CO. PROJ. Nº 26-62

DIV. "C".

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

780
797+50

129+00
~~[illegible]~~
755+00

808+08
808+56

C

D.V

49-00
4°-22
5°.30

130
45

23.79
45
22-34
45
21°49'

91.6
87.4
4.2

Original Xsec. for Uncl. Order #6 Page 78

Alignment Notes Pages 2 to 7

Original Xsec. Page's 8 to 43

Original Xsec. Driveways Page 44
Sta. 827+27

Original Xsec. Channel Change (45 to 47)
Sta. 819+45

Original Xsec. Channel Change (48)
Sta. 795+20 to 798+90

Original Xsec. Driveways (49)
Sta. 808+03 & 808+56

Original Xsec. H. D.
Sta. 605+80 Rt. (50
Sta. 613+00 Rt. 51)

Original Channel Change (52)
Sta 808+30

W. 106 x 40 Sta. 808+40
Page 53

Original Xsec. Central (54 to 56)
Fire. Cut off.

X sec. Sta 819+50 - 819+96 (57)

Final Xsec. Hand Ditch (59 to 60)
Sta. 771 to 789

Final Xsec. Hand Ditch
Sta. 729 + 740+68 (61 to 62)

Original Xsec. Channel (62)
Change Sta. 741

Final Xsec. Hand Ditch (63, 64)
Sta. 790 to 808+27

Final Xsec Channel Change
Sta. 808+40 (65)

Xsec. for rebalance
of Quantities Sta. 761 to 799 (66 to 70)

Original Xsec for Borrow
Pit. Sta. 789+00 - 792+50 (71. 72)

Grade Change
Sta 785 to 797+50 (73-74)

Sta	P.	Left	Right
573+83½	P.T.		
590+72½	P.I.	31°58'	
587+44½	P.C.		
578+00	P.O.T.		
573+00	P.O.T.		
563+00	P.O.T.		

Left

Right 6/30/25

587+44.4
588 - 1°-24'
+50 - 2°-39'
589 - 3°-54'
+50 - 5°-09'
590 - 6°-24'
+50 - 7°-39'
591 - 8°-54'
+50 - 10°-09'
592 - 11°-24'
+50 - 12°-39'
593 - 13°-54'
+50 - 15°-09'
593+44.4 - 15°-54'

Hub
32.5
59.3
43.97
Hub

Δ 31°58'
D 5° Lt.
T 328.33
L 639.33

587+35.7 P.C
588+50
589
+50
590
+50
591
+50
592
+50
593
+50
593+44.7 P.T.

Def.
0° 3'
2° 3'
4° 3'
6° 3'
8° 3'
10° 3'
12° 3'
14° 3'
16° 3'
18° 3'
20° 3'
22° 3'
24° 3'
25°18'

18°-7½' Hub 100'

Straight in 36°-7½' Hub 100'

Central Connection
Δ 50° 19'
D 8° Rt.
T. 336.7
L. 629.0

41.55
27.76
606 P.O.T.
T.P.
T.P.
26.45
25.85

Sta	P.	L.	R
620+00	P.O.T.		
611+47.04	P.T.		
609+02.75	P.I		24°50'
606+50.37	P.C.		
599+00	P.O.T.		
595+79.1	P.O.T.		

Lt ℄ Rt

4/30/29

606+50.39

607 -1°-14.5

+50 -2°-29.6

608 -5°-44.5

+50 -4°-59.5

609 -6°-14.5

+50 -7°-29.5

610 -8°-44.5

+50 -9°-59.5

611 -11°-14.5

+47.04 -12°-25'

Side Ties

72.33

61.80

Δ -24°58'

D 5°84

T 252.38

L 496.67

Sta.	P.	L.	R
682+59.2	P.T.		
678+82.5	P.I.		15°11'
675+68.41	P.C.		
672+00	P.O.T.		
650+00	P.O.T.		
640+00	P.O.T.		
630+00	P.O.T.		

+59.73 7°36' P.T.

7/1/20

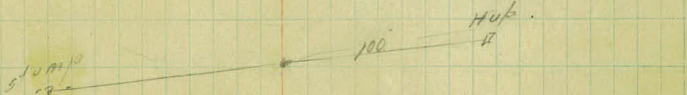
682	7°00'				
681	6°00'	A	15°12'	Δ	15°11'
680	5°00'	D	2° Rt.	D	2° Rt
679	4°00'	Δ T.	382.27	T	381.84
678	3°00'	L.	760.0'	L	759.17
677	2°00'				
676	1°00'				

+82.0 P.I

66.6

60.81

674+99.73 P.C



Sta. P. L. R.

770+00
770+00 2 = P.O.T.

759+00
759+01 = P.O.T.

751+00
751+00 2 = P.O.T.

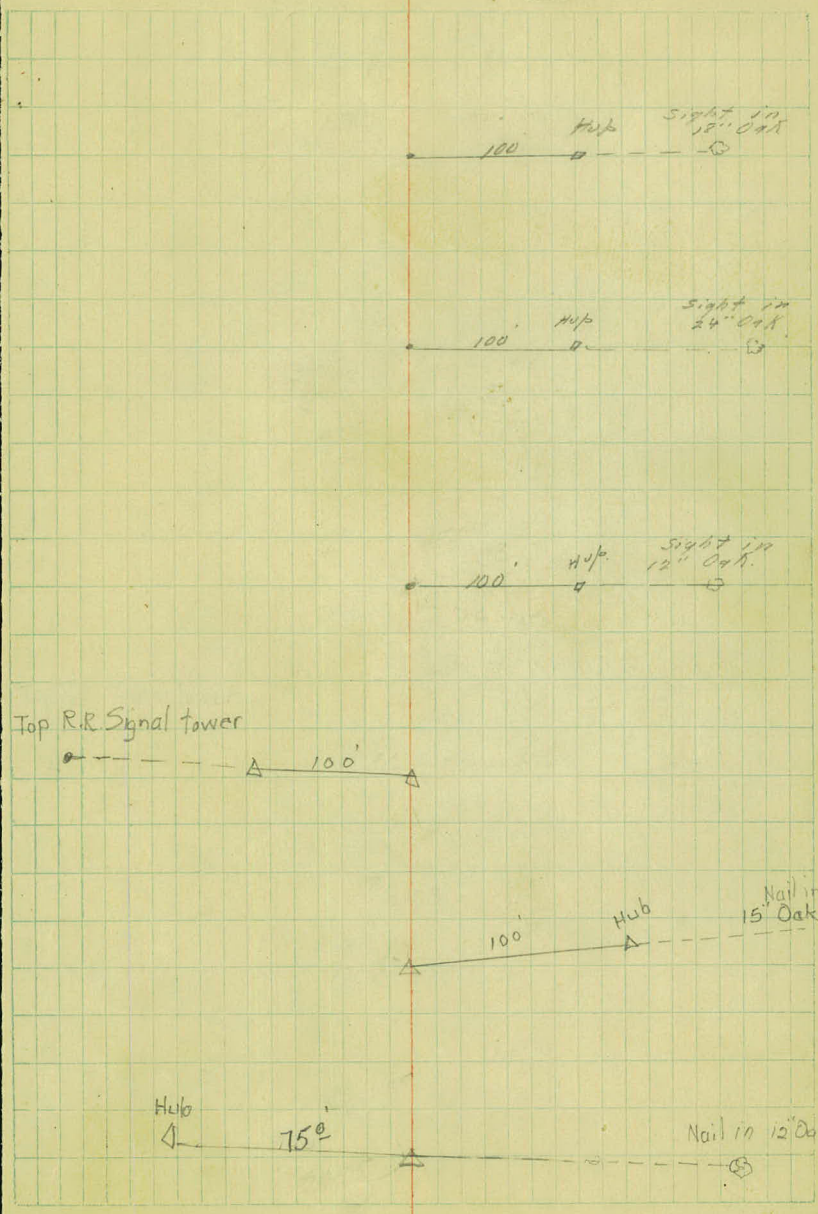
734+00 P.O.T.
734+00 35 =

724+00 P.O.T.
724+00 7 =

717+00 P.O.T.
717+01 43 =

Equa.
682+59.58 =
709+54.70

Lt. ℄ Rt


Hub
100
Sight in 12" Oak
Hub
100
Sight in 24" Oak
Hub
100
Sight in 12" Oak
Top R.R. Signal tower
100'
Hub
100'
Nail in 15" Oak
Hub
75°
Nail in 12" Oak

Sta	P	Δ	Bt.
812+33.9	P.O.T.		
807+85.2	P.T.		
800+45.2	P.I	54°03'	
800+15.2	P.C.		
792+00			
792+01.3	= P.O.T		
782+00			
783+01	= P.O.T		

499+45
524+00
Lt
Rt

179-08
5-9-03
13 0 5-7

Sight on top of Semaphore

R.R
Hub
100'

+88.47	Def
+50	29° 31.5'
	27° 59'
807	25 59'
+50	23 59'
806	21 59'
+50	19 59'
805	17 59'
+50	15 59'
804	13 59'
+50	11 59'
803	9 59'
+50	7 59'
802	5 59'
+50	3° 59
801	1° 59.16
800 +50.35	0°00

Hub
39.88
33.15
Hub

Δ 39°41'31"
D 5° 17'
T 401.98
L 738.17

Sight on Point on Top of Semaphore.

Hub — 75' — 100' — Hub

No ties

Sta		L.	R.
837+84.1 = 809+13.8	P.O.T	Equa.	End of Div. "C"
819+08			
832+40.7	P.T.		
825+09.8	P.I.		48°27'
816+45.7	P.C.		

816+75 47

817+00 -5°-49' 819+08 Beg of Bridge Det 3°56' } Bridge
818 -6°-19' 818+72 End of 4°54' }
819 -6°-49'
820 -7°-19' 4°54'
821 -8°-49'
822 -9°-19'
823 -9°-49'
824 -11°-19'
825 -12°-49'
826 -14°-19'
827 -15°-49'
828 -17°-19'
829 -18°-49'
830 -20°-19'
831 -21°-49'
832 -23°-19'
47
840 -24°-13'

Δ 42°27'
D 3°
T 359.41
L 161.37

FP.
50.60

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B. M.	5.2	918.73		913.40	
563				913.5	5.2
564				13.7	5.0
T.P.	5.67	919.65	4.75	913.98	
565				13.8	5.9
750				13.7	6.0
566				13.7	6.0
567				13.5	6.2
150				13.4	6.3
568				13.3	6.4
T.P.	8.10	917.41	10.34	909.31	
569				13.2	4.2
763				13.1	4.3
570				13.1	4.3
150				13.0	4.4

Inst. .....
Rod. .....
Chain. .....

8-25-26

Left C L Right

Sp. in Sta. 50 Lt Sta. 560 + 65

3.6/50 3.6/3.9 +1.3 4.1/20 4.7/-0.5 (5.2) 4.7/20 3.4/4.9 +0.3 5.0/50

6.8/50 3.5/7.3 +0.2 2.7/7.4 -2.4 2.5/-2.5 (5.0) 2.6/7.2 2.2 3.0/5/7.2 +0.3 7.2/50

5.5/50 3.2/5.6 +0.3 5.9/20 6.2/-0.3 (5.9) 2.0/6.1 -0.2 3.1/6.3 +2.1 6.2/50

4.9/50 3.6/5.1 +0.9 5.1/20 5.0/+1.0 (6.0) 5.1/20 3.4/5.3 +0.7 5.2/50

4.7/50 3.5/4.7 +1.3 4.7/20 4.7/+1.3 (6.0) 4.7/20 3.5/4.8 +1.2 4.9/50

4.4/50 3.3/4.5 +1.7 4.5/20 4.6/+1.6 (6.2) 4.8/20 3.5/5.1 +1.1 5.2/50

5.0/50 3.6/4.8 +1.5 4.7/20 4.6/+1.5 (6.3) 4.8/20 3.5/5.1 +1.2 5.5/50

4.8/50 3.8/6.9 0.0 6.1/20 5.5/+0.9 (6.4) 5.2/20 3.7/5.1 +1.3 5.3/50

10.0/50 3.8/10.1 -5.9 9.2/-5.0 (4.2) 2.4 7.6/-3.2 5.8/50

10.4/50 9.8/20 9.6/+4.3 9.2/20 7.3/50

10.5/50 3.6/10.0 -5.7 9.5/-5.2 (4.3) 2.9.0/8.8 -4.5 7.4/50

9.2/50 2.6/8.7 -4.3 8.2/-3.8 (4.4) 2.7/7.5 3.1 5.9/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		917.41 ✓			
571				913.0	4.4
150				13.1	4.3
572				13.1	4.3
150				13.1	4.3
573				13.2	4.2
T.P.	3.59	915.78 ✓	5.22	912.19 ✓	
150				13.2	2.6
574				13.3	2.5
140				13.3	2.5
B.M.			2.56	913.22	913.20
575				13.4	2.4
B.M.	4.54	917.74 ✓	2.56	913.20	
576				13.5	4.2
577				13.6	4.1
578				13.7	4.0

Inst. .....
Rod. .....
Chain. .....

Left			G. L.		Right	
5.5 / 5.1	3.2 3 / 5.4 / +1.5	2.2 2 / 5.3 / -0.9	5.0 / -0.6	(4.4) 2.1 5 / 4.9 / -0.5	2.3 3 / 4.7 / +2.7	4.4 / 50
2.9 / 50	3.5 6 / 3.1 / +1.2	3.2 / 20	3.2 / +1.1	(4.3) 3.3 / 20	3.5 3 / 3.3 / +1.0	3.3 / 50
1.8 / 50	3.7 4 / 1.9 / +2.4	2.2 / 20	2.4 / +1.9	(4.3) 2.6 / 20	3.5 9 / 2.9 / +1.4	3.0 / 50
1.7 / 50	3.6 / 1.8 / -2.5	2.0 / 20	2.4 / +1.9	(4.3) 2.9 / 20	3.5 6 / 3.1 / +1.2	3.2 / 50
2.8 / 50	3.5 3 / 2.7 / +1.5	3.2 / 20	3.6 / +0.6	(4.2) 3.7 / 20	3.4 7 / 3.9 / +0.3	4.2 / 50
3.1 / 50	3.2 3 / 3.6 / 1.5	2.3 3 / 3.7 / -1.1	4.2 / -1.6	(2.6) .2 5 / 4.3 / -1.7	3.1 / 4.4 / +0.7	4.4 / 50
	5.5 / 50	2.6 4 / 5.8 / -3.3	6.0 / -3.5	(2.5) 1.6 4 / 5.8 / -3.3	5.4 / 50	
	6.6 / 50	6.5 / 20	6.2	(2.5) 5.8 / 22	5.3 / 50	
	6.0 / 50	2.6 7 / 5.5 / -3.1	4.9 / -2.5	(2.4) 2.2 7 / 4.8 / -2.4	3 3 / 4.6 / +0.3	5.0 / 50
15 Oak 50 Lt 5.6 - 3.5 / 5.6 / 50	3.2 3 / 5.3 / +1.4	2.2 3 / 5.1 / -0.9	4.7 / -0.5	(4.2) 2.2 4 / 5.0 / -0.8	3.2 4 / 5.1 / +1.6	5.8 / 50
4.1 / 50	3.3 9 / 4.0 / +0.1	2.0 0 / 4.1 / 0.0	4.8 / -0.7	(4.1) 2.4 4 / 5.5 / +1.4	3.1 4 / 5.7 / +0.9	6.8 / 50
3.5 / 50	3.4 4 / 3.6 / +0.4	2.0 0 / 4.0 / 0.0	4.6 / -0.6	(4.0) 2.3 6 / 5.2 / -1.2	3.1 4 / 5.6 / +0.9	6.1 / 50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		917.74			
+50				913.7	4.0
T.P.	3.90	919.21	2.43	915.31	
579				13.7	5.5
580				13.6	5.6
581				13.4	5.8
+50				13.3	5.9
T.P.	2.36	918.48	3.09	916.12	
582				13.2	5.3
+50				13.1	5.4
583				12.9	5.6
584				12.5	6.0
585				12.0	6.5
T.P	3.00	915.65	5.83	912.65	
586				11.5	4.2
+50				11.2	4.5

Inst. .....
Rod. .....
Chain. .....

10

Left — C L — Right

3.1 / 50	3.7 / 3.0 / 1.0	3.4 / 22	3.6 / +0.4	(4.0)	3.9 / 4.3 / -0.3	3.9 / 4.5 / 2.0	4.8 / 50	
4.5 / 50	4.4 / +1.1	4.4 / 22	4.4 / +1.1	(5.5)	4.7 / 22	3.5 / 5.0 / +0.5	5.5 / 50	
5.3 / 50	4.7 / 5.0 / +0.6	4.7 / 21	4.7 / +0.9	(5.6)	4.7 / 23	3.9 / 4.8 / +0.8	5.1 / 50	
5.1 / 50	3.7 / 4.8 / +1.0	4.7 / 20	4.2 / +1.6	(5.8)	4.1 / 21	3.3 / 4.1 / +1.7	4.1 / 50	
6.7 / 50	3.9 / 6.4 / +2.0	2.0 / 5.9 / 0.0	5.1 / +0.8	(5.9)	4.5 / 20	3.8 / 4.2 / +1.7	4.0 / 50	
8" Oak 72' Rt. Sta. 581+45								
	9.4 / 50	1.8 / 8.7 / -3.4	6.8 / -1.5	(5.3)	2.0 / 5.6 / -1.3	1.1 / 4.8 / +0.5	3.7 / 50	
	10.5 / 50	0.6 / 10.2 / -4.8	8.5 / -3.1	(5.4)	2.4 / 6.8 / -1.4	3.3 / 5.7 / +2.0	5.0 / 50	
	8.8 / 50	2.6 / 8.6 / -3.0	7.6 / -2.0	(5.6)	2.3 / 6.6 / -1.0	3.2 / 6.2 / +1.7	5.6 / 50	
7.1 / 50	3.2 / 6.8 / +1.7	2.2 / 6.9 / -0.9	6.4 / -0.4	(6.0)	2.0 / 6.0 / 0.0	3.4 / 5.6 / +0.4	5.4 / 50	
	6.8 / 50	6.7 / 33.9 / 6.2 / 20	6.1 / +0.4	(6.5)	6.0 / 20	3.4 / 5.8 / +0.7	5.8 / 50	
4.2 / 50	3.1 / 4.0 / +0.2	3.5 / 20	3.9 / +0.8	(4.2)	3.5 / 20	3.4 / 3.5 / +0.1	3.8 / 50	
4.5 / 50	3.2 / 4.7 / +0.3	2.0 / 4.5 / 0.0	4.5 / 0.0	(4.5)	4.2 / 20	3.4 / 4.3 / +0.2	4.9 / 50	

Cross Sections

Sta.	B. S.	H. I.	F. S.	Gr. R.	L.	C	R.
		915.65 ✓					
587				911.0	5.0	4.7	4.4
+44.1				10.8	5.5	4.9	4.3
588				10.5	6.1	5.2	4.3
+50				10.2	6.4	5.5	4.6
589				10.0	6.6	5.7	4.8
B.M.	3.05	913.94 ✓	4.80	910.85 ✓		910.89	
+50				09.7	5.1	4.2	3.3
590				09.5	5.3	4.4	3.5
+50				09.2	5.6	4.7	3.8
591				Ditch 08.4 09.0	5.8	4.9	4.0
+50				08.8	6.0	5.1	4.2
592				5.4 08.7	6.1	5.2	4.3
T.P. +50	5.58	912.01 ✓	7.51	906.43 ✓	8.7		5.2
593				5.4 08.6	6.0 43	3.4	2.5
+50				08.6		3.4	
594				08.7	4.2	3.3	2.4

Inst.
Rod.
Chain.

	Left	C L	Right
+0.32 / -0.32	4.3 / 50 — 34 3/4.4 +0.6	4.5 +0.2 — (4.7) — 2° 4.7 0.0	3° 4.1 +2.2 — 4.8 / 50
+0.63 / -0.63	4.3 / 50 — 36 4/4.4 +1.1	4.2 +0.3 — (4.9) — 2° 4.3 0.0	37 4/4.3 0.0 — 4.3 / 50
+0.88 / -0.88	4.1 / 50 — 31 4/4.7 +1.4 — 4.5 / 22	4.2 +1.0 — (5.2) — 3.9 / 20	34 4/3.9 +0.4 — 3.6 / 20
+0.88 / -0.88	4.4 / 50 — 31 4/5.0 +1.4 — 4.5 / 22	4.1 +1.4 — (5.5) — 4.3 / 20	34 4/4.2 -0.4 — 3.9 / 50
+0.88 / -0.88	5.6 / 50 — 31 3/5.6 +1.0 — 5.2 / 50	5.8 -0.1 — (5.7) — 2° 5.7 -0.9	32 4/5.5 +1.8 — 5.4 / 50
110 Lt. 588+50			
+0.88 / -0.88	6.3 / 50 — 34 4/6.2 +1.4 — 24 4/6.0 -0.9	5.9 -1.7 — (4.2) — 26 3/5.4 -2.1	30 4/5.4 +0.4 — 5.2 / 50
+0.88 / -0.88	8.2 / 50 — 27 0/7.8 2.5	6.7 -2.5 — (4.4) — 3.6 6.3 -2.8	5.8 / 50
+0.88 / -0.88	8.6 / 50 — 29 3/8.0 3.4	7.4 -2.7 — (4.7) — 26 4/6.8 -3.0	6.6 / 50
+0.88 / -0.88	8.9 / 50 — 27 3/8.9 -2.6	8.4 -3.5 — (4.9) — 27 4/8.1 -4.1	7.8 / 50
+0.88 / -0.88	7.6 / 50 — 8.5 / 50 — 27 3/8.6 -2.6	9.0 -3.9 — 29 3/9.0 -4.8	9.0 / 50 (5.1)
+0.88 / -0.88	8.5 / 50 — 8 / 50 — 26 3/8.2 -2.1	8.6 -3.4 — 31 3/9.7 -5.4	9.7 / 50 (5.2)
	7.3 / 50 — 7.6 / 50	8.3 -3.1 — 32 3/9.0 -4.7	9.9 / 50 (5.2)
+0.88 / -0.88	4.2 / 50 — 30 4/5.0 +1.6 — 25 3/5.5 1.2	6.0 -2.6 — 28 3/6.5 -4.0	6.8 / 50 (3.4)
	3.4 / 50 — 3.4 +3.2 — 4.1 / 22	5.2 -1.8 — 26 3/5.9 -3.9	6.4 / 50 (3.4)
+0.88 / -0.88	2.2 / 50 — 32 3/3.5 +3.1	4.5 -1.2 — 25 3/5.0 -2.6	5.3 / 50 (3.3)

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		912.01			
+50				908.8	3.2
595				08.8	3.2
T. P.	4.08	913.34	2.75	909.26	
+47				08.8	4.5
+58				08.9	4.4
+64				08.9	4.4
+80				08.9	4.4
B.M.	1.49	915.55	+0.72 ?	914.06	
+95				08.9	6.7
596				08.9	6.7
+15				08.9	6.7
+82				09.1	6.5
597				09.1	6.5
+11				09.1	6.5

Inst.
Rod.
Chain.

12

W Left C L Right

+0.16 3.6/50 3.9/4.0/+2.6 2.1/4.1/-0.7 5.1/3.2/-1.9 3.4/4.6/-1.6 3.1/4.3/-1.2 4.3/50
-0.16

2.9/50 3.3/3.1/+3.5 2.0/3.2/0.0 3.4/3.2/-0.2 2.1/3.7/-0.5 2.1/3.6/+2.1 4.0/50

4.3/50 3.3/4.4/+3.5 2.4/4.7/-0.7 5.5/4.5/-1.0 5.2/9 6.7/18 6.7/25 2.0/6.5/-2.0 4.2/45 4.1/50

4.3/50 4.9/27 6.3/7 4.4/6.0 4.3/13 4.2/29 4.0/50

4.4/50 4.6/44 4.2/16 4.4/4.4 4.2/15 4.0/36 4.0/50

5.8/50 4.4/40 4.4/21 4.4/4.0 4.0/22 4.3/35 6.9/50

10' @ 80' Lt 539+40
6.4/50 6.3/43 6.2/15 6.7/6.4 9.1/17 10.3/31 11.0/50

6.4/50 6.1/31 6.2/16 6.7/8.5/-1.8 2.8/11.1/4.4 11.7/40 11.8/50

6.3/50 2.6/8.9/-2.2 10.9/11 6.1/11.4/4.7 2.1/10.6/-3.9 10.9/50

7.7/50 3.2/7.2/1.8 2.3/7.8/1.3 6.5/8.6/-2.1 2.5/9.0/-2.5 3.0/8.9/+0.1 8.7/50

7.1/50 3.2/6.7/+2.3 2.0/6.5/0.0 6.5/6.3/+0.2 2.0/6.5/0.0 3.3/6.5/0.0 6.3/50

8.5/50 3.8/8.4/+0.6 2.5/8.3/-1.8 6.5/8.6/+2.9 3.3/7.6/-1.1 3.2/7.2/+1.8 6.6/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
+43				909.x	6.4
+64				09.3	6.3
598				09.3	6.3
+50				09.5	6.1
599				09.6	6.0
+50				09.8	5.8
600				09.9	5.7
+50				10.1	5.5
601				10.x	5.4
T.P.	5.56	913.98	7.13	908.42	
+50				10.4	3.6
602				10.3	3.7
+50				10.3	3.7

Inst. .....
Rod. .....
Chain. .....

Left C L Right

8.9 / 50 — 9.3 / 20 — 8.9 (6.4) — 8.3 / 20 — 7.9 / 50

8.9 / 50 — 27.8 / 10.2 / -3.9 — 10.3 (6.3) -4.0 — 26.7 / 9.4 / -3.1 — 8.7 / 50

6.9 / 50 — 37.3 / 7.3 / +1.5 — 27.7 / 7.2 / +0.9 — 7.6 (6.3) -1.3 — 24.9 / 7.9 / -1.6 — 31.1 / 8.2 / +0.7 — 8.2 / 50

3.3 / 50 — 38.0 / 3.3 / +2.8 — 3.4 / 20 — 3.5 (6.1) +2.6 — 3.8 / 20 — 31.1 / 3.9 / +2.2 — 4.0 / 50

1.9 / 50 — 39.9 / 1.9 / -4.1 — 2.0 / 20 — 2.7 (6.0) +3.6 — 2.9 / 20 — 38.9 / 2.6 / +3.4 — 2.5 / 50

2.4 / 50 — 2.3 / 20 — 2.2 (5.9) — 2.5 / 20 — 2.8 / 50

3.5 / 50 — 31.5 / 3.2 / +2.5 — 3.1 / 20 — 3.2 (5.7) +2.5 — 3.3 / 20 — 4.2 / 26 — 36.8 / 3.6 / 30 — 36.8 / 3.7 / +2.0 — 3.9 / 50

5.4 / 50 — 5.4 / 20 — 5.3 (5.5) — 5.4 / 10 — 6.1 / 15 — 5.4 / 20 — 6.2 / 20

7.9 / 50 — 36.6 / 7.5 / +0.4 — 26.0 / 7.4 / -2.0 — 7.6 (5.4) -2.2 — 7.9 / 4 — 7.4 / 8 — 25.9 / 7.9 / -2.5 — 91 / 50

7.2 / 50 — 25.4 / 6.9 / -3.3 — 6.9 (3.6) -3.3 — 29.3 / 8.8 / -2.4 — 9.0 / 50

7.3 / 50 — 25.9 / 6.6 / -2.9 — 6.1 (3.7) -2.4 — 25.0 / 6.2 / -2.5 — 6.4 / 50

6.6 / 50 — 26.0 / 5.7 / -2.0 — 5.1 (3.7) -1.9 — 22.1 / 4.4 / -0.7 — 32.1 / 4.4 / +1.8 — 4.2 / 50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
603				910.2	3.8
+50				10.0	4.0
604				09.9	4.1
T.P.	6.05	916.31	3.72	910.26	
+50				09.8	6.5
605				09.6	6.7
					L. & R.
+46				09.5	6.7 6.8 7
606				09.3	6.7 7.0 7
+50				09.2	6.5 7.1 7
607				09.0	6.4 7.3 8
+50				08.9	6.5 7.4 8
608				08.7	6.7 7.6 8
+50				08.5	6.9 7.8 8
T.P. 689	7.86	918.12	6.05	910.26	
				08.4	8.8 9.7 10

J. F.

Inst.
Rod.
Chain.

14

Left	C L	Right
6.2 / 50	3.8	
5.8 / +0.5	5.1 / -1.3	4.6 / +1.7
5.6 / -1.8	4.6 / -0.8	4.6 / 14 / 50
5.6 / 50	4.0	5.6 / 50
5.3 / 20	5.5	5.2 / 50
3.6 / 50	4.1	
3.7 / 4.1	4.8 / -0.7	5.6 / -1.5
4.3 / -0.2	5.6 / 20	5.8 / +0.8 / 5.5 / 50
4.9 / 50	6.5	
4.7 / +1.8	6.5 / 0.6	7.3 / -0.8
7.8 / +1.2	7.7 / 37	6.2 / 40 / 6.7 / 50
5.5 / 50	6.7	
6.1 / +0.6	7.5 / -0.8	8.3 / -1.6
7.4 / +1.8	6.4 / 42	6.6 / 50
+0.1 / -0.16	6.8	
7.0 / 50	10.3 / 3.6	11.3 / -4.5
10.0 / -3.0	8.0 / +1.5	7.6 / 40 / 9.0 / 50
+0.28 / -0.28	7.0	
11.2 / 50	11.2 / -4.5	11.2 / -4.2
8.9 / -1.6	7.0 / +0.3	9.1 / 50
+0.62 / -0.62	7.1	
7.6 / 50	7.3 / -1.7	7.0 / +0.5
6.3 / +0.8	5.0 / 20	6.0 / 1.7
9.5 / 50	7.3	
5.3 / 50	4.6 / +1.8	3.8 / 20
3.3 / +1.0	3.1 / 20	5.0 / +3.2
8.2 / 50	7.4	
+0.88 / -0.88	4.1 / 50	3.5 / +3.0
2.8 / 20	2.3 / +5.1	2.2 / 20
4.0 / +4.3	4.8 / 44 / 7.4 / 50	
+0.88 / -0.88	7.6	
3.9 / 50	3.6 / +3.1	3.7 / 20
2.8 / +4.8	3.1 / 20	4.8 / +3.7
7.6 / 50	7.8	
4.0 / 50	4.0 / +2.9	3.9 / 20
3.8 / +4.0	4.1 / 20	5.7 / +3.0
8.1 / 50		
+0.88 / -0.88	9.1	
6.2 / 50	6.2 / +2.6	6.2 / 20
6.4 / +3.3	7.0 / 20	8.2 / +2.5
10.8 / 50		

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R. L	Gr. R. ℄	Gr. R. R
		918.12 ✓					
+50				908.3	8.9	9.8	
B.M.	1.32	911.63 ✓	7.81	910.31 ✓			
610				08.2	2.5	3.4	4
+50				08.2	2.5	3.4	4
611				08.1	2.6	3.5	4
+47				08.1	2.9	3.5	4
612				08.1	3.2	3.5	3
613				2.7 08.1	8.9	3.5	
B.M.	0.39	910.70 ✓	1.32	910.31 ✓			
614				3.0 08.1	7.7	2.6	
615				3.3 08.1	7.4	2.6	
616				3.6 08.1	7.1	2.6	
617				3.9 08.1	6.8	2.6	
618				4.2 08.2	6.5	2.5	

Inst.
Rod.
Chain.

8-13-26

15

Left C L Right

+0.88 / -0.88 2.0

6.9/50 | 6.8/+2.1 | 7.1/2.0 | 7.6/-2.2 (4.8) | 8.1/20 | 8.2/3.4 | 9.3/1.4 | 11.8/50

75' Lt. 6.10

3.2/50 | 2.2/+0.3 | 2.5/0.0 | 2.7/-0.7 (3.4) | 2.6/31 | 3.5/34 | 3.8/+0.5 | 5.6/50

+0.88 / -0.88 2.0

50/50 | 4.7/+0.3 | 4.6/-2.1 | 4.7/-1.3 (3.4) | 3.9/25 | 5.0/+1.8 | 6.7/41 | 6.3/50

+0.88 / -0.88 2.0

6.6/50 | 5.9/+3.3 | 5.5/-2.0 (3.5) | 5.2/-0.8 | 4.6/+2.3 | 5.7/50

+0.62 / -0.62 1.0

6.6/50 | 6.3/3.4 | 6.1/-2.6 (3.5) | 6.4/-2.9 | 6.5/+0.1 | 5.4/50

+0.26 / -0.26

7.8/50 | 7.6/4.5 | 7.7/-4.2 (3.5) | 8.2/-4.4 | 8.1/50

8.2/10.7 | 7.7/50

2.2/+0.7 | 9.4/-4.9 | 9.2/-5.7 (3.5) | 9.2/-5.7 | 9.2/0.0 | 9.7/50

7.1/50 | 6.9/+0.8 | 6.9/+0.8 | 6.8/-4.2 | 6.7/-4.1 (2.6) | 6.3/+1.4 | 6.3/+1.4 | 6.2/50

6.9/50 | 6.7/+0.7 | 6.7/+0.7 | 6.7/-4.1 | 6.5/-3.9 (2.6) | 6.2/-3.6 | 6.1/+1.3 | 5.8/+1.6 | 5.5/50

5.2/50 | 5.5/+1.6 | 5.6/+1.5 | 5.7/-3.1 | 5.8/-3.2 (2.6) | 5.7/-3.1 | 5.8/+1.3 | 5.9/+1.2 | 5.7/50

5.6/50 | 5.6/+1.3 | 5.7/+1.1 | 5.7/-3.1 | 5.6/-3.0 (2.6) | 5.5/-2.9 | 5.5/+1.3 | 5.3/+1.5 | 5.2/50

5.6/50 | 5.4/+1.1 | 5.4/+1.1 | 5.4/-2.9 | 4.5/-2.0 (2.5) | 4.6/-2.1 | 4.5/+2.0 | 4.2/+2.3 | 4.1/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		910.70 ✓			
619				908.4	2.3
T.P.	5.18	915.15 ✓	0.73	909.97 ✓	
620				08.7	6.5
B.M.	2.61	915.12 ✓	2.61	912.54 ✓	912.51
621				09.0	6.1
+50				09.1	6.0
622				09.3	5.8
623				09.6	5.5
+50				09.7	5.4
624				09.9	5.2
+50				10.0	5.1
625				10.2	4.9
+50				10.3	4.8
626				10.5	4.6
T.P.	7.74	919.31 ✓	3.55	911.57 ✓	

Inst.
Rod.
Chain.

8/16, 1926 16

Left	C L	Right
1.7 / 50	2.3	1.1 / 50
3.4 / 2.0 / +0.3 / 1.6 / 7	1.2 / +1.1 / 1.1 / 20	3.5 / 1.0 / +1.3 / 0.7 / 50
3.6 / 50	6.5	3.9 / 50
3.9 / 3.2 / +3.3 / 2.7 / 20	3.3 / +3.2 / 3.7 / 20	3.6 / 4.0 / 3 / +2.5
60 Ft. 6.20+0.5		
4.2 / 50	6.1	6.3 / 50
3.6 / 5 / 4.3 / +1.8 / 4.7 / 20	4.7 / +1.4 / 5.2 / 20	3.4 / 1 / 5.7 / +1.2
5.3 / 50	6.0	8.1 / 50
3.8 / 6.0 / 0.0 / 2.4 / 6.8 / -0.8	7.9 / -1.9 / 2.5 / 8.5	3 / 8.5 / 0.0
6.1 / 50	5.8	8.3 / 50
3.1 / 7.5 / +0.8 / 2.8 / 7.8 / 2.0	9.3 / -3.5 / 2.9 / 8.9 / -3.1	
7.0 / 50	5.5	6.3 / 50
3.0 / 7.9 / +0.1 / 2.5 / 8.0 / -3.5	8.6 / -3.1 / 2.6 / 7.5 / -2.0	3.2 / 7.2 / +0.8
3.7 / 50	5.4	5.8 / 50
3.5 / 4.5 / +0.9 / 6.3 / -0.9	1.0 / 6.4 / 2 / -1.0	3 / 6.2 / +1.7
2.8 / 50	5.2	7.0 / 50
3.4 / 3.1 / +0.1 / 3.7 / 26	5.2 / 0.0 / 2.3 / 6.2 / +1.0	3.1 / 6.6 / 1.1
3.6 / 50	5.1	6.2 / 50
3.5 / 6 / 3.9 / +1.2 / 4.2 / 20	4.9 / +0.2 / 2.3 / 5.5 / -0.4	3.2 / 5.9 / +1.7
5.4 / 50	4.9	7.6 / 50
3.2 / 6.2 / +1.2 / 6 / 6.6 / 2.1	7.2 / -2.3 / 2.6 / 7.0 / -2.1	3.3 / 7.2 / +0.2
3.5 / 50	4.8	4.8 / 50
3.6 / 3.9 / +0.9 / 4.6 / 20	4.8 / 0.0 / 4.7 / 20	3.9 / 4.7 / +0.1
2.0 / 50	4.6	4.7 / 50
3.3 / 1.6 / +3.0	2.3 / +2.3 / 3.4 / 20	3.4 / 6.7 / +0.4

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		919.31			
+50				910.6	8.7
627				10.8	8.5
+50				10.9	8.4
628				11.1	8.2
+60				11.3	8.0
629				11.4	7.9
+50				11.5	7.8
630				11.5	7.8
B.M.	9.77	921.38	7.73	911.58	911.61
+40				11.5	9.9
631				11.4	10.0
B.M	7.02	918.63	9.77	911.61	
632				11.1	7.5
+50				11.0	7.6

Inst.
Rod.
Chain.

Left C L Right

5.7/50 38A 5.6/+3.1 5.9/+2.8 7.1/20 (8.7) 44.7 8.4/+0.3 9.3/50

4.6/50 39.2 5.2/+3.3 6.0/20 6.1/+1.8 (8.5) 7.8/20 33.8 8.5/0.0 8.0/50

3.6/50 40.2 3.8/-4.6 4.9/20 7.7/+0.7 (8.4) 35.7 10.3/-1.9 39.8 10.4/+0.5 10.5/50

4.6/50 38.3 5.2/+3.0 6.0/20 6.9/+1.3 (8.2) 8.0/20 32.3 9.2/+1.5 10.6/50

4.4/50 39.3 4.3/+3.7 4.4/20 4.9/+3.1 (8.0) 7.4/20 33.3 9.4/+2.1 9.5/50

4.2/50 39.3 4.2/+3.7 4.4/20 5.0/+2.9 (7.9) 7.0/20 38.7 8.3/+2.1 10.5/50

2.5/50 42.1 2.3/+5.5 2.5/20 3.1/+4.4 (7.8) 5.1/20 35.7 6.5/+1.3 9.0/50

1.3/50 44.1 0.9/6.9 0.6/20 1.8/+6.0 (7.8) 4.2/20 35.7 6.5/+1.3 8.3/50

50 Rl. 630+40

2.9/50 42.2 2.9/+7.1 3.2/20 4.1/+5.8 (9.9) 7.6/20 33.6 10.0/2.4 10.9/50

8.0/50 39.4 10.3/+0.3 40.6 10.2/+0.2 10.5/+0.5 (10.0) 21.8 10.6/-0.6 32.2 10.6/+1.9 10.5/50

3.7/50 37.4 5.1/+2.4 6.2/20 6.8/+0.7 (7.5) 7.1/20 34.5 6.8/+0.5 7.0/50

3.1/50 31.8 4.9/+2.7 8.5/-0.9 (7.6) 24.8 9.2/-1.6 32.7 9.3/+0.8 9.4/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
633				910.8	7.8
150				10.7	7.9
634				10.5	8.1
+50				10.4	8.2
635				10.2	8.4
T.P.	9.05	916.11	11.57	907.06	
+50				10.1	6.0
636				09.9	6.2
+50				09.8	6.3
637				09.6	6.5
+50				09.5	6.6
638				09.3	6.8
639				08.8	7.3

Inst. .....
Rod. .....
Chain. .....

Left C L Right

7.8

7.7 / 50 | 3° 5 / 9.3 / +1.0 | 2° 5 / 9.7 / -1.9 | 13.1 / -4.3 | 3° 04 / 13.0 / -5.2 | 13.0 / 50

7.9

11.7 / 50 | 3° 0 / 11.9 / -4.0 | 12.6 / -4.7 | 3° 08 / 13.3 / -5.4 | 13.1 / 50

8.1

7.6 / 50 | 3° 9 / 9.3 / +1.3 | 2° 5 / 9.9 / -1.8 | 11.6 / -3.5 | 3° 0 / 13.2 / -5.1 | 11.9 / 50

8.2

5.5 / 50 | 3° 4 / 9.1 / +1.6 | 2° 6 / 10.2 / -2.0 | 14.0 / -5.8 | 3° 4 / 15.4 / -7.2 | 16.2 / 50

8.4

7.9 / 50 | 3° 06 / 10.5 / +0.4 | 2° 1 / 11.1 / 2.7 | 13.4 / -5.0 | 8.4 / 15.6 / -7.2 | 17.0 / 50

8-17-26

6.0

Rt { 11.7 / 50 | 3° 0 / 11.0 / -5.0 | 8.8 / -2.8 | 2° 3 / 7.3 / +1.5 | 3° 1 / 6.7 / +1.8 | 5.3 / 50 } Lt.

6.2

6.0 / 50 | 3° 1 / 6.9 / +1.8 | 2° / 7.4 / -1.2 | 7.6 / 20 | 8.8 / -2.6 | 2° / 7.6 / -3.4 | 9.0 / 50

6.3

8.8 / 50 | 2° 0 / 9.3 / -3.0 | 9.8 / -3.5 | 2° 1 / 9.9 / -3.6 | 7.9 / 50

6.5

8.1 / 50 | 3° 0 / 7.7 / +1.3 | 2° 4 / 7.9 / -1.4 | 7.9 / -1.4 | 2° 3 / 7.8 / -1.3 | 3° 0 / 7.7 / +1.3 | 7.2 / 50

6.6

7.1 / 50 | 3° 4 / 6.4 / +0.7 | 6.1 / 20 | 6.1 / +0.5 | 2° 0 / 6.6 / 0.0 | 3° 0 / 6.1 / +0.5 | 5.5 / 50

6.8

6.9 / 50 | 3° 1 / 6.2 / +0.6 | 6.0 / 20 | 6.4 / +0.4 | 6.4 / 20 | 3° 8 / 6.1 / +0.7 | 5.7 / 50

7.3

6.7 / 50 | 3° 6 / 5.4 / +1.9 | 4.8 / 20 | 4.1 / +3.2 | 3.9 / 20 | 3° 4 / 7.2 / +3.1 | 4.7 / 50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		916.1			
+50				908.5	7.6
640				08.0	8.1
+50				07.5	8.6
641				07.0	9.1
B.M	3.58	912.61	7.10	909.01	909.03
+63				06.5	6.1
642				06.0	6.6
643				05.0	7.6
644				04.0	8.6
+50				03.5	9.1
645				03.0	9.6
T.P.	0.88	904.83	8.66	903.95	
+50				02.5	2.3
646				02.0	2.8
T.P.	3.37	902.62	5.58	899.25	
B.M			0.65	901.97	901.93

Inst. .....
Rod. .....
Chain. .....

8/17-16 19

Left			C L		Right	
			(7.6)			
7.5 / 50	3.0 / 6.1 / -1.5	5.0 / 20	4.0 / +3.6	3.6 / 20	8.8 / 4.3 / +3.3	5.2 / 50
			(8.1)			
8.8 / 50	3.1 / 7.5 / +0.6	6.5 / 20	5.3 / +2.8	5.1 / 20	3.1.3 / 5.8 / +2.3	6.9 / 50
			(8.6)			
10.6 / 50	3.3 / 9.6 / +1.5	2.1 / 9.0 / -0.4	7.7 / +0.9	7.5 / 20	3.1 / 8.3 / +0.3	9.9 / 50
			(9.1)			
12.8 / 50	3.1 / 11.7 / -2.6	11.1 / -2.0	26.9 / 11.4 / -2.3	3.0 / 11.4 / +0.2	12.0 / 50	
			(6.1)			
12.7 / 50	3.2.6 / 12.4 / -6.3	12.3 / +6.2	3.3 / 12.8 / -6.7	12.3 / 50		
			(6.6)			
13.2 / 50	3.3.6 / 13.4 / -6.8	13.3 / -6.7	3.3.4 / 13.3 / -6.7	12.9 / 50		
			(7.6)			
12.8 / 50	3.1 / 13.2 / -5.6	13.3 / -5.7	3.1.4 / 13.3 / -5.7	12.7 / 50		
			(8.6)			
10.2 / 50	3.1.4 / 10.2 / +0.9	2.4.6 / 10.1 / +1.5	9.9 / -1.3	2.4.5 / 10.1 / -1.5	3.1.1 / 10.4 / +0.7	11.2 / 50
			(9.1)			
10.0 / 50	3.2.6 / 9.9 / +1.7	2.1.5 / 9.6 / -0.5	9.1 / 0.0	8.6 / 20	3.1.8 / 8.4 / +0.7	8.3 / 50
			(9.6)			
10.5 / 50	3.3.1 / 10.7 / +1.4	2.3.0 / 10.6 / -1.0	9.8 / -0.2	9.0 / 20	3.6.1 / 8.4 / +1.2	8.2 / 50
			(2.3)			
3.5 / 50	3.1.8 / 3.6 / +1.2	2.4.3 / 3.7 / -1.4	3.4 / -1.1	2.1 / 3.0 / -0.7	3.3.6 / 1.4 / +2.4	1.2 / 50
			(2.9)			
4.1 / 50	3.1.6 / 4.3 / +1.0	2.4.8 / 4.4 / -1.6	4.6 / -1.8	2.3.6 / 4.0 / -1.2	3.2.4 / 3.7 / +1.6	3.0 / 50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	1.56	903.49		901.93	
647				901.0	2.5
648				900.0	3.5
649				899.0	4.5
+60				98.5	5.0
+77				98.4	5.1
+86				98.3	5.2
650				98.3	5.3
+12				98.2	5.3
+30				98.1	5.4
651				97.7	5.8
652				97.3	6.2
653				97.3	6.2

Inst. .....
Rod. .....
Chain. .....

8/4-26

2/0

Left C L Right

48 Rt. 648+40

(3.5)

3.9/50 31.7/3.7/+1.1 24.3/3.9/-1.4 3.8/-1.3 21.8/3.1/-0.6 33.6/2.6/+2.4 2.4/50

(3.5)

5.2/50 31.7/4.9/+1.1 24.3/4.9/-1.4 4.8/-1.3 20.6/3.7/-0.2 33.0/4.0/+2.0 3.0/39 3.0/50

(4.5)

6.9/50 30.5/6.7/+0.3 26.3/6.6/-2.1 6.6/-2.1 26.0/6.5/-2.0 31.8/6.5/+0.5 6.0/50

(5.0)

4.6/50 30.9/6.9/+0.6 26.9/7.3/-2.3 7.0/-2.0 25.7/6.9/-1.9 32.7/6.7/+0.8 6.6/50

(5.1)

7.2/50 7.0/46 4.7/34 4.7/17 6.2/7 7.1 7.4/7 7.2/19 6.7/21 6.5/35 6.5/50

(5.2)

6.9/50 6.9/41 4.7/30 4.7 6.9/11 7.4/19 6.5/29 6.5/50

(5.3)

6.7/50 31.1/7.1/+0.7 25.0/7.1/-1.8 7.0/18 5.0/7 4.7/+0.6 4.5/19 32.0/6.5/+1.3 6.8/41 6.9/48 6.7/50

(5.3)

7.2/50 6.8/24 7.3/12 7.1 6.8/4 4.6/19 4.5/42 6.3/50

(5.4)

7.0/50 31.4/7.0/+0.9 24.8/7.0/-1.6 6.8/-1.7 6.8/6 7.5/8 25.4/7.2/-1.8 31.4/7.0/+0.9 6.7/37 4.7/50

(5.8)

7.7/50 31.8/7.1/+1.2 23.0/7.1/-1.3 7.1/-1.3 23.2/7.1/-1.3 32.2/7.1/+1.5 6.9/50

(6.2)

7.6/50 32.9/7.4/+1.3 24.1/7.4/+1.2 7.4/-1.2 23.6/7.4/-1.2 32.0/7.4/+1.3 7.3/50

(6.2)

8.0/50 31.5/7.8/+0.9 24.8/7.8/-1.6 7.6/1.4 23.1/7.5/-1.3 32.9/7.4/+1.3 7.4/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		903.49			
+50				897.3	6.2
654				97.3	6.2
T.P.	7.15	903.22	7.42	896.07	
655				97.4	5.8
+50				97.5	5.7
656				97.5	5.7
T.P.					
+50				97.5	5.7
657				97.4	5.8
658				97.3	5.9
659				97.0	6.2
660				96.7	6.5
661				96.4	6.8
T.P.	1.42	898.68	5.96	897.26	
662				96.1	2.6

Inst.
Rod.
Chain.

8/4

21

Left C L Right

(6.7)

7.8/50 7.4/27 7.4 7.5/16 7.5/36 7.6/50

(6.2)

7.3/50 31.8/7.5 +1.2 24.5/7.7 7.9 -1.7 24.7/7.6 +1.4 32.0/7.4 1.3 7.4/50

(5.8)

6.8/50 7.6/42 7.3/37 32.0/7.0 +1.3 24.2/7.2 -1.4 7.1 1.3 24.3/7.2 +1.4 31.7/7.2 +1.1 7.0/50

(5.7)

6.9/50 6.9/40 6.5/19 6.6 6.7/19 6.3/42 5.7/50

(5.7)

6.9/50 32.4/6.6 +1.6 23.0/6.7 7.0 6.2 -0.5 5.5/20 35.0/6.5 +0.8 4.5/50

(5.7)

6.5/50 33.0/6.2 +2.0 20.9/5.7 0.8 4.7 +1.0 4.6/25 35.6/4.5 +1.2 4.4/50

(5.8)

6.4/50 33.8/5.8 0.0 5.4/20 5.0 +0.8 4.8/20 35.7/4.5 +1.3 4.0/50

(5.8)

5.9/50 34.2/5.6 +0.3 5.3/20 5.0 +0.9 4.5/20 35.9/4.5 +1.4 4.5/50

6.2/50 34.1/6.0 +0.2 5.8/20 6.0 +0.2 20.8/6.2 0.0 33.9/6.2 0.0 6.2/50

8.0/50 7.2/37 33.0/7.0 +2.0 28.9/6.8 -0.3 6.5 0.0 6.2/20 34.5/6.0 +0.5 6.0/50

7.4/50 6.7/42 33.9/6.7 +0.1 6.5/20 6.3 +0.5 5.7/20 35.5/5.7 +1.1 5.5/50

2.5/50 34.1/2.4 +0.2 2.2/20 1.8 +0.8 1.5/20 35.6/1.5 +1.1 1.5/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		898.68 ✓			
663				895.8	2.9
664				95.5	3.2
+50				95.4	3.3
665				95.2	3.5
666				94.9	3.8
667				94.6	4.1
+50				94.5	4.2
668				94.3	4.4
+50				94.2	4.5
669				94.1	4.6
B.M.	2.71	900.77 ✓	.61	898.07 ✓	898.06
+50				94.1	6.7
670				94.1	6.7

Inst. .....
Rod. .....
Chain. .....

221

Left C L Right

3.2/50 33.9/+0.1 7.8/2.5/20 2.2/+0.7 1.8/20 35.1/+1.3 1.6/1.6/50

5.3/50 31.2/+0.8 4.9/23.9/-1.3 4.5/3.9/-0.7 21.2/-0.4 3.6/33.1/+2.2 3.5/3.4/50

7.0/50 26.2/-3.1 6.9/6.1/-2.8 25.6/-2.8 6.1/6.9/38 5.7/50

7.1/50 26.4/-3.2 6.7/6.8/-3.3 25.9/-2.6 6.1/5.9/4.1 5.1/50

7.4/50 25.8/-2.9 6.9/5.5/-1.7 24.2/-1.4 5.2/31.5/+1.0 5.3/5.6/50

6.9/50 24.4/-2.2 6.3/5.8/-1.9 33.6/-1.2 5.3/33.3/+1.5 5.1/5.0/50

5.6/50 31.8/+1.2 5.5/23.9/-1.3 5.5/5.9/-1.7 24.8/-2.4 6.6/6.4/50

6.2/50 30.5/+0.3 6.6/26.6/+2.2 6.6/7.0/-2.6 25.5/-2.8 7.2/7.0/50

7.8/50 26.8/-3.3 7.3/7.4/-2.9 6.3/7.1/-2.6 7.2/50

6.5/50 24.7/-2.1 6.7/6.8/-2.2 24.9/-2.4 7.0/7.5/50

10.4/50 10.0/23 9.8 9.4/18 12.0/28 12.0/41 10.0/46 9.4/50

8.8/50 9/30.1/+0.6 8.6/25.7/-1.9 8.6/9.0/-2.3 25.8/-2.9 9.6/9.7/32 9.8/50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R. L. & R.
		900.77 ✓			
+50				894.1	6.7
671				894.2	6.6
+50				894.3	6.5
672				894.3	6.5
+50				894.4	6.4
673				894.4	6.4
T.P	4.34	898.35 ✓	6.76	894.01 ✓	
674				894.5	3.9
675				894.6	3.6 3.8 4
+50				894.7	3.4 3.7 4
676				894.7	3.4 3.7 4
+50				894.8	3.3 3.6 3
677				894.8	3.3 3.6 3
T.P	3.05	900.03 ✓	1.37	896.98 ✓	
B.M.			1.65	898.38 ✓	898.37

Inst. .....
Rod. .....
Chain. .....

		Left		C L		Right	
W.	3						
		7.8/50	35.8/7.3 +1.9 / 21.5/7.2 −0.5	7.1 −0.4	21.4/7.1 −0.4	33.0/7.2 −2.0	7.2/50
		7.6/50	33.7/7.0 +2.1	6.0 +0.6	34.8/5.9 +0.7	6.0/50	
		6.2/50	5.3/21	5.0	5.1/22	5.1/50	
		6.8/50	36.3/6.2 +0.3 / 5.7/21	4.8 +1.7	4.5/21	31.1/4.3 +2.2	4.3/50
		7.1/50	6.0/24	4.9	4.1/22	3.6/50	
		7.2/50	33.7/6.7 +2.2 / 6.2/17	5.2 +1.2	4.4/23	27.3/3.8 +2.6	3.5/50
		5.1/50	32.4/4.8 −1.6 / 23.7/4.8 −0.9	4.7 −0.6	20.3/3.9 0.0	34.7/3.3 +0.6	2.6/50
				(3.8)			
+0.22		6.0/50	35.1/5.2 +0.9 / 23.3/4.7 −1.1	3.9 −0.1	35.4/2.9 +1.1	2.6/50	
−0.22							
				(3.7)			
+0.34		6.5/50	30.6/5.7 +0.3 / 26.0/5.5 −2.0	3.8 −0.1	2.8/22	35.9/2.5 +1.4	2.2/50
−0.34							
				(3.7)			
+0.34		6.9/50	27.7/5.9 −2.4	4.4 −0.7	2.8/15	36.0/2.4 +1.5	2.1/50
−0.34							
				(3.6)			
+1.34		7.2/50	26.0/6.3 −3.0	5.0 −1.4	3.7/20	35.9/2.7 +1.2	2.1/50
−0.34							
				(3.6)			
+0.34		6.3/50	30.3/5.6 +0.2 / 26.3/5.4 −2.1	4.8 −1.2	20.4/4.1 −0.2	34.5/3.4 −0.5	2.7/50
−0.34							

50' Rt. 14" Oak

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Cr.	B.
		900.03 ✓			L	C
+50				894.9	4.8	5.1
678				94.8	4.9	5.2
+50				94.7	5.0	5.3
679				94.6	5.1	5.4
+50				94.4	5.3	5.6
680				94.2	5.5	5.8
+50				93.9	5.8	6.1
681				93.6	6.1	6.4
+50				93.2	6.5	6.8
682				92.8	6.9	7.2
682+59.58 = 709+54.7				92.4	7.4	7.6
710				92.1		7.9
711				91.7		8.3
+46				91.6		8.4
T.P.			6.61	893.42 ✓		
712				91.2		

Inst.
Rod.
Chain.

8/10 24

Left C L Right

3

+0.34 -0.34

7.1/50 | 7.2/-0.1 | 6.9/-2.1 | 7.3/-2.2 | 7.3/-1.9 | 6.8/+1.1 | 6.4/42 | 6.0/50

+0.34 -0.34

6.7/50 | 6.6/40.8 | 6.7/-1.8 | 6.4/3 | 7.0/-1.8 | 6.9/-1.4 | 6.2/-1.8 | 5.5/50

4.9/50 | 5.2/+2.3 | 5.8/-0.8 | 5.8/+0.5 | 5.7/-0.1 | 5.6/0.0 | 4.9/50

+0.34 -0.34

4.1/50 | 4.0/+1.1 | 4.5/20 | 4.9/+1.0 | 4.5/20 | 4.3/+1.4 | 4.6/50

4.1/50 | 3.7/+1.6 | 3.8/20 | 3.8/+1.8 | 3.8/20 | 3.8/+2.1 | 3.8/50

+0.34 -0.34

4.1/50 | 4.0/+1.5 | 3.9/20 | 3.9/+1.9 | 3.8/20 | 4.0/+2.1 | 4.1/50

+0.34 -0.34

4.8/50 | 4.5/+1.3 | 4.5/20 | 4.5/+1.6 | 4.3/20 | 4.7/+1.7 | 4.9/50

+0.34 -0.34

5.6/50 | 5.5/+0.6 | 5.2/21 | 5.5/+0.9 | 5.7/24 | 6.2/+0.5 | 6.6/50

+0.34 -0.34

6.0/50 | 6.3/+0.2 | 6.5/0.0 | 7.2/-0.4 | 8.0/-0.9 | 8.3/+1.3 | 8.8/50

+0.34 -0.34

7.4 | 7.7/+1.7 | 8.1/-1.2 | 9.1/-1.9 | 10.6/-3.1 | 11.1/50

+0.22 -0.22

11.2/50 | 11.7/39 | 11.3/-3.9 | 11.6/-4.0 | 11.4/-3.6 | 11.4/50

11.2/50 | 11.1/-3.2 | 11.7/-3.8 | 12.0/4 | 11.3/+3.4 | 11.3/50

19.5/38 | 10.3/50

11.4/30 | 11.7/-3.4 | 11.7/15 | 12.7/11 | 12.7/9 | 11.4/4 | 11.8/-3.5 | 11.6/-3.3 | 11.9/50

13.1/35 | 12.0/41 | 12.0/30 | 11.3/50

11.4/31 | 11.8/-3.4 | 11.6/15 | 10.4/10 | 10.0/-1.6 | 10.3/10 | 11.4/15 | 11.4/-3.0 | 12.4/31 | 11.6/37

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	1.62	897.60		895.98	
T.P.	5.16	894.75	8.01	889.59	
712+00				91.4	3.4
712+50				91.3	3.5
713				91.1	3.7
714				90.8	4.0
+50				90.7	4.1
715				90.5	4.3
+45				90.4	4.4
716				90.2	4.6
717				89.9	4.9
718				89.6	5.2
T.P.	4.80	894.60	4.95		889.80
719				89.3	5.3
720				89.0	5.6
721				88.7	5.9

Inst. W.H.C.
Rod. A.L.P.
Chain. T.A.S. W.E.A.

Oct 2 1926 25

Left C.L. Right

R.R. Spike in Stp 70 Lt. 680+40

3.4
6.4 / √0 — 25.7 / 6.1 / -2.7 — 6.4 / 2.0 — √.6 / -2.2 — √.2 / 19 — √.7 / +0.7 — 10.C. / 31.1 — 4.8 / 4.3 — 4.1 / √0

3.0
3.7 / √0 — 24.1 / 3.3 / +0.2 — 20.0 / 3.5 / 0.0 — 3.8 / -0.3 — 5.5 / 0.0 / 20.0 — 3.7 / +0.2 / 33.5 — 3.6 / √0

3.1
3.1 / √0 — 35.0 / 2.9 / +0.8 — 3.1 / 2.0 — 3.8 / +0.7 — 8.7 / 6.0 / 20.0 — 3.3 / +0.9 / 34.9 — 3.8 / √0

4.9
4.8 / √0 — 26.1 / 4.4 / +1.1 — 21.8 / 4.6 / -0.6 — 4.2 / -0.2 — 4.9 / 0.0 / 20.0 — 4.0 / 0.0 / 33.8 — 3.5 / √0

4.1
8.2 / √0 — 28.4 / 8.2 / -0.1 — 7.7 / -3.6 — 6.7 / 17 — 5.6 / -1.5 / 24.5 — 4.9 / +1.7 / 32.6 — 4.2 / √0

4.3
8.3 / √0 — 28.0 / 8.3 / -4.0 — 8.7 / -3.9 — 8.1 / 16 — 7.8 / -3.0 / 26.0 — √.7 / √0

4.4
8.6 / √0 — 28.2 / 8.5 / -4.1 — 8.2 / -3.8 — 7.2 / 13 — 6.8 / -2.5 / 25.0 — 6.6 / +0.2 / 34.5 — D.C. — 6.3 / √0

4.6
7.0 / √0 — 8.5 / 4.3 — 6.1 / +1.0 — 24.8 / 6.2 / -1.6 — √.5 / -0.1 — 4.9 / -0.3 / 20.9 — 4.6 / 0.0 / 33.8 — 4.5 / √0

4.9
4.5 / √0 — 39.6 / 4.4 / +0.5 — 4.3 / 2.0 — 4.1 / +0.8 — 3.7 / 2.5 — 3.7 / +1.2 / 40.6 — 3.6 / √0

5.2
6.0 / √0 — 3.7 6.0 / +1.7 — 22.4 / 6.0 / -0.8 — √.8 / -0.6 — √.8 / -0.6 / 21.8 — √.2 / +2.3 / 33.5 — D.C. — √.3 / √0

5.3
√.6 / √0 — D.C. / 3.0 / +2.0 — 21.7 / √.7 / +0.4 — √.5 / -0.2 — √.1 / 2.0 — √.4 / 40.1 / 39.0 — 4.8 / √0

5.6
4.9 / √0 — 40.5 / 4.5 / +1.1 — 4.6 / 2.0 — 4.8 / +0.8 — √.4 / 2.0 — √.8 / +2.3 / 33.5 — D.C. — √.8 / √0

5.9
√.7 / √0 — 38.8 / √.9 / 0.0 — 22.1 / 4.6 / -0.7 — 4.6 / -0.7 — √.9 / 6.0 / 20.0 — √.1 / +0.8 / 40.0 — 4.6 / √0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. El.
		894.60			
722				888.4	6.2
723				88.2	6.4
B.M.	2.86	892.97	(4.59) →	88.01	
T.P.	5.11	892.19	6.20	886.67	
		892.08			
724				88.0	4.2 4.1
725				87.9	4.3 4.
726				87.8	4.4 4.3
T.P.	3.68	891.58	4.29	887.90	
		891.47		887.79	
727				87.7	3.9 3.8
728				87.6	4.0 3.9
729				883.6 87.5	4.0 4.1 8.0
730				83.4 87.4	4.1 4.2 8.2
731				83.2 87.3	4.1 4.3 8.4
T.P.	2.71	889.34	4.95	886.52	
732		889.23		83.0 87.4	1.9 1.8 6.3
733				82.8 87.3	1.9 6.
T.P.			3.33	886.01	1.8
				885.90	

In-t. W.A.C.
Rod. R.L.P.
Chain. R.A.S. W.A

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Left				C L		Right	
7.5 / 50	20 36.3 / 7.5 +1.2	7.8 / 1.1		7.2 (6) / -1.0	6.7 / -0.5 / 21.5	6.0 / +0.7 / 4.00	5.1 / 50
9.1 / 50	27.0 / 8.9 -3.5	8.9 / 78		8.5 (6) / -2.1	7.2 / -0.8 / 22.4	6.7 / +0.7 / 10.0 / 28.8	6.4 / 50
Spk. in 8" Oak 60' Lt. Sta. 731+25							
	7.0 / 50	6.7 / -2.5		5.9 / -1.7	5.6 / -1.4	5.2 / 41.5	5.1 / 50
1.0 / 50	6.6 / +0.2	6.7 / -2.9		6.5 / -2.2	4.6 / +0.3	3.4 / +0.9	3.0 / 50
7.2 / 50	7.0 / 35	6.8 / -1.4		4.7 / -0.3	4.0 / 20	3.6 / +0.8	3.5 / 50
6.8 / 50	6.6 / 35	6.2 / -2.3		4.4 / -0.5	3.5 / 20	3.0 / +0.9	3.0 / 50
	6.6 / 50	6.8 / -2.9		5.5 / -1.8	4.4 / -0.4	3.4 / +0.6	3.0 / 50
6.9 / 50	6.7 / +1.3	6.3 / +1.7	6.4 / -2.3	6.1 / -2.0	5.7 / +1.6	5.3 / +2.7	4.2 / 50
6.9 / 50	6.9 / +1.3	7.0 / +1.2	7.1 / -2.9	5.7 / -1.5	5.4 / -1.2	5.3 / +2.9	6.1 / +2.1	6.4 / 50
7.2 / 50	7.0 / +1.4	7.1 / +1.3	7.1 / +2.9	6.6 / -2.4	6.2 / -2.0	6.2 / +2.2	6.0 / +2.1	6.3 / 50
5.1 / 50	4.7 / +1.6	4.8 / +1.5	4.6 / -2.7	4.9 / -3.0	4.7 / +2.8	4.7 / +1.6	4.7 / +1.6	4.6 / 50
4.8 / 50	4.9 / +1.6	4.8 / +1.7	4.8 / -2.9	4.5 / -2.6	4.5 / -2.6	4.6 / +1.9	4.6 / +1.9	4.5 / 50
Nail in 6" Tree 50' Rt. Sta. 732							

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	3.20	889.52		886.32	
T.P.	4.35	884.80	5.07	884.45	
734				887.4	1.4
735				87.4	1.4
736				87.4	1.4
737				87.4	1.4
738				87.4	1.4
739				87.4	1.4
740				87.4	1.4
+36				87.4	
+55				87.4	
T.P.	6.42	889.17	6.05	882.75	
+70				87.4	1.8
741				87.4	1.8
742				87.4	1.8
T.P.	(Established Later)			882.77	

Inst. .....
Rod. .....
Chain. .....

8/10-1926

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	Left		C L	Right	
35' LH. 732 +85					
4.9 / 50	31.6 5 / 4.7 +1.5	31.6 5 / 4.7 +1.5	26.8 8 / 4.8 -3.4	4.7 -3.3	26.4 4 / 4.6 -3.2	31.2 2 / 4.4 +1.8	31.2 3 / 4.4 +1.8	4.4 / 50
4.7 / 50	31.8 8 / 4.6 +1.8	31.7 7 / 4.6 +1.8	26.8 8 / 4.6 +3.2	4.4 -3.0	26.3 3 / 4.4 -3.0	31.1 1 / 4.5 +1.9	31.8 9 / 4.5 +1.9	4.4 / 50
5.0 / 50	31.1 1 / 5.0 -1.6	31.1 1 / 5.0 +1.6	26.8 8 / 4.8 -3.4	4.8 -3.4	26.8 8 / 4.8 -3.4	30.9 9 / 4.5 +2.1	31.0 1 / 4.5 +2.1	4.9 / 50
5.3 / 50	31.8 9 / 4.9 +1.9	31.1 1 / 4.9 +1.9	27.4 4 / 5.1 -3.7	5.0 -3.6	27.2 2 / 5.0 -3.6	30.9 9 / 4.7 +2.1	31.1 1 / 4.7 +2.1	4.4 / 50
5.2 / 50	31.2 2 / 5.2 +1.8	31.8 8 / 5.2 +1.8	26.8 8 / 4.8 -3.4	4.8 -3.4	26.9 9 / 4.7 -3.3	30.2 2 / 5.2 +2.8	31.0 1 / 4.2 +2.8	4.0 / 50
5.4 / 50	31.1 1 / 5.8 1.9	31.0 0 / 5.8 +1.4	28.1 1 / 5.7 -4.3	5.0 -3.9	27.8 8 / 5.3 -3.9	30.7 7 / 4.9 +2.3	31.0 0 / 4.9 +2.3	5.1 / 50
5.8 / 50	28.7 7 / 5.7 +1.7	28.7 7 / 5.7 +1.7	28.0 0 / 5.7 -4.3	5.4 -4.0	28.1 1 / 5.6 -4.2	31.2 2 / 5.6 +1.8	18.9 9 / 5.6 +1.8	5.5 / 50
	6.1 / 50	6.1 / 16	6.0	6.5 / 11	7.2 / 13	7.0 / 23	7.1 / 31	8.3 / 50
	6.5 / 50	6.5 / 32	7.4 / 15	7.1 / 8	8.8	8.2 / 15	7.4 / 18	6.9 / 32	7.0 / 50
7.2 / 50	8.7 / 34	9.4 / 26	8.7 / 16	7.6 / 10	7.3	7.4 / 13	7.2 / 28	7.1 / 44	6.6 / 50
7.5 / 50	31.6 6 / 7.7 +0.5	31.6 6 / 7.7 +0.5	31.6 6 / 7.7 -5.9	7.1 -5.3	28.8 8 / 6.0 -4.2	31.8 8 / 6.2 +2.0	31.0 0 / 6.2 +2.0	6.4 / 50
6.8 / 50	28.8 8 / 6.7 1.5	31.6 6 / 6.2 1.5	29.9 9 / 6.3 -4.5	5.0 -4.0	26.8 8 / 5.2 -3.4	30.5 5 / 5.2 +2.5	31.6 6 / 5.2 2.5	5.2 / 50
6 Pop. 150' LH. 741 +85								

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Cr. F.
		889.17			
743				82.0 887.4	1.8
744				82.5 87.4	1.8
T.P.	5.04	893.81	0.40	888.77	
745				83.0 87.4	6.4
+50				83.5 87.4	6.4
746				83.5 87.4	6.4
+50				84.0 87.4	6.4
747				84.0 87.4	6.4
+65				87.4	6.4
748				87.4	6.4
+50		898.74		87.4	6.4
T.P.	6.0	~~898.74~~	1.07	892.74	
749				87.4	11.3
+50				87.4	11.3

Inst.
Rod.
Chain.

9-10-26

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Left	C L	Right
5.4/50 · 3.9 0/5.2/+2.0 · 3.1 0/5.2/+2.0 · 2.6 0/5.2/3.4	5.0/-3.2	2.6 0/4.8/-3.0 · 3.0 6/4.8/+2.4 · 3.9 4/4.8/+3.4 · 4.8/50
6.0/50 · 3.7 7/6.0/+0.7 · 3.3 3/6.0/+0.7 · 2.8 0/5.8/-4.0	5.6/-3.8	2.7 0/5.3/-3.5 · 3.1 5/5.2/+1.5 · 3.6 5/5.2/+1.5 · 5.3/50
(8) 60' Rt 746 · 9.9/50 · 3.2 2/9.9/+0.9 · 3.1 2/9.9/+0.9 · 2.6 6/9.7/-3.3	9.2/-2.8	2.4 5/9.2/-2.8 · 3 1/9.2/+1.6 · 3.8 6/9.3/+1.5 · 9.3/50
10.5/50 · 3.7 3/10.2/+0.1 · 3.3 3/10.2/+0.1 · 2.7 6/10.2/-3.8	9.8/-3.4	2.6 9/9.6/-3.2 · 3.3 7/9.7/+0.6 · 3.7 7/9.6/+0.7 · 9.3/50
9.3/50 · 3.8 0/9.3/+1.0 · 3.4 2/9.2/+1.1 · 2.5 4/9.1/+2.5	9.5/-3.1	2.6 8/8.2/+1.8 · 5.0 6/7.8/+2.5 · 5.0 8/7.5/+2.8 · 7.0/50
9.9/50 · 3.7 0/9.8/0.0 · 3.3 8/9.6/+0.2 · 2.4 0/9.5/+3.1	8.0/-1.6	2.3 0/7.4/+1.0 · 2.8 2/7.1/+2.7 · 3.0 0/6.8/+3.0 · 6.5/50
9.0/50 · 3.8 2/8.7/+1.1 · 3.2 0/8.8/+1.0 · 2.4 0/8.7/-2.3	8.8/-2.4	2.2 0/7.4/-1.0 · 2.9 3/6.6/+3.2 · 3.4 0/6.2/+3.6 · 5.7/50
8.1/50 · 2.5 0/6.4/0.0 · 5.9/20	5.3/+1.1	5.0/20 · 5.0 0/4.7/+1.7
5.0 0/5.3/+1.1 · 4.1/20	3.9/+2.5	3.7/20 · 5.0 0/3.7/+2.7
5.0 0/3.0/+3.4 · 2.2/20	1.7/+4.7	2.1/20 · 5.0 0/3.1/+3.3
5.0 0/6.5/+4.8 · 5.5/20	5.4/+5.9	5.9/20 · 5.0 0/7.4/+3.9
5.0 0/6.6/+4.7 · 5.4/20	4.9/+6.4	4.7/20 · 5.0 0/5.4/+5.9

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		898.74			
750				887.4	11.3
+50				87.4	11.3
751				87.4	11.3
+50				87.4	11.3
T. P.		✓	4.54	994.20	894.20
B.M.	1.64	898.41		896.77	
752				87.4	11.0
T.P.	2.36	890.39	10.38	888.03	
753				87.4	3.0
754				87.4	3.0
755				87.4	3.0
756				87.4	3.0
T.P.	6.78	892.50	4.67	885.72	
757				87.4	5.1
758				87.4	5.1
+50				87.4	5.1

L. t. .....
Rod. .....
Chain. .....

7/26/36

Left	C L	Right
60 8.2 / +3.1	5.8 / 20	4.9 / +6.4	4.3 / 20	60 5.0 / +6.3
50 8.9 / +2.4	6.2 / 20	4.8 / +6.5	4.0 / 20	50 4.3 / +7.0
50 9.6 / +1.7	7.2 / 20	4.9 / +6.4	3.8 / 20	50 2.8 / +8.5
50 9.9 / +1.4	8.0 / 20	6.2 / +5.1	4.6 / 20	50 3.3 / +8.0

Sill in 18" Oak 70 Ft Sta. 744+60

50 7.8 / +1.2	9.2 / 50	7.6 / +4.4	6.8 / 20	50 6.3 / +5.1
52 / 50	9 4.9 / -1.9	6 5.0 / -2.0	4.8 / -1.8	8 4.6 / -1.6	5 4.5 / -1.5	4.4 / 50
6.4 / 50	2 6.1 / -3.1	6.0 / -3.0	6 6.0 / -3.0	6.1 / 50
6.4 / 50	6 6.4 / -3.4	6.3 / -3.3	6 6.0 / -3.0	5.8 / 50
6.4 / 50	4 6.1 / -3.1	5.9 / -2.9	5 5.9 / -2.9	5.8 / 50
8.0 / 50	5 8.0 / -2.9	7.6 / -2.5	6 7.4 / -2.3	7.5 / 40	7.2 / 50
5.9 / 50	7 5.5 / -0.4	6 5.3 / -0.2	4.8 / +0.3	4.9 / 20	4 4.7 / +0.4	5.0 / 50
5.2 / 50	4 4.8 / +0.3	4.3 / 20	4.0 / +1.1	4.0 / 20	5 4.2 / +0.9	4.3 / 50

Original Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		892.50			
759				887.4	5.1
+50				87.4	5.1
T.P.	7.14	893.73	5.93	886.57	
760				87.3	4.4
761				87.2	4.5
762				87.0	4.7
763				86.8	4.9
T.P.	4.27	892.70	5.30	888.43	
+40				86.7	4.0
764				86.6	4.1
+50				86.5	4.2
765				86.4	4.3
766				86.2	4.5
+30				86.1	4.4

Inst.
Rod.
Chain.

7/30/46

30

Left C L Right

6.0		5.2		5.1		4.7		4.6		4.6	4.8
50	3°	-0.5	2°	00		+0.4		20	8°	+0.5	50
		7.5		7.1		6.9		6.5		4.5	
		50	4°	-20		7.8	2°	-1.4		50	
		8.2		7.8		7.8		7.5		7.0	
	5°	7.8	2°	-1.4		-1.4	2°	-1.1	5°	-0.6	
		7.2		6.7		6.0		5.2		4.1	
	5°	-0.7	2°	-0.2		+0.5		20	5°	+2.4	
		6.1		5.5		4.1		3.1		1.8	
	5°	+0.6		20		+2.6		20	5°	+4.9	
		7.4	5.4	5.0	5.5	5.7	5.4	4.3		3.1	
	5°	-0.5	55	50	30	20	+1.5	20	5°	+3.8	
		4.8	5.6	4.3	4.7	4.2		3.2		2.6	
	5°	-0.8	33	24	20	+1.8		20	5°	+3.4	
		6.2	5.6	4.6	5.2	5.6			5°	4.7	
	5°	-0.1	21	14	+0.9	20			5°	+1.4	
		5.8	5.6	4.4		5.3	6.0		5°	4.9	
	5°	+0.4	16	+1.8		11	24		5°	+1.3	
		5.1	5.6	5.2		4.4	5.5	5.8	5°	5.5	
	5°	+1.2	24	+1.1		11	22	34	5°	+0.8	
		6.1		6.5		6.6	4.4	5.8	5°	6.7	
	5°	+0.4	40°	00		-0.1	17	30	5°	-0.2	
			6.5	6.4		6.8	6.8	6.6	7.3	7.7	
			50	21		-0.2	25	54	44	50	

Original Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		892.70			
767				886.0	6.7
768				85.8	6.9
T.P.	5.66	891.54	6.82	885.88	
769				85.6	5.9
+16				85.6	5.9
+25				85.6	5.9
B.M.			4.88	886.66	
+50				85.5	6.0
+68				85.5	6.0
+83				85.5	6.0
770				85.4	6.1
+50				85.3	6.2
	2.18	887.83	5.89	885.65	
771				85.2	2.6
+38				85.1	2.7

Inst. P.T. Co. No. 6
Rod. Beethaum
Chain Rectangular Notes

7/26/26

Left			C L		Right	
					6.8	7.3 X
5 0 / 8.2 +1.5	0 / 7.2 -0.5	7.4	4.7 / 7.5 -0.8		4.6	5 0 / -0.6
5 0 / 7.5 -0.6	7.5 -0.6	7.4 -0.5	3 / 7.5 -0.6		7.7 4.1	5 0 / 7.2 -0.3
5 0 / 6.3 -0.4	0 / 5.9 5 / 0.0	5.7 +0.2	5.7 2.0		5 0 / 5.7 +0.2	
6.3 5.0	5.6 2.3	5.4 +0.7	6.3 1.6		6.0 5.3	4.5 4.6	4.8 5.0
5.4 5.0	5.7 3.3	6.3 2.5	6.6 -0.7	6.2 2.8	4.8 4.1	4.6 5.0
Spk in 24" Oak 75' Lt. Sta. 76 9 + 40						
	5.8 5.0	5.6 1.8	5.0 +0.5	5.0 4.0	5.2 5.0	
	5.8 5.0	6.0 1.7	5.8 +0.2	5.0 1.1	4.1 5.3	4.1 5.0
4.1 5.0	6.5 3.8	5.9 2.4	4.8 1.8	4.7 +1.3	4.1 2.6	4.0 5.0	
	5 0 / 6.4 +0.7	4.8 2.0	4.3 +1.8	4.2 2.0	5 0 / 4.1 +2.0	
	5 0 / 5.7 +0.5	5.0 2.6	4.8 +1.4	4.8 1.7	5 0 / 6.2 +1.0	
	5 0 / 2.7 -0.3	5.3 2.0	2.7 -0.1	4 / 5.2 -0.6	5 0 / 3.6 -1.0	
5 0 / 3.7 -1.0	5 3 / 4.5 -1.6	4.7 -1.0	5 4 / 6.5 -2.8		5 0 / 5.7 -3.0	

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.	
		887.83			℄	D
772				885.0	2.8	7
T.P.	2.41	886.84	3.40	884.43		
773				84.8	2.0	7.
774				84.5	2.3	7.
775				84.0	2.8	8
776				83.4	3.4	8.
T. P.	2.82	885.98	5.78	881.06	881.16	
777				8>.8	1.2	6
778				8>.>	1.8	7.
TP.	1.96	882.43	3.51	880.47		
779				81.6	0.8	5.
X 780				81.0	1.4	6.4
781				80.1	2.0	6
782				79.8	2.6	7.
783				79.2	3.2	8.

Inst. .....
Rod. .....
Chain. .....

H.J.G. 7/30-1926 32
A.L.B
G.W. .....

Left C L Right

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.	
		882.43			℄	D
784				878.6	3.8	8.
T.P.	2.56	880.59	4.40	878.03		
T.P	3.00	881.03		878.03		
785				78.0	3.0	7.
T.P	5.0	880.53	5.5	875.53		
786				72.5 77.4	3.1	8
T.P	5.4	879.83	6.1	874.43		
787				71.9 76.7	3.1	7
T.P.	6.07	880.12	6.54	874.05		
788				76.0	4.1	8
789				75.0	5.1	9.
790				73.8	6.3	
+30				73.5	6.6	
791				73.5	7.6	
+50				71.9	8.2	
792				71.7	8.9	
B.M	5.37	880.02	5.37	874.75	874.65	
+50				70.6	9.4 (6.5)	

Inst. ..... New BM
Rod. ..... 8.75 & 9
Chain. 4.83 .....

100' Rt Sta 786+55
Spike in Root of Triple Birch.

33

Left	C L	Right
6.7 / 50	6.4 / 50	6.4 / 50
6.5 Rt Sta 784+85 3" Triple tree		
5.4 / 50	4.6 / 4.6 / 4.6 / 4.6 / 4.4 / 50	
5.9 / 50	5.7 / 5.5 / 5.6 / 5.4 / 5.1 / 50	
5.3 / 50	5.4 / 5.5 / 5.3 / 4.9 / 5.0 / 50	
7.4 / 7.6 / 7.6 / 7.4 / 7.3 / 7.0 / 6.8 / 6.8 / 7.3 / 50		
8.3 / 8.3 / 8.3 / 7.6 / 7.4 / 7.1 / 7.3 / 6.6 / 50		
8.6 / 8.2 / 8.9 / 7.8 / 6.8 / 6.9 / 6.1 / 4.7 / 50		
9.2 / 8.6 / 7.8 / 7.4 / 6.0 / 4.7 / 5.0 / 5.0 / 50		
7.4 / 8.1 / 7.9 / 6.8 / 6.7 / 5.6 / 4.5 / 3.3 / 2.7 / 50		
10.1 / 8.7 / 8.1 / 7.2 / 6.6 / 5.7 / 5.6 / 3.9 / 4.0 / 50		
11.2 / 10.5 / 10.2 / 8.0 / 7.0 / 6.5 / 6.7 / 50		
11.9 / 11.6 / 11.4 / 10.5 / 10.1 / 9.9 / 9.7 / 50		

Cross Sections

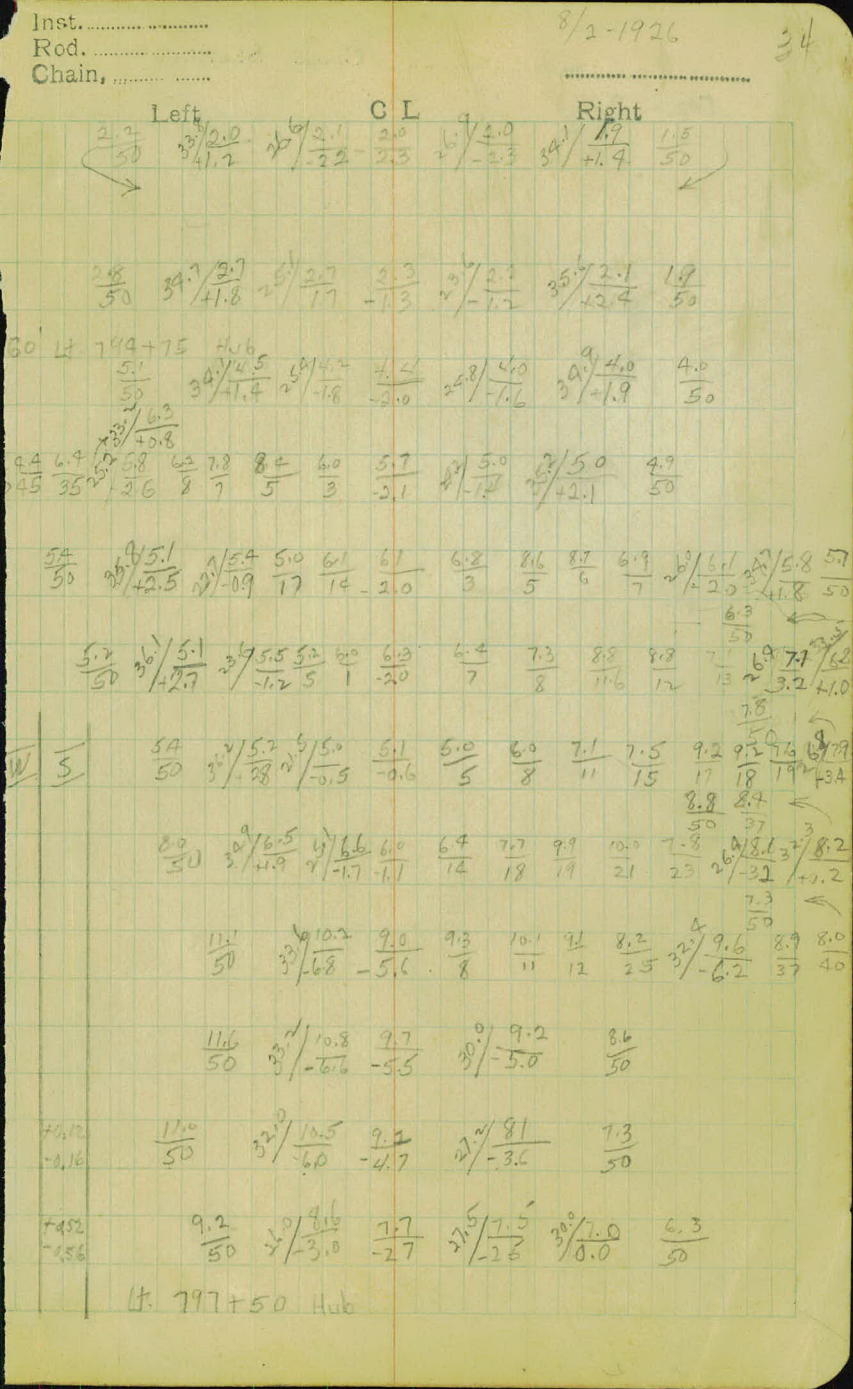
Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
T.P.	1.45	869.62 ✓	11.85	868.17 ✓	
793				869.9 -03	
794				68.6 1.0	(8.)
T.P	2.98	869.66 ✓	2.94	866.68 ✓	
795				67.3 2.4	(3.
796				66.1 3.6	(10
+50				65.6 4.1	(11
+77				65.4 4.3	(11
* 797				65.2 4.5	
+50				64.8 4.9	
T.P.	2.41	867.81 ✓	4.26	865.40 ✓	
798				64.4 3.4	
799				63.6 4.2	
+42				63.3 4.5	
				℄ R.	
800				63.8 5.0	4.5
T.P.	4.58	867.60 ✓	4.79	863.02 ✓	

Inst. .....
Rod. .....
Chain, ...

8/2-1926

34

Left C L Right



Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.	
		867.60 ✓				
801				867.0	5.6	4.1
T.P.	10.99	868.29 ✓	10.30	857.30 ✓		
802				61.2	7.1	5.6
* 803				60.4	7.9	6.4
162				59.7	8.6	7.1
804				59.2	9.1	7.6
163				58.0	10.3	8.8
805				57.2	11.1	9.6
T.P.	2.16	859.68 ✓	11.59	856.70 ✓		
806				54.8	4.9	3.4
150				53.6	6.1	4.6
B.M	3.56	854.63 ✓	8.55	851.13 ✓	851.0	
807				52.4	2.2	0.7
117				52.0	2.6	
150				51.0	3.6	2.2

Inst. .....
Rod. .....
Chain. .....

8/3-1926 Cloudy 35

W	S	Left			C L		Right		
2.0	+1.24 / -1.48	7.8 / 50	36.5 / 7.2 / +2.1	22.0 / 6.8 / 2.0	6.2 / -0.6	23.4 / 5.8 / -1.7	31 / 5 / 5.6 / +1.5	5.1 / 50	
2.0	+1.24 / -1.48	7.0 / 50	36.4 / 6.6 / +1.7	6.3 / 21	5.5 / +1.6	4.9 / 23	35.3 / 4.6 / +1.0	4.2 / 50	
2.0	+1.24 / -1.48	7.7 / 50	38.4 / 7.3 / +1.8	7.0 / 22	6.2 / +1.7	35.4 / 5.2 / +1.2	4.9 / 50		
2.0	+1.24 / -1.48	9.0 / 50	38.3 / 8.2 / +1.6	7.4 / 25	5.6 / +3.0	4.6 / 21	38.3 / 4.1 / +3.0	3.6 / 50	
2.0	+1.24 / -1.48	10.5 / 50	36 / 9.7 / +0.6	8.5 / 25	6.4 / +2.7	5.1 / 23	38.3 / 4.6 / +3.0	3.5 / 50	
2.0	+1.24 / -1.48	13.2 / 50	33.5 / 13.0 / 1.0	12.3 / -0.8	10.2 / +0.9	8.5 / 3	37.1 / 6.6 / +2.2	4.8 / 50	
2.0	+1.24 / -1.48	14.5 / 50	33.5 / 13.8 / +1.0	13.5 / -1.2	12.1 / -1.0	10.1 / 19	20 / 9.9 / -0.3	36.1 / 8.0 / +1.6	5.7 / 50
2.0	+1.24 / -1.48		9.7 / 50	25.4 / 7.8 / -1.7	6.2 / -1.3	24.4 / 4.8 / -1.4	35 / 4.2 / +1.7	3.8 / 50	
2.0	+1.24 / -1.48		11.5 / 50	28 / 10.3 / -3.0	8.5 / -2.4	34.3 / 6.7 / -2.3	30.8 / 6.6 / +0.5	5.5 / 50	
2.0	+1.24 / -1.48	Culv. Rt. 808+66	10.5 / 50	36.2 / 10.0 / -6.6	7.4 / -5.2	28.7 / 4.8 / -0.1	36.1 / 3.8 / +2.7		
2.0	+1.24 / -1.48			10.5 / 50	10.3 / 23	9.5	9.0 / 12	6.7 / 27	4.4 / 47	4.0 / 50
2.0	+1.14 / -1.40	11.6 / 21	12.1 / 17	25 / 11.3 / -6.6 / 13.2 / 15	11.1 / 50 / 14.4 / 9	11.6 / 8	10.5 / -6.9	31.6 / 8.0 / -5.8	7.8 / 32	6.2 / 50

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R. L	Gr. R. C	Gr. R. R
		859.63 ✓					
808				850.5	5.1	4.1	3.9
+44				50.2	4.9	4.4	3.9
+66				50.1	4.8	4.5	4.2
T.P.	5.88	847.52 ✓	12.99	841.64 ✓			
T.P. +98	6.79	853.88 ✓	0.43	847.09 ✓ ~~49.8~~			
B.M.	12.07	863.09 ✓		851.07			
T.P.	8.78	869.94 ✓	1.93	861.16 ✓			
808+98				49.8			
809+00				49.5			
+06				49.5			
+14				49.4			
+42				49.3	4.6		
+55				49.2	4.7		
810				49.0	4.9		
T.P.	8.64	859.71 ✓	2.81	851.07			
+80				48.6	11.1		
811				48.5	11.2		

Inst.
Rod.
Chain.

Left C L Right

W. | S.

+0.98 / -1.18

+0.48 / -0.52

+0.32 / -0.32

+0.10 / -0.16

S.W. cor. Top Slab Culv. at 809+42

Face Cap = 40/39

" " = 40/39

Top Rail 40

Face Cap = 39

Top Slab

S.W. Cor. Culv. Rt. 809+42

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		859.71 ✓			
+37				848.4	11.3
+58				48.2	11.5
+70				48.1	11.6
812				48.0	11.7
T.P.	850	867.81 ✓	0.40	859.31 ✓	
+30				47.8	20.0
+56				47.7	
+85				47.7	
813				47.7	20.1
+22				47.7	20.1
+36				47.7	20.1
+63				47.6	20.2
814				47.6	20.2

Inst. .....
Rod. .....
Chain. .....

Left				C L			Right	
6.3 / 50	4 3/5.6 / 57		5.5 / 20	5.9 / +5.4	6.3 / 20	4 3/6.8 / 5.0		6.6 / 50
7.2 / 50	4 3/7.1 / 44	7.3 / 20	7.11 / 14	5.5 / 5	5.2 / +6.3	5.4 / 20	4 3/5.1 / +6.4	5.0 / 50
+3.8 / 50	6.2 / 50	4 3/6.8 / 9.8		7.4 / 20	7.9 / +3.7	6.0 / 20	5.2 / 31	4 3/4.5 / 7.0	4.8 / 50
	1.8 / 29	3.2 / 20	5.0 / 8	5.7 / +6.0	6.6 / 20	4 3/6.5 / 5.2		6.3 / 50
5 3/8.1 / +12.0	7.4 / 27	8.9 / 17	9.8 / +11.3	8.7 / 6	3.9 / 30	2.8 / 50		
50 / 7.9 / 12.2	6.0 / 20	5.9 / 13	9.2 / +10.9	10.0 / 3	10.2 / 20	10.5 / 42	4 3/9.1 / 10.2	9.9 / 50	9.5 / 50
50 / 6.9 / 13.2		5.6 / 20	5.0 / +15.1	7.5 / 17	10.1 / 28	4 3/11.1 / 9.0		11.0 / 50	
50 / 6.7 / +13.5	5.9 / 20		5.3 / +14.9	5.2 / 20	5.7 / 46	50 / 6.1 / +14.1			
50 / 7.7 / +12.5	7.4 / 20		7.7 / +12.5	7.7 / 20	50 / 7.7 / +12.5				

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		867.81 ✓			
+41				847.6	20.2
815				47.5	20.3
+50				47.4	20.4
816				47.4	20.4
T.P.	2.87	859.71 ✓	10.97	856.84 ✓	11.9
817				47.3	12.4
+50				47.1	12.1 12.6
818				47.0	12.2 12.7
T.P	0.86	848.39 ✓	12.18	847.53 ✓	
+36				46.9	1.0 1.5
+51				46.7	1.2 1.7
+68				46.7	1.2 1.7
+74				46.7	
+94				46.7	

Inst.
Rod.
Chain.

		Left		C L		Right	
W	S						
		10.2 / 50 4 9 / 10.2 / 84	10.6 / 20	10.9 / -9.3	11.1 / 20	4 / 11.1 / +9.1	11.1 / 50
		11.9 / 50 4 6 / 11.9 / 84	11.7 / 20	11.2 / +9.1	11.3 / 20	4 / 11.2 / 9.1	11.2 / 50
		11.1 / 50 4 9 / 10.9 / +9.5	10.6 / 20	10.6 / +9.8	10.8 / 20	8 / 11.7 / 8.7	11.7 / 50
+0.04		12.5 / 50 4 5 / 12.7 / -7.7	12.8 / 20	12.9 / +7.5	13.7 / 20	4 6 / 13.4 / +7.2	13.4 / 50
-0.16							
		Nail in ∅ Oak 85 Rt 815+55					
+0.52		6.3 / 50 4 / 6.5 / 5.4	6.9 / 20	7.2 / +5.2	7.1 / 20	4 / 7.2 / +5.7	7.1 / 50
-0.52							
+0.52		5.5 / 50 4 9 / 6.4 / +5.7	6.8 / 20	7.4 / +5.2	7.9 / 20	4 9 / 8.4 / +4.7	8.4 / 50
-0.52		9.7 / 40 13.7 / 44	12.0 / 50				
+0.52		9.5 / 127 9.8 / 77	7.1 / 27	7.5 / 22	10.1 / 18	10.7 / +2.0	11.5 / 20	3 8 / 12.5 / +0.7	12.5 / 40	12.6 / 50
-0.52		41 / 37 2.8 / 4.6	3.0 / 50							
+0.52		3.5 / -2.5	5.0 / 20	7.9 / 17	7.5 / 14	5.3 / 4	5.0 / -3.5	5.4 / 15	7.9 / 32	2 8 7 / 16.1 / -14.1	16.1 / 50
-0.52		6.1 / 50									
+0.52		8.7 / 34 4 0 / 4.7 / -3.5	5.1 / 15	11.0 / 2	11.3 / -9.6	13.5 / 18	15.6 / 26	4 0 / 17.1 / -14.9	
-0.52		9.8 / 44 2.4 / 5.1									
+0.52		4 / 5.5 / -4.3	4.3 / 24	7.8 / 10	5.7 / 7	6.0 / -4.3	6.4 / 7	10.7 / 27	4 0 / 12.0 / 11.3		
-0.52		8.2 / 41	12.6 / 50								
+0.52		3 / 6.7 / -3.5	6.0 / 23	9.1 / 18	10.2 / 4	5.7 / -4.0	7.0 / 22	13.0 / 45	4 0 / 18.6 / -16.4		
-0.52											
+0.52		4 0 / 17.5 / -16.3	10.9 / 28	14.5 / 11	15.2 / -13.5	15.1 / 16	2 / 8.0 / 5.8	8.6 / 41	13.4 / 50		
-0.52											

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
	0.23	848.39 / 836.46 ✓	12.16	836.23 ✓	L. & R. 10.7 -9.7
819				846.7	-10.2
			9.98	826.48 ✓	
+42				46.6	
+50				46.5	
B.M.	3.77	835.90 ✓	4.34	832.12 ✓	832.13 ✓
820				46.4	-11.0 -10.5 -
+16				46.3	-10.9 -10.4 -
B.M.	4.01	836.14 ✓	3.97	832.13 ✓	
+64				46.2	-10.6 10.1
+75				46.1	-10.0
821				46.1	10.5 10.0 -
+65				46.0	-10.4 9.9 -
822				45.9	-10.3 -9.8 -
+25				45.9	10.3 9.8 -
+28					

Inst. .....
Rod. .....
Chain. .....

Ele B.M. 8-7-44 N.W. Cor. of Radius Curb of Bridge

39

W S

Left C L Right

+0.52 / -0.52

Water El. 9/14

CREEK

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

+0.52 / -0.52

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
B.M.	6.54	838.67	4.01	832.13	℄ R. L.
+50					
+73				845.9	-7.2 -6.7 -
+88					
			7.0		℄ R. L.
823				46.0	-7.3 -6.8 -7
+44				46.1	-7.4 -6.9 -
T.P	7.06	843.95	1.78	836.89	
+54				46.1	-2.1
+62				46.1	-2.1 -1.6 -
+65				46.1	-2.1 -1.6 -3
+76				46.2	-2.2
+87					
		841.24	?	O.K. Taken by P. Coone	
					-5.1 -4.4 -5
824				46.2	-5.1
+38				46.5	-5.3 -4.8 -5
+83				46.7	-5.7
825				46.7	-5.7
	10.64	851.56	0.32	840.92	
	8.80	859.56	0.80	850.74	

Inst.
Rod.
Chain.

4/0

W	S	Left	C L	Right
	+0.52			
	-0.52			
	+0.52		9.7 9.0 7.1 5.6 5.7 3.1 2.9	
	-0.52		-16.9 6 10 15 33 -9.8 50	
	+0.52			
	-0.52			
	+0.52	6.5 5.5	5.1 4.4 4.0 4.0	
	-0.52	-14.3 27	-12.4 28 -10.8 50	
	+0.52	3.9 4.9 6.1 5.7	5.0 4.0 3.9 3.2	
	-0.52	50 -12.8 44 35	-12.4 22 -10.7 50	
	+0.52	0.2 2.2 7.7 10.3 10.5 6.5 6.1	6.1 6.7 5.6 5.9 8.6 9.6 8.0	
	-0.52	50 40 28 19 13 4	5 8 14 17 24 35 50	
	+0.52	5.7 6.6 7.2		
	-0.52	3.6 -9.2 50		
3.4	3.4 7.1 9.6 9.6 6.6	5.9 4.4 3.4 2.6 1.1		
0.0	2.0 11 9 3	-8.0 16 17 -6.2 50		
+0.52	7.2 5.4 6 5.6 7.6 8.5 9.1	8.8 7.0 6.2 6.9 8.2 8.4		
-0.52	27 17 13 11 8 5	2 9 17 30 41 50		
	6.9 50			
	+0.52			
	-0.52			
		5.6 (-5.1)		
	+0.52	4.1 4.5 4.4 5.2	5.4 5.6 4.7 6.1 6.1 4.1 4.2	
	-0.52	50 -10.1 26 10	11 19 23 27 -9.6 46 50	
		Above H.I.		
	+0.52	4.3 6.2 5.0 5.3 4.8	(-5.3) 5.3 6.3 8.9	
	-0.52	50 -9.7 24 18 -10.1	14 34 58 2 to 6	
		Above H.I.	(-5.7)	
	+0.52	+14.2 +14.5 +10.0 10	5.8 5.0 7.1 9.4 2 to 6	
	-0.52	50 40 34 8	4 12 24	
	+0.52	+14.0 +14.0 +8.4 +3.3 2.0 2.0 (-5.7)	4.7 6.5 7.4 9.0	
	-0.52	50 38 30 11 2 -7.7	4 18 32 35	

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		859.56			
+33				847.X	12.7 12.9 11
+65				47.4	
826				47.6	12.0 12.5
827				48.3	11.3 11.6
+27				48.5	
+40				48.6	11.0
828				49.1	10.5 11.0
829				50.0	9.6 10.1 9
+50				50.5	9.1 9.6 8
830		858.98		51.0	8.6 9.1 8
13.19	5.20	859.98	5.77	853.77	853.78
+21				51.2	8.2
+43		59.0 / 11.2		51.4	8.0 9.1 8
+71				51.7	8.3
831				52.0	8.0 8.5
+47				52.5	7.5 8.0 7

Inst.
Rod.
Chain.

W	S	Left					C L				Right			
							(2.2)							
	+0.52	4.6	4.8	4.6	4.6	4.2	16.0	20.8	4.8	4.2	20.7			
	-0.52	50	4.3	7.3	21	18.2	19	27	-9.3	50				
	+0.52		4.6	4.7	4.5	4.7	(12.4) 4.5	10.7	14.0	17.0	21.3			
	-0.52		50	44	26	25	24	38	45	50	21			
	+0.52	5.0	4.8	5.0	4.9	4.7	(12.0) 4.6	5.4	4.6	4.2				
	-0.52	50	4.3	7.6.5	33	17.7	30	4.5	17.9	50				
	+0.52	5.3	4.9	5.3	5.3	5.2	(11.3) 5.3	5.3	5.3	5.5				
	-0.52	50	4.3	7.6.5	24	16.3	24	4.3	7.6.5	50				
	+0.52			5.2	5.2	5.0	5.2	5.4						
	-0.52			50	30	(11.6)	24	50						
	+0.52						(10.6)							
	-0.52													
	+0.52			7.9	6.6	6.2	6.4	6.6		6.6				
	-0.52			50	3.4 7.3.4	27	16.3	26	4.1 7.4.2					
	+0.52			7.9	5 7.3	7.4	6.9	(9.6) 6.4	3 7.6.6	6.6				
	-0.52			50	3.4 7.1.3	29	17.7	24	3.9 7.3.5	50				
	+0.52	6.6 50	7.1	5.0 7.2.5	8.2	7.9	7.8	7.2 (9.1)	6.7	3 7.6.6	6.6			
	-0.52	4.4	7.1	5.0 7.2.8	51	24	18	17.9	27	3 7.5.0	50			
	+0.52	4.5 50	4.8	4.8	4.0	6.9	7.8	8.0	7.1 (8.6)	6.8	3 7.6.8	6.8		
	-0.52	8 7.1.9	5.7	5.2	18	14	4	3	17.6	2.5	0 7.2.3	50	=+1.8	
		Split. 1.4 T. N. 2.7 5.7 7. 9.6 5 +1.0.												
	+0.52	5.0	5.2	6.2	6.6	7.2	8.1	8.3 (8.8)	8.0	7.1	7.2	6.9	6.7	
	-0.52	50	2.7	37	30	13	8	+0.5	3.0	6	32	50		
	+0.52	5.1 50	5.2	6.2	6.6	7.0	8.0	8.4 (8.6)	8.4	7.2	6.9	3 7.4 6.7	6.6	
	-0.52	3.8 5.1.5	+3.1	27	19	7	4	+0.2	6	10	25	+2.4	50	
	+0.52	5.2	5.0	5.0	6.0	6.6	7.0	8.5	8.2	7.1	6.9	6.6		
	-0.52	50	40	26	24	19	(8.3)	9	16	18	25	50		
		5.2 46		6.2 48	7.0 50									
	+0.52	4.9	4.8	5.3	6.0	6.1	6.8	7.3	8.1	8.2	7.1	7.1	7.1	
	-0.52	3 5.2.6	33	20	17	10	+1.2 (8.0)	9	18	21	24	+1.9	50	
		6.8 52		6.7 40	6.0 46	6.0 50								
	+0.52	3 5.1.5	4.8	5.0	6.5	6.4	5.9	6.3	6.3	5.8	6.3	7.6	7.0	6.5 6.5
	-0.52	4.0	26	14	8	6	+1.6	7	14	17	21	27	+1.0	36 50
							(7.5)							

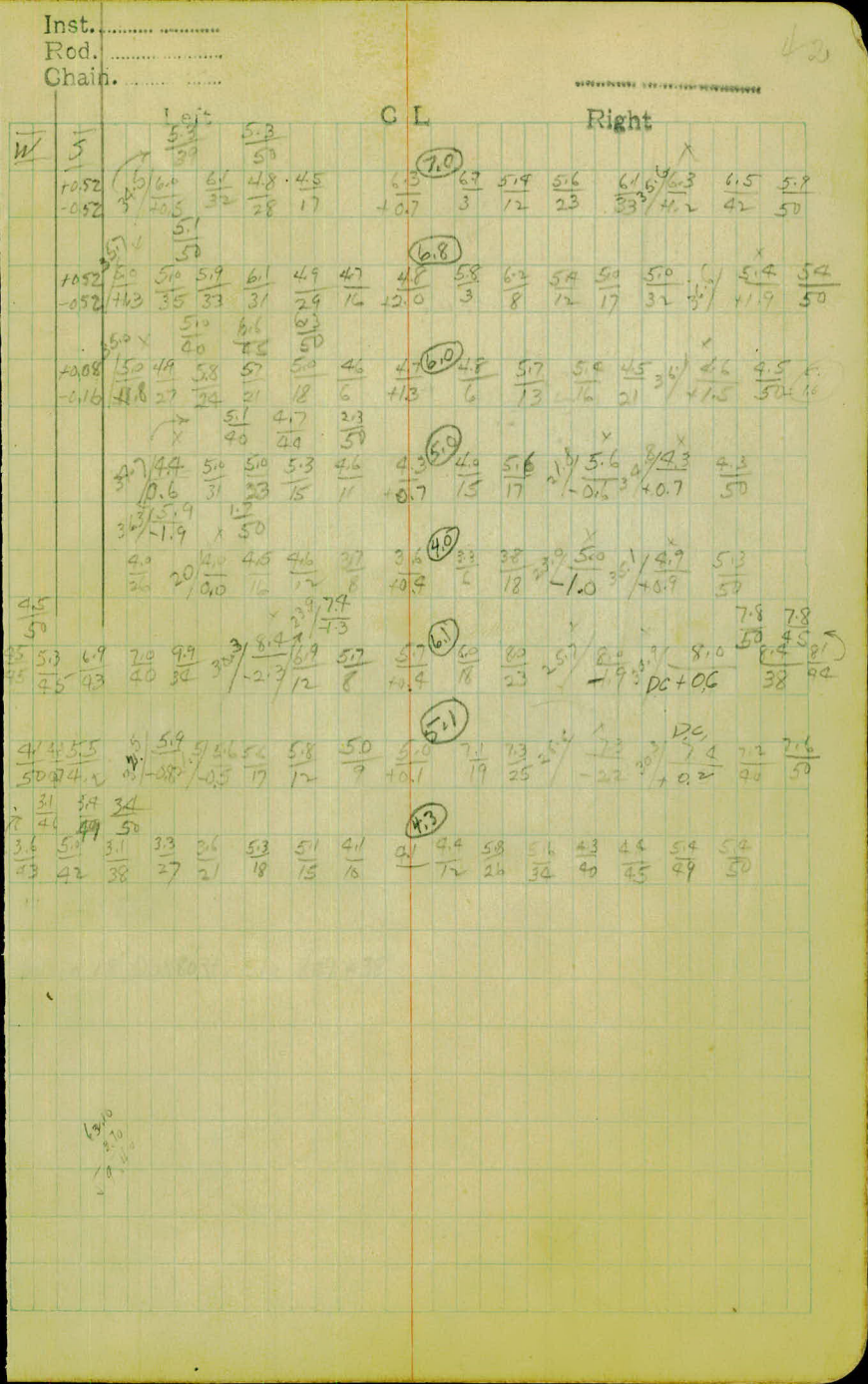
60.0

Cross Sections

Sta.	B. S.	H. I.	F. S.	Grade	Gr. R.
		858.98			± L. R.
832		859.98		853.0	7.0 7.5 6.5 Δ
+23				53.2	6.8 7.3 6.7
833				54.0	6.0 6.1 5.
834				55.0	5.0
835				56.0	4.0
		862.10		856.17	
T.P.	5.93	863.10	2.81	857.17	
836				57.0	6.1
837				58.0	5.1
+84 (END OF DIV. C.)				58.8	4.3
B.M.			3.70	859.40	859.40

Inst. .....
Rod. .....
Chain. .....

Left C L Right



Readings to Check Original X-Sec.

Sta. 830 To 837

B.M.	1.06	260.46		259.40	
837				58.0	2.5
836				57.0	3.5
835				56.0	4.5
834				55.0	5.5
833				54.0	6.5
832				53.0	7.5
831				52.0	1.5
+43				51.4	9.1
830				51.0	9.5

W.H.C.

Sept 28, 1926

A.L.P.

W. A.

R.

21.5 / 3.0 / -.05

23 / +0.2

23.9 / 4.8 / -1.3

6.1

5.5 / +1.0 / 23.0

4.8 / 50

49 / +1.6 / 50

V. +18 5.1 / 50

7.2 / 50 = +1.3

7.3 / +18 /

7.6 / 50 = +1.4

F.E. Sta. 827 +27

Right

Sta.	B.S.	H.I.	F.S.	Grade.	Gr. R.
B.M.	5.60	859.38		853.78	
0+25				51.1	8.3
+55				54.1	5.3

Left

0+25				51.2	8.2
0+50				53.7	5.7

11.1 | 5.2 +3.1 | 5.1 +3.2 | 5.2 3.1 | 11.1

8.2 | 5.1 +0.2 | 5.0 +0.3 | 5.1 +0.2 | 8.2

11.1 | 5.1 3.1 | 5.3 +2.9 | 5.3 +2.9 | 10.9

8.3 | 5.4 +0.3 | 5.6 +0.1 | 5.4 +0.3 | 8.3

Channel Change Right 819+40

Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
	4.13 6.64	836.26 ✓ 835.94 ✓	4.96	832.13 831.30	
0+00				825.1	10.5 ✓
+22				25.2	10.7 ✓
+46				25.3	10.6 ✓
T.P.	7.05	842.58 ✓	0.41	835.53 ✓	
+56				25.3	17.3 ✓
+66				25.4	17.2 ✓
+78				25.4	17.2 ✓
1				25.5	17.1 ✓
+29				25.6	17.0 ✓
T.P.	0.92	834.6 ✓	8.90	833.68 ✓	
+75				25.8	8.8 ✓
2				25.9	8.7 ✓
+22				26.0	8.6 ✓
+40				26.1	8.5 ✓

8/5-1926 45

Lt. ℄ Rt.

30' Lt. 822+00

9.1 / 20 | 11 9 / 8.9 / +1.9 | 9.0 / 10 | 5.1 / 3 | 5.0 / +5.8 | 5.9 / 8 | 4.9 / 5.9 / +4.9 | 5.7 / 20

4.4 / 20 | 16.1 / 4.6 / +6.1 | 5.3 / 11 | 5.6 / +5.1 | 5.7 / 10 | 15 / 5.6 / +5.1 | 5.4 / 20

Above H.1. ↖

3.0 / 20 | 12 4 / 3.2 / +7.4 | 3.3 / 11 | 3.5 / +7.1 | 2.4 / 9 | 1.0 / 16 | 20 2 / 0.4 / +10.2 | -0.8 / 25

4.9 / 26 | 2 3 / 5.0 / +12.3 | 4.8 / 13 | 4.0 / +13.3 | 2.8 / 12 | 24 4 / 2.9 / +14.4 | 3.1 / 27

4.5 / 26 | 2 8 / 4.4 / +12.8 | 4.3 / 13 | 3.9 / +13.3 | 4.1 / 6 | 4.0 / 17 | 3.7 / 21 | 4 2 9 / 4.3 / +12.9 | 6.1 / 25

4.7 / 27 | 23 9 / 4.2 / +13.0 | 4.7 / 12 | 6.1 / 7 | 8.9 / +8.3 | 10.7 / 7 | 16 / 11.5 / +5.7 | 11.4 / 21

5.2 / 25 | 21 9 / 5.2 / +11.9 | 5.5 / 20 | 11.5 / 9 | 13.4 / +3.7 | 12 1 / 15.0 / +2.1 | 15.3 / 20

8.0 / 22 | 15 6 / 11.5 / +5.5 | 11.6 / 14 | 12.0 / +5.0 | 15 11 / 11.3 / +5.7 | 11.2 / 20

2.9 / 20 | 15 9 / 2.9 / +5.9 | 3.2 / 16 | 3.2 / 12 | 14 3 / 4.5 / +4.3 | 7.4 / 23

2.0 / 20 | 10 5 / 2.2 / +6.5 | 4.5 / 42 | 11 6 / 7.1 / +7.6 | 7.1 / 20

2.5 / 18 | 14 1 / 4.5 / +4.1 | 8.0 / 6 | 7.5 / +7.1 | 12 8 / 6.2 / +2.4 | 5.4 / 16

1.9 / 20 | 15 1 / 3.4 / +5.1 | 5.0 / 10 | 4.5 / +4.0 | 19 / 3.5 / +5.0 | 3.1 / 20

Sta	B.S	H.I.	F.S	Grade	Gr. Rd.
		834.6 ✓			
2+55				826.1	8.5 ✓
3				26.3	8.3 ✓
+58				26.5	8.1 ✓
+70				26.6	8.0 ✓
+76				26.6	8.0 ✓
		Channel Change - Left			
		835.94 ✓			
0+13				25.1	10.8 ✓
+31				25.0	10.9 ✓
+40				24.9	11.0 ✓
+50				24.9	11.0 ✓
80				24.8	11.1 ✓

Lt. ℄ Rt.

0.8/20 17.1/0.9/7.6 1.3/8 8.5/5 1.9/3 1.7/+6.8 16.6/1.9 2.1/20

3.0/20 15.8/2.5 4.4/13 2.7/11 3.1/+5.2 15.4/2.9/+5.0 2.7/20

3.5/20 15.6/2.5/+5.6 3.2/+4.9 16.1/2.0/+6.1 1.8/20

8.9/15 8.1/10 3.3/+4.7 16.9/2.0/+6.0 1.7/20

7.6 2.6/13 16.9/2.0/+6.0 1.9/20

5.9/20 14.7/6.1/+4.7 6.0/11 7.2/4 8.6/+2.2 11.9/8.9/+1.9 8.2/20

5.0/20 16.9/4.9/+6.0 5.4/9 8.1/+2.8 7.2/10 13.7/7.2/+3.7 8.0/20

3.8/20 17.1/3.9/+7.1 2.8/13 3.0/9 7.2/3 7.0/2 5.3/+5.7 4.3/5 6.3/13 14.3/6.7/4.3 7.5/15 10.3/17 10.7/20

4.5/20 16.3/4.7/+6.8 3.3/9 8.3/3 11.4/-0.4 11.7/25

11.6/20 11.6/12 11.6/6 11.5/+0.1 9.5/4 7.3/8 14.3/4.8/+4.3 6.8/20

Sta.	B.S.	H.I.	F.S.	Grade	Gr. Rd.
		835.94 ✓			
1 + 00				24.7	11.2
+28				24.6	11.3
+42				24.5	11.4
+57				24.5	11.4

Lt. ℄ Rt.

11.7/20	11.0/13	7.1/7	7.0/2	6.8/+4.4	13.9/3.9	7.3	6.8/20		
11.6/20	10.1/12	10.1/9	7.3/+6.0	7.9/12	13.8/3.8	7.5	7.9/20		
11.6/20	11.1/8	10.6/4	9.8/+1.6	8.2/9	13.3/+3.3	8.1	8.1/20		
8.0/20	8.1/15	10.8/14	11.8	10.2/6	11.6/+1.6	9.8	7.8/17	7.8/20	

Channel Change

40' Rt.	795+20 +0	H.I.	798.+90	Gr. Rd.
T.P.	+ 4.85	867.87	863.02	
795+20			862.2	5.7
+25			62.2	5.7
+50			61.7	6.2
796			61.0	6.9
+50			60.2	7.7
797			59.5	8.4
+50			58.8	9.1
+90			58.2	9.7
798			58.0	9.9
798+05			58.0	9.9
+50			58.0	9.9
+85			58.0	9.9
+90			58.0	9.9

Lt. ℄ Rt.

Beginning of Ditch

2.6/8	5.2/2.5 +3.2	3.1 +3.5	3.8/3.9 +1.8	3.9/5	2.3/8
3.0/8	5.2/3.0 +3.2	3.8 +3.7	5.4/2.8 +3.4	2.6/8	
3.5/8	5/3.4 +3.5	3.4 +3.5	5.5/3.4 +3.5	3.9/8	
4.5/8	5.3/4.4 +3.3	4.3 +3.4	5.1/4.1 +3.6	4.2/8	
6.1/8	4.3/6.1 +2.3	6.2 +2.2	4.1/5.7 +2.7	5.7/8	
6.3/8	4.6/6.5 +2.6	7.0 +2.1	4.3/6.8 +2.3	6.7/8	
7.4/8	4.1/7.6 +2.1	7.6 +2.7	4.0/7.7 +2.0	7.7/8	
	9.9/8	9.9/0.0	9.8/8		
	9.7/8	9.7/2	9.4	8.1/8	
9.2/8	3.1/8.8 +1.1	8.9 +1.0	3.0/8.9 1.0	8.8/8	
9.5/8	2.7/9.2 +0.7	9.1 +0.8	2.6/9.3 +0.6	9.0/8	

End of Ditch

Original x Sec. Driveway Rt. Sta. 808+03.

B.M.	1.90	852.97	851.07
0+20	= 20' Rt. of Sta. 808+03		
0+37			
0+41			
0+47			
0+75			

Original x Sec. Driveway Lt. Sta. 808+56.

0+20	
0+37	
0+57	
0+89	

C.W.S.
D.S.
W.W.

S.W. Slab of Cvlt. N. of Sta 80 8+00

5.3 / 20	1.7	1.0 / 20
9.1 / 24	7.1	7.7 / 25
11.5 / 26	10.5	9.8 / 25
9.0 / 25	8.7	7.0 / 26
8.0 / 25	6.0	5.0 / 20

		3.4		
	8.2 / 15	6.2	4.2 / 12	0.4 / 15
8.3 / 17	7.3 / 10	7.5	6.0 / 10	3.2 / 17
8.2 / 13	7.4 / 10	6.0	5.2 / 9	2.2 / 13

Hand Ditch Rt. Sta. 605+80

		+	H.I.	−	Grade	
		0.62	910.88		910.26	
0	+00				904.0	6.9
	+10				903.9	7.0
	+18				903.8	7.1
	+28				903.7	7.2
	+40				903.6	7.3
	+66				903.5	7.4

4.0 / 8	4.9 / +2.9 = 4.0	6.9 / +2.6	4.5 / +2.5 = 4.4	9.7 / 8
2.2 / 8	6.7 / +4.7 = 2.3	2.9 / +4.1	6.5 / +4.5 = 2.5	2.5 / 8
2.3 / 8	6.9 / +4.9 = 2.2	2.8 / +4.3	6.3 / +4.3 = 2.8	2.6 / 8
4.4 / 8	4.8 / +2.8 = 4.4	4.4 / +2.8	4.9 / +2.9 = 4.3	4.4 / 8
5.6 / 8	3.5 / 1.5 = 5.8	5.8 / +1.5	3.9 / +1.6 = 5.7	5.5 / 8
	7.4 / 8	7.4 / 0.0		7.4 / 8

HAND DITCH Rt. Sta 613+00

	+	H.I.	−	Grade	
B.M	0.70	911.01		910.31	
0+00				902.5	8.5
+25				902.5	8.5
+50				02.4	8.6
+90				02.4	8.6
1+00				02.4	8.6
+10				2.4	8.6
+30				2.4	8.6
+54				2.3	8.7

	8.5 / 8	8.5 / 0.0		8.8 / 8
8.4 / 8	2.0 | 8.5 / 0.0	8.4 / +0.1	2.1 | 8.4 / +0.1	8.6 / 8
8.0 / 8	2.5 | 8.1 / +0.5	8.1 / +0.5	2.5 | 8.1 / +0.5	8.0 / 8
6.0 / 8	4.7 | 5.9 / +2.7	6.0 / +2.6	4.9 | 6.0 / +2.6	6.0 / 8
9.5 / 8	6.2 | 4.7 / +4.2	4.7 / +3.9	5.6 | 5.0 / 3.6	5.2 / 8
	4.9 / 8	4.9	5.2 / 8	
7.2 / 8	3.6 | 7.0 / +1.6	6.9 / +1.7	3.8 | 6.8 / +1.8	6.9 / 8
	8.7 / 8	8.7 / 0.0	8.6 / 8	

Channel Change Sta. 808+30

Sta.	+	H.I.	−	Grade	
B.M.	0.96	852.03		851.07	
0+00				41.5	10.5
+50				41.5	10.5
+85				41.5	10.5
+90					

8.2/8 4.2/8.3 +2.2 8.0/+2.5 4.6/7.9 +2.6 8.1/8

7.7/8 4.5/8.0 +2.5 8.0/+2.5 4.5/8.0 +2.5 8.0/8

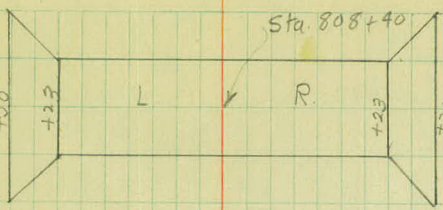
9.7/8 11.7/7 11.0/5 3.2/9.3 +1.7 8.8/+1.7 4.3/8.3 +2.3 8.2/8

END

Monolithic Culv. Sta. 808+40

808+40 W. 106 x 40'

B.M.	0.96	852.03	851.07	
808+40=00			41.5	10.5
+23			41.4	10.6
+28			41.4	10.6
+30			41.4	10.6
00			41.5	10.5
+23			41.6	10.4
+28			41.6	10.4
+30			41.6	10.4



Left

10.4 / 6.2	10.9	10.6 / 6.2
8.1 / 6.2	8.3	7.9 / 6.2
8.4 / 9	8.2	7.5 / 9
8.4 / 10	8.1	7.6 / 10

Right

10.4 / 6.2	10.9	10.6 / 6.2
10.5 / 6.2	10.0	8.5 / 6.2
10.9 / 9	10.3	8.0 / 9
10.5 / 10	10.4	8.0 / 10

Original Sta.	X-Sec. +	Slope Central Ave. H.I	Stakes connection —	Grade	G.I.
B.M.	3.92	914.81			
587+35.1					
587+50				910.7	5.1 4.1
588+00				10.5	5.6 4.3
588+50				10.2	5.7 4.6
589+00			08.7	10.1	6.0 4.7
589+50			09.1	10.1	3.5 6.0 4.7
590+00			08.6	10.1	3.5 6.0 4.7
+50			09.1	10.2	3.4 5.9 4.6
591			09.8	10.2	3.4 5.9 4.6
+50			09.7	10.5	3.2 5.6 4.3
592			09.1	10.7	2.9 5.4 4.1
+50			08.5	11.0	2.6 5.1 3.8

54

910.89 spike in 20" Oak 110' sta. 588+50

(Same as Anoka Line)

Sh Hr Line of Anoka

Lt	℄	Rt	Super	Wd
		$\frac{3.7}{20}$ $\frac{5.3}{23}$ $\frac{5.4}{33}$ $\frac{2.9}{37}$ $\frac{3.9}{+2.2}$/388	$\frac{+0.9}{-1.0}$	1.0
		$\frac{3.7}{18}$ $\frac{5.7}{23}$ $\frac{5.3}{29}$ $\frac{3.9}{33}$ $\frac{3.0}{+2.6}$/389	$\frac{+1.2}{-1.3}$	1.0
		$\frac{4.3}{7}$ $\frac{6.7}{10}$ $\frac{6.0}{19}$ $\frac{3.5}{23}$ $\frac{3.0}{+2.7}$/40.1	$\frac{+1.2}{-1.3}$	2.0
$\frac{4.0}{8}$ $\frac{5.9}{4}$	$\frac{6.1}{-1.4}$	$\frac{5.5}{5}$ $\frac{4.3}{7}$ $\frac{3.8}{+2.2}$/393	$\frac{+1.2}{-1.3}$	2.0
25.2 $\frac{6.1}{-2.6}$ $\frac{6.4}{24}$ $\frac{3.6}{19}$ $\frac{6.0}{17}$	$\frac{5.7}{-1.0}$	$\frac{4.8}{+1.2}$/37.8	$\frac{+1.2}{-1.3}$	2.0
26.0/$\frac{6.5}{-3.0}$	$\frac{6.2}{-1.5}$	$\frac{6.0}{0.0}$/25.2 $\frac{5.7}{+0.3}$/36.5	$\frac{+1.2}{-1.3}$	2.0
25.6/$\frac{6.2}{-2.8}$	$\frac{5.7}{-1.1}$	$\frac{5.1}{2.0}$ $\frac{4.9}{+1.0}$/37.5	$\frac{+1.2}{-1.3}$	2.0
24.6/$\frac{5.7}{-2.3}$	$\frac{5.0}{-0.4}$	$\frac{4.0}{+1.9}$/38.8	$\frac{+1.2}{-1.3}$	2.0
27.2/$\frac{6.8}{-3.6}$	$\frac{5.1}{+0.5}$	$\frac{4.2}{+1.4}$/37.1	$\frac{+1.2}{-1.3}$	2.0
28.4/$\frac{7.1}{-4.2}$	$\frac{5.7}{-1.6}$	$\frac{4.8}{2.0}$ $\frac{4.2}{+1.2}$/37.8	$\frac{+1.2}{-1.3}$	2.0
30.8/$\frac{8.0}{-5.4}$	$\frac{6.3}{-2.5}$	$\frac{5.3}{-0.2}$/22.6 $\frac{4.6}{+0.5}$/36.8	$\frac{+1.2}{-1.3}$	2.0

Sta.	+	H.I.	−	Grade	Gr. Rd
		914.81			
593+00			08.8	11.3	3.5 (2.8 4.8)
593+647			09.9	11.7	3.1 (2.2 4.1)
T.P.	7.05	917.05	4.81		
594+00			10.4	11.9	5.2 (4.5 5.9)
+50			11.6	12.2	4.9 (4.5 5.3)
595+00			11.8	12.5	4.6
+50			12.8	12.8	4.3
596+00			12.8	13.1	4.0
+50			12.7	13.4	3.7
T.P.	4.60	918.31	3.34		
597			12.9	13.6	4.7
+50			14.2	13.7	4.6
598			15.2	13.8	4.5
599			15.1	13.8	4.5
600			14.7	13.8	4.9

	Lt.	C	Rt		S.	W.
	31.0/ 7.8 -5.5	6.0 -2.5	5.1 -0.3 /22.6	4.4 +0.4 /36.6	+1.2 -1.3	2.0
	27.2 6.8 -4.6	4.9 -1.8	4.5 -0.4 /22.2	4.5 D.C +2.1 /34.2	+0.9 -1.0	1.0
910.00						
	26.4/ 7.7 -3.2	6.7 -1.5	6.2 -0.3 /20.6	6.3 / D.C. +2.1 / 33.7	+0.7 -0.7	0.0
D.C 30.8/ 6.5 +0.5	25.4/ 6.3 -1.8	5.5 -0.6	5.5 -0.2 /20.6	5.3 0.0 /34.0	+0.4 -0.4	
D.C 31.7/ 6.0 +1.1	23.6/ 5.8 -1.2	5.3 -0.7	4.8 -0.2 /20.6	4.6 0.0 /34.0	+0.0 -0.0	
D.C 32.6/ 5.1 +1.7	21.5/ 4.8 -0.5	4.3 0.0	4.0 2.0	4.1 +0.2 /34.3		
D.C 31.7/ 5.4 +1.1	23.0/ 5.0 -1.0	4.3 -0.3	4.2 -0.2 /20.6	4.3 / D.C +2.2 /33.3		
D.C 30.8 5.7 +0.5	25.1/ 5.4 -1.1	4.4 -0.7	4.4 -0.7 /22.1	4.3 / D.C. +1.9 /32.9		
913.71	Top G.R. Post 200' Lt. 596+50					
D.C. 31.7/ 4.3 +0.9	23.9/ 6.0 -1.3	5.4 -0.7	5.5 -0.8 /22.4	5.5 / DC +1.7 /32.6		
D.C. 33.2/ 5.0 +2.1	20.0/ 4.6 0.0	4.1 +0.5	4.3 2.0	4.4 +0.2 /34.3		
	35.1/ 3.8 +0.7	3.1 +1.4	3.3 2.0	3.2 +1.3 /36.0		
	35.2/ 3.7 +0.8	3.2 +1.3		3.5 +1.0 /35.5		
	35.1 4.1 +0.7	3.6 +1.2		4.1 +0.7 /35.1		

Sta.	+	H.I	−	Grade	Gr. Rd.
		918.31			
600+50			12.6	9133	5.0
601+00			11.4	13.1	5.2
T.P.	4.91	917.16	6.06		
+50			11.7	12.9	4.3
602			13.2	12.7	4.5
+47			14.0	12.6	4.6
+69			12.5	12.8	4.7
603			12.2	12.4	4.8
+19			13.0	12.8	4.4
+80			12.9	12.9	4.3
604			12.9	12.9	4.3
B.M.			1.61		

4 ℄ RH. Sept 24, 1926

D.C. 320 / 5.5 +2.0 ; 22.1 / 5.7 −0.1 ; 5.7 −0.7 ; 5.7 −0.7 / 22.1 ; 6.0 +1.8 / 7.6 / 32.3

6.1 5.0 ; 6.1 4.3 ; 7.7 3.8 ; DC 31.2 / 6.9 +0.8 ; 25.1 / 6.9 −1.7 ; 6.9 −1.7 ; 6.9 −1.7 / 25.1 ; 6.9 +0.8 / 34.2

9.12.25.

RCV = 4.6 / 36 ; 9.8 / 30 ; 25.1 / 6.10 −1.7 ; 5.5 −1.2 ; 5.6 −1.3 / 23.9 ; 5.3 +1.3 / D.C. / 32.0

PaV$_c$ 4.6 / 36 ; 4.6 / 19 ; 5.2 / 17 ; 5.3 / 13 ; 9.0 / 9 ; 4.0 +0.5 ; 4.3 / 2.0 ; 4.2 +0.3 / 34.5

Pave = 4.45 / 18 ; 4.3 / 12 ; 5.0 / 8 ; 4.5 / 3 ; 3.2 +1.4 ; 2.9 +1.7 / 26.5

PaV = 4.44 / 14 ; 4.5 / 6 ; 5.2 / 3 ; 4.7 / 0.0 ; 4.3 / 2 ; 2.7 / 5 ; 3.0 +1.7 / 36.5

PaV$_1$ = 4.38 / 10 ; 4.2 / 3 ; 5.0 −0.7 ; 4.2 / 7 ; 2.5 / 9 ; 2.8 +2.0 / 37.0

PaV = 4.35 / 7 ; 4.2 ; 4.6 / 2 ; 5.0 / 4 ; 4.7 / 9 ; 3.0 / 12 ; 2.7 / 17 ; 3.1 / 40

4.3 / PaV. 8 ; 4.2 / 8 ; 4.7 / 11 ; 4.5 / 17 ; 2.6 / 19 ; 2.9 +1.4 / 36.1

4.2.6 ; 4.25 / 2 = Pav. ; 3.6 / 13 ; 3.2 / 33

9.15.25. Spike in T.P. −5' RH. 60/4 20

West End of Bridge

	+	H.I.	−	Grade
B.M.	5.31	837.44		832.13
B.M.			5.31	832.13
B.M.	6.06	838.19		832.13
819+50				26.8
+55				29.5
+72				31.2
+86				33.4
+96				33.0

Sp. in 10' @ 50' Lt. Sta 822+10

Sp. in 10' @ 50' Lt. Sta 819+08 (Established)

11.4/50 — 11.4 — 11.4/50

11.4/50 9.0/41 10.4/37 8.7/31 10.4/18 10.3/10 8.7

7.2/9 6.9/25 6.6/36 6.0/50

Water

11.6/32 11.1/31 10.9/28 9.6/26 9.4/13 8.7/8 7.0

6.0/8 6.0/30 5.5/38 1.2/50

Water

11.2/31 9.0/24 9.7/27 6.1/10 7.2/9 4.8

5.6/7 4.2/14 3.6/20 4.8/29 4.5/42 3.0/50

Water

11.6/28 10.1/26 7.5/15 5.9/11 5.2/6 5.2

5.0/13 4.4/19 4.7/31 3.8/38 2.9/50

Final Section Hand Ditch 771+32 – 789+00 LH RH

BM	3.33	889.99		886.66	
771+22					
+52				87.2	1.8
772+00				85.0	5.0
773+00				84.8	5.2
774+00				84.5	5.5
775+00				84.0	6.0
TP	2.73	883.48	7.24	880.75	
776+00				83.4	0.1
777+00				82.8	0.7
778+00				82.2	1.3
779+00				81.6	1.9
780+00				81.0	2.5
781+00				80.4	3.1

		883 - 8			
782+00				79.8	3.7
783+00				79.2	4.3
T.P.	4.13	880.16	7.45	876.03	
784+00				78.6	1.6
785+00				78.0	2.2
786+00				77.4	2.8
787+00				76.7	3.5
788+00				76.0	4.2
789+00				75.0	5.2
T.P.	2.15	878.66	3.65	876.51	
	5.27	874.00	2.93	880.93	
BM.			3.36	880.64	586.66

79/38 86/37 88/33 79/32 77 (3.7) 70/32 89/33.5 79/37 76/34

79/38 91/37 91/33 77/31.5 77 (4.3) 77/31.5 75/33 75/38 77/37

72/39.5 65/38 65/33 54/31 65 (1.6) 43/31 67/33 65/37.5 42/34

54/39.5 72/37.5 73/34 50/31 45 (2.2) 40/30 70/32 70/33.5 40/40

60/39.4 81/38 81/33.5 58/31 57 (2.8) 57/36.4 77/32.8 71/38.5 54/37.7

64/40 85/38.5 86/33 66/30.7 65 (3.5) 65/33 91/32.6 91/37 65/39

78/32 90/37 88/34 77/32 75 (4.7) 74/31 73 57 74/39 End.

82/39 95/37 95/34 91/31 8.1

50 d

Solution 20 lbs 75 1/2 76 1/4 5 4 9 76 9 4 40

Final Sections Hand Ditch 729 - 740+68

BM	3.32	88.22		84.90	
729				87.5	1.7
730				87.4	1.8
731				87.4	1.8
732				87.4	1.8
733				87.4	1.8
734				87.2	2.0
735				87.2	2.0
736				87.2	2.0
737				87.2	2.0
738				87.2	2.0
T.P	5.07	88.07	5.22	88.00	
739				87.2	1.9
740				87.	1.9

44	59	57	44	48					
38½	36	33	31						
46	59	58	47	3.4	31	5.9	5.8	3.8	
38½	38.5	33½	32		30.5	33½	37½	37	
47	61	62	48	44	39	60	61	41	
39	37	33	32		31	33	37	39	
47	62	62	47	4.8	42	62	62	43	
38½	37½	33	31½		32	33	37	38½	
48	62	62	47	4.5	43	60	62	44	
39	38	33½	31½		31	32.5	36.5	33½	
50	69	69	53	54	49	67	66	50	
38½	37	33	32		31½	33½	37	38	
54	73	71	54	5.3	51	70	71	52	
39	37	33½	31		31	33	37½	39	
59	76	76	59	5.7	55	76	77	56	
39	37	33	31½		31	33	37½	38½	
58	79	80	58	6.0	59	76	78	63	
39	37	33	32		31	33	37	37½	
62	82	82	63	6.1	54	80	81	54	
39	37	33½	31½		32	34.5	38	42	
58	78	75	55	5.7	61	75	77	61	
39½	37½	33	31½		32	38.5	37.5	28	
66	81	79	64	6.0	60	79	80	62	
38½	37	33	31½		31½	38	38	39.5	

Sta	+	HI	−	Elev	
		889.07			
740+41				87.4	1.7
768				87.4	1.7
BM.	6.31	889.07	6.31	882.77	882.76

Right.

Cross Section	Change	Change	Sta. 741
			GRd
0+00			9.0
0+25			9.1
+50			9.2
+70			9.3
+80			9.4

Left.

0+00				7.7	
0+25				9.8	
+45				9.9	

$\frac{6.7}{34}$ $\frac{8.4}{38}$ $\frac{8.3}{32}$ $\frac{66}{325}$ $\frac{6.8}{-}$ $\frac{8.0}{32}$ $\frac{8.5}{335}$ $\frac{8.5}{38}$ $\frac{7.0}{39}$

$\frac{7.5}{375}$ $\frac{7.0}{36}$ $\frac{8.2}{32}$ $\frac{2.8}{31}$ $\frac{7.7}{-}$

Apiche in Poplar 150' 4+5+9 7+4+75

$\frac{8.5}{5}$ $2.5/\frac{8.5}{-85}$ 7.0 $\frac{7.6}{-14}/\frac{3.4}{-}$ $\frac{7.6}{5}$

$\frac{2.5}{5}$ $3.6/\frac{7.5}{16}$ 7.3 $\frac{7.3}{-14}/3.9$ $\frac{7.3}{5}$

$\frac{2.1}{.5}$ $4.2/\frac{7.0}{2.4}$ 7.0 $\frac{6.8}{-24}/4.8$ $\frac{6.8}{6}$

$5.9/\frac{6.4}{-2.9}$ 6.1 $\frac{6.4}{3.1}/6.9$

$5.6/\frac{6.8}{-2.6}$ 6.2 $\frac{6.4}{3.6}$

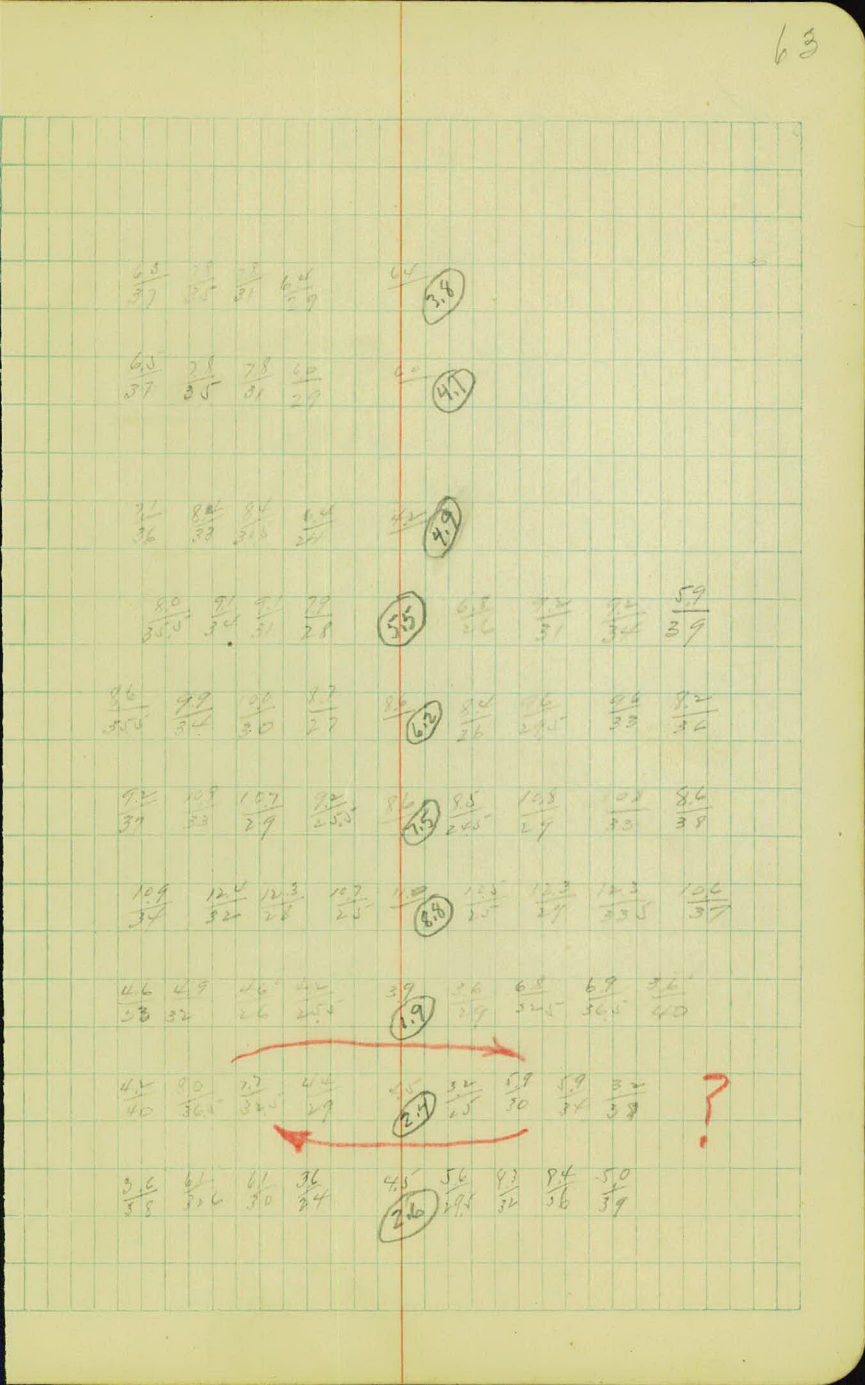
$60/\frac{2.8}{-1.9}$ 7.5 $\frac{2.8}{-1.9}/60$

$2.4/\frac{8.6}{-1.4}$ 8.3 $\frac{8.1}{-1.7}/3.7$

$2.4/\frac{7.5}{0.4}$ 9.9 $\frac{8.8}{-11}/3.1$

Final Xsection Hand Datah

St.		HI		Elev
BM	2.78	889.44 ✓		886.66
T.P.	2.32	883.58 ✓	8.18	881.26 ✓
T.P.	1.73	877.58 ✓	7.73	875.85 ✓
790+00				
+30				
T.P.	6.88	876.08 ✓	8.38	869.20 ✓
BM	1.55	876.11 ✓	1.55	874.56 ✓
792+00				
+50				
793				
794				
795				
T.P.	2.43	867.95 ✓	10.59	865.52 ✓
796				
+50				
+77				


3.8
4.1
4.9
5.5
6.2
7.5
8.8
1.9
2.4
2.6
?

Sta	+	HI	−	Elev
		867.95 ✓		
797				
+50				
798				
799				
+46				
800+00				
801+00				
T.P.	5.05	867.95 ✓	5.05	862.90 ✓
T.P	12.4	857.76 ✓	11.43	856.52 ✓
B.M.	6.75	859.82 ✓	6.75	851.01 ✓ 851.07
806+50				
T.P	2.76	851.27 ✓	9.31	848.51 ✓
807+50				
808				
+77	=00	End Ditch on Right		

$\frac{34}{285}$ $\frac{64}{335}$ $\frac{63}{295}$ $\frac{32}{33}$ $\frac{34}{}$ (2.4) $\frac{62}{295}$ $\frac{91}{335}$ $\frac{89}{34}$ $\frac{60}{35}$

$\frac{44}{35}$ $\frac{63}{34}$ $\frac{63}{295}$ $\frac{42}{35}$ (3.2) $\frac{64}{37}$ $\frac{92}{34}$ $\frac{92}{37}$ $\frac{67}{37}$

+ 70 = 00 0 1 2 0 1 2

92 (3.6) $\frac{75}{315}$ $\frac{120}{335}$ $\frac{120}{295}$ $\frac{94}{37}$

100 (4.4) $\frac{94}{35}$ $\frac{101}{33}$ $\frac{101}{37}$ $\frac{91}{37}$

93 (4.7) $\frac{80}{33}$ $\frac{92}{34}$ $\frac{93}{37}$ $\frac{73}{37}$

81 (5.2) $\frac{72}{32}$ $\frac{94}{33}$ $\frac{124}{37}$ $\frac{68}{315}$

66 (6.0) $\frac{61}{27}$ $\frac{74}{30}$ $\frac{70}{295}$ $\frac{57}{35}$

(4.2) $\frac{51}{27}$ $\frac{65}{30}$ $\frac{65}{335}$ $\frac{45}{35}$

(0.3) $\frac{54}{32}$ $\frac{58}{356}$ $\frac{55}{386}$ $\frac{3.9}{40.6}$

(0.6) $\frac{74}{38}$ $\frac{97}{39}$ $\frac{97}{93}$ $\frac{68}{46}$

$\frac{73}{36}$ $\frac{100}{37}$ $\frac{98}{42}$ $\frac{73}{45}$

Final section Channel change Sta 808+40

BM	2.65	85372	0.20	85107
+90				
+85				
+50				
0+00				
BM			2.65	85107

(12.3)

10.7 / 3.5	11.8 / 2	12.1	12.1 / 2	10.7 / 3.5
10.0 / 4	11.8 / 2	12.1	11.8 / 2	11.0 / 4
9.7 / 4.5	10.0 / 2	10.1	12.0 / 2	9.7 / 4.5
9.5 / 8.5	12.9 / 3.5	10.2	12.1 / 5.5	9.2 / 8.5

4/20/27

Cross-Sections for re-balance of Quantities.

Sta	+	H I	-	Elev
BM	5.72	89.23		886.66
761				5.7
762				5.4
763				5.6
+40				5.7
764				5.8
+50				5.9
765				6.0
766				6.2
+30				6.3
767				6.4
768				6.6

GNS
P.O
A.B
T.M.

66

60/50	73/44	100/27	50/20	48	48/20	87/26	94/44	92/50
118/50	90/44	90/28	55/20	55	52/20	92/28	98/39	92/50
93/50	74/46	98/29	57/21	57	56/21	97/29	92/40	45/50
62/50	96/45	100/30	60/21	58	55/21	98/28	92/42	93/50
60/50	96/45	100/29	58/20	64	60/20	102/27	98/42	92/50
52/50	92/45	98/29	64/21	65	60/20	97/27	100/42	46/50
46/50	97/45	100/29	65/20	63	62/20	102/27	102/43	52/50
60/50	93/46	103/29	64/20	65	62/20	100/27	102/45	65/50
62/51	98/46	100/29	63/21	66	62/20	100/26	103/42	70/50
75/50	98/46	100/27	62/20	67	65/20	102/26	102/46	70/50
72/50	102/46	102/27	66/20	68	68/20	102/26	105/45	68/50

Sta	+	HI	−	Elev
		892.38		
769				6.8
+16				6.8
+25				6.8
+50				6.9
+68				6.9
+83				6.9
770				7.0
+50				7.1
771				7.2
+38				7.3
772				7.4

70/50	102/46	105/27	6.5/20	6.5	6.8/20	10.0/26	10.8/45	7.0/50	
6.6/50	10.6/46	10.2/27	6.4/20	6.6	6.9/21	9.5/28	9.6/45	5.8/50	
6.7/50	9.7/46	10.6/27	6.6/20	7.5	6.7/20	7.5/28	7.0/40	5.5/46	6.0/50
	6.7/50	6.4/24	6.2/20	5.5	5.5/20		5.8/35	6.2/50	
		6.6/50	6.6/32	7.1/21	7.2	6.6/20	8.8/25	9.0/35	9.3/42	5.0/50
6.2/50	10.6/42	10.6/29	7.8/20	4.8	7.0/20	10.7/28	10.8/42	4.8/50		
	6.6/50	10.5/43	11.0/28	7.3/20	7.2	7.0/20	11.0/28	11.0/42	4.8/50	
6.6/50	10.6/44	11.0/29	7.2/20	7.3	6.8/20	11.3/29	11.2/43	6.0/50		
7.0/50	11.4/43	11.6/29	7.2/20	7.2	7.0/20	11.8/29	11.8/43	8.2/50		
+50	8.2/50	11.4/45	11.7/28	7.2/20	7.8	6.8/19	6.3/22	10.2/28	10.5/31	11.8/33	11.8/37	10.3/38	10.3/50
10.5/50	10.9/38	11.0/37	10.9/34	10.9/21	10.2/16	9.0/20	7.2	7.0/20	10.5/27.34	10.5/33	12.4/37	12.6/40	10.2/50	10.4/50

Sta	+	HI	−	Elev.
		992.38.		
773				7.6
T.P.	2.72	887.11.	7.93	884.45.
774				2.7
775				3.2
776				3.8
777				4.4
778				5.0
779				5.6
780				6.2
781				6.8
782				7.4
783				8.0

$\frac{10.0}{50}$	$\frac{11.0}{39}$	$\frac{12.8}{37}$	$\frac{12.8}{34}$	$\frac{11.0}{32}$	$\frac{10.8}{28}$	$\frac{6.8}{20}$	$\frac{6.8}{}$	$\frac{6.8}{20}$	$\frac{10.8}{27}$	$\frac{10.8}{32}$	$\frac{12.6}{33}$	$\frac{12.6}{37}$	$\frac{10.7}{39}$	$\frac{11.0}{50}$
$\frac{6.1}{50}$	$\frac{6.1}{39}$	$\frac{8.0}{37}$	$\frac{8.0}{33}$	$\frac{6.1}{32}$	$\frac{6.0}{28}$	$\frac{2.1}{21}$	2.0	$\frac{2.0}{21}$	$\frac{6.0}{28}$	$\frac{5.5}{32}$	$\frac{7.8}{34}$	$\frac{7.5}{37}$	$\frac{6.1}{39}$	$\frac{5.8}{50}$
$\frac{6.4}{50}$	$\frac{6.2}{40}$	$\frac{8.8}{38}$	$\frac{9.0}{34}$	$\frac{6.4}{32}$	$\frac{6.4}{28}$	$\frac{2.2}{20}$	2.8	$\frac{2.8}{21}$	$\frac{6.5}{28}$	$\frac{6.5}{31}$	$\frac{8.2}{33}$	$\frac{8.4}{38}$	$\frac{6.2}{39}$	$\frac{6.4}{50}$
$\frac{7.0}{50}$	$\frac{7.2}{40}$	$\frac{9.0}{38}$	$\frac{8.8}{34}$	$\frac{7.1}{32}$	$\frac{6.7}{28}$	$\frac{3.0}{20}$	2.8	$\frac{2.8}{20}$	$\frac{6.3}{28}$	$\frac{7.1}{30}$	$\frac{9.2}{33}$	$\frac{9.2}{36}$	$\frac{6.8}{39}$	$\frac{6.5}{50}$
$\frac{7.4}{50}$	$\frac{7.4}{40}$	$\frac{9.5}{38}$	$\frac{9.2}{34}$	$\frac{7.4}{32}$	$\frac{7.4}{28}$	$\frac{3.6}{20}$	3.3	$\frac{3.4}{21}$	$\frac{6.2}{27}$	$\frac{6.8}{30}$	$\frac{10.0}{34}$	$\frac{10.0}{37}$	$\frac{6.8}{39}$	$\frac{6.8}{50}$
$\frac{8.0}{50}$	$\frac{8.1}{40}$	$\frac{10.0}{37}$	$\frac{10.0}{34}$	$\frac{8.5}{31}$	$\frac{7.8}{27}$	$\frac{4.3}{21}$	4.4	$\frac{4.2}{21}$	$\frac{7.4}{27}$	$\frac{7.7}{30}$	$\frac{10.3}{34}$	$\frac{10.4}{37}$	$\frac{7.7}{40}$	$\frac{7.6}{50}$
$\frac{9.9}{50}$	$\frac{8.7}{41}$	$\frac{10.8}{38}$	$\frac{10.8}{34}$	$\frac{8.7}{32}$	$\frac{8.4}{28}$	$\frac{5.3}{21}$	5.5	$\frac{5.1}{21}$	$\frac{8.4}{27}$	$\frac{9.0}{31}$	$\frac{10.7}{34}$	$\frac{10.9}{36}$	$\frac{9.0}{39}$	$\frac{8.6}{50}$
												$\frac{11.1}{37}$	$\frac{9.3}{38}$	$\frac{9.5}{50}$
$\frac{9.6}{50}$	$\frac{9.3}{40}$	$\frac{11.2}{38}$	$\frac{11.0}{34}$	$\frac{10.0}{32}$	$\frac{10.0}{29}$	$\frac{6.0}{21}$	$\frac{6.5}{}$	$\frac{8.1}{4}$	$\frac{8.1}{10}$	$\frac{7.5}{12}$	$\frac{8.2}{25}$	$\frac{9.4}{28}$	$\frac{9.2}{32}$	$\frac{11.2}{34}$
$\frac{10.4}{50}$	$\frac{10.2}{39}$	$\frac{11.5}{37}$	$\frac{11.5}{32}$	$\frac{10.4}{30}$	$\frac{10.3}{28}$	$\frac{9.2}{23}$	9.0	$\frac{9.0}{20}$	$\frac{10.3}{27}$	$\frac{10.2}{32}$	$\frac{11.8}{34}$	$\frac{11.6}{37}$	$\frac{10.6}{39}$	$\frac{10.2}{50}$
$\frac{11.6}{50}$	$\frac{11.6}{38}$	$\frac{12.3}{37}$	$\frac{12.3}{34}$	$\frac{11.4}{33}$	$\frac{11.4}{28}$	$\frac{9.8}{21}$	9.8	$\frac{9.8}{22}$	$\frac{11.1}{28}$	$\frac{11.1}{32}$	$\frac{12.6}{33}$	$\frac{12.6}{38}$	$\frac{11.2}{39}$	$\frac{11.4}{50}$
$\frac{11.4}{50}$	$\frac{11.2}{39}$	$\frac{12.7}{37}$	$\frac{12.7}{34}$	$\frac{11.1}{32}$	$\frac{11.4}{27}$	$\frac{10.0}{23}$	10.5	$\frac{10.0}{21}$	$\frac{11.2}{26}$	$\frac{11.0}{32}$	$\frac{13.0}{34}$	$\frac{13.0}{36}$	$\frac{10.7}{39}$	$\frac{11.0}{50}$

Sta	+	H.I	-	Elev
		887.17.		
784				8.6
T.P	0.97	878.72.	9.42	877.75.
785				0.7
786				1.3
787				2.0
788				2.7
789				3.7
790				4.9
+30				5.2
791				6.2
+50				6.8
792				7.5
+50				8.1

R Ramsey

14.5	11.7	13.3	13.5	11.7	11.4	12.0	10.0	9.8	11.4	11.7	18.5	13.5	11.0	11.0	
50	40	37	34	32	26	22		21	25	31	33	36	39	50	
9.6	9.5	5.7	6.0	3.4	3.5	2.9	3.5	3.3	3.0	9.7	2.6	2.6	5.6	5.6	2.6	2.5	
50	39	38	34	31	25	21	14		13	21	25	30	33	36	40	50	
4.6	4.4	6.5	6.6	4.1	4.4	2.6	4.4	4.2	4.2	2.4	4.2	3.8	6.2	6.2	3.5	4.0	
50	39	37	34	31	25	22	16		15	21	25	30	33	38	40	50	
5.0	4.7	7.0	7.0	5.2	5.0	3.7	5.3	5.3		5.2	3.0	5.0	4.3	7.0	7.0	4.7	4.7
50	40	38	32	30	25	21	15			13	21	25	31	33	38	40	50
6.2	5.8	7.4	7.2	6.2	6.0	4.7	6.4	5.8		6.1	4.0	5.4	6.1	7.4	7.2	5.2	5.8
50	38	36	32	31	26	20	12			16	21	26	31	33	37	39	50
7.0	6.4	8.3	8.5	6.6	7.0	6.0	6.7	6.1		6.4	3.4	5.7	5.7	8.1	8.1	5.2	5.2
50	38	31	33	31	26	23	20			12	20	24	29	31	37	40	50
																Enl IA, RA +25	
7.5	6.8	9.0	8.7	7.4	7.3	6.2	7.4	6.6		5.6	5.1	5.1	4.7	3.5			
50	37	35	30	29	25	22	17			22	28	35	41	20			
8.0	7.3	8.8	9.0	7.4	6.8	6.4	6.5	4.8				3.8		3.2			
50	37	35	31	29	26	22	19					26		50			
+30 End Pitch L.F.																	
8.4	7.3	9.5	7.0	6.8	11.7	5.6		4.5			2.5		1.5				
50	36	34	33	30	27	24					32		50				
8.8	7.4	10.2	10.1	7.0	7.9	5.6	6.8	4.5			3.5		2.7				
50	37	36	35	34	31	29	26				24		50				
10.0	9.6	11.7	10.7	9.0	7.5	8.3		7.0			5.5		4.8				
50	36	33	29	24	19	14					25		50				
																+50 Beg Pitch PA	
10.6	10.6	11.7	11.8	10.6	9.7	10.5		10.2	9.5	7.7	9.2	9.2	11.7	11.5	8.4	8.2	
50	37	34	31	28	22	15			13	19	23	25	30	34	39	50	

Sta	+	HI	-	Elev
T.P.	2.97	871.81.	9.88	868.84.
793				1.9
794				3.7
795				4.5
796				5.7
+50				6.2
+77				6.4
797				6.6
+50				7.0
T.P.	4.70	867.81.	8.70	863.11.
798				3.4
799				4.2
T.P.	0.65	861.15.	7.31	860.50.
BM			10.12	851.03. = 851.0

$\frac{4.4}{50}$ $\frac{4.2}{36}$ $\frac{5.7}{33}$ $\frac{5.7}{30}$ $\frac{4.3}{25}$ $\frac{3.3}{21}$ $\frac{4.1}{14}$ 4.2 $\frac{4.2}{15}$ $\frac{2.6}{20}$ $\frac{4.0}{24}$ $\frac{4.0}{26}$ $\frac{5.3}{30}$ $\frac{5.3}{33}$ $\frac{4.0}{37}$ $\frac{3.6}{50}$

$\frac{5.1}{50}$ $\frac{4.6}{36}$ $\frac{6.8}{33}$ $\frac{6.1}{30}$ $\frac{4.8}{25}$ $\frac{3.0}{18}$ $\frac{4.3}{10}$ 4.4 $\frac{4.3}{11}$ $\frac{2.6}{19}$ $\frac{4.2}{24}$ $\frac{6.5}{29}$ $\frac{6.6}{33}$ $\frac{3.8}{38}$ $\frac{4.0}{50}$

$\frac{7.2}{50}$ $\frac{6.1}{36}$ $\frac{8.2}{32}$ $\frac{8.2}{29}$ $\frac{6.2}{25}$ $\frac{6.3}{24}$ $\frac{5.2}{20}$ $\frac{6.2}{15}$ 6.6 $\frac{6.0}{14}$ $\frac{4.6}{20}$ $\frac{6.2}{25}$ $\frac{8.3}{29}$ $\frac{8.2}{33}$ $\frac{6.0}{37}$ $\frac{6.3}{50}$

$\frac{7.5}{10}$ $\frac{10.1}{7}$ $\frac{10.4}{4}$

$\frac{8.6}{50}$ $\frac{8.4}{33}$ $\frac{9.4}{31}$ $\frac{8.4}{27}$ $\frac{8.4}{26}$ $\frac{6.8}{22}$ $\frac{7.5}{17}$ $\frac{8.1}{3}$ 7.7 $\frac{7.5}{10}$ $\frac{4.5}{20}$ $\frac{7.2}{25}$ $\frac{7.1}{29}$ $\frac{11.1}{34}$ $\frac{11.2}{36}$ $\frac{7.6}{41}$ $\frac{7.2}{50}$

$\frac{7.8}{50}$ $\frac{7.2}{38}$ $\frac{9.8}{34}$ $\frac{9.8}{30}$ $\frac{7.0}{24}$ $\frac{5.0}{18}$ $\frac{8.4}{8}$ 8.2 $\frac{9.4}{4}$ $\frac{11.0}{5}$ $\frac{11.0}{6}$ $\frac{9.3}{7}$ $\frac{9.1}{11}$ $\frac{5.7}{21}$ $\frac{8.2}{26}$ $\frac{8.2}{29}$ $\frac{12.1}{32}$ $\frac{12.0}{36}$ $\frac{8.1}{40}$ $\frac{8.1}{50}$

$\frac{7.1}{50}$ $\frac{7.5}{38}$ $\frac{10.4}{33}$ $\frac{12.0}{30}$ $\frac{7.0}{24}$ $\frac{7.0}{22}$ $\frac{4.7}{19}$ $\frac{7.2}{9}$ 8.5 $\frac{9.7}{10}$ $\frac{11.6}{11}$ $\frac{11.0}{12}$ $\frac{9.3}{13}$ $\frac{9.1}{21}$ $\frac{9.3}{26}$ $\frac{9.3}{27}$ $\frac{12.6}{33}$ $\frac{12.6}{36}$ $\frac{8.8}{39}$ $\frac{8.5}{50}$

$\frac{7.4}{50}$ $\frac{7.4}{39}$ $\frac{10.1}{34}$ $\frac{10.0}{30}$ $\frac{7.2}{23}$ $\frac{5.2}{17}$ $\frac{7.2}{8}$ 7.4 $\frac{7.5}{5}$ $\frac{7.0}{9}$ $\frac{9.7}{16}$ $\frac{8.0}{23}$ $\frac{10.0}{27}$ $\frac{10.1}{30}$ $\frac{12.8}{32}$ $\frac{13.2}{35}$ $\frac{9.8}{38}$ $\frac{9.5}{50}$

$\frac{9.3}{50}$ $\frac{8.6}{37}$ $\frac{10.2}{35}$ $\frac{10.2}{29}$ $\frac{8.7}{25}$ $\frac{7.0}{18}$ $\frac{8.2}{12}$ 8.3 $\frac{9.0}{14}$ $\frac{11.3}{18}$ $\frac{11.0}{20}$ $\frac{8.2}{24}$ $\frac{10.4}{28}$ $\frac{11.6}{31}$ $\frac{13.3}{34}$ $\frac{13.3}{37}$ $\frac{11.0}{40}$ $\frac{11.0}{50}$

@ 7.5 E/D, left bk

$\frac{10.7}{50}$ $\frac{13.2}{36}$ $\frac{9.4}{18}$ 9.0 $\frac{9.0}{6}$ $\frac{10.0}{7}$ $\frac{10.4}{8}$ $\frac{9.0}{9}$ $\frac{8.7}{19}$ $\frac{9.4}{27}$ $\frac{9.7}{37}$ $\frac{8.1}{39}$ $\frac{7.3}{50}$

$\frac{12.0}{50}$ $\frac{10.2}{21}$ 9.5 $\frac{9.2}{20}$ $\frac{8.5}{23}$ $\frac{8.6}{29}$ $\frac{9.0}{33}$ $\frac{9.8}{34}$ $\frac{9.8}{37}$ $\frac{8.8}{38}$ $\frac{8.8}{50}$

S.W. Cor Top Slab Culv Rt St 809+42

Borrow Pit Rt - Original.

	Sta	+	H.I	−	Elev
	BM.	5.77	880.42		874.65
	789+00				75.0
	+50				74.4
	790+00				73.8
*	+50				73.2
*	+75				72.9
*	791+00				72.5
*	+50				71.9
*	792+00				71.2
*	+25				70.9
	+50				70.6
	New BM.			483	875.59

50'
Right of ℄

Spike in stump 99'Rt sta 792+

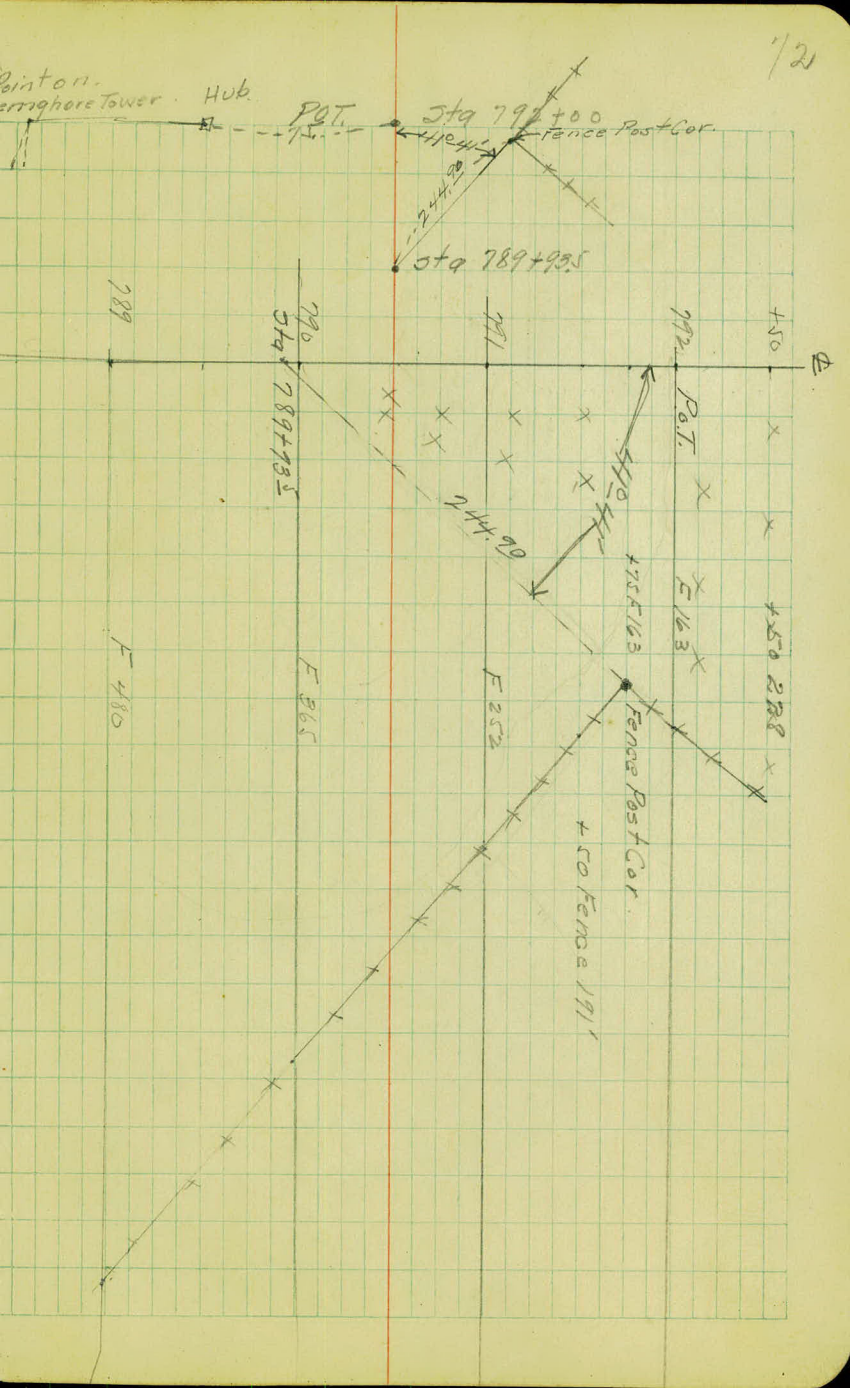
(5.4)	6.8 / 50	5.6 / 100	5.3 / 144	4.3 / 150	4.6 / 180	4.3 / 200	3.4 / 230	3.6 / 250	4.3 / 270	4.8 / 300
(6.0)	6.5 / 50	6.0 / 70	5.3 / 92	4.4 / 100	4.7 / 130	4.2 / 150	3.2 / 175	2.5 / 200	3.5 / 250	3.8 / 275	5.0 / 285	5.7 / 300
(6.6)	5.3 / 50	5.3 / 75	4.4 / 100	3.7 / 125	2.5 / 150	2.1 / 200	3.2 / 230	3.8 / 250	4.1 / 266	4.7 / 270	5.8 / 285	6.6 / 300
(7.3)	× 3.6 / 50	3.6 / 55	4.0 / 60	2.9 / 100	2.5 / 150	3.6 / 200	3.8 / 235	5.1 / 242	5.5 / 250	6.6 / 300		
(7.7)	× 3.7 / 50	× 2.4 / 69	× 1.7 / 73	2.2 / 83	2.7 / 100	3.1 / 150	4.6 / 200	4.3 / 210	5.7 / 220	6.5 / 242	6.8 / 250		
(7.9)	× 3.1 / 50	× 2.2 / 88	× 1.5 / 95	2.0 / 100	2.7 / 106	4.5 / 150	5.0 / 186	5.8 / 197	6.5 / 200	6.9 / 240			
(8.5)	× 4.4 / 50	× 3.8 / 60	× 3.8 / 100	× 4.5 / 138	× 4.5 / 139.5	5.0 / 150	5.8 / 155	7.6 / 180	7.6 / 193				
(9.2)	× 6.3 / 50	× 6.7 / 62	× 6.4 / 67	× 6.3 / 100	× 6.9 / 137	× 7.4 / 142	× 7.8 / 150	× 8.5 / 172	× 8.0 / 186				
(9.5)	× 8.2 / 50	× 8.0 / 100	× 7.7 / 114	× 8.2 / 116	× 7.4 / 150	× 9.5 / 200							
(9.8)	× 10.0 / 50	× 9.8 / 100	× 9.8 / 152	× 9.8 / 200									

Spike in Root of Triple Birch 100'Rt Sta 786+55.

Borrow Pit

Alignment Property line & Topography

Sta 789+93.5


Pointon
Hub
P.O.T.
Sta 790+00
Fence Post Cor.
244.99
Sta 789+93.5
789
790
791
792
+50
℄
Sta 789+73.5
244.99
P.O.T.
+50
+55.63
+50 2.88
F 480
F 265
F 252
Fence Post Cor.
+50 Fence 1.91

Grade Change.

Sta	+	HI	−	Elev	C.R.
B.M.	3.56	879.45		875.89	
785				77.9	1.3
786				76.8	2.5
787				75.9	3.3
788				74.8	4.4
789				73.7 (C −1.0, D 70.5)	5.5 (D. 8.7)
+50				73.1 (70.0)	6.1 (D 9.2)
790				72.6 (69.5)	6.6 (9.7)
			4.69		
+30				72.3 (69.7)	6.9 (10.0)
791				71.5 (68.5)	7.7 (10.7)
+50				70.9 (68.0)	8.3 (11.2)
T.P.	3.70	875.88	6.99	872.18	
792				70.4 (67.5)	5.5 (8.7)

Sta	+	HI	−	Elev	G.R.
		875.88			
792+50				69.8 (620)	12.1 6.1 8.9
793				69.3 (665)	6.6 9.4
794				68.2	13.7 7.7
795				67.1	14.8 8.8
T.P.	4.13	868.92	11.09	864.79	
796				66.1	8.8 2.8
+50				65.7	9.2 3.2
+77				65.4	3.5
797				65.2	3.7
+50				64.8	10.7 4.1
T.P.	10.64	876.36	3.20	865.72	
B.M.			1.70	874.66	

Sta	+	HI	-	Elev.	GR.
B.M.	2.16	892.28		890.12	
T.P.	1.61	890.94	2.95	889.33	
729+00				87.5	3.4
730				87.4	3.5
731				87.4	3.5
732					
733					
734					
735					
736					
T.P.	3.65	889.93	4.66	886.28	
737				87.4	2.5
738					
739					
	Culvert				
740					
741					
742					
743					
744					
745					
T.P.	4.95	892.41	2.47	887.46	
746				87.4	5.0

Spike rd 8" Oak 60'61 Ofg 721 ± 2V"

		892.41			
747					
748					
749					
750					
751					
752					
753					
754					
755					
T.P	3.97	892.05	4.33	888.08	
T.P	3.07	890.54	4.58	887.47	
BM			3.81	886.69	886.66

58

51

50

52

87

55

49

54

46

Spike in 24" Oak 25' Lt Sta 76+40

Sta	+	HI	−	Elev.	
BM.	2.14	892.26		890.12	
720+00				88.1	4.1
10					
724+00				87.8	4.5
50					
725+00				87.5	4.8
50					
726+00				87.2	5.1
50					
727+00				84.9	5.4
TP	2.51	891.82	2.95	889.31	
728+00				86.7	5.1

Spirits in 8" Qnt. 60 U.P. 72 H.P.

61
-20

67
-2.4 / 2.48

35.9 / 68
DF / +34

68 / 2.40
-20

66
-.17

35
+.43 / 4.08

DC / 71
35.8 / +0.5

58 / 2.4
-.07

48
+.03

43
+1.1 / 4.5

DC / 74
35.8 / +05

69 / 23.0
-1.5

52
+.15

39
+1.1 / 4.4

DC / 68
36.1 / +08

71
-.20

57
-.06

34
+.16 / 4.2

Partial X Sec. Between Sta. 812+32 & Sta. 809+50.

For Uncl. Order #6

					Rod
B.M.	1.90	852.97		851.07	
T.P.	6.49	858.56	0.90	852.07	
809+50				49.3	9.3
+75				49.1	9.5
810+00				49.0	9.6
+25				48.9	9.7
+50				48.9	9.7
811+00				48.5	10.1
T.P.	9.67	863.50	4.73	853.83	
+25				48.4	15.1
+50				48.3	15.2
+71				48.1	15.4
+92				48.0	15.5
812+00				48.0	15.5
+12				47.9	15.6
+32				47.8	15.7
T.P.	2.27	853.60	12.17	851.33	
T.P.	1.47	852.45	2.62	850.98	
B.M.			4.90	847.55	

6-8-27

S.W. Cor. Slab Culv Rt. Sta. 808+66

C.W.S.
D.S.
B.W.
H.Y.

$\frac{8.4}{50}$ $\frac{9.5}{38}$ $\frac{8.0}{21}$ $\frac{10.2}{17}$ $\frac{\boxed{9.4}}{9.0}$ $\frac{8.0}{14}$ $\frac{9.5}{22}$ $\frac{10.0}{37}$ $\frac{14.0}{50}$

$\frac{10.5}{50}$ $\frac{8.0}{35}$ $\frac{11.0}{32}$ $\frac{11.0}{24}$ $\frac{9.7}{19}$ $\frac{\boxed{9.5}}{8.3}$ $\frac{6.4}{7}$ $\frac{9.0}{16}$ $\frac{10.8}{32}$ $\frac{12.0}{50}$

$\frac{9.8}{50}$ $\frac{8.0}{47}$ $\frac{9.0}{40}$ $\frac{11.4}{39}$ $\frac{12.2}{37}$ $\frac{12.2}{28}$ $\frac{9.4}{22}$ $\frac{9.1}{16}$ $\frac{7.5}{2}$ $\frac{\boxed{8.6}}{8.6}$ $\frac{6.4}{6}$ $\frac{8.4}{10}$ $\frac{8.4}{12}$ $\frac{10.6}{14}$ $\frac{10.0}{35}$ $\frac{12.3}{46}$ $\frac{13.2}{50}$

$\frac{8.6}{50}$ $\frac{8.6}{35}$ $\frac{11.8}{34}$ $\frac{12.0}{24}$ $\frac{10.5}{22}$ $\frac{10.3}{7}$ $\frac{6.3}{3}$ $\frac{\boxed{9.7}}{7.4}$ $\frac{4.8}{8}$ $\frac{8.6}{18}$ $\frac{10.6}{50}$

$\frac{8.6}{50}$ $\frac{9.4}{36}$ $\frac{11.8}{35}$ $\frac{12.0}{24}$ $\frac{11.0}{22}$ $\frac{10.2}{7}$ $\frac{6.7}{3}$ $\frac{\boxed{9.8}}{8.9}$ $\frac{5.0}{10}$ $\frac{9.7}{21}$ $\frac{11.0}{50}$

$\frac{5.7}{50}$ $\frac{6.0}{40}$ $\frac{10.8}{36}$ $\frac{11.5}{25}$ $\frac{10.0}{23}$ $\frac{9.2}{7}$ $\frac{\boxed{10.1}}{5.2}$ $\frac{1.5}{7}$ $\frac{7.0}{17}$ $\frac{7.8}{43}$ $\frac{9.1}{44}$ $\frac{9.1}{47}$ $\frac{7.5}{48}$ $\frac{7.6}{50}$

$\frac{9.0}{50}$ $\frac{7.0}{44}$ $\frac{9.2}{42}$ $\frac{14.8}{34}$ $\frac{14.5}{11}$ $\frac{\boxed{15.1}}{6.5}$ $\frac{2.3}{9}$ $\frac{9.8}{19}$ $\frac{9.4}{25}$ $\frac{9.8}{40}$ $\frac{12.8}{43}$ $\frac{13.3}{47}$ $\frac{10.5}{48}$ $\frac{10.5}{50}$

$\frac{10.5}{50}$ $\frac{6.0}{41}$ $\frac{15.0}{30}$ $\frac{14.5}{10}$ $\frac{\boxed{15.2}}{6.4}$ $\frac{0.7}{10}$ $\frac{8.2}{19}$ $\frac{9.5}{39}$ $\frac{12.4}{44}$ $\frac{9.5}{48}$ $\frac{9.4}{50}$

$\frac{9.3}{50}$ $\frac{9.0}{47}$ $\frac{3.0}{37}$ $\frac{12.0}{25}$ $\frac{14.5}{21}$ $\frac{14.2}{4}$ $\frac{\boxed{15.4}}{13.0}$ $\frac{8.0}{13}$ $\frac{7.7}{37}$ $\frac{12.0}{41}$ $\frac{9.0}{47}$ $\frac{8.6}{50}$

$\frac{5.5}{50}$ $\frac{4.0}{39}$ $\frac{6.5}{32}$ $\frac{10.7}{31}$ $\frac{14.2}{23}$ $\frac{14.8}{3}$ $\frac{\boxed{15.5}}{12.2}$ $\frac{9.5}{5}$ $\frac{8.6}{9}$ $\frac{6.2}{15}$ $\frac{8.0}{21}$ $\frac{9.5}{37}$ $\frac{10.7}{40}$ $\frac{8.9}{41}$ $\frac{9.5}{50}$

$\frac{1.0}{38}$ $\frac{11.0}{28}$ $\frac{14.2}{23}$ $\frac{15.0}{3}$ $\frac{\boxed{15.5}}{13.0}$ $\frac{9.0}{5}$ $\frac{5.5}{13}$ $\frac{6.4}{30}$ $\frac{3.6}{28}$ $\frac{2.5}{40}$ $\frac{9.8}{50}$

$\frac{0.5}{40}$ $\frac{13.3}{25}$ $\frac{\boxed{15.5}}{15.3}$ $\frac{14.2}{29}$ $\frac{12.5}{33}$ $\frac{8.5}{38}$ $\frac{7.5}{50}$

$\frac{2.0}{42}$ $\frac{12.8}{20}$ $\frac{\boxed{15.7}}{14.8}$ $\frac{14.3}{24}$ $\frac{10.5}{32}$ $\frac{5.0}{38}$ $\frac{6.0}{50}$

N.W. Cor. of Bridge

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

Made in Germany.