

PLAN SURVEY.
CO. RD. "E" CONN.

From Lexington Avenue
To Anoka Cut-off.

CO. PROJ. N^o 26-07
FILE N^o 5

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 2/27/26

File No. "5"

H2. Mine. Co. Road. "E" Connection

Transit Notes. - 2 Pages.

ANOKA CUT-OFF

±

Station

Ang. ht. Ang. Rt.

228 + 00 P.O.T.

217 + 25⁸ ✓ P.T.

215 + 63.7 P.I. 89°50'

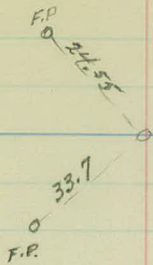
212 + 76⁶ ✓ P.C.

212 + 53.1 P.O.T.

N 59° 32' W ✓

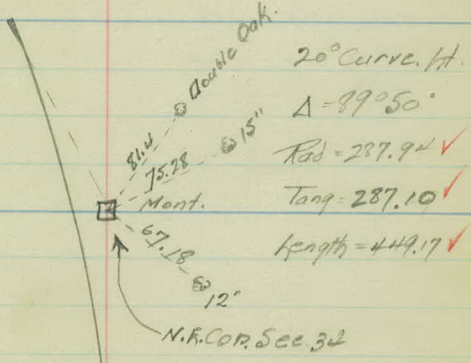
x

N 00° 18' E ✓



Sta. - Def.

- 212+76° - 0°00'
- 213+00 - 2°20'
- +50 - 7°20'
- 214+00 - 12°20'
- +50 - 17°20'
- 215+00 - 22°20'
- +50 - 27°20'
- 216+00 - 32°20'
- +50 - 37°20'
- 217+00 - 42°20'
- +25.8 - 44°55'



Hexington Ave

Sta. Point H. Rt.

N 18° 03' W ✓

259+03¹ ✓ P.C.C. = H. line P.C. 259+03¹

257+41⁸ P.I.

71°-29'

x

255+19⁵ ✓ P.C.

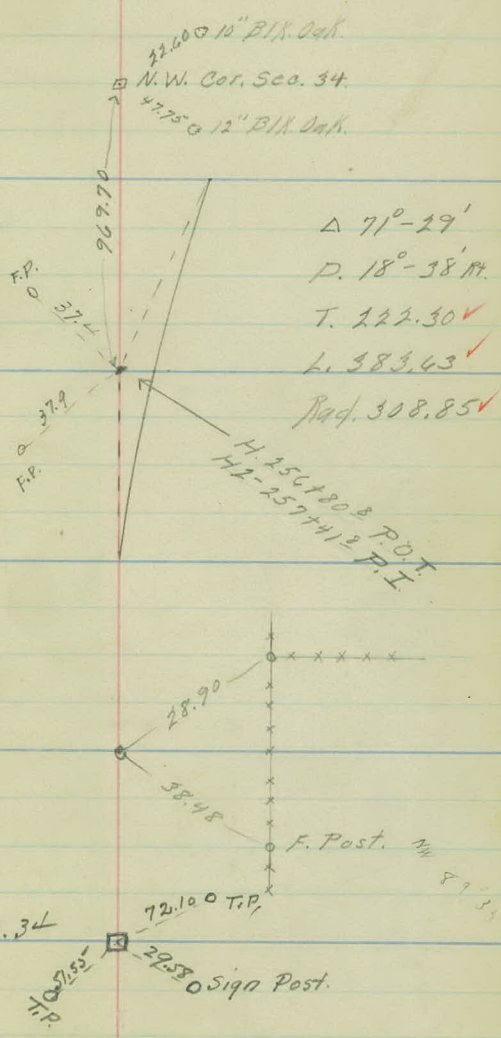
N 89° 32' W ✓

249+63⁶ P.O.T.

240+74¹ P.O.T. Mont & Hamline Ave.

H² Line.

- 259703⁺00-00
- 259700-0°-17³'
- 258750-4°-56⁸'
- 258700-9°-36³'
- 257750-14°-15²'
- 257700-18°-55³'
- 256750-23°-34⁸'
- 256700-28°-14³'
- 255750-32°-53⁸'
- 255719⁵-35°-44⁵'



32.60° 10" B.I.K. Oak.
 N.W. Cor. Sec. 34.
 47.75° 12" B.I.K. Oak.

Δ 71°-29'
 P. 18°-38' M.
 T. 222.30 ✓
 L. 383.43 ✓
 Rad. 308.85 ✓

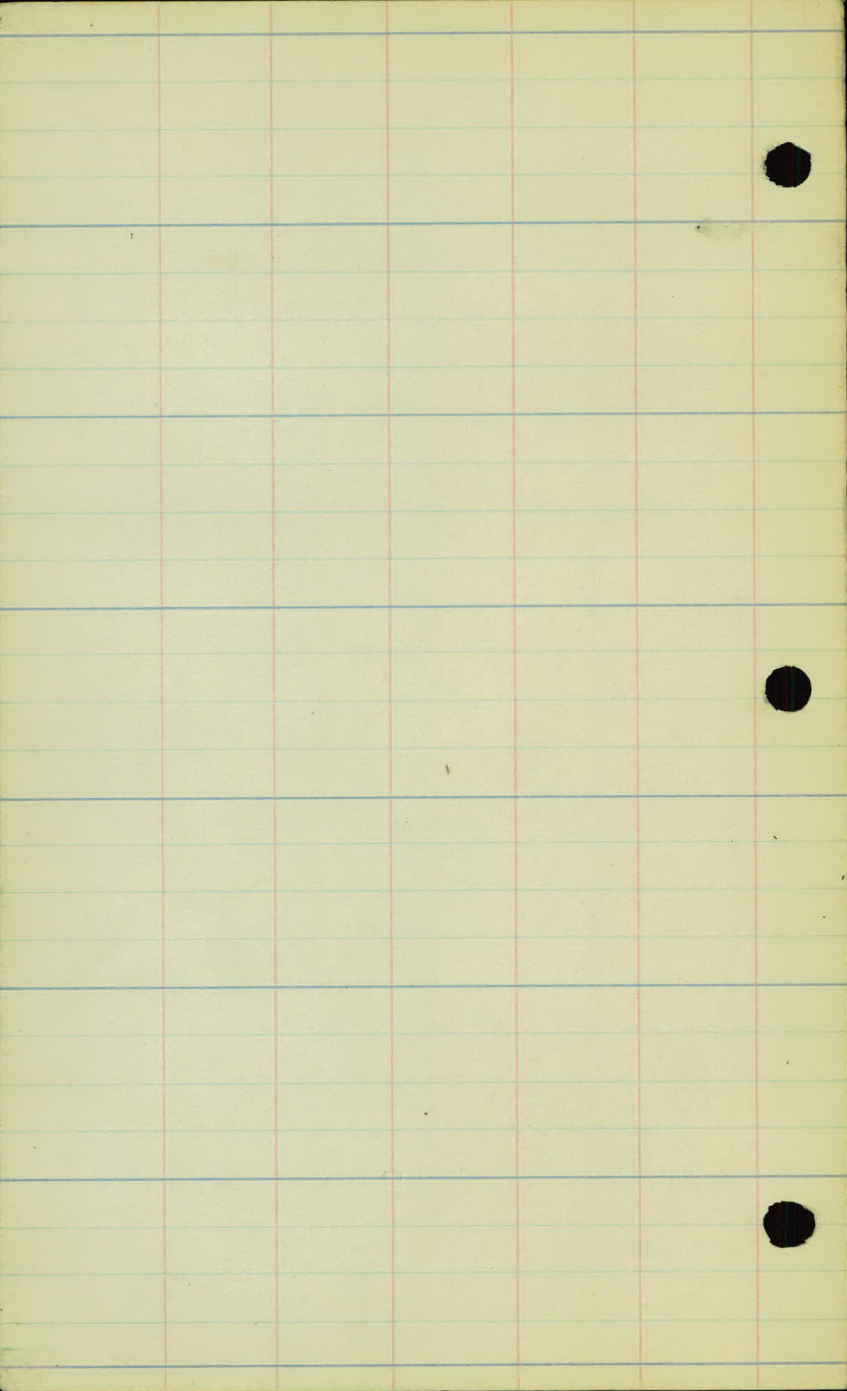
H 256780.8 P.O.T.
 H 257741.2 P.I.

No. 1/4 Cor. Sec. 34

70.55°
 T.I.P.

72.10° T.I.P.
 2930 Sign Post.

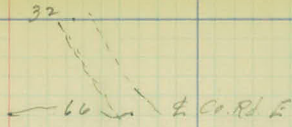
F. Post. 1/4
 89° 35'



H² line

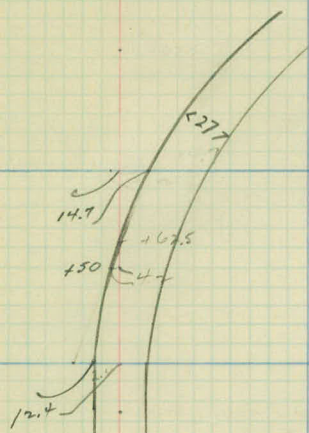
32

216



7

215



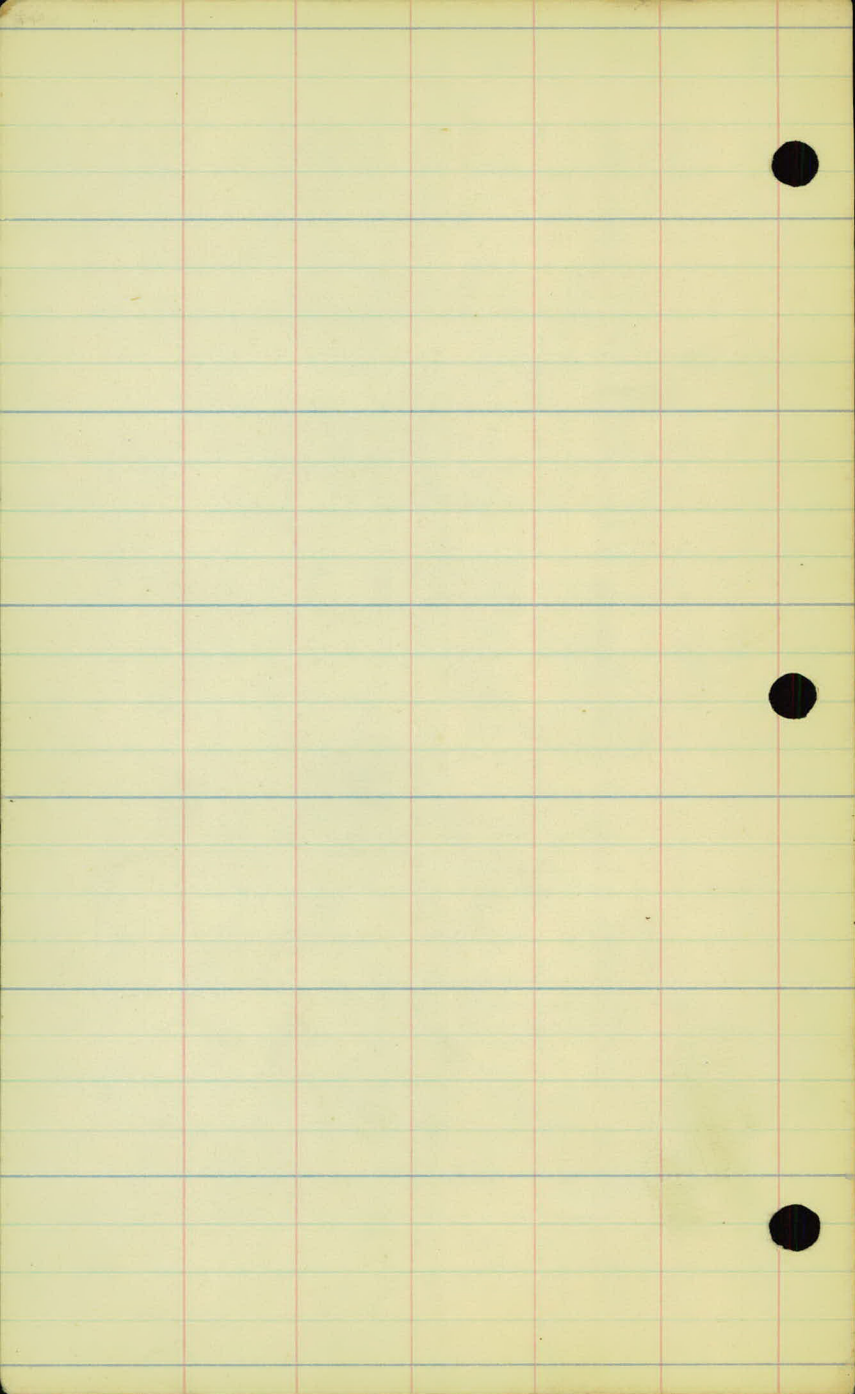
214

213

227.7

212

2 Hoxington Ave.



H2 line.

⊕

228

125 T.P. 16' H

222

100 T.P. 15.5 H

221

81 T.P. 16' H

220

155 T.P. 16' H

219

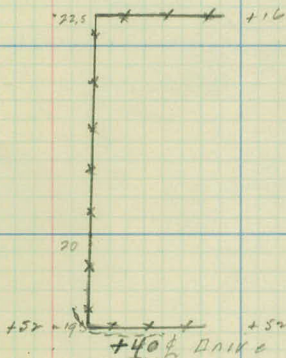
130 T.P. 16' H

218

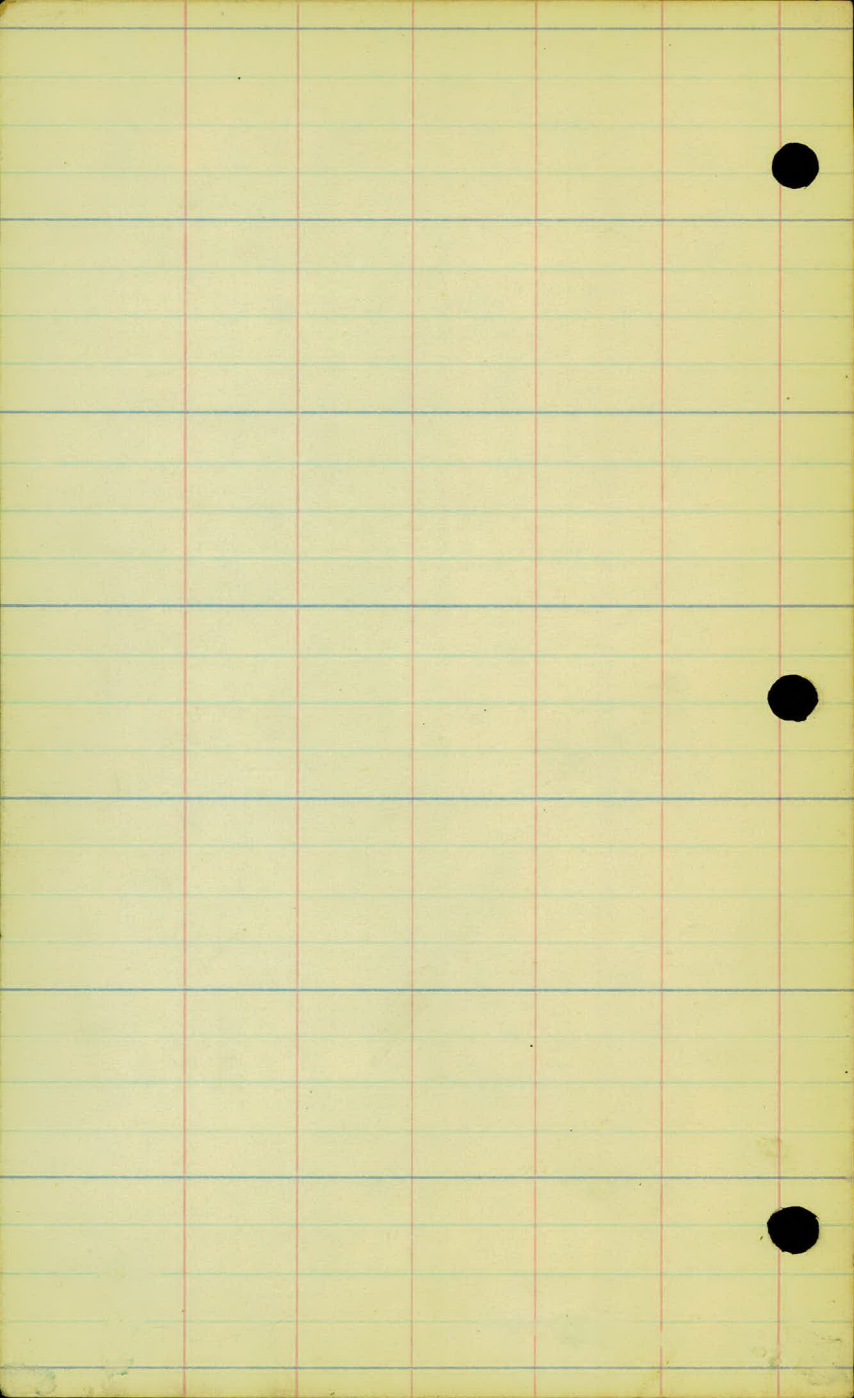
217

104 T.P. 11' R 216

Cultivated
Co. Road "E"
Cultivated



Co. Rd. "E"



H2 line

230

20'



229

+96 T.P. 15.5

20

228

+60 T.P. 16.5

+57 + + + 185 +57

19'

227

Cultivated

226

+25 T.P. 15.5

Cultivated

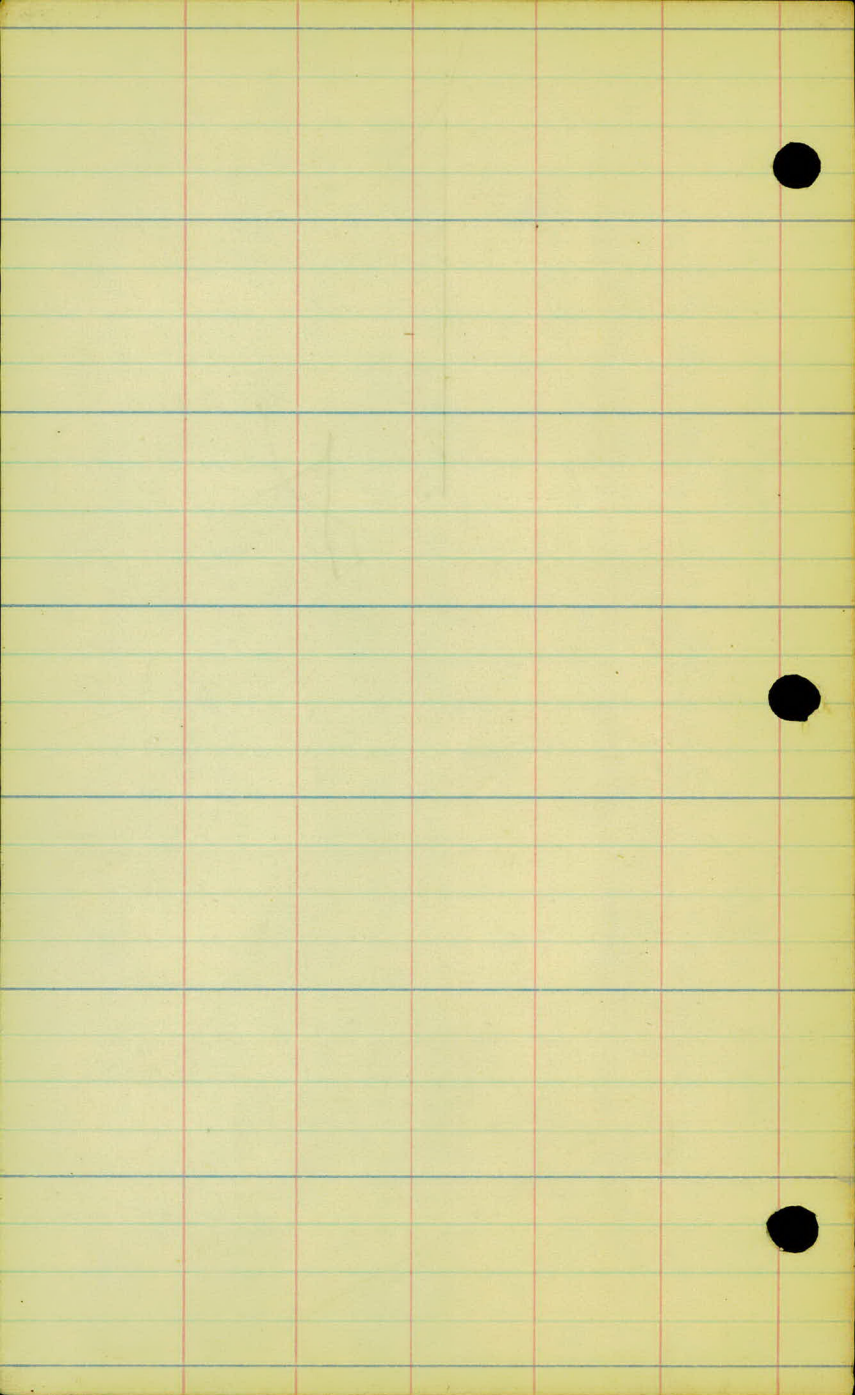
225

+92 T.P. 15

224

+54 T.P. 15.5

223



H2 line

287

+31 T.P. 16' ht

26'

286

26'

Cultivated hand

+07 T.P. 16' ht

27'

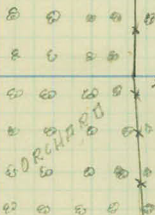
285

284

+85 T.P. 15.5 ht

27'

Cultivated hand



283

+60 T.P. 15.5

27'

282

27'

12x18 Shed



+70

+35 T.P. 15.5

23'

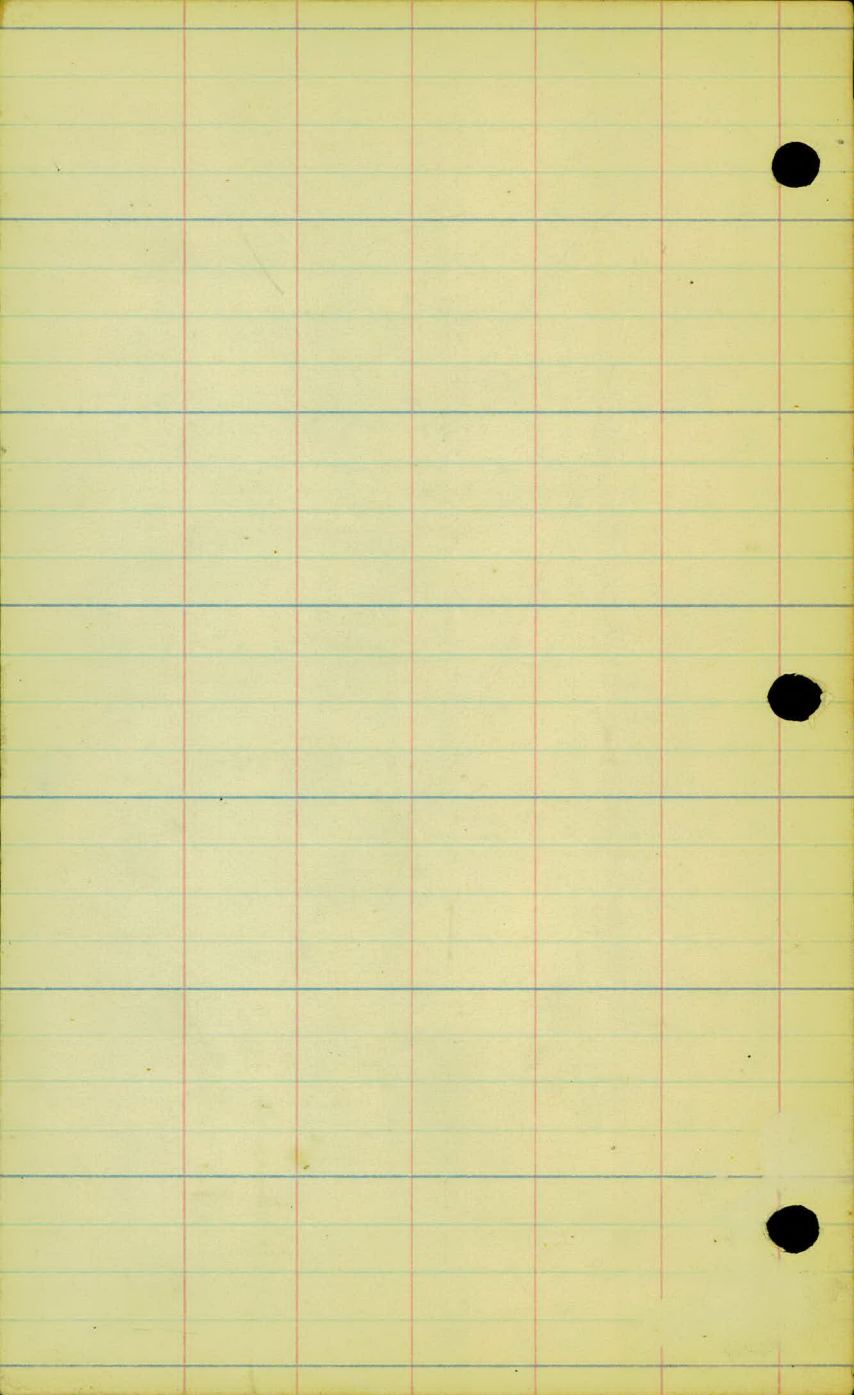
281

20'

+43 1/2 Hoive

+10 T.P. 15.5 ht

280



H₂ line.

241

23 21



243

23 21

+15 Farm Entrance

22'

+29 Box Fence

242

25

37 - +36



91'

+67

+25 +99 End Colv.

241

+74 1/2 Hamline Ave.



36'

+50

+59 End Colv. +54 Rd. sign 21.5 R/L

(15" x 40' Colv. C.M.P.)

+25 T.P. 16.561

240



239

25'

+26 T.P. 17.47

Cultivated.

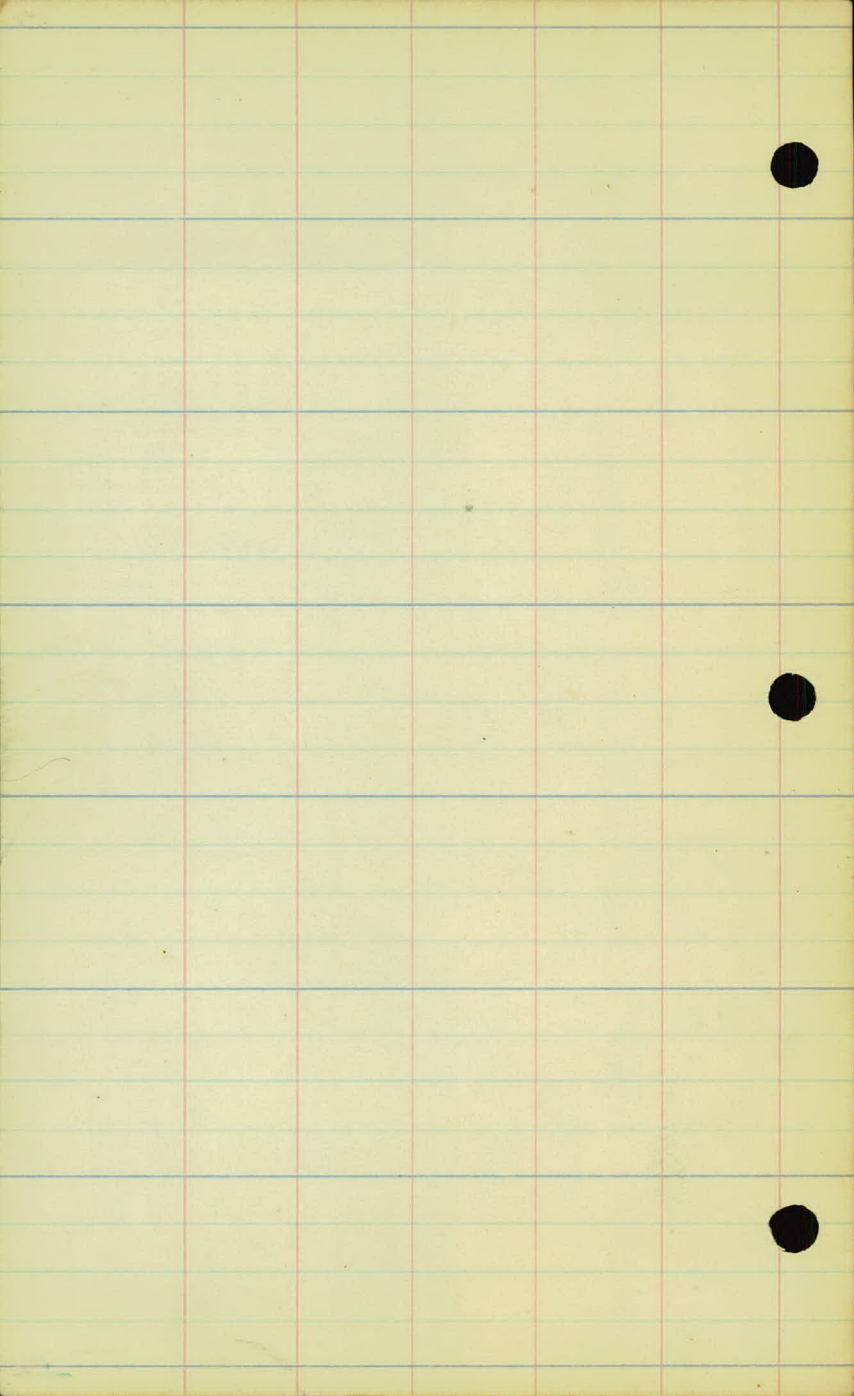
Cultivated

238

25'

+27 T.P. 165

237



H2 line

251

Timber

24.5 20'

28.5

23.5

22

+66 Farm Entrance

22 34'

22 34'

22 28.5
22 +75

23 20'

+77 (12" C.M.P)

Not located

23' 21'

250

249

248

247

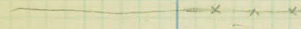
246

245

204

Cultivated

Cultivated



#

67

84

72

34

14'

9'

Ha line

259

Marsh

+50 Edge, Marsh

257

+50 Fence Xing

256

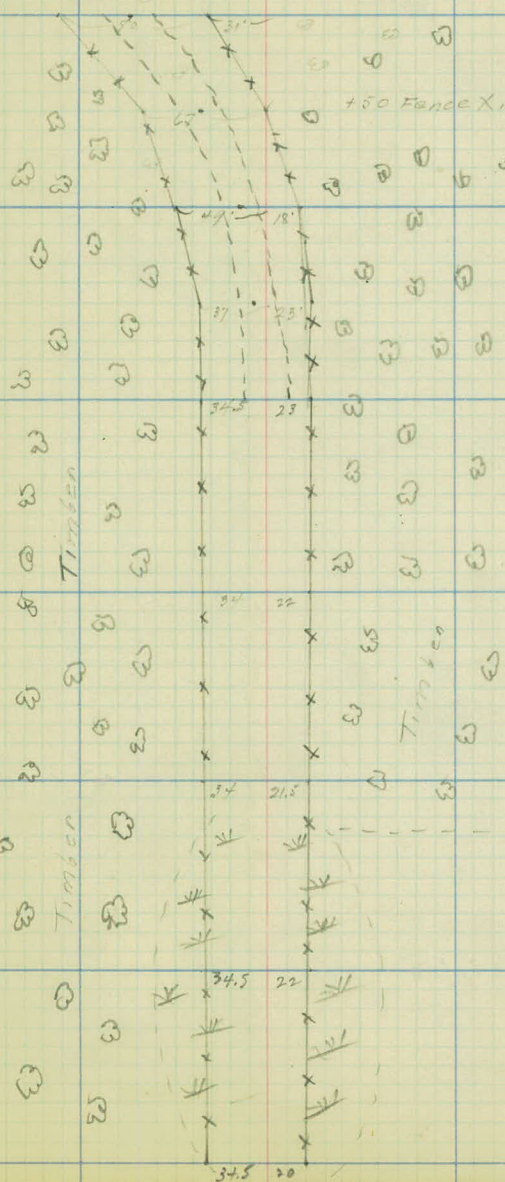
255

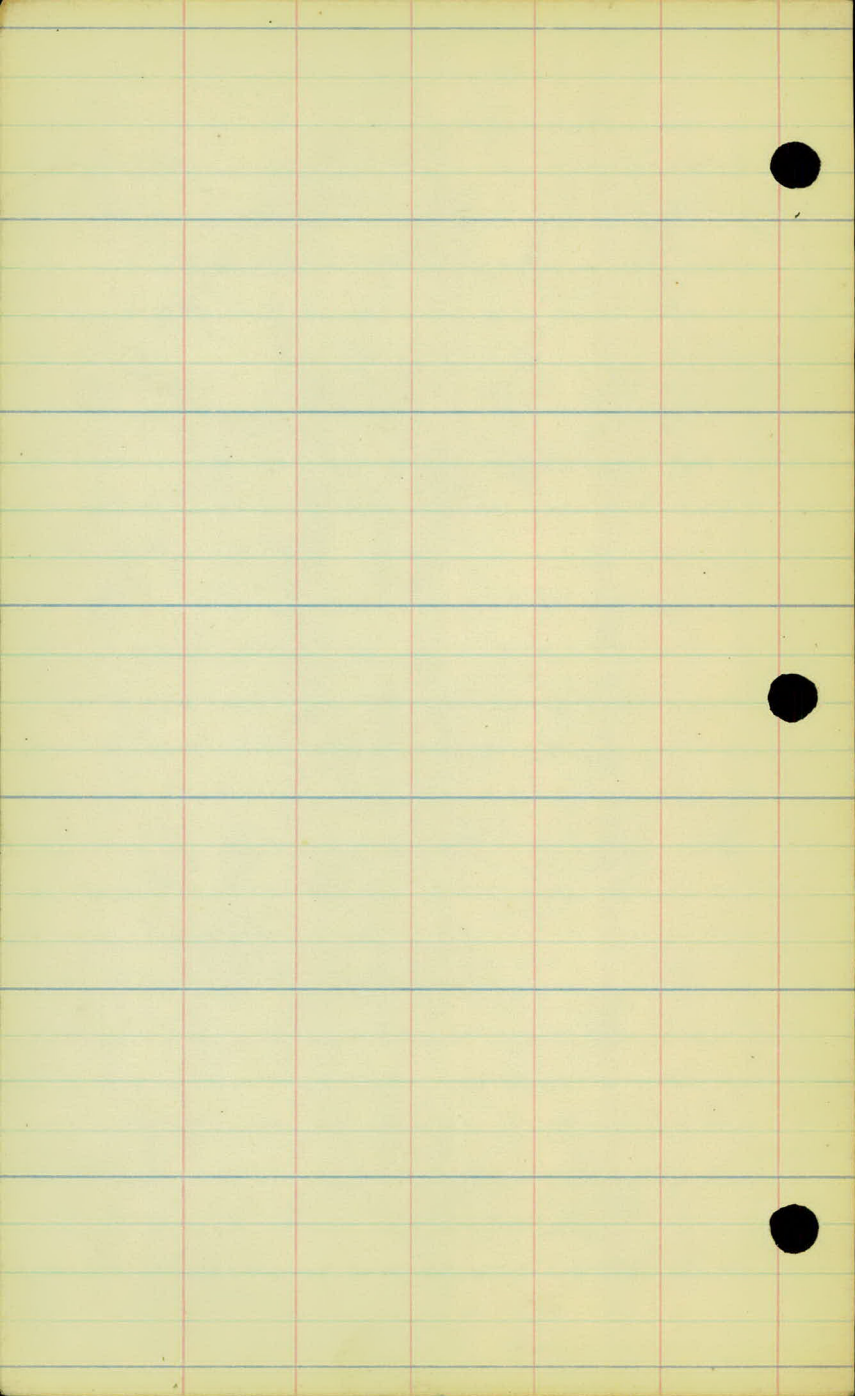
254

253

252

251





H2 hinc.

259



+25 Edge Marsh



251

$$\begin{array}{r} 287.94 \\ .99.71 \\ \hline 287.94 \\ 201.558 \\ 259.146 \\ 259.146 \\ \hline 287.104974 \end{array}$$

$$\begin{array}{r} 287.94 \\ .99.71 \\ \hline 287.94 \\ 201.558 \\ 259.146 \\ 259.146 \\ \hline 287.104974 \\ 256.227948 \\ \hline .877926 \end{array}$$

$$\begin{array}{r} 23.4 \\ 6 \\ \hline 1404 \\ 120 \\ \hline 2026 \\ 25.8 \\ 6 \\ \hline 154.8 \\ 120 \\ \hline 34.8 \end{array}$$

$$\begin{array}{r} 212+76.6 \quad - \quad 0000' \\ 213+00 \quad - \quad 2020' \\ +50 \quad - \quad 7020' \\ 214+00 \quad - \quad 12020' \\ +50 \quad - \quad 17020' \\ 215+00 \quad - \quad 22020' \\ +50 \quad - \quad 27020' \\ 216+00 \quad - \quad 32020' \\ +50 \quad - \quad 37020' \\ 217+00 \quad - \quad 42020' \\ +25.8 \quad - \quad 44055' \end{array}$$

$$\begin{array}{r} 214+39.7 \\ 2+87.1 \\ \hline 217+25.8 \checkmark \\ 4+49.2 \\ \hline 212+76.6 \\ 2+87.1 \\ \hline 215+63.7 \checkmark \end{array}$$

H² Line

Center line levels
from Sta. 210+00 to Sta. 259+03.

Sta.	+	H.I.	-	Rod.	Elev.
B.M.	0.76	953.07 ✓		952.31 ✓	
210		On Pavement		7.66	745.41.
	+50	"		6.50	945.77 946.77
211		"		4.75	748.12.
	+50	"		3.92	749.15.
212		"		3.23	749.84.
	+50	"		2.95	750.09.
	+76 ²	P.C.		3.00	750.07.
213		"		3.02	750.05.
	+50	"		3.42	749.65.
	+62 ⁵	Edge of Pavement		3.69	749.38.
	+78			4.1	749.0.
	+84			5.6	747.5.
214				6.1	747.0.
	+06			4.2	748.9.
	+15			4.6	748.5.
	+50			5.6	744.5.
T.P.	3.38	945.01 ✓	11.44	941.65 ✓	
215				4.6	740.4.
	+50			6.7	738.3.
216				6.5	738.5.
	+21			5.2	739.8.
	+29			3.4	741.6.
	+50			3.5	741.5.
217				4.0	741.0.
	+15 ⁸	P.T.		4.1	740.9.
	+50			4.4	740.6.

1/28/25

H² Line

Spk. in 30" Oak, 65' Pt. Sta. 213+40.

46.69
 $\frac{4.58}{14.7} = \text{Edge of Pavement.}$

Sta.	+	H.I.	-	Red.	Elev.
		745.01			
218				48	940.2
	+50			54	939.4
219				63	938.7
	+50			73	937.7
220				80	937.0
	+50			84	935.6
221				85	936.5
T.P.	6.74	943.48	8.17	936.74	
	+50			63	937.2
222				60	937.5
	+50			53	938.2
223				45	939.0
	+50			42	939.3
224				40	939.5
	+50			41	939.4
225				48	938.7
	+50			53	938.2
226				57	937.8
	+50			54	939.1
227				55	938.0
	+50			53	938.2
228				52	938.3
	+50			51	938.4
T.P.	1.21	940.78	4.91	938.57	
229				1.4	938.4
	+50			2.8	938.0

H² Line.

1/28/25

Sta.	+	H.I. ✓ 940.78	-	Rod.	Elev.
230				3.5	937.3.
+50				1.8	937.0.
B.M.			4.45	934.53 ✓	
231				4.3	936.5.
+50				4.8	936.0.
232				5.7	935.4.
+50				5.3	935.5.
+88				5.7	935.1.
233				6.0	934.8.
+50				8.1	932.7.
234				8.9	931.9.
+50				10.0	930.8.
+80				11.0 ✓	929.8.
T.P.	0.59	930.13 ✓	11.24	929.54	
235				13	928.8.
+50				3.4	926.7.
236				4.7	925.4.
+50				5.4	924.5.
237				5.9	924.2.
+50				5.8	924.3.
238				5.7	924.4.
+50				5.4	924.7.
239				4.8	925.3.
T.P.	7.58	934.98 ✓	4.75	925.40 ✓	
+50				8.5	926.5.
240				6.9	928.1.

1/28/25

H² Line.

Spk. in 4" Poplar 40' Lt. Sta 130+85.

Sta.	+	H.I.	-	Red.	Elev.
		734.98			
	+50			5.3	929.7.
P.M.	4.48	934.24	3.23	931.76	
	+74	Center of Hamilton Ave.		5.4	930.4.
241				5.0	931.2.
	+50			3.9	932.3.
242				3.5	932.7.
	+50			3.7	932.3.
243				4.3	931.9.
	+50			4.8	931.4.
244				5.1	931.1.
T.P.	2.61	941.93	4.92	931.32	
	+50			2.5	931.4.
245				8.4	932.3.
	+50			2.2	933.7.
246				6.0	934.9.
	+50			4.0	936.9.
247				2.3	938.4.
	+50			0.8	940.1.
T.P.	5.41	945.82	0.51	940.41	
248				4.3	941.5.
	+50			2.8	943.0.
249				2.7	943.1.
	+50			2.6	943.2.
250				3.1	942.7.
	+50			4.2	941.4.
251				5.2	940.6.

1/28/25

H. 2 Line.

Spk. in T.P. 100 ft. 519. 440 + 95.

$\frac{7.1}{300}$	$\frac{6.8}{150}$	$\frac{6.4}{100}$	$\frac{5.5}{50}$	$\frac{5.3}{50}$	$\frac{5.1}{100}$	$\frac{5.5}{150}$	$\frac{6.0}{200}$
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Sta.	+	H.I.	-	Red.	Elev.
		745.82			
	+50			4.1	939.7
B.M.			6.54	939.28	
152				6.6	939.2
	+50			7.1	938.7
153				7.4	938.4
	+50			8.6	937.2
154				10.2	935.4
T.P.	0.48	936.19	10.11	935.71	
	+50			2.9	933.3
155				4.7	931.5
	+19 ³			5.4	930.8
	+50			6.7	929.5
156				7.0	927.2
	+20			7.7	926.5
	+31			6.3	929.9
	+50			8.1	928.0
T.P.	0.94	927.60	9.53	926.44	
157				5.9	921.7
T.P.	4.28	922.63	11.25	916.35	
	+50			7.9	914.7
158				7.7	912.9
	+50			2.9	913.7
159				8.0	914.6
	+03 ¹	P.C.C.		8.0	914.6
B.M.			5.23	917.40	
T.P.	11.37	933.48	0.52	932.11	

1/27/25

H² Line

Spt. 10" Dg. 50' Rt. Sta. 250+25

$$Q \text{ of Rd.} = \frac{5.9}{14} \quad 927.3$$

$$Q \text{ of Rd.} = \frac{10.9}{34} \quad 925.3$$

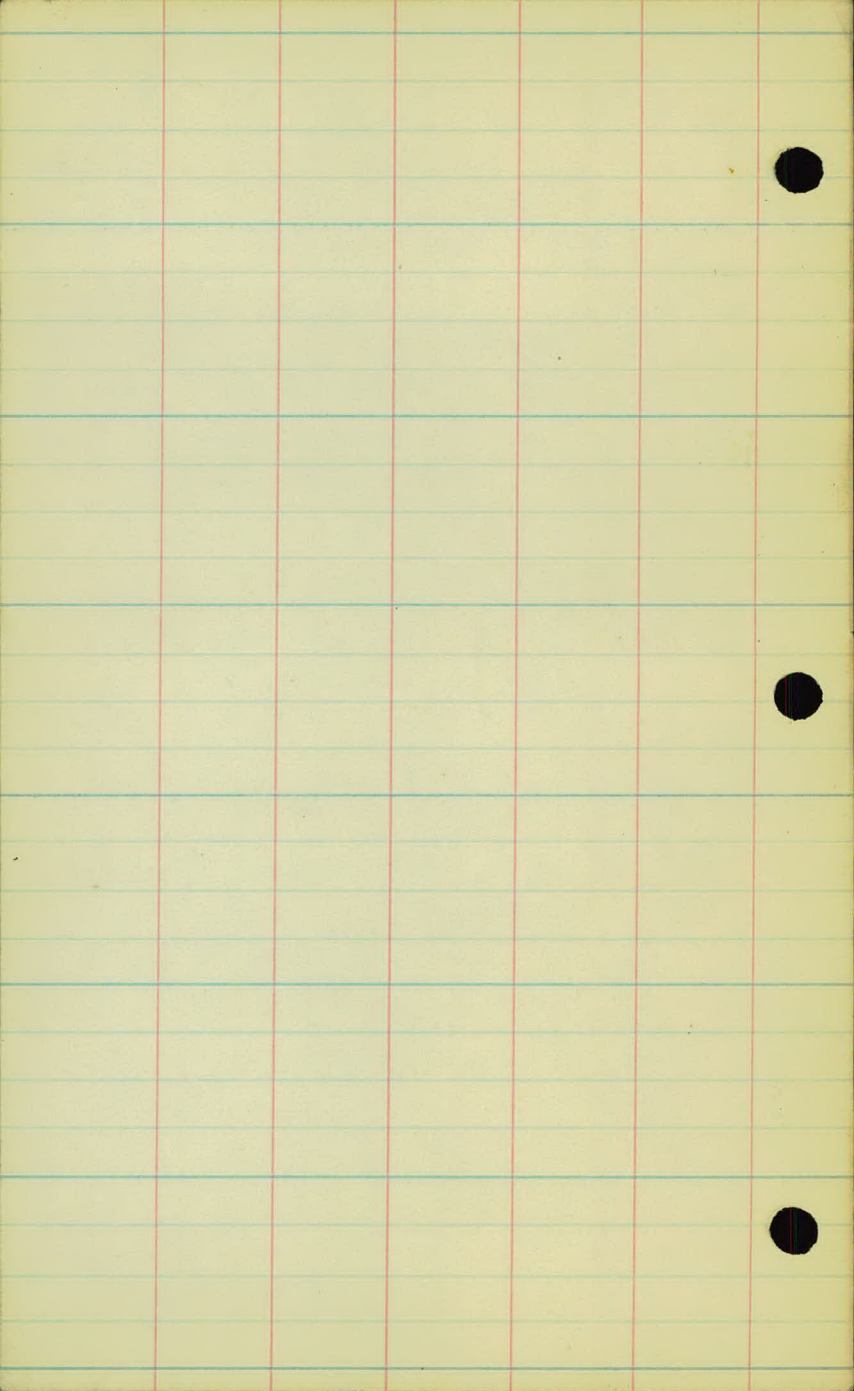
Spt. 15" Dg. 50' Rt. Sta. 258+40

Sta.	+	H.I.	-	E/cv
		933.48		
T. 1 ^o	10.05	941.67	1.84	931.62
B.M.			0.69	940.98 940.94

1/29/30

H² Line

Spk in 15" Oak 40" Pt Sta, 154+85 on H. Line.



H² Line.

Check levels from B.M. on
H. Line to beginning of H² Line.

Sta.	+	H.I.	-	Elev
B.M.	3.43	744.39		740.96
	5.86	741.59	8.64	735.73
B.M.	8.57	747.83	2.33	759.26
	0.70	737.44	11.09	736.74
	0.71	732.91	5.24	732.20
B.M.			1.17	731.74
	7.45	733.78	8.58	724.53
	8.35	741.82	0.51	733.47
B.M.			5.51	730.31
	6.20	744.43	3.59	738.23
	7.05	746.41	7.07	737.34
	8.90	754.17	1.14	745.27
B.M.			1.84	752.31

1/28/25

H² Line.

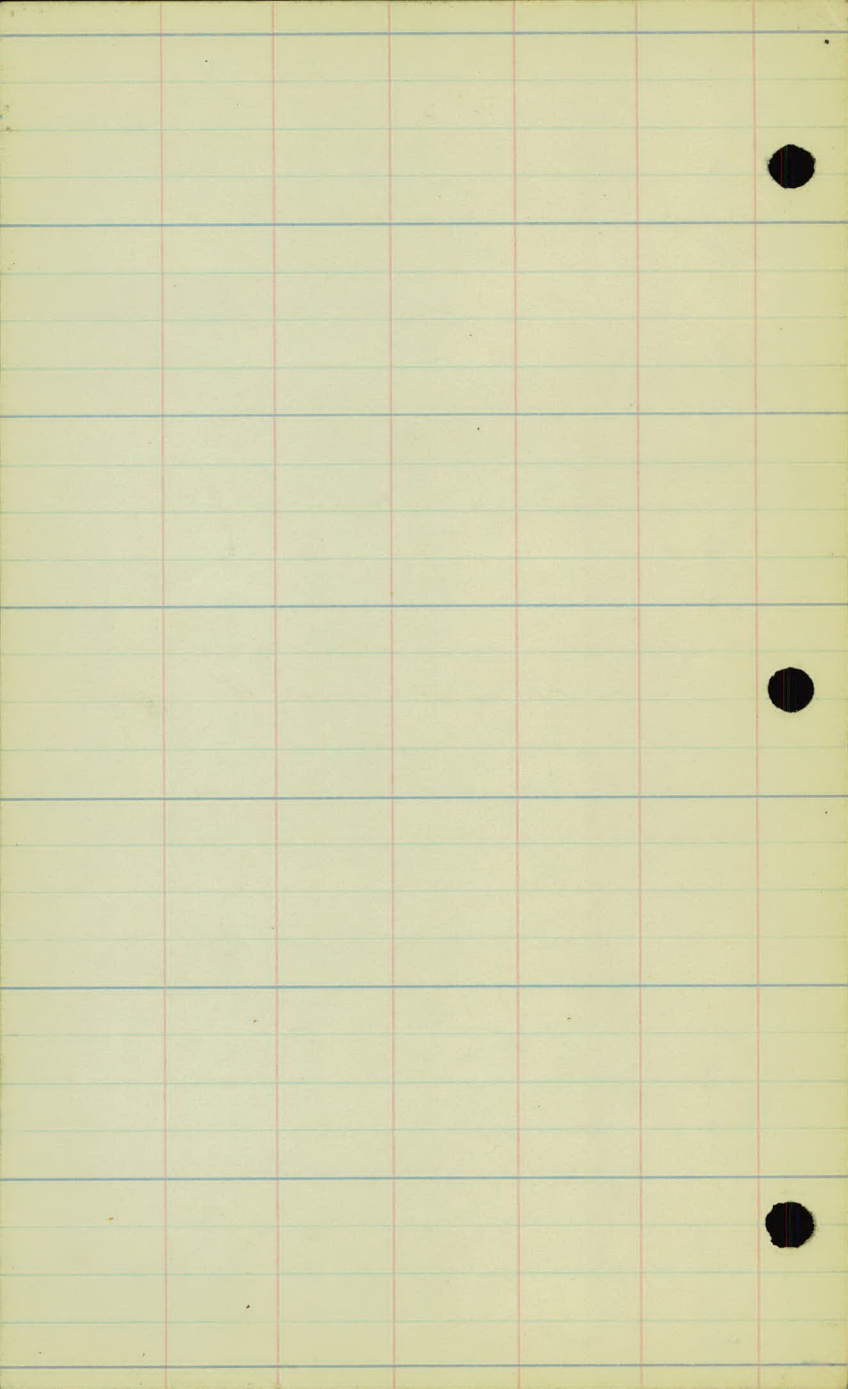
SpK. in 15" Oak. 40 Rt. Sta. 154+85 on H. Line

SpK. in 18" Oak. 50 Lt. Sta. 150+85

SpK. in T.P. 100 Rt. Sta. 140+95,

SpK. in 6" Poplar 40 Rt. Sta. 130+85.

SpK. in 50" Oak. 65 Rt. Sta. 113+40.



1/29/30

H² Line.

X sections from Sta. 212+76
to Sta. 259+03.

Sta.	+	H.I.	-	Elev.
B.M.	1.27	953.58		952.31 Elev
212 + 74 ⁶				950.1

213				50.1
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+50				49.6
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+78				49.2
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+88				46.7
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214				47.2
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+14				48.6
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+50				44.5
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215				40.4
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T.P.	4.21	946.98	10.81	942.77
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214 + 50

215				40.4
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+50				38.3
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216				38.6
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1/29/25

H² Line

$\frac{6.7}{50}$	$\frac{6.4}{33}$	$\frac{6.3}{28}$	$\frac{6.9}{27}$	$\frac{6.8}{24}$	$\frac{3.6}{17}$	3.5	$\frac{3.6}{17}$	$\frac{5.3}{19}$	$\frac{5.4}{23}$	$\frac{2.1}{29}$	$\frac{2.0}{33}$	$\frac{1.6}{50}$
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$\frac{6.5}{50}$	$\frac{6.0}{33}$	$\frac{6.3}{28}$	$\frac{6.8}{24}$	$\frac{6.8}{22}$	$\frac{3.7}{16}$	3.5	$\frac{4.0}{19}$	$\frac{5.4}{23}$	$\frac{5.4}{26}$	$\frac{3.2}{29}$	$\frac{3.1}{33}$	$\frac{2.6}{50}$
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$\frac{3.8}{50}$	$\frac{3.5}{33}$	$\frac{3.6}{20}$	$\frac{6.4}{14}$	$\frac{6.4}{12}$	$\frac{4.0}{8}$	4.0	$\frac{4.0}{14}$	$\frac{4.3}{29}$	$\frac{5.5}{33}$	$\frac{5.8}{50}$
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$\frac{4.5}{50}$	$\frac{3.8}{33}$	$\frac{3.3}{15}$	$\frac{7.3}{9}$	$\frac{6.5}{5}$	4.4	$\frac{4.6}{24}$	$\frac{5.0}{41}$	$\frac{6.0}{50}$
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$\frac{5.5}{50}$	$\frac{5.0}{33}$	$\frac{4.0}{10}$	6.9	$\frac{4.6}{5}$	$\frac{4.9}{30}$	$\frac{5.2}{48}$	$\frac{6.1}{50}$
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$\frac{10.2}{50}$	$\frac{6.9}{33}$	$\frac{4.7}{11}$	$\frac{4.8}{3}$	6.4	$\frac{7.2}{6}$	$\frac{4.8}{11}$	$\frac{5.0}{35}$	$\frac{5.3}{50}$
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$\frac{10.3}{50}$	$\frac{8.5}{33}$	$\frac{6.7}{14}$	5.0	$\frac{5.2}{5}$	$\frac{7.5}{11}$	$\frac{7.2}{16}$	$\frac{5.3}{21}$	$\frac{5.5}{50}$
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9.1	$\frac{4.8}{23}$	$\frac{4.9}{29}$	$\frac{7.9}{34}$	$\frac{7.7}{38}$	$\frac{6.0}{41}$	$\frac{5.9}{50}$
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(12.2)	$\frac{10.6}{16}$	$\frac{7.9}{33}$	$\frac{6.7}{50}$
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$\frac{8.9}{50}$	$\frac{7.8}{33}$	$\frac{5.8}{16}$	(2.9)
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$\frac{10.9}{50}$	$\frac{10.0}{33}$	$\frac{8.6}{14}$	4.6
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$\frac{12.2}{50}$	$\frac{11.0}{33}$	$\frac{10.2}{14}$	8.7	$\frac{7.0}{16}$	$\frac{5.4}{33}$	$\frac{3.2}{50}$
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$\frac{11.8}{50}$	$\frac{11.0}{33}$	$\frac{10.0}{14}$	8.4	$\frac{6.8}{14}$	$\frac{4.7}{18}$	$\frac{3.7}{37}$	$\frac{3.4}{50}$
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Sta.	+	H.I.	-	E/cv.	Elev.
		946.98			
	+31				938.9
	+50				415
217					412
	+75				404
218					403
	+50				395
219					387
T.P.	5.25	943.17	9.06	937.92	
	+75				374
220					371
	+50				367
221					366
T.P.	5.26	943.27	5.16	938.01	
B.M.			6.92	936.35	936.33

1/29/25

H² Line.

11.2	10.8	9.8				5.5	4.6	4.7	2.9	1.7
50	33	14	8.1			5	22	36	45	50

11.3	10.7	10.2	7.7	6.2		4.9	5.0	4.9	3.5	2.7	1.5
50	33	26	6	3	5.5	15	30	33	40	45	50

11.6	10.6	9.6	6.4			6.3	6.7	4.7	3.7	
50	33	18	12	5.8		15	20	32	50	

8.6	8.2	8.2	7.5			7.0	6.8	6.0	5.2	
50	33	14	13	6.4		13	20	33	50	

6.8	6.5	6.6	8.0	7.4		7.3	7.8	6.7	6.2	5.6
50	33	20	17	12	6.7	13	17	20	33	50

4.3	4.4	4.3	5.0	8.2	8.0		8.0	8.3	4.8	5.5	5.9
50	33	21	17	15	12	7.5	13	17	22	33	50

5.8	5.5	5.3	9.2	8.9		8.9	9.1	4.8	5.1	5.9
50	33	20	15	12	8.3	13	16	21	33	50

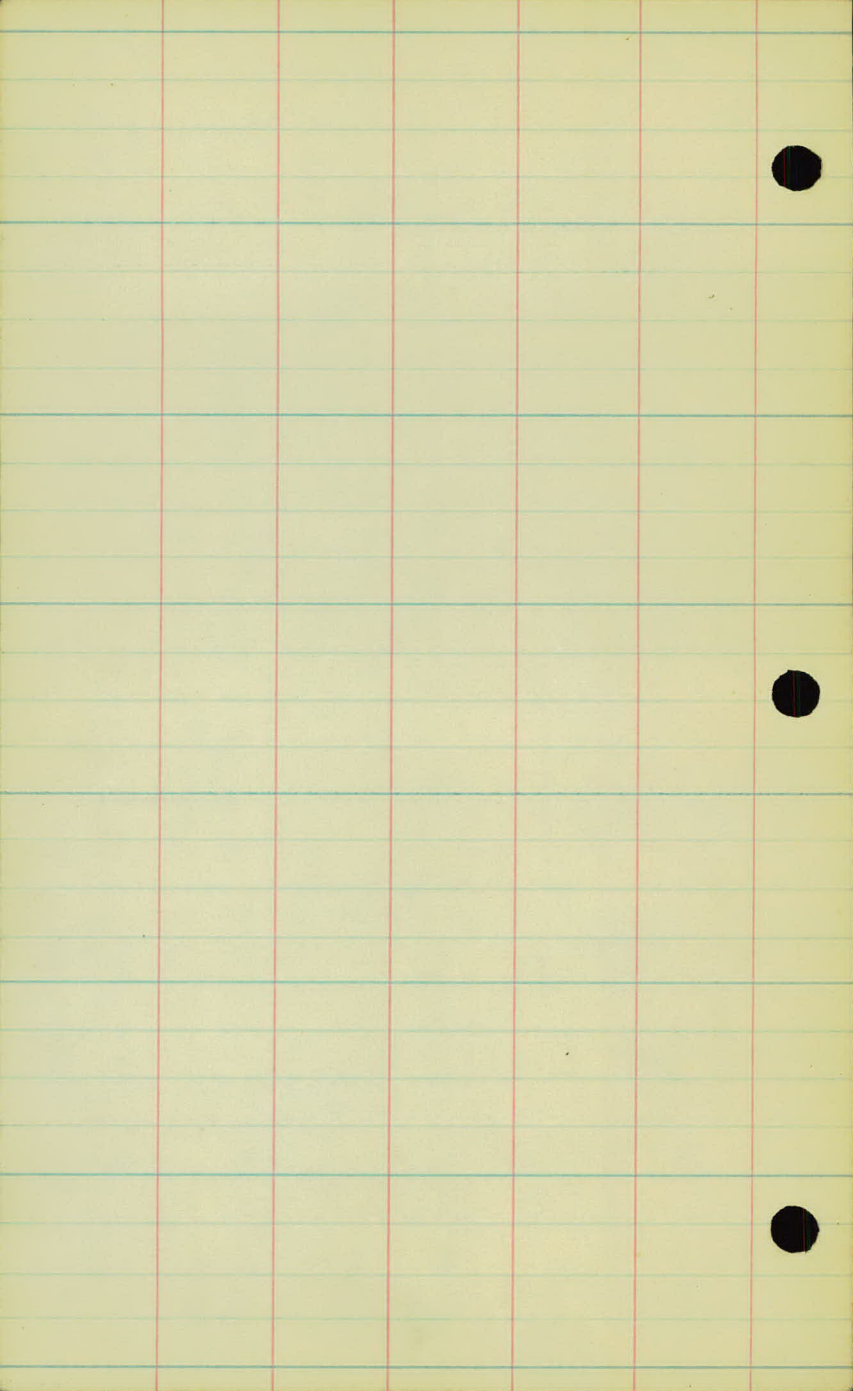
5.7	5.6	5.6	6.9	6.4		4.3	6.9	6.0	6.4	6.5
50	33	19	15	12	5.8	14	17	19	33	50

6.5	6.9	7.0	7.4	6.6		6.9	8.2	7.9	7.4	
50	33	19	17	11	4.1	14	20	33	50	

8.3	8.9	9.6	7.4			7.7	10.0	9.8	9.5	
50	33	18	15	6.5		19	23	33	50	

9.4	10.3	10.2	7.5			6.8	7.5	7.8	9.4	9.6
50	33	20	15	6.6		8	18	22	33	50

spk. in tree. 40' Lt. Sta. 230 + 85.





Sta.	+	H.I	-	Elev.
B.M.	6.97	943.30		936.33
T.P	6.38	944.40	5.28	938.02
222+00				375.
+50				38.2
223+00				38.9
+50				39.3
224+00				38.6
+50				39.4
225+00				38.7
+50				38.2
226+00				37.8
227+00				38.0
T.P.	5.24	943.26	6.38	938.02
+35				38.1
228+00				38.3
B.M.	4.92	943.25	6.93	936.33
229+00				38.3

222+00

Spike in Tree. ht. sta. 230+85

10.9	10.2	9.7	9.7	9.2	7.5	6.9	7.5	9.2	7.2	7.2	7.2
50.0	37.0	21.0	19.0	16.0	11.0	6.9	13.0	17.0	20.0	35.0	50.0

9.4	9.5	7.0	7.7	7.0	6.2	6.7	7.4	6.3	5.5	5.5
50.0	39.0	21.0	16.0	12.0	6.2	12.0	16.0	20.0	32.0	50.0

9.1	6.6	5.7	6.8	6.1	5.5	5.8	6.7	5.3	3.7	2.6
50.0	36.0	17.0	15.0	11.0	5.5	11.0	17.0	20.0	33.0	50.0

7.0	5.5	4.6	5.9	5.7	5.1	5.3	5.9	4.0	2.1	2.8
50.0	34.0	19.0	16.0	11.0	5.1	12.0	18.0	22.0	36.0	50.0

3.7	1.7	1.4	5.9	5.1	4.9	5.8	3.4	1.4	2.5	
50.0	31.0	21.0	15.0	9.0	4.9	18.0	17.0	22.0	35.0	50.0

1.8	1.8	2.6	6.4	5.5	5.0	5.5	6.3	4.0	4.2	4.8
50.0	35.0	21.0	15.0	9.0	5.0	11.0	18.0	21.0	37.0	50.0

5.3	7.1	7.3	6.4	6.0	5.7	6.1	6.7	7.1	6.7	7.3	7.1
50.0	24.0	18.0	14.0	8.0	5.7	10.0	17.0	18.0	20.0	37.0	50.0

9.0	9.0	7.3	7.0	6.7	6.2	6.5	7.0	7.4	6.5	4.8	6.1
50.0	23.0	22.0	14.0	10.0	6.2	10.0	18.0	19.0	21.0	38.0	50.0

9.4	9.7	9.7	10.5	9.6	7.4	6.9	7.0	7.2	9.1	7.0	7.2	6.6	
50.0	41.0	23.0	21.0	19.0	14.0	11.0	6.6	13.0	18.0	20.0	22.0	35.0	50.0

9.1	8.8	9.6	10.2	9.9	7.9	7.0	6.8	7.5	9.6	8.7	8.4	
50.0	35.0	23.0	22.0	19.0	14.0	11.0	6.4	12.0	16.0	18.0	36.0	50.0

9.4	9.8	9.6	7.0	5.7	5.2	5.4	5.9	6.6	6.4	6.3	6.0
50.0	20.0	16.0	13.0	9.0	5.2	10.0	14.0	16.8	18.0	22.0	50.0

3.7	3.9	4.5	5.8	5.7	5.4	5.4	5.7	4.7	4.0	3.3	
50.0	35.0	18.0	16.0	13.0	9.0	5.0	11.0	16.0	19.0	33.0	50.0

Spike in tree 40' ht. sta. 230+85

4.8	6.4	5.9	5.4	4.2	5.4	5.2	5.5	4.5	3.0	2.1	
50	33	34	17	16	10	5.0	12	15	17	33	50

Sta.	+	H.I.	-	Elev.
230		943.25		937.3
	+50			369
231				365
	+70			359
T.P.	7.53	942.77	8.01	935.24
232				354
	+45			354
233				348
	+70			323
234				319
T.P.	2.30	937.54	7.53	935.24
	+70			301
235				284
T.P.	2.25	929.11	10.68	926.86
	+50			267
236				254

H² Line

1/30/20

$\frac{6.7}{50}$	$\frac{6.9}{33}$	$\frac{6.6}{19}$	$\frac{7.0}{17}$	$\frac{6.6}{11}$	6.0	$\frac{6.1}{10}$	$\frac{6.6}{14}$	$\frac{6.0}{17}$	$\frac{5.6}{33}$	$\frac{5.7}{50}$
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$\frac{7.5}{50}$	$\frac{7.5}{33}$	$\frac{7.4}{17}$	$\frac{7.1}{13}$	6.4	$\frac{6.8}{14}$	$\frac{7.2}{15}$	$\frac{6.6}{17}$	$\frac{6.3}{33}$	$\frac{6.2}{50}$
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$\frac{8.2}{50}$	$\frac{7.6}{33}$	$\frac{7.1}{15}$	$\frac{7.3}{11}$	6.8	$\frac{7.2}{13}$	$\frac{7.8}{14}$	$\frac{6.5}{19}$	$\frac{5.8}{33}$	$\frac{5.5}{50}$
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$\frac{13.5}{50}$	$\frac{12.5}{33}$	$\frac{12.2}{21}$	$\frac{11.5}{16}$	$\frac{8.2}{11}$	7.4	$\frac{7.9}{13}$	$\frac{8.2}{17}$	$\frac{7.7}{15}$	$\frac{7.7}{33}$	$\frac{7.1}{50}$
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$\frac{12.5}{50}$	$\frac{11.8}{33}$	$\frac{9.3}{15}$	$\frac{8.1}{12}$	7.4	$\frac{7.7}{14}$	$\frac{8.3}{17}$	$\frac{7.0}{18}$	$\frac{6.2}{33}$	$\frac{4.9}{50}$
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$\frac{5.3}{50}$	$\frac{4.0}{33}$	$\frac{3.3}{13}$	$\frac{8.8}{15}$	$\frac{8.1}{12}$	7.4	$\frac{7.7}{12}$	$\frac{8.3}{14}$	$\frac{9.9}{17}$	$\frac{1.2}{27}$	$\frac{0.6}{33}$	$\frac{0.3}{50}$
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$\frac{3.7}{50}$	$\frac{8.5}{33}$	$\frac{3.5}{34}$	$\frac{9.3}{16}$	$\frac{7.5}{14}$	$\frac{8.6}{12}$	8.0	$\frac{9.0}{14}$	$\frac{9.5}{17}$	$\frac{4.8}{24}$	$\frac{4.5}{33}$	$\frac{4.7}{50}$
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$\frac{10.3}{50}$	$\frac{10.1}{33}$	$\frac{10.5}{19}$	$\frac{11.5}{17}$	$\frac{11.5}{15}$	$\frac{11.2}{14}$	10.5	$\frac{11.1}{13}$	$\frac{11.4}{15}$	$\frac{11.0}{19}$	$\frac{11.2}{33}$	$\frac{11.1}{50}$
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$\frac{9.2}{50}$	$\frac{9.5}{33}$	$\frac{10.2}{20}$	$\frac{12.2}{14}$	$\frac{11.8}{17}$	10.9	$\frac{10.6}{14}$	$\frac{12.2}{16}$	$\frac{12.2}{19}$	$\frac{11.7}{20}$	$\frac{10.9}{33}$	$\frac{11.0}{50}$
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$\frac{5.1}{50}$	$\frac{3.4}{33}$	$\frac{4.7}{21}$	$\frac{7.4}{14}$	$\frac{8.1}{11}$	7.4	$\frac{8.0}{15}$	$\frac{8.9}{18}$	$\frac{2.3}{26}$	$\frac{2.1}{33}$	$\frac{1.8}{50}$
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$\frac{9.8}{50}$	$\frac{8.1}{33}$	$\frac{8.3}{22}$	$\frac{10.6}{18}$	$\frac{9.9}{15}$	8.7	$\frac{7.2}{15}$	$\frac{10.2}{18}$	$\frac{3.7}{25}$	$\frac{2.8}{33}$	$\frac{2.1}{50}$
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$\frac{8.3}{50}$	$\frac{7.8}{33}$	$\frac{6.5}{22}$	$\frac{6.3}{17}$	$\frac{3.6}{14}$	2.4	$\frac{1.5}{15}$	$\frac{3.2}{18}$	$\frac{2.8}{33}$	$\frac{1.4}{50}$
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$\frac{7.9}{50}$	$\frac{7.7}{33}$	$\frac{8.5}{19}$	$\frac{4.6}{14}$	3.7	$\frac{4.3}{16}$	$\frac{5.6}{18}$	$\frac{5.6}{33}$	$\frac{4.9}{50}$
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66
15
✓

Sta.	+	H.I.	-	Elev.
		929.11		
137				924.2
	+70			24.3
138				244
	+50			24.6
239				253
T.P.	10.41	936.19	3.35	925.78
	+80			27.4
140				28.0
	+48			29.5
	+74			30.7
141				31.2
	+08			31.6
B.M.	7.22	938.98	4.44	931.75
	+42			32.4
142				32.7

H² Line.

$\frac{8.9}{50}$	$\frac{10.0}{33}$	$\frac{8.9}{17}$	$\frac{5.7}{13}$	4.9	$\frac{5.7}{14}$	$\frac{7.5}{18}$	$\frac{7.3}{33}$	$\frac{7.2}{50}$
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$\frac{6.9}{50}$	$\frac{7.7}{33}$	$\frac{9.3}{19}$	$\frac{5.9}{14}$	4.8	$\frac{5.4}{14}$	$\frac{7.0}{16}$	$\frac{6.6}{33}$	$\frac{7.0}{50}$
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$\frac{7.8}{50}$	$\frac{8.7}{33}$	$\frac{8.2}{18}$	$\frac{5.7}{14}$	4.7	$\frac{5.7}{15}$	$\frac{7.7}{18}$	$\frac{7.5}{33}$	$\frac{7.2}{50}$
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$\frac{8.5}{50}$	$\frac{9.1}{33}$	$\frac{8.9}{19}$	$\frac{5.2}{13}$	4.5	$\frac{5.2}{12}$	$\frac{9.9}{30}$	$\frac{9.7}{33}$	$\frac{9.7}{50}$
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$\frac{7.8}{50}$	$\frac{7.7}{33}$	$\frac{7.5}{19}$	$\frac{4.9}{14}$	3.8	$\frac{5.1}{15}$	$\frac{8.7}{21}$	$\frac{7.3}{33}$	$\frac{8.9}{50}$
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$\frac{9.1}{50}$	$\frac{8.0}{33}$	$\frac{7.9}{22}$	$\frac{10.2}{17}$	$\frac{9.2}{14}$	8.8	$\frac{9.4}{13}$	$\frac{10.3}{14}$	$\frac{6.5}{21}$	$\frac{6.7}{33}$	$\frac{6.9}{50}$
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$\frac{8.1}{50}$	$\frac{6.7}{33}$	$\frac{7.1}{23}$	$\frac{5.8}{18}$	$\frac{9.3}{19}$	$\frac{8.9}{14}$	8.2	$\frac{8.9}{13}$	$\frac{9.7}{19}$	$\frac{6.6}{21}$	$\frac{7.0}{33}$	$\frac{7.6}{50}$
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$\frac{7.6}{50}$	$\frac{6.3}{33}$	$\frac{6.9}{30}$	$\frac{7.6}{19}$	$\frac{7.2}{12}$	6.7	$\frac{6.6}{14}$	$\frac{7.9}{19}$	$\frac{7.1}{21}$	$\frac{7.5}{33}$	$\frac{8.3}{50}$
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$\frac{5.6}{50}$	$\frac{5.4}{33}$	$\frac{5.5}{14}$	5.5	$\frac{5.6}{14}$	$\frac{5.6}{33}$	$\frac{5.5}{50}$
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$\frac{6.6}{50}$	$\frac{5.7}{35}$	$\frac{5.1}{22}$	5.0	$\frac{5.7}{23}$	$\frac{6.7}{24}$	$\frac{5.8}{26}$	$\frac{5.8}{33}$	$\frac{4.2}{50}$
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$\frac{3.1}{50}$	$\frac{3.8}{40}$	$\frac{6.2}{37}$	$\frac{6.1}{21}$	$\frac{4.7}{14}$	4.4	$\frac{4.7}{11}$	$\frac{5.8}{23}$	$\frac{6.6}{25}$	$\frac{5.9}{29}$	$\frac{5.4}{33}$	$\frac{4.0}{50}$
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SPK in T. 17 100' H. Sta. 240 + 95.

$\frac{1.4}{50}$	$\frac{2.1}{34}$	$\frac{4.5}{31}$	$\frac{5.1}{40}$	$\frac{7.8}{18}$	$\frac{7.9}{14}$	$\frac{7.4}{14}$	6.6	$\frac{6.5}{9}$	$\frac{7.2}{10}$	$\frac{7.5}{17}$	$\frac{2.1}{24}$	$\frac{2.4}{33}$	$\frac{3.4}{50}$
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$\frac{5.0}{50}$	$\frac{4.5}{33}$	$\frac{3.9}{21}$	$\frac{6.9}{19}$	6.3	$\frac{6.5}{8}$	$\frac{6.8}{9}$	$\frac{7.9}{15}$	$\frac{3.0}{22}$	$\frac{3.3}{33}$	$\frac{4.3}{50}$
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Sta.	+	H.I.	-	Elev.
		938.98		
143				931.9
	+50			31.5
T.P.	4.83	935.96	7.85	931.13
144				31.2
	+75			
		Cross Drain 12" C.M. Drains Lt. (31.5)		
		2.24.1 = Inv. Elev. on Rt. Left side not found.		
		26.7		
145				32.3
	+65			
T.P.	10.76	945.75	0.97	934.99
146				35.1
	+50			
				36.9
147				38.7
148				41.5
T.P.	4.00	947.12	2.65	945.12
149				43.1
	+45			
				43.2
150				42.6

1/30/25

H² Line

$\frac{5.8}{50}$	$\frac{6.6}{33}$	$\frac{6.0}{21}$	$\frac{8.2}{18}$	$\frac{7.6}{13}$	7.1	$\frac{7.7}{13}$	$\frac{8.4}{14}$	$\frac{8.6}{17}$	$\frac{8.0}{18}$	$\frac{6.7}{23}$	$\frac{6.8}{33}$	$\frac{6.5}{50}$
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$\frac{8.0}{50}$	$\frac{9.0}{33}$	$\frac{8.0}{23}$	$\frac{9.2}{19}$	$\frac{8.1}{14}$	7.5	$\frac{7.9}{8}$	$\frac{8.3}{11}$	$\frac{9.0}{16}$	$\frac{6.3}{19}$	$\frac{5.6}{33}$	$\frac{4.8}{50}$
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$\frac{8.2}{50}$	$\frac{8.7}{33}$	$\frac{8.0}{22}$	$\frac{5.8}{18}$	$\frac{5.2}{14}$	4.8	$\frac{5.7}{15}$	$\frac{7.3}{18}$	$\frac{7.5}{33}$	$\frac{8.5}{50}$
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$\frac{12.4}{50}$	$\frac{12.3}{33}$	$\frac{11.6}{28}$	$\frac{4.9}{15}$	4.5	$\frac{5.5}{15}$	$\frac{7.2}{25}$	$\frac{11.4}{33}$	$\frac{11.6}{50}$
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$\frac{12.2}{50}$	$\frac{11.7}{33}$	$\frac{11.3}{26}$	$\frac{4.3}{15}$	3.7	$\frac{3.6}{15}$	$\frac{9.9}{24}$	$\frac{10.3}{33}$	$\frac{10.2}{50}$
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$\frac{6.4}{50}$	$\frac{7.0}{33}$	$\frac{6.3}{23}$	$\frac{2.9}{17}$	1.8	$\frac{2.8}{16}$	$\frac{4.4}{19}$	$\frac{4.8}{33}$	$\frac{4.0}{50}$
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$\frac{11.2}{50}$	$\frac{12.7}{33}$	$\frac{11.5}{20}$	$\frac{12.3}{19}$	$\frac{12.2}{16}$	$\frac{11.4}{14}$	10.7	$\frac{11.2}{11}$	$\frac{11.8}{14}$	$\frac{12.2}{20}$	$\frac{10.0}{28}$	$\frac{9.5}{33}$	$\frac{9.1}{50}$
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$\frac{6.9}{50}$	$\frac{7.0}{33}$	$\frac{6.6}{21}$	$\frac{10.3}{17}$	$\frac{9.4}{14}$	8.9	$\frac{9.2}{13}$	$\frac{10.6}{15}$	$\frac{10.6}{22}$	$\frac{3.8}{32}$	$\frac{3.6}{50}$
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$\frac{6.3}{50}$	$\frac{5.4}{33}$	$\frac{5.0}{20}$	$\frac{8.7}{16}$	$\frac{8.0}{14}$	7.1	$\frac{8.0}{15}$	$\frac{9.4}{19}$	$\frac{2.7}{32}$	$\frac{1.9}{50}$
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$\frac{5.4}{50}$	$\frac{4.6}{33}$	$\frac{3.7}{21}$	$\frac{5.8}{18}$	$\frac{5.0}{14}$	4.3	$\frac{4.8}{12}$	$\frac{5.0}{17}$	$\frac{5.5}{24}$	$\frac{1.9}{31}$	$\frac{1.3}{50}$
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$\frac{3.8}{50}$	$\frac{3.8}{33}$	$\frac{3.4}{20}$	$\frac{4.9}{19}$	$\frac{5.0}{17}$	$\frac{4.6}{14}$	4.0	$\frac{4.3}{10}$	$\frac{5.0}{15}$	$\frac{1.8}{22}$	$\frac{2.1}{33}$	$\frac{1.9}{50}$
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$\frac{3.3}{50}$	$\frac{3.5}{33}$	$\frac{3.7}{22}$	$\frac{4.7}{30}$	$\frac{5.1}{18}$	$\frac{4.5}{16}$	3.9	$\frac{4.3}{14}$	$\frac{5.0}{15}$	$\frac{5.0}{18}$	$\frac{2.2}{22}$	$\frac{2.7}{33}$	$\frac{2.1}{50}$
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$\frac{5.8}{50}$	$\frac{4.4}{33}$	$\frac{3.4}{24}$	$\frac{6.0}{21}$	$\frac{5.9}{19}$	$\frac{5.1}{17}$	4.5	$\frac{5.4}{14}$	$\frac{5.8}{16}$	$\frac{5.7}{17}$	$\frac{1.6}{22}$	$\frac{2.0}{33}$	$\frac{2.4}{50}$
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Sta	+	H.I.	-	Elev.
		947.12		
251				40.7
B.M.	7.82	947.10	7.82	939.28
+52				39.8
252				39.2
253				38.3
+34				37.7
254				35.6
T.P.	1.85	937.23	11.72	935.38
+61				32.9
255				31.4
+50				29.4
256				27.1
T.P.	1.40	931.31	7.52	929.71
+32				29.6
+50				28.0
257				21.7
T.P.	0.55	921.41	10.45	920.86

H² Line.

10.1	10.3	9.9	9.5	9.0		7.6	9.0	9.0	8.6	9.1	9.0
50	33	27	22	19	6.4	13	15	17	19	33	50

SpK in 18" Oak 50' Lt. Stg. 250 + 85.

10.2	10.7	10.2	8.8	8.1	11.0	8.1	11.0	11.1	10.6
50	33	27	25	21	7.3	11	17	33	50

10.7	11.6	11.3	9.0		5.8	9.6	11.2	11.3	11.1
50	33	27	21	7.7	12	16	18	33	50

8.8	10.2	10.3	11.4	9.6		9.7	11.0	10.9	10.8	9.5
50	33	27	25	21	8.8	14	17	23	42	50

7.4	8.2	8.4	11.5	11.4	10.4	10.2	10.9	10.8	9.8	9.4	8.0	
50	33	28	22	21	19	7.4	12	15	18	20	33	50

2.8	3.5	3.5	12.9	12.0		12.2	12.8	12.8	6.7	7.2	7.2
50	33	31	20	18	11.5	12	13	15	20	33	50

0.6	1.4	1.7	6.0	5.9	5.0	5.0	5.7	5.7	3.6	3.8	3.8	
50	33	29	23	22	20	4.3	12	14	16	19	33	50

2.4	3.0	2.9	7.5	6.5		6.3	7.1	7.2	3.0	3.4	3.9
50	33	29	24	20	5.8	11	14	15	20	33	50

3.6	2.6	9.2	8.5	7.8		8.2	9.1	2.5	2.2	2.0
50	32	26	22	11	7.8	11	13	20	33	50

7.9	7.9	11.9	11.1	10.0		10.1	10.6	10.6	4.7	3.5	3.4
50	43	37	33	19	10.1	2	3	5	12	33	50

6.8	5.5	5.9	6.0		0.6	0.0	0.4
50	29	8	5	1.7	14	33	50

7.1	6.0	6.4	7.0	3.7		2.6	2.0	2.0
50	35	16	13	8	3.3	14	33	50

9.5	10.6	9.9	10.8		8.6	9.5	4.4
50	48	40	16	9.6	14	33	50

Sta. + H.I. - Elev.

721.41

+50

914.7

258

12.9

+50

13.7

259

74.6

+03²

14.6

T.P. 4.05 718.62 6.84 914.57

B.M. 1.23 917.39 917.40

H² Line.

$\frac{6.7}{50}$	$\frac{7.0}{33}$	$\frac{6.9}{14}$	6.7	$\frac{5.4}{17}$	$\frac{4.2}{33}$	$\frac{2.11}{50}$
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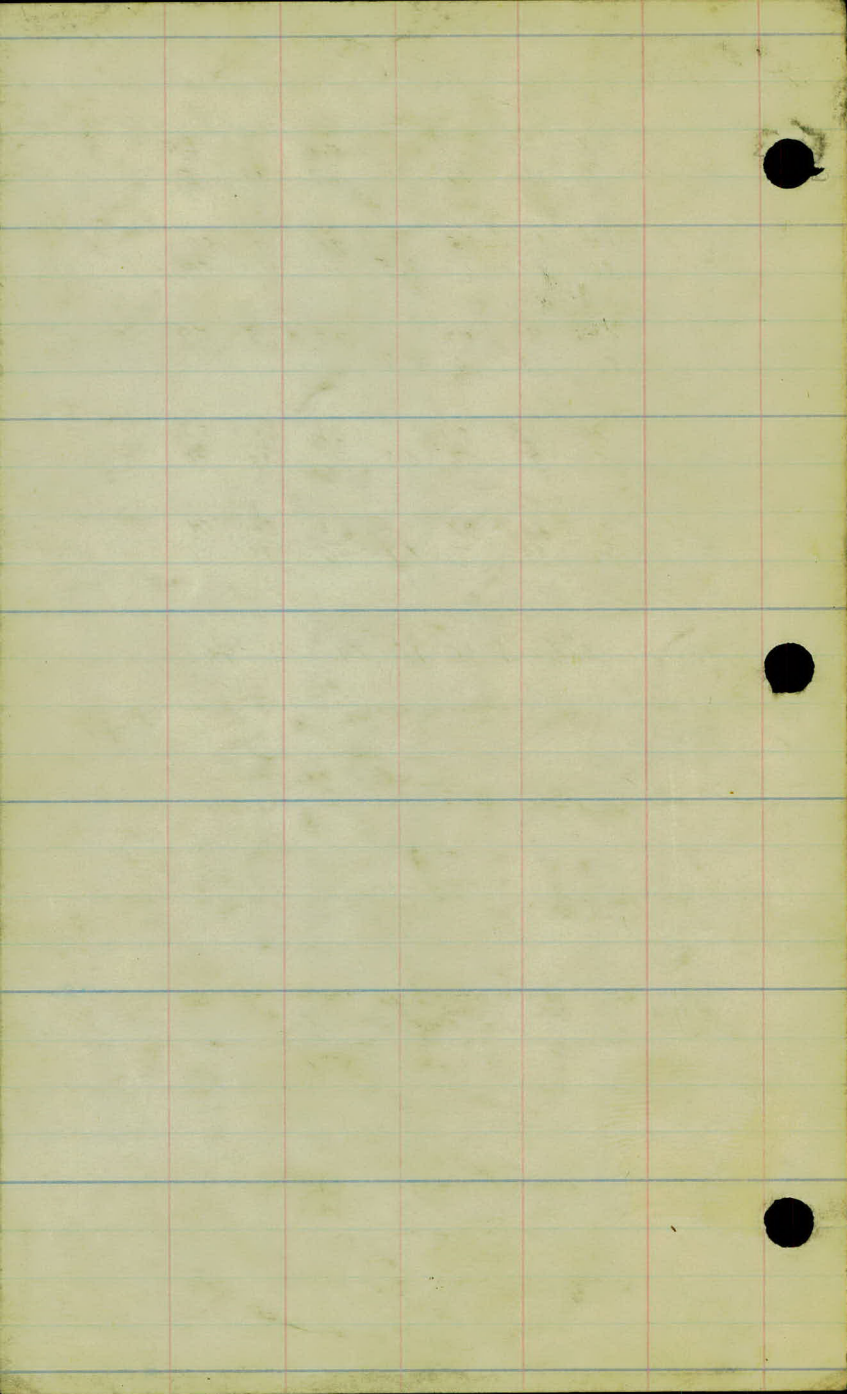
$\frac{8.4}{50}$	$\frac{8.6}{33}$	$\frac{8.5}{14}$	8.5	$\frac{7.8}{14}$	$\frac{6.4}{36}$	$\frac{5.0}{50}$
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$\frac{4.4}{50}$	$\frac{7.1}{33}$	$\frac{8.2}{14}$	7.7	$\frac{7.3}{20}$	$\frac{6.5}{33}$	$\frac{5.9}{50}$
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$\frac{9.0}{50}$	$\frac{8.8}{33}$	$\frac{7.9}{14}$	6.8	$\frac{6.2}{14}$	$\frac{6.0}{33}$	$\frac{5.3}{50}$
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$\frac{9.1}{50}$	$\frac{8.8}{33}$	$\frac{7.2}{14}$	6.8	$\frac{6.3}{14}$	$\frac{6.0}{33}$	$\frac{5.4}{50}$
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SPK. in 15" Oak. 50' Rt. Sta. 158740.



Plans - in-hand Insp.

26-07

H.D.K.
P.E.B.

3/26/26

215+00 F.E. Lt. - No. Cul. Regi.

217+40 F.E. Rt. - P. 15" X 24' C.M.

220+90 Rem. - 12" X 30' C.M. - P. 18" P₃

226+65 - Rem. - 10" X 33' V.P. - P 18" P₃

230+43 - F.E. Lt. - P. 15" X 24' C.M.

235+25 - 239+30 G.R. Lt.

235+30 F.E. Rt. - P. 15" X 24' C.M.

237+60 - 239+30 G.R. Rt.

238+50 - Rem. 12" X 36' C.M. - V.P. - P 18" P₃

240+74 - Insp. 15" X 44' C.M. - Allow. to Remain

242+95 - F.E. Rt. - P. 15" X 24' C.M.

243+60 - 245+60 G.R. R and Lt.

244+77 - Rem. - 12" X 45' C.M. - P. 18" P₃

248+66 - F.E. Lt. - 10p. - 12" X 16" C.M.
Rem. - Rep. - 12" X 24"

249+60 - 250 - C/ & Gr. 2 Trs. -

253+20 - F.E. Rt. - P. 15" X 24" C.M.

252+00 - No Culv. Reg. - Drains So. & N. -

253 to 259 C/ & Gr. 60 Trs. -

2489.