>39</u>	<u>17</u>	12.8	<u>21</u>	<u>50</u>

Above H.I.

17.7	14.8	10.5		1.5	+2.2
<u>50</u>	<u>37</u>	<u>19</u>	5.5	<u>2.3</u>	<u>50</u>

17.5	15.2	9.8		0.9	+1.4	+3.8	+5.1
<u>50</u>	<u>39</u>	<u>19</u>	4.3	<u>2.0</u>	<u>31</u>	<u>41</u>	<u>50</u>

18.2	15.8	7.4		0.8	+3.6
<u>50</u>	<u>47</u>	<u>17</u>	4.8	<u>2.5</u>	<u>50</u>

		H.I.	-	Red	Elev.
549	+	908.01 ✓			
+69				7.9	900.1
T.P.	0.44	896.24 ✓	12.21	895.80 ✓	
245				9.8	892.5
+20				8.7	87.4
+56	Edge of Pond			10.8	85.5
244				10.8	85.5
+75	Edge of Pond			10.8	85.5
267				10.4	84.1
+25				6.7	89.4
T.P.	12.93	902.75 ✓	0.46	895.80 ✓	
T.P.	12.32	920.89 ✓	0.14	908.57 ✓	
+64 ✓				5.0	915.9
+71 ²⁵	Top of Rail			4.08	16.81
+76 ³⁵	Top of Rail			4.04	16.85
+87 ⁰	Top of Rail			3.89	17.80
+91 ²	Top of Rail			3.89	17.88

Lt.

Rt.

20.7	19.2	11.8		4.9	2.2
65	50	18	7.7	20	50

Edge of Pond

Top of Ice	10.7	10.6	7.4	6.3	1.5	+4.1	+5.5
	50	42	24	10	3.8	8	31

Edge of Lake

Top of Ice	10.8				3.6	+2.8	+5.4
	48			2.7	17	35	50

On Ice

10.8		10.2	7.6	4.8
50	10.8	23	35	50

Edge of Pond

On Ice	10.8				10.8	7.7	7.7	4.0
	50	11.8			19	39	47	60

10.7		7.4	6.1
50	10.2	71	50

7.5	6.4		6.7	3.8
50	35	6.7	23	50

5.0		4.5
50	5.0	50

4.70	4.42	4.24		3.83	3.57	2.95
200	100	50	4.08	50	100	200

4.67	4.36	4.21		3.79	3.55	2.94
200	100	50	4.04	50	100	200

4.67	4.39	4.14		3.55	3.29	2.52
200	100	50	3.89	50	100	200

4.70	4.58	4.18		3.57	3.27	2.54
200	100	50	3.89	50	100	200

S + 9. + H. L. - Prod. E/Ex.

920.89 ✓

248 ✓ 5.5 915.4

T.P. 0.62 909.78 ✓ 11.73 909.14 ✓

T.P. 0.44 898.23 ✓ 12.01 897.77 ✓

T.P. 9.01 895.11 ✓ 12.13 886.10 ✓

+35 6.7 88.4

+50 10.4 84.7

B.M. 3.70 891.41 ✓

269 11.8 83.3

+50 10.1 85.0 ✓

270 7.1 86.0 ✓

+50 8.4 86.7 ✓

271 10.5 84.6 ✓

+29 12.9 82.8 ✓

272 8.5 86.6 ✓

+54 0.2 94.9 ✓

T.P. 9.44 900.70 ✓ 3.75 891.34 ✓

273 6.4 894.4 ✓

Lt.

Rt.

$\frac{5.5}{50}$			$\frac{4.9}{50}$
	5.5		

$\frac{6.6}{50}$			$\frac{4.7}{50}$
	6.7		

$\frac{8.7}{50}$			$\frac{8.9}{50}$
	10.4		

Spk. in 24" Oak 150 N. Sta. 268+72.

$\frac{2.9}{50}$	$\frac{11.2}{24}$	11.8	$\frac{11.6}{28}$	$\frac{11.4}{50}$
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$\frac{6.1}{50}$	$\frac{8.3}{28}$	10.1	$\frac{11.9}{28}$	$\frac{12.0}{50}$
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$\frac{2.9}{50}$	$\frac{4.6}{28}$	9.1	$\frac{11.7}{28}$	$\frac{12.1}{50}$
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$\frac{0.9}{50}$	$\frac{2.1}{48}$	$\frac{6.2}{14}$	8.4	$\frac{10.1}{24}$	$\frac{12.4}{50}$
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$\frac{4.6}{50}$	$\frac{6.9}{37}$	$\frac{9.4}{7}$	10.5	$\frac{11.7}{24}$	$\frac{12.0}{41}$	$\frac{11.7}{50}$
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$\frac{7.1}{50}$	$\frac{8.8}{40}$	$\frac{14.1}{5}$	12.3	$\frac{12.8}{33}$	$\frac{12.9}{50}$
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$\frac{2.3}{50}$	$\frac{5.4}{28}$	8.5	$\frac{10.3}{32}$	$\frac{10.9}{50}$
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Above H.I.

$\frac{+5.8}{50}$	$\frac{+3.1}{28}$	0.2	$\frac{4.4}{35}$	$\frac{7.7}{50}$
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Above H.I.

$\frac{+2.0}{50}$	$\frac{0.0}{30}$	6.4	$\frac{8.6}{12}$	$\frac{9.6}{24}$	$\frac{9.7}{50}$
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Sta.	+	H.I.	-	Red.	Elev
		900.80 ✓			
+38				7.0	893.8 ✓
+75				4.3	896.5 ✓
274				6.5	94.3 ✓
T.P.	0.85	892.00 ✓	9.65	891.15 ✓	
+50				5.3	86.7 ✓
275				10.8	81.2 ✓
+50				12.8	79.2 ✓
276				12.7	79.3 ✓
276 +54 ²⁴				11.9	80.1 ✓
T.P.	1.15	892.38 ✓	0.77	891.23 ✓	
T.P.	1.70	885.01 ✓	9.07	883.31 ✓	
B.M.	3.73	886.18 ✓	2.57	882.44 ✓	882.45 ✓
T.P.	9.98	895.52 ✓	0.64	885.54 ✓	
T.P.	11.40	898.20 ✓	8.72	886.80 ✓	
277				85.9 ✓	
+50				91.4 ✓	
278				95.9 ✓	

1/12/36
42

Lt.

Rt.

$\frac{1.5}{50}$ $\frac{2.1}{33}$ $\frac{4.3}{17}$ 7.0 $\frac{9.0}{30}$ $\frac{8.8}{38}$ $\frac{8.0}{50}$

$\frac{4.5}{50}$ $\frac{3.3}{30}$ 4.3 $\frac{7.5}{34}$ $\frac{7.0}{50}$

$\frac{7.6}{50}$ $\frac{6.8}{35}$ 4.5 $\frac{7.7}{37}$ $\frac{6.7}{50}$

$\frac{10.3}{50}$ $\frac{10.9}{27}$ 10.8 $\frac{10.6}{27}$ $\frac{10.3}{50}$

$\frac{12.7}{50}$ $\frac{12.9}{27}$ 12.8 $\frac{12.8}{27}$ $\frac{12.8}{50}$

$\frac{12.5}{50}$ $\frac{12.7}{32}$ 12.7 $\frac{12.7}{24}$ $\frac{12.8}{50}$

$\frac{11.6}{50}$ $\frac{11.8}{25}$ 11.9 $\frac{12.1}{27}$ $\frac{12.6}{50}$

Spk in Twin Oak 38 Lt. 281427
Spk in Twin Oak 44 Lt. 281450

W.H.C.
A.L.P.
M.G. } 2-26-26
H.B.

$\frac{12.9}{50}$ $\frac{12.6}{30}$ $\frac{12.3}{30}$ $\frac{14.2}{36}$ $\frac{15.1}{50}$

$\frac{2.3}{40}$ $\frac{7.0}{23}$ 6.8 $\frac{7.9}{33}$ $\frac{10.0}{50}$

$\frac{1.0}{50}$ $\frac{2.1}{25}$ 7.3 $\frac{3.3}{31}$ $\frac{5.1}{50}$

Sta	+ H.I	- Elev.
	898.20 ✓	
278+40		97.1
T.P.	1.80 892.26 ✓	7.74 890.46 ✓
279		89.5
40		82.9
280		80.0
T.P.	3.61 883.28 ✓	12.59 879.67 ✓
281		78.7
	0.83 883.28 ✓	0.83 882.45 ✓
281+50		79.8
282+00		80.1
283+00		78.7
284+00		77.0
285		76.0
403	2 + Bottom ditch 3' Wide.	74.9
286		77.0
287		77.9
T.P.	11.34 890.18 ✓	4.44 878.84 ✓

Lt. L Pt.

$\frac{+05}{9870}$ $\frac{50}{50}$	$\frac{90}{72}$	$\frac{10}{27}$	1.1	$\frac{21}{31}$	$\frac{47}{50}$
$\frac{0.5}{50}$	$\frac{2.6}{22}$	28		$\frac{2.6}{29}$	$\frac{41}{50}$
$\frac{63}{50}$	$\frac{87}{24}$	9.4		$\frac{10.0}{32}$	$\frac{107}{50}$
$\frac{89}{50}$	$\frac{112}{23}$	$\frac{12.0}{2}$		$\frac{13.0}{32}$	$\frac{136}{50}$
$\frac{17}{50}$	$\frac{3.8}{22}$	4.6			$\frac{54}{50}$

Spt. in Twin Dak 30' Lt. 281+27

$\frac{05}{50}$	$\frac{24}{25}$	3.5			$\frac{11.2}{50}$
$\frac{04}{50}$	$\frac{19}{25}$	2.2		$\frac{1.3}{28}$	$\frac{5.0}{50}$
$\frac{17}{50}$	$\frac{3.3}{23}$	4.6		$\frac{57}{29}$	$\frac{63}{50}$
$\frac{47}{50}$	$\frac{1.5}{24}$	6.3		$\frac{7.2}{35}$	$\frac{6.8}{50}$ $\frac{21}{68}$ $\frac{8.3}{71}$ = Lt Bott Ditch.
$\frac{49}{50}$	$\frac{7.2}{30}$	7.3		$\frac{6.6}{28}$	$\frac{6.8}{50}$

Lt Bott Ditch

$\frac{82}{72}$	$\frac{6.8}{68}$	$\frac{6.8}{50}$	$\frac{6.7}{33}$	6.3	$\frac{5.9}{25}$	$\frac{6.0}{50}$
$\frac{67}{50}$	$\frac{6.3}{28}$	5.4		$\frac{4.8}{28}$	$\frac{11.3}{50}$	

Sta.	+	H.I.	-	E lev.
288		890.18 ✓		77.0
+50				79.5
289				81.4
+34				83.2
290				81.3
+50				79.9
291				78.4
292				77.5
T.P.	6.89	885.27 ✓	11.80	878.38 ✓
293				77.1
294				77.7
+50				79.5
B.M.	2.67	885.24 ✓	2.60	882.67 ✓
295				82.2

Station	+	H.I	-	Elev.
		885.24 ✓		
295+15				83.2 ✓
+35				94.8
296+00				94.8
T.P.	11.95	894.78 ✓	2.41	882.83 ✓
295+15				53.2
T.P.	5.00	899.57 ✓	0.21	894.57 ✓
295+55				94.8 ✓
296+00				94.8 ✓
+45				93.8 ✓
297+00				88.5 ✓
T.P.	2.65	891.44 ✓	1.78	888.79 ✓
+35				85.8 ✓
298+00				83.9 ✓
+50				81.6 ✓
299				79.2 ✓
T.P.	4.80	885.03 ✓	11.21	880.23 ✓

A. L Rt.

cont'd $\frac{20}{50}$ $\frac{3.5}{28}$ $\frac{5.5}{50}$

+9.6 cont'd $\frac{13}{32}$ $\frac{4.0}{50}$

+9.6 cont'd $\frac{17}{50}$

$\frac{4.5}{50}$ $\frac{7.5}{29}$ (11.6)

$\frac{2.8}{50}$ $\frac{3.0}{36}$ $\frac{4.8}{50}$

$\frac{3.9}{50}$ $\frac{4.6}{28}$ $\frac{4.8}{50}$ $\frac{5.2}{25}$

$\frac{4.5}{50}$ $\frac{5.6}{30}$ $\frac{5.8}{50}$ $\frac{2.1}{29}$ $\frac{5.6}{39}$ $\frac{12.0}{50}$

$\frac{8.2}{50}$ $\frac{9.3}{27}$ $\frac{11.1}{50}$ $\frac{12.4}{30}$ $\frac{14.9}{50}$

$\frac{2.7}{50}$ $\frac{3.4}{32}$ $\frac{5.6}{50}$ $\frac{7.0}{25}$ $\frac{8.7}{50}$

$\frac{4.5}{50}$ $\frac{5.3}{27}$ $\frac{7.5}{50}$ $\frac{9.4}{26}$ $\frac{11.0}{50}$

$\frac{8.1}{50}$ $\frac{9.5}{25}$ $\frac{9.8}{50}$ $\frac{11.5}{28}$ $\frac{12.5}{50}$

$\frac{10.9}{50}$ $\frac{11.9}{24}$ $\frac{12.2}{50}$ $\frac{14.0}{35}$ $\frac{13.9}{50}$

Station	+	H.I	-	E lev.
		885.03 ✓		
300				77.8
301				78.8
+50				80.9
+80				83.2
302+00				86.2
+38				89.1
303				89.0
+36				87.4
T.P.	11.77	894.62 ✓	2.18	882.85 ✓
T.P.	9.30	902.93 ✓	0.99	893.63 ✓
301+80				87.7
302+00				86.2
+38				89.1
303+00				89.0
T.P.	1.25	894.86 ✓	9.30	893.63 ✓

$\frac{6.7}{50}$	$\frac{21}{30}$	7.2	$\frac{77}{25}$	$\frac{8.6}{50}$
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$\frac{57}{50}$	$\frac{57}{23}$	$\frac{62}{25}$	$\frac{76}{29}$	$\frac{82}{50}$
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$\frac{10.9}{50}$	$\frac{0.2}{33}$	$\frac{2.1}{19}$	4.1	$\frac{6.8}{30}$	$\frac{76}{50}$
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cont'd	$\frac{0.0}{6}$	$\frac{1.8}{1}$	$\frac{4.5}{17}$	$\frac{7.2}{50}$
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- 1.2 cont'd	$\frac{2.0}{9}$	$\frac{4.8}{21}$	$\frac{7.4}{50}$
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- 4.1 cont'd	$\frac{0.8}{7}$	$\frac{2.7}{18}$	$\frac{6.2}{35}$	$\frac{7.2}{50}$
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- 4.0 cont'd	$\frac{3.3}{76}$	$\frac{6.0}{36}$	$\frac{7.4}{50}$
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- 2.4 cont'd	$\frac{2.0}{11}$	$\frac{6.0}{31}$	$\frac{7.5}{50}$
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$\frac{2.0}{50}$	$\frac{8.6}{31}$	(19.7)
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$\frac{11.2}{904.1}$	$\frac{1.3}{37}$	$\frac{10.0}{75}$	16.7
$\frac{50}{50}$			

$\frac{12}{50}$	$\frac{3.9}{35}$	$\frac{7.8}{12}$	$\frac{10.1}{5}$	13.8
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$\frac{7.4}{50}$	$\frac{9.4}{32}$	$\frac{11.1}{5}$	13.4
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sta	+	A.I	-	Elev.
		894.86 ✓		
303/36				87.4 .
303+70				85.0 .
30400				84.5 .
+50				81.0 .
305+00				78.9
B.M.	0.52	884.82 ✓	10.56	874.30 ✓
303+70				85.0
304				84.5
+50				81.0
305				78.9 .
+50				78.4 .
306				77.8 .
+50				78.3 .
307+00				80.3 .

Lt -

£

Rt.

$\frac{2.6}{50}$	$\frac{4.2}{28}$	$\frac{5.5}{6}$	7.5
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$\frac{3.5}{50}$	$\frac{4.5}{28}$	$\frac{6.4}{11}$	7.9
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$\frac{3.0}{50}$		$\frac{6.1}{13}$	$\frac{13.4}{-}$
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$\frac{4.7}{50}$	$\frac{5.5}{30}$		$\frac{13.9}{-}$
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$\frac{4.4}{50}$	$\frac{7.4}{26}$	(16.0)	
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R.R. SP. AC. 11 16' dat 20' Lt 519 304+83

+0.2	$\frac{6.0}{22}$	$\frac{7.0}{50}$
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0.3	$\frac{4.6}{16}$	$\frac{6.0}{20}$	$\frac{7.2}{50}$
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3.8	$\frac{4.1}{10}$	$\frac{6.7}{20}$	$\frac{7.5}{50}$
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3.9	$\frac{7.2}{27}$	$\frac{3.8}{50}$
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$\frac{4.8}{50}$	$\frac{9.5}{46}$	$\frac{7.9}{37}$	$\frac{5.0}{16}$	6.4	$\frac{7.3}{26}$	$\frac{8.0}{50}$
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$\frac{8.0}{50}$	$\frac{2.3}{44}$	$\frac{5.5}{18}$	7.0	$\frac{7.8}{30}$	$\frac{8.1}{50}$
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$\frac{7.5}{50}$	$\frac{9.0}{39}$	$\frac{3.0}{32}$	$\frac{4.8}{16}$	$\frac{6.5}{-}$	$\frac{7.0}{27}$	$\frac{8.0}{50}$
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17 poud. & E/cv.

$\frac{7.0}{61}$	$\frac{7.8}{53}$	$\frac{6.8}{18}$	$\frac{7.5}{16}$	$\frac{4.5}{-}$	$\frac{5.9}{7}$	$\frac{7.0}{26}$	$\frac{7.4}{50}$
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Sta	+	H.I	-	Elev.	
		884.82 ✓			
307+28				81.5	
+73				92.0	
308				95.0	
308+10				96.0	
T.P.	11.77	893.68 ✓	3.13	881.69 ✓	
T.P.	10.54	903.28 ✓	0.94	892.72 ✓	
307+73				11.3	92.0
308				5.9	95.0
+50				7.3	96.0
+75				6.1	97.1
309				5.8	97.5
+50				7.0	96.3
+10				9.7	93.6
+50				11.4	91.9
311				13.0	90.3
+50				13.4	89.9
312				12.4	90.9
+24				11.4	91.7

L1. E RT.
Above E. E/ev

$\frac{+276}{70}$ $\frac{+223}{49}$ $\frac{+160}{34}$ $\frac{+72}{18}$ $\frac{111}{6}$ 33 $\frac{48}{15}$ $\frac{61}{23}$ $\frac{71}{10}$

-7.2

$\frac{32}{19}$ $\frac{49}{31}$ $\frac{59}{34}$ $\frac{66}{50}$

-10.2

$\frac{30}{81}$ $\frac{49}{47}$ $\frac{56}{50}$

-11.2

$\frac{16}{50}$

Nail in wood 70' RT. Ste. 308+50

Above H.I.

$\frac{+80}{75}$ $\frac{+34}{45}$ $\frac{37}{20}$ 11.3

Above H.I.

$\frac{+87}{76}$ $\frac{+72}{58}$ $\frac{12}{24}$ 8.3 $\frac{10.2}{7}$

Above H.I.

$\frac{+110}{81}$ $\frac{+72}{63}$ $\frac{20}{23}$ 7.3 $\frac{10.9}{15}$ $\frac{13.7}{31}$

Above H.I.

$\frac{+106}{88}$ $\frac{+77}{68}$ $\frac{12}{25}$ 5.8 $\frac{12.2}{34}$ $\frac{14.6}{50}$ $\frac{20.5}{80}$

$\frac{06}{54}$ $\frac{54}{28}$ 9.7 $\frac{13.2}{23}$ $\frac{17.2}{48}$ $\frac{19.7}{61}$

$\frac{30}{55}$ $\frac{78}{25}$ 11.4 $\frac{13.3}{12}$ $\frac{19.6}{36}$ $\frac{21.9}{62}$

$\frac{22}{53}$ $\frac{86}{23}$ 13.0 $\frac{16.5}{30}$ $\frac{21.6}{50}$
Above H.I.

$\frac{+60}{60}$ $\frac{35}{24}$ 12.4 $\frac{20.1}{20}$ $\frac{22.1}{50}$

Sta.	T	H. I.	-	Roof.	Elev.
		903.28			
+44				9.1	894.2
+53				10.2	93.1
+64				12.4	90.9
T. P.	2.38	893.41	12.25	891.03	
T. P.	3.41	885.48	11.54	881.87	
+90				2.8	82.7
313				5.4	82.1
+45				4.4	81.1
314				6.9	78.6
+50				2.0	77.5
315				8.7	76.8
	7.04	885.94	6.60	878.88	
314				8.2	77.7
	4.43	885.94	4.43	881.51	881.53
317				7.6	78.3
318				7.3	78.6
+75				6.3	79.6
319				5.6	80.4

Lt.

Rt.

Above H.I.

+108	+113			10.3	23.4
60	24	10.2		18	54

Above H.I.

+31.4	+26.4	+18.4	+12.2	+8.7		5.4	5.9
85	68	55	40	30	2.8	30	50

+14.1	+10.0	+3.4	0.3			5.2	6.2
54	47	30	14	3.4		24	50

2.2	2.7	3.4				5.0	6.0	7.2
50	48	14	4.4			15	24	50

5.4	6.2			8.2	8.7
50	25	6.9		34	50

8.90

Top of Ice
Top of Valentine Lake 2/24/20

7.5	8.2			8.0	9.0	8.7	Top of Ice
50	30	8.7		24	50		

7.3	7.6			9.3	9.4
50	27	8.2		34	50

Spk. 12" Oak 75' Lt. Sta. 316 + 75

6.2	7.3			8.5	9.2
50	25	7.6		40	50

5.3	6.5			7.7	8.0
50	28	7.3		28	50

3.3	5.1			7.3	7.5
50	18	6.3		25	50

Above H.I.

+0.3	2.1	3.3	4.7			7.0	7.1
50	40	32	30	5.4		25	50

S. No.	+	H. I.	-	Red.	Elev.
		885.96			
	+50			5.3	80.7
320				5.4	80.4
321				6.8	79.2
	+50			5.7	80.3
322				4.5	81.5
T.P.	4.93	887.22	3.49	882.27	
	+50			5.1	82.1
323				6.7	80.5
	+52			9.3	77.9
	+53	Bottoms of ditch		10.7	76.5
	+55			10.7	76.5
	+56			9.1	78.1
324				6.8	78.4
T.P.	4.84	888.55	3.53	883.69	
	+34			8.9	79.7
	+64	From R/L		5.2	83.4
325				2.2	86.4
T.P.	11.82	700.04	0.33	799.22	

- Above H.I.

$\frac{+1.0}{50}$	$\frac{1.0}{35}$	$\frac{2.6}{28}$	5.3	$\frac{6.4}{25}$	$\frac{7.4}{50}$
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$\frac{0.0}{50}$	$\frac{2.9}{37}$	5.6	$\frac{6.3}{29}$	$\frac{7.4}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{3.1}{50}$	$\frac{5.9}{17}$	6.8	$\frac{7.6}{22}$	$\frac{7.9}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{3.6}{50}$	$\frac{4.9}{28}$	5.7	$\frac{6.8}{32}$	$\frac{7.2}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{4.4}{50}$	$\frac{4.8}{22}$	4.5	$\frac{4.6}{30}$	$\frac{5.5}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{4.6}{50}$	$\frac{6.1}{30}$	5.1	$\frac{5.7}{29}$	$\frac{6.9}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{8.2}{50}$	$\frac{7.4}{27}$	6.7	$\frac{6.8}{30}$	$\frac{7.8}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{11.0}{50}$	Bottom of Pitch	$\frac{10.5}{50}$
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$\frac{8.9}{50}$	$\frac{8.9}{30}$	8.8	$\frac{8.3}{25}$	$\frac{7.1}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{8.5}{50}$	$\frac{8.3}{30}$	8.9	$\frac{8.5}{20}$	$\frac{7.7}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{6.4}{100}$	$\frac{6.1}{50}$	5.2	$\frac{4.8}{30}$	$\frac{4.2}{100}$
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$\frac{1.9}{30}$	$\frac{1.6}{25}$	1.2	$\frac{2.2}{26}$	$\frac{2.8}{36}$
------------------	------------------	-----	------------------	------------------

Stn.	T	H.I.	-	Rock	Elev.
		900.04			
+55				3.7	96.3
324				0.5	900.0
	8.29	908.17	0.14	899.88	
+30				5.4	02.8
B.M.			4.42	903.75	903.74
T.P.	9.38	917.34	0.19	907.98	
+75				6.3	11.1
327				4.1	13.3
+45				2.8	14.6
328				6.5	10.9
+50				10.4	07.0
+75				10.4	06.8
T.P.	1.59	908.41	10.54	904.82	
329				5.0	03.4
+50				5.1	03.3
330				7.1	00.6

11

11.

$\frac{2.7}{50}$ $\frac{3.1}{37}$ 3.7 $\frac{4.3}{15}$ $\frac{8.4}{50}$

$\frac{1.0}{50}$ $\frac{1.3}{24}$ 0.5 $\frac{0.5}{15}$ $\frac{3.0}{50}$

$\frac{7.7}{50}$ $\frac{7.9}{40}$ $\frac{6.6}{15}$ 5.4 $\frac{4.9}{20}$ $\frac{6.6}{42}$ $\frac{8.2}{50}$

Spk in 15" Box Elder 250' H. Sta. 326+50

$\frac{11.7}{50}$ $\frac{9.8}{30}$ 6.3 $\frac{5.7}{15}$ $\frac{7.2}{33}$ $\frac{11.5}{50}$

$\frac{8.3}{50}$ $\frac{6.6}{27}$ 4.1 $\frac{3.7}{25}$ $\frac{6.3}{38}$ $\frac{10.8}{50}$

$\frac{1.6}{50}$ $\frac{1.8}{20}$ 2.8 $\frac{4.2}{15}$ $\frac{11.1}{50}$

↑ Above H.I.

$\frac{4.2}{50}$ 0.0 $\frac{2.7}{19}$ 6.5 10.8 24 $\frac{13.1}{50}$

$\frac{4.4}{50}$ $\frac{7.7}{24}$ 10.4 $\frac{12.6}{26}$ $\frac{14.6}{50}$

$\frac{4.3}{50}$ $\frac{5.4}{37}$ $\frac{9.6}{12}$ 10.6 12.1 13 $\frac{15.4}{50}$

↑ Above H.I.

$\frac{4.8}{50}$ $\frac{12.2}{34}$ $\frac{2.4}{14}$ 5.0 6.9 26 $\frac{9.6}{50}$

↑ Above H.I.

$\frac{4.3}{50}$ $\frac{4.0}{40}$ $\frac{6.0}{30}$ $\frac{1.3}{23}$ 5.1 9.9 25 $\frac{13.7}{50}$

$\frac{10.8}{50}$ $\frac{0.0}{40}$ $\frac{2.1}{30}$ 7.8 $\frac{11.5}{30}$ $\frac{16.0}{50}$

Sta.	T	H.I.	-	Ref.	Elev
		908.41			
	+40			12.2	896.2
	+80			13.0	95.4
331				11.4	897.0
	+50			7.9	900.5
332				7.5	00.9
	+40			6.2	02.2
	+85			2.1	06.3
333				2.5	05.9
T.P.	3.54	900.47	10.50	197.91	
	+45			1.2	900.4
	+75			4.4	894.1
334				2.6	91.9
T.P.	2.55	892.70	10.92	890.15	
	+60			4.3	88.4
335				4.7	88.0
	+12			4.8	87.9
	+98			6.8	85.9
	+70			8.0	84.7

Lt							
4.5	4.9	9.4			14.6	17.2	
50	41	22	12.2		25	50	

4.6	7.0	11.3			15.0	17.9	
50	38	20	13.0		25	50	

5.5	7.1	10.5			13.0	12.1	
50	40	18	11.4		20	50	

5.3	6.6	7.9			7.2	8.6	11.4
50	41	30	7.9		15	32	50

4.0	7.4				6.7	3.5	
50	27	7.5			14	50	

Above H.I.

1.6	1.8	2.4			1.4	12.3	12.3
50	37	25	2.1		7	45	50

Above H.I.

1.7	2.3				1.7	10.2	10.2
50	25	2.5			15	34	50

Above H.I.

1.32	1.2				2.8	2.1	
50	33	1.2			30	50	

Above H.I.

1.45	1.8	1.8	4.0		9.0	7.5	
50	10	39	12	6.4	24	50	

Above H.I.

1.36	1.6	10.5	3.0		10.1	10.8	11.4
50	42	40	25	8.6	12	21	50

1.9	1.4	1.9			5.0	4.5	5.4
50	38	15	4.3		23	42	50

Bottom of Ditch

4.8	4.3				5.0	5.2	6.9
50	32	4.7			20	25	50

Bottom of Ditch

5.6	5.9				7.5	11.0	11.0	7.3	6.5
50	30	6.8			29	32	35	40	50

Sta.	+	H.I.	-	Red.	Elev.
		892.70			
336				5.5	84.2
337				8.9	83.8
338				5.9	83.8
	8.93	893.17	8.44	884.24	
+50				7.5	83.7
339				9.2	84.0
340				5.0	85.2
341				5.8	87.4
+35				4.8	88.4
+38				6.5	86.7
+44				6.5	86.7
+47				4.8	88.4
342				3.2	90.0
	10.17	900.41	1.93	890.24	
B.M.	4.62	900.29	4.71	895.70	895.67
+15				7.4	90.7
+20				8.1	92.2
+50				8.1	92.2
+75				5.2	95.1

Bottom of Ditch

11

ft. Bottom of Pitch

$\frac{80}{50}$	$\frac{83}{25}$	8.5	$\frac{88}{20}$	$\frac{96}{50}$	$\frac{106}{52}$	$\frac{106}{55}$	$\frac{94}{58}$
-----------------	-----------------	-----	-----------------	-----------------	------------------	------------------	-----------------

Bottom of Pitch

$\frac{87}{50}$	$\frac{87}{30}$	8.9	$\frac{90}{23}$	$\frac{88}{44}$	$\frac{106}{46}$	$\frac{106}{49}$	$\frac{88}{51}$
-----------------	-----------------	-----	-----------------	-----------------	------------------	------------------	-----------------

$\frac{89}{50}$	$\frac{90}{20}$	8.9	$\frac{90}{30}$	$\frac{93}{50}$
-----------------	-----------------	-----	-----------------	-----------------

$\frac{77}{50}$	$\frac{87}{25}$	9.2	$\frac{95}{30}$	$\frac{94}{50}$
-----------------	-----------------	-----	-----------------	-----------------

$\frac{56}{50}$	$\frac{71}{25}$	8.0	$\frac{89}{25}$	$\frac{92}{50}$
-----------------	-----------------	-----	-----------------	-----------------

Bottom of Pitch

$\frac{27}{50}$	$\frac{44}{30}$	5.8	$\frac{61}{21}$	$\frac{89}{23}$	$\frac{89}{29}$	$\frac{62}{32}$	$\frac{62}{50}$
-----------------	-----------------	-----	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{22}{50}$	$\frac{23}{43}$	$\frac{35}{30}$	3.2	$\frac{12}{31}$	$\frac{0.9}{50}$
-----------------	-----------------	-----------------	-----	-----------------	------------------

spk in F.Col. 81 Lt. Sta. 542715'

$\frac{94}{50}$	$\frac{75}{30}$	$\frac{89}{23}$	81	$\frac{60}{28}$	$\frac{40}{50}$
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$\frac{90}{50}$	$\frac{90}{32}$	$\frac{75}{29}$	81	$\frac{54}{22}$	$\frac{3.3}{50}$
-----------------	-----------------	-----------------	----	-----------------	------------------

$\frac{89}{50}$	$\frac{23}{25}$	$\frac{75}{27}$	$\frac{10}{14}$	5.2	$\frac{29}{30}$	$\frac{18}{50}$
-----------------	-----------------	-----------------	-----------------	-----	-----------------	-----------------

Sta.	+	H.I.	-	Red.	Elev
		900.29			
343				5.2	95.1
	+25			6.2	94.1
	+70			7.1	93.2
344				7.0	93.3
	+30			6.9	93.4
	+40			7.2	93.1
345				7.2	93.1
	+35			4.4	95.9
	+50			6.2	94.1
	+70			6.7	93.6
346				5.3	95.0
	+50				
	+50			1.2	99.1
T.P.	12.91	911.87	1.13	899.14	
347				21	909.8
T.P.	11.79	922.75	0.91	910.94	
	+35			4.9	15.9
	+38			5.5	17.3
	+75			2.9	19.8

H

R

$$\frac{88}{50} \frac{79}{36} \frac{70}{34} \frac{69}{15} \quad 5.2 \quad \frac{2.5}{25} \quad \frac{1.5}{50}$$

$$\frac{86}{50} \frac{78}{32} \frac{71}{30} \frac{72}{14} \quad 6.2 \quad \frac{3.5}{23} \quad \frac{1.1}{50}$$

$$\frac{84}{50} \frac{76}{21} \frac{71}{19} \quad 7.1 \quad \frac{6.1}{30} \quad \frac{5.3}{50}$$

$$\frac{7.2}{50} \frac{7.6}{13} \frac{6.9}{4} \quad 7.0 \quad \frac{6.6}{35} \quad \frac{5.7}{50}$$

$$\frac{5.3}{50} \frac{6.2}{32} \frac{6.9}{18} \quad 7.2 \quad \frac{6.8}{10} \quad \frac{5.2}{30} \quad \frac{3.2}{50}$$

$$\frac{1.9}{50} \frac{4.2}{44} \frac{4.9}{37} \frac{3.4}{30} \quad 4.4 \quad \frac{6.8}{14} \quad \frac{7.2}{21} \quad \frac{6.7}{27} \quad \frac{5.1}{50}$$

$$\frac{1.7}{50} \frac{4.0}{40} \frac{5.6}{15} \quad 6.2 \quad \frac{6.8}{18} \quad \frac{6.7}{25} \quad \frac{5.8}{50}$$

Above H.I.

$$\frac{4.4}{50} \frac{1.2}{30} \frac{3.5}{15} \quad 5.3 \quad \frac{6.3}{23} \quad \frac{4.4}{45} \quad \frac{6.0}{50}$$

Above H.I.

$$\frac{11.50}{40} \frac{11.50}{50} \frac{11.21}{45} \frac{7.78}{33} \frac{7.36}{15} \frac{10.3}{9} \quad 1.2 \quad \frac{4.0}{43} \quad \frac{4.7}{50}$$

$$\frac{16.0}{50} \frac{16.1}{36} \frac{14.3}{32} \frac{12.2}{23} \quad 2.1 \quad \frac{4.6}{14} \quad \frac{5.8}{42} \quad \frac{5.8}{50}$$

$$\frac{3.1}{50} \frac{2.1}{25} \frac{3.1}{23} \quad 5.5 \quad \frac{2.2}{22} \quad \frac{10.3}{50}$$

$$\frac{2.3}{50} \frac{2.6}{13} \frac{3.0}{12} \quad 2.7 \quad \frac{3.1}{15} \quad \frac{4.8}{32} \quad \frac{5.8}{50}$$

Sta.	+	H.I.	-	Red.	2-lev.
		922.75			
348				5.9	16.9
	+37			11.9	10.9
	+33			12.7	10.1
	+83			12.2	10.6
349					11.5
	+50			7.2	15.6
350				2.5	20.3
T.P.	2.98	923.27	2.44	920.29	
	+40			2.2	21.1
	+65			4.2	19.1
351				9.3	14.0
Eq. 49.					
351 + 59 41 =					
351 + 73 20				10.5	12.8
T.P.	4.21	922.08	5.40	917.87	
T.P.	10.23	927.20	5.11	916.97	
B.M.			9.37	917.83	917.85

TO - B 40

3/2/26
55

Lt.

Rt.

$\frac{12.2}{50}$ $\frac{12.0}{42}$ $\frac{5.9}{2}$ 5.9 $\frac{4.0}{20}$ $\frac{4.0}{50}$

$\frac{16.0}{50}$ $\frac{13.7}{22}$ 12.7 $\frac{11.8}{10}$ $\frac{10.5}{19}$ $\frac{9.3}{50}$

$\frac{14.3}{50}$ $\frac{12.6}{33}$ $\frac{11.8}{25}$ $\frac{11.7}{9}$ 11.3 $\frac{11.6}{9}$ $\frac{10.5}{25}$ $\frac{9.7}{38}$ $\frac{9.8}{50}$

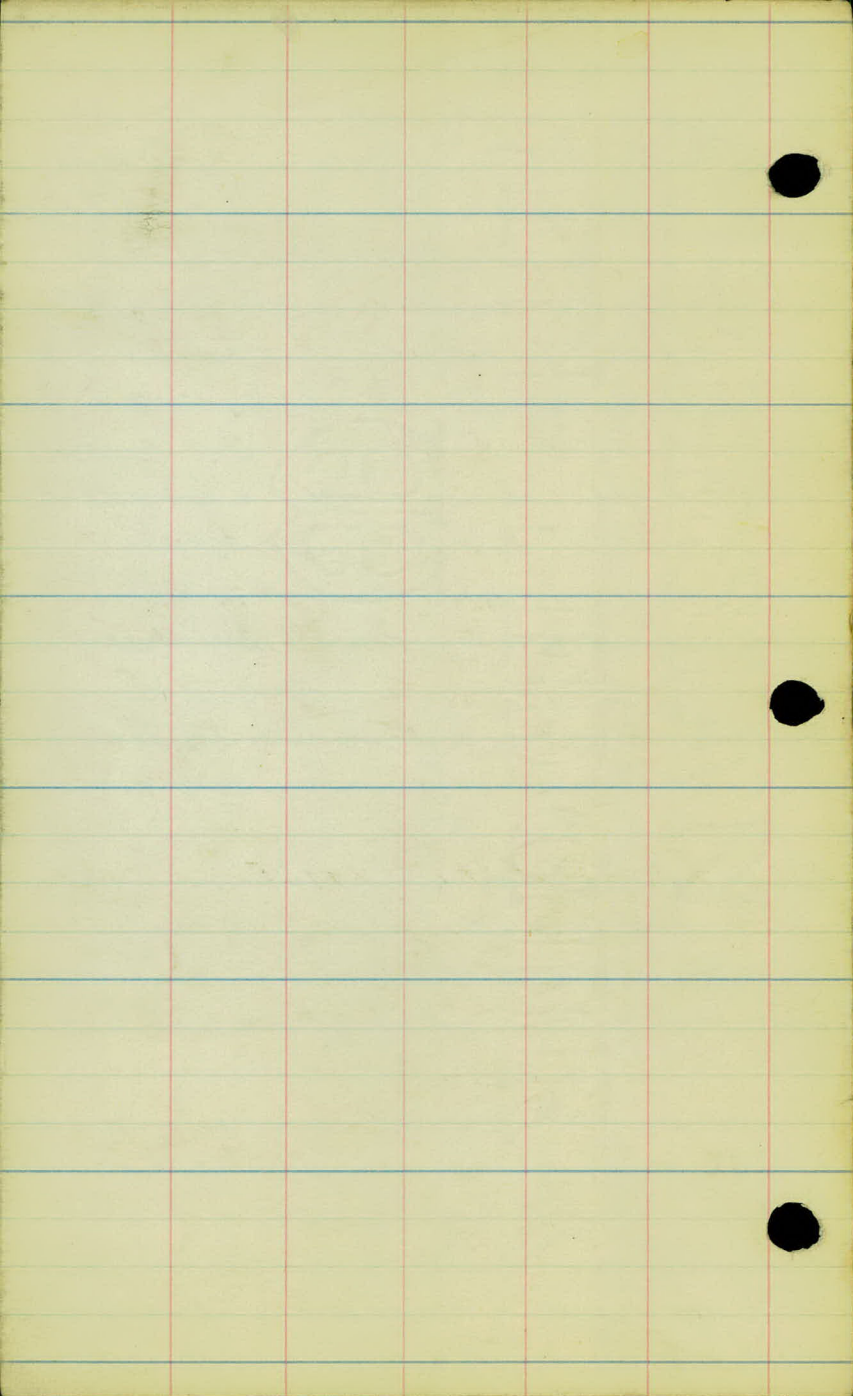
$\frac{5.4}{50}$ $\frac{2.6}{25}$ 2.5 $\frac{2.8}{20}$ $\frac{4.6}{50}$

$\frac{5.9}{50}$ $\frac{4.0}{35}$ $\frac{2.6}{16}$ 2.2 $\frac{2.9}{70}$ $\frac{3.6}{24}$ $\frac{3.2}{40}$ $\frac{3.8}{50}$

$\frac{12.2}{50}$ $\frac{10.9}{20}$ 9.3 $\frac{6.4}{15}$ $\frac{3.9}{33}$ $\frac{4.1}{50}$

$\frac{11.0}{50}$ $\frac{11.3}{30}$ $\frac{11.4}{4}$ 10.5 $\frac{10.2}{20}$ $\frac{10.1}{50}$

Spk in T.P. 60 Lt. Sta. 374+25.



Proj #26-62

Act. Topog. from
Sta. 260+00 to Sta. 352+00.

264

263

262

241

260

259

Woods

Woods

270

269

248

267

244

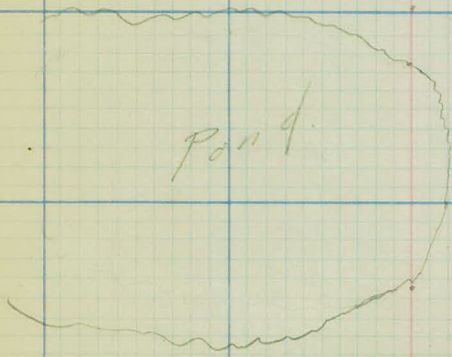
265

244

Hay
Field.

172 N.W. Fence.

101 N.W. F.



10000

277

276

275

274

273

272

271

270

cultivated field

59

Hay

field

Hay

field

283

282

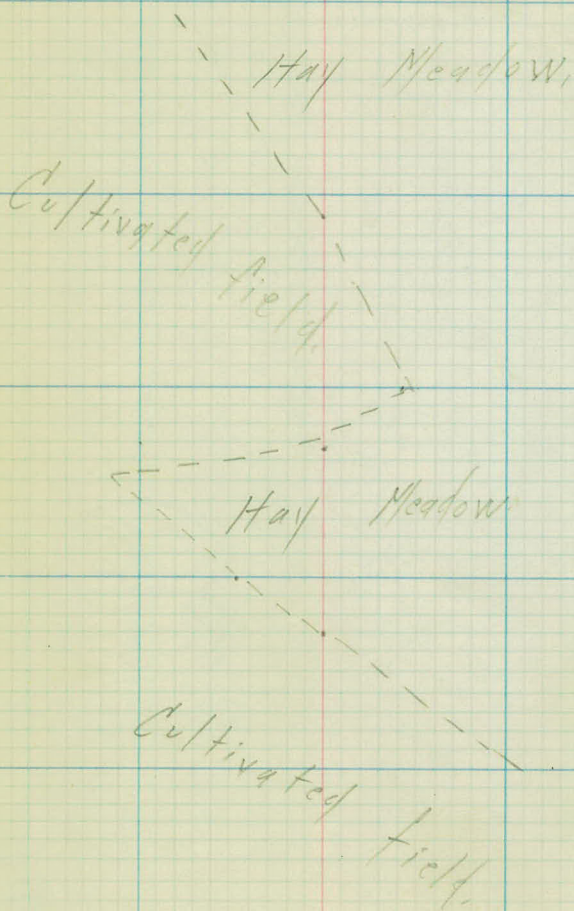
281

280

279

~~278~~

278
~~277~~



1/2 Power line
credit.

1/2 Steel tower,
1/2 Power line 56
1/2 P.R. 54
1/2 High Power
line over head.

289

288

287

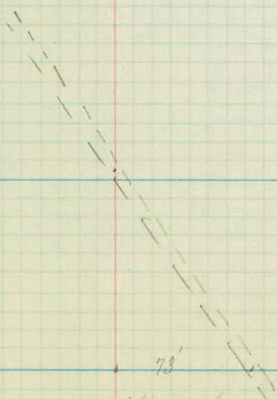
284

285

284

283

Hay Meadow



104 pits.

Hay Meadow

295

294

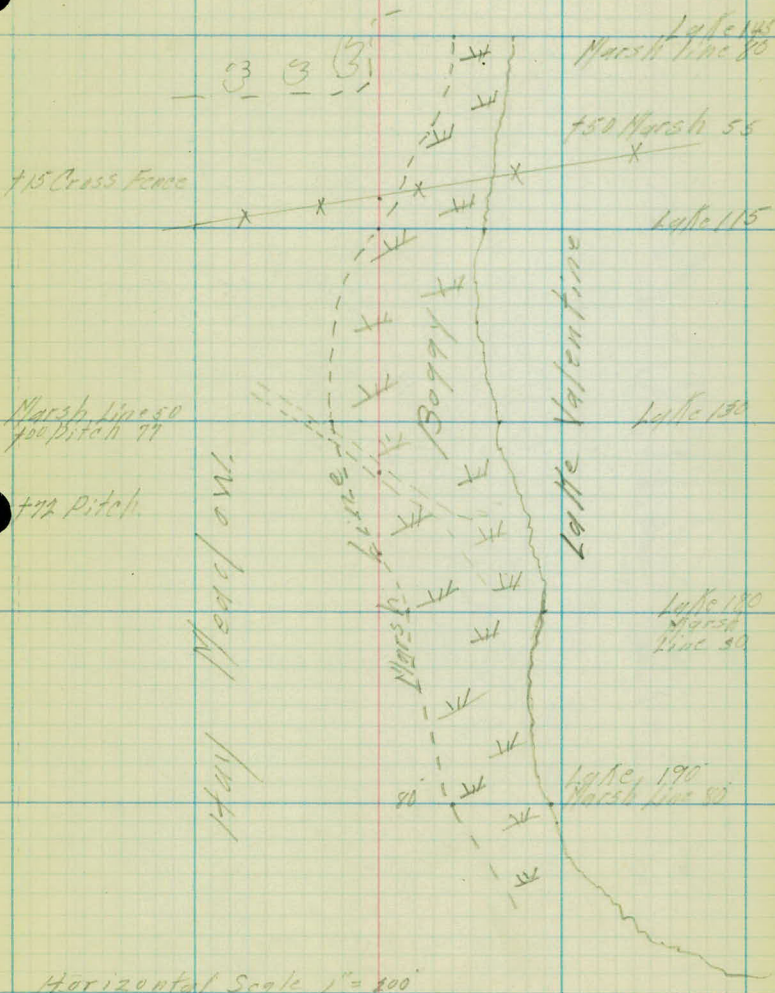
293

292

291

290

289



33 33 33

Latta 145
Marsh Line 80

Latta 115
Marsh 55

+15 Cross Fence

Marsh Line 50
+20 Pitch 77

+72 Pitch

Hay Meadow

Boggy

Latta 115

Latta 130

Latta 180
Marsh Line 30

Latta 190
Marsh Line 50

Horizontal Scale 1" = 100'

301

300

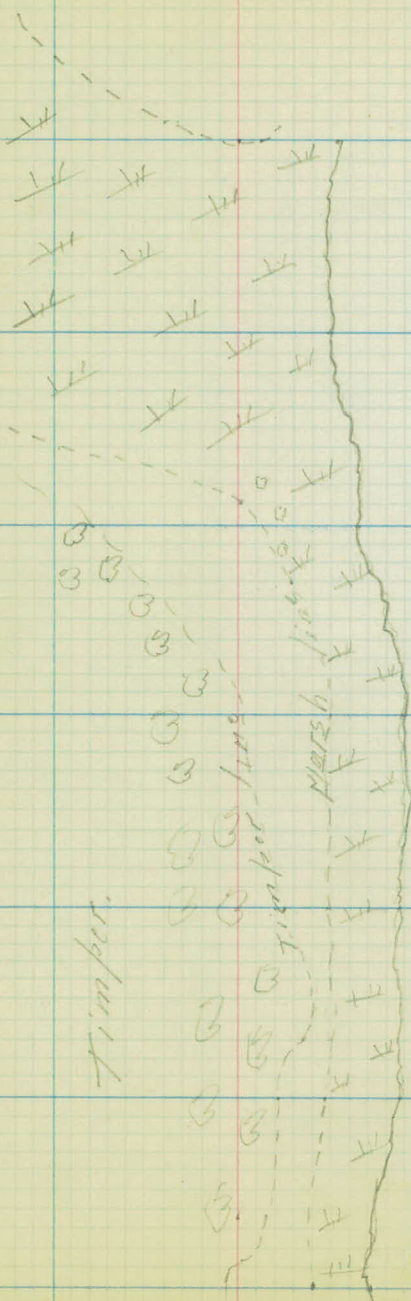
299

298

297

296

295



Lake 107

Lake 98

Lake 190

Lake 175

Marsh 98
Lake 177

Marsh 98
Lake 178

307

304

305

304

303

302

301

313

312

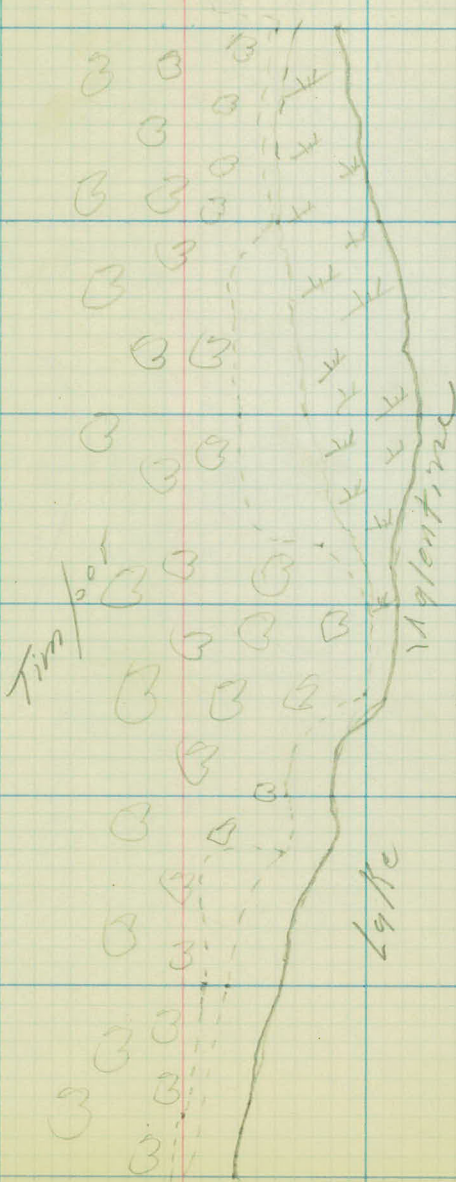
311

310

309

308

307



19/10/65

19/10/215

19/10/160

19/10/235

+50 19/10/220

19/10/160

19/10/107

319

318

317

316

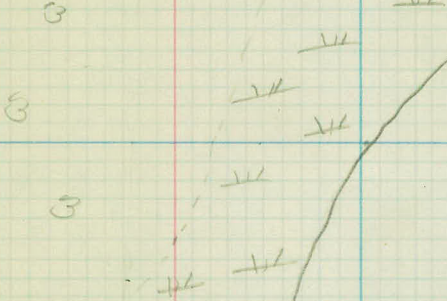
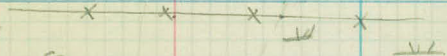
315

314

313

2/26/64
66

493 Cross Fence



1940 125

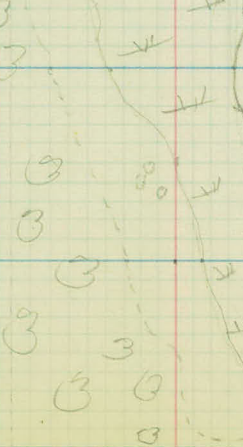
1940 130

1940 85

458 Cross Fence



Timber



Lytle Valentine

1940 64

1940 109

325

324

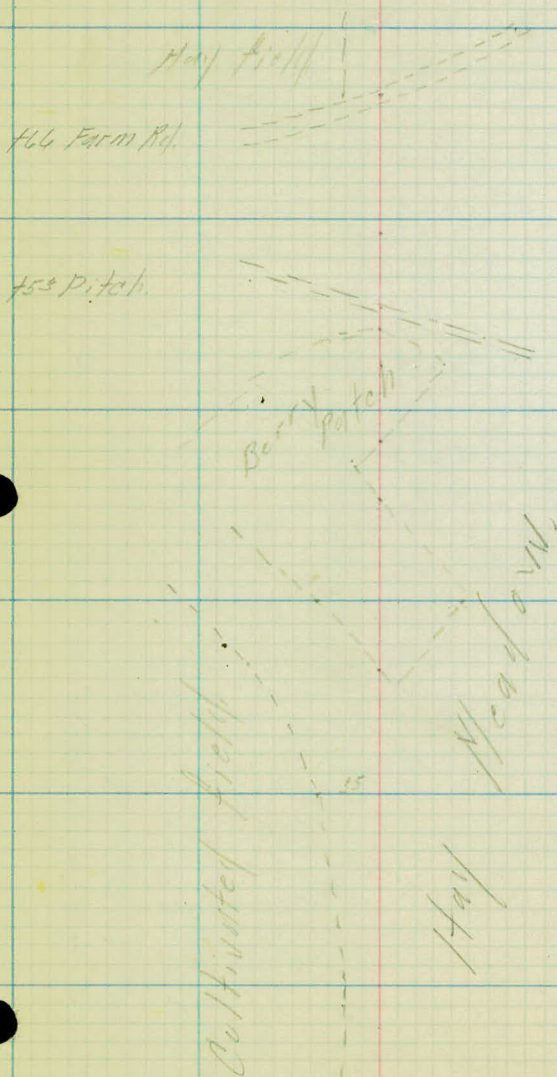
323

322

321

320

319



331

330

329

328

327

326

325

2/25/20
68

Hay field



Field

x x x x x x x x 182 Cross Fence

Cultivated

Cultivated field

187 P.P. 60

337

336

335

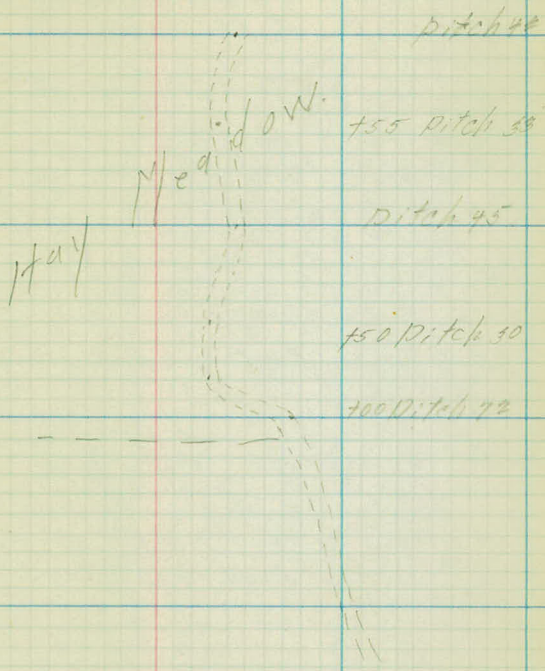
334

333

332

331

2/25/69
69



Hay field

343

342

341

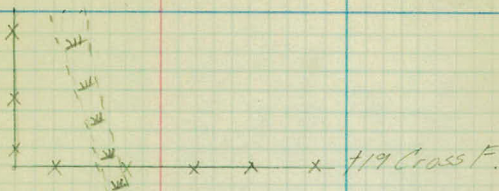
340

339

338

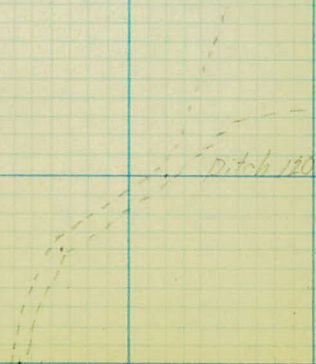
337

+19 F. Cor. 81 h



+40 G. Pitch
+00 Pitch 2.3

Hay Meadows



349

348

347

346

345

344

343

2/25/46
↑↑

700 F 45

F. 0

F. 36

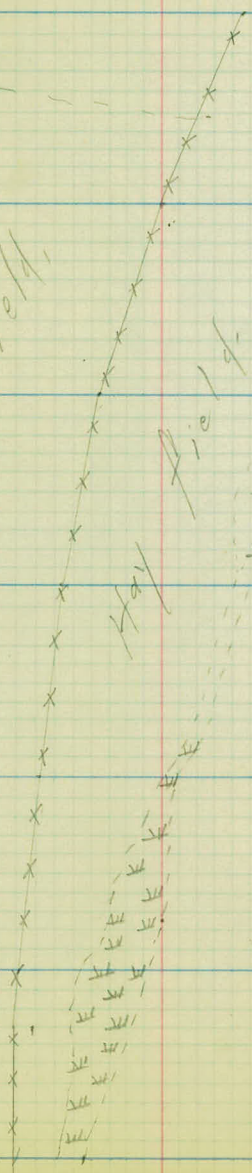
Cultivated field

field

Hay

10 ft ditch 45'

Hay field



352

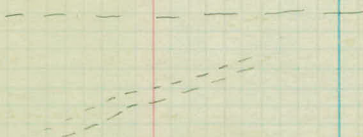
351

350

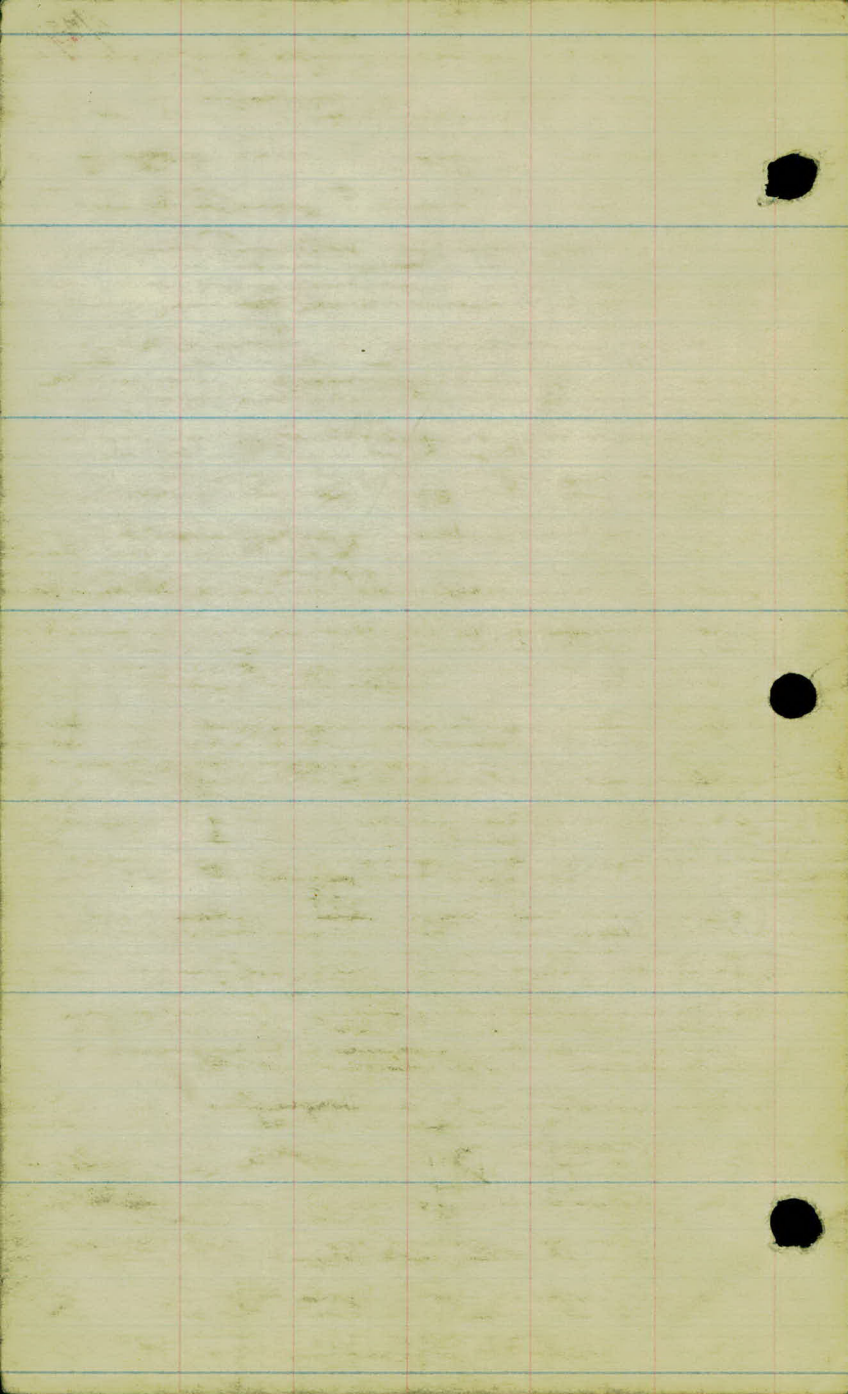
349

Cultivated field

135 Farm Rd.



Hay field



(26-62)

Revision

Sta 587+44.2

to Sta. 682+59.58 = 709+54.2.

Station

Ang. Pt. Ang. Pt.

595+79.3 P.O.T. $\frac{1}{2}$ Cent

593+83.4 P.T.

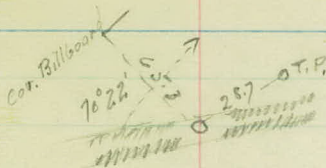
590+72.4 P.I. $31^{\circ} 58'$

M 61-18 W
N 81-18 N

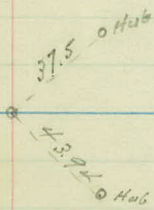
587+44.1 P.C. = 587+44.1 "H" line

FROM ALIGN
19

M 61-09 W
N 81-09 N



- 587+44.1 - 0°00'
- 589+00 - 10°24'
- 589+00 - 30°54'
- 590+00 - 60°24'
- 591+00 - 80°54'
- 592+00 - 110°24'
- 593+00 - 130°54'
- 593+00 - 150°59'



5° Curve left.
 $\Delta = 310.58'$
 Rad. = 1146.28 ✓
 Tang = 328.33 ✓
 Length = 639.33 ✓

Station

Ang. ht. Ang. Rd.

4

620+00 P.O.T

611+47.04 ✓ P.T.

609+02.75 ✓ P. I.

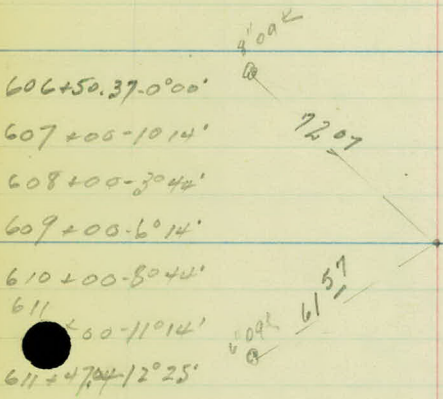
24° 50'

606+50.37 ✓ P.C.

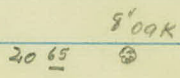
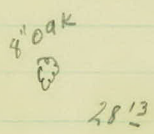
599+00 P.O.T

N 56° - 27' W

N 81° - 19' W



5° Curve RT.
 $\Delta = 24^\circ 50'$
 Rad = 1146.28
 Tang = 252.38 ✓
 Length = 496.67 ✓



Station

Ang. ht. [±] Ang. Rl

672+00 P.O.T

650+00 P.O.T

640+00 P.O.T

630+00 P.O.T

N 56° - 27' W

5' high
10" stamp
4848

5120

12 oak

F.P.
4575

41.78 F.P.

35 ¹³/_— 10 oak

7793 8 oak

Station

Ang. ht. Ang. TR.

TO ALIGN
21

682+59.57 = 709+54.7

682+59.58 P.T.	7-35.30
682	7° 00'
681	6° 00'
680	5° 00'
679	4° 00'
678	3° 00'
678+82.25 P.I.	15° 11'
677	2° 00'
676	1° 00'
675+00.41 P.C.	0-00

N 41°-16' W

N 56°-27' W

392.9

£

2-19-26

18

77

2° C. Rt

Tan = 381.84 ✓

L.C. = 759.17 ✓

Rad = 2864.93

PI 678+82.25

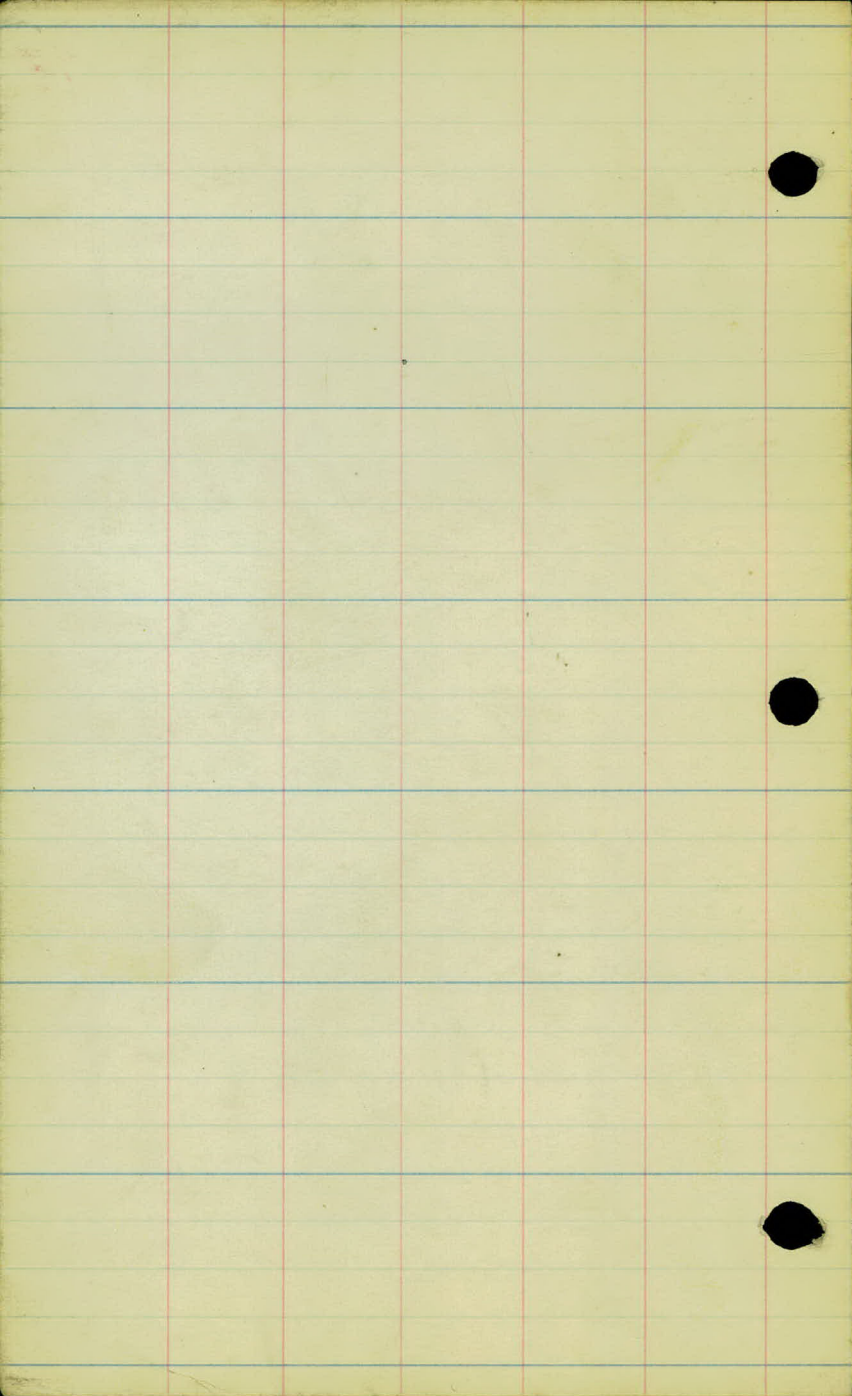
6' OAK
⊗

669'

SPIKE

3' OAK
⊗

6130'



594
78

Rd #93
"H" hinc. Rev.
Sta. 587-682

593

592

Meadow land

591

590

+34 FENCE 28'

FENCE 1'

+50 FENCE 27'

+71 F. CUR. 8'

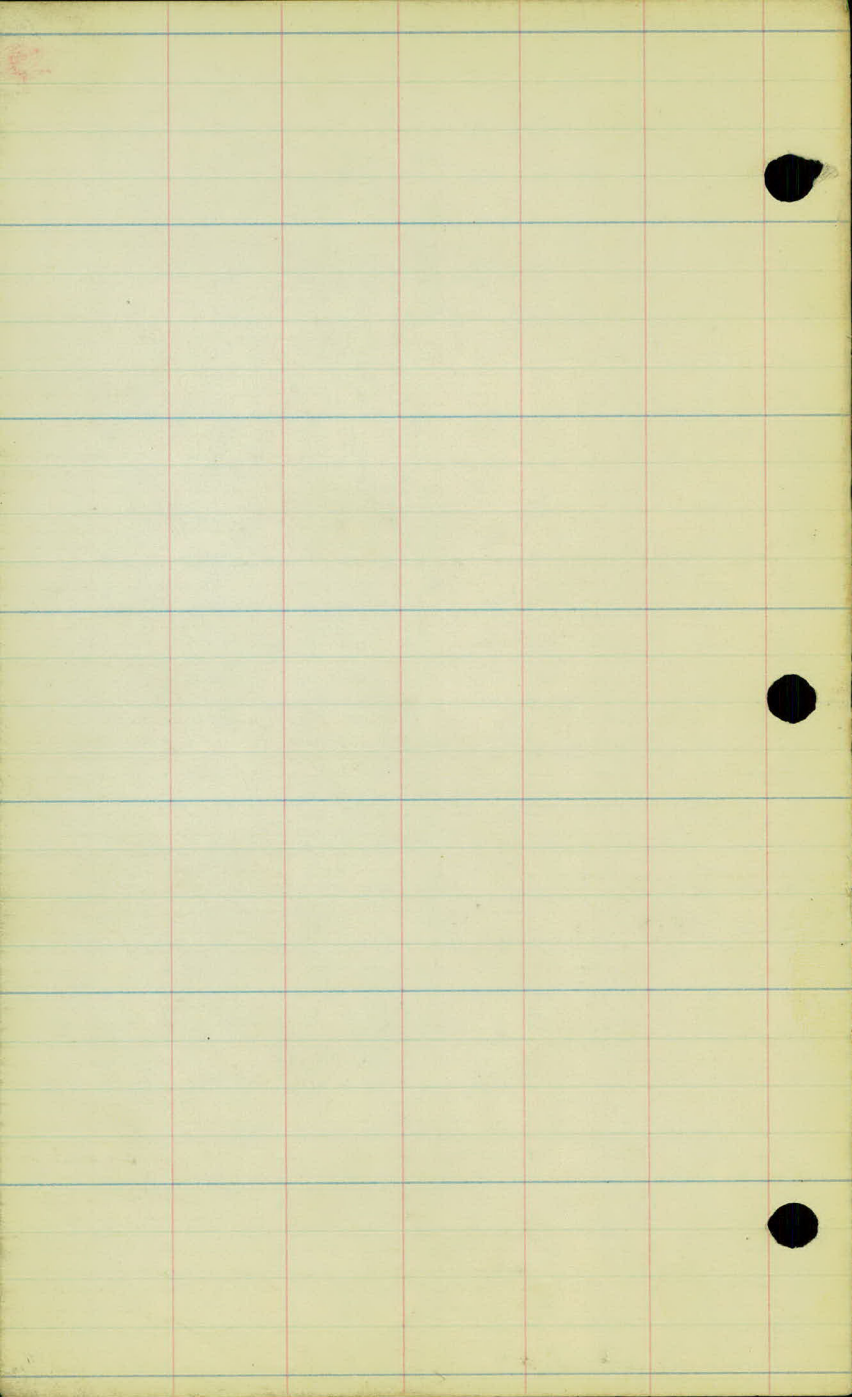
+50 F. 30'

589

588

CULTIVATED

587



+56 END OF BRUSH

4 Trees

+ END OF BRUSH

2 Trees

600

5 Trees

9 Trees

599

7 Trees

13 Trees

3sq. Brush

3sq. Brush

598

WOODS

WOODS



+16 FENCE

597

+73 T.P. 48'

Flora City Fuel + Transp. Co

+35 SIGN 32' 19' x 19' → A

+04 T.P. 16' 596

+79.3 ± P.O.V

Central Ave

+06 Well Head 23' 595

+89 FEEL'

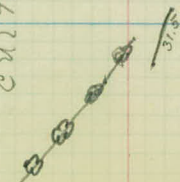
+178 BILLBOARD 135'

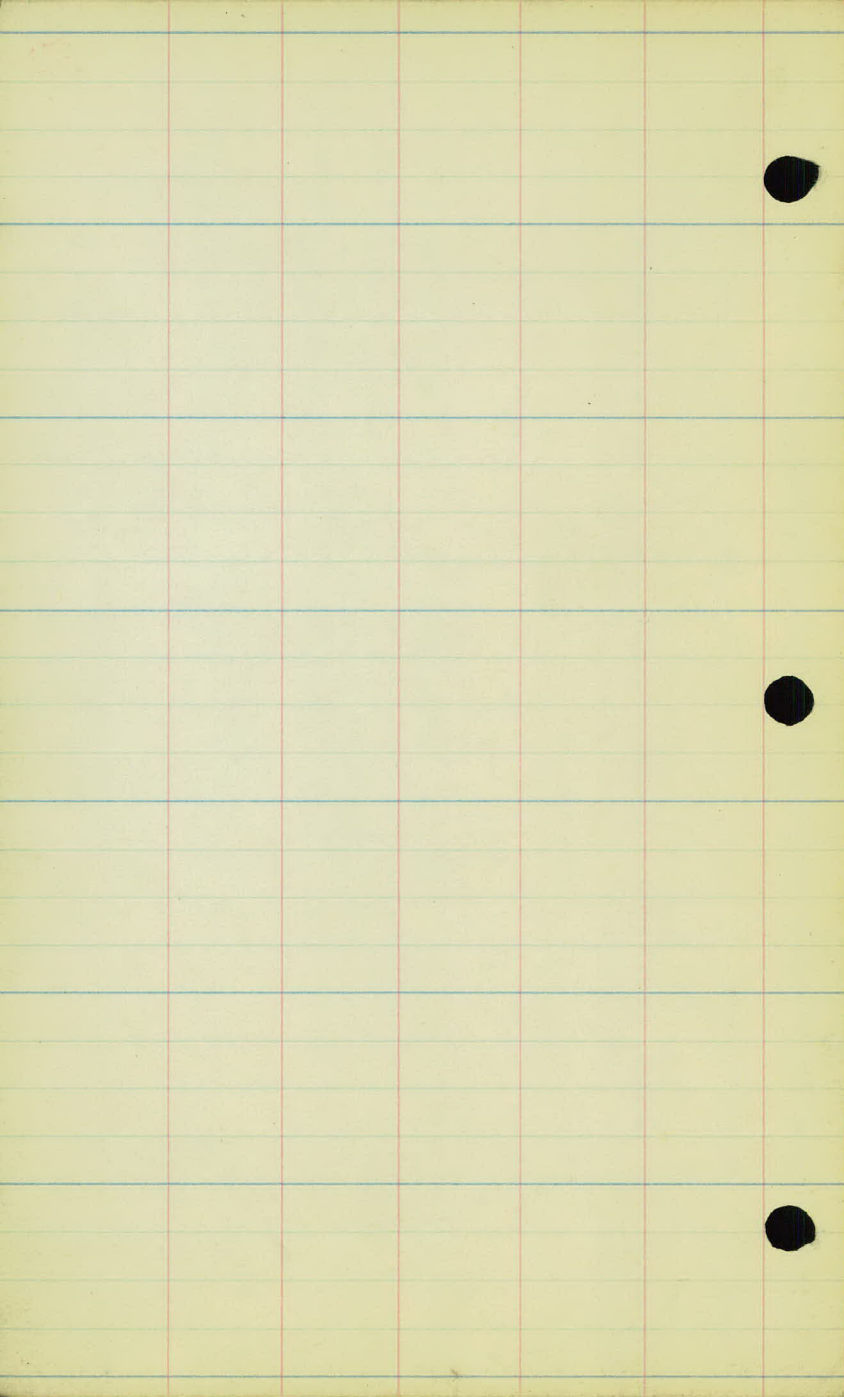
CULTIVATED

+66 6" tree

TREE LINE 47'

594





608

80

4 Trees

6 Trees

607

1 Tree
Beg of BYUSH

1 Tree
Beg of BYUSH

606

50'
40'
Top. to to Bank

40'
3 Trees

+00 END OF BYUSH

END OF BYUSH. +00

605

2 Trees

1 Tree

40'
62'
Loddie Lake

604

3 Trees

right Bush

95

edge of water 150. out from Top. of bank

603

1 Tree

120

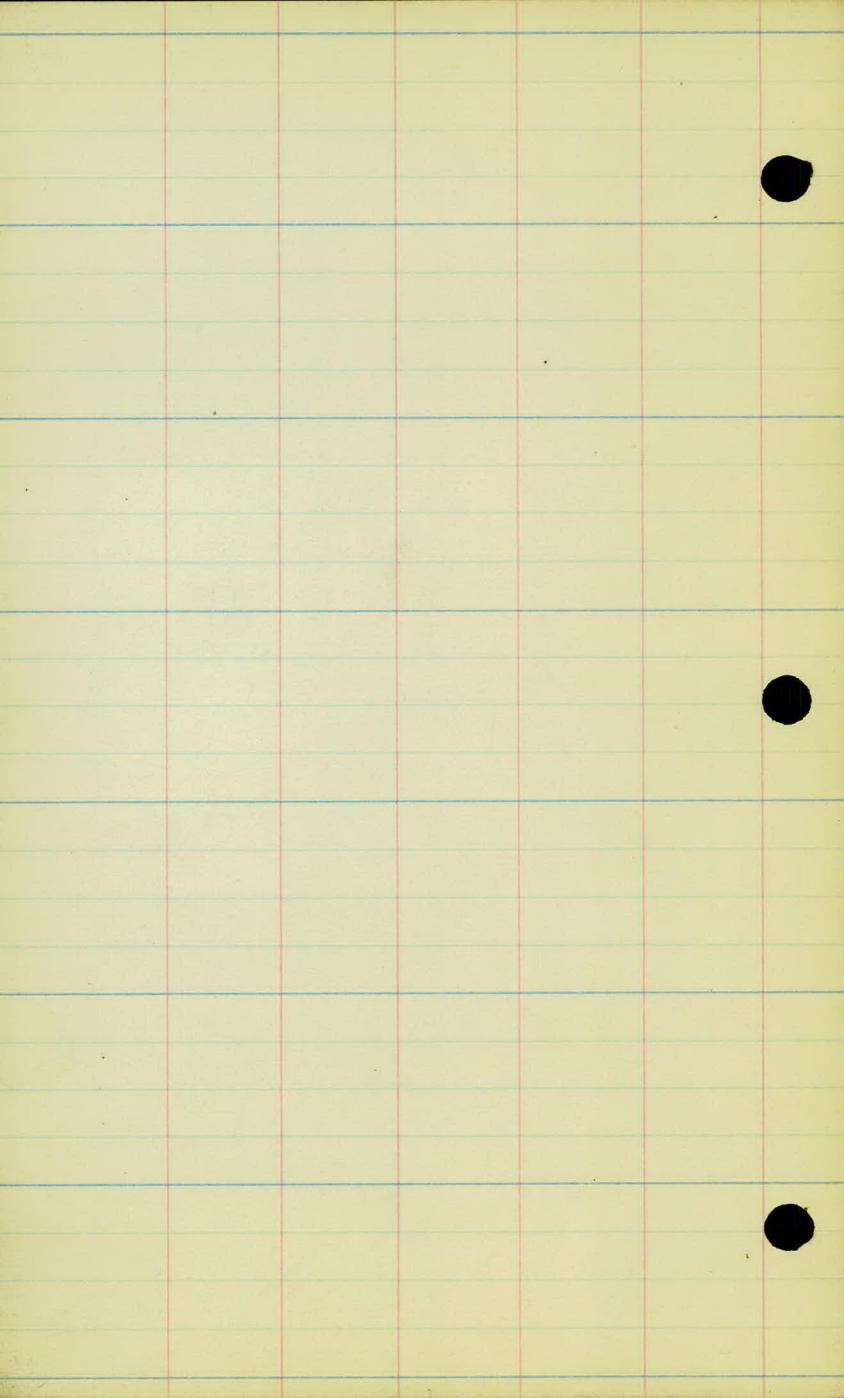
Top. of Bank

602

howhand

155

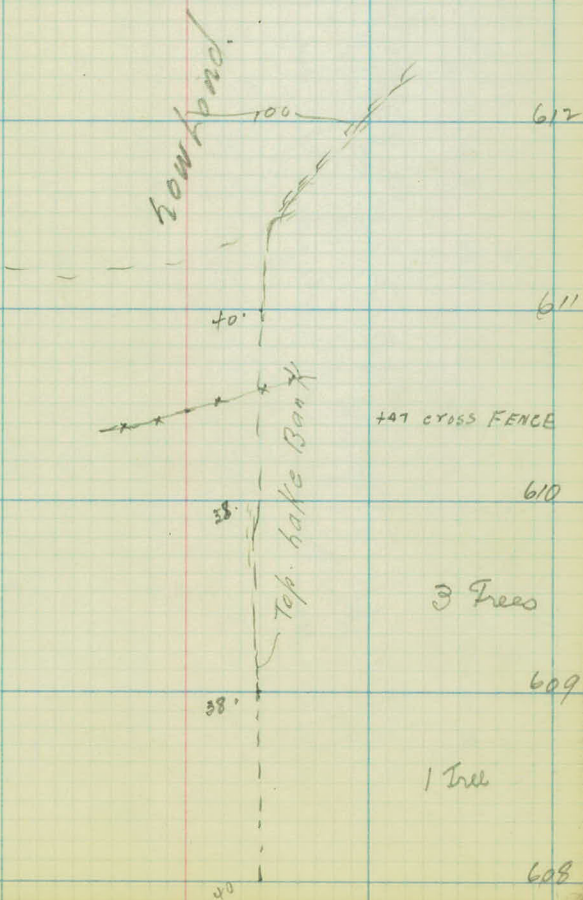
601



67
81

Lowland

lowland



612

611

47 CROSS FENCE

610

1 Tree

3 Trees

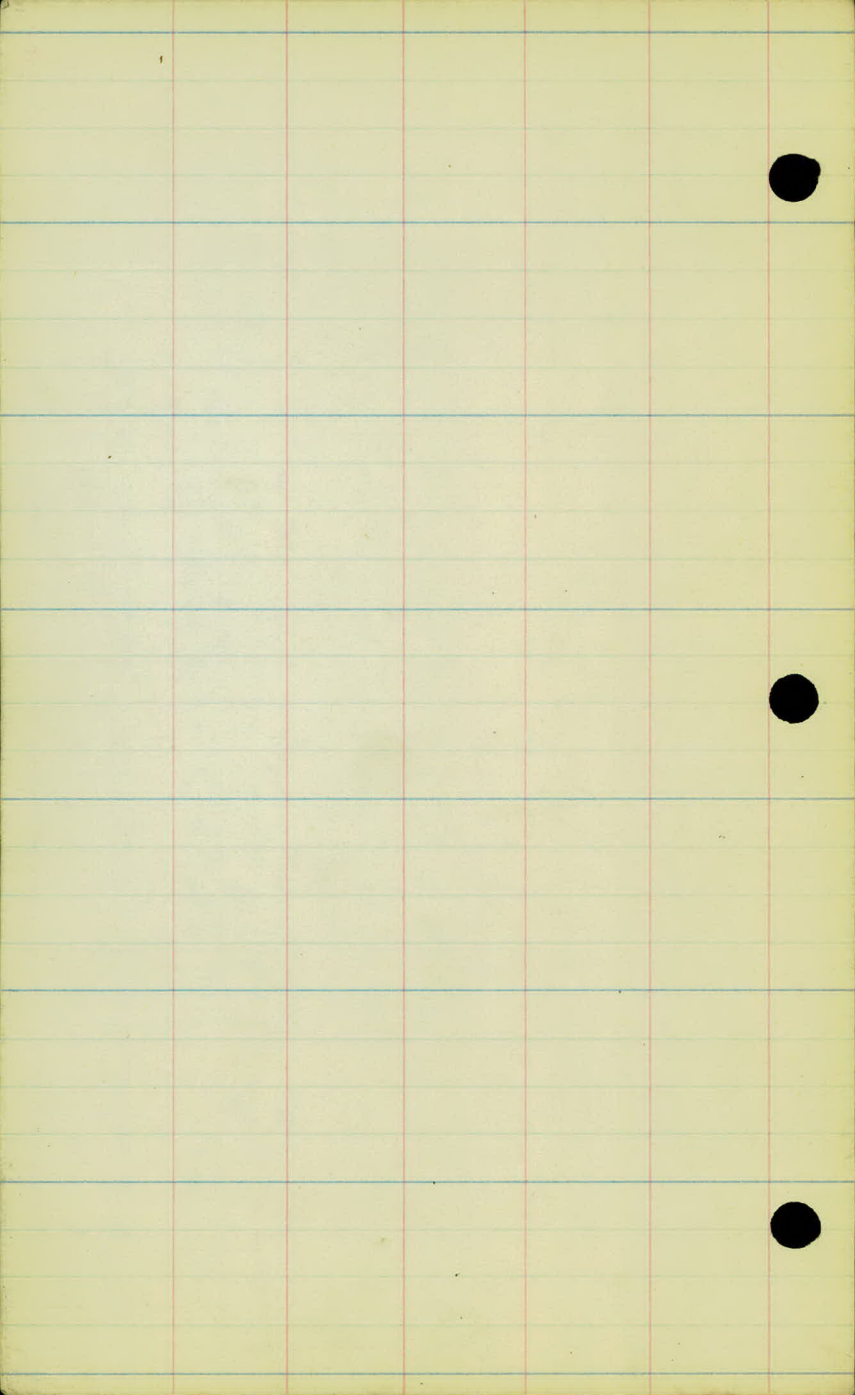
609

6 Trees

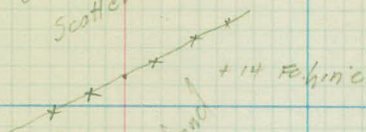
1 Tree

608

40



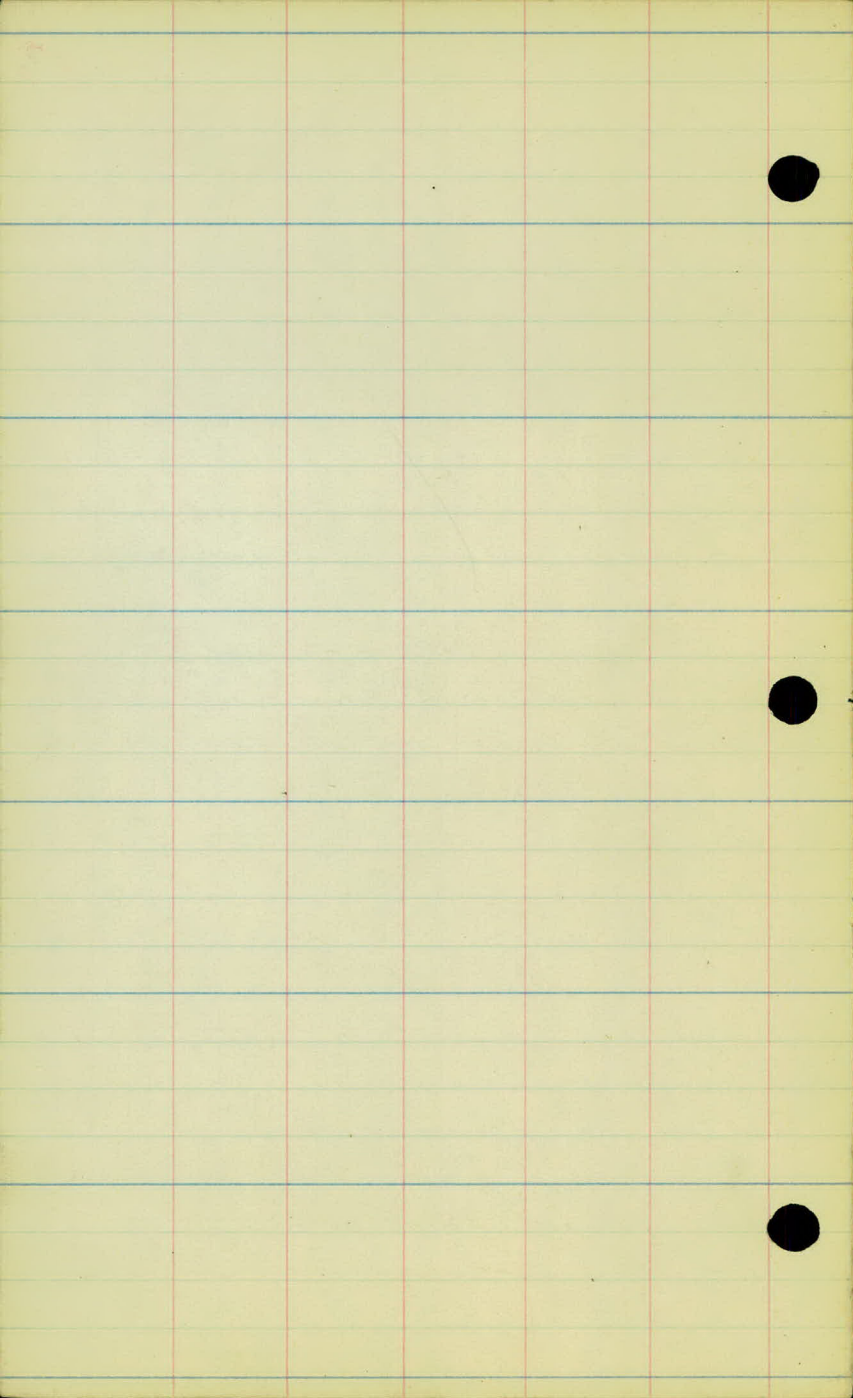
undeveloped hand.
Scattered Scrub Oaks



undeveloped hand



undeveloped hand.
Scattered Scrub Oaks



Road
+ 94 ft Road
+ 59 ft. Xing

649

lowhand

648

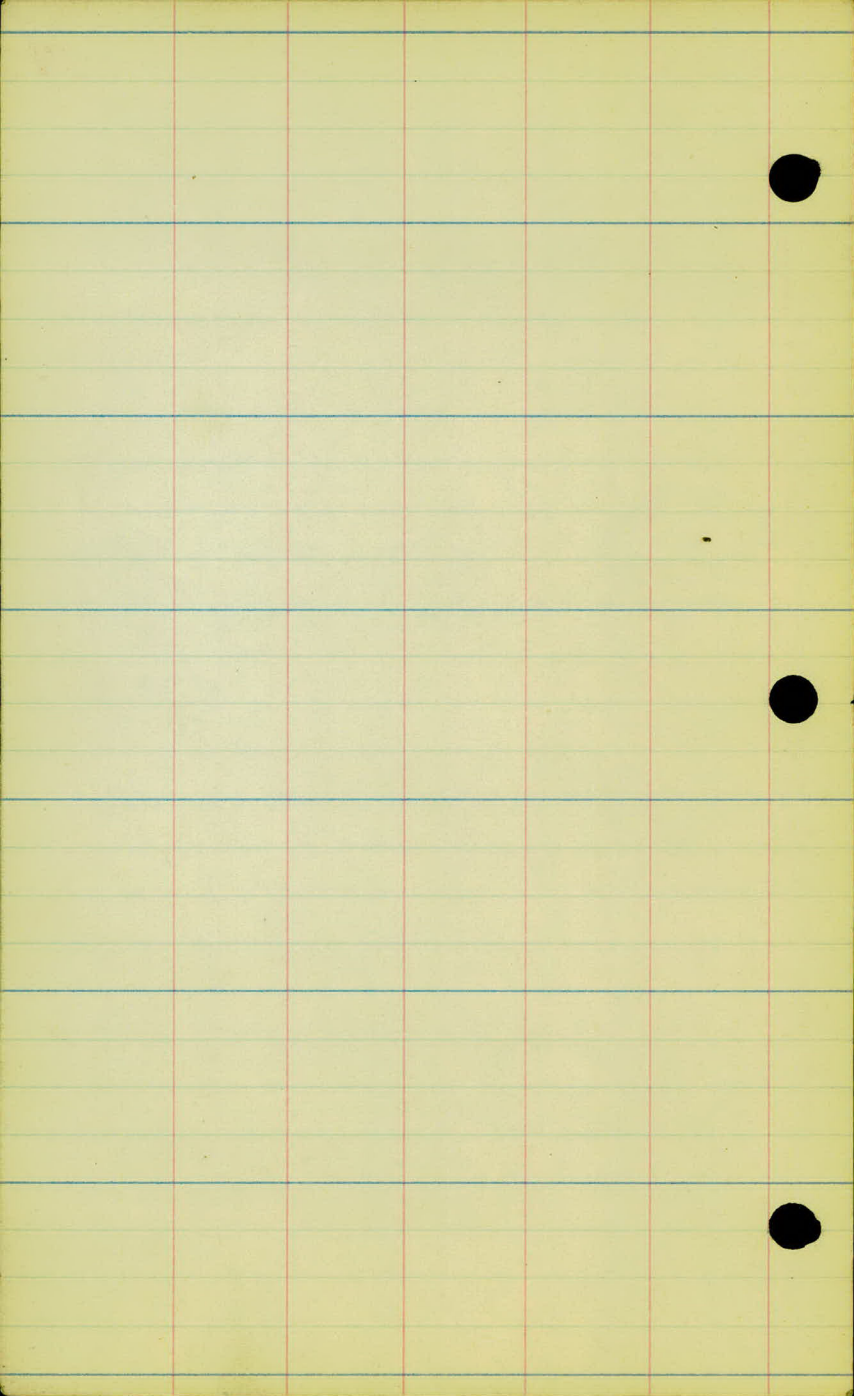
Scattered
Timber

644

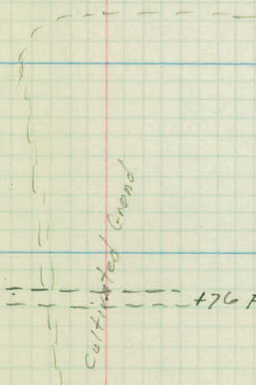
Undeveloped
hand
33°
+ 50 ft. Xing
+ 64 ft. Xing

642.00

641.00



Meadowland



640

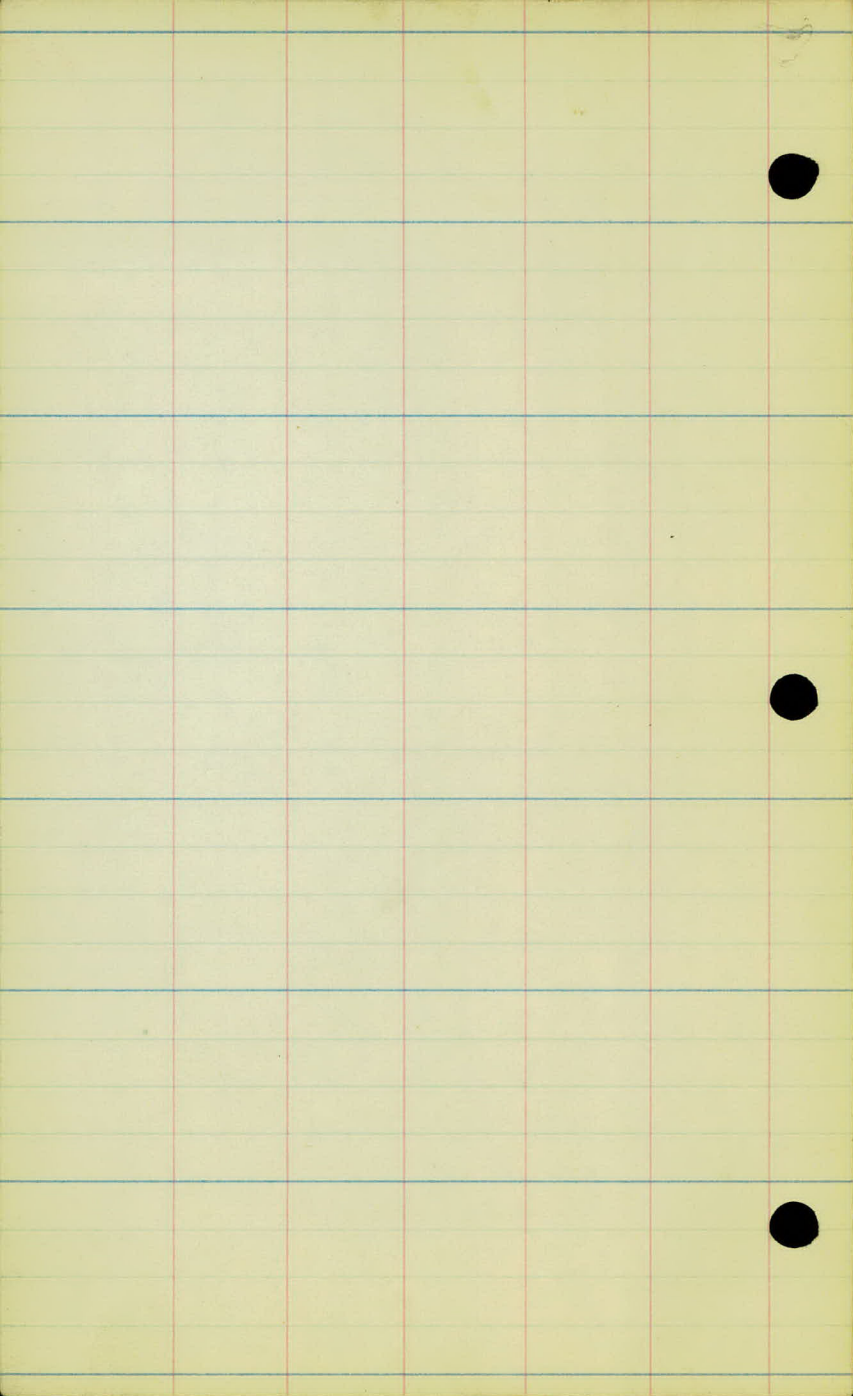
Meadowland

433 Fa. Xing

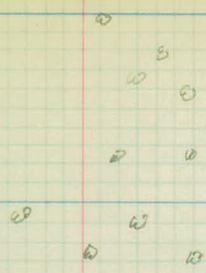
659

658

650

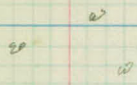


674
85



673

Scattered
Timber

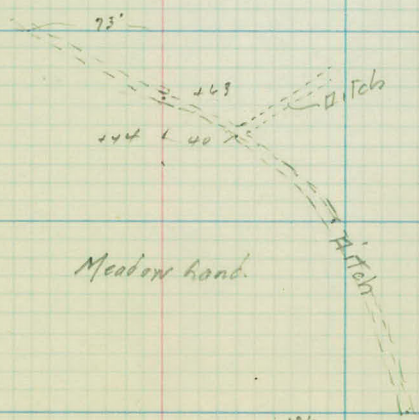


672



671

undeveloped
land.



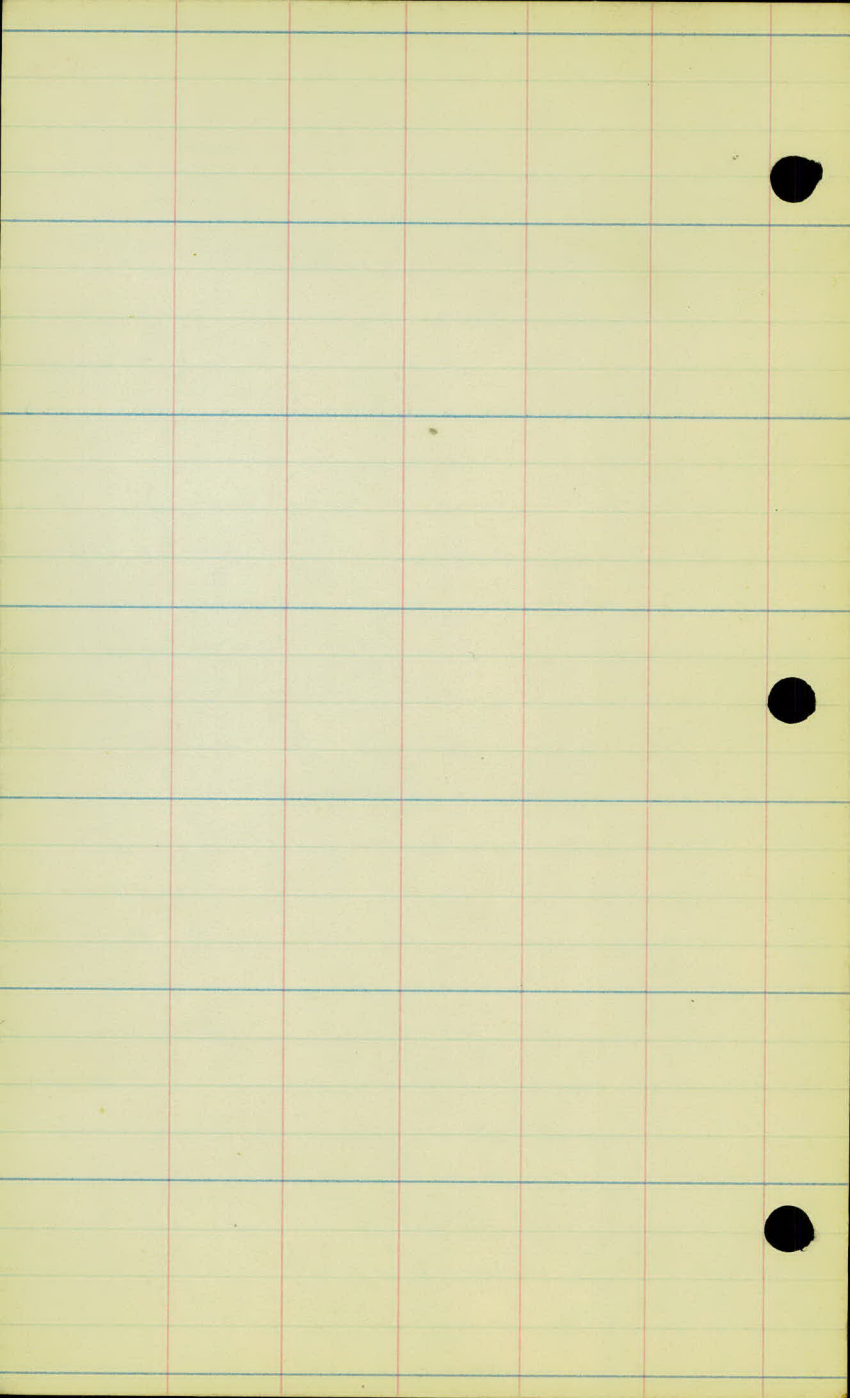
670

669

Meadow land.

136

668



Cultivated
land.

680

77'

679

117 1/2 Rd

678

ROAD

90'

Rd. 90' Rd 677

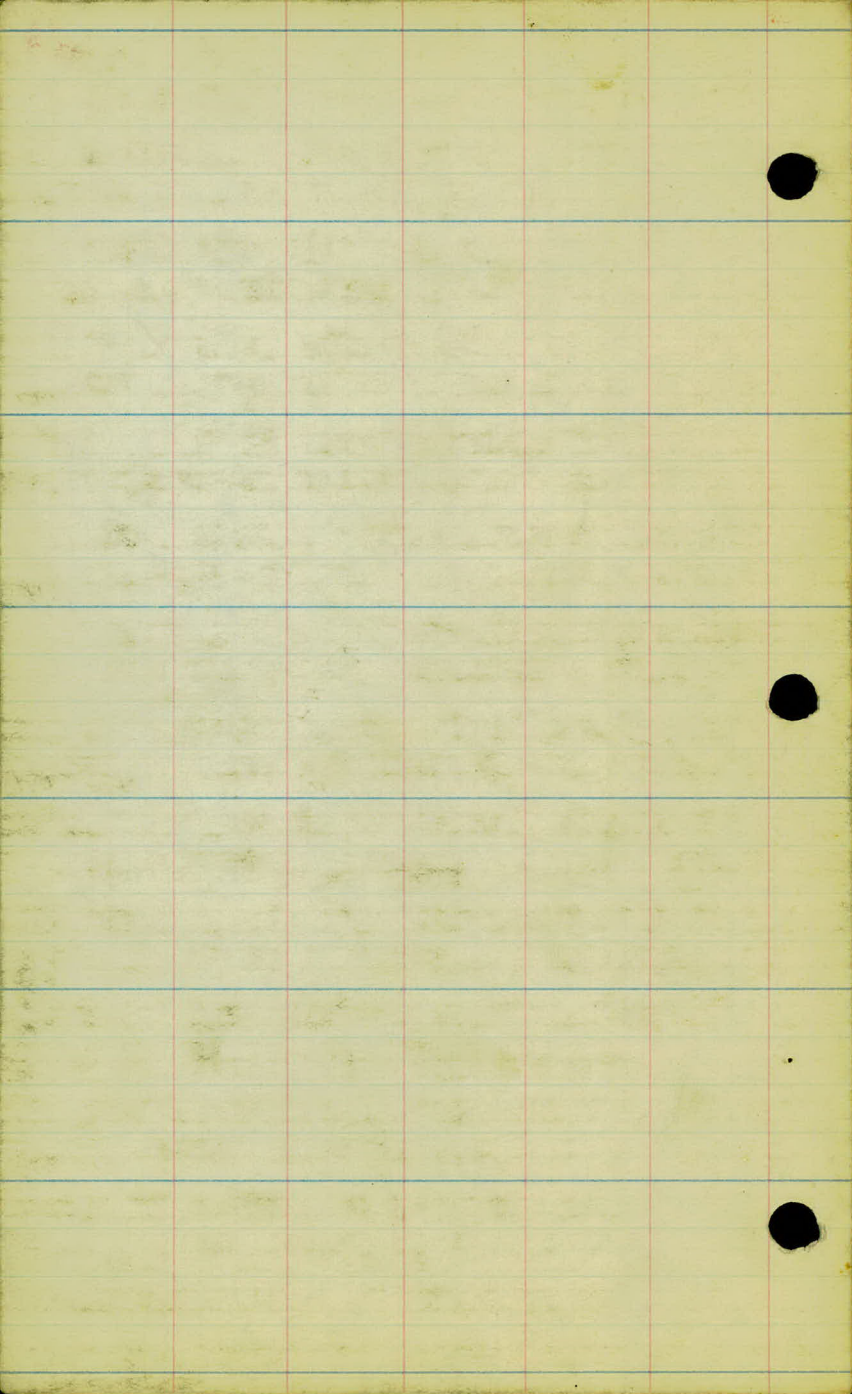
676

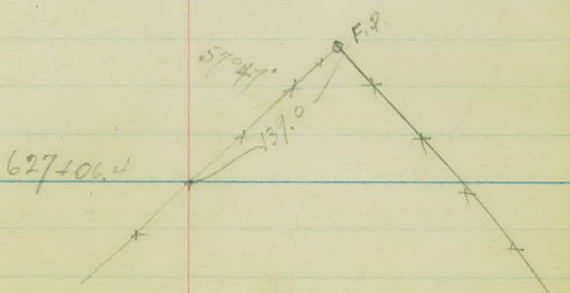
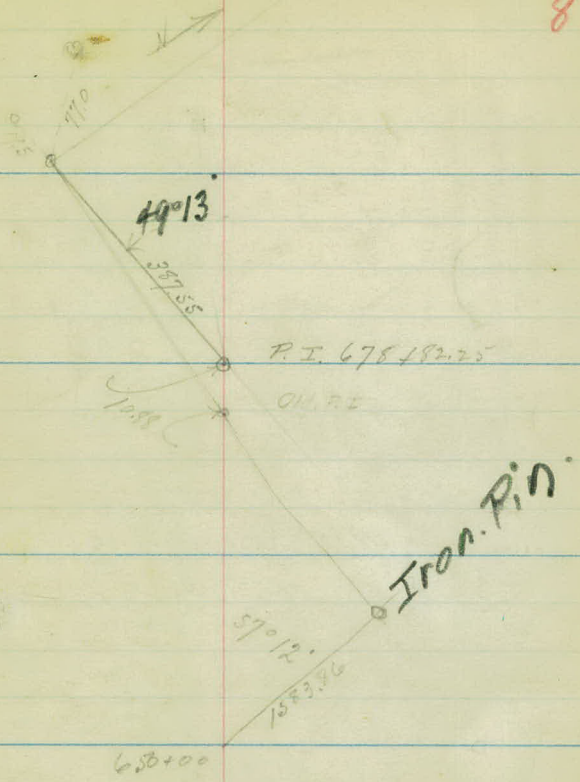
Undeveloped
land

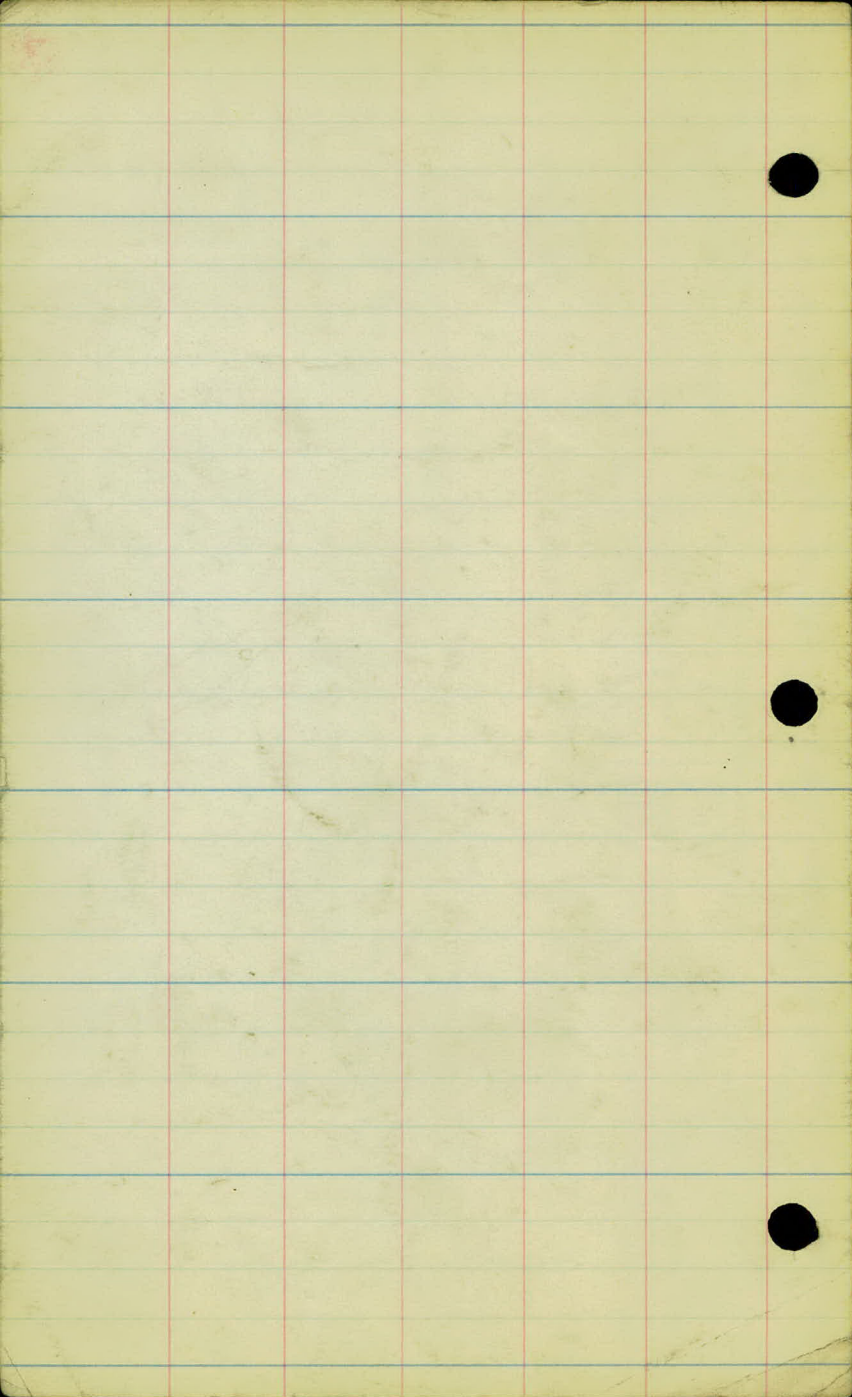
Scattered
Timber

675

674







Road #93.

"H" line Revision.

Sta. 587 - 682

Levels 587-682.

X-Sections - 650 - 682.

Austin	}	2/24/26
SKooglan		
Fritz		
Alexander		
JonKoski		
Wilshusen		

Office of Ramsey Co. Engineer
 ST. PAUL, MINN.

Date Filed.....

File No. 1.....

Sta.	T	H.I	-	Elev
B.M	5.23	916.12		
587+44 ¹⁰	P.C.		4.8	911.3 ✓
588			4.3	11.8 ✓
589			6.0	10.1 ✓
+50			7.7	08.4 ✓
590			9.0	07.1 ✓
591			10.5	05.6 ✓
+50			11.1	05.0 ✓
592			10.7	05.4 ✓
T.P.	7.60	913.82 ✓	9.90	906.22 ✓
593			8.7	05.1 ✓
+50			7.1	06.7 ✓
594			6.2	07.6 ✓
+50			6.8	07.0 ✓
595			4.9	08.9 ✓

910.89 Spike in 20" OAK 110' Lt 588+50

Sta.	+	H.I.	-	Elev.
		913.82 ✓		
595+48			5.9	907.9 ✓
+55			6.6	07.2 ✓
+60			5.0	08.8 ✓
+69.8			4.67	909.15 ✓
+79.3			4.53	909.29 ✓
+88.8			4.42	909.40 ✓
+95			4.5	09.3 ✓
596			6.6	07.2 ✓
+15			9.6	04.2 ✓
+20			8.3	05.5 ✓
+82			6.8	07.0 ✓
+88			4.7	09.1 ✓
597			4.5	09.3 ✓

Edge of Conc Pav.

Central Ave Pavement

<u>445</u>	<u>45</u>	<u>455</u>	<u>465</u>
200	150	100	50

<u>45</u>	<u>46</u>	<u>46</u>	<u>46</u>
50	100	150	200

Edge of Conc Pav.

Sta.	T	H.I.	-	Elev.
		913.82 ✓		
+05			4.9	908.9 ✓
+10			6.5	07.3 ✓
+40			6.8	07.0 ✓
+75			8.5	05.3 ✓
598			5.8	08.0
T.P.	8.45	917.53 ✓	4.74	909.08 ✓
+50			5.0	12.5
599			4.3	13.2 ✓
B.M.			3.47	914.06 ✓
600			5.0	12.5 ✓
+50			7.1	10.4 ✓
601			9.5	08.0 ✓
+50			10.3	07.2 ✓
602			9.6	07.9 ✓
603			8.5	09.0 ✓

3. Nails
SPICE 00 10" OAK 80' Lt. 599+40

900.62 = Elev. Top. Ice. Laddie Lake. 2/24/26.

Sta.		H.I.	-	Elev.
		91753 ✓		
+50			8.9	908.6 ✓
604			8.0	09.5 ✓
T.P.	6.02	91635 ✓	7.70	910.33 ✓
+50			6.1	10.3 ✓
605			7.5	08.9 ✓
+50			11.5	04.9 ✓
606			11.0	05.4 ✓
+50			6.2	10.2 ✓
607			3.3	13.1 ✓
+50			7.2	14.2 ✓
608			7.8	13.6 ✓
T.P.	138	91451 ✓	3.22	913.13 ✓
			913.13	
609			2.6	11.9 ✓
610			5.6	08.9 ✓

Sta.	+	H.I.	-	Elev
		914.51 ✓		
B.M.			4.70	910.31 ✓
	+50		7.6	06.9 ✓
611			8.3	06.2 05.2 ✓
	+50		9.0	05.5 ✓
612			10.5	04.0 ✓
	+50		11.5	03.0 ✓
613			12.4	02.1 ✓
T.P.	643	910.00 ✓	10.94 ✓	903.57 ✓
614			5.6	04.4 ✓
615			5.6	04.4 ✓
616			4.9	05.1 ✓
617			4.8	905.2 ✓
	+50		5.4	04.6 ✓
618			3.8	06.2 ✓

SPK ON 10" OAK STUMP 75' L+ 610+00

Sta.		H.I.		Elev.	Flev.
519.		910.00 ✓			
+50			2.7	907.3 ✓	
619			0.50	09.5 ✓	
T.P.	6.11	915.67 ✓	0.44	909.56 ✓	
+50			5.0	10.7 ✓	
620			3.8	11.9 ✓	
B.M.	4.52	917.03 ✓	3.16	912.51 ✓	
+50				5.3	911.7 ✓
621 +00				6.6	10.4 ✓
+50				9.8	07.2 ✓
+75				11.4	05.6 ✓
622 +00				11.2	05.8 ✓
+50				10.5	06.5 ✓ 07.5 ✓
623 +00				10.2	06.8 ✓
+50				8.1	08.9 ✓
624 +00				7.1	09.9 ✓

2-19-76

94

SPK 00 8" OAK 60' RT 670+05

Station	+	H.I.	-	Red.	Elev.
		917.03 ✓			
624	+50			6.8	910.2 ✓
625	+00			8.9	08.1 ✓
	+50			6.5	10.5 ✓
626	+00			4.1	12.9 ✓
	+50			3.6	13.4 ✓
627	+00			4.3	12.7 ✓
T.P.	7.29	921.02 ✓	3.30	913.73 ✓	
	+50			9.4	11.6 ✓
628	+00			8.5	12.5 ✓
	+50			7.3	13.7 ✓
629	+00			6.6	14.4 ✓
	+50			5.0	16.0 ✓
630	+00			3.4	17.6 ✓
	+25			3.1	17.9 ✓

Station	+	H.I.	-	Red.	Elev.
		921.02 ✓			
630+50				4.2	916.8 ✓
B.M.				9.41	911.61 ✓
631+00				10.1	10.9 ✓
+50				9.2	11.8 ✓
632+00				9.1	11.9 ✓
+50				10.8	10.2 ✓
T.P.	1.95	912.56 ✓	10.41	910.61 ✓	
633+00				6.0	06.6 ✓
+50				6.7	05.9 ✓
634+00				8.6	07.0 ✓
+25				6.0	06.6 ✓
+50				9.1	04.5 ✓
635+00				7.2	05.4 ✓
+50				5.4	07.2 ✓
636+00				5.3	07.3 ✓

Spike in 16" Oak. 50' R# Sta 630+40

Station	+	H.I.	-	Rod	Elev.
		912.56 ✓			
636+50				6.1	906.5 ✓
637+00				4.2	08.4 ✓
+50				2.3	10.3 ✓
638+00				2.7	09.9 ✓
T.P.	5.04	915.88 ✓	1.72	913.84 ✓	
+50				5.2	10.7 ✓
639+00				3.8	12.1 ✓
+50				3.7	12.2 ✓
640+00				5.0	10.9 ✓
B.M.				6.85	909.03 ✓
+50				7.5	08.4 ✓
641+00				10.8	05.1 ✓
+50				14.2	01.7 ✓
T.P.	3.68	908.53 ✓	11.03	904.85 ✓	
642+00				9.1	899.4 ✓
+50				9.6	98.9 ✓

Spike in 12" OAK 60' Rt. Sta. 640+00

Station	+	H.I.	-	Red.	Elev.
		908.53 ✓			
643+00				9.3	899.2 ✓
+50				7.9	900.6 ✓
644+00				5.7	02.8 ✓
+50				5.0	03.5 ✓
645+00				5.7	02.8 ✓
+50				7.1	01.4 ✓
646+00				8.3	900.2 ✓
+50				8.3	900.2 ✓
647+00				8.7	899.8 ✓
T.P.	3.08	903.93 ✓	7.68	900.85	
+50				4.5	99.4 ✓
648+00				5.1	98.8 ✓
B.M.				2.00	901.93 ✓
+50				5.8	98.1 ✓
649+00				6.8	97.1 ✓

Spike in 8" OAK 45' Rt. Jtn 648+40

Station + H.I. - Rod. Elev.

903.93 ✓

649+50 7.0 896.9 ✓

+64 7.2 96.7 ✓

+74 7.6 96.3 ✓

+85 5.7 98.2 ✓

+87 5.0 98.9 ✓

+94 $\frac{1}{2}$ Road. 4.8 99.1 ✓

650+00 5.0 98.9 ✓

+03 5.0 98.9 ✓

+05 5.5 98.4 ✓

+12 7.3 96.6 ✓

+17 7.3 96.6 ✓

+25 7.7 96.2 ✓

+33 6.7 97.2 ✓

FROM R-113

651+00 7.2 96.7 ✓

652+00 7.4 96.5 ✓

653+00 8.0 95.9 ✓

T.P. 6.35 903.46 ✓ 6.82 997.11 ✓

+50 7.1 96.4 ✓

654+00 7.6 95.9 ✓

57.

K

A7.

99

$$\frac{7.2}{50} \quad \frac{7.2}{25.0} \quad 7.2 \quad \frac{7.2}{25.0} \quad \frac{7.0}{50.0}$$

$$\frac{7.7}{50.0} \quad \frac{7.4}{25.0} \quad 7.4 \quad \frac{7.4}{25.0} \quad \frac{7.3}{50}$$

$$\frac{8.2}{50.0} \quad \frac{8.0}{25.0} \quad 8.0 \quad \frac{7.8}{25.0} \quad \frac{7.4}{50.0}$$

$$\frac{7.6}{50.0} \quad \frac{7.2}{25.0} \quad 7.1 \quad \frac{7.4}{25} \quad \frac{7.2}{50.0}$$

$$\frac{7.7}{50.0} \quad \frac{7.4}{25.0} \quad 7.6 \quad \frac{7.3}{25.0} \quad \frac{7.0}{50.0}$$

Station	+	H.I.	-	Rod. Elev.	Flev.
		903.46			
655	+00			7.1	896.4 ✓
	+50			6.8	96.7 ✓
656	+00			6.3	97.2 ✓
	+50			4.8	98.7 ✓
657	+00			5.1	98.4 ✓
658	+00			5.0	98.5 ✓
659	+00			6.2	97.3 ✓
	+76	Field Road			
660	+00			6.6	96.9 ✓
	T.P.	3.11	900.96 ✓	5.61	897.85 ✓
661	+00			4.0	97.0 ✓
662	+00			4.0	97.0 ✓
663	+00			4.3	96.7 ✓
664	+00			6.0	95.0 ✓
	+50			8.2	92.8 ✓

ht. # ft.

655-100

$\frac{7.0}{50.0}$ $\frac{7.8}{38.0}$ $\frac{7.2}{25.0}$ 7.1 $\frac{7.3}{25.0}$ $\frac{7.1}{50.0}$

$\frac{7.0}{50.0}$ $\frac{7.0}{30.0}$ $\frac{6.7}{10.0}$ 6.8 $\frac{6.6}{25.0}$ $\frac{6.4}{37.0}$ $\frac{5.6}{50.0}$

$\frac{6.6}{50.0}$ $\frac{6.7}{25.0}$ 6.3 $\frac{4.8}{30.0}$ $\frac{4.4}{50.0}$

$\frac{6.7}{50.0}$ $\frac{6.2}{25.0}$ 4.8 $\frac{4.6}{25.0}$ $\frac{4.6}{50.0}$

$\frac{6.4}{50.0}$ $\frac{5.6}{25.0}$ 5.1 $\frac{5.0}{25.0}$ $\frac{4.2}{50.0}$

$\frac{6.2}{50.0}$ $\frac{5.6}{25.0}$ 5.0 $\frac{4.6}{25.0}$ $\frac{4.6}{50.0}$

$\frac{6.4}{50.0}$ $\frac{6.2}{25.0}$ 6.2 $\frac{6.2}{25.0}$ $\frac{6.8}{50.0}$

$\frac{8.5}{50.0}$ $\frac{7.7}{37.0}$ $\frac{7.4}{33.0}$ $\frac{7.2}{25.0}$ 6.6 $\frac{6.4}{25.0}$ $\frac{6.4}{50.0}$

$\frac{5.0}{50.0}$ $\frac{4.7}{47.0}$ $\frac{4.2}{42.0}$ 4.0 $\frac{3.3}{25.0}$ $\frac{3.0}{50.0}$

$\frac{4.8}{50.0}$ $\frac{4.4}{25.0}$ 4.0 $\frac{3.5}{25.0}$ $\frac{3.7}{50.0}$

$\frac{5.5}{50.0}$ $\frac{4.8}{25.0}$ 4.3 $\frac{3.8}{25.0}$ $\frac{3.8}{50.0}$

$\frac{8.2}{50.0}$ $\frac{7.7}{44.0}$ $\frac{7.3}{36.0}$ $\frac{6.8}{25.0}$ 6.0 $\frac{5.5}{25.0}$ $\frac{5.2}{50.0}$

$\frac{9.2}{50.0}$ $\frac{8.6}{25.0}$ 8.2 $\frac{8.0}{25.0}$ $\frac{7.5}{50.0}$

Station	+	H.I.	-	Rod Elev.	Flev.
		900.96 ✓			
665	+00			6.8	892.2 ✓
666	+00			7.7	93.3 ✓
667	+00			8.0	93.0 ✓
	T.P.	5.30	899.24 ✓	7.02	892.94 ✓
	+50			6.4	92.8 ✓
668	+00			7.4	91.8 ✓
	+50			7.8	91.4 ✓
669	+00			7.2	92.0 ✓
	+50			7.5	91.7 ✓
	+58.5			5.3	90.9 ✓
	+59.5	Ditch Bottom		10.0	89.2 ✓
	+63	✓ ✓		10.6	88.6 ✓
	+64.5			5.2	91.0 ✓
670	+00			7.5	91.7 ✓
	+50			5.2	94.0 ✓
671	+00			4.4	94.8 ✓

ht

k

RH.

101

$$\frac{9.2}{50.0} \quad \frac{8.6}{25.0} \quad 8.8 \quad \frac{8.3}{25.0} \quad \frac{8.0}{50.0}$$

$$\frac{9.5}{50.0} \quad \frac{9.0}{30.0} \quad \frac{8.5}{13.0} \quad 7.7 \quad \frac{7.3}{25.0} \quad \frac{8.0}{50.0}$$

$$\frac{9.0}{50.0} \quad \frac{8.5}{25.0} \quad 8.0 \quad \frac{7.5}{25.0} \quad \frac{7.0}{50.0}$$

$$\frac{6.2}{50.0} \quad \frac{6.0}{25.0} \quad 6.4 \quad \frac{7.2}{25.0} \quad \frac{6.5}{50.0}$$

$$\frac{7.2}{50.0} \quad \frac{7.0}{30.0} \quad 7.4 \quad \frac{7.4}{25.0} \quad \frac{7.0}{50.0}$$

$$\frac{8.0}{50.0} \quad \frac{8.4}{25.0} \quad 7.8 \quad \frac{7.8}{25.0} \quad \frac{7.6}{50.0}$$

$$\frac{7.0}{50.0} \quad \frac{7.2}{25.0} \quad 7.2 \quad \frac{7.2}{20.0} \quad \frac{7.8}{45.0} \quad \frac{7.6}{50.0}$$

$$\frac{8.6}{50.0} \quad \frac{8.2}{25.0} \quad 7.5 \quad \frac{7.5}{25.0} \quad \frac{7.7}{50.0}$$

$$\frac{7.2}{50.0} \quad \frac{7.0}{25.0} \quad 7.5 \quad \frac{7.5}{25.0} \quad \frac{8.0}{50.0}$$

$$\frac{6.4}{50.0} \quad \frac{5.5}{25.0} \quad 5.2 \quad \frac{5.5}{25.0} \quad \frac{5.7}{50.0}$$

$$\frac{6.4}{50} \quad \frac{5.0}{25.0} \quad 4.4 \quad \frac{4.4}{25.0} \quad \frac{4.7}{50.0}$$

Station	+	H.I.	-	Rod.	Elev.
		899.24 ✓			
671+50				3.2	896.0 ✓
B.M.				1.18	898.06 ✓
672+00				3.2	96.0 ✓
+50				3.2	96.0 ✓
T.P.	3.98	901.68 ✓	1.54	897.70 ✓	
673+00				5.8	95.9 ✓
674+00				7.8	93.9 ✓
675+00				7.0	94.7 ✓
T.P.	4.32	899.75 ✓	6.25	895.43 ✓	
+50				5.0	94.8 ✓
676+00				5.7	94.1 ✓
+50				6.3	93.5 ✓
677+00				6.0	93.8 ✓
+50				7.0	92.8 ✓
B.M.				1.38	898.37 ✓
678+00				6.5	93.3 ✓

H.

*

R.

$\frac{4.7}{50.0}$	$\frac{4.0}{37.0}$	$\frac{3.6}{25.0}$	3.2	$\frac{3.4}{25.0}$	$\frac{3.3}{50.0}$
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Spike in 18" Oak 40' R4 Sta 671+65

$\frac{5.0}{50.0}$	$\frac{5.0}{47.0}$	$\frac{4.7}{35.0}$	$\frac{4.2}{25.0}$	3.2	$\frac{2.7}{25.0}$	$\frac{2.7}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{4.4}{25.0}$	3.2	$\frac{2.4}{25.0}$	$\frac{2.2}{50.0}$
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$\frac{8.2}{50.0}$	$\frac{7.8}{37.0}$	$\frac{7.5}{25.0}$	5.8	$\frac{5.3}{25.0}$	$\frac{4.5}{50.0}$
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$\frac{8.3}{50.0}$	$\frac{8.2}{25.0}$	7.8	$\frac{7.2}{25.0}$	$\frac{6.0}{50.0}$
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$\frac{9.0}{50.0}$	$\frac{8.0}{25.0}$	7.0	$\frac{6.3}{70.0}$	$\frac{6.0}{50.0}$
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$\frac{8.0}{50.0}$	$\frac{6.8}{25.0}$	5.0	$\frac{4.7}{4.0}$	$\frac{4.0}{7.0}$	$\frac{4.0}{29.0}$	$\frac{3.6}{50.0}$
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$\frac{8.0}{50.0}$	$\frac{7.0}{25.0}$	5.7	$\frac{5.0}{9.0}$	$\frac{4.0}{15.0}$	$\frac{3.6}{35.0}$	$\frac{3.4}{50.0}$
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$\frac{8.4}{50.0}$	$\frac{7.6}{26.0}$	6.3	$\frac{5.3}{19.0}$	$\frac{4.6}{24.0}$	$\frac{3.5}{50.0}$
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$\frac{7.7}{50.0}$	$\frac{6.8}{25.0}$	6.0	$\frac{4.7}{30.0}$	$\frac{4.2}{50.0}$
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$\frac{6.5}{50.0}$	$\frac{7.0}{30.0}$	$\frac{6.5}{13.0}$	7.0	$\frac{7.4}{25.0}$	$\frac{5.4}{50.0}$
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Spike in 16" Oak 125' R4 Sta 677+50

$\frac{6.4}{50.0}$	$\frac{6.4}{35.0}$	$\frac{6.2}{15.0}$	6.5	$\frac{6.3}{25.0}$	$\frac{5.4}{40.0}$	$\frac{5.2}{50.0}$
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Station	+	H.I.	-	Rod	Elev.
		899.75 ✓			
679+00				4.2	895.6 ✓
680+00				3.5	96.3 ✓
B.M.				3.77	896.06 } ✓
+50				4.0	895.98 } ✓
681+00				5.2	94.6 ✓
+50				6.7	93.1 ✓
682+00				8.8	91.0 ✓
+59.58	P.T. =			11.0	88.8 ✓
B.M.				3.77	895.98 ✓

TO B - 92

H.

4

H.

103

$$\frac{3.8}{50.0} \quad \frac{4.0}{25.0} \quad 4.2 \quad \frac{4.2}{25.0} \quad \frac{3.7}{50.0}$$

$$\frac{3.8}{50.0} \quad \frac{3.5}{25.0} \quad 3.5 \quad \frac{3.5}{25.0} \quad \frac{3.7}{50.0}$$

Spike in stp. 70' ht sta 680+40 = 707+

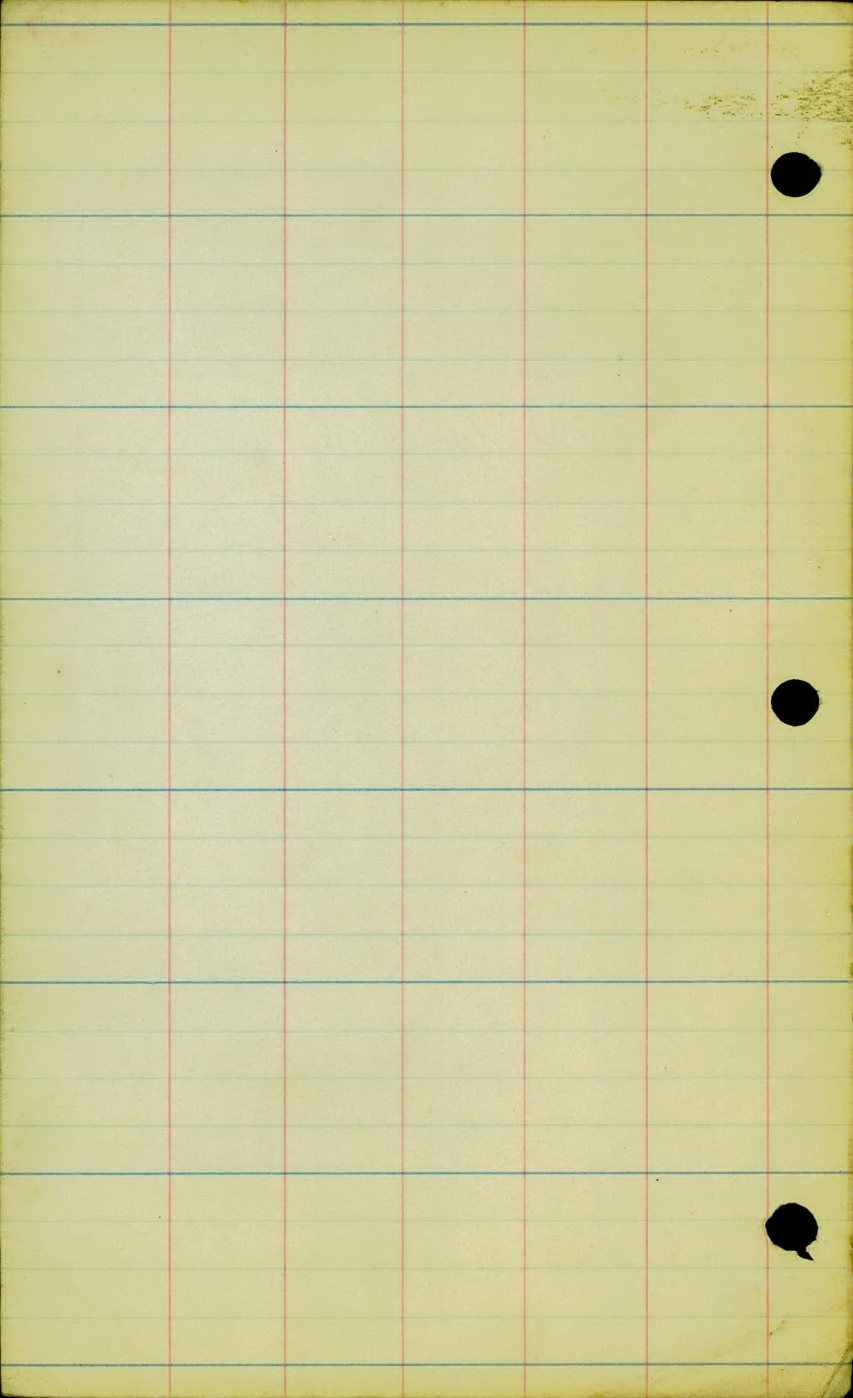
$$\frac{4.3}{50.0} \quad \frac{4.2}{25.0} \quad 4.0 \quad \frac{4.0}{25.0} \quad \frac{4.4}{50.0}$$

$$\frac{5.2}{50.0} \quad \frac{5.2}{25.0} \quad 5.2 \quad \frac{5.5}{25.0} \quad \frac{6.0}{50.0}$$

$$\frac{6.0}{50.0} \quad \frac{6.5}{20.0} \quad 6.7 \quad \frac{7.4}{25.0} \quad \frac{7.8}{50.0}$$

$$\frac{7.2}{50.0} \quad \frac{7.6}{25.0} \quad 8.8 \quad \frac{10.2}{25.0} \quad \frac{10.2}{50.0}$$

$$\frac{11.0}{50.0} \quad \frac{11.0}{25.0} \quad 11.0 \quad \frac{10.7}{25.0} \quad \frac{10.8}{50.0}$$



Anoka Line
X-sections

Line change.

Sta. 587+44.5 to 682+

FROM B-78

Station	+	H.I	-	Elev.
B.M.	4.55	915.44 ✓		910.89
587+44.1				11.3 ✓
588				11.8 ✓
+50				11.3 ✓
589				10.4 ✓
+50				08.2 ✓
590				07.2 ✓
+50				06.6 ✓
591				05.7 ✓
592				05.4 ✓
T.P.	6.94	913.18 ✓	9.20	906.24
593				06.1 ✓
594				07.7 ✓
+50				07.2 ✓
595				08.8 ✓

Lt.

2

Rt.

W.H.C
A.L.P.
H.B.
M.O.
105
2-24-16

Spike in 20" Oak 110 Lt. 588 + 50

$\frac{3.9}{50}$

$\frac{3.9}{40}$

41

$\frac{3.8}{40}$

$\frac{3.8}{50}$

$\frac{3.8}{50}$

$\frac{3.7}{25}$

$\frac{3.6}{-}$

$\frac{3.5}{26}$

$\frac{3.2}{50}$

$\frac{4.2}{50}$

$\frac{4.2}{25}$

$\frac{4.1}{0.0}$

$\frac{3.7}{30}$

$\frac{3.5}{50}$

$\frac{5.0}{50}$

$\frac{5.0}{8}$

$\frac{5.0}{-}$

$\frac{5.1}{30}$

$\frac{4.8}{50}$

$\frac{7.6}{50}$

$\frac{7.3}{27}$

72

$\frac{7.0}{30}$

$\frac{6.4}{50}$

$\frac{8.3}{50}$

$\frac{8.2}{26}$

$\frac{8.2}{-}$

$\frac{7.5}{30}$

$\frac{7.2}{50}$

$\frac{8.0}{50}$

$\frac{8.3}{28}$

$\frac{8.8}{-}$

$\frac{8.3}{27}$

$\frac{7.6}{50}$

$\frac{10.2}{50}$

$\frac{9.7}{29}$

77

$\frac{9.6}{33}$

$\frac{9.3}{50}$

$\frac{8.9}{50}$

$\frac{9.5}{30}$

100

$\frac{10.8}{26}$

$\frac{11.2}{50}$

$\frac{5.5}{50}$

$\frac{7.0}{24}$

$\frac{7.1}{-}$

$\frac{7.6}{30}$

$\frac{7.8}{50}$

$\frac{4.0}{50}$

$\frac{4.3}{27}$

55

$\frac{6.6}{30}$

$\frac{6.8}{50}$

$\frac{4.6}{50}$

$\frac{5.2}{27}$

60

$\frac{5.6}{27}$

$\frac{5.6}{50}$

$\frac{3.8}{50}$

$\frac{4.1}{28}$

44

$\frac{4.7}{17}$

$\frac{5.2}{50}$

Station	+	H.I	-	Elev.
595+47		93.18 ✓		08.1 ✓
+58				07.3 ✓
+64				09.0 ✓
+80				09.18 ✓
+95				09.4 09.3
596+00				07.3 ✓
+15				04.4 ✓
+82				07.4 ✓
597				09.4 ✓
+11				07.4 ✓
T.P.	4.80	915.06 ✓	2.92	910.26 ✓
+43				06.7 ✓
+64				05.5 ✓
598+00				08.4 ✓

4. 2 Pt.

$\frac{40}{50}$	$\frac{43}{29}$	5.1	$\frac{5.1}{16}$	$\frac{5.8}{28}$	$\frac{4.0}{43}$	$\frac{4.0}{50}$
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$\frac{43}{50}$	$\frac{5.2}{26}$	5.9	$\frac{4.1}{17}$	$\frac{3.9}{50} = \text{ave.}$
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$\frac{4.6}{50}$	$\frac{5.2}{39}$	$\frac{5.3}{16}$	4.2	$\frac{4.0}{11}$	$\frac{3.9}{50}$
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$\frac{4.2}{50}$			3.90	$\frac{3.2}{30}$	$\frac{3.8}{50}$
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$\frac{4.0}{50}$			3.8	$\frac{2.0}{27}$	$\frac{3.3}{50}$
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$\frac{3.7}{50}$	$\frac{3.8}{12}$		3.9	$\frac{2.7}{20}$	$\frac{2.3}{50}$
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$\frac{3.6}{50}$	$\frac{3.6}{24}$	$\frac{3.3}{12}$	3.8	$\frac{2.7}{16}$	$\frac{3.1}{50}$
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$\frac{6.2}{50}$	$\frac{6.0}{27}$		5.8	$\frac{6.0}{28}$	$\frac{6.1}{50}$
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$\frac{3.8}{50}$	$\frac{3.3}{26}$		3.8	$\frac{3.8}{30}$	$\frac{3.7}{50}$
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$\frac{5.3}{50}$			5.8		$\frac{5.8}{50}$
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$\frac{8.3}{50}$	$\frac{8.2}{26}$		8.4	$\frac{7.8}{26}$	$\frac{7.2}{50}$
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$\frac{8.6}{50}$	$\frac{7.5}{27}$		7.6	$\frac{7.2}{28}$	$\frac{8.1}{50}$
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$\frac{6.0}{50}$	$\frac{6.4}{30}$		6.7		$\frac{6.8}{50}$
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station	+	H.I	-	Elev.
		915.06		
598+50				12.1 ✓
T.P.	5.02	918.30 ✓	1.78	913.28 ✓
599				13.4 ✓
+50				13.5 ✓
P.M.	4.23	918.30 ✓	4.23	914.07
600				12.6 ✓
+50				10.5 ✓
T.P.	5.42	913.55 ✓	10.17	908.13 ✓
601				08.2 ✓
+50				07.2 ✓
602				08.1 ✓
+50				09.2 ✓
603				09.3 ✓
+50				08.7 ✓
604				09.6 ✓
T.P.	6.00	916.35 ✓	3.20	910.35 ✓

Lt. 2 Rt.

$\frac{26}{50}$ $\frac{25}{28}$ 30 $\frac{31}{28}$ $\frac{33}{40}$ $\frac{30}{50}$

$\frac{46}{50}$ $\frac{45}{25}$ $\frac{49}{-}$ $\frac{51}{28}$ $\frac{51}{50}$

$\frac{53}{50}$ $\frac{48}{25}$ 48 $\frac{51}{25}$ $\frac{53}{50}$

3- nails 10" Oak 80' Lt. No. 599+40

$\frac{52}{50}$ $\frac{57}{21}$ 57 $\frac{69}{27}$ $\frac{66}{50}$

$\frac{80}{50}$ $\frac{80}{32}$ 78 $\frac{84}{25}$ $\frac{90}{50}$

$\frac{53}{50}$ $\frac{52}{29}$ 54 $\frac{60}{27}$ $\frac{69}{50}$

$\frac{65}{50}$ $\frac{64}{25}$ 64 $\frac{71}{28}$ $\frac{83}{50}$

$\frac{66}{50}$ $\frac{61}{25}$ $\frac{55}{-}$ $\frac{55}{24}$ $\frac{53}{50}$

$\frac{60}{50}$ $\frac{57}{30}$ $\frac{44}{-}$ $\frac{34}{40}$ $\frac{34}{50}$

$\frac{57}{50}$ $\frac{49}{20}$ $\frac{43}{-}$ $\frac{42}{34}$ $\frac{42}{50}$

$\frac{52}{50}$ $\frac{49}{25}$ $\frac{49}{-}$ $\frac{50}{29}$ $\frac{50}{50}$

$\frac{30}{50}$ $\frac{37}{27}$ 40 $\frac{49}{20}$ $\frac{42}{50}$

Station	+	H.I	-	Elev.
		916.35 ✓		
604+50				10.1 ✓
605+00				08.9 ✓
+46				05.4 ✓
606				06.0 ✓
+50	r.c.			10.3 ✓
607				13.4 ✓
+50				14.3 ✓
608				13.7 ✓
T.P.	0.56	915.14 ✓	1.77	914.58 ✓
609				11.9 ✓
+50				10.8 ✓
610				09.0 ✓
B.M.	4.81	915.14	4.81	910.33 ✓
+50				07.0 ✓

Lt		L	Rt	
$\frac{4.5}{50}$	$\frac{5.3}{22}$	63	$\frac{7.1}{23}$	$\frac{6.0}{50}$
$\frac{5.3}{50}$	$\frac{6.6}{20}$	75	$\frac{7.9}{18}$	$\frac{6.8}{43}$ $\frac{9.0}{50}$
$\frac{6.5}{50}$	$\frac{10.0}{20}$	<u>110</u>	$\frac{10.4}{24}$	$\frac{6.6}{36}$ $\frac{8.6}{50}$
$\frac{11.4}{50}$	$\frac{11.4}{23}$	<u>104</u>	$\frac{7.1}{24}$	$\frac{7.4}{43}$ $\frac{8.3}{50}$
$\frac{7.5}{50}$	$\frac{7.1}{24}$	<u>61</u>		$\frac{5.8}{34}$ $\frac{8.5}{50}$
$\frac{5.8}{50}$	$\frac{3.8}{25}$	30		$\frac{2.9}{23}$ $\frac{4.2}{39}$ $\frac{7.5}{50}$
$\frac{3.9}{50}$	$\frac{3.0}{30}$	21		$\frac{3.6}{41}$ $\frac{6.8}{50}$
$\frac{3.8}{50}$	$\frac{2.7}{15}$	<u>27</u>	$\frac{3.2}{32}$	$\frac{4.9}{45}$ $\frac{6.0}{50}$
$\frac{3.0}{50}$	$\frac{3.0}{33}$	32		$\frac{4.2}{35}$ $\frac{7.6}{50}$
$\frac{3.7}{50}$	$\frac{4.0}{22}$	<u>43</u>	$\frac{5.1}{34}$	$\frac{8.1}{50}$
$\frac{5.2}{50}$	$\frac{5.5}{26}$	61	$\frac{6.1}{30}$	$\frac{9.2}{50}$

spike on 10" oak stump 75' Lt. Sta 610400

$\frac{2.1}{50}$	$\frac{7.9}{15}$	81	$\frac{7.6}{30}$	$\frac{9.0}{50}$
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Station	+	H.I	-	Elev.	
611 to 0		915.14 ✓		06.3	✓
747	RT.			05.6	✓
612				04.1	✓
613				02.7	✓
T.R	6.24	909.88 ✓	11.50	903.64	✓
614				04.5	✓
615				04.4	✓
616				05.0	✓
617				05.2	✓
618 ✓				06.3	✓
619				09.5	✓
T.P.	6.24	915.80 ✓	032	909.56	✓
620				12.0	✓
B.M.	3.25	915.80 ✓	3.25	912.55	✓
621				10.6	✓

$\frac{94}{50}$	$\frac{92}{23}$	$\frac{88}{}$	$\frac{87}{28}$	$\frac{87}{50}$
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$\frac{100}{50}$	$\frac{78}{33}$	$\frac{95}{}$	$\frac{98}{28}$	$\frac{89}{50}$
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$\frac{113}{50}$	$\frac{108}{25}$	$\frac{110}{}$	$\frac{114}{26}$	$\frac{114}{50}$
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$\frac{112}{50}$	$\frac{118}{30}$	$\frac{124}{}$	$\frac{121}{17}$	$\frac{123}{50}$
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$\frac{60}{50}$	$\frac{56}{25}$	$\frac{54}{}$	$\frac{52}{30}$	$\frac{47}{50}$
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$\frac{59}{50}$	$\frac{58}{25}$	$\frac{55}{}$	$\frac{52}{30}$	$\frac{46}{50}$
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$\frac{45}{50}$	$\frac{45}{28}$	$\frac{49}{}$	$\frac{49}{25}$	$\frac{49}{50}$
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$\frac{43}{50}$	$\frac{48}{20}$	$\frac{47}{}$	$\frac{44}{28}$	$\frac{43}{50}$
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$\frac{44}{50}$	$\frac{43}{25}$	$\frac{36}{}$	$\frac{37}{25}$	$\frac{32}{50}$
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$\frac{28}{50}$	$\frac{10}{25}$	$\frac{54}{}$	$\frac{48}{28}$	$\frac{42}{50}$
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$\frac{43}{50}$	$\frac{31}{25}$	$\frac{38}{}$	$\frac{45}{30}$	$\frac{43}{50}$
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8" Dak 60' H. Sta. 620 + 05

$\frac{48}{50}$	$\frac{48}{25}$	$\frac{57}{}$	$\frac{60}{25}$	$\frac{72}{50}$
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station	+	H.I	-	Elev.
621+50		915.80 ✓		07.4 ✓
622				06.0 ✓
623				06.9 ✓
623+50				09.0 ✓
624				08.1 ✓ 10.1 ✓
+50				10.5 ✓
625				08.3 ✓
+50				10.1 ✓
626				13.0 ✓
T.P	6.10	919.86 ✓	2.04	913.76 ✓
+50				13.6 ✓
627				12.8 ✓
+50				11.9 ✓
628				12.7 ✓

Lt.

\$

Rt.

$\frac{6.1}{50}$	$\frac{7.0}{29}$	8.4	$\frac{93}{25}$	$\frac{8.7}{50}$
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$\frac{6.7}{50}$	$\frac{8.2}{28}$	9.8	$\frac{9.3}{30}$	$\frac{8.8}{50}$
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$\frac{7.5}{50}$	$\frac{8.2}{27}$	8.9	$\frac{8.2}{22}$	$\frac{6.7}{50}$
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$\frac{4.8}{50}$	$\frac{5.9}{25}$	6.8	$\frac{6.8}{25}$	$\frac{6.5}{50}$
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$\frac{3.4}{50}$	$\frac{3.7}{35}$	5.7	$\frac{4.6}{28}$	$\frac{7.1}{50}$
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$\frac{4.1}{50}$	$\frac{4.5}{28}$	5.3	$\frac{5.1}{23}$	$\frac{6.8}{50}$
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$\frac{5.8}{50}$	$\frac{7.0}{27}$	7.5	$\frac{7.3}{27}$	$\frac{8.0}{50}$
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$\frac{4.1}{50}$	$\frac{4.7}{30}$	5.7	$\frac{5.5}{29}$	$\frac{5.1}{50}$
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$\frac{2.5}{50}$	$\frac{2.0}{22}$	2.8	$\frac{4.2}{27}$	$\frac{5.1}{50}$
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Top Stake 626

Feb 25, 1926

$\frac{6.0}{50}$	$\frac{5.8}{20}$	6.3	$\frac{7.8}{24}$	$\frac{9.5}{50}$
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$\frac{5.7}{50}$	$\frac{6.2}{25}$	7.1	$\frac{8.2}{25}$	$\frac{9.2}{50}$
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$\frac{4.0}{50}$	$\frac{5.0}{23}$	8.0	$\frac{9.5}{20}$	$\frac{10.7}{50}$
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$\frac{5.4}{50}$	$\frac{6.4}{25}$	7.2	$\frac{9.0}{25}$	$\frac{11.7}{50}$
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station	+	H.I	-	Elev.
		919.86 ✓		
628+60				14.8 ✓
629+00				15.5 ✓ 14.5 ✓
+50				16.0 ✓
630+00				17.6 ✓
+40				17.3 ✓
B.M.	692	918.57 ✓	821	911.65 ✓
631+00				11.0 ✓
632+00				12.1 ✓
+50				10.2 ✓
633+00				06.6 ✓
+50				06.1 ✓
634+00				07.1 ✓
T.P.	764	915.62 ✓	10.59	907.98 ✓
+50				04.9 ✓
635				05.4 ✓

H. L RH

$\frac{4.7}{50}$ $\frac{4.8}{25}$ $\frac{5.1}{50}$ $\frac{7.3}{18}$ $\frac{9.7}{50}$

$\frac{4.4}{50}$ $\frac{4.8}{22}$ $\frac{5.4}{50}$ $\frac{7.7}{25}$ $\frac{10.6}{50}$

$\frac{2.7}{50}$ $\frac{2.8}{25}$ $\frac{3.9}{50}$ $\frac{5.6}{23}$ $\frac{8.9}{50}$

$\frac{1.3}{50}$ $\frac{0.8}{25}$ $\frac{2.3}{50}$ $\frac{5.2}{28}$ $\frac{8.7}{50}$

$\frac{1.6}{50}$ $\frac{1.7}{19}$ $\frac{2.6}{50}$ $\frac{5.8}{18}$ $\frac{7.2}{50}$

16" oak 50' RT+ Sta 630 + 40

$\frac{6.1}{50}$ $\frac{7.4}{25}$ $\frac{7.6}{50}$ $\frac{7.8}{25}$ $\frac{7.8}{50}$

$\frac{3.6}{50}$ $\frac{5.7}{25}$ $\frac{6.5}{50}$ $\frac{6.7}{25}$ $\frac{6.7}{50}$

$\frac{3.1}{50}$ $\frac{6.8}{24}$ $\frac{8.4}{50}$ $\frac{9.3}{23}$ $\frac{9.3}{50}$

$\frac{7.8}{50}$ $\frac{9.9}{22}$ $\frac{12.0}{50}$ $\frac{12.1}{30}$ $\frac{12.9}{50}$

$\frac{11.6}{50}$ $\frac{11.4}{30}$ $\frac{12.5}{50}$ $\frac{13.0}{22}$ $\frac{12.9}{58}$

$\frac{7.5}{50}$ $\frac{9.3}{29}$ $\frac{11.5}{50}$ $\frac{12.8}{28}$ $\frac{13.5}{50}$

$\frac{2.9}{50}$ $\frac{7.6}{25}$ $\frac{10.7}{50}$ $\frac{11.9}{27}$ $\frac{12.9}{50}$

$\frac{5.1}{50}$ $\frac{8.2}{27}$ $\frac{10.2}{50}$ $\frac{11.6}{28}$ $\frac{12.1}{50}$

Station	+	H.I	-	Elev.
		915.62 ✓		
635+50				07.3 ✓
636+00				07.6 ✓
+50				06.8 ✓
637+00				08.6 ✓
+50				09.9 ✓
638+00				10.1 ✓
639				12.3 ✓
+50				12.3 ✓
640				11.1 ✓
B.M.	2.89	911.96 ✓	1.55	909.07 ✓
+50				(08.4) 08.6 ✓
641				(05.0) 05.2 ✓
+63				(00.5) 00.7 ✓
642				(899.3) 899.5 ✓

L Z Rt.

$$\frac{48}{50} \quad \frac{66}{28} \quad 8.3 \quad \frac{104}{25} \quad \frac{109}{50}$$

$$\frac{48}{50} \quad \frac{65}{29} \quad \frac{80}{1} \quad \frac{84}{30} \quad \frac{79}{50}$$

$$\frac{78}{50} \quad \frac{86}{27} \quad \frac{88}{1} \quad \frac{85}{24} \quad \frac{70}{50}$$

$$\frac{80}{50} \quad \frac{24}{27} \quad 70 \quad \frac{67}{34} \quad \frac{60}{50}$$

$$\frac{64}{50} \quad \frac{56}{32} \quad \frac{57}{1} \quad \frac{54}{27} \quad \frac{50}{50}$$

$$\frac{61}{50} \quad \frac{53}{25} \quad \frac{55}{1} \quad \frac{50}{25} \quad \frac{5.1}{50}$$

$$\frac{59}{50} \quad \frac{41}{23} \quad \frac{33}{1} \quad \frac{51}{20} \quad \frac{39}{50}$$

$$\frac{62}{50} \quad \frac{46}{50} \quad \frac{33}{1} \quad \frac{31}{26} \quad \frac{46}{50}$$

$$\frac{71}{50} \quad \frac{56}{23} \quad \frac{45}{1} \quad \frac{46}{24} \quad \frac{65}{50}$$

12" Oak 60' Rt. 640

$$\frac{55}{50} \quad \frac{43}{22} \quad 34 \quad \frac{34}{25} \quad \frac{51}{50}$$

$$\frac{80}{50} \quad \frac{70}{28} \quad 68 \quad \frac{68}{24} \quad \frac{82}{50}$$

$$\frac{11.5}{50} \quad \frac{11.2}{26} \quad \frac{113}{1} \quad \frac{122}{25} \quad \frac{12.1}{50}$$

$$\frac{12.0}{50} \quad \frac{124}{25} \quad \frac{125}{1} \quad \frac{125}{25} \quad \frac{125}{50}$$

Sta.	+	H.I.	-	Elev.
		911.96 ✓		
643				99.2 99.4!
644				02.9 03.1 ✓
T.P.	3.27	907.19 ✓	8.14	903.82 ✓
+50				03.5 03.7 ✓
645				02.8 03.0 ✓
645+50				01.3 01.5 ✓
646				900.1 900.3 ✓
647				899.8 900.0 ✓
T.P.	3.14	904.06 ✓	6.27	900.92 ✓
648				899.0 ✓
649				97.2 ✓
+60				97.1 ✓
+77				96.6 ✓
+86				99.1 ✓
650 +00				99.1 ✓
+12				96.8 ✓
650 +30				97.1 ✓

TO R-99

D.M., 2.08 901.98 ✓

4.

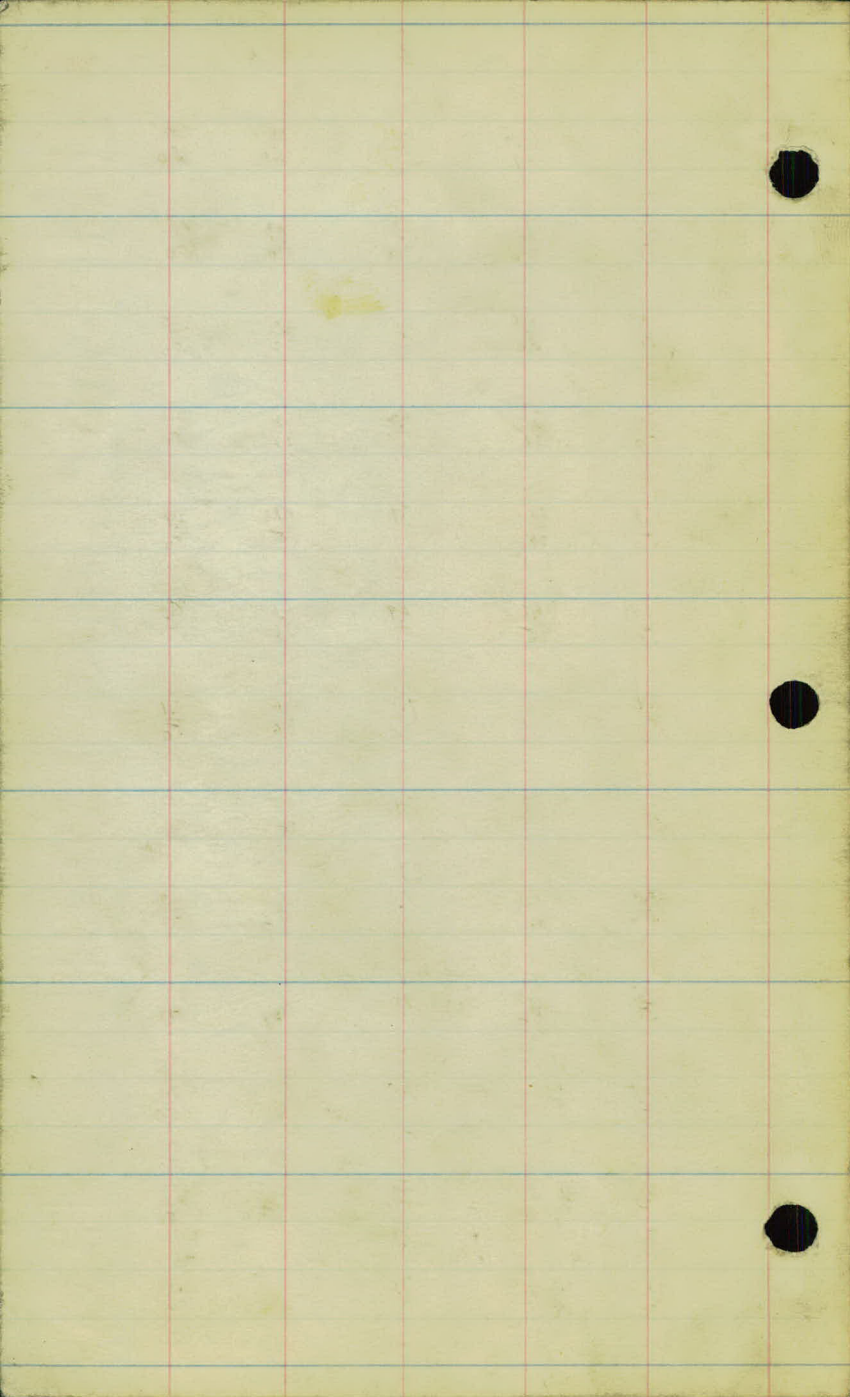
2

Rt

113

$\frac{125}{50}$	$\frac{126}{19}$	126	$\frac{124}{28}$	$\frac{120}{50}$
$\frac{74}{50}$	$\frac{72}{22}$	$\frac{89}{-}$	$\frac{73}{28}$	$\frac{10.1}{50}$
$\frac{46}{50}$	$\frac{46}{30}$	35	$\frac{30}{22}$	$\frac{2.5}{50}$
$\frac{5.1}{50}$	$\frac{5.0}{25}$	$\frac{4.2}{-}$	$\frac{32}{24}$	$\frac{2.1}{50}$
$\frac{5.8}{50}$	$\frac{6.1}{28}$	$\frac{5.7}{-}$	$\frac{4.8}{25}$	$\frac{2.7}{50}$
$\frac{6.4}{50}$	$\frac{6.7}{25}$	$\frac{6.9}{-}$	$\frac{6.6}{18}$	$\frac{6.0}{50}$
$\frac{7.3}{50}$		7.2	$\frac{6.6}{26}$	$\frac{5.7}{50}$
$\frac{5.1}{50}$	$\frac{5.1}{23}$	$\frac{5.1}{-}$	$\frac{3.5}{30}$	$\frac{2.6}{50}$
$\frac{6.9}{50}$	$\frac{6.9}{30}$	6.9	$\frac{6.9}{23}$	$\frac{6.6}{50}$
$\frac{7.5}{50}$	$\frac{7.3}{26}$	7.0	$\frac{7.0}{27}$	$\frac{6.9}{50}$
$\frac{4.5}{50}$	$\frac{6.0}{23}$	7.5	$\frac{7.1}{23}$	$\frac{7.0}{50}$
$\frac{5.0}{50}$		5.0	$\frac{7.1}{25}$	$\frac{6.8}{50}$
$\frac{7.6}{50}$	$\frac{7.1}{19}$	$\frac{5.1}{-}$	$\frac{5.0}{26}$	$\frac{6.8}{50}$
$\frac{7.0}{50}$	$\frac{7.0}{24}$	$\frac{7.3}{-}$	$\frac{5.0}{20}$	$\frac{4.9}{50}$
$\frac{7.1}{50}$	$\frac{6.9}{28}$	7.0	$\frac{7.8}{15}$	$\frac{5.2}{50}$
			$\frac{7.3}{36}$	$\frac{5.2}{50}$

8' oak 45' Rt. Sta. 648+40



~~126~~
114

Proj. # 26-62

X. Sections on Line Revision
from Sta. 800+00 to Sta. 837+84¹⁰

FROM-B-110

Sta.	+	H.I.	-	Elev.
B.M.	1.24	875.91 ✓		874.65
	1.64	867.90 ✓	9.67	244.24 ✓
800				60.2
801				61.7
T.P.	5.40	848.14 ✓	5.14	842.74 ✓
802				63.1
803				62.6
+62				63.0
804				62.0
+65				57.4
805				56.4
T.P.	0.94	850.21 ✓	10.27	857.27 ✓
806				53.6
+50				51.2
807				47.6
+17				45.4
T.P.	6.11	852.52 ✓	11.90	846.31 ✓

Lt.

Rt.

$\frac{90}{50}$	$\frac{8.3}{18}$	7.7	$\frac{70}{18}$	$\frac{6.3}{50}$
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$\frac{78}{50}$	$\frac{7.1}{16}$	6.2	$\frac{5.5}{17}$	$\frac{5.2}{50}$
-----------------	------------------	-----	------------------	------------------

$\frac{6.8}{50}$	$\frac{5.8}{14}$	5.0	$\frac{4.1}{29}$	$\frac{3.6}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{74}{50}$	$\frac{6.5}{24}$	5.5	$\frac{4.9}{18}$	$\frac{4.4}{50}$
-----------------	------------------	-----	------------------	------------------

$\frac{8.5}{50}$	$\frac{6.6}{12}$	$\frac{5.6}{17}$	5.1	$\frac{4.0}{25}$	$\frac{2.7}{50}$
------------------	------------------	------------------	-----	------------------	------------------

$\frac{10.1}{50}$	$\frac{8.3}{24}$	6.1	$\frac{4.7}{24}$	$\frac{3.6}{45}$	$\frac{3.0}{50}$
-------------------	------------------	-----	------------------	------------------	------------------

$\frac{13.2}{50}$	$\frac{12.1}{17}$	10.7	$\frac{7.6}{32}$	$\frac{4.6}{50}$
-------------------	-------------------	------	------------------	------------------

$\frac{14.5}{50}$	$\frac{13.3}{28}$	11.7	$\frac{8.5}{18}$	$\frac{7.2}{49}$	$\frac{5.3}{50}$
-------------------	-------------------	------	------------------	------------------	------------------

$\frac{7.6}{50}$	$\frac{5.0}{12}$	4.4	$\frac{3.5}{16}$	$\frac{2.0}{50}$
------------------	------------------	-----	------------------	------------------

$\frac{10.2}{50}$	$\frac{8.4}{22}$	7.0	$\frac{6.4}{12}$	$\frac{5.8}{16}$	$\frac{3.9}{50}$
-------------------	------------------	-----	------------------	------------------	------------------

$\frac{12.7}{50}$	$\frac{12.1}{16}$	10.4	$\frac{10.0}{11}$	$\frac{6.5}{50}$
-------------------	-------------------	------	-------------------	------------------

$\frac{13.6}{50}$	$\frac{13.3}{27}$	12.8	$\frac{12.2}{12}$	$\frac{7.7}{50}$
-------------------	-------------------	------	-------------------	------------------

Sta. + H.I. - F/ev.

852.52 ✓

+50

44.4

808

43.0

+44

42.8

+44

47.9

B.M. 12.65 863.74 ✓ 1.42 851.10 851.07 ✓

7.90 869.51 ✓ 2.51 861.21 ✓

+98

66.7

809

67.1

+04

67.4

+14

66.7

T.P. 1.43 858.67 ✓ 11.87 857.24 ✓

T.P. 4.28 854.29 ✓ 7.58 851.09 ✓

+42

51.7

+55

50.0

810

48.9

+80

49.8

Sta.	+	H.I.	-	Elev.
		854.37 ✓		
811				51.7
T.P.	4.72	859.82 ✓	1.27	853.10 ✓
	+37			53.9
	+58			54.6
	+70			52.1
812				54.1
T.P.	10.82	870.03 ✓	0.61	859.21 ✓
812				
	+30			65.2
	+54			65.4
	+85			64.2
813				59.0
	+22			58.5
	+34			62.8
	+43			62.5

1/6/22
~~117~~
117

LT

RT

$\frac{14}{50} \frac{2.2}{28} \quad 2.7 \quad \frac{3.3}{32} \quad \frac{3.6}{50}$

$\frac{70}{50} \frac{5.5}{39} \quad 5.9 \quad \frac{6.3}{25} \quad \frac{6.5}{50}$

$\frac{71}{50} \frac{7.1}{13} \quad 5.2 \quad \frac{5.6}{24} \quad \frac{5.6}{50}$

$\frac{5.9}{50} \frac{7.1}{24} \quad 7.7 \quad \frac{4.9}{24} \quad \frac{4.9}{50}$

$\frac{1.4}{50} \quad 5.7 \quad \frac{5.5}{28} \quad \frac{5.6}{50}$

$\frac{3.5}{64} \quad \frac{6.6}{50} \quad 15.9$
Top of Nail

$\frac{4.1}{50} \frac{2.74}{35} \frac{2.74}{21} \quad 4.8$
Top of Nail

$\frac{5.2}{50} \frac{3.52}{39.5} \frac{3.32}{21.5} \quad 4.6$
Top of Nail

$\frac{9.8}{50} \frac{10.4}{44} \frac{11.6}{36} \frac{11.6}{24} \quad 5.8$
 $\frac{3.91}{32} \frac{3.70}{33.5} \quad \frac{5.3}{50}$

$\frac{10.4}{58} \frac{9.3}{27} \frac{12.0}{4} \quad 11.0$
 $\frac{6.1}{32} \quad \frac{5.0}{50}$

$\frac{9.9}{50} \frac{8.6}{30} \frac{7.7}{12} \quad 11.5$
 $\frac{11.6}{38} \quad \frac{11.0}{50}$

$\frac{9.1}{50} \frac{7.8}{24} \quad 7.2 \quad \frac{8.9}{13} \quad \frac{12.2}{29} \quad \frac{13.0}{50}$

$\frac{7.0}{50} \frac{8.6}{50} \quad 7.5 \quad \frac{7.7}{43} \quad \frac{8.7}{50}$

Sta.	T	H. I.	-	Elev
814		870.03 ✓		60.2
+41				57.1
815				56.7
T.P.	1.06	859.29 ✓	1180	858.23 ✓
+50				57.4
816				55.0
817				52.7
+50				52.5
T.P.	1.41	854.79 ✓	4.11	853.18 ✓
818				49.3
T.P.	3.81	846.87 ✓	10.73	844.06 ✓
+46				43.5
+51				37.6
+48				42.7
+74				42.6
T.P.	0.55	843.06 ✓	434	842.51 ✓

Lt.

Rt.

~~118~~
118

$\frac{100}{50}$ $\frac{96}{25}$ 9.8 $\frac{98}{22}$ $\frac{98}{50}$

$\frac{133}{50}$ $\frac{132}{27}$ 12.9 $\frac{130}{28}$ $\frac{128}{50}$

$\frac{141}{50}$ $\frac{138}{25}$ 13.3 $\frac{136}{27}$ $\frac{133}{50}$

$\frac{13}{50}$ 19 $\frac{19}{30}$ 1.9 $\frac{2.5}{37}$ $\frac{2.6}{50}$

$\frac{3.7}{59}$ $\frac{40}{25}$ 4.3 $\frac{48}{30}$ $\frac{50}{50}$

$\frac{5.8}{50}$ $\frac{61}{30}$ 6.4 $\frac{65}{28}$ $\frac{63}{50}$

$\frac{5.3}{50}$ $\frac{5.7}{33}$ 6.8 $\frac{7.7}{25}$ $\frac{7.8}{50}$

$\frac{6.8}{50}$ $\frac{81}{48}$ $\frac{81}{45}$ $\frac{45}{40}$ $\frac{46}{29}$ $\frac{60}{24}$ $\frac{63}{21}$ $\frac{4.9}{14}$ 5.5 $\frac{6.7}{31}$ $\frac{7.6}{38}$ $\frac{10.7}{45}$ $\frac{12.2}{50}$

$\frac{2.1}{50}$ $\frac{1.3}{44}$ $\frac{2.3}{22}$ $\frac{6.3}{14}$ 3.4 $\frac{3.8}{18}$ $\frac{8.7}{28}$ $\frac{14.6}{50}$

(44.3)

$\frac{6.5}{50}$ $\frac{2.3}{31}$ $\frac{3.3}{11}$ 7.3 11.5 14.3 15.5

(35.4)

(43.1)

$\frac{7.4}{50}$ $\frac{5.9}{43}$ $\frac{3.2}{20}$ 4.2 $\frac{4.7}{7}$ $\frac{13.0}{27}$ $\frac{17.1}{50}$

(34.7)

(42.5)

$\frac{10.2}{50}$ $\frac{5.5}{39}$ $\frac{3.4}{13}$ 4.3 $\frac{4.9}{18}$ $\frac{16.2}{44}$ $\frac{17.1}{50}$

(36.8)

Sta.	+	H.I.	-	Elem.
		843.04 ✓		
+94				32.9
819				31.8
+42				31.1
+50				27.6
T.P.	2.48	834.72 ✓	10.82	832.24 ✓
820				27.5
+14				29.7
+64				30.1
+75				31.7
821				31.5
T.P.	3.81	835.39 ✓	3.14	831.58 ✓
+65				31.0
B.M.				3.14 832.15 ✓ 832.13
822				30.0
+25				29.9
+28	Edge of Creck.			27.9

11/7/26
~~119~~
119

Lt.

Rt.

(38.6)

116 56 45 106
59 35 24 11

74 23 29 75
14 35 40 50

(36.9)

(33.5)

112 111 66 60 120
50 46 38 31 21 11.3

106 29 31 46
22 41 45 50

(33.7)

(28.1)

15.7 120 148 15.3
50 40 31 12 12.0

106 4.2 4.8
46 55 68

(31.9)

(27.8)

135 15.4 192 15.7 15.7 140 15.3
78 48 55 55 41 40 21 15.5

121 104 5.1 54
7 47 56 75

(31.7)

(27.5)

46 46 72 107 7.2 7.2 7.2 7.4
70 60 56 40 40 24 24 8.0

7.2 6.0 0.9 0.3
21 29 39 50

(28.1)

(24.0)

44 44 72 107 7.2 7.2 5.7
45 54 48 36 36 24 20 5.0

5.1 1.9 1.5
25 35 50

(29.6)

(24.1)

47 60 72 106 7.2 7.2 46
45 53 47 31 31 14 10 4.6

4.8 2.0 1.8 1.3
15 21 43 50

(32.7)

(24.1)

53 53 72 106 7.2 7.2 60 3.9
75 64 57 40 40 24 22 14 3.0

2.2 1.3
55 50

(32.3)

72 108 7.2 7.2 60 3.2
100 128 128 60 37 24 3.2

3.3 1.1
28 50

(Edge of creek
top of tree)

53 47
50 24

5.1 5.8 7.2 7.2 10.5 7.2 67
17 47 50 71 71 91 95

Spk in 10" tree 50 Lt. 57 4.8 2.2 + 10

4.7 4.3 5.6
50 15 7 5.4

4.6 5.4 7.2 7.2 9.9 7.2 4.9 2.6
5 15 18 24 24 51 55 65

(Edge of creek
top of tree)
bore 102

4.7 4.8 6.2 5.0
50 28 18 5 5.5

7.5 7.5 11.0 7.5 6.2 4.3 1.5 + 3.2
2 14 14 30 32 40 50 66

4.7 4.6 6.3 5.2 5.5
50 32 21 4 1/2 7.5

7.5 11.0 7.5 6.0 4.9 0.9 + 3.0
14 14 27 30 37 50 65

Sta.		H.I.		Elev.
579	+	835.39 ✓	-	
+50	Center of Creek			24.3
+73	Edge of Creek			27.8
+88				33.8
T.P.	9.39	843.18 ✓	1.60	833.79 ✓
823				33.8
+44				33.8
+54				37.7
+62				37.8
+74				34.8
+87				39.0
824				36.0
+38				36.7
+83				36.5
825				39.5

11/7/26
~~120~~
 120

14. Edge of Creek
 1/4 of Ice

5.7 6.4 5.5 5.8 7.6 7.4 7.6 6.0 5.9 1.3 +0.7 +1.6 +2.3
 50 41 31 18 16 11.1 15 19 26 52 43 50 60
 Edge of Creek
 Bottom of Creek Above H.I.

7.6 11.0 4.6 7.3 7.6 7.8 7.6 11.1 7.6 6.2 4.4 7.0 7.7 +0.7 +0.7
 120 100 100 50 75 60 50 10 10 7.4 5 11. 23 50 60

Edge of Creek
 Top of Ice
 60 76 106 76 76 68 1.0 0.7 +2.3
 91 85 50 50 18 17 4 1.6 2.0 50

12.3 11.5 10.2 8.1 8.5
 80 54 50 24 21 50
 Above H.I.

2.9 11.3 11.3 9.3 9.4 7.6
 70 60 54 28 9.4 33 50

1.7 0.7 2.3 7.2 7.4 6.6 4.7 7.5 7.0
 50 42 34 17 11 4 5.5 15 25 50

3.1 2.7 2.7 7.7 9.3 3.7 1.1 0.2 3.4
 30 29 24 13 9 5.4 18 42 58 80

6.1 6.7 5.9 3.3 3.9 2.2 7.4 5.2 4.1 5.6 4.3
 50 41 29 15 10 2 8.4 7 10 73 35 50

5.5 5.5 7.0 4.8 3.8 8.2 7.6 5.6 8.0 8.0
 50 40 4 2 4.2 4 11 27 37 47 50

5.5 5.6 6.0 7.4 7.9 7.3 9.3 7.5 10.7
 60 50 23 7.2 21 50 84 87 100 101

5.8 6.6 7.0 7.6 10.7
 65 31 21 6.5 17 36 45

3.9 1.7 6.1 7.2 8.7 10.7
 74 7 4.7 19 27 29

17 3.7 6.5 7.5 9.2 10.7
 5 34 42 44

Sta.	T	H.I.	-	Elev.
825+33		843.18 ✓		
825+65				
T.P.	12.42	855.15 ✓	0.45	842.73 ✓
T.P.	7.37	860.00 ✓	2.52	852.63 ✓
824+38				
824+83				
825				
825+33				55.5
825+65				55.0
T.P.	2.79	859.75 ✓ 858.75	3.04	856.76 ✓
826				55.1
827				54.6
+40				54.8
828				53.5
829				52.9
B.M.	6.25	860.03 ✓	5.93	853.82 ✓ 853.78

14

RT.

~~121~~
121

$$\frac{-123}{}$$

$$\begin{array}{r} 46 \\ 27 \\ \hline 73 \end{array} \quad \begin{array}{r} 70 \\ 68 \\ \hline 138 \end{array} \quad \begin{array}{r} 96 \\ 74 \\ \hline 170 \end{array} \quad \begin{array}{r} 103 \\ 77 \\ \hline 180 \end{array}$$

$$\frac{-113}{}$$

$$\frac{38}{55}$$

$$\frac{5.8}{75} \quad \frac{5.7}{65} \quad 23.3$$

$$\frac{4.6}{70} \quad \frac{4.4}{59} \quad 23.5$$

$$\frac{4.2}{50} \quad \frac{4.4}{59} \quad 20.5$$

$$\frac{4.8}{50} \quad \frac{4.8}{45} \quad 4.5$$

$$\frac{5.1}{50} \quad \frac{5.1}{25} \quad 5.0 \quad \frac{4.8}{26}$$

$$\frac{4.7}{50} \quad \frac{4.7}{33} \quad 4.7 \quad \frac{4.6}{28} \quad \frac{4.7}{50}$$

$$\frac{5.4}{50} \quad \frac{5.1}{30} \quad 5.2 \quad \frac{5.1}{28} \quad \frac{5.6}{50}$$

$$\frac{5.2}{50} \quad \frac{5.2}{30} \quad 5.0 \quad \frac{5.2}{30} \quad \frac{5.8}{50}$$

$$\frac{6.7}{50} \quad \frac{6.6}{30} \quad 6.5 \quad \frac{6.3}{30} \quad \frac{6.2}{50}$$

$$\frac{8.0}{50} \quad \frac{7.3}{35} \quad 4.9 \quad \frac{4.6}{30} \quad \frac{4.5}{50}$$

519. + H.I. - Elev

860.03 ✓

+50

52.4

830

52.7

+21

52.9

+43

51.5

+71

52.9

831

53.2

+47

53.2

832

53.7

+15

55.1

833

55.3

834

55.7

T.P.

4.22

869.14 ✓

3.11

856.92 ✓

835

56.4

1/7/25
~~134~~
122

lt.

rt.

2. Rf.

$\frac{5.1}{7.5}$ $\frac{5.4}{5.8}$ $\frac{6.1}{5.5}$ $\frac{8.3}{5.1}$ $\frac{7.7}{5.2}$ $\frac{7.2}{7.4}$ $\frac{6.8}{5.0}$

2. Rf.

$\frac{4.9}{6.0}$ $\frac{5.6}{4.3}$ $\frac{6.0}{4.0}$ $\frac{7.5}{2.2}$ $\frac{8.1}{1.9}$ $\frac{8.4}{1.0}$ $\frac{8.5}{8}$ $\frac{7.1}{7.3}$ $\frac{7.1}{3.0}$ $\frac{6.6}{5.0}$

2. Rf.

$\frac{4.9}{5.3}$ $\frac{5.2}{3.9}$ $\frac{6.3}{3.6}$ $\frac{7.1}{1.6}$ $\frac{8.1}{1.3}$ $\frac{8.2}{1}$ $\frac{7.0}{7.1}$ $\frac{6.6}{5.2}$ $\frac{6.6}{5.0}$

2. Rf.

$\frac{5.2}{4.0}$ $\frac{4.9}{4.7}$ $\frac{5.2}{5.3}$ $\frac{6.0}{5.0}$ $\frac{6.9}{8}$ $\frac{7.7}{5}$ $\frac{8.2}{8.5}$ $\frac{7.2}{6}$ $\frac{6.7}{8}$ $\frac{6.6}{5.0}$

2. Rf.

$\frac{5.3}{5.4}$ $\frac{4.9}{5.9}$ $\frac{5.5}{2.5}$ $\frac{6.1}{2.3}$ $\frac{7.1}{7.1}$ $\frac{8.4}{9}$ $\frac{8.1}{1.3}$ $\frac{7.1}{1.6}$ $\frac{6.8}{5.9}$ $\frac{6.7}{5.0}$

2. Rf.

$\frac{6.6}{5.3}$ $\frac{5.2}{4.7}$ $\frac{4.2}{1.5}$ $\frac{5.3}{2.0}$ $\frac{6.0}{1.8}$ $\frac{7.2}{6.8}$ $\frac{8.0}{9}$ $\frac{7.9}{1.3}$ $\frac{7.1}{2.2}$ $\frac{6.8}{2.4}$ $\frac{6.7}{5.0}$

2. Rf.

$\frac{6.0}{5.0}$ $\frac{6.0}{4.8}$ $\frac{6.7}{4.6}$ $\frac{6.7}{4.3}$ $\frac{5.0}{3.8}$ $\frac{4.8}{2.6}$ $\frac{4.9}{1.2}$ $\frac{6.4}{8}$ $\frac{6.0}{6.8}$ $\frac{6.2}{3.0}$ $\frac{7.4}{2.5}$ $\frac{7.1}{3.4}$ $\frac{6.5}{3.6}$ $\frac{6.5}{5.0}$

2. Rf.

$\frac{5.5}{5.0}$ $\frac{5.4}{3.9}$ $\frac{6.3}{5.1}$ $\frac{6.1}{5.3}$ $\frac{4.1}{2.9}$ $\frac{4.6}{1.8}$ $\frac{4.9}{4}$ $\frac{6.5}{6.3}$ $\frac{6.5}{4}$ $\frac{5.5}{9}$ $\frac{5.8}{3.0}$ $\frac{5.8}{2.5}$ $\frac{5.8}{5.0}$

2. Rf.

$\frac{5.0}{5.0}$ $\frac{5.0}{3.6}$ $\frac{5.7}{3.4}$ $\frac{6.0}{3.2}$ $\frac{5.0}{2.9}$ $\frac{4.7}{1.4}$ $\frac{4.7}{4.9}$ $\frac{6.2}{4}$ $\frac{5.5}{1.0}$ $\frac{5.2}{2.3}$ $\frac{5.4}{5.0}$

2. Rf.

$\frac{3.3}{5.4}$ $\frac{5.8}{5.0}$ $\frac{6.6}{4.8}$ $\frac{6.9}{4.5}$ $\frac{5.1}{4.0}$ $\frac{4.9}{2.9}$ $\frac{5.8}{2.4}$ $\frac{5.6}{2.2}$ $\frac{5.1}{1.9}$ $\frac{4.6}{7}$ $\frac{4.7}{4.7}$ $\frac{5.0}{8}$ $\frac{5.6}{1.3}$ $\frac{5.4}{1.4}$ $\frac{4.6}{2.0}$ $\frac{4.5}{5.0}$

Top of Rail

2. Rf.

$\frac{1.76}{5.2}$ $\frac{2.2}{5.5}$ $\frac{4.9}{5.0}$ $\frac{5.1}{4.3}$ $\frac{3.4}{3.8}$ $\frac{4.0}{3.0}$ $\frac{5.0}{1.7}$ $\frac{5.1}{1.4}$ $\frac{4.7}{1.1}$ $\frac{4.7}{4.3}$ $\frac{4.5}{1.5}$ $\frac{5.5}{1.9}$ $\frac{5.5}{2.2}$ $\frac{4.2}{2.8}$ $\frac{4.3}{5.0}$

Top of Rail

2. Rf.

$\frac{4.4}{4.7}$ $\frac{5.4}{4.5}$ $\frac{3.5}{3.5}$ $\frac{3.5}{3.0}$ $\frac{3.5}{2.5}$ $\frac{3.5}{2.5}$ $\frac{3.5}{1.7}$ $\frac{3.5}{1.5}$ $\frac{3.5}{1.2}$ $\frac{3.5}{1.0}$ $\frac{3.5}{6.7}$ $\frac{6.5}{5}$ $\frac{6.5}{1.3}$ $\frac{7.2}{2.0}$ $\frac{8.1}{2.4}$ $\frac{8.0}{4.3}$ $\frac{8.5}{5.0}$

Sta. + H. I. - E/ev.

863.14 ✓

834

57.4

837

58.1

Elev.

837 + 84¹²

= 807 + 15⁸

59.0

B.M.

1.75

859.39 ✓

1/8/25
~~123~~
123

Top of Nail

4.12 4.6 7.1 9.3 9.7 7.5 7.4 5.7
49.5 47 39 36 33 29 14 8 5.7

2.11.

5.7 6.1 8.0 8.3 7.9
5 18 23 38 50

Top of Nail.

3.58 4.0 5.5 7.9 7.8 5.6 5.8 5.0
5.0 4.7 4.1 3.8 3.4 3.2 1.2 9 5.0

2.11.

4.9 5.2 7.2 7.6
4 15 20 50

Top of Nail.

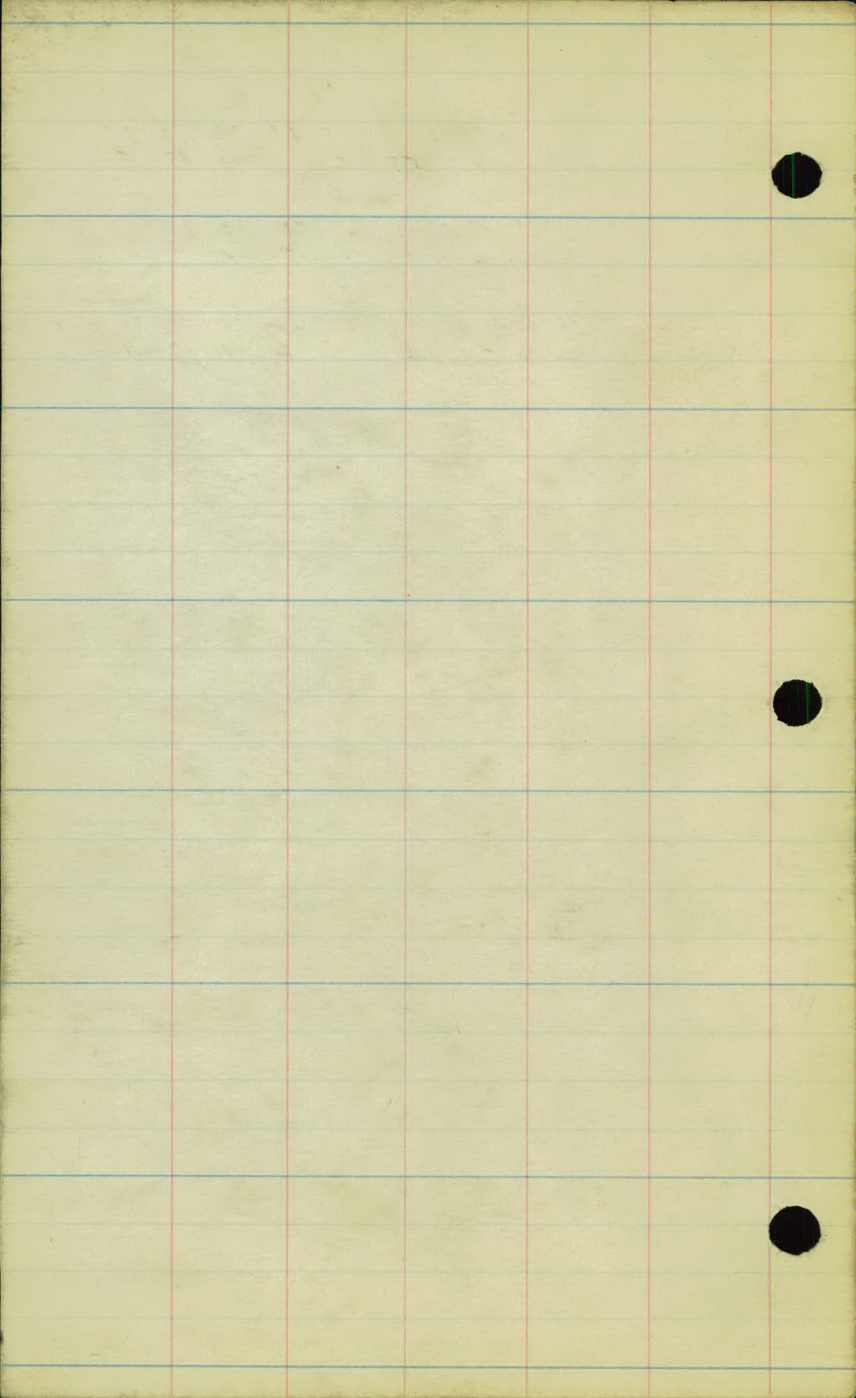
2.95 3.3 3.6 4.0 4.9 3.0 3.6 5.1 5.0 4.4
5.05 4.9 4.3 4.2 4.0 3.7 2.2 1.9 1.4 1.1 4.1

2.11.

4.1 4.2 5.4 5.7 5.2 4.2 4.4 5.5
2 12 17 17 17 40 45 50

SEE STATE
NOTES

PAGE 12



3/14/27

C.W.S.

D.S.

AB

T.M.

Alignment.
29128321
Sta 385 - 299+7929 = Eya

26-62

Div A.

Sta	Point	Δ ht	Δ Rt	Calc Bearing
-----	-------	------	------	--------------

Elev

$299 + 79^{\text{cm}} = 298 + 83^{\text{cm}}$ End.

$295 + 87^{\text{cm}}$

- +50
- 95
- +50
- 94
- +50
- 93
- +50
- 92

- 34°-22'
- 32°-30
- 30°-00
- 27°-30
- 25°-00
- 23°-30
- 20°-00
- 17°-30
- 15°-00

Δ 68°-45'

D 10°-Rt

T. 392 ^{45'}

$292 + 92^{\text{cm}}$

P.I.

- +50
- 91
- +50
- 90
- +50
- 89

- 68°-45'
- 12°-30
- 10°-00
- 7°-30
- 5°-00
- 2°-30
- 00°-00'

L. 687 ^{50'}

$288 + 99^{\text{cm}}$

P.C.

00°-00

3/15/27
CWA
D.S.
A.B.
T.M.

X Sections
Line Revision.
Sta 215-299+79.03
P6-62
DIVA.

Sta + or - Elev

285 + 0.52

+ 50

77.2 .

286 + 0.0

76.9 .

+ 50

73.1 .

287 + 0.0

72.8 .

+ 50

75.7 .

+ 86

78.7 .

288

76.6 .

+ 28

76.7 .

+ 99.3

80.8 .

289 + 50

83.8 .

290

85.4 .

same assignment

8.4/50, 8.4/39, 10.4/34, 9.1/30, 8.4/29, 8.6/15, 8.5, 8.4/20, 8.6/50

9.0/50, 9.1/38, 8.7/21, 8.5, 8.5/24, 8.0/50

7.0/50, 9.0/34, 9.0/14, 8.3, 7.6/15, 8.2/38, 7.7/50

7.0/50, 7.3/37, 8.7/22, 7.5, 7.2/24, 7.0/50

8.8/50, 7.2/13, 6.8/9, 6.8, 6.2/24, 6.8/50

7.0/50, 9.0/27, 7.0/5, 6.7, 6.2/24, 7.0/39, 7.0/50

7.3/50, 8.8/19, 8.8, 6.6/5, 6.6/24, 7.4/45, 7.2/50

9.0/50, 9.2/40, 8.6/21, 5.5, 8.2/11, 7.2/17, 7.0/34, 6.6/50

6.0/50, 5.2/31, 4.5/19, 4.5, 4.4/17, 6.0/20, 5.3/35, 3.8/50

2.7/50, 2.7/24, 2.2/11, 1.6, 0.6/32, 4.0/35, 4.0/50

5.4/50, 5.4/25, 5.3, 5.4/14, 4.3/44, 9.5/50

Sta +/- Elev

290+50 87.3.

291+00 88.6.

+17. +37 86.5.

+50 82.6.

292+00 77.9.

+50 77.9.

293 78.1.

+50 78.0.

294 78.0.

+50 78.2.

295 79.5.

+50 82.1.

+75 85.4.

$\frac{3.0}{50}$ $\frac{4.0}{27}$ 34 $\frac{3.6}{23}$ $\frac{7.0}{50}$

$\frac{+33}{50}$ $\frac{+32+20}{45}$ $\frac{0.0}{30}$ $\frac{0.0}{10}$ 21 $\frac{4.2}{11}$ $\frac{6.7}{28}$ $\frac{8.7}{50}$

$\frac{0.6}{50}$ $\frac{2.0}{31}$ $\frac{4.8}{16}$ $\frac{8.5}{16}$ $\frac{10.8}{16}$ $\frac{13.5}{38}$ $\frac{15.0}{50}$

$\frac{8.5}{50}$ $\frac{10.0}{30}$ $\frac{11.0}{18}$ 12.4 $\frac{13.3}{27}$ $\frac{14.8}{50}$

$\frac{5.0}{50}$ $\frac{5.4}{21}$ 64 $\frac{7.2}{18}$ $\frac{7.4}{40}$ $\frac{7.6}{50}$

$\frac{7.5}{50}$ $\frac{8.0}{44}$ $\frac{8.0}{23}$ $\frac{8.2}{25}$ $\frac{8.4}{25}$ $\frac{8.4}{50}$

$\frac{8.8}{50}$ $\frac{8.7}{27}$ $\frac{8.2}{28}$ $\frac{8.5}{28}$ $\frac{8.5}{50}$

$\frac{8.7}{50}$ $\frac{8.8}{28}$ 8.4 $\frac{8.6}{18}$ $\frac{8.6}{19}$ $\frac{8.4}{22}$ $\frac{8.4}{26}$ $\frac{8.5}{50}$

$\frac{9.0}{50}$ $\frac{9.0}{30}$ 9.2 $\frac{8.2}{25}$ $\frac{8.2}{50}$

$\frac{7.5}{50}$ $\frac{7.8}{30}$ $\frac{8.0}{30}$ $\frac{8.3}{25}$ $\frac{8.2}{50}$

$\frac{4.8}{50}$ $\frac{5.8}{22}$ 67 $\frac{7.2}{28}$ $\frac{7.8}{50}$

$\frac{+0.9}{50}$ $\frac{0.4}{44}$ $\frac{4.8}{29}$ $\frac{7.0}{18}$ 70 $\frac{10.2}{32}$ $\frac{10.6}{50}$

$\frac{5.4}{60}$ $\frac{5.3}{40}$ $\frac{+3.8}{30}$ $\frac{0.0}{19}$ $\frac{0.7}{17}$ $\frac{4.2}{9}$ 60 $\frac{8.0}{19}$ $\frac{9.5}{50}$

Sta	tor-	Elev
296+00		924.

+21		967.
-----	--	------

297		948.
-----	--	------

+50		932.
-----	--	------

298		887.
-----	--	------

+25		866.
-----	--	------

299		940.
-----	--	------

+50		835.
-----	--	------

-298+83 =		
299+7903 =		836.

3/15/22
CWS AB
D.J. T.M.

$$\frac{26}{50} \quad \frac{33}{20} \quad \frac{57}{4} \quad 76 \quad \frac{21}{9} \quad \frac{120}{16} \quad \frac{144}{35} \quad \frac{158}{50}$$

$$\frac{28}{50} \quad \frac{24}{39} \quad \frac{30}{17} \quad 31 \quad \frac{37}{7} \quad \frac{74}{13} \quad \frac{101}{29} \quad \frac{153}{50}$$

$$\frac{51}{50} \quad \frac{51}{42} \quad \frac{51}{19} \quad 52 \quad \frac{52}{30} \quad \frac{54}{50}$$

$$\frac{65}{50} \quad \frac{65}{26} \quad 68 \quad \frac{70}{24} \quad \frac{74}{50}$$

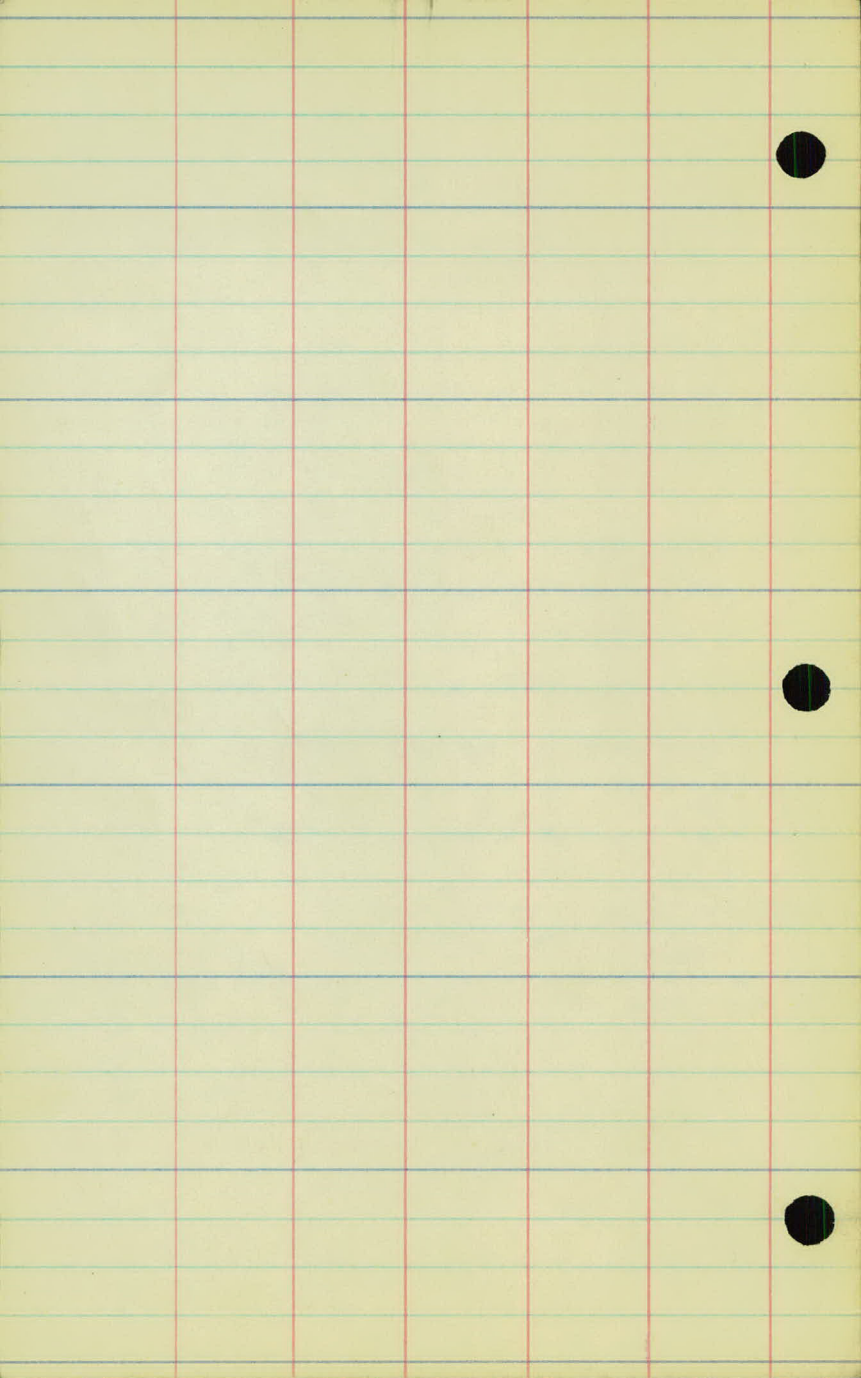
$$\frac{16}{50} \quad \frac{28}{21} \quad 38 \quad \frac{47}{24} \quad \frac{63}{50}$$

$$\frac{30}{50} \quad \frac{42}{25} \quad 60 \quad \frac{68}{28} \quad \frac{75}{50}$$

$$\frac{64}{50} \quad \frac{72}{21} \quad 85 \quad \frac{104}{21} \quad \frac{116}{50}$$

$$\frac{95}{50} \quad \frac{110}{24} \quad 110 \quad \frac{123}{20} \quad \frac{140}{50}$$

$$\frac{115}{50} \quad \frac{120}{24} \quad \frac{115}{19} \quad 118 \quad \frac{124}{22} \quad \frac{144}{29} \quad \frac{152}{50}$$



3/15/27.

C.W.S.
D.S.
T.M.
A.R.

± levels.

Line Revision.

Sta 285-299+79⁰⁰.

26-62

Div A.

Sta	+	HI	-	Elev.
B.M.	2.33	884.67	✓	882.34
285+05.2				
+50				77.2 • 7.5
286				76.9 • 7.8
+50				73.1 • 11.6
287				77.8 • 6.9
+50				78.7 • 6.0
+86				78.7 • 6.0
288				76.6 • 8.1
+28				76.7 • 8.0
T.P.	10.14	890.09	4.72	879.95 •
+99.2				80.8 • 9.3
289+50				83.8 • 6.3
290				85.4 • 4.7

3/15/27

spike in 10" Oak 215' Rt 284+75

same as original.

Sta	+	HI	-	Elev		
290	+50	890.09.		87.3.	28	
291				85.6.	15	
	+50			82.6.	75	
292				79.9.	10.2	
	+50			77.9.	12.2	
293				78.1.	12.0	
	+50			78.0.	12.1	
	+54	Edge Ditch		78.0.	12.1.	E.D.
	+55	Bottom D.		76.7.	13.4.	B.D.
	+56	" "		76.7.	13.4.	BD
	+57	Edge Ditch.		77.9.	12.2.	EP
294				78.0.	12.1.	

3/25/27

13.0
100

13.5
50

13.8
50

14.0
100

	+	HI	-	Flor	
		890.09			
294				78.2	11.9
					1
295				79.5	10.6
	+50			82.1	8.0
	+75			85.4	4.7
	+87.5			88.6	1.5
T.P.	8.78	896.76	2.11	887.98	
296				92.4	4.4
	+21			96.7	0.1
297				94.8	2.0
	+50			93.2	3.6
298				88.7	8.1
	+25			86.6	10.2
299				84.0	12.8
	+50			83.5	13.3
299 + 299 = 298 + 83.2				83.6	13.2
T.P.	1.51	889.49	8.78	887.98	
B.M.			6.82	882.67	882.65

3/15/27

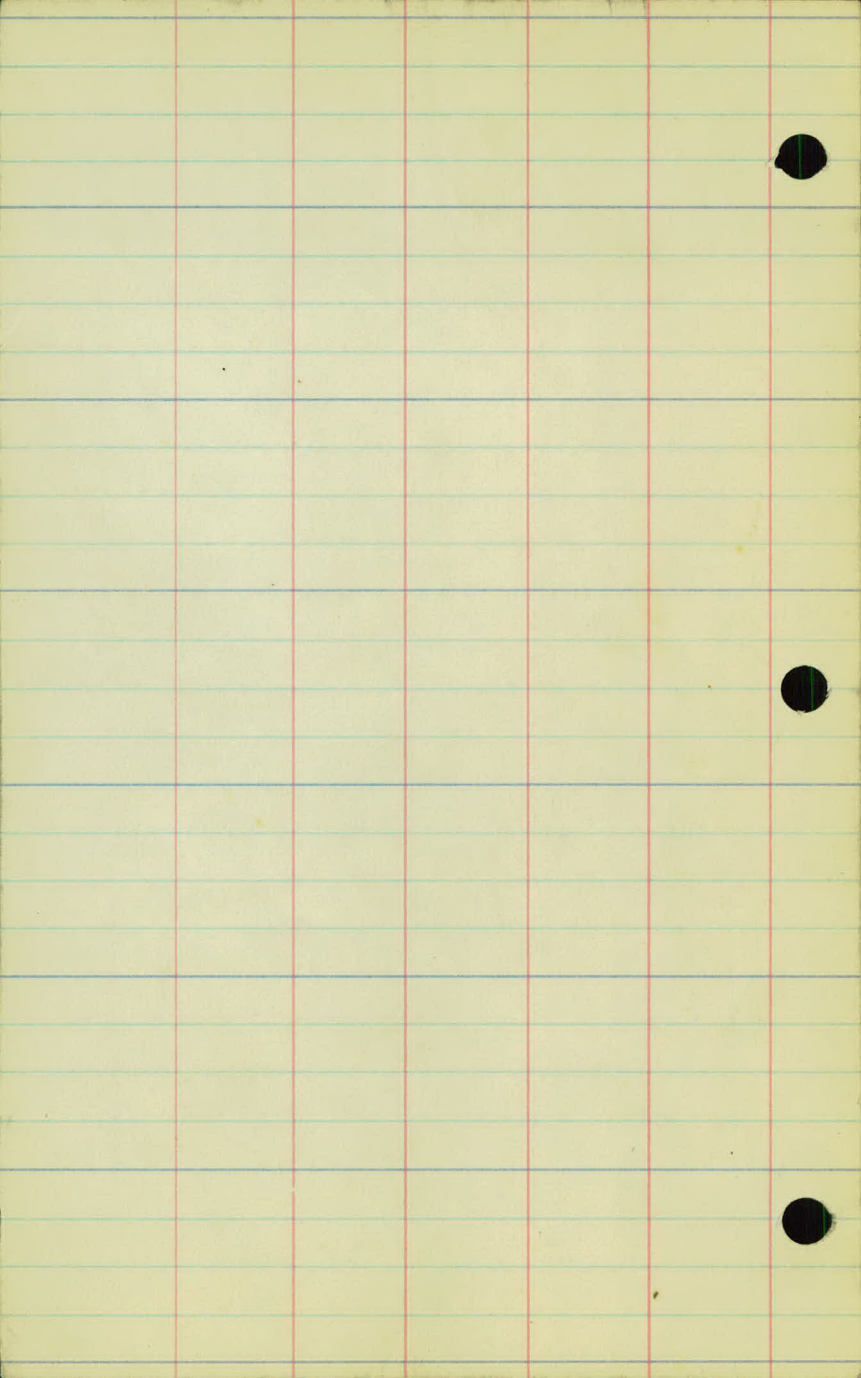
C.W.S.

D.S.

A.G.

T.M.

RR. spike 8" Oak 584 5+7 294 + 75



Proj. # 27-62 B.

Line Revision from Sta.

303+91⁵⁶ to Sta. 328+84.

Sta. Point. A H. A Rt. ^{Calc} Bearing

308+90⁷⁹ P.O.T.

308+76⁰³ P.T. 12°-07'
 +50 11°-28' ✓
 308 10°-13' ✓
 +50 8°-59' ✓
 307 7°-43' ✓
 +50 6°-28' ✓

306+37⁴⁵ P.I. A-24°-14'
 306 5°-13' ✓ D-5°
 +50 3°-58' ✓ T.-246⁰⁹
 305 2°-43' L.-484⁶⁷
 +50 1°-28' R.-1146.28
 304 0°-13'

303+91³⁶ P.C.

4-18-27

Sta. Point. A Lt. A Rt. ^{date} Bearing

328+84 ²¹ P.O.T. = 329+01 ⁹⁰

328+36 ⁵⁴

2°-46⁵

328

2°-24⁶

+50

1°-54⁶

327

1°-24⁶

⁸⁹

326+97 P.I.

5°-33

Δ-5°-33

150

0°-54⁶

D-2° Rt.

326

0°-24⁶

T-138 ⁸⁵

325+59 ⁰⁴ P.C.

L-277 ⁵⁰

R.-2864.93

Proj. # 26-62 "D"

Line Revision.

X. sections & center line

Levels from Sta. 309+91 to Sta. 328+36.

Sta.	T	M. I.	-	Red	Flev.
B.M.	3.08	896.65		893.57	
	4.54	888.23	12.36	884.29	✓
303 + 91 ⁵⁶				6.2	882.6
304				6.0	82.8
+50				6.0	82.8
305				5.9	82.9
+50				5.8	83.0
306				6.3	82.5
+50				7.0	81.8
307				6.5	82.3
	11.80	899.53	1.10	897.73	
303 + 91 ⁵⁶				8	82.6
304					82.8
304 + 50					82.8
305					82.9

SPK in 10" DIA 60 14.5 ft. 305+00.

$\frac{80}{36}$ $\frac{78}{25}$ $\frac{60}{18}$ $\frac{6.0}{21}$ $\frac{10.9}{30}$ $\frac{11.5}{44}$

$\frac{7.7}{37}$ $\frac{78}{24}$ $\frac{60}{18}$ $\frac{6.1}{20}$ $\frac{10.9}{30}$ $\frac{11.5}{44}$

$\frac{8.1}{35}$ $\frac{7.3}{22}$ $\frac{6.1}{17}$ $\frac{5.9}{22}$ $\frac{10.8}{32}$ $\frac{11.4}{38}$

$\frac{8.1}{34}$ $\frac{7.5}{18}$ $\frac{5.9}{14}$ $\frac{5.7}{26}$ $\frac{11.5}{38}$ $\frac{11.8}{42}$
→ shore line

$\frac{0.8}{40}$ $\frac{4.8}{35}$ $\frac{5.3}{31}$ $\frac{7.7}{27}$ $\frac{7.0}{15}$ $\frac{6.1}{11}$ $\frac{5.4}{14}$ $\frac{5.0}{30}$ $\frac{11.5}{45}$ $\frac{12.3}{50}$
→ shore line

$\frac{5.0}{33}$ $\frac{6.6}{25}$ $\frac{9.0}{21}$ $\frac{8.9}{9}$ $\frac{6.4}{5}$ $\frac{5.4}{19}$ $\frac{4.5}{37}$ $\frac{11.5}{50}$
→ shore line

$\frac{1.5}{22}$ $\frac{7.2}{12}$ $\frac{7.4}{1}$ $\frac{6.6}{3}$ $\frac{5.1}{23}$ $\frac{4.5}{43}$ $\frac{11.4}{56}$
→ shore line

$\frac{6.1}{3}$ $\frac{6.5}{12}$ $\frac{5.6}{14}$ $\frac{4.7}{29}$ $\frac{4.4}{50}$ $\frac{11.3}{66}$
→ shore line

$\frac{7.2}{60}$ $\frac{7.8}{49}$ (16.9)

$\frac{6.7}{60}$ $\frac{7.7}{50}$ (16.9)

$\frac{5.2}{53}$ $\frac{6.5}{47}$ (16.7)

$\frac{6.5}{52}$ $\frac{8.5}{44}$ (16.6)

Sta.	T	H. Iy	-	Rod	Elev.
305+50		899.53			83.0
306					82.5
306+50					81.8
307					82.3
307+50.				9.0	90.5
T.P.	12.67	911.25	0.95	898.58	
307					82.3
307+50					90.5
308				11.6	899.7
T.P.	7.53	918.41	0.17	911.08	
308					99.7
308+50				12.5	906.1
309				11.1	907.5
469				15.3	903.3
T.P.	1.17	908.02	11.74	906.85	
780				12.7	885.3

$$\begin{array}{r} 1.9 \\ 59 \end{array} \quad \begin{array}{r} 4.5 \\ 53 \end{array} \quad \begin{array}{r} 6.6 \\ 48 \end{array} \quad \begin{array}{r} 9.3 \\ 43 \end{array} \quad (16.5)$$

$$\begin{array}{r} 0.8 \\ 60 \end{array} \quad \begin{array}{r} 4.8 \\ 49 \end{array} \quad \begin{array}{r} 10.3 \\ 40 \end{array} \quad \begin{array}{r} 11.6 \\ 37 \end{array} \quad (17.0)$$

$$\begin{array}{r} 3.9 \\ 61 \end{array} \quad \begin{array}{r} 5.0 \\ 52 \end{array} \quad \begin{array}{r} 9.0 \\ 37 \end{array} \quad \begin{array}{r} 10.0 \\ 27 \end{array} \quad (17.7)$$

$$\begin{array}{r} 0.5 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad \begin{array}{r} 9.7 \\ 10 \end{array} \quad (17.2)$$

9.0

$$\begin{array}{r} 7.8 \\ 66 \end{array} \quad \begin{array}{r} 7.5 \\ 59 \end{array} \quad \begin{array}{r} 8.6 \\ 41 \end{array} \quad \begin{array}{r} 10.6 \\ 29 \end{array} \quad (29.0)$$

$$\begin{array}{r} 1.6 \\ 60 \end{array} \quad \begin{array}{r} 0.0 \\ 52 \end{array} \quad \begin{array}{r} 0.6 \\ 42 \end{array} \quad \begin{array}{r} 2.0 \\ 30 \end{array} \quad \begin{array}{r} 3.7 \\ 20 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad (20.8)$$

$$\begin{array}{r} 0.5 \\ 28 \end{array} \quad \begin{array}{r} 1.6 \\ 13 \end{array} \quad \begin{array}{r} 2.6 \\ 10 \end{array} \quad 11.6$$

$$\begin{array}{r} 4.1 \\ 64 \end{array} \quad \begin{array}{r} 4.1 \\ 52 \end{array} \quad \begin{array}{r} 5.8 \\ 36 \end{array} \quad (18.9)$$

$$\begin{array}{r} 2.1 \\ 75 \end{array} \quad \begin{array}{r} 1.7 \\ 62 \end{array} \quad \begin{array}{r} 2.7 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 35 \end{array} \quad \begin{array}{r} 7.0 \\ 20 \end{array} \quad \begin{array}{r} 8.6 \\ 11 \end{array} \quad \begin{array}{r} 10.6 \\ 3 \end{array} \quad 12.5$$

$$\begin{array}{r} 1.7 \\ 75 \end{array} \quad \begin{array}{r} 3.1 \\ 53 \end{array} \quad \begin{array}{r} 4.2 \\ 43 \end{array} \quad \begin{array}{r} 7.0 \\ 25 \end{array} \quad \begin{array}{r} 9.5 \\ 9 \end{array} \quad 11.1 \quad \frac{11.7}{2}$$

$$\begin{array}{r} 3.1 \\ 71 \end{array} \quad \begin{array}{r} 4.9 \\ 57 \end{array} \quad \begin{array}{r} 6.9 \\ 45 \end{array} \quad \begin{array}{r} 11.8 \\ 14 \end{array} \quad 15.3$$

$$\begin{array}{r} 0.7 \\ 82 \end{array} \quad \begin{array}{r} 3.5 \\ 9 \end{array} \quad \begin{array}{r} 4.4 \\ 3 \end{array} \quad 12.7$$

Sta. + H.I. - Rod Elev.

908.02

310 14.0 94.0

310+84 16.7 91.3

0.89 897.10 11.81 894.21

6.13 891.88 11.35 885.75

307+50 90.5

~~99.7~~

308 99.7

308+50 06.1

309 07.5

~~03.3~~

309+64 03.3

T.P. 6.58 892.28 6.18 885.70

309+80 95.3

310 94.0

310+84 91.3

311 5.3 87.0

+50 5.3 87.0

$$\begin{array}{r} 0.5 \quad 2.4 \quad 4.8 \\ 28 \quad 18 \quad 6 \quad 14.0 \end{array}$$

$$\begin{array}{r} 2.1 \quad 3.7 \quad 6.2 \\ 36 \quad 24 \quad 6 \quad 16.7 \end{array}$$

$$\begin{array}{r} 1.4 \quad 2.5 \quad 8.5 \quad 7.7 \quad 7.5 \quad 7.5 \quad 13.3 \quad 14.6 \\ 11 \quad 18 \quad 26 \quad 38 \quad 55 \quad 67 \quad 90 \\ 10.9 \\ 76 \end{array}$$

$$- 7.8 \quad 7.3 \quad 7.7 \quad 7.6 \quad 7.7 \quad 7.1 \quad 6.6 \quad 6.9 \quad 8.7 \\ 14 \quad 21 \quad 31 \quad 32 \quad 46 \quad 48 \quad 62 \quad 69$$

$$- 14.2 \quad 2.8 \quad 6.7 \quad 7.5 \quad 7.0 \quad 6.4 \quad 6.3 \quad 7.0 \quad 3.5 \\ 4 \quad 39 \quad 41 \quad 34 \quad 66 \quad 74 \quad 81 \quad 85$$

$$- 15.6 \quad 1.7 \quad 6.6 \quad 6.7 \quad 7.6 \quad 6.9 \quad 6.4 \quad 5.9 \\ 14 \quad 25 \quad 43 \quad 44 \quad 59 \quad 60 \quad 75 \\ 1.7 \quad 6.7 \\ 92 \quad 84$$

$$- 11.4 \quad 0.4 \quad 6.0 \quad 6.5 \quad 6.3 \quad 7.0 \quad 6.6 \quad 6.0 \quad 6.2 \\ 8 \quad 18 \quad 25 \quad 46 \quad 47 \quad 62 \quad 64 \quad 80 \\ 2.9 \quad 7.0 \\ 92 \quad 85$$

$$- 3.0 \quad 5.8 \quad 7.0 \quad 6.5 \quad 7.5 \quad 7.0 \quad 6.4 \quad 6.5 \quad 7.4 \quad 5.8 \\ 13 \quad 36 \quad 46 \quad 48 \quad 62 \quad 64 \quad 78 \quad 86 \quad 91$$

$$- 1.7 \quad 5.7 \quad 6.3 \quad 7.1 \quad 6.5 \quad 7.4 \quad 6.8 \quad 6.2 \quad 6.6 \quad 7.5 \quad 4.7 \\ 10 \quad 13 \quad 33 \quad 46 \quad 47 \quad 62 \quad 63 \quad 79 \quad 86 \quad 90$$

$$1.0 \quad 4.6 \quad 6.2 \quad 6.4 \quad 6.8 \quad 6.1 \quad 5.9 \quad 8.3 \\ 7 \quad 31 \quad 46 \quad 47 \quad 61 \quad 74 \quad 79$$

↑ Above H.I.

$$+ 4.5 \quad 4.0 \quad 5.5 \quad 5.8 \quad 5.4 \quad 6.6 \quad 6.0 \quad 6.0 \quad 8.8 \\ 54 \quad 38 \quad 21 \quad 5.3 \quad 22 \quad 45 \quad 48 \quad 60 \quad 73 \quad 77 \\ 5.4 \\ 4.5$$

↑ Above H.I.

$$+ 2.0 \quad 4.9 \quad 5.4 \quad 5.7 \quad 6.2 \quad 10.0 \\ 52 \quad 42 \quad 15 \quad 5.3 \quad 29 \quad 73 \quad 82$$

Sta.	+	H.I.	-	Roof	Elev
312		892.28		4.8	87.5
312 + 50				4.8	87.5
313				6.4	85.9
313 + 14				6.8	85.5
313 + 38				10.8	81.5
B.M.			12.65	879.63	879.64
T.P.	10.29	917.14		906.85	
309 + 80					895.3
310					94.0
310 + 84					91.3
311					87.0
311 + 50					87.0
T.P.	10.97	924.14	1.97	915.17	
312					87.5
312 + 50					87.5

→ Above H.I.

$$\begin{array}{r} \frac{12.0}{45} \quad \frac{51}{32} \quad 4.8 \quad \frac{52}{75} \quad \frac{5.4}{34} \quad \frac{6.1}{38} \quad \frac{5.6}{49} \quad \frac{5.7}{70} \quad \frac{9.8}{78} \end{array}$$

$$\begin{array}{r} \frac{1.2}{43} \quad \frac{5.1}{37} \quad \frac{4.6}{14} \quad \frac{4.8}{10} \quad 4.8 \quad \frac{4.7}{9} \quad \frac{4.3}{17} \quad \frac{5.6}{24} \quad \frac{5.4}{44} \quad \frac{6.0}{63} \quad \frac{7.0}{69} \quad \frac{10.8}{77} \end{array}$$

$$\begin{array}{r} \frac{2.0}{33} \quad \frac{6.4}{22} \quad \frac{6.4}{8} \quad 6.4 \quad \frac{5.8}{13} \quad \frac{5.3}{38} \quad \frac{5.5}{40} \quad \frac{7.2}{71} \quad \frac{12.4}{81} \end{array}$$

$$\begin{array}{r} \frac{2.7}{34} \quad \frac{5.9}{25} \quad \frac{6.3}{12} \quad 6.8 \quad \frac{8.6}{8} \quad \frac{8.2}{18} \quad \frac{5.4}{28} \quad \frac{6.3}{40} \quad \frac{6.7}{53} \quad \frac{6.9}{67} \quad \frac{13.8}{82} \\ 14.0 \\ 79 \end{array}$$

$$\begin{array}{r} \frac{5.5}{38} \quad \frac{7.3}{26} \quad \frac{7.5}{14} \quad \frac{10.6}{8} \quad 10.8 \quad 10 \quad \frac{11.0}{19} \quad \frac{8.4}{23} \quad \frac{8.4}{23} \quad \frac{6.3}{27} \quad \frac{5.9}{36} \quad \frac{6.3}{42} \quad \frac{7.7}{62} \quad \frac{7.7}{69} \end{array}$$

On Hubs.

$$\begin{array}{r} \frac{0.7}{78} \quad \frac{6.4}{41} \quad (21.8) \end{array}$$

$$\begin{array}{r} \frac{2.0}{75} \quad \frac{6.3}{49} \quad (23.1) \end{array}$$

$$\begin{array}{r} \frac{6.2}{75} \quad \frac{8.1}{56} \quad \frac{11.5}{35} \quad (25.8) \end{array}$$

$$\begin{array}{r} \frac{5.1}{100} \quad \frac{6.6}{75} \quad \frac{8.2}{57} \quad (30.0) \end{array}$$

$$\begin{array}{r} \frac{5.0}{100} \quad \frac{5.9}{75} \quad \frac{6.2}{56} \quad (30.0) \end{array}$$

$$\begin{array}{r} \frac{9.3}{100} \quad \frac{8.5}{75} \quad \frac{8.8}{49} \quad (38.6) \end{array}$$

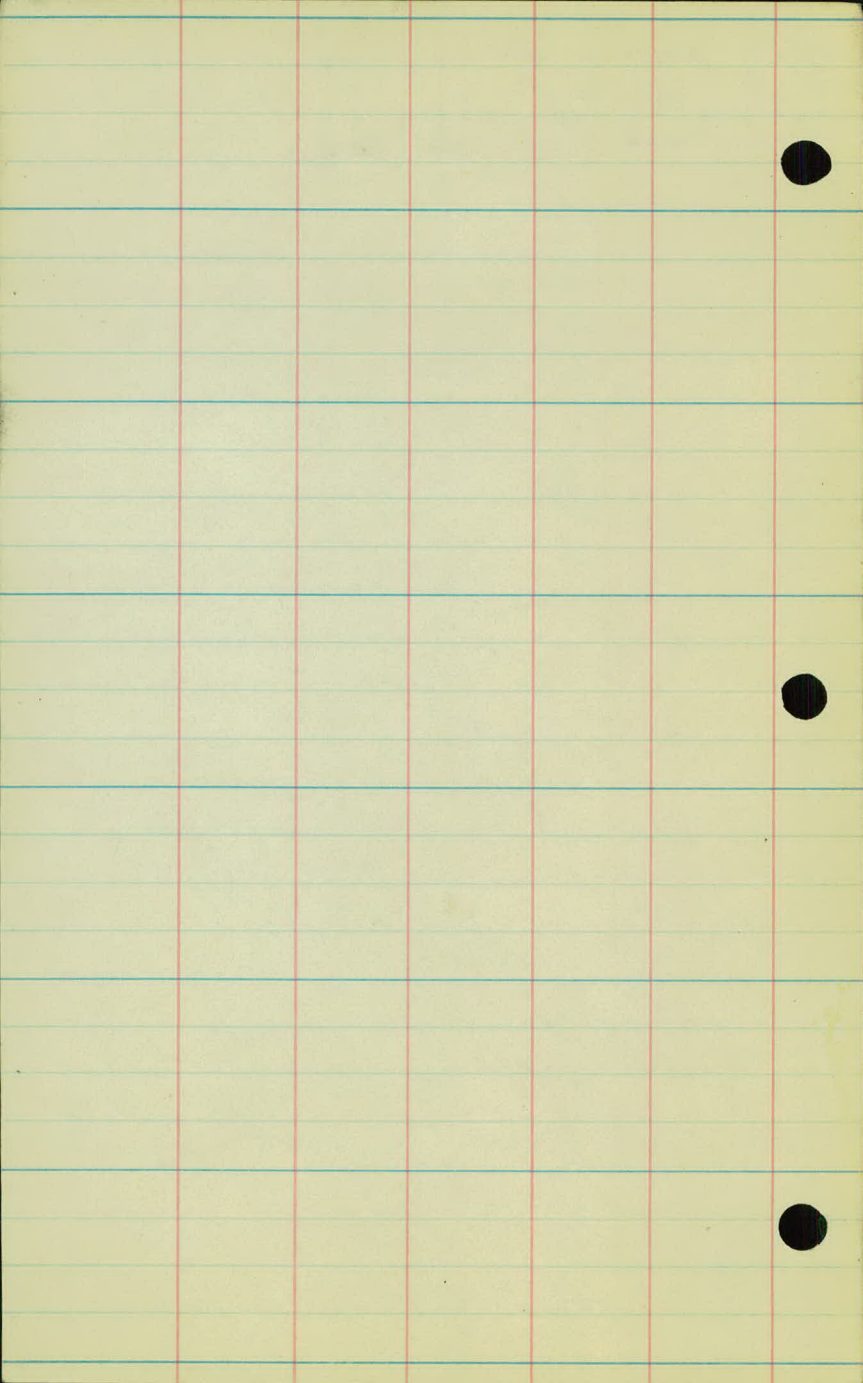
$$\begin{array}{r} \frac{2.5}{100} \quad \frac{2.5}{75} \quad \frac{3.0}{64} \quad \frac{4.4}{56} \quad (38.6) \end{array}$$

Sta.	+	H. I.	-	Rod Elev.	Elev.
313		926.14			85.9
	0.38	917.62	8.90	917.24	
313+14					85.5
313+38					81.5
T.P.	2.00	907.74	11.88	905.74	
313+38					81.5
	1.85	897.95	11.64	896.10	
	5.74	892.11	11.60	886.35	
13.M.			12.47	879.64	879.64

$$\frac{74}{100} \quad \frac{86}{83} \quad \frac{96}{75} \quad \frac{122}{58} \quad \frac{141}{49} \quad (40.2)$$

$$\frac{4.9}{75} \quad \frac{11.4}{52} \quad \frac{17.4}{39} \quad (32.1)$$

$$\frac{3.7}{75} \quad \frac{13.5}{50} \quad (26.2)$$



4/19/27

CW.S.
D.S.
A.B.
T.M.

X Section.

Sta	+ ✓	HI	-	Elev ✓
B.M.	889.32	9.66		879.66

314+00				78.9
--------	--	--	--	------

+50				77.1
-----	--	--	--	------

315+00				77.5
--------	--	--	--	------

+12				81.6
-----	--	--	--	------

+24				81.9
-----	--	--	--	------

+50				81.5
-----	--	--	--	------

B.M.	10.60	890.26 ✓	9.66	879.66 ✓
------	-------	----------	------	----------

+60				78.5
-----	--	--	--	------

316+00				78.5
--------	--	--	--	------

317+00				81.3
--------	--	--	--	------

318+00				83.5
--------	--	--	--	------

319				85.8
-----	--	--	--	------

T.P.	5.94	894.89 ✓	1.31	889.75 ✓
------	------	----------	------	----------

Lake Elev

$\frac{85}{50}$	$\frac{98}{20}$	104	$\frac{102}{9}$	$\frac{46}{20}$	$\frac{37}{23}$	$\frac{3.7}{50}$	$\frac{5.0}{78}$	$\frac{12.6}{88}$
-----------------	-----------------	-----	-----------------	-----------------	-----------------	------------------	------------------	-------------------

$\frac{105}{50}$	$\frac{114}{29}$	12.2	$\frac{110}{40}$	$\frac{5.0}{17}$	$\frac{5.6}{27}$	$\frac{12.1}{41}$
------------------	------------------	------	------------------	------------------	------------------	-------------------

$\frac{110}{50}$	$\frac{127}{28}$	$\frac{118}{18}$	$\frac{72}{12}$	$\frac{70}{24}$	$\frac{110}{29}$	$\frac{133}{37}$
------------------	------------------	------------------	-----------------	-----------------	------------------	------------------

$\frac{110}{50}$	$\frac{115}{35}$	$\frac{110}{10}$	27	$\frac{20}{21}$	$\frac{10.0}{24}$	$\frac{10.5}{46}$	$\frac{133}{50}$
------------------	------------------	------------------	----	-----------------	-------------------	-------------------	------------------

$\frac{108}{50}$	$\frac{110}{36}$	$\frac{108}{15}$	$\frac{75}{9}$	$\frac{7.4}{7.4}$	$\frac{70}{22}$	$\frac{90}{24}$	$\frac{96}{43}$	$\frac{120}{50}$
------------------	------------------	------------------	----------------	-------------------	-----------------	-----------------	-----------------	------------------

$\frac{108}{50}$	$\frac{110}{35}$	$\frac{115}{14}$	$\frac{115}{6}$	$\frac{78}{7}$	$\frac{5.5}{23}$	$\frac{70}{27}$	$\frac{9.5}{44}$	$\frac{12.2}{52}$
------------------	------------------	------------------	-----------------	----------------	------------------	-----------------	------------------	-------------------

$\frac{120}{50}$	$\frac{126}{12}$	$\frac{133}{4}$	118	$\frac{7.5}{8}$	$\frac{6.0}{28}$	$\frac{8.6}{35}$	$\frac{10.0}{45}$	$\frac{11.2}{50}$	$\frac{133}{57}$
------------------	------------------	-----------------	-----	-----------------	------------------	------------------	-------------------	-------------------	------------------

$\frac{107}{50}$	$\frac{117}{25}$	$\frac{118}{13}$	$\frac{133}{7}$	$\frac{133}{5}$	$\frac{118}{5}$	$\frac{4.5}{16}$	$\frac{4.0}{32}$	$\frac{50}{40}$	$\frac{5.5}{53}$	$\frac{96}{66}$	$\frac{133}{72}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	-----------------	------------------	-----------------	------------------

$\frac{7.2}{50}$	$\frac{10.2}{30}$	$\frac{110}{20}$	$\frac{13.2}{13}$	$\frac{13.0}{9}$	$\frac{11.5}{9}$	$\frac{11.5}{3}$	90	$\frac{2.7}{13}$	$\frac{3.5}{30}$	$\frac{4.0}{55}$	$\frac{12.5}{73}$
------------------	-------------------	------------------	-------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	-------------------

$\frac{6.2}{50}$	$\frac{80}{37}$	$\frac{93}{18}$	$\frac{10.7}{16}$	$\frac{11.2}{12}$		$\frac{6.8}{14}$	$\frac{2.0}{30}$	$\frac{2.0}{50}$	$\frac{2.0}{50}$	$\frac{12.2}{72}$
------------------	-----------------	-----------------	-------------------	-------------------	--	------------------	------------------	------------------	------------------	-------------------

$\frac{+60}{50}$	$\frac{00}{30}$	$\frac{30}{23}$	$\frac{6.2}{6}$	45	$\frac{1.2}{6}$	$\frac{1.3}{28}$	$\frac{1.5}{47}$	$\frac{190}{70}$
------------------	-----------------	-----------------	-----------------	----	-----------------	------------------	------------------	------------------

319 + H.I. - 120
89484

320 87.5

321 89.9

322 90.9

323 91.4

324 92.2

T.P. 9.78 899.65 ✓ 5.02 889.87 ✓

+50 92.4

325 92.9

+5900 93.1

326 93.4

+50 93.7

327 93.7

$\frac{6.6}{50}$ $\frac{8.6}{40}$ $\frac{11.6}{9}$ 7.4 $\frac{5.6}{4}$ $\frac{5.5}{23}$ $\frac{5.6}{44}$ $\frac{15.8}{66}$

$\frac{10.6}{50}$ $\frac{13.0}{18}$ $\frac{5.0}{20}$ $\frac{4.8}{40}$ $\frac{5.0}{40}$ $\frac{16.8}{64}$

$\frac{1.40}{50}$ $\frac{13.5}{37}$ $\frac{4.2}{5}$ 4.0 $\frac{3.8}{50}$ $\frac{4.2}{38}$ $\frac{14.0}{58}$

$\frac{17.0}{50}$ $\frac{15.8}{37}$ $\frac{4.0}{8}$ $\frac{3.5}{17}$ $\frac{3.2}{17}$ $\frac{3.5}{35}$ $\frac{15.0}{58}$

$\frac{15.8}{50}$ $\frac{15.0}{38}$ $\frac{2.8}{11}$ 2.7 $\frac{2.7}{15}$ $\frac{2.8}{30}$ $\frac{13.5}{56}$

$\frac{17.0}{50}$ $\frac{16.0}{38}$ $\frac{7.3}{13}$ 7.3 $\frac{7.2}{28}$ $\frac{16.0}{47}$ $\frac{16.0}{50}$

$\frac{8.2}{50}$ $\frac{10.0}{25}$ $\frac{9.0}{19}$ $\frac{6.8}{14}$ $\frac{4.8}{27}$ $\frac{7.4}{27}$ $\frac{12.2}{38}$ $\frac{13.0}{50}$

$\frac{1.0}{50}$ $\frac{2.3}{34}$ $\frac{3.0}{32}$ $\frac{8.0}{25}$ $\frac{7.8}{19}$ $\frac{6.6}{14}$ 6.6 $\frac{6.8}{27}$ $\frac{8.2}{30}$ $\frac{8.2}{36}$ $\frac{4.5}{42}$ $\frac{5.7}{50}$

$\frac{6.0}{50}$ $\frac{0.3}{39}$ $\frac{0.7}{36}$ $\frac{8.5}{24}$ $\frac{8.0}{20}$ $\frac{6.4}{15}$ 6.3 $\frac{6.6}{26}$ $\frac{8.3}{29}$ $\frac{8.3}{32}$

$\frac{8.2}{24}$ $\frac{7.7}{19}$ $\frac{6.2}{17}$ 6.0 $\frac{6.6}{25}$ $\frac{8.0}{29}$ $\frac{8.4}{33}$

$\frac{7.8}{23}$ $\frac{7.5}{19}$ $\frac{6.0}{16}$ 6.0 $\frac{6.4}{24}$ $\frac{7.7}{26}$ $\frac{8.2}{31}$

Jt9 + H.I. / -
89965

327+50

93.7

328+00

93.5

+36⁵⁴

93.4

328+8.421=
329+012

93.3

T.P. 10.37 903.39

6.63 893.02

B.M.

319 90020=90023

B.M. 6.23 906.46

90023

326+00

93.4

+50

93.7

327

93.7

+50

93.7

328

93.5

+36⁵⁴

93.4

E900

93.3

4/19/27

$$\frac{77}{23} \quad \frac{77}{19} \quad \frac{61}{17} \quad 6.9 \quad \frac{6.4}{23} \quad \frac{8.0}{27} \quad \frac{8.0}{32}$$

$$\frac{74}{23} \quad \frac{75}{20} \quad \frac{61}{18} \quad 6.2 \quad \frac{6.7}{21} \quad \frac{8.4}{26} \quad \frac{8.7}{30}$$

$$\frac{75}{24} \quad \frac{72}{20} \quad \frac{64}{16} \quad 6.3 \quad \frac{6.7}{22} \quad \frac{8.4}{26} \quad \frac{8.5}{32}$$

$$\frac{77}{27} \quad \frac{77}{23} \quad \frac{64}{19} \quad 6.4 \quad \frac{6.6}{21} \quad \frac{7.9}{25} \quad \frac{8.0}{29}$$

3rd PP 80 Lt 5th.

$$(13.1)$$

$$\frac{7.3}{44} \quad \frac{7.3}{50}$$

$$(12.8)$$

$$\frac{2.8}{51} \quad \frac{2.7}{54}$$

$$(12.8)$$

$$\frac{0.0}{52} \quad \frac{0.0}{55}$$

$$(12.8)$$

$$\frac{2.2}{50} \quad \frac{2.3}{55}$$

$$(13.0)$$

$$\frac{3.4}{48} \quad \frac{3.5}{50}$$

$$(13.1)$$

$$\frac{4.5}{46} \quad \frac{4.6}{50}$$

$$(13.2)$$

$$\frac{7.8}{49} \quad \frac{8.0}{45} \quad \frac{7.2}{50}$$

Sta + H.I. - Elev

326+50 93.7

T.P. 11.90 916.43 1.93 904.53

327+00 93.7

T.P. 5.63 920.69 1.57 915.06

+50 93.7

328 93.5

+36 ~~54~~ 93.4

Equip 93.3

T.P. 1.02 912.29 9.42 911.27

B.M. 12.06 900.23

$$\frac{30}{50} \quad \frac{30}{46} \quad \frac{35}{42}$$

12.8

$$\frac{50}{50} \quad \frac{50}{49} \quad \frac{55}{47}$$

22.7

$$\frac{38}{53} \quad \frac{46}{47}$$

27.0

$$\frac{45}{55} \quad \frac{64}{49}$$

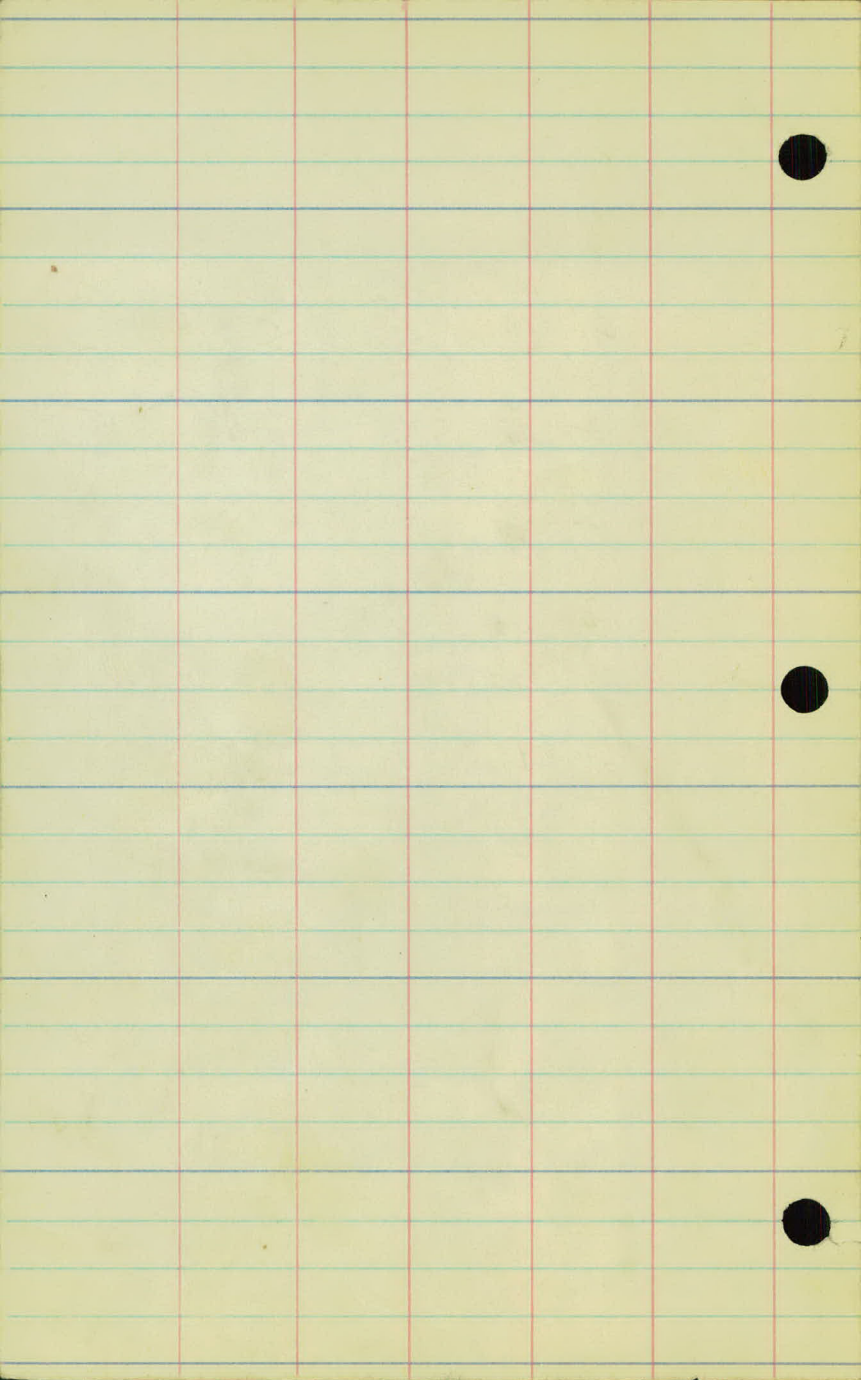
27.2

$$\frac{76}{55} \quad \frac{90}{49}$$

27.3

$$\frac{94}{54} \quad \frac{104}{50}$$

27.4



3/17/27

C.W.S.

X Sections.

D.S.

Line Revision.

AB

T.M.

~~318774~~

309450 - 318779²⁵ =

26-62

Dir B.

Sta + or - Elev.

309 + 50 85.0.

310 + 00 85.4
84.9

+ 50 85.4
84.9

311 + 00 85.8.

+ 20 ↓
+ 0.3 86.1.

+ 50 86.4.

312 + 00 86.4.

+ 50 86.4.

+ 81.69 86.9.

313 86.8.

+ 23 86.5.

+ 26 82.1.

3/12/27
 C.W.S.
 D.S.
 A.B.
 T.M.

$\frac{25}{40}$ $\frac{75}{27}$ $\frac{67}{9}$ $\frac{78}{8}$ 71 $\frac{70}{7}$ $\frac{65}{8}$ $\frac{65}{25}$ $\frac{70}{26}$ $\frac{70}{32}$ $\frac{51}{37}$ $\frac{48}{50}$

$\frac{50}{50}$ $\frac{70}{42}$ $\frac{76}{9}$ $\frac{85}{8}$ 78 $\frac{78}{6}$ $\frac{72}{7}$ $\frac{77}{23}$ $\frac{82}{26}$ $\frac{86}{30}$ $\frac{52}{35}$ $\frac{82}{50}$

- $\frac{45}{50}$ $\frac{84}{37}$ $\frac{80}{24}$ $\frac{75}{9}$ $\frac{80}{8}$ $\frac{80}{5}$ $\frac{73}{21}$ $\frac{73}{23}$ $\frac{83}{28}$ $\frac{87}{29}$ $\frac{87}{35}$ $\frac{100}{50}$ $\frac{115}{50}$

$\frac{00}{56}$ $\frac{44}{50}$ $\frac{62}{47}$ $\frac{67}{11}$ $\frac{71}{6}$ 75 $\frac{70}{6}$ $\frac{67}{20}$ $\frac{97}{25}$ $\frac{107}{34}$ $\frac{117}{50}$

✓ $\frac{00}{102}$ $\frac{50}{91}$ $\frac{67}{74}$ $\frac{65}{50}$ $\frac{66}{8}$ 72 $\frac{70}{7}$ $\frac{70}{21}$ $\frac{102}{27}$ $\frac{120}{50}$

$\frac{00}{102}$ $\frac{50}{90}$ $\frac{65}{79}$ $\frac{70}{50}$ $\frac{60}{33}$ $\frac{70}{30}$ 70 $\frac{66}{17}$ $\frac{73}{25}$ $\frac{112}{31}$ $\frac{122}{50}$

✓ $\frac{00}{89}$ $\frac{60}{77}$ $\frac{60}{37}$ $\frac{65}{7}$ 70 $\frac{65}{7}$ $\frac{75}{21}$ $\frac{70}{29}$ $\frac{110}{37}$ $\frac{120}{56}$

✓ $\frac{00}{80}$ $\frac{65}{70}$ $\frac{60}{50}$ $\frac{55}{20}$ $\frac{60}{10}$ 68 $\frac{65}{15}$ $\frac{70}{24}$ $\frac{70}{34}$ $\frac{80}{38}$ $\frac{125}{45}$ $\frac{125}{50}$

✓ $\frac{00}{67}$ $\frac{60}{57}$ $\frac{65}{30}$ $\frac{55}{17}$ $\frac{60}{10}$ 65 $\frac{62}{18}$ $\frac{70}{26}$ $\frac{78}{46}$ $\frac{100}{50}$ $\frac{55}{50}$

$\frac{00}{67}$ $\frac{70}{50}$ $\frac{70}{35}$ $\frac{65}{20}$ 66 $\frac{65}{19}$ $\frac{80}{50}$

$\frac{492}{65}$ $\frac{00}{54}$ $\frac{30}{50}$ $\frac{75}{39}$ $\frac{80}{12}$ 70 $\frac{70}{12}$ $\frac{65}{15}$ $\frac{62}{21}$ $\frac{78}{35}$ $\frac{80}{50}$

✓ $\frac{150}{66}$ $\frac{471}{56}$ $\frac{125}{50}$ $\frac{70}{37}$ $\frac{77}{15}$ $\frac{108}{7}$ 112 $\frac{65}{8}$ $\frac{65}{17}$ $\frac{80}{26}$ $\frac{85}{32}$ $\frac{55}{50}$

279 + or - Elev

313 + 54 811.

314 + 00 798.

+ 50 783.

315 + 00 782.

+ 28 771.

+ 50 778.

+ 78 778.

316 784.

+ 50 779.

160¹⁵ 786.

317 835.

+ 32 59 873.

$$\begin{array}{cccccccccccc} +13.3 & +8.0 & 0.0 & 2.0 & 7.0 & 8.0 & 11.0 & 12.2 & 12.2 & 7.4 & 7.0 & 7.8 & 8.2 \\ 76 & 64 & 46 & 44 & 30 & 22 & 17 & \underline{11} & 3 & 21 & 30 & 34 & 50 \end{array}$$

$$\begin{array}{cccc} 7.7 & 8.5 & 9.6 & \\ 50 & 22 & \underline{11} & \\ & & & 100 & 4.8 & 3.8 & 4.0 \\ & & & 11 & 22 & 28 & 50 \end{array}$$

$$\begin{array}{cccc} 9.5 & 100 & 110 & 11.7 & 4.5 & 4.2 \\ 50 & 25 & \underline{11} & 15 & 32 & 50 \end{array}$$

$$\begin{array}{cccccc} 10.5 & 10.5 & 11.5 & 110 & 120 & 9.5 & 6.4 & 6.5 & 130 \\ 50 & 43 & 28 & \underline{11} & 18 & 26 & 31 & 44 & 50 \end{array}$$

$$\begin{array}{cccccc} 10.8 & 11.0 & & 12.2 & 11.8 & 7.5 & 6.8 & 100 & 10.2 \\ 50 & 27 & & \underline{11} & 10 & 19 & 42 & 46 & 50 \end{array}$$

$$\begin{array}{cccccc} 10.5 & 110 & 116 & 11.6 & 7.0 & 70 & 94 & 7.0 \\ 50 & 33 & \underline{11} & 2 & 12 & 39 & 41 & 50 \end{array}$$

$$\begin{array}{cccccc} & & & & & & & & 125 \\ 10.2 & 110 & 112 & 11.6 & 11.5 & 12.7 & 6.6 & 6.2 & 50 \\ 50 & 25 & \underline{11} & 4 & 8 & 11 & 22 & 36 & 44 \end{array}$$

$$\begin{array}{cccccc} 9.2 & 100 & 10.9 & 110 & 110 & 12.5 & 12.2 & 5.5 & 5.5 \\ 50 & 40 & 19 & \underline{11} & 1 & 2 & 9 & 27 & 50 \end{array}$$

$$\begin{array}{cccccc} 8.7 & 9.7 & 10.7 & 120 & 11.5 & 110 & 2.6 & 3.5 \\ 50 & 26 & 9 & 8 & \underline{11} & 3 & 20 & 50 \end{array}$$

$$\begin{array}{cccccc} 8.4 & 9.6 & 10.2 & 12.4 & 12.5 & 10.8 & 10.8 & 2.5 & 3.4 & 5.0 \\ 50 & 24 & 12 & 9 & 4 & 1 & \underline{11} & 29 & 50 & \end{array}$$

$$\begin{array}{cccccc} 8.4 & 9.5 & 9.8 & 120 & 11.7 & 10.5 & 10.2 & 5.6 & 2.2 & 3.2 & 5.0 \\ 50 & 30 & 22 & 19 & 14 & 12 & 10 & \underline{11} & 8 & 50 & \end{array}$$

$$\begin{array}{cccccc} 9.2 & 100 & 12.2 & 12.2 & 10.6 & 10.5 & 10 & 50 & 60 & 5.0 \\ 50 & 32 & 29 & 25 & 22 & 20 & \underline{11} & 43 & 50 & \end{array}$$

Sta	+or-	Elev
318		880.
+50		886.
+84.2 =	Equal	889.

X sec. Extended on the right from Sta. 315+78 to Sta. 318+00.

315+78

316

+50

+60¹⁵

317

+36⁵⁹

318

3/17/27
 C.W.S.
 D.S.
 A.B.
 T.M.

$\frac{12}{14}$

$\frac{7.8}{50}$	$\frac{8.8}{43}$	$\frac{12.2}{40}$	$\frac{12.0}{36}$	$\frac{9.2}{33}$	$\frac{9.4}{31}$	$\frac{1.5}{29}$	$\frac{11.4}{50}$	$\frac{11.8}{57}$
------------------	------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------

$\frac{7.2}{50}$	$\frac{8.5}{35}$	$\frac{8.8}{20}$	$\frac{9.8}{}$	$\frac{1.0}{22}$	$\frac{11.5}{43}$	$\frac{11.0}{50}$
------------------	------------------	------------------	----------------	------------------	-------------------	-------------------

$\frac{6.2}{50}$	$\frac{7.4}{34}$	$\frac{8.7}{20}$	$\frac{9.5}{}$	$\frac{0.7}{21}$	$\frac{11.2}{42}$	$\frac{11.2}{50}$
------------------	------------------	------------------	----------------	------------------	-------------------	-------------------

→ shore line

11.5	$\frac{5.3}{41}$	$\frac{7.6}{46}$	$\frac{12.0}{58}$	$\frac{12.0}{63}$
------	------------------	------------------	-------------------	-------------------

→ shore line

11.2	$\frac{5.3}{50}$	$\frac{5.2}{54}$	$\frac{9.5}{60}$	$\frac{10.1}{67}$	$\frac{11.8}{71}$
------	------------------	------------------	------------------	-------------------	-------------------

→ shore line

11.5	$\frac{5.5}{50}$	$\frac{5.4}{67}$	$\frac{11.8}{80}$
------	------------------	------------------	-------------------

→ water

10.9	$\frac{3.5}{50}$	$\frac{5.6}{67}$	$\frac{11.8}{81}$	$\frac{13.8}{86}$
------	------------------	------------------	-------------------	-------------------

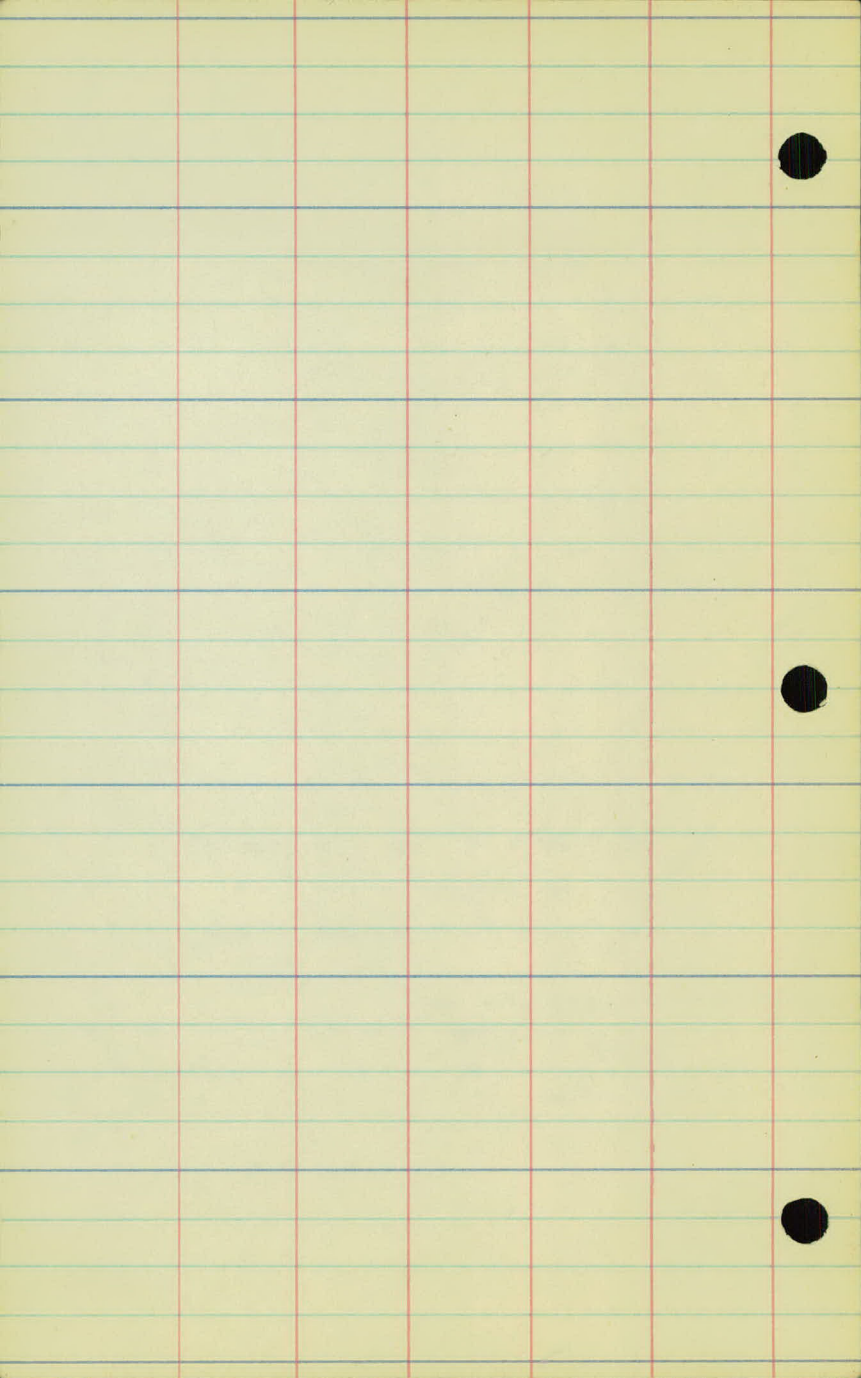
→ water

5.6	$\frac{3.3}{50}$	$\frac{3.4}{57}$	$\frac{12.0}{76}$	$\frac{13.0}{81}$
-----	------------------	------------------	-------------------	-------------------

→ water

2.1	$\frac{3.1}{44}$	$\frac{11.5}{65}$	$\frac{11.6}{70}$
-----	------------------	-------------------	-------------------

1.2	$\frac{1.7}{29}$	$\frac{12.0}{53}$	$\frac{12.3}{54}$
-----	------------------	-------------------	-------------------



3/17/27
C.W.S.
D.S.
A.B.
T.M.

X Sections Cont.

Top Slope

309+50 - 313+36

26-62

Div "B"

Sta	+	HI	-	Elev	
B.M.	11.22	904.77		893.57	
T.P.	9.36	913.78	0.37	904.42	
309+50			4.75	909.08	85.0

310					85.4
-----	--	--	--	--	------

+50					85.4
-----	--	--	--	--	------

311.					85.8
------	--	--	--	--	------

T.P.	10.56	926.14	4.20	909.58	
------	-------	--------	------	--------	--

+20					86.1
-----	--	--	--	--	------

+50					86.4
-----	--	--	--	--	------

312					86.4
-----	--	--	--	--	------

+50					86.4
-----	--	--	--	--	------

T.P.	6.96	926.04	1.06	919.08	
------	------	--------	------	--------	--

81.69.					86.9
--------	--	--	--	--	------

313					86.8
-----	--	--	--	--	------

+23					86.5
-----	--	--	--	--	------

+36					82.1
-----	--	--	--	--	------

Spine in 12" Oak 454 304+95.

$$\frac{5.0}{20} \quad \frac{65}{85} \quad \frac{95}{50}$$

28.8

$$\frac{72}{75} \quad \frac{10.8}{58}$$

28.4

$$\frac{8.3}{79} \quad \frac{12.4}{59}$$

28.4

$$\frac{5.5}{104} \quad \frac{92}{81} \quad \frac{11.7}{60}$$

28.0

$$\frac{9.2}{132} \quad \frac{11.8}{106}$$

34.0

$$\frac{8.5}{38} \quad \frac{10.6}{106}$$

33.7

$$\frac{7.5}{128} \quad \frac{20}{98}$$

32.7

$$\frac{1.0}{117} \quad \frac{1.0}{84}$$

33.7

$$\frac{2.8}{106} \quad \frac{4.4}{78}$$

39.1

$$\frac{1.5}{114} \quad \frac{5.2}{80}$$

39.2

$$\frac{4.4}{104} \quad \frac{12.5}{69}$$

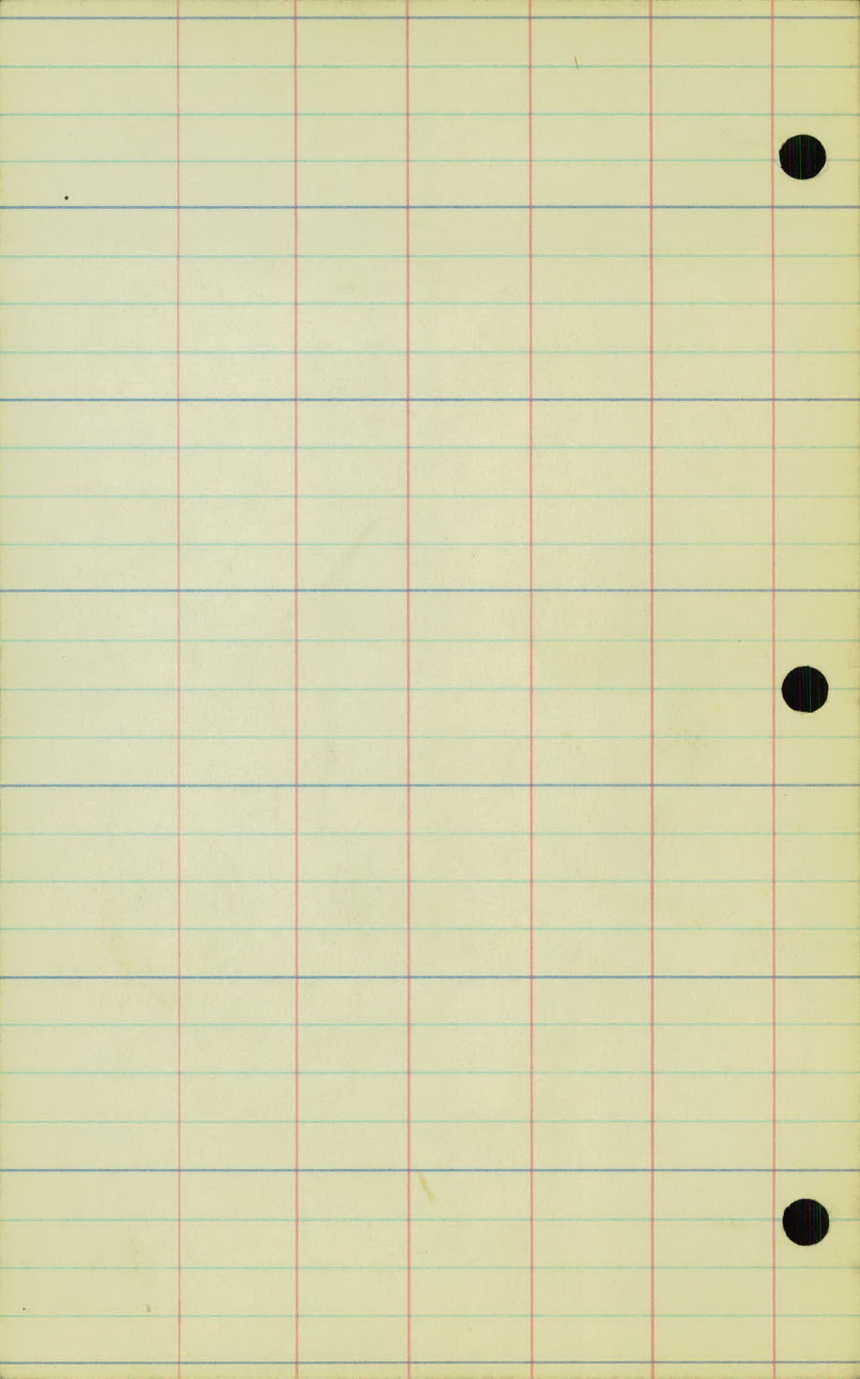
39.5

$$\frac{7.8}{93} \quad \frac{120}{80}$$

43.9

Sta	+	HT	-	Elev
		926.04		
T.P.	0.61	914.47	12.18	913.86
T.P.	0.49	903.64	11.32	903.15
T.P.	0.90	892.91	11.63	892.01
B.M.			13.22	879.69

spike in 6" Poplar 100 Ft. Sta 312+50



3/15/27

Alignment

C.W.S.
P.S.
A.B.
T.M.

$$305 + 29^{36} - 318 + 84^{+2}$$

26-62.

Div B

279 Point A Lt 4 Rt.

316+60⁵¹ PT 13°-08'

+50 12°-37'

316 10°-07'

+50 7°-37' Δ 26°16'

315+51⁶⁹ PT 26°-16' D 10°

315 5°-07' T. 133.85

+50 2°-37' L 262.67

314 00°-07' R. 573.69

313+97⁸⁴ PC 00°-00'

312+81⁶⁹ P.L. 18°-48°

+50 18-01'

312 16°-46'

+50 15°-31'

311 14°-16'

+50 13°-01'

310 11°-26'

+50 10°-31'

309+19²¹ PT 37°-37'

309 9°-16'

+50 8°-01'

308 6°-46'

+50 5°-31'

307 4°-16'

+50 3°-01'

306 1°-46'

+50 00°-31'

305+29²⁶ PC 00°-07'

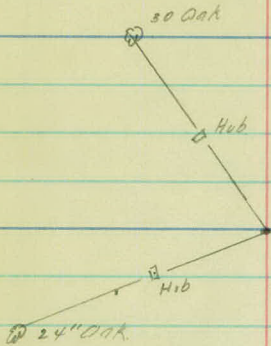
A 37°-37'

D. 5° Lt

T. 390.44

L 752.33

R 1146.28

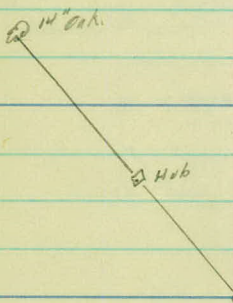


0.7
6.5

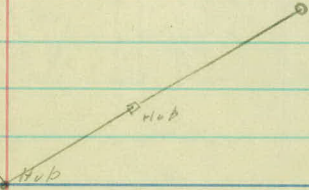
Sta Point AL AR

318 + 79 ²⁵			
318 + 84 ⁴⁴	P.T.	7°-23 ³⁰	Δ 140 ⁴⁷
+50		50'-40'	D 100
318 + 11 ⁰¹	P.T.	14°-47'	T 74 ⁴²
318		3°-10	L 147 ⁸³
+50		00°-40'	R 523 ⁶⁹
317 + 36 ⁵⁹	P.C.	0°-0	

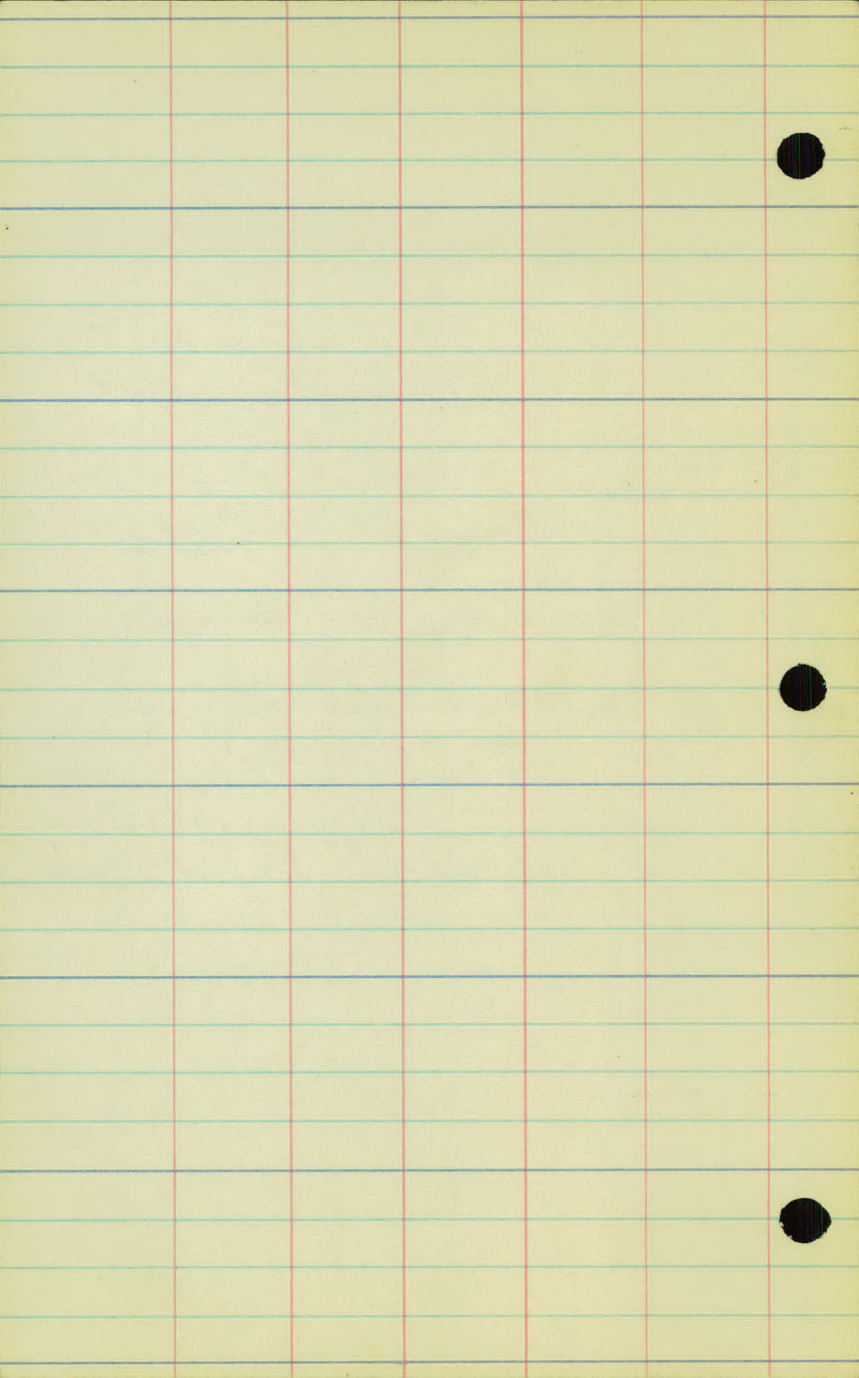
W. Oak.



T.P.



Hub



3/17/27

C.W.S

D.S.

AB

T.M.

Topography

309 - 3/8+84

26 - 62

Div B.

314

Hwy to Cattle Pass 4' x 16' x 42'

313

312

311

310

309

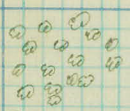
3/17/27

+ 757 - 1 -

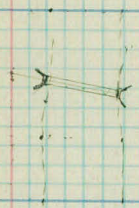
Lowland.

End Tree

16 Trees



+ 54 B.W 20-50



+ 65 - 19'

Borrow Pt.

Road

404 X Drain 30" X 90 P³

318

317

316

315

3/17/27

G.W.S.
D.S.
A.B.
T.M.

+84 F. 50'

+71 T. 42'

+00 T 49'
F 47'

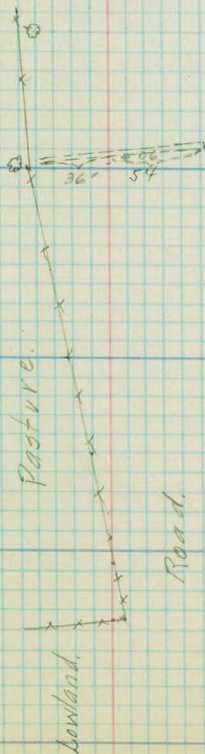
+50 F 39'

F 24'

+50 F 11'

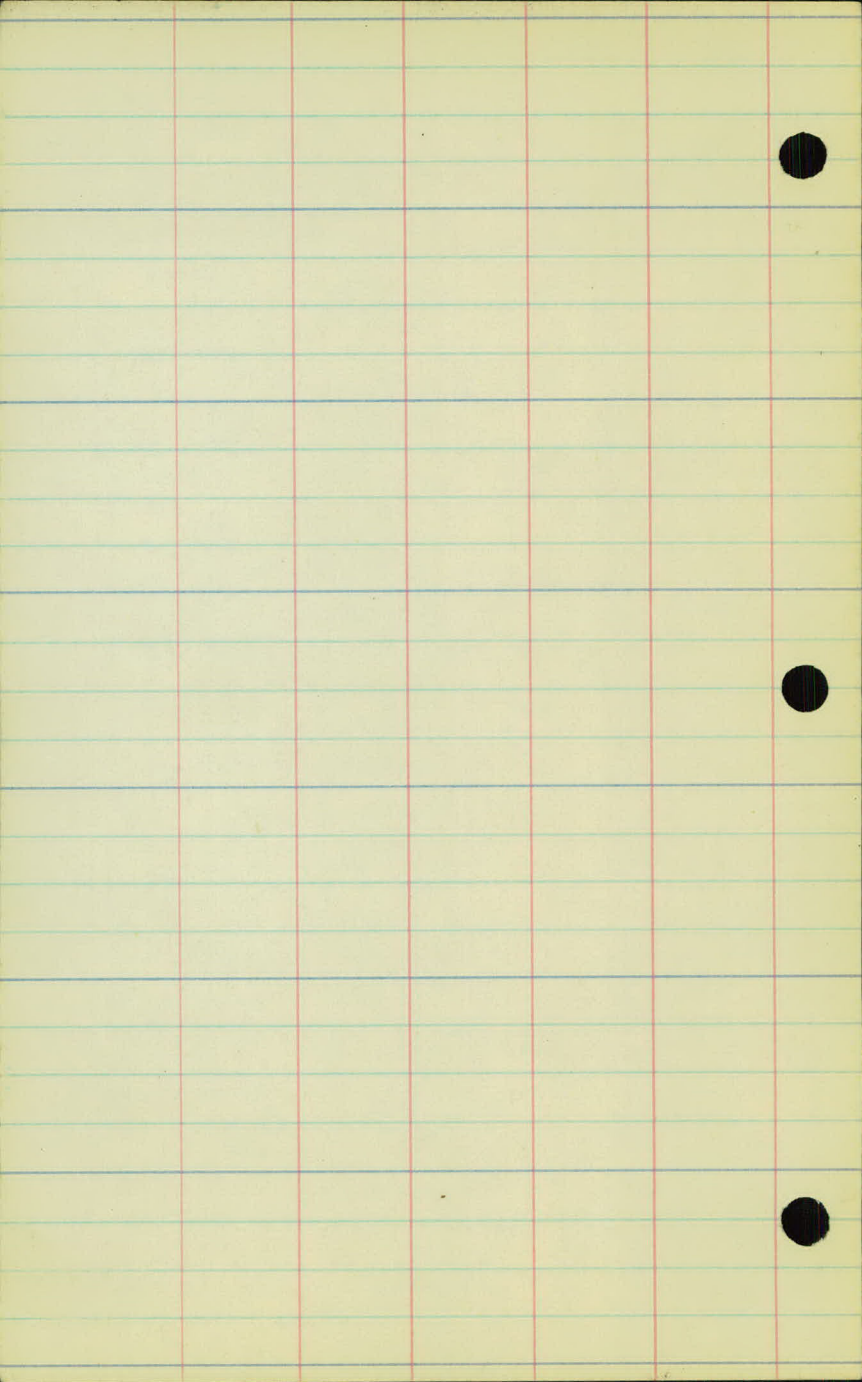
F 1.

+65 F



+65 F Cor 4'

lowland



3/17/27

to Levels.
309 - 318+84^N

C.W.S.
D.S.
A.B.
T.M.

26 - 62

Div B

Sta	+	H I	-	Elev	
B M,	8.90	888.56		879.66	
309+50				885.0.	36.
310				85.4 <u>84.9</u>	3.2
+50				85.4 <u>84.9</u>	3.2
311				85.8.	2.8
+50				86.4.	2.2
312				86.4.	2.2
+50				86.4.	2.2
+81 ⁶³				86.9.	1.7
313				86.8.	1.8
+73				86.5.	2.1
+36				82.1.	6.5
+54				81.1.	7.5

3/17/27

Spike in 6" Maple 100 Rt Sta 312+50

Sta	+ HI	-	Elev
	888.56		
314	79.8.		8.8
+50	78.3.		10.3
315	78.2.		10.4
+28	77.1.		11.5
+50	77.8.		10.8
78	77.8.		10.8
316	78.4.		10.2
+12	78.9.		9.7
+20	77.4.		11.2
+42	77.0.		11.6
+50	77.9.		10.7
+60 ⁵¹	78.6.		10.0

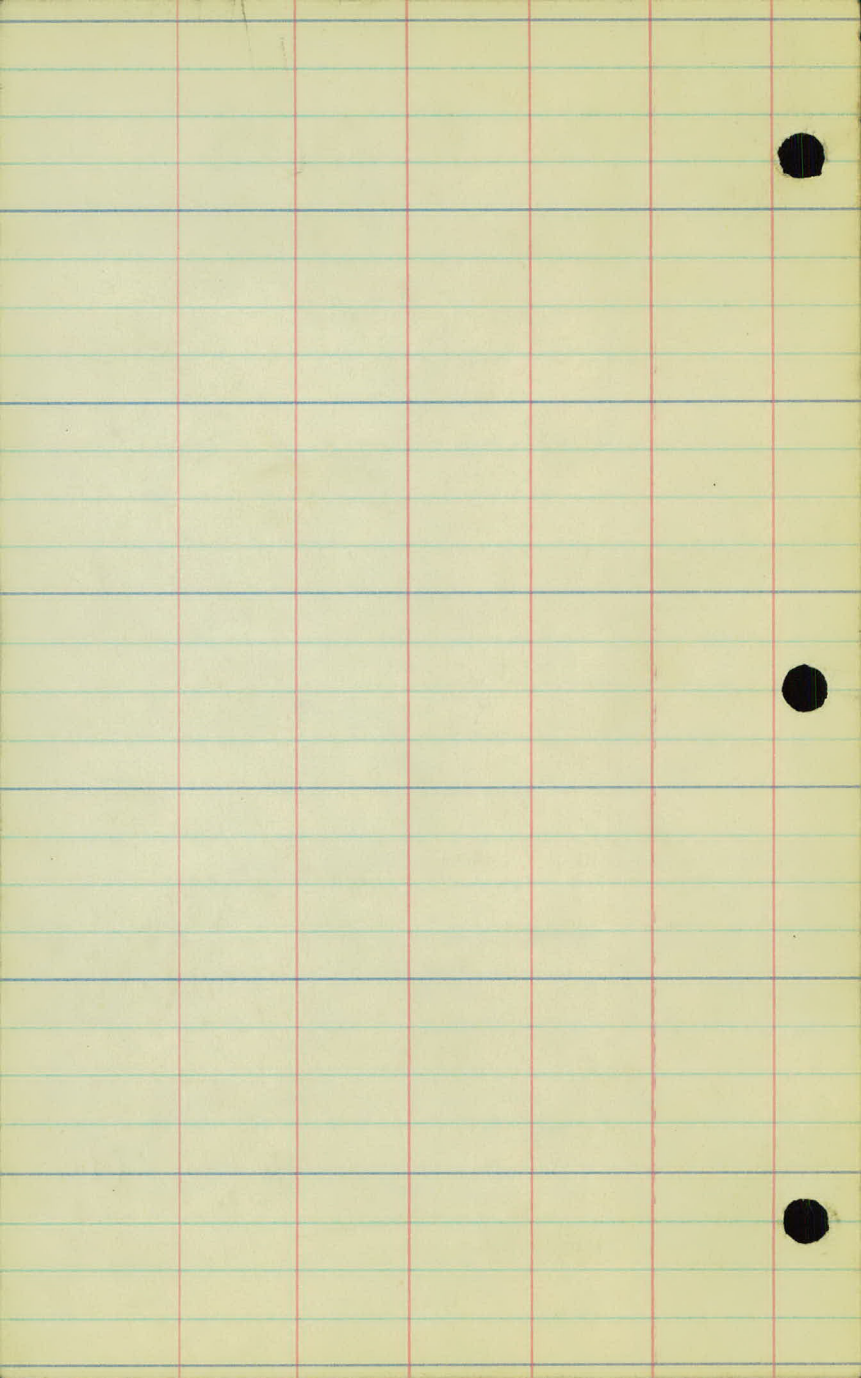
3/17/27



270	+	HI	-	Fler.
		888.56		
317		83.8.		4.8
136 ⁵⁹		87.3.		1.3
+50		87.3.		1.3
318		88.0.		0.6
+50		88.6.		0.0
$\frac{318+34^{42}}{318+39^{25}}$ Equiv.		88.9.		1.03
1319			8.90	879.66

3/12/27

Spike 6" Poplar 100' at Sta 312+50

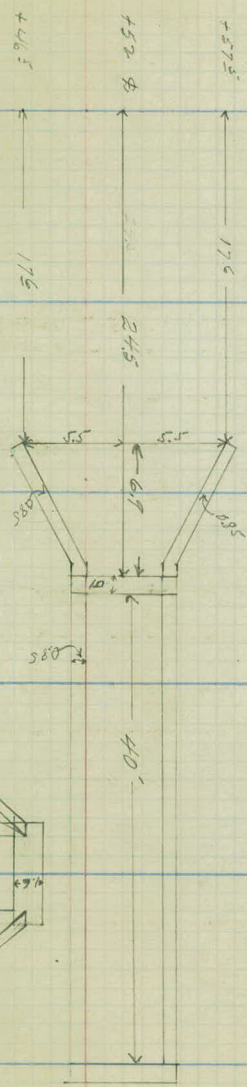
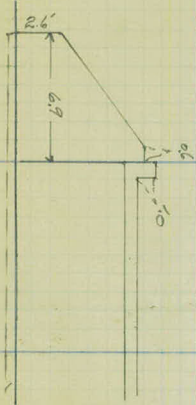


Topography
Cattle Pass
Sta 318+52.

4/25/27
C. W. S.
D. S.
A. B.
T. M.

+52 @ Cattle Pass

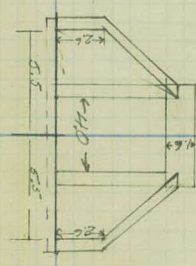
313



+57.5'
 +52.8'
 +46.5'

17.6
 24.5
 4.0

57.5' Beg Wing Wall 17.6
 +52 Head Wall 25.5'
 +52 to Left to Pass 24.5
 +46.5' Beg Wing Wall 17.6



T





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