

OFFICE OF
RAMSEY COUNTY ENGINEER

FINAL NOTES

ANOKA CUT-OFF

PROJ. NO 26-62-B

FILE NO

11-1-28

"5"

KEUFFEL & ESSER CO.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

22.00

150.000
08
250 000

150
5
21750 23

3

59.04
40.96
100.00

325 + 509.04 01.00

326 00.25
+50 00.55

327 10.25
+50 10.55

328 20.25
+365.04 20.46

40.96
60
245860

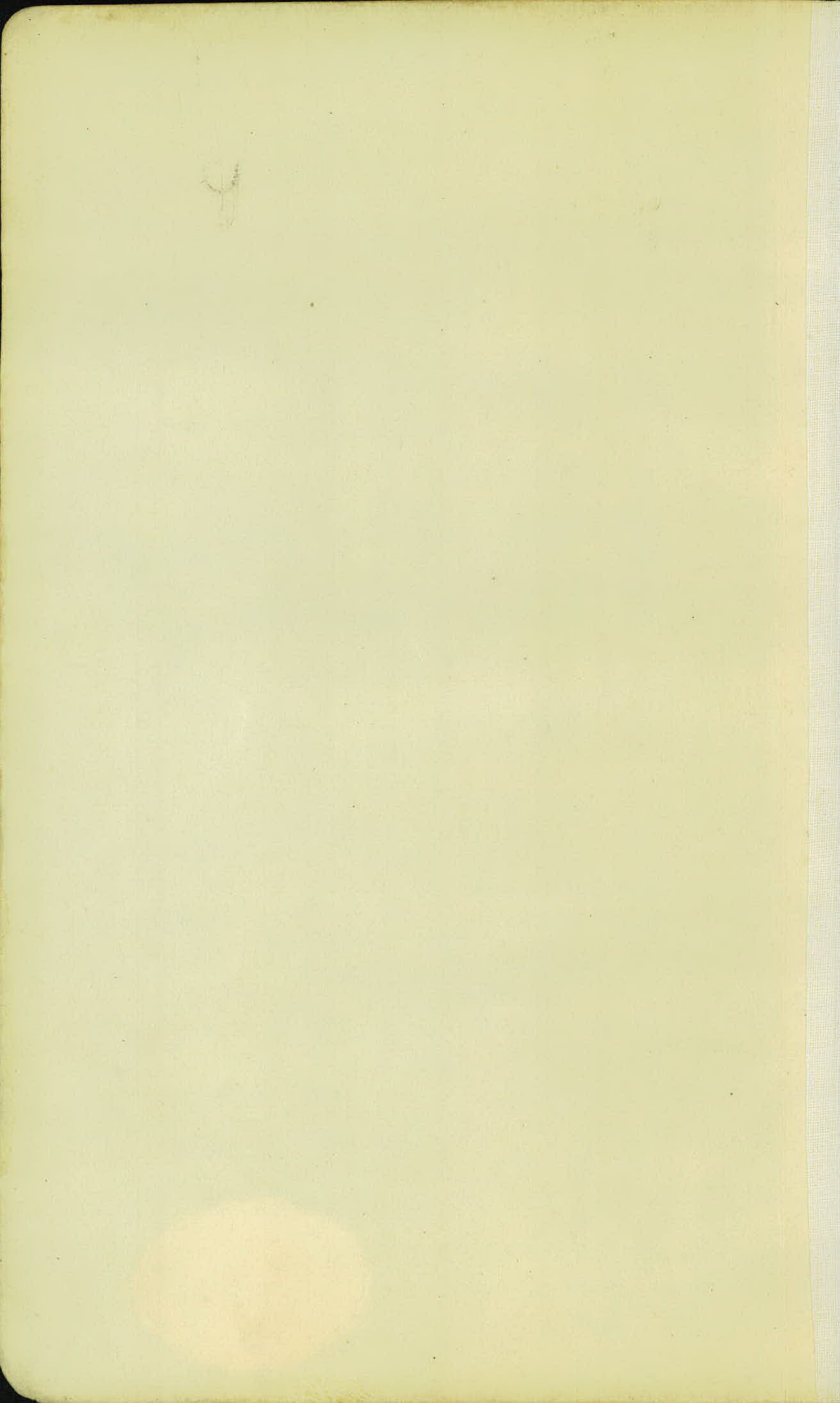
3654
60
219240

20-25
26
2047

5.33
2.60
1.93 465

2/333
1665
120
465





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6-15	Final x section 317+00 - 353+50
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77	C.M.I.
75-76	Original x Sec. of Borrow Pit. 304+00 - 310+50.
70-71	Final x Sec. Borrow Pit. 311+00 - 313+45.
36-43	Final x Sec 424+58 - 456+00
80	Farm Ent.
44-47	X Sec Borrow Pit 304+50 - 314+00
48-50	Final x Sec 314+50 - 328+00
52-57	Final x Sec 394+50 - 424+24
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	From 551+00 - 565 Cont Book 2 Div B.
30-35	Originals of line change - 304+00 to 327+00

Final x sections.

Sta	+	HZ	-	Elev	
B.M.	176	895.33		893.57	
T.P. B.M.	440	887.75	11.98	893.35	
302				82.2	56
+38				82.3	5.5
303				82.4	5.4
+36				82.5	5.3
+70				82.7	5.1
304				82.8	5.0
TP	11.98	895.33	4.40	893.35	
TP	12.13	905.69	1.77	893.26	
302				82.2	23.5
+38				82.3	23.4
303				82.4	23.3
+36				82.5	23.2
+70				82.7	23.0
				82.8	22.9
304.					
B.M.			12.13	893.56	893.57

$$\frac{75}{30} \quad \frac{75}{23} \quad \frac{60}{20} \quad 56 \quad \frac{56}{20} \quad \frac{87}{26} \quad \frac{104}{50}$$

$$\frac{69}{32} \quad \frac{73}{22} \quad \frac{60}{20} \quad \textcircled{5.5} \quad \frac{53}{20} \quad \frac{76}{25} \quad \frac{102}{50}$$

$$\frac{68}{36} \quad \frac{70}{23} \quad \frac{56}{20} \quad 54 \quad \frac{54}{20} \quad \frac{81}{26} \quad \frac{102}{50}$$

$$\frac{68}{36} \quad \frac{66}{21} \quad \frac{55}{19} \quad 53 \quad \frac{52}{20} \quad \frac{82}{27} \quad \frac{102}{50}$$

$$\frac{67}{37} \quad \frac{64}{22} \quad \frac{53}{20} \quad 51 \quad \frac{51}{20} \quad \frac{98}{30} \quad \frac{108}{50}$$

$$\frac{63}{38} \quad \frac{65}{23} \quad \frac{51}{20} \quad \textcircled{5.0} \quad \frac{52}{23} \quad \frac{102}{32} \quad \frac{108}{50}$$

$$\frac{11}{50}$$

$$\frac{28}{51}$$

$$\frac{105}{50}$$

$$\frac{105}{48}$$

$$\frac{134}{50}$$

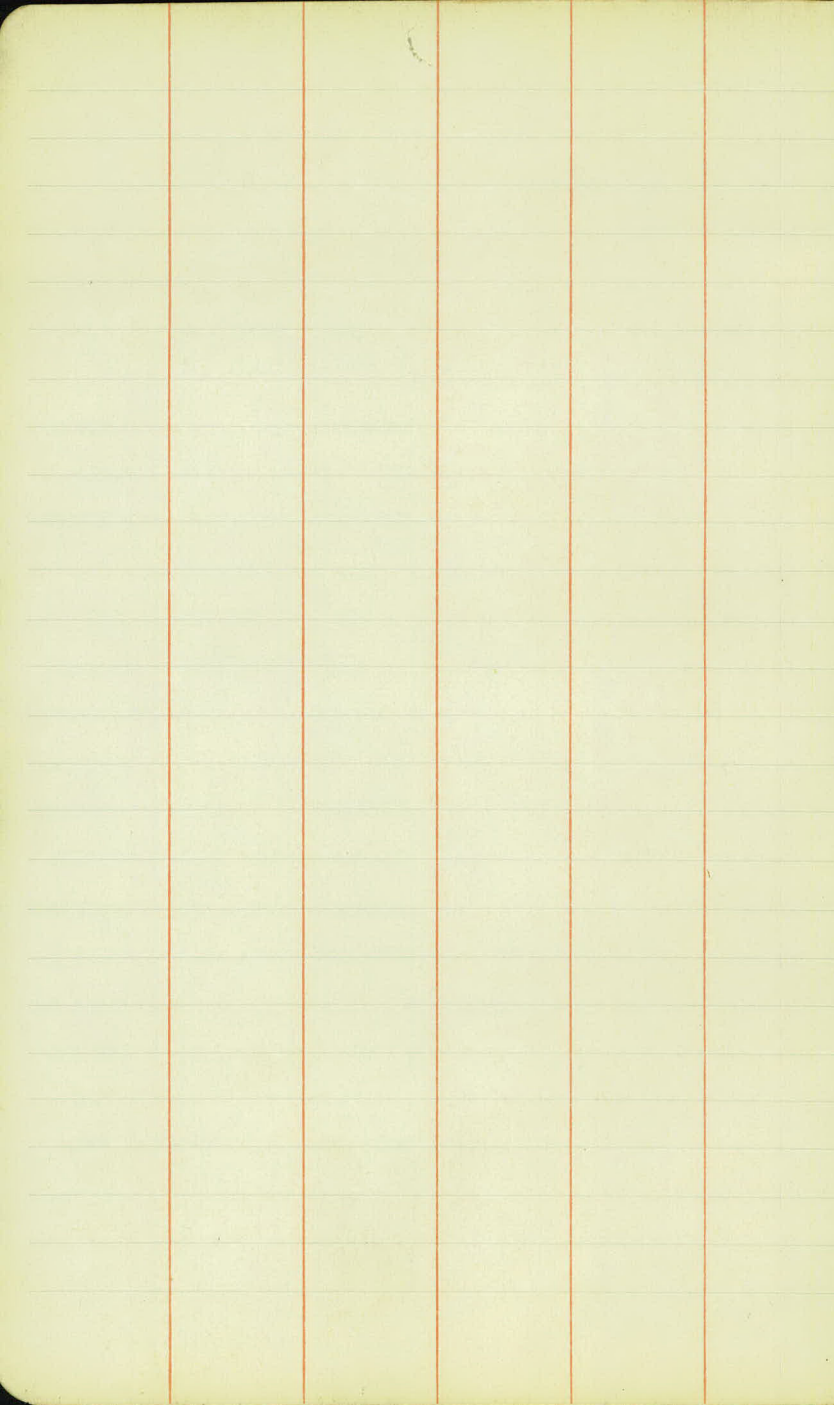
$$\frac{134}{49}$$

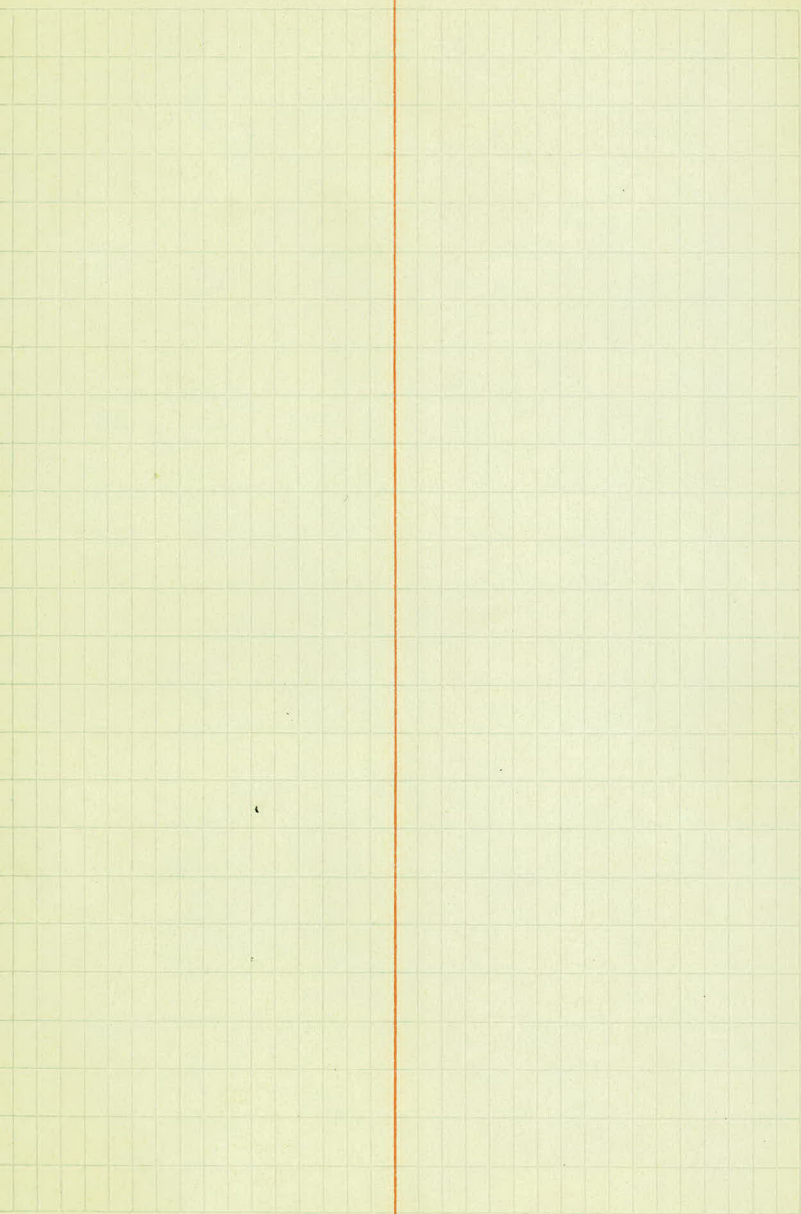
$$\frac{143}{50}$$

$$\frac{145}{49}$$

$$\frac{139}{50}$$

$$\frac{140}{49}$$





Sta	+	HI	-	Elev
B.M.	10.91	890.57		879.66
319+00				89.0
+50				89.3
320				89.6
+50				89.9
321				90.2
T.P.	2.40	892.53	0.44	890.10
+50				90.5
322				91.8
+50				92.0
323				92.2
+50				92.4

90.8

2 spike in 6" Maple 70' Rt sta 304+95

$$\begin{array}{ccccccc} & & & \textcircled{1.6} & & & \\ \frac{4.4}{50} & \frac{7.8}{32} & \frac{1.8}{21} & \frac{1.5}{20} & \frac{1.2}{20} & \frac{11.2}{40} & \frac{11.5}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.3} & & & \\ \frac{2.7}{50} & \frac{6.6}{31} & \frac{1.1}{20} & \frac{1.1}{20} & \frac{1.1}{20} & \frac{11.0}{40} & \frac{12.0}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.0} & & & \\ \frac{5.2}{50} & \frac{7.0}{32} & \frac{0.5}{20} & \frac{0.8}{20} & \frac{1.0}{20} & \frac{10.8}{40} & \frac{11.8}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{2.7} & & & \\ \frac{6.5}{50} & \frac{7.6}{32} & \frac{0.6}{20} & \frac{0.5}{20} & \frac{0.8}{20} & \frac{12.2}{45} & \frac{12.7}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{0.4} & & & \\ \frac{7.7}{50} & \frac{8.7}{37} & \frac{0.2}{20} & \frac{0.1}{20} & \frac{0.2}{20} & \frac{12.3}{46} & \frac{12.6}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{5.0} & & & \\ \frac{11.0}{50} & \frac{12.0}{39} & \frac{2.0}{20} & 2.7 & \frac{3.0}{20} & \frac{14.4}{24} & \frac{14.7}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.1} & & & \\ \frac{12.0}{50} & \frac{11.8}{42} & \frac{2.7}{20} & 2.3 & \frac{2.5}{20} & \frac{12.8}{43} & \frac{13.4}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.5} & & & \\ \frac{13.3}{50} & \frac{12.4}{44} & \frac{2.3}{20} & 2.0 & \frac{2.2}{20} & \frac{12.5}{43} & \frac{13.2}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.3} & & & \\ \frac{14.3}{50} & \frac{13.7}{45} & \frac{2.0}{20} & 1.8 & \frac{1.8}{20} & \frac{13.4}{45} & \frac{14.0}{50} \end{array}$$

$$\begin{array}{ccccccc} & & & \textcircled{1.1} & & & \\ \frac{15.5}{50} & \frac{1.8}{20} & & 1.9 & \frac{1.4}{20} & \frac{14.8}{43} & \frac{14.5}{50} \end{array}$$

819	+	HI	-	5166	
		893.53			
824					92.6
T.P	1.71	894.29	0.95	892.58	
+34					92.7
+66					92.8
325					92.9
T.P	9.76	902.34	1.71	892.58	
B.M	2.06	902.29	2.06	900.28	900.23
+37					93.1
+50					93.1
326					93.2
+30					93.2
+75					93.3
327+00					93.3
+50					93.4

11 $\frac{14.8}{50}$ $\frac{12}{20}$ $\frac{10.9}{10}$ $\frac{12}{10}$ $\frac{12.7}{45}$ $\frac{13.2}{50}$

Turn on end Culvert $\frac{13.8}{50}$ $\frac{13.5}{46}$ $\frac{1.7}{20}$ $\frac{1.6}{17}$ $\frac{1.9}{20}$ $\frac{12.4}{44}$ $\frac{13.2}{56}$

$\frac{11.6}{50}$ $\frac{11.2}{41}$ $\frac{1.7}{20}$ $\frac{1.5}{15}$ $\frac{1.6}{20}$ $\frac{10.8}{40}$ $\frac{11.3}{50}$

$\frac{2.5}{50}$ $\frac{2.0}{32}$ $\frac{1.6}{20}$ $\frac{1.4}{17}$ $\frac{1.7}{20}$ $\frac{8.3}{33}$ $\frac{9.1}{50}$

spike in PPGolt $\frac{8.2}{50}$ $\frac{9.2}{30}$ $\frac{11.3}{29}$ $\frac{10.6}{24}$ $\frac{9.2}{20}$ $\frac{9.2}{20}$ $\frac{9.5}{20}$ $\frac{11.8}{30}$ $\frac{13.4}{20}$

Drive Lt $\frac{2.0}{50}$ $\frac{2.8}{34}$ $\frac{8.5}{20}$ $\frac{4.2}{17}$ $\frac{9.2}{20}$ $\frac{10.0}{33}$ $\frac{11.8}{50}$ Drive Rt

$\frac{3.3}{50}$ $\frac{3.6}{42}$ $\frac{4.1}{39}$ $\frac{10.8}{27}$ $\frac{10.6}{24}$ $\frac{9.0}{20}$ $\frac{9.0}{20}$ $\frac{7.4}{20}$ $\frac{10.5}{53}$ $\frac{11.1}{29}$ $\frac{4.5}{37}$ $\frac{4.3}{40}$ $\frac{5.6}{50}$

$\frac{2.0}{50}$ $\frac{2.0}{44}$ $\frac{2.6}{41}$ $\frac{10.8}{29}$ $\frac{10.3}{24}$ $\frac{8.7}{20}$ $\frac{9.1}{88}$ $\frac{9.2}{20}$ $\frac{10.4}{43}$ $\frac{11.0}{29}$ $\frac{2.0}{41}$ $\frac{1.8}{44}$ $\frac{2.9}{50}$

$\frac{10.5}{27}$ $\frac{10.2}{23}$ $\frac{9.8}{20}$ $\frac{9.0}{89}$ $\frac{9.2}{20}$ $\frac{10.4}{24}$ $\frac{10.8}{29}$

$\frac{3.0}{36}$ $\frac{10.2}{26}$ $\frac{10.0}{23}$ $\frac{8.5}{20}$ $\frac{9.0}{87}$ $\frac{9.1}{20}$ $\frac{10.3}{23}$ $\frac{10.7}{28}$

$\frac{0.0}{40}$ $\frac{4.0}{33}$ $\frac{10.4}{25}$ $\frac{10.0}{22}$ $\frac{8.6}{20}$ $\frac{8.9}{88}$ $\frac{9.1}{20}$ $\frac{10.3}{24}$ $\frac{10.7}{29}$

Sta	+	HI	-	Elev	
328		902.29 [✓]		93.4	
+50				93.4	
+75				93.4	
329				93.3	
+50				93.3	93.5
330				93.2	
T.P	3.98	892.61 [✓]	8.66	893.63 [✓]	
+40				93.1	
+80				93.0	
331				93.0	
+50				92.9	
332				92.8	
+50					

(8.9)

$\frac{8.0}{39}$	$\frac{5.2}{31}$	$\frac{10.2}{24}$	$\frac{9.8}{21}$	$\frac{8.7}{20}$	$\frac{8.6}{20}$	$\frac{9.2}{20}$	$\frac{10.4}{24}$	$\frac{10.8}{29}$
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(8.9)

$\frac{9.0}{39}$	$\frac{5.0}{32}$	$\frac{10.4}{24}$	$\frac{10.0}{22}$	$\frac{9.0}{20}$	$\frac{8.8}{20}$	$\frac{9.3}{20}$	$\frac{10.6}{23}$	$\frac{11.2}{28}$
------------------	------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------

(8.9)

$\frac{10.4}{25}$	$\frac{10.1}{22}$	$\frac{8.5}{20}$	$\frac{9.0}{20}$	$\frac{9.2}{20}$	$\frac{10.7}{23}$	$\frac{11.1}{28}$
-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------

(9.0)

$\frac{10.4}{25}$	$\frac{10.2}{22}$	$\frac{8.9}{20}$	$\frac{8.9}{20}$	$\frac{9.2}{20}$	$\frac{10.5}{23}$	$\frac{11.0}{28}$	$\frac{3.5}{39}$	$\frac{5.1}{42}$	$\frac{4.2}{50}$
-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	------------------	------------------	------------------

(9.0)

$\frac{10.4}{27}$	$\frac{10.0}{22}$	$\frac{8.7}{20}$	$\frac{8.8}{20}$	$\frac{9.2}{20}$	$\frac{10.4}{23}$	$\frac{11.0}{28}$	$\frac{6.2}{35}$	$\frac{6.1}{37}$	$\frac{9.0}{50}$
-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	------------------	------------------	------------------

(9.1)

$\frac{10.5}{27}$	$\frac{10.1}{22}$	$\frac{8.7}{20}$	$\frac{8.7}{20}$	$\frac{8.8}{20}$	$\frac{10.1}{23}$	$\frac{10.5}{27}$	$\frac{7.6}{32}$	$\frac{7.3}{35}$	$\frac{10.0}{50}$
-------------------	-------------------	------------------	------------------	------------------	-------------------	-------------------	------------------	------------------	-------------------

(4.5)

$\frac{6.6}{29}$	$\frac{5.8}{22}$	$\frac{4.4}{20}$	$\frac{4.2}{20}$	$\frac{4.3}{20}$	$\frac{5.7}{23}$	$\frac{6.2}{27}$	$\frac{5.0}{29}$	$\frac{4.7}{32}$	$\frac{6.3}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

(4.6)

$\frac{6.0}{27}$	$\frac{5.7}{23}$	$\frac{4.0}{20}$	$\frac{4.2}{20}$	$\frac{4.5}{20}$	$\frac{5.9}{23}$	$\frac{6.5}{28}$	$\frac{5.3}{29}$	$\frac{5.0}{32}$	$\frac{6.5}{45}$	$\frac{6.0}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

(4.6)

$\frac{6.2}{29}$	$\frac{5.5}{23}$	$\frac{4.2}{20}$	$\frac{4.2}{20}$	$\frac{4.5}{20}$	$\frac{5.5}{23}$	$\frac{6.4}{27}$	$\frac{4.5}{30}$	$\frac{4.2}{34}$	$\frac{6.0}{44}$	$\frac{5.2}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

(4.7)

$\frac{6.4}{29}$	$\frac{5.5}{23}$	$\frac{4.3}{20}$	$\frac{4.1}{20}$	$\frac{4.0}{20}$	$\frac{5.6}{23}$	$\frac{6.3}{28}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------

(4.8)

$\frac{6.0}{29}$	$\frac{5.3}{22}$	$\frac{4.4}{20}$	$\frac{4.4}{20}$	$\frac{4.7}{20}$	$\frac{6.0}{23}$	$\frac{6.5}{28}$
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Sta	+	HI	-	Elev
		897.61		
332	+85			92.7
333				92.6
	+45			92.5
	+75			92.5
334				92.4
	+60			92.3
335				92.4
T. P.M.			690	890.71
DM	10.27	910.50		900.33
326	+95			93.3
327				93.3
	+50			93.4
328				93.4
	+50			93.4

$$\begin{array}{r} 4.9 \\ \frac{68}{29} \quad \frac{61}{23} \quad \frac{45}{20} \\ \hline 4.5 \end{array} \quad \begin{array}{r} \frac{29}{20} \quad \frac{65}{23} \quad \frac{68}{26} \end{array}$$

$$\begin{array}{r} 5.0 \\ \frac{66}{28} \quad \frac{59}{22} \quad \frac{45}{20} \\ \hline 4.6 \end{array} \quad \begin{array}{r} \frac{49}{10} \quad \frac{64}{23} \quad \frac{68}{26} \end{array}$$

$$\begin{array}{r} 5.1 \\ \frac{70}{30} \quad \frac{65}{28} \quad \frac{49}{20} \\ \hline 4.7 \end{array} \quad \begin{array}{r} \frac{52}{20} \quad \frac{65}{22} \quad \frac{68}{27} \quad \frac{68}{37} \quad \frac{64}{40} \quad \frac{61}{50} \end{array}$$

$$\begin{array}{r} 5.1 \\ \frac{70}{30} \quad \frac{64}{28} \quad \frac{49}{20} \\ \hline 5.0 \end{array} \quad \begin{array}{r} \frac{53}{20} \quad \frac{66}{23} \quad \frac{70}{25} \quad \frac{60}{27} \quad \frac{66}{55} \end{array}$$

$$\begin{array}{r} 5.2 \\ \frac{72}{31} \quad \frac{64}{33} \quad \frac{51}{20} \\ \hline 5.0 \end{array} \quad \begin{array}{r} \frac{53}{20} \quad \frac{74}{25} \quad \frac{86}{50} \end{array}$$

$$\begin{array}{r} 5.3 \\ \frac{69}{50} \quad \frac{73}{37} \quad \frac{81}{34} \quad \frac{70}{25} \quad \frac{52}{20} \\ \hline 5.1 \end{array} \quad \begin{array}{r} \frac{55}{20} \quad \frac{75}{28} \quad \frac{100}{45} \quad \frac{110}{50} \end{array}$$

$$\begin{array}{r} 5.4 \\ \frac{100}{50} \quad \frac{70}{28} \quad \frac{53}{20} \quad \frac{52}{20} \quad \frac{55}{20} \quad \frac{106}{31} \quad \frac{120}{50} \end{array}$$

Top Pack 50' L-843 335+50

20142 in 20 60' L-843 322+50

$$\frac{61}{50} \quad \frac{65}{47}$$

$$17.2$$

$$\frac{61}{48} \quad \frac{61}{50}$$

$$\frac{2.8}{50}$$

$$17.8$$

$$\frac{43}{49} \quad \frac{42}{50}$$

$$17.1$$

$$\frac{56}{47} \quad \frac{56}{50}$$

$$17.1$$

$$\frac{70}{45} \quad \frac{66}{48} \quad \frac{67}{50}$$

$$17.1$$

$$\frac{85}{43} \quad \frac{80}{47} \quad \frac{81}{50}$$

910.50 ✓

328+75

93.4

331+50

92.9

332+100

92.8

+50

92.7

+85

333+00

92.6

T.P

9.76

919.57 ✓

0.37

910.13 ✓

327+50

93.4

328

93.4

+50

93.4

+75

93.4

329

93.3

+50

93.3

330

93.2

T.P

1.70

910.93 ✓

10.66

909.23 ✓

+40

93.1

+50

93.0

331

93.0

+50

92.9

332

92.8

+50

92.7

+85

(17.1)

$\frac{8.8}{42}$ $\frac{8.5}{44}$ $\frac{9.2}{50}$

(17.6)

$\frac{13.3}{37}$ $\frac{13.3}{40}$ $\frac{15.3}{50}$

(17.7)

$\frac{7.1}{47}$ $\frac{6.8}{50}$

(17.8)

$\frac{12.0}{36}$ $\frac{7.5}{44}$ $\frac{2.0}{50}$ $\frac{1.5}{52}$

$\frac{12.0}{34}$ $\frac{5.5}{45}$ $\frac{0.2}{57}$ $\frac{0.0}{54}$

(17.9)

$\frac{12.2}{35}$ $\frac{7.0}{43}$ $\frac{1.4}{50}$ $\frac{0.8}{53}$

(26.5)

(26.0)

(26.5)

(26.0)

(26.6)

(26.6)

(26.7)

(17.8)

(17.9)

(17.9)

(18.0)

(18.1)

(18.2)

$\frac{4.8}{53}$ $\frac{5.2}{50}$
 $\frac{5.5}{55}$ $\frac{3.3}{50}$
 $\frac{6.8}{54}$ $\frac{7.7}{50}$
 $\frac{6.8}{54}$ $\frac{7.8}{50}$
 $\frac{8.5}{52}$ $\frac{8.2}{50}$
 $\frac{8.0}{52}$ $\frac{9.0}{49}$
 $\frac{11.4}{50}$ $\frac{11.8}{44}$

$\frac{7.2}{50}$ $\frac{8.4}{46}$
 $\frac{7.6}{50}$ $\frac{8.0}{49}$ $\frac{8.7}{46}$
 $\frac{8.0}{50}$ $\frac{8.4}{49}$ $\frac{9.2}{44}$
 $\frac{8.2}{50}$ $\frac{8.4}{48}$ $\frac{9.1}{45}$
 $\frac{7.1}{50}$ $\frac{8.2}{46}$
 $\frac{4.2}{53}$ $\frac{5.1}{50}$
 $\frac{4.2}{54}$ $\frac{5.1}{50}$

910.93 ✓

333

92.6

45

92.5

+75

92.5

334

92.5

TP

1.13

900.40 ✓

11.66

899.27 ✓

B.M.T.P.

5.06

895.77

2.72

890.68 ✓ = 890.71

335+38

895.74

Big Hand Ditch
on Rt 335+10 92.7

336

92.0

+50

91.9

337

91.8

+50

91.7

338

End Hand Ditch
Sta 328+00 on Rt. 91.6
Big Hand Ditch
325+00 on Rt

+50

91.6

339

91.7

+50

92.0

$\frac{41}{50}$ $\frac{50}{50}$
 $\frac{26}{50}$ $\frac{85}{47}$
 $\frac{60}{50}$ $\frac{62}{49}$ $\frac{72}{46}$
 $\frac{70}{50}$ $\frac{73}{48}$ $\frac{83}{46}$

(8.3)
 (8.4)
 (8.4)
 (8.5)

Top Rock Lt 5+0 33+50

$\frac{90}{50}$ $\frac{88}{31}$ $\frac{26}{21}$ $\frac{34}{35}$ $\frac{35}{20}$ $\frac{96}{33}$ $\frac{100}{43}$ $\frac{136}{45}$ $\frac{136}{46}$ $\frac{94}{50}$

HO HO

(3.7)

$\frac{108}{50}$ $\frac{107}{34}$ $\frac{40}{21}$ $\frac{37}{21}$ $\frac{38}{21}$ $\frac{106}{35}$ $\frac{108}{44}$ $\frac{127}{46}$ $\frac{127}{47}$ $\frac{110}{50}$

HO HO

(3.8)

$\frac{108}{50}$ $\frac{93}{27}$ $\frac{46}{20}$ $\frac{47}{20}$ $\frac{42}{20}$ $\frac{123}{36}$ $\frac{115}{46}$ $\frac{126}{48}$ $\frac{126}{48}$ $\frac{165}{50}$

HO HO

(3.9)

$\frac{102}{50}$ $\frac{102}{32}$ $\frac{90}{27}$ $\frac{46}{20}$ $\frac{46}{20}$ $\frac{40}{20}$ $\frac{92}{27}$ $\frac{113}{37}$ $\frac{121}{45}$ $\frac{130}{46}$ $\frac{130}{48}$ $\frac{123}{50}$

HO HO

(4.0)

$\frac{100}{50}$ $\frac{92}{27}$ $\frac{50}{20}$ $\frac{48}{20}$ $\frac{45}{20}$ $\frac{88}{37}$ $\frac{122}{38}$ $\frac{123}{47}$ $\frac{128}{49}$ $\frac{128}{49}$ $\frac{123}{50}$

HO HO

1CC:

(4.1)

$\frac{107}{50}$ $\frac{103}{36}$ $\frac{47}{20}$ $\frac{47}{21}$ $\frac{44}{21}$ $\frac{90}{28}$ $\frac{120}{41}$ $\frac{123}{48}$ $\frac{130}{48}$ $\frac{130}{49}$ $\frac{123}{50}$

HO HO

(4.1)

$\frac{100}{33}$ $\frac{100}{33}$ $\frac{85}{28}$ $\frac{43}{21}$ $\frac{42}{20}$ $\frac{94}{29}$ $\frac{120}{28}$ $\frac{118}{50}$

(4.0)

$\frac{103}{80}$ $\frac{103}{43}$ $\frac{117}{44}$ $\frac{117}{40}$ $\frac{110}{34}$ $\frac{113}{35}$ $\frac{40}{20}$ $\frac{85}{27}$ $\frac{124}{35}$ $\frac{123}{50}$

(3.7)

$\frac{96}{50}$ $\frac{96}{45}$ $\frac{114}{46}$ $\frac{115}{40}$ $\frac{102}{37}$ $\frac{105}{34}$ $\frac{87}{20}$ $\frac{27}{20}$ $\frac{37}{20}$ $\frac{90}{27}$ $\frac{124}{38}$ $\frac{122}{50}$

Sta	+	HT	-	Elev
		895.77		
		895.74		
342				92.3
	+50			92.8
341				93.3
				End of Dist. in 1st
				341 = 90
				Begin Dist. in 2nd
				341 = 50 94.0
	+50			
T.P	2.63	901.45	2.95	892.82
		901.42		892.74
344				94.7
BM	4.62	901.41	4.62	896.53
		901.42		896.79
	+20			94.9
	+50			95.4
	+75			95.8
343				96.3
	+25			96.7
	+50			97.4
344				97.9

80 84 106 102 96 93 37
 50 44 42 37 35 31 20

(3.4)

32 25 11.5 11.8
 21 38 50

74 80 98 94 86 86 30
 50 43 41 37 34 32 20

(2.9)

26 2.7 10.1 19.5
 20 35 50

5.5 63 80 80 73 73 22
 50 43 41 36 34 30 20

(2.2)

22 8.7 9.0
 20 33 50

46 55 72 71 63 61 12
 50 40 41 36 34 30 20

(1.7)

14 16 7.5 7.8 7.8 7.6 8.0
 20 33 34 35 36 50

101 113 128 124 118 115 67
 50 44 42 37 34 30 20

(6.7)

6.5 6.5 9.6 10.6 12.3 12.3 9.8 9.8
 20 26 32 35 3.6 37 50

spike in Cor. F. Post Pt 349 342+20

110 160 66 63 8.8 10.4 10.4 6.0 5.0
 50 29 20 20 29 34 37 40 50

(6.0)

108 103 95 63 5.5 5.7 6.6 7.8 10.1 10.1 5.2 4.4
 50 32 28 20 20 24 30 36 38 43 50

(5.6)

104 97 91 60 5.7 5.0 6.3 7.1 9.6 9.6 3.0 2.6
 50 35 27 20 20 23 29 37 40 48 50

(5.1)

101 90 82 56 4.7 4.5 6.3 7.0 9.5 9.5 2.6
 50 36 26 20 20 25 30 38 41 50

(4.7)

100 91 80 52 4.4 4.2 6.2 6.4 9.2 9.4 2.1
 50 34 26 20 20 24 30 38 41 50

(4.0)

100 90 4.8 4.1 3.7 5.7 6.3 9.0 9.3 4.8
 50 29 20 20 25 29 37 42 50

(3.5)

92 96 4.3 3.6 2.6 7.4 8.8 9.2 9.3 7.0
 50 32 21 20 31 36 40 43 50

Sta	+	HT	-	Elev
		901.41		
344+50				98.7
345				99.5
+35				900.1
+50				900.3
T.P.	10.05	909.81 ✓	1.68	899.73 ✓
346				01.1
+50				01.9
347				02.7
+38				03.3
+50				03.5
+75				03.9
				04.3
348				

$$\frac{83}{50} \frac{84}{44} \frac{90}{40} \frac{80}{38} \frac{87}{34} \frac{85}{32} \frac{85}{24}$$

$$\textcircled{2.7} \quad 26 \frac{18}{20} \frac{70}{31} \frac{72}{33} \frac{88}{37} \frac{88}{42} \frac{60}{45} \frac{67}{50}$$

$$\frac{64}{50} \frac{72}{47} \frac{83}{40} \frac{80}{36} \frac{80}{35} \frac{76}{32} \frac{30}{22}$$

$$\textcircled{1.9} \quad 17 \frac{11}{20} \frac{57}{33} \frac{88}{39} \frac{88}{44} \frac{44}{50}$$

$$\frac{34}{50} \frac{54}{40} \frac{74}{39} \frac{72}{38} \frac{58}{34} \frac{53}{29} \frac{21}{22}$$

$$\textcircled{1.3} \quad 4 \frac{0.3}{20} \frac{68}{35} \frac{72}{38} \frac{88}{40} \frac{90}{44} \frac{68}{45} \frac{66}{50}$$

$$\frac{26}{50} \frac{53}{40} \frac{72}{38} \frac{64}{35} \frac{60}{29} \frac{20}{22}$$

$$\textcircled{1.1} \quad 07 \frac{0.1}{20} \frac{75}{37} \frac{76}{38} \frac{86}{39} \frac{90}{43} \frac{71}{45} \frac{70}{50}$$

$$\frac{57}{50} \frac{86}{35} \frac{122}{33} \frac{120}{30} \frac{112}{26} \frac{72}{22}$$

$$\textcircled{8.1} \quad 86 \frac{76}{20} \frac{155}{36} \frac{160}{39} \frac{163}{40} \frac{165}{43} \frac{160}{44} \frac{150}{50} \quad \text{2nd Pitch 519}$$

$$\frac{104}{28} \frac{100}{25} \frac{87}{22}$$

$$\textcircled{7.9} \quad 76 \frac{70}{20} \frac{130}{33} \frac{134}{50}$$

$$\frac{94}{28} \frac{74}{24} \frac{80}{22}$$

$$\textcircled{7.1} \quad 72 \frac{63}{20} \frac{79}{24} \frac{80}{28} \frac{67}{31} \frac{60}{35} \frac{70}{37} \frac{80}{50}$$

$$\frac{87}{28} \frac{83}{25} \frac{94}{22}$$

$$\textcircled{6.5} \quad 65 \frac{57}{20} \frac{74}{23} \frac{75}{29}$$

$$\frac{86}{28} \frac{80}{24} \frac{71}{22}$$

$$\textcircled{6.3} \quad 61 \frac{56}{20} \frac{71}{24} \frac{73}{30}$$

$$\frac{83}{28} \frac{77}{25} \frac{66}{22}$$

$$\textcircled{5.9} \quad 56 \frac{52}{20} \frac{68}{24} \frac{70}{29}$$

$$\frac{77}{29} \frac{71}{24} \frac{62}{22}$$

$$\textcircled{5.5} \quad 53 \frac{48}{20} \frac{63}{23} \frac{67}{28}$$

Sta	+	HZ	-	Flow
		909.81 ✓		
348+50				05.2
349				05.9
+50				06.7
350				07.5
+40				08.1
T.P	8.20	917.43 ✓	0.88	909.23 ✓
351				09.1
^{351.54} = 73.20				10.5
352				10.5
+50				11.3
353				12.1
+50				12.8
T.P.	7.58	922.60 ✓	2.41	915.02 ✓
B 17			2.03	920.56 - 920.53
				920.57

33	26	28	20	67	54	44	(4.6)	3.8	5.8	6.2
50	40	36	29	24	22	✓		20	24	28

16	06	10	6.0	5.5	47	37	(3.9)	3.1	4.4	5.0
50	41	37	28	24	22	✓		20	23	29

53	52	3.5	(3.1)	2.3	3.6	4.0
30	24	22	30	20	23	28

5.0	4.6	3.2	(2.1)	1.3	2.5	3.0
29	24	22	20	20	23	27

4.2	3.8	2.4	(1.7)	0.6	2.0	2.4
29	25	22	11	20	23	29

56	57	6.5	10.3	10.5	9.0	7.7	(8.3)	7.1	8.7	9.0
50	38	35	29	24	21	✓		20	22	26

5.2	5.5	6.2	9.8	7.2	7.8	7.1	(6.9)	6.7	8.1	8.4	5.6	5.0	4.7
50	37	30	28	23	20	✓		20	24	28	32	36	50

4.0	4.0	5.2	9.1	8.7	7.2	6.6	(6.9)	6.6	7.6	8.1	7.0	6.6
50	38	34	28	23	20	✓		20	23	25	30	50

4.6	3.6	4.2	8.1	7.7	6.1	6.0	(6.1)	6.0	7.6	8.0	7.2	7.0	7.7
56	37	34	27	23	20	6.0		20	25	29	31	35	50

6.0	5.6	6.1	7.6	7.3	5.7	5.5	(5.3)	5.1	7.3	7.5	7.0	6.6	7.0
50	33	29	27	24	20	5.5		20	26	29	30	33	50

8.0	5.8	6.0	7.0	6.5	4.8	4.6	(4.6)	4.5	5.6	6.5	4.4	4.2	4.4
50	32	28	26	24	20	4.6		20	23	29	33	36	50

spike in Cor Fence Post Rt 29 251+00

Sta	+	HI	-	Elev ✓
BM ₁	0.90	921.43		920.53
346+50				01.9
347				02.7
438				03.3
+50				03.5
+75				03.9
348				04.3
+50				05.2
349				05.9
+50				06.7
350				07.5
+40				08.1
351+00				09.1

2 pipe in Cor Fence Post R+Stg 357+00.

$$\frac{27}{50}$$

(19.5)

$$\frac{40}{50}$$

(18.7)

$$\frac{27}{50}$$

(18.1)

$$\frac{23}{46} \quad \frac{20}{50}$$

$$\frac{30}{50}$$

(17.9)

$$\frac{25}{41} \quad \frac{20}{44} \quad \frac{20}{50}$$

$$\frac{22}{50} \quad \frac{20}{47} \quad \frac{22}{44}$$

(17.5)

$$\frac{42}{50}$$

$$\frac{125}{50} \quad \frac{117}{44} \quad \frac{110}{41}$$

(17.1)

$$\frac{34}{50}$$

(16.2)

$$\frac{86}{40} \quad \frac{81}{43} \quad \frac{78}{50}$$

(15.5)

$$\frac{91}{39} \quad \frac{86}{43} \quad \frac{88}{50}$$

$$\frac{82}{50} \quad \frac{85}{45} \quad \frac{88}{41}$$

(14.7)

$$\frac{63}{42} \quad \frac{60}{44} \quad \frac{61}{50}$$

$$\frac{66}{50} \quad \frac{65}{48} \quad \frac{65}{41}$$

(13.9)

$$\frac{32}{24} \quad \frac{30}{47} \quad \frac{30}{50}$$

$$\frac{44}{50} \quad \frac{41}{48} \quad \frac{41}{40}$$

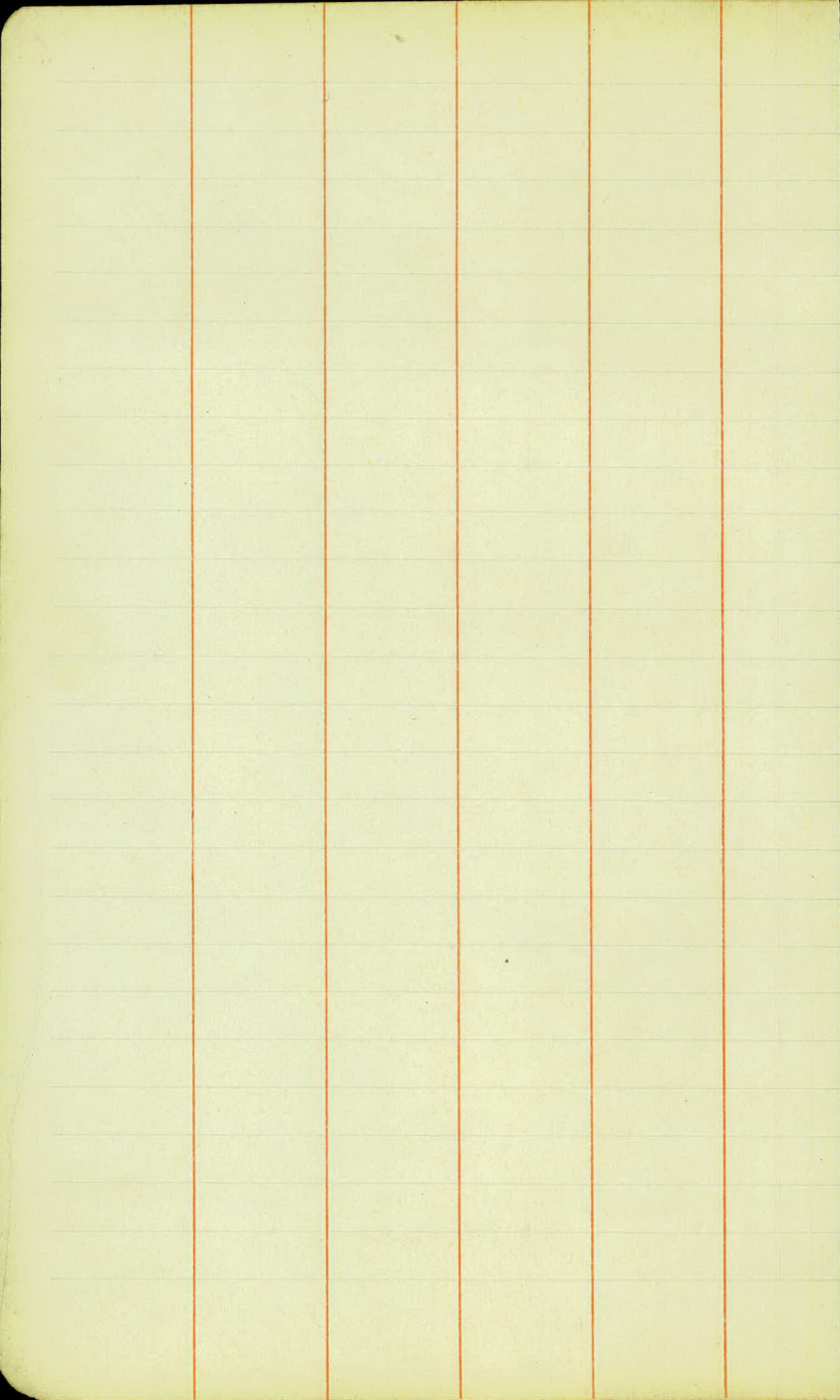
(13.3)

$$\frac{21}{27} \quad \frac{17}{50}$$

(12.3)

$$\frac{22}{24} \quad \frac{22}{45} \quad \frac{23}{50}$$

continued on page 20



The image shows a page of graph paper with a grid of small squares. A vertical red line runs down the center of the page, dividing it into two equal halves. The grid is composed of 20 columns and 20 rows of squares. The paper is off-white and shows some signs of age and wear.

B.M. 0.71 921.24 ✓ 920.53

354+00 08.0

+50 7.7

355+00 7.6

+50 7.7

356 8.1

+50 8.6
E. D. 1/4 L
+60

357 9.3

T.P. 0.24 912.10 ✓ 9.38 911.86 ✓

+57 1.0

358 1.8

1
+50 2.5

359 3.1

+50 3.4

$$\begin{array}{cccccccccccc} \frac{11.4}{50} & \frac{7.8}{32.5} & \frac{8.3}{29} & \frac{10.4}{26.7} & \frac{10.1}{24} & \frac{9.2}{20} & \frac{8.7}{20} & \frac{8.1}{20} & \frac{9.0}{22.6} & \frac{9.5}{29} & \frac{5.6}{31.5} & \frac{5.1}{37.7} & \frac{5.2}{50} \end{array}$$

80

$$\begin{array}{cccccccccccc} \frac{8.5}{50} & \frac{7.8}{32} & \frac{7.5}{31} & \frac{10.0}{27} & \frac{9.7}{23} & \frac{7.5}{20} & \frac{7.8}{20} & \frac{7.9}{20} & \frac{8.7}{22} & \frac{9.2}{28.5} & \frac{4.0}{38} & \frac{3.7}{41} & \frac{3.7}{50} \end{array}$$

7.7

$$\begin{array}{cccccccccccc} \frac{6.1}{50} & \frac{5.3}{37} & \frac{5.7}{32} & \frac{9.6}{26.5} & \frac{8.9}{23} & \frac{7.8}{20} & \frac{7.5}{20} & \frac{7.7}{20} & \frac{9.1}{22.5} & \frac{9.3}{30} & \frac{3.9}{37.5} & \frac{3.6}{41} & \frac{4.0}{50} \end{array}$$

7.6

$$\begin{array}{cccccccccccc} \frac{4.0}{50} & \frac{4.0}{40} & \frac{4.4}{37} & \frac{9.7}{28} & \frac{7.2}{44.5} & \frac{8.1}{20} & \frac{7.6}{20} & \frac{7.9}{20} & \frac{8.9}{22} & \frac{9.2}{27.5} & \frac{4.0}{37} & \frac{3.8}{40} & \frac{3.6}{50} \end{array}$$

7.7

$$\begin{array}{cccccccccccc} \frac{3.9}{50} & \frac{4.0}{40} & \frac{4.4}{37} & \frac{10.8}{29} & \frac{9.6}{23.5} & \frac{8.3}{20} & \frac{7.9}{20} & \frac{8.0}{20} & \frac{9.2}{23} & \frac{9.5}{24.5} & \frac{5.0}{36} & \frac{4.7}{40.5} & \frac{4.6}{50} \end{array}$$

81

$$\begin{array}{cccccccccccc} \frac{6.3}{50} & \frac{4.4}{36} & \frac{6.9}{33} & \frac{10.9}{27.4} & \frac{12.7}{23.5} & \frac{9.8}{20} & \frac{8.5}{20} & \frac{8.5}{20} & \frac{10.0}{23} & \frac{10.3}{33} & \frac{9.0}{33.5} & \frac{8.4}{50} \end{array}$$

8.6

$$\begin{array}{cccccccccccc} \frac{11.4}{50} & \frac{11.8}{31} & \frac{12.4}{20} & \frac{12.8}{25.5} & \frac{9.5}{20} & \frac{7.2}{20} & \frac{9.5}{20} & \frac{13.0}{27.5} & \frac{13.1}{37.5} & \frac{12.8}{50} \end{array}$$

9.3

$$\begin{array}{cccccccccccc} \frac{9.6}{50} & \frac{9.7}{46} & \frac{10.2}{28} & \frac{11}{21} & \frac{9.8}{20} & \frac{1.2}{20} & \frac{7.9}{26.5} & \frac{7.5}{50} \end{array}$$

1.0

$$\begin{array}{cccccccccccc} \frac{13.0}{50} & \frac{12.9}{42} & \frac{1.9}{20} & \frac{1.3}{20} & \frac{1.7}{20.5} & \frac{11.9}{40} & \frac{12.5}{50} \end{array}$$

18

$$\begin{array}{cccccccccccc} \frac{14.2}{55} & \frac{14.1}{45} & \frac{2.7}{21} & \frac{2.0}{20} & \frac{2.1}{19} & \frac{1.50}{44} & \frac{1.4.5}{50} \end{array}$$

2.0

$$\begin{array}{cccccccccccc} \frac{15.9}{50} & \frac{15.5}{45} & \frac{3.0}{20} & \frac{2.5}{20} & \frac{2.9}{20} & \frac{1.4.9}{44} & \frac{15.4}{50} \end{array}$$

3.1

$$\begin{array}{cccccccccccc} \frac{16.0}{50} & \frac{15.6}{45} & \frac{3.5}{20} & \frac{2.9}{20} & \frac{3.5}{20} & \frac{15.0}{44} & \frac{15.4}{50} \end{array}$$

3.4

Sta	+	H I	-	Flow	
360		912.10 ✓			3.7
260					3.7
361					3.7
+50					3.4
T.P.	10.44	120.18 ✓	2.36	909.74 ✓	
362					11.1
+55					10.5
363					10.0
+45					9.6
364					9.1
1					
+50					8.6
T.P.	11.38	924.08 ✓		7.48	912.70 ✓
365					12.0
+50					11.5
366					11.0

(3.7)

$\frac{160}{50}$	$\frac{154}{44}$	$\frac{34}{20}$	$\frac{32}{20}$	$\frac{56}{20}$	$\frac{144}{41}$	$\frac{147}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

(3.7)

$\frac{140}{50}$	$\frac{139}{42}$	$\frac{36}{20}$	$\frac{32}{20}$	$\frac{37}{20}$	$\frac{127}{37}$	$\frac{133}{43}$	$\frac{125}{45}$	$\frac{126}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

(3.7)

$\frac{114}{50}$	$\frac{116}{42}$	$\frac{126.85}{41.5}$	$\frac{30}{20}$	$\frac{37}{20}$	$\frac{92}{29.5}$	$\frac{97}{34}$	$\frac{86}{36.5}$	$\frac{6.5}{50}$
------------------	------------------	-----------------------	-----------------	-----------------	-------------------	-----------------	-------------------	------------------

(3.4)

$\frac{46}{50}$	$\frac{45}{31}$	$\frac{57}{27.5}$	$\frac{49.33}{22.5}$	$\frac{33}{20}$	$\frac{34}{20}$	$\frac{47}{23.5}$	$\frac{5.3}{30}$	$\frac{66}{36}$	$\frac{60}{39.5}$	$\frac{105}{40}$	$\frac{110}{50}$
-----------------	-----------------	-------------------	----------------------	-----------------	-----------------	-------------------	------------------	-----------------	-------------------	------------------	------------------

(11)

$\frac{76}{50}$	$\frac{72}{37}$	$\frac{75}{35}$	$\frac{124}{28}$	$\frac{122}{24}$	$\frac{11}{20}$	$\frac{109}{20}$	$\frac{119}{23}$	$\frac{130}{27.5}$	$\frac{47}{41}$	$\frac{44}{45}$	$\frac{52}{50}$
-----------------	-----------------	-----------------	------------------	------------------	-----------------	------------------	------------------	--------------------	-----------------	-----------------	-----------------

(10.5)

$\frac{2.2}{50}$	$\frac{2.0}{46}$	$\frac{2.4}{43}$	$\frac{11.9}{29}$	$\frac{11.4}{22}$	$\frac{10.4}{20}$	$\frac{102}{20}$	$\frac{102}{23}$	$\frac{112}{29}$	$\frac{119}{34}$	$\frac{8.6}{30}$	$\frac{83}{30}$	$\frac{191}{50}$
------------------	------------------	------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	------------------

(0.0)

$\frac{64}{50}$	$\frac{69}{47}$	$\frac{15}{45}$	$\frac{11.7}{20}$	$\frac{11.0}{42}$	$\frac{10.1}{20}$	$\frac{91}{20}$	$\frac{98}{20}$	$\frac{107}{23}$	$\frac{114}{27}$	$\frac{9.5}{32}$	$\frac{93}{35}$	$\frac{114}{50}$
-----------------	-----------------	-----------------	-------------------	-------------------	-------------------	-----------------	-----------------	------------------	------------------	------------------	-----------------	------------------

(9.6)

$\frac{65}{50}$	$\frac{97}{47}$	$\frac{14}{44}$	$\frac{11.2}{30}$	$\frac{10.7}{23}$	$\frac{7.6}{20}$	$\frac{94}{20}$	$\frac{96}{23}$	$\frac{102}{28}$	$\frac{109}{31}$	$\frac{8.6}{34}$	$\frac{85}{34}$	$\frac{9.5}{50}$
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(7)

$\frac{13}{50}$	$\frac{13}{46}$	$\frac{17}{43}$	$\frac{10.5}{30}$	$\frac{10.1}{22.5}$	$\frac{9}{20}$	$\frac{88}{20}$	$\frac{96}{20}$	$\frac{100}{23}$	$\frac{10.5}{29}$	$\frac{46}{38}$	$\frac{40}{42}$	$\frac{45}{50}$
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(8.6)

$\frac{15}{50}$	$\frac{14}{45}$	$\frac{1.9}{42}$	$\frac{7.8}{29}$	$\frac{7.6}{23}$	$\frac{8.5}{20}$	$\frac{84}{20}$	$\frac{84}{23}$	$\frac{9.5}{29}$	$\frac{100}{42}$	$\frac{1.0}{47}$	$\frac{0.2}{47}$	$\frac{0.0}{50}$
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(12.0)

$\frac{58}{50}$	$\frac{56}{42}$	$\frac{59}{41}$	$\frac{13.5}{29}$	$\frac{13.1}{23}$	$\frac{11.9}{20}$	$\frac{11.8}{20}$	$\frac{12.9}{22}$	$\frac{13.3}{30}$	$\frac{22}{46}$	$\frac{1.5}{50}$
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(11.5)

$\frac{80}{50}$	$\frac{7.1}{41}$	$\frac{7.4}{38}$	$\frac{13.1}{29}$	$\frac{12.7}{23}$	$\frac{11.6}{20}$	$\frac{11.4}{20}$	$\frac{11.1}{20}$	$\frac{12.4}{23}$	$\frac{12.7}{31}$	$\frac{1.3}{48}$	$\frac{0.3}{50}$
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(11.0)

$\frac{115}{50}$	$\frac{98}{35}$	$\frac{102}{33}$	$\frac{13.1}{28}$	$\frac{11.8}{21}$	$\frac{11}{20}$	$\frac{109}{20}$	$\frac{10.8}{20}$	$\frac{11.8}{23}$	$\frac{12.3}{31}$	$\frac{0.8}{48}$	$\frac{0.0}{57}$
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Sty	+	HI	-	E/cv	
		424.68 ✓			
366+50					10.5
367					10.0
T.P	3.22	917.21 ✓	10.09	913.99 ✓	
+40					3.1
368					2.1
+15					2.0
+21					1.9
+27					1.8
+50					1.6
369					1.2
+53					0.8
T.P	7.94	924.76 ✓	0.39	916.5 ✓	
370					8.1
+25					8.0

$$\frac{144}{50} \quad \frac{122}{25} \quad \frac{116}{30} \quad \frac{124}{29} \quad \frac{121}{23} \quad \frac{109}{20} \quad \frac{105}{20} \quad \frac{106}{20} \quad \frac{117}{23} \quad \frac{120}{29} \quad \frac{54}{39} \quad \frac{43}{44} \quad \frac{39}{50}$$

(10.5)

$$\frac{151}{50} \quad \frac{123}{28} \quad \frac{128}{27} \quad \frac{120}{23} \quad \frac{105}{20} \quad \frac{99}{20} \quad \frac{115}{23} \quad \frac{117}{28} \quad \frac{88}{32} \quad \frac{84}{35} \quad \frac{81}{50}$$

(10.0)

$$\frac{103}{50} \quad \frac{83}{30} \quad \frac{30}{20} \quad \frac{26}{20} \quad \frac{2.5}{20} \quad \frac{55}{24} \quad \frac{21}{31} \quad \frac{7.4}{50}$$

(3.1)

$$\frac{126}{50} \quad \frac{132}{50} \quad \frac{12.5}{40} \quad \frac{2.4}{20} \quad \frac{2.4}{20} \quad \frac{12.1}{39}$$

(2.1)

$$\frac{12.5}{50} \quad \frac{12.5}{40} \quad \frac{2.2}{20} \quad \frac{2.2}{20} \quad \frac{13.3}{40} \quad \frac{13.7}{50}$$

(2.9)

$$\frac{11.9}{50} \quad \frac{12.2}{40} \quad \frac{12.2}{20} \quad \frac{1.9}{20} \quad \frac{2.2}{20} \quad \frac{13.5}{41} \quad \frac{14.0}{50}$$

(1.9)

$$\frac{11.4}{50} \quad \frac{11.7}{40} \quad \frac{2.1}{20} \quad \frac{2.3}{20} \quad \frac{14.0}{42} \quad \frac{14.2}{50}$$

(1.8)

$$\frac{10.5}{50} \quad \frac{10.6}{38} \quad \frac{1.8}{20} \quad \frac{2.1}{20} \quad \frac{13.1}{42} \quad \frac{14.4}{50}$$

(1.6)

$$\frac{9.0}{50} \quad \frac{9.4}{36} \quad \frac{1.5}{20} \quad \frac{1.3}{20} \quad \frac{12.3}{41} \quad \frac{12.2}{50}$$

(1.2)

$$\frac{2.7}{50} \quad \frac{4.1}{34} \quad \frac{4.9}{30} \quad \frac{4.0}{25} \quad \frac{1.0}{20} \quad \frac{0.8}{20} \quad \frac{8.1}{34} \quad \frac{8.2}{50}$$

(0.8)

$$\frac{6.1}{50} \quad \frac{6.0}{37} \quad \frac{6.3}{34} \quad \frac{10.4}{27} \quad \frac{10.0}{24} \quad \frac{5.2}{20} \quad \frac{8.2}{20} \quad \frac{9.6}{23} \quad \frac{10.5}{28} \quad \frac{9.3}{51} \quad \frac{10.0}{30}$$

(8.1)

$$\frac{5.8}{50} \quad \frac{5.5}{37} \quad \frac{5.8}{34} \quad \frac{10.0}{27} \quad \frac{9.6}{23} \quad \frac{8.1}{20} \quad \frac{8.1}{20} \quad \frac{9.5}{23} \quad \frac{10.1}{27} \quad \frac{6.7}{33} \quad \frac{6.5}{36} \quad \frac{6.8}{50}$$

(8.0)

370

+

HI

-

Elev

924.76 ✓

370+55

7.8

371

7.5

+55

7.4

372

7.2

+50

7.0

373

6.8

+53

6.6

374

6.4

+11

6.4

T.P.

8.73

926.65 ✓

6.84

917.72 ✓

B.M.

10.37

927.81 ✓

9.31

917.34 ✓ = 917.4

+30

18.5

+60

18.5

375

18.5

$\frac{68}{50}$ $\frac{62}{36}$ $\frac{66}{33}$ $\frac{100}{27}$ $\frac{96}{23}$ $\frac{82}{20}$

7.8

$\frac{77}{20}$ $\frac{91}{23}$ $\frac{99}{27}$ $\frac{5.8}{34}$ $\frac{5.2}{37}$ $\frac{5.1}{50}$

$\frac{6.7}{50}$ $\frac{6.6}{36}$ $\frac{6.7}{33}$ $\frac{7.5}{28}$ $\frac{91}{23}$ $\frac{80}{20}$

7.5

$\frac{7.6}{20}$ $\frac{9.1}{23}$ $\frac{9.7}{27}$ $\frac{5.3}{35}$ $\frac{4.6}{39}$ $\frac{4.0}{50}$

$\frac{5.8}{50}$ $\frac{5.4}{37}$ $\frac{5.8}{34}$ $\frac{7.2}{27}$ $\frac{9.8}{23}$ $\frac{7.8}{20}$

7.4

$\frac{7.6}{20}$ $\frac{9.1}{23}$ $\frac{9.3}{29}$ $\frac{2.5}{39}$ $\frac{1.8}{43}$ $\frac{1.3}{50}$

$\frac{4.9}{50}$ $\frac{4.8}{37}$ $\frac{5.1}{34}$ $\frac{9.5}{27}$ $\frac{8.9}{22}$ $\frac{7.5}{20}$

7.2

$\frac{7.4}{20}$ $\frac{8.8}{23}$ $\frac{8.8}{29}$ $\frac{6.5}{42}$ $\frac{0.0}{45}$ $\frac{0.0}{50}$ above 41. $\left(\frac{+0.2}{46}\right)$ $\left(\frac{+0.6}{50}\right)$

$\frac{5.3}{50}$ $\frac{5.7}{34}$ $\frac{6.0}{33}$ $\frac{9.0}{28}$ $\frac{8.6}{23}$ $\frac{7.3}{20}$

7.0

$\frac{7.2}{20}$ $\frac{8.5}{23}$ $\frac{8.9}{29}$ $\frac{3.3}{38}$ $\frac{2.6}{42}$ $\frac{1.8}{48}$ $\frac{2.0}{50}$

$\frac{8.1}{50}$ $\frac{8.1}{29}$ $\frac{8.8}{27}$ $\frac{8.6}{23}$ $\frac{7.6}{20}$

6.8

$\frac{6.8}{20}$ $\frac{7.8}{22}$ $\frac{8.1}{29}$ $\frac{5.9}{32}$ $\frac{3.7}{50}$

$\frac{8.3}{50}$ $\frac{8.4}{30}$ $\frac{8.8}{29}$ $\frac{8.7}{24}$ $\frac{6.9}{20}$

6.6

$\frac{6.5}{20}$ $\frac{7.1}{22}$ $\frac{6.9}{31}$ $\frac{5.9}{32}$ $\frac{5.7}{50}$

$\frac{7.7}{50}$ $\frac{8.1}{36}$ $\frac{8.8}{32}$ $\frac{8.3}{23}$ $\frac{6.9}{20}$

6.4

$\frac{6.0}{11}$ $\frac{6.0}{21}$ $\frac{6.0}{31}$ $\frac{2.5}{41}$ $\frac{0.2}{50}$

$\frac{7.5}{50}$ $\frac{8.2}{32}$ $\frac{8.9}{27}$ $\frac{7.0}{28}$

6.4

$\frac{6.3}{21}$ $\frac{6.9}{29}$ $\frac{2.8}{36}$ $\frac{6.3}{45}$ $\left(\frac{+0.7}{50}\right)$ above 42

$\frac{124}{50}$ $\frac{113}{46}$ $\frac{106}{36}$ $\frac{100}{20}$

9.3

$\frac{9.1}{20}$ $\frac{10.0}{22}$ $\frac{10.5}{29}$ $\frac{3.0}{39}$ $\frac{2.5}{44}$ $\frac{2.0}{50}$

$\frac{116}{50}$ $\frac{111}{35}$ $\frac{101}{31}$ $\frac{101}{28}$ $\frac{108}{26}$ $\frac{106}{22}$ $\frac{98}{20}$

9.3

$\frac{9.1}{20}$ $\frac{10.1}{23}$ $\frac{10.7}{30}$ $\frac{2.5}{44}$ $\frac{1.7}{50}$

$\frac{58}{50}$ $\frac{65}{38}$ $\frac{70}{35}$ $\frac{112}{27}$ $\frac{110}{24}$ $\frac{94}{20}$

9.3

$\frac{9.1}{20}$ $\frac{10.2}{24}$ $\frac{11.0}{30}$ $\frac{2.2}{43}$ $\frac{1.6}{46}$ $\frac{1.0}{50}$

Sta	+	HI	-	Flev
		927.81		
375 +50				18.3
376				18.0
T.P	6.32	✓ 924.18	9.95	✓ 917.86
+55				17.4
377				16.9
+40				16.3
+73				15.9
378				15.5
+50				14.8
379				14.1
+30				13.9
B.M.	2.07.	✓ 917.90	8.35	✓ 915.83
+53				13.5
+56				13.5
				915.84

9.5

$\frac{94}{50}$	$\frac{84}{36}$	$\frac{88}{32}$	$\frac{112}{28}$	$\frac{106}{23}$	$\frac{94}{20}$	$\frac{94}{20}$	$\frac{91}{20}$	$\frac{101}{23}$	$\frac{104}{31}$	$\frac{20}{43}$	$\frac{11}{46}$	$\frac{0.4}{50}$
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9.8

$\frac{120}{50}$	$\frac{102}{33}$	$\frac{103}{31}$	$\frac{113}{28}$	$\frac{111}{24}$	$\frac{95}{20}$	$\frac{97}{20}$	$\frac{92}{20}$	$\frac{103}{23}$	$\frac{110}{30}$	$\frac{40}{40}$	$\frac{31}{44}$	$\frac{25}{50}$
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6.8

$\frac{115}{50}$	$\frac{95}{22}$	$\frac{63}{20}$	$\frac{64}{20}$	$\frac{65}{20}$	$\frac{74}{20}$	$\frac{80}{23}$	$\frac{39}{32}$	$\frac{51}{36}$	$\frac{20}{40}$	$\frac{20}{50}$
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7.3

$\frac{143}{50}$	$\frac{125}{31}$	$\frac{63}{20}$	$\frac{68}{20}$	$\frac{70}{20}$	$\frac{85}{22}$	$\frac{90}{29}$	$\frac{45}{36}$	$\frac{38}{40}$	$\frac{24}{50}$
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7.9

$\frac{145}{50}$	$\frac{125}{29}$	$\frac{25}{20}$	$\frac{70}{20}$	$\frac{77}{20}$	$\frac{85}{22}$	$\frac{96}{31}$	$\frac{42}{38}$	$\frac{35}{41}$	$\frac{20}{50}$
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8.3

$\frac{143}{50}$	$\frac{115}{27}$	$\frac{32}{20}$	$\frac{78}{20}$	$\frac{80}{20}$	$\frac{91}{22}$	$\frac{100}{30}$	$\frac{35}{39}$	$\frac{27}{42}$	$\frac{15}{50}$
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8.7

$\frac{142}{50}$	$\frac{106}{25}$	$\frac{36}{20}$	$\frac{71}{20}$	$\frac{82}{20}$	$\frac{73}{22}$	$\frac{101}{20}$	$\frac{42}{38}$	$\frac{34}{42}$	$\frac{25}{50}$
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9.4

$\frac{144}{50}$	$\frac{121}{26}$	$\frac{93}{20}$	$\frac{91}{20}$	$\frac{92}{20}$	$\frac{103}{22}$	$\frac{110}{31}$	$\frac{60}{37}$	$\frac{54}{41}$	$\frac{46}{50}$
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10.1

$\frac{144}{50}$	$\frac{127}{26}$	$\frac{98}{20}$	$\frac{98}{20}$	$\frac{100}{20}$	$\frac{110}{22}$	$\frac{116}{30}$	$\frac{81}{36}$	$\frac{76}{39}$	$\frac{70}{50}$
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10.9

$\frac{148}{50}$	$\frac{132}{26}$	$\frac{100}{20}$	$\frac{102}{20}$	$\frac{103}{20}$	$\frac{113}{23}$	$\frac{117}{27}$	$\frac{78}{36}$	$\frac{100}{40}$	$\frac{97}{50}$
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3p. Be in 21 N1 ap/c Rts + 379 + 71

9.4

$\frac{94}{50}$	$\frac{104}{45}$	$\frac{101}{40}$	$\frac{66}{33}$	$\frac{57}{24}$	$\frac{46}{20}$	$\frac{112}{44}$	$\frac{46}{20}$	$\frac{60}{23}$	$\frac{64}{30}$	$\frac{34}{35}$	$\frac{30}{38}$	$\frac{32}{50}$
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4.4

$\frac{88}{50}$	$\frac{96}{43}$	$\frac{103}{41}$	$\frac{102}{38}$	$\frac{65}{31}$	$\frac{58}{23}$	$\frac{46}{20}$	$\frac{47}{20}$	$\frac{5.5}{25}$	$\frac{6.0}{31}$	$\frac{3.5}{34}$	$\frac{30}{37}$	$\frac{34}{50}$
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	+	HI	-	E/c ✓	
		912.90			
379+61				13.4	
+67				13.2	
+71				13.1	
+81				13.0	
380				12.7	
+03				12.7	
+09				12.6	
+43				12.2	
+67				12.0	
+80				11.9	
381		✓		11.8	
BM	1.54	712.38	2.07	715.83	715.84
+28				11.8	

$$\frac{81}{50} \quad \frac{80}{38} \quad \frac{83}{34} \quad \frac{48}{20} \quad \frac{45}{26} \quad \frac{49}{20} \quad \frac{57}{23} \quad \frac{62}{31} \quad \frac{56}{34} \quad \frac{50}{37} \quad \frac{35}{50}$$

$$\frac{80}{50} \quad \frac{48}{20} \quad \frac{49}{20} \quad \frac{50}{20} \quad \frac{60}{23} \quad \frac{63}{30} \quad \frac{38}{33} \quad \frac{32}{36} \quad \frac{40}{50}$$

$$\frac{82}{50} \quad \frac{78}{46} \quad \frac{41}{20} \quad \frac{47}{20} \quad \frac{50}{20} \quad \frac{62}{23} \quad \frac{63}{30} \quad \frac{58}{33} \quad \frac{34}{36} \quad \frac{40}{50}$$

$$\frac{80}{50} \quad \frac{75}{40} \quad \frac{50}{20} \quad \frac{50}{20} \quad \frac{64}{24} \quad \frac{66}{30} \quad \frac{44}{33} \quad \frac{40}{36} \quad \frac{45}{50}$$

$$\frac{78}{50} \quad \frac{68}{32} \quad \frac{53}{20} \quad \frac{52}{20} \quad \frac{50}{20} \quad \frac{64}{23} \quad \frac{70}{30} \quad \frac{48}{32} \quad \frac{45}{35} \quad \frac{50}{50}$$

$$\frac{80}{50} \quad \frac{61}{26} \quad \frac{52}{40} \quad \frac{51}{20} \quad \frac{50}{20} \quad \frac{64}{23} \quad \frac{71}{29} \quad \frac{57}{31} \quad \frac{47}{35} \quad \frac{51}{50}$$

$$\frac{94}{50} \quad \frac{80}{45} \quad \frac{66}{38} \quad \frac{53}{20} \quad \frac{50}{20} \quad \frac{64}{24} \quad \frac{70}{30} \quad \frac{53}{32} \quad \frac{59}{35} \quad \frac{56}{50}$$

$$\frac{26}{50} \quad \frac{27}{41} \quad \frac{21}{37} \quad \frac{81}{28} \quad \frac{72}{27} \quad \frac{60}{20} \quad \frac{54}{20} \quad \frac{57}{28} \quad \frac{72}{29} \quad \frac{50}{35} \quad \frac{55}{40}$$

$$\frac{16}{50} \quad \frac{08}{41} \quad \frac{13}{38} \quad \frac{30}{28} \quad \frac{22}{24} \quad \frac{61}{30} \quad \frac{55}{20} \quad \frac{52}{37} \quad \frac{63}{41} \quad \frac{62}{46} \quad \frac{40}{50}$$

$$\frac{16}{50} \quad \frac{10}{41} \quad \frac{14}{37} \quad \frac{20}{28} \quad \frac{25}{24} \quad \frac{62}{20} \quad \frac{55}{20} \quad \frac{48}{34} \quad \frac{42}{50}$$

$$\frac{16}{50} \quad \frac{13}{41} \quad \frac{17}{37} \quad \frac{20}{28} \quad \frac{26}{23} \quad \frac{62}{20} \quad \frac{55}{20} \quad \frac{43}{35} \quad \frac{47}{50}$$

sp. ko in 20" 19 sp/12 P+ 5/6 579-71

$$\frac{68}{50} \quad \frac{12}{44} \quad \frac{15}{38} \quad \frac{28}{29} \quad \frac{23}{24} \quad \frac{57}{30} \quad \frac{57}{20} \quad \frac{70}{25} \quad \frac{72}{29} \quad \frac{22}{36} \quad \frac{20}{39} \quad \frac{27}{48} \quad \frac{40}{50}$$

Sta		HI		Elev
		917.35		
381+70				11.9
382				11.9
+50				12.2
383				12.5
+30				12.6
+50				12.8
384				13.1
+42				13.3
385				13.7
T.P.	7.94	922.32 ✓	3.00	914.35
+65				14.1
386				14.3
+80				14.5

$$\begin{array}{cccccccc} \frac{2.1}{50} & \frac{2.6}{39} & \frac{2.0}{35} & \frac{7.8}{30} & \frac{2.7}{26} & \frac{5.6}{20} & \frac{5.5}{31} & \frac{5.3}{20} & \frac{7.2}{23} & \frac{7.4}{29} & \frac{3.0}{34} & \frac{2.4}{38} & \frac{1.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{3.7}{50} & \frac{4.4}{36} & \frac{5.0}{33} & \frac{2.2}{29} & \frac{7.4}{25} & \frac{5.6}{20} & \frac{5.5}{50} & \frac{5.0}{20} & \frac{7.3}{24} & \frac{7.4}{27} & \frac{4.7}{33} & \frac{4.0}{37} & \frac{3.5}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.2}{50} & \frac{7.4}{36} & \frac{7.1}{31} & \frac{7.7}{29} & \frac{7.0}{24} & \frac{5.4}{20} & \frac{5.2}{50} & \frac{5.3}{20} & \frac{6.6}{25} & \frac{6.6}{29} & \frac{5.6}{30} & \frac{5.2}{34} & \frac{4.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{6.4}{50} & \frac{5.7}{35} & \frac{6.0}{29} & \frac{7.0}{28} & \frac{7.0}{23} & \frac{5.0}{20} & \frac{4.7}{50} & \frac{4.8}{20} & \frac{6.3}{24} & \frac{6.6}{29} & \frac{4.4}{32} & \frac{4.2}{35} & \frac{4.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.6}{50} & \frac{4.7}{34} & \frac{5.0}{32} & \frac{7.0}{28} & \frac{6.7}{25} & \frac{4.7}{20} & \frac{4.8}{50} & \frac{4.7}{20} & \frac{6.3}{24} & \frac{6.5}{29} & \frac{4.4}{32} & \frac{4.0}{34} & \frac{4.0}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{6.1}{50} & \frac{5.2}{34} & \frac{5.5}{29} & \frac{7.1}{26} & \frac{6.8}{23} & \frac{4.8}{19} & \frac{4.6}{50} & \frac{4.4}{20} & \frac{6.4}{26} & \frac{6.6}{30} & \frac{4.5}{32} & \frac{4.0}{35} & \frac{3.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{7.0}{50} & \frac{6.6}{28} & \frac{7.1}{27} & \frac{6.8}{24} & \frac{4.4}{20} & \frac{4.4}{50} & \frac{4.6}{20} & \frac{6.3}{23} & \frac{6.6}{29} & \frac{6.1}{31} & \frac{5.5}{34} & \frac{4.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.0}{50} & \frac{5.6}{30} & \frac{6.0}{29} & \frac{5.6}{23} & \frac{4.1}{20} & \frac{3.8}{50} & \frac{4.0}{20} & \frac{5.8}{24} & \frac{6.1}{29} & \frac{5.7}{30} & \frac{5.4}{34} & \frac{3.7}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{1.6}{50} & \frac{2.0}{34} & \frac{5.6}{29} & \frac{6.2}{23} & \frac{3.7}{20} & \frac{3.3}{50} & \frac{3.2}{20} & \frac{5.0}{24} & \frac{5.2}{28} & \frac{2.5}{32} & \frac{2.0}{38} & \frac{1.2}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{2.6}{50} & \frac{3.1}{43} & \frac{3.3}{39} & \frac{9.8}{28} & \frac{8.7}{23} & \frac{5.4}{20} & \frac{8.2}{50} & \frac{8.1}{20} & \frac{9.6}{24} & \frac{10.0}{28} & \frac{4.0}{37} & \frac{3.6}{44} & \frac{3.7}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{3.3}{50} & \frac{2.7}{42} & \frac{2.8}{39} & \frac{10.0}{28} & \frac{10.0}{23} & \frac{8.1}{20} & \frac{8.0}{50} & \frac{8.1}{20} & \frac{9.8}{23} & \frac{10.1}{28} & \frac{3.3}{38} & \frac{2.8}{41} & \frac{2.6}{50} \end{array}$$

$$\begin{array}{cccccccc} \frac{5.8}{50} & \frac{5.4}{36} & \frac{6.0}{33} & \frac{10.0}{27} & \frac{9.6}{23} & \frac{7.7}{20} & \frac{7.8}{50} & \frac{8.0}{20} & \frac{9.4}{23} & \frac{9.5}{29} & \frac{0.8}{41} & \frac{0.3}{50} \end{array}$$

Sta	+	MI	-	Elev
387		922.32 ¹		14.6
	+50			14.4
388				14.3
	+50			13.9
389				13.4
	+50			12.4
390				11.9
T.P.	2.20	914.09 ¹	10.43	911.89 [✓]
	+61			10.8
	+84			10.4
391				10.1
T.P.				
	+50			9.3
392				8.5

Sta	+	HI	-	Elev ✓	
		914.09			
392 + 50				8.1	
393				7.8	
+ 50				7.6	
394				7.6 ✓	
T.P.	7.25	914.39 ✓	6.95	909.14 ✓	
B.M.			3.74	910.65 ✓	910.68

$$\begin{array}{r} 157 \\ \hline 50 \end{array} \quad \begin{array}{r} 148 \\ \hline 38 \end{array} \quad \begin{array}{r} 61 \\ \hline 20 \end{array} \quad \begin{array}{r} \textcircled{60} \\ \hline 58 \end{array} \quad \begin{array}{r} 58 \\ \hline 20 \end{array} \quad \begin{array}{r} 126 \\ \hline 35 \end{array} \quad \begin{array}{r} 126 \\ \hline 50 \end{array} \quad \text{Beg Ditch} \\ 372 + 50 = 00$$

$$\begin{array}{r} 137 \\ \hline 50 \end{array} \quad \begin{array}{r} 137 \\ \hline 32 \end{array} \quad \begin{array}{r} 64 \\ \hline 20 \end{array} \quad \begin{array}{r} \textcircled{63} \\ \hline 62 \end{array} \quad \begin{array}{r} 63 \\ \hline 20 \end{array} \quad \begin{array}{r} 124 \\ \hline 33 \end{array} \quad \begin{array}{r} 125 \\ \hline 34 \end{array} \quad 132 \quad 134 \quad 118 \quad 116 \\ 36 \quad 41 \quad 43 \quad 50$$

$$\begin{array}{r} 140 \\ \hline 50 \end{array} \quad \begin{array}{r} 123 \\ \hline 31 \end{array} \quad \begin{array}{r} 64 \\ \hline 20 \end{array} \quad \begin{array}{r} \textcircled{65} \\ \hline 62 \end{array} \quad \begin{array}{r} 64 \\ \hline 20 \end{array} \quad \begin{array}{r} 118 \\ \hline 31 \end{array} \quad \begin{array}{r} 120 \\ \hline 33 \end{array} \quad \begin{array}{r} 133 \\ \hline 36 \end{array} \quad \begin{array}{r} 134 \\ \hline 40 \end{array} \quad \begin{array}{r} 115 \\ \hline 43 \end{array} \quad \begin{array}{r} 110 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 145 \\ \hline 50 \end{array} \quad \begin{array}{r} 140 \\ \hline 35 \end{array} \quad \begin{array}{r} 66 \\ \hline 20 \end{array} \quad \begin{array}{r} \textcircled{65} \\ \hline 62 \end{array} \quad \begin{array}{r} 64 \\ \hline 20 \end{array} \quad \begin{array}{r} 117 \\ \hline 32 \end{array} \quad \begin{array}{r} 115 \\ \hline 34 \end{array} \quad \begin{array}{r} 130 \\ \hline 36 \end{array} \quad \begin{array}{r} 136 \\ \hline 41 \end{array} \quad \begin{array}{r} 140 \\ \hline 43 \end{array} \quad \begin{array}{r} 118 \\ \hline 50 \end{array}$$

opike in 6" Pop 220 '94 5th 2.

Sta	+	HI	-	Elev		
B.M.	0.66	894.23 ¹		893.57		
T.P.	4.57	888.20 ¹	10.60	883.63 ¹	6.2	4
304+00				82.8		5.4
+50				83.0	6.1	4
305+00				83.2	5.9	4
+50				83.4		5.0
306+00				83.6	5.7	3.9
+50				83.8		4.8
307+00				84.0	5.8	3
+50				84.2		4.6
T.P.	5.11	890.78 ^v	2.53	885.67 ¹	5.3	3
308+00				84.4		4.4
+50				84.6	7.3	5
+76 ⁰³				84.7	7.1	6.2
						6.5

spike in 12" oak 50h + sta.

W 5.4
 1.0 2.4/1.38 0070 7.4 0.67 5.4 5.4 5.5 10.2 10.5 11.0
 8.0 5049 4437 30 2.1/-0.5 19 20 20 29 -59/31.8 50

W 5.2
 2.0 5.5/4.80 7.4 7.5 8.7 6.6 5.5 5.4 5.3 10.6 10.6 11.1
 2.0 504743 35 30 2.0/-0.9 21 18 -0.7 21 34 -6.3/2.6 50

W 5.0 Water Edge
 0 4.5/3.0 0070 26/26 2.8/6.8 6.5 5.4 5.4 5.0 5.2 10.5 11.2
 0 50 4571.34 32 103 2.8/-0.9 16 14 -0.4 -0.9/2.8 25 36 41

W 4.8
 0 4.5/2.2 0.4 4.1/4.1 4.6 7.0 0.7 6.2 5.6 5.2 4.4 4.3 4.5 10.9 11.5
 0 4845 39 35 1.6 31 28 2.0 13 11 -0.4 -0.5 21.0 30 41 30 43 50

W 4.6
 2.0 0.0 2.0 4.7 4.6 7.1 7.3 8.4 7.9 5.9 5.2 5.2 4.5 4.1 10.0 4.1 10.9 11.9
 3.8 3.4 2 -1.2 23 21 12 7 6 -11 12 -0.8 21.6 41 30.4 36 48 50

W 4.4
 2.0 0.0 1.1 3.0 6.1 6.8 6.9 6.5 5.4 4.5 4.1 3.9 7.1 11.0
 2.9 2.7 2.0 1.4 7 2.0 -2.1 9 -1.0/2.0 41 39 44 50 5.8

W 4.2
 2.0 0.0 2.0 5.5 5.8 5.8 5.0 4.4 4.2 4.1 4.0 3.7
 8 6 3 -1.6 2 5 16 -0.9/2.8 41 40 29.8 50

W 4.0
 2.0 +2.2 0.0 5.0 4.9 4.2 4.0 4.0 3.1
 3 15 15 -1.1/2.2 41 40 27.7 50

W 6.4
 2.0 5.7 6.7 6.4 6.4 6.4 6.8 5.5
 15 -1.2/2.2 41 31 32 50

W 6.2
 2.0 3.9 6.0 5.6 6.5 5.8
 20 2.0 3.0 3.9 4.0 5.0

W 6.1
 4.5 5.1 5.5 6.5 6.5
 22 33 41 22 50

Sta	+	HI	-	Elev	
		890.78			
309+00				84.8	6.0
	+69			85.1	5.7
	+80			85.1	5.7
310+00				85.2	5.6
	+50			85.4	5.4
	+84			85.5	5.3
B.M.			11.11	879.67	= 879.66
T.P.	6.00	892.81	3.97	886.81	
311+00				85.6	7.2
	+50			85.8	7.0
312+00				86.0	6.8
	+50			86.2	6.6
313+00				86.4	6.4
B.M.			13.14	879.67	= 879.66

54

(6.0) $\frac{1.4}{18} \quad \frac{4.4}{24} \quad \frac{5.8}{30.6} / \frac{19.0}{43} \quad \frac{5.6}{43} \quad \frac{6.4}{44} \quad \frac{6.2}{50}$

(5.7) $\frac{0.0}{7} \quad \frac{3.2}{13} \quad \frac{5.8}{27} \quad \frac{5.6}{00/31.0} \quad \frac{5.1}{45} \quad \frac{5.9}{46} \quad \frac{5.8}{50}$

(5.7) $\frac{0.0}{6} \quad \frac{4.3}{14} \quad \frac{5.4}{21} \quad \frac{5.5}{36} \quad \frac{5.0}{47} \quad \frac{5.7}{48} \quad \frac{5.7}{50}$

above HI

(5.6) $\frac{+3.5}{+7.1} \quad \frac{0.0}{5} \quad \frac{4.6}{13} \quad \frac{5.5}{22} \quad \frac{5.5}{+0.1/31.2} \quad \frac{4.9}{47} \quad \frac{5.8}{48} \quad \frac{5.7}{50}$

above HI

(5.4) $\frac{2.5}{+7.7} \quad \frac{0.0}{3} \quad \frac{4.6}{13} \quad \frac{5.5}{22} \quad \frac{5.4}{00/31.0} \quad \frac{4.9}{47} \quad \frac{5.3}{48} \quad \frac{5.2}{50}$

above HI

(5.3) $\frac{+0.9}{+0.2} \quad \frac{0.0}{1} \quad \frac{3.3}{8} \quad \frac{4.3}{20} \quad \frac{4.8}{+0.5/31.8} \quad \frac{4.7}{46} \quad \frac{5.2}{47} \quad \frac{5.0}{50}$

spike in 8" Birch N+sta.

(7.2) $\frac{+1.6}{50} \quad \frac{2.0}{43} \quad \frac{3.5}{30} / \frac{4.2}{+3.0} \quad \frac{5.6}{29} \quad \frac{5.8}{14} \quad \frac{5.8}{+1.4} \quad \frac{6.3}{13} \quad \frac{6.2}{+1.0/32.5} \quad \frac{6.3}{45} \quad \frac{6.7}{47} \quad \frac{6.9}{50}$

(7.0) $\frac{0.3}{50} \quad \frac{3.4}{33} / \frac{5.3}{+1.7} \quad \frac{5.7}{15} \quad \frac{6.1}{+0.9} \quad \frac{5.7}{14} \quad \frac{6.1}{+0.9/32.4} \quad \frac{6.5}{50} \quad \frac{5.2}{44}$

(6.8) $\frac{+1.7}{46} \quad \frac{0.0}{42} \quad \frac{3.3}{33} / \frac{5.6}{+1.7} \quad \frac{5.8}{16} \quad \frac{5.3}{+1.5} \quad \frac{5.3}{9} \quad \frac{6.0}{+0.8/32.2} \quad \frac{6.6}{40} \quad \frac{6.0}{50}$

(6.6) $\frac{1.7}{42} \quad \frac{5.3}{37} \quad \frac{3.4}{33} / \frac{5.8}{0.8} \quad \frac{5.8}{23} \quad \frac{5.6}{12} \quad \frac{5.2}{+1.4} \quad \frac{4.7}{12} \quad \frac{4.8}{17} \quad \frac{6.1}{25} \quad \frac{6.3}{+0.3/31.4} \quad \frac{6.1}{46} \quad \frac{6.4}{50}$

(6.4) $\frac{0.0}{356} \quad \frac{3.0}{33} / \frac{2.0}{+4.4} \quad \frac{4.6}{28} \quad \frac{4.9}{21} / \frac{6.9}{-0.5} \quad \frac{6.9}{11} \quad \frac{6.9}{-0.5} \quad \frac{6.7}{11} \quad \frac{6.6}{18} \quad \frac{5.6}{30} \quad \frac{5.9}{+0.5/31.8} \quad \frac{6.0}{40} \quad \frac{6.8}{50}$

- 519	+	HI	-	Elev	
B.M.	6.97	900.54 ✓		892.57	17.8
306+00				83.6	16.9
	+50			83.8	17.8
T.P.	12.59	911.17 ✓	1.96	898.58 ✓	16.7
307+00				84.0	28.1
T.P.	12.68	911.26 ✓	12.59	898.58 ✓	27.2
	+50			84.2	28.0
					27.1
308+00				84.4	27.8
T.P.	9.64	918.09 ✓	2.81	908.45 ✓	26.9
308+50				84.4	34.6
	+50			84.6	33.7
					34.4
					33.5
7 76 ¹³				85.7	
309+00				84.8	34.2
	+69			85.1	33.3
T.P.	6.52	913.37 ✓	11.24	906.85 ✓	33.1
	+80				33.0

$$50 \begin{array}{r} 5.4 \\ +12.4 \\ \hline 17.8 \end{array} \quad \begin{array}{r} 6.1 \\ 48 \\ \hline 54.1 \end{array} \quad \begin{array}{r} 7.8 \\ 46 \\ \hline 12.4 \end{array}$$

(16.9)

$$50 \begin{array}{r} 6.1 \\ 11.5 \\ \hline 17.6 \end{array} \quad \begin{array}{r} 11.0 \\ 33 \\ \hline 14.3 \end{array}$$

(16.7)

$$50 \begin{array}{r} 9.0 \\ 19.1 \\ \hline 28.1 \end{array} \quad \begin{array}{r} 9.6 \\ 39 \\ \hline 48.6 \end{array} \quad \begin{array}{r} 11.9 \\ 24 \\ \hline 14.3 \end{array} \quad \begin{array}{r} 13.0 \\ 21 \\ \hline 15.1 \end{array}$$

(27.2)

$$0 \begin{array}{r} 0.5 \\ +23.5 \\ \hline 24.0 \end{array} \quad \begin{array}{r} 0.8 \\ 40 \\ \hline 40.8 \end{array} \quad \begin{array}{r} 2.1 \\ 28 \\ \hline 30.1 \end{array} \quad \begin{array}{r} 3.9 \\ 18 \\ \hline 21.9 \end{array} \quad \begin{array}{r} 5.1 \\ 14 \\ \hline 19.1 \end{array}$$

(27.1)

$$\begin{array}{r} 1.9 \\ 11 \\ \hline 12.9 \end{array} \quad \begin{array}{r} 3.1 \\ 9 \\ \hline 12.1 \end{array} \quad \begin{array}{r} 12.7 \\ +14.2 \\ \hline 26.9 \end{array}$$

(26.9)

$$50 \begin{array}{r} 3.8 \\ +30.8 \\ \hline 34.6 \end{array} \quad \begin{array}{r} 4.8 \\ 46 \\ \hline 50.8 \end{array} \quad \begin{array}{r} 6.4 \\ 26 \\ \hline 32.4 \end{array}$$

(33.7)

$$50 \begin{array}{r} 2.0 \\ +32.4 \\ \hline 34.4 \end{array} \quad \begin{array}{r} 3.9 \\ 37 \\ \hline 40.9 \end{array} \quad \begin{array}{r} 6.7 \\ 19 \\ \hline 25.7 \end{array} \quad \begin{array}{r} 9.3 \\ 6 \\ \hline 15.3 \end{array} \quad \begin{array}{r} 10.2 \\ 3 \\ \hline 13.2 \end{array} \quad \begin{array}{r} 12.0 \\ +21.5 \\ \hline 33.5 \end{array}$$

(33.5)

$$\begin{array}{r} 2.5 \\ 50 \\ \hline 52.5 \end{array} \quad \begin{array}{r} 4.4 \\ 34 \\ \hline 38.4 \end{array} \quad \begin{array}{r} 6.2 \\ 20 \\ \hline 26.2 \end{array} \quad \begin{array}{r} 9.3 \\ 3 \\ \hline 12.3 \end{array} \quad \begin{array}{r} 10.3 \\ \hline 10.3 \end{array}$$

(33.4)

$$50 \begin{array}{r} 2.8 \\ +31.4 \\ \hline 34.2 \end{array} \quad \begin{array}{r} 3.8 \\ 41 \\ \hline 44.8 \end{array} \quad \begin{array}{r} 6.2 \\ 27 \\ \hline 33.2 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \\ \hline 21.4 \end{array} \quad \begin{array}{r} 10.6 \\ +22.7 \\ \hline 33.3 \end{array} \quad \begin{array}{r} 11.0 \\ 2 \\ \hline 13.0 \end{array} \quad \begin{array}{r} 12.6 \\ 4 \\ \hline 16.6 \end{array}$$

(33.3)

$$50 \begin{array}{r} 5.1 \\ +28.0 \\ \hline 33.1 \end{array} \quad \begin{array}{r} 8.8 \\ 31 \\ \hline 39.8 \end{array} \quad \begin{array}{r} 11.7 \\ 14 \\ \hline 26.7 \end{array} \quad \begin{array}{r} 14.8 \\ +18.4 \\ \hline 33.2 \end{array}$$

(33.0)

$$\begin{array}{r} 1.0 \\ 50 \\ \hline 51.0 \end{array} \quad \begin{array}{r} 2.4 \\ 42 \\ \hline 44.4 \end{array} \quad \begin{array}{r} 4.6 \\ 29 \\ \hline 33.6 \end{array} \quad \begin{array}{r} 7.3 \\ 17 \\ \hline 24.3 \end{array} \quad \begin{array}{r} 9.8 \\ 3 \\ \hline 12.8 \end{array}$$

(28.3)

Sta	+	HI	-	Elev	
		912.37			
310+00				85.2	28.2
	+50			85.4	28.0
	+84			85.5	27.9
B.M.			4.32	909.05	909.03
New B.M.			0.83	913.04	
B.M.	923	888.89		879.66	
313+14				86.5	2.4
	+38			86.6	2.3
314+00				86.8	2.1
	+10			87.0	1.9
315+00				87.2	1.7
	+12			87.2	
	+24			87.3	1.6

50 / $\frac{2.3}{425.9}$ $\frac{4.4}{37}$ $\frac{7.2}{20}$ $\frac{9.9}{6}$ $\frac{16.4}{3}$ (28.2)

50 / $\frac{3.8}{424.2}$ $\frac{5.4}{43}$ $\frac{8.8}{23}$ $\frac{1.8}{5}$ (28.0)

50 / $\frac{5.2}{422.7}$ $\frac{7.3}{38}$ $\frac{8.9}{24}$ $\frac{11.0}{8}$ $\frac{18.2}{5}$ (27.9)

Notch in Tree Lt Sta

Notch in 70" Oak 55' Lt Sta 309+90

Spike 8" Birch 100' Rt Sta 312+50

30 / $\frac{0}{15.2}$ $\frac{0.0}{30.7}$ $\frac{1.1}{28}$ $\frac{20.8}{20}$ $\frac{2.8}{-0.4}$ $\frac{3.2}{16}$ $\frac{3.4}{-1.0}$ $\frac{4.0}{5}$ $\frac{5.3}{12}$ $\frac{4.6}{19}$ $\frac{3.3}{-0.9}$ $\frac{2.1}{2}$ $\frac{1.8}{27}$ $\frac{2.6}{19}$ $\frac{1.9}{30}$ (2.4)

ave HI
5.2 / $\frac{0.0}{59}$ $\frac{0.0}{30.8}$ $\frac{1.3}{30.8}$ $\frac{1.1}{27}$ $\frac{4.7}{-2.4}$ $\frac{6.4}{20}$ $\frac{6.2}{12}$ $\frac{7.3}{-5.0}$ $\frac{7.8}{12}$ $\frac{4.7}{2.1}$ $\frac{4.5}{-2.2}$ $\frac{2.4}{24}$ $\frac{2.7}{29}$ $\frac{2.7}{1.6}$ $\frac{2.7}{30.6}$ $\frac{2.7}{30}$ (2.3)

8.1 / $\frac{48.8}{50}$ $\frac{9.3}{33}$ $\frac{9.4}{6.7}$ $\frac{10.0}{24}$ $\frac{10.0}{10}$ $\frac{9.8}{-9.9}$ $\frac{9.8}{9}$ $\frac{4.3}{20}$ $\frac{3.3}{-1.2}$ $\frac{2.4}{22.4}$ $\frac{3.2}{35}$ $\frac{3.6}{50}$ (2.1)

10.3 / $\frac{3.1}{50}$ $\frac{10.5}{-8.6}$ $\frac{10.7}{27}$ $\frac{11.0}{12}$ $\frac{11.6}{-9.7}$ $\frac{10.9}{4}$ $\frac{4.7}{17}$ $\frac{4.4}{-2.5}$ $\frac{5.0}{2}$ $\frac{5.2}{37}$ $\frac{11.6}{4}$ (1.9) Edge of Water

10.5 / $\frac{38.4}{50}$ $\frac{10.8}{-9.1}$ $\frac{11.0}{15}$ $\frac{11.2}{-9.5}$ $\frac{7.7}{7}$ $\frac{6.2}{18}$ $\frac{6.7}{25}$ $\frac{10.1}{28}$ $\frac{11.6}{34}$ $\frac{13.2}{37}$ (1.7) E.W.

10.0 / $\frac{10.9}{50}$ $\frac{13.8}{27}$ $\frac{7.8}{11}$ $\frac{7.8}{4}$ $\frac{7.0}{9}$ $\frac{7.0}{23}$ $\frac{9.9}{26}$ $\frac{11.7}{46}$ (1.7) E.W.

10.4 / $\frac{4}{50}$ $\frac{10.8}{38}$ $\frac{10.7}{9.4}$ $\frac{7.1}{14}$ $\frac{7.2}{8}$ $\frac{6.7}{-5.6}$ $\frac{8.7}{21}$ $\frac{9.9}{24}$ $\frac{9.4}{73}$ $\frac{11.8}{34.6}$ $\frac{14.0}{43}$ $\frac{14.0}{49}$ $\frac{14.0}{50}$ (1.6)

Sta	+	HI	-	Elev.	
		888.89			
315+50				87.4	1.5
+60				87.4	
316+00				87.6	1.3
317+00				88.0	0.9
318+00				88.5	0.4
T.P.	8.36	894.51	2.74	886.15	
319+00				89.0	5.2
T.P.	8.06	894.24	2.33	886.18	
320+00				89.6	4.6
321+00				90.2	4.0
322+00				90.8	3.4
323+00				91.4	2.8
324+00				92.0	2.2
+50				92.3	1.9

151
122
121

(15)

$$\frac{104}{50} \quad 378 / \frac{104}{-8.9} \quad \frac{105}{24} \quad \frac{11.7}{8} \quad \frac{7.3}{-5.8} \quad \frac{5.2}{2.4} \quad \frac{7.6}{28} \quad \frac{8.1}{-6.6} / 33.2 \quad \frac{7.5}{41} \quad \frac{10.3}{50}$$

(115)

$$\frac{10.5}{50} \quad \frac{106}{27} \quad \frac{11.2}{11} \quad \frac{11.8}{9} \quad \frac{12.1}{6} \quad \frac{10.6}{-} \quad \frac{6.6}{8} \quad \frac{5.4}{20} \quad \frac{4.7}{33} \quad \frac{6.7}{37} \quad \frac{9.3}{50}$$

(13)

$$\frac{9.3}{50} \quad 374 / \frac{10.0}{-8.7} \quad \frac{10.5}{12} \quad \frac{11.6}{10} \quad \frac{11.7}{5} \quad \frac{10.3}{-9.0} \quad \frac{3.2}{1.4} \quad \frac{2.6}{-1.3} / 2.6 \quad \frac{2.6}{3.5} \quad \frac{4.2}{50}$$

(09)

$$\frac{7.8}{50} \quad 354 / \frac{8.4}{-7.5} \quad \frac{9.5}{15} \quad \frac{11.8}{12} \quad \frac{11.6}{9} \quad \frac{10.1}{6} \quad \frac{9.9}{5} \quad \frac{7.3}{-6.4} \quad \frac{1.4}{13} \quad \frac{1.8}{-0.9} / 20.8 \quad \frac{2.5}{50}$$

(04)

$$\frac{5.6}{50} \quad 337 / \frac{7.0}{-6.6} \quad \frac{8.0}{18} \quad \frac{10.0}{12} \quad \frac{9.3}{7} \quad \frac{5.2}{-4.8} \quad \frac{0.7}{11} \quad \frac{0.7}{-0.3} / 20.6 \quad \frac{0.4}{50}$$

(55)

$$\frac{1}{0} \quad 340 / \frac{0.5}{+2.0} \quad 2.8 / \frac{6.9}{1.4} \quad \frac{9.2}{14} \quad \frac{10.5}{5} \quad \frac{8.6}{-3.8} \quad \frac{5.4}{6} \quad \frac{5.6}{-0.1} / 20.2 \quad \frac{5.7}{47} \quad \frac{7.4}{50}$$

Top Hub R75 + 9. 318 + 90

$$\frac{6.1}{50} \quad \frac{7.8}{40} \quad 290 / \frac{9.1}{-4.5} \quad \frac{10.0}{21} \quad \frac{10.7}{9} \quad \frac{6.6}{-2.0} \quad \frac{4.8}{3} \quad \frac{4.8}{-0.2} / 20.4 \quad \frac{5.0}{44} \quad \frac{8.2}{50}$$

(40)

$$\frac{9.9}{50} \quad 364 / \frac{11.2}{-7.2} \quad \frac{12.0}{22} \quad \frac{12.3}{17} \quad \frac{4.2}{-0.2} \quad \frac{4.0}{0.0} / 20.0 \quad \frac{4.4}{4.1} \quad \frac{9.1}{50}$$

(3.4)

$$\frac{13.1}{50} \quad 392 / \frac{13.0}{-9.6} \quad \frac{13.0}{25} \quad \frac{3.5}{4} \quad \frac{3.2}{10.1} \quad \frac{3.4}{0.0} / 20.9 \quad \frac{3.6}{3.7} \quad \frac{9.1}{50}$$

(2.8)

$$\frac{15.3}{50} \quad 44.8 / \frac{15.2}{-12.4} \quad \frac{15.2}{34} \quad \frac{3.0}{8} \quad \frac{2.7}{+0.1} \quad \frac{2.8}{0.0} / 20 \quad \frac{2.8}{3.4} \quad \frac{10.9}{50}$$

(2.2)

$$\frac{15.2}{50} \quad 45.8 / \frac{15.1}{12.9} \quad \frac{14.6}{36} \quad \frac{4.2}{19} \quad \frac{2.0}{10} \quad \frac{1.8}{10.4} \quad \frac{2.0}{+0.2} / 20 \quad \frac{2.1}{3.1} \quad \frac{10.8}{50}$$

(1.9)

$$\frac{11.2}{50} \quad 384 / \frac{11.0}{+9.2} \quad \frac{10.6}{33} \quad \frac{4.3}{20} \quad \frac{1.6}{12} \quad \frac{1.4}{+0.3} \quad \frac{1.4}{20} \quad \frac{1.6}{2.8} \quad \frac{3.6}{3.5} \quad \frac{10.8}{4.8} \quad \frac{10.9}{50}$$

Sta	+	HI	-	Elev	
		894.24			
325				92.6	1.6
T.P.	9.87	902.41 ^v	1.70	892.54 ^v	9.3
+59.04				92.9	9.5
326				93.0	9.1
+50				93.2	8.7 9.2
327				93.3	8.8 9.1
B.M.			2.14	900.27 ^v	= 900.23

$$\frac{30}{50} \quad \frac{40}{40} \quad 25.4 \frac{43}{-27} \quad \frac{46}{23} \quad \frac{13}{15} \quad \frac{4}{25} \quad \frac{15}{20} \quad \frac{2.5}{27} \quad \frac{6.4}{36} \quad \frac{7.0}{50}$$

(1.6)

$$\frac{50}{34} \quad \frac{55}{31} \quad \frac{105}{25.2} \quad \frac{6/106}{-1.3} \quad \frac{102}{17} \quad \frac{92}{14} \quad \frac{92}{+03} \quad \frac{9.4}{20} \quad \frac{9.5}{26} \quad \frac{10.4}{28} \quad \frac{110}{34} \quad \frac{2.2}{40} \quad \frac{8.4}{50}$$

(9.5)

$$\frac{27.25}{39} \quad \frac{116}{25.2} \quad \frac{8/110}{-19} \quad \frac{105}{19} \quad \frac{8.5}{16} \quad \frac{8.9}{+05} \quad \frac{9.2}{20} \quad \frac{9.3}{26} \quad \frac{106}{28} \quad \frac{111}{33} \quad \frac{3.4}{43} \quad \frac{30}{46} \quad \frac{3.4}{50}$$

(9.2)

$$\frac{+1.4}{46} \quad \frac{+06}{41} \quad \frac{0.0}{40} \quad 23.6 \frac{107}{-1.8} \quad \frac{101}{20} \quad \frac{8.9}{17} \quad \frac{8.6}{+06} \quad \frac{9.0}{20} \quad \frac{9.3}{25} \quad \frac{10.4}{27} \quad \frac{10.8}{32} \quad \frac{0.0}{49} \quad \frac{+1.6}{52}$$

(9.1)

$$\frac{+9.0}{50} \quad \frac{+8.4}{48} \quad \frac{0.0}{37} \quad 22.6 \frac{101}{-1.3} \quad \frac{9.9}{19} \quad \frac{8.6}{15} \quad \frac{8.6}{+05} \quad \frac{8.5}{19} \quad \frac{9.0}{24} \quad \frac{10.2}{26} \quad \frac{10.6}{32} \quad \frac{0.0}{47} \quad \frac{+3.9}{52}$$

Sta	+	HI	-	Elev.
B.14.	4.01	898.55	✓	894.54

424+58

+75

425

426

3.27

897.81

4.01

894.54 ✓

427

+75

428

+50

429

+50

spike in T.P 40' 17+ 5+ 42+ 40

(2.9)

$\frac{7.2}{50}$	$\frac{7.2}{28}$	$\frac{2.7}{21}$	27	$\frac{2.8}{19}$	$\frac{3.0}{40}$	$\frac{4.0}{50}$	C/ev. Ave
------------------	------------------	------------------	----	------------------	------------------	------------------	-----------

(3.1)

$\frac{8.0}{50}$	$\frac{8.2}{31}$	$\frac{2.8}{21}$	28	$\frac{2.8}{17}$	$\frac{3.1}{50}$	C/ev. Ave
------------------	------------------	------------------	----	------------------	------------------	-----------

(3.4)

$\frac{9.0}{50}$	$\frac{8.4}{31}$	$\frac{5.3}{33}$	$\frac{3.0}{20}$	32	$\frac{3.0}{20}$	$\frac{3.2}{50}$	C/ev. Ave
------------------	------------------	------------------	------------------	----	------------------	------------------	-----------

(5.1)

$\frac{10.3}{50}$	$\frac{10.2}{32}$	$\frac{9.6}{27}$	$\frac{5.2}{20}$	52	$\frac{5.2}{20}$	$\frac{9.0}{26}$	$\frac{18.0}{36}$	$\frac{10.3}{50}$
-------------------	-------------------	------------------	------------------	----	------------------	------------------	-------------------	-------------------

spike in T.P 40' 17+ into 42+ 40

(6.1)

$\frac{9.5}{50}$	$\frac{9.5}{29}$	$\frac{8.6}{25}$	$\frac{6.1}{26}$	61	$\frac{6.0}{20}$	$\frac{8.2}{24}$	$\frac{9.3}{29}$	$\frac{9.0}{50}$
------------------	------------------	------------------	------------------	----	------------------	------------------	------------------	------------------

+10 Bag ditch

(7.4)

91	$\frac{8.1}{30}$	$\frac{10.3}{28}$	$\frac{10.2}{26}$	$\frac{9.2}{25}$	$\frac{7.2}{21}$	74	$\frac{7.1}{20}$	$\frac{8.8}{24}$	$\frac{9.2}{27}$	$\frac{8.8}{31}$	$\frac{7.2}{33}$	$\frac{6.1}{50}$
----	------------------	-------------------	-------------------	------------------	------------------	----	------------------	------------------	------------------	------------------	------------------	------------------

(7.9)

$\frac{8.7}{50}$	$\frac{8.7}{31}$	$\frac{10.7}{29}$	$\frac{10.2}{26}$	$\frac{8.1}{25}$	76	$\frac{7.8}{20}$	$\frac{9.3}{24}$	$\frac{9.6}{27}$	$\frac{8.9}{31}$	$\frac{5.3}{36}$	$\frac{4.6}{39}$	$\frac{4.5}{50}$
------------------	------------------	-------------------	-------------------	------------------	----	------------------	------------------	------------------	------------------	------------------	------------------	------------------

(6.8)

$\frac{5.0}{50}$	$\frac{5.4}{37}$	$\frac{10.9}{31}$	$\frac{10.6}{25}$	$\frac{9.2}{20}$	90	$\frac{8.9}{20}$	$\frac{10.2}{24}$	$\frac{10.3}{27}$	$\frac{9.6}{31}$	$\frac{2.9}{41}$	$\frac{1.9}{50}$
------------------	------------------	-------------------	-------------------	------------------	----	------------------	-------------------	-------------------	------------------	------------------	------------------

(9.7)

$\frac{1.6}{50}$	$\frac{2.3}{43}$	$\frac{11.5}{32}$	$\frac{11.2}{24}$	$\frac{9.9}{20}$	98	$\frac{9.8}{20}$	$\frac{11.2}{24}$	$\frac{11.2}{28}$	$\frac{10.7}{32}$	$\frac{3.4}{40}$	$\frac{2.6}{45}$	$\frac{2.9}{50}$
------------------	------------------	-------------------	-------------------	------------------	----	------------------	-------------------	-------------------	-------------------	------------------	------------------	------------------

(10.6)

$\frac{3.6}{50}$	$\frac{4.2}{41}$	$\frac{12.3}{32}$	$\frac{12.3}{23}$	$\frac{10.5}{20}$	108	$\frac{10.7}{20}$	$\frac{12.1}{25}$	$\frac{12.1}{28}$	$\frac{11.7}{31}$	$\frac{5.0}{40}$	$\frac{4.7}{50}$
------------------	------------------	-------------------	-------------------	-------------------	-----	-------------------	-------------------	-------------------	-------------------	------------------	------------------

370 + HI - Elev

897.81 ✓

430

T.P

4.58

890.77 ✓

11.62

886.19 ✓

+50

431

+50

432

+50

433

+50

434

T.P

0.37

881.74 ✓

7.40

881.37 ✓

+50

435

$$\begin{array}{r} 51 \\ 50 \end{array} \quad \begin{array}{r} 59 \\ 41 \end{array} \quad \begin{array}{r} 182 \\ 32 \end{array} \quad \begin{array}{r} 131 \\ 23 \end{array} \quad \begin{array}{r} 117 \\ 20 \end{array} \quad 118 \quad \begin{array}{r} 117 \\ 20 \end{array} \quad \begin{array}{r} 132 \\ 25 \end{array} \quad \begin{array}{r} 132 \\ 30 \end{array} \quad \begin{array}{r} 67 \\ 39 \end{array} \quad \begin{array}{r} 72 \\ 50 \end{array}$$

11.5

$$\begin{array}{r} 00 \\ 50 \end{array} \quad \begin{array}{r} 10 \\ 38 \end{array} \quad \begin{array}{r} 20 \\ 31 \end{array} \quad \begin{array}{r} 69 \\ 24 \end{array} \quad \begin{array}{r} 54 \\ 20 \end{array} \quad 58 \quad \begin{array}{r} 57 \\ 20 \end{array} \quad \begin{array}{r} 21 \\ 24 \end{array} \quad \begin{array}{r} 72 \\ 28 \end{array} \quad \begin{array}{r} 67 \\ 32 \end{array} \quad \begin{array}{r} 28 \\ 34 \end{array} \quad \begin{array}{r} 23 \\ 38 \end{array} \quad \begin{array}{r} 31 \\ 50 \end{array}$$

5.4

$$\begin{array}{r} 24 \\ 50 \end{array} \quad \begin{array}{r} 32 \\ 36 \end{array} \quad \begin{array}{r} 80 \\ 31 \end{array} \quad \begin{array}{r} 78 \\ 23 \end{array} \quad \begin{array}{r} 64 \\ 20 \end{array} \quad 61 \quad \begin{array}{r} 63 \\ 20 \end{array} \quad \begin{array}{r} 81 \\ 24 \end{array} \quad \begin{array}{r} 81 \\ 30 \end{array} \quad \begin{array}{r} 56 \\ 31 \end{array} \quad \begin{array}{r} 52 \\ 34 \end{array} \quad \begin{array}{r} 62 \\ 50 \end{array}$$

6.3

$$\begin{array}{r} 50 \\ 50 \end{array} \quad \begin{array}{r} 43 \\ 44 \end{array} \quad \begin{array}{r} 54 \\ 34 \end{array} \quad \begin{array}{r} 88 \\ 30 \end{array} \quad \begin{array}{r} 86 \\ 23 \end{array} \quad \begin{array}{r} 69 \\ 20 \end{array} \quad 74 \quad \begin{array}{r} 74 \\ 20 \end{array} \quad \begin{array}{r} 92 \\ 24 \end{array} \quad \begin{array}{r} 90 \\ 30 \end{array} \quad \begin{array}{r} 73 \\ 32 \end{array} \quad \begin{array}{r} 81 \\ 50 \end{array}$$

1.2

$$\begin{array}{r} 64 \\ 50 \end{array} \quad \begin{array}{r} 65 \\ 42 \end{array} \quad \begin{array}{r} 74 \\ 34 \end{array} \quad \begin{array}{r} 97 \\ 32 \end{array} \quad \begin{array}{r} 95 \\ 24 \end{array} \quad \begin{array}{r} 80 \\ 20 \end{array} \quad 80 \quad \begin{array}{r} 80 \\ 20 \end{array} \quad \begin{array}{r} 100 \\ 25 \end{array} \quad \begin{array}{r} 101 \\ 29 \end{array} \quad \begin{array}{r} 88 \\ 30 \end{array} \quad \begin{array}{r} 91 \\ 50 \end{array}$$

4.0

$$\begin{array}{r} 73 \\ 50 \end{array} \quad \begin{array}{r} 88 \\ 42 \end{array} \quad \begin{array}{r} 78 \\ 33 \end{array} \quad \begin{array}{r} 104 \\ 32 \end{array} \quad \begin{array}{r} 103 \\ 24 \end{array} \quad \begin{array}{r} 82 \\ 21 \end{array} \quad 84 \quad \begin{array}{r} 87 \\ 20 \end{array} \quad \begin{array}{r} 108 \\ 23 \end{array} \quad \begin{array}{r} 112 \\ 28 \end{array} \quad \begin{array}{r} 96 \\ 30 \end{array} \quad \begin{array}{r} 110 \\ 50 \end{array}$$

4.8

$$\begin{array}{r} 81 \\ 50 \end{array} \quad \begin{array}{r} 88 \\ 33 \end{array} \quad \begin{array}{r} 112 \\ 31 \end{array} \quad \begin{array}{r} 111 \\ 23 \end{array} \quad \begin{array}{r} 89 \\ 21 \end{array} \quad 89 \quad \begin{array}{r} 91 \\ 20 \end{array} \quad \begin{array}{r} 114 \\ 24 \end{array} \quad \begin{array}{r} 115 \\ 28 \end{array} \quad \begin{array}{r} 109 \\ 30 \end{array} \quad \begin{array}{r} 126 \\ 50 \end{array}$$

9.4

$$\begin{array}{r} 96 \\ 50 \end{array} \quad \begin{array}{r} 100 \\ 33 \end{array} \quad \begin{array}{r} 121 \\ 31 \end{array} \quad \begin{array}{r} 121 \\ 23 \end{array} \quad \begin{array}{r} 93 \\ 20 \end{array} \quad 94 \quad \begin{array}{r} 94 \\ 20 \end{array} \quad \begin{array}{r} 118 \\ 24 \end{array} \quad \begin{array}{r} 120 \\ 28 \end{array} \quad \begin{array}{r} 114 \\ 30 \end{array} \quad \begin{array}{r} 124 \\ 50 \end{array}$$

9.9

$$\begin{array}{r} 108 \\ 50 \end{array} \quad \begin{array}{r} 109 \\ 33 \end{array} \quad \begin{array}{r} 140 \\ 31 \end{array} \quad \begin{array}{r} 140 \\ 28 \end{array} \quad \begin{array}{r} 98 \\ 22 \end{array} \quad 97 \quad \begin{array}{r} 100 \\ 20 \end{array} \quad \begin{array}{r} 120 \\ 24 \end{array} \quad \begin{array}{r} 121 \\ 29 \end{array} \quad \begin{array}{r} 125 \\ 50 \end{array}$$

10.3

5th End Ditch

$$\begin{array}{r} 40 \\ 50 \end{array} \quad \begin{array}{r} 40 \\ 34 \end{array} \quad \begin{array}{r} 60 \\ 34 \end{array} \quad \begin{array}{r} 62 \\ 31 \end{array} \quad \begin{array}{r} 39 \\ 28 \end{array} \quad \begin{array}{r} 10 \\ 20 \end{array} \quad 1.0 \quad \begin{array}{r} 10 \\ 20 \end{array} \quad \begin{array}{r} 40 \\ 22 \end{array} \quad \begin{array}{r} 52 \\ 50 \end{array}$$

1.5

$$\begin{array}{r} 62 \\ 50 \end{array} \quad \begin{array}{r} 64 \\ 38 \end{array} \quad \begin{array}{r} 21 \\ 37 \end{array} \quad \begin{array}{r} 70 \\ 32 \end{array} \quad \begin{array}{r} 63 \\ 32 \end{array} \quad \begin{array}{r} 63 \\ 29 \end{array} \quad \begin{array}{r} 43 \\ 26 \end{array} \quad \begin{array}{r} 09 \\ 20 \end{array} \quad 1.0 \quad \begin{array}{r} 10 \\ 20 \end{array} \quad \begin{array}{r} 57 \\ 29 \end{array} \quad \begin{array}{r} 64 \\ 33 \end{array} \quad \begin{array}{r} 65 \\ 50 \end{array}$$

1.6

579

+

HI

-

Elev

881.74 ✓

435+50

436

+50

437

B.M.

8.82.

882.99 ✓

7.57

874.17 ✓

+28

43

+65

75

438

+45

+70

+94

26.
36

(17)

$\frac{72}{50}$ $\frac{76}{41}$ $\frac{85}{39}$ $\frac{84}{37}$ $\frac{72}{33}$ $\frac{64}{30}$ $\frac{12}{20}$ 1.5 $\frac{15}{20}$ $\frac{67}{29}$ $\frac{74}{32}$ $\frac{77}{50}$

$\frac{68}{50}$ $\frac{72}{40}$ $\frac{84}{39}$ $\frac{85}{36}$ $\frac{75}{35}$ $\frac{69}{32}$ $\frac{50}{29}$ $\frac{46}{25}$ $\frac{11}{20}$ $\frac{14}{20}$ $\frac{14}{20}$ $\frac{70}{30}$ $\frac{81}{37}$ $\frac{86}{50}$

(17)

$\frac{72}{50}$ $\frac{73}{44}$ $\frac{94}{49}$ $\frac{92}{40}$ $\frac{74}{39}$ $\frac{78}{33}$ $\frac{68}{31}$ $\frac{12}{20}$ 14 $\frac{14}{18}$ $\frac{63}{28}$ $\frac{112}{34}$ $\frac{103}{50}$

(17)

436+90 Bog Ditch.
Bridge.

spike in 10" Birch 70' Lt St 436+70

$\frac{115}{50}$ $\frac{92}{45}$ $\frac{92}{34}$ $\frac{21}{20}$ $\frac{24}{20}$ $\frac{24}{20}$ $\frac{104}{36}$ $\frac{116}{40}$ $\frac{128}{42}$ $\frac{129}{45}$ $\frac{119}{49}$ $\frac{115}{50}$

(30)

$\frac{128}{50}$ $\frac{118}{41}$ $\frac{94}{33}$ $\frac{24}{20}$ $\frac{23}{20}$ $\frac{25}{20}$ $\frac{103}{31}$ $\frac{113}{40}$ $\frac{126}{42}$ $\frac{127}{44}$ $\frac{113}{46}$ $\frac{110}{50}$

(30)

$\frac{104}{50}$ $\frac{105}{34}$ $\frac{24}{20}$ $\frac{25}{20}$ $\frac{25}{20}$ $\frac{91}{33}$ $\frac{110}{40}$ $\frac{123}{42}$ $\frac{127}{45}$ $\frac{110}{46}$ $\frac{106}{50}$

(30)

$\frac{101}{50}$ $\frac{100}{37}$ $\frac{87}{31}$ $\frac{24}{20}$ $\frac{25}{20}$ $\frac{26}{20}$ $\frac{100}{34}$ $\frac{106}{37}$ $\frac{126}{41}$ $\frac{127}{44}$ $\frac{103}{46}$ $\frac{109}{50}$
275 End Ditch

(30)

$\frac{95}{50}$ $\frac{105}{41}$ $\frac{94}{33}$ $\frac{27}{21}$ $\frac{23}{20}$ 2 $\frac{24}{20}$ $\frac{115}{38}$ $\frac{124}{40}$ $\frac{102}{50}$ old creek
+ 30 Bog Ditch.

(30)

$\frac{113}{50}$ $\frac{115}{45}$ $\frac{108}{37}$ $\frac{24}{20}$ $\frac{23}{20}$ $\frac{30}{20}$ $\frac{52}{27}$ $\frac{90}{27}$ $\frac{108}{47}$ $\frac{123}{48}$ $\frac{124}{52}$ $\frac{113}{53}$

(17)

$\frac{137}{50}$ $\frac{129}{40}$ $\frac{27}{20}$ $\frac{27}{20}$ $\frac{28}{20}$ $\frac{93}{36}$ $\frac{110}{41}$ $\frac{122}{43}$ $\frac{132}{49}$ $\frac{116}{48}$ $\frac{113}{50}$

(17)

$\frac{128}{50}$ $\frac{148}{45}$ $\frac{124}{34}$ $\frac{27}{20}$ $\frac{23}{20}$ $\frac{26}{20}$ $\frac{108}{34}$ $\frac{121}{39}$ $\frac{136}{50}$

(14)

439

+

H I

-

Elev

882.99 ✓

439

+30

440

+50

441

+64

442

+50

443

+30

+73

444

T.P.

11.44

888.98 ✓

5.40

877.54 ✓

$$\frac{10.1}{50} \quad \frac{10.6}{37} \quad \frac{2.5}{20} \quad \frac{2.2}{3.0} \quad \frac{2.6}{20} \quad \frac{10.8}{35} \quad \frac{12.5}{42} \quad \frac{13.6}{50}$$

$$\frac{10.2}{50} \quad \frac{10.0}{35} \quad \frac{2.5}{20} \quad \frac{2.2}{3.0} \quad \frac{2.6}{20} \quad \frac{9.3}{30} \quad \frac{10.0}{40} \quad \frac{9.9}{50}$$

$$\frac{10.1}{50} \quad \frac{10.8}{43} \quad \frac{9.8}{35} \quad \frac{2.4}{20} \quad \frac{2.1}{3.0} \quad \frac{2.4}{20} \quad \frac{2.7}{31} \quad \frac{9.3}{39} \quad \frac{9.9}{50}$$

$$\frac{10.1}{50} \quad \frac{9.5}{39} \quad \frac{8.3}{31} \quad \frac{1.9}{19} \quad \frac{2.1}{19} \quad \frac{2.3}{19} \quad \frac{8.0}{30} \quad \frac{7.5}{37} \quad \frac{7.2}{50}$$

$$\frac{9.8}{50} \quad \frac{10.2}{35} \quad \frac{2.3}{20} \quad \frac{2.3}{2.0} \quad \frac{2.5}{20} \quad \frac{8.2}{29} \quad \frac{9.3}{38} \quad \frac{9.9}{50}$$

$$\frac{11.7}{50} \quad \frac{10.9}{39} \quad \frac{9.9}{34} \quad \frac{2.0}{19} \quad \frac{2.1}{20} \quad \frac{7.8}{30} \quad \frac{8.7}{37} \quad \frac{9.1}{50}$$

$$\frac{9.0}{50} \quad \frac{9.4}{35} \quad \frac{8.3}{31} \quad \frac{2.3}{20} \quad \frac{2.1}{20} \quad \frac{2.5}{20} \quad \frac{7.7}{31} \quad \frac{9.1}{38} \quad \frac{9.2}{50}$$

$$\frac{8.1}{50} \quad \frac{7.7}{32} \quad \frac{7.1}{28} \quad \frac{1.9}{19} \quad \frac{2.1}{19} \quad \frac{2.6}{19} \quad \frac{8.0}{30} \quad \frac{9.3}{37} \quad \frac{9.9}{50}$$

$$\frac{7.0}{50} \quad \frac{6.8}{31} \quad \frac{6.2}{28} \quad \frac{1.8}{20} \quad \frac{1.8}{19} \quad \frac{2.2}{19} \quad \frac{5.6}{24} \quad \frac{6.0}{31} \quad \frac{6.1}{51}$$

$$\frac{8.0}{50} \quad \frac{7.2}{36} \quad \frac{6.4}{29} \quad \frac{1.9}{20} \quad \frac{1.8}{19} \quad \frac{2.1}{19} \quad \frac{4.9}{23} \quad \frac{5.7}{29} \quad \frac{6.1}{50}$$

+ 40 Beg Ditch.

$$\frac{6.8}{50} \quad \frac{6.6}{35} \quad \frac{6.0}{27} \quad \frac{2.0}{20} \quad \frac{1.2}{20} \quad \frac{1.7}{20} \quad \frac{5.0}{27} \quad \frac{5.3}{31} \quad \frac{3.5}{33} \quad \frac{3.9}{42} \quad \frac{3.5}{50}$$

$$\frac{6.7}{50} \quad \frac{6.4}{33} \quad \frac{5.5}{21} \quad \frac{1.9}{20} \quad \frac{1.2}{20} \quad \frac{1.6}{20} \quad \frac{3.8}{24} \quad \frac{4.8}{30} \quad \frac{3.8}{32} \quad \frac{3.5}{50}$$

Sta	+	HI	-	Elev
B.M.	11.02	889.03 ✓	11.00	877.98 = 878.01 ✓
444+40				

445

+50

446

+50

447

+50

448

+50

449

T.P.	9.58	897.65 ✓	0.96	888.07 ✓
+50				

spike in Twin Tree 175' Lt Sta 445+30

$\frac{11.5}{50}$ $\frac{11.7}{40}$ $\frac{11.8}{29}$ $\frac{7.4}{20}$ $\frac{7.2}{20}$ $\frac{7.6}{20}$ $\frac{11.1}{29}$ $\frac{11.5}{31}$ $\frac{10.9}{32}$ $\frac{11.8}{50}$
+40 End Pitch

$\frac{9.1}{50}$ $\frac{10.1}{25}$ $\frac{6.8}{20}$ $\frac{7.3}{20}$ $\frac{7.4}{20}$ $\frac{10.5}{23}$ $\frac{11.1}{32}$ $\frac{11.7}{50}$

$\frac{10.0}{50}$ $\frac{10.9}{32}$ $\frac{10.6}{27}$ $\frac{6.7}{19}$ $\frac{6.9}{19}$ $\frac{6.8}{19}$ $\frac{10.3}{25}$ $\frac{9.6}{50}$
+90 = Beg D. Pitch Rt. 4 Lt

$\frac{9.0}{50}$ $\frac{8.4}{30}$ $\frac{9.1}{29}$ $\frac{9.0}{26}$ $\frac{8.0}{23}$ $\frac{6.5}{20}$ $\frac{6.4}{20}$ $\frac{8.4}{23}$ $\frac{8.4}{28}$ $\frac{7.0}{31}$ $\frac{6.9}{50}$

$\frac{5.9}{50}$ $\frac{6.0}{34}$ $\frac{8.1}{30}$ $\frac{8.1}{25}$ $\frac{6.0}{20}$ $\frac{6.1}{20}$ $\frac{5.8}{20}$ $\frac{7.7}{24}$ $\frac{7.7}{30}$ $\frac{4.9}{33}$ $\frac{4.3}{50}$

$\frac{7.5}{29}$ $\frac{7.4}{25}$ $\frac{5.0}{20}$ $\frac{5.0}{20}$ $\frac{5.0}{20}$ $\frac{7.1}{24}$ $\frac{7.1}{29}$

$\frac{6.4}{30}$ $\frac{6.2}{24}$ $\frac{4.0}{20}$ $\frac{4.3}{20}$ $\frac{4.4}{20}$ $\frac{6.3}{24}$ $\frac{6.3}{29}$

$\frac{4.7}{30}$ $\frac{5.1}{23}$ $\frac{3.0}{20}$ $\frac{3.2}{20}$ $\frac{3.2}{20}$ $\frac{5.4}{23}$ $\frac{5.1}{29}$

$\frac{3.8}{29}$ $\frac{3.8}{24}$ $\frac{2.1}{20}$ $\frac{2.2}{20}$ $\frac{1.9}{20}$ $\frac{4.1}{24}$ $\frac{3.8}{30}$

$\frac{1.2}{32}$ $\frac{2.7}{26}$ $\frac{2.7}{25}$ $\frac{0.8}{20}$ $\frac{0.9}{20}$ $\frac{1.1}{20}$ $\frac{3.1}{25}$ $\frac{3.1}{27}$ $\frac{2.4}{31}$

$\frac{9.8}{30}$ $\frac{10.4}{26}$ $\frac{10.4}{23}$ $\frac{8.6}{20}$ $\frac{8.4}{20}$ $\frac{8.6}{20}$ $\frac{10.6}{25}$ $\frac{10.2}{30}$

Sta

+

HI

-

Elev.

89765 ✓

450

+50

451

+50

452

+50

453

+50

454

+50

455

(7.7)

$\frac{7.0}{30}$	$\frac{9.8}{28}$	$\frac{9.8}{23}$	$\frac{7.7}{20}$	7.7	$\frac{7.5}{20}$	$\frac{8.9}{24}$	$\frac{8.7}{30}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

(6.7)

$\frac{8.5}{30}$	$\frac{9.1}{27}$	$\frac{9.1}{24}$	$\frac{7.4}{20}$	6.6	$\frac{6.3}{20}$	$\frac{7.9}{24}$	$\frac{7.6}{28}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

(5.9)

$\frac{7.2}{30}$	$\frac{8.1}{26}$	$\frac{8.0}{24}$	$\frac{6.2}{20}$	5.5	$\frac{5.1}{20}$	$\frac{6.8}{24}$	$\frac{6.8}{26}$	$\frac{6.0}{30}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(5.1)

$\frac{6.4}{30}$	$\frac{7.2}{26}$	$\frac{7.2}{24}$	$\frac{5.2}{20}$	5.0	$\frac{5.6}{20}$	$\frac{6.4}{24}$	$\frac{6.5}{26}$	$\frac{5.8}{30}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(4.4)

$\frac{5.8}{30}$	$\frac{6.6}{25}$	$\frac{6.6}{23}$	$\frac{4.9}{20}$	4.6	$\frac{5.9}{20}$	$\frac{5.6}{23}$	$\frac{5.6}{25}$	$\frac{4.8}{30}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(3.9)

$\frac{10}{39}$	$\frac{1.7}{36}$	$\frac{5.5}{31}$	$\frac{6.4}{26}$	$\frac{5.8}{23}$	$\frac{4.3}{20}$	3.7	$\frac{3.6}{20}$	$\frac{5.2}{24}$	$\frac{5.5}{26}$	$\frac{4.5}{30}$
-----------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(3.3)

$\frac{3.1}{50}$	$\frac{1.2}{38}$	$\frac{2.1}{35}$	$\frac{5.6}{30}$	$\frac{6.3}{28}$	$\frac{6.1}{25}$	$\frac{3.8}{20}$	3.2	$\frac{2.9}{20}$	$\frac{4.9}{24}$	$\frac{4.8}{26}$	$\frac{3.8}{32}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(2.9)

$\frac{3.9}{50}$	$\frac{2.7}{36}$	$\frac{3.1}{33}$	$\frac{5.9}{29}$	$\frac{5.7}{25}$	$\frac{3.3}{20}$	2.7	$\frac{2.6}{20}$	$\frac{4.1}{24}$	$\frac{4.0}{27}$	$\frac{3.5}{30}$
------------------	------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(2.5)

$\frac{5.5}{50}$	$\frac{5.0}{31}$	$\frac{5.1}{27}$	$\frac{4.2}{23}$	$\frac{2.5}{20}$	2.4	$\frac{2.0}{20}$	$\frac{3.8}{24}$	$\frac{3.8}{28}$	$\frac{2.5}{29}$	$\frac{1.8}{33}$	$\frac{1.7}{41}$	$\frac{1.5}{50}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------	------------------	------------------	------------------

(2.2)

$\frac{5.7}{50}$	$\frac{5.7}{32}$	$\frac{4.7}{25}$	$\frac{2.6}{20}$	1.6	$\frac{1.6}{20}$	$\frac{3.9}{25}$	$\frac{5.0}{31}$	$\frac{4.5}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

(1.9)

$\frac{6.6}{50}$	$\frac{7.0}{31}$	$\frac{5.8}{27}$	$\frac{2.1}{20}$	1.5	$\frac{1.3}{20}$	$\frac{5.6}{29}$	$\frac{6.6}{34}$	$\frac{6.9}{50}$
------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------	------------------

Sta		HI		Elev
	-	897.65	-	
455+50				
456				
B.M.			1.83	895.82
				895.81
B.M.	1.06	906.87	?	895.81
453+50				
453				
+50				
452				
T.P.	9.62	910.24	6.25	900.62
+50				
451				
+50				

$$\frac{66}{50} \quad \frac{80}{30} \quad \frac{13}{19} \quad 0.7 \quad \textcircled{11.6} \quad \frac{0.6}{20} \quad \frac{8.0}{36} \quad \frac{8.0}{50}$$

$$\frac{9.0}{50} \quad \frac{9.1}{31} \quad \frac{1.3}{20} \quad 0.7 \quad \textcircled{11.2} \quad \frac{0.5}{19} \quad \frac{8.0}{32} \quad \frac{9.1}{50}$$

3 W. Car Cattle Pass Lt side.

$$\textcircled{12.1} \quad \frac{8.2}{36} \quad \frac{7.6}{40} \quad \frac{7.1}{50}$$

$$\textcircled{12.5} \quad \frac{5.2}{42} \quad \frac{4.6}{46} \quad \frac{4.3}{50}$$

$$\textcircled{13.1} \quad \frac{2.5}{46} \quad \frac{1.7}{50}$$

$$\frac{8.8}{50} \quad \frac{8.3}{42} \quad \frac{8.8}{38} \quad \textcircled{13.6} \quad \frac{1.0}{48} \quad \frac{0.0}{53}$$

$$\frac{103}{50} \quad \frac{103}{45} \quad \frac{107}{43} \quad \textcircled{17.6} \quad \frac{2.7}{50} \quad \frac{1.6}{54}$$

$$\frac{9.8}{50} \quad \frac{9.7}{47} \quad \frac{10.3}{45} \quad \textcircled{18.4} \quad \frac{3.3}{50} \quad \frac{2.6}{53}$$

$$\frac{101}{50} \quad \frac{104}{48} \quad \frac{108}{45} \quad \textcircled{19.2} \quad \frac{4.6}{50} \quad \frac{4.0}{54}$$

549

+

HZ

-

F10 ✓

910.24 ✓

450

+50

449

T.P.

1.47

899.53 ✓

12.18

898.06 ✓

+50

448

+50

447

T.P.

2.12

889.18 ✓

12.47

887.06 ✓

B.M.

11.16

878.02 ✓

878.01

$$\frac{11.4}{50} \quad \frac{11.6}{47} \quad \frac{12.3}{44}$$

20.2

$$\frac{6.8}{50} \quad \frac{6.1}{54}$$

$$\frac{12.4}{50} \quad \frac{12.5}{48} \quad \frac{12.8}{44}$$

21.2

$$\frac{9.4}{48} \quad \frac{8.5}{53}$$

$$\frac{12.6}{60} \quad \frac{12.6}{49} \quad \frac{12.9}{46}$$

22.0

$$\frac{11.5}{47} \quad \frac{11.0}{50}$$

$$\frac{4.5}{50} \quad \frac{4.1}{48} \quad \frac{4.5}{44}$$

12.5

$$\frac{3.7}{44} \quad \frac{3.1}{48} \quad \frac{3.1}{50}$$

$$\frac{7.4}{50} \quad \frac{7.3}{45} \quad \frac{7.8}{41}$$

13.5

$$\frac{5.9}{43} \quad \frac{5.6}{46} \quad \frac{5.8}{50}$$

$$\frac{10.7}{50} \quad \frac{10.6}{42} \quad \frac{11.1}{37}$$

14.5

$$\frac{9.7}{39} \quad \frac{8.8}{44} \quad \frac{8.7}{50}$$

$$\frac{13.0}{50} \quad \frac{11.7}{43} \quad \frac{11.7}{39} \quad \frac{13.3}{34}$$

15.5

$$\frac{12.1}{37} \quad \frac{11.4}{40} \quad \frac{11.7}{50}$$

X Section, Lind Division

Sta	+	HI	-	Elev.
T.P.B.M.	5.48.	888.83.		883.35.
304+50				83.0
305				83.2
+50				83.4
306+00				83.6
+50				83.8
307				84.0
+50				84.2
308				84.4
+50				84.6
+76 ⁰⁰				84.7
309				84.8

5.8

$$\frac{74}{36} \quad \frac{77}{24} \quad \frac{67}{22} \quad 60 \quad \frac{63}{28} \quad \frac{116}{36} \quad \frac{118}{50}$$

5.6

$$\frac{75}{35} \quad \frac{77}{25} \quad \frac{66}{22} \quad 60 \quad \frac{57}{29} \quad \frac{117}{37} \quad \frac{120}{50}$$

5.4

$$\frac{0.5}{40} \quad \frac{43}{35} \quad \frac{52}{31} \quad \frac{82}{25} \quad \frac{62}{21} \quad 59 \quad \frac{49}{35} \quad \frac{117}{44} \quad \frac{122}{50}$$

5.2

$$\frac{75}{24} \quad \frac{77}{20} \quad \frac{62}{18} \quad 60 \quad \frac{46}{43} \quad \frac{83}{50} \quad \frac{122}{56}$$

5.0

$$\frac{66}{20} \quad \frac{73}{12} \quad \frac{65}{11} \quad 60 \quad \frac{42}{51} \quad \frac{120}{65}$$

4.8

$$\frac{63}{21} \quad \frac{65}{13} \quad \frac{56}{11} \quad 55 \quad \frac{44}{54} \quad \frac{106}{65}$$

4.6

$$\frac{0.0}{20} \quad \frac{50}{11} \quad 50 \quad \frac{40}{48} \quad \frac{66}{53} \quad \frac{73}{63} \quad \frac{104}{50}$$

4.4

$$\frac{0.5}{19} \quad \frac{43}{13} \quad 43 \quad \frac{46}{20} \quad \frac{68}{24} \quad \frac{70}{31} \quad \frac{38}{37} \quad \frac{38}{50}$$

4.2

$$\frac{10}{19} \quad \frac{40}{14} \quad 42 \quad \frac{42}{20} \quad \frac{65}{25} \quad \frac{64}{29} \quad \frac{35}{35} \quad \frac{37}{50}$$

4.1

$$\frac{0.0}{19} \quad \frac{40}{12} \quad 42 \quad \frac{40}{21} \quad \frac{68}{25} \quad \frac{60}{30} \quad \frac{34}{35} \quad \frac{40}{50}$$

4.0

$$\frac{0.4}{17} \quad \frac{22}{14} \quad \frac{38}{12} \quad 42 \quad \frac{40}{21} \quad \frac{57}{24} \quad \frac{55}{30} \quad \frac{35}{32} \quad \frac{40}{50}$$

Sta	+	HI	-	Elev
		888.83.		
309+69				85.1 3.7
+80				85.1
310				85.2
T.P.	5.80	890.93 900.93	370	885.13.
+50				85.4
+84				85.5
311+00				85.6
+50				85.8
312+00				86.0
+50				86.2
313+00				86.4
+14				86.5
+38				86.6

879.66

890.93.
900.93

314				86.8
BM			11.30	879.63.
BM	3.85	897.42.		893.57.
304+50				83.0
305				83.2
F50				83.4
306				83.6
T.P.	12.77	900.94.	9.25	888.17.
+50				83.8
T.P.	11.21	911.14.	1.11	899.83.
317				84.0
+50				84.2
T.P.	8.61	916.72.	2.91	908.12.
308				84.4
+50				84.6
+76.25				84.7

$$\frac{00}{50} \quad \frac{10.7}{39} \quad \frac{12.6}{38} \quad \frac{12.6}{36} \quad \frac{10.7}{35} \quad \frac{8.7}{29} \quad \frac{4.5}{21} \quad \frac{4.1}{43} \quad \frac{4.5}{19} \quad \frac{6.5}{23} \quad \frac{6.5}{27} \quad \frac{4.5}{31} \quad \frac{6.0}{50}$$

$$\frac{3.8}{50} \quad \frac{4.5}{47}$$

(14.4)

$$\frac{4.7}{50} \quad \frac{6.2}{45}$$

(14.2)

$$\frac{3.5}{50} \quad \frac{4.5}{47} \quad \frac{8.5}{44}$$

(14.0)

$$\frac{2.6}{50}$$

(13.8)

$$\frac{6.5}{50} \quad \frac{9.3}{39} \quad \frac{11.5}{38} \quad \frac{13.3}{27}$$

(17.1)

$$\frac{8.8}{50} \quad \frac{10.8}{32}$$

(27.0)

$$\frac{0.4}{50} \quad \frac{3.3}{40}$$

(26.8)

Nail

$$\frac{2.5}{50} \quad \frac{3.7}{37} \quad \frac{6.0}{20}$$

(32.3)

$$\frac{0.8}{50} \quad \frac{3.5}{13}$$

(32.1)

$$\frac{0.9}{50} \quad \frac{4.5}{23}$$

(32.0)

Sta	+	HI	-	Elev.
		916.72.		
309+00				84.8
	+69			85.1
	+80			85.1
310+00				85.2
	+50			85.4
	+84			85.5
311+00				85.6
	+50			85.8
T.P.	12.53	925.73.	3.52	919.20.
312				86.0
	+50			86.2
313.				86.4
T.P.	1.13	918.35	8.57	917.22
	+14			86.5
T.P.	1.82	906.55 907.55	12.62	905.73

$$\frac{14}{50} \quad \frac{50}{25}$$

(31.9)

$$\frac{37}{50} \quad \frac{61}{35}$$

(31.6)

$$\frac{44}{50} \quad \frac{67}{36}$$

(31.6)

$$\frac{56}{50} \quad \frac{72}{39}$$

(31.5)

$$\frac{73}{50} \quad \frac{98}{37}$$

(31.3)

$$\frac{86}{50} \quad \frac{105}{38}$$

(31.2)

$$\frac{64}{75} \quad \frac{75}{60}$$

(31.1)

$$\frac{56}{75} \quad \frac{56}{56}$$

(30.9)

$$\frac{81}{75} \quad \frac{88}{50}$$

(39.7)

$$\frac{21}{75} \quad \frac{42}{53}$$

(39.5)

$$\frac{92}{75} \quad \frac{155}{48}$$

(39.3)

$$\frac{50}{75} \quad \frac{87}{60} \quad \frac{180}{40}$$

(31.9)

Sta	+	HI	-	Elev	
T.P	2.70	900.95 899.95	930	898.25 899.25	
313+38				86.6	
313+40				86.4	
T.P	1.90	894.14 893.14	871	892.24 891.24	
T.P	2.83	889.14.	783	886.31.	
B.M.	2.51	889.17.	751	879.63.	519.66
314+50				87.0	2.2
315				87.2	
+12				87.2	
+24				87.3	
+50				87.4	
+60				87.4	
316				87.6	
317				88.0	
318				88.5	
T.P.	716	895.61	0.72	888.45.	

$$\frac{7.0}{50}$$

$$\frac{11.3}{70}$$

$$\frac{12.0}{37}$$

144

$$\frac{58}{40}$$

$$\frac{96}{33}$$

spine in PP 60' N 5th 326+10

22

WE.

$$\frac{106}{50}$$

$$\frac{101}{34}$$

$$\frac{27}{21}$$

$$\frac{26}{21}$$

$$\frac{5.2}{26}$$

$$\frac{5.5}{36}$$

$$\frac{12.5}{43}$$

20

WE.

$$\frac{110}{50}$$

$$\frac{110}{41}$$

$$\frac{10.0}{35}$$

$$\frac{30}{21}$$

$$\frac{2.8}{22}$$

$$\frac{30}{22}$$

$$\frac{12.8}{39}$$

20

EW.

$$\frac{108}{50}$$

$$\frac{110}{34}$$

$$\frac{2.7}{21}$$

$$\frac{27}{22}$$

$$\frac{30}{22}$$

$$\frac{11.6}{39}$$

$$\frac{12.8}{49}$$

19

EW.

$$\frac{106}{50}$$

$$\frac{106}{38}$$

$$\frac{2.6}{22}$$

$$\frac{26}{22}$$

$$\frac{30}{22}$$

$$\frac{9.5}{35}$$

$$\frac{10.2}{43}$$

$$\frac{12.5}{50}$$

18

$$\frac{10.5}{50}$$

$$\frac{10.3}{36}$$

$$\frac{2.6}{22}$$

$$\frac{2.4}{22}$$

$$\frac{2.7}{22}$$

$$\frac{90}{33}$$

$$\frac{80}{38}$$

$$\frac{11.0}{50}$$

18

$$\frac{10.0}{50}$$

$$\frac{10.6}{36}$$

$$\frac{2.6}{22}$$

$$\frac{2.7}{22}$$

$$\frac{2.7}{22}$$

$$\frac{7.5}{34}$$

$$\frac{10.2}{52}$$

17

$$\frac{9.6}{50}$$

$$\frac{9.6}{35}$$

$$\frac{2.4}{21}$$

$$\frac{2.9}{22}$$

$$\frac{2.9}{22}$$

$$\frac{3.9}{27}$$

$$\frac{4.8}{50}$$

17

$$\frac{8.6}{50}$$

$$\frac{8.6}{35}$$

$$\frac{1.8}{21}$$

$$\frac{1.8}{23}$$

$$\frac{1.8}{23}$$

$$\frac{2.7}{27}$$

$$\frac{3.0}{50}$$

27

$$\frac{6.0}{50}$$

$$\frac{6.7}{29}$$

$$\frac{1.4}{21}$$

$$\frac{9.8}{22}$$

$$\frac{1.0}{26}$$

$$\frac{1.3}{50}$$

Sta	+	HI	-	Elev
		895.61.		
319				89.0
320				89.6
321				90.2
T.P.	203	892.96.	4.68	890.93.
322				90.8
323				91.4
+50				
324				92.0
T.P.	2.45	898.01.	0.40	892.56.
+50				92.3
325				92.6
5914				92.9
326				93.0

$$\frac{11}{50} \quad \frac{42}{35} \quad \frac{80}{31} \quad \frac{80}{22} \quad \frac{67}{19} \quad \textcircled{6.6} \quad \frac{70}{28} \quad \frac{6.8}{47} \quad \frac{8.2}{50}$$

$$\frac{73}{50} \quad \frac{104}{28} \quad \frac{53}{20} \quad \textcircled{6.0} \quad \frac{66}{43} \quad \frac{9.8}{50}$$

$$\frac{113}{50} \quad \frac{120}{24} \quad \frac{110}{30} \quad \frac{58}{20} \quad \textcircled{5.4} \quad \frac{58}{40} \quad \frac{106}{50}$$

$$\frac{118}{50} \quad \frac{112}{38} \quad \frac{57}{29} \quad \frac{23}{20} \quad \textcircled{2.2} \quad \frac{20}{26} \quad \frac{25}{37} \quad \frac{83}{50}$$

$$\frac{152}{50} \quad \frac{148}{46} \quad \frac{48}{29} \quad \frac{15}{20} \quad \textcircled{1.6} \quad \frac{16}{33} \quad \frac{100}{50}$$

$$\frac{155}{50} \quad \frac{153}{45} \quad \frac{44}{29} \quad \frac{15}{21} \quad \textcircled{1.0} \quad \frac{13}{32} \quad \frac{9.8}{50}$$

$$\frac{140}{50} \quad \frac{130}{42} \quad \frac{45}{29} \quad \frac{29}{21} \quad \textcircled{0.7} \quad \frac{10}{31} \quad \frac{9.7}{50}$$

$$\frac{150}{50} \quad \frac{144}{37} \quad \frac{85}{28} \quad \frac{55}{20} \quad \textcircled{5.7} \quad \frac{55}{28} \quad \frac{140}{45} \quad \frac{14.8}{50}$$

$$\frac{58}{50} \quad \frac{7.8}{24} \quad \frac{51}{20} \quad \textcircled{5.4} \quad \frac{58}{27} \quad \frac{10.1}{36} \quad \frac{11.5}{50}$$

$$\frac{60}{26} \quad \frac{61}{18} \quad \frac{46}{15} \quad \textcircled{5.1} \quad \frac{49}{26} \quad \frac{50}{27} \quad \frac{60}{34} \quad \frac{30}{39} \quad \frac{44}{50}$$

$$\frac{58}{26} \quad \frac{60}{19} \quad \frac{46}{16} \quad \textcircled{5.0} \quad \frac{46}{24} \quad \frac{50}{28} \quad \frac{60}{34}$$

Sta	+	NI	-	Elev
		898.01.		
326	+50			93.2
327	+00			93.3
	+50			
328				
T.P.	10.28	903.16.	5.73	892.88.
B.M.	12.95	903.16.	2.95	900.21.
T.P.	5.49	898.37.	10.28	892.88.
334	+00			92.4.
	+60			92.3
T.P.	4.40	895.03.	7.74	890.63.
335				92.2
	+38			92.2
336				92.0
	+50			91.9

$$\begin{array}{r} 55 \\ \hline 25 \end{array} \quad \begin{array}{r} 57 \\ \hline 20 \end{array} \quad \begin{array}{r} 45 \\ \hline 16 \end{array} \quad 44 \quad \begin{array}{r} 49 \\ \hline 24 \end{array} \quad \begin{array}{r} 60 \\ \hline 27 \end{array} \quad \begin{array}{r} 58 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 50 \\ \hline 24 \end{array} \quad \begin{array}{r} 55 \\ \hline 19 \end{array} \quad \begin{array}{r} 48 \\ \hline 16 \end{array} \quad 44 \quad \begin{array}{r} 46 \\ \hline 22 \end{array} \quad \begin{array}{r} 57 \\ \hline 25 \end{array} \quad \begin{array}{r} 56 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 46 \\ \hline 23 \end{array} \quad \begin{array}{r} 50 \\ \hline 18 \end{array} \quad \begin{array}{r} 43 \\ \hline 16 \end{array} \quad 44 \quad \begin{array}{r} 48 \\ \hline 22 \end{array} \quad \begin{array}{r} 58 \\ \hline 25 \end{array} \quad \begin{array}{r} 57 \\ \hline 32 \end{array}$$

$$\begin{array}{r} 46 \\ \hline 25 \end{array} \quad \begin{array}{r} 52 \\ \hline 20 \end{array} \quad \begin{array}{r} 43 \\ \hline 18 \end{array} \quad 45 \quad \begin{array}{r} 51 \\ \hline 21 \end{array} \quad \begin{array}{r} 65 \\ \hline 24 \end{array} \quad \begin{array}{r} 60 \\ \hline 30 \end{array}$$

(6.0)

$$\begin{array}{r} +5.7 \\ \hline 50 \end{array} \quad \begin{array}{r} +4.8 \\ \hline 49 \end{array} \quad \begin{array}{r} 10 \\ \hline 41 \end{array} \quad \begin{array}{r} 78 \\ \hline 35 \end{array} \quad \begin{array}{r} 78 \\ \hline 25 \end{array} \quad \begin{array}{r} 57 \\ \hline 20 \end{array} \quad 57 \quad \begin{array}{r} 61 \\ \hline 19 \end{array} \quad \begin{array}{r} 77 \\ \hline 22 \end{array} \quad \begin{array}{r} 95 \\ \hline 50 \end{array}$$

(6.1)

$$\begin{array}{r} 85 \\ \hline 50 \end{array} \quad \begin{array}{r} 88 \\ \hline 35 \end{array} \quad \begin{array}{r} 88 \\ \hline 32 \end{array} \quad \begin{array}{r} 62 \\ \hline 20 \end{array} \quad 60 \quad \begin{array}{r} 62 \\ \hline 20 \end{array} \quad \begin{array}{r} 101 \\ \hline 29 \end{array} \quad \begin{array}{r} 120 \\ \hline 50 \end{array}$$

(2.8)

$$\begin{array}{r} 79 \\ \hline 53 \end{array} \quad \begin{array}{r} 60 \\ \hline 27 \end{array} \quad \begin{array}{r} 50 \\ \hline 21 \end{array} \quad 27 \quad \begin{array}{r} 30 \\ \hline 20 \end{array} \quad \begin{array}{r} 78 \\ \hline 29 \end{array} \quad \begin{array}{r} 95 \\ \hline 50 \end{array}$$

(2.8)

$$\begin{array}{r} 85 \\ \hline 50 \end{array} \quad \begin{array}{r} 80 \\ \hline 31 \end{array} \quad \begin{array}{r} 31 \\ \hline 21 \end{array} \quad 30 \quad \begin{array}{r} 30 \\ \hline 20 \end{array} \quad \begin{array}{r} 87 \\ \hline 31 \end{array} \quad \begin{array}{r} 93 \\ \hline 42 \end{array} \quad \begin{array}{r} 126 \\ \hline 45 \end{array} \quad \begin{array}{r} 125 \\ \hline 48 \end{array} \quad \begin{array}{r} 90 \\ \hline 44 \end{array} \quad \begin{array}{r} 90 \\ \hline 50 \end{array}$$

+15309 H.D.

(3.0)

$$\begin{array}{r} 104 \\ \hline 50 \end{array} \quad \begin{array}{r} 101 \\ \hline 33 \end{array} \quad \begin{array}{r} 38 \\ \hline 20 \end{array} \quad 32 \quad \begin{array}{r} 32 \\ \hline 19 \end{array} \quad \begin{array}{r} 101 \\ \hline 30 \end{array} \quad \begin{array}{r} 107 \\ \hline 43 \end{array} \quad \begin{array}{r} 121 \\ \hline 45 \end{array} \quad \begin{array}{r} 124 \\ \hline 44 \end{array} \quad \begin{array}{r} 102 \\ \hline 49 \end{array} \quad \begin{array}{r} 102 \\ \hline 50 \end{array}$$

(3.1)

$$\begin{array}{r} 105 \\ \hline 50 \end{array} \quad \begin{array}{r} 105 \\ \hline 30 \end{array} \quad \begin{array}{r} 40 \\ \hline 20 \end{array} \quad 37 \quad \begin{array}{r} 37 \\ \hline 19 \end{array} \quad \begin{array}{r} 112 \\ \hline 33 \end{array} \quad \begin{array}{r} 110 \\ \hline 38 \end{array} \quad \begin{array}{r} 101 \\ \hline 40 \end{array} \quad \begin{array}{r} 108 \\ \hline 45 \end{array} \quad \begin{array}{r} 122 \\ \hline 42 \end{array} \quad \begin{array}{r} 122 \\ \hline 48 \end{array} \quad \begin{array}{r} 110 \\ \hline 49 \end{array} \quad \begin{array}{r} 109 \\ \hline 50 \end{array}$$

Sta

F

895.03.

337

91.8

+50

91.7

338

91.6

+50

91.6

339

91.7

+50

92.0

340.

T.P.

7.34

900.24.

213

892.90.

BM

346

896.78.

896.79

3.2

$\frac{10.0}{50}$	$\frac{10.4}{31}$	$\frac{11.4}{20}$	$\frac{3.8}{-}$	$\frac{3.6}{19}$	$\frac{10.8}{33}$	$\frac{11.5}{44}$	$\frac{12.5}{45}$	$\frac{12.5}{48}$	$\frac{11.8}{49}$	$\frac{11.7}{50}$
-------------------	-------------------	-------------------	-----------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

3.3

$\frac{10.6}{50}$	$\frac{10.6}{41}$	$\frac{11.0}{40}$	$\frac{10.3}{30}$	$\frac{13}{20}$	$\frac{4.0}{-}$	$\frac{4.2}{19}$	$\frac{9.2}{28}$	$\frac{11.2}{34}$	$\frac{11.7}{46}$	$\frac{12.2}{47}$	$\frac{12.5}{48}$	$\frac{11.7}{50}$
-------------------	-------------------	-------------------	-------------------	-----------------	-----------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	-------------------

3.4

$\frac{11.0}{50}$	$\frac{12.0}{37}$	$\frac{9.0}{29}$	$\frac{4.0}{21}$	$\frac{3.8}{-}$	$\frac{4.0}{18}$	$\frac{2.7}{26}$	$\frac{9.8}{36}$	$\frac{12.2}{39}$	$\frac{13.0}{48}$	$\frac{11.6}{49}$	$\frac{11.6}{50}$
	$\frac{11.1}{50}$	$\frac{10.4}{33}$	$\frac{4.0}{20}$	$\frac{3.4}{-}$	$\frac{4.0}{19}$	$\frac{10.2}{29}$	$\frac{11.2}{37}$	$\frac{11.2}{50}$			

3.3

$\frac{9.7}{50}$	$\frac{9.7}{46}$	$\frac{10.8}{45}$	$\frac{10.6}{40}$	$\frac{10.2}{39}$	$\frac{9.7}{33}$	$\frac{3.8}{21}$	$\frac{3.4}{-}$	$\frac{3.6}{19}$	$\frac{10.2}{30}$	$\frac{11.5}{37}$	$\frac{11.7}{50}$
------------------	------------------	-------------------	-------------------	-------------------	------------------	------------------	-----------------	------------------	-------------------	-------------------	-------------------

3.0

$\frac{9.1}{45}$	$\frac{10.4}{44}$	$\frac{10.1}{38}$	$\frac{9.5}{37}$	$\frac{9.1}{33}$	$\frac{3.3}{21}$	$\frac{3.3}{-}$	$\frac{3.7}{19}$	$\frac{10.8}{33}$	$\frac{11.3}{38}$	$\frac{11.8}{50}$
------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	------------------	-------------------	-------------------	-------------------

$\frac{7.3}{50}$	$\frac{7.8}{45}$	$\frac{10.2}{43}$	$\frac{9.4}{38}$	$\frac{8.7}{36}$	$\frac{8.2}{32}$	$\frac{3.0}{20}$	$\frac{2.8}{-}$	$\frac{2.8}{20}$	$\frac{10.1}{35}$	$\frac{11.1}{50}$
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split in F-Cor R4029 243+20

Sta	+	HI	-	Elev	
B.M.	348	914.18		910.68	
394+50				907.7	6.5
395				08.0	6.2
+30				08.3	5.9
+50				08.7	5.5
396				09.1	5.1
+50				09.8	4.4
397				10.5	3.7
+50				11.0	3.2
398				11.5	2.7
T.P.	832	921.73	0.77	913.41	
+50				11.9	9.8
399				12.2	9.5

spike in 12" Poplar 200 LHS 398410

$\frac{128}{50}$ $\frac{146}{56}$ $\frac{110}{25}$ $\frac{61}{18}$ 23 $\frac{60}{21}$ $\frac{133}{25}$ $\frac{134}{50}$

$\frac{115}{50}$ $\frac{130}{35}$ $\frac{60}{20}$ 60 $\frac{55}{20}$ $\frac{123}{32}$ $\frac{133}{50}$

$\frac{100}{50}$ $\frac{103}{38}$ $\frac{113}{36}$ $\frac{122}{34}$ $\frac{110}{33}$ $\frac{55}{21}$ 57 $\frac{57}{20}$ $\frac{102}{28}$ $\frac{114}{50}$

$\frac{94}{50}$ $\frac{92}{36}$ $\frac{106}{32}$ $\frac{51}{26}$ 55 $\frac{56}{20}$ $\frac{91}{27}$ $\frac{102}{50}$

$\frac{70}{50}$ $\frac{67}{31}$ $\frac{83}{23}$ $\frac{48}{20}$ 50 $\frac{50}{20}$ $\frac{78}{26}$ $\frac{82}{50}$

$\frac{62}{50}$ $\frac{64}{30}$ $\frac{72}{30}$ $\frac{70}{26}$ $\frac{43}{20}$ 44 $\frac{48}{19}$ $\frac{60}{24}$ $\frac{65}{25}$ $\frac{65}{28}$ $\frac{58}{29}$ $\frac{60}{50}$

$\frac{60}{50}$ $\frac{58}{31}$ $\frac{66}{29}$ $\frac{64}{25}$ $\frac{42}{20}$ 40 $\frac{40}{20}$ $\frac{62}{25}$ $\frac{68}{28}$ $\frac{42}{31}$ $\frac{35}{50}$

$\frac{44}{50}$ $\frac{40}{30}$ $\frac{57}{29}$ $\frac{57}{24}$ $\frac{36}{20}$ 35 $\frac{35}{19}$ $\frac{50}{22}$ $\frac{50}{29}$ $\frac{22}{34}$ $\frac{18}{35}$ $\frac{15}{50}$

$\frac{20}{50}$ $\frac{36}{34}$ $\frac{54}{30}$ $\frac{48}{23}$ $\frac{32}{20}$ 28 $\frac{28}{17}$ $\frac{40}{21}$ $\frac{40}{30}$ $\frac{07}{34}$ $\frac{02}{50}$

$\frac{88}{50}$ $\frac{84}{37}$ $\frac{88}{32}$ $\frac{124}{30}$ $\frac{117}{22}$ $\frac{103}{21}$ 77 $\frac{94}{26}$ $\frac{114}{23}$ $\frac{112}{29}$ $\frac{74}{35}$ $\frac{70}{37}$ $\frac{70}{50}$

$\frac{75}{50}$ $\frac{70}{37}$ $\frac{115}{29}$ $\frac{120}{24}$ $\frac{102}{21}$ 76 $\frac{95}{21}$ $\frac{113}{25}$ $\frac{112}{30}$ $\frac{65}{37}$ $\frac{65}{50}$

921.73.

399+50

12.4

9.3

400

12.6

9.1

+50

12.6

9.1

401

12.6

9.1

T.P

2.50

918.75.

548

716.25.

+50

12.5

6.3

402

12.3

6.5

+50

12.0

6.8

403

11.7

7.1

+50

11.2

7.6

404

10.7

8.1

+17

10.5

8.3

+50

10.2

8.6

$\frac{53}{50}$	$\frac{50}{40}$	$\frac{58}{37}$	$\frac{112}{30}$	$\frac{112}{23}$	$\frac{100}{20}$	97	$\frac{95}{19}$	$\frac{110}{24}$	$\frac{106}{30}$	$\frac{58}{36}$	$\frac{60}{50}$
-----------------	-----------------	-----------------	------------------	------------------	------------------	----	-----------------	------------------	------------------	-----------------	-----------------

$\frac{37}{50}$	$\frac{35}{42}$	$\frac{45}{39}$	$\frac{108}{29}$	$\frac{110}{24}$	$\frac{92}{20}$	92	$\frac{93}{20}$	$\frac{118}{24}$	$\frac{102}{31}$	$\frac{55}{37}$	$\frac{55}{50}$
-----------------	-----------------	-----------------	------------------	------------------	-----------------	----	-----------------	------------------	------------------	-----------------	-----------------

$\frac{36}{50}$	$\frac{32}{42}$	$\frac{42}{40}$	$\frac{110}{30}$	$\frac{110}{24}$	$\frac{91}{20}$	92	$\frac{94}{21}$	$\frac{112}{25}$	$\frac{108}{30}$	$\frac{50}{39}$	$\frac{51}{50}$
-----------------	-----------------	-----------------	------------------	------------------	-----------------	----	-----------------	------------------	------------------	-----------------	-----------------

$\frac{20}{50}$	$\frac{25}{44}$	$\frac{35}{40}$	$\frac{107}{29}$	$\frac{107}{24}$	$\frac{93}{21}$	90	$\frac{90}{20}$	$\frac{110}{24}$	$\frac{108}{30}$	$\frac{53}{37}$	$\frac{47}{44}$	$\frac{54}{50}$
-----------------	-----------------	-----------------	------------------	------------------	-----------------	----	-----------------	------------------	------------------	-----------------	-----------------	-----------------

$\frac{25}{50}$	$\frac{20}{40}$	$\frac{30}{36}$	$\frac{84}{29}$	$\frac{85}{24}$	$\frac{65}{21}$	61	$\frac{60}{21}$	$\frac{80}{25}$	$\frac{78}{29}$	$\frac{32}{36}$	$\frac{28}{37}$	$\frac{29}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{22}{50}$	$\frac{40}{37}$	$\frac{42}{24}$	$\frac{83}{29}$	$\frac{84}{23}$	$\frac{66}{20}$	64	$\frac{65}{21}$	$\frac{83}{24}$	$\frac{85}{29}$	$\frac{38}{36}$	$\frac{33}{38}$	$\frac{35}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{60}{50}$	$\frac{56}{35}$	$\frac{60}{32}$	$\frac{85}{28}$	$\frac{88}{28}$	$\frac{67}{19}$	68	$\frac{67}{21}$	$\frac{88}{26}$	$\frac{88}{29}$	$\frac{60}{34}$	$\frac{55}{36}$	$\frac{55}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{76}{50}$	$\frac{72}{33}$	$\frac{80}{29}$	$\frac{86}{28}$	$\frac{88}{23}$	$\frac{73}{20}$	72	$\frac{73}{21}$	$\frac{90}{24}$	$\frac{95}{30}$	$\frac{72}{34}$	$\frac{70}{35}$	$\frac{71}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{77}{50}$	$\frac{71}{33}$	$\frac{78}{30}$	$\frac{88}{29}$	$\frac{88}{25}$	$\frac{74}{22}$	76	$\frac{76}{21}$	$\frac{91}{24}$	$\frac{90}{30}$	$\frac{71}{33}$	$\frac{77}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{84}{50}$	$\frac{28}{34}$	$\frac{88}{30}$	$\frac{95}{29}$	$\frac{95}{25}$	$\frac{77}{22}$	81	$\frac{80}{26}$	$\frac{96}{22}$	$\frac{101}{28}$	$\frac{96}{29}$	$\frac{103}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	------------------	-----------------	------------------

$\frac{85}{50}$	$\frac{83}{34}$	$\frac{98}{30}$	$\frac{96}{26}$	$\frac{80}{23}$	83	$\frac{87}{19}$	$\frac{101}{21}$	$\frac{103}{29}$	$\frac{105}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	------------------	------------------	------------------

$\frac{85}{50}$	$\frac{95}{35}$	$\frac{107}{28}$	$\frac{95}{23}$	$\frac{84}{21}$	88	$\frac{93}{20}$	$\frac{107}{23}$	$\frac{113}{32}$	$\frac{113}{50}$
-----------------	-----------------	------------------	-----------------	-----------------	----	-----------------	------------------	------------------	------------------

718.75.

405				09.7	9.1
+50				09.2	9.6
406				08.7	10.1
T.P	2.09	910.84.	10.00	908.75.	
+50				08.2	2.6
407				07.7	3.1
+50				07.2	3.6
408				06.7	4.1
+50				06.2	4.6
B.M.			4.45	906.39.	= 906.36
409				05.7	5.1
+50				05.2	5.6
410				04.7	6.1
+50				04.2	6.6

$$\frac{112}{50} \quad \frac{110}{26} \quad \frac{87}{21} \quad \frac{94}{21} \quad \frac{96}{20} \quad \frac{115}{24} \quad \frac{115}{27} \quad \frac{110}{50}$$

$$\frac{114}{50} \quad \frac{117}{26} \quad \frac{90}{20} \quad \frac{98}{21} \quad \frac{102}{20} \quad \frac{117}{23} \quad \frac{117}{50}$$

$$\frac{122}{50} \quad \frac{122}{26} \quad \frac{95}{20} \quad \frac{102}{21} \quad \frac{105}{20} \quad \frac{122}{23} \quad \frac{120}{50}$$

$$\frac{52}{50} \quad \frac{47}{25} \quad \frac{23}{20} \quad \frac{28}{21} \quad \frac{33}{20} \quad \frac{47}{23} \quad \frac{47}{28} \quad \frac{41}{50}$$

$$\frac{55}{50} \quad \frac{54}{25} \quad \frac{25}{20} \quad \frac{32}{21} \quad \frac{37}{20} \quad \frac{53}{23} \quad \frac{52}{50}$$

$$\frac{52}{50} \quad \frac{52}{26} \quad \frac{31}{21} \quad \frac{35}{21} \quad \frac{44}{20} \quad \frac{52}{24} \quad \frac{55}{28} \quad \frac{55}{50}$$

$$\frac{52}{50} \quad \frac{54}{25} \quad \frac{34}{19} \quad \frac{41}{21} \quad \frac{46}{20} \quad \frac{65}{25} \quad \frac{65}{28} \quad \frac{55}{31} \quad \frac{48}{50}$$

$$\frac{52}{50} \quad \frac{51}{31} \quad \frac{60}{29} \quad \frac{62}{25} \quad \frac{45}{20} \quad \frac{45}{21} \quad \frac{46}{79} \quad \frac{68}{23} \quad \frac{70}{30} \quad \frac{62}{56} \quad \frac{60}{50}$$

Top Port Point of PI 446+00 Lt 512 408+20

$$\frac{56}{50} \quad \frac{51}{37} \quad \frac{58}{35} \quad \frac{70}{23} \quad \frac{70}{25} \quad \frac{51}{21} \quad \frac{51}{21} \quad \frac{50}{19} \quad \frac{73}{24} \quad \frac{74}{33} \quad \frac{64}{34} \quad \frac{66}{50}$$

$$\frac{52}{50} \quad \frac{54}{37} \quad \frac{78}{33} \quad \frac{77}{24} \quad \frac{57}{20} \quad \frac{56}{21} \quad \frac{58}{20} \quad \frac{80}{25} \quad \frac{85}{32} \quad \frac{70}{34} \quad \frac{68}{50}$$

$$\frac{50}{50} \quad \frac{53}{41} \quad \frac{57}{37} \quad \frac{80}{34} \quad \frac{80}{23} \quad \frac{63}{20} \quad \frac{60}{20} \quad \frac{63}{20} \quad \frac{88}{25} \quad \frac{91}{33} \quad \frac{72}{35} \quad \frac{63}{37} \quad \frac{65}{50}$$

$$\frac{56}{50} \quad \frac{60}{38} \quad \frac{88}{34} \quad \frac{85}{23} \quad \frac{66}{19} \quad \frac{68}{20} \quad \frac{66}{19} \quad \frac{95}{24} \quad \frac{97}{32} \quad \frac{65}{36} \quad \frac{55}{39} \quad \frac{54}{50}$$

Sta

K

HI

910.84.

+11

03.7

7.1

+50

03.2

7.6

+70

03.0

7.8

+12

02.7

8.1

+41

02.3

8.5

+13

01.7

9.1

+11

01.6

9.2

T.P

5.79

908.03

8.60

902.4

+50

01.2

6.8

+14

900.7

7.3

+50

00.2

7.8

+15

899.7

8.3

+50

99.2

8.8

$\frac{46}{50}$ $\frac{52}{38}$ $\frac{90}{34}$ $\frac{90}{24}$ $\frac{70}{20}$ 70 $\frac{74}{21}$ $\frac{98}{25}$ $\frac{100}{32}$ $\frac{57}{38}$ $\frac{53}{41}$ $\frac{57}{50}$

$\frac{48}{50}$ $\frac{50}{43}$ $\frac{54}{40}$ $\frac{98}{34}$ $\frac{98}{24}$ $\frac{77}{20}$ 77 $\frac{77}{19}$ $\frac{106}{24}$ $\frac{107}{32}$ $\frac{74}{37}$ $\frac{70}{39}$ $\frac{68}{50}$

$\frac{50}{50}$ $\frac{54}{43}$ $\frac{60}{40}$ $\frac{95}{34}$ $\frac{100}{23}$ $\frac{80}{20}$ 78 $\frac{78}{19}$ $\frac{111}{25}$ $\frac{110}{33}$ $\frac{77}{37}$ $\frac{70}{41}$ $\frac{72}{50}$

$\frac{53}{50}$ $\frac{53}{43}$ $\frac{60}{40}$ $\frac{100}{34}$ $\frac{105}{24}$ $\frac{81}{20}$ 80 $\frac{80}{20}$ $\frac{111}{25}$ $\frac{115}{32}$ $\frac{67}{38}$ $\frac{61}{41}$ $\frac{61}{50}$

$\frac{47}{50}$ $\frac{53}{41}$ $\frac{104}{53}$ $\frac{106}{23}$ $\frac{88}{20}$ 85 $\frac{88}{20}$ $\frac{115}{25}$ $\frac{110}{33}$ $\frac{57}{41}$ $\frac{52}{44}$ $\frac{52}{50}$

$\frac{31}{50}$ $\frac{40}{44}$ $\frac{108}{35}$ $\frac{111}{24}$ $\frac{93}{21}$ 90 $\frac{90}{20}$ $\frac{122}{23}$ $\frac{118}{32}$ $\frac{60}{41}$ $\frac{53}{44}$ $\frac{55}{50}$

$\frac{36}{50}$ $\frac{38}{44}$ $\frac{108}{34}$ $\frac{114}{24}$ $\frac{94}{21}$ 92 $\frac{92}{20}$ $\frac{122}{24}$ $\frac{122}{33}$ $\frac{60}{41}$ $\frac{55}{45}$ $\frac{57}{50}$

$\frac{16}{50}$ $\frac{13}{47}$ $\frac{18}{44}$ $\frac{82}{34}$ $\frac{86}{33}$ $\frac{66}{20}$ 66 $\frac{72}{20}$ $\frac{97}{25}$ $\frac{97}{34}$ $\frac{41}{40}$ $\frac{35}{44}$ $\frac{38}{50}$

$\frac{34}{50}$ $\frac{40}{42}$ $\frac{85}{36}$ $\frac{98}{29}$ $\frac{94}{24}$ $\frac{73}{20}$ 75 $\frac{77}{19}$ $\frac{100}{24}$ $\frac{112}{29}$ $\frac{103}{33}$ $\frac{45}{41}$ $\frac{38}{44}$ $\frac{43}{50}$

$\frac{53}{50}$ $\frac{56}{40}$ $\frac{100}{35}$ $\frac{100}{30}$ $\frac{92}{23}$ $\frac{77}{20}$ 81 $\frac{85}{19}$ $\frac{100}{22}$ $\frac{107}{29}$ $\frac{105}{33}$ $\frac{58}{39}$ $\frac{55}{41}$ $\frac{56}{50}$

$\frac{67}{50}$ $\frac{72}{39}$ $\frac{102}{25}$ $\frac{107}{27}$ $\frac{106}{23}$ $\frac{84}{19}$ 87 $\frac{86}{19}$ $\frac{92}{24}$ $\frac{112}{28}$ $\frac{108}{32}$ $\frac{83}{36}$ $\frac{76}{41}$ $\frac{78}{50}$

$\frac{80}{50}$ $\frac{86}{38}$ $\frac{105}{36}$ $\frac{113}{30}$ $\frac{113}{22}$ $\frac{90}{18}$ 90 $\frac{94}{19}$ $\frac{113}{23}$ $\frac{118}{28}$ $\frac{118}{32}$ $\frac{104}{35}$ $\frac{100}{39}$ $\frac{104}{50}$

908.03.

416

98.7

9.3

T.P.

527

908.67.

963

898.40.

+50

98.2

5.5

417

97.7

6.0

+50

97.2

6.5

418

96.7

7.0

T.P.

432

900.20.

779

895.88.

+50

96.2

4.0

419

95.7

4.5

+62

95.3

4.9

+20

95.1

5.1

+50

95.1

5.1

B.M.

6.75

901.29.

565

894.55.

894.54

421

95.3

6.0

+60

95.7

5.6

$$\frac{78}{50} \quad \frac{92}{37} \quad \frac{123}{33} \quad \frac{125}{27} \quad \frac{125}{23} \quad \frac{93}{19} \quad 94 \quad \frac{95}{21} \quad \frac{115}{34} \quad \frac{133}{50}$$

$$\frac{65}{50} \quad \frac{74}{36} \quad \frac{92}{33} \quad \frac{95}{26} \quad \frac{55}{20} \quad 56 \quad \frac{54}{20} \quad \frac{96}{27} \quad \frac{115}{50}$$

$$\frac{92}{50} \quad \frac{102}{37} \quad \frac{108}{36} \quad \frac{104}{30} \quad \frac{90}{25} \quad \frac{60}{20} \quad 60 \quad \frac{62}{20} \quad \frac{120}{30} \quad \frac{133}{50}$$

$$\frac{115}{50} \quad \frac{120}{41} \quad \frac{125}{36} \quad \frac{126}{26} \quad \frac{65}{20} \quad 65 \quad \frac{70}{20} \quad \frac{130}{28} \quad \frac{133}{30} \quad \frac{140}{50}$$

$$\frac{132}{50} \quad \frac{130}{41} \quad \frac{135}{40} \quad \frac{133}{37} \quad \frac{128}{32} \quad \frac{74}{20} \quad 74 \quad \frac{77}{20} \quad \frac{133}{31} \quad \frac{142}{39} \quad \frac{142}{50}$$

$$\frac{94}{50} \quad \frac{74}{39} \quad \frac{101}{38} \quad \frac{92}{29} \quad \frac{43}{19} \quad 43 \quad \frac{46}{20} \quad \frac{90}{28} \quad \frac{110}{32} \quad \frac{107}{50}$$

$$\frac{96}{50} \quad \frac{90}{36} \quad \frac{88}{28} \quad \frac{46}{20} \quad 46 \quad \frac{46}{20} \quad \frac{90}{28} \quad \frac{100}{50}$$

$$\frac{90}{50} \quad \frac{85}{36} \quad \frac{90}{35} \quad \frac{85}{27} \quad \frac{50}{20} \quad 50 \quad \frac{50}{20} \quad \frac{85}{26} \quad \frac{96}{32} \quad \frac{100}{50}$$

$$\frac{74}{50} \quad \frac{74}{33} \quad \frac{82}{34} \quad \frac{82}{28} \quad \frac{82}{23} \quad \frac{52}{20} \quad 54 \quad \frac{52}{19} \quad \frac{74}{24} \quad \frac{88}{50}$$

$$\frac{61}{50} \quad \frac{61}{30} \quad \frac{75}{28} \quad \frac{72}{23} \quad \frac{55}{20} \quad 54 \quad \frac{54}{20} \quad \frac{72}{24} \quad \frac{80}{28} \quad \frac{70}{31} \quad \frac{78}{50}$$

Spills in T.R. 40' R + 54, 42 + 40

$$\frac{61}{50} \quad \frac{66}{31} \quad \frac{80}{27} \quad \frac{78}{23} \quad \frac{60}{20} \quad 64 \quad \frac{65}{20} \quad \frac{87}{26} \quad \frac{87}{33} \quad \frac{82}{35} \quad \frac{88}{50}$$

$$\frac{74}{50} \quad \frac{86}{33} \quad \frac{94}{32} \quad \frac{70}{20} \quad \frac{61}{20} \quad 57 \quad \frac{57}{21} \quad \frac{107}{31} \quad \frac{113}{50}$$

901.29.

422

95.9

5.4

+50

96.2

5.1

423

96.4

4.9

+50

96.4

4.9

424

96.2

5.1

+24

96.1

5.2

B.M.

6.75

894.54.

$\frac{27}{50}$	$\frac{93}{35}$	$\frac{100}{33}$	$\frac{100}{27}$	$\frac{56}{20}$	$\frac{55}{20}$		$\frac{54}{21}$	$\frac{11.4}{33}$	$\frac{11.4}{50}$
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$\frac{27}{50}$	$\frac{88}{37}$	$\frac{97}{36}$	$\frac{100}{32}$	$\frac{88}{25}$	$\frac{53}{20}$	$\frac{51}{20}$	$\frac{52}{22}$	$\frac{103}{29}$	$\frac{11.8}{43}$	$\frac{11.8}{50}$
-----------------	-----------------	-----------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	-------------------	-------------------

$\frac{66}{50}$	$\frac{80}{35}$	$\frac{90}{32}$	$\frac{90}{26}$	$\frac{48}{20}$	48	$\frac{48}{22}$	$\frac{100}{29}$	$\frac{11.5}{32}$	$\frac{11.5}{50}$
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Clev Acc

$\frac{44}{50}$	$\frac{40}{41}$	$\frac{72}{52}$	$\frac{68}{25}$	$\frac{50}{21}$	48	$\frac{52}{27}$	$\frac{9.5}{33}$	$\frac{11.2}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	------------------	-------------------

$\frac{48}{50}$	$\frac{46}{28}$	50	$\frac{50}{35}$	$\frac{93}{43}$	$\frac{100}{50}$
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$\frac{60}{50}$	$\frac{48}{33}$	52	$\frac{50}{29}$	$\frac{52}{39}$	$\frac{97}{46}$	$\frac{101}{50}$
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2/pike in top 40' at sta 424-400

Sta	+	HI	-	Elev	
B.M.	7.27	903.08		895.81	
456+50				97.0	6.1
457				97.5	5.6
+50				98.1	5.0
458				98.7	4.4
T.P.	7.75	907.69	3.14	899.94	
+50				99.4	8.3
459				900.2	7.5
+70				01.3	6.4
460				01.8	5.9
+50				02.6	5.1
461				03.4	4.3
+50				04.2	3.5

2 W Cor Head Wall Cattle Pass

$\frac{11.7}{50}$ $\frac{12.0}{31}$ $\frac{6.0}{20}$ 5.5 $\frac{5.8}{20}$ $\frac{13.3}{34}$ $\frac{13.8}{50}$

$\frac{9.0}{50}$ $\frac{9.3}{27}$ $\frac{5.4}{20}$ 5.0 $\frac{5.3}{21}$ $\frac{11.4}{32}$ $\frac{12.4}{50}$

$\frac{3.8}{50}$ $\frac{4.2}{35}$ $\frac{7.5}{32}$ $\frac{7.5}{27}$ $\frac{5.0}{21}$ 4.5 $\frac{4.9}{20}$ $\frac{10.7}{31}$ $\frac{11.5}{50}$

$\frac{2.0}{50}$ $\frac{1.4}{40}$ $\frac{2.0}{38}$ $\frac{6.5}{32}$ $\frac{6.3}{25}$ $\frac{4.2}{20}$ 4.0 $\frac{4.3}{21}$ $\frac{8.0}{27}$ $\frac{11.2}{50}$

$\frac{3.9}{50}$ $\frac{4.9}{41}$ $\frac{5.2}{40}$ $\frac{10.0}{34}$ $\frac{10.3}{26}$ $\frac{8.0}{20}$ 8.1 $\frac{8.3}{20}$ $\frac{11.5}{26}$ $\frac{13.7}{50}$

$\frac{4.5}{50}$ $\frac{5.2}{39}$ $\frac{5.5}{37}$ $\frac{9.5}{31}$ $\frac{9.0}{24}$ $\frac{7.2}{20}$ 7.2 $\frac{7.3}{20}$ $\frac{10.0}{25}$ $\frac{11.7}{50}$

$\frac{5.5}{50}$ $\frac{6.6}{36}$ $\frac{6.8}{34}$ $\frac{8.7}{31}$ $\frac{8.7}{25}$ $\frac{6.3}{20}$ 6.3 $\frac{6.5}{20}$ $\frac{10.0}{26}$ $\frac{9.5}{50}$

$\frac{5.3}{50}$ $\frac{6.3}{35}$ $\frac{6.6}{33}$ $\frac{8.1}{31}$ $\frac{8.1}{25}$ $\frac{6.0}{20}$ 5.8 $\frac{5.9}{20}$ $\frac{8.3}{26}$ $\frac{8.6}{30}$ $\frac{8.0}{31}$ $\frac{8.0}{50}$

$\frac{4.1}{50}$ $\frac{4.8}{35}$ $\frac{5.0}{34}$ $\frac{7.0}{31}$ $\frac{7.2}{26}$ $\frac{4.9}{20}$ 4.9 $\frac{5.2}{20}$ $\frac{7.3}{25}$ $\frac{7.7}{30}$ $\frac{5.5}{34}$ $\frac{5.1}{35}$ $\frac{5.3}{50}$

$\frac{2.8}{50}$ $\frac{3.2}{37}$ $\frac{3.5}{35}$ $\frac{6.4}{31}$ $\frac{6.0}{25}$ $\frac{4.2}{20}$ 4.1 $\frac{4.3}{20}$ $\frac{6.4}{26}$ $\frac{6.7}{31}$ $\frac{3.3}{35}$ $\frac{3.2}{38}$ $\frac{3.6}{50}$

$\frac{2.8}{50}$ $\frac{3.1}{36}$ $\frac{3.3}{34}$ $\frac{5.3}{32}$ $\frac{5.5}{25}$ $\frac{3.5}{20}$ 3.4 $\frac{3.5}{20}$ $\frac{5.0}{24}$ $\frac{5.6}{30}$ $\frac{2.6}{35}$ $\frac{3.0}{50}$

Sta.	+	H.I.	-	Elev.	
		907.69			
462				05.0	2.7
T.P.	10.35	915.43 [✓]	2.61	905.08 [✓]	
	+50			05.8	9.6
463				06.6	8.8
	+50			07.4	8.0
464				08.2	7.2
	+50			08.9	6.5
465				09.6	5.8
	+50			10.1	5.3
466				10.4	5.0
	+50			10.6	4.8
467				10.9	4.5

$$\frac{2.3}{50} \quad \frac{2.3}{35} \quad \frac{2.5}{34} \quad \frac{4.4}{30} \quad \frac{4.4}{24} \quad \frac{2.6}{20} \quad 2.6 \quad \frac{2.6}{20} \quad \frac{4.3}{26} \quad \frac{4.6}{30} \quad \frac{2.1}{35} \quad \frac{3.0}{37} \quad \frac{2.3}{50}$$

$$\frac{6.5}{50} \quad \frac{6.6}{40} \quad \frac{6.2}{38} \quad \frac{11.4}{31} \quad \frac{11.3}{25} \quad \frac{9.4}{20} \quad 9.3 \quad \frac{9.5}{20} \quad \frac{11.0}{26} \quad \frac{11.4}{31} \quad \frac{7.4}{37} \quad \frac{7.4}{39} \quad \frac{8.0}{50}$$

$$\frac{2.7}{50} \quad \frac{3.7}{43} \quad \frac{4.1}{41} \quad \frac{10.1}{32} \quad \frac{10.0}{24} \quad \frac{8.6}{20} \quad 8.6 \quad \frac{8.6}{20} \quad \frac{10.0}{26} \quad \frac{10.3}{31} \quad \frac{6.3}{37} \quad \frac{6.3}{40} \quad \frac{7.3}{50}$$

$$\frac{3.0}{50} \quad \frac{3.0}{41} \quad \frac{9.2}{32} \quad \frac{9.2}{26} \quad \frac{7.7}{20} \quad 7.6 \quad \frac{7.6}{20} \quad \frac{9.0}{25} \quad \frac{9.3}{29} \quad \frac{6.1}{36} \quad \frac{6.0}{38} \quad \frac{7.4}{50}$$

$$\frac{3.5}{50} \quad \frac{3.5}{41} \quad \frac{3.7}{40} \quad \frac{8.5}{31} \quad \frac{8.5}{25} \quad \frac{7.2}{20} \quad 7.1 \quad \frac{7.1}{20} \quad \frac{8.5}{25} \quad \frac{8.8}{30} \quad \frac{6.7}{35} \quad \frac{6.6}{36} \quad \frac{8.2}{50}$$

$$\frac{4.2}{50} \quad \frac{3.8}{39} \quad \frac{4.2}{37} \quad \frac{8.0}{30} \quad \frac{7.6}{24} \quad \frac{6.3}{20} \quad 6.2 \quad \frac{6.4}{20} \quad \frac{8.1}{25} \quad \frac{8.2}{30} \quad \frac{7.3}{32} \quad \frac{7.3}{33} \quad \frac{9.2}{50}$$

$$\frac{3.7}{50} \quad \frac{3.6}{38} \quad \frac{3.7}{37} \quad \frac{7.0}{30} \quad \frac{6.8}{24} \quad \frac{5.7}{20} \quad 5.6 \quad \frac{5.7}{20} \quad \frac{7.3}{24} \quad \frac{7.8}{30} \quad \frac{7.3}{31} \quad \frac{9.5}{50}$$

$$\frac{2.7}{50} \quad \frac{2.6}{39} \quad \frac{2.8}{37} \quad \frac{6.5}{30} \quad \frac{6.5}{24} \quad \frac{5.3}{20} \quad 5.0 \quad \frac{5.1}{20} \quad \frac{6.2}{24} \quad \frac{7.2}{31} \quad \frac{6.8}{32} \quad \frac{6.4}{33} \quad \frac{7.6}{50}$$

$$\frac{2.4}{50} \quad \frac{2.4}{38} \quad \frac{6.1}{31} \quad \frac{6.0}{24} \quad \frac{5.0}{20} \quad 4.6 \quad \frac{4.6}{20} \quad \frac{6.0}{25} \quad \frac{6.2}{30} \quad \frac{4.1}{34} \quad \frac{4.7}{50}$$

$$\frac{1.4}{50} \quad \frac{1.5}{38} \quad \frac{6.2}{30} \quad \frac{5.8}{24} \quad \frac{4.7}{20} \quad 4.5 \quad \frac{4.0}{20} \quad \frac{5.8}{24} \quad \frac{6.1}{30} \quad \frac{2.2}{37} \quad \frac{2.0}{39} \quad \frac{2.3}{50}$$

$$\frac{1.5}{50} \quad \frac{1.3}{40} \quad \frac{1.4}{38} \quad \frac{6.0}{30} \quad \frac{5.5}{23} \quad \frac{4.5}{20} \quad 4.4 \quad \frac{4.4}{20} \quad \frac{5.5}{24} \quad \frac{6.0}{30} \quad \frac{0.2}{41} \quad \frac{0.0}{42} \quad \frac{0.1}{50}$$

915.43

Sta.	+	H.I.	-	Elev	
T.P.B.M.	1.15	915.41	1.11	914.32	914.26
467+50				10.9	4.5
468				10.8	4.6
+50				10.6	4.8
469				10.5	4.9
+50				10.3	5.1
470				10.2	5.2
+50				10.0	5.4
471				09.9	5.5
+50				09.7	5.7
472				09.6	5.8
+50				09.4	6.0

$$\frac{2.4}{50} \quad \frac{2.1}{37} \quad \frac{6.0}{29} \quad \frac{5.8}{23} \quad \frac{4.6}{20} \quad 4.4 \quad \frac{4.4}{20} \quad \frac{5.5}{24} \quad \frac{5.8}{30} \quad \frac{0.5}{40} \quad \frac{0.3}{50}$$

$$\frac{3.4}{50} \quad \frac{3.7}{36} \quad \frac{6.0}{30} \quad \frac{5.8}{25} \quad \frac{4.4}{20} \quad 4.4 \quad \frac{4.4}{20} \quad \frac{5.8}{25} \quad \frac{6.2}{29} \quad \frac{1.0}{39} \quad \frac{0.7}{50}$$

$$\frac{5.5}{50} \quad \frac{5.0}{33} \quad \frac{7.0}{30} \quad \frac{6.7}{25} \quad \frac{4.5}{19} \quad 4.4 \quad \frac{4.4}{20} \quad \frac{6.0}{26} \quad \frac{6.2}{33} \quad \frac{2.2}{29} \quad \frac{1.7}{50}$$

$$\frac{6.3}{50} \quad \frac{5.4}{33} \quad \frac{7.0}{30} \quad \frac{6.7}{24} \quad \frac{4.8}{20} \quad 4.5 \quad \frac{4.6}{20} \quad \frac{6.7}{26} \quad \frac{6.8}{31} \quad \frac{3.3}{37} \quad \frac{3.2}{50}$$

$$\frac{7.3}{50} \quad \frac{6.6}{32} \quad \frac{7.3}{29} \quad \frac{7.2}{24} \quad \frac{5.0}{20} \quad 4.8 \quad \frac{5.0}{20} \quad \frac{6.6}{26} \quad \frac{6.3}{33} \quad \frac{4.7}{35} \quad \frac{4.3}{50}$$

$$\frac{7.6}{50} \quad \frac{7.2}{31} \quad \frac{7.7}{30} \quad \frac{7.5}{25} \quad \frac{5.2}{20} \quad 5.0 \quad \frac{5.0}{20} \quad \frac{7.2}{26} \quad \frac{7.2}{30} \quad \frac{5.8}{33} \quad \frac{5.5}{50}$$

$$\frac{7.8}{50} \quad \frac{7.4}{31} \quad \frac{7.7}{30} \quad \frac{7.6}{24} \quad \frac{5.2}{20} \quad 5.0 \quad \frac{5.0}{19} \quad \frac{7.7}{25} \quad \frac{7.9}{30} \quad \frac{6.8}{31} \quad \frac{6.5}{50}$$

$$\frac{8.0}{50} \quad \frac{7.8}{31} \quad \frac{8.3}{30} \quad \frac{8.2}{25} \quad \frac{5.6}{20} \quad 5.3 \quad \frac{5.3}{20} \quad \frac{7.7}{23} \quad \frac{8.2}{29} \quad \frac{7.8}{31} \quad \frac{7.7}{50}$$

$$\frac{8.5}{50} \quad \frac{8.5}{25} \quad \frac{5.6}{20} \quad 5.5 \quad \frac{5.6}{19} \quad \frac{8.5}{26} \quad \frac{8.4}{50}$$

$$\frac{8.8}{50} \quad \frac{8.8}{26} \quad \frac{6.0}{20} \quad 5.7 \quad \frac{5.8}{20} \quad \frac{9.0}{25} \quad \frac{9.0}{50}$$

$$\frac{9.0}{50} \quad \frac{9.0}{26} \quad \frac{6.0}{20} \quad 5.8 \quad \frac{6.0}{20} \quad \frac{9.4}{27} \quad \frac{9.3}{50}$$

Sta.	+	H.I.	-	Elev.	
		915.41			
473				09.3	6.1
T.P.	3.99	913.24 ✓	6.16	909.25 ✓	
B.M.	4.49	913.10 ✓	4.63	908.61 ✓	
+50				09.1	4.0
474				09.0	4.1
+50				08.9	4.2
475				08.7	4.4
+50				08.5	4.6
476				08.4	4.7
+50				08.2	4.9
477				08.1	5.0
+62				07.8	5.3
478				07.6	5.5

$\frac{9.0}{50}$ $\frac{9.2}{26}$ $\frac{4.2}{20}$ 60 $\frac{6.2}{20}$ $\frac{9.2}{26}$ $\frac{9.4}{50}$

$\frac{6.5}{50}$ $\frac{6.5}{25}$ $\frac{4.0}{20}$ 38 $\frac{4.0}{20}$ $\frac{7.0}{26}$ $\frac{7.0}{50}$
 $\frac{6.0}{50}$ $\frac{5.0}{30}$ $\frac{6.7}{30}$ $\frac{6.5}{26}$ $\frac{4.2}{20}$ $\frac{4.1}{20}$ $\frac{4.2}{20}$ $\frac{6.5}{26}$ $\frac{6.5}{50}$

$\frac{4.5}{50}$ $\frac{5.0}{33}$ $\frac{6.5}{30}$ $\frac{6.8}{25}$ $\frac{4.3}{20}$ 43 $\frac{4.2}{20}$ $\frac{6.5}{26}$ $\frac{6.8}{30}$ $\frac{5.8}{32}$ $\frac{6.1}{50}$

$\frac{4.2}{50}$ $\frac{4.2}{34}$ $\frac{6.2}{30}$ $\frac{6.2}{25}$ $\frac{4.5}{20}$ 44 $\frac{4.5}{20}$ $\frac{6.6}{26}$ $\frac{6.6}{30}$ $\frac{5.6}{32}$ $\frac{5.8}{50}$

$\frac{3.4}{50}$ $\frac{3.6}{35}$ $\frac{6.6}{29}$ $\frac{6.4}{25}$ $\frac{4.6}{19}$ 46 $\frac{4.7}{20}$ $\frac{6.6}{26}$ $\frac{7.0}{30}$ $\frac{5.2}{33}$ $\frac{5.2}{50}$

$\frac{3.4}{50}$ $\frac{3.6}{35}$ $\frac{7.2}{28}$ $\frac{7.0}{24}$ $\frac{4.8}{20}$ 46 $\frac{4.9}{20}$ $\frac{6.8}{25}$ $\frac{7.3}{30}$ $\frac{4.6}{34}$ $\frac{5.0}{50}$

$\frac{5.5}{50}$ $\frac{3.6}{36}$ $\frac{7.2}{29}$ $\frac{7.0}{24}$ $\frac{5.2}{20}$ 48 $\frac{5.1}{20}$ $\frac{7.2}{26}$ $\frac{7.5}{29}$ $\frac{4.2}{35}$ $\frac{4.2}{50}$

$\frac{4.2}{50}$ $\frac{4.3}{35}$ $\frac{7.1}{29}$ $\frac{6.7}{23}$ $\frac{5.1}{20}$ 50 $\frac{5.1}{20}$ $\frac{6.8}{25}$ $\frac{7.0}{30}$ $\frac{4.0}{35}$ $\frac{3.7}{50}$

$\frac{5.6}{50}$ $\frac{5.5}{35}$ $\frac{6.8}{31}$ $\frac{6.8}{27}$ $\frac{5.6}{21}$ 52 $\frac{5.2}{20}$ $\frac{7.6}{26}$ $\frac{7.7}{30}$ $\frac{4.8}{33}$ $\frac{4.9}{50}$

$\frac{5.4}{50}$ $\frac{5.3}{33}$ 55 $\frac{5.5}{20}$ $\frac{8.0}{25}$ $\frac{8.0}{29}$ $\frac{5.5}{33}$ $\frac{5.6}{50}$

Sta	T	HI	-	Elev	
		913.10			
479				06.9	6.7
480				06.0	7.1
481				05.1	8.0
+50				04.7	8.4
482				04.5	8.6
T.P.	4.27	909.81 ✓	7.56	905.52 ✓	
+50				04.4	5.4
483				04.3	5.5
+50				04.3	5.5
484				04.4	5.4
+50				04.4	5.4
485				04.5	5.3

$$\frac{66}{50} \quad \frac{66}{38} \quad \frac{90}{34} \quad \frac{85}{26} \quad \frac{63}{20} \quad 61 \quad \frac{63}{20} \quad \frac{85}{25} \quad \frac{90}{29} \quad \frac{68}{32} \quad \frac{70}{50}$$

$$\frac{84}{50} \quad \frac{83}{38} \quad \frac{100}{35} \quad \frac{91}{26} \quad \frac{72}{20} \quad 70 \quad \frac{72}{20} \quad \frac{96}{26} \quad \frac{100}{30} \quad \frac{90}{32} \quad \frac{90}{50}$$

$$\frac{81}{50} \quad \frac{81}{38} \quad \frac{106}{34} \quad \frac{105}{25} \quad \frac{81}{20} \quad 78 \quad \frac{82}{20} \quad \frac{98}{25} \quad \frac{105}{30} \quad \frac{86}{32} \quad \frac{88}{50}$$

$$\frac{85}{50} \quad \frac{84}{37} \quad \frac{106}{35} \quad \frac{107}{28} \quad \frac{84}{20} \quad 82 \quad \frac{84}{20} \quad \frac{107}{25} \quad \frac{107}{30} \quad \frac{85}{33} \quad \frac{85}{50}$$

$$\frac{94}{50} \quad \frac{94}{38} \quad \frac{110}{34} \quad \frac{108}{26} \quad \frac{88}{20} \quad 86 \quad \frac{88}{20} \quad \frac{110}{26} \quad \frac{111}{30} \quad \frac{96}{32} \quad \frac{96}{50}$$

$$\frac{76}{50} \quad \frac{75}{37} \quad \frac{77}{36} \quad \frac{77}{25} \quad \frac{53}{20} \quad 54 \quad \frac{54}{20} \quad \frac{80}{25} \quad \frac{80}{30} \quad \frac{75}{31} \quad \frac{75}{50}$$

$$\frac{81}{50} \quad \frac{80}{24} \quad \frac{55}{20} \quad 55 \quad \frac{55}{20} \quad \frac{82}{27} \quad \frac{85}{31} \quad \frac{81}{32} \quad \frac{83}{50}$$

$$\frac{65}{50} \quad \frac{65}{47} \quad \frac{84}{42} \quad \frac{78}{27} \quad \frac{54}{40} \quad 54 \quad \frac{55}{20} \quad \frac{76}{26} \quad \frac{80}{30} \quad 87 \quad \frac{87}{50}$$

$$\frac{51}{50} \quad \frac{52}{48} \quad \frac{84}{44} \quad \frac{83}{28} \quad \frac{55}{20} \quad 54 \quad \frac{54}{20} \quad \frac{68}{23} \quad \frac{77}{30} \quad \frac{73}{31} \quad \frac{82}{50}$$

$$\frac{57}{50} \quad \frac{57}{49} \quad \frac{88}{45} \quad \frac{78}{27} \quad \frac{54}{20} \quad 53 \quad \frac{53}{19} \quad \frac{76}{25} \quad \frac{80}{29} \quad \frac{72}{30} \quad \frac{76}{50}$$

$$\frac{61}{50} \quad \frac{61}{48} \quad \frac{87}{44} \quad \frac{87}{28} \quad \frac{53}{20} \quad 52 \quad \frac{52}{20} \quad \frac{82}{28} \quad \frac{85}{34} \quad \frac{62}{38} \quad \frac{63}{50}$$

909.81

485+50

04.5

5.3

486

04.6

5.2

T.P.

4.47

909.51

477

905.04

+50

04.6

4.9

487

04.6

4.9

+50

04.5

5.0

488

04.4

5.1

+50

04.2

5.3

489

04.1

5.4

490

03.8

5.7

+50.

03.7

5.8

491

03.6

5.9

B.M.

5.25

904.26

904.23

in South
X Kelum
Washburn
900.

6/11/27

915.82

63

$\frac{21}{50}$ $\frac{20}{31}$ $\frac{27}{30}$ $\frac{24}{27}$ $\frac{52}{21}$ $\frac{50}{-}$ $\frac{50}{20}$ $\frac{27}{28}$ $\frac{80}{37}$ $\frac{62}{37}$ $\frac{63}{50}$

$\frac{22}{50}$ $\frac{66}{32}$ $\frac{77}{30}$ $\frac{24}{26}$ $\frac{54}{20}$ $\frac{51}{-}$ $\frac{53}{20}$ $\frac{26}{27}$ $\frac{77}{37}$ $\frac{52}{42}$ $\frac{50}{50}$

$\frac{60}{50}$ $\frac{50}{33}$ $\frac{70}{31}$ $\frac{65}{24}$ $\frac{49}{20}$ $\frac{47}{-}$ $\frac{47}{20}$ $\frac{70}{27}$ $\frac{75}{37}$ $\frac{40}{43}$ $\frac{40}{50}$

$\frac{45}{50}$ $\frac{42}{35}$ $\frac{66}{31}$ $\frac{65}{25}$ $\frac{48}{20}$ $\frac{47}{-}$ $\frac{47}{20}$ $\frac{68}{25}$ $\frac{72}{35}$ $\frac{40}{42}$ $\frac{42}{50}$

$\frac{53}{50}$ $\frac{31}{36}$ $\frac{68}{30}$ $\frac{68}{25}$ $\frac{48}{20}$ $\frac{49}{-}$ $\frac{50}{20}$ $\frac{68}{25}$ $\frac{71}{30}$ $\frac{37}{36}$ $\frac{42}{50}$

$\frac{28}{50}$ $\frac{27}{37}$ $\frac{68}{30}$ $\frac{68}{25}$ $\frac{50}{20}$ $\frac{48}{-}$ $\frac{50}{20}$ $\frac{68}{24}$ $\frac{73}{29}$ $\frac{40}{36}$ $\frac{44}{50}$

$\frac{34}{50}$ $\frac{36}{36}$ $\frac{72}{29}$ $\frac{72}{24}$ $\frac{51}{20}$ $\frac{50}{-}$ $\frac{51}{20}$ $\frac{70}{25}$ $\frac{73}{30}$ $\frac{50}{34}$ $\frac{50}{50}$

$\frac{45}{50}$ $\frac{46}{37}$ $\frac{50}{35}$ $\frac{78}{30}$ $\frac{77}{26}$ $\frac{54}{20}$ $\frac{54}{20}$ $\frac{72}{25}$ $\frac{72}{30}$ $\frac{48}{35}$ $\frac{47}{50}$

$\frac{58}{50}$ $\frac{57}{34}$ $\frac{80}{29}$ $\frac{75}{25}$ $\frac{55}{20}$ $\frac{55}{-}$ $\frac{57}{20}$ $\frac{77}{25}$ $\frac{80}{31}$ $\frac{56}{30}$ $\frac{56}{50}$

$\frac{59}{50}$ $\frac{59}{33}$ $\frac{82}{30}$ $\frac{78}{25}$ $\frac{58}{20}$ $\frac{57}{-}$ $\frac{57}{20}$ $\frac{78}{25}$ $\frac{80}{30}$ $\frac{59}{33}$ $\frac{60}{50}$

$\frac{66}{50}$ $\frac{68}{32}$ $\frac{81}{30}$ $\frac{77}{26}$ $\frac{58}{20}$ $\frac{57}{-}$ $\frac{58}{20}$ $\frac{78}{26}$ $\frac{80}{30}$ $\frac{64}{33}$ $\frac{64}{50}$

spike in 15" Oak 70 ft sta 49100

909.57

491+50

03.6

5.9

492+00

03.6

5.9

+50

03.7

5.8

493+00

03.8

5.7

T.P.

891

913.09 ✓

5.23

904.18 ✓

+50

04.0

9.1

494

04.2

8.9

+50

04.5

8.6

495

04.7

8.4

+50

05.0

8.1

496

05.4

7.7

+50

05.9

7.2

136 Beg H.D.
+55 End H.D.
H.D. H.D.

$\frac{63}{50}$ $\frac{80}{31}$ $\frac{84}{30}$ $\frac{80}{24}$ $\frac{58}{20}$ 58 $\frac{58}{20}$ $\frac{80}{26}$ $\frac{85}{30}$ $\frac{72}{31}$ $\frac{83}{33}$ $\frac{81}{34}$ $\frac{70}{41}$ $\frac{67}{50}$

$\frac{110}{50}$ $\frac{104}{30}$ $\frac{58}{20}$ 58 $\frac{58}{20}$ $\frac{87}{27}$ $\frac{98}{28}$ $\frac{98}{32}$ $\frac{82}{34}$ $\frac{20}{50}$

$\frac{114}{50}$ $\frac{112}{30}$ $\frac{56}{20}$ 56 $\frac{56}{20}$ $\frac{81}{25}$ $\frac{90}{32}$ $\frac{77}{34}$ $\frac{66}{50}$

$\frac{107}{50}$ $\frac{98}{29}$ $\frac{55}{19}$ 53 $\frac{55}{20}$ $\frac{88}{29}$ $\frac{91}{33}$ $\frac{56}{38}$ $\frac{52}{50}$

$\frac{117}{50}$ $\frac{115}{46}$ $\frac{120}{45}$ $\frac{117}{29}$ $\frac{86}{20}$ 84 $\frac{85}{20}$ $\frac{125}{31}$ $\frac{128}{34}$ $\frac{77}{41}$ $\frac{75}{50}$

$\frac{96}{53}$ $\frac{96}{50}$ $\frac{133}{43}$ $\frac{120}{29}$ $\frac{85}{20}$ 83 $\frac{84}{20}$ $\frac{130}{52}$ $\frac{130}{35}$ $\frac{70}{43}$ $\frac{76}{50}$

$\frac{90}{50}$ $\frac{90}{48}$ $\frac{132}{42}$ $\frac{124}{32}$ $\frac{83}{20}$ 83 $\frac{84}{20}$ $\frac{128}{32}$ $\frac{130}{36}$ $\frac{70}{46}$ $\frac{72}{50}$

$\frac{96}{50}$ $\frac{96}{49}$ $\frac{130}{43}$ $\frac{125}{35}$ $\frac{82}{20}$ 82 $\frac{82}{20}$ $\frac{120}{32}$ $\frac{126}{39}$ $\frac{84}{45}$ $\frac{85}{50}$

$\frac{104}{50}$ $\frac{104}{45}$ $\frac{115}{43}$ $\frac{105}{27}$ $\frac{80}{20}$ 77 $\frac{78}{20}$ $\frac{98}{26}$ $\frac{110}{43}$ $\frac{98}{45}$ $\frac{98}{50}$

$\frac{104}{50}$ $\frac{104}{26}$ $\frac{75}{20}$ 75 $\frac{75}{20}$ $\frac{110}{37}$ $\frac{105}{50}$

$\frac{100}{50}$ $\frac{104}{27}$ $\frac{71}{20}$ 71 $\frac{71}{20}$ $\frac{102}{27}$ $\frac{96}{50}$

913.09

497

06.5

6.6

498

07.9

5.2

+50

08.8

4.3

499

09.7

3.4

T.P.

736

918.03 ✓

2.42

910.67 ✓

B.M.

2.24

915.77 ✓

915.82

$\frac{82}{50}$	$\frac{82}{40}$	$\frac{92}{44}$	$\frac{90}{26}$	$\frac{64}{20}$	$\frac{64}{20}$	$\frac{65}{20}$	$\frac{90}{28}$	$\frac{92}{45}$	$\frac{82}{46}$	$\frac{81}{50}$
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$\frac{45}{50}$	$\frac{46}{48}$	$\frac{75}{44}$	$\frac{64}{25}$	$\frac{50}{20}$	$\frac{51}{20}$	$\frac{51}{20}$	$\frac{73}{27}$	$\frac{80}{47}$	$\frac{64}{49}$	$\frac{64}{50}$
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$\frac{26}{50}$	$\frac{26}{49}$	$\frac{65}{44}$	$\frac{56}{24}$	$\frac{42}{20}$	$\frac{43}{20}$	$\frac{43}{20}$	$\frac{64}{26}$	$\frac{76}{46}$	$\frac{57}{49}$	$\frac{58}{50}$
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$\frac{18}{49}$	$\frac{58}{44}$	$\frac{50}{33}$	$\frac{34}{20}$	$\frac{35}{20}$	$\frac{35}{20}$	$\frac{50}{24}$	$\frac{64}{31}$	$\frac{72}{46}$	$\frac{50}{49}$	$\frac{50}{50}$
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spike in 20" str. 52' Rt str 500.90

Sta	+	HI	-	Elev
B.M.	5.68	915.74		910.06
524	+00			08.3
	+50			08.4
525				08.6
	+50			08.8
526				09.0
	+50			09.2
527				09.4
	+50			09.7
528				09.9
	+50			10.2
529				10.4
	+50			10.7

2.11.2
2.5
W. W.
4.4

6/11/27

spike in 24" Ogd wt sta 27+32

$\frac{103}{50}$ $\frac{103}{26}$ $\frac{75}{20}$ $\frac{75}{20}$ $\frac{102}{25}$ $\frac{102}{31}$ $\frac{110}{48}$ $\frac{100}{29}$ $\frac{100}{50}$

(7.3)

$\frac{104}{50}$ $\frac{104}{26}$ $\frac{74}{20}$ $\frac{74}{20}$ $\frac{100}{26}$ $\frac{112}{47}$ $\frac{9.8}{50}$

(7.1)

$\frac{102}{50}$ $\frac{100}{26}$ $\frac{72}{20}$ $\frac{72}{20}$ $\frac{96}{24}$ $\frac{10.8}{47}$ $\frac{92}{49}$ $\frac{92}{50}$

(6.9)

$\frac{100}{34}$
 $\frac{9.8}{50}$ $\frac{9.8}{48}$ $\frac{104}{47}$ $\frac{9.8}{26}$ $\frac{72}{20}$ $\frac{72}{20}$ $\frac{6.9}{20}$ $\frac{8.5}{23}$ $\frac{86}{26}$ $\frac{100}{33}$ $\frac{106}{46}$ $\frac{7.9}{49}$ $\frac{7.8}{50}$

(6.7)

$\frac{9.2}{50}$ $\frac{9.2}{49}$ $\frac{107}{47}$ $\frac{9.4}{31}$ $\frac{9.4}{25}$ $\frac{6.8}{20}$ $\frac{7.2}{20}$ $\frac{6.8}{20}$ $\frac{90}{23}$ $\frac{107}{47}$ $\frac{8.4}{49}$ $\frac{8.4}{50}$

(6.5)

$\frac{90}{50}$ $\frac{80}{49}$ $\frac{10.5}{46}$ $\frac{8.5}{27}$ $\frac{8.5}{24}$ $\frac{6.5}{20}$ $\frac{6.5}{20}$ $\frac{6.5}{20}$ $\frac{90}{24}$ $\frac{10.7}{47}$ $\frac{8.8}{49}$ $\frac{8.8}{50}$

(6.3)

$\frac{7.3}{50}$ $\frac{7.7}{49}$ $\frac{100}{45}$ $\frac{8.8}{34}$ $\frac{80}{26}$ $\frac{80}{23}$ $\frac{60}{20}$ $\frac{60}{20}$ $\frac{7.7}{22}$ $\frac{10.5}{46}$ $\frac{80}{48}$ $\frac{7.8}{50}$

(6.0)

$\frac{7.4}{50}$ $\frac{7.4}{49}$ $\frac{100}{46}$ $\frac{9.8}{37}$ $\frac{80}{24}$ $\frac{60}{20}$ $\frac{60}{20}$ $\frac{60}{20}$ $\frac{8.1}{24}$ $\frac{8.8}{34}$ $\frac{103}{47}$ $\frac{82}{48}$ $\frac{80}{50}$

(5.8)

$\frac{8.2}{50}$ $\frac{9.2}{48}$ $\frac{8.1}{26}$ $\frac{5.8}{20}$ $\frac{5.8}{21}$ $\frac{7.8}{25}$ $\frac{8.3}{31}$ $\frac{10.2}{46}$ $\frac{76}{28}$ $\frac{7.4}{50}$

(5.5)

$\frac{9.6}{50}$ $\frac{9.2}{27}$ $\frac{5.4}{20}$ $\frac{5.5}{20}$ $\frac{8.2}{25}$ $\frac{8.5}{34}$ $\frac{9.8}{47}$ $\frac{80}{49}$ $\frac{7.8}{50}$

(5.3)

$\frac{9.5}{50}$ $\frac{90}{27}$ $\frac{5.3}{20}$ $\frac{5.3}{20}$ $\frac{7.8}{25}$ $\frac{7.8}{32}$ $\frac{9.4}{41}$ $\frac{9.5}{49}$ $\frac{76}{49}$ $\frac{7.4}{50}$

(5.0)

$\frac{8.7}{50}$ $\frac{8.3}{26}$ $\frac{5.1}{21}$ $\frac{5.0}{20}$ $\frac{4.8}{20}$ $\frac{6.8}{25}$ $\frac{7.1}{27}$ $\frac{8.1}{40}$ $\frac{66}{43}$ $\frac{6.5}{50}$

Sta	+	HZ	-	Elev
529		915.74 ✓		
530				11.0
+40				11.2
531				11.6
T.P.	7.41	918.98 ✓	4.17	911.57 ✓
+50				11.9
532				12.2
+50				12.5
533				12.8
+50				13.1
534				13.3
+50				13.4
535				13.5
+50				13.5

(47)

$\frac{74}{50}$	$\frac{71}{30}$	$\frac{77}{29}$	$\frac{70}{24}$	$\frac{48}{20}$	47	$\frac{48}{20}$	$\frac{63}{25}$	$\frac{65}{33}$	$\frac{57}{35}$	$\frac{55}{50}$
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(45)

$\frac{63}{50}$	$\frac{61}{32}$	$\frac{73}{29}$	$\frac{68}{25}$	$\frac{47}{20}$	45	$\frac{47}{20}$	$\frac{62}{28}$	$\frac{62}{31}$	$\frac{48}{33}$	$\frac{46}{36}$	$\frac{44}{50}$
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(41)

$\frac{40}{50}$	$\frac{40}{34}$	$\frac{62}{29}$	$\frac{60}{24}$	$\frac{42}{20}$	39	$\frac{42}{20}$	$\frac{55}{24}$	$\frac{58}{30}$	$\frac{28}{36}$	$\frac{24}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----	-----------------	-----------------	-----------------	-----------------	-----------------

(71)

$\frac{55}{50}$	$\frac{53}{38}$	$\frac{55}{36}$	$\frac{92}{30}$	$\frac{88}{24}$	$\frac{74}{20}$	70	$\frac{70}{20}$	$\frac{87}{24}$	$\frac{88}{31}$	$\frac{46}{37}$	$\frac{44}{50}$
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(68)

$\frac{43}{50}$	$\frac{43}{38}$	$\frac{86}{30}$	$\frac{84}{25}$	$\frac{68}{20}$	47	$\frac{67}{20}$	$\frac{80}{23}$	$\frac{86}{30}$	$\frac{37}{38}$	$\frac{34}{50}$
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(65)

$\frac{40}{50}$	$\frac{40}{38}$	$\frac{86}{28}$	$\frac{84}{24}$	$\frac{67}{20}$	64	$\frac{66}{20}$	$\frac{80}{24}$	$\frac{81}{29}$	$\frac{32}{39}$	$\frac{30}{50}$
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(62)

$\frac{41}{50}$	$\frac{40}{39}$	$\frac{41}{37}$	$\frac{81}{28}$	$\frac{78}{24}$	$\frac{63}{20}$	64	$\frac{63}{20}$	$\frac{78}{23}$	$\frac{81}{27}$	$\frac{36}{38}$	$\frac{34}{50}$
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(59)

$\frac{34}{50}$	$\frac{40}{37}$	$\frac{78}{28}$	$\frac{77}{24}$	$\frac{61}{20}$	61	$\frac{62}{20}$	$\frac{76}{23}$	$\frac{80}{29}$	$\frac{35}{37}$	$\frac{35}{50}$
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(57)

$\frac{26}{50}$	$\frac{26}{39}$	$\frac{27}{29}$	$\frac{71}{24}$	$\frac{58}{20}$	57	$\frac{58}{20}$	$\frac{73}{24}$	$\frac{75}{28}$	$\frac{30}{38}$	$\frac{30}{50}$
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(56)

$\frac{24}{50}$	$\frac{25}{39}$	$\frac{75}{28}$	$\frac{70}{24}$	$\frac{58}{20}$	56	$\frac{56}{20}$	$\frac{70}{23}$	$\frac{72}{28}$	$\frac{28}{38}$	$\frac{30}{50}$
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(55)

$\frac{28}{50}$	$\frac{30}{38}$	$\frac{76}{29}$	$\frac{70}{25}$	$\frac{55}{20}$	56	$\frac{58}{20}$	$\frac{70}{23}$	$\frac{76}{29}$	$\frac{27}{38}$	$\frac{27}{50}$
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(55)

$\frac{38}{50}$	$\frac{37}{37}$	$\frac{78}{30}$	$\frac{70}{24}$	$\frac{55}{20}$	56	$\frac{56}{20}$	$\frac{66}{23}$	$\frac{74}{30}$	$\frac{30}{38}$	$\frac{29}{50}$
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Sta	+	HZ	-	Elev
		918.98 ✓		
536				13.5
	+50			13.3
537				13.2
	+50			13.0
538				12.8
	+50			12.6
539				12.5
	+50			12.5
540				12.5
T.P.	5.36	917.81 ✓	6.53	912.45 ✓
	+50			12.5
541				12.6
B.M.	4.10	918.07 ✓	3.87	913.94 ✓
542				12.7
				913.97

(5.5)

$\frac{43}{50}$ $\frac{40}{37}$ $\frac{77}{30}$ $\frac{74}{26}$ $\frac{56}{20}$ $\frac{54}{20}$ $\frac{56}{20}$ $\frac{66}{22}$ $\frac{74}{30}$ $\frac{31}{37}$ $\frac{33}{50}$

(5.7)

$\frac{47}{50}$ $\frac{38}{37}$ $\frac{78}{31}$ $\frac{74}{27}$ $\frac{54}{20}$ $\frac{54}{20}$ $\frac{57}{20}$ $\frac{76}{25}$ $\frac{78}{30}$ $\frac{45}{36}$ $\frac{45}{50}$

(5.8)

$\frac{42}{50}$ $\frac{43}{37}$ $\frac{45}{36}$ $\frac{78}{31}$ $\frac{70}{24}$ $\frac{56}{20}$ $\frac{56}{20}$ $\frac{76}{26}$ $\frac{76}{30}$ $\frac{57}{34}$ $\frac{60}{50}$

(6.0)

$\frac{50}{50}$ $\frac{53}{36}$ $\frac{55}{35}$ $\frac{84}{32}$ $\frac{80}{27}$ $\frac{55}{20}$ $\frac{55}{20}$ $\frac{60}{20}$ $\frac{75}{26}$ $\frac{80}{31}$ $\frac{68}{33}$ $\frac{72}{50}$

(6.2)

$\frac{66}{50}$ $\frac{68}{35}$ $\frac{20}{34}$ $\frac{87}{31}$ $\frac{84}{26}$ $\frac{62}{20}$ $\frac{61}{20}$ $\frac{62}{20}$ $\frac{84}{26}$ $\frac{88}{50}$

(6.4)

$\frac{80}{50}$ $\frac{85}{31}$ $\frac{93}{30}$ $\frac{86}{25}$ $\frac{61}{20}$ $\frac{61}{20}$ $\frac{63}{20}$ $\frac{102}{27}$ $\frac{101}{50}$

(6.5)

$\frac{100}{50}$ $\frac{105}{28}$ $\frac{66}{20}$ $\frac{64}{20}$ $\frac{64}{20}$ $\frac{114}{30}$ $\frac{105}{50}$

(6.5)

$\frac{104}{50}$ $\frac{108}{29}$ $\frac{65}{20}$ $\frac{64}{20}$ $\frac{64}{20}$ $\frac{105}{28}$ $\frac{100}{50}$

(6.5)

$\frac{101}{50}$ $\frac{101}{27}$ $\frac{67}{20}$ $\frac{67}{20}$ $\frac{65}{20}$ $\frac{94}{26}$ $\frac{88}{50}$

(5.3)

$\frac{84}{50}$ $\frac{84}{26}$ $\frac{56}{20}$ $\frac{56}{20}$ $\frac{52}{20}$ $\frac{77}{25}$ $\frac{82}{41}$ $\frac{74}{42}$ $\frac{71}{50}$

(5.7)

$\frac{81}{50}$ $\frac{80}{26}$ $\frac{57}{20}$ $\frac{57}{20}$ $\frac{57}{20}$ $\frac{73}{23}$ $\frac{83}{43}$ $\frac{74}{44}$ $\frac{72}{50}$

(5.4)

$\frac{75}{50}$ $\frac{74}{31}$ $\frac{77}{30}$ $\frac{76}{29}$ $\frac{73}{27}$ $\frac{71}{28}$ $\frac{57}{20}$ $\frac{54}{20}$ $\frac{53}{20}$ $\frac{67}{22}$ $\frac{87}{43}$ $\frac{66}{47}$ $\frac{63}{50}$

Sta	+	HZ	-	E/ed
		918.07		
543				12.8
544				12.9
545				13.0
546				13.1
547				13.2
548				13.2
549				13.1
550				13.0
550				12.8
550				12.7
T.P.	3.10	916.46 ✓	4.71	913.36 ✓
551				12.5
551				12.4

C.H.W.
D.S.
H.W.
H.Y.

6/12/27

6.9 $\frac{66}{50}$ $\frac{76}{32}$ $\frac{70}{30}$ $\frac{5.2}{25}$ $\frac{5.2}{20}$ **5.3** $\frac{51}{21}$ $\frac{5.2}{20}$ $\frac{7.0}{26}$ $\frac{8.2}{24}$ $\frac{5.3}{48}$ $\frac{5.2}{29}$ $\frac{5.2}{50}$

$\frac{6.0}{50}$ $\frac{5.7}{33}$ $\frac{7.4}{30}$ $\frac{6.5}{25}$ $\frac{5.0}{20}$ **5.2** $\frac{4.9}{20}$ $\frac{5.2}{20}$ $\frac{6.5}{26}$ $\frac{7.2}{30}$ $\frac{5.0}{34}$ $\frac{4.9}{35}$ $\frac{5.1}{50}$

$\frac{6.0}{50}$ $\frac{5.8}{31}$ $\frac{6.1}{33}$ $\frac{7.5}{31}$ $\frac{6.7}{25}$ $\frac{5.1}{20}$ **5.1** $\frac{4.9}{20}$ $\frac{5.0}{20}$ $\frac{7.0}{26}$ $\frac{7.7}{31}$ $\frac{6.3}{33}$ $\frac{6.2}{34}$ $\frac{6.4}{50}$

$\frac{6.3}{50}$ $\frac{5.3}{34}$ $\frac{7.2}{31}$ $\frac{5.0}{20}$ **5.0** $\frac{4.6}{20}$ $\frac{5.0}{20}$ $\frac{7.0}{26}$ $\frac{7.3}{31}$ $\frac{5.3}{34}$ $\frac{5.4}{50}$

$\frac{3.4}{50}$ $\frac{3.1}{36}$ $\frac{7.1}{30}$ $\frac{6.5}{26}$ $\frac{4.8}{20}$ **4.1** $\frac{4.7}{20}$ $\frac{6.0}{25}$ $\frac{7.0}{32}$ $\frac{2.7}{37}$ $\frac{2.8}{50}$

$\frac{3.2}{50}$ $\frac{2.2}{38}$ $\frac{6.8}{30}$ $\frac{6.1}{24}$ $\frac{4.7}{20}$ **4.9** $\frac{4.7}{20}$ $\frac{7.0}{20}$ $\frac{6.6}{26}$ $\frac{6.3}{31}$ $\frac{2.8}{37}$ $\frac{2.6}{50}$

$\frac{2.6}{50}$ $\frac{2.7}{37}$ $\frac{6.6}{31}$ $\frac{6.0}{25}$ $\frac{4.7}{20}$ **4.9** $\frac{4.6}{20}$ $\frac{4.8}{20}$ $\frac{6.6}{26}$ $\frac{7.0}{31}$ $\frac{4.0}{36}$ $\frac{4.1}{50}$

$\frac{3.6}{50}$ $\frac{4.0}{36}$ $\frac{6.8}{31}$ $\frac{6.5}{25}$ $\frac{4.7}{20}$ **5.0** $\frac{4.7}{20}$ $\frac{5.0}{20}$ $\frac{7.0}{26}$ $\frac{7.2}{30}$ $\frac{6.0}{32}$ $\frac{6.4}{50}$

$\frac{4.3}{50}$ $\frac{4.8}{35}$ $\frac{7.2}{31}$ $\frac{6.3}{24}$ $\frac{5.0}{20}$ **5.1** $\frac{4.7}{20}$ $\frac{4.9}{20}$ $\frac{8.1}{24}$ $\frac{9.7}{50}$

$\frac{4.5}{50}$ $\frac{3.3}{34}$ $\frac{7.2}{31}$ $\frac{6.2}{23}$ $\frac{4.9}{20}$ **5.3** $\frac{4.8}{20}$ $\frac{5.0}{20}$ $\frac{9.5}{30}$ $\frac{11.0}{50}$

$\frac{4.3}{50}$ $\frac{3.2}{35}$ $\frac{7.0}{32}$ $\frac{6.2}{24}$ $\frac{5.1}{20}$ **5.4** $\frac{4.8}{21}$ $\frac{5.2}{21}$ $\frac{10.4}{30}$ $\frac{11.2}{50}$

$\frac{2.2}{50}$ $\frac{2.9}{37}$ $\frac{3.2}{35}$ $\frac{5.5}{31}$ $\frac{5.5}{26}$ $\frac{3.5}{20}$ **4.0** $\frac{3.5}{20}$ $\frac{4.0}{20}$ $\frac{7.2}{27}$ $\frac{8.3}{50}$

$\frac{1.7}{50}$ $\frac{2.2}{38}$ $\frac{2.6}{36}$ $\frac{5.5}{31}$ $\frac{5.4}{25}$ $\frac{4.0}{20}$ **4.1** $\frac{3.7}{20}$ $\frac{4.1}{20}$ $\frac{6.8}{28}$ $\frac{7.1}{31}$ $\frac{5.8}{33}$ $\frac{5.7}{35}$ $\frac{6.0}{50}$

Partial X-section of Borrow Pit.

Sta.	+	H. I.	-	Elev.	
B.M.	13.06	892.72		879.66	
311				885.6	7.1
311+05				85.6	7.1
311+50				85.8	6.9
312				86.0	6.7
312+50				86.2	6.5
312+65				86.3	6.4
312+90				86.4	6.3
312+95 = 313+00.				86.4	6.3
313+20				86.4	6.3
313+45				86.6	6.1
313+54				86.6	6.1
B.M.			13.06	879.66	

12-10-26

Lt.

Spk. 100 6" Maple 70 Rf. Sta. 312+65.

<u>0.3</u>	<u>5.6</u>	<u>5.6</u>	<u>6.3</u>	
58	50	35	14	6.8

<u>0.0</u>	<u>4.9</u>	<u>5.5</u>	<u>5.7</u>	<u>5.8</u>	<u>6.1</u>	
106	102	71	50	32	14	6.7

<u>1.3</u>	<u>5.2</u>	<u>6.1</u>	<u>5.7</u>	<u>5.4</u>	<u>5.9</u>	
106	100	77	50	42	25	6.2

<u>0.0</u>	<u>5.4</u>	<u>5.8</u>	<u>5.3</u>	<u>5.8</u>	
100	91	70	44	18	6.1

<u>2.2</u>	<u>5.0</u>	<u>5.6</u>	<u>4.6</u>	<u>6.0</u>	
95	91	67	37	23	6.0

<u>2.3</u>	<u>5.7</u>	<u>5.8</u>	<u>4.8</u>	<u>4.6</u>	<u>5.8</u>	
73	87	63	50	34	24	6.1

<u>2.5</u>	<u>5.7</u>	<u>6.3</u>	<u>5.5</u>	<u>5.5</u>	<u>5.4</u>	
92	88	57	50	28	12	6.1

<u>5.0</u>	<u>5.9</u>	<u>6.6</u>	<u>6.4</u>	<u>5.9</u>	<u>5.7</u>	<u>5.5</u>	
91	86	71	60	50	27	14	6.0

<u>3.7</u>	<u>6.6</u>	<u>7.0</u>	<u>5.5</u>	
83	76	42	17	4.6

<u>2.1</u>	<u>7.0</u>	<u>7.0</u>	<u>10.6</u>	<u>10.6</u>	<u>8.5</u>	<u>6.2</u>	<u>6.0</u>	
79	71	53	47	34	23	18	10	7.1

<u>3.8</u>	<u>5.9</u>	<u>10.6</u>	<u>11.1</u>	<u>8.5</u>	<u>6.1</u>	<u>6.2</u>	
79	67	50	33	21	17	10	7.1

Over.

Sta.	+	H. I.	-	Elev.	
B.M.	4.30	913.40		909.10	
311				885.6	27.8
311+05				85.6	27.8
311+50				85.8	27.6
T.P.	11.58	923.87	1.11	912.29	
312				886.0	37.9
312+50				86.2	37.7
312+65				86.3	37.6
312+90				86.4	37.5
312+95 = 313+00				86.4	37.5
T.P.	1.57	913.65	11.79	912.08	
313+20				886.4	27.3
T.P.	2.49	903.63	12.51	901.14	
313+45				886.6	17.0
T.P.	0.30	892.19	11.74	879.89	
B.M.			12.50	879.69	879.66

12-10-26

71

$$\frac{5.8}{100} \quad \frac{9.2}{75} \quad \frac{11.1}{61}$$

$$\frac{4.7}{108}$$

$$\frac{5.5}{110}$$

$$\frac{8.3}{103}$$

$$\frac{2.9}{110}$$

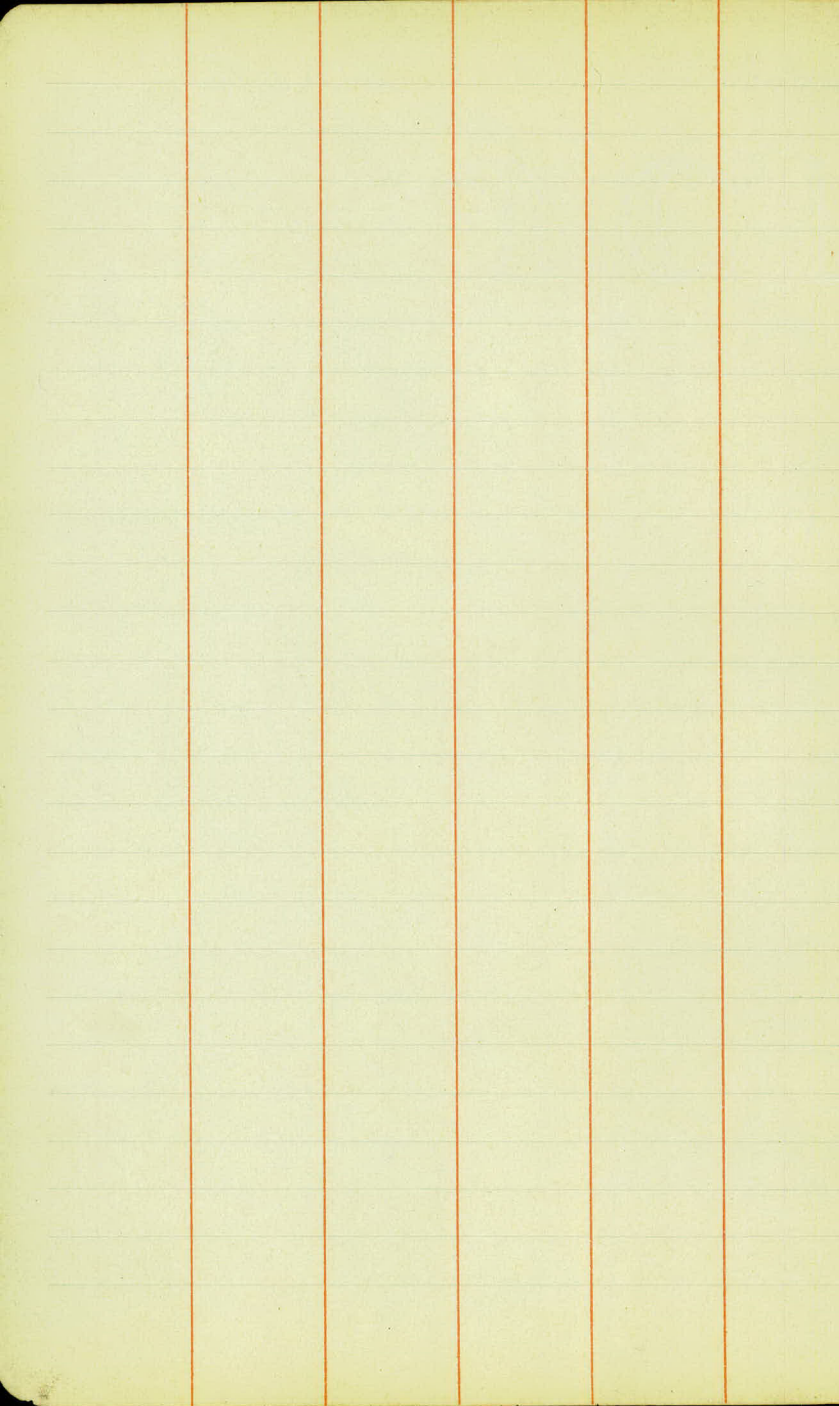
$$\frac{2.0}{101}$$

$$\frac{6.2}{94}$$

$$\frac{7.8}{94}$$

$$\frac{5.8}{88}$$

$$\frac{9.6}{82}$$



The image shows a page of graph paper with a grid of small squares. A vertical red line runs down the center of the page, dividing it into two equal halves. The grid covers most of the page, leaving a small margin at the top and bottom. The paper is off-white or light yellow.

Cattle Pass,

B N.

9.26

888.92

879.66

Cattle Pass

* Line Division.

Right

Left

		90		
		17'		
	$\frac{6.6}{10.0}$	$\frac{10.6}{6}$	$\frac{10.6}{6}$	$\frac{6.8}{10}$
		11.2		
		14'		
	$\frac{7.5}{10}$	$\frac{8.2}{10}$		$\frac{7.8}{10}$
<hr/>				
		80		
		12'		
	$\frac{7.4}{10}$	8.2		$\frac{8.6}{10}$
		12'		
	$\frac{6.8}{10}$	7.8		$\frac{8.8}{10}$
		18'		
	$\frac{7.2}{10}$	8.2	$\frac{8.4}{5}$	$\frac{7.8}{10}$
		+29		
	$\frac{5.3}{10}$	7.8		$\frac{7.3}{10}$
		$\frac{7.3}{4}$		

ORIGINALS OF PROPOSED BORROW PIT,

Sta.	+	H.I.	-	Elev.	
B.M.	10.06	903.63		879.57	
304				882.8	20.8
304+16				82.8	20.8
304+50				83.0	20.6
305				83.2	20.4
T.P.	11.25	912.12	2.74	900.87	
304				882.8	29.3
304+16				82.8	29.3
304+50				83.0	29.1
305				83.2	28.9
B.M.	1.69	912.25	1.54	910.54	
T.P.	1.80	901.49	12.54	879.69	
305+50				883.4	18.1
306				83.6	17.9
306+50				83.8	17.7

12-10-26

Lt.

Spk. in 10" Oak 60' Lt. Sta. 304+95.

$\frac{0.5}{126}$	$\frac{7.2}{109}$	$\frac{6.6}{92}$	$\frac{9.4}{70}$	$\frac{11.8}{48}$
-------------------	-------------------	------------------	------------------	-------------------

$\frac{1.7}{114}$	$\frac{5.1}{94}$	$\frac{8.4}{70}$	$\frac{10.8}{48}$
-------------------	------------------	------------------	-------------------

$\frac{0.3}{111}$	$\frac{3.0}{96}$	$\frac{7.0}{70}$	$\frac{10.7}{48}$
-------------------	------------------	------------------	-------------------

$\frac{0.6}{94}$	$\frac{7.2}{70}$	$\frac{12.5}{50}$
------------------	------------------	-------------------

$\frac{6.6}{140}$

$\frac{5.4}{140}$

$\frac{4.6}{140}$

$\frac{1.5}{140}$	$\frac{1.5}{134}$	$\frac{2.2}{126}$	$\frac{4.6}{111}$
-------------------	-------------------	-------------------	-------------------

Nail in Tree 140 Lt. Sta. 304+82.

$\frac{3.0}{70}$	$\frac{8.2}{60}$	$\frac{14.3}{50}$
------------------	------------------	-------------------

$\frac{1.7}{140}$	$\frac{1.7}{120}$	$\frac{1.7}{92}$	$\frac{2.1}{80}$	$\frac{4.3}{76}$	$\frac{7.2}{64}$	$\frac{15.8}{50}$
-------------------	-------------------	------------------	------------------	------------------	------------------	-------------------

$\frac{4.3}{140}$	$\frac{5.1}{128}$	$\frac{5.0}{100}$	$\frac{6.4}{70}$	$\frac{8.3}{65}$	$\frac{11.4}{50}$
-------------------	-------------------	-------------------	------------------	------------------	-------------------

Sta.	T	H. I.	-	Elev.	
		901.49			
307				884.0	17.5
T.P.	10.73	912.04	0.18	901.31	
305+50				883.4	28.6
307				84.0	28.0
307+28				84.1	27.9
307+50				84.2	27.8
T.P.	10.03	920.85	1.22	910.82	
307+73				884.3	36.6
308				84.4	36.5
308+50				84.6	36.3
309				84.8	36.1
309+50				85.0	35.9
T.P.	2.24	914.86	8.25	912.60	
310				885.2	29.7
310+50				85.4	29.5
B.M.			5.79	909.07	909.10

Lt.

12-10-26

$$\begin{array}{r} 0.7 \\ 56 \end{array} \quad \begin{array}{r} 30 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 140 \end{array} \quad \begin{array}{r} 5.0 \\ 114 \end{array} \quad \begin{array}{r} 4.9 \\ 95 \end{array}$$

$$\begin{array}{r} 138 \\ 140 \end{array} \quad \begin{array}{r} 136 \\ 134 \end{array} \quad \begin{array}{r} 116 \\ 115 \end{array} \quad \begin{array}{r} 98 \\ 103 \end{array} \quad \begin{array}{r} 8.3 \\ 85 \end{array} \quad \begin{array}{r} 90 \\ 70 \end{array} \quad \begin{array}{r} 76 \\ 65 \end{array}$$

$$\begin{array}{r} 124 \\ 140 \end{array} \quad \begin{array}{r} 113 \\ 132 \end{array} \quad \begin{array}{r} 70 \\ 111 \end{array} \quad \begin{array}{r} 38 \\ 94 \end{array} \quad \begin{array}{r} 3.2 \\ 80 \end{array} \quad \begin{array}{r} 3.9 \\ 70 \end{array} \quad \begin{array}{r} 4.7 \\ 65 \end{array} \quad \begin{array}{r} 6.5 \\ 54 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 96 \\ 140 \end{array} \quad \begin{array}{r} 6.1 \\ 124 \end{array} \quad \begin{array}{r} 0.7 \\ 75 \end{array} \quad \begin{array}{r} 0.6 \\ 83 \end{array} \quad \begin{array}{r} 1.7 \\ 70 \end{array} \quad \begin{array}{r} 2.4 \\ 65 \end{array} \quad \begin{array}{r} 4.4 \\ 53 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 163 \\ 140 \end{array} \quad \begin{array}{r} 8.2 \\ 105 \end{array} \quad \begin{array}{r} 7.9 \\ 89 \end{array} \quad \begin{array}{r} 9.5 \\ 70 \end{array} \quad \begin{array}{r} 10.3 \\ 65 \end{array} \quad \begin{array}{r} 12.2 \\ 54 \end{array} \quad \begin{array}{r} 13.5 \\ 50 \end{array}$$

$$\begin{array}{r} 13.7 \\ 140 \end{array} \quad \begin{array}{r} 7.5 \\ 115 \end{array} \quad \begin{array}{r} 6.2 \\ 108 \end{array} \quad \begin{array}{r} 5.9 \\ 96 \end{array} \quad \begin{array}{r} 8.7 \\ 70 \end{array} \quad \begin{array}{r} 7.3 \\ 65 \end{array} \quad \begin{array}{r} 11.3 \\ 53 \end{array} \quad \begin{array}{r} 12.3 \\ 50 \end{array}$$

$$\begin{array}{r} 8.1 \\ 140 \end{array} \quad \begin{array}{r} 5.9 \\ 130 \end{array} \quad \begin{array}{r} 3.8 \\ 115 \end{array} \quad \begin{array}{r} 5.4 \\ 92 \end{array} \quad \begin{array}{r} 8.6 \\ 70 \end{array} \quad \begin{array}{r} 9.5 \\ 65 \end{array} \quad \begin{array}{r} 11.7 \\ 83 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ 140 \end{array} \quad \begin{array}{r} 4.4 \\ 115 \end{array} \quad \begin{array}{r} 5.9 \\ 96 \end{array} \quad \begin{array}{r} 7.8 \\ 70 \end{array} \quad \begin{array}{r} 10.5 \\ 65 \end{array} \quad \begin{array}{r} 12.4 \\ 55 \end{array} \quad \begin{array}{r} 13.4 \\ 50 \end{array}$$

$$\begin{array}{r} 1.8 \\ 140 \end{array} \quad \begin{array}{r} 2.4 \\ 132 \end{array} \quad \begin{array}{r} 6.0 \\ 105 \end{array} \quad \begin{array}{r} 12.2 \\ 70 \end{array} \quad \begin{array}{r} 12.9 \\ 44 \end{array} \quad \begin{array}{r} 16.3 \\ 50 \end{array}$$

$$\begin{array}{r} 0.6 \\ 121 \end{array} \quad \begin{array}{r} 2.2 \\ 112 \end{array} \quad \begin{array}{r} 4.0 \\ 88 \end{array} \quad \begin{array}{r} 7.4 \\ 70 \end{array} \quad \begin{array}{r} 10.2 \\ 65 \end{array} \quad \begin{array}{r} 13.3 \\ 50 \end{array}$$

$$\begin{array}{r} 0.6 \\ 131 \end{array} \quad \begin{array}{r} 2.7 \\ 115 \end{array} \quad \begin{array}{r} 6.8 \\ 94 \end{array} \quad \begin{array}{r} 11.3 \\ 70 \end{array} \quad \begin{array}{r} 12.2 \\ 65 \end{array} \quad \begin{array}{r} 15.2 \\ 50 \end{array}$$

Nil in 10" O.H. 80 Lt 310 + 20.

C 19.

252+50	15" x 24	LT
242+05	24" x 24	RT
342+00	15" x 24	LT
353+00	15" x 24	LT
"	15" x 25	RT
370	15 x 24	RT
369+80	15 x 24	LT
379+45	15 x 24	RT
382+25	15' x 24	LT
282+95	15' x 24	LT
390+80	15' x 24	RT



X section Drive Lt Sta 325+50

BM

1.28

30025

0+00

106

120

140

170

Drive on Rt 252+50

" " Rt 342+05 ✓

" " Lt 342+00 ✓

" " Lt 352+00 ✓

" " Rt 352+00 ✓

" " Rt 367+25 ✓

" " Rt 370+00 ✓

" " Lt 367+80 ✓

" " Lt 378+10

Rt 379+45

Lt 382+25

Lt 382+95

Rt 390+80

Lt 390+70

$$\frac{25}{15} \quad \frac{6.3}{11} \quad \frac{20}{10} \quad 21 \quad \frac{24}{7} \quad \frac{81}{10} \quad \frac{6.5}{8}$$

$$\frac{25}{15} \quad \frac{6.5}{10} \quad 67 \quad \frac{17}{6} \quad \frac{76}{9} \quad \frac{43}{13} \quad \frac{42}{15}$$

$$\frac{6.5}{15} \quad \frac{57}{10} \quad \frac{5.8}{9} \quad 5.8 \quad \frac{5.8}{6} \quad \frac{6.5}{8} \quad \frac{20}{14} \quad \frac{30}{25}$$

$$\frac{4.5}{15} \quad \frac{4.2}{10} \quad \frac{4.2}{7} \quad 4.1 \quad \frac{4.2}{5} \quad \frac{4.6}{9} \quad \frac{1.2}{11} \quad \frac{2.0}{15}$$

$$\frac{26}{15} \quad \frac{1.3}{9} \quad 41 \quad \frac{1.2}{6} \quad \frac{1.3}{8} \quad \frac{0.5}{10} \quad \frac{0.7}{15}$$

$$50' \times 22' \times 1' = 41 \text{ cu yds.}$$

$$28' \times 20' \times 1' = 21 \text{ cu y.}$$

$$37' \times 17' \times 3' = 32 \text{ cy}$$

$$30 \text{ yds.} = 30 \text{ cy.}$$

$$22' \times 15' \times 1' = 12 \text{ cy}$$

$$11 \times 12 \times 1.5 = 70 \text{ cy}$$

$$15 \times 12 \times 2' = 130 \text{ cy}$$

$$9 \times 15 \times 2' = 100 \text{ y}$$

$$30 \text{ yds.} = 30 \text{ cy.}$$

$$10' \times 20' \times 1' = 80 \text{ y}$$

$$20 \times 9' \times 1' = 50 \text{ y}$$

$$20' \times 9' \times 1' = 60 \text{ y}$$

$$12 \times 18 \times 1' = 80 \text{ y}$$

$$20 \times 12 \times 1' = 90 \text{ cy.}$$

Xsection Borrow Pit

B.M.	11.68	891.34 ✓		879.66	
309+50					6.3
310+00					6.1
310+50					5.9
311+00					5.7
T.P.	12.85	903.84 ✓	0.35	890.99 ✓	
T.P.	9.32	907.73 ✓	5.43	898.41 ✓	
309+50					22.7
310+00					22.5
+50					22.3
311+00					22.1
T.P.	5.67	904.08 ✓	9.32	898.41 ✓	
T.P.	0.30	891.29 ✓	13.09	890.99 ✓	
B.M.			11.63	879.66 ✓	

CWS 4/25/27

AB
T.M

+47 = 00 Point

Spike in 8.
 $\frac{00}{42}$ $\frac{3.6}{36}$ $\frac{60}{39}$ $\frac{60}{9}$ $\frac{68}{7}$ $\frac{64}{-}$

$\frac{00}{53}$ $\frac{5.0}{44}$ $\frac{6.2}{27}$ $\frac{5.7}{9}$ $\frac{6.3}{8}$ $\frac{6.0}{-}$

$\frac{00}{53}$ $\frac{5.7}{44}$ $\frac{5.7}{21}$ $\frac{5.5}{8}$ $\frac{60}{7}$ $\frac{5.7}{-}$

$\frac{00}{52}$ $\frac{9.8}{47}$ $\frac{5.0}{26}$ $\frac{5.0}{8}$ $\frac{5.7}{5}$ 5.5

$\frac{3.2}{55}$ $\frac{3.2}{50}$ $\frac{11.8}{47.5}$

$\frac{3.6}{66}$ $\frac{4.6}{61}$ $\frac{12.5}{58}$

$\frac{5.0}{67}$ $\frac{5.8}{62}$ $\frac{12.5}{59}$

$\frac{4.8}{66}$ $\frac{5.5}{61}$ $\frac{12.5}{59}$

454+40	16 X 22 X 1 Lt 20 X 22 X 1 ⁵ Rt	
447+40	17' X 9" X 3'	Ex. 16" X 20 X 1
446+00	14' X 21' X 1" L 21 X 8 X 2' R	
444+00	15' X 8' X 2' R.	
440+50	20 X 35 X 2 L.	
440+00	21' X 35 X 2 Rt.	
433+85	7 X, 19 X 3.5 Lt.	
432+50	21 X 6 X 2.5 Rt.	
432+70	19 X 10 X 2.5 Lt.	

KEITH'S RAILROAD CURVE TABLES.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle
of Intersection or I. P.= $23^{\circ} 20'$ to the R. at Station
542+72.

Ext. in Tab. IV opposite $23^{\circ} 20'$ =120.87
 $120.87 \div 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20'$ =1183.1
 $1183.1 \div 10 = 118.31$.

Tab. V. correction for A. $23^{\circ} 20'$ for a 10° Cur.=0.16
 $118.31 + 0.16 = 118.47$ =corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. $23^{\circ} 20' = 23.33^{\circ} \div 10 = 2.3333$ =L. C.

$2^{\circ} 19\frac{1}{2}'$ =def. for sta.	543	I. P.=sta.	542+72
$4^{\circ} 49\frac{1}{2}'$ = " " "	+50	Tan.=	1.18.47
$7^{\circ} 19\frac{1}{2}'$ = " " "	543	B. C.=sta.	541+53.53
$9^{\circ} 49\frac{1}{2}'$ = " " "	+50	L. C.=	2.33.33
$11^{\circ} 40'$ = " " "	543+	E. C.=sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3'$ (def. for 1 ft. of 10° Cur.)= $139.41'$ =
 $2^{\circ} 19\frac{1}{2}'$ =def. for sta. 542.

Def. for 50 ft.= $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft.= $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve

(These tables are published in Field Books of
KEUFFEL & ESSER Co., New York, N. Y.)

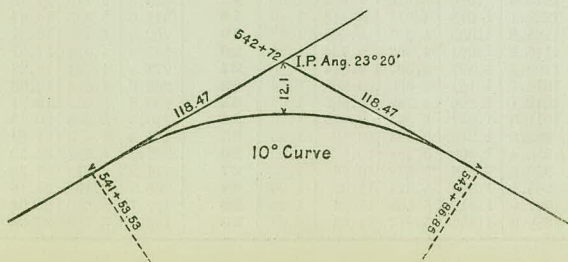


TABLE I. — Minutes in Decimals of a Degree.

1'	.0167	11'	.1833	21'	.3500	31'	.5167	41'	.6833	51'	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

TABLE II. — Inches in Decimals of a Foot.

1-16	3-32	¹ / ₈	3-16	¹ / ₄	5-16	³ / ₈	¹ / ₂	⁵ / ₈	³ / ₄	⁷ / ₈
.0052	.0078	.0104	.0156	.0208	.0260	.0313	.0417	.0521	.0625	.0729
1	2	3	4	5	6	7	8	9	10	11
.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167

TABLE III. — Radii, Ordinates and Deflections.

Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot	Deg.	Radius	Mid. Ord.	Tan. Def.	Chd. Def.	Def. for 1 Foot
0° 10'	34377.	.036	.145	.291	0.05'	7°	819.0	1.528	6.105	12.21	2.10
20	17189.	.073	.291	.582	0.10	20'	781.8	1.600	6.395	12.79	2.20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	8	716.8	1.746	6.976	13.95	2.40
1	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674.7	1.855	7.411	14.82	2.55
20	4297.3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	9	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2.037	8.136	16.27	2.80
50	3125.4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
2	2864.9	.436	1.745	3.490	0.60	40	593.4	2.110	8.426	16.85	2.90
10	2644.6	.473	1.891	3.781	0.65	10	573.7	2.183	8.716	17.43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2.292	9.150	18.30	3.15
30	2292.0	.545	2.181	4.363	0.75	11	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2.511	10.02	20.04	3.45
50	2022.4	.618	2.472	4.945	0.85	12	478.3	2.620	10.45	20.91	3.60
3	1910.1	.655	2.618	5.235	0.90	30	459.3	2.730	10.89	21.77	3.75
10	1809.6	.691	2.763	5.526	0.95	13	441.7	2.839	11.32	22.64	3.90
20	1719.1	.727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637.3	.764	3.054	6.108	1.05	14	410.3	3.058	12.18	24.37	4.20
40	1562.9	.800	3.199	6.398	1.10	30	396.2	3.168	12.62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	15	383.1	3.277	13.05	26.11	4.50
4	1432.7	.873	3.490	6.980	1.20	30	370.8	3.387	13.49	26.97	4.65
10	1375.4	.909	3.635	7.271	1.25	16	359.3	3.496	13.92	27.84	4.80
20	1322.5	.945	3.718	7.561	1.30	30	348.5	3.606	14.35	28.70	4.95
30	1273.6	.982	3.926	7.852	1.35	17	338.3	3.716	14.78	29.56	5.10
40	1228.1	1.018	4.071	8.143	1.40	18	319.6	3.935	15.64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	19	302.9	4.155	16.51	33.01	5.70
5	1146.3	1.091	4.362	8.724	1.50	20	287.9	4.374	17.37	34.73	6.00
10	1109.3	1.127	4.507	9.014	1.55	21	274.4	4.594	18.22	36.44	6.30
20	1074.7	1.164	4.653	9.305	1.60	22	262.0	4.814	19.08	38.16	6.60
30	1042.1	1.200	4.798	9.596	1.65	23	250.8	5.025	19.94	39.87	6.90
40	1011.5	1.237	4.943	9.886	1.70	24	240.5	5.255	20.79	41.58	7.20
50	982.6	1.273	5.088	10.18	1.75	25	231.0	5.476	21.64	43.28	7.50
6	955.4	1.309	5.234	10.47	1.80	26	222.3	5.697	22.50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	27	214.2	5.918	23.35	46.69	8.10
20	905.1	1.382	5.524	11.05	1.90	28	206.7	6.139	24.19	48.38	8.40
30	881.9	1.418	5.669	11.34	1.95	29	199.7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	30	193.2	6.583	25.88	51.76	9.00

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

IV

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
31°	1589.0	216.8	41°	2142.2	387.4	51°	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32	1643.0	230.9	42	2199.4	407.6	52	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33	1697.2	246.1	43	2257.0	428.5	53	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34	1751.7	261.8	44	2314.9	450.0	54	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35	1806.6	278.1	45	2373.3	472.1	55	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.8	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36	1861.7	294.9	46	2432.1	494.8	56	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37	1917.1	312.2	47	2491.3	518.2	57	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38	1972.9	330.2	48	2551.0	542.2	58	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.2	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39	2029.0	348.6	49	2611.2	566.9	59	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40	2085.4	367.7	50	2671.8	592.3	60	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV Tangents and External to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62	3442.7	954.8	72	4162.8	1352.6	82	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63	3511.1	990.2	73	4239.7	1398.0	83	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64	3580.3	1026.6	74	4317.6	1444.6	84	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65	3650.2	1063.9	75	4396.5	1492.4	85	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66	3720.9	1102.2	76	4476.5	1541.4	86	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67	3792.4	1141.4	77	4557.6	1591.6	87	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68	3864.7	1181.6	78	4639.8	1643.0	88	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69	3937.9	1222.7	79	4723.2	1695.8	89	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70	4011.9	1265.0	80	4807.7	1749.9	90	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

TABLE IV. — Tangents and Externals to a 1° Curve.

Angle	Tangent	External	Angle	Tangent	External	Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20	5864.6	2469.3	20	6992.0	3310.1	20	8388.9	4429.2
30	5881.7	2481.5	30	7012.7	3326.1	30	8415.1	4450.9
40	5898.8	2493.8	40	7033.6	3342.3	40	8441.5	4472.7
50	5916.0	2506.1	50	7054.5	3358.5	50	8468.0	4494.6
92	5933.2	2518.5	102	7075.5	3374.9	112	8494.6	4516.6
10	5950.5	2531.0	10	7096.6	3391.2	10	8521.3	4538.8
20	5967.9	2543.5	20	7117.8	3407.7	20	8548.1	4561.1
30	5985.3	2556.0	30	7139.0	3424.3	30	8575.0	4583.4
40	6002.7	2568.6	40	7160.3	3440.9	40	8602.1	4606.0
50	6020.2	2581.3	50	7181.7	3457.6	50	8629.3	4628.6
93	6037.8	2594.0	103	7203.2	3474.4	113	8656.6	4651.3
10	6055.4	2606.8	10	7224.7	3491.3	10	8684.0	4674.2
20	6073.1	2619.7	20	7246.3	3508.2	20	8711.5	4697.2
30	6090.8	2632.6	30	7268.0	3525.2	30	8739.2	4720.3
40	6108.6	2645.5	40	7289.8	3542.4	40	8767.0	4743.6
50	6126.4	2658.5	50	7311.7	3559.6	50	8794.9	4766.9
94	6144.3	2671.6	104	7333.6	3576.8	114	8822.9	4790.4
10	6162.6	2684.7	10	7355.6	3594.2	10	8851.0	4814.1
20	6180.2	2697.9	20	7377.8	3611.7	20	8879.3	4837.8
30	6198.3	2711.2	30	7399.9	3629.2	30	8907.7	4861.7
40	6216.4	2724.5	40	7422.2	3646.8	40	8936.3	4885.7
50	6234.6	2737.9	50	7444.6	3664.5	50	8965.0	4909.9
95	6252.8	2751.3	105	7467.0	3682.3	115	8993.8	4934.1
10	6271.1	2764.8	10	7489.6	3700.2	10	9022.7	4958.6
20	6289.4	2778.3	20	7512.2	3718.2	20	9051.7	4983.1
30	6307.9	2792.0	30	7534.9	3736.2	30	9080.9	5007.8
40	6326.3	2805.6	40	7557.7	3754.4	40	9110.3	5032.6
50	6344.8	2819.4	50	7580.5	3772.6	50	9139.8	5057.6
96	6363.4	2833.2	106	7603.5	3791.0	116	9169.4	5082.7
10	6382.1	2847.0	10	7626.6	3809.4	10	9199.1	5107.9
20	6400.8	2861.0	20	7649.7	3827.9	20	9229.0	5133.3
30	6419.5	2875.0	30	7672.9	3846.5	30	9259.0	5158.8
40	6438.4	2889.0	40	7696.3	3865.2	40	9289.2	5184.5
50	6457.3	2903.1	50	7719.7	3884.0	50	9319.5	5210.3
97	6476.2	2917.3	107	7743.2	3902.9	117	9349.9	5236.2
10	6495.2	2931.6	10	7766.8	3921.9	10	9380.5	5262.3
20	6514.3	2945.9	20	7790.5	3940.9	20	9411.3	5288.6
30	6533.4	2960.3	30	7814.3	3960.1	30	9442.2	5315.0
40	6552.6	2974.7	40	7838.1	3979.4	40	9473.2	5341.5
50	6571.9	2989.2	50	7862.1	3998.7	50	9504.4	5368.2
98	6591.2	3003.8	108	7886.2	4018.2	118	9535.7	5395.1
10	6610.6	3018.4	10	7910.4	4037.8	10	9567.2	5422.1
20	6630.1	3033.1	20	7934.6	4057.4	20	9598.9	5449.2
30	6649.6	3047.9	30	7959.0	4077.2	30	9630.7	5476.5
40	6669.2	3062.8	40	7983.5	4097.1	40	9662.6	5504.0
50	6688.8	3077.7	50	8008.0	4117.0	50	9694.7	5531.7
99	6708.6	3092.7	109	8032.7	4137.1	119	9727.0	5559.4
10	6728.4	3107.7	10	8057.4	4157.3	10	9759.4	5587.4
20	6748.2	3122.9	20	8082.3	4177.5	20	9792.0	5615.5
30	6768.1	3138.1	30	8107.3	4197.9	30	9824.8	5643.8
40	6788.1	3153.3	40	8132.3	4218.4	40	9857.7	5672.3
50	6808.2	3168.7	50	8157.5	4239.0	50	9890.8	5700.9
100	6828.3	3184.1	110	8182.8	4259.7	120	9924.0	5729.7
10	6848.5	3199.6	10	8208.2	4280.5	10	9957.5	5758.6
20	6868.8	3215.1	20	8233.7	4301.4	20	9991.0	5787.7
30	6889.2	3230.8	30	8259.3	4322.4	30	10025.0	5817.0
40	6909.6	3246.5	40	8285.0	4343.6	40	10059.0	5846.5
50	6930.1	3262.3	50	8310.8	4364.8	50	10093.0	5876.1

Table V. Corrections for use with table IV,

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For Tangents Add														
ANGLE	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.10	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34

For Externals Add														
ANGLE	CURVE 5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.266	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96

VIII

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R — sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

CURVE FORMULAS.

$$T = R \tan \frac{1}{2} I$$

$$T = \frac{50 \tan \frac{1}{2} I}{\text{Sin. } D}$$

$$\text{Sin. } D = \frac{50}{R}$$

$$\text{Sin. } D = \frac{50 \tan \frac{1}{2} I}{T}$$

$$R = T \cot. \frac{1}{2} I$$

$$R = \frac{50}{\text{Sin. } D}$$

$$E = R \text{ ex. sec. } \frac{1}{2} I$$

$$E = T \tan \frac{1}{4} I$$

$$\text{Chord def.} = \frac{\text{chord}^2}{R}$$

$$\text{No. chords} = \frac{\frac{1}{2} I}{D}$$

$$\text{Tan. def.} = \frac{1}{2} \text{ chord def.}$$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance: Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.— Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10. $10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. 25. $25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875 =$ Base.

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

Natural Sines

deg.	0'	10'	20'	30'	40'	50'	deg.	0'	10'	20'	30'	40'	50'	deg.	
0	0000	0029	0058	0087	0116	0145	89	140	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1279	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10

deg.	0'	10'	20'	30'	40'	50'	deg.
80	9848	9853	9858	9863	9868	9872	9
81	9877	9881	9886	9890	9894	9899	8
82	9903	9907	9911	9914	9918	9922	7
83	9925	9929	9932	9936	9939	9942	6
84	9945	9948	9951	9954	9957	9959	5
85	9962	9964	9967	9969	9971	9974	4
86	9976	9978	9980	9981	9983	9985	3
87	9986	9988	9989	9990	9992	9993	2
88	9994	9995	9996	9997	9997	9998	1
89	9998	9999	9999	9999	I.0000	I.0000	0

Natural Cosines

110 96.3 x 50 =
 1146.3

X

Natural Tangents

deg.	0'	10'	20'	30'	40'	50'	deg.	0'	10'	20'	30'	40'	50'	deg.	
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642	49
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952	48
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271	47
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601	46
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942	45
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295	44
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0599	1.0661	43
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041	42
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436	41
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847	40
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276	39
11	1944	1974	2004	2035	2065	2095	78	51	1.2349	1.2423	1.2497	1.2572	1.2647	1.2723	38
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190	37
13	2309	2339	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3434	1.3514	1.3597	1.3680	36
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193	35
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4735	34
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301	33
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900	32
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534	31
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205	30
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917	29
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676	28
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486	27
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353	26
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283	25
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286	24
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369	23
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545	22
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826	21
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228	20
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770	19
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475	18
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371	17
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495	16
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891	15
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617	14
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747	13
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382	12
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658	11
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764	10
deg.	60'	50'	40'	30'	20'	10'	deg.	60'	50'	40'	30'	20'	10'	deg.	

deg.	0'	10'	20'	30'	40'	50'	deg.
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3138	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.711	11.059	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.77	0
deg.	60'	50'	40'	30'	20'	10'	deg.

Natural Cotangents

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

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