

CROSS SECTIONS

ANOKA CUTOFF

From
Sta. 188+30
To
Sta. 837+84.1

RAMSEY CO. PROJ. N^o 26.62

Road ^o/_c N^o 93
FILE N^o 5

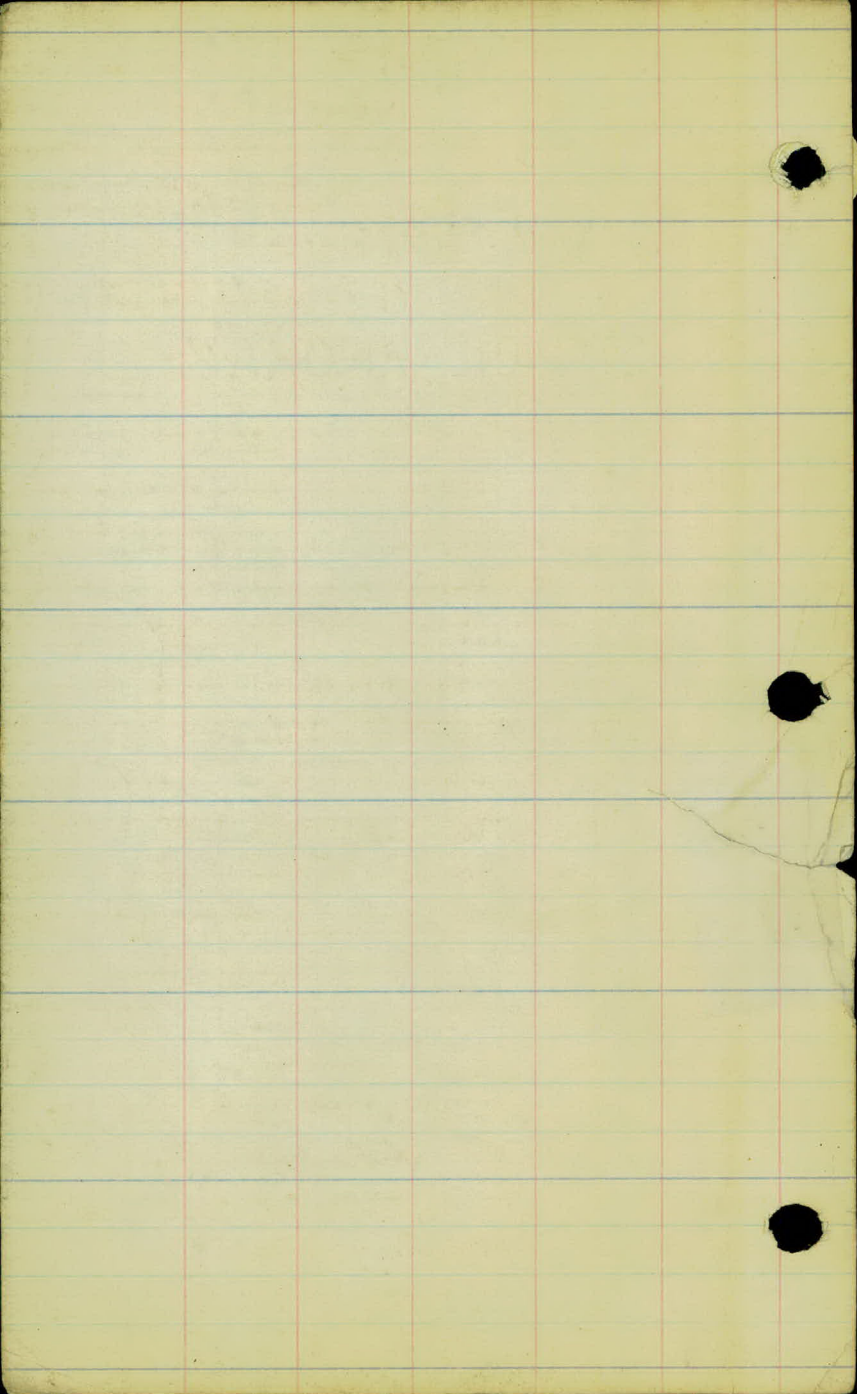
of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed..... 6-8-26

File No..... 5

CROSS-SECTIONS

ST. PAUL - ANOKA



RAMSEY COUNTY
ST-PAUL-ANOKA SURVEY

"H" LINE

CROSS-SECTIONS

station 188+30 to

"H" Line

Station	+	H.I	-	Rod	Elev.
B.M.	7.41	927.61 ✓			930.02 ✓
188+30				3.3	22.9 ✓
188+65				6.5	21.7 ✓
189+00				8.0	19.6 ✓
189+50				10.4	17.2 ✓
T.P.	6.02	916.73 ✓	11.10		916.51 ✓
190+00				2.3	14.4 ✓
190+50				3.9	12.8 ✓
191+00				4.6	12.1 ✓
191+50				5.8	10.9 ✓
192+00				6.0	10.7 ✓
192+50				5.0	11.7 ✓
192+75				3.7	13.0 ✓
193+00				4.4	12.3 ✓

SEE R-10

Lt. 2 Lt. W.H. Parsons Jan, 12, 1925
S.M.N.
122000

On top of concrete wall 67 ft. sta. 186+63 ("H" Line)

$\frac{41}{50}$	$\frac{41}{25}$	$\frac{38}{16}$	$\frac{39}{25}$	$\frac{32}{50}$		✓	
$\frac{53}{50}$	$\frac{59}{25}$	$\frac{65}{16}$	$\frac{73}{25}$	$\frac{81}{50}$		✓	
$\frac{68}{50}$	$\frac{74}{33}$	$\frac{78}{16}$	$\frac{80}{16}$	$\frac{81}{16}$	$\frac{93}{33}$	$\frac{105}{50}$	✓
$\frac{87}{50}$	$\frac{103}{33}$	$\frac{105}{16}$	$\frac{104}{16}$	$\frac{105}{16}$	$\frac{114}{33}$	$\frac{124}{50}$	✓
$\frac{12}{50}$	$\frac{14}{33}$	$\frac{23}{16}$	$\frac{23}{16}$	$\frac{20}{16}$	$\frac{25}{33}$	$\frac{33}{50}$	✓
$\frac{30}{50}$	$\frac{30}{33}$	$\frac{37}{16}$	$\frac{39}{16}$	$\frac{34}{16}$	$\frac{39}{33}$	$\frac{42}{50}$	✓
$\frac{38}{50}$	$\frac{39}{33}$	$\frac{43}{16}$	$\frac{46}{16}$	$\frac{48}{16}$	$\frac{53}{33}$	$\frac{50}{50}$	✓
$\frac{50}{50}$	$\frac{48}{33}$	$\frac{55}{16}$	$\frac{58}{16}$	$\frac{57}{16}$	$\frac{56}{33}$	$\frac{52}{50}$	✓
$\frac{57}{50}$	$\frac{57}{33}$	$\frac{58}{16}$	$\frac{60}{16}$	$\frac{58}{16}$	$\frac{57}{33}$	$\frac{54}{50}$	✓
$\frac{59}{50}$	$\frac{59}{33}$	$\frac{53}{16}$	$\frac{50}{16}$	$\frac{47}{16}$	$\frac{54}{33}$	$\frac{54}{50}$	✓
$\frac{55}{50}$	$\frac{51}{33}$	$\frac{41}{16}$	$\frac{57}{16}$	$\frac{57}{16}$	$\frac{50}{33}$	$\frac{54}{50}$	✓
$\frac{57}{50}$	$\frac{53}{33}$	$\frac{47}{16}$	$\frac{44}{16}$	$\frac{44}{16}$	$\frac{56}{33}$	$\frac{65}{50}$	✓

Station	+	H.I	-	Red	Elev.	
		716.73				
193+35				5.9	910.8	✓
+80				5.6	11.1	✓
194+00				5.1	11.6	✓
T.R	5.79	917.44 ✓	5.08		911.65	✓
194+50				8.0	09.4	✓
194+75				9.0	08.4	✓
195+00				8.4	09.0	✓
+49				5.7	11.7	✓
75				5.4	12.0	✓
196+00				7.0	10.4	✓
735				9.0	08.4	✓
770				7.2	10.2	✓
197+00				4.5	12.9	✓

Lt. E Rt.

$\frac{82}{50}$ $\frac{71}{33}$ $\frac{64}{16}$ 59 $\frac{57}{16}$ $\frac{65}{33}$ $\frac{70}{50}$ ✓

$\frac{68}{50}$ $\frac{63}{33}$ $\frac{57}{16}$ 56 $\frac{58}{16}$ $\frac{66}{33}$ $\frac{71}{50}$ ✓

$\frac{57}{50}$ $\frac{53}{33}$ $\frac{51}{16}$ 51 $\frac{52}{16}$ $\frac{57}{33}$ $\frac{57}{50}$ ✓

$\frac{70}{50}$ $\frac{86}{33}$ $\frac{80}{16}$ 80 $\frac{83}{16}$ $\frac{83}{33}$ $\frac{82}{50}$ ✓

$\frac{84}{50}$ $\frac{75}{33}$ $\frac{88}{16}$ 70 $\frac{73}{16}$ $\frac{77}{33}$ $\frac{76}{50}$ ✓

$\frac{89}{50}$ $\frac{85}{33}$ $\frac{83}{16}$ 84 $\frac{88}{16}$ $\frac{97}{33}$ $\frac{99}{50}$ ✓

$\frac{49}{50}$ $\frac{48}{33}$ $\frac{54}{16}$ 57 $\frac{62}{16}$ $\frac{75}{33}$ $\frac{76}{50}$ ✓

$\frac{42}{50}$ $\frac{43}{33}$ $\frac{48}{16}$ 54 $\frac{63}{16}$ $\frac{79}{33}$ $\frac{75}{50}$ ✓

$\frac{48}{50}$ $\frac{52}{33}$ $\frac{58}{16}$ 70 $\frac{80}{16}$ $\frac{81}{33}$ $\frac{89}{50}$ ✓

$\frac{64}{50}$ $\frac{74}{33}$ $\frac{82}{16}$ 70 $\frac{81}{16}$ $\frac{87}{33}$ $\frac{85}{50}$ ✓

$\frac{67}{50}$ $\frac{72}{33}$ $\frac{67}{16}$ 72 $\frac{70}{16}$ $\frac{75}{33}$ $\frac{72}{50}$ ✓

$\frac{51}{50}$ $\frac{47}{33}$ $\frac{44}{16}$ 45 $\frac{49}{16}$ $\frac{51}{33}$ $\frac{63}{50}$ ✓

Station	+	H.I	-	Rod	Elev.	
		917.46				
197+30				3.9	13.5	✓
197+65				5.6	11.8	✓
198+00				7.3	10.1	✓
198+47				8.5	8.9	✓
199+00				6.8	10.6	✓
750				4.5	12.9	✓
200+00				3.1	14.3	✓
T.P	390	919.33	2.01		915.43	✓
200+50				4.7	14.6	✓
201+00				5.3	14.0	✓
B.M	305	917.43	5.75		913.58 = 13.57	✓
201+36				4.6	12.8	✓
756				8.4	9.0	✓
202+00				8.9	8.5	✓

H. L. Rt.

$\frac{3.0}{50}$	$\frac{3.0}{33}$	$\frac{3.3}{16}$	3.9	$\frac{4.6}{16}$	$\frac{5.7}{33}$	$\frac{6.9}{50}$	✓
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$\frac{2.8}{50}$	$\frac{4.6}{33}$	$\frac{4.4}{16}$	5.6	$\frac{7.0}{16}$	$\frac{8.0}{33}$	$\frac{8.1}{50}$	✓
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$\frac{3.0}{50}$	$\frac{4.3}{33}$	$\frac{5.5}{16}$	7.3	$\frac{8.9}{16}$	$\frac{10.2}{33}$	$\frac{11.3}{50}$	✓
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$\frac{3.0}{50}$	$\frac{4.4}{33}$	$\frac{6.2}{16}$	8.5	$\frac{10.8}{16}$	$\frac{13.4}{33}$	$\frac{14.2}{50}$	✓
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$\frac{2.1}{50}$	$\frac{3.2}{33}$	$\frac{4.9}{16}$	6.8	$\frac{9.2}{16}$	$\frac{11.6}{33}$	$\frac{13.7}{50}$	✓
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$\frac{1.7}{50}$	$\frac{2.5}{33}$	$\frac{3.5}{16}$	5.5	$\frac{6.0}{16}$	$\frac{7.7}{33}$	$\frac{8.5}{50}$	✓
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$\frac{2.6}{50}$	$\frac{2.8}{33}$	$\frac{2.6}{16}$	3.1	$\frac{3.7}{16}$	$\frac{4.6}{33}$	$\frac{5.2}{50}$	✓
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Top stake 200

$\frac{7.4}{50}$	$\frac{6.8}{33}$	$\frac{5.6}{16}$	4.7	$\frac{4.1}{20}$	$\frac{10.6}{27}$	$\frac{10.5}{34}$	$\frac{10.5}{38}$	$\frac{10.2}{50}$	✓
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$\frac{8.2}{50}$	$\frac{7.4}{33}$	$\frac{6.5}{16}$	5.3	$\frac{5.0}{8}$	$\frac{8.1}{15}$	$\frac{9.6}{20}$	$\frac{9.5}{22}$	$\frac{7.6}{50}$	✓
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Spike in 12" oak 50' Rt Sta 202 + 50

$\frac{5.5}{50}$	$\frac{3.5}{33}$	$\frac{5.1}{16}$	4.6	$\frac{8.1}{6}$	$\frac{8.9}{11}$	$\frac{7.6}{27}$	$\frac{7.5}{47}$	$\frac{8.2}{50}$	✓
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$\frac{4.1}{50}$	$\frac{5.0}{33}$	$\frac{4.6}{16}$	4.7	2.4	$\frac{2.6}{4}$	$\frac{7.7}{7}$	$\frac{7.6}{23}$	$\frac{2.4}{41}$	$\frac{6.5}{50}$	✓
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$\frac{5.8}{50}$	$\frac{6.0}{33}$	$\frac{6.6}{22}$	$\frac{7.2}{12}$	$\frac{8.6}{9}$	8.9	$\frac{8.5}{16}$	$\frac{8.9}{35}$	$\frac{9.8}{40}$	$\frac{6.3}{44}$	$\frac{4.6}{50}$	✓
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Station	+	H.I	-	Rod	Elev.
		917.43 ✓			
202+50				9.6	907.8 ✓
203+00				10.1	07.3 ✓
+50				10.7	06.7 ✓
204+00				11.7	05.7 ✓
T.P.	7.47	912.71 ✓	11.19		906.24 ✓
+40				2.8	04.9 ✓
205+00				11.2	02.5 ✓
T.P.	3.74	906.24 ✓	10.61		903.10 ✓
205+50				6.7	900.1 ✓
206+00				9.1	897.7 ✓
+50				11.5	95.3 ✓
207+00					
T.P.	1.52	897.08 ✓	11.28		895.56 ✓
207+00				3.6	93.5 ✓
207+45				6.4	90.7 ✓

H. S. H.

$\frac{40}{50}$ $\frac{47}{53}$ $\frac{5.6}{14}$ $\frac{9.8}{14}$ $\frac{10.0}{9}$ $\frac{9.4}{5}$ 9.6 $\frac{9.4}{16}$ $\frac{10.0}{25}$ $\frac{10.2}{28}$ $\frac{9.2}{35}$ $\frac{6.4}{39}$ $\frac{5.0}{44}$ $\frac{5.0}{50}$ ✓

$\frac{4.0}{50}$ $\frac{4.1}{40}$ $\frac{4.1}{24}$ $\frac{10.0}{17}$ $\frac{10.8}{11}$ $\frac{12.0}{6}$ 10.1 $\frac{9.1}{16}$ $\frac{9.1}{21}$ $\frac{9.5}{25}$ $\frac{8.1}{36}$ $\frac{8.0}{50}$ ✓

$\frac{3.5}{50}$ $\frac{4.4}{35}$ $\frac{5.1}{25}$ $\frac{10.4}{19}$ $\frac{11.5}{12}$ $\frac{10.8}{7}$ 10.7 $\frac{11.2}{21}$ $\frac{11.8}{24}$ $\frac{11.1}{32}$ $\frac{7.9}{37}$ $\frac{5.9}{44}$ $\frac{5.9}{50}$ ✓

$\frac{3.5}{50}$ $\frac{4.4}{35}$ $\frac{4.7}{23}$ $\frac{11.7}{15}$ $\frac{12.1}{9}$ $\frac{11.6}{5}$ $\frac{11.7}{5}$ $\frac{11.9}{23}$ $\frac{12.5}{28}$ $\frac{12.1}{23}$ $\frac{9.5}{37}$ $\frac{8.5}{50}$ ✓

$\frac{1.1}{50}$ $\frac{1.7}{38}$ $\frac{3.0}{28}$ $\frac{5.6}{76}$ $\frac{8.7}{10}$ $\frac{9.5}{9}$ $\frac{9.1}{5}$ 8.8 $\frac{9.0}{27}$ $\frac{10.3}{32}$ $\frac{9.7}{37}$ $\frac{8.2}{40}$ $\frac{7.8}{50}$ ✓

$\frac{4.0}{50}$ $\frac{7.4}{37}$ $\frac{7.4}{29}$ $\frac{7.1}{12}$ $\frac{10.1}{5}$ $\frac{11.4}{3}$ 11.2 $\frac{10.6}{2}$ $\frac{10.8}{19}$ $\frac{11.2}{35}$ $\frac{13.2}{39}$ $\frac{13.3}{50}$ ✓

Top Sta ke 205
+2.0 0.6 2.6 4.7 6.7 6.8 5.4 5.8 10.0
= 908.8 3.7 2.9 1.5 5 8 4.1 5.0 ✓
 $\frac{50}{50}$

$\frac{10.5}{50}$ $\frac{0.5}{43}$ $\frac{5.0}{22}$ 9.1 $\frac{9.6}{12}$ $\frac{6.6}{21}$ $\frac{6.5}{50}$ ✓

$\frac{5.1}{50}$ $\frac{5.9}{32}$ $\frac{7.3}{76}$ $\frac{11.5}{76}$ $\frac{11.8}{19}$ $\frac{7.6}{27}$ $\frac{7.0}{50}$ ✓

$\frac{13.5}{28}$ $\frac{7.6}{41}$ $\frac{7.1}{50}$ ✓

$\frac{0.8}{50}$ $\frac{1.6}{45}$ $\frac{3.0}{24}$ $\frac{3.6}{5}$ $\frac{3.6}{5}$ $\frac{4.2}{12}$ ✓

$\frac{6.4}{50}$ $\frac{6.8}{35}$ $\frac{7.1}{19}$ 6.4 $\frac{5.4}{8}$ $\frac{4.1}{30}$ $\frac{2.3}{36}$ $\frac{1.8}{40}$ $\frac{4.2}{48}$ $\frac{4.7}{48}$ $\frac{4.7}{50}$ ✓

Station	+	H.I	-	Rod	Elev.
		892.08 ✓			
207+75				7.8	889.3 ✓
208+00				8.6	885 ✓
FROM R-21					
208+34				7.1	880 ✓
209+00				7.0	888.1 ✓
209+50				6.2	90.9 ✓
T.P.	6.07	900.71 ✓	2.44		894.64 ✓
210+00				6.8	93.9 ✓
4/0				5.1	95.6 ✓
770				5.4	95.3 ✓
211+00				7.5	93.2 ✓
722				9.2	91.5 ✓
T.P.	4.77	893.75 ✓	11.73		882.98 ✓
211+50				5.8	88.0 ✓
212+00				12.3	81.5 ✓

Station	+	H.I	-	Rod	Elev.
		893.75 ✓			
212+50				13.4	80.4 ✓
213+00				13.2	80.6 ✓
+50				13.1	80.7 ✓
214+00				12.9	80.9 ✓
214+50				11.6	82.2 ✓
T.P.	5.12	898.85 ✓	0.02		893.73 ✓
214+50					
+80					
215+00					
215+50					
+78					
B.M.	0.11	889.33 ✓	9.63		889.22 ✓
214+80				4.8	84.5 ✓
215+00				4.0	85.3 ✓

Lt. Q Rt.

$\frac{10.2}{50}$ $\frac{12.7}{30}$ 13.4 13.5 $\frac{13.5}{19}$ 13.5 $\frac{13.5}{50}$

✓

11.0 $\frac{12.6}{40}$ $\frac{13.7}{25}$ 13.2 $\frac{13.4}{25}$ 13.5 $\frac{13.5}{50}$

✓

10.3 $\frac{12.0}{40}$ $\frac{13.2}{55}$ 13.1 13.5 $\frac{13.5}{30}$ 13.6 $\frac{13.6}{50}$

✓

7.7 $\frac{9.2}{41}$ $\frac{11.5}{24}$ 12.9 13.2 $\frac{13.2}{25}$ 13.6 $\frac{13.6}{50}$

✓

cont'd $\frac{9.6}{16}$ 11.6 12.5 $\frac{12.8}{30}$ 12.7 $\frac{12.7}{50}$

✓

$\frac{3.1}{50}$ $\frac{4.1}{42}$ $\frac{6.9}{32}$

cont'd

✓

$\frac{1.9}{50}$ $\frac{4.6}{25}$ $\frac{7.8}{15}$ $\frac{12.0}{7}$

cont'd

✓

+11.8 +10.8 +8.7 +5.2
 $\frac{1.7}{50}$ $\frac{2.7}{36}$ $\frac{4.8}{24}$ $\frac{8.2}{73}$

cont'd

✓

+8.9 +8.0 +5.2 +1.8
 $\frac{4.1}{50}$ $\frac{5.0}{33}$ $\frac{7.8}{17}$ $\frac{11.2}{4}$

cont'd

✓

+5.6 +5.9 +4.7
 $\frac{9.6}{50}$ $\frac{4.3}{32}$ $\frac{10.5}{20}$

cont'd

✓

Spike in 24" Oak 60' Rt. Sta. 17707

4.8 $\frac{5.2}{6}$ $\frac{8.2}{20}$ $\frac{7.0}{50}$

✓

$\frac{4.0}{5}$ $\frac{6.2}{10}$ $\frac{8.4}{25}$ $\frac{2.9}{50}$

✓

Station	+	H. I	-	Rod	Elev.
		889.33	✓		
216750				3.5	85.8 ✓
215718				5.9	83.6 ✓
216700				7.0	82.3 ✓
734				8.9	80.4 ✓
760				9.3	80.0 ✓
780				6.1	83.2 ✓
217700				4.8	84.5 ✓
B.M.	7.58	798.78	✓		889.20 ✓
730				14.0	84.8 ✓
765				12.4	86.4 ✓
218700				9.3	89.5 ✓
740				5.2	83.6 ✓ 93.6 ✓
772				3.4	85.4 ✓ 75.4 ✓

H Q R+

contd $\frac{3.5}{7}$ $\frac{5.1}{26}$ $\frac{2.6}{26}$ $\frac{2.7}{50}$

✓

contd $\frac{3.8}{11}$ 5.7 $\frac{7.1}{14}$ $\frac{8.2}{19}$ $\frac{2.8}{50}$

✓

$\frac{4.0}{50}$ $\frac{5.4}{31}$ $\frac{6.4}{16}$ 7.0 $\frac{8.1}{25}$ $\frac{7.3}{50}$

✓

$\frac{6.8}{50}$ $\frac{7.7}{40}$ $\frac{8.4}{17}$ 8.9 $\frac{8.2}{20}$ $\frac{7.0}{50}$

✓

$\frac{8.3}{50}$ $\frac{8.2}{37}$ $\frac{9.0}{14}$ 9.3 $\frac{9.0}{7}$ $\frac{7.3}{17}$ $\frac{8.0}{26}$ $\frac{8.2}{50}$

✓

$\frac{8.0}{50}$ $\frac{2.1}{26}$ $\frac{6.2}{13}$ 6.1 $\frac{5.2}{9}$ $\frac{4.4}{22}$ $\frac{5.7}{35}$ $\frac{6.8}{50}$

✓

$\frac{7.8}{50}$ $\frac{8.6}{36}$ $\frac{7.3}{19}$ 4.8 $\frac{3.7}{8}$ $\frac{1.0}{28}$ $\frac{1.4}{42}$ $\frac{3.9}{50}$

✓

Spike in Oct At 17405

$\frac{18.7}{50}$ $\frac{16.3}{20}$ $\frac{14.0}{15}$ $\frac{11.8}{15}$ $\frac{9.5}{30}$ $\frac{6.6}{50}$

✓

$\frac{18.5}{50}$ $\frac{14.7}{23}$ $\frac{12.4}{14}$ $\frac{10.9}{14}$ $\frac{8.5}{28}$ $\frac{5.2}{50}$

✓

$\frac{7.8}{50}$ $\frac{7.4}{23}$ 9.0 $\frac{7.1}{28}$ $\frac{4.6}{50}$

✓

$\frac{4.4}{50}$ $\frac{4.0}{37}$ 5.2 $\frac{4.6}{23}$ $\frac{4.8}{50}$

✓

$\frac{5.1}{50}$ $\frac{3.0}{26}$ $\frac{3.4}{11}$ $\frac{5.0}{20}$ $\frac{6.2}{50}$

✓

Station	+	H.I	-	Rod	Elev.
		895.78 ✓			
219+00				56	93.2 ✓
	150			94	89.4 ✓
220+00				98	89.0 ✓
T.P.	2.69	898.68 ✓	8.79		899.99 ✓
	150			80	90.7 ✓
221+00				72	91.5 ✓
	135			68	91.9 ✓
221+65				52	93.5 ✓
222+00				07	98.0 ✓
T.P.	10.63	908.81 ✓	0.50		898.18 ✓
	100			90	899.8 ✓
222+65				95	99.3 ✓
223+00				36	900.2 ✓
	166			46	04.2 ✓

Lt. Rt.

$\frac{64}{50}$	$\frac{55}{70}$	56	$\frac{67}{73}$	$\frac{96}{50}$	✓
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$\frac{71}{50}$	$\frac{78}{30}$	$\frac{88}{74}$	$\frac{98}{70}$	$\frac{105}{38}$	$\frac{113}{80}$	✓
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$\frac{83}{50}$	$\frac{82}{34}$	$\frac{89}{76}$	98	$\frac{100}{15}$	$\frac{88}{33}$	$\frac{103}{50}$	✓
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Top stake 220

$\frac{107}{50}$	$\frac{95}{41}$	$\frac{87}{30}$	$\frac{74}{74}$	80	$\frac{83}{18}$	$\frac{85}{33}$	$\frac{94}{50}$	✓
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$\frac{110}{50}$	$\frac{105}{33}$	$\frac{89}{17}$	$\frac{72}{-}$	$\frac{60}{15}$	$\frac{59}{32}$	$\frac{83}{50}$	✓
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$\frac{74}{50}$	$\frac{87}{33}$	$\frac{75}{76}$	68	$\frac{66}{22}$	$\frac{50}{41}$	$\frac{94}{80}$	✓
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$\frac{57}{50}$	$\frac{55}{35}$	$\frac{46}{76}$	52	$\frac{57}{15}$	$\frac{67}{32}$	$\frac{88}{50}$	✓
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$\frac{95}{50}$	$\frac{93}{30}$	$\frac{91}{13}$	97	$\frac{24}{19}$	$\frac{37}{36}$	$\frac{52}{50}$	✓
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Nail in stake 224

$\frac{62}{50}$	$\frac{72}{33}$	$\frac{81}{76}$	80	$\frac{103}{17}$	$\frac{113}{34}$	$\frac{133}{50}$	✓
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$\frac{37}{50}$	$\frac{57}{31}$	$\frac{78}{13}$	85	$\frac{12}{76}$	$\frac{124}{33}$	$\frac{139}{50}$	✓
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$\frac{22}{50}$	$\frac{44}{81}$	$\frac{66}{74}$	86	$\frac{105}{76}$	$\frac{125}{30}$	$\frac{150}{50}$	✓
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$\frac{107}{50}$	$\frac{07}{38}$	$\frac{20}{27}$	$\frac{31}{76}$	46	$\frac{70}{15}$	$\frac{27}{33}$	$\frac{125}{50}$	✓
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Station	+	H.I	-	Rod	Elev.
		908.81 ✓			
224+00				6.1	902.7 ✓
T.P.	10.66	914.39 ✓	5.08		903.73 ✓
224+50				9.3	905.1 ✓
225+00				3.7	910.7 ✓
T.P.	10.59	922.32 ✓	2.66		911.73 ✓
+39				9.0	913.3 ✓
+60				5.5	916.8 ✓
T.P.	11.84	931.99 ✓	2.37		919.95 ✓
226+00				7.3	924.5 ✓
+33				3.0	928.8 ✓
+72				1.4	930.4 ✓
227+00				2.3	929.5 ✓
+50				5.4	936.4 ✓
228+00				11.3	920.5 ✓
T.P.	1.65	927.32 ✓	6.12		925.67 ✓
228+50				3.1	924.2 ✓

Lt.

A

Rt.

W.H.C.
FERGUSON
EdwinJan 14,
1925

$\frac{0.3}{50}$	$\frac{30}{30}$	$\frac{4.8}{75}$	$\frac{6.1}{61}$	$\frac{7.1}{76}$	$\frac{8.4}{33}$	$\frac{9.1}{50}$	✓
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Top Stake Sta. 22440.0

$\frac{3.6}{50}$	$\frac{5.1}{37}$	$\frac{7.6}{22}$	$\frac{9.3}{93}$	$\frac{10.3}{22}$	$\frac{8.7}{50}$		✓
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$\frac{0.7}{50}$		$\frac{7.3}{28}$	$\frac{3.7}{37}$	$\frac{4.0}{22}$	$\frac{4.5}{26}$	$\frac{3.8}{50}$	✓
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$\frac{5.4}{50}$	$\frac{6.4}{33}$	$\frac{7.5}{17}$	$\frac{9.0}{9.0}$	$\frac{10.7}{23}$	$\frac{11.4}{50}$		✓
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$\frac{1.6}{50}$	$\frac{2.4}{32}$	$\frac{3.5}{75}$	$\frac{5.5}{5.5}$	$\frac{7.7}{16}$	$\frac{9.5}{33}$	$\frac{10.6}{50}$	✓
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$\frac{4.5}{50}$	$\frac{5.0}{32}$	$\frac{5.6}{76}$	$\frac{7.3}{73}$	$\frac{10.4}{75}$	$\frac{13.4}{33}$	$\frac{15.3}{50}$	✓
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$\frac{2.4}{50}$	$\frac{1.4}{30}$	$\frac{1.9}{72}$	$\frac{3.0}{3.0}$	$\frac{5.6}{21}$	$\frac{7.2}{33}$	$\frac{8.9}{50}$	✓
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$\frac{1.7}{50}$	$\frac{1.3}{33}$	$\frac{1.1}{16}$	$\frac{1.4}{1.4}$	$\frac{2.7}{17}$	$\frac{5.5}{34}$	$\frac{7.1}{50}$	✓
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$\frac{2.5}{50}$	$\frac{3.1}{33}$	$\frac{2.7}{16}$	$\frac{2.3}{2.3}$	$\frac{3.0}{19}$	$\frac{5.1}{37}$	$\frac{6.4}{50}$	✓
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$\frac{5.0}{50}$	$\frac{2.0}{31}$	$\frac{6.5}{14}$	$\frac{5.4}{5.4}$	$\frac{4.2}{19}$	$\frac{4.1}{33}$	$\frac{4.1}{50}$	✓
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$\frac{9.9}{50}$	$\frac{10.4}{45}$	$\frac{11.6}{33}$	$\frac{11.7}{16}$	$\frac{11.3}{11.3}$	$\frac{12.5}{14}$	$\frac{7.4}{33}$	$\frac{9.6}{50}$	✓
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$\frac{9.0}{50}$	$\frac{9.4}{46}$	$\frac{4.3}{11}$	$\frac{3.0}{18}$	$\frac{3.1}{3.1}$	$\frac{5.7}{19}$	$\frac{8.9}{36}$	$\frac{11.3}{50}$	✓
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Station	+	H.I	-	Rod.	Elev.
		927.32 ✓			
228+75				3.5	23.8 ✓
229+00				7.0	20.3 ✓
T.P.	0.44	918.31 ✓	945		917.27 ✓
+32				2.7	15.6 ✓
+70				7.7	10.6 ✓
230+00					
T.P.	0.89	908.90 ✓	10.30		908.01 ✓
230+00 +				4.4	04.5 ✓
B.M.	3.87	904.74 ✓	8.03		900.87 ✓
230+30				6.9	897.8 ✓
230+50				11.5	893.2 ✓
230+73				13.6	91.1 ✓
231+00				11.8	92.9 ✓
+24				6.8	97.9 ✓
+65				5.2	99.5 ✓

Station		H.I	-	Rod	Elev.	
232+00		904.74 ✓		28	01.9 ✓	
T.P.	1.36	914.33 ✓	1.77		902.97 ✓	
232+14				11.6	02.7 ✓	
+1/2				54	08.9 ✓	
+75				14	12.9 ✓	
T.P.	4.71	916.71 ✓	2.33		912.00 ✓	
233+00				57	11.0 ✓	
+38				53	11.4 ✓	
+75				4.6	12.1 ✓	
234+00				7.4	09.3 ✓	
+25				9.3	07.4 ✓	
+72				9.7	07.0 ✓	
235+00				9.7	07.0 ✓	
T.P.	5.95	912.94 ✓	2.72		907.99 ✓	
234+25						

Lt. 8

Rt. W.H.O. Persons Jan. 16, 1935
Ealvin Nabony
+23
72.2
31
00
50 ✓

7.5 68 - 5.1 2.8 2.8
50 31 14 5

2.2 26
16

Top Stake 232

17.2 14.9 13.3 11.6 9.8
50 33 16

10.5 10.1 10.5 8 8.5 7.0
15 24 30 37 44 50 ✓

16.2 13.2 11.2 9.4 7.5
50 46 16

8.3 8.2 8.1 7.7 8.4
15 28 34 37 50 ✓

8.1 6.3 2.7 1.7 5.6
50 40 24

6.0 6.0 6.5 5.6 6.0
8 15 20 30 34 50 ✓

Top of Stake 233 to 0

7.9 2.9 2.2 5.7 7.2
50 26 7

6.7 6.7 7.0 5.0 5.4
10 17 23 28 32 50 ✓

6.2 5.6 1.3 1.1 5.3 5.3
50 37 23 15 7

5.6 3.7 5.0 7.4
10 12 23 50 ✓

10.3 2.7 3.8 4.8 4.6
50 41 21 15

6.5 9.2 13.7
14 30 50 ✓

2.8 2.7 5.4 5.0 7.4
50 37 21 11

9.5 13.0 15.3 19.8 21.5
11 25 36 41 50 ✓

9.6 7.3 5.6 5.1 8.0 9.3
50 34 16 16 6

4.2 4.2 5.9 5.9 7.2 9.7
50 47 43 21 11

5.4 5.2 7.1 8.0 7.7
50 38 21 11

-7.5 -12.8 -15.0
14.0 19.2 21.5
26 36 50 ✓

Station	+	H.I	-	Rod	Elev.
234+72		913.94 ✓			
235+00					
+34				7.9	906.0 ✓
+48				10.0	903.9 ✓
+70					
236+00					
T.P.	0.50	903.16 ✓	11.28		902.66 ✓
235+34					
235+48					
235+70				7.8	895.4 ✓
236				10.7	91.4 S.B. 92.5 ✓
+50					85.3 S.B. 91.6 ✓
237+00					91.8 ✓ 89.4 S.B.

Lt. 8

Rt.

$$\begin{array}{r} -5.4 \quad -12.0 \quad -14.9 \\ 12.3 \quad 18.9 \quad 21.8 \\ \hline 17 \quad 31 \quad 50 \end{array}$$

✓

$$\begin{array}{r} -2.3 \quad -4.6 \quad -6.2 \quad -10.4 \quad -13.8 \\ 24 \quad 120 \quad 138 \quad 180 \quad 214 \\ \hline 12 \quad 19 \quad 23 \quad 36 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 28 \quad 33 \quad 33 \quad 29 \quad 46 \quad 79 \quad 13.8 \\ 50 \quad 42 \quad 38 \quad 28 \quad 6 \quad 7 \quad 18 \end{array}$$

✓

$$\begin{array}{r} 3.4 \quad 2.0 \quad 3.8 \quad 10.0 \quad 12.0 \\ 50 \quad 45 \quad 23 \quad 8 \end{array}$$

✓

$$\begin{array}{r} +14.2 \quad +12.4 \quad +7.1 \\ 44 \quad 63 \quad 11.5 \\ \hline 50 \quad 35 \quad 17 \end{array}$$

$$\begin{array}{r} 7.5 \quad 13.0 \\ 50 \quad 37 \end{array}$$

$$\begin{array}{r} -9.4 \quad -12.9 \quad -14.2 \\ 6.5 \quad 10.0 \quad 11.3 \\ \hline 23 \quad 38 \quad 50 \end{array}$$

✓

$$\begin{array}{r} -7.8 \quad -10.8 \quad -12.1 \\ 7.0 \quad 10.0 \quad 11.5 \\ \hline 15 \quad 33 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 5.7 \quad 7.8 \quad 9.2 \quad 10.4 \quad 11.3 \\ 11 \quad - \quad 9 \quad 16 \quad 50 \end{array}$$

Top
to ✓

$$\begin{array}{r} 6.5 \quad 2.8 \quad 11.9 \\ 35 \quad 20 \quad 107 \end{array}$$

$$\begin{array}{r} 11 \quad 13.6 \quad 16 \\ 20 \quad 20 \quad 50 \quad 50 \end{array}$$

$$\begin{array}{r} 9.1 \quad 11.0 \quad 12.6 \quad 17.9 \quad 19.8 \quad 19.6 \\ 50 \quad 24 \quad 25 \quad 50 \quad 25 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 10.1 \quad 10.6 \quad 11.0 \quad 12.4 \quad 13.8 \quad 18.6 \quad 19.1 \\ 50 \quad 45 \quad 33 \quad 25 \quad 50 \quad 25 \quad 50 \end{array}$$

✓

station	+	H.I	-	Rod	Elev.
237+50		903.16 ✓		9.8	893.4 ✓
+75				4.6	98.6 ✓
238+00				0.7	902.5 ✓
T.P.	11.42	914.57 ✓	0.01		903.15 ✓
+50				5.7	08.9 ✓
+74				3.7	10.9 ✓
T.P.	11.17	924.48 ✓	1.26		913.31 ✓
239+00				7.8	16.7 ✓
+32				2.6	21.9 ✓
T.P.	2.80	932.53 ✓	0.75		923.73 ✓
+70				10.4	22.1 ✓
240+00				8.7	23.8 ✓
+30				9.9	23.6 ✓
+72				11.7	20.8 ✓
241+00				10.3	22.2 21.2 ✓

station	+	H.I	-	Rbd	Elev.	
		732.53	✓			
241+28				7.5	923.0	✓
154				7.4	25.1	✓
B.M.	9.24	734.73	✓	7.04	925.49	✓
242+00				12.0	22.7	✓
723				14.0	20.7	✓
150				13.4	21.3	✓
243+00				3.1	31.6	✓
T.P.	11.37	743.82	✓	2.28	932.45	✓
+4/2				4.6	39.2	✓
244+00				4.1	39.4	✓
727				6.1	37.7	✓
170				12.3	31.5	✓
T.P.	6.30	939.55	✓	10.57	933.25	✓
245+00				9.5	30.0	✓
246+00				9.7	29.9	✓

Lt. R Pt.

$\frac{84}{50}$	$\frac{28}{36}$	$\frac{20}{16}$	$\frac{10.0}{8}$	95	$\frac{112}{12}$	$\frac{10.6}{18}$	$\frac{14.8}{41}$	$\frac{17.3}{50}$ ✓
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$\frac{70}{50}$	$\frac{78}{19}$	$\frac{91}{5}$	74	$\frac{73}{7}$	$\frac{79}{28}$	$\frac{146}{50}$ ✓
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Spike in 20" Oak 50' Lt sta 24/195

$\frac{94}{50}$	$\frac{26}{45}$	$\frac{8.6}{35}$	$\frac{10.7}{25}$	$\frac{11.3}{74}$	120	$\frac{18.0}{12}$	$\frac{14.3}{50}$ ✓
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$\frac{72}{50}$	$\frac{85}{37}$	$\frac{12.3}{29}$	$\frac{13.0}{20}$	$\frac{140}{20}$	$\frac{14.7}{25}$	$\frac{15.3}{50}$ ✓
-----------------	-----------------	-------------------	-------------------	------------------	-------------------	---------------------

$\frac{5.0}{50}$	$\frac{87}{39}$	$\frac{11.3}{23}$	134	$\frac{14.3}{23}$	$\frac{15.3}{50}$ ✓
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$\frac{19}{50}$	$\frac{46}{73.5}$	$\frac{14}{40}$	31	$\frac{56}{24}$	$\frac{7.7}{38}$	$\frac{7.0}{50}$ ✓
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$\frac{8.5}{50}$	$\frac{2.0}{44}$	$\frac{4.2}{36}$	$\frac{4.3}{17}$	46	$\frac{5.7}{20}$	$\frac{7.6}{50}$ ✓
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$\frac{79}{50}$	$\frac{84}{43}$	$\frac{6.8}{30}$	$\frac{5.7}{20}$	44	$\frac{3.7}{22}$	$\frac{3.7}{50}$ ✓
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$\frac{83}{50}$	$\frac{83}{47}$	$\frac{7.1}{43}$	$\frac{6.4}{18}$	61	$\frac{5.3}{25}$	$\frac{5.1}{50}$ ✓
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$\frac{10.5}{50}$	$\frac{11.8}{20}$	120	$\frac{13.0}{22}$	$\frac{13.1}{50}$ ✓
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March

$\frac{97}{50}$	$\frac{9.7}{25}$	95	$\frac{9.7}{25}$	$\frac{9.8}{50}$ ✓
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$\frac{77}{50}$	$\frac{94}{39}$	$\frac{9.7}{25}$	97	$\frac{9.7}{25}$	$\frac{9.7}{50}$ ✓
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Station	+	H.I	-	Rod	Elev.	
246+58		939.55 ✓		9.0	930.6	✓
247+00				6.4	33.2	✓
+40				4.0	35.6	✓
170				4.5	35.1	✓
248+00				2.7	36.9	✓
T.P.	10.15	947.54 ✓	2.16		937.39	✓
+50				8.9	38.6	✓
249+00				6.1	41.4	✓
+54				2.9	44.6	✓
250+00				4.5	43.0	✓
T.P.	1.91	945.43 ✓	4.02		943.52	✓
+50				4.8	40.6	✓
251+00				7.1	38.3	✓
+50				10.7	34.7	✓

Lt. E Pt.

$\frac{50}{50}$ $\frac{6.2}{35}$ $\frac{7.7}{17}$ 9.0 9.7 9.8 ✓

$\frac{4.7}{50}$ $\frac{4.6}{30}$ $\frac{5.4}{16}$ 6.4 6.9 9.6 ✓

$\frac{5.8}{50}$ $\frac{5.2}{11}$ $\frac{4.3}{6}$ 4.0 4.6 5.8 6.5 6.7 ✓

$\frac{6.1}{50}$ 5.0 4.8 3.5 3.1 4.2 4.5 ✓

$\frac{6.1}{50}$ $\frac{5.5}{43}$ $\frac{3.9}{23}$ 2.7 0.9 0.2 4.0 ✓

$\frac{16.2}{50}$ $\frac{12.6}{33}$ $\frac{10.5}{17}$ 8.9 6.0 4.8 6.5 ✓

$\frac{15.3}{50}$ $\frac{10.3}{25}$ $\frac{7.2}{18}$ 6.1 5.4 5.2 5.8 4.9 ✓

$\frac{10.2}{50}$ $\frac{7.5}{37}$ $\frac{5.0}{19}$ 2.9 2.0 2.2 3.6 3.3 3.9 ✓

$\frac{12.6}{50}$ $\frac{8.6}{25}$ $\frac{5.8}{12}$ 4.5 3.8 3.5 4.5 3.8 ✓

Top Hat 740

$\frac{13.8}{50}$ $\frac{10.5}{30}$ $\frac{7.5}{14}$ 4.8 2.8 3.3 3.5 ✓

$\frac{14.3}{50}$ $\frac{11.4}{33}$ $\frac{8.9}{16}$ 7.1 1.3 7.3 11 ✓

$\frac{16.3}{50}$ $\frac{12.0}{17}$ 10.7 7.7 3.3 ✓

Station	f	H.I	-	Rod	Elev.
		945.43 ✓			
T.P. 252+00	7.54	944.26 ✓	11.71	8.2	933.72 ✓ 33.1 ✓
+50				6.0	35.3 ✓
253+00				3.7	37.6 ✓
T.P.	6.68	944.85 ✓	3.09		938.17 ✓
+30				6.5	38.4 ✓
+60				5.5	39.4 ✓
254+00				5.2	39.7 ✓
+50				6.6	38.3 ✓
B.M.	3.90	944.85	3.90		940.95 ✓
255+00				2.0	36.9 ✓
T.P.	0.40	936.73 ✓	8.52		936.33 ✓
+50				5.1	31.6 ✓
256+00				10.8	25.9 ✓
T.P.	1.29	928.20 ✓	7.82		926.91 ✓
+30				5.4	22.8 ✓
+51				7.5	20.7 ✓

Lt R RT

W.H.C.
Persons
Galvin
Mahoney
Jan. 17,
1925

Top Stake Sta 252+00
123 103 71 82 5.6 3.3 1.5 ✓
50 34 16

94 78 70 60 4.2 2.0 .00 ✓
50 36 16 15 31 50

84 65 47 3.7 1.8 1.4 7.04 7.07 ✓
50 36 16 76 31 94.7 78.3
35 54

12.0 87 74 6.5 6.9 5.9 2.9 3.2 ✓
50 32 17 7 10 26 50

85 85 86 79 6.0 5.8 4.8 3.4 3.8 ✓
50 48 43 75 78 22 40 50

73 62 54 5.2 5.6 6.6 5.9 ✓
50 37 20 20 38 50

85 79 74 6.6 6.6 6.8 7.1 ✓
50 35 19 79 35 50

spike in 15" Oak 40' pt. 254+85

86 87 86 8.0 7.3 6.6 5.8 ✓
50 41 24 16 30 50

54 5.3 54 5.1 5.0 4.1 3.0 ✓
50 32 15 14 30 50

11.9 11.2 11.3 10.8 10.4 12.0 9.6 ✓
50 33 20 16 30 50

Top Stake 256+00

70 64 55 5.4 5.0 4.5 3.4 ✓
50 34 18 76 32 50

86 72 68 7.5 5.1 4.0 ✓
50 25 14 22 50

Station	+	H.I	-	Rod	Elev.	
		928.20 ✓				
256+76				6.0	922.2	✓
+93				7.1	21.1	✓
257+00				10.5	17.7	✓
+114				12.2	16.0	✓
T.P.	0.45	919.44 ✓	9.21		918.99	✓
+50				5.8	13.6	✓
258+00				6.4	13.0	✓
+80				6.1	13.3	✓
<u>SEE R-38</u>						
259+00				5.0	14.4	✓
+40				4.1	15.3	✓
T.P.	7.40	926.42 ✓	0.42		919.02	✓
+70				9.2	17.2	✓
260+00				7.0	18.4	✓
+40				5.0	21.4	✓

Lt. Q Rt

~~$\frac{7.4}{50}$ $\frac{7.6}{35}$ $\frac{6.1}{18}$ 6.9 $\frac{5.4}{17}$ $\frac{5.5}{34}$ $\frac{6.2}{50}$ ✓~~

~~$\frac{7.9}{50}$ $\frac{6.9}{20}$ 7.1 $\frac{7.6}{10}$ $\frac{8}{29}$ $\frac{7.0}{50}$ ✓~~

~~$\frac{6.0}{50}$ $\frac{7.8}{25}$ 10.5 $\frac{10.0}{8}$ $\frac{7.6}{24}$ $\frac{7.2}{50}$ ✓~~

~~$\frac{9.0}{50}$ $\frac{12.4}{36}$ $\frac{12.1}{17}$ $\frac{12.2}{1}$ $\frac{11.0}{18}$ $\frac{9.8}{35}$ $\frac{8.1}{50}$ ✓~~

~~$\frac{6.0}{50}$ $\frac{6.3}{53}$ $\frac{6.1}{16}$ 5.8 $\frac{5.5}{17}$ $\frac{4.7}{33}$ $\frac{3.3}{50}$ ✓~~

~~$\frac{5.7}{50}$ $\frac{6.1}{44}$ $\frac{6.6}{16}$ 6.4 $\frac{6.6}{17}$ $\frac{6.1}{33}$ $\frac{5.0}{50}$ ✓~~

~~$\frac{4.3}{50}$ $\frac{4.8}{38}$ $\frac{5.5}{17}$ 6.1 $\frac{5.8}{16}$ $\frac{5.0}{34}$ $\frac{4.2}{50}$ ✓~~

~~$\frac{6.8}{50}$ $\frac{5.9}{33}$ $\frac{5}{15}$ 5.0 $\frac{7}{16}$ $\frac{8.3}{50}$ ✓~~

~~$\frac{7.8}{50}$ $\frac{5.9}{33}$ $\frac{4.4}{18}$ 4.1 $\frac{5.0}{15}$ $\frac{2.5}{27}$ $\frac{4.4}{50}$ ✓~~

Top Stake 60

~~$\frac{15.6}{50}$ $\frac{12.1}{31}$ $\frac{10.4}{16}$ 9.0 $\frac{6.6}{17}$ $\frac{7.1}{30}$ $\frac{5.9}{50}$ ✓~~

~~$\frac{16.2}{50}$ $\frac{7.1}{29}$ $\frac{7.2}{15}$ 8.0 $\frac{7.0}{17}$ $\frac{5.3}{32}$ $\frac{4.0}{50}$~~

~~$\frac{15.2}{50}$ $\frac{11.7}{38}$ $\frac{6.9}{15}$ 5.0 $\frac{3.1}{17}$ $\frac{0.6}{35}$ $\frac{10.9}{50}$ ✓~~

Station	+	H.I	-	Rod	Elev.
		926.42 ✓			
260+77				2.0	24.4 ✓
261+60				2.5	23.9 ✓
T.P.	0.30	925.33 ✓	1.29		925.03 ✓
+50				2.8	21.5 ✓
262+60				6.1	19.2 ✓
+55				11.4	13.9 ✓
T.P.	4.74	918.68 ✓	11.39		913.94 ✓
263+00				8.9	09.8 ✓
+55				10.5	08.2 ✓
264+00				6.6	12.1 ✓
+17				6.0	12.7 ✓
+40				7.5	11.2 ✓
+75					
T.P.	1.56	908.41 ✓	11.83		906.85 ✓
264+75				31	05.3 ✓

Lt.

±

Rt

$\frac{11.8}{50}$	$\frac{89}{34}$	$\frac{53}{18}$	20	$\frac{07}{9}$	$\frac{+2.7}{929.1}$	$\frac{44.8}{931.2}$	✓
					$\frac{34}{50}$		

$\frac{13.5}{50}$	$\frac{81}{25}$	$\frac{81}{25}$	2.5	$\frac{114}{927.8}$	$\frac{15.1}{936.5}$		✓
				$\frac{23}{50}$			

$\frac{12.7}{50}$	$\frac{86}{31}$	$\frac{57}{15}$	3.8	$\frac{21}{18}$	$\frac{0.7}{29}$	$\frac{+11}{926.4}$	✓
						$\frac{50}{50}$	

$\frac{14.7}{50}$	$\frac{12.6}{33}$	$\frac{10.5}{18}$	6.1	$\frac{2.9}{18}$	$\frac{0.9}{30}$	$\frac{+3.2}{928.5}$	✓
						$\frac{50}{50}$	

$\frac{14.0}{50}$	$\frac{16.3}{39}$	$\frac{14.0}{16}$	$\frac{11.4}{15}$	$\frac{8.1}{15}$	$\frac{3.8}{34}$	$\frac{10}{50}$	✓
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$\frac{17.5}{50}$	$\frac{13.4}{31}$	$\frac{10.5}{8}$	2.9	$\frac{5.5}{16}$	$\frac{2.6}{34}$	$\frac{0.8}{50}$	✓
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$\frac{14.6}{50}$	$\frac{13.7}{23}$	$\frac{10.5}{23}$	10.5	$\frac{6.5}{27}$	$\frac{5.4}{50}$		✓
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$\frac{15.6}{50}$	$\frac{12.8}{30}$	$\frac{12.8}{30}$	6.6	$\frac{2.7}{27}$	$\frac{1.1}{50}$		✓
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$\frac{15.2}{50}$	$\frac{2.3}{30}$	$\frac{9.7}{17}$	6.0	$\frac{2.2}{27}$	$\frac{0.6}{50}$		✓
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$\frac{15.7}{50}$	$\frac{13.4}{32}$	$\frac{10.4}{16}$	7.5	$\frac{4.0}{23}$	$\frac{1.9}{39}$	$\frac{1.1}{50}$	✓
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$\frac{+3.7}{1.7}$	$\frac{+6.6}{6.8}$		
$\frac{2.1}{50}$	$\frac{50}{50}$		✓

$\frac{9.0}{50}$	$\frac{6.2}{33}$	$\frac{4.1}{15}$	3.1				✓
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Station	+	H.I	-	Rod	Elev.
		908.41 ✓			
265+00				6.5	901.9 ✓
T.P.	4.38	901.70 ✓	11.09		897.32 ✓
+10				6.1	95.6 ✓
266+00				4.3	97.4 ✓
+38				1.0	00.7 ✓
+60					
B.M.	10.25	<u>corr.</u> 906.17 ✓	5.81		895.89 ✓
266+38					895.92 ✓
+60				4.7	901.5 ✓
+83				7.1	899.1 ✓
T.P.	4.99	901.55 ✓	9.61		896.56 ✓
267+00				5.8	95.8 ✓
+10				8.1	93.5 ✓
+15				12.0	89.6 ✓
+23				7.7	93.9 ✓

Station	+	H.I	-	Rod	Elev
		901.55 ✓			
267+42				4.2	897.4 ✓
267+60					
T.P.	11.94	912.86 ✓	0.63		900.92 ✓
267+42					
267+60				5.4	907.5 ✓
T.P.	10.36	922.36 ✓	0.86		912.00 ✓
T.P.	4.64	922.45 ✓	4.55		917.81 ✓
267+60					
267+72				5.7	16.8 ✓
267+84				5.6	16.9 ✓
+92				5.2	17.3 ✓
268+00				5.4	17.1 ✓
114				13.0	08.9 09.5 ✓
T.P.	182	912.57 ✓	11.70		910.75 ✓
268+14					
T.P.	1.34	902.62 ✓	11.29		901.28 ✓

Lt.

R

Rt.

4.2

5.1
30

5.2
30

✓

1.7
50

✓

16.3
7.2
50

✓

5.4

✓

Top Stake 26800

6.0
50

✓

5.8
50

5.7

2.12
30

✓

5.5
50

5.6

2.5
30

✓

6.8
50

2.5

5.2
30

✓

11.8
50

4.4

2.8
30

✓

13.0

6.1
30

✓

13.0
50

✓

station	+	H.I	-	Rod	Elev.
		902.62 ✓			
268+30				6.9	895.7 ✓
+40				11.6	91.0 ✓
+50				14.3	88.3 ✓
+75				14.3	88.3 ✓
T.P.	0.65	891.72 ✓	11.55		891.07 ✓
269+00				4.8	86.9 ✓
+30				4.8	86.9 ✓
+67				8.5	83.2 ✓
270+00				8.6	83.1 ✓
+50				8.7	83.0 ✓
271+00				5.7	86.0 ✓
+25				5.0	86.7 ✓
+50				7.1	84.6 ✓

Lt.

R

Rt.

$$\frac{14.0}{50}$$

$$69$$

$$\frac{0.0}{50}$$

✓

$$\frac{15.3}{50}$$

$$\frac{116}{50}$$

$$\frac{3.8}{50}$$

✓

$$\frac{16.2}{50}$$

$$14.3$$

$$\frac{10.6}{50}$$

✓

$$\frac{17.6}{50}$$

$$\frac{16.6}{58}$$

$$14.3$$

$$\frac{14.1}{19}$$

$$\frac{12.2}{27}$$

$$\frac{12.0}{50}$$

✓

Nail in F.R. H. 768+80

$$\frac{7.6}{50}$$

$$\frac{6.1}{33}$$

$$48$$

$$\frac{3.0}{28}$$

$$\frac{1.1}{50}$$

✓

$$\frac{8.3}{50}$$

$$\frac{7.0}{32}$$

$$\frac{6.2}{17}$$

$$4.8$$

$$\frac{4.7}{33}$$

$$\frac{3.7}{50}$$

✓

$$\frac{8.7}{50}$$

$$\frac{8.8}{33}$$

$$8.5$$

$$\frac{7.4}{23}$$

$$\frac{6.2}{42}$$

$$\frac{6.2}{50}$$

✓

$$\frac{8.9}{50}$$

$$\frac{8.8}{33}$$

$$\frac{8.8}{16}$$

$$8.6$$

$$\frac{8.7}{33}$$

$$\frac{8.4}{50}$$

✓

$$\frac{8.9}{50}$$

$$\frac{8.9}{33}$$

$$8.7$$

$$\frac{8.4}{33}$$

$$\frac{8.9}{50}$$

✓

$$\frac{7.2}{50}$$

$$\frac{6.7}{33}$$

$$5.7$$

$$\frac{4.5}{33}$$

$$\frac{4.9}{50}$$

✓

$$\frac{7.8}{50}$$

$$\frac{7.3}{42}$$

$$\frac{6.6}{26}$$

$$5.0$$

$$\frac{5.1}{24}$$

$$\frac{6.5}{50}$$

✓

$$\frac{9.2}{50}$$

$$\frac{8.2}{37}$$

$$\frac{7.4}{17}$$

$$21$$

$$\frac{7.4}{23}$$

$$\frac{8.7}{50}$$

✓

Station	+	H.I	-	Rod	Elev.
		891.72 ✓			
271+77				9.2	882.5 ✓
272+00				9.5	82.2 ✓
+50				8.5	83.2 ✓
273+00				4.8	86.9 ✓
T.P.	11.99	899.79 ✓	3.92		887.80 ✓
+30				9.8	90.0 ✓
+70				8.7	91.6 ✓
274+00				7.0	92.8 ✓
+30				6.1	93.7 ✓
+57				7.3	92.5 ✓
T.P.	0.22	892.58 ✓	7.43		892.36 ✓
275+00				6.2	86.4 ✓
+40				10.9	81.7 ✓
276+00				13.5	79.1 ✓ 89.1

Lt. L Rt.

$\frac{9.5}{50}$	$\frac{9.5}{33}$	92	$\frac{9.5}{33}$	$\frac{9.6}{50}$	✓
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$\frac{9.3}{50}$	$\frac{9.1}{33}$	95	$\frac{9.1}{33}$	$\frac{9.4}{50}$	✓
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$\frac{5.1}{50}$	$\frac{6.8}{27}$	85	$\frac{9.7}{33}$	$\frac{9.9}{50}$	✓
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$\frac{70.7}{892.4}$	$\frac{2.0}{22}$	48	$\frac{7.0}{15}$	$\frac{7.2}{36}$	$\frac{7.5}{50}$	✓
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top stake 273

$\frac{5.4}{50}$	$\frac{7.9}{33}$	98	$\frac{12.2}{27}$	$\frac{13.2}{50}$	✓
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$\frac{4.9}{50}$	$\frac{7.8}{33}$	$\frac{5.7}{16}$	82	$\frac{6.8}{16}$	$\frac{5.5}{33}$	$\frac{5.4}{50}$	✓
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$\frac{2.8}{50}$	$\frac{6.2}{26}$	$\frac{7.0}{13}$	70	$\frac{5.7}{20}$	$\frac{3.6}{36}$	$\frac{2.3}{50}$	✓
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$\frac{2.3}{50}$	$\frac{3.5}{30}$	$\frac{4.7}{17}$	61	$\frac{5.7}{18}$	$\frac{4.5}{38}$	$\frac{4.0}{50}$	✓
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$\frac{6.2}{50}$	$\frac{6.6}{23}$	73	$\frac{7.0}{20}$	$\frac{6.5}{34}$	$\frac{5.9}{50}$	✓
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Top stake 278400

$\frac{7.0}{50}$	$\frac{7.0}{37}$	$\frac{6.3}{18}$	62	$\frac{5.1}{24}$	$\frac{4.7}{38}$	$\frac{4.7}{50}$	✓
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$\frac{11.0}{50}$	$\frac{11.1}{24}$	$\frac{10.9}{15}$	10.9	$\frac{10.6}{20}$	$\frac{10.7}{37}$	$\frac{10.5}{50}$	✓
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$\frac{13.5}{50}$	$\frac{13.4}{35}$	13.5	$\frac{13.5}{26}$	$\frac{13.3}{50}$	✓
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station	+	H.I	-	rod	Elev.
		893.58			
276+54				13.0	79.6 ✓
277+00				10.6	82.0 ✓
145				7.0	85.6 ✓
T.P.	6.73	899.09 ✓	0.22		892.36 ✓
278+00				7.6	91.5 ✓
+45				3.7	95.4 ✓
+70				2.6	96.5 ✓
279+00				3.1	96.0 ✓
+27				6.0	93.1 ✓
T.P.	1.36	889.10 ✓	11.35		887.74 ✓
+60				1.5	87.6 ✓
280+00				6.9	83.2 ✓
+50				10.1	79.0 ✓
281+00				11.4	77.7 ✓

Lt.

Z

Rt.

$$\frac{13.5}{50}$$

$$\frac{13.1}{33}$$

$$\frac{13.0}{0}$$

$$\frac{13.5}{28}$$

$$\frac{13.4}{50} \checkmark$$

$$\frac{10.4}{50}$$

$$\frac{10.7}{25}$$

$$10.6$$

$$\frac{12.3}{30}$$

$$\frac{12.6}{50} \checkmark$$

$$\frac{7.5}{50}$$

$$\frac{7.2}{29}$$

$$7.0$$

$$\frac{9.1}{25}$$

$$\frac{10.8}{50} \checkmark$$

$$\frac{8.1}{50}$$

$$\frac{6.7}{23}$$

$$7.6$$

$$\frac{7.6}{21}$$

$$\frac{12.0}{50} \checkmark$$

$$\frac{2.3}{50}$$

$$\frac{2.9}{29}$$

$$\frac{3.7}{}$$

$$\frac{4.1}{7.4}$$

$$\frac{5.7}{33} \frac{7.8}{50} \checkmark$$

$$\frac{1.3}{50}$$

$$\frac{1.7}{31}$$

$$2.5$$

$$\frac{3.7}{31}$$

$$\frac{6.0}{37} \frac{8.0}{50} \checkmark$$

$$\frac{2.6}{50}$$

$$\frac{2.4}{27}$$

$$3.1$$

$$\frac{2.8}{7.4}$$

$$\frac{5.3}{30} \frac{10.4}{50} \checkmark$$

$$\frac{6.1}{50}$$

$$\frac{7.8}{28}$$

$$\frac{6.0}{}$$

$$\frac{8.5}{33}$$

$$\frac{12.3}{50} \checkmark$$

$$\frac{1.5}{50}$$

$$\frac{1.9}{20}$$

$$1.5$$

$$\frac{2.8}{25}$$

$$\frac{4.3}{40} \frac{5.9}{50} \checkmark$$

$$\frac{6.5}{50}$$

$$\frac{6.9}{25}$$

$$6.9$$

$$\frac{7.2}{25}$$

$$\frac{8.9}{50} \checkmark$$

$$\frac{9.3}{50}$$

$$\frac{9.8}{30}$$

$$\frac{10.1}{}$$

$$\frac{10.8}{28}$$

$$\frac{10.8}{50} \checkmark$$

$$\frac{10.4}{50}$$

$$\frac{10.9}{27}$$

$$\frac{11.4}{}$$

$$\frac{11.6}{28}$$

$$\frac{12.1}{50} \checkmark$$

Station	+	H.I	-	Rod	Elv.
		214.10 ✓			
282+00				1.6	877.5 ✓
T.P.	3.80	886.15 ✓	6.75		883.35 ✓
283+00				9.4	76.7 ✓
F.M.	3.72	^{corrected} 886.17 ✓	3.72		882.43 ✓
284+00				9.5	76.7 ✓
X Sec. 216 h 284+27					
285+00				9.0	76.9 ✓
286+00				2.2	78.0 ✓
287+00				7.3	78.9 ✓
T.P.	9.44	889.14 ✓	6.47		889.70 ✓
+63				7.8	81.3 ✓
288+00				7.2	81.9 ✓
+35				8.1	81.0 ✓
+70				9.9	79.2 ✓
T.P.	4.42	883.95 ✓	9.61		877.53 ✓
289+00				5.2	78.8 ✓

Station	+	H.I	-	Rod Elev.	
		883.95 ✓			
289+50				6.2	77.8 ✓
290+00				6.0	78.0 ✓
+50				6.3	77.7 ✓
291+00				6.2	77.8 ✓
+41				6.1	77.9 ✓
292+00				6.4	77.6 ✓
+50				6.7	77.3 ✓
293+00				6.8	77.3 ✓
+50				6.6	77.4 ✓
294+00				6.5	77.5 ✓
+50				4.9	79.1 ✓
B.M.	4.00	886.66 ✓	1.29		882.66 ✓
295+00				5.1	81.0 ✓

Lt.

E

Rt.

$\frac{2.7}{50}$	$\frac{4.5}{30}$	$\frac{5.9}{19}$	6.2	$\frac{6.4}{22}$	$\frac{6.7}{50}$	✓
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$\frac{3.0}{50}$	$\frac{4.7}{30}$	$\frac{5.6}{24}$	6.0	$\frac{6.9}{25}$	$\frac{6.9}{50}$	✓
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$\frac{4.2}{50}$	$\frac{5.1}{33}$	$\frac{5.8}{19}$	6.3	$\frac{6.8}{23}$	$\frac{6.9}{50}$	✓
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$\frac{4.9}{50}$	$\frac{5.5}{25}$		6.2	$\frac{6.5}{28}$	$\frac{6.8}{50}$	✓
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$\frac{5.1}{50}$	$\frac{6.0}{27}$		6.1	$\frac{7.0}{28}$	$\frac{7.0}{50}$	✓
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$\frac{5.9}{50}$	$\frac{6.2}{29}$		6.4	$\frac{6.9}{28}$	$\frac{7.2}{50}$	✓
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$\frac{6.3}{50}$	$\frac{6.5}{33}$		6.7	$\frac{7.2}{29}$	$\frac{7.0}{50}$	✓
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$\frac{6.0}{50}$	$\frac{6.9}{30}$		6.8	$\frac{7.2}{24}$	$\frac{7.5}{50}$	✓
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$\frac{6.3}{50}$	$\frac{6.6}{33}$		6.6	$\frac{7.2}{30}$	$\frac{7.3}{50}$	✓
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$\frac{5.7}{50}$	$\frac{6.2}{28}$		6.5	$\frac{6.9}{26}$	$\frac{7.1}{50}$	✓
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$\frac{4.0}{50}$	$\frac{4.5}{26}$		4.9	$\frac{6.1}{27}$	$\frac{7.0}{50}$	✓
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oak spike in 12" oak 50 ft sta 294+75

$\frac{2.5}{50}$	$\frac{4.7}{18}$		5.7	$\frac{7.1}{26}$	$\frac{8.5}{50}$	
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station	+	H.I	-	Rod	Elev.
		886.66			
295+38				4.3	82.4 ✓
+70					
296+00 ✓					
+30 ✓					
296+70 ✓					
T.P.	11.34	897.02 ✓	0.98		885.68 ✓
295+38					
295+70				9.3	87.7 ✓
296+00				5.6	91.4 ✓
296+30				3.1	93.9 ✓
296+70				5.0	92.0 ✓
T.P.	7.73	891.16 ✓	7.59		889.43 ✓
297+00				2.7	88.5 ✓
297+50				7.5	83.7 ✓
T.P.	2.97	885.97 ✓	8.16		883.00 ✓

Lt. E Rt

$$\frac{0.7}{18}$$

$$\frac{4.3}{18}$$

$$\frac{5.8}{22}$$

$$\frac{7.8}{50}$$

✓

$$\begin{array}{r} -4.9 \\ 3.2 \\ \hline 13 \end{array} \quad \begin{array}{r} -6.6 \\ 4.1 \\ \hline 25 \end{array} \quad \begin{array}{r} -8.9 \\ 7.2 \\ \hline 50 \end{array}$$

✓

$$\begin{array}{r} -3.7 \\ 1.0 \\ \hline 13 \end{array} \quad \begin{array}{r} -6.7 \\ 4.0 \\ \hline 23 \end{array} \quad \begin{array}{r} -7.9 \\ 5.2 \\ \hline 36 \end{array} \quad \begin{array}{r} -9.3 \\ 6.6 \\ \hline 50 \end{array}$$

✓

$$\begin{array}{r} -8.5 \\ 1.2 \\ \hline 20 \end{array} \quad \begin{array}{r} -9.7 \\ 3.4 \\ \hline 27 \end{array} \quad \begin{array}{r} -12.5 \\ 5.2 \\ \hline 40 \end{array} \quad \begin{array}{r} -13.6 \\ 6.3 \\ \hline 50 \end{array}$$

✓

$$\begin{array}{r} -5.4 \\ 0.9 \\ \hline 19 \end{array} \quad \begin{array}{r} -10.3 \\ 4.9 \\ \hline 40 \end{array} \quad \begin{array}{r} -11.3 \\ 5.9 \\ \hline 50 \end{array}$$

$$\begin{array}{r} +11.4 \\ 5.3 \\ \hline 50 \end{array} \quad \begin{array}{r} +7.7 \\ 7.2 \\ \hline 35 \end{array}$$

✓

$$\begin{array}{r} 11 \\ 50 \end{array} \quad \begin{array}{r} 14 \\ 28 \end{array} \quad \begin{array}{r} 2.1 \\ 19 \end{array} \quad \begin{array}{r} 4.6 \\ 12 \end{array} \quad 9.3$$

✓

$$\begin{array}{r} 1.8 \\ 50 \end{array} \quad \begin{array}{r} 2.0 \\ 28 \end{array} \quad \begin{array}{r} 2.7 \\ 10 \end{array} \quad 5.6$$

✓

$$\begin{array}{r} 2.5 \\ 50 \end{array} \quad \begin{array}{r} 2.5 \\ 26 \end{array} \quad 3.1$$

✓

$$\begin{array}{r} 2.5 \\ 50 \end{array} \quad \begin{array}{r} 3.9 \\ 27 \end{array} \quad 5.0$$

✓

Top stake 297 +00

$$\begin{array}{r} 2.2 \\ 50 \end{array} \quad \begin{array}{r} 1.5 \\ 24 \end{array} \quad 2.7 \quad \begin{array}{r} 4.4 \\ 71 \end{array} \quad \begin{array}{r} 8.2 \\ 29 \end{array} \quad \begin{array}{r} 10.6 \\ 50 \end{array}$$

✓

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 6.0 \\ 17 \end{array} \quad 7.5 \quad \begin{array}{r} 9.1 \\ 23 \end{array} \quad \begin{array}{r} 11.4 \\ 50 \end{array}$$

✓

Station	+	H.I	-	Rod	Elev.
		815.97 ✓			
298+00				4.0	822.0 ✓
+50				5.6	80.4 ✓
299+00				7.6	78.4 ✓
+50				2.3	77.7 ✓
300+00				8.7	77.3 ✓
+50				8.8	77.2 ✓✓
301+00				7.8	78.2 ✓
+50				6.5	79.5 ✓
+75				4.8	81.2 ✓
302+00				2.9	83.1 ✓
+13				1.2	84.8 ✓
+50					
303+00					

Lt. ♀ Rt.

$\frac{0.8}{50}$	$\frac{3.3}{70}$	40	$\frac{5.7}{24}$	$\frac{7.6}{50}$	✓
$\frac{2.9}{50}$	$\frac{3.7}{73}$	56	$\frac{6.2}{18}$	$\frac{8.1}{34}$	$\frac{8.7}{50}$ ✓
$\frac{5.5}{50}$	$\frac{6.6}{70}$	7.6	$\frac{8.1}{31}$	$\frac{9.1}{50}$	
$\frac{7.1}{50}$	$\frac{7.8}{75}$	83	$\frac{7.2}{17}$	$\frac{7.5}{50}$	
$\frac{8.0}{50}$	$\frac{8.2}{74}$	87	$\frac{7.4}{23}$	$\frac{9.4}{50}$	
$\frac{8.0}{50}$	$\frac{7.9}{74}$	88	$\frac{7.5}{25}$	$\frac{8.5}{50}$	
$\frac{6.9}{50}$	$\frac{7.1}{74}$	78	$\frac{7.0}{25}$	$\frac{7.4}{50}$	
$\frac{4.1}{50}$	$\frac{4.1}{51}$	$\frac{5.2}{16}$	65	$\frac{8.0}{25}$	$\frac{7.1}{50}$
$\frac{2.3}{50}$	$\frac{0.9}{37}$	$\frac{2.6}{16}$	48	$\frac{7.0}{25}$	$\frac{8.7}{50}$
		29	$\frac{5.6}{12}$	$\frac{7.2}{27}$	$\frac{8.5}{50}$
		12	$\frac{5.1}{16}$	$\frac{7.2}{26}$	$\frac{8.5}{50}$
			(83.8)	(81.0)	(79.1) (77.8)
			2.2	5.0	8.9
			7	17	31
			8.2	50.	
			(84.4)	(81.8)	(80.3) (77.8)
			1.6	4.2	5.8
			8	15.	23
					50

Station	+	H.I	-	Rod Eley.
		285.97		
303+30				
T.P.	10.33	896.10	✓ 0.20	885.77 ✓
302+00				
302+13				
302+50				2.5 87.6 ✓
303+00				7.1 89.0 ✓
303+30				6.3 89.8 ✓
303+57				2.4 87.7 ✓
304+00				11.8 84.3 ✓
T.P.	0.68	889.63	✓ 7.15	882.95 ✓
304+00				
+27				6.6 83.0 ✓
+64				8.7 80.9 ✓
305+00				10.4 79.2 ✓
B.M.			5.35	884.28 ✓
B.M.	1.05	885.35	✓	884.30 ✓

Lt. E

Rt.

97.6 96.1 89.9 84.4

Top R.I. Guard Stake

11.8 2.5 3.2 6.2 11.7
197.6 33 24 17 5
50

101.9 100.4 94.9 89.6

11.8 14.3 15.2 6.5
901.9 900.8 71 7
50 37

5.7 73.1 00 5.4 85
901.8 899.2 16 7
50 38

10.2 1.5 2.5 3.9 71
890.3 35 76 6
50

2.2 2.9 2.2 60
50 27 6

4.4 5.5 6.8 84 13.3 12.1 12.4
50 28 8 10 29 50

4.5 5.6 7.6 11.8
50 29 10

Nail in foot of stake with 204/40

81.5 80.3 78.6 77.6

8.1 9.3 11.0 12.0
7 76 21 50

2.5 10.2 5.8 66 8.5 9.4 11.2 12.1
191.9 889.9 8 6 76 23 50
50 23

13.3 10 4.6 8.7 9.5 1.3 12.2
892.9 76 17 8 16 50
50

12.3 10 4.9 7.8 9.2 10.4 12.1 12.1
191.9 38 76 20 7 33 50
50

RR spike in 14" oak 20' Lt Sta 305+0.3

Station	+	H.I	-	Rod	Elev.
		885.35 ✓			
305	+50			7.2	78.2 ✓
306	+00			7.4	78.0 ✓
	+50			7.5	77.9 ✓
307	+00			7.0	77.4 ✓
	+47			6.1	79.3 ✓
308	+00			4.0	81.4 ✓
	+19			7.5	82.9 ✓
	+50				
309	+00				
	T.P	11.39	895.48 ✓	1.26	884.09 ✓
308	+00				
308	+19				
	+50			8.4	87.1 ✓

Lt. £ Rt.

9.2 S.B.

$\frac{+5.2}{828.6}$	$\frac{0.7}{45}$	$\frac{3.8}{32}$	$\frac{5.2}{16}$	72	$\frac{8.0}{27}$	$\frac{8.5}{50}$
$\frac{50}{50}$						

9.4 S.B.

$\frac{1.2}{50}$	$\frac{3.4}{44}$	$\frac{5.7}{20}$	$\frac{6.8}{14}$	74	$\frac{8.5}{33}$	$\frac{8.7}{50}$
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9.6 S.B.

$\frac{1.1}{50}$	$\frac{3.2}{42}$	$\frac{5.2}{27}$	$\frac{6.7}{17}$	75	$\frac{8.6}{29}$	$\frac{8.6}{50}$
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9.4.5B

$\frac{+5.7}{82.1}$	$\frac{+3.2}{187.6}$	$\frac{3.0}{30}$	$\frac{5.1}{13}$	$\frac{6.1}{8}$	70	$\frac{8.1}{30}$	$\frac{8.6}{50}$
$\frac{50}{50}$	$\frac{40}{40}$						

$\frac{+5.6 + 0.2}{901.0}$	$\frac{+5.0}{825.4}$	$\frac{+0.3}{825.1}$	$\frac{3.9}{17}$	$\frac{5.0}{4}$	61	$\frac{7.7}{33}$	$\frac{8.5}{50}$
$\frac{50}{50}$	$\frac{42}{35}$	$\frac{27}{27}$					

$\frac{3.8}{2}$	40	$\frac{4.1}{9}$	$\frac{6.5}{14}$	$\frac{7.6}{27}$	$\frac{8.0}{50}$
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25	$\frac{4.1}{5}$	$\frac{5.1}{16}$	$\frac{6.6}{23}$	$\frac{7.6}{50}$
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(82.0)	(80.7)	(78.7)	(78.2)
$\frac{3.4}{16}$	$\frac{4.7}{27}$	$\frac{6.7}{40}$	$\frac{7.2}{50}$

(83.9)	(82.5)	(81.2)
$\frac{1.5}{28}$	$\frac{2.9}{42}$	$\frac{4.2}{50}$

(900.2)	(9A.5)	(91.4)
$\frac{+4.7}{900.2}$	$\frac{1.0}{30}$	$\frac{4.1}{22}$
$\frac{50}{50}$		

(900.5)	(9A.5)	(87.9)
$\frac{+3.0}{900.5}$	$\frac{1.0}{27}$	$\frac{1.6}{12}$
$\frac{50}{50}$		

$\frac{+3.8}{899.3}$	$\frac{0.7}{28}$	$\frac{3.8}{11}$	84
$\frac{50}{50}$			

Station	+	H.I	-	Rod	Elev.
		895.48 ✓			
309+00				49	90.6 ✓
+50				44	91.1 ✓
310+00				61	89.4 ✓
T.P.	7.64	895.77 ✓	7.35		888.13 ✓
310+46				84	87.4 ✓
311+00				11.0	84.8 ✓
+50				12.3	83.5 ✓
312+00				12.2	83.6 ✓
T.P.	2.96	887.29 ✓	11.44		884.33 ✓
+26				2.6	83.7 ✓
+67				27	85.6 ✓
+84				3.7	83.6 ✓
313+00				5.3	82.0 ✓
+25				5.7	84.6 ✓

Lt. R Pt.

$\frac{+0.9}{900.14}$	$\frac{0.2}{24}$	$\frac{3.5}{9}$	1.9
50			

$\frac{+3.7}{897.2}$	$\frac{0.2}{28}$	$\frac{1.7}{19}$	4.1	$\frac{6.7}{11}$	$\frac{9.5}{28}$	$\frac{12.0}{50}$
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$\frac{+1.0}{897.4}$	$\frac{0.0}{38}$	$\frac{3.9}{16}$	6.1	$\frac{10.0}{21}$	$\frac{12.0}{26}$	$\frac{13.0}{50}$
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TOP I.T. GOUND stake

$\frac{0.0}{50}$	$\frac{1.0}{40}$	$\frac{3.7}{24}$	$\frac{6.4}{8}$	8.4	$\frac{11.3}{14}$	$\frac{13.1}{27}$	$\frac{14.7}{50}$
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$\frac{0.6}{50}$	$\frac{4.5}{27}$	$\frac{8.4}{9}$	11.0	$\frac{12.6}{10}$	$\frac{14.7}{36}$	$\frac{16.0}{50}$
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$\frac{1.0}{50}$	$\frac{5.4}{25}$	$\frac{10.0}{11}$	12.3	$\frac{14.2}{16}$	$\frac{15.1}{41}$	$\frac{15.9}{50}$
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$\frac{1.17}{897.0}$	$\frac{0.4}{41}$	$\frac{4.2}{27}$	$\frac{9.2}{13}$	12.2	$\frac{14.5}{20}$	$\frac{15.5}{42}$	$\frac{15.8}{50}$
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TOP STAKE B.I.S.

$\frac{+13.4}{900.7}$	$\frac{+6.4}{893.7}$	$\frac{2.0}{9}$	3.6	$\frac{4.8}{8}$	$\frac{6.0}{25}$	$\frac{7.3}{50}$
50	27					

$\frac{+17.0}{904.3}$	$\frac{+9.0}{896.3}$		17	$\frac{5.0}{10}$	$\frac{6.3}{26}$	$\frac{7.5}{50}$
50	27					

$\frac{+20.0}{907.6}$	$\frac{+10.3}{897.6}$	$\frac{2.0}{7}$	3.7	$\frac{5.2}{7}$	$\frac{6.4}{27}$	$\frac{7.6}{50}$
50	24					

$\frac{+12.5}{897.8}$	$\frac{+2.0}{897.3}$	$\frac{0.7}{13}$	5.8		$\frac{6.8}{24}$	$\frac{8.2}{50}$
50	27					

$\frac{+3.8}{897.1}$	$\frac{3.5}{26}$	$\frac{4.8}{16}$	5.1	$\frac{2.0}{19}$		$\frac{8.5}{50}$
50						

Station	+	H.I	-	Rod	Elev.	
		887.29	✓			
313+25				6.2	881.1	✓
T.P.	7.59	882.43	✓	7.45	879.84	✓
314+00				3.2	79.2	✓
+50				4.7	77.7	✓
315+00				5.2	77.2	✓
316+00				4.7	77.7	✓
317+00				3.8	78.6	✓
B.M.	4.77	886.30	✓	0.90	881.53	✓
318+00				7.1	79.2	✓
+65				5.9	80.4	✓
319+00				4.9	81.2	✓
+30				3.7	82.6	✓
+67				2.4	83.9	✓
320+00				2.4	83.9	✓
T.P.	6.18	890.88	✓	1.60	884.70	✓

Station	+	H.J	-	Rod	Elev.
		890.88 ✓			
320+50				7.3	83.6 ✓
321+00				8.4	82.5 ✓
+50				9.0	81.9 ✓
322+00				9.1	81.8 ✓
+35				9.6	81.3 ✓
+70				10.2	80.7 ✓
323+00				11.0	79.9 ✓
T.P.	8.05	888.77 ✓	7.96		880.92 ✓
+60				11.2	77.8 ✓
324+00				10.8	78.2 ✓
+67				8.4	80.6 ✓
325+00				5.4	83.6 ✓
T.P.	11.99	899.99 ✓	0.97		888.00 ✓
+62				5.1	94.9 ✓
T.P.	11.07	910.63 ✓	0.43		899.56 ✓

ft. \$ ft.

$\frac{54}{50}$ $\frac{2.2}{40}$ $\frac{5.8}{18}$ 73 $\frac{7.9}{8}$ $\frac{9.9}{22}$ $\frac{11.6}{50}$

$\frac{34}{50}$ $\frac{5.6}{34}$ $\frac{7.2}{16}$ 84 $\frac{11.2}{27}$ $\frac{11.9}{50}$

$\frac{4.5}{50}$ $\frac{6.7}{26}$ 90 $\frac{11.0}{33}$ $\frac{11.6}{50}$

$\frac{7.8}{50}$ $\frac{7.8}{25}$ $\frac{9.0}{10}$ 91 $\frac{9.5}{14}$ $\frac{9.4}{30}$ $\frac{2.5}{50}$

$\frac{9.6}{50}$ $\frac{9.7}{30}$ 96 $\frac{9.5}{50}$ $\frac{5.5}{50}$

$\frac{11.3}{50}$ $\frac{11.2}{32}$ 102 $\frac{9.5}{30}$ $\frac{9.0}{50}$

$\frac{12.3}{50}$ $\frac{12.0}{31}$ 110 $\frac{10.2}{28}$ $\frac{9.4}{50}$

Top stake 323

$\frac{11.4}{50}$ $\frac{11.4}{30}$ 112 $\frac{10.8}{30}$ $\frac{10.4}{50}$

$\frac{11.1}{50}$ $\frac{11.1}{23}$ 108 $\frac{11.0}{30}$ $\frac{10.9}{50}$

$\frac{8.4}{50}$ $\frac{8.5}{29}$ 84 $\frac{8.0}{27}$ $\frac{8.1}{50}$

$\frac{6.0}{50}$ $\frac{5.7}{28}$ 54 $\frac{5.3}{16}$ $\frac{4.6}{40}$ $\frac{4.9}{50}$

$\frac{4.2}{50}$ $\frac{4.8}{23}$ 51 $\frac{5.4}{28}$ $\frac{5.5}{30}$ $\frac{4.1}{50}$

Station	+	H.I	-	Rod Elev.	
		110.63 ✓			
315+85				12.0	898.6 ✓
326+00				11.0	899.6 ✓
+50				11.4	994 99.2 ✓
B.M.	6.89	900.63 ✓	6.89		903.74 ✓
327+00				8.0	902.6 ✓
T.P.	11.84	900.79 ✓	16.8		908.95 ✓
+50				11.6	09.2 ✓
+77				7.3	13.5 ✓
328+00				4.7	16.1 ✓
+75				3.0	17.8 ✓
+62				6.2	14.6 ✓
329+00				8.2	12.6 ✓
T.P.	2.84	916.55 ✓	7.08		913.71 ✓
+50				4.7	11.9 ✓
+76				5.6	11.0 ✓

W.H.C. PERSONS
GALVAD
MAY 1900
(cold & windy)

H. E. Rt.

$\frac{12.0}{50}$ $\frac{12.2}{76}$ 12.0 13.1 $\frac{14.0}{50}$

$\frac{9.0}{50}$ $\frac{10.0}{33}$ $\frac{10.9}{13}$ $\frac{11.0}{6}$ 4.7 12.4 $\frac{12.8}{50}$

$\frac{11.0}{50}$ $\frac{11.5}{31}$ $\frac{11.5}{12}$ 11.4 10.1 $\frac{88}{50}$

R.S. Spike in 15" BX Elder 185' Lt. Sta 327 to 0

$\frac{2.9}{50}$ $\frac{8.1}{78}$ 8.0 6.4 $\frac{3.8}{50}$

$\frac{14.9}{50}$ $\frac{13.6}{22}$ 14.6 9.2 $\frac{7.3}{50}$

$\frac{10.5}{50}$ $\frac{9.2}{25}$ 7.8 5.2 $\frac{3.7}{22}$ $\frac{3.7}{44}$ $\frac{3.7}{50}$

$\frac{7.2}{50}$ $\frac{5.5}{26}$ 4.7 $\frac{4.0}{10}$ 2.4 $\frac{3.4}{50}$

$\frac{7.0}{50}$ $\frac{5.1}{28}$ 3.0 2.2 $\frac{3.0}{27}$ $\frac{1.4}{29}$ $\frac{1.4}{50}$

$\frac{7.7}{50}$ $\frac{7.7}{21}$ 6.2 8.9 $\frac{6.9}{22}$ $\frac{3.4}{34}$ $\frac{7.3}{50}$

$\frac{11.5}{50}$ $\frac{10.6}{25}$ 8.2 $\frac{7.6}{24}$ $\frac{10.5}{50}$

Top Stake 327.9

$\frac{7.1}{50}$ $\frac{8.0}{36}$ $\frac{6.2}{20}$ 4.7 4.6 $\frac{6.0}{23}$ $\frac{4.5}{45}$ $\frac{7.7}{50}$

$\frac{2.6}{50}$ $\frac{6.8}{26}$ 5.6 4.0 $\frac{6.3}{17}$ $\frac{4.6}{76}$ $\frac{7.7}{50}$

Station	+	H.I	-	Rod	Elev.
330+00				6.0	70.6 ✓
+30				9.5	67.1 ✓
+60				9.7	66.9 ✓
331+00				7.8	68.8 ✓
+40				7.0	69.6 ✓
T.P.	635	919.24 ✓	3.66		912.89 ✓
+70				8.0	11.2 ✓
332+00				7.4	11.8 ✓
+42				8.4	10.8 ✓
333+00				8.0	11.3 ✓
+45				9.0	10.2 ✓
+75				10.2	09.0 ✓
334+00				11.3	07.9 ✓
T.P.	184	909.82 ✓	11.26		907.98 ✓

H. Z RT.

$\frac{9.1}{50}$ $\frac{8.2}{29}$ 6.0 $\frac{4.4}{15}$ $\frac{5.1}{30}$ 6.6 $\frac{7.8}{50}$

$\frac{7.2}{50}$ $\frac{9.4}{28}$ 9.5 $\frac{8.2}{12}$ $\frac{7.7}{32}$ $\frac{8.4}{46}$ $\frac{7.5}{50}$

$\frac{8.9}{50}$ $\frac{8.7}{30}$ 9.7 $\frac{12.1}{33}$ $\frac{13.1}{50}$

$\frac{4.7}{50}$ $\frac{5.5}{30}$ 7.8 $\frac{10.9}{25}$ $\frac{14.3}{44}$ $\frac{15.5}{50}$

$\frac{2.6}{50}$ $\frac{2.8}{26}$ 7.0 $\frac{11.7}{24}$ $\frac{14.7}{46}$ $\frac{15.2}{50}$

top sta. to 332

$\frac{2.9}{50}$ $\frac{2.1}{37}$ $\frac{4.5}{20}$ 8.0 $\frac{12.0}{15}$ $\frac{16.7}{35}$ $\frac{17.7}{44}$ $\frac{18.7}{50}$

$\frac{1.8}{50}$ $\frac{3.2}{29}$ $\frac{5.2}{18}$ 8.4 $\frac{12.0}{16}$ $\frac{16.7}{39}$ $\frac{18.3}{50}$

$\frac{2.4}{50}$ $\frac{3.9}{36}$ $\frac{5.7}{20}$ 8.4 $\frac{12.0}{17}$ $\frac{16.2}{46}$ $\frac{17.6}{50}$

$\frac{2.8}{50}$ $\frac{4.9}{28}$ 8.0 $\frac{14.0}{23}$ $\frac{10.1}{44}$ $\frac{14.0}{50}$

$\frac{2.0}{50}$ $\frac{2.8}{26}$ 9.0 $\frac{11.2}{19}$ $\frac{12.6}{34}$ $\frac{12.6}{50}$

$\frac{9.1}{50}$ $\frac{10.2}{32}$ 10.2 $\frac{12.0}{15}$ $\frac{15.6}{33}$ $\frac{17.2}{50}$

$\frac{12.3}{50}$ $\frac{13.0}{25}$ 11.3 $\frac{13.2}{24}$ $\frac{15.5}{43}$ $\frac{18.4}{50}$

2.8 sphy POT. 331/100

Station	+	H.I	-	Rod	Elev.
		909.82 ✓			
334+76				3.8	867.0 ✓
+47				7.9	861.9 ✓
T.P.	0.91	898.93 ✓	11.80		898.02 ✓
+76				6.0	922.9 ✓
335+00				10.0	88.9 ✓
+30				11.2	87.7 ✓
+62				10.6	88.3 ✓
T.P.	2.69	889.99 ✓	11.63		887.30 ✓
336+00				4.2	85.8 ✓
337+00				5.7	84.3 ✓
338+00				6.3	83.7 ✓
+48				5.1	84.9 ✓
339+00				1.6	85.4 ✓
T.P.	9.83	896.29 ✓	3.53		886.46 ✓
339+50				8.8	87.5 ✓

Lt. A Rt.

$\frac{86}{50}$	$\frac{8.1}{40}$	$\frac{6.4}{23}$	$\frac{3.8}{20}$	$\frac{3.8}{20}$	$\frac{5.7}{44}$	$\frac{7.2}{47}$	$\frac{10.1}{50}$
$\frac{10.2}{5}$	$\frac{10.5}{31}$		7.7	$\frac{6.4}{27}$	$\frac{8.2}{43}$	$\frac{10.5}{47}$	$\frac{12.3}{56}$
$\frac{5.2}{50}$		$\frac{6.2}{16}$	6.0	$\frac{3.8}{20}$	$\frac{2.8}{31}$	$\frac{3.8}{44}$	$\frac{5.2}{47}$
$\frac{9.1}{50}$	$\frac{7.8}{24}$		10.0	$\frac{9.8}{36}$	$\frac{7.0}{41}$	$\frac{8.6}{50}$	
$\frac{10.6}{50}$	$\frac{11.0}{24}$		11.2		$\frac{11.0}{25}$	$\frac{10.6}{50}$	
$\frac{9.1}{50}$	$\frac{9.1}{25}$		10.6		$\frac{11.3}{28}$	$\frac{11.7}{50}$	
$\frac{3.0}{50}$	$\frac{3.7}{23}$		$\frac{4}{2}$		$\frac{4}{23}$	$\frac{4}{50}$	
$\frac{4.8}{50}$	$\frac{5.1}{24}$		5.7		$\frac{6.1}{25}$	$\frac{6.0}{50}$	
$\frac{4.9}{50}$	$\frac{5.3}{33}$		6.3		$\frac{6.0}{25}$	$\frac{5.8}{50}$	
$\frac{4.2}{50}$	$\frac{5.1}{27}$		5.1		$\frac{5.7}{25}$	$\frac{6.0}{50}$	
$\frac{5.7}{50}$	$\frac{2.8}{28}$		$\frac{4}{6}$		$\frac{5.1}{22}$	$\frac{5.4}{50}$	
$\frac{4.5}{50}$	$\frac{5.6}{33}$	$\frac{7.8}{15}$	2.8		$\frac{10.4}{23}$	$\frac{11.1}{50}$	

station	+	H.I	-	Rod	Elev.
		896.79 ✓			
346+00				6.9	89.4 ✓ ●
+50				5.3	91.3 (circled) 91.0 ✓
341+00				4.1	92.2 ✓
+52				1.8	94.5 ✓
342+00				1.1	95.2 ✓
T.P.	5.60	901.86 ✓	0.03		896.76 ✓
+35				5.9	96.0 ✓
B.M.	6.20	901.86 ✓	6.20		895.66 ✓ ●
+70				5.7	96.2 ✓
343+00				6.5	95.4 ✓
+50				8.3	93.6 ✓
344+00				7.7	94.2 ✓
+50				2.4	99.5 ✓
345+00				2.0	98.9 ✓ ●
T.P.	1.14	910.73 ✓	2.27		899.59 ✓

Lt.

R

Rt.

$\frac{12.7}{897.0}$	$\frac{10}{37}$	$\frac{3.2}{26}$	$\frac{5.1}{10}$	49	$\frac{8.7}{23}$	$\frac{10.7}{50}$
50						

$\frac{12.7}{899.0}$	$\frac{10}{36}$	$\frac{3.6}{22}$		53	$\frac{7.7}{23}$	$\frac{9.3}{50}$
50						

$\frac{4.3}{101.6}$	$\frac{0.7}{30}$	$\frac{2.5}{19}$		41	$\frac{6.0}{76}$	$\frac{7.7}{33}$	$\frac{8.7}{50}$
50							

$\frac{4.2}{101.5}$	$\frac{13.3}{844.6}$	$\frac{0.9}{6}$		18	$\frac{3.2}{15}$	$\frac{5.1}{27}$	$\frac{7.0}{50}$
50	23.						

$\frac{11.4}{104.5}$	$\frac{+3.9}{100.2}$			14	$\frac{3.2}{12}$	$\frac{4.4}{28}$	$\frac{6.1}{43}$	$\frac{6.6}{50}$
50	20							

$\frac{12.4}{102.4}$	$\frac{1.5}{25}$	$\frac{2.6}{18}$		39	$\frac{7.6}{11}$	$\frac{10.8}{32}$	$\frac{11.9}{50}$
50							

R.R. Spike in Cor F.P. 3' 8" Sta. 342+55

$\frac{11.0}{104.9}$	$\frac{1.5}{32}$	$\frac{4.5}{10}$	$\frac{4.9}{2}$	57	$\frac{9.4}{12}$	$\frac{10.8}{22}$	$\frac{11.0}{50}$
50							

$\frac{11.3}{103.2}$	$\frac{0.7}{28}$	$\frac{4.3}{12}$	$\frac{4.9}{3}$	65	$\frac{9.0}{5}$	$\frac{10.8}{19}$	$\frac{10.8}{38}$	$\frac{9.8}{50}$
50								

$\frac{13.8}{103.7}$	$\frac{2.4}{904.3}$	$\frac{2.2}{22}$	$\frac{4.2}{16}$	$\frac{5.6}{4}$	23	$\frac{7.5}{8}$	$\frac{0.3}{25}$	$\frac{12.0}{40}$	$\frac{7.3}{50}$
50	44								

$\frac{4.4}{101.3}$	$\frac{1.0}{21}$	$\frac{3.5}{5}$		77	$\frac{8.8}{8}$		$\frac{9.7}{20}$	$\frac{9.3}{50}$
50								

$\frac{5.7}{107.6}$	$\frac{2.1}{904.6}$	$\frac{0.0}{13}$	$\frac{1.1}{2}$	24	$\frac{6.0}{9}$	$\frac{8.1}{25}$	$\frac{9.5}{50}$
50	78						

$\frac{16.3}{101.4}$	$\frac{0.0}{21}$	$\frac{1.7}{12}$	$\frac{2.3}{7}$	30	$\frac{6.8}{13}$	$\frac{8.1}{32}$	$\frac{8.6}{50}$
50							

Station	+	H.I	-	Rod	Elev.
		909.73	✓		
345+50				7.8	900.9 ✓
346+00				23	07.4 ✓
+22					
+50					
347+00					
T.P	11.54	921.38 ✓	0.89		909.84 ✓
346+22				11.5	09.9 ✓
+50				9.2	14.2 (circled) 12.2 ✓
347+00				5.0	10.4 ✓
+50				1.8	19.6 ✓
+77				2.3	19.1 ✓
348+00				6.0	15.4 ✓
+75				10.0	11.4 ✓

Lt.

Q

Rt.

$\frac{2.8}{50}$	$\frac{8.6}{20}$	1.8	$\frac{12.0}{70}$	$\frac{14.2}{28}$	$\frac{15.2}{50}$
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$\frac{6.0}{50}$	$\frac{1.0}{38}$	$\frac{2.2}{20}$	3.3	$\frac{3.4}{2}$	$\frac{6.6}{7}$	$\frac{11.1}{20}$	$\frac{14.1}{34}$	$\frac{15.8}{50}$
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(2.9)	(98.0)	(95.9)
29	127	148
17	38	50

(5.5)	(90.5)	(98.0)
12	102	127
17	34	50

(9.7)	(A.7)	(2.2)
10	60	85
29	43	50

$\frac{8.7}{50}$	$\frac{10.5}{19}$	1.5	$\frac{11.5}{2}$	$\frac{14.8}{6}$
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$\frac{6.9}{50}$	$\frac{2.5}{27}$	9.2	$\frac{2.2}{2}$	$\frac{12.5}{5}$
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$\frac{3.7}{50}$	$\frac{4.5}{28}$	5.0	$\frac{4.8}{5}$	$\frac{7.0}{10}$
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$\frac{4.9}{50}$	$\frac{3.2}{37}$	$\frac{2.1}{14}$	1.8	$\frac{0.9}{15}$	$\frac{2.2}{18}$	$\frac{3.1}{33}$	$\frac{5.3}{50}$
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$\frac{7.0}{50}$	$\frac{5.4}{21}$	2.3	$\frac{0.1}{17}$	$\frac{1.5}{21}$	$\frac{2.9}{34}$	$\frac{3.7}{50}$
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$\frac{10.6}{50}$	$\frac{9.6}{30}$	$\frac{8.0}{10}$	6.0	$\frac{3.8}{11}$	$\frac{1.7}{22}$	$\frac{2.3}{25}$	$\frac{1.7}{50}$
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$\frac{13.9}{50}$	$\frac{12.6}{33}$	$\frac{10.9}{17}$	10.0	$\frac{6.3}{19}$	$\frac{5.2}{29}$	3.5
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station	+	H.I	-	Rod	Elev.	
		921.28 ✓				
348	+50			4.6	909.8 ✓	●
349	+00			11.5	89.9 ✓	
	+50			7.6	13.8 ✓	
350	+00			2.7	12.7 ✓	
T.P.		4.56	924.17 ✓	1.77	919.61 ✓	
	+50			7.9	21.3 ✓	
351	+00			8.9	15.3 ✓	●
	+35			10.9	13.3 ✓	
	+73			11.2	13.0 ✓	
FROM R-355						
352	+00			12.2	12.0 ✓	
	+50			11.6	12.6 ✓	
353	+00			11.1	13.1 ✓	
	+50			10.2	14.0 ✓	●

W.H.C. Persons
Galvia
Mabo ray
Jan 23, 1925

(cold & windy)

	Lt.		Rt.	
$\frac{15.0}{50}$	$\frac{13.3}{27}$	11.6	$\frac{10.9}{18}$	$\frac{7.6}{34}$
				$\frac{7.3}{50}$

$\frac{15.0}{50}$	$\frac{13.1}{27}$	11.5	$\frac{10.6}{27}$	$\frac{7.3}{50}$
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$\frac{11.0}{50}$	$\frac{8.7}{26}$	7.6	$\frac{6.9}{24}$	$\frac{7.2}{50}$
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$\frac{7.5}{50}$	$\frac{3.4}{22}$	2.7	$\frac{2.0}{18}$	$\frac{3.0}{34}$	✓
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Top stake 350+00

$\frac{7.6}{50}$	$\frac{5.8}{38}$	$\frac{3.5}{15}$	2.1	$\frac{4.2}{19}$	$\frac{3.8}{38}$	$\frac{4.4}{50}$	✓
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$\frac{11.5}{50}$	$\frac{10.6}{27}$	$\frac{10.3}{15}$	8.9	$\frac{7.0}{15}$	$\frac{4.6}{33}$	$\frac{4.6}{50}$	✓
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$\frac{12.6}{50}$	$\frac{12.9}{37}$	$\frac{12.5}{22}$	10.9	$\frac{9.2}{16}$	$\frac{6.7}{36}$	$\frac{6.5}{50}$	✓
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$\frac{11.7}{50}$	$\frac{12.0}{27}$	$\frac{12.2}{8}$	11.2	$\frac{11.1}{38}$	$\frac{10.7}{50}$	✓
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$\frac{10.4}{50}$		$\frac{11.8}{27}$	13.2	$\frac{13.6}{27}$	$\frac{13.2}{50}$	✓
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$\frac{10.8}{50}$	$\frac{10.1}{45}$	$\frac{7.9}{28}$	11.6	$\frac{12.3}{18}$	$\frac{13.3}{33}$	$\frac{14.0}{50}$	✓
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$\frac{12.4}{50}$	$\frac{11.7}{28}$		11.1	$\frac{11.8}{18}$	$\frac{13.0}{30}$	$\frac{13.3}{50}$	✓
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$\frac{14.0}{50}$	$\frac{12.5}{37}$	$\frac{10.7}{20}$	10.2		$\frac{10.9}{27}$	$\frac{11.3}{50}$	✓
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Station	+	H.I	-	Rod	Elev.	
		924.17 ✓				
354+00				8.7	15.5 ✓	●
+50				7.0	17.2 ✓	
355+00				6.3	17.9 ✓	
T.P.	1.69	929.37 ✓	5.49		918.68 ✓	
+50				2.5	17.9 ✓	
356+00				3.7	16.7 ✓	
+50				6.1	14.3 ✓	●
357+00				11.6	08.8 ✓	
T.P.	0.32	910.01 ✓	10.68		909.69 ✓	
+57				6.9	08.1 ✓	
358+00				11.5	898.5 ✓	
+50				13.8	962 ✓	
359+00				13.8	96.2 ✓	
360+00				13.2	96.7 ✓	●

L. S. Rt.

$\frac{14.5}{50}$ $\frac{16.0}{32}$ 8.7 $\frac{8.1}{20}$ $\frac{7.8}{42}$ $\frac{8.1}{50}$ ✓

$\frac{11.0}{50}$ $\frac{10.0}{38}$ $\frac{8.1}{18}$ 7.0 $\frac{6.1}{31}$ $\frac{6.2}{50}$ ✓

$\frac{8.5}{50}$ $\frac{7.6}{32}$ 6.3 $\frac{5.5}{30}$ $\frac{6.4}{50}$ ✓

$\frac{2.7}{50}$ $\frac{2.7}{38}$ $\frac{2.6}{16}$ 2.5 $\frac{2.3}{21}$ $\frac{1.9}{35}$ $\frac{2.6}{50}$ ✓

$\frac{2.7}{50}$ $\frac{3.3}{33}$ $\frac{3.5}{16}$ 3.7 $\frac{3.4}{16}$ $\frac{3.4}{33}$ $\frac{3.4}{50}$ ✓

$\frac{5.0}{50}$ $\frac{5.6}{36}$ $\frac{5.7}{16}$ 6.1 $\frac{6.8}{16}$ $\frac{7.3}{33}$ $\frac{7.3}{50}$ ✓

$\frac{8.8}{50}$ $\frac{10.7}{33}$ $\frac{11.2}{16}$ 11.6 $\frac{11.7}{16}$ $\frac{11.6}{33}$ $\frac{11.7}{50}$ ✓

$\frac{7.6}{50}$ $\frac{7.7}{33}$ $\frac{7.5}{16}$ 6.9 $\frac{7.0}{16}$ $\frac{7.3}{33}$ $\frac{7.1}{50}$ ✓

$\frac{10.4}{50}$ $\frac{11.2}{25}$ 11.5 $\frac{11.5}{25}$ $\frac{11.4}{50}$ ✓

$\frac{12.1}{50}$ $\frac{13.5}{25}$ 13.8 $\frac{12.3}{25}$ $\frac{12.3}{50}$ ✓

$\frac{13.2}{50}$ $\frac{13.8}{25}$ 13.8 $\frac{13.3}{25}$ $\frac{13.0}{50}$ ✓

$\frac{14.0}{50}$ $\frac{13.3}{25}$ 13.3 $\frac{13.3}{25}$ $\frac{12.9}{50}$ ✓

Station	+	H.I	-	Rod	Elev.	
		910.01 ✓				
360+60				13.5	896.5 ✓	●
361+00				10.0	900.0 ✓	
+50				0.7	909.3 ✓	
T.P.	11.92	921.80 ✓	0.13		909.88 ✓	
362+00				6.6	15.2 ✓	
+50				3.0	18.8 ✓	
363+00				6.0	15.8 ✓	●
+50				5.5	16.3 ✓	
364+00				2.1	18.9 ✓	
T.P.	6.46	926.35 ✓	1.91		919.89 ✓	
+50				6.3	20.1 ✓	
365+00				5.4	21.0 ✓	
+50				4.7	21.7 ✓	
366+00				5.9	20.5 ✓	●

	H.	L	RT.				
$\frac{12.8}{50}$	$\frac{134}{25}$	13.5	$\frac{130}{25}$	$\frac{112}{50}$		✓	
$\frac{5.7}{50}$	$\frac{104}{25}$	10.0	$\frac{90}{25}$	$\frac{5.1}{50}$		✓	
$\frac{24}{50}$	$\frac{24}{25}$	0.7	$\frac{90}{25}$	$\frac{4.0}{50}$		✓	
$\frac{80}{50}$	$\frac{70}{25}$	6.6	$\frac{51}{30}$	$\frac{60}{50}$		✓	
$\frac{36}{50}$	$\frac{33}{25}$	3.0	$\frac{7.1}{25}$	$\frac{10.8}{50}$		✓	
$\frac{2.1}{50}$	$\frac{24}{28}$	$\frac{44}{9}$	6.0	$\frac{60}{74}$	$\frac{10.1}{30}$	$\frac{123}{50}$	✓
$\frac{19}{50}$	$\frac{2.5}{30}$	$\frac{39}{24}$	5.5	$\frac{7.8}{2}$	$\frac{10.1}{25}$	$\frac{11.1}{50}$	✓
$\frac{24}{50}$	$\frac{1.5}{37}$	$\frac{19}{20}$	2.9	$\frac{40}{16}$	$\frac{5.0}{33}$	$\frac{5.5}{50}$	✓
$\frac{7.2}{50}$	$\frac{6.5}{25}$	6.3	$\frac{6.1}{25}$	$\frac{5.5}{50}$		✓	
$\frac{7.1}{50}$	$\frac{6.2}{25}$	5.4	$\frac{3.9}{25}$	$\frac{8.1}{50}$		✓	
$\frac{7.1}{50}$	$\frac{7.0}{25}$	4.7	$\frac{3.7}{14}$	$\frac{3.6}{28}$	$\frac{2.4}{50}$	✓	
$\frac{12.5}{50}$	$\frac{10.1}{25}$	5.9	$\frac{4.9}{8}$	$\frac{3.4}{30}$	$\frac{1.2}{50}$	✓	

station	+	H.I	-	Rod	Elev.	
		926.35 ✓				
366+50				9.8	16.6 ✓	
367+00				11.7	14.7 ✓	
T.P.	0.08	915.73 ✓	10.70		915.65 ✓	
+40				4.1	11.6 ✓	
	2.72	913.45 ✓	10.00		905.73 ✓	
368				8.5	05.0 ✓	
+15				8.4	05.1 ✓	
+21				12.3	01.3 ✓	
+27				8.4	05.1 ✓	
+50				9.9	03.6 ✓	
369+00				7.4	05.1 ✓	
+53				3.5	10.0 ✓	
T.P.	11.48	923.02 ✓	19.1		911.54 ✓	
370+00				5.0	18.0 ✓	
+15				2.2	20.8 ✓	

W.H.C. Persons
Sally D. Mahoney
1978
(Windy)

Lt. E Rt.

15.0 12.3 98 70 57
50 75 75 50

✓

13.6 13.0 117 98 71
50 70 78 50

✓

70 ft Stake 367 100

8.5 6.0 41 48 57
50 78 75 50

✓

71 13.0 72 74 85 80 79 79
50 36 79 76 21 40 50

✓

84 8.0 10.8 11.8 84 91 93 74
50 21 11 7 9 26 50

✓

77 8.2 77 123 93 98 7.6
50 36 15 9 21 50

✓

70 28 78 84 123 98 101 10.1
50 36 12 8 18 30 50

✓

67 7.3 71 9.9 103 98 123 15.6
50 33 73 21 36 41 50

✓

49 6.5 74 83 72
50 75 25 50

✓

12.0 6.0 16 8.5 4.6 4.8
91.5 76 15 75 50

✓

4.3 3.9 4.3 5.0 7.6 8.5
50 70 72 31 50

✓

3.7 2.4 2.2 3.5 5.0 5.4
50 76 78 78 37 50

✓

Station	+	H.I	-	Rod	Elev.
		923.02 ✓			
370	+55			3.0	920.0 ✓
371	+00			3.5	19.5 ✓
T.P.	9.78	929.63 ✓	2.67		920.35 ✓
	+55			7.7	21.9 ✓
377	+00			7.5	22.1 ✓
	+50			9.1	19.8 ✓
373	+00			11.8	17.8 ✓
	+53			11.7	17.7 ✓
377	+00			10.9	18.7 ✓
	+11			10.8	18.8 ✓
	+30			11.5	18.1 ✓
	+60			6.5	23.1 ✓
B.M.			11.75		917.88 ✓

Lt S Rt.

$\frac{46}{50}$ $\frac{36}{25}$ 3.0 $\frac{37}{29}$ $\frac{32}{50}$ ✓

$\frac{45}{50}$ $\frac{40}{27}$ 3.5 $\frac{27}{28}$ $\frac{23}{30}$ ✓

$\frac{103}{50}$ $\frac{90}{25}$ 77 $\frac{72}{28}$ $\frac{63}{50}$ ✓

$\frac{95}{50}$ $\frac{87}{28}$ 75 $\frac{51}{22}$ $\frac{40}{50}$ ✓

$\frac{92}{50}$ $\frac{78}{28}$ 98 $\frac{20}{28}$ $\frac{56}{50}$ ✓

$\frac{123}{50}$ $\frac{123}{27}$ 118 $\frac{105}{28}$ $\frac{80}{50}$ ✓

$\frac{123}{50}$ $\frac{133}{25}$ 119 $\frac{114}{18}$ $\frac{101}{26}$ $\frac{101}{50}$ ✓

$\frac{123}{50}$ $\frac{131}{25}$ $\frac{120}{10}$ 109 $\frac{109}{25}$ $\frac{100}{50}$ ✓

$\frac{123}{50}$ $\frac{131}{26}$ $\frac{120}{28}$ 108 $\frac{104}{22}$ $\frac{101}{38}$ $\frac{56}{50}$ ✓

$\frac{122}{50}$ $\frac{116}{26}$ 115 $\frac{70}{15}$ $\frac{72}{26}$ $\frac{45}{32}$ $\frac{40}{50}$ ✓

$\frac{120}{50}$ $\frac{125}{35}$ $\frac{96}{27}$ $\frac{85}{13}$ 65 $\frac{63}{12}$ $\frac{52}{30}$ $\frac{32}{50}$ ✓

Sp. to in T.P. 55' Lt. Sta. 374720

Station

+

H. I

-

Rod

Elev.

		H.I.	-	Red.	Elev.
579	+				
B.M.	10.20	928.05 ✓		917.85	917.85 ✓
375				5.8	922.5 ✓
+50				4.0	922.1 ✓
376				7.0	921.1 ✓
+55				11.5	916.4 ✓
T.P.	6.67	913.02 ✓	11.72	914.35 ✓	
377				7.7	915.3 ✓
+40				8.6	914.4 ✓
378				5.8	917.2 ✓
T.P.	4.03	918.90 ✓	8.15	914.87 ✓	
379				4.7	914.0 ✓
+30				5.3	913.6 ✓
+53				4.7	914.2 ✓
+56				7.2	911.7 ✓
+47				7.3	911.6 ✓
+71				5.4	913.5 ✓

11/17/25
46

Lt.

Rt.

Sp. in T.P. 55' L Sta. 374+25

$\frac{4.1}{50}$ $\frac{6.8}{42}$ $\frac{6.7}{33}$ $\frac{6.4}{14}$ 5.7 $\frac{4.3}{14}$ $\frac{3.1}{33}$ $\frac{1.4}{50}$ ✓

$\frac{7.1}{50}$ $\frac{5.6}{33}$ $\frac{7.2}{14}$ 6.0 $\frac{4.3}{16}$ $\frac{2.6}{33}$ $\frac{0.8}{50}$ ✓

$\frac{12.2}{50}$ $\frac{10.2}{33}$ $\frac{8.8}{14}$ 7.0 $\frac{5.3}{14}$ $\frac{4.1}{33}$ $\frac{2.6}{50}$ ✓

$\frac{15.2}{50}$ $\frac{13.7}{33}$ $\frac{12.4}{14}$ 11.5 $\frac{7.3}{16}$ $\frac{7.7}{33}$ $\frac{6.1}{50}$ ✓

$\frac{13.0}{50}$ $\frac{11.7}{33}$ $\frac{9.9}{14}$ 7.7 $\frac{5.4}{14}$ $\frac{5.4}{33}$ $\frac{1.4}{50}$ ✓

$\frac{13.5}{50}$ $\frac{11.8}{33}$ $\frac{7.8}{14}$ 8.4 $\frac{5.9}{16}$ $\frac{3.4}{33}$ $\frac{1.0}{50}$ ✓

$\frac{12.7}{50}$ $\frac{10.0}{33}$ $\frac{7.6}{14}$ 5.8 $\frac{4.5}{14}$ $\frac{1.9}{33}$ $\frac{1.9}{50}$ ✓

$\frac{7.6}{50}$ $\frac{8.0}{33}$ $\frac{6.9}{14}$ 4.9 $\frac{1.2}{16}$ $\frac{1.2}{33}$ $\frac{1.7}{50}$ ✓

$\frac{7.9}{50}$ $\frac{8.5}{33}$ $\frac{7.4}{14}$ 5.3 $\frac{3.4}{16}$ $\frac{1.7}{17}$ $\frac{1.7}{34}$ $\frac{2.9}{45}$ $\frac{7.4}{47}$ $\frac{4.1}{50}$ ✓

$\frac{12.7}{50}$ $\frac{10.7}{46}$ $\frac{8.2}{37}$ $\frac{7.7}{33}$ $\frac{5.6}{16}$ 4.7 $\frac{7.1}{4}$ $\frac{5.7}{24}$ $\frac{3.7}{26}$ $\frac{3.6}{33}$ $\frac{4.2}{50}$

$\frac{11.5}{50}$ $\frac{10.6}{44}$ $\frac{7.5}{35}$ $\frac{7.5}{33}$ $\frac{5.8}{17}$ $\frac{5.2}{5}$ 7.2 $\frac{6.4}{20}$ $\frac{3.8}{24}$ $\frac{4.2}{33}$ $\frac{7.3}{50}$

$\frac{7.4}{50}$ $\frac{7.4}{33}$ $\frac{7.8}{14}$ 7.3 $\frac{4.6}{7}$ $\frac{4.4}{16}$ $\frac{3.9}{33}$ $\frac{4.6}{50}$

$\frac{2.6}{50}$ $\frac{8.7}{33}$ $\frac{7.5}{4}$ 5.4 $\frac{4.4}{14}$ $\frac{4.2}{33}$ $\frac{4.9}{50}$

Sta.	+	H.I.	-	Red.	Elev.
		918.90 ✓			
	+81			5.4	913.5 ✓
380				5.6	913.3 ✓
	+03			5.4	913.3 ✓
	+09			8.5	910.4 ✓
	+43	Center of cross ref.		4.5	912.4 ✓
	+67			7.1	911.8 ✓
	+80			1.6	917.3 ✓
381				2.1	916.8 ✓
	+28			3.3	915.4 ✓
382				4.2	912.7 ✓
	+50			7.5	911.4 ✓
T.P	8.15	910.34 ✓	6.69	912.21 ✓	
383				7.4	913.0 ✓
	+20			7.1	913.3 ✓

1/17/25
47

Lt

Rt

$\frac{9.1}{50}$	$\frac{8.8}{33}$	$\frac{8.0}{21}$	$\frac{6.3}{19}$	5.4	$\frac{5.6}{16}$	$\frac{5.1}{33}$	$\frac{5.5}{30}$	✓
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$\frac{9.1}{50}$	$\frac{8.2}{33}$	$\frac{8.3}{21}$	$\frac{8.7}{8}$	$\frac{6.2}{4}$	5.6	$\frac{5.2}{16}$	$\frac{5.4}{33}$	$\frac{5.9}{50}$	✓
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$\frac{9.2}{50}$	$\frac{7.9}{33}$	$\frac{8.1}{18}$	$\frac{8.5}{8}$	5.6	$\frac{5.1}{16}$	$\frac{5.4}{33}$	$\frac{6.0}{50}$	✓
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$\frac{8.7}{50}$	$\frac{9.4}{47}$	$\frac{8.1}{33}$	$\frac{8.8}{14}$	8.5	$\frac{5.8}{4}$	$\frac{5.2}{16}$	$\frac{5.9}{33}$	$\frac{6.1}{50}$	✓
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$\frac{3.4}{50}$	$\frac{2.1}{33}$	$\frac{2.3}{30}$	$\frac{7.7}{20}$	6.5	$\frac{7.1}{15}$	$\frac{7.9}{26}$	$\frac{5.8}{30}$	$\frac{5.8}{33}$	$\frac{6.7}{50}$	✓
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$\frac{2.6}{50}$	$\frac{1.5}{33}$	$\frac{0.9}{21}$	$\frac{1.2}{14}$	7.1	$\frac{5.7}{21}$	$\frac{6.0}{33}$	$\frac{6.1}{38}$	$\frac{7.1}{50}$	✓
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$\frac{2.6}{50}$	$\frac{1.5}{33}$	$\frac{1.6}{16}$	1.6	$\frac{6.8}{8}$	$\frac{6.2}{14}$	$\frac{5.4}{29}$	$\frac{5.7}{33}$	$\frac{5.9}{45}$	$\frac{6.4}{50}$	✓
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$\frac{2.5}{50}$	$\frac{1.9}{33}$	$\frac{1.6}{14}$	1.1	$\frac{2.0}{13}$	$\frac{2.8}{20}$	$\frac{3.5}{24}$	$\frac{3.5}{30}$	$\frac{5.4}{33}$	$\frac{4.6}{46}$	$\frac{4.8}{50}$
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$\frac{2.1}{50}$	$\frac{3.6}{33}$	$\frac{3.2}{16}$	3.3	$\frac{3.3}{14}$	$\frac{3.3}{33}$	$\frac{3.5}{44}$	$\frac{4.9}{36}$	$\frac{5.0}{50}$
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$\frac{5.4}{50}$	$\frac{6.0}{33}$	$\frac{6.3}{16}$	6.2	$\frac{6.0}{16}$	$\frac{5.5}{33}$	$\frac{5.0}{50}$
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$\frac{8.5}{50}$	$\frac{8.4}{33}$	$\frac{8.0}{16}$	7.5	$\frac{7.3}{14}$	$\frac{6.5}{33}$	$\frac{6.1}{50}$
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$\frac{9.3}{50}$	$\frac{9.0}{33}$	$\frac{8.3}{16}$	7.4	$\frac{7.1}{14}$	$\frac{7.0}{33}$	$\frac{7.2}{50}$
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$\frac{8.7}{50}$	$\frac{7.7}{33}$	$\frac{6.9}{14}$	7.1	$\frac{6.8}{14}$	$\frac{6.7}{33}$	$\frac{7.0}{50}$
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Sta.	+	H.I.	-	Rod.	Elev.
		920.96			
384				7.3	911.1 ✓
	+42			8.8	911.6 ✓
385				4.4	916.0 ✓
T.P.	5.57	924.37 ✓	1.54	918.10 ✓	
	+65			4.5	919.9 ✓
386				4.5	919.9 ✓
	+50			5.9	918.5 ✓
387				5.6	918.8 ✓
388				5.8	918.4 ✓
	+50			7.2	917.2 ✓
389				8.4	915.8 ✓
T.P.	0.69	915.60 ✓	9.46	914.91 ✓	
390				3.5	912.1 ✓
	+61			5.6	910.0 ✓
	+84			5.5	910.1 ✓

27

PT

$\frac{9.6}{50}$	$\frac{9.8}{33}$	$\frac{9.4}{14}$	9.3	$\frac{9.4}{14}$	$\frac{8.7}{33}$	$\frac{7.7}{50}$
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$\frac{8.6}{50}$	$\frac{8.8}{33}$	$\frac{8.9}{14}$	8.8	$\frac{8.6}{16}$	$\frac{8.2}{33}$	$\frac{6.8}{50}$
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$\frac{4.2}{50}$	$\frac{4.1}{33}$	$\frac{4.4}{14}$	4.4	$\frac{4.7}{14}$	$\frac{4.9}{33}$	$\frac{4.2}{50}$
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$\frac{5.6}{50}$	$\frac{4.7}{33}$	$\frac{4.7}{14}$	4.5	$\frac{5.0}{14}$	$\frac{5.2}{33}$	$\frac{5.2}{50}$
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$\frac{5.3}{50}$	$\frac{4.4}{33}$	$\frac{4.3}{14}$	4.5	$\frac{4.8}{14}$	$\frac{4.8}{33}$	$\frac{4.6}{50}$
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$\frac{7.7}{50}$	$\frac{7.1}{33}$	$\frac{6.9}{14}$	5.9	$\frac{4.5}{14}$	$\frac{2.9}{33}$	$\frac{1.8}{50}$
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$\frac{10.8}{50}$	$\frac{7.3}{33}$	$\frac{7.6}{14}$	5.6	$\frac{4.0}{14}$	$\frac{2.8}{33}$	$\frac{2.4}{50}$
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$\frac{7.6}{50}$	$\frac{6.9}{33}$	$\frac{6.3}{14}$	5.8	$\frac{5.3}{14}$	$\frac{4.9}{33}$	$\frac{4.8}{50}$
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$\frac{7.4}{50}$	$\frac{8.8}{33}$	$\frac{8.0}{14}$	7.2	$\frac{6.4}{14}$	$\frac{5.6}{33}$	$\frac{5.5}{50}$
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$\frac{10.3}{50}$	$\frac{7.6}{33}$	$\frac{8.8}{14}$	8.6	$\frac{8.1}{14}$	$\frac{7.9}{33}$	$\frac{7.8}{50}$
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$\frac{6.7}{50}$	$\frac{5.5}{33}$	$\frac{4.1}{14}$	5.5	$\frac{1.9}{14}$	$\frac{0.9}{33}$	$\frac{1.1}{50}$
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$\frac{8.4}{50}$	$\frac{7.4}{33}$	$\frac{6.1}{14}$	5.4	$\frac{3.8}{14}$	$\frac{2.5}{33}$	$\frac{3.1}{50}$
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$\frac{7.5}{50}$	$\frac{8.4}{33}$	$\frac{7.2}{14}$	5.5	$\frac{5.5}{14}$	$\frac{5.3}{33}$	$\frac{5.6}{50}$
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Sta.	+	H.I.	-	Red.	Elev.
		915.60 ✓			
391				8.1	907.5 ✓
T.P.	1.80	909.47 ✓	10.93	704.67 ✓	
	+50			5.7	901.8 ✓
392				7.6	899.9 ✓
	+50			7.5	900.0 ✓
393				6.1	901.4 ✓
	+50			5.5	902.0 ✓
394				6.1	901.4 ✓
	+50			8.0	899.5 ✓
395				6.2	901.3 ✓ <u>901.2</u>
	+50			3.4	903.9 ✓
T.P.	7.82	916.39 ✓	6.90	906.57 ✓	
396				9.7	906.7 ✓
B.M.			5.72	910.67 ✓	910.68 ✓
397				6.7	909.7 ✓
398				4.0	912.4 ✓

Lt.

Rt.

$\frac{11.2}{50}$ $\frac{9.5}{33}$ $\frac{7.9}{16}$ 8.1 $\frac{8.0}{16}$ $\frac{8.0}{33}$ $\frac{8.1}{50}$

$\frac{8.5}{50}$ $\frac{7.6}{33}$ $\frac{7.0}{16}$ 5.7 $\frac{5.1}{16}$ $\frac{4.3}{33}$ $\frac{3.6}{50}$

$\frac{9.6}{50}$ $\frac{9.3}{33}$ $\frac{8.5}{16}$ 7.6 $\frac{6.7}{16}$ $\frac{5.8}{33}$ $\frac{5.1}{50}$

$\frac{8.8}{50}$ $\frac{8.2}{33}$ $\frac{8.0}{14}$ 7.5 $\frac{6.9}{16}$ $\frac{6.3}{33}$ $\frac{5.6}{50}$

$\frac{6.9}{50}$ $\frac{6.6}{33}$ $\frac{6.0}{16}$ 6.1 $\frac{5.8}{16}$ $\frac{5.5}{33}$ $\frac{4.9}{50}$

$\frac{6.9}{50}$ $\frac{6.2}{33}$ $\frac{5.4}{16}$ 5.5 $\frac{5.4}{16}$ $\frac{5.1}{33}$ $\frac{4.4}{50}$

$\frac{7.5}{50}$ $\frac{6.8}{33}$ $\frac{6.3}{16}$ 6.1 $\frac{5.5}{16}$ $\frac{5.0}{33}$ $\frac{5.0}{50}$

$\frac{8.4}{50}$ $\frac{8.5}{33}$ $\frac{6.3}{16}$ 8.0 $\frac{7.8}{16}$ $\frac{7.4}{33}$ $\frac{7.1}{50}$

$\frac{4.7}{50}$ $\frac{4.5}{33}$ $\frac{4.5}{16}$ 6.2 $\frac{6.2}{16}$ $\frac{6.1}{33}$ $\frac{6.2}{50}$

$\frac{3.2}{50}$ $\frac{4.2}{33}$ $\frac{3.9}{16}$ 3.6 $\frac{2.7}{16}$ $\frac{4.2}{33}$ $\frac{4.2}{50}$

$\frac{9.2}{50}$ $\frac{9.0}{33}$ $\frac{9.8}{16}$ 9.7 $\frac{9.5}{16}$ $\frac{10.7}{33}$ $\frac{10.8}{50}$

$\frac{8.4}{50}$ $\frac{8.1}{33}$ $\frac{7.5}{16}$ 6.7 $\frac{6.0}{16}$ $\frac{6.3}{33}$ $\frac{6.0}{50}$

$\frac{5.0}{50}$ $\frac{4.7}{33}$ $\frac{4.1}{16}$ 4.0 $\frac{3.3}{16}$ $\frac{2.6}{33}$ $\frac{2.2}{50}$

Sta.	+	H.I.	-	Rod.	Elev.
		916.39 ✓			
T.P.	7.90	922.73 ✓	1.54	914.23 ✓	
399				7.4	915.1 ✓
400				5.4	917.1 ✓
401				5.4	917.3 ✓
+50				4.9	917.8 ✓
402				7.7	915.0 ✓
+50				10.1	912.4 ✓
403				11.2	911.5 ✓
+50				11.4	911.3 ✓
T.P.	0.84	912.40 ✓	11.17	911.56 ✓	
404				2.1	910.3 ✓
+17				2.5	909.9 ✓
+45				4.5	907.9 ✓
405				5.2	907.2 ✓
406				5.9	906.5 ✓

Lt.

Rt.

$\frac{8.4}{50}$ $\frac{8.1}{33}$ $\frac{7.6}{14}$ 7.6 $\frac{7.6}{14}$ $\frac{7.6}{33}$ $\frac{7.5}{50}$

$\frac{4.5}{50}$ 5.0 $\frac{5.2}{14}$ 5.4 $\frac{5.7}{14}$ $\frac{6.2}{33}$ $\frac{6.5}{50}$

$\frac{3.6}{50}$ $\frac{4.0}{33}$ $\frac{4.9}{14}$ 5.4 $\frac{5.8}{14}$ $\frac{5.8}{33}$ $\frac{4.2}{50}$

$\frac{6.4}{50}$ $\frac{5.8}{33}$ $\frac{5.4}{14}$ 4.9 $\frac{5.9}{14}$ $\frac{6.4}{33}$ $\frac{7.0}{50}$

$\frac{8.0}{50}$ $\frac{7.9}{33}$ $\frac{7.6}{14}$ 7.7 $\frac{6.7}{14}$ $\frac{6.9}{33}$ $\frac{7.1}{50}$

$\frac{9.9}{50}$ $\frac{9.9}{33}$ $\frac{10.1}{14}$ 10.1 $\frac{10.1}{14}$ $\frac{10.0}{33}$ $\frac{9.6}{50}$

$\frac{11.6}{50}$ $\frac{11.5}{33}$ $\frac{11.4}{14}$ 11.2 $\frac{11.3}{14}$ $\frac{11.3}{33}$ $\frac{10.9}{50}$

$\frac{11.4}{50}$ $\frac{11.5}{33}$ $\frac{11.1}{14}$ 11.4 $\frac{11.6}{14}$ $\frac{11.6}{33}$ $\frac{11.6}{50}$

$\frac{1.8}{50}$ $\frac{1.9}{33}$ $\frac{2.1}{14}$ 2.1 $\frac{2.6}{14}$ $\frac{2.5}{24}$ $\frac{3.1}{37}$ $\frac{3.6}{33}$ $\frac{3.6}{50}$

$\frac{2.1}{50}$ $\frac{2.2}{33}$ $\frac{2.2}{14}$ 2.5 $\frac{3.4}{3}$ $\frac{4.0}{14}$ $\frac{4.1}{33}$ $\frac{4.2}{50}$

$\frac{4.0}{50}$ $\frac{4.1}{47}$ $\frac{4.9}{40}$ $\frac{3.4}{33}$ $\frac{4.2}{14}$ 4.5 $\frac{4.8}{14}$ $\frac{4.9}{33}$ $\frac{5.0}{50}$

$\frac{4.6}{50}$ $\frac{4.7}{33}$ $\frac{5.0}{14}$ 5.2 $\frac{5.1}{14}$ $\frac{5.3}{33}$ $\frac{5.1}{50}$

$\frac{5.5}{50}$ $\frac{5.8}{33}$ $\frac{6.0}{14}$ 5.9 $\frac{5.8}{14}$ $\frac{5.9}{33}$ $\frac{6.0}{50}$

Sta.	+	H.I.	-	Red.	Elev.
		912.40 ✓			
407				4.9	915.5 ✓
408				4.9	905.5 ✓
T.P.	3.20	910.05 ✓	5.55	906.85 ✓	
109				4.7	905.4 ✓
410				5.3	904.8 ✓
	+50			4.9	905.2 ✓
411				4.0	906.1 ✓
	+70			5.7	904.7 ✓ 904.4 ✓
412				5.4	904.7 ✓
	+41			3.8	906.3 ✓
413				3.4	906.5 ✓
	+11			3.1	907.0 ✓
		1.69	906.23 ✓	5.51	904.54 ✓
414				1.7	904.5 ✓
415				5.5	900.7 ✓

LT

RT

51

$$\frac{6.7}{50} \quad \frac{6.8}{33} \quad \frac{6.8}{16} \quad 6.9 \quad \frac{7.0}{14} \quad \frac{7.1}{33} \quad \frac{7.0}{50}$$

$$\frac{6.5}{50} \quad \frac{6.7}{33} \quad \frac{6.7}{16} \quad 6.9 \quad \frac{7.3}{14} \quad \frac{7.2}{33} \quad \frac{6.4}{50}$$

$$\frac{4.7}{50} \quad \frac{4.4}{33} \quad \frac{4.5}{16} \quad 4.7 \quad \frac{4.9}{14} \quad \frac{5.2}{33} \quad \frac{5.2}{50}$$

$$\frac{4.1}{50} \quad \frac{4.7}{33} \quad \frac{5.1}{16} \quad 5.3 \quad \frac{5.7}{14} \quad \frac{5.6}{33} \quad \frac{5.5}{50}$$

$$\frac{4.8}{50} \quad \frac{4.9}{33} \quad \frac{4.7}{16} \quad 4.7 \quad \frac{4.8}{14} \quad \frac{4.8}{33} \quad \frac{4.4}{50}$$

$$\frac{4.1}{50} \quad \frac{4.2}{33} \quad \frac{4.1}{16} \quad 4.0 \quad \frac{4.6}{14} \quad \frac{4.6}{33} \quad \frac{4.9}{50}$$

$$\frac{4.2}{50} \quad \frac{4.8}{33} \quad \frac{5.1}{16} \quad 5.7 \quad \frac{6.4}{16} \quad \frac{6.4}{33} \quad \frac{6.2}{50}$$

$$\frac{4.4}{50} \quad \frac{4.9}{33} \quad \frac{5.3}{16} \quad 5.4 \quad \frac{5.2}{16} \quad \frac{5.2}{33} \quad \frac{5.2}{50}$$

$$\frac{4.5}{50} \quad \frac{4.2}{33} \quad \frac{3.7}{16} \quad 3.8 \quad \frac{4.2}{16} \quad \frac{4.4}{33} \quad \frac{4.5}{50}$$

Barn $\frac{2.4}{41} \quad \frac{2.6}{33} \quad \frac{2.1}{29} \quad \frac{2.7}{14} \quad 3.6 \quad \frac{3.7}{14} \quad \frac{4.5}{33} \quad \frac{4.7}{50}$

Barn $\frac{2.8}{33} \quad \frac{2.6}{25} \quad \frac{2.2}{14} \quad 3.1 \quad \frac{4.1}{14} \quad \frac{4.8}{33} \quad \frac{5.0}{50}$

$$\frac{1.9}{50} \quad \frac{1.8}{33} \quad \frac{1.8}{16} \quad 1.7 \quad \frac{1.7}{14} \quad \frac{2.0}{33} \quad \frac{2.4}{50}$$

$$\frac{5.2}{50} \quad \frac{5.0}{33} \quad \frac{5.4}{16} \quad 5.5 \quad \frac{5.6}{14} \quad \frac{6.0}{33} \quad \frac{6.1}{50}$$

Sta.	+	H.I.	-	Rod	Elev
		906.23	✓		
414				8.5	897.7 ✓
T.P.	2.47	897.79	✓	10.91	895.32 ✓
417				5.4	892.2 ✓
	+50			7.0	890.8 ✓
418				7.1	890.7 ✓
419				7.0	890.8 ✓
	+62			6.3	891.5 ✓
420				4.9	892.9 ✓
	+50			3.8	894.0 ✓
421				4.0	893.8 ✓
	+60			6.5	891.3 ✓
B.M.				7.04	890.73 ✓
					890.73 ✓

Lt.

Rt.

$\frac{6.2}{50}$ $\frac{6.8}{33}$ $\frac{7.8}{14}$ 8.5 $\frac{9.7}{14}$ $\frac{10.9}{33}$ $\frac{11.7}{50}$

$\frac{3.2}{50}$ $\frac{4.3}{33}$ $\frac{4.9}{14}$ 5.4 $\frac{6.3}{14}$ $\frac{6.8}{33}$ $\frac{7.5}{50}$

$\frac{5.0}{50}$ $\frac{5.8}{33}$ $\frac{6.3}{14}$ $\frac{7.4}{23}$ $\frac{8.2}{20}$ $\frac{6.9}{17}$ $\frac{6.7}{14}$ 7.0 $\frac{7.3}{14}$ $\frac{7.3}{21}$ $\frac{8.0}{24}$ $\frac{7.8}{33}$ $\frac{8.4}{50}$

$\frac{6.6}{50}$ $\frac{6.9}{33}$ $\frac{7.1}{16}$ 7.1 $\frac{7.4}{14}$ $\frac{8.0}{33}$ $\frac{8.1}{50}$

$\frac{6.8}{50}$ $\frac{6.7}{33}$ $\frac{7.0}{14}$ 7.0 $\frac{6.7}{14}$ $\frac{6.9}{33}$ $\frac{7.1}{50}$

$\frac{6.3}{50}$ $\frac{6.3}{33}$ $\frac{6.2}{14}$ 6.3 $\frac{6.8}{14}$ $\frac{7.0}{33}$ $\frac{7.0}{50}$

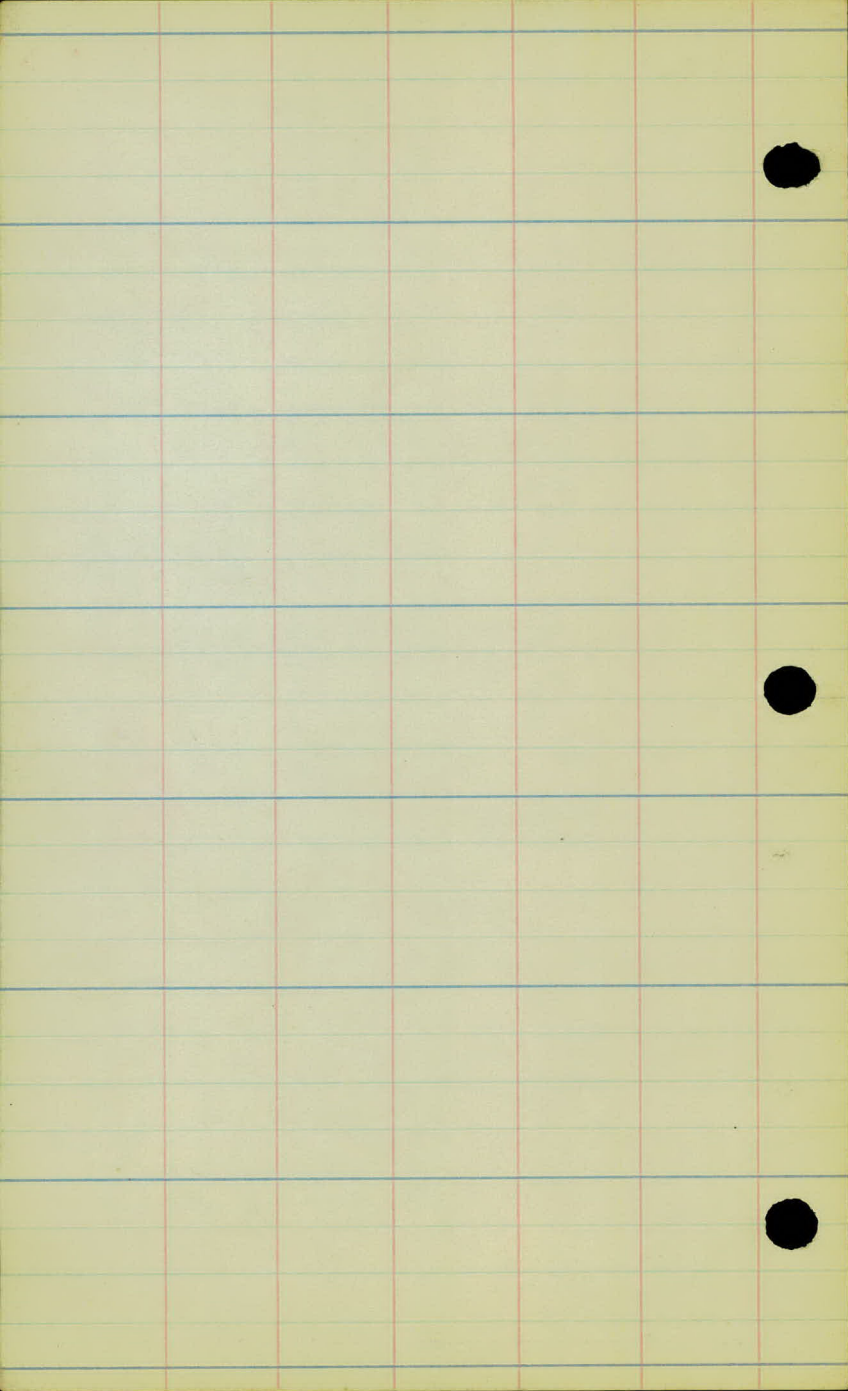
$\frac{4.9}{50}$ $\frac{4.7}{33}$ $\frac{4.8}{16}$ 4.9 $\frac{5.2}{14}$ $\frac{5.5}{33}$ $\frac{5.8}{50}$

$\frac{3.5}{50}$ $\frac{3.4}{33}$ $\frac{3.8}{16}$ 3.8 $\frac{3.9}{14}$ $\frac{4.3}{33}$ $\frac{5.0}{50}$

$\frac{2.7}{50}$ $\frac{2.9}{33}$ $\frac{3.4}{16}$ 4.0 $\frac{4.1}{14}$ $\frac{4.9}{33}$ $\frac{5.1}{50}$

$\frac{3.5}{50}$ $\frac{4.6}{33}$ $\frac{5.9}{14}$ 6.5 $\frac{7.2}{14}$ $\frac{7.4}{33}$ $\frac{7.2}{50}$

spt. in 20" Poplar 136 Rt. Sta. 419 + 35.



X SECTIONS

422 to 439+30

Austin.

B.M.	9.10	899.83 ✓		890.73 ✓
422+00			10.0	89.8 ✓
423+00			8.6	91.2 ✓
+50			7.3	92.5 ✓
424+00			6.7	93.1 ✓
+24			4.7	95.1 ✓
+58			5.4	94.4 ✓
T.P.	4.39	998.80 ✓	5.42	894.41 ✓
+72			8.7	90.1 ✓
425+00			9.3	89.5 ✓
426+00			10.2	88.6 ✓
427+00			10.5	88.3 ✓
+75			9.4	89.4 ✓
428+00			8.0	90.8 ✓
+50			5.0	93.8 ✓

1-19-25

"H" line

54

Spin 20" Pop 136' RT Sta 419+35

$\frac{6.3}{50.0}$	$\frac{8.0}{32.0}$	$\frac{9.0}{16.0}$	10.0	$\frac{9.5}{25.0}$	$\frac{7.6}{50.0}$	✓
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422+00

$\frac{5.0}{50.0}$	$\frac{6.4}{32.0}$	$\frac{7.6}{16.0}$	9.6	$\frac{9.1}{16.0}$	$\frac{8.8}{30.0}$	$\frac{9.8}{50.0}$	✓
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$\frac{3.4}{50.0}$	$\frac{3.7}{42.0}$	$\frac{5.5}{37.0}$	$\frac{6.3}{16.0}$	7.3	$\frac{8.2}{25.0}$	$\frac{9.0}{50.0}$	✓
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L.R.I

$\frac{5.6}{50.0}$	$\frac{5.8}{46.0}$	$\frac{4.6}{38.0}$	$\frac{4.1}{26.0}$	$\frac{5.0}{11.0}$	$\frac{6.6}{5.0}$	6.7	$\frac{7.7}{18.0}$	$\frac{7.7}{35.0}$	$\frac{8.3}{50.0}$	✓
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$\frac{6.8}{50.0}$	$\frac{7.0}{44.0}$	$\frac{6.8}{31.0}$	$\frac{5.1}{29.0}$	$\frac{4.4}{12.0}$	4.7	$\frac{5.5}{9.0}$	$\frac{4.7}{14.0}$	$\frac{8.2}{25.0}$	$\frac{8.3}{48.0}$	$\frac{8.6}{50.0}$	✓
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L.R.I

$\frac{9.6}{50.0}$	$\frac{9.6}{36.0}$	$\frac{9.0}{25.0}$	$\frac{9.2}{9.0}$	5.4	$\frac{4.8}{12.0}$	$\frac{5.3}{25.0}$	$\frac{6.1}{31.0}$	$\frac{9.5}{40.0}$	$\frac{10.0}{50.0}$	✓
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L.R.I

$\frac{9.2}{50.0}$	$\frac{8.4}{27.0}$	$\frac{8.6}{16.0}$	8.7	$\frac{4.8}{6.0}$	$\frac{4.0}{23.0}$	$\frac{4.6}{34.0}$	$\frac{6.0}{42.0}$	$\frac{9.8}{48.0}$	$\frac{9.5}{50.0}$	✓
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L.R.I

$\frac{6.8}{50.0}$	$\frac{9.2}{25.0}$	9.3	$\frac{8.8}{20.0}$	$\frac{5.2}{25.0}$	$\frac{4.4}{41.0}$	$\frac{4.7}{50.0}$	✓
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$\frac{9.8}{50.0}$	$\frac{10.2}{25.0}$	10.2	$\frac{10.3}{25.0}$	$\frac{10.3}{50.0}$	✓
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$\frac{10.4}{50.0}$	$\frac{10.0}{25.0}$	10.5	$\frac{10.2}{25.0}$	$\frac{9.7}{50.0}$	✓
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$\frac{9.6}{50.0}$	$\frac{9.5}{25.0}$	9.4	$\frac{9.2}{12.0}$	$\frac{7.5}{30.0}$	$\frac{7.0}{50.0}$	✓
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$\frac{9.4}{50.0}$	$\frac{9.4}{30.0}$	$\frac{9.0}{16.0}$	$\frac{7.8}{9.0}$	8.0	$\frac{6.7}{16.0}$	$\frac{6.2}{30.0}$	$\frac{5.2}{50.0}$	✓
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$\frac{6.0}{50.0}$	$\frac{5.6}{35.0}$	$\frac{5.2}{16.0}$	5.0	$\frac{4.3}{16.0}$	$\frac{3.6}{32.0}$	$\frac{2.2}{50.0}$	✓
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898.90 ✓

T.P. 0.98 896.78 ✓ 3.00 895.80 ✓

429+00 1.0 95.8 ✓

430+00 4.5 92.3 ✓

+50 7.0 89.8 ✓

431+00 9.8 87.0 ✓

+50 11.4 85.4 ✓

T.P. 1.17 816.50 ✓ 11.45 885.33 ✓

432+00 883.5 ✓

433+00 881.4 ✓

434+00 879.4 ✓

+50 878.0 ✓

435+00 875.5 ✓

+50 874.2

436+00 874.2 ✓

T.P. 2.58 876.83 ✓ 12.25 894.25 ✓

"H" LINE

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$\frac{0.8}{50.0}$	$\frac{0.8}{25.0}$	1.0	$\frac{1.1}{25.0}$	$\frac{1.5}{50.0}$ ✓	<u>429+00</u>
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$\frac{4.3}{50.0}$	$\frac{4.2}{25.0}$	4.5	$\frac{4.6}{20.0}$	$\frac{5.1}{33.0}$	$\frac{5.5}{50.0}$ ✓
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$\frac{6.2}{50.0}$	$\frac{6.4}{33.0}$	$\frac{6.7}{19.0}$	7.0	$\frac{7.8}{18.0}$	$\frac{9.0}{36.0}$	$\frac{9.4}{50.0}$ ✓
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$\frac{8.2}{50.0}$	$\frac{8.6}{32.0}$	$\frac{9.0}{16.0}$	9.8	$\frac{10.6}{18.0}$	$\frac{11.3}{32.0}$	$\frac{12.0}{50.0}$ ✓
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$\frac{11.0}{50.0}$	$\frac{11.0}{32.0}$	$\frac{11.4}{16.0}$	11.4	$\frac{12.0}{13.0}$	$\frac{12.6}{28.0}$	$\frac{14.2}{50.0}$ ✓
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$\frac{2.0}{50.0}$	$\frac{2.6}{39.0}$	$\frac{2.8}{24.0}$	$\frac{3.0}{9.0}$	3.0	$\frac{3.5}{16.0}$	$\frac{4.0}{32.0}$	$\frac{4.5}{50.0}$ ✓
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$\frac{4.0}{50.0}$	$\frac{4.0}{36.0}$	$\frac{5.0}{26.0}$	$\frac{4.5}{12.0}$	5.1	$\frac{5.4}{16.0}$	$\frac{6.5}{33.0}$	$\frac{7.5}{50.0}$ ✓
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$\frac{6.2}{50.0}$	$\frac{6.5}{27.0}$	$\frac{6.7}{13.0}$	7.1	$\frac{7.3}{25.0}$	$\frac{7.6}{40.0}$	$\frac{7.7}{50.0}$ ✓
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$\frac{8.8}{50.0}$	$\frac{8.2}{32.0}$	$\frac{8.5}{22.0}$	8.5	$\frac{8.6}{16.0}$	$\frac{9.3}{32.0}$	$\frac{9.8}{50.0}$ ✓
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$\frac{10.7}{50.0}$	$\frac{11.0}{25.0}$	11.0	$\frac{11.0}{28.0}$	$\frac{11.3}{50.0}$ ✓
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$\frac{11.6}{50.0}$	$\frac{12.2}{25.0}$	12.3	$\frac{11.9}{16.0}$	$\frac{12.0}{36.0}$	$\frac{12.2}{50.0}$ ✓
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$\frac{11.4}{50.0}$	$\frac{12.0}{32.0}$	$\frac{12.3}{18.0}$	12.3	$\frac{12.7}{24.0}$	$\frac{13.0}{38.0}$	$\frac{13.3}{50.0}$ ✓
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876.93 ✓

436 + 20

873.1 ✓

B.M.

4.09 872.74 ✓

+68 Edge. water

970.9 ✓

+83

5.9 970.9 ✓

+96 Edge. water

437 + 00

872.6 ✓

B.M. 4.75 877.48 ✓

872.73 ✓

+28

872.5 ✓

+45

871.3 ✓

+64 to creek

S.B. 863.7
870.9 ✓

+75

871.3 ✓

438 + 00

871.2 ✓

+45

871.3 ✓

+70

S.B. 863.9
870.9 ✓

+94

873.6 ✓

439 + 30

872.9 ✓

T.P. 7.30 880.26 ✓ 4.52 872.96 ✓

43642 $\frac{1.7}{50.0}$ $\frac{2.7}{28.0}$ $\frac{3.0}{120}$ 3.7 $\frac{5.0}{8.0}$ $\frac{5.8}{20.0}$ $\frac{5.0}{27.0}$ $\frac{5.8}{35.0}$ $\frac{5.0}{50.0}$ ✓

$\frac{4.6}{50.0}$ $\frac{4.8}{35.0}$ $\frac{4.6}{23.0}$ $\frac{5.0}{9.0}$ 5.9 $\frac{5.9}{15.0}$ $\frac{5.6}{17.0}$ $\frac{5.5}{30.0}$ $\frac{5.5}{35.0}$ $\frac{5.7}{50.0}$

Top. Ice

Edge Water

$\frac{5.8}{42.1}$ $\frac{4.7}{32.0}$ $\frac{5.2}{20.0}$ $\frac{4.7}{9.0}$ 4.2 $\frac{4.3}{15.0}$ $\frac{4.5}{28.0}$ $\frac{4.4}{50.0}$ ✓

15" Pop. 35' ht 540 438 450

$\frac{5.6}{50.0}$ $\frac{5.7}{36.0}$ $\frac{5.5}{23.0}$ $\frac{6.6}{120}$ $\frac{5.6}{4.0}$ 5.0 $\frac{4.8}{13.0}$ $\frac{5.1}{21.0}$ $\frac{5.7}{32.0}$ $\frac{7.0}{44.0}$ $\frac{6.0}{50.0}$ ✓

$\frac{5.2}{50.0}$ $\frac{5.2}{30.0}$ $\frac{5.6}{20.0}$ $\frac{6.7}{120}$ 6.2 $\frac{5.9}{7.0}$ $\frac{5.1}{14.0}$ $\frac{6.2}{22.0}$ $\frac{6.0}{30.0}$ $\frac{5.2}{42.0}$ $\frac{5.0}{50.0}$ ✓

$\frac{14.1}{6.6}$ $\frac{13.8}{6.6}$ $\frac{14.0}{6.6}$ ✓
25.0 6.6 25.0

$\frac{4.5}{50.0}$ $\frac{5.4}{37.0}$ $\frac{4.2}{24.0}$ $\frac{5.7}{5.0}$ 6.2 $\frac{13.6}{6.6}$ $\frac{13.6}{6.6}$ $\frac{5.4}{47.0}$ $\frac{5.0}{50.0}$ ✓

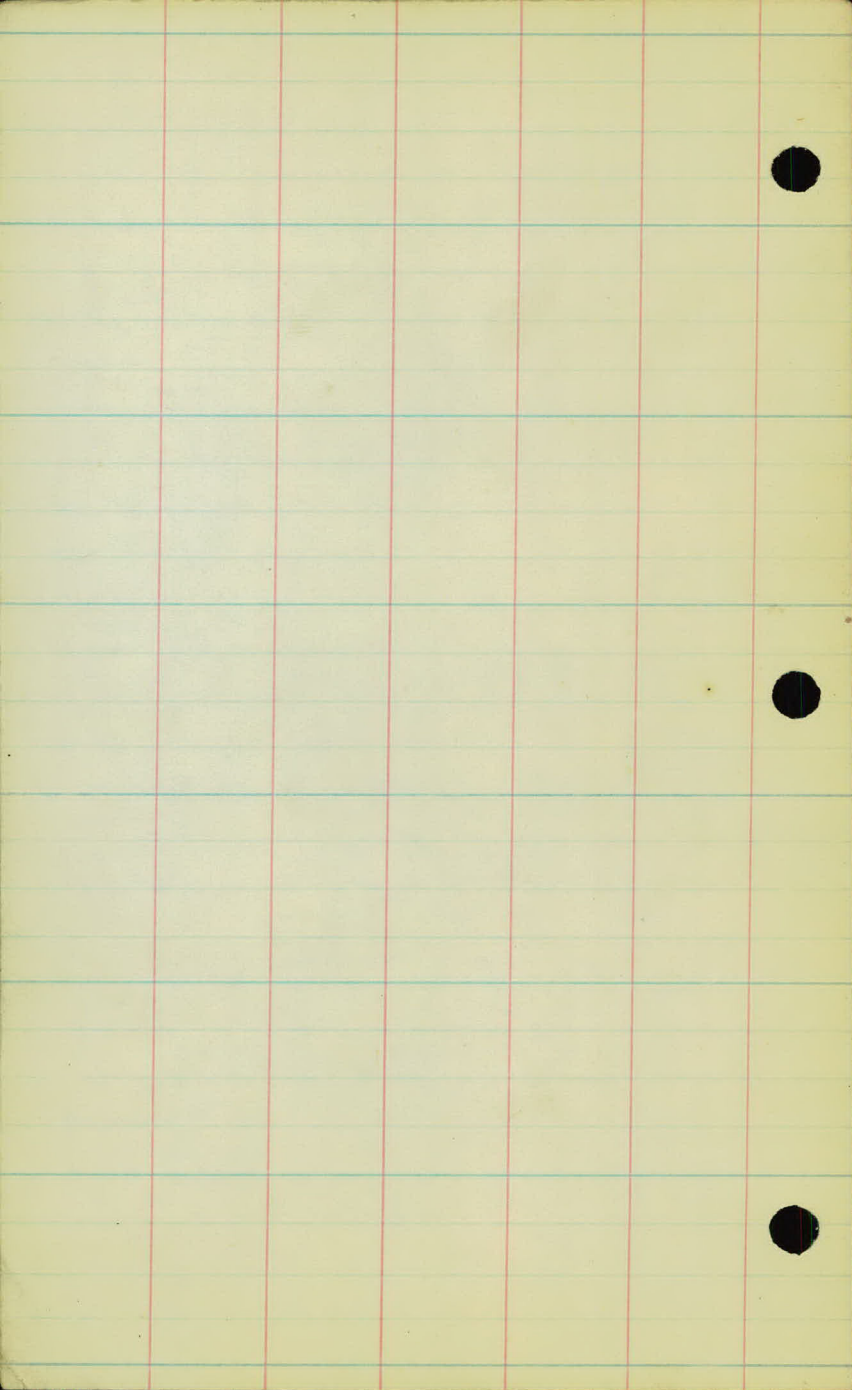
$\frac{6.0}{50.0}$ $\frac{5.6}{23.0}$ $\frac{4.8}{11.0}$ 6.3 $\frac{6.2}{7.0}$ $\frac{5.6}{10.0}$ $\frac{6.0}{22.0}$ $\frac{6.6}{27.0}$ $\frac{11.5}{44.0}$ $\frac{11.5}{50.0}$ ✓
9.6 13.5 13.5
50
39.0

$\frac{5.6}{50.0}$ $\frac{6.6}{40.0}$ $\frac{5.2}{34.0}$ $\frac{5.8}{18.0}$ $\frac{5.2}{8.0}$ 6.2 $\frac{6.5}{10.0}$ $\frac{11.8}{25.0}$ $\frac{6.6}{38.0}$ $\frac{5.7}{42.0}$ $\frac{5.1}{50.0}$ ✓
13.8 13.6

$\frac{11.0}{10.0}$ $\frac{11.0}{8.6}$ $\frac{13.7}{32.0}$ $\frac{13.6}{25}$ 6.6 $\frac{13.6}{6.6}$ $\frac{13.6}{6.6}$ $\frac{11.5}{6.5}$ $\frac{6.0}{24.0}$ $\frac{5.8}{43.0}$ $\frac{5.8}{50.0}$ ✓

$\frac{4.6}{50.0}$ $\frac{5.0}{35.0}$ $\frac{4.5}{19.0}$ 3.9 $\frac{4.9}{17.0}$ $\frac{6.6}{28.0}$ $\frac{7.8}{50.0}$ ✓

$\frac{4.4}{50.0}$ $\frac{4.5}{37.0}$ $\frac{4.8}{16.0}$ 4.6 $\frac{4.6}{9.0}$ $\frac{4.8}{16.0}$ $\frac{4.0}{31.0}$ $\frac{4.7}{41.0}$ $\frac{4.0}{50.0}$



Station + H.I. - Rod. Elev.

880.26 ✓

440+00

72.0 ✓

441+00

72.6 ✓

+64

72.0 ✓

442+00

72.3 ✓

+50

73.3 ✓

443+00

77.2 ✓

+30

76.3 ✓

+73

78.5 ✓

444+00

78.9 ✓

+40

77.5 ✓

443 (~~24" Culvert in place~~) (Vit. Pipell' Cont.)

445+00

77.1 ✓

T.P. 12.75 890.90 ✓ 2.11 878.15 ✓

+50

77.9 ✓

446+00

81.7 ✓

1-19-25

♀

"H" line

58

ht.

ht

$\frac{7.3}{50.0}$	$\frac{8.2}{34.0}$	$\frac{8.0}{17.0}$	$\frac{9.0}{4.0}$	8.3	$\frac{5.6}{16.0}$	$\frac{7.2}{24.0}$	$\frac{6.5}{37.0}$	$\frac{7.0}{50.0}$	✓
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$\frac{7.0}{50.0}$	$\frac{7.6}{32.0}$	$\frac{8.0}{16.0}$	$\frac{7.5}{10.0}$	7.7	$\frac{7.2}{7.0}$	$\frac{8.6}{34.0}$	$\frac{7.2}{46.0}$	$\frac{6.8}{50.0}$	✓
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$\frac{8.7}{50.0}$	$\frac{8.7}{46.0}$	$\frac{8.0}{25.0}$	8.3	$\frac{8.4}{17.0}$	$\frac{7.5}{24.0}$	$\frac{6.0}{40.0}$	$\frac{6.2}{50.0}$
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$\frac{6.0}{50.0}$	$\frac{7.2}{22.0}$	$\frac{7.6}{7.0}$	8.0	$\frac{7.0}{16.0}$	$\frac{6.4}{40.0}$	$\frac{6.2}{50.0}$
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$\frac{5.5}{50.0}$	$\frac{5.0}{42.0}$	$\frac{4.8}{26.0}$	$\frac{5.6}{13.0}$	7.0	$\frac{7.4}{20.0}$	$\frac{7.1}{37.0}$	$\frac{7.0}{50.0}$
--------------------	--------------------	--------------------	--------------------	-----	--------------------	--------------------	--------------------

$\frac{4.0}{50.0}$	$\frac{4.1}{25.0}$	3.1	$\frac{3.5}{25.0}$	$\frac{3.2}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{5.0}{43.0}$	$\frac{3.8}{28.0}$	$\frac{4.2}{14.0}$	4.0	$\frac{3.2}{25.0}$	$\frac{3.1}{50.0}$
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$\frac{4.1}{50.0}$	$\frac{3.5}{26.0}$	$\frac{2.2}{17.0}$	1.8	$\frac{0.7}{25.0}$	$\frac{0.5}{50.0}$
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$\frac{4.0}{50.0}$	$\frac{3.3}{15.0}$	$\frac{1.8}{6.0}$	1.4	$\frac{1.3}{25.0}$	$\frac{0.7}{38.0}$	$\frac{0.8}{50.0}$
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$\frac{3.4}{50.0}$	$\frac{3.2}{34.0}$	$\frac{3.0}{12.0}$	2.8	$\frac{2.5}{25.0}$	$\frac{3.2}{50.0}$
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$\frac{0.5}{50.0}$	$\frac{0.6}{46.0}$	$\frac{1.3}{27.0}$	$\frac{2.7}{12.0}$	3.2	$\frac{3.4}{25.0}$	$\frac{2.7}{50.0}$
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$\frac{11.8}{50.0}$	$\frac{13.1}{25.0}$	13.0	$\frac{12.4}{25.0}$	$\frac{11.3}{42.0}$	$\frac{11.3}{50.0}$
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$\frac{11.0}{50.0}$	$\frac{10.6}{46.0}$	$\frac{9.5}{25.0}$	9.2	$\frac{8.3}{20.0}$	$\frac{8.6}{40.0}$	$\frac{8.6}{50.0}$
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Station	+	H.I.	-	Rod Elev.
		890.90 ✓		
447+00				86.7 ✓
+50				89.9 ✓
T.P.	12.64	902.59 ✓	0.95	889.95 ✓
448+00				92.9 ✓
+70				97.5 ✓
449+00				98.3 ✓
+50				899.0 ✓
T.P.	7.50	909.59 ✓	0.20	902.39 ✓
450+00				901.4 ✓
+50				03.4 ✓
451+00				04.5 ✓
+50				03.7 ✓
452+00				902.5 ✓
T.P.	6.59	904.69 ✓	11.79	898.10 ✓
453+00				899.0 ✓
454+00				94.6 ✓

1-19-25

Ht.

±

"H" line

59

$\frac{4.3}{50.0}$	$\frac{3.5}{40.0}$	$\frac{4.2}{22.0}$	4.2	$\frac{3.7}{25.0}$	$\frac{3.3}{50.0}$
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$\frac{2.0}{50.0}$	$\frac{1.6}{26.0}$	$\frac{0.6}{8.0}$	1.0	$\frac{1.0}{25.0}$	$\frac{0.2}{50.0}$
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$\frac{10.3}{50.0}$	$\frac{10.3}{25.0}$	9.7	$\frac{9.0}{15.0}$	$\frac{9.0}{28.0}$	$\frac{8.8}{50.0}$
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$\frac{6.1}{50.0}$	$\frac{5.5}{42.0}$	$\frac{5.2}{28.0}$	5.1	$\frac{5.2}{25.0}$	$\frac{5.4}{50.0}$
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$\frac{5.0}{50.0}$	$\frac{4.4}{20.0}$	4.8	$\frac{3.7}{22.0}$	$\frac{3.0}{40.0}$	$\frac{3.0}{50.0}$
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$\frac{4.8}{50.0}$	$\frac{4.5}{28.0}$	3.6	$\frac{2.2}{25.0}$	$\frac{1.2}{50.0}$
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$\frac{11.0}{50.0}$	$\frac{9.9}{22.0}$	8.5	$\frac{7.0}{25.0}$	$\frac{5.7}{50.0}$
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$\frac{10.2}{50.0}$	$\frac{9.6}{48.0}$	$\frac{7.7}{22.0}$	6.5	$\frac{4.7}{25.0}$	$\frac{3.7}{50.0}$
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$\frac{9.4}{50.0}$	$\frac{8.7}{38.0}$	$\frac{7.5}{20.0}$	5.4	$\frac{3.8}{25.0}$	$\frac{2.4}{50.0}$
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$\frac{10.3}{50.0}$	$\frac{9.6}{32.0}$	$\frac{7.6}{16.0}$	6.2	$\frac{4.0}{25.0}$	$\frac{1.3}{50.0}$
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$\frac{11.7}{50.0}$	$\frac{10.5}{34.0}$	$\frac{9.1}{16.0}$	7.4	$\frac{5.8}{16.0}$	$\frac{4.8}{32.0}$	$\frac{3.2}{50.0}$
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On P.I. spike Sta 453+50

$\frac{9.8}{50.0}$	$\frac{8.3}{32.0}$	$\frac{6.8}{15.0}$	5.7	$\frac{4.5}{16.0}$	$\frac{3.0}{32.0}$	$\frac{2.0}{50.0}$
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$\frac{12.2}{50.0}$	$\frac{11.2}{25.0}$	10.1	$\frac{9.5}{16.0}$	$\frac{9.0}{38.0}$	$\frac{8.5}{50.0}$
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Station	+	H.I.	-	Rob.	Elev.
		904.69 ✓			
454 + 50					92.1 ✓
T.P.	9.55	901.80 ✓	12.44	892.25 ✓	
455 + 00					91.1 ✓
+ 50					89.2 ✓
456 + 00					88.2 ✓
+ 50					89.7 ✓
457 + 00					92.6 ✓
+ 50					95.5 ✓
458 + 00					97.2 ✓
+ 50					98.6 ✓
T.P.	9.11	908.71 ✓	2.20	899.60 ✓	
459 + 00					99.5 ✓
+ 70					98.2 ✓
460 + 00					899.9 ✓
+ 50					902.7 ✓
B.M.	6.59	908.67 ✓		6.63	902.08 ✓

1-20-25

H.

E

"H" line
R

60

$\frac{12.8}{50.0}$	$\frac{12.6}{27.0}$	$\frac{12.6}{16.0}$	12.6	$\frac{12.2}{25.0}$	$\frac{11.7}{50.0}$
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$\frac{11.0}{50.0}$	$\frac{11.4}{30.0}$	$\frac{11.0}{14.0}$	10.7	$\frac{11.2}{25.0}$	$\frac{11.3}{50.0}$
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$\frac{10.7}{50.0}$	$\frac{12.5}{25.0}$	12.6	$\frac{12.5}{25.0}$	$\frac{12.3}{50.0}$
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$\frac{13.1}{50.0}$	$\frac{13.6}{25.0}$	13.6	$\frac{13.8}{23.0}$	$\frac{13.4}{37.0}$	$\frac{13.0}{50.0}$
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$\frac{10.5}{50.0}$	$\frac{10.5}{34.0}$	$\frac{11.7}{15.0}$	12.1	$\frac{12.4}{24.0}$	$\frac{12.6}{50.0}$
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$\frac{8.0}{50.0}$	$\frac{8.0}{39.0}$	$\frac{8.5}{20.0}$	9.2	$\frac{10.0}{18.0}$	$\frac{10.2}{35.0}$	$\frac{11.0}{50.0}$
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$\frac{2.4}{50.0}$	$\frac{2.7}{38.0}$	$\frac{5.3}{16.0}$	6.3	$\frac{8.3}{16.0}$	$\frac{9.5}{32.0}$	$\frac{10.4}{50.0}$
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$\frac{902.5}{50.0}$	$\frac{0.7}{31.0}$	$\frac{2.4}{21.0}$	4.6	$\frac{6.2}{17.0}$	$\frac{6.8}{34.0}$	$\frac{9.3}{50.0}$
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$\frac{903.7}{50.0}$	$\frac{0.7}{25.0}$	3.2	$\frac{5.4}{25.0}$	$\frac{7.5}{50.0}$
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$\frac{5.5}{50.0}$	$\frac{7.3}{26.0}$	9.2	$\frac{10.9}{23.0}$	$\frac{12.6}{50.0}$
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$\frac{6.6}{50.0}$	$\frac{8.3}{25.0}$	10.5	$\frac{11.4}{14.0}$	$\frac{11.1}{28.0}$	$\frac{10.5}{50.0}$
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$\frac{6.6}{50.0}$	$\frac{9.0}{25.0}$	8.8	$\frac{9.0}{25.0}$	$\frac{8.4}{50.0}$
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$\frac{5.3}{50.0}$	$\frac{6.0}{25.0}$	6.0	$\frac{6.0}{25.0}$	$\frac{6.2}{50.0}$
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Spike in 12" stump. 40' Rt. Sta 460+30

Station	+	H.I.	-	Rod. Elev.
		908.67 ✓		
461+00				904.7 ✓
+50				04.7 ✓
462+00				05.4 ✓
T.P.	7.92	916.12 ✓	0.47	908.20 ✓
+70				10.0 ✓
463+00				11.2 ✓
+50				12.0 ✓
464+00				11.6 ✓
+50				10.6 ✓
465+00				10.7 ✓
+50				11.5 ✓
466+00				12.6 ✓
467+00				14.5 ✓
T.P.	2.05	916.70 ✓	1.47	914.65 ✓

1-20-25

Ht.

L

"H" hine
R.

61

$\frac{3.8}{50.0}$	$\frac{4.3}{25.0}$	4.0	$\frac{3.9}{25.0}$	$\frac{4.7}{50.0}$
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$\frac{3.8}{50.0}$	$\frac{4.1}{25.0}$	4.0	$\frac{3.4}{16.0}$	$\frac{3.7}{36.0}$	$\frac{4.0}{50.0}$
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$\frac{3.2}{50.0}$	$\frac{3.4}{25.0}$	3.3	$\frac{2.9}{25.0}$	$\frac{3.4}{50.0}$
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$\frac{5.7}{50.0}$	$\frac{5.9}{25.0}$	6.1	$\frac{6.5}{25.0}$	$\frac{8.2}{50.0}$
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$\frac{4.2}{50.0}$	$\frac{4.6}{25.0}$	4.9	$\frac{6.0}{25.0}$	$\frac{8.0}{50.0}$
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$\frac{3.7}{50.0}$	$\frac{3.7}{19.0}$	4.1	$\frac{4.8}{16.0}$	$\frac{6.1}{32.0}$	$\frac{8.2}{50.0}$
--------------------	--------------------	-----	--------------------	--------------------	--------------------

$\frac{4.3}{50.0}$	$\frac{4.4}{25.0}$	4.5	$\frac{5.3}{16.0}$	$\frac{6.8}{32.0}$	$\frac{9.1}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.8}{25.0}$	5.5	$\frac{6.9}{18.0}$	$\frac{10.0}{50.0}$
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$\frac{4.6}{50.0}$	$\frac{4.6}{25.0}$	5.4	$\frac{6.9}{16.0}$	$\frac{9.1}{32.0}$	$\frac{10.3}{50.0}$
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$\frac{3.4}{50.0}$	$\frac{3.8}{25.0}$	4.0	$\frac{6.5}{25.0}$	$\frac{8.5}{50.0}$
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$\frac{3.2}{50.0}$	$\frac{3.2}{25.0}$	3.5	$\frac{4.4}{25.0}$	$\frac{5.6}{50.0}$
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$\frac{2.4}{50.0}$	$\frac{2.0}{25.0}$	1.6	$\frac{1.0}{25.0}$	$\frac{0.7}{50.0}$
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Station	+	H.I	-	Rod Elev.	
		916.70	✓		
468+00				13.5	✓
469+00				10.9	✓
470+00				09.0	✓
471+00				07.4	✓
472+00				06.4	✓
T.P.	7.48	914.06	✓	10.12	906.58 ✓
473+00				06.3	✓
474+00				07.0	✓
+50				07.8	✓
475+00				08.7	✓
476+00				09.2	✓
477+00				09.1	✓
B.M	2.91	911.73	✓	5.21	{ 908.82 ✓ 908.85 ✓
+62	± H ²			08.2	✓
478+00				07.3	✓

1-20-25

H.

E

"H" line

R.

62

$\frac{4.7}{50.0}$	$\frac{4.3}{25.0}$	3.2	$\frac{2.5}{28.0}$	$\frac{2.1}{50.0}$
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$\frac{7.6}{50.0}$	$\frac{6.7}{25.0}$	5.9	$\frac{5.0}{25.0}$	$\frac{4.5}{50.0}$
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$\frac{9.0}{50.0}$	$\frac{8.4}{25.0}$	7.7	$\frac{7.4}{25.0}$	$\frac{6.9}{50.0}$
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$\frac{9.4}{50.0}$	$\frac{9.2}{25.0}$	9.3	$\frac{9.3}{25.0}$	$\frac{9.0}{50.0}$
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$\frac{10.0}{50.0}$	$\frac{10.3}{25.0}$	10.3	$\frac{10.2}{25.0}$	$\frac{10.8}{50.0}$
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$\frac{7.6}{50.0}$	$\frac{7.8}{25.0}$	7.8	$\frac{7.7}{25.0}$	$\frac{8.0}{50.0}$
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$\frac{6.7}{50.0}$	$\frac{6.8}{25.0}$	7.1	$\frac{7.5}{25.0}$	$\frac{7.7}{50.0}$
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$\frac{5.4}{50.0}$	$\frac{6.0}{25.0}$	6.8	$\frac{6.6}{25.0}$	$\frac{7.1}{50.0}$
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$\frac{5.0}{50.0}$	$\frac{5.0}{25.0}$	5.4	$\frac{6.2}{25.0}$	$\frac{6.8}{50.0}$
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$\frac{4.3}{50.0}$	$\frac{4.4}{25.0}$	4.9	$\frac{5.6}{25.0}$	$\frac{6.0}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{5.2}{25.0}$	5.0	$\frac{5.0}{29.0}$	$\frac{5.7}{31.0}$	$\frac{5.1}{35.0}$	$\frac{4.7}{50.0}$
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Sp. in T.P. 95' R4 Sta 476-117

$\frac{4.2}{50.0}$	$\frac{4.2}{27.0}$	$\frac{4.8}{20.0}$	$\frac{7.0}{15.0}$	3.5	$\frac{3.5}{13.0}$	$\frac{4.4}{17.0}$	$\frac{3.4}{20.0}$	$\frac{3.5}{50.0}$
--------------------	--------------------	--------------------	--------------------	-----	--------------------	--------------------	--------------------	--------------------

$\frac{4.0}{50.0}$	$\frac{4.0}{38.0}$	$\frac{4.2}{28.0}$	$\frac{5.0}{20.0}$	$\frac{4.5}{17.0}$	4.4	$\frac{4.2}{25.0}$	$\frac{4.0}{50.0}$
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Station	+	H.I	-	Rod Elev.
		911.73 ✓		
479	+00			06.1 ✓
480	+00			04.2 ✓
481	+00			04.9 ✓
	+50			04.9 ✓
482	+00			03.9 ✓
T.P.		3.55 908.32 ✓	6.96	904.77 ✓
	+50			902.0 ✓
483	+00			01.5 ✓
	+50			01.9 ✓
484	+00			03.3 ✓
	+50			03.4 ✓
485	+00			03.1 ✓
	+03	(24" Culv.)		
	+50			03.1 ✓
486	+00			03.9 ✓

1-20-25

"H" line.

63

ht.

♀

RH.

$$\frac{5.5}{50.0} \quad \frac{5.5}{25.0} \quad 5.6 \quad \frac{5.4}{25.0} \quad \frac{5.3}{50.0}$$

$$\frac{7.0}{50.0} \quad \frac{7.2}{25.0} \quad 7.5 \quad \frac{7.5}{25.0} \quad \frac{7.4}{50.0}$$

$$\frac{6.7}{50.0} \quad \frac{6.6}{25.0} \quad 6.8 \quad \frac{6.9}{25.0} \quad \frac{7.3}{50.0}$$

$$\frac{7.1}{50.0} \quad \frac{7.1}{25.0} \quad 6.8 \quad \frac{7.0}{25.0} \quad \frac{7.0}{50.0}$$

$$\frac{9.0}{50.0} \quad \frac{9.0}{25.0} \quad 7.8 \quad \frac{8.0}{25.0} \quad \frac{8.0}{50.0}$$

$$\frac{5.9}{50.0} \quad \frac{6.2}{25.0} \quad 6.3 \quad \frac{6.0}{22.0} \quad \frac{6.0}{50.0}$$

$$\frac{6.6}{50.0} \quad \frac{6.7}{25.0} \quad 6.8 \quad \frac{6.6}{25.0} \quad \frac{6.7}{50.0}$$

$$\frac{5.0}{50.0} \quad \frac{4.7}{32.0} \quad 6.4 \quad \frac{6.3}{22.0} \quad \frac{6.6}{42.0} \quad \frac{7.0}{50.0}$$

$$\frac{3.7}{50.0} \quad \frac{4.2}{25.0} \quad 5.0 \quad \frac{5.2}{21.0} \quad \frac{6.7}{50.0}$$

$$\frac{4.1}{50.0} \quad \frac{4.6}{25.0} \quad 4.9 \quad \frac{5.6}{22.0} \quad \frac{5.6}{42.0} \quad \frac{6.1}{50.0}$$

$$\frac{5.1}{50.0} \quad \frac{4.8}{22.0} \quad 5.2 \quad \text{Witch} \quad \frac{7.5}{8.0} \quad \frac{4.4}{13.0} \quad \frac{4.6}{29.0} \quad \frac{5.2}{50.0}$$

$$\frac{5.7}{50.0} \quad \frac{5.4}{25.0} \quad 5.2 \quad \frac{5.0}{25.0} \quad \frac{4.7}{50.0}$$

$$\frac{5.7}{50.0} \quad \frac{4.8}{20.0} \quad 4.4 \quad \frac{3.6}{25.0} \quad \frac{3.3}{50.0}$$

Station	+	H.I.	-	Rod. Elev.
		908.32		
486+50				904.9 ✓
T.P.	4.37	911.09 ✓	1.60	906.72 ✓
T.P.	3.13	908.81 ✓	5.41	905.68 ✓
B.M.			4.58	904.23 ✓

487+00				906.2 ✓
+50				06.7 ✓
488+00				06.6 ✓
489+00				04.8 ✓
490+00				03.8 ✓
+50				03.7 ✓
491+00				02.9 ✓
+50				01.2 ✓
492+00				899.7 ✓
+50				99.6 ✓

1-20-25

ht.

±

"H" line
Ad.

64

$\frac{4.7}{50.0}$	$\frac{4.1}{36.0}$	$\frac{3.3}{26.0}$	$\frac{3.4}{13.0}$	3.4	$\frac{3.0}{25.0}$	$\frac{2.7}{50.0}$
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Top to stake 487+00

Spike in 15" Oak 70' ht. sta 491+00

$\frac{-1.3}{50.0}$	$\frac{-1.0}{33.0}$	$\frac{-0.5}{18.0}$	$\frac{+0.5}{21.0}$	$\frac{-0.7}{50.0}$
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$\frac{-0.5}{50.0}$	$\frac{-0.2}{25.0}$	$\frac{-0.3}{25.0}$	$\frac{-0.7}{50.0}$
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$\frac{+0.5}{50.0}$	$\frac{+0.2}{27.0}$	$\frac{-0.8}{25.0}$	$\frac{-1.0}{50.0}$
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$\frac{+0.3}{50.0}$	$\frac{0.0}{25.0}$	$\frac{0.0}{25.0}$	$\frac{-0.3}{50.0}$
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$\frac{+0.3}{50.0}$	$\frac{+0.4}{25.0}$	$\frac{+0.2}{25.0}$	$\frac{0.0}{50.0}$
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$\frac{0.0}{50.0}$	$\frac{-0.1}{25.0}$	$\frac{-0.2}{25.0}$	$\frac{-0.5}{50.0}$
--------------------	---------------------	---------------------	---------------------

$\frac{+0.3}{50.0}$	$\frac{0.0}{25.0}$	$\frac{+0.2}{25.0}$	$\frac{+0.8}{50.0}$
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$\frac{-0.7}{50.0}$	$\frac{-0.4}{25.0}$	$\frac{+0.3}{25.0}$	$\frac{+1.0}{36.0}$	$\frac{0.0}{39.0}$	$\frac{+1.2}{45.0}$	$\frac{+1.5}{50.0}$
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$\frac{-0.8}{50.0}$	$\frac{-0.5}{25.0}$	$\frac{+1.0}{25.0}$	$\frac{+3.0}{50.0}$
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$\frac{-1.2}{50.0}$	$\frac{-1.3}{25.0}$	$\frac{+1.8}{25.0}$	$\frac{+3.5}{50.0}$
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Station	+	H.I.	-	Rod.	Elev.
493+00					901.6 ✓
	+50				03.9 ✓
494+00					05.7 ✓
	+50				05.6 ✓
495+00					04.4 ✓
	+50				03.2 ✓
496+00					02.5 ✓
	+50				02.9 ✓
497+00					04.4 ✓
498+00					07.5 ✓
499+00					08.7 ✓
500+00					09.8 ✓
	+50				13.4 ✓
	+50				914.4 ✓

1-20-25

H.

E

"H" line
xl.

65

$$\begin{array}{r} -2.5 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -1.7 \\ \hline 31.0 \end{array} \quad \begin{array}{r} -0.9 \\ \hline 15.0 \end{array}$$

$$\begin{array}{r} +1.5 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +2.8 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -2.1 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -1.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.8 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +1.9 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -1.7 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.7 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -1.2 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -0.6 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.5 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -1.2 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -0.7 \\ \hline 30.0 \end{array} \quad \begin{array}{r} -0.5 \\ \hline 15.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -0.3 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} -0.3 \\ \hline 50.0 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 50.0 \end{array} \quad \begin{array}{r} 0.0 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.5 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ \hline 50.0 \end{array} \quad \begin{array}{r} -0.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} +0.4 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.4 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} +1.7 \\ \hline 50.0 \end{array} \quad \begin{array}{r} +0.8 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} -0.7 \\ \hline 25.0 \end{array} \quad \begin{array}{r} -1.2 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} +2.0 \\ \hline 50.0 \end{array} \quad \begin{array}{r} +1.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} -1.0 \\ \hline 25.0 \end{array} \quad \begin{array}{r} -1.3 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} +1.8 \\ \hline 50.0 \end{array} \quad \begin{array}{r} +0.8 \\ \hline 25.0 \end{array}$$

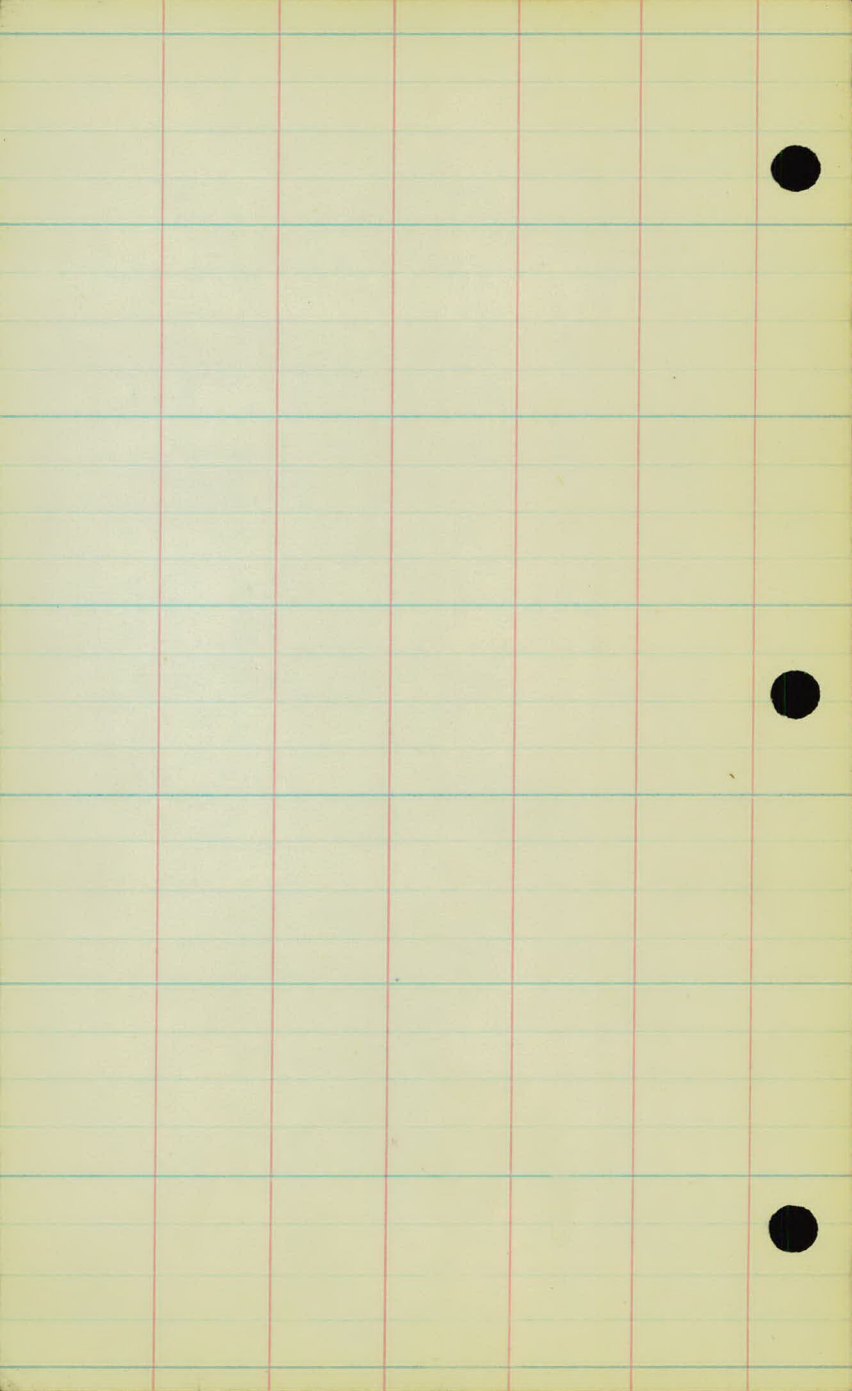
$$\begin{array}{r} -1.0 \\ \hline 25.0 \end{array} \quad \begin{array}{r} -1.4 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50.0 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} -0.6 \\ \hline 25.0 \end{array} \quad \begin{array}{r} -1.0 \\ \hline 50.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 50.0 \end{array} \quad \begin{array}{r} +0.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ \hline 25.0 \end{array} \quad \begin{array}{r} +0.3 \\ \hline 50.0 \end{array}$$



1/21/35

66

Sta.	+	H.I.	-	Red.	Elev.
B.M.	2.83	918.76 ✓		915.93 ✓	
T.P.	7.68	919.82 ✓	4.42	912.14 ✓	
500 + 70				5.2	914.6 ✓
+95				4.8	915.0 ✓
501				7.2	912.4 ✓
+11	Center of cross Ref.			5.9	913.7 ✓
+44				7.4	912.4 ✓
+48				4.4	915.4 ✓
+78				4.7	915.1 ✓
502				5.2	914.4 ✓
503				5.3	914.5 ✓
504				8.9	910.9 ✓
+50				8.8	911.0 ✓
505				8.2	911.4 ✓
T.P.	6.54	915.70 ✓	7.68	912.14 ✓	
506				5.3	913.4 ✓

1/21/26
67

Lt.

Rt.

SpK in 15" Oak 70 Lt. Sta. 509 + 70.

$\frac{6.7}{50}$ $\frac{7.7}{35}$ $\frac{7.0}{32}$ $\frac{4.7}{30}$ $\frac{5.0}{14}$ 5.2 $\frac{5.2}{14}$ $\frac{5.2}{33}$ $\frac{4.9}{50}$ 500 + 70

$\frac{6.9}{50}$ $\frac{6.0}{33}$ $\frac{6.3}{23}$ $\frac{7.6}{4}$ $\frac{6.6}{2}$ 4.8 $\frac{4.9}{14}$ $\frac{4.9}{33}$ $\frac{4.6}{50}$

$\frac{7.4}{50}$ $\frac{6.7}{44}$ $\frac{6.2}{39}$ $\frac{6.0}{27}$ $\frac{6.3}{14}$ 7.2 $\frac{6.3}{4}$ $\frac{4.8}{5}$ $\frac{4.9}{16}$ $\frac{4.9}{33}$ $\frac{4.7}{50}$

$\frac{4.0}{50}$ $\frac{4.0}{33}$ $\frac{4.4}{29}$ $\frac{7.4}{24}$ $\frac{6.6}{23}$ $\frac{6.1}{17}$ 5.9 $\frac{6.2}{9}$ $\frac{7.2}{25}$ $\frac{6.1}{31}$ $\frac{4.5}{33}$ $\frac{4.5}{50}$

$\frac{4.1}{50}$ $\frac{4.2}{33}$ $\frac{4.5}{24}$ $\frac{4.0}{23}$ $\frac{4.2}{16}$ $\frac{4.9}{7}$ 7.4 $\frac{6.7}{6}$ $\frac{5.8}{22}$ $\frac{6.0}{33}$ $\frac{6.9}{50}$

$\frac{4.2}{50}$ $\frac{4.0}{33}$ $\frac{4.6}{28}$ $\frac{4.3}{16}$ 4.4 $\frac{6.9}{3}$ $\frac{6.8}{8}$ $\frac{5.8}{25}$ $\frac{5.8}{33}$ $\frac{6.6}{50}$

$\frac{4.2}{50}$ $\frac{4.4}{33}$ $\frac{4.6}{16}$ 4.7 $\frac{4.3}{14}$ $\frac{4.6}{33}$ $\frac{6.7}{36}$ $\frac{6.5}{42}$ $\frac{6.2}{50}$

$\frac{4.3}{50}$ $\frac{4.5}{33}$ $\frac{4.6}{16}$ 5.2 $\frac{5.1}{14}$ $\frac{4.8}{33}$ $\frac{4.4}{50}$

$\frac{5.1}{50}$ $\frac{5.3}{33}$ $\frac{5.2}{14}$ 5.3 $\frac{5.2}{16}$ $\frac{5.6}{33}$ $\frac{5.9}{50}$

$\frac{7.9}{50}$ $\frac{8.2}{33}$ $\frac{8.4}{16}$ 9.0 $\frac{7.2}{16}$ $\frac{7.1}{33}$ $\frac{7.3}{50}$

$\frac{8.8}{50}$ $\frac{8.5}{33}$ $\frac{8.9}{16}$ 8.8 $\frac{8.8}{14}$ $\frac{9.0}{33}$ $\frac{8.7}{50}$

$\frac{8.5}{50}$ $\frac{8.3}{33}$ $\frac{8.4}{16}$ 8.2 $\frac{8.0}{14}$ $\frac{8.0}{33}$ $\frac{8.3}{50}$

$\frac{5.8}{50}$ $\frac{5.7}{33}$ $\frac{5.4}{16}$ 5.3 $\frac{4.5}{16}$ $\frac{4.8}{33}$ $\frac{4.6}{50}$

Sta.	+	H.I.	-	Red.	E/cv.
		918.70 ✓			
+50				4.5	914.2 ✓
507				4.9	913.8 ✓
508				4.1	914.4 ✓
509				3.3	915.4 ✓
T.P.	4.34	919.72	3.32	915.38 ✓	
510				4.4	915.3 ✓
511				4.3	915.4 ✓
512				7.2	912.5 ✓
+50				8.1	911.4 ✓
513				7.9	911.8 ✓
+50				7.2	912.5 ✓
514				7.2	912.5 ✓
B.M.			3.79	915.93 ✓	915.93 ✓

Lt.

3.79 RT.

$\frac{5.1}{50}$ $\frac{4.8}{33}$ $\frac{4.9}{24}$ $\frac{4.7}{14}$ 4.5 $\frac{4.5}{16}$ $\frac{4.3}{33}$ $\frac{4.6}{50}$ ✓

$\frac{4.7}{50}$ $\frac{4.8}{33}$ $\frac{4.9}{14}$ 4.9 $\frac{5.0}{16}$ $\frac{4.9}{33}$ $\frac{4.7}{50}$ ✓

$\frac{4.7}{50}$ $\frac{4.8}{33}$ $\frac{4.5}{16}$ 4.1 $\frac{3.7}{16}$ $\frac{3.1}{33}$ $\frac{2.9}{50}$ ✓

$\frac{4.2}{50}$ $\frac{4.2}{33}$ $\frac{3.8}{14}$ 3.3 $\frac{3.0}{14}$ $\frac{2.3}{33}$ $\frac{2.3}{50}$ ✓

$\frac{4.7}{50}$ $\frac{4.7}{33}$ $\frac{4.6}{14}$ 4.4 $\frac{4.1}{16}$ $\frac{4.1}{33}$ $\frac{4.1}{50}$ ✓

$\frac{4.6}{50}$ $\frac{4.4}{33}$ $\frac{4.5}{14}$ 4.3 $\frac{4.9}{16}$ $\frac{5.5}{33}$ $\frac{6.2}{50}$ ✓

$\frac{5.8}{50}$ $\frac{6.2}{33}$ $\frac{7.0}{14}$ 7.2 $\frac{7.5}{16}$ $\frac{8.1}{33}$ $\frac{8.2}{50}$ ✓

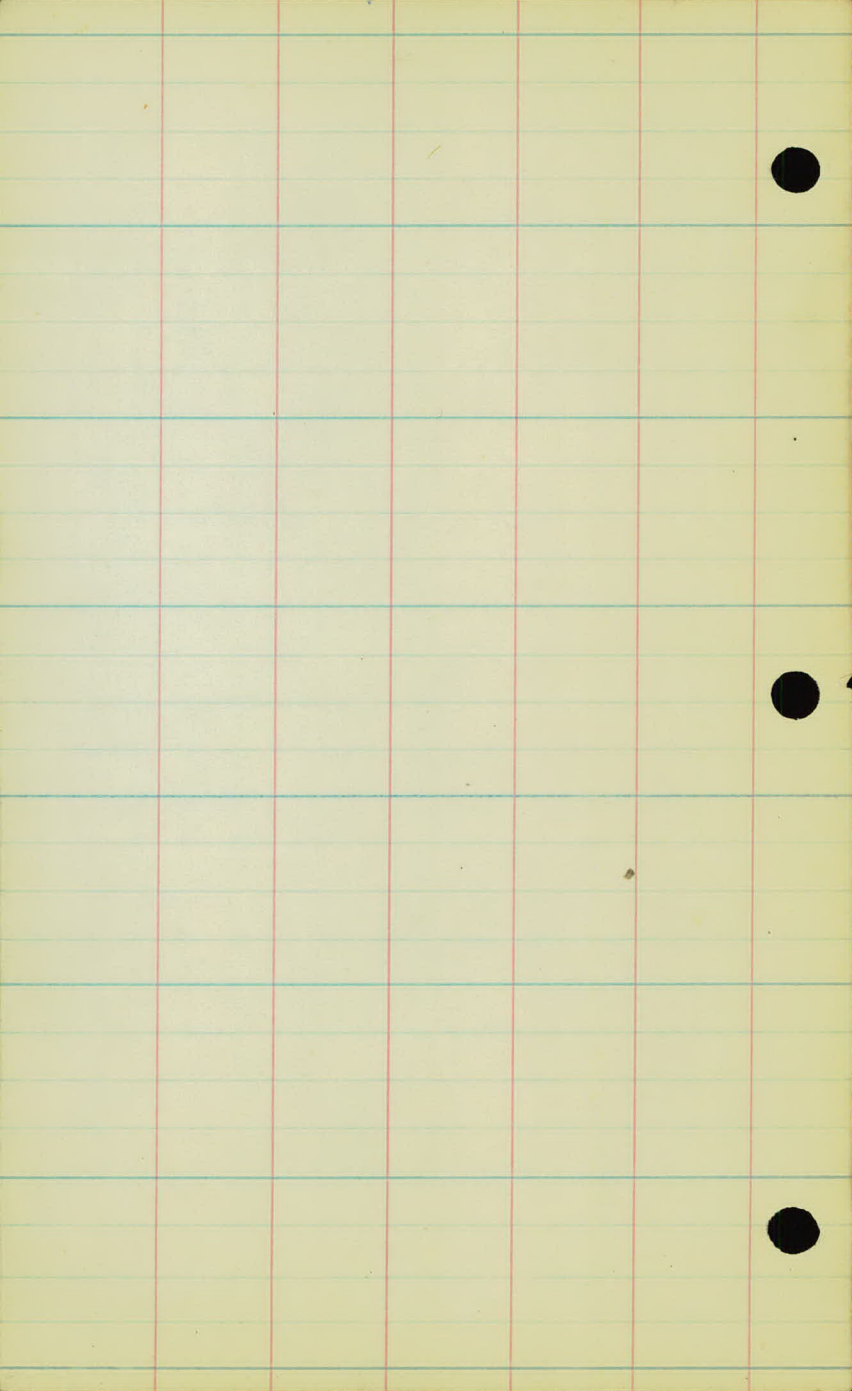
$\frac{7.2}{50}$ $\frac{7.7}{33}$ $\frac{8.1}{14}$ 8.1 $\frac{8.2}{16}$ $\frac{8.2}{33}$ $\frac{8.3}{50}$ ✓

$\frac{8.0}{50}$ $\frac{7.7}{33}$ $\frac{7.8}{14}$ 7.9 $\frac{7.6}{14}$ $\frac{7.7}{33}$ $\frac{7.7}{50}$ ✓

$\frac{7.8}{50}$ $\frac{7.6}{33}$ $\frac{7.3}{14}$ 7.2 $\frac{7.0}{14}$ $\frac{7.2}{33}$ $\frac{7.2}{50}$ ✓

$\frac{8.0}{50}$ $\frac{7.8}{33}$ $\frac{7.3}{14}$ 7.4 $\frac{7.2}{14}$ $\frac{7.5}{33}$ $\frac{7.7}{50}$ ✓

sprk in 15" Oak, 70' Lt. Stg. 509 + 90.



Sta.	+	H.I.	-	Red.	Elev.
B.M.	3.67	919.60 ✓		915.93 ✓	
T.P.	1.68	914.15 ✓	7.15	912.47 ✓	
515					909.4 ✓
	+13				08.7 ✓
516					09.3 ✓
	+45				09.1 ✓
517					07.8 ✓
	+85				06.8 ✓
518					06.8 ✓
	+10				07.1 ✓
	+25				10.8 ✓
	+31				11.2 ✓
	+39				07.1 ✓
	+77				06.7 ✓
	+84				909.0 ✓

Lt.

Rt.

Sp. N. in 15" Oak. 70' Lt. Sta. 509+90.

$\frac{4.5}{50}$ $\frac{4.6}{33}$ $\frac{4.7}{14}$ 4.7 $\frac{4.6}{14}$ $\frac{4.7}{33}$ $\frac{5.0}{50}$ ✓

$\frac{4.4}{50}$ $\frac{4.7}{33}$ $\frac{5.0}{14}$ 5.4 $\frac{5.4}{14}$ $\frac{5.3}{33}$ $\frac{5.3}{50}$ ✓

$\frac{4.1}{50}$ $\frac{4.3}{33}$ $\frac{4.7}{14}$ 4.8 $\frac{5.0}{14}$ $\frac{5.0}{33}$ $\frac{5.1}{50}$ ✓

$\frac{4.0}{50}$ $\frac{4.3}{33}$ $\frac{4.7}{14}$ 5.0 $\frac{5.2}{14}$ $\frac{5.2}{33}$ $\frac{5.4}{50}$ ✓

$\frac{5.3}{50}$ $\frac{5.8}{33}$ $\frac{6.3}{14}$ 6.3 $\frac{6.4}{14}$ $\frac{6.4}{33}$ $\frac{6.0}{50}$ ✓

$\frac{7.2}{50}$ $\frac{8.0}{46}$ $\frac{8.0}{33}$ $\frac{7.9}{14}$ 7.3 $\frac{6.6}{14}$ $\frac{6.1}{33}$ $\frac{5.5}{50}$ ✓

$\frac{3.5}{50}$ $\frac{3.5}{38}$ $\frac{4.7}{33}$ $\frac{6.6}{77}$ $\frac{7.4}{10}$ $\frac{7.8}{18}$ 7.3 $\frac{6.7}{14}$ $\frac{6.3}{33}$ $\frac{5.9}{50}$ ✓

$\frac{3.2}{50}$ $\frac{3.6}{33}$ $\frac{3.6}{30}$ $\frac{4.3}{21}$ $\frac{6.5}{4}$ 7.0 $\frac{6.6}{16}$ $\frac{6.1}{33}$ $\frac{6.0}{50}$ ✓

$\frac{7.8}{50}$ $\frac{7.3}{37}$ $\frac{8.8}{14}$ 3.3 $\frac{3.5}{6}$ $\frac{7.3}{12}$ $\frac{6.2}{33}$ $\frac{6.6}{43}$ $\frac{3.5}{48}$ $\frac{3.2}{50}$ ✓

On Ice →

$\frac{7.3}{50}$ $\frac{7.3}{29}$ $\frac{3.5}{18}$ 2.9 $\frac{6.6}{5}$ $\frac{6.1}{33}$ $\frac{2.8}{41}$ $\frac{4.4}{50}$ ✓

$\frac{7.3}{50}$ $\frac{7.8}{14}$ 7.0 $\frac{6.4}{18}$ $\frac{2.9}{36}$ $\frac{4.4}{41}$ $\frac{3.7}{50}$ ✓

$\frac{7.3}{50}$ 7.4 $\frac{4.2}{6}$ $\frac{5.3}{11}$ $\frac{3.2}{24}$ $\frac{6.2}{34}$ $\frac{6.4}{50}$ ✓

$\frac{7.3}{50}$ $\frac{5.1}{4}$ 5.1 $\frac{5.0}{8}$ $\frac{3.5}{21}$ $\frac{6.6}{29}$ $\frac{6.2}{50}$ ✓

Sta.	+	H.I.	-	Rod. Elev
519		914.15		09.6 ✓
+09				10.7 ✓
+10				06.2 ✓
+50				06.4 ✓
T.P.	390	910.23 ✓	7.82	906.33 ✓
520				06.4 ✓
521				05.4 ✓
+50				05.0 ✓
522				05.5 ✓
523				05.4 ✓
524				05.6 ✓
525				05.9 ✓
+50				06.6 ✓
524				906.6 ✓

Lt.

Rt.

$\frac{7.3}{50}$	$\frac{7.3}{24}$	$\frac{4.3}{17}$	$\frac{5.4}{10}$	4.5	$\frac{2.3}{8}$	$\frac{7.4}{18}$	$\frac{6.7}{44}$	$\frac{4.6}{50}$	✓
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$\frac{7.3}{50}$	$\frac{7.3}{32}$	$\frac{4.4}{24}$	$\frac{5.4}{18}$	$\frac{3.7}{7}$	3.4	$\frac{7.6}{11}$	$\frac{7.3}{40}$	$\frac{6.0}{50}$	✓
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$\frac{7.3}{50}$	$\frac{7.3}{40}$	$\frac{5.1}{34}$	$\frac{5.1}{26}$	$\frac{3.7}{14}$	7.9	$\frac{8.0}{16}$	$\frac{7.2}{27}$	$\frac{7.9}{33}$	$\frac{8.0}{50}$	✓
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$\frac{4.7}{50}$	$\frac{3.7}{36}$	$\frac{7.4}{29}$	$\frac{7.5}{14}$	7.7	$\frac{8.0}{16}$	$\frac{8.1}{33}$	$\frac{7.9}{50}$	✓
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$\frac{3.6}{50}$	$\frac{3.3}{45}$	$\frac{4.0}{33}$	$\frac{3.2}{16}$	3.8	$\frac{3.9}{16}$	$\frac{3.9}{33}$	$\frac{4.1}{50}$	✓
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$\frac{4.1}{50}$	$\frac{4.3}{33}$	$\frac{4.8}{16}$	4.8	$\frac{5.0}{16}$	$\frac{5.2}{33}$	$\frac{5.4}{50}$	✓
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$\frac{4.8}{50}$	$\frac{5.0}{33}$	$\frac{5.1}{16}$	5.2	$\frac{5.2}{16}$	$\frac{5.0}{33}$	$\frac{5.3}{50}$	✓
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$\frac{5.2}{50}$	$\frac{5.0}{33}$	$\frac{4.8}{16}$	4.7	$\frac{4.7}{16}$	$\frac{4.7}{33}$	$\frac{4.7}{50}$	✓
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$\frac{5.0}{50}$	$\frac{5.5}{33}$	$\frac{5.2}{16}$	4.8	$\frac{4.4}{16}$	$\frac{4.3}{33}$	$\frac{3.7}{50}$	✓
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$\frac{4.7}{50}$	$\frac{4.7}{33}$	$\frac{4.5}{16}$	4.4	$\frac{4.5}{16}$	$\frac{4.3}{33}$	$\frac{4.5}{50}$	✓
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$\frac{4.6}{50}$	$\frac{4.6}{33}$	$\frac{4.5}{16}$	4.3	$\frac{4.3}{16}$	$\frac{3.8}{33}$	$\frac{3.5}{50}$	✓
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$\frac{4.2}{50}$	$\frac{4.3}{33}$	$\frac{3.9}{16}$	3.4	$\frac{3.0}{16}$	$\frac{2.7}{33}$	$\frac{2.2}{50}$	✓
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$\frac{3.6}{50}$	$\frac{3.7}{33}$	$\frac{3.7}{16}$	3.4	$\frac{3.5}{16}$	$\frac{3.4}{33}$	$\frac{2.8}{50}$	✓
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Sta.	+	H.I.	-	Rod.	Elev.
		910.23 ✓			
	+50				06.7 ✓
527					07.6 ✓
	6.40	914.17 ✓	1.46	907.77 ✓	
528					07.4
B.M.	4.13	914.19 ✓	4.13	910.04 ✓	910.04 ✓
529					07.3 ✓
530					09.2 ✓
	+40				10.1 ✓
T.P.	7.73	920.35 ✓	1.77	912.42 ✓	
531					12.3 ✓
	+50				13.9 ✓
532					15.0 ✓
	+50				15.4 ✓
533					15.3 ✓
534					16.3 ✓
T.P.	3.51	920.97 ✓	2.89	917.46 ✓	
535					16.6 ✓

Lt.

Rt.

$\frac{2.1}{50}$ $\frac{2.6}{33}$ $\frac{3.1}{14}$ 3.5 $\frac{3.5}{14}$ $\frac{3.3}{33}$ $\frac{3.2}{50}$ ✓

$\frac{1.8}{50}$ $\frac{2.1}{33}$ $\frac{2.5}{14}$ 2.6 $\frac{2.2}{14}$ $\frac{2.2}{33}$ $\frac{2.1}{50}$ ✓

$\frac{7.1}{50}$ $\frac{7.2}{33}$ $\frac{6.9}{14}$ 4.8 $\frac{6.5}{14}$ $\frac{6.1}{33}$ $\frac{5.9}{50}$ ✓

S.P.K. in 24" Oak 75' Lt. Sta. 527732.

$\frac{7.8}{50}$ $\frac{7.4}{33}$ $\frac{7.2}{14}$ 6.9 $\frac{6.6}{14}$ $\frac{6.2}{33}$ $\frac{5.7}{50}$ ✓

$\frac{5.8}{50}$ $\frac{5.8}{33}$ $\frac{5.1}{14}$ 4.9 $\frac{4.5}{14}$ $\frac{4.2}{33}$ $\frac{3.8}{50}$ ✓

$\frac{4.9}{50}$ $\frac{4.7}{33}$ $\frac{4.5}{14}$ 4.1 $\frac{3.0}{14}$ $\frac{2.7}{33}$ $\frac{2.5}{50}$ ✓

$\frac{8.8}{50}$ $\frac{8.6}{33}$ $\frac{8.0}{14}$ 8.0 $\frac{7.6}{14}$ $\frac{7.0}{33}$ $\frac{6.7}{50}$ ✓

$\frac{6.9}{50}$ $\frac{6.8}{33}$ $\frac{6.6}{14}$ 6.4 $\frac{6.1}{14}$ $\frac{6.0}{33}$ $\frac{5.5}{50}$ ✓

$\frac{5.6}{50}$ $\frac{5.6}{33}$ $\frac{5.3}{14}$ 5.3 $\frac{5.2}{14}$ $\frac{5.0}{33}$ $\frac{4.7}{50}$ ✓

$\frac{5.3}{50}$ $\frac{5.2}{33}$ $\frac{5.1}{14}$ 4.9 $\frac{4.6}{14}$ $\frac{4.5}{33}$ $\frac{4.4}{50}$ ✓

$\frac{5.4}{50}$ $\frac{5.4}{33}$ $\frac{5.2}{14}$ 5.0 $\frac{5.0}{14}$ $\frac{4.7}{33}$ $\frac{4.7}{50}$ ✓

$\frac{4.0}{50}$ $\frac{4.1}{33}$ $\frac{4.0}{14}$ 4.0 $\frac{4.1}{14}$ $\frac{4.1}{33}$ $\frac{4.3}{50}$ ✓

$\frac{4.6}{50}$ $\frac{4.7}{33}$ $\frac{4.7}{14}$ 4.4 $\frac{4.6}{14}$ $\frac{4.6}{33}$ $\frac{4.6}{50}$ ✓

Sta.	+	H.I.	-	Rod.	Elev.
		920.97	✓		
536					16.0 ✓
537					14.3 ✓
T.P.	2.34	915.12	✓	8.19	912.78 ✓
538					11.7 ✓
750					09.5 ✓
539					07.9 ✓
540					09.1 ✓
541					10.2 ✓
542					11.0 ✓
543					12.0 ✓
B.M.	6.34	920.31	✓	1.17	913.95 ✓ 913.97 ✓
544					13.0 ✓
545					12.3 ✓
546					12.9 ✓
547					15.5 ✓

Lt.

Rt.

$\frac{6.2}{50}$ $\frac{5.7}{33}$ $\frac{5.2}{16}$ 5.0 $\frac{4.8}{16}$ $\frac{5.1}{33}$ $\frac{5.2}{50}$ ✓

$\frac{6.0}{50}$ $\frac{6.3}{33}$ $\frac{6.4}{16}$ 4.7 $\frac{7.2}{14}$ $\frac{7.7}{33}$ $\frac{8.1}{50}$ ✓

$\frac{2.4}{50}$ $\frac{2.7}{33}$ $\frac{2.9}{16}$ 3.4 $\frac{4.2}{14}$ $\frac{4.9}{33}$ $\frac{5.0}{50}$ ✓

$\frac{4.3}{50}$ $\frac{4.8}{33}$ $\frac{5.1}{16}$ 5.6 $\frac{6.1}{14}$ $\frac{6.3}{33}$ $\frac{6.1}{50}$ ✓

$\frac{6.1}{50}$ $\frac{6.3}{33}$ $\frac{6.8}{16}$ 7.2 $\frac{7.5}{16}$ $\frac{7.1}{33}$ $\frac{6.6}{50}$ ✓

$\frac{6.2}{50}$ $\frac{6.3}{33}$ $\frac{6.2}{16}$ 6.0 $\frac{5.6}{14}$ $\frac{5.2}{33}$ $\frac{4.8}{50}$ ✓

$\frac{5.4}{50}$ $\frac{5.2}{33}$ $\frac{5.3}{16}$ 4.9 $\frac{4.8}{14}$ $\frac{4.7}{33}$ $\frac{4.5}{50}$ ✓

$\frac{4.6}{50}$ $\frac{4.5}{33}$ $\frac{4.2}{16}$ 4.1 $\frac{4.0}{16}$ $\frac{3.8}{33}$ $\frac{3.5}{50}$ ✓

$\frac{4.0}{50}$ $\frac{3.7}{33}$ $\frac{3.5}{16}$ 3.1 $\frac{3.0}{14}$ $\frac{2.7}{33}$ $\frac{2.4}{50}$ ✓

SpK in stump 60 Rt. Sta. 543779.
 $\frac{8.2}{50}$ $\frac{7.9}{33}$ $\frac{7.5}{16}$ 7.3 $\frac{7.2}{16}$ $\frac{7.2}{33}$ $\frac{7.3}{50}$ ✓

$\frac{8.3}{50}$ $\frac{8.2}{33}$ $\frac{8.0}{16}$ 8.0 $\frac{8.0}{16}$ $\frac{8.4}{33}$ $\frac{8.6}{50}$ ✓

$\frac{7.6}{50}$ $\frac{7.5}{33}$ $\frac{7.4}{16}$ 7.4 $\frac{7.6}{14}$ $\frac{7.6}{33}$ $\frac{7.7}{50}$ ✓

$\frac{5.4}{50}$ $\frac{5.2}{33}$ $\frac{5.3}{16}$ 4.8 $\frac{5.0}{14}$ $\frac{5.0}{33}$ $\frac{5.1}{50}$ ✓

Sta.	+	H.I.	-	Red.	Elev.
		720.31	✓		
	+50				16.0 ✓
548					15.0 ✓
549					11.8 ✓
T.P.	5.52	918.21	✓	7.62	912.69 ✓
550					10.3 ✓
	+50				10.6 ✓
551					12.4 ✓
	+50				13.5 ✓
552					13.6 ✓
553					13.1 ✓
554					14.1 ✓
T.P.	1.51	915.76	✓	3.96	914.25 ✓
555					11.8 ✓
556					08.9 ✓
557					07.2 ✓

Sta.	+	H.I.	-	Red.	Elev.
		915.76 ✓			
558					06.2 ✓
	+35				05.6 ✓
559					07.4 ✓
T.P.	10.48	918.81 ✓	7.43	901.33 ✓	
	+50				08.2 ✓
560					10.2 ✓
561					14.1 ✓
	+50				15.4 ✓
562					15.4 ✓
B.M.	5.83	919.23 ✓	5.52	915.43 ✓	913.42 ✓
563					15.8 ✓
564					11.4 ✓
565					13.5 ✓
	+50				14.6 ✓
T.P.	2.63	918.14 ✓	3.72	915.51 ✓	
564					14.9 ✓

Lt.

Pt.

1/21/25
75

$\frac{8.7}{50}$	$\frac{8.9}{33}$	$\frac{9.3}{14}$	9.6	$\frac{10.1}{16}$	$\frac{10.5}{33}$	$\frac{10.4}{50}$	✓
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$\frac{9.0}{50}$	$\frac{9.1}{33}$	$\frac{10.0}{14}$	10.2	$\frac{10.2}{16}$	$\frac{10.4}{33}$	$\frac{10.4}{50}$	✓
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$\frac{7.9}{50}$	$\frac{8.2}{33}$	$\frac{8.4}{16}$	8.4	$\frac{7.0}{16}$	$\frac{9.0}{33}$	$\frac{9.2}{50}$	✓
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$\frac{9.8}{50}$	$\frac{10.1}{33}$	$\frac{10.8}{14}$	10.6	$\frac{10.9}{16}$	$\frac{10.9}{33}$	$\frac{11.1}{50}$	✓
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$\frac{7.7}{50}$	$\frac{7.9}{33}$	$\frac{8.2}{16}$	8.6	$\frac{7.9}{16}$	$\frac{9.4}{33}$	$\frac{9.5}{50}$	✓
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$\frac{5.3}{50}$	$\frac{5.2}{33}$	$\frac{4.9}{14}$	4.7	$\frac{4.4}{16}$	$\frac{4.2}{33}$	$\frac{4.2}{50}$	✓
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$\frac{3.8}{50}$	$\frac{3.7}{33}$	$\frac{3.4}{14}$	3.4	$\frac{3.5}{16}$	$\frac{3.2}{33}$	$\frac{3.7}{50}$	✓
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$\frac{3.1}{50}$	$\frac{3.3}{33}$	$\frac{3.4}{14}$	3.4	$\frac{3.6}{16}$	$\frac{3.8}{33}$	$\frac{4.0}{50}$	✓
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SpK in Stumpf 50 Lt. Sta. 560 + 65

$\frac{4.1}{50}$	$\frac{4.4}{33}$	$\frac{4.7}{14}$	5.4	$\frac{5.2}{16}$	$\frac{5.3}{33}$	$\frac{5.5}{50}$	✓
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$\frac{7.2}{50}$	$\frac{7.7}{33}$	$\frac{7.9}{15}$	7.8	$\frac{7.7}{16}$	$\frac{7.7}{33}$	$\frac{7.6}{50}$	✓
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$\frac{5.3}{50}$	$\frac{5.4}{33}$	$\frac{5.6}{14}$	5.7	$\frac{5.7}{16}$	$\frac{5.6}{33}$	$\frac{5.4}{50}$	✓
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$\frac{4.4}{50}$	$\frac{4.7}{33}$	$\frac{4.7}{14}$	4.6	$\frac{4.6}{16}$	$\frac{4.7}{33}$	$\frac{4.4}{50}$	✓
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$\frac{3.3}{50}$	$\frac{3.2}{33}$	$\frac{3.2}{14}$	3.2	$\frac{3.2}{16}$	$\frac{3.3}{33}$	$\frac{3.4}{50}$	✓
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Sta		H.I.	-	Rock	Elev.
567		918.14 ✓			15.0 ✓
	+50				15.1 ✓
568					13.9 ✓
569					08.4 ✓
	+63				07.9 ✓
570					08.1 ✓
	+50				09.2 ✓
571					12.6 ✓
T.P.	2.35	917.97 ✓	2.52	915.62 ✓	
	+50				14.3 ✓
572					15.2 ✓
	+50				15.1 ✓
573					13.6 ✓
	+50				11.8 ✓

Lt.

Rt.

$\frac{2.8}{50}$	$\frac{2.9}{33}$	$\frac{3.0}{16}$	3.1	$\frac{3.2}{16}$	$\frac{3.5}{33}$	$\frac{3.9}{50}$	✓
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$\frac{3.4}{50}$	$\frac{3.2}{33}$	$\frac{3.0}{16}$	3.0	$\frac{3.2}{16}$	$\frac{3.5}{33}$	$\frac{3.9}{50}$	✓
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$\frac{5.2}{50}$	$\frac{4.7}{33}$	$\frac{3.7}{16}$	4.2	$\frac{3.6}{16}$	$\frac{3.6}{33}$	$\frac{3.8}{50}$	✓
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$\frac{10.6}{50}$	$\frac{10.6}{33}$	$\frac{10.6}{16}$	9.7	$\frac{8.8}{16}$	$\frac{7.8}{33}$	$\frac{6.7}{50}$	✓
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$\frac{11.0}{50}$	$\frac{10.6}{33}$	$\frac{10.3}{16}$	10.2	$\frac{9.8}{16}$	$\frac{9.2}{33}$	$\frac{8.1}{50}$	✓
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$\frac{11.2}{50}$	$\frac{10.5}{33}$	$\frac{10.3}{16}$	10.0	$\frac{9.9}{16}$	$\frac{9.2}{33}$	$\frac{8.1}{50}$	✓
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$\frac{9.6}{50}$	$\frac{9.3}{33}$	$\frac{9.1}{16}$	8.9	$\frac{8.4}{16}$	$\frac{7.8}{33}$	$\frac{6.8}{50}$	✓
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$\frac{6.3}{50}$	$\frac{6.0}{33}$	$\frac{5.7}{16}$	5.5	$\frac{5.7}{16}$	$\frac{5.3}{33}$	$\frac{4.8}{50}$	✓
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$\frac{3.5}{50}$	$\frac{3.4}{33}$	$\frac{3.7}{16}$	3.7	$\frac{3.7}{16}$	$\frac{3.8}{33}$	$\frac{3.8}{50}$	✓
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$\frac{2.1}{50}$	$\frac{2.5}{33}$	$\frac{2.7}{16}$	2.8	$\frac{3.1}{16}$	$\frac{3.3}{33}$	$\frac{3.4}{50}$	✓
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$\frac{2.2}{50}$	$\frac{2.4}{33}$	$\frac{2.6}{16}$	2.7	$\frac{3.2}{16}$	$\frac{3.6}{33}$	$\frac{3.7}{50}$	✓
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$\frac{3.2}{50}$	$\frac{3.4}{33}$	$\frac{3.7}{16}$	4.4	$\frac{4.2}{16}$	$\frac{4.7}{33}$	$\frac{4.8}{50}$	✓
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$\frac{5.3}{50}$	$\frac{5.6}{33}$	$\frac{5.8}{16}$	4.2	$\frac{6.3}{16}$	$\frac{6.3}{33}$	$\frac{6.3}{50}$	✓
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Sta	+	H.I.	-	Rock	Elev
		717.97 ✓			
574					09.9 ✓
	+40				09.6 ✓
575					09.9 ✓
T.P.	5.94	717.97 ✓	5.94	712.03 ✓	
576					13.1 ✓
577					13.0 ✓
B.M.			4.77	713.22 ✓	713.20 ✓
578					13.3 ✓
T.P.	6.45	919.70 ✓	4.74	913.25 ✓	
	+50				14.2 ✓
579					14.8 ✓
580					14.6 ✓
581					15.1 ✓
	+50				14.2 ✓
T.P.	2.44	917.74 ✓	4.42	915.28 ✓	
582					11.9 ✓
	+50				910.0 ✓

Lt.

Rt.

$\frac{78}{50}$ $\frac{78}{33}$ $\frac{8.0}{14}$ 8.1 $\frac{7.9}{14}$ $\frac{7.8}{33}$ $\frac{7.6}{50}$ ✓

$\frac{8.7}{50}$ $\frac{8.7}{33}$ $\frac{8.6}{14}$ 8.4 $\frac{8.0}{14}$ $\frac{7.7}{33}$ $\frac{7.5}{50}$ ✓

$\frac{8.2}{50}$ $\frac{7.9}{33}$ $\frac{7.4}{14}$ 7.1 $\frac{6.3}{14}$ $\frac{6.9}{33}$ $\frac{7.1}{50}$ ✓

$\frac{5.7}{50}$ $\frac{5.3}{33}$ $\frac{5.1}{14}$ 4.9 $\frac{5.0}{14}$ $\frac{5.4}{33}$ $\frac{5.8}{50}$ ✓

$\frac{4.4}{50}$ $\frac{4.3}{33}$ $\frac{4.1}{14}$ 5.0 $\frac{5.3}{14}$ $\frac{6.1}{33}$ $\frac{6.6}{50}$ ✓

Spk. in 15" Oak 50' Lt. Stg. 576 + 35.

$\frac{3.7}{50}$ $\frac{3.9}{33}$ $\frac{4.2}{14}$ 4.7 $\frac{5.2}{14}$ $\frac{5.8}{33}$ $\frac{6.4}{50}$ ✓

$\frac{5.0}{50}$ $\frac{5.0}{33}$ $\frac{5.2}{14}$ 5.5 $\frac{6.0}{14}$ $\frac{6.3}{33}$ $\frac{6.9}{50}$ ✓

$\frac{4.9}{50}$ $\frac{4.8}{33}$ $\frac{4.9}{14}$ 4.9 $\frac{4.7}{14}$ $\frac{5.5}{33}$ $\frac{5.9}{50}$ ✓

$\frac{5.7}{50}$ $\frac{5.4}{33}$ $\frac{5.3}{14}$ 5.1 $\frac{4.9}{14}$ $\frac{5.3}{33}$ $\frac{5.5}{50}$ ✓

$\frac{5.4}{50}$ $\frac{5.2}{33}$ $\frac{5.0}{14}$ 4.4 $\frac{4.6}{14}$ $\frac{4.5}{33}$ $\frac{4.5}{50}$ ✓

$\frac{7.1}{50}$ $\frac{6.7}{33}$ $\frac{6.3}{14}$ 5.5 $\frac{5.0}{14}$ $\frac{4.6}{33}$ $\frac{4.5}{50}$ ✓

$\frac{8.6}{50}$ $\frac{8.2}{33}$ $\frac{7.8}{14}$ 5.8 $\frac{4.9}{14}$ $\frac{3.7}{33}$ $\frac{3.1}{50}$ ✓

$\frac{9.6}{50}$ $\frac{7.9}{44}$ $\frac{7.9}{33}$ $\frac{8.8}{14}$ 7.7 $\frac{6.5}{14}$ $\frac{5.9}{33}$ $\frac{4.1}{50}$ ✓

Sta + H.I. - Rod. Elev.
 717.74 ✓

583 10.9 ✓

584 12.3 ✓

585 12.4 ✓

584 12.3 ✓

+50 11.3 ✓

587 11.4 ✓

TO R-104 ✓

T.P. 2.46 913.81 ✓ 6.39 911.35 ✓

~~+50 11.5 ✓~~

588 11.9 ✓

~~+50 11.6 ✓~~

589 10.7 ✓

B.M. 2.90 910.91 ✓ 910.39 ✓

~~+50 09.4 ✓~~

590 08.7 ✓

~~+50 09.4 ✓~~

Lt.

Rt.

$\frac{5.1}{50}$ $\frac{8.0}{33}$ $\frac{7.5}{14}$ 4.8 $\frac{5.9}{14}$ $\frac{5.1}{33}$ $\frac{4.7}{50}$

$\frac{6.0}{50}$ $\frac{6.1}{33}$ $\frac{5.8}{14}$ 5.4 $\frac{5.3}{14}$ $\frac{5.0}{33}$ $\frac{4.6}{50}$

$\frac{5.5}{50}$ $\frac{5.6}{33}$ $\frac{5.2}{14}$ 5.3 $\frac{5.1}{14}$ $\frac{5.0}{33}$ $\frac{4.7}{50}$

$\frac{6.5}{50}$ $\frac{5.8}{33}$ $\frac{5.5}{14}$ 5.4 $\frac{5.4}{14}$ $\frac{5.3}{33}$ $\frac{5.0}{50}$

$\frac{6.3}{50}$ $\frac{6.3}{33}$ $\frac{4.5}{14}$ 6.4 $\frac{6.1}{14}$ $\frac{6.1}{33}$ $\frac{6.1}{50}$

$\frac{6.3}{50}$ $\frac{6.5}{33}$ $\frac{6.3}{14}$ 6.3 $\frac{6.5}{14}$ $\frac{6.6}{33}$ $\frac{6.6}{50}$

$\frac{2.3}{50}$ $\frac{2.3}{33}$ $\frac{2.3}{14}$ 2.3 $\frac{2.2}{14}$ $\frac{2.2}{33}$ $\frac{2.2}{50}$

$\frac{2.3}{50}$ $\frac{2.3}{33}$ $\frac{2.2}{14}$ 1.9 $\frac{2.1}{14}$ $\frac{1.7}{33}$ $\frac{1.4}{50}$

$\frac{2.8}{50}$ $\frac{2.6}{33}$ $\frac{2.4}{14}$ 2.2 $\frac{1.9}{14}$ $\frac{1.6}{33}$ $\frac{1.4}{50}$

$\frac{4.0}{50}$ $\frac{3.9}{33}$ $\frac{3.5}{14}$ 3.1 $\frac{2.8}{14}$ $\frac{2.6}{33}$ $\frac{2.5}{50}$

Spr. in 20" Oak 110 ft. Sta. 588 + 50

$\frac{5.7}{50}$ $\frac{5.3}{33}$ $\frac{4.6}{14}$ 4.4 $\frac{4.2}{14}$ $\frac{4.0}{33}$ $\frac{3.8}{50}$

$\frac{5.9}{50}$ $\frac{5.6}{33}$ $\frac{5.6}{14}$ 5.1 $\frac{4.7}{14}$ $\frac{4.8}{33}$ $\frac{4.2}{50}$

$\frac{5.7}{50}$ $\frac{5.4}{33}$ $\frac{4.6}{12}$ 4.4 $\frac{4.1}{14}$ $\frac{3.8}{33}$ $\frac{3.7}{50}$

Sta	+	H.I.	-	Rod.	Elev.
591		913.51 ✓			09.8 ✓
+50					09.8 ✓
592					09.1 ✓
+50					08.5 ✓
593					08.8 ✓
+64 ²					10.1 ✓
T.P.	8.37	918.54 ✓	3.64	916.17 ✓	
594					10.6 ✓
+50					11.5 ✓
595					11.9 ✓
+50					12.8 ✓
596					12.8 ✓
+50					12.6 ✓
597					13.1 ✓

LH.

RT.

$\frac{5.4}{50}$ $\frac{5.1}{33}$ $\frac{4.3}{16}$ $\frac{4.2}{8}$ 4.0 $\frac{3.5}{16}$ $\frac{3.0}{33}$ $\frac{2.5}{50}$

$\frac{6.8}{50}$ $\frac{5.9}{33}$ $\frac{4.6}{14}$ 4.0 $\frac{3.4}{16}$ $\frac{2.8}{33}$ $\frac{2.7}{50}$

$\frac{6.7}{50}$ $\frac{6.2}{33}$ $\frac{5.3}{14}$ 4.7 $\frac{4.0}{7}$ $\frac{2.9}{33}$ $\frac{2.9}{50}$

$\frac{7.9}{50}$ $\frac{6.9}{33}$ $\frac{6.1}{16}$ 5.3 $\frac{4.4}{16}$ $\frac{3.8}{33}$ $\frac{3.0}{50}$

$\frac{7.3}{50}$ $\frac{6.7}{33}$ $\frac{5.5}{16}$ 5.0 $\frac{4.2}{16}$ $\frac{3.6}{33}$ $\frac{3.2}{50}$

$\frac{6.6}{50}$ $\frac{6.0}{33}$ $\frac{5.2}{23}$ $\frac{4.4}{14}$ 3.9 $\frac{3.3}{16}$ $\frac{3.2}{33}$ $\frac{3.4}{50}$

$\frac{10.8}{50}$ $\frac{7.8}{33}$ $\frac{8.5}{14}$ 7.9 $\frac{7.5}{14}$ $\frac{7.4}{33}$ $\frac{7.6}{50}$

$\frac{8.8}{50}$ $\frac{7.8}{33}$ $\frac{7.5}{14}$ 7.0 $\frac{6.6}{16}$ $\frac{6.6}{33}$ $\frac{6.4}{50}$

$\frac{7.7}{50}$ $\frac{7.3}{33}$ $\frac{6.9}{14}$ 6.6 $\frac{6.3}{16}$ $\frac{6.0}{33}$ $\frac{5.5}{50}$

$\frac{7.1}{50}$ $\frac{6.4}{33}$ $\frac{6.1}{14}$ 5.7 $\frac{5.8}{14}$ $\frac{5.5}{33}$ $\frac{5.0}{50}$

$\frac{7.1}{50}$ $\frac{6.4}{33}$ $\frac{6.0}{14}$ 5.7 $\frac{5.8}{14}$ $\frac{5.7}{33}$ $\frac{5.5}{50}$

$\frac{7.4}{50}$ $\frac{6.8}{33}$ $\frac{5.9}{14}$ 5.9 $\frac{5.9}{14}$ $\frac{5.8}{33}$ $\frac{5.7}{50}$

$\frac{6.9}{50}$ $\frac{6.3}{33}$ $\frac{5.5}{14}$ 5.4 $\frac{5.5}{14}$ $\frac{5.3}{33}$ $\frac{5.6}{50}$

Sta.	+	H.I.	-	Red.	Elev.
		718.54 ✓			
598					15.4 ✓
599					15.2 ✓
T.P.	3.58	719.47 ✓	2.63	715.91 ✓	
600					14.8 ✓
+50					12.7 ✓
601					11.6 ✓
+50					11.8 ✓
602					13.3 ✓
+47					14.1 ✓
+69					12.4 ✓
603					12.0 ✓
+19					13.2 ✓
+72					12.9 ✓
604		Farm Rd. on Rt.			12.9 ✓

Lt.

Rt.

$\frac{46}{50}$ $\frac{3.9}{33}$ $\frac{3.4}{16}$ 3.1 $\frac{3.4}{16}$ $\frac{3.2}{33}$ $\frac{3.5}{50}$

$\frac{3.7}{50}$ $\frac{3.7}{33}$ $\frac{3.2}{16}$ 3.3 $\frac{3.4}{14}$ $\frac{3.9}{33}$ $\frac{4.0}{50}$

$\frac{3.0}{50}$ $\frac{5.1}{33}$ $\frac{4.7}{16}$ 4.7 $\frac{4.8}{14}$ $\frac{5.0}{33}$ $\frac{5.3}{50}$

$\frac{7.3}{63}$ $\frac{7.1}{56}$ $\frac{8.6}{53}$ $\frac{8.3}{50}$ $\frac{6.4}{43}$ $\frac{6.6}{33}$ $\frac{6.7}{14}$ 6.8 $\frac{6.8}{14}$ $\frac{6.8}{33}$ $\frac{6.9}{50}$

5.0 $\frac{6.8}{43}$ $\frac{8.6}{39}$ $\frac{8.6}{36}$ $\frac{7.9}{33}$ $\frac{8.2}{14}$ 7.9 $\frac{7.9}{14}$ $\frac{7.8}{33}$ $\frac{7.6}{50}$

$\frac{7.2}{50}$ $\frac{7.2}{33}$ $\frac{6.8}{31}$ $\frac{8.6}{28}$ $\frac{8.2}{24}$ $\frac{7.9}{25}$ $\frac{7.9}{14}$ 7.7 $\frac{7.7}{14}$ $\frac{7.5}{33}$ $\frac{7.6}{50}$

$\frac{6.7}{50}$ $\frac{6.9}{33}$ $\frac{6.9}{17}$ $\frac{7.8}{14}$ $\frac{6.2}{10}$ 6.2 $\frac{6.2}{14}$ $\frac{6.3}{33}$ $\frac{6.3}{50}$

$\frac{8.2}{50}$ $\frac{8.5}{48}$ $\frac{6.9}{44}$ $\frac{6.9}{33}$ $\frac{6.2}{11}$ $\frac{7.5}{8}$ $\frac{7.5}{5}$ 5.4 $\frac{4.8}{16}$ $\frac{4.7}{33}$ $\frac{4.7}{50}$

$\frac{7.9}{50}$ $\frac{8.4}{45}$ $\frac{6.9}{42}$ $\frac{6.9}{33}$ $\frac{6.2}{7}$ $\frac{7.7}{4}$ 7.1 $\frac{5.2}{5}$ $\frac{5.0}{33}$ $\frac{5.0}{50}$

$\frac{8.7}{50}$ $\frac{8.1}{40}$ $\frac{6.8}{38}$ $\frac{6.8}{33}$ $\frac{6.3}{3}$ 7.5 $\frac{6.9}{5}$ $\frac{4.7}{10}$ $\frac{4.8}{33}$ $\frac{5.0}{50}$

$\frac{8.0}{50}$ $\frac{8.1}{36}$ $\frac{6.8}{34}$ $\frac{6.8}{33}$ $\frac{6.7}{14}$ 6.3 $\frac{7.4}{3}$ $\frac{7.0}{7}$ $\frac{5.1}{13}$ $\frac{4.9}{33}$ $\frac{5.0}{50}$

$\frac{6.4}{50}$ $\frac{5.2}{33}$ $\frac{8.1}{38}$ $\frac{6.4}{26}$ $\frac{6.7}{14}$ 6.6 $\frac{6.0}{10}$ $\frac{6.6}{11}$ $\frac{6.2}{18}$ $\frac{5.1}{20}$ $\frac{4.6}{33}$ $\frac{4.2}{50}$

$\frac{5.8}{50}$ $\frac{6.0}{43}$ $\frac{8.0}{33}$ $\frac{8.4}{30}$ $\frac{8.2}{26}$ $\frac{6.7}{24}$ 6.6 $\frac{6.3}{4}$ $\frac{5.6}{21}$ $\frac{5.0}{33}$ $\frac{4.9}{50}$ $\frac{4.6}{100}$

Sta.	+	H.I.	-	Roof.	Elev.
		919.49	✓		
605					12.8 ✓
604					12.7 ✓
B.M.			3.90	915.59 ✓	915.57 ✓

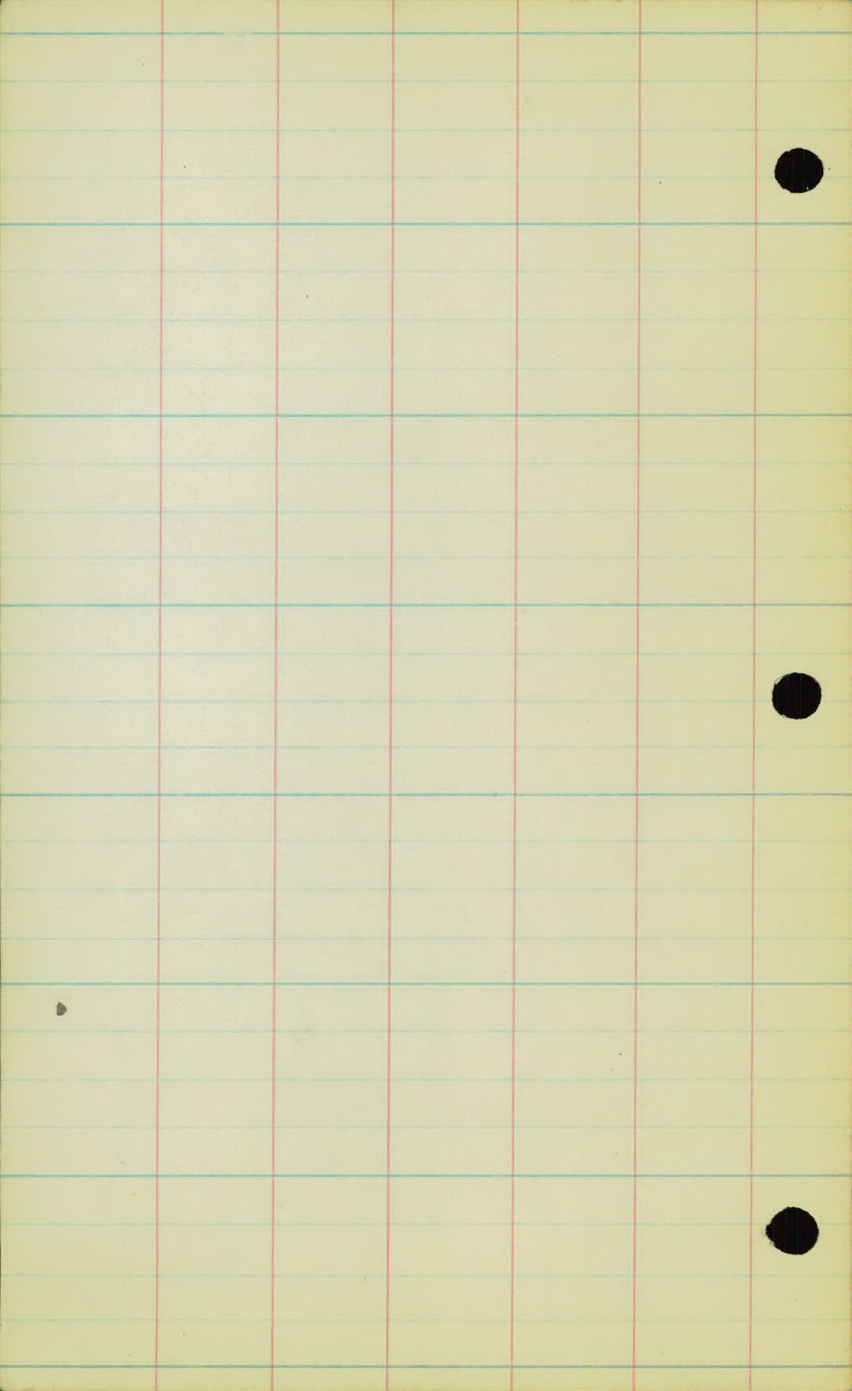
1/22/25

Lt.

Rt.

81

<u>4.1</u>	<u>4.0</u>	<u>4.1</u>	<u>8.3</u>	<u>7.6</u>	<u>6.7</u>		<u>6.0</u>	<u>8.2</u>	<u>8.0</u>	<u>4.3</u>	<u>4.2</u>	<u>4.1</u>
50	33	31	29	19	18	4.7	16	20	23	29	33	50
<u>4.4</u>	<u>4.3</u>	<u>4.2</u>	<u>8.4</u>	<u>8.1</u>	<u>6.8</u>		<u>6.8</u>	<u>6.1</u>	<u>8.1</u>	<u>3.2</u>	<u>3.7</u>	<u>4.0</u>
50	33	29	19	16	14	6.8	16	19	23	31	33	50



Anoka. line.
Central Ave. X-sections.
Sta. 607 to 625

Station	+	H.I.	-	Rod.	Elev
B.M.	2.05	917.62 ✓			915.57 ✓
607+00					12.56 ✓
608+00					12.40 ✓
609+00					12.32 ✓
610+00					12.34 ✓
T.P.	8.26	917.70 ✓	8.18	909.44 ✓	
611+00					12.40 ✓
612+00					12.50 ✓
613+00					12.62 ✓
614+00					12.70 ✓
615+00					12.77 ✓
616+00					12.85 ✓
617+00					12.84 ✓
T.P.	5.30	917.79 ✓	5.23	912.47 ✓	
618+00					12.97 ✓

(607+00)

Spike in T.P. Rt. Sta 604+20

5.6	4.9	7.2	7.0	4.9	5.16	5.15	4.8	7.3	7.7	4.8	4.4	4.71	
50.0	27.0	23.0	30.0	16.0	9.0	5.06	9.0	15.0	19.0	22.8	26.0	29.0	50.0

6.9	6.7	7.0	7.2	7.6	7.4	5.3	5.30	5.28	5.0	5.3	7.4	7.3	6.6	7.0	
50.0	46.0	31.0	25.5	24.0	19.0	15.5	9.0	5.22	9.0	12.5	16.0	17.5	22.0	23.5	35.0

7.0 6.5
50.0 17.0

6.7	6.0	7.6	7.5	7.9	7.6	5.7	5.2	5.38	5.38	5.1	5.6	8.7	7.7	7.3	7.3	
50.0	32.0	30.5	25.0	24.0	22.0	18.5	16.0	9.0	5.30	9.0	12.0	17.0	21.5	24.0	29.0	50.0

12.2	11.3	11.5	7.0	5.3	5.37	5.36	5.2	7.6	10.3	10.6	10.0	10.0	
50.0	29.0	27.0	26.0	15.5	9.0	5.38	9.0	16.0	21.5	26.0	29.5	32.0	50.0

9.5	9.3	9.5	9.8	9.8	5.6	5.40	5.40	5.1	9.7	8.7	7.8	8.0	8.6	
50.0	36.0	24.5	23.5	21.5	5.0	9.0	5.30	9.0	15.0	21.0	22.5	24.5	42.0	50.0

7.0	7.0	7.6	7.7	7.1	5.3	5.28	5.28	5.2	5.4	7.4	7.8	7.1	7.8	
50.0	24.5	23.5	20.5	18.0	15.0	9.0	5.20	9.0	11.0	15.5	19.0	21.0	23.0	50.0

7.0	6.8	7.8	7.6	4.7	5.2	5.1	5.18	5.0	5.1	7.6	7.4	6.9	6.2	6.4	
50.0	25.0	22.0	18.5	13.5	13.0	9.0	5.08	9.0	12.0	16.0	20.0	22.5	21.5	34.0	50.0

6.1	5.8	7.2	7.2	7.8	7.5	5.2	5.07	5.07	5.1	7.4	7.5	6.8	5.0	5.7	
50.0	20.8	25.0	23.5	22.5	19.0	15.0	9.0	5.0	9.0	14.5	21.0	23.0	25.5	29.0	50.0

5.0	5.5	6.4	6.8	7.6	7.4	4.9	4.98	4.98	4.9	7.3	7.6	7.0	5.8	6.0	
50.0	25.0	24.0	23.0	21.5	18.5	14.0	9.0	4.93	9.0	17.0	22.0	27.0	29.0	30.5	50.0

6.1	6.6	7.1	6.2	4.7	4.93	4.93	5.2	7.7	8.0	7.1	7.3	
50.0	25.0	23.0	18.0	13.0	9.0	4.85	9.0	16.5	20.5	24.0	28.5	50.0

7.2	7.3	7.0	7.9	5.0	4.92	4.95	5.1	5.8	8.0	8.4	7.1	7.4	7.6	
50.0	25.5	25.0	19.5	14.5	9.0	4.96	9.0	14.5	17.0	21.0	25.0	27.5	31.0	50.0

Spike in T.P. 27 hett. Sta 617+17

3.9	4.4	5.3	7.0	6.2	4.7	4.93	4.92	5.1	6.4	6.8	6.6	4.6	5.0	
50.0	27.0	25.5	21.5	18.0	14.5	9.0	4.80	9.0	17.0	19.5	22.5	24.0	28.5	50.0

Station	+	H.I.	-	Rod.	Elev.
		917.77			
619+00					912.84 ^v
B.M.				3.12	914.65 ^v
620+00					12.84 ^v
621+00					12.86 ^v
622+00					12.87 ^v
T.P.	5.18	918.30	4.65	913.12	
623+00					12.87 ^v
624+00					12.91 ^v
625+00					12.93 ^v
T.P.	4.58	917.50	5.18	913.12	
B.M.				2.86	914.64 ^v

Drainage Note.

610+11 2' x 2' x 45.2' Concrete Box Culvert.
 Extends 23' Rt.
 vv 22.2 ft.
 Intake Elev = 906.0
 Invert. vv = 905.9
 Drains left.

ht.

E

Rt.

84

(619400)

$\frac{3.5}{50.0}$	$\frac{3.7}{27.5}$	$\frac{5.1}{25.5}$	$\frac{6.2}{20.0}$	$\frac{5.3}{16.5}$	$\frac{4.9}{15.5}$	$\frac{5.0}{9.0}$	4.93	$\frac{5.06}{9.0}$	$\frac{5.0}{17.5}$	$\frac{6.6}{22.0}$	$\frac{6.5}{21.5}$	$\frac{5.3}{24.5}$	$\frac{4.5}{30.0}$	$\frac{4.8}{50.0}$
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Spike in 12" OAK 40' left. Sta 619450

$\frac{5.4}{50.0}$	$\frac{5.8}{26.0}$	$\frac{6.6}{24.5}$	$\frac{7.0}{21.0}$	$\frac{4.5}{14.0}$	$\frac{5.0}{9.0}$	4.93	$\frac{5.01}{9.0}$	$\frac{5.2}{17.5}$	$\frac{6.8}{21.0}$	$\frac{7.0}{23.5}$	$\frac{6.2}{24.5}$	$\frac{5.5}{27.5}$	$\frac{5.6}{50.0}$
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$\frac{6.5}{50.0}$	$\frac{6.2}{25.0}$	$\frac{7.4}{21.0}$	$\frac{7.0}{19.5}$	$\frac{6.0}{16.5}$	$\frac{5.5}{14.0}$	$\frac{4.8}{12.5}$	$\frac{4.99}{9.0}$	4.91	$\frac{5.08}{9.0}$	$\frac{5.1}{17.5}$	$\frac{6.8}{20.5}$	$\frac{7.1}{23.0}$	$\frac{5.3}{26.5}$	$\frac{4.7}{30.0}$	$\frac{5.2}{50.0}$
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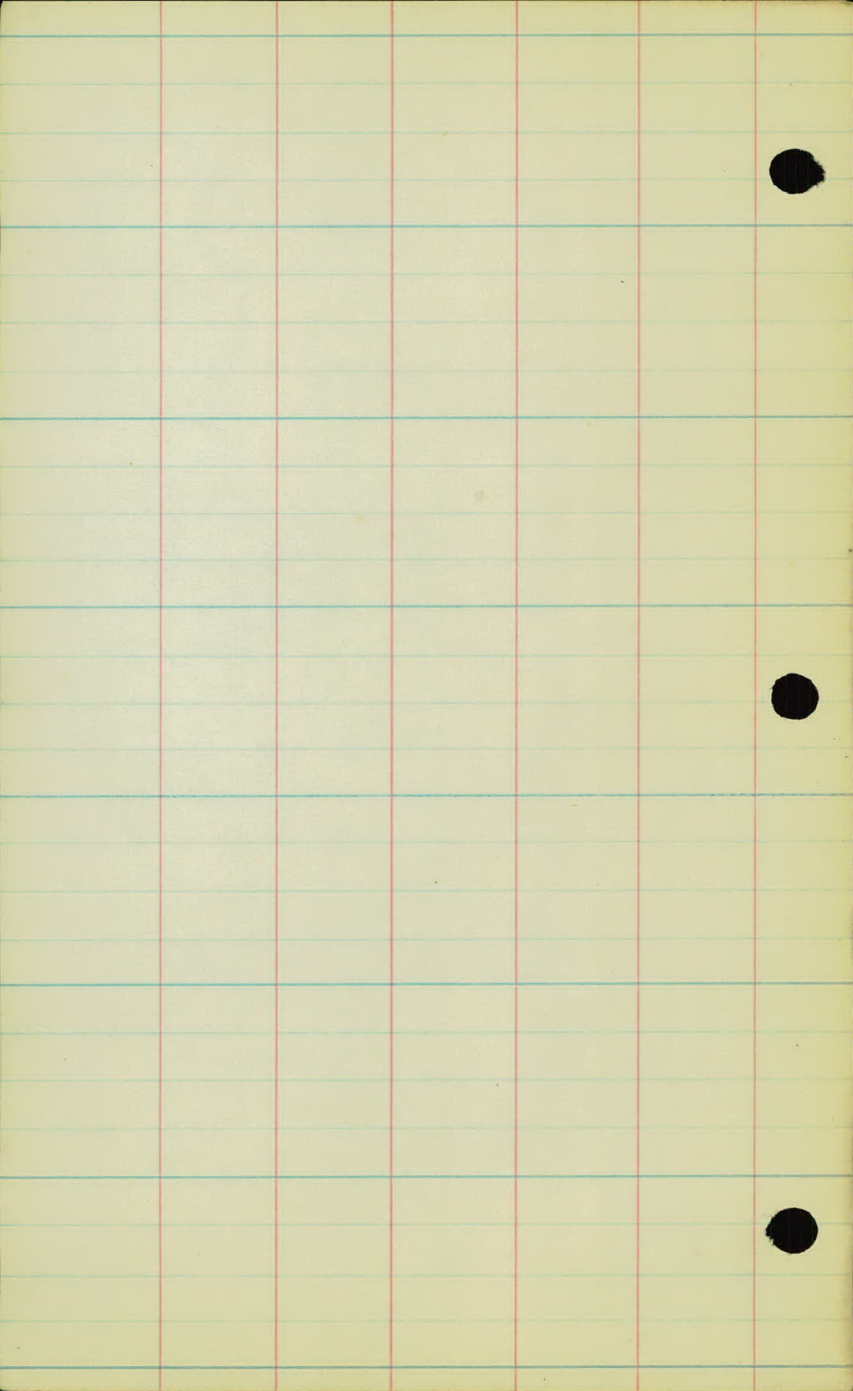
$\frac{7.2}{50.0}$	$\frac{7.4}{47.0}$	$\frac{7.3}{27.0}$	$\frac{7.6}{24.5}$	$\frac{7.2}{17.5}$	$\frac{5.0}{13.0}$	$\frac{5.00}{9.0}$	4.80	$\frac{4.96}{9.0}$	$\frac{5.3}{17.0}$	$\frac{7.1}{20.0}$	$\frac{7.4}{25.5}$	$\frac{7.0}{32.0}$	$\frac{6.8}{50.0}$
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$\frac{6.4}{50.0}$	$\frac{6.4}{26.0}$	$\frac{7.4}{21.5}$	$\frac{8.4}{19.5}$	$\frac{5.4}{14.0}$	$\frac{5.53}{9.0}$	5.43	$\frac{5.50}{9.0}$	$\frac{5.5}{16.0}$	$\frac{7.9}{20.5}$	$\frac{8.0}{22.0}$	$\frac{6.8}{25.5}$	$\frac{6.0}{30.5}$	$\frac{6.0}{42.5}$	$\frac{6.0}{50.0}$
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$\frac{6.2}{50.0}$	$\frac{6.2}{45.0}$	$\frac{6.5}{40.0}$	$\frac{6.3}{36.0}$	$\frac{6.2}{35.5}$	$\frac{8.0}{22.0}$	$\frac{7.8}{18.5}$	$\frac{5.4}{14.0}$	$\frac{5.07}{9.0}$	5.39	$\frac{5.45}{9.0}$	$\frac{5.6}{17.0}$	$\frac{7.7}{21.0}$	$\frac{7.7}{22.0}$	$\frac{5.5}{26.5}$	$\frac{5.0}{31.0}$	$\frac{5.1}{50.0}$
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$\frac{7.3}{37.0}$	$\frac{7.5}{33.0}$	$\frac{7.0}{28.5}$	$\frac{7.0}{26.5}$	$\frac{8.3}{23.5}$	$\frac{8.0}{18.5}$	$\frac{5.6}{13.5}$	$\frac{5.47}{9.0}$	5.37	$\frac{5.00}{9.0}$	$\frac{5.5}{17.0}$	$\frac{7.3}{20.0}$	$\frac{7.2}{22.5}$	$\frac{5.6}{27.0}$	$\frac{5.1}{32.5}$	$\frac{5.4}{50.0}$
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Spike in 12" OAK 40' left. Sta 619450



Station	+	H.I.	-	Rod.	Elev.
B.M	2.57	917.22 ✓			914.65
T.P.	5.27	918.16 ✓	4.33	912.59 ✓	
626+00					12.89
627+00					12.91
+50					12.89 ✓
+80					13.06
628+00					10.86
+20					14.16
+50					14.16
629+00					14.56
+50					15.56
630+00					16.36
+50					16.6 ✓
T.P.	2.81	919.46 ✓	1.51	916.65 ✓	
631+00					16.3

1-21-25

ht.

*

626100
RI "H"line 86

Spike in 12" OAK 40' ht. Sta 619+50

$\frac{1.7}{50.0}$	$\frac{7.4}{38.0}$	$\frac{7.4}{25.0}$	$\frac{8.2}{20.0}$	$\frac{5.3}{19.0}$	$\frac{5.30}{9.0}$	5.27	$\frac{5.32}{9.0}$	$\frac{5.4}{17.0}$	$\frac{7.5}{22.0}$	$\frac{6.8}{26.0}$	$\frac{6.2}{50.0}$
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$\frac{7.3}{50.0}$	$\frac{8.0}{44.0}$	$\frac{7.2}{37.0}$	$\frac{6.5}{25.0}$	$\frac{8.0}{20.0}$	$\frac{5.1}{13.0}$	$\frac{5.32}{8.5}$	5.25	$\frac{5.32}{9.5}$	$\frac{5.2}{17.0}$	$\frac{7.3}{23.0}$	$\frac{6.8}{27.0}$	$\frac{6.0}{50.0}$
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$\frac{5.4}{50.0}$	$\frac{5.1}{20.0}$	$\frac{8.3}{13.0}$	$\frac{5.0}{7.0}$	$\frac{5.27}{1.6}$	5.27	$\frac{5.23}{7.6}$	$\frac{5.32}{16.4}$	$\frac{5.4}{24.0}$	$\frac{7.0}{22.0}$	$\frac{4.3}{26.0}$	$\frac{4.2}{50.0}$
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$\frac{4.6}{50.0}$	$\frac{4.6}{36.0}$	$\frac{4.3}{15.0}$	$\frac{7.1}{9.0}$	$\frac{7.1}{4.0}$	5.1	$\frac{5.25}{15.0}$	$\frac{5.4}{31.0}$	$\frac{7.0}{26.0}$	$\frac{3.4}{44.0}$	$\frac{3.0}{50.0}$
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$\frac{4.2}{50.0}$	$\frac{4.3}{25.0}$	$\frac{4.3}{8.0}$	$\frac{7.0}{2.0}$	7.3	$\frac{7.0}{8.0}$	$\frac{5.2}{7.0}$	$\frac{5.27}{25.0}$	$\frac{5.2}{45.0}$	$\frac{5.8}{49.0}$	$\frac{5.6}{50.0}$
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$\frac{4.2}{50.0}$	$\frac{4.2}{22.0}$	4.0	$\frac{6.7}{7.0}$	$\frac{6.8}{12.0}$	$\frac{5.2}{17.0}$	$\frac{5.27}{35.0}$	$\frac{5.1}{50.0}$
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$\frac{4.1}{50.0}$	$\frac{4.1}{28.0}$	4.0	$\frac{4.2}{14.0}$	$\frac{6.5}{22.0}$	$\frac{6.6}{27.0}$	$\frac{5.1}{32.0}$	$\frac{5.25}{50.0}$
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$\frac{3.8}{50.0}$	$\frac{3.7}{25.0}$	3.4	$\frac{3.6}{25.0}$	$\frac{3.7}{46.0}$	$\frac{6.2}{50.0}$
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$\frac{2.9}{50.0}$	$\frac{2.8}{35.0}$	2.6	$\frac{2.6}{25.0}$	$\frac{2.7}{50.0}$
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$\frac{2.7}{50.0}$	$\frac{2.3}{25.0}$	1.8	$\frac{2.0}{25.0}$	$\frac{2.4}{50.0}$
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$\frac{2.0}{50.0}$	$\frac{1.7}{25.0}$	1.6	$\frac{1.8}{25.0}$	$\frac{2.2}{50.0}$
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$\frac{3.0}{50.0}$	$\frac{2.9}{25.0}$	3.2	$\frac{3.4}{29.0}$	$\frac{4.4}{29.5}$	$\frac{4.0}{39.0}$	$\frac{3.8}{50.0}$
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1289

1288

12.91

Station	+	H.I	-	Rod.	Elev.
		919.46			
631+50					16.5
631+75					16.5
632+00					15.8
+50					16.0
633+00					14.8
+50					13.9
B.M.				3.65	915.81 ✓
634+00					13.9
+50					12.8
635+00					11.4
+50					10.6
T.P.	4.15	915.11 ✓	8.50	910.96 ✓	
636+00					910.1
637+00					09.9
838+00					10.2

1-21-25

Ht.

2

"H" hinc
K.P.

87

631+50

$\frac{3.7}{50.0}$	$\frac{3.0}{25.0}$	3.0	$\frac{3.2}{8.0}$	$\frac{4.2}{9.0}$	$\frac{3.5}{16.0}$	$\frac{3.6}{24.0}$	$\frac{4.1}{32.0}$	$\frac{4.6}{39.0}$		
$\frac{3.5}{50.0}$	$\frac{3.0}{33.0}$	$\frac{2.8}{14.0}$	3.0	$\frac{4.0}{0.5}$	$\frac{3.6}{7.0}$	$\frac{3.2}{14.0}$	$\frac{4.0}{23.0}$	$\frac{4.3}{31.0}$	$\frac{3.1}{32.0}$	$\frac{2.5}{42.0}$

$\frac{3.4}{50.0}$	$\frac{2.6}{18.0}$	$\frac{2.8}{5.0}$	$\frac{3.9}{4.0}$	3.7	$\frac{3.4}{9.0}$	$\frac{4.0}{16.0}$	$\frac{3.4}{25.0}$	$\frac{2.8}{26.0}$	$\frac{2.5}{35.0}$	$\frac{3.4}{50.0}$
$\frac{4.0}{50.0}$	$\frac{3.7}{30.0}$	$\frac{3.4}{11.5}$	$\frac{4.6}{11.0}$	3.5	$\frac{3.5}{3.0}$	$\frac{4.0}{12.0}$	$\frac{4.2}{19.0}$	$\frac{2.9}{22.0}$	$\frac{2.4}{28.0}$	$\frac{3.6}{50.0}$

$\frac{5.1}{50.0}$	$\frac{4.8}{25.0}$	$\frac{5.0}{13.0}$	$\frac{5.7}{12.0}$	$\frac{5.3}{9.0}$	4.7	$\frac{4.7}{2.0}$	$\frac{5.7}{12.0}$	$\frac{5.6}{18.0}$	$\frac{4.4}{18.5}$	$\frac{3.7}{28.0}$	$\frac{4.6}{50.0}$
$\frac{5.7}{50.0}$	$\frac{5.7}{27.0}$	$\frac{5.5}{15.0}$	$\frac{6.5}{14.0}$	$\frac{6.2}{11.0}$	5.6	$\frac{6.2}{13.0}$	$\frac{6.2}{18.0}$	$\frac{5.2}{17.0}$	$\frac{4.2}{27.0}$	$\frac{5.4}{50.0}$	

Spike 24" OAK 40' H. 516 33 475

$\frac{3.7}{50.0}$	$\frac{3.8}{33.0}$	$\frac{4.0}{22.0}$	$\frac{6.6}{15.0}$	$\frac{6.7}{11.0}$	5.6	$\frac{6.5}{14.0}$	$\frac{6.6}{18.0}$	$\frac{5.0}{22.0}$	$\frac{4.4}{22.0}$	$\frac{4.0}{27.0}$	$\frac{5.4}{50.0}$
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$\frac{4.3}{50.0}$	$\frac{4.3}{35.0}$	$\frac{4.3}{21.0}$	$\frac{7.5}{15.0}$	$\frac{7.6}{12.0}$	6.7	$\frac{8.0}{15.0}$	$\frac{8.0}{20.0}$	$\frac{4.6}{25.0}$	$\frac{4.6}{31.0}$	$\frac{5.5}{50.0}$
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$\frac{7.4}{50.0}$	$\frac{7.0}{34.0}$	$\frac{7.4}{21.0}$	$\frac{9.5}{12.0}$	$\frac{8.9}{8.0}$	8.1	$\frac{9.1}{16.0}$	$\frac{9.0}{17.0}$	$\frac{8.0}{21.0}$	$\frac{5.7}{27.0}$	$\frac{6.8}{50.0}$
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$\frac{11.8}{50.0}$	$\frac{16.2}{23.0}$	$\frac{11.2}{14.0}$	$\frac{7.2}{9.0}$	8.9	$\frac{9.6}{14.0}$	$\frac{9.8}{19.0}$	$\frac{9.5}{25.0}$	$\frac{8.8}{28.0}$	$\frac{9.3}{50.0}$
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Fence Post 635 475 K.P.

$\frac{9.0}{50.0}$	$\frac{8.5}{24.0}$	$\frac{9.0}{13.0}$	$\frac{5.5}{9.0}$	5.0	$\frac{5.7}{14.0}$	$\frac{7.8}{18.0}$	$\frac{7.8}{32.0}$	$\frac{7.7}{50.0}$
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$\frac{8.6}{50.0}$	$\frac{9.0}{24.0}$	$\frac{8.4}{12.0}$	$\frac{5.6}{9.0}$	5.2	$\frac{6.0}{14.0}$	$\frac{8.8}{20.0}$	$\frac{10.0}{50.0}$
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$\frac{5.8}{50.0}$	$\frac{6.4}{20.0}$	$\frac{7.0}{19.0}$	$\frac{7.4}{15.0}$	$\frac{5.5}{11.0}$	4.9	$\frac{5.3}{9.0}$	$\frac{5.7}{15.0}$	$\frac{6.7}{18.0}$	$\frac{6.8}{26.0}$	$\frac{7.8}{50.0}$
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Station	+	H.I.	-	Rod	Elev.
		915.11			
639 +00					10.3
640 +00					9.4
641 +00					9.1
642 +00					9.1
T.P.	7.12	915.88 ✓	6.35	908.76 ✓	
643 +00					709.1
+50					09.8
644 +00					10.0
645 +00					11.2
646 +00					10.5
B.M.				4.06	911.82 ✓ 911.33
+50					10.2
647 +00					09.4
+50					09.2
648 +00					09.0
					09.0

1-21-25

Ht.

±

H^o time

Ht.

88

639100

$\frac{4.3}{50.0}$	$\frac{4.2}{27.0}$	$\frac{6.3}{19.0}$	$\frac{6.3}{13.0}$	$\frac{5.4}{11.0}$	4.8	$\frac{5.2}{10.0}$	$\frac{5.3}{17.0}$	$\frac{6.0}{20.0}$	$\frac{5.7}{24.0}$	$\frac{4.7}{28.0}$	$\frac{5.2}{38.0}$	$\frac{5.5}{50.0}$	$\frac{5.2}{45.0}$
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$\frac{5.6}{50.0}$	$\frac{5.6}{22.0}$	$\frac{7.4}{20.0}$	$\frac{6.8}{13.0}$	$\frac{5.8}{10.0}$	5.7	$\frac{6.0}{10.0}$	$\frac{6.2}{16.0}$	$\frac{7.0}{17.0}$	$\frac{7.0}{27.0}$	$\frac{6.7}{26.0}$	$\frac{7.4}{50.0}$
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$\frac{7.1}{50.0}$	$\frac{8.0}{23.0}$	$\frac{8.0}{15.0}$	$\frac{6.4}{11.0}$	6.0	$\frac{6.4}{10.0}$	$\frac{6.5}{16.0}$	$\frac{7.7}{20.0}$	$\frac{9.2}{24.0}$	$\frac{9.0}{40.0}$	$\frac{10.0}{45.0}$	$\frac{8.7}{50.0}$
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$\frac{9.0}{50.0}$	$\frac{8.4}{35.0}$	$\frac{9.4}{26.0}$	$\frac{9.5}{23.0}$	$\frac{8.0}{13.0}$	$\frac{6.5}{9.0}$	6.0	$\frac{6.7}{11.0}$	$\frac{6.9}{18.0}$	$\frac{7.8}{22.0}$	$\frac{7.5}{27.0}$	$\frac{8.0}{50.0}$
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$\frac{8.8}{50.0}$	$\frac{9.0}{35.0}$	$\frac{8.7}{20.0}$	$\frac{8.4}{12.0}$	$\frac{7.0}{7.0}$	6.8	$\frac{6.4}{8.0}$	$\frac{7.0}{19.0}$	$\frac{9.0}{24.0}$	$\frac{8.2}{30.0}$	$\frac{7.0}{33.0}$	$\frac{7.0}{50.0}$
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$\frac{8.6}{50.0}$	$\frac{7.7}{27.0}$	$\frac{7.7}{12.0}$	$\frac{6.5}{7.0}$	6.1	$\frac{5.7}{8.0}$	$\frac{6.4}{18.0}$	$\frac{7.5}{23.0}$	$\frac{8.3}{31.0}$	$\frac{7.3}{33.0}$	$\frac{6.8}{50.0}$
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$\frac{6.2}{50.0}$	$\frac{5.6}{20.0}$	$\frac{6.7}{16.0}$	$\frac{6.8}{11.0}$	$\frac{6.0}{7.0}$	5.9	$\frac{5.6}{9.0}$	$\frac{6.3}{17.0}$	$\frac{7.2}{23.0}$	$\frac{8.2}{28.0}$	$\frac{7.2}{32.0}$	$\frac{5.7}{34.0}$	$\frac{6.0}{50.0}$
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$\frac{4.0}{50.0}$	$\frac{3.6}{21.0}$	$\frac{5.2}{17.0}$	$\frac{6.0}{9.0}$	$\frac{4.8}{5.0}$	4.7	$\frac{4.5}{9.0}$	$\frac{4.8}{20.0}$	$\frac{5.9}{24.0}$	$\frac{6.8}{30.0}$	$\frac{6.0}{32.0}$	$\frac{2.9}{37.0}$	$\frac{2.7}{50.0}$
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$\frac{4.8}{50.0}$	$\frac{4.0}{17.0}$	$\frac{6.0}{14.0}$	$\frac{6.6}{7.0}$	$\frac{5.6}{3.0}$	5.4	$\frac{4.7}{11.0}$	$\frac{5.6}{21.0}$	$\frac{7.2}{31.0}$	$\frac{5.2}{35.0}$	$\frac{3.6}{37.0}$	$\frac{3.6}{50.0}$
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Sp. in 18" Oak 55' h + sta 645470

$\frac{6.0}{50.0}$	$\frac{4.8}{28.0}$	$\frac{5.0}{13.0}$	$\frac{6.4}{7.0}$	$\frac{6.0}{3.0}$	5.7	$\frac{5.4}{11.0}$	$\frac{5.9}{21.0}$	$\frac{6.9}{26.0}$	$\frac{6.5}{29.0}$	$\frac{4.8}{34.0}$	$\frac{3.2}{35.0}$	$\frac{3.1}{50.0}$
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$\frac{9.2}{50.0}$	$\frac{8.0}{28.0}$	$\frac{7.1}{12.0}$	6.5	$\frac{6.2}{11.0}$	$\frac{6.8}{21.0}$	$\frac{7.8}{27.0}$	$\frac{7.5}{31.0}$	$\frac{4.5}{37.0}$	$\frac{4.0}{50.0}$
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$\frac{9.6}{50.0}$	$\frac{9.5}{17.0}$	$\frac{9.4}{8.0}$	$\frac{7.0}{4.0}$	6.7	$\frac{6.3}{11.0}$	$\frac{7.0}{21.0}$	$\frac{8.2}{26.0}$	$\frac{7.5}{30.0}$	$\frac{7.0}{32.0}$	$\frac{6.3}{50.0}$
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$\frac{9.3}{50.0}$	$\frac{9.5}{20.0}$	$\frac{9.7}{9.0}$	$\frac{7.2}{5.0}$	6.9	$\frac{6.0}{11.0}$	$\frac{7.0}{22.0}$	$\frac{9.1}{25.0}$	$\frac{8.5}{36.0}$	$\frac{7.9}{50.0}$
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Station	+	H.I.	-	Rod. Elev.	Elev.
		915.88			
649+00		✓		✓	09.9
T.P.	8.52	918.21	6.19	909.69	
+50					909.5
650+00					09.7
+50					09.9
651+00					10.1
652+00					11.3
653+00					13.1
654+00					12.2
+50					12.5
655+00					12.7
+35					12.5
					1/2 Rd. Right
656+00		✓		✓	13.3
T.P.	3.26	917.21	4.26	913.95	

1-21-25
649400

H.

4

H.

"H" hinc 89

$\frac{7.7}{50.0}$ $\frac{9.9}{18.0}$ $\frac{9.8}{17.0}$ $\frac{10.0}{9.0}$ $\frac{6.8}{4.0}$ 6.5 $\frac{6.2}{11.0}$ $\frac{6.7}{23.0}$ $\frac{9.5}{17.0}$ $\frac{9.4}{35.0}$ $\frac{9.3}{50.0}$

$\frac{9.1}{50.0}$ $\frac{10.1}{20.0}$ $\frac{11.2}{16.0}$ $\frac{11.2}{8.0}$ $\frac{8.8}{4.0}$ 8.7 $\frac{8.4}{11.0}$ $\frac{9.0}{24.0}$ $\frac{11.2}{28.0}$ $\frac{10.7}{33.0}$ $\frac{10.7}{50.0}$

$\frac{8.2}{50.0}$ $\frac{8.1}{14.0}$ $\frac{9.8}{11.0}$ $\frac{9.2}{6.0}$ $\frac{9.6}{4.0}$ 8.5 $\frac{8.2}{11.0}$ $\frac{8.7}{19.0}$ $\frac{9.0}{23.0}$ $\frac{8.5}{28.0}$ $\frac{8.7}{50.0}$

$\frac{7.8}{50.0}$ $\frac{7.8}{15.0}$ $\frac{9.0}{9.0}$ $\frac{9.5}{3.0}$ 8.3 $\frac{7.8}{11.0}$ $\frac{8.3}{19.0}$ $\frac{9.0}{24.0}$ $\frac{8.0}{26.0}$ $\frac{8.0}{50.0}$

$\frac{9.0}{50.0}$ $\frac{8.7}{27.0}$ $\frac{9.0}{9.0}$ $\frac{8.2}{3.0}$ 8.1 $\frac{7.6}{12.0}$ $\frac{8.2}{22.0}$ $\frac{8.5}{24.0}$ $\frac{8.0}{25.0}$ $\frac{7.8}{50.0}$

$\frac{6.4}{50.0}$ $\frac{5.8}{16.0}$ $\frac{7.2}{11.0}$ $\frac{6.7}{7.0}$ 6.9 $\frac{6.4}{12.0}$ $\frac{7.3}{22.0}$ $\frac{8.2}{26.0}$ $\frac{7.8}{29.0}$ $\frac{6.2}{32.0}$ $\frac{6.7}{50.0}$

$\frac{3.5}{50.0}$ $\frac{3.6}{15.0}$ $\frac{5.6}{11.0}$ $\frac{6.2}{8.0}$ $\frac{5.2}{4.0}$ 5.1 $\frac{4.8}{13.0}$ $\frac{5.2}{22.0}$ $\frac{6.1}{25.0}$ $\frac{5.5}{29.0}$ $\frac{3.1}{34.0}$ $\frac{2.9}{50.0}$

$\frac{5.7}{50.0}$ $\frac{5.9}{36.0}$ $\frac{6.4}{20.0}$ $\frac{7.1}{10.0}$ $\frac{7.1}{4.0}$ $\frac{6.0}{1.0}$ 6.0 $\frac{5.4}{12.0}$ $\frac{5.9}{24.0}$ $\frac{6.4}{27.0}$ $\frac{5.9}{30.0}$ $\frac{5.4}{50.0}$

$\frac{6.4}{50.0}$ $\frac{6.2}{20.0}$ $\frac{6.9}{12.0}$ $\frac{7.0}{5.0}$ $\frac{6.2}{2.0}$ 5.7 $\frac{5.4}{14.0}$ $\frac{6.5}{24.0}$ $\frac{8.2}{28.0}$ $\frac{8.0}{37.0}$ $\frac{7.6}{50.0}$

$\frac{4.5}{50.0}$ $\frac{4.6}{20.0}$ $\frac{5.8}{12.0}$ $\frac{6.3}{7.0}$ $\frac{5.6}{4.0}$ 5.5 $\frac{5.5}{11.0}$ $\frac{6.4}{25.0}$ $\frac{7.8}{30.0}$ $\frac{9.2}{37.0}$ $\frac{9.2}{50.0}$

$\frac{3.6}{50.0}$ $\frac{4.2}{22.0}$ $\frac{5.3}{4.0}$ 5.7 $\frac{5.7}{13.0}$ $\frac{6.2}{38.0}$ $\frac{6.7}{50.0}$

$\frac{3.3}{50.0}$ $\frac{3.6}{19.0}$ $\frac{5.2}{14.0}$ $\frac{5.0}{8.0}$ 4.9 $\frac{4.4}{3.0}$ $\frac{4.6}{13.0}$ $\frac{4.4}{18.0}$ $\frac{5.0}{21.0}$ $\frac{3.8}{27.0}$ $\frac{4.8}{50.0}$

Station	+	H.I	-	Rod. Elev.
		917.21		
656+50				13.6
657+00				13.8
658+00				11.4
B.M.	2.77	917.81 ✓	2.17	915.04 ✓
+50				(2.23) 915.04
				10.2
659+00				09.5
660+00				09.1
+40				10.2
661+00				13.4
662+00				12.6
+50				12.6
663+00				13.0
664+00				15.1
T.P.	7.13	922.26 ✓	2.68	915.13 ✓

1-21-25

Ht.

±

Ht.

"H" hinc

90

656450

$\frac{3.1}{50.0}$	$\frac{3.2}{19.0}$	$\frac{4.6}{15.0}$	$\frac{4.3}{8.0}$	3.6	$\frac{3.1}{9.0}$	$\frac{3.0}{19.0}$	$\frac{3.6}{23.0}$	$\frac{2.2}{30.0}$	$\frac{2.1}{43.0}$	$\frac{2.0}{50.0}$
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$\frac{2.3}{50.0}$	$\frac{1.9}{19.0}$	$\frac{3.5}{13.0}$	3.4	$\frac{2.5}{11.0}$	$\frac{3.2}{21.0}$	$\frac{1.1}{30.0}$	$\frac{0.9}{50.0}$
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$\frac{6.7}{50.0}$	$\frac{5.5}{16.0}$	$\frac{6.0}{14.0}$	5.8	$\frac{5.6}{9.0}$	$\frac{5.3}{22.0}$	$\frac{5.6}{25.0}$	$\frac{4.8}{30.0}$	$\frac{4.2}{50.0}$
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Sp. in Tanca, Post 15' Ht. Sta 661400 1/22/25

$\frac{9.3}{50.0}$	$\frac{7.8}{15.0}$	$\frac{7.7}{5.0}$	7.6	$\frac{7.7}{10.0}$	$\frac{7.5}{21.0}$	$\frac{9.4}{24.0}$	$\frac{8.0}{27.0}$	$\frac{8.0}{42.0}$	$\frac{8.0}{50.0}$
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$\frac{10.8}{50.0}$	$\frac{11.4}{19.0}$	$\frac{11.6}{16.0}$	$\frac{11.4}{8.0}$	$\frac{9.0}{4.0}$	8.3	$\frac{8.0}{12.0}$	$\frac{8.5}{23.0}$	$\frac{11.7}{30.0}$	$\frac{11.8}{34.0}$	$\frac{11.2}{38.0}$	$\frac{11.0}{50.0}$
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$\frac{11.3}{50.0}$	$\frac{11.3}{11.0}$	$\frac{11.6}{14.0}$	$\frac{11.3}{6.0}$	8.7	$\frac{7.6}{4.0}$	$\frac{7.3}{14.0}$	$\frac{8.0}{24.0}$	$\frac{11.6}{31.0}$	$\frac{11.6}{38.0}$	$\frac{10.5}{50.0}$
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$\frac{6.4}{50.0}$	$\frac{7.0}{21.0}$	$\frac{6.5}{13.0}$	$\frac{7.6}{6.0}$	7.6	$\frac{7.0}{4.0}$	$\frac{7.0}{12.0}$	$\frac{6.8}{21.0}$	$\frac{8.0}{26.0}$	$\frac{7.0}{33.0}$	$\frac{6.8}{44.0}$	$\frac{7.0}{50.0}$
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$\frac{3.3}{50.0}$	$\frac{3.5}{15.0}$	4.4	$\frac{4.4}{3.0}$	$\frac{5.5}{6.0}$	$\frac{5.7}{15.0}$	$\frac{5.0}{26.0}$	$\frac{4.8}{32.0}$	$\frac{3.1}{36.0}$	$\frac{2.8}{50.0}$
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$\frac{8.0}{50.0}$	$\frac{6.2}{21.0}$	$\frac{5.5}{8.0}$	5.2	$\frac{5.4}{12.0}$	$\frac{4.7}{29.0}$	$\frac{4.4}{50.0}$
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$\frac{7.6}{50.0}$	$\frac{6.0}{21.0}$	$\frac{5.6}{9.0}$	5.2	$\frac{5.3}{13.0}$	$\frac{5.0}{27.0}$	$\frac{4.7}{50.0}$
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$\frac{4.1}{50.0}$	$\frac{4.4}{22.0}$	$\frac{4.5}{4.0}$	4.8	$\frac{4.9}{13.0}$	$\frac{5.2}{29.0}$	$\frac{5.2}{42.0}$	$\frac{5.4}{50.0}$
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$\frac{2.2}{50.0}$	$\frac{2.2}{40.0}$	$\frac{2.4}{10.0}$	$\frac{3.3}{7.0}$	$\frac{3.2}{1.0}$	2.7	$\frac{3.0}{7.0}$	$\frac{3.7}{9.0}$	$\frac{8.7}{15.0}$	$\frac{8.3}{16.0}$	$\frac{3.6}{34.0}$	$\frac{4.5}{50.0}$
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Station	+	H.I.	-	Rod.	Elev.
		922.26			
665+00					15.3
666+00					15.8
667+00					16.9
+50					16.7
668+00					15.8
669+00					13.6
670+00					10.7
T.P.	3.72	914.54	11.44	910.82	
671+00					909.7
672+00					09.0
+50					08.5
673+00					07.9
674+00					06.4
B.M.			8.21	906.33	906.29

1-22-25

"H" line.

91

665400

$\frac{5.8}{50.0}$	$\frac{5.6}{20.0}$	$\frac{6.0}{7.0}$	$\frac{6.8}{8.0}$	7.0	$\frac{7.0}{7.0}$	$\frac{7.5}{9.0}$	$\frac{7.8}{23.0}$	$\frac{8.1}{31.0}$	$\frac{8.5}{33.0}$	$\frac{9.4}{50.0}$
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$\frac{4.8}{50.0}$	$\frac{5.2}{22.0}$	$\frac{5.8}{7.0}$	$\frac{6.4}{5.0}$	6.5	$\frac{6.6}{4.0}$	$\frac{7.0}{9.0}$	$\frac{6.9}{15.0}$	$\frac{7.7}{38.0}$	$\frac{8.4}{50.0}$
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$\frac{3.7}{50.0}$	$\frac{4.0}{42.0}$	$\frac{4.8}{6.0}$	$\frac{5.4}{5.0}$	5.4	$\frac{5.1}{4.0}$	$\frac{5.7}{7.0}$	$\frac{5.7}{14.0}$	$\frac{5.4}{15.0}$	$\frac{6.0}{35.0}$	$\frac{6.7}{50.0}$
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$\frac{4.3}{50.0}$	$\frac{5.0}{25.0}$	$\frac{5.8}{5.0}$	5.6	$\frac{5.3}{7.0}$	$\frac{5.5}{9.0}$	$\frac{5.5}{14.0}$	$\frac{5.2}{15.0}$	$\frac{5.2}{36.0}$	$\frac{5.7}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{5.8}{26.0}$	$\frac{5.9}{4.0}$	6.5	$\frac{6.6}{12.0}$	$\frac{6.7}{18.0}$	$\frac{6.0}{37.0}$	$\frac{6.5}{50.0}$
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$\frac{6.5}{50.0}$	$\frac{7.8}{21.0}$	$\frac{8.2}{10.0}$	8.7	$\frac{9.1}{12.0}$	$\frac{9.5}{35.0}$	$\frac{9.6}{42.0}$	$\frac{7.7}{50.0}$
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$\frac{9.2}{50.0}$	$\frac{11.2}{20.0}$	11.6	$\frac{11.6}{14.0}$	$\frac{12.5}{26.0}$	$\frac{12.8}{41.0}$	$\frac{12.8}{50.0}$
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$\frac{3.8}{50.0}$	$\frac{4.5}{21.0}$	$\frac{4.8}{7.0}$	4.8	$\frac{5.0}{12.0}$	$\frac{5.6}{22.0}$	$\frac{6.2}{41.0}$	$\frac{6.3}{50.0}$
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$\frac{6.2}{50.0}$	$\frac{6.0}{22.0}$	5.5	$\frac{5.4}{13.0}$	$\frac{6.0}{22.0}$	$\frac{6.0}{43.0}$	$\frac{6.1}{50.0}$
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$\frac{7.0}{50.0}$	$\frac{6.8}{37.0}$	$\frac{6.2}{15.0}$	6.0	$\frac{5.8}{12.0}$	$\frac{5.9}{27.0}$	$\frac{4.8}{31.0}$	$\frac{4.5}{43.0}$	$\frac{4.5}{50.0}$
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$\frac{7.7}{50.0}$	$\frac{7.4}{26.0}$	$\frac{6.5}{12.0}$	6.6	$\frac{6.6}{11.0}$	$\frac{6.5}{24.0}$	$\frac{5.1}{29.0}$	$\frac{4.7}{43.0}$	$\frac{4.7}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.7}{40.0}$	$\frac{4.5}{18.0}$	8.1	$\frac{7.7}{13.0}$	$\frac{7.7}{26.0}$	$\frac{7.5}{52.0}$	$\frac{7.4}{50.0}$
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Sp. in 10" OAK 50' ht sta 674+00

Station	+	H.I	-	Rod	Elev.
		914.54			06.0
675+00					
676+00		✓		✓	05.3
T.P.	8.26	913.84	8.96	905.58	
+50					05.4
677+00					05.7
B.M.				6.15	907.49 ✓ 907.70
678+00		✓		✓	06.4
T.P.	1.80	912.72	2.92	910.92	
+50					06.7
679+00					08.4
+50					09.5
680+00					09.3
681+00					07.3
682+00					06.8
<u>FROM R-103</u>					
683+00					05.9
684+00					05.4

(675+00)

$\frac{8.4}{50.0}$	$\frac{8.4}{29.0}$	$\frac{8.3}{14.0}$	8.5	$\frac{8.4}{11.0}$	$\frac{9.0}{20.0}$	$\frac{9.7}{21.0}$	$\frac{8.6}{50.0}$
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$\frac{10.3}{50.0}$	$\frac{10.0}{28.0}$	$\frac{10.6}{25.0}$	$\frac{10.6}{13.0}$	$\frac{9.5}{9.0}$	9.2	$\frac{9.3}{13.0}$	$\frac{9.6}{26.0}$	$\frac{9.4}{53.0}$	$\frac{8.7}{35.0}$	$\frac{8.4}{50.0}$
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$\frac{10.3}{50.0}$	$\frac{10.4}{24.0}$	$\frac{11.4}{22.0}$	$\frac{11.0}{12.0}$	$\frac{9.0}{5.0}$	8.4	$\frac{8.6}{12.0}$	$\frac{9.4}{17.0}$	$\frac{9.2}{26.0}$	$\frac{8.8}{36.0}$	$\frac{8.0}{50.0}$
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$\frac{11.4}{50.0}$	$\frac{11.6}{25.0}$	$\frac{12.2}{21.0}$	$\frac{11.2}{11.0}$	$\frac{8.6}{3.0}$	8.1	$\frac{8.2}{5.0}$	$\frac{8.3}{11.0}$	$\frac{10.2}{18.0}$	$\frac{10.3}{51.0}$	$\frac{9.6}{35.0}$	$\frac{8.9}{50.0}$
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sp. in OAK H. sta 678+03

$\frac{7.0}{50.0}$	$\frac{6.9}{28.0}$	$\frac{8.3}{24.0}$	$\frac{8.7}{16.0}$	$\frac{7.5}{9.0}$	7.4	$\frac{7.2}{10.0}$	$\frac{7.0}{14.0}$	$\frac{7.8}{18.0}$	$\frac{8.2}{26.0}$	$\frac{6.4}{34.0}$	$\frac{6.2}{50.0}$
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$\frac{5.3}{50.0}$	$\frac{5.6}{26.0}$	$\frac{6.5}{24.0}$	$\frac{6.0}{17.0}$	$\frac{5.8}{13.0}$	6.0	$\frac{6.1}{18.0}$	$\frac{6.6}{21.0}$	$\frac{6.5}{26.0}$	$\frac{5.8}{30.8}$	$\frac{5.4}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.7}{29.0}$	$\frac{4.6}{18.0}$	4.3	$\frac{4.9}{21.0}$	$\frac{5.2}{32.0}$	$\frac{5.0}{34.0}$	$\frac{5.4}{50.0}$
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$\frac{3.4}{50.0}$	$\frac{3.4}{23.0}$	3.2	$\frac{3.3}{2.0}$	$\frac{4.2}{6.0}$	$\frac{4.4}{11.0}$	$\frac{4.0}{13.0}$	$\frac{4.4}{34.0}$	$\frac{5.1}{50.0}$
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$\frac{2.3}{50.0}$	$\frac{2.7}{29.0}$	$\frac{3.3}{21.0}$	3.4	$\frac{4.2}{3.0}$	$\frac{4.7}{10.0}$	$\frac{4.2}{12.0}$	$\frac{5.0}{38.0}$	$\frac{5.7}{50.0}$
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$\frac{3.3}{50.0}$	$\frac{4.3}{30.0}$	$\frac{4.7}{16.0}$	5.4	$\frac{5.5}{4.0}$	$\frac{5.2}{7.0}$	$\frac{6.1}{32.0}$	$\frac{6.6}{50.0}$
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$\frac{5.4}{50.0}$	$\frac{5.9}{19.0}$	5.9	$\frac{6.0}{4.0}$	$\frac{6.4}{6.0}$	$\frac{6.5}{11.0}$	$\frac{6.2}{15.0}$	$\frac{6.7}{28.0}$	$\frac{6.6}{50.0}$
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$\frac{5.6}{50.0}$	$\frac{6.4}{33.0}$	$\frac{6.7}{18.0}$	$\frac{7.5}{17.0}$	$\frac{7.5}{13.0}$	$\frac{7.0}{4.0}$	6.8	$\frac{7.0}{4.0}$	$\frac{7.7}{9.0}$	$\frac{7.8}{17.0}$	$\frac{7.3}{20.0}$	$\frac{7.3}{37.0}$	$\frac{7.3}{50.0}$
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$\frac{7.6}{50.0}$	$\frac{7.7}{22.0}$	$\frac{8.3}{18.0}$	$\frac{8.3}{12.0}$	$\frac{7.6}{6.0}$	7.3	$\frac{7.7}{7.0}$	$\frac{8.4}{9.0}$	$\frac{8.5}{19.0}$	$\frac{8.2}{20.0}$	$\frac{8.5}{50.0}$
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Station	+	H.I.	-	Rod.	Elev.
		912.72			
685+00					15.2
T.P.	8.72	906.07	7.37	905.35	
686+00					04.3
687+00					02.2
688+00					899.8
689+00					98.6
690+00					98.8
T.P.	3.35	902.27	7.15	898.92	
691+00					898.7
+50					98.8
692+00					98.2
+50					97.7
693+00					97.5
+40					97.7
+70					97.8
B.M				3.51	898.76 898.79

685+00

$\frac{7.7}{50.0}$	$\frac{7.6}{30.0}$	$\frac{7.7}{17.0}$	$\frac{9.7}{12.0}$	$\frac{9.4}{8.0}$	$\frac{7.9}{6.0}$	7.5	$\frac{7.7}{6.0}$	$\frac{8.2}{8.0}$	$\frac{8.4}{17.0}$	$\frac{7.6}{21.0}$	$\frac{7.4}{50.0}$
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$\frac{2.4}{50.0}$	$\frac{2.4}{31.0}$	$\frac{2.6}{21.0}$	$\frac{3.0}{11.0}$	$\frac{2.2}{7.0}$	1.8	$\frac{2.0}{6.0}$	$\frac{2.7}{8.0}$	$\frac{3.4}{18.0}$	$\frac{2.1}{21.0}$	$\frac{2.6}{31.0}$	$\frac{2.5}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.7}{29.0}$	$\frac{4.4}{16.0}$	$\frac{4.7}{14.0}$	$\frac{4.6}{12.0}$	$\frac{4.2}{10.0}$	3.9	$\frac{4.1}{3.0}$	$\frac{4.7}{8.0}$	$\frac{4.7}{10.0}$	$\frac{4.1}{11.0}$	$\frac{4.5}{16.0}$	$\frac{5.0}{20.0}$	$\frac{5.2}{27.0}$
												$\frac{3.8}{50.0}$	$\frac{4.6}{27.0}$

$\frac{7.5}{50.0}$	$\frac{7.0}{27.0}$	$\frac{7.5}{26.0}$	$\frac{7.4}{21.0}$	$\frac{6.7}{18.0}$	$\frac{6.5}{11.0}$	6.3	$\frac{6.5}{6.0}$	$\frac{6.8}{8.0}$	$\frac{6.8}{10.0}$	$\frac{6.5}{11.0}$	$\frac{6.8}{17.0}$	$\frac{7.2}{22.0}$	$\frac{7.2}{26.0}$
												$\frac{6.0}{50.0}$	$\frac{6.2}{27.0}$

$\frac{9.7}{50.0}$	$\frac{8.7}{29.0}$	$\frac{8.8}{22.0}$	$\frac{8.5}{20.0}$	$\frac{8.2}{15.0}$	$\frac{7.8}{11.0}$	7.5	$\frac{7.6}{4.0}$	$\frac{8.2}{8.0}$	$\frac{8.8}{24.0}$	$\frac{8.0}{26.0}$	$\frac{7.4}{36.0}$	$\frac{8.0}{40.0}$	$\frac{8.2}{50.0}$
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$\frac{7.7}{50.0}$	$\frac{9.4}{31.0}$	$\frac{9.3}{25.0}$	$\frac{8.8}{22.0}$	$\frac{7.8}{15.0}$	$\frac{9.2}{14.0}$	$\frac{7.7}{9.0}$	7.3	$\frac{7.7}{5.0}$	$\frac{8.2}{9.0}$	$\frac{9.1}{24.0}$	$\frac{8.2}{26.0}$	$\frac{9.0}{29.0}$	$\frac{8.8}{50.0}$
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$\frac{3.2}{50.0}$	$\frac{4.3}{32.0}$	$\frac{5.5}{29.0}$	$\frac{5.5}{22.0}$	$\frac{3.7}{17.0}$	$\frac{4.1}{15.0}$	3.6	$\frac{3.9}{6.0}$	$\frac{4.2}{8.0}$	$\frac{4.0}{11.0}$	$\frac{4.0}{14.0}$	$\frac{4.7}{21.0}$	$\frac{3.8}{23.0}$	$\frac{3.5}{34.0}$
												$\frac{4.0}{50.0}$	

$\frac{4.0}{50.0}$	$\frac{4.7}{31.0}$	$\frac{6.2}{28.0}$	$\frac{5.8}{23.0}$	$\frac{5.8}{17.0}$	$\frac{4.3}{14.0}$	3.5	$\frac{3.5}{8.0}$	$\frac{3.2}{9.0}$	$\frac{4.3}{19.0}$	$\frac{3.0}{22.0}$	$\frac{3.0}{31.0}$	$\frac{2.6}{33.0}$	
												$\frac{3.0}{50.0}$	$\frac{2.6}{49.0}$

$\frac{5.0}{50.0}$	$\frac{5.4}{31.0}$	$\frac{6.2}{28.0}$	$\frac{5.8}{22.0}$	$\frac{4.3}{16.0}$	$\frac{4.7}{14.0}$	4.1	$\frac{4.6}{6.0}$	$\frac{4.4}{10.0}$	$\frac{5.0}{13.0}$	$\frac{5.0}{18.0}$	$\frac{4.0}{22.0}$	$\frac{4.0}{28.0}$	
												$\frac{3.0}{50.0}$	$\frac{3.5}{37.0}$

$\frac{5.0}{50.0}$	$\frac{5.2}{29.0}$	$\frac{6.2}{27.0}$	$\frac{5.9}{22.0}$	$\frac{4.4}{17.0}$	$\frac{4.7}{15.0}$	$\frac{4.3}{9.0}$	4.6	$\frac{5.7}{16.0}$	$\frac{5.0}{18.0}$	$\frac{4.3}{28.0}$	$\frac{4.7}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{5.6}{32.0}$	$\frac{6.5}{29.0}$	$\frac{6.3}{22.0}$	$\frac{5.0}{17.0}$	$\frac{4.3}{9.0}$	4.8	$\frac{5.7}{14.0}$	$\frac{4.3}{19.0}$	$\frac{4.3}{24.0}$	$\frac{4.6}{32.0}$	$\frac{5.0}{50.0}$
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$\frac{5.2}{50.0}$	$\frac{5.7}{34.0}$	$\frac{6.5}{32.0}$	$\frac{6.4}{23.0}$	$\frac{5.0}{16.0}$	4.6	$\frac{4.8}{6.0}$	$\frac{7.0}{14.0}$	$\frac{4.7}{22.0}$	$\frac{8.0}{28.0}$	$\frac{8.2}{32.0}$	$\frac{10.3}{37.0}$	$\frac{5.3}{50.0}$
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$\frac{5.7}{50.0}$	$\frac{6.0}{36.0}$	$\frac{6.5}{31.0}$	$\frac{7.6}{27.0}$	$\frac{6.4}{28.0}$	$\frac{4.9}{17.0}$	4.5	$\frac{4.6}{7.0}$	$\frac{10.0}{11.0}$	$\frac{9.5}{17.0}$	$\frac{8.0}{23.0}$	$\frac{4.4}{32.0}$	$\frac{4.5}{50.0}$
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Sp. in Tree Rt. 694+00

Station	+	HI	-	Rob	Elev
B.M.	5.15	903.93 ✓		898.78	
693+80					897.8
694+00					97.9
+50					98.2
695+00					96.9
+50					97.2
696+00					97.7
+50					98.3
697+00					99.1
+65					900.2
698+00					900.5
+50					900.3
699+00					899.5
T.P.	3.45	903.17 ✓	4.21	899.72 ✓	

1-23-25

±

"H" line
RT

94

(693+90)

ht.

Sp. in Tree RT 694+00

$\frac{7.0}{50.0}$	$\frac{7.2}{31.0}$	$\frac{4.4}{25.0}$	$\frac{6.7}{19.0}$	6.1	$\frac{6.3}{15.0}$	$\frac{5.7}{27.0}$	$\frac{6.8}{42.0}$	$\frac{7.4}{50.0}$
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$\frac{7.3}{50.0}$	$\frac{7.3}{34.0}$	$\frac{11.8}{25.0}$	$\frac{6.0}{13.0}$	6.0	$\frac{6.7}{21.0}$	$\frac{6.8}{50.0}$
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$\frac{7.5}{50.0}$	$\frac{7.5}{38.0}$	$\frac{12.1}{29.0}$	$\frac{6.5}{15.0}$	5.7	$\frac{6.4}{9.0}$	$\frac{7.7}{15.0}$	$\frac{7.8}{24.0}$	$\frac{6.3}{28.0}$	$\frac{6.4}{50.0}$
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$\frac{4.4}{50.0}$	$\frac{6.6}{41.0}$	$\frac{12.2}{34.0}$	$\frac{7.5}{15.0}$	7.0	$\frac{7.1}{9.0}$	$\frac{8.0}{15.0}$	$\frac{7.7}{24.0}$	$\frac{6.6}{27.0}$	$\frac{6.0}{50.0}$
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$\frac{8.3}{50.0}$	$\frac{8.8}{42.0}$	$\frac{12.7}{32.0}$	$\frac{8.0}{25.0}$	$\frac{7.2}{16.0}$	6.7	$\frac{6.9}{12.0}$	$\frac{8.5}{17.0}$	$\frac{7.2}{24.0}$	$\frac{6.1}{27.0}$	$\frac{4.8}{50.0}$
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$\frac{4.4}{50.0}$	$\frac{4.7}{45.0}$	$\frac{12.9}{38.0}$	$\frac{7.7}{29.0}$	$\frac{7.0}{16.0}$	6.2	$\frac{5.8}{4.0}$	$\frac{5.8}{12.0}$	$\frac{6.0}{14.0}$	$\frac{5.8}{23.0}$	$\frac{4.6}{26.0}$	$\frac{3.3}{50.0}$
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$\frac{13.8}{52.0}$	$\frac{8.3}{44.0}$	$\frac{7.8}{16.0}$	$\frac{6.3}{11.0}$	5.6	$\frac{5.6}{4.0}$	$\frac{5.1}{7.0}$	$\frac{4.0}{24.0}$	$\frac{2.6}{50.0}$
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$\frac{7.8}{50.0}$	$\frac{6.0}{23.0}$	$\frac{5.0}{10.0}$	4.8	$\frac{4.3}{7.0}$	$\frac{3.4}{25.0}$	$\frac{2.4}{50.0}$
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$\frac{6.8}{50.0}$	$\frac{5.0}{14.0}$	$\frac{4.3}{8.0}$	3.7	$\frac{4.0}{4.0}$	$\frac{3.2}{6.0}$	$\frac{2.7}{26.0}$	$\frac{2.3}{50.0}$
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$\frac{5.6}{50.0}$	$\frac{4.2}{18.0}$	$\frac{3.7}{8.0}$	3.4	$\frac{3.6}{4.0}$	$\frac{3.2}{7.0}$	$\frac{2.9}{25.0}$	$\frac{2.6}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.2}{33.0}$	$\frac{3.5}{20.0}$	$\frac{4.1}{16.0}$	$\frac{3.6}{13.0}$	$\frac{3.4}{7.0}$	3.4	$\frac{4.0}{22.0}$	$\frac{4.2}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.3}{14.0}$	$\frac{4.7}{16.0}$	$\frac{4.4}{13.0}$	4.4	$\frac{4.8}{5.0}$	$\frac{4.5}{7.0}$	$\frac{4.6}{26.0}$	$\frac{5.9}{50.0}$
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Station	+	H.I.	-	Rod	Elev.
		903.17 ✓			
699+35					899.2
700+00					900.5
701+00					897.1
+50					97.5
702+00					97.5
703+00					95.2
+50					96.0
704+00					97.4
+50					96.2
T.P.	3.97	901.17 ✓	5.97	997.20 ✓	
705+00					895.5
+50					95.4
706+00					96.0

699+35

$\frac{3.8}{50.0}$	$\frac{3.7}{18.0}$	$\frac{4.1}{16.0}$	$\frac{3.6}{13.0}$	4.0	$\frac{4.5}{4.0}$	$\frac{4.2}{6.0}$	$\frac{4.6}{27.0}$	$\frac{5.0}{50.0}$
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$\frac{3.1}{50.0}$	$\frac{2.8}{17.0}$	$\frac{3.2}{16.0}$	$\frac{2.7}{13.0}$	2.7	$\frac{3.2}{4.0}$	$\frac{3.0}{6.0}$	$\frac{3.1}{25.0}$	$\frac{3.8}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{5.7}{20.0}$	$\frac{6.1}{18.0}$	$\frac{5.6}{8.0}$	6.1	$\frac{6.2}{9.0}$	$\frac{6.2}{25.0}$	$\frac{5.9}{50.0}$
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$\frac{4.5}{50.0}$	$\frac{5.2}{20.0}$	$\frac{5.7}{18.0}$	$\frac{5.7}{9.0}$	5.7	$\frac{5.8}{5.0}$	$\frac{6.5}{26.0}$	$\frac{6.0}{50.0}$
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$\frac{5.0}{50.0}$	$\frac{5.5}{19.0}$	$\frac{6.0}{17.0}$	$\frac{5.5}{9.0}$	5.7	$\frac{6.0}{3.0}$	$\frac{5.6}{6.0}$	$\frac{5.5}{35.0}$	$\frac{5.2}{50.0}$
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$\frac{8.5}{50.0}$	$\frac{8.7}{20.0}$	$\frac{9.0}{11.0}$	9.0	$\frac{7.4}{2.0}$	$\frac{6.8}{21.0}$	$\frac{5.4}{50.0}$
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$\frac{6.8}{50.0}$	$\frac{7.0}{27.0}$	$\frac{7.5}{25.0}$	$\frac{7.3}{14.0}$	$\frac{7.4}{4.0}$	7.2	$\frac{6.4}{23.0}$	$\frac{5.0}{50.0}$
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$\frac{7.0}{50.0}$	$\frac{6.7}{34.0}$	$\frac{7.2}{32.0}$	$\frac{6.4}{22.0}$	$\frac{6.5}{10.0}$	$\frac{6.0}{8.0}$	5.8	$\frac{5.2}{25.0}$	$\frac{4.4}{50.0}$
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$\frac{9.4}{50.0}$	$\frac{9.8}{33.0}$	$\frac{9.6}{26.0}$	$\frac{8.0}{21.0}$	7.0	$\frac{5.6}{30.0}$	$\frac{4.8}{50.0}$
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$\frac{7.8}{50.0}$	$\frac{7.5}{39.0}$	$\frac{6.7}{21.0}$	5.7	$\frac{4.7}{28.0}$	$\frac{3.7}{50.0}$
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$\frac{6.9}{50.0}$	$\frac{6.7}{27.0}$	5.8	$\frac{5.0}{27.0}$	$\frac{4.3}{50.0}$
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$\frac{5.6}{50.0}$	$\frac{5.2}{25.0}$	5.7	$\frac{4.8}{29.0}$	$\frac{4.2}{50.0}$
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Station	+	H.I	-	Rob.	Elev.
		901.17			
706+50					96.5
707+00					96.4
B.M	4.96	901.02 ✓	5.11	896.06 ✓	
+50					895.10
708+00					94.6
+50					92.8
B.M			4.96	896.06 ✓	

1-23-25

706400

H.

E

TH.

"H" line

76

$\frac{4.7}{50.0}$	$\frac{4.7}{25.0}$	4.7	$\frac{4.8}{26.0}$	$\frac{4.8}{50.0}$
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$\frac{5.1}{50.0}$	$\frac{5.0}{28.0}$	4.8	$\frac{5.0}{28.0}$	$\frac{5.3}{50.0}$
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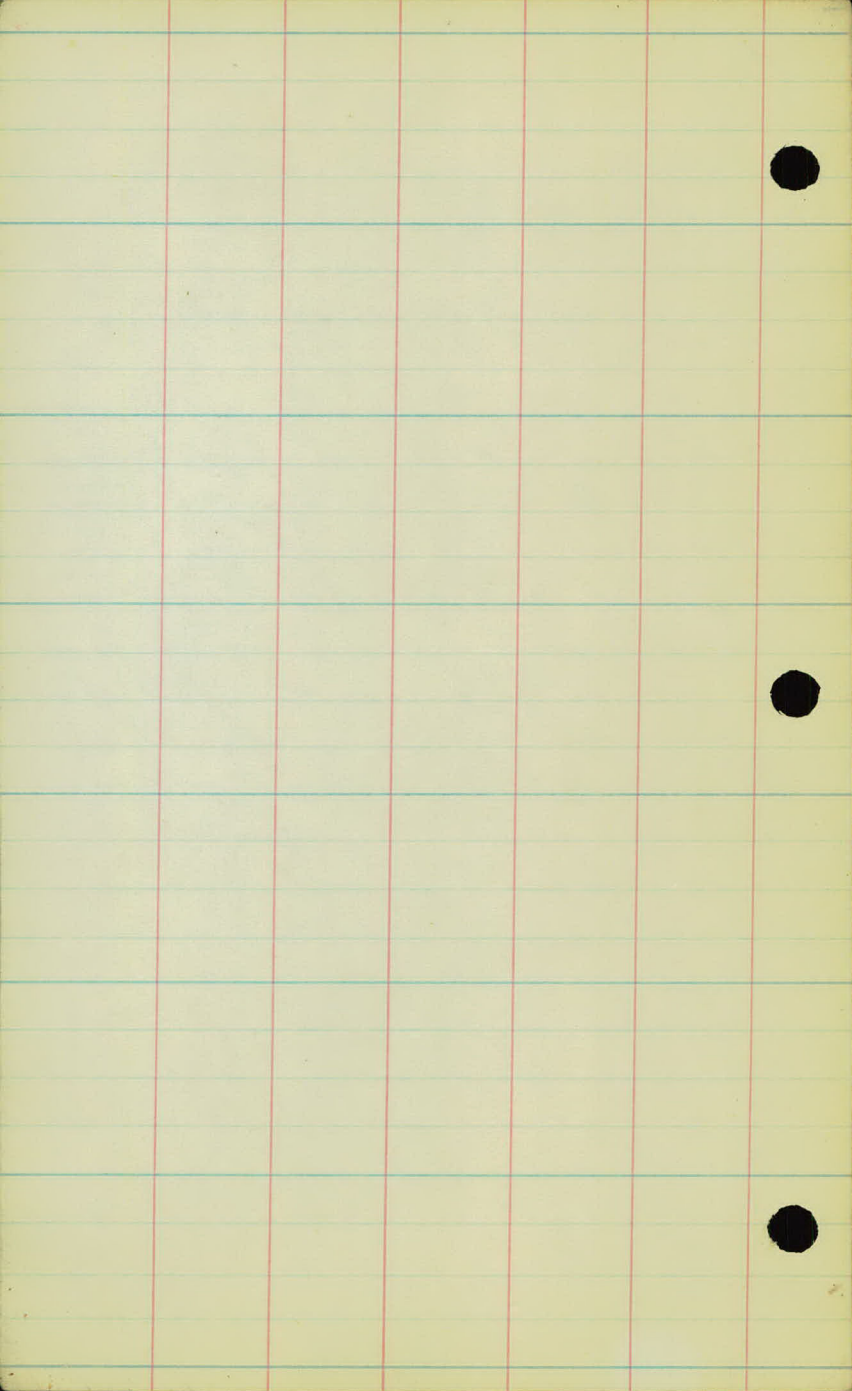
Sp. in stp. 70' ht. st 707+50

$\frac{5.7}{50.0}$	$\frac{5.5}{25.0}$	5.4	$\frac{5.5}{28.0}$	$\frac{6.4}{50.0}$
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$\frac{6.3}{50.0}$	$\frac{6.1}{19.0}$	6.4	$\frac{7.2}{25.0}$	$\frac{8.2}{50.0}$
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$\frac{7.0}{50.0}$	$\frac{7.3}{28.0}$	8.2	$\frac{9.1}{25.0}$	$\frac{9.8}{50.0}$
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Sp. in stump. 70' ht. st 707+50



Sta.	+	H.I.	-	Red.	Elev.
B.M.	1.10	897.16	✓	896.06	
709					90.9
	+35				88.9
710					88.8
711					88.9
	+46				90.4
712					89.2
T.P.	6.67	896.68	✓	7.15	890.01
	+50				91.3
713					91.8
714					90.7
T.P.	3.99	893.69	✓	6.98	889.70
	+50				87.2
715					87.0
	+45				87.0
716					89.6

90.7

Lt.

Rt.

Spk. in Stamp 70' Lt. Sta. 707150.
 $\frac{5.0}{50}$ $\frac{5.2}{33}$ $\frac{5.6}{16}$ 4.3 $\frac{7.3}{16}$ $\frac{7.6}{33}$ $\frac{8.0}{44}$ $\frac{7.7}{50}$ ✓

$\frac{7.0}{50}$ $\frac{7.5}{33}$ $\frac{8.0}{16}$ 8.3 $\frac{9.9}{16}$ $\frac{8.0}{33}$ $\frac{8.3}{50}$ ✓

$\frac{8.1}{50}$ $\frac{7.8}{33}$ $\frac{8.1}{16}$ 8.4 $\frac{8.3}{16}$ $\frac{7.9}{33}$ $\frac{8.0}{50}$ ✓

$\frac{7.2}{50}$ $\frac{7.4}{33}$ $\frac{8.5}{33}$ $\frac{8.8}{12}$ $\frac{9.8}{11}$ $\frac{7.5}{8}$ $\frac{8.4}{5}$ 2.3 $\frac{8.3}{16}$ $\frac{8.6}{33}$ $\frac{8.2}{50}$ ✓

$\frac{8.7}{50}$ $\frac{8.8}{39}$ $\frac{9.4}{35}$ $\frac{7.1}{35}$ $\frac{8.2}{33}$ $\frac{8.6}{32}$ $\frac{8.5}{16}$ $\frac{7.5}{10}$ 6.8 $\frac{6.9}{10}$ $\frac{8.2}{17}$ $\frac{8.2}{28}$ $\frac{7.2}{33}$ $\frac{9.2}{38}$ $\frac{8.1}{42}$ $\frac{8.2}{50}$

$\frac{8.5}{50}$ $\frac{8.3}{33}$ $\frac{8.3}{16}$ 8.0 $\frac{7.7}{16}$ $\frac{7.7}{33}$ $\frac{7.2}{39}$ $\frac{6.5}{42}$ $\frac{6.1}{50}$

$\frac{5.5}{50}$ $\frac{5.1}{33}$ $\frac{5.3}{16}$ 5.4 $\frac{5.4}{16}$ $\frac{5.5}{33}$ $\frac{5.3}{50}$

$\frac{4.7}{50}$ $\frac{4.7}{33}$ $\frac{4.8}{16}$ 4.7 $\frac{5.2}{16}$ $\frac{5.3}{33}$ $\frac{5.3}{50}$

$\frac{6.2}{50}$ $\frac{6.0}{33}$ $\frac{6.2}{16}$ 4.0 $\frac{5.8}{16}$ $\frac{5.6}{33}$ $\frac{5.0}{50}$

$\frac{4.9}{50}$ $\frac{6.7}{33}$ $\frac{6.7}{16}$ 6.4 $\frac{5.5}{16}$ $\frac{5.8}{33}$ $\frac{3.0}{50}$

$\frac{7.0}{50}$ $\frac{6.9}{33}$ $\frac{6.8}{16}$ 6.7 $\frac{6.6}{16}$ $\frac{5.8}{33}$ $\frac{4.9}{50}$

$\frac{7.0}{50}$ $\frac{7.1}{33}$ $\frac{7.2}{16}$ 6.7 $\frac{6.0}{16}$ $\frac{5.0}{33}$ $\frac{4.9}{50}$

$\frac{5.7}{50}$ $\frac{4.9}{33}$ $\frac{4.4}{16}$ 4.1 $\frac{3.7}{16}$ $\frac{3.5}{33}$ $\frac{3.0}{50}$

Sta.	+	H.I.	-	Red.	E/ev.
		873.69			
717					91.0
T.P.	3.38	874.25	2.82	890.87	
718					89.3
719					89.4
720					90.0
T.P.	1.42	893.19	2.48	891.77	
721					88.3
722					87.7
723					86.4
724					86.5
B.M.			3.09	890.10	890.12

Lt.

Rt.

$\frac{3.4}{50}$	$\frac{3.0}{33}$	$\frac{2.9}{14}$	2.8	$\frac{2.7}{14}$	$\frac{2.7}{33}$	$\frac{2.5}{50}$
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$\frac{4.7}{50}$	$\frac{5.0}{33}$	$\frac{5.0}{14}$	5.0	$\frac{4.8}{14}$	$\frac{4.7}{33}$	$\frac{4.5}{50}$
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$\frac{5.2}{50}$	$\frac{5.3}{33}$	$\frac{5.1}{14}$	4.9	$\frac{4.6}{14}$	$\frac{4.6}{33}$	$\frac{4.6}{50}$
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$\frac{3.5}{50}$	$\frac{3.7}{33}$	$\frac{4.0}{14}$	4.3	$\frac{4.7}{14}$	$\frac{5.1}{33}$	$\frac{5.2}{50}$
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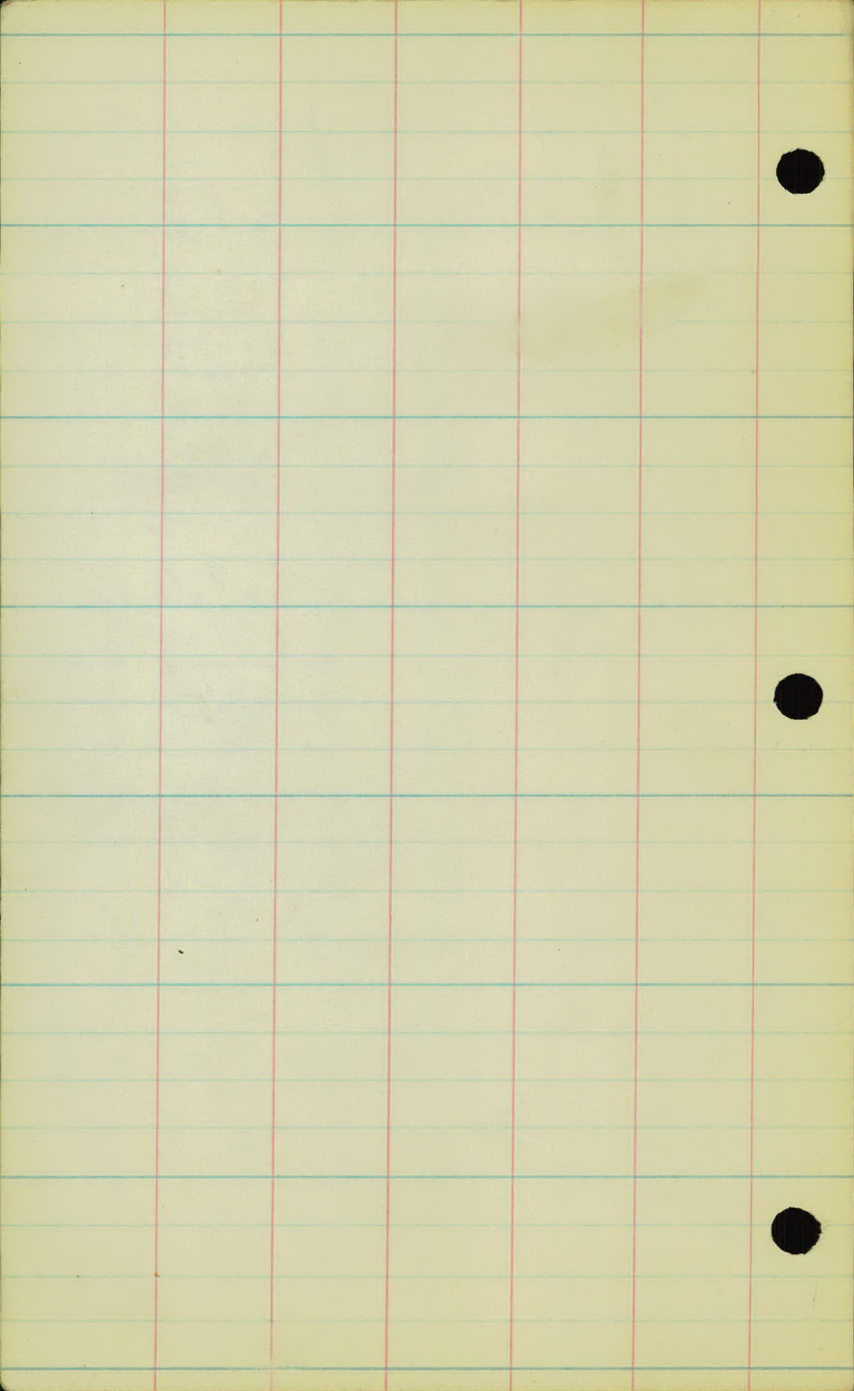
$\frac{3.6}{50}$	$\frac{4.5}{33}$	$\frac{4.7}{14}$	4.9	$\frac{4.8}{14}$	$\frac{4.9}{33}$	$\frac{5.2}{50}$
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$\frac{6.0}{33}$	$\frac{5.8}{33}$	$\frac{5.7}{14}$	5.5	$\frac{5.2}{14}$	$\frac{4.5}{33}$	$\frac{3.5}{50}$
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$\frac{7.5}{50}$	$\frac{7.5}{33}$	$\frac{7.3}{14}$	6.8	$\frac{5.7}{14}$	$\frac{5.2}{33}$	$\frac{5.0}{50}$
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$\frac{7.7}{50}$	$\frac{7.4}{33}$	$\frac{7.1}{14}$	6.7	$\frac{6.3}{14}$	$\frac{5.9}{33}$	$\frac{5.7}{50}$
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SpK. in 8" CgK. 60' Lt. Sta. 721 + 25.



Station	+	HI	-	Red.	Elev.
B.M.	2.23	992.35 ✓			890.12
T.P.	4.47	991.91 ✓	5.01	987.34 ✓	
725+00					85.8
726+00					87.8
727+00					87.4
728+00					86.4
729+00					85.6
730+00					86.3
T.P.	2.79	989.74 ✓	4.86	986.95 ✓	
731+00					85.1
732+00					84.9
733+00					85.1
T.P.	5.65	890.03 ✓	5.36	984.38 ✓	
B.M.				3.73	886.30 ✓ 886.32
T.P.	4.89	989.27 ✓	5.65	884.28 ✓	
734+00					84.4
735+00					84.7

6.7

6

74

"H" hinc 101

Spike in 8" OAK 60' ht sta 721+25

$\frac{6.3}{50.0}$	6.0	$\frac{2.4}{15.0}$	$\frac{3.4}{33.0}$	$\frac{2.7}{50.0}$
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$\frac{6.5}{50.0}$	$\frac{6.5}{35.0}$	$\frac{4.7}{13.0}$	4.0	$\frac{3.5}{25.0}$	$\frac{3.0}{50.0}$
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$\frac{6.7}{50.0}$	$\frac{6.5}{29.0}$	$\frac{5.3}{14.0}$	4.4	$\frac{3.4}{30.0}$	$\frac{3.0}{50.0}$
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$\frac{6.6}{50.0}$	$\frac{6.4}{36.0}$	$\frac{6.2}{8.0}$	5.4	$\frac{4.2}{25.0}$	$\frac{3.3}{50.0}$
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$\frac{6.5}{50.0}$	$\frac{6.0}{17.0}$	6.2	$\frac{5.2}{30.0}$	$\frac{5.0}{50.0}$
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$\frac{6.6}{50.0}$	$\frac{6.8}{22.0}$	5.5	$\frac{5.6}{22.0}$	$\frac{5.0}{35.0}$	$\frac{6.6}{50.0}$
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$\frac{4.7}{50.0}$	$\frac{4.8}{15.0}$	4.6	$\frac{4.3}{23.0}$	$\frac{4.4}{50.0}$
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$\frac{4.9}{50.0}$	$\frac{4.8}{33.0}$	$\frac{4.6}{15.0}$	4.8	$\frac{4.8}{16.0}$	$\frac{4.4}{38.0}$	$\frac{4.7}{50.0}$
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$\frac{5.1}{50.0}$	$\frac{4.9}{25.0}$	4.6	$\frac{4.7}{23.0}$	$\frac{4.6}{50.0}$
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Spike in 6" Birch 35' ht sta 732+30

$\frac{5.0}{50.0}$	$\frac{5.0}{25.0}$	4.9	$\frac{4.8}{25.0}$	$\frac{4.5}{50.0}$
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$\frac{5.0}{50.0}$	$\frac{4.8}{25.0}$	4.6	$\frac{4.6}{25.0}$	$\frac{4.6}{50.0}$
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Station	+	H.I.	-	Rod.	Elev.
		899.27			
736	+00				84.5
737	+00				84.1
738	+00				84.3
739	+00				84.1
740	+00				83.8
T.P.	3.97	888.41	4.73	894.54	
	+36				883.1
	+55	£. Crack (36" Cut)			80.1
T.P.	4.51	889.05	3.87	894.54	
	+70				82.3
741	+00				82.6
742	+00				83.9
743	+00				84.5
744	+00				84.0
745	+00				84.7

H.

E

R.

"H" line 102

$\frac{5.1}{50.0}$ $\frac{4.7}{25.0}$ 4.8 $\frac{4.8}{25.0}$ $\frac{4.6}{50.0}$

$\frac{5.0}{50.0}$ $\frac{5.0}{25.0}$ 5.2 $\frac{5.2}{25.0}$ $\frac{4.7}{50.0}$

$\frac{5.7}{50.0}$ $\frac{5.2}{25.0}$ 5.0 $\frac{4.7}{25.0}$ $\frac{4.7}{50.0}$

$\frac{5.7}{50.0}$ $\frac{5.7}{25.0}$ 5.2 $\frac{5.4}{25.0}$ $\frac{5.4}{50.0}$

$\frac{6.3}{50.0}$ $\frac{6.0}{25.0}$ 5.5 $\frac{6.0}{25.0}$ $\frac{5.8}{50.0}$

$\frac{5.7}{50.0}$ $\frac{5.7}{25.0}$ 5.3 $\frac{5.6}{15.0}$ $\frac{6.2}{34.0}$ $\frac{8.0}{50.0}$

$\frac{5.8}{50.0}$ $\frac{5.9}{32.0}$ $\frac{6.7}{15.0}$ $\frac{8.3}{19.0}$ 8.3 $\frac{6.3}{20.0}$ $\frac{5.6}{37.0}$ $\frac{6.0}{50.0}$

Top. & Stake 540 740 400

$\frac{7.0}{50.0}$ $\frac{7.0}{32.0}$ $\frac{8.4}{28.0}$ $\frac{9.0}{20.0}$ $\frac{6.8}{13.0}$ 6.8 $\frac{6.4}{14.0}$ $\frac{6.8}{27.0}$ $\frac{5.6}{50.0}$

$\frac{7.2}{50.0}$ $\frac{7.4}{32.0}$ $\frac{6.8}{17.0}$ 6.5 $\frac{5.5}{25.0}$ $\frac{5.8}{50.0}$

$\frac{6.5}{50.0}$ $\frac{6.0}{25.0}$ 5.2 $\frac{4.8}{25.0}$ $\frac{4.5}{50.0}$

$\frac{5.2}{50.0}$ $\frac{4.7}{25.0}$ 4.6 $\frac{4.5}{25.0}$ $\frac{4.6}{50.0}$

$\frac{6.0}{50.0}$ $\frac{5.9}{25.0}$ 5.1 $\frac{5.0}{25.0}$ $\frac{5.0}{50.0}$

$\frac{5.0}{50.0}$ $\frac{4.8}{25.0}$ 4.4 $\frac{4.3}{25.0}$ $\frac{4.4}{50.0}$

Station	+	H.I.	-	Rod.	Elev.
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899.05

745+50

84.3

746+00

84.6

T.P. 6.46 ✓ 891.96 3.85 895.50 ✓

+50

85.9

747+00

85.0

+65

88.2

748+00

90.0

T.P. 8.59 ✓ 899.39 1.17 ✓ 896.79

+50

92.2

749+00

93.4

+50

93.7

750+00

94.1

+50

93.9

751+00

93.6

B.M 0.59 ✓ 897.35 2.62 ✓ 896.76

896.77

Ht.

E

RH.

"H"line 103

$\frac{5.4}{50.0}$	$\frac{5.2}{25.0}$	4.8	$\frac{5.0}{25.0}$	$\frac{4.8}{50.0}$
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$\frac{4.6}{20.0}$	$\frac{4.3}{25.0}$	$\frac{4.3}{16.0}$	4.5	$\frac{4.0}{6.0}$	$\frac{3.1}{25.0}$	$\frac{2.6}{38.0}$	$\frac{2.1}{50.0}$
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$\frac{8.2}{50.0}$	$\frac{7.5}{25.0}$	$\frac{6.8}{20.0}$	6.1	$\frac{5.6}{25.0}$	$\frac{5.1}{50.0}$
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$\frac{7.0}{50.0}$	$\frac{7.0}{25.0}$	7.0	$\frac{6.2}{16.0}$	$\frac{5.6}{22.0}$	$\frac{4.6}{36.0}$	$\frac{4.2}{50.0}$
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$\frac{6.2}{50.0}$	$\frac{5.0}{50.0}$	$\frac{4.4}{20.0}$	3.8	$\frac{3.0}{24.0}$	$\frac{3.0}{50.0}$
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$\frac{3.8}{50.0}$	$\frac{2.5}{25.0}$	2.0	$\frac{2.0}{25.0}$	$\frac{1.7}{50.0}$
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$\frac{8.1}{50.0}$	$\frac{7.6}{25.0}$	7.2	$\frac{8.2}{25.0}$	$\frac{8.8}{50.0}$
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$\frac{7.3}{50.0}$	$\frac{6.4}{25.0}$	6.0	$\frac{7.0}{25.0}$	$\frac{8.3}{50.0}$
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$\frac{7.5}{50.0}$	$\frac{6.4}{25.0}$	5.1	$\frac{5.5}{25.0}$	$\frac{6.4}{50.0}$
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$\frac{8.8}{50.0}$	$\frac{7.0}{25.0}$	5.3	$\frac{5.0}{25.0}$	$\frac{5.7}{50.0}$
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$\frac{9.7}{50.0}$	$\frac{7.5}{25.0}$	5.5	$\frac{4.8}{25.0}$	$\frac{5.3}{50.0}$
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$\frac{10.3}{50.0}$	$\frac{9.5}{25.0}$	5.8	$\frac{4.2}{25.0}$	$\frac{3.7}{50.0}$
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Sp. in 30" Oak 50' Rt. Sta 751405

Station	+	H.I.	-	Rod.	Elev.
		897.35 ✓			
751 +50					92.4
752 +00					91.1
T.P.	2.85	889.49 ✓	10.71	896.64 ✓	
753 +00					85.7
754 +00					84.8
755 +00					84.7
756 +00					84.8
757 +00					85.2
T.P.	3.65	892.21 ✓	0.93	898.56 ✓	
758 +00					87.7
+50					88.6
759 +00					87.8
+50					85.6
760 +00					86.1
761 +00					87.8

H.

E

RA.

"H" line

104

$$\frac{8.5}{50.0} \quad \frac{7.2}{25.0} \quad 5.0 \quad \frac{3.0}{25.0} \quad \frac{1.7}{50.0}$$

$$\frac{9.1}{50.0} \quad \frac{8.2}{25.0} \quad 6.3 \quad \frac{5.4}{25.0} \quad \frac{4.4}{50.0}$$

$$\frac{3.8}{50.0} \quad \frac{3.7}{25.0} \quad 3.8 \quad \frac{3.7}{25.0} \quad \frac{3.7}{50.0}$$

$$\frac{5.0}{50.0} \quad \frac{4.9}{25.0} \quad 4.7 \quad \frac{4.9}{25.0} \quad \frac{5.0}{50.0}$$

$$\frac{5.1}{50.0} \quad \frac{5.0}{25.0} \quad 4.8 \quad \frac{4.8}{25.0} \quad \frac{4.6}{50.0}$$

$$\frac{5.1}{50.0} \quad \frac{4.8}{25.0} \quad 4.7 \quad \frac{4.7}{25.0} \quad \frac{4.8}{50.0}$$

$$\frac{4.8}{50.0} \quad \frac{4.6}{25.0} \quad 4.3 \quad \frac{4.2}{25.0} \quad \frac{3.9}{25.0}$$

$$\frac{5.6}{50.0} \quad \frac{4.9}{25.0} \quad 4.5 \quad \frac{4.5}{25.0} \quad \frac{4.3}{50.0}$$

$$\frac{5.2}{50.0} \quad \frac{4.2}{25.0} \quad 3.6 \quad \frac{3.5}{25.0} \quad \frac{3.4}{50.0}$$

$$\frac{5.6}{50.0} \quad \frac{5.0}{25.0} \quad 4.4 \quad \frac{4.4}{25.0} \quad \frac{4.8}{50.0}$$

$$\frac{-0.8}{50.0} \quad \frac{-0.5}{25.0} \quad +0.5 \quad \frac{0.0}{50.0}$$

$$\frac{-0.8}{50.0} \quad \frac{-0.4}{25.0} \quad +0.7 \quad \frac{+1.2}{50.0}$$

$$\frac{-1.2}{50.0} \quad \frac{-0.7}{25.0} \quad +1.0 \quad \frac{+1.7}{50.0}$$

Station	+	H.I.	-	Rob	Elev.
		892.21			
762+00					89.8
763+00					88.5
T.P.	2.37	893.00 ✓	1.58	890.63	
+40					88.3 ✓
B.M.				2.34	890.66
764+00					87.4
+50					88.4
765+00					87.6
766+00					86.2
+30					86.4
767+00					85.4
768+00					85.5
T.P.	4.69	891.14 ✓	6.55	886.45 ✓	
769+00					86.0
+16					86.3
+25					84.9

Station	+	H.I.	-	Red.	Elev.
		891.14			
769+50	±	Red			86.4
	+68				85.3
	+93				86.8
770+00					87.1
	+50				86.7
771+00					85.1
T.P.	0.78	886.90 ✓	5.02	886.12 ✓	
	+38				83.6
772+00					82.1
773+00					81.8
774+00					81.4
T.P.	3.98	885.53 ✓	5.35	881.55 ✓	
B.M				8.90	891.63 ✓

ht.

£

ht.

$\frac{5.4}{50.0}$	$\frac{5.0}{25.0}$	4.7	$\frac{4.2}{25.0}$	$\frac{4.3}{50.0}$
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$\frac{5.6}{50.0}$	$\frac{5.6}{25.0}$	5.8	$\frac{4.7}{25.0}$	$\frac{3.7}{35.0}$	$\frac{3.6}{50.0}$
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$\frac{5.4}{50.0}$	$\frac{4.9}{39.0}$	$\frac{4.2}{25.0}$	4.3	$\frac{3.6}{25.0}$	$\frac{3.7}{50.0}$
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$\frac{5.3}{50.0}$	$\frac{4.5}{24.0}$	4.0	$\frac{3.7}{25.0}$	$\frac{3.5}{50.0}$
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$\frac{5.1}{50.0}$	$\frac{4.5}{25.0}$	4.4	$\frac{4.5}{23.0}$	$\frac{4.9}{50.0}$
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$\frac{5.5}{50.0}$	$\frac{5.3}{25.0}$	6.0	$\frac{6.7}{26.0}$	$\frac{7.3}{50.0}$
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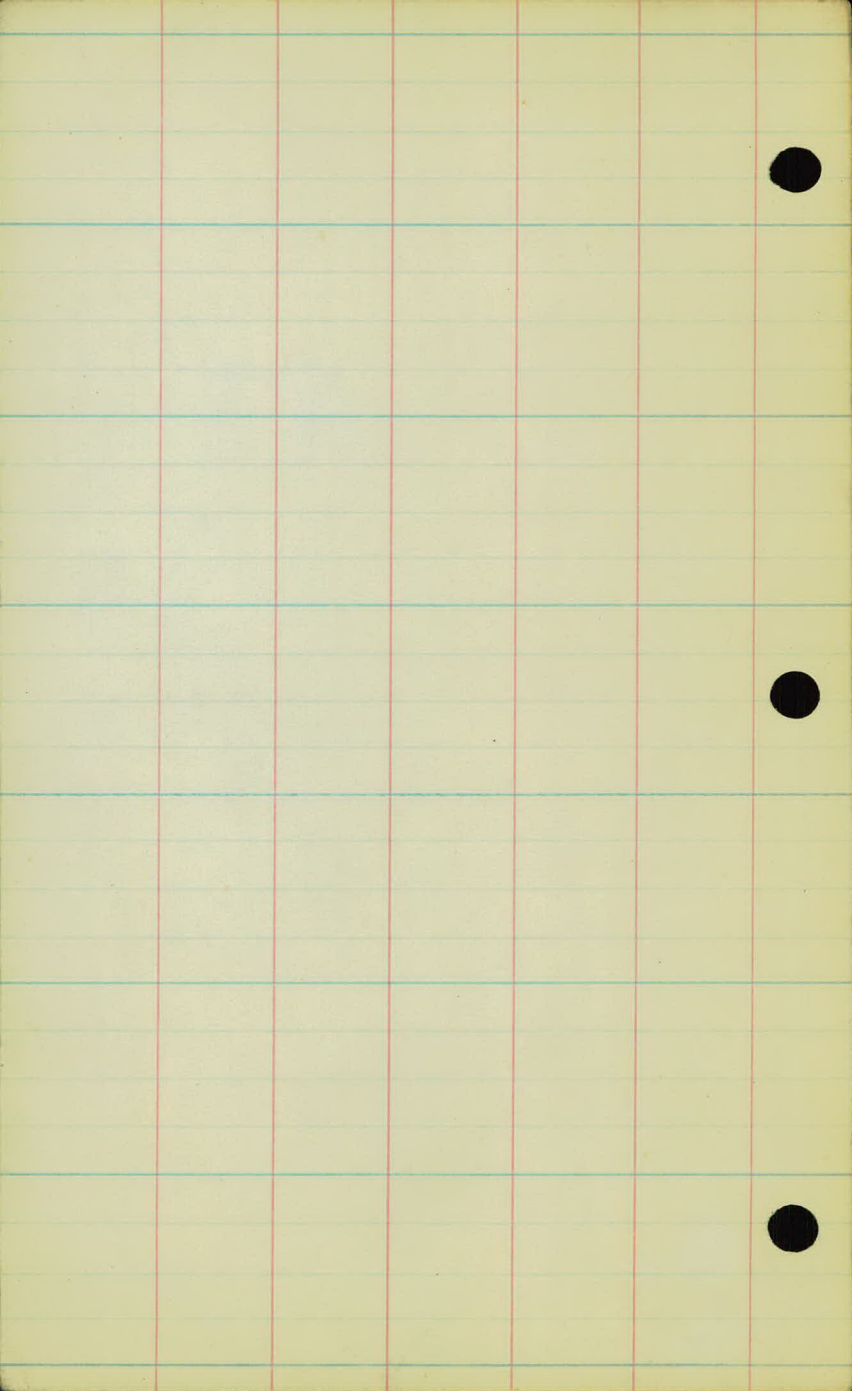
$\frac{2.7}{50.0}$	$\frac{3.0}{21.0}$	$\frac{3.5}{11.0}$	3.3	$\frac{4.0}{15.0}$	$\frac{4.7}{30.0}$	$\frac{4.7}{50.0}$
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$\frac{4.8}{50.0}$	$\frac{4.0}{23.0}$	$\frac{4.7}{11.0}$	4.8	$\frac{4.6}{25.0}$	$\frac{4.8}{50.0}$
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$\frac{4.5}{50.0}$	$\frac{5.4}{32.0}$	$\frac{4.9}{15.0}$	5.1	$\frac{5.0}{25.0}$	$\frac{5.0}{50.0}$
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$\frac{5.7}{50.0}$	$\frac{5.5}{25.0}$	5.4	$\frac{5.3}{30.0}$	$\frac{5.3}{50.0}$
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50 ht. sta 778 to 0



X SECTIONS

775 to 836+759

Amster & Crane.

Sta.	+	H.I.	-	Rad	Elev.
B.M.	2.98	884.68		881.70	
775				3.7	881.0
776				3.7	881.0
777				4.5	880.2
778				5.1	879.6
T.P.	1.41	881.81	4.28	880.40	
779				3.3	878.5
780				4.0	877.8
781				4.4	877.4
782				5.4	876.4
783				5.5	876.3
784				5.4	876.4
T.P.	1.27	877.90	5.20	876.61	
785				2.2	875.7
786				3.1	874.8
787				4.0	873.9

£ "A" WNE
 TT

1/13/25
 108

sph. in 6" Birch 65 Lt. Sta. 778+00

$\frac{3.7}{50}$ $\frac{3.6}{33}$ $\frac{3.6}{16}$ 3.7 $\frac{3.6}{14}$ $\frac{3.7}{33}$ $\frac{3.6}{33}$

775+00

$\frac{4.0}{50}$ $\frac{4.2}{33}$ $\frac{4.1}{14}$ 3.7 $\frac{4.0}{16}$ $\frac{4.2}{33}$ $\frac{4.2}{50}$

$\frac{4.6}{50}$ $\frac{4.6}{33}$ $\frac{4.5}{14}$ 4.5 $\frac{4.4}{14}$ $\frac{4.3}{33}$ $\frac{4.1}{50}$

$\frac{5.1}{50}$ $\frac{5.1}{33}$ $\frac{5.1}{14}$ 5.1 $\frac{4.9}{14}$ $\frac{4.9}{33}$ $\frac{4.8}{50}$

$\frac{3.2}{50}$ $\frac{3.8}{33}$ $\frac{3.1}{14}$ 3.3 $\frac{2.8}{14}$ $\frac{3.2}{33}$ $\frac{3.0}{50}$

$\frac{3.7}{50}$ $\frac{4.0}{33}$ $\frac{4.1}{14}$ 4.0 $\frac{3.8}{14}$ $\frac{3.6}{33}$ $\frac{3.6}{50}$

$\frac{4.4}{50}$ $\frac{4.6}{33}$ $\frac{4.6}{14}$ 4.4 $\frac{4.5}{14}$ $\frac{4.6}{33}$ $\frac{4.7}{50}$

$\frac{5.4}{50}$ $\frac{5.4}{33}$ $\frac{5.2}{14}$ 5.4 $\frac{5.4}{14}$ $\frac{5.4}{33}$ $\frac{5.2}{50}$

$\frac{5.5}{50}$ $\frac{5.4}{33}$ $\frac{5.7}{14}$ 5.5 $\frac{5.5}{14}$ $\frac{5.3}{33}$ $\frac{5.3}{50}$

$\frac{5.8}{50}$ $\frac{5.6}{33}$ $\frac{5.5}{14}$ 5.4 $\frac{5.4}{14}$ $\frac{5.6}{33}$ $\frac{5.4}{50}$

$\frac{2.0}{50}$ $\frac{2.3}{33}$ $\frac{2.4}{14}$ 2.2 $\frac{2.1}{14}$ $\frac{1.7}{33}$ $\frac{1.5}{50}$

$\frac{3.3}{50}$ $\frac{3.3}{33}$ $\frac{3.3}{14}$ 3.1 $\frac{2.9}{14}$ $\frac{2.8}{33}$ $\frac{2.7}{50}$

$\frac{3.8}{50}$ $\frac{3.8}{33}$ $\frac{4.0}{14}$ 4.0 $\frac{4.1}{14}$ $\frac{4.0}{33}$ $\frac{3.9}{50}$

Sta	+	H.I.	-	Rod	Elev.
		877.90			✓
788				4.7	873.0 ✓
T.P.	5.83	879.03 ✓	4.70	873.20 ✓	
789				6.7	872.6 ✓
790				6.4	872.6 ✓
	+30			4.8	874.2 ✓
791				4.6	874.4 ✓
	+50			4.8	874.2 ✓
792	Corrected ✓			7.1	871.9 ✓
B.M.	4.40	879.05 ✓	4.40	874.63	874.65
	+50			10.3	868.8 ✓
793				11.3	867.8 ✓
T.P.	1.42	870.07 ✓	10.40	868.65 ✓	
794				2.4	867.7 ✓
795				4.5	865.6 ✓
796				5.8	864.3 ✓
	+50			6.6	863.5 ✓

17.

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17.

$\frac{5.0}{50}$	$\frac{5.1}{33}$	$\frac{5.1}{16}$	4.9	$\frac{4.7}{16}$	$\frac{4.6}{33}$	$\frac{4.5}{50}$	<u>788</u>
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$\frac{6.9}{50}$	$\frac{7.0}{33}$	$\frac{6.5}{16}$	6.4	$\frac{6.5}{16}$	$\frac{5.5}{33}$	$\frac{5.3}{50}$
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$\frac{7.5}{50}$	$\frac{7.5}{33}$	$\frac{7.1}{16}$	6.4	$\frac{6.0}{9}$	$\frac{5.7}{16}$	$\frac{5.4}{27}$	$\frac{5.0}{33}$	$\frac{3.8}{39}$	$\frac{3.7}{50}$
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$\frac{7.4}{50}$	$\frac{7.4}{33}$	$\frac{6.3}{16}$	$\frac{5.8}{6}$	4.8	$\frac{4.9}{16}$	$\frac{4.3}{22}$	$\frac{3.3}{33}$	$\frac{3.8}{40}$	$\frac{3.3}{50}$
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$\frac{8.1}{50}$	$\frac{7.0}{33}$	$\frac{5.5}{27}$	$\frac{5.2}{16}$	$\frac{5.2}{7}$	4.6	$\frac{3.6}{16}$	$\frac{4.3}{27}$	$\frac{2.5}{33}$	$\frac{1.6}{50}$
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$\frac{8.2}{50}$	$\frac{7.4}{33}$	$\frac{6.5}{16}$	$\frac{5.6}{10}$	4.8	$\frac{4.6}{16}$	$\frac{3.2}{33}$	$\frac{2.9}{50}$
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$\frac{10.0}{50}$	$\frac{7.6}{33}$	$\frac{8.5}{16}$	7.1	$\frac{5.8}{16}$	$\frac{5.4}{33}$	$\frac{4.7}{50}$
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S.P.K. in stump 75' Rt. Sta. 792+20.

$\frac{10.8}{50}$	$\frac{10.6}{33}$	$\frac{10.4}{16}$	10.3	$\frac{9.9}{16}$	$\frac{8.7}{33}$	$\frac{8.4}{50}$
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$\frac{11.3}{50}$	$\frac{11.4}{33}$	$\frac{11.0}{16}$	11.3	$\frac{11.2}{16}$	$\frac{11.0}{33}$	$\frac{10.5}{50}$
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$\frac{3.1}{50}$	$\frac{2.8}{33}$	$\frac{2.5}{16}$	2.4	$\frac{2.4}{16}$	$\frac{2.2}{33}$	$\frac{2.2}{50}$
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$\frac{5.1}{50}$	$\frac{4.6}{33}$	$\frac{4.2}{16}$	4.5	$\frac{4.2}{16}$	$\frac{4.2}{33}$	$\frac{4.0}{50}$
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$\frac{6.0}{50}$	$\frac{6.5}{43}$	$\frac{6.5}{33}$	$\frac{5.4}{14}$	$\frac{5.6}{12}$	$\frac{7.0}{8}$	$\frac{8.6}{7}$	$\frac{8.6}{5}$	$\frac{6.2}{4}$	5.8	$\frac{5.4}{16}$	$\frac{5.2}{33}$	$\frac{5.1}{50}$
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$\frac{5.8}{50}$	$\frac{5.5}{33}$	$\frac{5.2}{18}$	$\frac{6.4}{13}$	6.4	$\frac{7.0}{4}$	$\frac{8.3}{5}$	$\frac{7.0}{6}$	$\frac{6.6}{16}$	$\frac{6.1}{33}$	$\frac{5.7}{50}$
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Sta.	+	H.I.	-	Rod.	Elev.
		870.07			
+77				6.5	863.6 ✓
797				5.5	864.6 ✓
+50				6.3	863.8 ✓
798				10.9	859.2 ✓
T.P.	8.41	867.68	10.80	859.27	
799 ✓				9.5	858.2 ✓
+42				8.7	859.0 ✓

TO R-114

SEE REVISED
LINE

800				7.6	860.1 ✓
+50				6.6	861.1 ✓
801				6.1	861.6 ✓
+50				5.9	861.8 ✓
802				5.4	862.3 ✓
+50				5.5	862.2 ✓
803				7.0	860.7 ✓

"H" LINE

1/13/26
110

Lt.

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Rt.

$\frac{5.6}{50}$	$\frac{5.8}{33}$	$\frac{5.4}{14}$	$\frac{5.4}{6}$	6.5	$\frac{7.4}{11}$	$\frac{8.8}{12}$	$\frac{7.2}{18}$	$\frac{7.5}{14}$	$\frac{7.1}{33}$	$\frac{6.6}{50}$
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797

$\frac{5.4}{50}$	$\frac{5.4}{33}$	$\frac{5.6}{14}$	5.5	4	$\frac{5.5}{11}$	$\frac{7.2}{17}$	$\frac{7.8}{18}$	$\frac{7.1}{18}$	$\frac{7.8}{19}$	$\frac{7.9}{33}$	$\frac{7.1}{50}$
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$\frac{7.1}{50}$	$\frac{6.6}{33}$	$\frac{6.9}{24}$	$\frac{6.3}{14}$	6.3	$\frac{6.2}{4}$	$\frac{7.1}{15}$	$\frac{8.0}{17}$	$\frac{9.6}{18}$	$\frac{7.5}{21}$	$\frac{8.4}{22}$	$\frac{9.0}{33}$	$\frac{8.4}{50}$
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$\frac{11.8}{50}$	$\frac{11.2}{33}$	$\frac{11.0}{16}$	10.9	$\frac{10.8}{16}$	$\frac{10.9}{33}$	$\frac{9.7}{50}$
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$\frac{11.3}{50}$	$\frac{10.3}{33}$	$\frac{9.8}{14}$	9.5	$\frac{8.9}{16}$	$\frac{8.8}{33}$	$\frac{8.3}{50}$
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$\frac{10.6}{50}$	$\frac{9.8}{33}$	$\frac{9.2}{16}$	8.9	$\frac{8.2}{16}$	$\frac{7.2}{33}$	$\frac{7.0}{50}$
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$\frac{9.0}{50}$	$\frac{8.2}{33}$	$\frac{7.9}{14}$	7.6	$\frac{7.0}{14}$	$\frac{6.6}{33}$	$\frac{6.2}{50}$
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$\frac{7.9}{50}$	$\frac{7.3}{33}$	$\frac{7.3}{14}$	6.6	$\frac{6.2}{16}$	$\frac{6.0}{33}$	$\frac{5.7}{50}$
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$\frac{7.9}{50}$	$\frac{7.6}{33}$	$\frac{6.6}{14}$	6.1	$\frac{5.8}{14}$	$\frac{5.5}{33}$	$\frac{5.1}{50}$
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$\frac{7.4}{50}$	$\frac{6.6}{33}$	$\frac{6.6}{14}$	5.9	$\frac{5.6}{14}$	$\frac{5.0}{33}$	$\frac{4.6}{50}$
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$\frac{7.2}{50}$	$\frac{6.8}{33}$	$\frac{6.2}{14}$	5.4	$\frac{5.0}{16}$	$\frac{4.7}{33}$	$\frac{3.9}{50}$
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$\frac{7.6}{50}$	$\frac{7.1}{33}$	$\frac{6.7}{33}$	$\frac{7.7}{22}$	$\frac{6.4}{20}$	$\frac{6.3}{14}$	5.5	$\frac{4.9}{14}$	$\frac{4.6}{33}$	$\frac{4.3}{50}$
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$\frac{8.6}{50}$	$\frac{7.8}{33}$	$\frac{7.4}{14}$	7.0	$\frac{6.3}{16}$	$\frac{5.8}{33}$	$\frac{4.9}{50}$
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Sta	+	H.I	-	Red.	Elev.
		867.68			
+50				7.9	859.8 ✓
804				10.3	857.4 ✓
T.P.	0.73	859.27 ✓	9.14	858.54	
+50				4.7	854.4 ✓
805				7.4	851.9 ✓
806				11.5	847.8 ✓
B.M.	3.94	855.01 ✓	8.21	851.06	851.07 ✓
+50				10.2	844.8 ✓
807				12.3	842.7 ✓
+10				11.2	843.8 ✓
+20.				10.4	844.4 ✓
808				10.0	845.0 ✓
+10				8.4	846.4 ✓
+18				7.7	847.3 ✓
+31				0.2	854.8 ✓
T.P.	10.84	865.48 ✓	0.37	854.44	

Lt. 6 Pt.

$\frac{9.7}{50}$ $\frac{9.2}{33}$ $\frac{8.8}{16}$ 7.9 $\frac{7.4}{16}$ $\frac{5.8}{33}$ $\frac{4.9}{50}$

804

$\frac{12.3}{50}$ $\frac{11.8}{33}$ $\frac{11.1}{16}$ 10.3 $\frac{10.5}{16}$ $\frac{9.2}{33}$ $\frac{7.8}{50}$

$\frac{1}{2}$ of Creek = $\frac{12.3}{200}$

$\frac{6.0}{50}$ $\frac{5.9}{33}$ $\frac{5.2}{16}$ 4.7 $\frac{4.1}{16}$ $\frac{3.6}{33}$ $\frac{2.6}{50}$

$\frac{7.3}{50}$ $\frac{7.3}{33}$ $\frac{7.4}{16}$ 7.2 $\frac{6.4}{16}$ $\frac{5.7}{33}$ $\frac{4.9}{50}$

$\frac{12.6}{50}$ $\frac{12.4}{33}$ $\frac{12.0}{16}$ 11.5 $\frac{10.7}{16}$ $\frac{9.8}{33}$ $\frac{8.4}{50}$

On top of coping S.E. Cor. of culvert Pt. Sta. 808+20

$\frac{11.5}{50}$ $\frac{11.3}{44}$ $\frac{11.3}{33}$ $\frac{11.2}{16}$ 10.2 $\frac{10.5}{16}$ $\frac{10.3}{33}$ $\frac{7.8}{50}$

$\frac{10.7}{50}$ $\frac{10.8}{33}$ $\frac{11.3}{14}$ 12.3 $\frac{11.1}{16}$ $\frac{10.9}{33}$ $\frac{10.6}{50}$

$\frac{10.2}{50}$ $\frac{10.6}{33}$ $\frac{10.6}{15}$ 11.2 $\frac{11.3}{14}$ $\frac{11.3}{33}$ $\frac{11.3}{50}$

$\frac{10.2}{50}$ $\frac{10.4}{33}$ $\frac{10.5}{16}$ 10.6 $\frac{10.6}{16}$ $\frac{11.6}{33}$ $\frac{11.3}{43}$ $\frac{11.3}{50}$

$\frac{7.6}{50}$ $\frac{5.9}{33}$ $\frac{9.4}{16}$ 10.0 $\frac{10.0}{16}$ $\frac{10.3}{30}$ $\frac{10.9}{33}$ $\frac{11.3}{39}$ $\frac{11.3}{50}$

$\frac{5.3}{50}$ $\frac{7.7}{33}$ $\frac{8.5}{16}$ 8.6 $\frac{7.1}{16}$ $\frac{10.5}{33}$ $\frac{11.4}{41}$ $\frac{11.4}{50}$

$\frac{3.7}{50}$ $\frac{6.7}{33}$ $\frac{7.0}{16}$ 7.7 $\frac{7.3}{16}$ $\frac{5.5}{16}$ $\frac{6.0}{16}$ $\frac{6.7}{33}$ $\frac{9.4}{50}$

0.1 $\frac{3.0}{16}$ $\frac{4.5}{31}$ $\frac{5.6}{33}$ $\frac{6.5}{50}$

Sta.	+	H.I.	-	Red.	Elev
		865.48			
808+31				10.7	854.8 ✓
+43				2.8	862.7 ✓
T.P.	6.16	868.70 ✓	2.94	862.54 ✓	
808+43					
+51				2.1	866.6 ✓
+61				1.0	867.7 ✓
+70				2.1	866.6 ✓
+80				6.1	862.6 ✓
+94					
T.P.	2.03	859.13 ✓	11.60	857.10 ✓	
808+94				7.0	852.1 ✓
809				8.0	851.1 ✓
+11				8.9	850.2 ✓
+60				10.3	848.8 ✓
+70				8.8	850.3 ✓

Lt.

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"H" LINE

1/14/25

RT.

112

$\frac{0.8}{50}$	$\frac{4.2}{33}$	$\frac{7.6}{16}$	10.7
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80pt31

2.5	$\frac{6.1}{16}$	$\frac{9.4}{33}$	$\frac{13.5}{50}$
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$\frac{67.7}{50}$	$\frac{67.0}{33}$	$\frac{66.5}{15}$	$\frac{66.3}{14}$
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$\frac{1.2}{50}$	$\frac{1.0}{33}$	$\frac{1.2}{17}$	2.1	$\frac{3.5}{76}$	$\frac{6.1}{33}$	$\frac{8.8}{50}$
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$\frac{2.2}{50}$	$\frac{1.6}{33}$	$\frac{1.1}{18}$	1.0	$\frac{1.3}{21}$	$\frac{1.2}{33}$	$\frac{2.5}{42}$	$\frac{3.1}{50}$
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$\frac{9.0}{50}$	$\frac{4.4}{33}$	$\frac{3.7}{19}$	2.1	$\frac{1.2}{19}$	$\frac{1.1}{33}$	$\frac{1.3}{50}$
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$\frac{14.7}{50}$	$\frac{11.8}{33}$	6.1	$\frac{2.5}{22}$	$\frac{2.0}{33}$	$\frac{1.3}{50}$
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$\frac{57.7}{33}$	$\frac{59.9}{50}$
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$\frac{8.6}{50}$	$\frac{8.6}{33}$	$\frac{9.5}{16}$	9.0
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$\frac{9.4}{50}$	$\frac{9.4}{39}$	$\frac{7.9}{33}$	8.0	$\frac{7.2}{78}$	$\frac{4.4}{33}$	$\frac{1.7}{50}$
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$\frac{7.6}{50}$	$\frac{9.7}{33}$	$\frac{9.4}{7}$	8.9	$\frac{7.3}{33}$	$\frac{4.2}{50}$
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$\frac{8.8}{50}$	$\frac{9.0}{33}$	$\frac{8.8}{72}$	$\frac{10.1}{8}$	10.3	$\frac{10.0}{17}$	$\frac{10.2}{33}$	$\frac{10.0}{42}$	$\frac{11.1}{50}$
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$\frac{8.7}{50}$	$\frac{9.0}{33}$	$\frac{9.3}{11}$	8.8	9.2	$\frac{11.1}{3}$	$\frac{11.3}{9}$	$\frac{10.0}{12}$	$\frac{10.4}{33}$	$\frac{11.2}{50}$
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Sta.	+	H.I.	-	Rad.	Elev.
		359.15			
810				9.5	849.6 ✓
	+41			9.5	849.6 ✓
811				5.1	854.0 ✓
	+38			4.3	854.8 ✓
	+51			5.5	853.6 ✓
	+75			5.1	854.0 ✓
	+92			4.0	855.1 ✓
812				2.0	857.1 ✓
812 + 05				1.0	858.1 ✓
T.P.	11.36	869.20	11.29	857.54 ✓	
811 + 75					
811 + 92					
812					
812 + 15					

Lt.

4 "H" LINE

1/14/35

113

Rt.

$\frac{9.0}{50}$	$\frac{9.3}{33}$	$\frac{9.4}{14}$	9.5	$\frac{10.6}{16}$	$\frac{10.4}{33}$	$\frac{10.9}{50}$
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810

$\frac{6.5}{50}$	$\frac{7.7}{33}$	$\frac{8.5}{14}$	9.5	$\frac{10.1}{16}$	$\frac{10.4}{33}$	$\frac{11.0}{50}$
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$\frac{6.2}{50}$	$\frac{5.2}{44}$	$\frac{4.6}{33}$	$\frac{4.7}{14}$	5.1	$\frac{5.5}{16}$	$\frac{5.9}{33}$	$\frac{6.9}{50}$
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$\frac{6.1}{50}$	$\frac{6.7}{33}$	$\frac{6.9}{28}$	$\frac{6.4}{12}$	4.3	$\frac{3.9}{8}$	$\frac{4.5}{33}$	$\frac{4.9}{50}$
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$\frac{4.2}{50}$	$\frac{5.6}{33}$	$\frac{6.0}{9}$	5.5	$\frac{4.9}{11}$	$\frac{3.7}{19}$	$\frac{3.9}{33}$	$\frac{4.2}{50}$
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$\frac{2.2}{33}$	$\frac{4.7}{15}$	5.1	$\frac{5.5}{17}$	$\frac{5.3}{26}$	$\frac{4.7}{33}$	$\frac{3.2}{46}$	$\frac{2.9}{50}$
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$\frac{0.5}{20}$	$\frac{3.0}{7}$	4.0	$\frac{4.8}{8}$	$\frac{5.3}{33}$	$\frac{4.9}{50}$
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2.0	$\frac{4.6}{11}$	$\frac{5.2}{18}$	$\frac{5.1}{33}$	$\frac{5.2}{50}$
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1.0	$\frac{4.8}{16}$	$\frac{5.2}{33}$	$\frac{5.2}{50}$
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61.8

7.4

50

66.5

66.1

62.3

2.9

3.1

6.9

50

44

33

66.7 66.1 66.1 59.4

2.5

3.1

4.1

2.8

50

32

27

11

12.1

66.5

66.2

66.0

64.8

59.4

2.9

3.0

3.2

4.4

7.8

50

33

27

42

7

Sta.	+	H.I.	-	Red.	Elev
		869.20			
812	+21			3.8	865.4 ✓
	+40			2.9	866.3 ✓
	+56			4.8	864.4 ✓
	+74			3.7	865.5 ✓
	+88			5.0	864.2 ✓
813				8.6	860.6 ✓
	+12			12.0	857.2 ✓
	+27			11.7	857.5 ✓
	+40			11.3	857.9 ✓
	+49			9.2	860.0 ✓
	+66			9.4	859.8 ✓
814				11.7	857.5 ✓
T.P.	2.21	860.41	11.00	859.20	✓
815				4.2	856.2 ✓

Lt.

¢

Rt.

812+21

$\frac{3.2}{50}$	$\frac{3.3}{33}$	$\frac{2.7}{14}$	$\frac{3.3}{8}$	3.8	$\frac{4.7}{5}$	$\frac{7.5}{11}$	$\frac{14.1}{28}$	$\frac{14.8}{37}$	$\frac{15.0}{50}$
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$\frac{3.4}{50}$	$\frac{3.7}{33}$	$\frac{4.2}{24}$	$\frac{3.7}{16}$	2.7	$\frac{2.9}{7}$	$\frac{3.8}{13}$	$\frac{4.1}{24}$	$\frac{6.8}{33}$	$\frac{10.6}{50}$
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$\frac{5.2}{50}$	$\frac{4.4}{33}$	$\frac{3.8}{26}$	$\frac{3.6}{12}$	4.8	$\frac{3.4}{15}$	$\frac{2.9}{26}$	$\frac{3.5}{33}$	$\frac{3.5}{41}$	$\frac{6.5}{50}$
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$\frac{11.9}{50}$	$\frac{10.4}{44}$	$\frac{7.4}{33}$	$\frac{6.5}{30}$	$\frac{5.2}{27}$	3.7	$\frac{3.7}{8}$	$\frac{5.0}{21}$	$\frac{3.9}{33}$	$\frac{3.5}{39}$	$\frac{3.1}{50}$
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$\frac{11.5}{50}$	$\frac{11.8}{33}$	$\frac{10.2}{20}$	$\frac{7.1}{12}$	$\frac{5.6}{4}$	5.0	$\frac{4.3}{11}$	$\frac{3.9}{26}$	$\frac{4.7}{33}$	$\frac{5.2}{41}$	$\frac{4.4}{50}$
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$\frac{10.9}{50}$	$\frac{11.8}{33}$	$\frac{12.3}{18}$	$\frac{10.7}{6}$	8.6	$\frac{5.6}{10}$	$\frac{5.0}{20}$	$\frac{4.0}{33}$	$\frac{4.0}{41}$	$\frac{4.8}{50}$
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$\frac{6.8}{50}$	$\frac{10.5}{33}$	$\frac{11.5}{28}$	$\frac{12.0}{14}$	12.1	$\frac{10.2}{10}$	$\frac{6.5}{21}$	$\frac{5.0}{33}$	$\frac{4.0}{50}$
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$\frac{7.1}{50}$	$\frac{6.9}{33}$	$\frac{7.2}{26}$	$\frac{10.1}{12}$	11.7	$\frac{12.0}{16}$	$\frac{10.9}{23}$	$\frac{9.0}{28}$	$\frac{6.2}{33}$	$\frac{4.7}{50}$
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$\frac{7.8}{50}$	$\frac{7.5}{33}$	$\frac{8.0}{15}$	11.3	$\frac{11.5}{19}$	$\frac{12.7}{33}$	$\frac{11.1}{40}$	$\frac{6.9}{50}$
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$\frac{8.4}{50}$	$\frac{8.3}{33}$	$\frac{8.3}{9}$	7.2	$\frac{11.5}{15}$	$\frac{11.8}{24}$	$\frac{12.8}{33}$	$\frac{13.2}{43}$	$\frac{12.0}{50}$
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$\frac{9.2}{50}$	$\frac{9.1}{33}$	$\frac{9.0}{16}$	9.4	$\frac{10.0}{16}$	$\frac{10.0}{27}$	$\frac{10.6}{33}$	$\frac{11.2}{37}$	$\frac{13.3}{43}$	$\frac{13.7}{50}$
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$\frac{12.6}{50}$	$\frac{12.5}{33}$	$\frac{12.0}{14}$	11.7	$\frac{12.3}{14}$	$\frac{12.5}{33}$	$\frac{12.8}{50}$
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$\frac{4.3}{50}$	$\frac{4.3}{33}$	$\frac{4.3}{14}$	4.2	$\frac{4.4}{16}$	$\frac{4.5}{33}$	$\frac{4.7}{50}$
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Sta.	+	H.I.	-	Red.	Elev.
		860.41			
+45				5.1	855.3 ✓
+54				5.5	854.9 ✓
+74				6.1	854.3 ✓
B.M.	0.66	856.07 ✓	5.01	855.40	855.41 ✓
+79				4.5	851.6 ✓
+92				5.8	850.3 ✓
816				12.1	844.0 ✓
T.P.	0.78	845.54 ✓	11.31	844.76 ✓	
+12				5.7	840.1 ✓
+19				9.5	838.0 ✓
+45				8.4	837.1 ✓
T.P.	3.07	837.72 ✓	10.89	834.65 ✓	
+54				4.9	832.8 ✓
+74				7.0	830.7 ✓
817				7.0	830.7 ✓
T.P.	5.75	838.57 ✓	5.10	832.62 ✓	
+17				7.5	830.9 ✓

1/15/25
115

\$ "H" LINE
RT.

Lt.

815+45

$\frac{5.2}{50}$ $\frac{5.1}{33}$ $\frac{5.2}{14}$ 5.1 $\frac{5.1}{14}$ $\frac{5.0}{33}$ $\frac{4.8}{50}$

$\frac{5.3}{50}$ $\frac{5.3}{33}$ $\frac{5.4}{14}$ 5.5 $\frac{5.5}{14}$ $\frac{6.1}{25}$ $\frac{7.7}{33}$ $\frac{10.5}{42}$ $\frac{9.8}{50}$

$\frac{7.8}{50}$ $\frac{6.1}{45}$ $\frac{5.7}{33}$ $\frac{5.7}{14}$ $\frac{5.7}{4}$ 6.1 $\frac{11.7}{14}$ $\frac{845.0}{33}$ $\frac{845.5}{36}$ $\frac{844.4}{42}$ $\frac{841.5}{50}$

SPK in stump RT. Stg. 815+60.

$\frac{4.6}{50}$ $\frac{4.3}{45}$ $\frac{1.6}{33}$ $\frac{1.5}{14}$ $\frac{1.0}{5}$ 4.5 $\frac{5.8}{7}$ $\frac{6.8}{14}$ $\frac{9.0}{17}$ $\frac{8.9}{20}$ $\frac{10.4}{25}$ $\frac{842.0}{31}$

$\frac{2.5}{50}$ $\frac{5.5}{41}$ $\frac{6.4}{33}$ $\frac{6.5}{31}$ $\frac{5.4}{22}$ $\frac{3.5}{11}$ $\frac{6.2}{4}$ 5.8 $\frac{845.5}{4}$ $\frac{845.1}{10}$ $\frac{841.3}{17}$ $\frac{838.7}{33}$ $\frac{834.6}{50}$

$\frac{1.7}{50}$ $\frac{1.7}{44}$ $\frac{2.5}{38}$ $\frac{4.6}{33}$ $\frac{6.6}{29}$ $\frac{8.1}{19}$ $\frac{8.2}{12}$ $\frac{7.8}{7}$ 12.1 $\frac{842.8}{12}$ $\frac{837.8}{17}$ $\frac{838.1}{21}$ $\frac{835.4}{33}$ $\frac{838.7}{43}$ $\frac{832.0}{50}$

$\frac{854.1}{50}$ $\frac{853.7}{33}$ $\frac{855.3}{29}$ $\frac{842.3}{14}$ 5.4 $\frac{9.6}{14}$ $\frac{832.2}{24}$ $\frac{831.5}{21}$ $\frac{830.6}{33}$ $\frac{831.9}{50}$

$\frac{852.5}{50}$ $\frac{853.5}{33}$ $\frac{852.1}{22}$ $\frac{845.5}{11}$ 7.5 $\frac{832.9}{12}$ $\frac{831.3}{14}$ $\frac{830.8}{33}$ $\frac{831.7}{41}$ $\frac{831.7}{50}$

$\frac{853.3}{50}$ $\frac{851.2}{33}$ $\frac{852.8}{25}$ $\frac{850.7}{22}$ $\frac{843.3}{7}$ 18 $\frac{831.4}{5}$ $\frac{830.2}{11}$ $\frac{830.7}{20}$ $\frac{831.4}{28}$ $\frac{831.5}{33}$ $\frac{831.5}{50}$

$\frac{853.3}{50}$ $\frac{853.2}{33}$ $\frac{851.7}{27}$ $\frac{843.7}{14}$ $\frac{836.7}{4}$ 4.9 $\frac{7.5}{5}$ $\frac{7.6}{15}$ $\frac{6.2}{25}$ $\frac{6.1}{33}$ $\frac{5.6}{50}$

$\frac{852.4}{50}$ $\frac{851.7}{34}$ $\frac{849.9}{34}$ $\frac{842.8}{14}$ $\frac{2.2}{8}$ $\frac{6.2}{4}$ 7.0 $\frac{7.0}{4}$ $\frac{7.7}{14}$ $\frac{6.7}{20}$ $\frac{6.7}{33}$ $\frac{5.8}{50}$

$\frac{847.7}{50}$ $\frac{846.5}{31}$ $\frac{843.3}{37}$ $\frac{3.0}{14}$ $\frac{6.9}{3}$ 7.0 $\frac{6.3}{14}$ $\frac{5.6}{33}$ $\frac{5.7}{50}$

$\frac{835.8}{50}$ $\frac{1.0}{41}$ $\frac{2.7}{33}$ $\frac{6.7}{20}$ $\frac{8.2}{72}$ 7.5 $\frac{7.1}{5}$ $\frac{6.7}{33}$ $\frac{6.3}{50}$

Sta.	+	H.I.	-	Rod.	Elev.
		838.37			
+50				6.7	832.0 ✓
+81				6.7	831.7 ✓
818				7.0	831.4 ✓
+22				7.2	831.2 ✓
+48				7.5	830.9 ✓
+57				10.4	827.8 ✓
+75				10.4	827.8 ✓
T.P.	8.17	839.54 ✓	7.00	831.37 ✓	
+93				11.5	828.0 ✓
817				9.2	830.5 ✓
+22				7.5	832.0 ✓
+30				6.7	832.8 ✓
+51				3.6	835.9 ✓
+65				3.8	835.7 ✓

L1.

A LINE

1/16/25

116

817+50

$\frac{8.1}{50}$	$\frac{8.8}{33}$	$\frac{6.6}{22}$	$\frac{6.2}{11}$	6.4	$\frac{6.6}{16}$	$\frac{6.4}{33}$	$\frac{6.2}{50}$
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$\frac{7.3}{50}$	$\frac{7.1}{46}$	$\frac{6.4}{33}$	$\frac{6.8}{14}$	6.7	$\frac{6.7}{16}$	$\frac{6.7}{33}$	$\frac{6.5}{50}$
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$\frac{9.4}{50}$	$\frac{9.2}{33}$	$\frac{9.1}{28}$	$\frac{8.2}{23}$	$\frac{9.6}{14}$	7.0	$\frac{6.6}{16}$	$\frac{6.6}{33}$	$\frac{6.5}{50}$
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$\frac{10.6}{50}$	$\frac{10.6}{14}$	$\frac{8.6}{13}$	$\frac{8.0}{7}$	7.2	$\frac{6.9}{16}$	$\frac{6.5}{33}$	$\frac{6.4}{50}$
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$\frac{5.9}{50}$	$\frac{5.9}{43}$	$\frac{10.6}{38}$	$\frac{10.6}{6}$	$\frac{8.3}{3}$	7.5	$\frac{7.1}{14}$	$\frac{6.8}{33}$	$\frac{6.2}{50}$
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$\frac{6.1}{50}$	$\frac{6.0}{46}$	$\frac{7.0}{42}$	$\frac{10.6}{33}$	10.6	7.7	$\frac{7.4}{14}$	$\frac{6.7}{33}$	$\frac{6.2}{50}$
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$\frac{6.8}{50}$	$\frac{6.5}{33}$	$\frac{6.9}{27}$	$\frac{10.6}{18}$	10.6	$\frac{10.6}{13}$	$\frac{7.9}{21}$	$\frac{7.0}{33}$	$\frac{6.6}{50}$
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$\frac{8.4}{50}$	$\frac{8.1}{33}$	$\frac{8.4}{14}$	$\frac{8.6}{10}$	11.5	$\frac{11.5}{30}$	$\frac{9.8}{33}$	$\frac{8.9}{39}$	$\frac{8.2}{50}$
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$\frac{8.5}{50}$	$\frac{8.2}{33}$	$\frac{8.9}{5}$	7.2	$\frac{11.5}{7}$	$\frac{11.5}{35}$	$\frac{9.3}{42}$	$\frac{8.2}{50}$
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$\frac{4.2}{50}$	$\frac{6.6}{33}$	$\frac{7.7}{24}$	$\frac{7.7}{14}$	7.5	$\frac{7.6}{14}$	$\frac{11.5}{31}$	$\frac{11.5}{42}$	$\frac{8.3}{50}$
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$\frac{3.1}{50}$	$\frac{3.1}{42}$	$\frac{4.0}{33}$	$\frac{7.0}{15}$	6.7	$\frac{6.6}{18}$	$\frac{7.2}{27}$	$\frac{9.0}{33}$	$\frac{9.0}{43}$	$\frac{7.2}{50}$
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$\frac{6.9}{50}$	$\frac{4.8}{40}$	$\frac{4.1}{33}$	$\frac{3.8}{31}$	$\frac{3.4}{21}$	3.4	$\frac{4.8}{22}$	$\frac{5.0}{33}$	$\frac{5.7}{50}$
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$\frac{8.8}{50}$	$\frac{8.2}{33}$	$\frac{7.7}{28}$	$\frac{6.8}{14}$	$\frac{4.6}{6}$	3.8	$\frac{3.6}{21}$	$\frac{3.4}{33}$	$\frac{3.5}{37}$	$\frac{4.4}{50}$
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Sta.	+	H.I.	-	Rod.	Elev
		839.54			
820	+83			8.4	831.1 ✓
	+14			7.7	831.8 ✓
	+21			8.2	831.3 ✓
	+25	On ice		10.3	826.2 S.B. 829.2 ✓
	+37	"		10.3	825.5 S.B. 829.2 ✓
	+44	"		10.3	827.9 S.B. 829.2 ✓
	+56	On ice		10.3	827.9 S.B. 829.2 ✓
	+73			2.2	837.3 ✓
T.P.	5.34	844.43	0.45	839.87 ✓	
820	+73				837.3 ✓
	+84			3.2	841.2 ✓
	+95			2.8	841.6 ✓
821				4.5	839.9 ✓

Lt.

\$

"H" LINE

1/16/25

Rt

117

819+89

$\frac{5.6}{50} \quad \frac{9.3}{39} \quad \frac{7.2}{33} \quad \frac{8.8}{17} \quad 8.4 \quad \frac{8.5}{8} \quad \frac{5.1}{33} \quad \frac{2.9}{50}$

$\frac{7.9}{50} \quad \frac{8.0}{33} \quad \frac{8.0}{6} \quad 8.4 \quad \frac{9.4}{10} \quad \frac{8.6}{33} \quad \frac{6.2}{50}$

$\frac{7.6}{50} \quad \frac{7.8}{33} \quad \frac{7.9}{14} \quad 7.7 \quad \frac{8.4}{4} \quad \frac{9.3}{24} \quad \frac{8.6}{33} \quad \frac{8.4}{50} \quad \frac{10.3}{49} \quad \frac{10.3}{50}$

$\frac{7.5}{50} \quad \frac{7.9}{33} \quad \frac{8.0}{14} \quad 8.2 \quad \frac{9.2}{7} \quad \frac{9.4}{18} \quad \frac{10.3}{21} \quad \frac{10.3}{33} \quad \frac{10.3}{50}$

$\frac{7.5}{50} \quad \frac{7.8}{33} \quad \frac{8.5}{15} \quad \frac{10.3}{11} \quad 10.5 \quad 13.3 \quad 13.3 \quad \frac{10.3}{50}$

$\frac{7.3}{50} \quad \frac{8.8}{34} \quad \frac{10.3}{30} \quad 10.5 \quad 14.0 \quad 15.1 \quad 14.0 \quad \frac{10.3}{25} \quad \frac{10.3}{50}$

$\frac{11.6}{50} \quad \frac{11.6}{10.3} \quad \frac{11.6}{10.3} \quad \frac{11.6}{33} \quad \frac{11.6}{9.2} \quad \frac{11.6}{50}$

$\frac{10.3}{50} \quad \frac{11.6}{10.3} \quad \frac{9.2}{10} \quad \frac{8.9}{19} \quad \frac{9.9}{21} \quad \frac{9.9}{26} \quad \frac{5.4}{37} \quad \frac{5.9}{50}$

$\frac{9.8}{50} \quad \frac{5.5}{37} \quad \frac{6.3}{24} \quad \frac{4.3}{14} \quad 2.2$

$\frac{5.1}{7} \quad \frac{2.7}{15} \quad \frac{2.6}{20} \quad \frac{13.5}{33} \quad \frac{13.5}{37} \quad \frac{2.6}{50}$

$\frac{11.5}{50} \quad \frac{7.4}{38} \quad \frac{5.1}{50} \quad \frac{4.4}{24} \quad \frac{4.2}{11} \quad 3.2 \quad \frac{2.4}{11} \quad \frac{1.1}{15} \quad \frac{1.5}{25} \quad \frac{12.2}{37} \quad \frac{12.2}{43} \quad \frac{7.5}{50}$

$\frac{9.0}{50} \quad \frac{8.5}{47} \quad \frac{5.7}{40} \quad \frac{2.8}{11} \quad 2.8 \quad \frac{4.6}{18} \quad \frac{5.0}{25} \quad \frac{7.6}{33} \quad \frac{8.4}{37} \quad \frac{10.9}{44} \quad \frac{12.2}{50}$

$\frac{5.8}{50} \quad \frac{5.4}{44} \quad \frac{3.8}{33} \quad \frac{1.9}{27} \quad \frac{2.0}{8} \quad 4.5 \quad \frac{6.2}{27} \quad \frac{7.7}{30} \quad \frac{8.6}{37} \quad \frac{12.5}{50}$

Sta.	+	H.I.	-	Red.	Elev.
		844.43			
+07				8.4	836.0 ✓
+20				8.7	835.7 ✓
+34				1.1	843.3 ✓
+43				1.3	843.1 ✓
+51				4.6	839.8 ✓
T.P.	2.74	843.91 ✓	3.26	841.17 ✓	
+71				10.2	833.7 ✓
+87				3.6	840.3 ✓
822				6.9	837.0 ✓
+10				5.2	838.7 ✓
+24				5.7	838.2 ✓
+51	Edge of Lake		On Ice.	11.7	832.2 ✓
+59			" "	11.7	832.2 ✓
+72			" "	11.7	832.2 ✓

830.2 S.B.

827.8 S.B.

Lt.

H^o LIME RT.

1/17/25
118

821+07

~~$\frac{40}{50} \frac{38}{33} \frac{2.6}{78} \frac{7.9}{5} 8.4 \frac{7.2}{22} \frac{8.2}{29} \frac{8.6}{43} \frac{11.3}{50}$~~

~~$\frac{2.9}{50} \frac{2.8}{33} \frac{2.4}{16} \frac{8.0}{5} 8.7 \frac{6.7}{14} \frac{2.4}{33} \frac{2.7}{39} \frac{7.8}{50}$~~

~~$\frac{3.2}{50} \frac{2.9}{33} \frac{2.5}{22} \frac{3.6}{12} \frac{1.4}{5} 1.1 \frac{1.1}{15} \frac{2.0}{17} \frac{14.7}{36} \frac{141.7}{50}$~~

~~$\frac{5.6}{50} \frac{5.3}{33} \frac{2.4}{25} \frac{2.6}{12} \frac{1.0}{9} 1.3 \frac{2.7}{8} \frac{12.2}{25} \frac{12.2}{50}$~~

~~$\frac{8.1}{50} \frac{6.7}{38} \frac{6.5}{33} \frac{5.7}{25} \frac{4.0}{19} \frac{3.8}{12} 4.6 \frac{13.2}{12.2} \frac{19.4}{50} \frac{17.5}{25}$~~

~~$\frac{2.8}{50} \frac{7.7}{33} \frac{6.9}{20} \frac{3.8}{15} \frac{2.4}{11} \frac{3.2}{7} 4.2 \frac{11.7}{2} \frac{11.7}{50} \frac{18.7}{25}$~~

~~$\frac{7.4}{50} \frac{7.3}{33} \frac{7.4}{15} \frac{2.9}{5} 3.4 \frac{11.7}{8} \frac{11.7}{50} \frac{18.3}{25}$~~

~~$\frac{3.9}{50} \frac{6.5}{45} \frac{6.9}{33} \frac{6.5}{19} \frac{6.4}{10} 6.9 \frac{5.0}{4} \frac{6.8}{10} \frac{13.7}{16} \frac{22.0}{50} \frac{17.8}{25}$~~

~~$\frac{1.2}{50} \frac{4.4}{45} \frac{2.2}{33} \frac{5.7}{17} 5.2 \frac{5.8}{5} \frac{11.7}{15} \frac{11.7}{50} \frac{191.2}{25}$~~

~~$\frac{6.8}{50} \frac{2.2}{33} \frac{1.7}{27} \frac{2.6}{14} 5.7 \frac{11.7}{9} \frac{11.7}{50} \frac{20.2}{25}$~~

~~$\frac{3.4}{50} \frac{2.8}{33} \frac{3.6}{23} \frac{3.4}{14} \frac{4.1}{11} 11.7 \frac{25.3}{11.7} \frac{25.5}{25}$~~

~~$\frac{2.9}{50} \frac{3.3}{31} \frac{5.1}{20} \frac{6.9}{12} \frac{11.7}{4} 13.7 \frac{25.1}{11.7} \frac{26.5}{25}$~~

~~$\frac{3.6}{50} \frac{4.4}{44} \frac{3.5}{33} \frac{4.6}{18} \frac{12.7}{5} 16.8 \frac{24.8}{11.7} \frac{22.9}{25}$~~

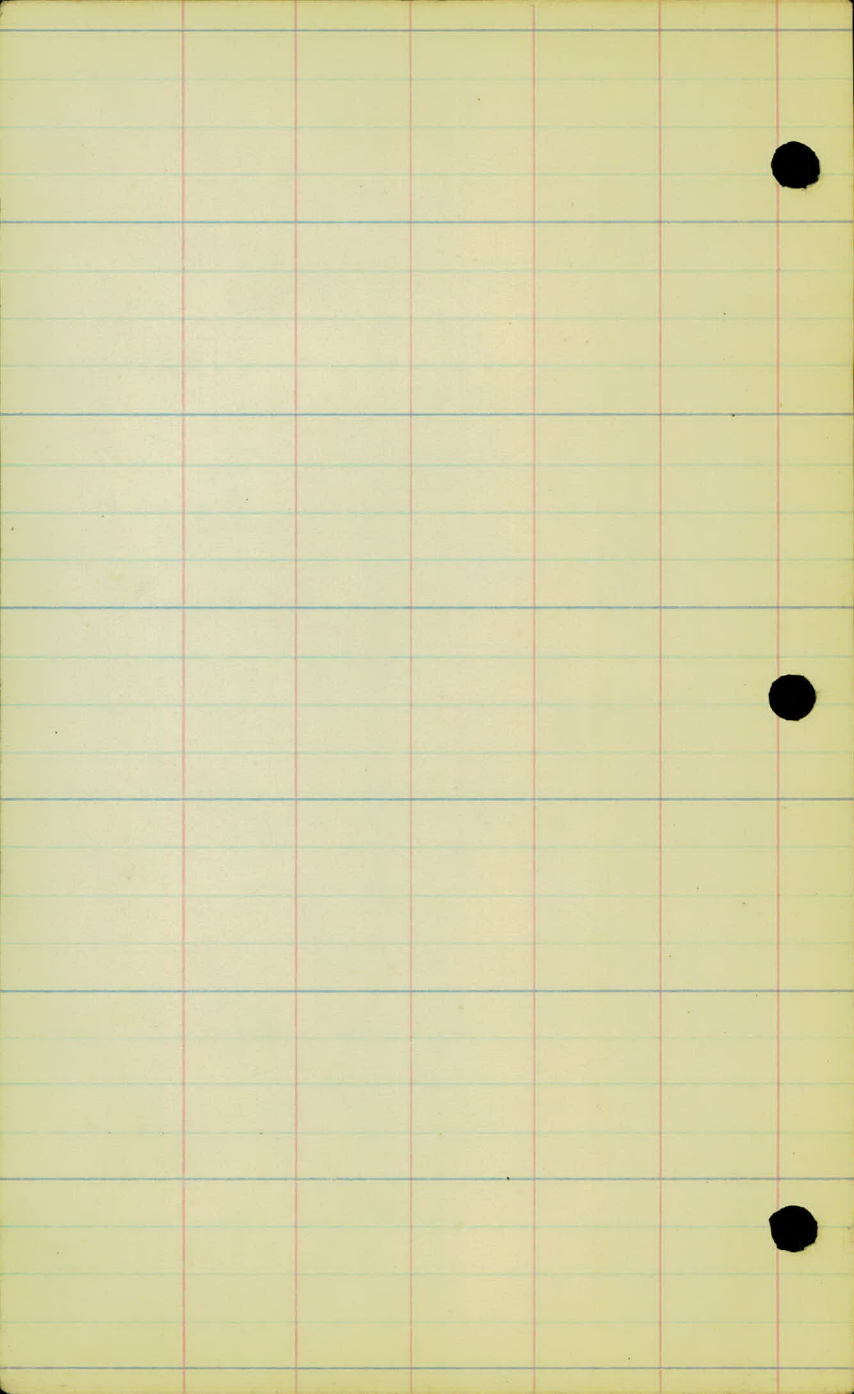
Sta.	+	H.I	-	Red.	F/ev.
		543.91			
+83			On Ice	11.7	826.0 S.B. 832.2 ✓
823			" "	11.7	817.6 S.B. 832.2 ✓
824			" "	11.7	816.1 S.B. 832.2 ✓
+12			" "	11.7	822.2 S.B. 832.2 ✓
+38			" "	11.7	827.2 S.B. 832.2 ✓
+55	Edge of Lake		On Ice	11.7	831.2 S.B. 832.2 ✓
+72				9.3	834.6 ✓
+85				9.1	834.8 ✓
825				7.8	836.1 ✓
+15				5.7	838.2 ✓
T.P.	10.62	853.79	0.74	843.17 ✓	
+26				8.6	845.2 ✓
T.P.	6.60	859.21	1.18	852.61 ✓	
+40				7.2	852.0 ✓
+77				6.2	853.0 ✓

Cross-sections taken from soundings

$$\begin{array}{r}
 823+25- \\
 \text{El. 822.1}
 \end{array}
 \quad
 \frac{0.0}{50}
 \quad
 \frac{+3.1}{25}
 \quad
 \frac{-3.4}{25}
 \quad
 \frac{-2.8}{50}$$

$$\begin{array}{r}
 +50- \\
 \text{El. 812.3}
 \end{array}
 \quad
 \frac{+5.6}{50}
 \quad
 \frac{+4.1}{25}
 \quad
 \frac{+3.3}{25}
 \quad
 \frac{+3.9}{50}$$

$$\begin{array}{r}
 +75- \\
 \text{El. 816A}
 \end{array}
 \quad
 \frac{+1.3}{50}
 \quad
 \frac{-2.1}{25}
 \quad
 \frac{-0.9}{25}
 \quad
 \frac{+3.1}{50}$$



H LINE

11/17/25

120

822+83

Lt

\$

Rt

6.1	9.0	11.7	17.9	24.9	
50	33	31	11.7	50	24.0
					25

24.9	25.6	26.3	25.3	26.6
25	11.7	50	11.7	50
				25

Plusses on insert →

27.8	27.9	27.8	20.6	21.9
25	11.7	50	11.7	50
				25

21.9	25.1	21.7	11.7	8.8	6.0	13.8
25	11.7	50	11.7	34	40	50
						25

22.4	24.4	16.7	11.7	10.4	4.2	0.7
25	11.7	50	11.7	25	40	50

23.3	23.2	12.7	7.1	4.8	3.5	2.7
25	11.7	50	11.7	7.4	1.4	3.3
						50

5.1	10.2	11.7	11.7	10.4	7.1	4.3	3.9	5.7
50	45	36	29	12	9.3	7	14	33
								50

6.7	6.8	6.9	8.0	9.4	8.4	7.6	6.5
50	40	33	18	12	7.1	11	33
							50

845.4	5.0	5.7	6.7	7.1	8.0	6.6	6.2	4.8
50	37	33	25	14	9.8	8	28	33
								50

55.5	0.8	4.6	5.2	3.7	1.0	0.5
50	12	12	5.7	2.3	3.3	4.2
						50

855.2	2.0	3.3	6.7	9.6	8.3	5.5	4.6	4.0	5.2
50	45	40	30	8	8.6	11	26	33	42
									50

7.0	6.7	6.4	7.8	6.0	6.2	6.5	6.3	7.5
50	33	7.4	7.2	9	16	26	33	44
								50

6.0	6.5	6.7	5.5	5.2	4.7	6.3
50	33	7.4	6.2	12	30	34
						50

Sta.	+	H.I.	-	Rod.	Elev.
		859.21			
+57				4.2	855.0 ✓
+75				4.5	854.7 ✓
+86				4.5	854.7 ✓
B.M.			5.44	853.77	853.78 ✓

WINE

1/17/25
121

11.

BT

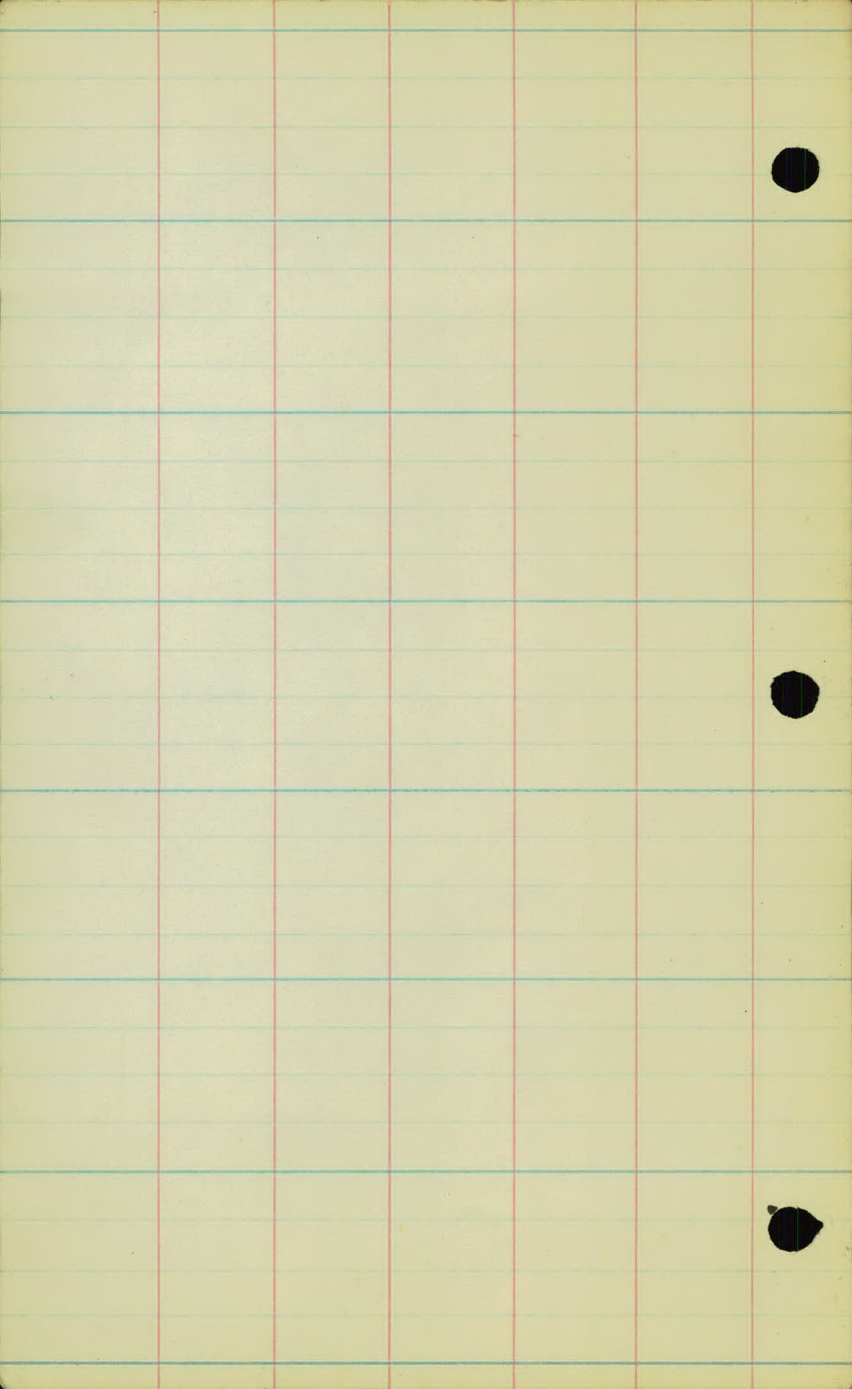
825+57

$\frac{4.8}{50}$	$\frac{4.7}{33}$	$\frac{4.6}{16}$	4.2	$\frac{4.0}{5}$	$\frac{6.5}{9}$	$\frac{6.9}{33}$	$\frac{7.3}{50}$
------------------	------------------	------------------	-----	-----------------	-----------------	------------------	------------------

$\frac{4.4}{50}$	$\frac{4.6}{33}$	$\frac{4.7}{16}$	4.5	$\frac{3.9}{6}$	$\frac{6.0}{9}$	$\frac{7.5}{25}$	$\frac{7.4}{33}$	$\frac{7.2}{50}$
------------------	------------------	------------------	-----	-----------------	-----------------	------------------	------------------	------------------

$\frac{4.7}{50}$	$\frac{4.9}{33}$	$\frac{4.7}{16}$	4.5	$\frac{4.5}{14}$	$\frac{4.4}{33}$	$\frac{4.2}{50}$
------------------	------------------	------------------	-----	------------------	------------------	------------------

SPK in T.P. 105 ft. Sta 828+30.



B.M.	4.49 858.27 ✓	853.78
826+00		54.3
827+00		53.6
828+00		53.1
+70	15" Sd/r	
829+00		53.1
+50		53.2
830+00		52.7
+50		54.3
831+00		53.5
+50		55.1
T.P.	5.95 861.87 ✓ 2.35 855.92 ✓	
832+00		55.5
833+00		55.7
834+00		56.5

Sp in T.P. 105' ht. 828+30

826+00

$\frac{4.1}{50.0}$ $\frac{4.2}{25.0}$ 4.0 $\frac{3.9}{25.0}$ $\frac{4.0}{50.0}$

$\frac{4.7}{50.0}$ $\frac{4.7}{25.0}$ 4.7 $\frac{4.7}{25.0}$ $\frac{4.6}{50.0}$

$\frac{5.8}{50.0}$ $\frac{5.3}{25.0}$ 5.2 $\frac{5.2}{25.0}$ $\frac{5.0}{50.0}$

$\frac{6.0}{50.0}$ $\frac{6.4}{45.0}$ $\frac{6.6}{40.0}$ $\frac{5.6}{37.0}$ $\frac{5.5}{25.0}$ 5.2 $\frac{5.2}{25.0}$ $\frac{5.1}{51.0}$

$\frac{4.5}{50.0}$ $\frac{5.2}{27.0}$ $\frac{6.7}{22.0}$ $\frac{6.5}{13.0}$ $\frac{5.5}{9.0}$ 5.1 $\frac{4.8}{25.0}$ $\frac{5.0}{50.0}$

Road

$\frac{2.3}{50.0}$ $\frac{3.2}{35.0}$ $\frac{4.8}{29.0}$ $\frac{4.2}{24.0}$ $\frac{5.0}{4.0}$ 6.2 $\frac{6.2}{11.0}$ $\frac{5.2}{15.0}$ $\frac{4.7}{50.0}$

$\frac{3.4}{47.0}$ $\frac{4.8}{50.0}$ $\frac{2.8}{32.0}$ $\frac{3.2}{20.0}$ $\frac{4.6}{14.0}$ $\frac{4.7}{10.0}$ 4.0 $\frac{4.0}{13.0}$ $\frac{5.2}{20.0}$ $\frac{5.2}{28.0}$ $\frac{4.2}{30.0}$ $\frac{4.0}{50.0}$

$\frac{3.8}{50.0}$ $\frac{3.7}{46.0}$ $\frac{4.6}{40.0}$ $\frac{3.3}{33.0}$ $\frac{2.8}{18.0}$ $\frac{3.3}{7.0}$ $\frac{4.8}{2.0}$ 4.8 $\frac{3.5}{8.0}$ $\frac{3.5}{27.0}$ $\frac{4.5}{37.0}$ $\frac{4.0}{50.0}$

$\frac{5.6}{40.0}$ $\frac{3.6}{45.0}$ $\frac{3.3}{38.0}$ $\frac{4.0}{28.0}$ $\frac{3.4}{22.0}$ $\frac{3.0}{10.0}$ 3.2 $\frac{4.0}{10.0}$ $\frac{3.3}{16.0}$ $\frac{3.2}{33.0}$ $\frac{3.4}{50.0}$

R.W $\frac{6.6}{36.0}$ $\frac{6.6}{27.0}$ $\frac{7.7}{22.0}$ $\frac{7.0}{17.0}$ $\frac{6.2}{5.0}$ 6.4 $\frac{6.8}{7.0}$ $\frac{7.3}{14.0}$ $\frac{6.4}{21.0}$ $\frac{6.4}{35.0}$ $\frac{6.2}{50.0}$

R.W $\frac{5.7}{31.0}$ $\frac{5.7}{22.0}$ $\frac{7.4}{17.0}$ $\frac{6.4}{11.0}$ 6.2 $\frac{6.2}{14.0}$ $\frac{7.3}{17.0}$ $\frac{6.0}{27.0}$ $\frac{6.3}{50.0}$

R.W $\frac{5.7}{26.0}$ $\frac{6.2}{19.0}$ $\frac{6.6}{13.0}$ $\frac{5.7}{8.0}$ 5.4 $\frac{5.6}{15.0}$ $\frac{7.0}{25.0}$ $\frac{6.6}{32.0}$ $\frac{7.0}{38.0}$ $\frac{6.8}{44.0}$ $\frac{7.3}{50.0}$

861.87

835.40

57.6

836.40

58.3

+76.9

59.2

B.M.

2.47

859.40 ✓

⌘

"H" LINE.

124

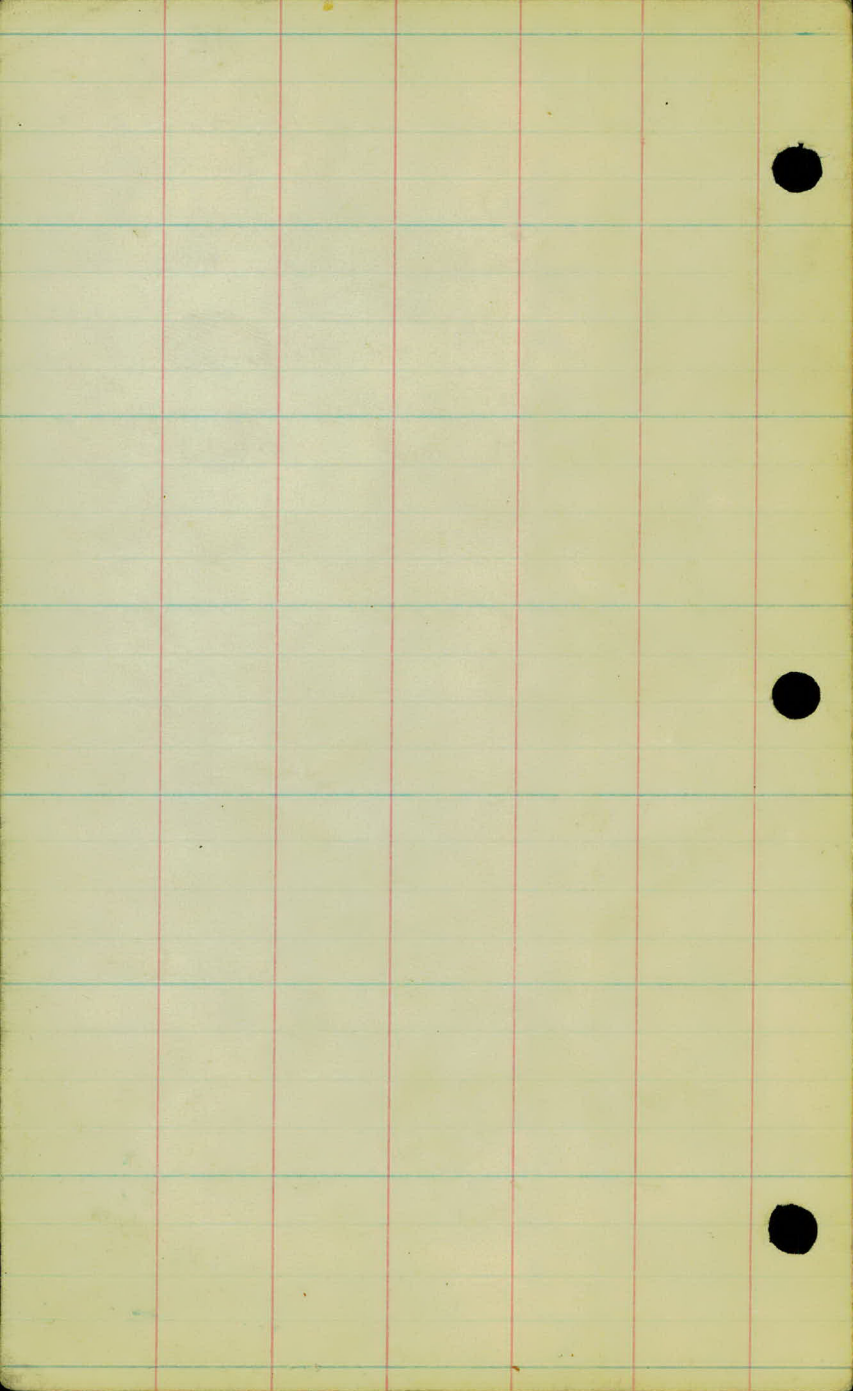
P35100

RW									
<u>6.2</u>	<u>6.4</u>	<u>4.6</u>			<u>4.8</u>	<u>6.6</u>	<u>6.3</u>	<u>6.3</u>	<u>6.6</u>
27.0	16.0	9.0	4.3		18.0	23.0	27.0	31.0	35.0

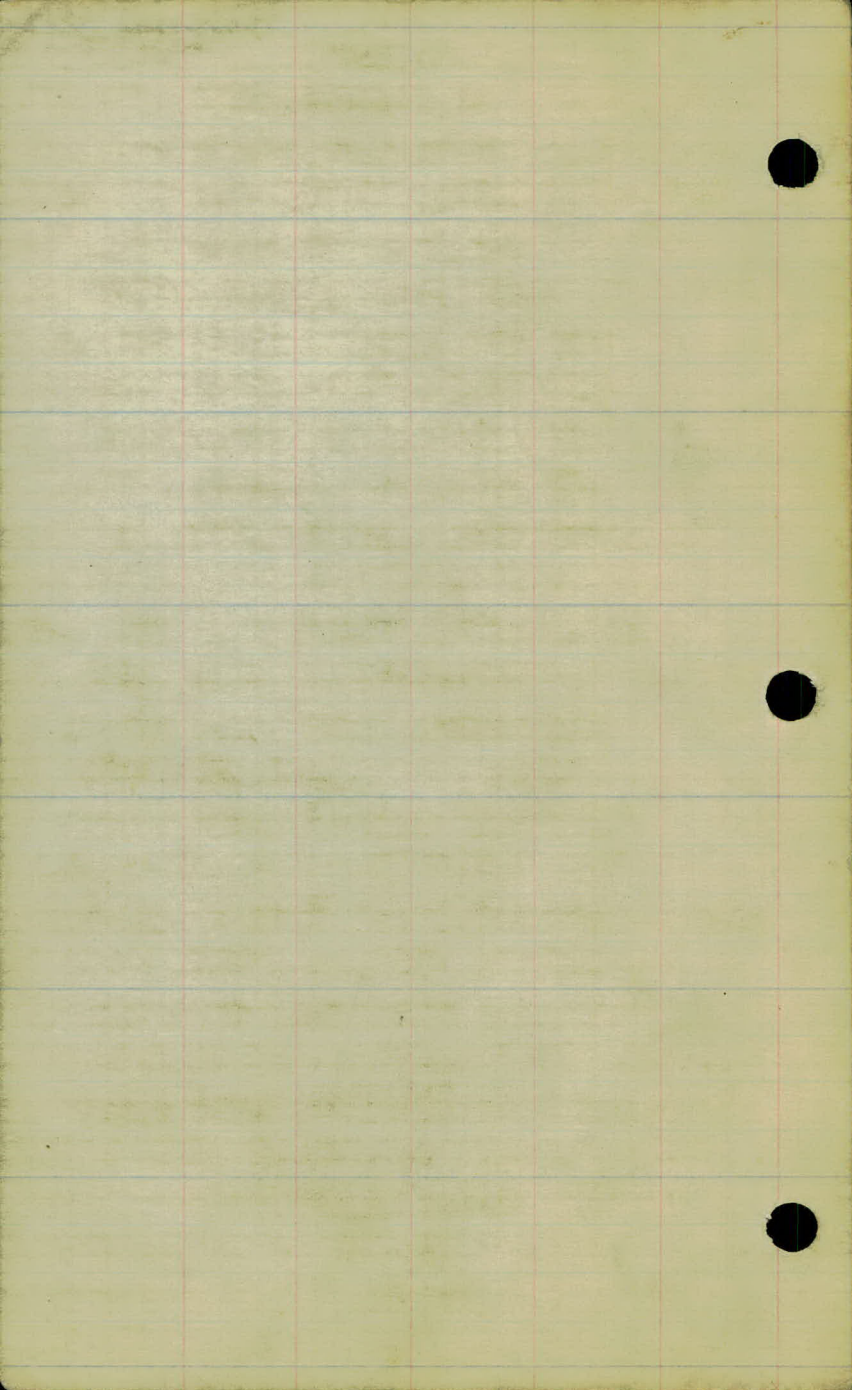
RW									
<u>4.2</u>	<u>4.2</u>	<u>5.0</u>	<u>3.7</u>		<u>4.0</u>	<u>5.8</u>	<u>6.0</u>	<u>5.8</u>	<u>6.3</u>
30.0	21.0	14.0	9.0	3.6	15.0	21.0	23.0	25.0	30.0

RW									
<u>3.0</u>	<u>2.3</u>	<u>4.0</u>	<u>3.0</u>		<u>3.4</u>	<u>4.4</u>	<u>4.2</u>	<u>4.0</u>	<u>3.0</u>
25.0	22.0	16.0	9.0	2.7	14.0	23.0	31.0	36.0	43.0

Sp. in 30" OAK 1st St 936+20



125



X sections.

low sections

sta 335+50 to 339+50

Project 26-62B

Sta.	7	HI	-	E/60
B.M.	0.45	900.68		900.23
T.P.	4.16	897.64	7.20	893.48

335 +100				92.2	5.4.
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+50				92.1	5.5.
-----	--	--	--	------	------

336				92.0	5.6.
-----	--	--	--	------	------

+50				91.9	5.7.
-----	--	--	--	------	------

T.P.	5.98	895.29	8.34	889.30
------	------	--------	------	--------

337				91.8	3.5.
-----	--	--	--	------	------

+50				91.7	3.6.
-----	--	--	--	------	------

338				91.6	3.7.
-----	--	--	--	------	------

+50				91.6	3.7.
-----	--	--	--	------	------

339				91.7	3.6.
-----	--	--	--	------	------

+50				91.9	3.4.
-----	--	--	--	------	------

T.P.	7.67	899.56	3.37	891.87
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B.M.			2.77	896.79
------	--	--	------	--------

Spike in P.P. 60' at Sta 324+50

$$\frac{115}{36} \quad \frac{112}{34} \quad \frac{56}{20} \quad 5.8 \quad \frac{5.5}{20} \quad \frac{12.0}{38} \quad \frac{12.2}{37}$$

$$\frac{133}{40} \quad \frac{130}{34} \quad \frac{20/66}{-1.0} \quad \frac{66}{-1.0} \quad \frac{61/20}{-0.5/20} \quad \frac{12.9}{35} \quad \frac{13.0}{39}$$

$$\frac{134}{32} \quad \frac{12.5}{27} \quad \frac{20/77}{-2.0} \quad \frac{7.8}{-2.1} \quad \frac{62}{-12/20} \quad \frac{13.7}{34} \quad \frac{13.3}{36}$$

$$\frac{110}{32} \quad \frac{105}{29} \quad \frac{20/5.7}{-2.2} \quad \frac{5.8}{-3.3} \quad \frac{50/20}{-1.5/20} \quad \frac{9.5}{29} \quad \frac{10.5}{37}$$

$$\frac{10.8}{33} \quad \frac{100}{28} \quad \frac{20/62}{-2.6} \quad \frac{63}{-3.7} \quad \frac{5.5}{-1.9/20} \quad \frac{9.0}{27} \quad \frac{12.0}{37}$$

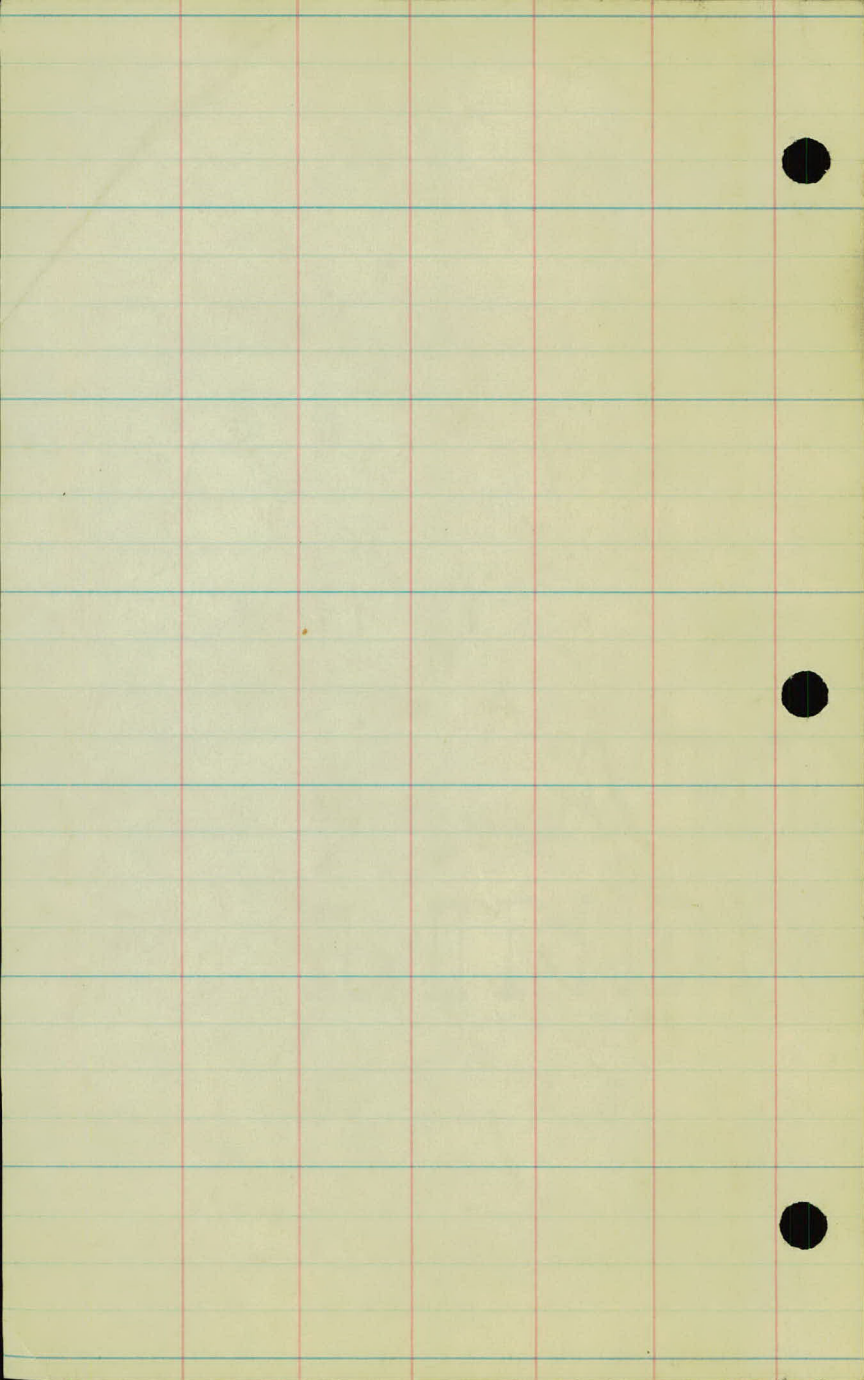
$$\frac{10.5}{33} \quad \frac{9.2}{25} \quad \frac{20/7.0}{-3.3} \quad \frac{5.6}{-1.9} \quad \frac{5.8/20}{-2.1/20} \quad \frac{8.5}{29} \quad \frac{11.0}{38}$$

$$\frac{11.5}{36} \quad \frac{10.5}{33} \quad \frac{20/4.3}{-0.6} \quad \frac{4.8}{-1.1} \quad \frac{4.6}{-0.9/20} \quad \frac{9.0}{27} \quad \frac{11.7}{37}$$

$$\frac{11.5}{38} \quad \frac{11.5}{34} \quad \frac{20/3.7}{-0.1} \quad \frac{4.0}{-0.4} \quad \frac{4.2}{-0.6} \quad \frac{10.2}{30} \quad \frac{12.2}{37}$$

$$\frac{9.7}{37} \quad \frac{10.0}{34} \quad \frac{3.3}{20} \quad \frac{3.5}{-0.1} \quad \frac{3.5/20}{-0.1/20} \quad \frac{10.2}{32} \quad \frac{12.0}{37}$$

Spike in F.G. Post Right Sta 342+00



02494