

OFFICE OF  
RAMSEY COUNTY ENGINEER

# FINAL CROSS-SECTIONS

AMOKA CUT-OFF

PROJ. 26-62-"C"

RAMSEY COUNTY ENGINEER

AMOKA CUT-OFF

# KEUFFEL & ESSER CO.

## DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

### TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.  
FOR SINGLE TRACK EXCAVATION.

*"Copyright, 1895, by Keuffel & Esser Co."*

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

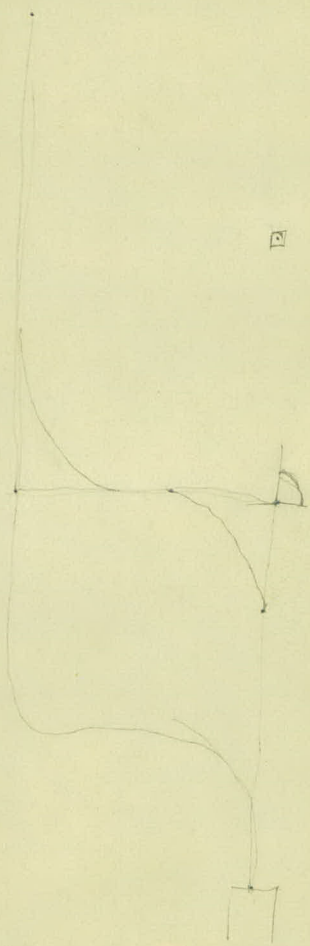
Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.



562+00 Beg Dir C.

A 88 N  
D 15.



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□

# INDEX.

Sta	St. d.	Description.	Page	Page
647+00	719+50	Final Xsections	2	8
829+50	837+84	" "	69	70
562+00	647+00	" "	14	26
588+50	604+00	Highway Nos Conn.	27	28
562+00	647+00	" Topography.	77	71 cont. 68-27
588+00 Rt 5+9	604+00	Highway Nos Conn.	66	65
790+00	792+00	Borrow Pit	60	
720+00	789+00	Topography.	64	61
720+00	81		30.	
808+03 808+63		Drive Ways	58.	
		Final X Sec of Channel		
		Change Rt. of Sta. 819+40	51	52
		Final X Sec. of Channel		
		Change Lt. of Sta. 819+40	52	
		Final X Sec. of X. Road Lt of		
		Sta. 827+18 & Rt of Sta. 827+59	9.	
Final Xsec	Sta. 809+50			
to	812 for	Uncl. Order #6	10	
807+00	837+84	Final Topography	53	56

Sta	+	HI	-	Elev	
B.M	1.76	913.67	✓	901.93	
647				01.0	2.7
648				900.0	3.7
649				899.0	4.7
+60				98.5	5.2
+77				98.4	5.3
+86				98.3	5.4
650				98.2	5.5
+12				98.2	5.5
+30				98.1	5.6
651				97.7	6.0
652				97.3	6.4

spike in 14" Cal 48' R+ 5+ 648+40

(27)

$\frac{43}{50}$	$\frac{40}{35}$	$\frac{56}{21}$	$\frac{52}{28}$	$\frac{24}{20}$	$\frac{24}{20}$	$\frac{27}{20}$	$\frac{52}{24}$	$\frac{52}{28}$	$\frac{28}{31}$	$\frac{20}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

(37)

$\frac{52}{50}$	$\frac{52}{36}$	$\frac{67}{22}$	$\frac{68}{28}$	$\frac{39}{21}$	$\frac{37}{20}$	$\frac{40}{26}$	$\frac{64}{30}$	$\frac{65}{36}$	$\frac{31}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{70}{50}$	$\frac{67}{37}$	$\frac{83}{33}$	$\frac{80}{29}$	$\frac{52}{21}$	$\frac{49}{20}$	$\frac{47}{28}$	$\frac{50}{32}$	$\frac{82}{36}$	$\frac{65}{50}$	$\frac{64}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{40}{51}$	$\frac{67}{40}$	$\frac{70}{36}$	$\frac{64}{32}$	$\frac{56}{27}$	$\frac{55}{20}$	$\frac{53}{21}$	$\frac{55}{29}$	$\frac{54}{33}$	$\frac{85}{36}$	$\frac{70}{50}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{68}{50}$	$\frac{50}{44}$	$\frac{54}{34}$	$\frac{55}{22}$	$\frac{56}{22}$	$\frac{55}{29}$	$\frac{81}{33}$	$\frac{82}{35}$	$\frac{70}{50}$	$\frac{67}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{72}{50}$	$\frac{72}{39}$	$\frac{51}{33}$	$\frac{55}{22}$	$\frac{55}{25}$	$\frac{57}{29}$	$\frac{87}{33}$	$\frac{67}{35}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{70}{50}$	$\frac{70}{36}$	$\frac{75}{35}$	$\frac{70}{27}$	$\frac{56}{22}$	$\frac{56}{25}$	$\frac{67}{34}$	$\frac{73}{42}$	$\frac{67}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{71}{50}$	$\frac{71}{32}$	$\frac{81}{31}$	$\frac{77}{27}$	$\frac{58}{21}$	$\frac{58}{20}$	$\frac{54}{31}$	$\frac{52}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{71}{50}$	$\frac{70}{32}$	$\frac{82}{30}$	$\frac{78}{27}$	$\frac{60}{21}$	$\frac{57}{21}$	$\frac{85}{27}$	$\frac{86}{29}$	$\frac{72}{31}$	$\frac{68}{44}$	$\frac{50}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{73}{32}$	$\frac{86}{29}$	$\frac{84}{26}$	$\frac{62}{20}$	$\frac{60}{20}$	$\frac{84}{26}$	$\frac{86}{30}$	$\frac{71}{33}$	$\frac{70}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{80}{50}$	$\frac{76}{33}$	$\frac{43}{30}$	$\frac{90}{26}$	$\frac{70}{21}$	$\frac{64}{20}$	$\frac{86}{26}$	$\frac{70}{30}$	$\frac{75}{33}$	$\frac{73}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

2/a	+	H.I.	-	F/3	✓
		903.69	✓		
653				97.3	6.4
+50				97.3	6.4
654				97.3	6.4
T.P.	4.11	901.92	✓	588	897.81 ✓
655				97.4	4.5
+50				97.5	4.4
656				97.5	4.4
+50				97.5	4.4
657				97.4	4.5
658				97.3	4.6
659				97.0	4.9
660				96.7	5.2
661				96.4	5.5

$$\frac{84}{50} \quad \frac{80}{31} \quad \frac{72}{27} \quad \frac{86}{24} \quad \frac{70}{20} \quad \frac{65}{-} \quad \frac{62}{21} \quad \frac{85}{26} \quad \frac{87}{30} \quad \frac{72}{33} \quad \frac{75}{50}$$

$$\frac{80}{30} \quad \frac{77}{31} \quad \frac{70}{28} \quad \frac{85}{26} \quad \frac{66}{20} \quad \frac{45}{-} \quad \frac{66}{20} \quad \frac{87}{26} \quad \frac{90}{30} \quad \frac{78}{33} \quad \frac{70}{50}$$

$$\frac{74}{50} \quad \frac{76}{31} \quad \frac{90}{28} \quad \frac{85}{24} \quad \frac{68}{20} \quad \frac{65}{-} \quad \frac{67}{20} \quad \frac{87}{25} \quad \frac{88}{30} \quad \frac{76}{33} \quad \frac{75}{50}$$

$$\frac{50}{50} \quad \frac{61}{32} \quad \frac{68}{29} \quad \frac{64}{25} \quad \frac{48}{20} \quad \frac{47}{-} \quad \frac{48}{20} \quad \frac{71}{26} \quad \frac{71}{30} \quad \frac{60}{34} \quad \frac{54}{50}$$

$$\frac{58}{50} \quad \frac{55}{32} \quad \frac{66}{28} \quad \frac{68}{25} \quad \frac{48}{20} \quad \frac{46}{-} \quad \frac{48}{20} \quad \frac{62}{26} \quad \frac{64}{31} \quad \frac{50}{36} \quad \frac{40}{50}$$

$$\frac{52}{50} \quad \frac{53}{33} \quad \frac{68}{29} \quad \frac{64}{25} \quad \frac{48}{20} \quad \frac{45}{-} \quad \frac{48}{20} \quad \frac{64}{25} \quad \frac{62}{29} \quad \frac{32}{36} \quad \frac{30}{50}$$

$$\frac{52}{50} \quad \frac{50}{34} \quad \frac{52}{33} \quad \frac{70}{29} \quad \frac{67}{25} \quad \frac{46}{20} \quad \frac{47}{-} \quad \frac{47}{20} \quad \frac{65}{24} \quad \frac{66}{29} \quad \frac{36}{35} \quad \frac{31}{37} \quad \frac{30}{50}$$

$$\frac{48}{50} \quad \frac{44}{34} \quad \frac{70}{29} \quad \frac{70}{25} \quad \frac{46}{20} \quad \frac{47}{-} \quad \frac{48}{20} \quad \frac{64}{25} \quad \frac{65}{30} \quad \frac{35}{36} \quad \frac{30}{39} \quad \frac{25}{50}$$

$$\frac{44}{50} \quad \frac{42}{37} \quad \frac{45}{34} \quad \frac{74}{29} \quad \frac{71}{25} \quad \frac{49}{20} \quad \frac{48}{-} \quad \frac{48}{20} \quad \frac{68}{28} \quad \frac{70}{29} \quad \frac{38}{35} \quad \frac{32}{39} \quad \frac{33}{50}$$

$$\frac{47}{50} \quad \frac{46}{35} \quad \frac{54}{33} \quad \frac{75}{29} \quad \frac{73}{25} \quad \frac{50}{20} \quad \frac{50}{-} \quad \frac{49}{20} \quad \frac{72}{26} \quad \frac{71}{29} \quad \frac{52}{34} \quad \frac{50}{36} \quad \frac{51}{50}$$

$$\frac{68}{50} \quad \frac{56}{32} \quad \frac{60}{35} \quad \frac{76}{31} \quad \frac{74}{25} \quad \frac{53}{20} \quad \frac{52}{-} \quad \frac{52}{20} \quad \frac{70}{26} \quad \frac{70}{31} \quad \frac{51}{35} \quad \frac{48}{38} \quad \frac{46}{50}$$

$$\frac{58}{50} \quad \frac{53}{36} \quad \frac{80}{30} \quad \frac{72}{25} \quad \frac{57}{20} \quad \frac{54}{-} \quad \frac{54}{20} \quad \frac{76}{25} \quad \frac{76}{30} \quad \frac{50}{35} \quad \frac{43}{39} \quad \frac{40}{50}$$

Sta		HI		E/c	
		90192 ✓			
662				96.1	5.8
663				95.8	6.1
664				95.5	6.4
T.P	2.53	89906 ✓	639	895.53 ✓	
+50				95.4	3.9
665				95.2	3.9
666				94.9	4.2
667				94.6	4.5
+50				94.5	4.6
668				94.3	4.8
+50				94.2	4.9
669				94.1	5.0
+50				94.1	5.0

$\frac{58}{50}$   $\frac{56}{38}$   $\frac{82}{31}$   $\frac{80}{26}$   $\frac{58}{20}$   $\frac{55}{50}$   $\frac{54}{20}$   $\frac{78}{25}$   $\frac{78}{29}$   $\frac{50}{30}$   $\frac{42}{38}$   $\frac{46}{50}$

$\frac{66}{50}$   $\frac{67}{37}$   $\frac{64}{35}$   $\frac{88}{30}$   $\frac{88}{26}$   $\frac{61}{20}$   $\frac{59}{50}$   $\frac{60}{20}$   $\frac{77}{25}$   $\frac{80}{30}$   $\frac{52}{35}$   $\frac{48}{39}$   $\frac{48}{50}$

$\frac{92}{50}$   $\frac{84}{27}$   $\frac{78}{32}$   $\frac{94}{26}$   $\frac{64}{20}$   $\frac{64}{50}$   $\frac{64}{20}$   $\frac{87}{25}$   $\frac{88}{30}$   $\frac{67}{34}$   $\frac{62}{37}$   $\frac{62}{50}$   
End Ditch +28 Rt

$\frac{73}{50}$   $\frac{72}{35}$   $\frac{76}{34}$   $\frac{72}{28}$   $\frac{66}{27}$   $\frac{38}{20}$   $\frac{38}{50}$   $\frac{35}{20}$   $\frac{62}{28}$   $\frac{60}{50}$   
End Ditch +55 Rt.

$\frac{75}{50}$   $\frac{70}{26}$   $\frac{40}{20}$   $\frac{41}{50}$   $\frac{40}{20}$   $\frac{63}{27}$   $\frac{63}{50}$   
Beg Ditch 61+37

$\frac{80}{50}$   $\frac{72}{27}$   $\frac{40}{20}$   $\frac{42}{50}$   $\frac{42}{20}$   $\frac{66}{28}$   $\frac{73}{35}$   $\frac{60}{38}$   $\frac{64}{50}$   
Beg Ditch 66+50

$\frac{72}{50}$   $\frac{68}{33}$   $\frac{76}{30}$   $\frac{76}{27}$   $\frac{46}{20}$   $\frac{45}{50}$   $\frac{44}{20}$   $\frac{72}{28}$   $\frac{71}{32}$   $\frac{55}{37}$   $\frac{52}{50}$   
End D. +30 Rt

$\frac{62}{50}$   $\frac{59}{33}$   $\frac{25}{30}$   $\frac{75}{27}$   $\frac{47}{20}$   $\frac{47}{50}$   $\frac{47}{20}$   $\frac{71}{27}$   $\frac{68}{50}$

$\frac{68}{50}$   $\frac{71}{30}$   $\frac{72}{29}$   $\frac{72}{26}$   $\frac{50}{20}$   $\frac{47}{50}$   $\frac{47}{20}$   $\frac{73}{26}$   $\frac{68}{50}$   
End ditch +15

$\frac{84}{50}$   $\frac{83}{27}$   $\frac{50}{20}$   $\frac{49}{50}$   $\frac{49}{20}$   $\frac{76}{26}$   $\frac{76}{50}$

$\frac{68}{50}$   $\frac{70}{25}$   $\frac{48}{20}$   $\frac{50}{50}$   $\frac{49}{20}$   $\frac{75}{26}$   $\frac{76}{50}$

$\frac{86}{50}$   $\frac{76}{27}$   $\frac{48}{20}$   $\frac{52}{50}$   $\frac{55}{20}$   $\frac{80}{36}$   $\frac{78}{30}$   $\frac{102}{32}$   $\frac{102}{35}$   $\frac{78}{40}$   $\frac{76}{50}$   
Beg Ditch +65 Beg Ditch +50

Stn		17I		Flow	
		899.06 ✓			
670				94.1	5.0
+50				94.1	5.0
671				94.2	4.9
+50				94.3	4.8
672				94.3	4.8
+50				94.4	4.7
673				94.4	4.7
674				94.5	4.6
675				94.6	4.5
B M	1.27	899.33 ✓	1.01	898.05 ✓	898.06 ✓
+50				94.7	4.6
676				94.7	4.6
+50				94.8	4.5

$\frac{7.2}{50}$	$\frac{7.0}{31}$	$\frac{8.2}{28}$	$\frac{8.0}{26}$	$\frac{5.1}{20}$	$\frac{5.2}{20}$	$\frac{5.1}{20}$	$\frac{8.5}{28}$	$\frac{8.7}{31}$	$\frac{7.8}{34}$	$\frac{8.2}{50}$
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$\frac{6.2}{50}$	$\frac{5.6}{34}$	$\frac{7.1}{30}$	$\frac{7.6}{26}$	$\frac{5.2}{20}$	$\frac{5.2}{20}$	$\frac{4.3}{20}$	$\frac{7.8}{26}$	$\frac{7.8}{29}$	$\frac{5.4}{33}$	$\frac{5.6}{50}$
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$\frac{5.8}{50}$	$\frac{5.4}{33}$	$\frac{7.5}{29}$	$\frac{7.2}{25}$	$\frac{4.8}{20}$	$\frac{4.8}{20}$	$\frac{4.8}{20}$	$\frac{7.2}{26}$	$\frac{7.2}{29}$	$\frac{4.4}{35}$	$\frac{4.4}{50}$
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$\frac{4.6}{50}$	$\frac{4.0}{37}$	$\frac{7.5}{29}$	$\frac{7.5}{27}$	$\frac{4.9}{20}$	$\frac{4.7}{20}$	$\frac{4.7}{20}$	$\frac{6.6}{26}$	$\frac{6.7}{30}$	$\frac{3.5}{33}$	$\frac{3.3}{38}$	$\frac{3.2}{50}$
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$\frac{5.2}{50}$	$\frac{4.4}{34}$	$\frac{7.1}{29}$	$\frac{7.3}{25}$	$\frac{4.3}{20}$	$\frac{4.7}{20}$	$\frac{4.6}{20}$	$\frac{6.6}{27}$	$\frac{6.8}{31}$	$\frac{2.6}{38}$	$\frac{2.6}{50}$	$\frac{2.5}{50}$
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$\frac{5.0}{50}$	$\frac{5.0}{34}$	$\frac{7.2}{31}$	$\frac{7.1}{27}$	$\frac{5.0}{20}$	$\frac{4.8}{20}$	$\frac{4.6}{20}$	$\frac{6.7}{27}$	$\frac{6.9}{31}$	$\frac{2.5}{39}$	$\frac{2.0}{41}$	$\frac{2.0}{50}$
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$\frac{5.8}{50}$	$\frac{4.9}{35}$	$\frac{5.3}{33}$	$\frac{7.5}{30}$	$\frac{7.5}{26}$	$\frac{4.6}{20}$	$\frac{4.6}{20}$	$\frac{7.0}{26}$	$\frac{7.2}{30}$	$\frac{2.0}{39}$	$\frac{1.6}{40}$	$\frac{2.0}{50}$
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$\frac{6.0}{50}$	$\frac{5.0}{34}$	$\frac{5.6}{33}$	$\frac{7.0}{30}$	$\frac{7.0}{26}$	$\frac{4.6}{20}$	$\frac{4.6}{20}$	$\frac{7.2}{27}$	$\frac{7.0}{31}$	$\frac{4.2}{35}$	$\frac{4.0}{37}$	$\frac{3.4}{50}$
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$\frac{6.6}{50}$	$\frac{6.0}{35}$	$\frac{6.2}{33}$	$\frac{7.2}{30}$	$\frac{7.1}{26}$	$\frac{4.3}{20}$	$\frac{4.4}{20}$	$\frac{4.6}{20}$	$\frac{6.8}{26}$	$\frac{7.0}{29}$	$\frac{3.5}{36}$	$\frac{3.7}{37}$	$\frac{3.2}{50}$
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Dipole in 15" Exp RT 24 672 + 55

$\frac{7.3}{50}$	$\frac{6.4}{35}$	$\frac{6.8}{34}$	$\frac{7.5}{31}$	$\frac{7.5}{28}$	$\frac{4.6}{20}$	$\frac{4.8}{20}$	$\frac{4.9}{20}$	$\frac{7.0}{26}$	$\frac{7.2}{30}$	$\frac{3.6}{36}$	$\frac{3.3}{38}$	$\frac{3.2}{50}$
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190 Ethd D. 106

$\frac{7.6}{50}$	$\frac{6.8}{33}$	$\frac{7.0}{30}$	$\frac{4.5}{20}$	$\frac{4.8}{20}$	$\frac{5.0}{20}$	$\frac{7.0}{27}$	$\frac{7.2}{31}$	$\frac{3.6}{37}$	$\frac{5.3}{39}$	$\frac{3.1}{50}$
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$\frac{8.2}{50}$	$\frac{7.2}{31}$	$\frac{4.3}{20}$	$\frac{4.8}{20}$	$\frac{5.0}{20}$	$\frac{7.2}{26}$	$\frac{7.4}{30}$	$\frac{3.7}{36}$	$\frac{3.6}{37}$	$\frac{3.1}{50}$
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Sta		HI		Elev	
		899.33	✓		
677				94.8	4.5
	+50			94.9	4.4
678				94.8	4.5
B M			0.97	898.36	898.37
	+50			94.7	4.6
679				94.6	4.7
	+50			94.4	4.9
680				94.2	5.1
	+50			93.9	5.4
681				93.6	5.7
T. P.	2.71	895.75	✓	6.09	893.24
	+50			93.2	2.8
682				92.8	3.2
682+5958 = 709+5420				92.4	3.6

+80 B. op 15 to 6  
 $\frac{74}{50}$   $\frac{61}{81}$   $\frac{72}{30}$   $\frac{67}{27}$   $\frac{41}{20}$   $\frac{47}{20}$   $\frac{49}{20}$   $\frac{70}{26}$   $\frac{73}{29}$   $\frac{44}{56}$   $\frac{38}{50}$

$\frac{63}{50}$   $\frac{62}{34}$   $\frac{67}{30}$   $\frac{67}{27}$   $\frac{43}{20}$   $\frac{47}{20}$   $\frac{50}{20}$   $\frac{69}{27}$   $\frac{71}{31}$   $\frac{58}{35}$   $\frac{54}{50}$

$\frac{57}{50}$   $\frac{60}{32}$   $\frac{61}{31}$   $\frac{68}{29}$   $\frac{63}{26}$   $\frac{43}{20}$   $\frac{48}{20}$   $\frac{48}{20}$   $\frac{64}{25}$   $\frac{64}{29}$   $\frac{58}{32}$   $\frac{48}{50}$

sp. 20 in 14" Oak 71 sta 677-70  
 $\frac{42}{50}$   $\frac{44}{35}$   $\frac{64}{32}$   $\frac{64}{25}$   $\frac{44}{20}$   $\frac{47}{20}$   $\frac{50}{20}$   $\frac{68}{26}$   $\frac{68}{30}$   $\frac{52}{33}$   $\frac{48}{36}$   $\frac{42}{50}$

$\frac{43}{50}$   $\frac{35}{39}$   $\frac{66}{30}$   $\frac{70}{26}$   $\frac{44}{20}$   $\frac{47}{20}$   $\frac{50}{20}$   $\frac{68}{27}$   $\frac{70}{31}$   $\frac{37}{37}$   $\frac{36}{39}$   $\frac{32}{50}$

$\frac{31}{50}$   $\frac{32}{42}$   $\frac{34}{40}$   $\frac{72}{30}$   $\frac{71}{26}$   $\frac{45}{20}$   $\frac{50}{20}$   $\frac{52}{20}$   $\frac{70}{26}$   $\frac{73}{30}$   $\frac{36}{38}$   $\frac{30}{20}$   $\frac{30}{51}$

$\frac{34}{51}$   $\frac{33}{42}$   $\frac{36}{40}$   $\frac{74}{32}$   $\frac{75}{28}$   $\frac{46}{20}$   $\frac{51}{20}$   $\frac{55}{20}$   $\frac{73}{26}$   $\frac{73}{30}$   $\frac{31}{37}$   $\frac{33}{39}$   $\frac{30}{50}$

$\frac{41}{50}$   $\frac{42}{44}$   $\frac{45}{41}$   $\frac{81}{33}$   $\frac{83}{30}$   $\frac{51}{20}$   $\frac{53}{20}$   $\frac{55}{20}$   $\frac{78}{27}$   $\frac{80}{30}$   $\frac{41}{38}$   $\frac{38}{39}$   $\frac{42}{50}$

$\frac{48}{50}$   $\frac{47}{44}$   $\frac{50}{41}$   $\frac{86}{33}$   $\frac{87}{29}$   $\frac{54}{20}$   $\frac{56}{20}$   $\frac{61}{20}$   $\frac{84}{26}$   $\frac{86}{30}$   $\frac{57}{35}$   $\frac{54}{37}$   $\frac{38}{50}$

$\frac{71}{50}$   $\frac{22}{45}$   $\frac{61}{35}$   $\frac{62}{31}$   $\frac{25}{20}$   $\frac{27}{20}$   $\frac{30}{20}$   $\frac{52}{28}$   $\frac{52}{31}$   $\frac{42}{24}$   $\frac{46}{50}$   
 +80=00 Ditch

$\frac{36}{50}$   $\frac{36}{44}$   $\frac{70}{35}$   $\frac{67}{31}$   $\frac{30}{20}$   $\frac{32}{20}$   $\frac{34}{20}$   $\frac{62}{27}$   $\frac{67}{50}$

End Ditch at E. Fla.  
 $\frac{72}{50}$   $\frac{75}{39}$   $\frac{75}{30}$   $\frac{36}{20}$   $\frac{37}{20}$   $\frac{40}{20}$   $\frac{68}{27}$   $\frac{74}{50}$

Sta	+	HI	-	E/cv	
		898.95	✓		
710				92.1	3.9
711				91.7	4.3
+46				91.6	4.4
712				91.4	4.6
+50				91.3	4.7
713				91.1	4.9
714				90.8	5.2
+50				90.7	5.3
715				90.5	5.5
+45				90.4	5.6
716				90.2	5.8
717				89.9	6.1

$$\frac{72}{50} \quad \frac{71}{28} \quad \frac{40}{20} \quad \frac{42}{20} \quad \frac{40}{20} \quad \frac{71}{28} \quad \frac{71}{50}$$

$$\frac{64}{50} \quad \frac{64}{35} \quad \frac{75}{28} \quad \frac{45}{28} \quad \frac{45}{20} \quad \frac{45}{20} \quad \frac{71}{28} \quad \frac{74}{50}$$

$$\frac{77}{50} \quad \frac{77}{41} \quad \frac{87}{36} \quad \frac{87}{36} \quad \frac{77}{33} \quad \frac{76}{29} \quad \frac{48}{20} \quad \frac{47}{20} \quad \frac{48}{20} \quad \frac{82}{50} \quad \frac{82}{35} \quad \frac{76}{36} \quad \frac{73}{50}$$

Beq Ditolah Lt RT at Stn

$$\frac{77}{50} \quad \frac{73}{27} \quad \frac{42}{20} \quad \frac{48}{20} \quad \frac{49}{20} \quad \frac{80}{29} \quad \frac{80}{33} \quad \frac{62}{39} \quad \frac{55}{50}$$

$$\frac{52}{50} \quad \frac{52}{37} \quad \frac{77}{31} \quad \frac{74}{27} \quad \frac{48}{28} \quad \frac{49}{20} \quad \frac{50}{20} \quad \frac{77}{31} \quad \frac{80}{36} \quad \frac{50}{45} \quad \frac{47}{50}$$

$$\frac{43}{50} \quad \frac{44}{40} \quad \frac{82}{31} \quad \frac{78}{27} \quad \frac{50}{20} \quad \frac{50}{20} \quad \frac{51}{20} \quad \frac{70}{26} \quad \frac{76}{31} \quad \frac{82}{34} \quad \frac{80}{35} \quad \frac{47}{44} \quad \frac{40}{50}$$

End R + 43

$$\frac{58}{50} \quad \frac{58}{39} \quad \frac{90}{32} \quad \frac{86}{28} \quad \frac{55}{20} \quad \frac{50}{20} \quad \frac{50}{20} \quad \frac{83}{30} \quad \frac{87}{34} \quad \frac{54}{41} \quad \frac{50}{43} \quad \frac{46}{50}$$

$$\frac{95}{50} \quad \frac{94}{29} \quad \frac{55}{20} \quad \frac{54}{20} \quad \frac{56}{20} \quad \frac{82}{29} \quad \frac{85}{33} \quad \frac{62}{38} \quad \frac{60}{41} \quad \frac{52}{50}$$

$$\frac{95}{50} \quad \frac{95}{27} \quad \frac{55}{20} \quad \frac{55}{20} \quad \frac{54}{20} \quad \frac{90}{31} \quad \frac{90}{35} \quad \frac{80}{39} \quad \frac{74}{50}$$

$$\frac{97}{50} \quad \frac{96}{29} \quad \frac{55}{20} \quad \frac{55}{20} \quad \frac{55}{20} \quad \frac{78}{26} \quad \frac{85}{27} \quad \frac{92}{35} \quad \frac{73}{40} \quad \frac{74}{50}$$

$$\frac{98}{50} \quad \frac{82}{30} \quad \frac{55}{20} \quad \frac{56}{20} \quad \frac{56}{20} \quad \frac{78}{28} \quad \frac{80}{32} \quad \frac{58}{36} \quad \frac{55}{50}$$

+20 = 309 D Hoh

$$\frac{57}{50} \quad \frac{57}{41} \quad \frac{85}{34} \quad \frac{88}{36} \quad \frac{58}{20} \quad \frac{58}{20} \quad \frac{58}{20} \quad \frac{88}{27} \quad \frac{90}{34} \quad \frac{52}{41} \quad \frac{48}{43} \quad \frac{48}{50}$$

544	+	HI	-	Flw	
		895.95 ✓			
718				89.6	6.4
BM	1.00	891.52 ✓	543	890.52 ✓	
719				89.3	2.2
+50		End			
BM			152	890.00 ✓	890.01

715+20	x Drain
911+77	Drive Culv Rt
678+50	Drive
677+75	Drive
669+63	x Drain
659+80	
659+80	
650+12	Rt
649+70	x Drain

$\frac{6.5}{50}$	$\frac{7.0}{37}$	$\frac{9.6}{32}$	$\frac{9.3}{27}$	$\frac{6.2}{20}$	$\frac{6.2}{20}$	$\frac{6.3}{20}$	$\frac{9.0}{29}$	$\frac{9.3}{35}$	$\frac{6.8}{40}$	$\frac{6.8}{42}$	$\frac{6.3}{50}$
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Spike in 16" Oak 50' RT Sta 718+50

$\frac{2.5}{50}$	$\frac{2.6}{42}$	$\frac{2.7}{38}$	$\frac{5.2}{33}$	$\frac{5.2}{27}$	$\frac{2.0}{20}$	$\frac{1.8}{18}$	$\frac{2.0}{20}$	$\frac{4.6}{28}$	$\frac{5.0}{34}$	$\frac{2.0}{40}$	$\frac{1.7}{50}$
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$\frac{2.3}{50}$	$\frac{2.4}{37}$	$\frac{2.2}{20}$	$\frac{2.4}{18}$	$\frac{2.4}{20}$	$\frac{2.7}{26}$	$\frac{2.8}{36}$	$\frac{3.2}{50}$
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Spike in 8" Oak 60' Lt Sta 721+25

24' x 54' P3

18" x 36.5 CM RT

23' x 10' x 15' Lt

35' x 10' x 1.0

30' x 54' P3

13 C.Y.

13 C.Y.

15' x 24 CM 2' C.Y. RT

2 C.Y.

15' x 24 CM 2 C.Y. Lt

2 C.Y.

18 x 36.5 CM 2 C.Y. RT

2 C.Y.

24" x 66 P3

Final x Sec. of Pri. x Rd Lt. Sta. 827+18

0+00 = 20 Lt. Sta. 827+18

0+08

0+14

0+23

0+35

0+49

0+65 0.0 Section.

Final x Sec. of Pri. x Rd. Rt. Sta. 827+39

0+00 = 20 Rt. Sta. 827+39

0+05

0+12

0+22

0+44

0+64

Left

Right

11-8-27

	<u>7.7</u>		<u>7.5</u>		
	12	7.5	11		
	<u>9.7</u>	<u>7.8</u>	<u>7.6</u>	<u>9.4</u>	
	12	7	10	13	
	<u>9.5</u>	<u>7.5</u>	<u>7.3</u>	<u>8.6</u>	
	13	7	9	14	
<u>2.2</u>	<u>5.5</u>	<u>6.3</u>	<u>6.3</u>	<u>7.3</u>	
15	9	5	8	14	
	<u>2.0</u>	<u>5.4</u>	<u>5.2</u>	<u>3.9</u>	<u>1.9</u>
	11	6	6	10	14
	<u>2.1</u>	<u>3.6</u>	<u>4.2</u>	<u>3.4</u>	<u>2.0</u>
	11	7	7	7	10
	<u>2.2</u>		<u>2.9</u>		
	6	2.2	6		

	<u>8.2</u>		<u>8.6</u>		
	11	8.2	12		
	<u>9.6</u>	<u>8.4</u>	<u>8.8</u>	<u>9.6</u>	
	12	9	10	14	
	<u>9.7</u>	<u>8.2</u>	<u>8.0</u>	<u>10.0</u>	
	11	8	10	15	
<u>2.1</u>	<u>5.9</u>	<u>7.5</u>	<u>6.7</u>	<u>5.5</u>	<u>2.2</u>
13	7	4	7	11	15
	<u>2.1</u>	<u>5.5</u>	<u>4.6</u>	<u>4.1</u>	<u>2.3</u>
	11	6	5	7	10
	<u>2.6</u>		<u>2.6</u>		
	10	2.6	6		

For Uncl. Order # 6

Sta	+	HI	-	Elev
B.M.	2.71	853.78		851.07
809+50				
+75				
810+00				
+25				
+50				
811+00				
+25				
+10				
+71				
+92				
812+00				

Left.

Right.

$$\frac{3.6}{50} \quad \frac{3.7}{52} \quad \frac{3.1}{22} \quad \frac{4.8}{20} \quad 44 \quad \frac{4.4}{19} \quad \frac{6.5}{33} \quad \frac{5.4}{27} \quad \frac{2.4}{32} \quad \frac{7.8}{50}$$

$$\frac{4.9}{50} \quad \frac{4.1}{34} \quad \frac{6.7}{31} \quad \frac{2.4}{25} \quad \frac{4.8}{21} \quad 44 \quad \frac{4.5}{19} \quad \frac{6.5}{24} \quad \frac{6.9}{29} \quad \frac{4.9}{34} \quad \frac{6.6}{42} \quad \frac{7.5}{50}$$

$$\frac{3.8}{50} \quad \frac{3.7}{57} \quad \frac{7.3}{33} \quad \frac{7.1}{25} \quad \frac{4.9}{21} \quad 47 \quad \frac{4.7}{19} \quad \frac{7.6}{26} \quad \frac{7.6}{30} \quad \frac{5.1}{37} \quad \frac{5.8}{50}$$

$$\frac{3.8}{50} \quad \frac{3.7}{37} \quad \frac{7.3}{33} \quad \frac{7.1}{25} \quad \frac{4.9}{21} \quad 50 \quad \frac{4.8}{19} \quad \frac{7.6}{26} \quad \frac{7.6}{30} \quad \frac{5.1}{37} \quad \frac{5.8}{50}$$

$$\frac{3.9}{50} \quad \frac{4.0}{38} \quad \frac{6.9}{30} \quad \frac{7.2}{26} \quad \frac{5.0}{22} \quad 49 \quad \frac{4.9}{20} \quad \frac{7.3}{26} \quad \frac{7.1}{30} \quad \frac{5.4}{33} \quad \frac{6.1}{50}$$

$$\frac{1.0}{50} \quad \frac{6.9}{43} \quad \frac{6.9}{32} \quad \frac{7.0}{27} \quad \frac{5.2}{22} \quad 50 \quad \frac{5.1}{20} \quad \frac{6.9}{24} \quad \frac{7.0}{29} \quad \frac{2.5}{36} \quad \frac{2.9}{50}$$

$$\frac{1.2}{50} \quad \frac{7.3}{44} \quad \frac{4.3}{38} \quad \frac{6.6}{33} \quad \frac{6.9}{26} \quad \frac{5.5}{21} \quad 54 \quad \frac{5.3}{20} \quad \frac{7.1}{25} \quad \frac{7.1}{30} \quad \frac{0.8}{38} \quad \frac{0.5}{50}$$

$$\frac{0.1}{50} \quad \frac{7.0}{46} \quad \frac{7.0}{44} \quad \frac{6.2}{32} \quad \frac{6.9}{26} \quad \frac{5.5}{21} \quad 56 \quad \frac{5.6}{20} \quad \frac{6.7}{34} \quad \frac{6.9}{30} \quad \frac{0.3}{39} \quad \frac{7.0}{57}$$

$$\frac{1.6}{50} \quad \frac{7.1}{48} \quad \frac{7.5}{43} \quad \frac{3.6}{34} \quad \frac{6.2}{30} \quad \frac{6.4}{23} \quad \frac{5.3}{20} \quad 54 \quad \frac{5.9}{20} \quad \frac{6.9}{25} \quad \frac{6.7}{30} \quad \frac{7.3}{41} \quad \frac{7.6}{50}$$

$$\frac{7.8}{50} \quad \frac{7.0}{38} \quad \frac{0.6}{28} \quad \frac{7.0}{19} \quad \frac{4.3}{11} \quad 58 \quad \frac{5.6}{19} \quad \frac{6.7}{22} \quad \frac{6.1}{34} \quad \frac{7.4}{44} \quad \frac{7.1}{50}$$

$$\frac{7.1}{50} \quad \frac{7.3}{34} \quad \frac{0.0}{27} \quad \frac{7.1}{20} \quad \frac{3.3}{18} \quad \frac{4.0}{14} \quad 57 \quad \frac{5.9}{17} \quad \frac{6.1}{22} \quad \frac{5.9}{34} \quad \frac{7.0}{45} \quad \frac{7.3}{50}$$

Sta

+

H.I.

-

Elev

801+00



Sta

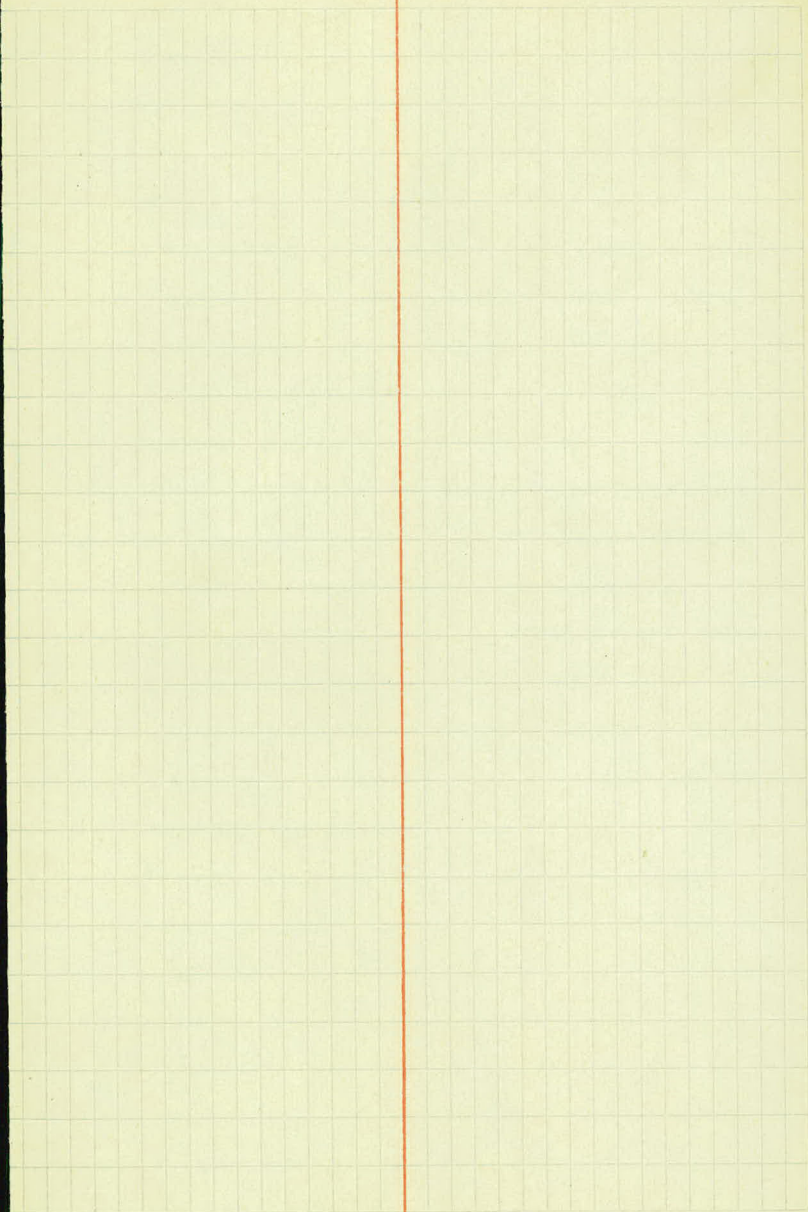
+

H I

-

Elev

1



Sta

+

HI

-

Elev

The image shows a page of graph paper with a grid of small squares. A vertical red line runs down the center of the page, dividing it into two equal halves. The grid consists of 20 columns and 30 rows of squares. The paper is off-white and shows some signs of age, such as slight discoloration and a few small spots.

Sta	+	H I	-	Elev
B.M.	475	918.15 <sup>✓</sup>		913.40
562+00				
563+00				
564+00				
565+00				
+50				
566+00				
567+00				
+50				
568+00				
T.P.	3.54	917.88 <sup>✓</sup>	3.81	914.34 <sup>✓</sup>
569+00				
+63				

10/24/27

spike in stump 50' ht to 560+65'

$\frac{24}{50}$	$\frac{28}{40}$	$\frac{25}{30}$	$\frac{25}{26}$	$\frac{52}{20}$	50	$\frac{42}{20}$	$\frac{25}{27}$	$\frac{23}{32}$	$\frac{60}{40}$	$\frac{35}{42}$	$\frac{35}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

(47)

$\frac{30}{50}$	$\frac{32}{39}$	$\frac{24}{31}$	$\frac{24}{27}$	$\frac{53}{20}$	50	$\frac{57}{20}$	$\frac{84}{28}$	$\frac{84}{29}$	$\frac{42}{37}$	$\frac{44}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(47)

$\frac{65}{50}$	$\frac{67}{33}$	$\frac{22}{31}$	$\frac{26}{29}$	$\frac{52}{20}$	50	$\frac{49}{20}$	$\frac{25}{28}$	$\frac{25}{31}$	$\frac{65}{33}$	$\frac{65}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(46)

$\frac{40}{50}$	$\frac{41}{32.5}$	$\frac{23}{31}$	$\frac{24}{28}$	$\frac{48}{20}$	49	$\frac{48}{20}$	$\frac{28}{29}$	$\frac{28}{32}$	$\frac{46}{20}$	$\frac{47}{50}$
-----------------	-------------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(44)

$\frac{30}{50}$	$\frac{35}{38}$	$\frac{31}{30}$	$\frac{31}{28}$	$\frac{50}{20}$	49	$\frac{51}{20}$	$\frac{39}{29}$	$\frac{30}{31}$	$\frac{37}{39}$	$\frac{38}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(46)

$\frac{32}{50}$	$\frac{32}{39}$	$\frac{28}{31}$	$\frac{32}{27}$	$\frac{52}{20}$	50	$\frac{50}{20}$	$\frac{26}{28}$	$\frac{27}{31.5}$	$\frac{33}{40}$	$\frac{33}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-------------------	-----------------	-----------------

(46)

$\frac{28}{50}$	$\frac{30}{39}$	$\frac{32}{30}$	$\frac{32}{27}$	$\frac{51}{20}$	50	$\frac{50}{20}$	$\frac{24}{27}$	$\frac{24}{30}$	$\frac{32}{31.5}$	$\frac{39}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-------------------	-----------------

(47)

$\frac{35}{50}$	$\frac{33}{39}$	$\frac{25}{30}$	$\frac{27}{28}$	$\frac{51}{20}$	48	$\frac{51}{20}$	$\frac{25}{27}$	$\frac{27}{29}$	$\frac{32}{38}$	$\frac{40}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(48)

$\frac{51}{50}$	$\frac{50}{37}$	$\frac{27}{31}$	$\frac{22}{31.5}$	$\frac{51}{20}$	51	$\frac{50}{20}$	$\frac{30}{27}$	$\frac{30}{31.5}$	$\frac{36}{38}$	$\frac{39}{50}$
-----------------	-----------------	-----------------	-------------------	-----------------	----	-----------------	-----------------	-------------------	-----------------	-----------------

(49)

$\frac{106}{50}$	$\frac{100}{33}$	$\frac{48}{20.5}$	45	$\frac{48}{20}$	$\frac{24}{21.5}$	$\frac{62}{50}$
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(47)

$\frac{110}{50}$	$\frac{103}{34}$	$\frac{48}{21}$	47	$\frac{50}{20}$	$\frac{23}{31}$	$\frac{25}{50}$
------------------	------------------	-----------------	----	-----------------	-----------------	-----------------

(46)

Sta

+

HI

✓

-

Elev

917.88

570+00

+50

571+00

+50

572+00

+50

573+00

+50

574

+40

575



Sta	+	H.I.	-	Elev
		✓ 917.88		
576				
B.M.	4.87	✓ 918.07	465	✓ 913.23

577

578

+50

579

B.M.	4.96	✓ 918.16	4.87	✓ 913.20
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580+00

581+00

+50

582

+50

583

10/25/27

+50 Beg Ditch

$\frac{56}{50}$	$\frac{53}{34}$	$\frac{20}{30.5}$	$\frac{74}{28.5}$	$\frac{43}{20}$	44	$\frac{42}{21}$	$\frac{65}{27.5}$	$\frac{65}{30}$	$\frac{55}{32.5}$	$\frac{51}{50}$
-----------------	-----------------	-------------------	-------------------	-----------------	----	-----------------	-------------------	-----------------	-------------------	-----------------

spike in 12" Oak 60' Lt 54

$\frac{45}{50}$	$\frac{43}{37}$	$\frac{12}{31}$	$\frac{73}{27}$	$\frac{49}{20}$	45	$\frac{47}{20}$	$\frac{58}{24.8}$	$\frac{72}{21.5}$	$\frac{72}{29}$	$\frac{60}{32}$	$\frac{70}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-------------------	-------------------	-----------------	-----------------	-----------------

$\frac{38}{50}$	$\frac{40}{38}$	$\frac{72}{31}$	$\frac{23}{28}$	$\frac{50}{20}$	46	$\frac{52}{23}$	$\frac{73}{28}$	$\frac{73}{29}$	$\frac{57}{34.5}$	$\frac{65}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-------------------	-----------------

$\frac{34}{50}$	$\frac{32}{39}$	$\frac{67}{32.5}$	$\frac{72}{29}$	$\frac{48}{20}$	47	$\frac{49}{20}$	$\frac{68}{26}$	$\frac{68}{30}$	$\frac{48}{34}$	$\frac{53}{50}$
-----------------	-----------------	-------------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{33}{50}$	$\frac{33}{40}$	$\frac{68}{31.5}$	$\frac{67}{28.5}$	$\frac{49}{20}$	48	$\frac{51}{20}$	$\frac{73}{27}$	$\frac{73}{30}$	$\frac{37}{35.5}$	$\frac{43}{50}$
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spike in 12" Oak 60' Lt 54

$\frac{42}{50}$	$\frac{40}{36.5}$	$\frac{25}{29.5}$	$\frac{75}{27}$	$\frac{55}{20}$	49	$\frac{53}{20}$	$\frac{78}{27.5}$	$\frac{77}{30}$	$\frac{38}{37}$	$\frac{48}{50}$
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$\frac{40}{50}$	$\frac{38}{37}$	$\frac{20}{29.5}$	$\frac{73}{27}$	$\frac{55}{20}$	50	$\frac{54}{20}$	$\frac{78}{25.5}$	$\frac{77}{28}$	$\frac{30}{38}$	$\frac{30}{50}$
-----------------	-----------------	-------------------	-----------------	-----------------	----	-----------------	-------------------	-----------------	-----------------	-----------------

$\frac{55}{50}$	$\frac{52}{34.5}$	$\frac{78}{29}$	$\frac{78}{25}$	$\frac{55}{20}$	51	$\frac{55}{24.5}$	$\frac{78}{26}$	$\frac{78}{29.5}$	$\frac{30}{38}$	$\frac{30}{50}$
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+95 End Ditch

8	$\frac{80}{50}$	$\frac{78}{28}$	$\frac{55}{20}$	52	$\frac{55}{20}$	$\frac{78}{28}$	$\frac{78}{31}$	$\frac{42}{26.5}$	$\frac{34}{50}$
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$\frac{104}{50}$	$\frac{98}{32.5}$	$\frac{55}{20}$	53	$\frac{55}{20}$	$\frac{77}{26.5}$	$\frac{78}{31}$	$\frac{50}{36}$	$\frac{43}{50}$
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$\frac{85}{50}$	$\frac{85}{29.5}$	$\frac{60}{20}$	54	$\frac{60}{20}$	$\frac{78}{28}$	$\frac{78}{21}$	$\frac{58}{36.5}$	$\frac{52}{50}$
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+00 Beg Ditch

Sta	+	HI	-	Elev
		918.96		
584				
T.P.	2.55	915.68	5.03	913.13
585				
586				
	+50			
587				
	+44'			
588				
	+50			
589				
	+50			
B.M.	4.81	915.70	4.81	910.89 = 910.89
590				

10/25/27

$\frac{63}{50}$	$\frac{64}{37}$	$\frac{78}{32.5}$	$\frac{78}{28.5}$	$\frac{61}{24}$	57	$\frac{60}{20}$	$\frac{83}{28.5}$	$\frac{83}{27}$	$\frac{54}{39}$	$\frac{50}{50}$
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$\frac{37}{50}$	$\frac{38}{38}$	$\frac{61}{32}$	$\frac{61}{28.5}$	$\frac{41}{21}$	58	$\frac{41}{20}$	$\frac{64}{28.5}$	$\frac{64}{27}$	$\frac{81}{38}$	$\frac{30}{50}$
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$\frac{44}{50}$	$\frac{38}{38}$	$\frac{64}{32.5}$	$\frac{64}{28}$	$\frac{45}{24.5}$	59	$\frac{44}{20}$	$\frac{64}{27}$	$\frac{65}{26.5}$	$\frac{36}{38}$	$\frac{38}{50}$
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$\frac{46}{50}$	$\frac{43}{38}$	$\frac{73}{32}$	$\frac{74}{28.5}$	$\frac{46}{20}$	60	$\frac{47}{20}$	$\frac{67}{28.5}$	$\frac{67}{31}$	$\frac{40}{37.5}$	$\frac{43}{50}$
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$\frac{45}{50}$	$\frac{45}{38.5}$	$\frac{78}{23}$	$\frac{78}{28}$	$\frac{53}{24}$	61	$\frac{49}{20}$	$\frac{70}{27}$	$\frac{72}{30}$	$\frac{50}{36.5}$	$\frac{47}{50}$
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$\frac{46}{50}$	$\frac{44}{40}$	$\frac{73}{36}$	$\frac{74}{32.5}$	$\frac{52}{24}$	62	$\frac{53}{22}$	$\frac{68}{30}$	$\frac{68}{32}$	$\frac{43}{38}$	$\frac{42}{50}$
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$\frac{42}{50}$	$\frac{44}{41}$	$\frac{72}{36}$	$\frac{75}{31}$	$\frac{59}{24}$	63	$\frac{56}{25}$	$\frac{76}{30}$	$\frac{77}{36}$	$\frac{40}{44}$	$\frac{76}{50}$
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$\frac{43}{50}$	$\frac{46}{40}$	$\frac{77}{34.5}$	$\frac{77}{28}$	$\frac{62}{22.5}$	64	$\frac{57}{14}$	Cutoffs.			
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$\frac{55}{50}$	$\frac{55}{40}$	$\frac{82}{35}$	$\frac{81}{29}$	$\frac{64}{22}$	65	$\frac{53}{20}$				
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$\frac{82}{50}$	$\frac{80}{36.7}$	$\frac{92}{34}$	$\frac{90}{29}$	$\frac{68}{32}$	66	$\frac{50}{20}$				
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+65 End of hole

spike in 18" dia 110' at 210 588453

$\frac{100}{50}$	$\frac{90}{27.5}$	$\frac{71}{22}$	$\frac{61}{22}$	$\frac{52}{18.5}$	$\frac{74}{38}$	$\frac{77}{40}$
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579

+

HI

-

Flev

915.70

590 +50

591

+50

T.P.

4.21

913.74<sup>✓</sup>

6.17

907.53<sup>✓</sup>

592

+50

593

+50

594

+50

595

+47

+58

10/25/27

$\frac{100}{50}$	$\frac{97}{294}$	$\frac{75}{225}$	64	$\frac{57}{20}$	$\frac{82}{28}$	$\frac{84}{50}$
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61

$\frac{108}{50}$	$\frac{98}{29}$	$\frac{78}{213}$	68	$\frac{61}{20}$	$\frac{94}{295}$	$\frac{96}{50}$
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62

$\frac{102}{50}$	$\frac{101}{31}$	$\frac{78}{225}$	68	$\frac{61}{21}$	$\frac{102}{30}$	$\frac{107}{50}$
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63

+ 45 Bay Ditch L.

$\frac{74}{53}$	$\frac{75}{27}$	$\frac{81}{36}$	$\frac{80}{34}$	$\frac{58}{215}$	50	$\frac{43}{20}$	$\frac{85}{30}$	$\frac{77}{50}$
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60

$\frac{71}{50}$	$\frac{71}{384}$	$\frac{84}{265}$	$\frac{84}{315}$	$\frac{60}{24}$	49	$\frac{43}{20}$	$\frac{80}{30}$	$\frac{97}{50}$
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50

$\frac{60}{50}$	$\frac{67}{39}$	$\frac{86}{265}$	$\frac{85}{295}$	$\frac{62}{225}$	50	$\frac{42}{20}$	$\frac{82}{31}$	$\frac{85}{50}$
-----------------	-----------------	------------------	------------------	------------------	----	-----------------	-----------------	-----------------

51

$\frac{50}{50}$	$\frac{51}{41}$	$\frac{82}{36}$	$\frac{80}{265}$	$\frac{58}{215}$	52	$\frac{42}{20}$	$\frac{74}{29}$	$\frac{82}{50}$
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52

$\frac{46}{50}$	$\frac{57}{40}$	$\frac{81}{245}$	$\frac{78}{25}$	$\frac{58}{20}$	51	$\frac{43}{20}$	$\frac{65}{18}$	$\frac{73}{50}$
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53

+ 45 Bay Ditch Rt.

$\frac{55}{50}$	$\frac{57}{39}$	$\frac{77}{37}$	$\frac{82}{34}$	$\frac{83}{28}$	$\frac{53}{30}$	52	49	$\frac{77}{275}$	$\frac{78}{30}$	$\frac{62}{34}$	$\frac{60}{50}$
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54

$\frac{46}{50}$	$\frac{49}{40}$	$\frac{83}{335}$	$\frac{87}{305}$	$\frac{82}{26}$	$\frac{51}{20}$	50	$\frac{41}{30}$	$\frac{65}{25}$	$\frac{75}{295}$	$\frac{74}{325}$	$\frac{56}{355}$	$\frac{58}{50}$
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49

+ 41 End Ditch Rt.

$\frac{49}{50}$	$\frac{48}{39}$	$\frac{83}{325}$	$\frac{85}{295}$	$\frac{80}{46}$	$\frac{50}{20}$	49	$\frac{49}{20}$	$\frac{82}{285}$	$\frac{67}{43}$	$\frac{50}{50}$
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42

$\frac{53}{50}$	$\frac{53}{39}$	$\frac{82}{33}$	$\frac{78}{26}$	$\frac{48}{20}$	48			$\frac{47}{20}$		$\frac{46}{50}$
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43

Per

Sta.	+	HI	-	Elev
		913.74		
	+64			
	+80			
	+95			
596				
	+15			
1	+82			
597				
	+11			
	+43			
	+64			
598				
	+50			
TP.	8.16	917.62	4.28	909.46

✓

✓

10/25/27

						(48)	C. Pav	Pav			
$\frac{5.5}{50}$	$\frac{5.8}{37}$	$\frac{7.8}{33.5}$	$\frac{8.2}{26}$	$\frac{4.8}{22}$	48	$\frac{48}{15}$	$\frac{20}{20}$	$\frac{45}{50}$			
+66 Ent Ditch Lt						(48)	Pav	Pav			
	$\frac{5.8}{51}$	$\frac{5.0}{44}$		$\frac{4.7}{29}$		48	$\frac{45}{24}$	$\frac{48}{37}$	$\frac{7.8}{50}$		
						(48)	Pav	Pav			
						48	$\frac{45}{20}$	$\frac{8.5}{29}$	$\frac{9.2}{50}$		
						(48)	Pav	Pav			
						48	$\frac{4.8}{20}$	$\frac{8.0}{27}$	$\frac{9.5}{38}$	$\frac{9.0}{50}$	
						(48)	Pav	Pav			
						48	$\frac{6.6}{50}$	$\frac{7.1}{26}$	$\frac{5.0}{20}$		
+50 Bay Ditch Lt						(46)					
						46	$\frac{4.6}{20}$	$\frac{2.0}{26.5}$	$\frac{7.1}{29}$	$\frac{6.4}{31.5}$	$\frac{6.8}{50}$
						(46)					
						46	$\frac{4.4}{20}$	$\frac{7.1}{26}$	$\frac{7.2}{29.5}$	$\frac{7.4}{31}$	$\frac{4.6}{50}$
						(46)					
						46	$\frac{4.9}{20}$	$\frac{7.3}{26}$	$\frac{7.6}{29.5}$	$\frac{5.4}{33}$	$\frac{4.8}{50}$
						(45)					
						45	$\frac{4.6}{20}$	$\frac{7.6}{26}$	$\frac{7.7}{32}$	$\frac{6.4}{34}$	$\frac{6.2}{50}$
						(47)					
						47	$\frac{4.7}{20}$	$\frac{7.0}{25.5}$	$\frac{7.1}{50}$		
+75 Bay Ditch Lt						(44)					
						44	$\frac{4.6}{20}$	$\frac{7.1}{26}$	$\frac{7.1}{29.5}$	$\frac{6.2}{31.5}$	$\frac{6.5}{50}$
						(44)					
						44	$\frac{4.8}{20}$	$\frac{6.8}{25}$	$\frac{7.0}{28}$	$\frac{2.0}{37}$	$\frac{7.0}{50}$

Sta	+	HI	-	Elev
B.M.	1.04	915.10 <sup>✓</sup>	3.54	914.08 <sup>✓</sup> = 914.06

599+00

+50

600+00

+50

601+00

+50

602+00

+50

603+00

+50

604+00

+50

11/20/27

Sp. 14 to 12" O.G.A. 80' at 54 599+40.

$\frac{15}{50}$	$\frac{15}{45}$	$\frac{88}{50}$	$\frac{88}{26.5}$	$\frac{58}{20}$	$\frac{55}{50}$	$\frac{5.8}{20}$	$\frac{80}{25.5}$	$\frac{80}{29}$	$\frac{2.2}{39.5}$	$\frac{2.2}{50}$
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(55)

$\frac{20}{50}$	$\frac{20}{41}$	$\frac{82}{29.5}$	$\frac{84}{22}$	$\frac{57}{20}$	$\frac{5.5}{50}$	$\frac{5.7}{19.5}$	$\frac{80}{24}$	$\frac{80}{27.5}$	$\frac{1.3}{38.5}$	$\frac{2.4}{50}$
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(55)

$\frac{31}{50}$	$\frac{28}{39}$	$\frac{82}{29}$	$\frac{80}{25.5}$	$\frac{51}{20}$	$\frac{50}{50}$	$\frac{5.3}{18.5}$	$\frac{79}{25}$	$\frac{77}{29.5}$	$\frac{3.2}{37}$	$\frac{3.4}{50}$
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(59)

$\frac{50}{50}$	$\frac{4.7}{34.5}$	$\frac{6.8}{30}$	$\frac{20}{26}$	$\frac{4.8}{20}$	$\frac{4.8}{50}$	$\frac{5.1}{20}$	$\frac{73}{24}$	$\frac{70}{24.5}$	$\frac{5.1}{33}$	$\frac{5.7}{50}$
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(50)

+85 End Ditch Rt

$\frac{7.5}{50}$	$\frac{6.5}{30.5}$	$\frac{7.0}{29}$	$\frac{6.8}{25}$	$\frac{5.0}{20}$	$\frac{50}{50}$	$\frac{5.0}{19.5}$	$\frac{75}{29}$	$\frac{72}{29}$	$\frac{8.7}{50}$
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(A)

to End Ditch Lt.

$\frac{8.0}{50}$	$\frac{8.0}{31}$	$\frac{7.0}{25.5}$	$\frac{5.0}{20}$	$\frac{5.0}{50}$	$\frac{5.0}{50}$	$\frac{5.0}{20}$	$\frac{8.1}{28}$	$\frac{8.5}{30}$	$\frac{9.1}{31.5}$	$\frac{10.1}{50}$
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(A)

$\frac{8.0}{50}$	$\frac{7.0}{28}$	$\frac{5.0}{20}$	$\frac{5.0}{50}$	$\frac{5.0}{50}$	$\frac{4.8}{19.5}$	$\frac{7.1}{26.5}$	$\frac{2.1}{26.5}$	$\frac{2.5}{50}$
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(A)

+10 Beg Pt. 184.

$\frac{7.6}{50}$	$\frac{7.2}{32}$	$\frac{6.5}{31}$	$\frac{6.5}{27}$	$\frac{5.0}{21.5}$	$\frac{5.0}{50}$	$\frac{5.0}{20.5}$	$\frac{7.0}{27.5}$	$\frac{7.1}{31}$	$\frac{5.5}{33.5}$	$\frac{5.3}{50}$
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(46)

$\frac{7.3}{50}$	$\frac{6.7}{31}$	$\frac{7.1}{30}$	$\frac{7.0}{26.5}$	$\frac{5.0}{20}$	$\frac{5.0}{50}$	$\frac{5.0}{20}$	$\frac{7.3}{27.5}$	$\frac{7.3}{30}$	$\frac{5.7}{33}$	$\frac{5.3}{50}$
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(A)

603 Beg Beg Ditch Lt

$\frac{6.1}{50}$	$\frac{6.4}{34}$	$\frac{7.8}{31.5}$	$\frac{7.4}{29}$	$\frac{5.3}{21}$	$\frac{5.7}{50}$	$\frac{5.0}{20.5}$	$\frac{7.4}{28}$	$\frac{7.6}{29.5}$	$\frac{6.6}{32.5}$	$\frac{6.5}{50}$
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(51)

$\frac{4.8}{50}$	$\frac{4.8}{35.5}$	$\frac{7.4}{30}$	$\frac{7.2}{26.5}$	$\frac{5.2}{20.5}$	$\frac{5.2}{50}$	$\frac{5.2}{20}$	$\frac{7.3}{28}$	$\frac{7.4}{31}$	$\frac{6.1}{32.5}$	$\frac{6.6}{50}$
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(50)

$\frac{3.0}{50}$	$\frac{3.4}{37}$	$\frac{7.1}{29.5}$	$\frac{7.2}{26}$	$\frac{5.1}{20.5}$	$\frac{5.2}{50}$	$\frac{5.2}{20}$	$\frac{7.8}{27.5}$	$\frac{7.8}{31.4}$	$\frac{6.6}{33.5}$	$\frac{5.2}{50}$
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(53)

379

+

HI

-

E/c

915.10

605+00

+46

606

T.P

395

913 88 ✓

5.17

908.93 ✓

+50

607

+50

608

+50

609

+50

610+00

+50

BM

355

913 86 ✓

355

910.83 = 910.31 ✓

611+00

+47

10/26/23

42	48	73	76	54
50	36	30.5	26.5	20

(15)

52	54	75	77	60	54	28
20.5	28	31	23.5	43	50	

(16)

71	80	51	51	58	84	95	66	78
50	27.5	20.5		21	27.5	30.5	33.5	50

+46 End Ditch

(18)

98	91	57	57	63	86	80	61	65	78
80	30	20.5		20	25.5	29	34.5	43	50

606-40 Bag Ditch Lt.

(17)

52	48	64	64	40	49	54	78	78	36	40	61
50	34	30	26	20		21	26	29	31	41	50

(19)

30	24	63	65	41	46	58	82	82	25	60
50	36.5	38	35	20		21	27.5	31	41	50

(20)

17	10	66	66	44	47	61	84	18	72	33	48
50	39	39	26	20		21	25.5	24	44.5	45.5	50

(22)

15	10	67	66	45	52	66	90	81	24	42	52
50	39.5	30	26	20		22	28	32	42	47	50

(23)

17	16	68	68	46	53	64	86	86	35	61
50	38.5	28	25	20		24.5	28.5	32	42	50

(25)

20	20	72	73	47	51	70	92	92	40	66
50	38.5	29	25	19.5		22	27.5	30.5	40	50

(26)

26	26	71	72	49	51	66	90	70	54	75
50	38	28.5	20.5	20.5		24.5	28	32	39	50

(27)

41	44	20	68	48	51	71	94	94	62	78
50	35	28.5	26	20.5		21	26	30.5	36.5	50

(29)

66	67	72	71	52	57	68	83	87	75	85
50	31	30	27	21		25.5	27	31	35.5	50

+50 End Ditch

spike in 6" Oak 75' Lt 50' 610-100

(31)

87	75	52	69	87	18	68	78
50	27.5	21	22	27.5	31.5	35.5	50

(32)

88	77	54	66	81	85	80	83	77
50	27	20	22	28	32	33	37	50

+60 End Ditch

Sta	+	HI	-	Elev
		913.86		
612+00				
613+00				
614+00				
615+00				
616+00				
T.P.	5.67	914.37 <sup>✓</sup>	5.16	908.70 <sup>✓</sup>
617+00				
618+00				
619+00				
620+00				
B.M.	3.25	916.26 <sup>✓</sup>	1.85	912.52 = 912.51 <sup>✓</sup>
621+00				
+50				
622+00				

10/26/27

(58)

$\frac{100}{50}$	$\frac{88}{29}$	$\frac{60}{20.5}$	60	$\frac{6.5}{20}$	$\frac{101}{30.5}$	$\frac{104}{50}$
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(58)

$\frac{100}{50}$	$\frac{103}{39}$	$\frac{110}{38}$	$\frac{110}{34}$	$\frac{62}{20.5}$	62	$\frac{6.5}{20}$	$\frac{109}{32}$	$\frac{109}{50}$
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61300 Bay Ditch Lt.

(58)

$\frac{102}{50}$	$\frac{102}{38}$	$\frac{105}{37}$	$\frac{103}{34}$	$\frac{100}{33}$	$\frac{61}{20}$	61	$\frac{6.1}{20}$	$\frac{83}{28}$	$\frac{85}{31.5}$	$\frac{103}{35}$	$\frac{104}{37.5}$	$\frac{95}{39}$	$\frac{91}{50}$
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(58)

$\frac{110}{50}$	$\frac{100}{38}$	$\frac{104}{37}$	$\frac{102}{33}$	$\frac{92}{32}$	$\frac{87}{28.5}$	$\frac{60}{20}$	58	$\frac{5.8}{19.5}$	$\frac{76}{26}$	$\frac{83}{32}$	$\frac{100}{34}$	$\frac{100}{38}$	$\frac{90}{39}$	$\frac{86}{50}$
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(58)

$\frac{85}{50}$	$\frac{86}{39}$	$\frac{76}{38}$	$\frac{90}{33}$	$\frac{82}{31.5}$	$\frac{76}{25}$	$\frac{61}{20}$	60	$\frac{6.0}{20}$	$\frac{74}{26.5}$	$\frac{78}{32}$	$\frac{100}{36.5}$	$\frac{100}{38}$	$\frac{90}{39}$	$\frac{90}{50}$
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(63)

$\frac{92}{50}$	$\frac{92}{39}$	$\frac{102}{38}$	$\frac{100}{33}$	$\frac{85}{31.5}$	$\frac{82}{25}$	$\frac{66}{20}$	64	$\frac{6.4}{21}$	$\frac{78}{27}$	$\frac{82}{31}$	$\frac{102}{34}$	$\frac{106}{37.5}$	$\frac{94}{39}$	$\frac{88}{50}$
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(62)

$\frac{93}{50}$	$\frac{91}{38}$	$\frac{100}{37.5}$	$\frac{97}{33}$	$\frac{88}{32}$	$\frac{85}{25}$	$\frac{65}{20}$	63	$\frac{6.3}{20}$	$\frac{73}{25}$	$\frac{75}{31}$	$\frac{94}{36.5}$	$\frac{93}{37.5}$	$\frac{81}{39}$	$\frac{80}{50}$
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(60)

$\frac{53}{50}$	$\frac{53}{34.5}$	$\frac{81}{39.5}$	$\frac{80}{26.5}$	$\frac{60}{20}$	61	$\frac{6.0}{20}$	$\frac{80}{27}$	$\frac{78}{31.5}$	$\frac{47}{31}$	$\frac{47}{50}$
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(57)

$\frac{29}{50}$	$\frac{26}{39.5}$	$\frac{80}{30}$	$\frac{80}{26}$	$\frac{59}{20}$	57	$\frac{5.9}{20}$	$\frac{78}{26.5}$	$\frac{78}{30.5}$	$\frac{31}{39}$	$\frac{30}{50}$
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Sp. 110 10 6 20 2 60 1 14 14 14

(63)

$\frac{53}{50}$	$\frac{53}{37.5}$	$\frac{90}{39.5}$	$\frac{83}{25.5}$	$\frac{74}{20}$	73	$\frac{7.3}{20}$	$\frac{75}{26.5}$	$\frac{92}{35}$	$\frac{70}{35}$	$\frac{78}{50}$
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(72)

$\frac{62}{50}$	$\frac{74}{34.5}$	$\frac{90}{30}$	$\frac{94}{26}$	$\frac{74}{20}$	72	$\frac{7.2}{20}$	$\frac{94}{27.5}$	$\frac{96}{32}$	$\frac{90}{36}$	$\frac{95}{50}$
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(10)

$\frac{73}{50}$	$\frac{84}{31}$	$\frac{90}{30}$	$\frac{70}{24.5}$	$\frac{72}{20}$	71	$\frac{7.1}{20}$	$\frac{90}{27}$	$\frac{88}{36.5}$	$\frac{94}{50}$
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Sta

+

HI

-

Elev

916.26

623+00

+50

624+00

+50

625+00

+50

626+00

+50

627

T.P

8.97

✓  
920.80

4.43

✓  
911.93

+50

628

628

+60

$\frac{81}{50}$	$\frac{84}{32}$	$\frac{91}{27}$	$\frac{90}{27}$	$\frac{68}{10}$	67	$\frac{67}{20}$	$\frac{83}{26}$	$\frac{87}{30}$	$\frac{73}{32}$	$\frac{75}{50}$
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67

$\frac{50}{50}$	$\frac{55}{36}$	$\frac{87}{29}$	$\frac{86}{25}$	$\frac{68}{20}$	65	$\frac{66}{21}$	$\frac{81}{27}$	$\frac{81}{31}$	$\frac{71}{34}$	$\frac{20}{50}$
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66

$\frac{39}{50}$	$\frac{43}{37}$	$\frac{84}{29}$	$\frac{83}{24}$	$\frac{66}{20}$	64	$\frac{64}{20}$	$\frac{76}{26}$	$\frac{77}{31}$	$\frac{74}{32}$	$\frac{82}{50}$
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64

$\frac{47}{50}$	$\frac{50}{37}$	$\frac{85}{30}$	$\frac{80}{25}$	$\frac{64}{20}$	63	$\frac{62}{19}$	$\frac{78}{26}$	$\frac{78}{31}$	$\frac{61}{33}$	$\frac{74}{50}$
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63

$\frac{65}{50}$	$\frac{72}{33}$	$\frac{85}{31}$	$\frac{84}{27}$	$\frac{61}{20}$	61	$\frac{61}{20}$	$\frac{78}{26}$	$\frac{78}{29}$	$\frac{73}{31}$	$\frac{87}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

61

$\frac{46}{50}$	$\frac{48}{35}$	$\frac{78}{29}$	$\frac{78}{25}$	$\frac{62}{20}$	60	$\frac{60}{20}$	$\frac{81}{27}$	$\frac{81}{30}$	$\frac{61}{34}$	$\frac{61}{50}$
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60

$\frac{31}{50}$	$\frac{28}{39}$	$\frac{78}{29}$	$\frac{78}{25}$	$\frac{62}{20}$	60	$\frac{61}{20}$	$\frac{80}{26}$	$\frac{80}{29}$	$\frac{52}{30}$	$\frac{57}{50}$
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60

$\frac{26}{50}$	$\frac{25}{39}$	$\frac{80}{31}$	$\frac{80}{28}$	$\frac{60}{21}$	56	$\frac{60}{19}$	$\frac{80}{24}$	$\frac{78}{30}$	$\frac{52}{35}$	$\frac{62}{50}$
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56

$\frac{10}{50}$	$\frac{17}{41}$	$\frac{78}{30}$	$\frac{78}{27}$	$\frac{57}{20}$	55	$\frac{56}{20}$	$\frac{76}{25}$	$\frac{78}{30}$	$\frac{52}{30}$	$\frac{57}{50}$
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55

$\frac{50}{50}$	$\frac{51}{44}$	$\frac{125}{29}$	$\frac{126}{26}$	$\frac{103}{20}$	99	$\frac{99}{19}$	$\frac{130}{27}$	$\frac{130}{31}$	$\frac{117}{34}$	$\frac{118}{50}$
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99

$\frac{65}{50}$	$\frac{68}{34}$	$\frac{126}{30}$	$\frac{124}{27}$	$\frac{100}{20}$	97	$\frac{98}{20}$	$\frac{125}{28}$	$\frac{126}{32}$	$\frac{110}{36}$	$\frac{125}{50}$
-----------------	-----------------	------------------	------------------	------------------	----	-----------------	------------------	------------------	------------------	------------------

97

$\frac{58}{50}$	$\frac{57}{40}$	$\frac{128}{29}$	$\frac{125}{25}$	$\frac{101}{20}$	98	$\frac{97}{20}$	$\frac{128}{28}$	$\frac{126}{31}$	$\frac{100}{36}$	$\frac{108}{50}$
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98

920 80

629

+50

630

B.M.

9.22

920.83 ✓

9.22

911.58 = 911.61 ✓

+40

631

632

+50

633

T.P.

306

914.48 ✓

9.41

911.42 ✓

+50

634

+50

635

9.4

$\frac{5.5}{50}$	$\frac{5.6}{40.5}$	$\frac{12.3}{29.5}$	$\frac{12.3}{24.5}$	$\frac{10.2}{20.2}$	$\frac{9.6}{20}$	$\frac{9.6}{20}$	$\frac{12.5}{27.5}$	$\frac{12.5}{30}$	$\frac{10.0}{35}$	$\frac{12.1}{50}$
------------------	--------------------	---------------------	---------------------	---------------------	------------------	------------------	---------------------	-------------------	-------------------	-------------------

9.3

$\frac{4.1}{50}$	$\frac{3.7}{43}$	$\frac{12.3}{31}$	$\frac{12.0}{26}$	$\frac{9.8}{20}$	$\frac{9.4}{20}$	$\frac{9.5}{20}$	$\frac{11.8}{26}$	$\frac{11.8}{30.5}$	$\frac{8.2}{36.5}$	$\frac{10.3}{50}$
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9.3

$\frac{2.5}{50}$	$\frac{2.5}{41}$	$\frac{12.0}{30}$	$\frac{12.0}{28}$	$\frac{9.8}{20.5}$	$\frac{9.4}{20}$	$\frac{9.8}{20}$	$\frac{11.8}{27}$	$\frac{11.8}{30}$	$\frac{8.0}{36}$	$\frac{9.8}{50}$
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Spide in 6" Oak 50 ft + 40

9.3

$\frac{2.7}{50}$	$\frac{2.0}{44.5}$	$\frac{12.0}{28.5}$	$\frac{12.0}{25}$	$\frac{10.0}{20}$	$\frac{9.3}{20.5}$	$\frac{9.6}{20.5}$	$\frac{12.1}{27}$	$\frac{12.1}{30.5}$	$\frac{9.5}{35}$	$\frac{10.2}{50}$
------------------	--------------------	---------------------	-------------------	-------------------	--------------------	--------------------	-------------------	---------------------	------------------	-------------------

9.4

$\frac{2.7}{50}$	$\frac{9.2}{36}$	$\frac{12.6}{30.5}$	$\frac{12.6}{26}$	$\frac{9.9}{20.5}$	$\frac{9.6}{20}$	$\frac{9.6}{20}$	$\frac{12.0}{26}$	$\frac{12.1}{29}$	$\frac{9.9}{33}$	$\frac{10.0}{50}$
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9.7

$\frac{5.8}{50}$	$\frac{2.0}{37.5}$	$\frac{12.4}{28}$	$\frac{12.4}{24.5}$	$\frac{10.1}{20}$	$\frac{9.7}{20}$	$\frac{9.7}{20}$	$\frac{12.1}{28}$	$\frac{12.1}{31}$	$\frac{9.0}{35}$	$\frac{9.0}{50}$
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9.8

$\frac{5.3}{50}$	$\frac{2.0}{38.5}$	$\frac{12.3}{29.5}$	$\frac{12.5}{26.5}$	$\frac{10.0}{20}$	$\frac{10.0}{20}$	$\frac{12.0}{27}$	$\frac{12.0}{30}$	$\frac{11.0}{33.5}$	$\frac{11.5}{50}$	
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+ 80 End Ditch ft.

10.0

$\frac{10.3}{50}$	$\frac{11.4}{33}$	$\frac{12.8}{29.5}$	$\frac{12.8}{26.5}$	$\frac{10.1}{20.5}$	$\frac{10.1}{20}$	$\frac{10.3}{20}$	$\frac{15.3}{37}$	$\frac{15.2}{50}$		
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+ 15 End Ditch ft.

3.8

$\frac{2.7}{50}$	$\frac{2.5}{29}$	$\frac{4.1}{20}$	$\frac{4.0}{20}$	$\frac{4.8}{33}$	$\frac{9.0}{50}$
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+ 80 End Ditch ft.

4.0

$\frac{2.8}{50}$	$\frac{4.3}{37}$	$\frac{6.8}{32}$	$\frac{6.8}{28}$	$\frac{4.2}{20}$	$\frac{4.1}{20}$	$\frac{8.7}{35}$	$\frac{9.7}{50}$
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4.1

$\frac{0.7}{50}$	$\frac{4.3}{36}$	$\frac{6.8}{31}$	$\frac{6.6}{28}$	$\frac{4.6}{20}$	$\frac{4.4}{20}$	$\frac{7.8}{26.5}$	$\frac{9.1}{32.5}$	$\frac{16.1}{38}$	$\frac{11.5}{50}$
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4.3

$\frac{3.8}{50}$	$\frac{5.8}{35}$	$\frac{6.8}{31}$	$\frac{6.6}{27}$	$\frac{4.3}{20}$	$\frac{4.2}{20}$	$\frac{4.5}{20}$	$\frac{7.6}{26.5}$	$\frac{8.5}{32}$	$\frac{12.0}{42}$	$\frac{12.8}{50}$
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914 48

635 + 50

636

+ 50

637

+ 50

638

639

+ 50

640

+ 50

641

T.P.

+ 63

0.11

908.25

6.34

908.4

$\frac{35}{50}$   $\frac{45}{37}$   $\frac{20}{32}$   $\frac{68}{275}$   $\frac{44}{20}$

4.4  
43

$\frac{45}{20}$   $\frac{93}{33}$   $\frac{101}{50}$

$\frac{46}{50}$   $\frac{57}{36}$   $\frac{73}{31}$   $\frac{72}{27}$   $\frac{47}{205}$

4.6  
45

$\frac{48}{20}$   $\frac{71}{29}$   $\frac{77}{50}$

+ 500g Ditch Rt.

50=00 Ditch.  $\frac{71}{50}$   $\frac{76}{38}$   $\frac{48}{20}$

4.7  
46

$\frac{47}{20}$   $\frac{74}{31}$   $\frac{74}{36}$   $\frac{64}{40}$   $\frac{63}{50}$

$\frac{66}{50}$   $\frac{63}{325}$   $\frac{70}{31}$   $\frac{67}{255}$   $\frac{48}{205}$

4.9  
46

$\frac{50}{20}$   $\frac{82}{30}$   $\frac{90}{34}$   $\frac{86}{38}$   $\frac{53}{465}$   $\frac{53}{50}$

$\frac{56}{50}$   $\frac{46}{35}$   $\frac{72}{285}$   $\frac{70}{25}$   $\frac{48}{20}$

5.0  
47

$\frac{54}{205}$   $\frac{70}{24}$   $\frac{94}{33}$   $\frac{94}{37}$   $\frac{41}{465}$   $\frac{40}{50}$

$\frac{54}{50}$   $\frac{50}{35}$   $\frac{76}{305}$   $\frac{74}{25}$   $\frac{54}{20}$

5.2  
51

$\frac{54}{20}$   $\frac{82}{265}$   $\frac{98}{325}$   $\frac{100}{365}$   $\frac{84}{41}$   $\frac{43}{475}$   $\frac{42}{50}$

$\frac{50}{50}$   $\frac{37}{37}$   $\frac{27}{31}$   $\frac{82}{25}$   $\frac{58}{20}$

5.7  
58

$\frac{58}{20}$   $\frac{82}{26}$   $\frac{96}{32}$   $\frac{83}{385}$   $\frac{28}{425}$   $\frac{28}{50}$

$\frac{56}{50}$   $\frac{44}{36}$   $\frac{80}{30}$   $\frac{82}{26}$   $\frac{62}{20}$

6.0  
61

$\frac{62}{205}$   $\frac{94}{31}$   $\frac{88}{40}$   $\frac{33}{48}$   $\frac{37}{50}$

$\frac{72}{50}$   $\frac{59}{35}$   $\frac{88}{30}$   $\frac{88}{26}$   $\frac{66}{20}$

6.5  
63

$\frac{66}{20}$   $\frac{101}{32}$   $\frac{96}{38}$   $\frac{47}{455}$   $\frac{54}{50}$

$\frac{87}{50}$   $\frac{80}{33}$   $\frac{91}{30}$   $\frac{88}{255}$   $\frac{70}{205}$

7.0  
67

$\frac{71}{20}$   $\frac{100}{295}$   $\frac{102}{38}$   $\frac{75}{44}$   $\frac{81}{50}$

$\frac{110}{50}$   $\frac{101}{28}$   $\frac{75}{20}$

7.5  
72

$\frac{75}{20}$   $\frac{115}{33}$   $\frac{116}{37}$   $\frac{100}{40}$   $\frac{107}{50}$

579.641700 End Ditch Lt.

$\frac{86}{50}$   $\frac{74}{325}$   $\frac{18}{20}$

8.0  
77

$\frac{19}{195}$   $\frac{82}{35}$   $\frac{28}{50}$

+ 50 End Ditch Rt.

908.25

642

643

644

+50

645

+50

646+00

B.M.

679

901.96 = 901.93

(23)

$\frac{88}{50}$	$\frac{84}{34.5}$	$\frac{68}{30}$	$\frac{24}{20}$	$\frac{23}{20}$	$\frac{87}{34}$	$\frac{85}{50}$
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(33)

$\frac{84}{50}$	$\frac{83}{32}$	$\frac{33}{20}$	$\frac{21}{20}$	$\frac{34}{20}$	$\frac{48}{24}$	$\frac{86}{34}$	$\frac{83}{50}$
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+75 Bay Ditch

(43)

$\frac{61}{50}$	$\frac{59}{32}$	$\frac{67}{29.5}$	$\frac{65}{27}$	$\frac{45}{20}$	$\frac{44}{20.5}$	$\frac{65}{27}$	$\frac{67}{30}$	$\frac{56}{32}$	$\frac{66}{50}$
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stake wood Bay Ditch.

(53)

$\frac{56}{50}$	$\frac{56}{31.5}$	$\frac{70}{29}$	$\frac{70}{26.5}$	$\frac{48}{20}$	$\frac{48}{21}$	$\frac{70}{28}$	$\frac{68}{31}$	$\frac{42}{36}$	$\frac{40}{50}$
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(63)

$\frac{60}{50}$	$\frac{63}{32.5}$	$\frac{73}{31}$	$\frac{73}{27}$	$\frac{53}{20}$	$\frac{50}{20}$	$\frac{54}{20}$	$\frac{78}{28}$	$\frac{76}{30}$	$\frac{40}{36}$	$\frac{34}{20}$
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(73)

$\frac{67}{50}$	$\frac{70}{32}$	$\frac{84}{28.5}$	$\frac{82}{26}$	$\frac{57}{20}$	$\frac{27}{20.5}$	$\frac{84}{29}$	$\frac{82}{32.5}$	$\frac{58}{35}$	$\frac{48}{50}$
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(83)

$\frac{76}{50}$	$\frac{76}{32.5}$	$\frac{87}{31}$	$\frac{87}{27}$	$\frac{62}{20}$	$\frac{62}{20}$	$\frac{88}{28}$	$\frac{88}{30}$	$\frac{70}{33}$	$\frac{66}{50}$
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spike in 8" oak 48ft of 64ft w

Sta	+	HI	-	Elev
B.M.	524	916.13		910.89
588+50				
589+00				
+50				
590+00				
+50				
591+00				
+50				
592+00				
+50				
593+00				
643				
594+00				

Spillo in 20" Cat. 110' 45" 588+50

59

60  $\frac{64}{22}$   $\frac{84}{29}$   $\frac{85}{32}$   $\frac{43}{40}$   $\frac{40}{50}$

60

$\frac{58}{10}$  60  $\frac{68}{21}$   $\frac{72}{29}$   $\frac{93}{32}$   $\frac{51}{39}$   $\frac{49}{50}$

60

$\frac{55}{31}$   $\frac{54}{20}$  41  $\frac{75}{22}$   $\frac{101}{28}$   $\frac{100}{32}$   $\frac{61}{38}$   $\frac{59}{50}$

60

$\frac{84}{50}$   $\frac{72}{27}$   $\frac{54}{21}$  60  $\frac{73}{22}$   $\frac{97}{29}$   $\frac{100}{32}$   $\frac{69}{38}$   $\frac{70}{50}$

59

$\frac{84}{50}$   $\frac{74}{33}$   $\frac{68}{28}$   $\frac{50}{20}$  59  $\frac{73}{22}$   $\frac{97}{27}$   $\frac{100}{31}$   $\frac{62}{38}$   $\frac{60}{50}$

59

$\frac{79}{50}$   $\frac{72}{27}$   $\frac{49}{20}$  57  $\frac{75}{22}$   $\frac{87}{29}$   $\frac{97}{32}$   $\frac{53}{39}$   $\frac{52}{50}$

56

$\frac{94}{50}$   $\frac{77}{34}$   $\frac{70}{27}$   $\frac{48}{20}$  56  $\frac{71}{22}$   $\frac{95}{29}$   $\frac{96}{32}$   $\frac{56}{38}$   $\frac{57}{50}$

54

$\frac{74}{50}$  ?  $\frac{80}{33}$   $\frac{45}{20}$  54  $\frac{69}{22}$   $\frac{92}{30}$   $\frac{93}{32}$   $\frac{54}{38}$   $\frac{53}{50}$   
38

51

$\frac{100}{50}$   $\frac{85}{31}$   $\frac{43}{21}$  50  $\frac{66}{22}$   $\frac{88}{29}$   $\frac{89}{32}$   $\frac{56}{38}$   $\frac{58}{50}$

48

$\frac{98}{50}$   $\frac{87}{35}$   $\frac{41}{20}$  47  $\frac{63}{22}$   $\frac{81}{30}$   $\frac{87}{33}$   $\frac{59}{37}$   $\frac{59}{50}$

44

$\frac{90}{50}$   $\frac{80}{32}$   $\frac{40}{20}$  42  $\frac{53}{21}$   $\frac{76}{29}$   $\frac{78}{32}$   $\frac{55}{37}$   $\frac{57}{50}$

42

$\frac{85}{50}$   $\frac{69}{30}$   $\frac{39}{20}$  41  $\frac{49}{20}$   $\frac{70}{27}$   $\frac{72}{31}$   $\frac{49}{36}$   $\frac{54}{50}$

Sta

+

HI

-

Elev

916.13 ✓

594+50

595+00

+50

T.P.

5.57

918.53 ✓

3.7

912.96 ✓

596

BM

2.07

917.62 ✓

2.99

915.54 = 915.55 ✓

+50

597

+50

598+00

599+00

600+00

+50

$$\begin{array}{cccccc} \frac{65}{50} & \frac{51}{32} & \frac{56}{31} & \frac{54}{28} & \frac{38}{20} & \frac{39}{31} \\ & & & & & \frac{44}{20} & \frac{69}{28} & \frac{69}{30} & \frac{40}{36} & \frac{42}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{58}{50} & \frac{50}{33} & \frac{55}{30} & \frac{55}{27} & \frac{38}{20} & \frac{34}{34} \\ & & & & & \frac{39}{20} & \frac{55}{27} & \frac{58}{31} & \frac{33}{36} & \frac{30}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{50}{50} & \frac{42}{33} & \frac{53}{31} & \frac{55}{27} & \frac{34}{20} & \frac{32}{32} \\ & & & & & \frac{32}{20} & \frac{53}{27} & \frac{54}{30} & \frac{28}{35} & \frac{28}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{74}{50} & \frac{68}{33} & \frac{78}{30} & \frac{79}{27} & \frac{56}{20} & \frac{55}{55} \\ & & & & & \frac{57}{20} & \frac{76}{28} & \frac{77}{31} & \frac{55}{36} & \frac{59}{60} \end{array}$$

spike in TP 25IT+54 60 4+20

$$\begin{array}{cccccc} \frac{68}{50} & \frac{60}{32} & \frac{65}{30} & \frac{67}{27} & \frac{45}{20} & \frac{42}{43} \\ & & & & & \frac{47}{20} & \frac{70}{28} & \frac{70}{31} & \frac{45}{35} & \frac{50}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{66}{50} & \frac{55}{33} & \frac{68}{30} & \frac{71}{27} & \frac{43}{20} & \frac{41}{41} \\ & & & & & \frac{43}{20} & \frac{62}{28} & \frac{60}{31} & \frac{47}{35} & \frac{47}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{56}{50} & \frac{44}{34} & \frac{66}{30} & \frac{69}{27} & \frac{41}{20} & \frac{40}{40} \\ & & & & & \frac{43}{20} & \frac{66}{27} & \frac{66}{30} & \frac{40}{36} & \frac{42}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{41}{50} & \frac{36}{36} & \frac{68}{29} & \frac{67}{26} & \frac{41}{20} & \frac{41}{40} \\ & & & & & \frac{63}{20} & \frac{63}{26} & \frac{63}{29} & \frac{29}{36} & \frac{30}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{32}{50} & \frac{27}{36} & \frac{60}{30} & \frac{61}{26} & \frac{40}{20} & \frac{41}{41} \\ & & & & & \frac{41}{20} & \frac{62}{25} & \frac{62}{29} & \frac{26}{36} & \frac{33}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{31}{50} & \frac{31}{36} & \frac{62}{30} & \frac{62}{26} & \frac{42}{20} & \frac{42}{42} \\ & & & & & \frac{42}{20} & \frac{61}{36} & \frac{58}{31} & \frac{34}{36} & \frac{38}{50} \end{array}$$

$$\begin{array}{cccccc} \frac{62}{48} & \frac{48}{45} & \frac{46}{34} & \frac{65}{30} & \frac{68}{27} & \frac{46}{20} & \frac{44}{44} \\ & & & & & \frac{45}{20} & \frac{63}{29} & \frac{64}{31} & \frac{49}{34} & \frac{52}{50} \end{array}$$

Sta

+

HI

-

Elev

601+00

917.62  
22  
147

+50

602+00

+47

+69

603+00

+19

+80

604+00

B.M.

915.55



Sta	+	H.I	-	Elev	
B.M.	290	892.91 ✓		890.01	
720 + 01					
721				88.7	4.2
722				88.4	4.5
723				88.2	4.7
724				88.0	4.9
725				87.8	5.1
726				87.8	5.1
				6	
727				87.7	5.2
728				87.6	5.3
729				87.5	5.4
T.P.	4.61	891.07 ✓	6.45	886.46 ✓	
730				87.4	3.7
731				87.4	3.7

11/31/27

spike in 8" Oak 60 knots 721+25-

$\frac{26}{50}$   $\frac{26}{42}$   $\frac{66}{31.5}$   $\frac{65}{29.5}$   $\frac{40}{21}$  38  $\frac{40}{20}$   $\frac{57}{24}$   $\frac{64}{29.5}$   $\frac{55}{34}$   $\frac{38}{37.6}$   $\frac{42}{50}$

$\frac{55}{50}$   $\frac{42}{41}$   $\frac{22}{35.5}$   $\frac{24}{30}$   $\frac{44}{27}$  42  $\frac{43}{20}$   $\frac{68}{29.5}$   $\frac{68}{32.7}$   $\frac{33}{40}$   $\frac{3.0}{50}$

$\frac{57}{50}$   $\frac{58}{38.5}$   $\frac{71}{34}$   $\frac{68}{38.5}$   $\frac{46}{20}$  46  $\frac{49}{21}$   $\frac{75}{27}$   $\frac{25}{31.5}$   $\frac{40}{40.5}$   $\frac{34}{50}$

+10 Ditch Lt.

$\frac{74}{50}$   $\frac{73}{26}$   $\frac{51}{20}$  50  $\frac{27}{20}$   $\frac{77}{26.5}$   $\frac{27}{35}$   $\frac{48}{40.5}$   $\frac{50}{50}$

$\frac{77}{50}$   $\frac{77}{26.5}$   $\frac{52}{21}$  51  $\frac{55}{20}$   $\frac{84}{25.5}$   $\frac{84}{29}$   $\frac{56}{38}$   $\frac{56}{50}$

$\frac{77}{50}$   $\frac{75}{25}$   $\frac{55}{20}$  55  $\frac{56}{20.5}$   $\frac{80}{28}$   $\frac{81}{36}$   $\frac{42}{41}$   $\frac{40}{50}$

$\frac{80}{50}$   $\frac{72}{26}$   $\frac{57}{20}$  58  $\frac{60}{21}$   $\frac{82}{27}$   $\frac{78}{38}$   $\frac{46}{44.5}$   $\frac{44}{50}$

+10 Bag Ditch Lt.

$\frac{81}{50}$   $\frac{81}{36}$   $\frac{88}{35}$   $\frac{88}{31}$   $\frac{85}{30}$   $\frac{72}{25}$   $\frac{61}{20}$  61  $\frac{61}{20}$   $\frac{78}{27.5}$   $\frac{80}{36}$   $\frac{44}{41.5}$   $\frac{44}{50}$

$\frac{81}{50}$   $\frac{80}{36}$   $\frac{90}{35}$   $\frac{92}{30}$   $\frac{86}{29.5}$   $\frac{82}{24.5}$   $\frac{64}{20}$  64  $\frac{65}{20}$   $\frac{74}{23}$   $\frac{82}{29}$   $\frac{81}{31.5}$   $\frac{48}{41}$   $\frac{45}{50}$

H.D.

$\frac{82}{50}$   $\frac{82}{38}$   $\frac{93}{37}$   $\frac{93}{33}$   $\frac{80}{32}$   $\frac{77}{24.5}$   $\frac{67}{20}$  65  $\frac{66}{20}$   $\frac{90}{28}$   $\frac{88}{37}$   $\frac{65}{40.5}$   $\frac{63}{50}$

Reg H.D.

$\frac{64}{50}$   $\frac{66}{38}$   $\frac{76}{37.5}$   $\frac{76}{33}$   $\frac{66}{32}$   $\frac{66}{26}$   $\frac{46}{20}$  46  $\frac{46}{20}$   $\frac{64}{31}$   $\frac{74}{39}$   $\frac{72}{37.5}$   $\frac{55}{39.5}$   $\frac{60}{50}$

$\frac{66}{50}$   $\frac{66}{39}$   $\frac{78}{37}$   $\frac{78}{33}$   $\frac{67}{32}$   $\frac{65}{26}$   $\frac{46}{20}$  47  $\frac{45}{21}$   $\frac{57}{31.5}$   $\frac{76}{33}$   $\frac{77}{38}$   $\frac{60}{39.5}$   $\frac{58}{50}$

Sta	+	H I	-	Flow	
		891.07			
732				87.4	3.7
733				87.4	3.7
734				87.4	3.7
735				87.4	3.7
736				87.4	3.7
737				87.4	3.7
738				87.4	3.7
739				87.4	3.7
740				87.4	3.7
T.P.	5.37	891.63	4.81	886.26	
+36				87.4	4.2
+55				87.4	4.2
+70				87.4	4.2

10/31/27

$\frac{70}{50}$	$\frac{62}{39}$	$\frac{80}{39}$	$\frac{80}{34}$	$\frac{66}{32}$	$\frac{64}{26}$	$\frac{46}{20}$	47	$\frac{47}{20}$	$\frac{66}{23}$	$\frac{78}{33}$	$\frac{78}{37}$	$\frac{64}{39}$	$\frac{64}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{65}{50}$	$\frac{65}{39}$	$\frac{80}{37}$	$\frac{80}{32}$	$\frac{66}{32}$	$\frac{46}{20}$	46	$\frac{46}{20}$	$\frac{65}{31}$	$\frac{78}{32}$	$\frac{80}{37}$	$\frac{65}{39}$	$\frac{62}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{74}{50}$	$\frac{72}{39}$	$\frac{84}{38}$	$\frac{82}{33}$	$\frac{71}{32}$	$\frac{67}{28}$	$\frac{49}{20}$	47	$\frac{50}{20}$	$\frac{66}{31}$	$\frac{82}{32}$	$\frac{82}{36}$	$\frac{67}{38}$	$\frac{67}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{74}{50}$	$\frac{71}{39}$	$\frac{86}{37}$	$\frac{86}{32}$	$\frac{71}{31}$	$\frac{66}{27}$	$\frac{49}{20}$	47	$\frac{46}{20}$	$\frac{60}{24}$	$\frac{64}{31}$	$\frac{82}{33}$	$\frac{83}{37}$	$\frac{69}{39}$	$\frac{68}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{73}{50}$	$\frac{74}{39}$	$\frac{88}{37}$	$\frac{90}{32}$	$\frac{73}{31}$	$\frac{47}{20}$	47	$\frac{46}{20}$	$\frac{71}{31}$	$\frac{88}{32}$	$\frac{81}{39}$	$\frac{71}{39}$	$\frac{72}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{76}{50}$	$\frac{72}{39}$	$\frac{92}{37}$	$\frac{92}{32}$	$\frac{72}{31}$	$\frac{69}{28}$	$\frac{50}{20}$	50	$\frac{48}{20}$	$\frac{68}{27}$	$\frac{90}{31}$	$\frac{90}{37}$	$\frac{73}{39}$	$\frac{68}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{80}{50}$	$\frac{75}{39}$	$\frac{92}{37}$	$\frac{92}{32}$	$\frac{77}{31}$	$\frac{70}{28}$	$\frac{48}{20}$	47	$\frac{46}{20}$	$\frac{65}{28}$	$\frac{68}{30}$	$\frac{91}{32}$	$\frac{92}{37}$	$\frac{68}{40}$	$\frac{66}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{81}{50}$	$\frac{81}{39}$	$\frac{94}{38}$	$\frac{92}{34}$	$\frac{81}{32}$	$\frac{77}{29}$	$\frac{49}{20}$	48	$\frac{47}{20}$	$\frac{71}{28}$	$\frac{73}{31}$	$\frac{94}{32}$	$\frac{98}{38}$	$\frac{73}{39}$	$\frac{72}{50}$
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$\frac{84}{50}$	$\frac{84}{39}$	$\frac{100}{37}$	$\frac{96}{33}$	$\frac{82}{32}$	$\frac{78}{29}$	$\frac{68}{25}$	$\frac{50}{20}$	49	$\frac{51}{20}$	$\frac{67}{23}$	$\frac{74}{27}$	$\frac{78}{31}$	$\frac{97}{32}$	$\frac{97}{37}$	$\frac{81}{39}$	$\frac{78}{50}$
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$\frac{94}{50}$	$\frac{92}{38}$	$\frac{103}{37}$	$\frac{106}{34}$	$\frac{94}{32}$	$\frac{85}{27}$	$\frac{80}{25}$	$\frac{56}{20}$	56	$\frac{58}{20}$	$\frac{96}{27}$	$\frac{100}{32}$	$\frac{106}{33}$	$\frac{110}{38}$	$\frac{98}{39}$	$\frac{100}{50}$
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$\frac{97}{50}$	$\frac{97}{39}$	$\frac{110}{37}$	$\frac{107}{32}$	$\frac{96}{32}$	$\frac{85}{27}$	$\frac{55}{20}$	58	$\frac{58}{21}$	$\frac{93}{26}$	$\frac{100}{32}$	$\frac{112}{38}$	$\frac{100}{40}$	$\frac{96}{50}$
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$\frac{101}{50}$	$\frac{110}{37}$	$\frac{112}{34}$	$\frac{98}{28}$	$\frac{57}{20}$	58	$\frac{58}{20}$	$\frac{88}{28}$	$\frac{95}{32}$	$\frac{110}{34}$	$\frac{114}{38}$	$\frac{94}{40}$	$\frac{96}{50}$
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579	+	H I	-	E/eu	
		891.63			
741+00				87.4	4.2
742+00				87.4	4.2
743+00				87.4	4.2
744+00				87.4	4.2
745+00				87.4	4.2
+50				87.4	4.2
746				87.4	4.2
+50				87.4	4.2
747				87.4	4.2
+65				87.4	4.2
748				87.4	4.2
T.P.	843	895.83	4.23	887.40	
+50				87.4	8.4

10/3/27

$\frac{103}{50}$   $\frac{103}{39}$   $\frac{118}{38}$   $\frac{120}{33}$   $\frac{101}{31}$   $\frac{70}{22}$   $\frac{56}{20}$  56  $\frac{56}{21}$   $\frac{90}{33}$   $\frac{117}{31.5}$   $\frac{117}{40}$   $\frac{88}{42}$   $\frac{82}{46}$   $\frac{88}{50}$

$\frac{91}{50}$   $\frac{90}{39}$   $\frac{103}{37.5}$   $\frac{103}{33}$   $\frac{88}{32.5}$   $\frac{87}{29}$   $\frac{75}{26}$   $\frac{54}{20}$  54  $\frac{54}{20}$   $\frac{76}{30}$   $\frac{110}{34}$   $\frac{110}{39}$   $\frac{76}{41.5}$   $\frac{67}{46}$   $\frac{75}{50}$

$\frac{77}{50}$   $\frac{77}{39}$   $\frac{98}{38}$   $\frac{98}{32}$   $\frac{80}{31}$   $\frac{75}{28.5}$   $\frac{70}{25}$   $\frac{54}{20}$  54  $\frac{54}{20}$   $\frac{71}{31}$   $\frac{101}{32.5}$   $\frac{100}{32.5}$   $\frac{72}{40}$   $\frac{65}{45}$   $\frac{73}{50}$

$\frac{87}{50}$   $\frac{86}{37.5}$   $\frac{94}{37}$   $\frac{92}{33}$   $\frac{84}{32}$   $\frac{74}{25}$   $\frac{52}{20}$  50  $\frac{52}{20}$   $\frac{70}{26}$   $\frac{80}{31.5}$   $\frac{95}{32.5}$   $\frac{94}{32.5}$   $\frac{78}{39}$   $\frac{74}{45}$   $\frac{78}{50}$

(42)

$\frac{78}{50}$   $\frac{78}{39}$   $\frac{92}{38}$   $\frac{91}{33}$   $\frac{77}{32}$   $\frac{72}{27}$   $\frac{48}{20}$  48  $\frac{48}{21}$   $\frac{60}{23}$   $\frac{64}{28}$   $\frac{72}{31}$   $\frac{90}{33}$   $\frac{90}{37.5}$   $\frac{72}{39}$   $\frac{67}{44.5}$   $\frac{73}{50}$

(42)

$\frac{85}{50}$   $\frac{83}{39}$   $\frac{90}{38}$   $\frac{90}{33.5}$   $\frac{83}{32.5}$   $\frac{80}{28}$   $\frac{68}{25}$   $\frac{48}{20}$  47  $\frac{50}{20.5}$   $\frac{67}{23}$   $\frac{67}{27}$   $\frac{70}{31}$   $\frac{90}{32}$   $\frac{90}{39}$   $\frac{77}{38.5}$   $\frac{68}{46}$   $\frac{74}{49}$   $\frac{76}{50}$

(42)

$\frac{74}{50}$   $\frac{73}{39}$   $\frac{80}{37.5}$   $\frac{90}{33}$   $\frac{71}{31}$   $\frac{71}{28}$   $\frac{48}{20}$  45  $\frac{48}{21}$   $\frac{88}{32}$   $\frac{83}{41}$   $\frac{50}{50}$

(42)

$\frac{82}{50}$   $\frac{78}{38}$   $\frac{93}{38}$   $\frac{90}{33}$   $\frac{77}{32.5}$   $\frac{75}{27}$   $\frac{46}{20}$  44  $\frac{46}{21}$   $\frac{78}{38}$   $\frac{80}{44}$   $\frac{47}{49}$   $\frac{47}{50}$

+75 End H.D.

(42)

$\frac{69}{50}$   $\frac{75}{40}$   $\frac{100}{37}$   $\frac{96}{27}$   $\frac{48}{20}$  46  $\frac{46}{20}$   $\frac{84}{30}$   $\frac{86}{42.5}$   $\frac{40}{50}$

(42)

$\frac{60}{50}$   $\frac{57}{47}$   $\frac{94}{41}$   $\frac{98}{31}$   $\frac{44}{20.5}$  44  $\frac{45}{21}$   $\frac{84}{29}$   $\frac{84}{39.5}$   $\frac{28}{50}$

(42)

$\frac{36}{50}$   $\frac{96}{45}$   $\frac{92}{30}$   $\frac{42}{20}$  42  $\frac{44}{21}$   $\frac{80}{29}$   $\frac{80}{38}$   $\frac{68}{42}$   $\frac{18}{50}$

(42)

$\frac{52}{50}$   $\frac{132}{39}$   $\frac{133}{30}$   $\frac{85}{20}$  84  $\frac{86}{20.5}$   $\frac{122}{31}$   $\frac{122}{37}$   $\frac{98}{44}$   $\frac{53}{50}$

Sta	+	H.I.	-	Elev	
		895.83 ✓			
749+00				87.4	8.4
	+50			87.4	8.4
750				87.4	8.4
	+50			87.4	8.4
751				87.4	8.4
	+50			87.4	8.4
752				87.4	8.4
	+17	892.23 ✓	7.77	888.06 ✓	
753				87.4	4.8
754				87.4	4.8
755				87.4	4.8
				8	
756				87.4	4.8
757				87.4	4.8

10/31/27

(84)

$\frac{3.9}{50}$   $\frac{13.0}{38}$   $\frac{13.5}{30}$   $\frac{8.5}{20}$   $\frac{85}{20}$   $\frac{88}{20}$   $\frac{12.8}{20}$   $\frac{12.6}{30}$   $\frac{9.7}{45}$   $\frac{4.7}{50}$

(85)

$\frac{4.2}{50}$   $\frac{13.1}{37.5}$   $\frac{13.5}{29}$   $\frac{8.6}{21}$   $\frac{85}{20}$   $\frac{8.5}{20}$   $\frac{12.4}{30}$   $\frac{12.3}{33}$   $\frac{9.1}{42}$   $\frac{2.8}{50}$

(86)

$\frac{5.3}{50}$   $\frac{13.8}{40}$   $\frac{13.9}{30}$   $\frac{8.8}{20}$   $\frac{88}{20}$   $\frac{8.8}{20}$   $\frac{12.3}{29}$   $\frac{12.2}{32}$   $\frac{10.0}{38}$   $\frac{4.8}{48}$   $\frac{2.3}{50}$

(87)

$\frac{6.4}{50}$   $\frac{12.8}{39}$   $\frac{12.2}{29}$   $\frac{9.1}{20}$   $\frac{86}{21}$   $\frac{8.9}{21}$   $\frac{12.3}{29.5}$   $\frac{12.2}{32}$   $\frac{11.3}{33}$   $\frac{9.0}{40}$   $\frac{1.8}{50}$

(84)

$\frac{7.0}{50}$   $\frac{13.0}{40}$   $\frac{12.5}{28}$   $\frac{9.0}{20}$   $\frac{89}{20}$   $\frac{9.0}{20}$   $\frac{11.7}{36}$   $\frac{11.7}{35}$   $\frac{0.2}{50}$

(84)

$\frac{7.2}{50}$   $\frac{12.8}{40}$   $\frac{12.5}{29}$   $\frac{8.8}{20}$   $\frac{88}{20}$   $\frac{8.8}{20}$   $\frac{11.2}{26}$   $\frac{11.2}{37.5}$   $\frac{0.7}{50}$

(84)

$\frac{7.5}{50}$   $\frac{12.8}{39}$   $\frac{12.8}{28}$   $\frac{8.8}{20}$   $\frac{89}{20}$   $\frac{8.8}{20}$   $\frac{11.8}{29}$   $\frac{11.5}{39}$   $\frac{3.4}{50}$

+ 85 End Ditch Lt.

(48)

$\frac{7.5}{50}$   $\frac{7.3}{38}$   $\frac{5.1}{20}$   $\frac{50}{21}$   $\frac{5.2}{21}$   $\frac{8.3}{30}$   $\frac{7.7}{43}$   $\frac{6.4}{45}$   $\frac{6.2}{50}$

+ 10 End Ditch Rt.

(48)

$\frac{8.2}{50}$   $\frac{7.7}{27}$   $\frac{5.2}{20}$   $\frac{50}{20.5}$   $\frac{5.2}{20.5}$   $\frac{7.8}{29}$   $\frac{8.0}{50}$

(48)

$\frac{8.2}{50}$   $\frac{8.0}{28}$   $\frac{4.7}{20}$   $\frac{4.7}{21}$   $\frac{7.7}{30}$   $\frac{7.7}{50}$

(48)

$\frac{8.3}{50}$   $\frac{8.0}{28}$   $\frac{5.1}{20}$   $\frac{4.8}{21}$   $\frac{4.8}{21}$   $\frac{7.7}{28}$   $\frac{7.8}{50}$

(48)

$\frac{7.7}{50}$   $\frac{7.5}{27}$   $\frac{5.0}{20}$   $\frac{4.7}{20}$   $\frac{4.7}{20}$   $\frac{6.8}{25}$   $\frac{7.0}{50}$

+ 15 Bay Ditch Rt.

+ 30 Bay Ditch Rt.

Sta	+	HI	-	Elev
758		892.23		48
	+50			48
759				48
	+50			48
760				49
761				50
762				52
T.P.	2.81	890.49 ✓	4.55	887.68 ✓
B.M.	4.09	890.75 ✓	3.88	886.61 ✓
763				886-66
	+40			
764				
	+50			
765				

10/21/27 / 11/2/27 K.P.

$\frac{57}{50}$

$\frac{72}{47}$

$\frac{77}{27.5}$

$\frac{48}{20}$

48

$\frac{50}{20}$

$\frac{75}{26}$

$\frac{76}{46}$

$\frac{59}{50}$

48

$\frac{57}{50}$

$\frac{74}{47}$

$\frac{71}{28}$

$\frac{50}{21}$

50

$\frac{50}{20}$

$\frac{83}{27}$

$\frac{80}{44}$

$\frac{41}{50}$

48

$\frac{61}{50}$

$\frac{77}{47}$

$\frac{75}{27}$

$\frac{50}{20}$

50

$\frac{57}{20}$

$\frac{80}{27}$

$\frac{81}{44}$

$\frac{26}{50}$

48

$\frac{72}{50}$

$\frac{84}{47}$

$\frac{84}{30}$

$\frac{57}{20}$

57

$\frac{54}{21}$

$\frac{84}{27.5}$

$\frac{84}{46}$

$\frac{60}{50}$

49

$\frac{66}{50}$

$\frac{87}{47}$

$\frac{87}{27}$

$\frac{52}{26}$

57

$\frac{57}{20}$

$\frac{92}{30}$

$\frac{92}{44}$

$\frac{84}{46}$

$\frac{57}{50}$

50

$\frac{60}{50}$

$\frac{94}{44}$

$\frac{91}{27}$

$\frac{57}{20}$

57

$\frac{53}{20.5}$

$\frac{87}{28}$

$\frac{78}{44}$

$\frac{26}{51}$

52

$\frac{48}{50}$

$\frac{88}{43.5}$

$\frac{86}{27}$

$\frac{55}{20}$

53

$\frac{54}{20}$

$\frac{90}{28.5}$

$\frac{88}{39}$

$\frac{02}{50}$

spike in 24' OAB 75' at 57 769+60

48

78

80

41

40

29

79

02

57

45

30

20

20

29

39

50

42

27

30

48

21

27

80

24

50

44

29

20

21

30

42

51

42

$\frac{46}{50}$

$\frac{82}{45}$

$\frac{82}{30}$

$\frac{42}{21}$

42

$\frac{42}{20}$

$\frac{82}{28.5}$

$\frac{82}{41}$

$\frac{28}{51}$

43

$\frac{36}{50}$

$\frac{78}{44}$

$\frac{78}{30}$

$\frac{46}{20}$

47

$\frac{43}{21}$

$\frac{78}{28.5}$

$\frac{80}{41.5}$

$\frac{28}{51}$

43

$\frac{30}{57}$

$\frac{80}{42}$

$\frac{82}{37}$

$\frac{74}{29}$

$\frac{48}{20}$

47

$\frac{47}{20}$

$\frac{85}{31}$

$\frac{83}{42}$

$\frac{35}{57}$

Sta

+

HI

-

Elev

890.75 ✓

766

+30

767

768

769

+16

+25

+50

+68

+83

770

TP

4.48

889.08 ✓

6.15

887.60 ✓

+50

11/2/27

40  
 $\frac{42}{57}$   $\frac{81}{74}$   $\frac{84}{31}$   $\frac{45}{20}$  40  $\frac{56}{20}$   $\frac{83}{29}$   $\frac{86}{43}$   $\frac{48}{50}$

41  
 $\frac{45}{51}$   $\frac{84}{45}$   $\frac{84}{30}$   $\frac{46}{20}$  41  $\frac{47}{20}$   $\frac{84}{29}$   $\frac{86}{44}$   $\frac{53}{50}$

45  
 $\frac{58}{51}$   $\frac{88}{45}$   $\frac{86}{29}$   $\frac{47}{20}$  45  $\frac{48}{20}$   $\frac{86}{28}$   $\frac{88}{44}$   $\frac{55}{50}$

50  
 $\frac{56}{50}$   $\frac{88}{43.5}$   $\frac{90}{29}$   $\frac{50}{21}$  50  $\frac{50}{20}$   $\frac{90}{29}$   $\frac{88}{44}$   $\frac{51}{50}$

52  
 $\frac{52}{57}$   $\frac{88}{43}$   $\frac{92}{28}$   $\frac{52}{21}$  52  $\frac{52}{20.5}$   $\frac{90}{28.5}$   $\frac{90}{44}$   $\frac{52}{50}$

52  
 $\frac{52}{57}$   $\frac{90}{43}$   $\frac{92}{28}$   $\frac{52}{21.5}$  52  $\frac{52}{25}$   $\frac{90}{34}$   $\frac{90}{38}$   $\frac{63}{44}$   $\frac{42}{48}$   $\frac{42}{50}$   
 +16 E.D.

52  
 $\frac{48}{57}$   $\frac{90}{44}$   $\frac{90}{30}$   $\frac{52}{22.5}$  52  $\frac{52}{30}$   $\frac{60}{32}$   $\frac{70}{36}$   $\frac{51}{43}$   $\frac{40}{50}$

53  
 $\frac{52}{50}$   $\frac{51}{30}$  53  $\frac{48}{28}$   $\frac{44}{50}$

53  
 $\frac{52}{50}$   $\frac{53}{25}$  53  $\frac{53}{26}$   $\frac{72}{32}$   $\frac{72}{44}$   $\frac{36}{50}$

53  
 $\frac{48}{50}$   $\frac{85}{42}$   $\frac{92}{30}$   $\frac{88}{31}$   $\frac{56}{22}$  53  $\frac{54}{20}$   $\frac{82}{27}$   $\frac{94}{38}$   $\frac{88}{43}$   $\frac{32}{50}$

54  
 $\frac{50}{50}$   $\frac{90}{41}$   $\frac{93}{29}$   $\frac{55}{19}$  54  $\frac{55}{20}$   $\frac{94}{30}$   $\frac{92}{42}$   $\frac{31}{51}$

58  
 $\frac{33}{57}$   $\frac{78}{43}$   $\frac{78}{29}$   $\frac{40}{20}$  58  $\frac{38}{31}$   $\frac{76}{30}$   $\frac{77}{44}$   $\frac{26}{51}$

sta	+	HI	-	Elev.
		889.08		
771				
738				
772				
773				
774				
775				
776				
777				
778				
T.P.	2.19	885.00	6.27	882.81
779				
780				
B.M.	284	884.89	3.95	881.05
781				

11/2/27

39

$\frac{38}{50}$	$\frac{78}{43}$	$\frac{82}{30}$	$\frac{40}{20}$	40	$\frac{41}{21}$	$\frac{80}{50}$	$\frac{80}{44}$	$\frac{47}{50}$
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40

+20 Reg H.P.

$\frac{50}{50}$	$\frac{82}{45}$	$\frac{82}{28}$	$\frac{42}{20}$	41	$\frac{43}{21}$	$\frac{64}{18}$	$\frac{70}{32}$	$\frac{82}{33}$	$\frac{82}{37.5}$	$\frac{20}{39}$	$\frac{70}{50}$
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160 Reg H.P.

41

$\frac{73}{50}$	$\frac{73}{39}$	$\frac{86}{37.5}$	$\frac{86}{33.5}$	$\frac{68}{31.5}$	$\frac{68}{26.5}$	$\frac{42}{21}$	41	$\frac{42}{21.5}$	$\frac{66}{28}$	$\frac{73}{31.5}$	$\frac{88}{30}$	$\frac{88}{38}$	$\frac{22}{39}$	$\frac{72}{50}$
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42

$\frac{72}{50}$	$\frac{75}{39}$	$\frac{93}{38}$	$\frac{92}{33}$	$\frac{78}{52}$	$\frac{21}{28}$	$\frac{46}{22}$	45	$\frac{44}{22}$	$\frac{73}{28}$	$\frac{76}{32}$	$\frac{20}{33}$	$\frac{92}{37.5}$	$\frac{75}{39}$	$\frac{75}{50}$
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43

$\frac{93}{50}$	$\frac{90}{39}$	$\frac{98}{38}$	$\frac{98}{33}$	$\frac{80}{32}$	$\frac{75}{29}$	$\frac{48}{22}$	41	$\frac{50}{23}$	$\frac{77}{29}$	$\frac{78}{31}$	$\frac{75}{32}$	$\frac{95}{37}$	$\frac{78}{39}$	$\frac{78}{50}$
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51

$\frac{86}{50}$	$\frac{86}{39}$	$\frac{100}{38}$	$\frac{101}{33}$	$\frac{85}{31.5}$	$\frac{80}{28}$	$\frac{52}{22}$	52	$\frac{53}{23}$	$\frac{78}{28}$	$\frac{86}{31}$	$\frac{100}{32.5}$	$\frac{100}{38}$	$\frac{82}{39}$	$\frac{82}{50}$
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57

$\frac{88}{50}$	$\frac{90}{40}$	$\frac{105}{38}$	$\frac{104}{33}$	$\frac{90}{32}$	$\frac{82}{28}$	$\frac{57}{22}$	56	$\frac{56}{22}$	$\frac{84}{29}$	$\frac{87}{31}$	$\frac{110}{32.5}$	$\frac{108}{37}$	$\frac{90}{39}$	$\frac{88}{50}$
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63

$\frac{96}{50}$	$\frac{94}{40}$	$\frac{112}{38}$	$\frac{114}{32}$	$\frac{95}{32}$	$\frac{88}{29}$	$\frac{61}{22}$	62	$\frac{62}{23}$	$\frac{90}{30}$	$\frac{114}{32}$	$\frac{114}{28}$	$\frac{91}{39}$	$\frac{90}{50}$
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69

$\frac{100}{50}$	$\frac{100}{40}$	$\frac{120}{38.5}$	$\frac{118}{33}$	$\frac{100}{31}$	$\frac{91}{28}$	$\frac{72}{22.5}$	71	$\frac{71}{22.5}$	$\frac{90}{28.5}$	$\frac{95}{30}$	$\frac{120}{32}$	$\frac{118}{38}$	$\frac{90}{40}$	$\frac{90}{50}$
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5.4

$\frac{74}{50}$	$\frac{66}{40}$	$\frac{85}{38.5}$	$\frac{85}{33}$	$\frac{63}{31}$	$\frac{61}{29}$	$\frac{37}{32}$	36	$\frac{38}{22}$	$\frac{58}{29}$	$\frac{68}{31}$	$\frac{84}{33}$	$\frac{84}{37}$	$\frac{67}{39}$	$\frac{66}{50}$
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40

$\frac{75}{50}$	$\frac{75}{39}$	$\frac{87}{38}$	$\frac{88}{33}$	$\frac{78}{30}$	$\frac{75}{28.5}$	$\frac{43}{21}$	44	$\frac{45}{21.5}$	$\frac{70}{28}$	$\frac{70}{31}$	$\frac{87}{33}$	$\frac{87}{37}$	$\frac{73}{38.5}$	$\frac{73}{50}$
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2 Nails in 6" Birch 45' at 29 7787 75'

$\frac{82}{50}$	$\frac{80}{38}$	$\frac{92}{37}$	$\frac{92}{33}$	$\frac{82}{32}$	$\frac{75}{26}$	$\frac{51}{20.5}$	79	$\frac{52}{20.5}$	$\frac{70}{25}$	$\frac{81}{32}$	$\frac{95}{33}$	$\frac{80}{37.5}$	$\frac{80}{38.5}$	$\frac{80}{50}$
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45

274

+

MI

-

Flav

884.89

782

783

784

785

786

T.P.

162

878.15

3.36

876.53

B.M.

460

879.25

3.60

874.53

874.64

887+00

788

789

790

+30

791

+50

1/2/27  
CWS.  
DS  
CF  
K.P.

5.1

90	90	100	95	90	88	61	59	59	85	88	101	101	90	88
$\frac{90}{50}$	$\frac{90}{38}$	$\frac{100}{37}$	$\frac{95}{35}$	$\frac{90}{32}$	$\frac{88}{26}$	$\frac{61}{20}$	$\frac{59}{21}$	$\frac{59}{26}$	$\frac{85}{26}$	$\frac{88}{22}$	$\frac{101}{33}$	$\frac{101}{38}$	$\frac{90}{35}$	$\frac{88}{50}$

5.7

92	90	104	102	90	90	64	62	62	88	91	107	107	90	92
$\frac{92}{50}$	$\frac{90}{34}$	$\frac{104}{37}$	$\frac{102}{33}$	$\frac{90}{32}$	$\frac{90}{27}$	$\frac{64}{25}$	$\frac{62}{20}$	$\frac{62}{20}$	$\frac{88}{26}$	$\frac{91}{32}$	$\frac{107}{32}$	$\frac{107}{38}$	$\frac{90}{39}$	$\frac{92}{50}$

6.3

97	92	112	112	93	92	70	68	68	88	90	112	114	90	90
$\frac{97}{50}$	$\frac{92}{40}$	$\frac{112}{38}$	$\frac{112}{34}$	$\frac{93}{31}$	$\frac{92}{28}$	$\frac{70}{25}$	$\frac{68}{20}$	$\frac{68}{20}$	$\frac{88}{26}$	$\frac{90}{31}$	$\frac{112}{33}$	$\frac{114}{37}$	$\frac{90}{39}$	$\frac{90}{50}$

6.9

100	100	121	121	98	98	78	74	75	88	88	118	117	88	87
$\frac{100}{50}$	$\frac{100}{40}$	$\frac{121}{38}$	$\frac{121}{33}$	$\frac{98}{35}$	$\frac{98}{27}$	$\frac{78}{21}$	$\frac{74}{21}$	$\frac{75}{21}$	$\frac{88}{20}$	$\frac{88}{26}$	$\frac{118}{30}$	$\frac{117}{32}$	$\frac{88}{40}$	$\frac{87}{50}$

7.5

107	107	128	128	110	108	86	84	86	101	104	127	127	105	102
$\frac{107}{50}$	$\frac{107}{40}$	$\frac{128}{37}$	$\frac{128}{34}$	$\frac{110}{31}$	$\frac{108}{27}$	$\frac{86}{20}$	$\frac{84}{20}$	$\frac{86}{20}$	$\frac{101}{25}$	$\frac{104}{30}$	$\frac{127}{33}$	$\frac{127}{37}$	$\frac{105}{39}$	$\frac{102}{50}$

8.6

Spoke in stump.

56	58	77	75	57	55	38	38	40	54	56	72	71	56	53
$\frac{56}{50}$	$\frac{58}{39}$	$\frac{77}{35}$	$\frac{75}{31}$	$\frac{57}{31}$	$\frac{55}{27}$	$\frac{38}{20}$	$\frac{38}{20}$	$\frac{40}{21}$	$\frac{54}{27}$	$\frac{56}{31}$	$\frac{72}{32}$	$\frac{71}{38}$	$\frac{56}{40}$	$\frac{53}{50}$

8.3

66	68	78	78	61	66	51	51	51	62	66	75	75	63	63
$\frac{66}{50}$	$\frac{68}{38}$	$\frac{78}{37}$	$\frac{78}{32}$	$\frac{61}{31}$	$\frac{66}{26}$	$\frac{51}{20}$	$\frac{51}{20}$	$\frac{51}{20}$	$\frac{62}{24}$	$\frac{66}{31}$	$\frac{75}{32}$	$\frac{75}{38}$	$\frac{63}{40}$	$\frac{63}{50}$

4.5

76	76	86	90	74	74	59	59	60	64	62	86	88	60	60
$\frac{76}{50}$	$\frac{76}{38}$	$\frac{86}{35}$	$\frac{90}{35}$	$\frac{74}{32}$	$\frac{74}{25}$	$\frac{59}{20}$	$\frac{59}{20}$	$\frac{60}{20}$	$\frac{64}{25}$	$\frac{62}{25}$	$\frac{86}{31}$	$\frac{88}{39}$	$\frac{60}{35}$	$\frac{60}{50}$

5.5

+25 End H.D.

83	80	91	94	82	82	67	67	67	97	102	70	62		
$\frac{83}{50}$	$\frac{80}{37}$	$\frac{91}{36}$	$\frac{94}{31}$	$\frac{82}{29}$	$\frac{82}{27}$	$\frac{67}{20}$	$\frac{67}{20}$	$\frac{67}{20}$	$\frac{97}{30}$	$\frac{102}{41}$	$\frac{70}{45}$	$\frac{62}{50}$		

+100 End H.D.

5.8

83	78	92	95	83	70	70	70	70	105	105	70	66		
$\frac{83}{50}$	$\frac{78}{36}$	$\frac{92}{34}$	$\frac{95}{30}$	$\frac{83}{28}$	$\frac{70}{21}$	$\frac{70}{21}$	$\frac{70}{20}$	$\frac{70}{20}$	$\frac{105}{29}$	$\frac{105}{38}$	$\frac{70}{44}$	$\frac{66}{50}$		

6.8

87	77	105	100	102	80	78	80	80	107	112	77	72		
$\frac{87}{50}$	$\frac{77}{36}$	$\frac{105}{33}$	$\frac{100}{39}$	$\frac{102}{27}$	$\frac{80}{21}$	$\frac{78}{21}$	$\frac{80}{20}$	$\frac{80}{20}$	$\frac{107}{28}$	$\frac{112}{38}$	$\frac{77}{45}$	$\frac{72}{50}$		

7.4

94	81	110	110	101	84	84	84	84	114	112	82	77		
$\frac{94}{50}$	$\frac{81}{36}$	$\frac{110}{33}$	$\frac{110}{35}$	$\frac{101}{27}$	$\frac{84}{21}$	$\frac{84}{21}$	$\frac{84}{21}$	$\frac{84}{21}$	$\frac{114}{30}$	$\frac{112}{41}$	$\frac{82}{47}$	$\frac{77}{50}$		

54

+

HI

-

Elco

879.25

792

+50

T.P.

1.57

872.82

8.00

871.25

793

794

795

796

+50

+77

T.P.

5.99

866.84

11.97

860.85

797

+50

798

799

11/3/27

100 B+ HD

8.1

$\frac{106}{50}$	$\frac{107}{36}$	$\frac{117}{34}$	$\frac{116}{29.5}$	$\frac{85}{24.5}$	$\frac{90}{21}$	$\frac{88}{21}$	$\frac{90}{21}$	$\frac{118}{27}$	$\frac{120}{42}$	$\frac{87}{48}$	$\frac{87}{50}$
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+50 B+ HD

8.7

$\frac{113}{50}$	$\frac{112}{36}$	$\frac{120}{21}$	$\frac{124}{30}$	$\frac{118}{28}$	$\frac{117}{25}$	$\frac{95}{21}$	$\frac{91}{21}$	$\frac{96}{24}$	$\frac{104}{26}$	$\frac{124}{30}$	$\frac{124}{34}$	$\frac{85}{38}$	$\frac{91}{50}$
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2.9

$\frac{53}{50}$	$\frac{52}{36}$	$\frac{66}{34}$	$\frac{66}{30}$	$\frac{54}{27}$	$\frac{48}{24}$	$\frac{37}{29.5}$	$\frac{37}{21.5}$	$\frac{50}{25}$	$\frac{51}{27}$	$\frac{61}{29}$	$\frac{62}{34}$	$\frac{50}{36}$	$\frac{46}{50}$
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4.2

$\frac{61}{50}$	$\frac{58}{37}$	$\frac{26}{33}$	$\frac{29}{30}$	$\frac{60}{26}$	$\frac{57}{24}$	$\frac{44}{20}$	$\frac{44}{21}$	$\frac{45}{21}$	$\frac{51}{24}$	$\frac{57}{21}$	$\frac{75}{29}$	$\frac{75}{33}$	$\frac{53}{38}$	$\frac{51}{50}$
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+50 B D.12h

5.5

$\frac{80}{48}$	$\frac{80}{46}$	$\frac{87}{32}$	$\frac{91}{33}$	$\frac{90}{28}$	$\frac{74}{26}$	$\frac{22}{25}$	$\frac{52}{20}$	$\frac{85}{21}$	$\frac{57}{24}$	$\frac{70}{25}$	$\frac{73}{29.5}$	$\frac{97}{32}$	$\frac{71}{36}$	$\frac{74}{50}$
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+50 B D.12h

6.7

$\frac{80}{58}$	$\frac{86}{48}$	$\frac{121}{42}$	$\frac{133}{44}$	$\frac{133}{35}$	$\frac{105}{30}$	$\frac{103}{28}$	$\frac{77}{27}$	$\frac{66}{20}$	$\frac{66}{21}$	$\frac{83}{22}$	$\frac{86}{29}$	$\frac{122}{33}$	$\frac{122}{36}$	$\frac{86}{40}$	$\frac{84}{50}$
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7.2

$\frac{90}{50}$	$\frac{122}{42}$	$\frac{136}{41}$	$\frac{136}{36}$	$\frac{71}{21}$	$\frac{71}{21}$	$\frac{71}{21}$	$\frac{92}{26}$	$\frac{95}{29}$	$\frac{133}{30}$	$\frac{133}{38}$	$\frac{94}{40}$	$\frac{70}{50}$
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7.4

$\frac{85}{50}$	$\frac{140}{42}$	$\frac{140}{34}$	$\frac{127}{33}$	$\frac{74}{20}$	$\frac{72}{21}$	$\frac{76}{21}$	$\frac{103}{26}$	$\frac{107}{29}$	$\frac{137}{31}$	$\frac{137}{35}$	$\frac{101}{39}$	$\frac{97}{50}$
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16

$\frac{24}{57}$	$\frac{34}{48}$	$\frac{83}{41}$	$\frac{82}{34}$	$\frac{15}{20}$	$\frac{15}{20}$	$\frac{18}{21.5}$	$\frac{50}{27}$	$\frac{52}{30}$	$\frac{74}{31}$	$\frac{80}{38.5}$	$\frac{50}{39}$	$\frac{43}{50}$
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2.0

$\frac{47}{54}$	$\frac{22}{44}$	$\frac{88}{43.5}$	$\frac{90}{36}$	$\frac{68}{35}$	$\frac{21}{20}$	$\frac{21}{20}$	$\frac{22}{21.5}$	$\frac{52}{29}$	$\frac{55}{31}$	$\frac{88}{39.5}$	$\frac{80}{37}$	$\frac{57}{39}$	$\frac{57}{50}$
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2.4

$\frac{97}{50}$	$\frac{95}{45}$	$\frac{85}{43}$	$\frac{97}{42}$	$\frac{96}{27}$	$\frac{92}{36}$	$\frac{93}{33}$	$\frac{30}{20.5}$	$\frac{38}{21}$	$\frac{31}{21}$	$\frac{66}{28}$	$\frac{72}{32}$	$\frac{87}{34}$	$\frac{87}{36}$	$\frac{75}{38}$	$\frac{65}{50}$
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+60 B7 D.12h

3.2

$\frac{110}{50}$	$\frac{91}{33}$	$\frac{40}{20}$	$\frac{37}{21}$	$\frac{37}{21}$	$\frac{75}{28}$	$\frac{82}{32}$	$\frac{84}{33}$	$\frac{84}{37}$	$\frac{84}{37}$	$\frac{77}{38}$	$\frac{80}{50}$
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Sta + H I - Elev

866.84 ✓

+42

800+00

T.P. B.M.

645

867.00 ✓

5.99

860.85 ✓

801

802

803

+62

804

+60

805

T.P.

923

858.05 ✓

7.45

857.85 ✓

806

+50

B.M.

851.07

807

10/4/27

+50 Beg H.D.

3.6

100	96	120	98	93	94	44	42	38	26	20	84	84	20	66
50	40	39	36	35	33	21		20	28	32	33	36	37	50

1

40

23	64	28	88	90	27	28	17	50	41	63	60	74	23	58	55
50	40	36	35	32	31	26	20		20	27	30	32	36	37	50

+50 End H.D.

North End Cul Rt 274 777490.

72	88	85	71	41	47	80	81	54	59
36	35	27	21.5		23	30	32	35	50

5.3

6.1

63	96	94	78	64	56	84	84	40
37	31	27	22		20	30	32	38

6.9

63	108	102	86	70	60	90	90	43
39	32	26	22		20	27	32	39.5

7.6

83	85	106	112	92	38	62	88	88	50	26
50	39	32	28	22		21	27	31	44	50

8.1

98	91	114	114	98	82	70	92	94	34	26
50	36	32	27	22		21	25	32	41	50

9.3

126	122	130	128	110	96	84	104	104	54	44
50	34	38	27	23		20	28	32	40	50

10.1

137	130	135	133	117	102	90	110	110	71	50
50	33	32	27	22		20	26.5	30	39	50

5.3

+100 806 Beg H.D.

77	63	72	20	50	36	24	50	61	61	50	32	22
50	33	31	29	22		20	27	28	30	30.5	33.5	50

+50 End Ditch Lt.

4.5

100		90	62		51	37	74	77	68	50	41
50		30	22			20	29	32	34	35	50

5.7

130	125	75		62	48	86	90	97	100	78	65
50	36	24			20	28	31	32	36	38	50

211

+

HI

-

Elev

858.08 ✓

807+17

+50

808

+44

+66

B.M.

346

854.53 ✓

203

851.06<sup>-</sup> = 851.07 ✓

+98

809

+06

+14

T.P.

683

857.47 ✓

389

859.62 ✓

+42

+55

810

10/4/27

6!

$\frac{12.4}{50}$	$\frac{130}{38}$	$\frac{78}{25}$	$\frac{66}{55}$	$\frac{102}{29}$	$\frac{10.1}{32}$	$\frac{11.4}{33}$	$\frac{108}{37}$	$\frac{9.3}{38}$	$\frac{78}{50}$
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7!

$\frac{148}{50}$	$\frac{142}{32}$	$\frac{82}{25}$	$\frac{6.1}{20}$	$\frac{100}{27}$	$\frac{105}{29}$	$\frac{114}{31}$	$\frac{117}{34}$	$\frac{132}{35}$	$\frac{132}{39}$	$\frac{108}{41}$	$\frac{103}{50}$
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7.6

$\frac{145}{50}$	$\frac{139}{34}$	$\frac{88}{25}$	$\frac{80}{21}$	$\frac{6.7}{28}$	$\frac{100}{36}$	$\frac{132}{38}$	$\frac{142}{41}$	$\frac{126}{43}$	$\frac{122}{50}$
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7.9

$\frac{130}{50}$	$\frac{124}{40}$	$\frac{148}{33}$	$\frac{88}{24}$	$\frac{84}{20}$	$\frac{80}{26}$	$\frac{150}{32}$	$\frac{160}{50}$
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8.0

$\frac{8.7}{50}$	$\frac{95}{21}$	$\frac{85}{20}$	$\frac{100}{35}$	$\frac{96}{50}$
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to p slab 3W Cor R+sta 809+42

$\frac{1.7}{19}$	$\frac{4.7}{15}$	$\frac{50}{15}$	$\frac{25}{19}$
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+122

$\frac{1.7}{19}$	$\frac{4.6}{15}$	$\frac{51}{15}$	$\frac{26}{19}$
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+126

$\frac{1.0}{19}$	$\frac{4.5}{15}$	$\frac{52}{15}$	$\frac{25}{19}$
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+129

$\frac{1.5}{19}$	$\frac{4.6}{15}$	$\frac{52}{15}$	$\frac{26}{19}$
------------------	------------------	-----------------	-----------------

+122

8.2

$\frac{50}{50}$	$\frac{56}{24}$	$\frac{80}{18}$	$\frac{83}{20}$	$\frac{7.3}{26}$	$\frac{5.3}{31}$	$\frac{5.8}{32}$	$\frac{7.7}{25}$	$\frac{7.7}{50}$
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8.3

$\frac{85}{50}$	$\frac{85}{35}$	$\frac{80}{25}$	$\frac{85}{23}$	$\frac{82}{27}$	$\frac{82}{19}$	$\frac{7.5}{24}$	$\frac{9.5}{24}$	$\frac{7.6}{32}$	$\frac{10.7}{40}$	$\frac{14.2}{50}$
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+ 59809 Ditch

8.5

$\frac{8.7}{50}$	$\frac{80}{40}$	$\frac{112}{37}$	$\frac{114}{29}$	$\frac{84}{20}$	$\frac{84}{19}$	$\frac{118}{28}$	$\frac{118}{31}$	$\frac{9.3}{36}$	$\frac{11.6}{46}$	$\frac{13.3}{15}$
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+ 55809 Ditch

Sta + H I - Elev.

857.47

+80

811+00

+37

+58

+70

T.P.

11.4

862.78

638

857.09

T.P.

5.88

868.47

0.19

862.59

808+98

809+00

+06

+14

T.P.

0.43

863.02

588

862.59

B.M.

11.93

857.09

857.09

8.9

$\frac{6.4}{50}$   $\frac{6.5}{41}$   $\frac{10.7}{32}$   $\frac{10.7}{26}$   $\frac{8.7}{20}$   $\frac{8.8}{20}$   $\frac{11.2}{24}$   $\frac{10.6}{29}$   $\frac{7.5}{31}$   $\frac{8.6}{50}$

9.0

$\frac{4.7}{50}$   $\frac{4.7}{41}$   $\frac{10.8}{33}$   $\frac{11.0}{26}$   $\frac{9.8}{20}$   $\frac{8.8}{20}$   $\frac{10.8}{24}$   $\frac{10.7}{29}$   $\frac{6.1}{36}$   $\frac{6.6}{50}$

9.1

$\frac{2.3}{50}$   $\frac{1.8}{43}$   $\frac{10.4}{31}$   $\frac{10.6}{25}$   $\frac{9.2}{20}$   $\frac{9.2}{20}$   $\frac{9.1}{20}$   $\frac{10.8}{25}$   $\frac{10.6}{30}$   $\frac{4.8}{38}$   $\frac{4.1}{47}$   $\frac{4.0}{50}$

9.3

$\frac{2.7}{50}$   $\frac{2.0}{41}$   $\frac{10.0}{29}$   $\frac{10.2}{22}$   $\frac{9.1}{19}$   $\frac{9.1}{20}$   $\frac{9.8}{20}$   $\frac{10.7}{24}$   $\frac{10.5}{32}$   $\frac{3.3}{41}$   $\frac{2.6}{50}$

9.4

$\frac{2.3}{50}$   $\frac{1.4}{40}$   $\frac{9.8}{29}$   $\frac{10.2}{22}$   $\frac{9.0}{19}$   $\frac{9.1}{20}$   $\frac{9.5}{21}$   $\frac{10.6}{25}$   $\frac{10.6}{31}$   $\frac{2.7}{42}$   $\frac{2.2}{50}$

11.0

$\frac{1.8}{50}$   $\frac{1.7}{31.9}$   $\frac{9.4}{31.9}$

1.5

$\frac{10.0}{31.6}$   $\frac{2.0}{31.6}$   $\frac{2.1}{50}$

$\frac{0.9}{50}$   $\frac{0.8}{31.9}$   $\frac{9.5}{31.9}$

1.4

$\frac{10.1}{31.6}$   $\frac{1.5}{31.6}$   $\frac{1.2}{50}$

$\frac{0.5}{50}$   $\frac{1.2}{31.9}$   $\frac{9.6}{31.9}$

1.1

$\frac{10.1}{31.6}$   $\frac{1.5}{31.6}$   $\frac{1.3}{50}$

$\frac{1.8}{50}$   $\frac{1.7}{31.9}$   $\frac{9.7}{31.9}$

1.8

$\frac{10.2}{31.6}$   $\frac{1.5}{31.6}$   $\frac{2.1}{50}$

✓ Cor stab

Sta	+	HI	-	Elev
B.M.	518	852.62		847.44

813+00

...  
+22



+36

+63

814

+41

815

+50

816

817

+50

818

✓

$$\begin{array}{ccc} \sqrt{56} & \sqrt{58} & \sqrt{50} \\ 32 & 21 & 19 \end{array} \quad \sqrt{48} \quad \sqrt{50} \quad \sqrt{50} \\ 20 \quad 30$$

(49)

$$\begin{array}{ccc} \sqrt{58} & 60 & \sqrt{53} \\ 32 & 21 & 20 \end{array} \quad \sqrt{50} \quad \sqrt{50} \quad \sqrt{56} \quad \sqrt{58} \\ 20 \quad 19 \quad 21 \quad 31$$

(56)

$$\begin{array}{ccc} 62 & 62 & \sqrt{51} \\ 30 & 24 & 20 \end{array} \quad \sqrt{51} \quad \sqrt{51} \quad 62 \quad 61 \\ 20 \quad 21 \quad 30$$

(50)

$$\begin{array}{ccc} 60 & 61 & \sqrt{51} \\ 31 & 23 & 21 \end{array} \quad \sqrt{51} \quad \sqrt{51} \quad 65 \quad 62 \\ 22 \quad 23 \quad 30$$

(50)

$$\begin{array}{ccc} 65 & 65 & \sqrt{51} \\ 30 & 23 & 20 \end{array} \quad \sqrt{51} \quad \sqrt{51} \quad 64 \quad 62 \\ 20 \quad 23 \quad 30$$

(50)

$$\begin{array}{ccc} 66 & 66 & \sqrt{50} \\ 32 & 23 & 20 \end{array} \quad \sqrt{52} \quad \sqrt{53} \quad 66 \quad 66 \\ 20 \quad 23 \quad 32$$

(51)

$$\begin{array}{ccc} 68 & 68 & \sqrt{50} \\ 33 & 24 & 20 \end{array} \quad \sqrt{52} \quad \sqrt{52} \quad 68 \quad 68 \\ 20 \quad 24 \quad 30$$

(52)

$$\begin{array}{ccc} 63 & 68 & 48 \\ 33 & 24 & 20 \end{array} \quad \sqrt{52} \quad \sqrt{53} \quad 72 \quad 72 \\ 20 \quad 25 \quad 30$$

(52)

$$\begin{array}{ccc} 68 & 64 & 49 \\ 33 & 24 & 20 \end{array} \quad \sqrt{53} \quad \sqrt{59} \quad 78 \quad 78 \\ 21 \quad 25 \quad 33$$

(53)

$$\begin{array}{ccc} 70 & 64 & 49 \\ 30 & 25 & 21 \end{array} \quad \sqrt{55} \quad \sqrt{61} \quad 82 \quad 82 \\ 20 \quad 25 \quad 31$$

(55)

$$\begin{array}{ccccccc} 21 & 22 & 70 & 51 & \sqrt{56} & 61 & 58 & 88 & 58 & 60 & 95 & 114 \\ 38 & 30 & 25 & 20 & 20 & 20 & 25 & 29 & 34 & 37 & 37 & 38 \end{array}$$

(56)

Sta

+

H I

-

Elev

~~852.62~~

T. P.

12.43

~~862.47~~

2.58

~~850.04~~

+22

+36

+63

814

+41

815

+50

816

817

+50

T. P.

1.50

~~857.54~~

12.43

~~850.04~~

818 +00

$$\frac{8.1}{57}$$

4.0

$$\frac{12}{42} \quad \frac{10}{48} \quad \frac{20}{50}$$

$$\frac{2.1}{57}$$

14.8

$$\frac{5.2}{43} \quad \frac{4.8}{50}$$

$$\frac{12}{57}$$

14.9

$$\frac{2.7}{48} \quad \frac{3.0}{50}$$

$$\frac{2.3}{57}$$

14.9

$$\frac{2.7}{49} \quad \frac{2.4}{50}$$

$$\frac{4.7}{52}$$

14.9

$$\frac{6.1}{47} \quad \frac{5.7}{50}$$

$$\frac{6.6}{50}$$

15.0

$$\frac{6.3}{46} \quad \frac{5.8}{50}$$

$$\frac{5.6}{50}$$

15.1

$$\frac{6.6}{46} \quad \frac{6.4}{50}$$

$$\frac{2.3}{50}$$

$$\frac{7.3}{47}$$

15.1

$$\frac{9.4}{44} \quad \frac{8.9}{50}$$

$$\frac{9.2}{50}$$

$$\frac{9.4}{42}$$

15.2

$$\frac{10.0}{43} \quad \frac{9.8}{50}$$

$$\frac{8.5}{50}$$

$$\frac{9.4}{46}$$

15.4

$$\frac{11.3}{40} \quad \frac{1.3}{50}$$

$$\frac{36}{50} \quad \frac{4.8}{47} \quad \frac{4.8}{45}$$

4.5

Sta

+

H Z  
51.5

-

E/ed.

+37

+51

+68

+74

+94

819+00

13 M.

3.83

251.27

4.11

847.43

847.44

820+00

+16

+64

+75

821+00

+65

Left

Right

$\frac{5.4}{50}$   $\frac{6.1}{41}$   $\frac{6.5}{29}$   $\frac{4.2}{20}$

$\frac{4.6}{20}$   $\frac{4.9}{20}$   $\frac{7.2}{26}$   $\frac{6.0}{29}$   $\frac{16.8}{50}$

$\frac{7.8}{50}$   $\frac{6.7}{48}$   $\frac{6.7}{35}$   $\frac{7.5}{30}$   $\frac{7.4}{27}$   $\frac{4.8}{21}$

$\frac{4.8}{20}$   $\frac{4.8}{23}$   $\frac{6.3}{26}$   $\frac{5.4}{29}$   $\frac{6.0}{41}$   $\frac{11.0}{50}$   $\frac{21.7}{73}$

$\frac{13.5}{50}$   $\frac{10.0}{45}$   $\frac{8.0}{37}$   $\frac{8.0}{28}$   $\frac{4.2}{21}$

$\frac{4.8}{20}$   $\frac{6.1}{23}$   $\frac{6.1}{27}$   $\frac{5.6}{29}$   $\frac{7.5}{50}$   $\frac{8.7}{61}$   $\frac{22.3}{84}$

$\frac{14.5}{50}$   $\frac{9.6}{38}$   $\frac{8.5}{30}$   $\frac{4.2}{22}$

$\frac{4.8}{19}$   $\frac{5.8}{22}$   $\frac{5.8}{27}$   $\frac{5.5}{30}$   $\frac{7.5}{50}$   $\frac{8.9}{65}$   $\frac{21.5}{85.80}$

$\frac{17.2}{42}$   $\frac{14.0}{40}$   $\frac{13.0}{37}$   $\frac{4.2}{22}$   $4.5$

$\frac{4.6}{18}$   $\frac{7.1}{50}$   $\frac{8.2}{60}$   $\frac{22.3}{71}$

$\frac{20.0}{50}$   $\frac{16.3}{42}$   $\frac{7.2}{26}$   $\frac{6.7}{20}$   $\frac{3.9}{17}$

$\frac{4.6}{20}$   $\frac{7.1}{20}$   $\frac{5.5}{27}$   $\frac{7.1}{50}$   $\frac{7.2}{53}$   $\frac{18.3}{64}$   $\frac{21.9}{78}$   $\frac{24.8}{86}$

$\frac{4.9}{26}$   $\frac{5.9}{20}$   $\frac{4.8}{4.4}$   $\frac{6.4}{20}$   $\frac{6.4}{25}$

11-5-27  
Crane

$\frac{5.6}{31}$   $\frac{4.2}{20}$   $\frac{5.0}{4.6}$   $\frac{6.5}{19}$   $\frac{6.5}{27}$

$\frac{7.7}{39}$   $\frac{5.7}{27}$   $\frac{4.6}{22}$   $\frac{5.5}{5.0}$   $\frac{6.7}{20}$   $\frac{7.7}{24}$   $\frac{7.7}{37}$

$\frac{7.1}{38}$   $\frac{5.5}{23}$   $\frac{4.6}{20}$   $\frac{5.6}{5.1}$   $\frac{6.7}{21}$   $\frac{8.1}{26}$   $\frac{8.1}{42}$

$\frac{7.2}{41}$   $\frac{6.1}{25}$   $\frac{4.7}{21}$   $\frac{5.5}{5.3}$   $\frac{6.6}{24}$   $\frac{8.5}{26}$   $\frac{8.5}{43}$

$\frac{7.4}{35}$   $\frac{6.1}{23}$   $\frac{5.0}{20}$   $\frac{6.2}{5.7}$   $\frac{6.7}{21}$   $\frac{7.0}{24}$   $\frac{8.3}{51}$   $\frac{9.1}{36}$   $\frac{9.1}{43}$

Sta.	+	H. I.	-	Elev.
		851.27		
822+00				
	+25			
	+75			
823+00				
	+44			
	+54			
	+65			
	+76			
824+00				
T.P.	1.71	840.33	12.65	838.62
820+00				
820+16				
820+64				

Left.

Right. 11-5-27

$\frac{7.7}{36}$	$\frac{6.8}{27}$	$\frac{4.8}{20}$	(5.4)	$\frac{6.1}{21}$	$\frac{6.9}{25}$	$\frac{8.3}{40}$
------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{7.4}{37}$	$\frac{6.2}{27}$	$\frac{5.0}{20}$	(5.4)	$\frac{6.0}{20}$	$\frac{7.1}{24}$	$\frac{7.7}{36}$
------------------	------------------	------------------	-------	------------------	------------------	------------------

$\frac{6.7}{52}$	$\frac{5.8}{23}$	$\frac{4.7}{20}$	(5.4)	$\frac{5.7}{20}$	$\frac{7.1}{27}$
------------------	------------------	------------------	-------	------------------	------------------

$\frac{6.5}{30}$	$\frac{5.5}{22}$	$\frac{4.6}{19}$	(5.3)	$\frac{5.5}{20}$	$\frac{6.3}{24}$
------------------	------------------	------------------	-------	------------------	------------------

	$\frac{9.5}{32}$	$\frac{4.6}{19}$	(5.2)	$\frac{5.3}{21}$	$\frac{13.4}{38}$	$\frac{15.8}{50}$
--	------------------	------------------	-------	------------------	-------------------	-------------------

$\frac{7.6}{50}$	$\frac{9.2}{39}$	$\frac{10.8}{32}$	$\frac{4.6}{19}$	(5.2)	$\frac{5.3}{21}$	$\frac{13.2}{38}$	$\frac{15.6}{50}$
------------------	------------------	-------------------	------------------	-------	------------------	-------------------	-------------------

$\frac{13.7}{50}$	$\frac{11.9}{36}$	$\frac{4.4}{20}$	(5.2)	$\frac{6.4}{20}$	$\frac{12.2}{34}$	$\frac{10.7}{41}$	$\frac{8.6}{50}$
-------------------	-------------------	------------------	-------	------------------	-------------------	-------------------	------------------

$\frac{13.5}{50}$	$\frac{13.0}{38}$	$\frac{4.4}{20}$	(5.1)	$\frac{5.4}{20}$	$\frac{10.6}{31}$	$\frac{10.4}{34}$	$\frac{8.8}{50}$
-------------------	-------------------	------------------	-------	------------------	-------------------	-------------------	------------------

$\frac{12.2}{50}$	$\frac{12.2}{38}$	$\frac{4.2}{20}$	(5.0)	$\frac{5.4}{20}$	$\frac{13.2}{35}$	$\frac{15.9}{50}$
-------------------	-------------------	------------------	-------	------------------	-------------------	-------------------

(46.1)	$\frac{4.2}{4.2}$	$\frac{5.2}{50}$	$\frac{5.6}{60}$
--------	-------------------	------------------	------------------

(46.0)	$\frac{5.2}{46}$	$\frac{6.3}{50}$
--------	------------------	------------------

(45.9)	$\frac{5.4}{51}$	$\frac{6.1}{54}$	$\frac{6.7}{59}$
--------	------------------	------------------	------------------

379.	+	H. I.	-	E/cv.
		840.33 ✓		
820 + 75				
821 + 00				
	5.26	840.86 ✓	4.73	835.60 ✓
821 + 65				
822 + 00				
822 + 25				
822 + 73				
823 + 00				
T.P.	11.56	848.69 ✓	3.73	837.13 ✓
B.M.	1.25	848.69 ✓	1.25	847.44 ✓
T.P.	1.27	837.64 ✓	12.32	836.37 ✓
820 + 00				
820 + 16				
820 + 64				
820 + 75				

Left.

Right

11-5-27

+5.8

$\frac{60}{55}$   $\frac{66}{60}$

+5.8

$\frac{67}{58}$   $\frac{95}{64}$   $\frac{96}{66}$

+5.1

$\frac{104}{60}$   $\frac{134}{70}$   $\frac{140}{80}$

+5.0

$\frac{93}{58}$   $\frac{93}{60}$   $\frac{84}{61}$   $\frac{66}{65}$

+5.0

$\frac{55}{48}$   $\frac{57}{53}$   $\frac{50}{60}$

+5.0

$\frac{50}{40}$   $\frac{48}{50}$

-5.1

$\frac{50}{40}$   $\frac{57}{46}$   $\frac{60}{50}$

11-7-27

$\frac{75}{58}$   $\frac{55}{49}$   $\frac{39}{44}$

+8.8

$\frac{66}{53}$   $\frac{51}{48}$

+8.5

$\frac{75}{60}$   $\frac{68}{55}$   $\frac{27}{50}$

+8.6

$\frac{97}{65}$   $\frac{87}{64}$   $\frac{74}{59}$   $\frac{13}{50}$

+8.5

Sta.	+	H. I.	-	Elev.
		837.64 ✓		
821+00				
T.P.	5.69	839.69 ✓	5.64	834.00 ✓
821+65				
822+00				
822+25				
822+73				
823+00				
823+44				
T.P.	12.32	851.30 ✓	0.71	838.98 ✓
B.M.	3.81	851.25 ✓	3.86	847.44 ✓
824+38				
824+83				
825+00				
825+33				

Left

Right.

11-7-27

$$\begin{array}{r} 8.8 \\ 63 \end{array} \quad \begin{array}{r} 7.8 \\ 60 \end{array} \quad \begin{array}{r} 5.3 \\ 59 \end{array}$$

+6.5

$$\begin{array}{r} 10.4 \\ 60 \end{array} \quad \begin{array}{r} 9.4 \\ 53 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array}$$

+6.3

$$\begin{array}{r} 9.2 \\ 58 \end{array} \quad \begin{array}{r} 8.8 \\ 53 \end{array} \quad \begin{array}{r} 6.6 \\ 50 \end{array}$$

+6.2

$$\begin{array}{r} 8.9 \\ 58 \end{array} \quad \begin{array}{r} 8.3 \\ 53 \end{array} \quad \begin{array}{r} 6.3 \\ 50 \end{array}$$

+6.2

$$\begin{array}{r} 10.1 \\ 55 \end{array} \quad \begin{array}{r} 8.4 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 45 \end{array}$$

+6.2

$$\begin{array}{r} 7.7 \\ 50 \end{array} \quad \begin{array}{r} 6.8 \\ 47 \end{array}$$

-6.3

$$\begin{array}{r} 0.0 \\ 50 \end{array} \quad \begin{array}{r} 2.3 \\ 43 \end{array} \quad \begin{array}{r} 1.6 \\ 39 \end{array}$$

-6.4

4.8

$$\begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 39 \end{array} \quad \begin{array}{r} 10.6 \\ 31 \end{array} \quad \begin{array}{r} 4.0 \\ 20 \end{array} \quad \begin{array}{r} 5.2 \\ 4.8 \end{array} \quad \begin{array}{r} 9.9 \\ 20 \end{array} \quad \begin{array}{r} 13.2 \\ 31 \end{array} \quad \begin{array}{r} 16.0 \\ 42 \end{array} \quad \begin{array}{r} 16.0 \\ 50 \end{array}$$

4.4

$$\begin{array}{r} 5.5 \\ 35 \end{array} \quad \begin{array}{r} 7.5 \\ 32 \end{array} \quad \begin{array}{r} 7.5 \\ 29 \end{array} \quad \begin{array}{r} 4.0 \\ 21 \end{array} \quad \begin{array}{r} 4.9 \\ 4.7 \end{array} \quad \begin{array}{r} 10.6 \\ 19 \end{array} \quad \begin{array}{r} 16.3 \\ 33 \end{array} \quad \begin{array}{r} 17.8 \\ 44 \end{array} \quad \begin{array}{r} 17.8 \\ 50 \end{array}$$

4.4

$$\begin{array}{r} 3.0 \\ 39 \end{array} \quad \begin{array}{r} 6.9 \\ 31 \end{array} \quad \begin{array}{r} 6.5 \\ 26 \end{array} \quad \begin{array}{r} 4.0 \\ 20 \end{array} \quad \begin{array}{r} 4.7 \\ 4.5 \end{array} \quad \begin{array}{r} 8.9 \\ 19 \end{array} \quad \begin{array}{r} 15.6 \\ 28 \end{array} \quad \begin{array}{r} 17.6 \\ 39 \end{array} \quad \begin{array}{r} 17.6 \\ 50 \end{array}$$

4.0

$$\begin{array}{r} 2.6 \\ 36 \end{array} \quad \begin{array}{r} 6.3 \\ 30 \end{array} \quad \begin{array}{r} 5.4 \\ 26 \end{array} \quad \begin{array}{r} 3.6 \\ 20 \end{array} \quad \begin{array}{r} 4.5 \\ 4.1 \end{array} \quad \begin{array}{r} 7.8 \\ 19 \end{array} \quad \begin{array}{r} 11.8 \\ 33 \end{array} \quad \begin{array}{r} 13.0 \\ 36 \end{array} \quad \begin{array}{r} 13.0 \\ 50 \end{array}$$

Sta.	+	H.I.	-	Elev.
		851.25		
825+65				
826+00				
T.P.	8.69	856.81	5.13	848.12
824+83				
825+00				
825+33				
825+65				
826+00				
827+00				
827+40				
828+00				
829+00				
829+50				

Left.

Right.

11-7-27

3.9

$\frac{20}{37}$   $\frac{5.9}{32}$   $\frac{5.3}{26}$   $\frac{3.4}{20}$

$\frac{4.5}{41}$   $\frac{6.5}{19}$   $\frac{7.5}{26}$   $\frac{4.4}{31}$   $\frac{9.1}{40}$   $\frac{9.1}{50}$

5.7

$\frac{2.0}{36}$   $\frac{6.3}{33}$   $\frac{5.7}{26}$   $\frac{2.0}{20}$

$\frac{4.5}{3.8}$   $\frac{6.3}{20}$   $\frac{6.5}{25}$   $\frac{4.2}{30}$   $\frac{3.4}{34}$

9.9

$\frac{1.7}{60}$   $\frac{1.6}{54}$

9.9

$\frac{1.7}{60}$   $\frac{1.5}{53}$

9.6

$\frac{2.0}{50}$   $\frac{2.2}{47}$

9.2

$\frac{2.1}{50}$   $\frac{2.4}{44}$

9.2

$\frac{2.1}{50}$   $\frac{2.1}{44}$

$\frac{1.9}{45}$   $\frac{1.8}{50}$

8.5

$\frac{2.6}{50}$   $\frac{2.6}{49}$   $\frac{10.3}{33}$   $\frac{10.2}{29}$   $\frac{8.2}{22}$

$\frac{9.2}{8.7}$   $\frac{10.9}{20}$   $\frac{11.0}{26}$   $\frac{2.7}{32}$   $\frac{2.8}{43}$   $\frac{2.8}{50}$

8.2

$\frac{2.5}{60}$   $\frac{2.6}{50}$   $\frac{8.6}{43}$   $\frac{10.1}{35}$   $\frac{10.2}{28}$   $\frac{7.8}{21}$

$\frac{8.7}{8.4}$   $\frac{10.4}{20}$   $\frac{10.4}{24}$   $\frac{2.7}{31}$   $\frac{2.7}{41}$   $\frac{2.7}{50}$

7.9

$\frac{3.7}{50}$   $\frac{3.8}{46}$   $\frac{8.5}{38}$   $\frac{9.8}{31}$   $\frac{9.4}{26}$   $\frac{7.3}{21}$

$\frac{8.6}{8.0}$   $\frac{9.8}{22}$   $\frac{9.8}{25}$   $\frac{4.9}{29}$   $\frac{3.5}{39}$   $\frac{3.3}{45}$   $\frac{3.3}{50}$

6.8

$\frac{5.3}{50}$   $\frac{4.7}{36}$   $\frac{8.8}{30}$   $\frac{8.8}{25}$   $\frac{6.6}{21}$

$\frac{7.8}{7.1}$   $\frac{9.0}{21}$   $\frac{9.0}{24}$   $\frac{3.6}{32}$   $\frac{3.3}{40}$   $\frac{3.3}{50}$

$\frac{3.7}{50}$   $\frac{5.1}{37}$   $\frac{7.7}{32}$   $\frac{7.7}{27}$   $\frac{5.9}{21}$

$\frac{7.0}{6.3}$   $\frac{8.4}{21}$   $\frac{8.3}{25}$   $\frac{3.9}{31}$   $\frac{3.8}{37}$   $\frac{3.8}{50}$

Sta.	-	H.I.	-	Elev.
		856.81		
830 +00				
T.P.	6.11	857.83	5.09	851.72
830 +21				
830 +43				
830 +71				
831 +00				
831 +47				
832 +00				
832 +23				
833 +00				
834 +00				
T.P.	8.49	863.33	2.99	854.84
835 +00				
836 +00				

Left.

Right.

11-7-27

29 20 5.2 5.7 51  
93 42 32 26 23

5.8 65 78 79 40 40  
20 24 29 34 50

46 44 48 51 59  
64 50 38 32 22

63 78 84 86 48 47  
21 25 31 35 50

48 46 5.2 5.5  
61 48 32 23

63 70 84 85 4.5 4.5  
20 25 30 36 50

48 48 5.4  
55 42 20

61 69 81 8.3 4.6 4.6  
21 25 30 37 50

50 47 5.2  
50 34 21

5.9 63 78 8.0 4.8 4.7  
20 24 31 35 50

39 51 5.4 4.6 4.6  
33 50 47 43 23

5.6 5.9 74 7.5 4.4 4.3  
20 25 31 35 50

32 33 7.4 6.7 4.6 4.4  
50 44 40 34 29 11

4.8 5.2 65 6.8 3.9 3.8  
21 25 30 37 50

3.9 2.9 3.0 6.7 6.7 4.9 4.4  
50 48 41 36 32 27 9

4.6 4.6 5.8 5.8 3.4 3.4  
20 26 31 37 50

2.9 4.7 2.7 5.9 6.1 4.0  
50 46 39 32 26 20

3.9 4.0 5.1 4.8 2.5 2.3  
20 30 32 37 50

0.3 2.3 3.0 5.1 5.2 3.1  
50 46 40 35 26 20

3.0 3.0 4.0 4.3 2.4 2.2  
20 25 31 37 50

50 55 8.2 8.8 7.7 7.5 7.6  
50 46 38 32 30 25 20

7.3 7.4 9.0 9.3 8.1 8.7  
20 25 28 31 50

4.8 5.3 7.4 100 9.3 9.1 6.8  
50 46 39 36 32 26 21

6.4 6.4 8.4 8.4 8.5 8.1  
22 27 30 32 50

Sta.	T	H. I.	-	Elev.
837+00		863.33 ✓		
837+84 <sup>L</sup>				
B.M.	4.49	862.52 ✓	5.30	858.03 ✓
T.P.	2.16	857.26 ✓	7.42	855.10 ✓
T.P.	2.48	850.59 ✓	9.15	848.11 ✓
B.M.			3.15	847.44 ✓

Left

Right.

11-7-27

4	56	84	64	87	87	55		57	76	80
70	42	37	33	30	26	21	5.2	21	28	50

37	35	5.1	37	34	75	78	45		44	74	72	59	49	58
50	43	40	37	33	29	25	19	4.1	30	27	30	34	44	50

SpK in 24" OqK 30 Rt. Std. 838 +00.

On Bridge.

Final x Sec of Channel Change  
 Right of Sta. 819 + 40.

Sta.	+	H.I.	-	Elev.
B.M.	1.42	848.86 ✓		847.44 ✓
T.P.	2.69	841.30 ✓	10.25	838.61 ✓
0+00				
0+22				
0+46				
0+54				
0+64				
0+78				
1+00				
1+29				
T.P.	2.91	836.71 ✓	7.50	833.80 ✓
1+75				
2+00				
2+22				
2+40				



Sta.	+	H. I.	-	Elev.
		836.71		
2+55				
3+00				
3+58				
3+70				
3+76				
T.P.	5.64	839.44	2.91	833.80
B.M.			7.33	832.11
				832.13

Final x Sec. of Channel  
Change Left Sta. 219+40.

B.M.	5.31	835.44		832.13
0+13				
0+31				
0+40				
0+50				
0+80				
1+00				
1+28				
1+42	Same as Original x Sec.			
B.M.			5.31	832.13

Left.

Right

11-9-27

3.5	3.0	3.6	2.5	1.00	1.10	(10.6)	11.0	10.0	7.8	4.4	5.2		
33	21	18	14	12	9	11.2	7	10	12	15	33		
	4.8	5.1	2.2	1.00	1.14	(10.4)	10.8	10.0	7.6	5.3	5.2		
	33	16	12	12	10	11.4	8	12	14	15	33		
7.5	9.9	6.8	6.2	8.4	10.0	11.2	(10.3)	10.8	9.7	8.4	4.7	4.1	4.4
33	24	22	17	16	13	10	10.8	6	11	14	16	22	33
		7.6	7.9	10.1	10.9	(10.1)	10.5	9.6	7.1	4.1	4.2	4.4	
		37	33	25	17	11.0	3	6	11	12	22	33	
		9.0	9.9	10.1	10.7	(10.7)	10.5	7.6	4.4	4.3			
		36	33	18	14	11.2	5	8	13	33			

11-8-27

		11.2	9.6	7.2	(10.3)	10.7	9.7						
		15	10	5	10.1	8	15						
		4.5	7.7	8.8	2.8	(10.4)	10.4	9.8	7.2	6.4			
		18	15	11	9	10.1	8	11	14	20			
2.9	3.6	6.0	8.0	8.9	2.5	(10.5)	9.9	7.9	7.4	6.5			
22	17	15	13	9	5	10.4	12	13	20	27			
		2.9	3.5	6.5	7.6	2.2	(10.5)	10.7	10.7	9.0	7.9	6.7	
		25	16	14	12	11	10.2	5	13	18	20	28	
4.6	4.7	7.1	7.0	7.8	8.7	10.4	(10.5)	11.7	11.9	11.3	7.0	6.5	5.7
33	29	27	23	17	14	11	11.1	3	7	11	13	20	33
7.5	8.0	9.0	10.5	11.2	12.0	10.1	(10.7)	6.7	6.1	6.1			
32	30	26	20	14	8	2	6.6	13	20	33			
6.5	8.0	10.7	11.0	11.3	9.7	8.5	7.3	6.2	6.6	8.3			
33	31	30	28	20	9	8	4	6.8	6	20	33		

839

838

+84 End of Div. C.

837

836

835

834

11-8-27



+84' Beg of  
24' Pavement

+38 Ref to  
Brick Yard.

+77 T.P. 37

+00 T.P. 26

+54 T.P. 28

834

833

832

831

830

829

11-8-27

95 T.P. 36

41 End of F. 45

F. 50

90 Cross Drain  
4" X 60" P<sup>2</sup>  
Extends 247' & 36' L.

68 T.P. 47

F. 68

4. Road 57  
F. 92

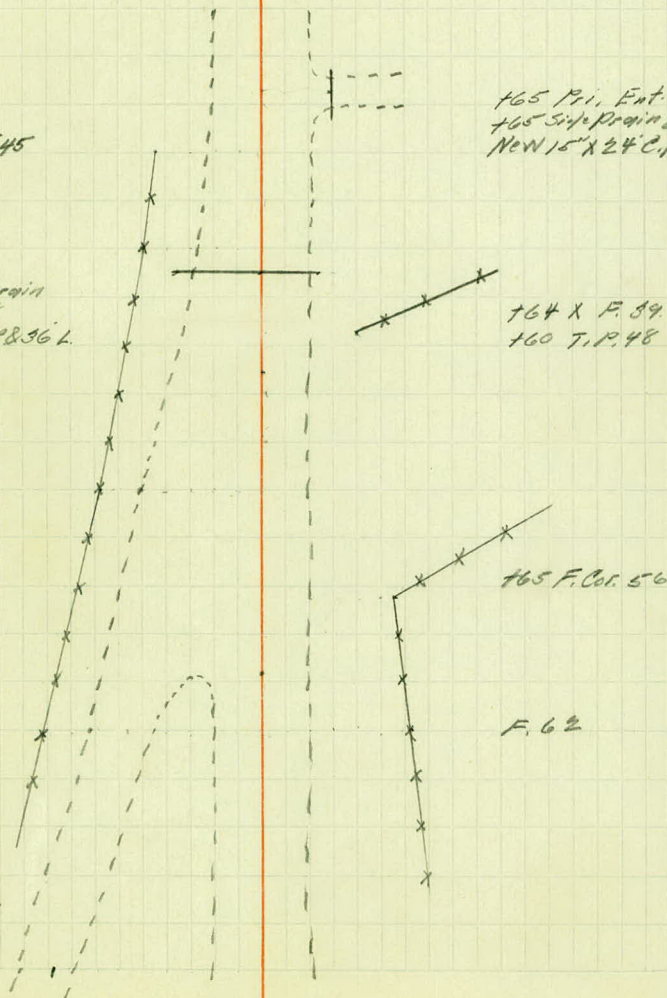
48 T.P. 55

165 Pri. Ent.  
165 Side Drain 88  
New 15" X 24" C.M.

164 X F. 89  
160 T.P. 48

165 F. Cor. 56

F. 62



829

828

827

826

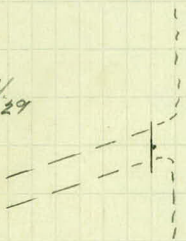
825

824

11-8-27

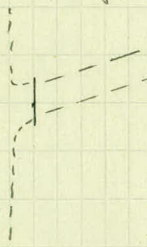
X. Road 88

19 Pri. Cross Hd.  
19 Side Drain 29  
New 15" x 24" C.M.

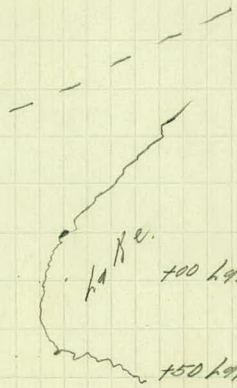
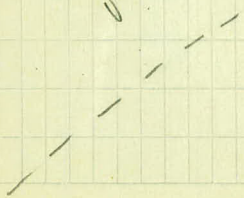


Cultivated

+59 Pri. X Road.  
+59 Side Drain 50  
New 15" x 24" C.M.



Cultivated



+100 Lake 60.

+150 Lake 57

824

823

822

821

820

819

818

817

816

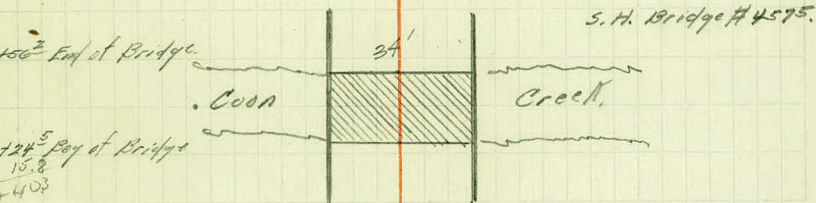
815

814

11-8-27

Woods & Brush

Woods & Brush



Woods & Brush

Woods & Brush

814

813

812

811

+69 E Privolt 15" X 24 CM.

+56 E Drive Rt 15" X 24 CM.

810.

+97 X Drain 24 X 48<sup>Ps</sup>

+05 under Pass G N

809

+30 Cattle Pass 6' X 10' X 48'

+03 E Drive Rt 18 X 36 CM.

808

807

+57 Beg Col 30

+44 Beg Col 32

11 13' 1 4' - 153. 13' 11  
+95.

+821

+8213-9 Col 41

ht sta 808+56 h

Drive Ways.

sta

+

HI

+

Elev

B.M.

3.61

852.67

851.07

+20

47.7

+37

47.7

+57

+83

ht sta 808+03

+20

+37

+41

+47

+75

50

$$\frac{112}{18}$$

$$\frac{51}{9}$$

59

$$\frac{50}{1}$$

$$\frac{48}{125}$$

$$\frac{20}{16}$$

70

$$\frac{95}{17}$$

$$\frac{63}{115}$$

$$\frac{60}{1}$$

$$\frac{56}{13}$$

$$\frac{25}{15}$$

70

$$\frac{98}{11}$$

$$\frac{72}{10}$$

$$\frac{70}{1}$$

$$\frac{60}{11}$$

$$\frac{25}{15}$$

51

$$\frac{38}{20}$$

$$\frac{32}{1}$$

$$\frac{29}{20}$$

59

$$\frac{115}{24}$$

$$\frac{102}{16}$$

$$\frac{38}{75}$$

$$\frac{38}{1}$$

$$\frac{40}{6}$$

$$\frac{90}{15}$$

$$\frac{95}{25}$$

60

$$\frac{128}{24}$$

$$\frac{104}{19}$$

$$\frac{100}{14}$$

$$\frac{41}{7}$$

$$\frac{42}{1}$$

$$\frac{42}{6}$$

$$\frac{176}{16}$$

$$\frac{114}{25}$$

65

$$\frac{98}{24}$$

$$\frac{96}{14}$$

$$\frac{47}{7}$$

$$\frac{47}{1}$$

$$\frac{47}{5}$$

$$\frac{90}{13}$$

$$\frac{78}{25}$$

60

$$\frac{94}{24}$$

$$\frac{84}{13}$$

$$\frac{40}{8}$$

$$\frac{60}{1}$$

$$\frac{60}{8}$$

$$\frac{72}{9}$$

$$\frac{62}{25}$$

$$+90 = 00$$

808

807

806

805

804

803

802

801

800

799

798

+90 1 Drain 20" X 66" P<sub>3</sub> 34 RT.  
32 Lt

797

796

795

794

793

792

+85 R Drive Lt '2" 15" X 24 C M<sub>1</sub>

791

790

Cont From Page 59

+ 73 Reg. Pueblo Cul 22'

24

+

HI

-

Elev

BM

5.45

880.10

874.65

789+00

+50

790+00

sta = 00

+50

+75

791+00

+50

792+00

+25

+50

apiko in stump 22' Rf of 392 100

same Original

same Original.

$\frac{29}{59}$     $\frac{22}{66}$     $\frac{43}{90}$     $\frac{41}{100}$

6.9

$\frac{76}{50}$     $\frac{73}{75}$     $\frac{73}{100}$     $\frac{76}{119}$     $\frac{70}{137}$     $\frac{22}{152}$

7.2

$\frac{77}{50}$     $\frac{21}{73}$     $\frac{22}{100}$     $\frac{75}{134}$     $\frac{68}{150}$     $\frac{30}{159}$     $\frac{32}{167}$

7.6

$\frac{81}{50}$     $\frac{26}{63}$     $\frac{73}{95}$     $\frac{74}{100}$     $\frac{72}{144}$     $\frac{20}{153}$     $\frac{41}{160}$

8.2

$\frac{85}{50}$     $\frac{27}{60}$     $\frac{27}{100}$     $\frac{71}{131}$     $\frac{61}{139}$     $\frac{47}{143}$     $\frac{47}{150}$

8.9

$\frac{92}{50}$     $\frac{24}{66}$     $\frac{84}{74}$     $\frac{85}{86}$     $\frac{88}{100}$     $\frac{80}{123}$     $\frac{63}{130}$     $\frac{73}{140}$

9.2

$\frac{98}{53}$     $\frac{96}{62}$     $\frac{96}{93}$     $\frac{95}{100}$     $\frac{93}{100}$     $\frac{70}{111}$     $\frac{78}{117}$     $\frac{82}{124}$

+ 37 End Cut.

$\frac{96}{50}$     $\frac{75}{76}$     $\frac{95}{100}$

Cont. Page 59

789

788

787

786

785

+17 & Drive Lt

" "  
(B) 15" X 24

784

783

782

781

780

779

778

777

776

775

774

773

+00 End Br & Timber

+00 End Brush

+10 Beg Brush

+00 Beg Brush

+05 Double Cut 36

+80 End Timber R4 & R5

+00 Timber R4 & R5

+22 XF 50' A 775 + 81

+45 XF 44' A + 81

772

771

770

+ 50% Foley Rd

30" X 42" B Pt  
30" X 42" B Wt

769

768

767

766

765

764

763

762

761

760

759

758

757

756

755

+60 E Timber

Low land

Timber

Low land

Timber

+30 End Timber

+34 Bag Cul 36

+23 + Bag Cul 35

Cultivated.

Cultivated.

+20 Bag Cultivation  
+20 End Timber

+85 Bag Cultivation  
+85 End Timber.

Timber

Timber

754

753

753 to o & Drive Lt.

752

751

750

749

748

747

746

745

744

743

742

741

741+00

790 Cattle Pass 4 X 6 X 50'

740

low land

Timber

low land

Timber

low land

F 65

+ 81 F 56

54

54

53

53

52

F 50

F 52

F 52

F 52

F 51

F 50

F 50

F 50

+ 88 F Cor 50 @ 45

739

738

737

736

735

440 E Drive 1st

15" X 24

734

733

732

731

730

729

728

726

725

724

723

722

721

720

28 Bagful 55'

400 End Timber

420 End Timber

400 Bag Timber

Lowland

470 End Timber

Timber

Timber

tos & Drive Rt.

604

603

602

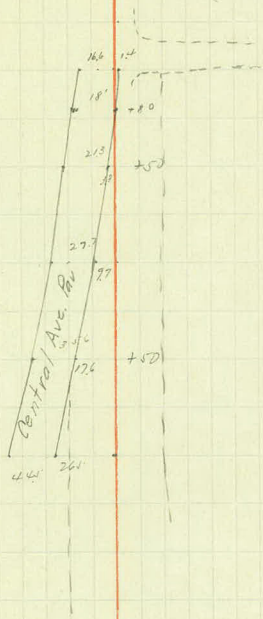
601

600

599

598

597



+19 MB 37'

+15 T.P 36'

+47 T.P 44'

Cultivated

Cultivated

596

595

594

593.

+95 X Drain

24" X 54' <sup>30.5 LT.</sup> 23.5 RT.

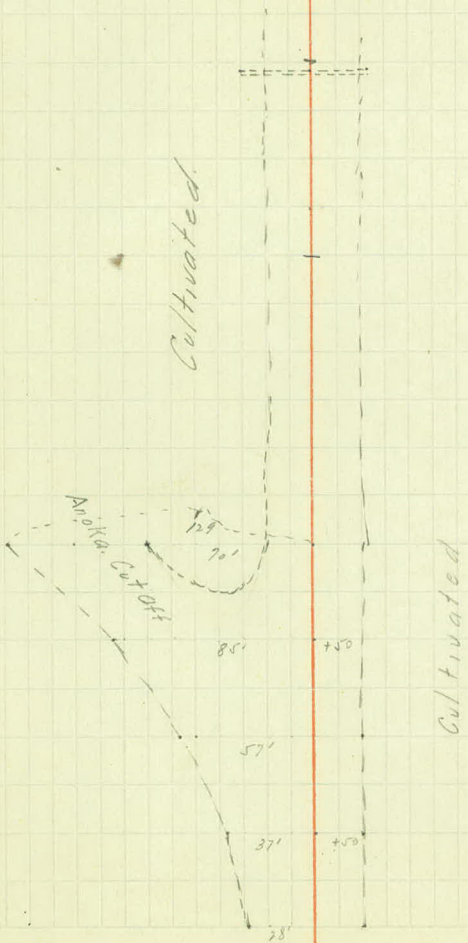
592

591

590+00

589+00

588+00



647

646

F 35'

F 33'

Timber



Timber

645

644

643

150 X Drain 24" X 60' Pa 30' Lt

31 Rt

642

641

+ 78 1/2 Drive Lt 15' X 24' C.M.

640

639

638

637

636

635

634

Cont. From Page 71.

F 23

F 62

Timber

+36 Bcg F. 34'

+52 Tr 39'  
+32 Tr 45'  
+16 Tr 41'  
F 57

F 52'

Pasture.

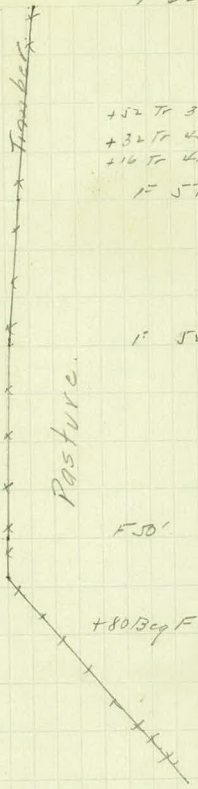
F 50'

+80 Bcg F 50' @ 642 +50

+66 Bcg Lot. 29'

Waste land

Waste land



Sta	+	H.I	-	Elev
B.M.	12.90	845.03 ✓		832.13
TP	9.43	852.06 ✓	2.40	842.63 ✓
TP	8.96	857.62 ✓	3.40	848.66 ✓

829+50

830

+20

+43

+71

831

+47

832

+23

833

(Copied by M.W.C.)  
5/23/27

CW 5  
DS  
H.B.  
T.M.

69  
6/14/27

Spk in 8' oak 55' Lt. sta 822+10

4.4/50 5.7/37 9.9/31 8.4/27 6.7/20 7.2 7.8/20 9.7/27 9.6/31 4.7/37 4.5/50

3.4/50 4.0/39 6.5/29 6.7/26 6.1/25 6.0/20 6.6 7.2/20 9.0/25 9.2/29 4.7/34 4.7/50

5.2/24 4.0/27 4.8/28 4.1/30 4.3/40 5.9/20 6.1 6.9/20 9.0/26 8.9/30 4.6/34 4.5/50

4.2/24 4.4/50 4.8/37 5.4/20 5.9/20 6.8 6.8/20 9.0/26 9.0/30 4.3/36 4.3/50

4.6/56 4.5/42 4.8/32 5.2/20 6.0 6.4/20 8.4/26 8.6/29 4.6/36 4.3/50

4.4/56 4.4/34 4.8/24 4.9/20 5.7 6.1/20 8.6/26 8.5/30 4.7/36 4.5/50

3.6/50 3.5/47 4.5/44 4.5/42 4.4/28 4.4/20 5.3 5.7/20 7.8/25 8.9/29 4.2/35 4.2/50

3.0/50 3.0/41 5.0/38 5.9/34 4.6/32 4.2/20 4.6 5.2/20 6.9/27 6.9/31 3.8/36 3.5/50

2.7/50 2.7/39 6.0/34 6.1/31 4.6/28 4.3 4.4/20 6.5/26 6.6/30 3.9/36 3.1/50

3.0/50 4.4/48 4.0/44 2.5/39 5.1/34 5.3/24 3.8/20 3.7 3.7/20 3.7/22 5.7/27 5.7/30 3.2/37 2.1/50

Sta	+	H.I.	-	Elev.
		857.62 ✓		
834				
T.P.	7.27	862.16 ✓	2.73	854.89 ✓
835				
836				
837				
+84				
B.M.			5.20	856.96 ✓
T.P.	2.24	857.13 ✓	7.27	854.89 ✓
T.P.	3.16	850.94 ✓	9.35	847.78 ✓
T.P.	2.51	845.15 ✓	8.30	842.64 ✓
B.M.			13.01	832.14 = 832.13

$\frac{0.4}{50}$   $\frac{2.0}{46}$   $\frac{2.8}{39}$   $\frac{4.9}{35}$   $\frac{4.9}{25}$   $\frac{2.8}{20}$   $\frac{2.8}{20}$   $\frac{2.6}{20}$   $\frac{5.4}{26}$   $\frac{5.3}{28}$   $\frac{2.0}{35}$   $\frac{2.0}{50}$

$\frac{4.4}{50}$   $\frac{4.7}{45}$   $\frac{5.1}{44}$   $\frac{8.0}{32}$   $\frac{8.5}{30}$   $\frac{8.5}{25}$   $\frac{6.5}{20}$   $\frac{5.8}{20}$   $\frac{6.1}{20}$   $\frac{8.6}{26}$   $\frac{8.6}{29}$   $\frac{7.0}{32}$   $\frac{7.4}{50}$

$\frac{4.4}{45}$   $\frac{5.0}{44}$   $\frac{6.2}{39}$   $\frac{9.0}{37}$   $\frac{8.0}{32}$   $\frac{8.0}{26}$   $\frac{5.5}{20}$   $\frac{4.8}{20}$   $\frac{5.2}{22}$   $\frac{7.2}{27}$   $\frac{7.3}{30}$   $\frac{7.1}{31}$   $\frac{6.9}{50}$

$\frac{3.0}{50}$   $\frac{3.6}{43}$   $\frac{7.2}{37}$   $\frac{5.2}{32}$   $\frac{4.4}{28}$   $\frac{8.0}{26}$   $\frac{4.4}{20}$   $\frac{4.0}{20}$   $\frac{4.3}{20}$   $\frac{6.4}{27}$   $\frac{6.7}{50}$

$\frac{5.5}{45}$   $\frac{2.5}{43}$   $\frac{4.0}{40}$   $\frac{2.3}{37}$   $\frac{2.2}{33}$   $\frac{6.0}{28}$   $\frac{6.0}{25}$   $\frac{3.4}{19}$   $\frac{2.9}{20}$   $\frac{3.1}{20}$   $\frac{6.2}{28}$   $\frac{6.2}{30}$   $\frac{4.7}{33}$   $\frac{4.6}{20}$

$\frac{2.5}{50}$   $\frac{2.6}{46}$

Spk. in 8" oak 55' Lt. 579 822+10

634

Topography. Cont. Page 68'

+49 x Drain

24" x 54" P<sub>3</sub>

27LT

28RT

633

632+00

631+00

630+00

629+00

628+00

627+00

626

625

624

623

622

621

620

619

618

617

616

615

614

22' +10  
48 287

Waste land



173 End FSI 'A 627+06

F 50

F 50

F 50

F 50

F 50

F 50

Pasture

F 50

Waste land

613 to 603 5th X Drain 24" X 54' P<sub>3</sub>

27 ft  
28 ft.

612

611

610

609

608

607

606

+80

X Drain

24" X 55' P<sub>3</sub>

28 ft  
29 ft.

605

604

603

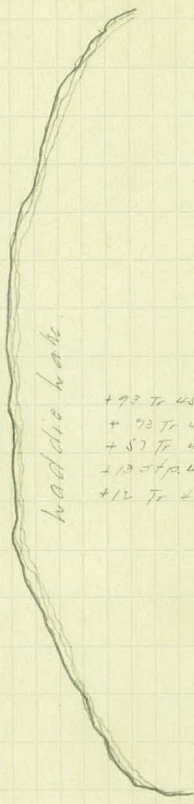
F50  
 E50  
 F50  
 F50  
 F50  
 +20 Tr 46'  
 F50  
 F50  
 F50  
 F50  
 F50  
 F50  
 F50  
 F50

Pasture & Small Trees



Waste land

haddie lake



haddie lake

+90 Tr 45'  
 +70 Tr 46'  
 +57 Tr 48'  
 +130 Tr 46'  
 +12 Tr 42'

602

601

600

599

598

597

+15 X Drain

20" 154<sup>E</sup> P<sub>3</sub>

596+00

+56 X Drain

24" 154 P<sub>3</sub>

28 ft.

26 ft.

595

594

3 Wmmp

+65 T 45

F50

F50

F50

Timber

+10 X Fence 50 @ 16'

+34 Cul 26'

+16 Rd 37 21

+88.5 Edge Pav

+63.5 Edge Pav

+73 M.B 33

+50 End Brush 45'

Big Brush 45'

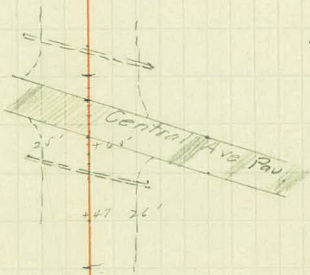
+25 Cul 26'

+90 TP 22'

+69 Pav 50'

+50 Pav 50'

+44 29 24



593

592

591

590

589

588

+30 @ Drive Lt.

15" X 24 CM.

+32 @ Drive Rt

15" X 24 CM.

587

Hayband

Was & Lead

Highway No 5  
Conn.

150

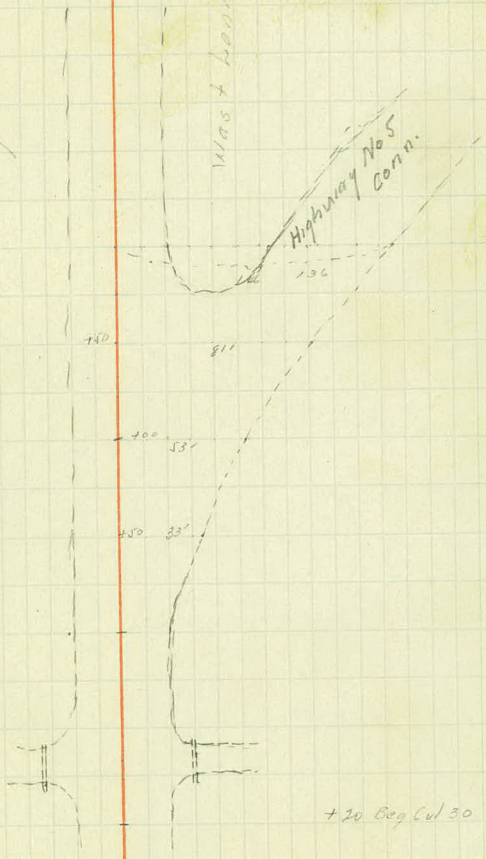
811

100 33'

150 33'

+18 Bog Cul 33'

+20 Bog Cul 30



586

585

584

583

582

581

580

+52 B Drive Rt.

+14 B Drive Lt

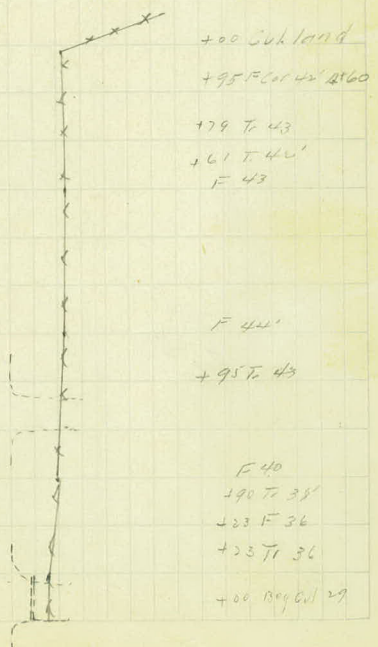
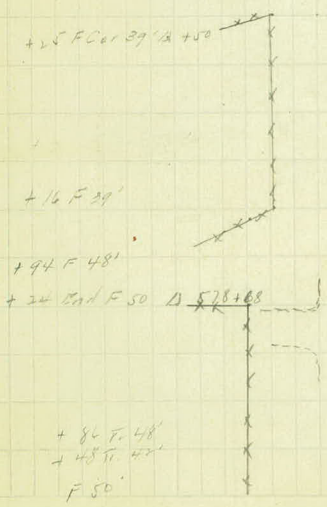
579

+12 Drive Rt.

15 x 24 CM.

578

Hayland



577

576

575

574

573

572

571

570

+ 69 X Drain

Rt 29'

Lt 31' 24" X 60' P<sub>3</sub>.

F 50

+50 T. 45'

F 50  
+92 T. 46

+65 T. 43

F 50

+86 T. 44

F 50'

+102 T. 39'

F 50'

+90 T. 40

+90 T. 46

+81 T. 39

+94 T. 44' 15"

F 49'

F 50

F 50

+97 T. 36

+84 T. 42'

+80 T. 36'

F 50

T. 41

F 53

+75 T. 47

+77 T. 48

+72 T. 41

+65 T. 44

+57 T. 44

+43 T. 39

+22 T. 47

+17 T. 36

F 50

+10 T. 48

+72 T. 40'

+46 T. 43'

+25 T. 43'

F 50'

+55 T. 38'

+75 T. 42

+48 T. 38'

+46 T. 43'

F 49.2

+24 T. 35'

+71 T. 41 F 50

+44 T. 39'

+90 T. 35'

+29 T. 46'

+26 T. 38

+20 T. 44

F 50

+53 T. 42 F. 50

+89 T. 40

+37 T. 44'

+31 T. 41'

+26 T. 48'

F 50'

F 50'

+36 T. 41'

+24 T. 44

76

101.

569

568

567

566

565

+87 & Drive Rt.

564

563

+02 B Drive Rt

15" x 24" CM.

562

F 50

+18 Tree 27'

F 50

+28 Tree 39'

F 50'

F 49.5

+25 F 26.49' @ +66

F 50

+96 T 36  
+87 T 32  
+82 T 42  
+80 T 48  
+74 T 50'

F 50

F 50

F 49.5

+20 Tree 46.5

+04 FC 49.5

+87

+02

+91 slip 48  
+97 slip 48  
+90 309 61 31'

BM	1.52	891.53		890.01
T.P.	0.70	890.00	2.23	889.30
729				
730				
731				
732				
BM			4.13	885.87
BM, Nail			4.09	885.91 = 885.90
733				
734				
735				
736				
T.P.	5.17	887.41	5.76	884.24
737				
738				
739				
740				
741				
BM				882.61 = 882.77
740 + 36				
+55				
+70				

3 pike in 8" Oak <sup>60</sup> Rt Sta 731+25

44  
42  
52  
56

3 pike in 6" Maple <sup>50</sup> Rt Sta 731+50

black catfish in Treasort St 732+00

52  
42  
58  
42  
57  
58  
40  
63  
60

$\frac{68}{38}$   $\frac{84}{36}$   $\frac{84}{33}$   $\frac{71}{32}$

76

$\frac{72}{32}$   $\frac{56}{34}$   $\frac{87}{38}$   $\frac{72}{39}$

$\frac{60}{39}$   $\frac{91}{38}$   $\frac{91}{34}$   $\frac{74}{32}$

74

$\frac{77}{30}$   $\frac{73}{32}$   $\frac{92}{36}$   $\frac{77}{37}$

$\frac{88}{39}$   $\frac{97}{37}$   $\frac{96}{36}$   $\frac{86}{32}$

70

$\frac{70}{31}$   $\frac{92}{33}$   $\frac{94}{37}$   $\frac{70}{40}$

274

889.41

742

743

744

745

746

747

T.P

9.88

898.39

0.91

888.50

748

749

4.38

894.01

= 894.20

T.P

4.35

892.41

10.33

888.06

T.P

4.09

890.88

5.62

886.79

4.19

886.61

= 886.66

57

52

60

50

52

45

84

53

Spike in 18" Oak 70' Wt 54 748+60

spike in 24" Oak 75' Wt 57 769+40

## Drive Ways:

	Rt		Rt #1		
Jtg.	Fill	Exc.	Fill	Exc.	
640+78	20x25x1				19
562+02			9x15x15		8
564+87			18x12x15		12
678+12			8x20x1		6
679+14	47x10x2				34
679+58			16x8x1		5
587+32	18x8x1		20x10x1		13
734+40			10x18x2		13
753+00	15x10x1				5
785+17	20x5x15				5
791+85	66yd.				6
810+56			9x20x15		10
810+69	10x22x2				15

# KEITH'S RAILROAD CURVE TABLES.

Published by KEUFFEL & ESSER CO., New York.

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## HOW TO USE KEITH'S TABLES.

### EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle  
of Intersection or I. P.= $23^{\circ} 20'$  to the R. at Station  
542+72.

Ext. in Tab. IV opposite  $23^{\circ} 20' = 120.87$   
 $120.87 \div 12 = 10.07$ . Say a  $10^{\circ}$  Curve.

Tan. in Tab. IV opp.  $23^{\circ} 20' = 1183.1$   
 $1183.1 \div 10 = 118.31$ .

Tab. V. correction for A.  $23^{\circ} 20'$  for a  $10^{\circ}$  Cur. = 0.16  
 $118.31 + 0.16 = 118.47 =$ corrected Tangent.

(If corrected Ext. is required find in same way)  
Ang.  $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333 =$ L. C.

$2^{\circ} 19\frac{1}{2}' =$ def. for sta.	543	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}' =$ " " "	+50	Tan.=	1.18.47
$7^{\circ} 19\frac{1}{2}' =$ " " "	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' =$ " " "	+50	L. C.=	2.33.33
$11^{\circ} 40' =$ " " "	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3'$  (def. for 1 ft. of  $10^{\circ}$  Cur.) =  $139.41' =$   
 $2^{\circ} 19\frac{1}{2}'' =$ def. for sta. 542.

Def. for 50 ft. =  $2^{\circ} 30'$  for a  $10^{\circ}$  Curve.

Def. for 36.86 ft. =  $1^{\circ} 50\frac{1}{2}'$  for a  $10^{\circ}$  Curve

(These tables are published in Field Books of  
KEUFFEL & ESSER Co., New York, N. Y.)

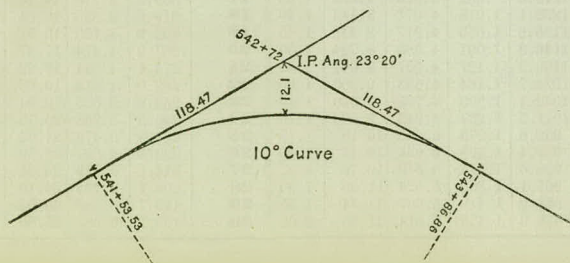


TABLE I. — Minutes in Decimals of a Degree.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	<sup>1</sup> / <sub>8</sub>	3-16	<sup>1</sup> / <sub>4</sub>	5-16	<sup>3</sup> / <sub>8</sub>	<sup>1</sup> / <sub>2</sub>	<sup>5</sup> / <sub>8</sub>	<sup>3</sup> / <sub>4</sub>	<sup>7</sup> / <sub>8</sub>
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
0° 10'	34377.	.036	.145	.291	0.05	7°	819.0	1.528	6.105	12.21	2.10
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	8	716.8	1.746	6.976	13.95	2.40
1	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	9	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
2	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	10	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2292.0	.545	2.181	4.363	0.75	11	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	12	478.3	2.620	10.45	20.91	3.60
3	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	13	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	14	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	15	383.1	3.277	13.05	26.11	4.50
4	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	16	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.781	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	17	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	18	319.6	3.825	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	19	302.9	4.155	16.51	33.01	5.70
5	1146.3	1.091	4.362	8.724	1.50	20	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	21	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	22	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	23	250.8	5.035	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	24	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	25	231.0	5.476	21.64	43.28	7.50
6	955.4	1.309	5.234	10.47	1.80	26	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	27	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	28	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	29	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	30	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>1°</b>	50.00	.22	<b>11°</b>	551.70	26.50	<b>21°</b>	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
<b>2</b>	100.01	.87	<b>12</b>	602.21	31.56	<b>22</b>	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
<b>3</b>	150.04	1.96	<b>13</b>	652.81	37.07	<b>23</b>	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
<b>4</b>	200.08	3.49	<b>14</b>	703.51	43.03	<b>24</b>	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
<b>5</b>	250.16	5.46	<b>15</b>	754.32	49.44	<b>25</b>	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
<b>6</b>	300.28	7.86	<b>16</b>	805.25	56.31	<b>26</b>	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
<b>7</b>	350.44	10.71	<b>17</b>	856.30	63.63	<b>27</b>	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
<b>8</b>	400.66	13.99	<b>18</b>	907.49	71.42	<b>28</b>	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
<b>9</b>	450.93	17.72	<b>19</b>	958.81	79.67	<b>29</b>	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
<b>10</b>	501.28	21.89	<b>20</b>	1010.3	88.39	<b>30</b>	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>31°</b>	1589.0	216.3	<b>41°</b>	2142.2	387.4	<b>51°</b>	2732.9	618.4
10'	1595.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
<b>32</b>	1643.0	230.9	<b>42</b>	2199.4	407.6	<b>52</b>	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
<b>33</b>	1697.2	246.1	<b>43</b>	2257.0	428.5	<b>53</b>	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
<b>34</b>	1751.7	261.8	<b>44</b>	2314.9	450.0	<b>54</b>	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
<b>35</b>	1806.6	278.1	<b>45</b>	2373.3	472.1	<b>55</b>	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.8	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
<b>36</b>	1861.7	294.9	<b>46</b>	2432.1	494.8	<b>56</b>	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
<b>37</b>	1917.1	312.2	<b>47</b>	2491.3	518.2	<b>57</b>	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
<b>38</b>	1972.9	330.2	<b>48</b>	2551.0	542.2	<b>58</b>	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.8	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
<b>39</b>	2029.0	348.6	<b>49</b>	2611.2	566.9	<b>59</b>	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
<b>40</b>	2085.4	367.7	<b>50</b>	2671.8	592.3	<b>60</b>	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>61°</b>	3375.0	920.2	<b>71°</b>	4086.9	1308.2	<b>81°</b>	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
<b>62</b>	3442.7	954.8	<b>72</b>	4162.8	1352.6	<b>82</b>	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
<b>63</b>	3511.1	990.2	<b>73</b>	4239.7	1398.0	<b>83</b>	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
<b>64</b>	3580.3	1026.6	<b>74</b>	4317.6	1444.6	<b>84</b>	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
<b>65</b>	3650.2	1063.9	<b>75</b>	4396.5	1492.4	<b>85</b>	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
<b>66</b>	3720.9	1102.2	<b>76</b>	4476.5	1541.4	<b>86</b>	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
<b>67</b>	3792.4	1141.4	<b>77</b>	4557.6	1591.6	<b>87</b>	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
<b>68</b>	3864.7	1181.6	<b>78</b>	4639.8	1643.0	<b>88</b>	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
<b>69</b>	3937.9	1222.7	<b>79</b>	4723.2	1695.8	<b>89</b>	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
<b>70</b>	4011.9	1265.0	<b>80</b>	4807.7	1749.9	<b>90</b>	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
<b>91°</b>	5830.5	2444.9	<b>101°</b>	6950.6	3278.1	<b>111°</b>	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
<b>92</b>	5933.2	2518.5	<b>102</b>	7075.5	3374.9	<b>112</b>	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
<b>93</b>	6037.8	2594.0	<b>103</b>	7203.2	3474.4	<b>113</b>	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
<b>94</b>	6144.3	2671.6	<b>104</b>	7333.6	3576.8	<b>114</b>	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
<b>95</b>	6252.8	2751.3	<b>105</b>	7467.0	3682.3	<b>115</b>	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
<b>96</b>	6363.4	2833.2	<b>106</b>	7603.5	3791.0	<b>116</b>	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
<b>97</b>	6476.2	2917.3	<b>107</b>	7743.2	3902.9	<b>117</b>	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
<b>98</b>	6591.2	3003.8	<b>108</b>	7886.2	4018.2	<b>118</b>	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
<b>99</b>	6708.6	3092.7	<b>109</b>	8032.7	4137.1	<b>119</b>	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
<b>100</b>	6828.3	3184.1	<b>110</b>	8182.8	4259.7	<b>120</b>	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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For Tangents Add															
ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.10	.22	.25	.28	.31	.34	.38	.42	.46	
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68	
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90	
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14	
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39	
35°	.11	.22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66	
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94	
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21	
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48	
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77	
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07	
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39	
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72	
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09	
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46	
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89	
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32	
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83	
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34	

## For Externals Add

5.09

ANGLE	CURVE	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020	
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083	
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135	
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188	
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264	
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341	
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445	
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550	
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700	
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851	
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01	
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17	
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39	
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62	
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91	
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20	
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58	
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96	

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord = sin of def. angle R				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

## CURVE FORMULAS.

$$T = R \tan \frac{1}{2} I$$

$$T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } D}$$

$$\text{Sin. } D = \frac{50}{R}$$

$$\text{Sin. } D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{50}{\text{Sin. } D}$$

$$E = R \text{ ex. sec. } \frac{1}{2} I$$

$$E = T \tan \frac{1}{2} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{\frac{1}{2} I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and Externals to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough; by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.— Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10.  $10^2 \div 200 = .5$ .  $100 + .5 = 100.5$  hyp.

Given Hyp. 100, Alt. 25.  $25^2 \div 200 = 3.125$ .  $100 - 3.125 = 96.875 =$  Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

## Natural Sines

deg.	0'	10'	20'	30'	40'	50'	deg.	deg.	0'	10'	20'	30'	40'	50'	deg.
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1279	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10

deg.	60'	50'	40'	30'	20'	10'	deg.	deg.	60'	50'	40'	30'	20'	10'	deg.
80	9848	9853	9858	9863	9868	9872	9								
81	9877	9881	9886	9890	9894	9899	8								
82	9903	9907	9911	9914	9918	9922	7								
83	9925	9929	9932	9936	9939	9942	6								
84	9945	9948	9951	9954	9957	9959	5								
85	9962	9964	9967	9969	9971	9974	4								
86	9976	9978	9980	9981	9983	9985	3								
87	9986	9988	9989	9990	9992	9993	2								
88	9994	9995	9996	9997	9997	9998	1								
89	9998	9999	9999	9999	I.0000	I.0000	0								

deg.	60'	50'	40'	30'	20'	10'	deg.
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## Natural Cosines

Natural Tangents

min.	0'	10'	20'	30'	40'	50'	sec. sec.	0'	10'	20'	30'	40'	50'	sec.	
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3432	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4735	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5828	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10

sec.	60'	50'	40'	30'	20'	10'	sec. sec.	60'	50'	40'	30'	20'	10'	sec.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9							
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8							
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7							
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6							
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5							
85	11.430	11.826	12.250	12.706	13.197	13.727	4							
86	14.300	14.924	15.605	16.350	17.169	18.075	3							
87	19.081	20.206	21.470	22.903	24.542	26.432	2							
88	28.636	31.242	34.368	38.189	42.964	49.104	1							
89	57.290	68.750	85.940	114.588	171.885	343.770	0							

Natural Cotangents

8856

886.66  
323  
859.89  
547  
884.42  
216  
886.58  
19.07  
876.51  
2.71  
879.22  
3.83  
875.39

886.58  
548  
881.10  
886.58  
9.94  
876.59

879.22  
4.63  
874.59

+36

+51

+68

+74

+94

819+00

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
32	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

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