

PLANS SURVEY  
EAST CO. LINE ROAD

From Highwood Road

To Carver's Lake

CO. PROJ. No 26-06

FILE No 1

Date Filed 5-27-25

File No 1

Alignment notes on Proj # 26-52  
E. Co. Line Road

From Highwood Road

To Carver's Lake

Crane  
Wilshusen  
Fritz  
Franko.

Sta.	Point	Lt.	Rt.	Course Bearing
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11+01 <sup>25</sup>	P.O.T.			
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9+91 <sup>L</sup>	P.O.T.			
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500°-00'W.

0+00	P.O.T.			
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o Fence Post.

35 25

30 41

o Fence Post.

Tree o 40 25

Tree o 45 65

o Guy Pole

37 25

stone Mont. □

37 85

P.P. o

1/4 Cor. W. line

Sec. 13 - T. 28 N. - R. 22 W.

Sta.	Point	Lt.	Rt.	Calc Bearing
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17+00	P.O.T.			
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17+91 <sup>55</sup>	P.O.T.			
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21+75.00
17+91.50
3 83.45

500°-00'W

17+04 <sup>2</sup>	P.O.T.			
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16+32 <sup>3</sup>	P.O.T.			
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4/23/25

Tree 9 25

Tree 5 9 4

M.O. Cor. Stone Mont.

34' 3" Willow

12" Willow

56 28 12" Willow

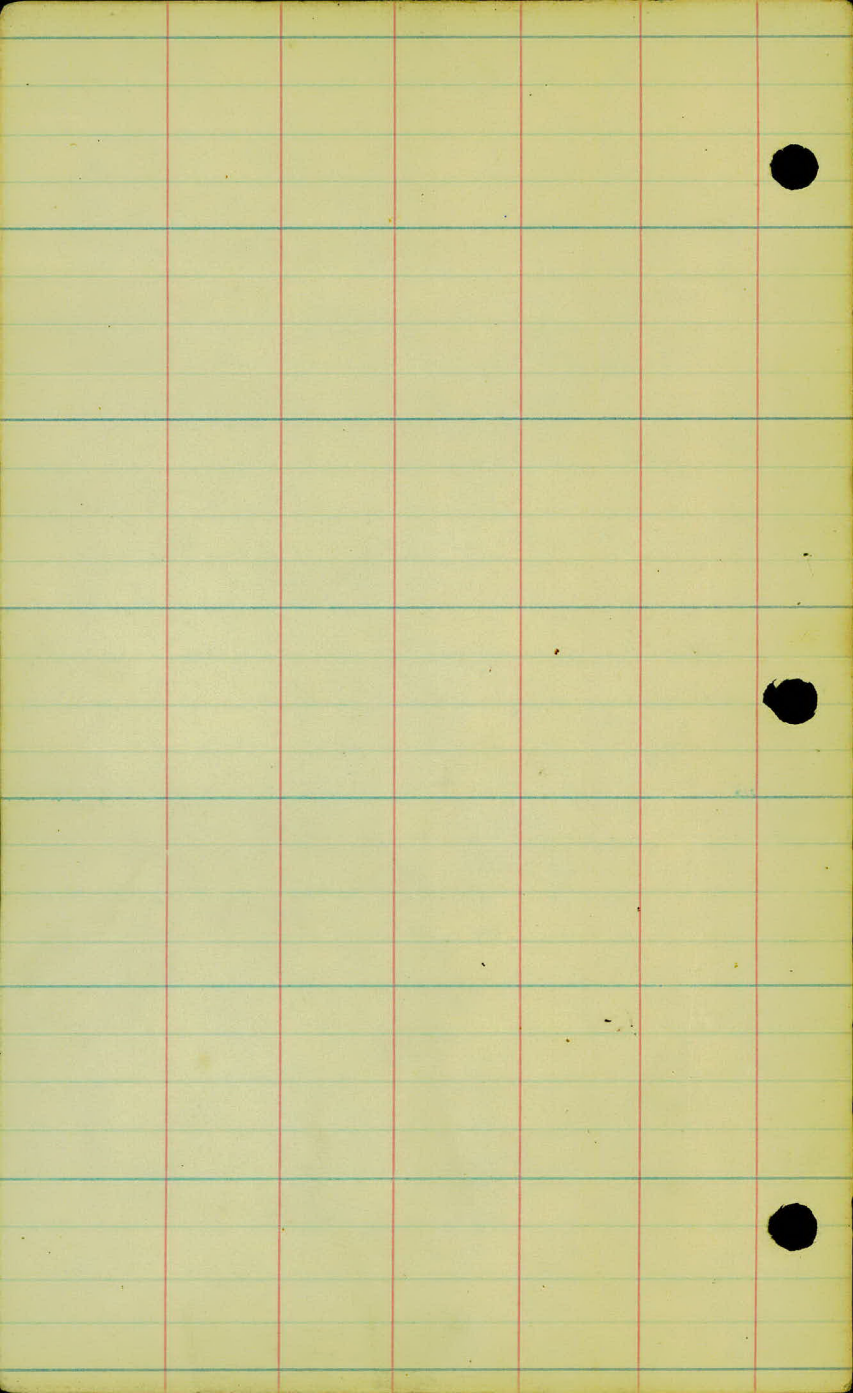
Tree 17 25

Tree 43 25

16 3 Tree

29 4

Tree



Art. Topog. on Proj. #46-52

sta.

4700

3700

2700

876.1 In. Elev.

1700

0700

F. 7 L.

Q. Rd. 3 R.

181 T. P. 18 R.

F. 8 L.

Q. Rd. 0.0

150 Q. Rd. 2 R.  
140 T. P. 21 R.

F. 6 L.

Q. Rd. 4 R.

150 Q. Rd. 5 R.

Pature

Cultivated field.

F. 8 L.

106 T. P. 24 R.  
Q. Rd. 3 R.

- 127 Bay Pipe 20 L.
- 122 Fill 2 L.
- 127 F. Cor. 25 L.
- 117 I. R. S. Direction
- 109 F. Cor. 24 L.
- 109 F. Cor. 17 L.

- 09 Cattle Pass 17 L.
- 10 F. Cor. 21 L.
- 10 F. Cor. 17 L.
- 18 F. 15 L.
- 18 F. P. 18 L.
- 18 F. Cor. 31 L.

12' wide Rd.

150 Q. Rd. 2 R.

Drains H.

- 120 T. P. 52 R.
- +14 Cross Drain
- 1 1/2" X 30 C.M. Cant. Fall
- Extends 15 L. & 15 R.
- +00 Cross Rd.

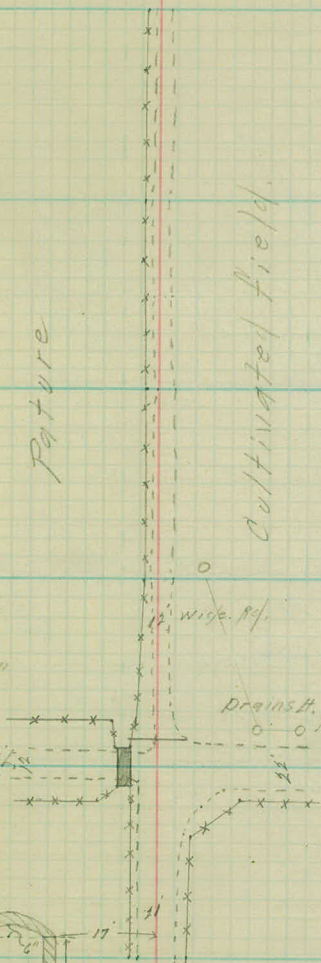
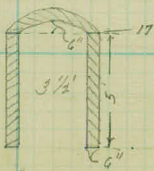
-17 F. Cor. 45 R.

- 38 F. Cor. 19 R.
- 55 Mail Box H. R.
- 70 " " "

F. 14 L.

F. 17 R.

0-17 Cattle Pass 17 L.  
3 1/2 x 5 x 18'  
Concrete  
With arch roof



379.

10700

9700

8700

7700

6700

5700

4700

4/27/25

10 Q. Ref. 13' L.

+50 Q. Ref. 10' L.

9 Q. Ref. 6' L.

8

161 F. Cor. 22' L.

7

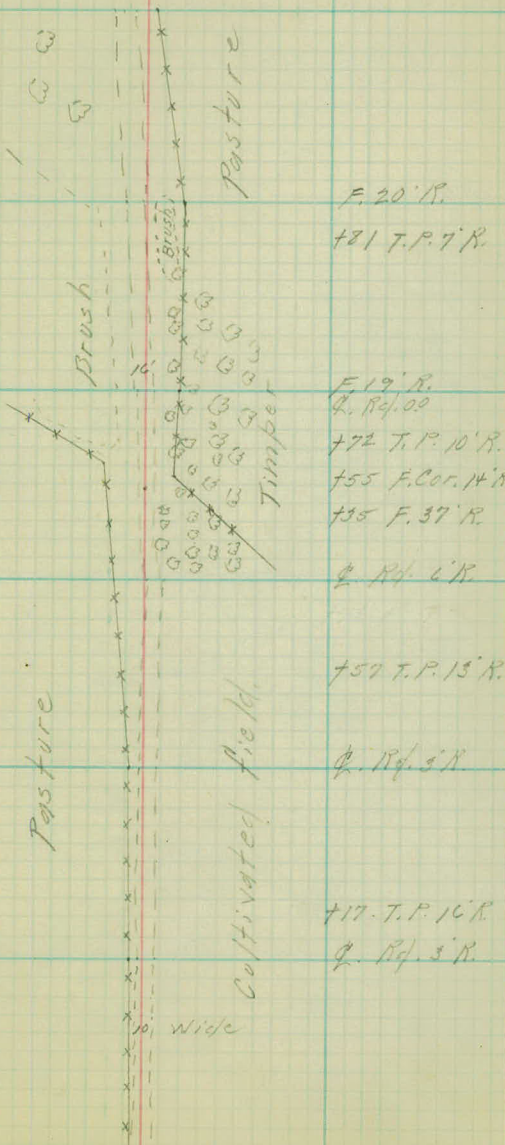
+73 - 4" - T. - 3' L.

6

F. 8' L.

5

F. 7' L.



F. 20' R.  
 +81 T. P. 7' R.  
 F. 19' R.  
 Q. Ref. 00  
 +72 T. P. 10' R.  
 +55 F. Cor. 14' R.  
 +35 F. 37' R.  
 Q. Ref. 6' R.  
 +57 T. P. 13' R.  
 Q. Ref. 5' R.  
 +17 T. P. 16' R.  
 Q. Ref. 3' R.

10' wide

Sta.

16+00

15+00

14+00

13+00

12+00

11+00

10+00

7/27/25

F. 17' L.  
F. 26' L.  
+90 F. Cor. 18' L.  
+85 F. Cor. 18' L.  
+75 F. Cor. 5' L.  
+65 Q. Rd. 14' L.

+70 F. L.  
+35 F. 35' R.

F. 26' L.  
Q. Rd. 19' L.

F. 25' L.  
Q. Rd. 19' L.

F. 23' L.  
Q. Rd. 17' L.

F. 22' L.  
Q. Rd. 15' L.

F. 21' L.  
Q. Rd. 14' L.

+54 F. Cor. 20' L.  
24'

+25 F. Ent.  
+01 F. Cor. 29' R.  
+01 F. Cor. 14' R.  
+01 F. Cor. 4' R.  
+01 T. 1. 4' R.

+18 F. Ent.  
+05 House



Cultivated field

Cultivated field

Planting Spaces



Sta.

10+00

19+00

18+00

17+00

16+00

7/27/25

+05 Lake 14' L.  
+70 Lake 45' L.

+55 Lake 40' L.

Lake 52' L.

+50 Lake 41' L.

+20 F. Cor. 5' L.  
+15 F. Cor. 3' L.  
+00 Lake 55' L.

+84 F. 20' L.  
+50 Lake 73' L.  
+49 - 12" T. - 20' L.  
+48 - 12" T. - 20' L.  
+08 - 15" T. - 17' L.  
F. 17' L.

+04 - 10" T. - 19' L.  
+50 - 11" T. - 15' L.  
+32 - 16" T. - 7' 50" L.  
+30 - 15" T. - 18' L.  
+30 F. Cor. 26' L.

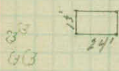
+04 F. 18' L.  
+06 F. 10' L.

Carver Lake

Bathing  
Break

Timber

Pasture

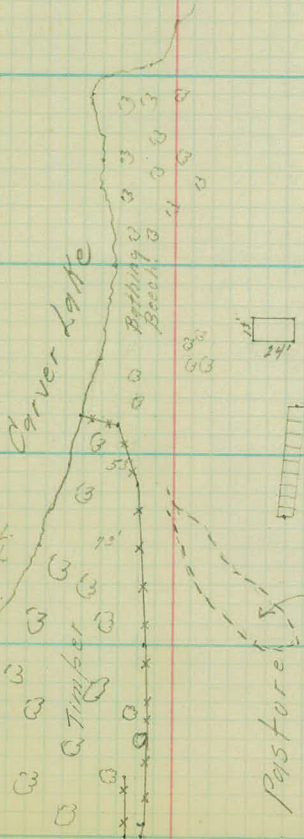


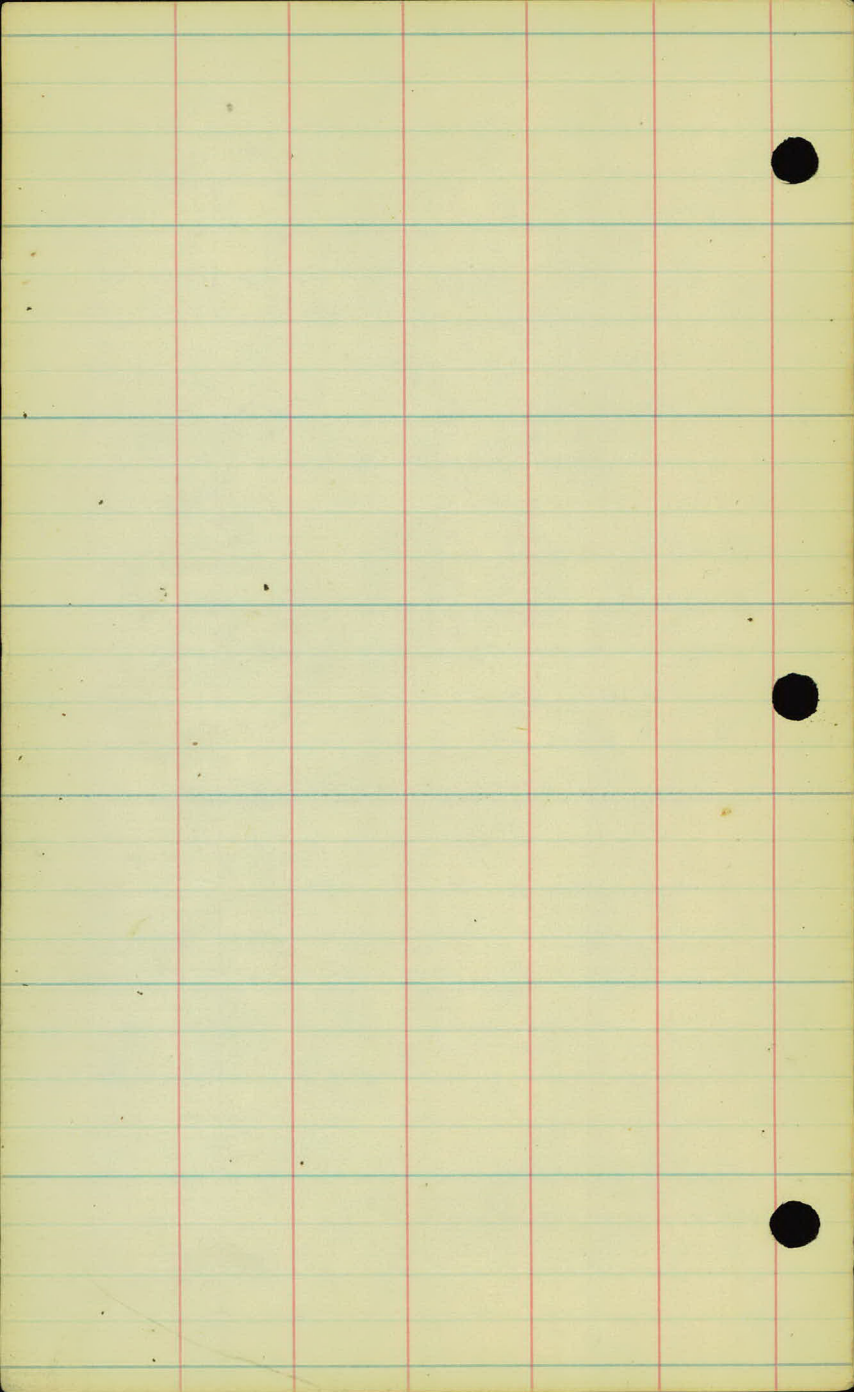
+60 Bath House 41' L.

+26 End of steps 66'

+67 Beginning of  
Woodch. steps. 60' L.  
3' Wide.

Washout filled  
with brush





Center line levels on Proj #16-52

Sta.	T	H.I.	-	Rod	Elev.	
B.M.	4.97	906.77		700.00		
0-200				3.0	904.0	
0-150				5.2	901.8	
0-100				4.1	900.7	
0-50				5.4	901.4	
0+00	Cross Rd.			4.9	902.1	
+06				5.2	901.8	
+29				7.9	899.1	
+50				8.9	898.1	
1+00				10.0	898.0	897.0
+50				10.5	896.5	
2+00				10.2	896.8	
+50				10.0	897.0	
3+00				9.5	897.7	
T.P.	5.99	901.62	11.34	895.63		
+50				6.7	888.9	914.9
+00				9.1	884.5	92.5
+50				7.4	886.2	92.7
+75				9.8	885.8	91.8
5+00				9.3	886.3	92.3
+50				8.0	887.4	93.6
+92				6.5	889.1	95.1
6+00				5.4	890.0	96.0
+23				3.4	892.0	96.0
+50				2.1	893.5	94.5
7+00				1.4	894.0	900.0
T.P.	10.71	912.24	0.09	901.53		

4/25/25

Sp. in P.P. 25' L. 0-28

<u>11.6</u>	<u>10.6</u>	<u>8.6</u>	<u>4.9</u>
100	74	50	19

<u>1.7</u>	<u>0.0</u>
50	75

4 775

Sta.	+	H.I.	-	Red.	Elev.
		912.24			
+50				8.8	903.4
8700				5.0	907.2
T.P.	10.84	922.57	0.53	911.71	
+50				8.9	913.7
+87				3.5	919.1
+92				2.4	918.2
9700				2.0	920.4
T.P.	10.64	932.33	0.88	921.69	
+50				4.9	925.4
+62				5.3	927.0
+65				4.2	928.1
T.P.	5.50	936.47	1.36	933.97	
+84				2.5	934.0
+84				0.4	936.1
10700				2.8	933.7
B.M.			4.57	931.90	
+24				3.7	932.8
+50				3.0	933.5
11700				2.1	934.4
+15				3.5	933.0
+50				2.0	928.5
T.P.	0.87	927.07	10.27	924.20	
12700				4.1	923.0
+40				2.2	918.9
T.P.	0.51	914.12	11.46	915.61	
13700				2.3	913.8

20.2

4/25/25

Spk. in Tree 50' H. Sta. 10 + 25.

Sta.	+	H.I.	-	Red.	Elev.
		916.12			
	+50			7.8	908.3
	+79			10.1	906.0
14	+00			10.3	905.8
	+44			10.0	906.1
	+50			9.3	906.8
	+88			2.5	913.4
15	+00			0.9	915.2
T.P.	4.02	919.84	0.30	915.82	
	+50			2.4	917.4
16	+00			1.5	918.3
	+32			1.5	918.3
B.M.				2.27	917.57
	+50			4.0	915.8
	+64			5.6	914.2
	+81			7.3	912.5
17	+00			10.9	908.9
T.P.	1.85	910.60	11.09	908.75	
	+11			4.3	906.3
T.P.	1.87	901.34	11.13	899.47	
T.P.	1.85	892.03	11.14	890.18	
	+50			4.2	887.8
T.P.	1.47	882.57	10.73	881.10	
	+73			4.8	877.8
18	+00			8.2	874.4
	+50			12.0	870.4
17	+00			11.8	870.8

4/25/25

SpK. in Tree 15' Lt. Sta. 16 + 32,

Sta.	+	H.I.	-	Rod.	Elev.
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882.57

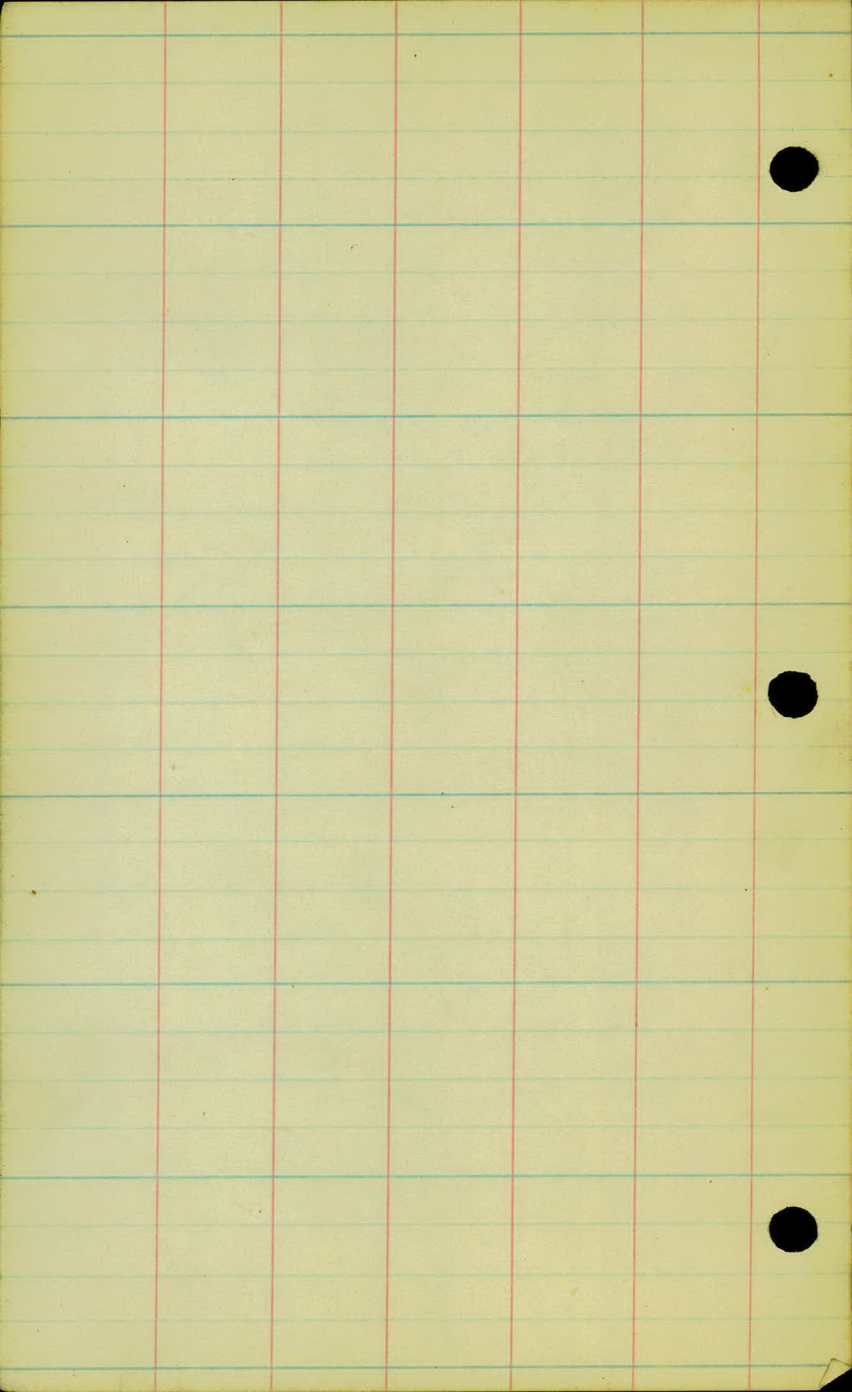
Water Elev = 14.2 868.4

B.M.

7.57 875.00

4/25/25

Spk. in 12" Tree 100' Ft. Sta. 18+30



x. sections on Proj # 15-52.

Sta.	+	H.I.	-	Elev.
B.M.	5.95	905.95		900.00
0-15				01.8
0-04				02.2
0+00				02.4
0+07				01.7
0+14	Cross Drain Inv. Elev. 896.1 drains H.			
0+16				900.3
0+23				899.6
0+50				98.1
1+00				97.0
+50				96.5
2+00				96.9
+50				97.0
3+00				97.8
+50				94.9
T.P.	7.37	902.34	10.94	894.97

Spt. 11 P.P. 25' Lt Stg. 0-28

$\frac{10.8}{33}$   $\frac{8.2}{14}$   $\frac{5.2}{10}$   $\frac{4.5}{5}$  4.2  $\frac{3.7}{10}$   $\frac{3.3}{29}$   $\frac{4.2}{33}$

$\frac{5.7}{33}$   $\frac{5.2}{28}$   $\frac{4.2}{15}$  3.8  $\frac{2.7}{23}$   $\frac{2.2}{33}$

$\frac{5.4}{33}$   $\frac{3.9}{19}$   $\frac{3.7}{10}$  3.6  $\frac{2.6}{19}$   $\frac{1.7}{33}$

$\frac{5.6}{33}$   $\frac{4.0}{19}$   $\frac{4.3}{6}$  4.3  $\frac{4.0}{13}$   $\frac{2.9}{21}$   $\frac{2.0}{33}$

$\frac{10.3}{33}$   $\frac{9.1}{18}$   $\frac{6.7}{15}$   $\frac{6.2}{3}$  5.7  $\frac{5.6}{8}$   $\frac{5.2}{10}$   $\frac{5.5}{14}$   $\frac{6.0}{18}$   $\frac{5.4}{33}$

$\frac{8.6}{33}$   $\frac{8.1}{24}$   $\frac{9.0}{23}$   $\frac{8.5}{14}$   $\frac{7.6}{14}$   $\frac{7.6}{11}$   $\frac{7.1}{4}$   $\frac{6.5}{2}$  6.4  $\frac{6.5}{7}$   $\frac{5.6}{10}$   $\frac{5.3}{33}$

$\frac{8.9}{33}$   $\frac{8.0}{7}$   $\frac{7.7}{5}$  7.9  $\frac{7.9}{7}$   $\frac{6.9}{9}$   $\frac{6.0}{33}$

$\frac{11.1}{33}$   $\frac{9.9}{4}$   $\frac{9.1}{4}$  9.0  $\frac{9.1}{7}$   $\frac{8.3}{12}$   $\frac{6.0}{33}$

$\frac{13.3}{33}$   $\frac{11.7}{17}$   $\frac{10.2}{4}$   $\frac{9.6}{2}$  9.5  $\frac{9.3}{8}$   $\frac{8.3}{18}$   $\frac{6.3}{33}$

$\frac{14.9}{33}$   $\frac{12.6}{15}$   $\frac{11.0}{4}$   $\frac{9.2}{2}$  9.1  $\frac{8.8}{10}$   $\frac{6.9}{22}$   $\frac{4.7}{33}$

$\frac{14.7}{33}$   $\frac{11.2}{12}$   $\frac{10.0}{4}$   $\frac{9.0}{4}$  9.0  $\frac{8.4}{6}$   $\frac{7.0}{9}$   $\frac{4.1}{22}$   $\frac{1.9}{33}$

$\frac{13.2}{33}$   $\frac{10.1}{15}$   $\frac{9.3}{7}$   $\frac{6.6}{4}$  8.2  $\frac{8.0}{4}$   $\frac{6.8}{8}$   $\frac{3.9}{21}$   $\frac{2.4}{33}$

$\frac{14.9}{33}$   $\frac{12.7}{17}$   $\frac{11.9}{8}$   $\frac{10.8}{4}$   $\frac{11.1}{2}$  11.1  $\frac{11.4}{4}$   $\frac{9.7}{8}$   $\frac{7.5}{24}$   $\frac{6.5}{33}$

Sta.	+	H.I	-	Elev.
		902.34		
4+00				92.7
+50				92.3
+75	Requires 24" Cross Drain			
5+00				92.3
+57				93.8
6+00				96.0
+34				899.2
7+00				900.2
T.P.	7.30	908.69	0.97	901.39 ✓
+50				03.5
8+00				07.3
T.P.	11.29	918.88	1.10	907.59 ✓
+34				11.5
+59				15.2
T.P.	11.14	928.57	1.47	917.41 ✓
8+59				15.2
+70				20.1

4/24/25

L.

R.

$\frac{11.8}{33}$	$\frac{11.4}{17}$	$\frac{10.7}{4}$	$\frac{9.6}{3}$	$\frac{9.5}{1}$	9.7	$\frac{9.4}{4}$	$\frac{9.1}{8}$	$\frac{8.2}{23}$	$\frac{7.0}{33}$
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$\frac{7.3}{33}$	$\frac{10.5}{8}$	10.1	$\frac{9.9}{6}$	$\frac{9.2}{22}$	$\frac{8.9}{33}$
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$\frac{11.7}{33}$	$\frac{11.0}{12}$	$\frac{10.4}{3}$	$\frac{10.1}{2}$	10.1	$\frac{10.0}{8}$	$\frac{8.4}{33}$
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$\frac{11.6}{33}$	$\frac{10.8}{17}$	$\frac{9.8}{5}$	$\frac{8.5}{2}$	8.4	$\frac{8.4}{7}$	$\frac{7.8}{23}$	$\frac{5.5}{33}$
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$\frac{10.5}{33}$	$\frac{9.7}{27}$	$\frac{8.1}{13}$	$\frac{7.3}{8}$	$\frac{5.9}{5}$	$\frac{5.9}{3}$	$\frac{6.2}{2}$	6.4	$\frac{6.2}{8}$	$\frac{5.5}{10}$	$\frac{2.8}{25}$	$\frac{1.1}{33}$
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$\frac{8.9}{33}$	$\frac{7.6}{24}$	$\frac{6.6}{12}$	$\frac{5.1}{7}$	$\frac{3.5}{3}$	3.2	$\frac{3.8}{2}$	$\frac{3.7}{8}$	$\frac{3.0}{9}$	$\frac{1.4}{22}$	$\frac{0.0}{19}$	$\frac{10.8}{33}$
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$\frac{8.8}{33}$	$\frac{8.0}{25}$	$\frac{7.0}{12}$	$\frac{2.4}{2}$	2.2	$\frac{1.9}{4}$	$\frac{1.5}{10}$	$\frac{0.0}{29}$	$\frac{10.4}{33} = +24$
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$\frac{14.0}{33}$	$\frac{12.5}{14}$	$\frac{5.3}{4}$	5.2	$\frac{5.3}{4}$	$\frac{6.7}{9}$	$\frac{7.1}{14}$	$\frac{5.2}{28}$	$\frac{4.4}{33}$
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$\frac{9.5}{33}$	$\frac{7.2}{17}$	$\frac{1.5}{9}$	$\frac{1.0}{3}$	$\frac{1.6}{2}$	1.4	$\frac{1.0}{9}$	$\frac{2.0}{15}$	$\frac{1.8}{20}$	$\frac{2.2}{23}$	$\frac{0.0}{27}$	$\frac{12.0}{33}$
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$\frac{15.3}{33}$	$\frac{15.1}{31}$	$\frac{12.5}{24}$	$\frac{11.2}{20}$	$\frac{7.5}{14}$	$\frac{7.0}{9}$	7.4	$\frac{6.7}{5}$	$\frac{5.9}{10}$	$\frac{4.6}{12}$	$\frac{4.3}{17}$	$\frac{5.3}{17}$	$\frac{4.7}{21}$
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$\frac{5.4}{33}$	$\frac{6.2}{31}$	$\frac{5.7}{25}$	$\frac{4.8}{21}$	$\frac{3.3}{14}$	$\frac{3.8}{8}$	3.7	$\frac{2.7}{4}$	$\frac{0.1}{7}$
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13.4	$\frac{9.2}{10}$	$\frac{8.4}{15}$	$\frac{8.2}{17}$	$\frac{6.4}{21}$	$\frac{3.8}{33}$
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$\frac{5.6}{33}$	$\frac{5.1}{28}$	$\frac{4.2}{19}$	$\frac{9.9}{12}$	$\frac{8.6}{1}$	8.5	$\frac{0.0}{9}$
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Sta.	T	H.I. ✓ 928.57	-	Elev.
9700				920.6
716				22.0
738				23.9
762				27.1
T. R.	11.72	938.35 ✓	1.94	926.63 ✓
8790				20.1
9700				20.6
9714				22.0
9738				23.9
9762				27.1
9774				32.2
9785				36.1
10700				33.7
B. M.			6.44	931.71 ✓
720				32.7

Lt.

Rt.

$\frac{5.2}{33}$	$\frac{2.5}{30}$	$\frac{2.1}{23}$	$\frac{7.4}{19}$	$\frac{9.2}{14}$	8.0	$\frac{4.9}{6}$	$\frac{3.0}{11}$
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$\frac{7.6}{24}$	$\frac{8.2}{14}$	$\frac{7.4}{12}$	$\frac{7.2}{1}$	6.4	$\frac{5.6}{13}$	$\frac{3.8}{15}$
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$\frac{6.1}{38}$	$\frac{7.1}{33}$	$\frac{6.8}{18}$	$\frac{4.7}{12}$	4.7	$\frac{4.4}{15}$	$\frac{2.8}{21}$	$\frac{1.0}{25}$
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$\frac{2.9}{32}$	$\frac{2.8}{19}$	$\frac{1.2}{15}$	1.5
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18.3	$\frac{9.9}{11}$	$\frac{7.8}{17}$	$\frac{7.5}{33}$
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17.8	$\frac{6.2}{16}$	$\frac{6.2}{21}$	$\frac{5.4}{33}$
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$\frac{10.1}{41}$	$\frac{9.2}{35}$	16.4	$\frac{10.7}{19}$	$\frac{2.6}{30}$	$\frac{2.7}{33}$
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$\frac{6.0}{53}$	$\frac{8.4}{50}$	14.5	$\frac{9.1}{28}$	$\frac{6.4}{33}$	$\frac{0.0}{41}$
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$\frac{5.7}{48}$	$\frac{3.2}{43}$	11.3	$\frac{9.8}{4}$	$\frac{7.5}{9}$	$\frac{7.3}{19}$	$\frac{3.9}{27}$	$\frac{0.1}{36}$
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$\frac{3.4}{43}$	$\frac{3.2}{37}$	$\frac{10.3}{28}$	$\frac{11.1}{20}$	$\frac{10.9}{7}$	$\frac{9.5}{5}$	6.2	$\frac{0.9}{4}$	$\frac{1.4}{21}$	$\frac{2.8}{33}$
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$\frac{3.6}{34}$	$\frac{3.3}{31}$	$\frac{8.7}{22}$	$\frac{9.7}{17}$	$\frac{9.6}{8}$	$\frac{7.9}{6}$	2.3	$\frac{1.4}{8}$	$\frac{4.1}{27}$	$\frac{4.7}{33}$
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$\frac{4.8}{33}$	$\frac{4.5}{27}$	$\frac{8.5}{20}$	$\frac{8.3}{14}$	$\frac{8.4}{8}$	$\frac{4.8}{3}$	4.7	$\frac{4.5}{14}$	$\frac{5.1}{20}$	$\frac{5.0}{33}$
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SPK. in Tree 50' Lt. Sta. 10 + 25.

$\frac{7.1}{33}$	$\frac{7.3}{23}$	$\frac{7.0}{9}$	$\frac{6.6}{5}$	5.7	$\frac{5.7}{11}$	$\frac{6.4}{18}$	$\frac{6.9}{33}$
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Sta.	+	M.I. ✓	-	Elev.
		938.35		
+75				934.6
11700				34.4
T.P.	1.24	928.95 ✓	10.64	927.71 ✓
+79				24.8
12700				23.1
+57				19.2
T.P.	1.27	918.34 ✓	11.84	917.09 ✓
13700				13.7
+66				06.9
14700.				05.8
+41				05.9
15700				15.2
T.P.	8.85	924.03 ✓	3.18	915.18 ✓
+50				17.3
16700				18.4
B.M.			6.44	917.59 ✓ 917.57
+32				18.3

4/24/25

Lt.

Rt.

$\frac{6.8}{33}$	$\frac{6.0}{25}$	$\frac{4.8}{13}$	$\frac{4.2}{11}$	3.8	$\frac{3.5}{19}$	$\frac{4.6}{33}$
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$\frac{7.2}{33}$	$\frac{5.8}{21}$	$\frac{4.2}{15}$	4.0	$\frac{4.5}{14}$	$\frac{5.9}{33}$
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$\frac{4.0}{33}$	$\frac{3.6}{26}$	$\frac{2.8}{21}$	$\frac{3.0}{11}$	4.2	$\frac{6.0}{18}$	$\frac{7.5}{33}$
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$\frac{5.7}{33}$	$\frac{5.4}{29}$	$\frac{4.8}{21}$	$\frac{4.6}{11}$	5.9	$\frac{7.4}{14}$	$\frac{8.7}{33}$
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$\frac{10.7}{33}$	$\frac{10.5}{27}$	$\frac{9.6}{20}$	$\frac{9.3}{13}$	$\frac{9.6}{11}$	9.8	$\frac{10.9}{14}$	$\frac{12.4}{33}$
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$\frac{3.0}{33}$	$\frac{2.9}{29}$	$\frac{2.3}{22}$	$\frac{2.7}{20}$	$\frac{3.0}{13}$	4.7	$\frac{6.3}{17}$	$\frac{8.3}{33}$
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$\frac{8.4}{33}$	$\frac{8.0}{24}$	$\frac{8.5}{23}$	$\frac{8.7}{18}$	$\frac{9.4}{14}$	$\frac{11.0}{5}$	11.5	$\frac{12.6}{7}$	$\frac{12.0}{33}$
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$\frac{10.3}{33}$	$\frac{10.2}{24}$	$\frac{10.8}{23}$	$\frac{10.9}{19}$	$\frac{11.6}{14}$	$\frac{12.4}{11}$	12.6	$\frac{12.8}{20}$	$\frac{12.6}{33}$
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$\frac{12.2}{33}$	$\frac{12.3}{24}$	$\frac{12.1}{19}$	$\frac{12.6}{14}$	12.5	$\frac{12.5}{20}$	$\frac{12.5}{33}$
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$\frac{7.7}{33}$	$\frac{7.1}{30}$	$\frac{6.1}{25}$	$\frac{5.4}{30}$	$\frac{4.6}{13}$	3.2	$\frac{3.0}{17}$	$\frac{1.7}{33}$
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$\frac{12.2}{33}$	$\frac{10.2}{25}$	$\frac{9.5}{22}$	$\frac{8.6}{17}$	$\frac{7.6}{4}$	6.7	$\frac{3.8}{19}$	$\frac{2.4}{33}$
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$\frac{10.8}{33}$	$\frac{9.3}{24}$	$\frac{7.6}{19}$	$\frac{6.6}{8}$	5.4	$\frac{4.5}{8}$	$\frac{3.0}{19}$	$\frac{2.0}{23}$	$\frac{1.4}{33}$
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Spk. in Tree 15 Lt. Str. 16 + 32.

$\frac{12.9}{33}$	$\frac{7.0}{23}$	$\frac{7.3}{17}$	$\frac{6.8}{9}$	5.7	$\frac{3.8}{18}$	$\frac{3.0}{33}$
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Sta.	T.	H.I.	-	Elev
		924.03		
+64		✓		913.8
T.P.	2.07	915.15	10.95	913.08
14+64				13.8
17+00				09.0
+11		✓		06.5
T.P.	0.13	905.41	9.87	905.28
17+00				09.0
+11				06.5
+23		✓		900.8
T.P.	4.34	898.32	11.43	893.98
17+23				900.8
+50		✓		887.7
T.P.	4.20	892.76	7.86	888.44
17+50				887.7
+73		✓		77.8
T.P.	4.10	885.00	11.84	880.90
17+73				77.8
18+00		✓		74.4
T.P.	3.27	876.44	11.83	873.17

Lt.

Rt.

$$\frac{12.1}{12} \quad 10.2 \quad \frac{8.2}{11} \quad \frac{6.8}{20} \quad \frac{7.0}{33}$$

$$\frac{10.6}{33} \quad \frac{6.3}{28} \quad \frac{3.8}{17} \quad \frac{5.1}{14} \quad \frac{5.1}{15} \quad 14$$

$$\frac{9.3}{7} \quad \frac{7.6}{4} \quad 4.2 \quad \frac{3.2}{9} \quad \frac{1.7}{27} \quad \frac{1.6}{33}$$

$$8.7 \quad \frac{7.6}{7} \quad \frac{5.4}{15} \quad \frac{3.4}{33} \quad \frac{5.3}{34} \quad \frac{2.5}{36}$$

$$\frac{13.6}{33} \quad \frac{8.4}{21} \quad \frac{5.1}{18} \quad \frac{5.8}{14} \quad \frac{5.8}{14} \quad \textcircled{+3.6}$$

$$\frac{17.5}{33} \quad \frac{14.5}{29} \quad \frac{8.5}{18} \quad \frac{9.7}{14} \quad \frac{9.5}{15}$$

$$\frac{12.2}{14} \quad \frac{12.2}{11} \quad \frac{9.0}{10} \quad \frac{6.4}{4} \quad 4.4 \quad \frac{0.2}{12} \quad \frac{0.3}{18} \quad \frac{7.9}{26} \quad \frac{0.0}{47}$$

$$\frac{12.8}{33} \quad \frac{9.5}{27} \quad \frac{6.9}{20} \quad \frac{5.1}{17}$$

$$10.4 \quad \frac{16.0}{9} \quad \frac{1.8}{25} \quad \frac{0.0}{38}$$

$$\frac{18.1}{33} \quad \frac{14.5}{25} \quad \frac{12.5}{19} \quad \frac{10.9}{14} \quad \frac{10.9}{11} \quad \frac{10.3}{8} \quad \frac{7.3}{5}$$

$$\frac{11.2}{10} \quad \frac{10.0}{11} \quad \frac{5.7}{23} \quad \frac{2.4}{33}$$

$$\frac{12.6}{33} \quad \frac{9.8}{20} \quad \frac{8.7}{14} \quad \frac{10.6}{8} \quad 7.2$$

$$10.4 \quad \frac{11.2}{8} \quad \frac{11.2}{17} \quad \frac{6.5}{26} \quad \frac{5.0}{33}$$

Sta. + H.I. - Elev.

876.44

18700

874.4

T.P.

+20

72.0

19700

70.7

B.M.

1.44

875.00

875.00

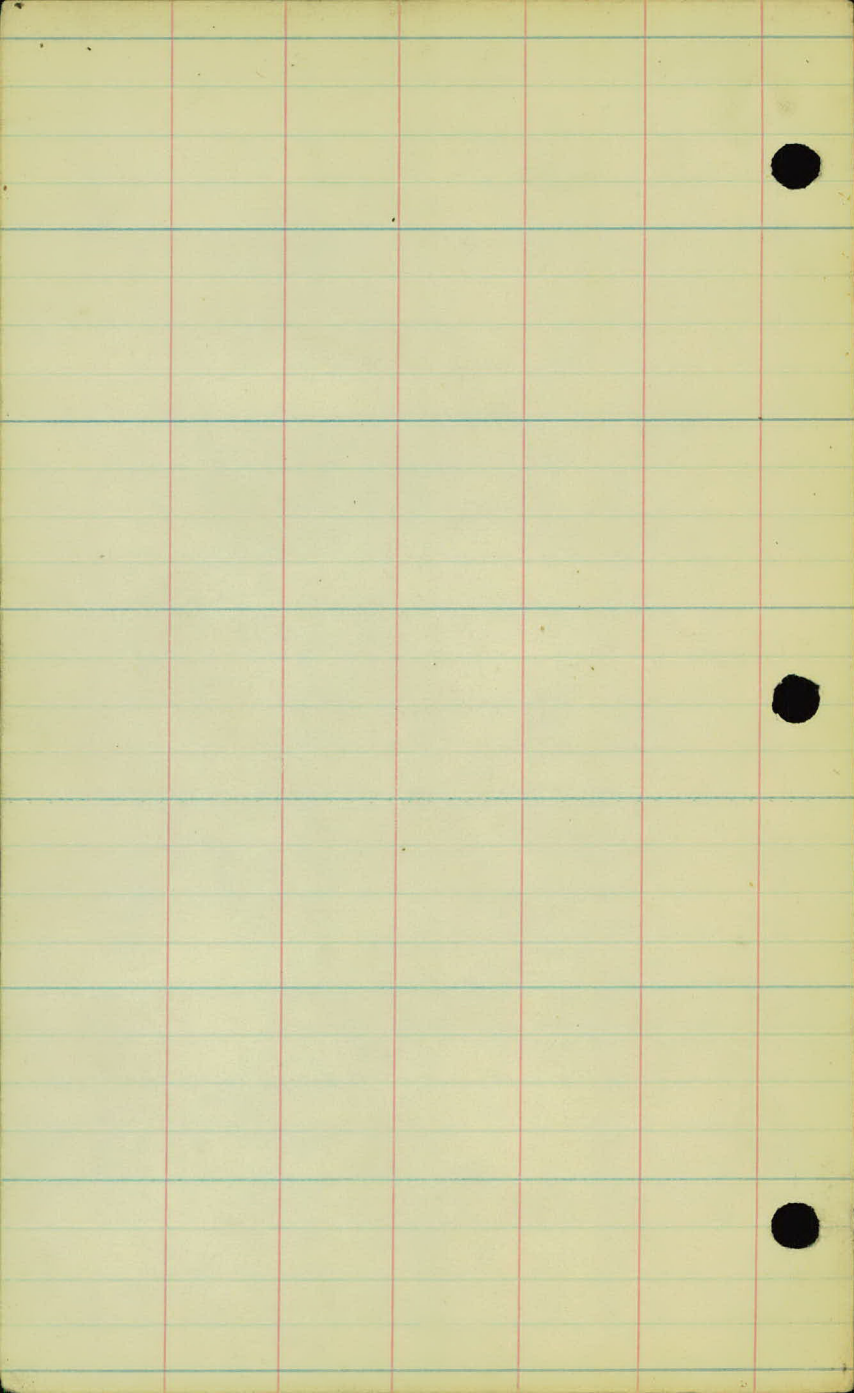
4/25/25

Water Elev. - 8.0      4.4  
52                      33

Water Elev. 80      60      4.7      5.0      4.7  
47      33      13      4.4      24      33

Water Elev. 80      74      6.5      5.0      4.2  
30      25      16      5.7      17      33

Spk. in 12" Tree 120' W. Sta. 18+30.



Canveng hole "B" line

Sta. 1+57 to 20+50

Station

Ang. ht. Ang Rt.

12+04.7 P.T.

11+09 P.I.

63°46'

9+84.3 P.C.

8+50 P.O.T

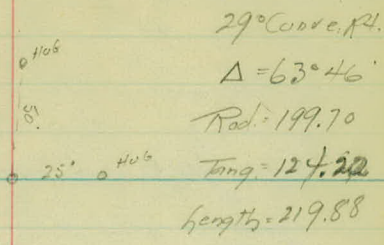
4+37.2 P.T.

3+00 P.I. 28°00'

1+57.0 P.C. = 1+57.0 Sea. line

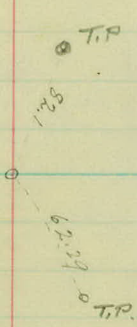
# "B" line

Sta - Def  
 9+45 - 0°00'  
 10+00 - 2°12'  
 +50 - 9°27'  
 11+00 - 16°42'  
 +50 - 23°57'  
 12+00 - 31°53'



29° Curve Pt.  
 $\Delta = 63^\circ 46'$   
 Rad. = 199.70  
 Tang. = 124.22  
 Length = 219.88

Sta - Def  
 1+57.0 - 0°00'  
 2+00 - 2°09'  
 +50 - 4°39'  
 3+00 - 7°09'  
 +50 - 9°39'  
 4+00 - 12°09'  
 +37 - 14°00'



10° Curve Pt.  
 $\Delta = 28^\circ 00'$   
 Rad. = 573.69  
 Tang. = 143.04  
 Length = 280.00

Station

Ang. ht. <sup>4</sup> Ang. Rt.

16+30.0 P.O.T

15+31.14 P.T.

14+26.5 P.I. 21° 12'

13+19.14 P.C.

# "B" line

Sta. - Elev

13+19.14 - 0000'

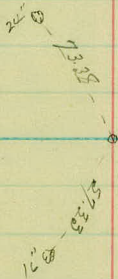
+50 - 1032 1/2'

14+00 - 4002 1/2'

+50 - 6035 1/2'

15+00 - 9002 1/2'

+31.14 - 10036'



10° Curve. H.

$\Delta = 21^\circ 12'$

Rad = 573.69

Tang = 107.36

Length = 212.00

Station

Ang. ht. <sup>±</sup> Ang. Rt.

20+50 P.O.T. End. "B" line

19+60.35

18+58.5 P.I. 36° 00'

17+48.6 P.C.

"B" line

6" @ 19.85'  $\rightarrow$  17.2 @ 12"

Sta. Def

17+48.6 - 0°00'

18+00 - 4°22'

+30 6°55'

+50 - 8°37'

19+00 - 12°52'

+60.35 - 18°00'

17° Curve. Rt.

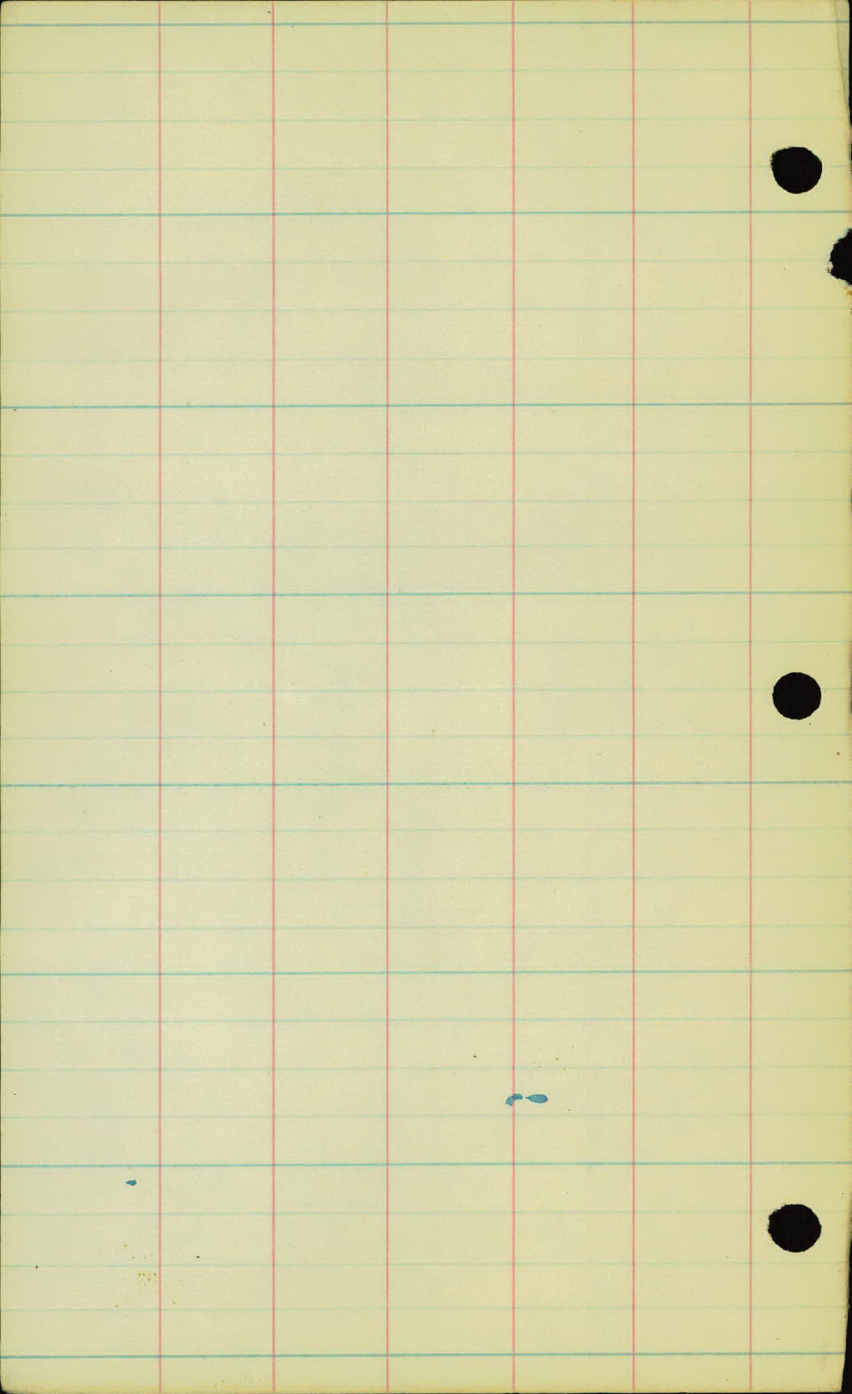
$\Delta = 36°00'$

Rad = 338.27

Tang = 109.91

Length = 211.76

30.95' @ 26.1'



Convens hake.

"B" line

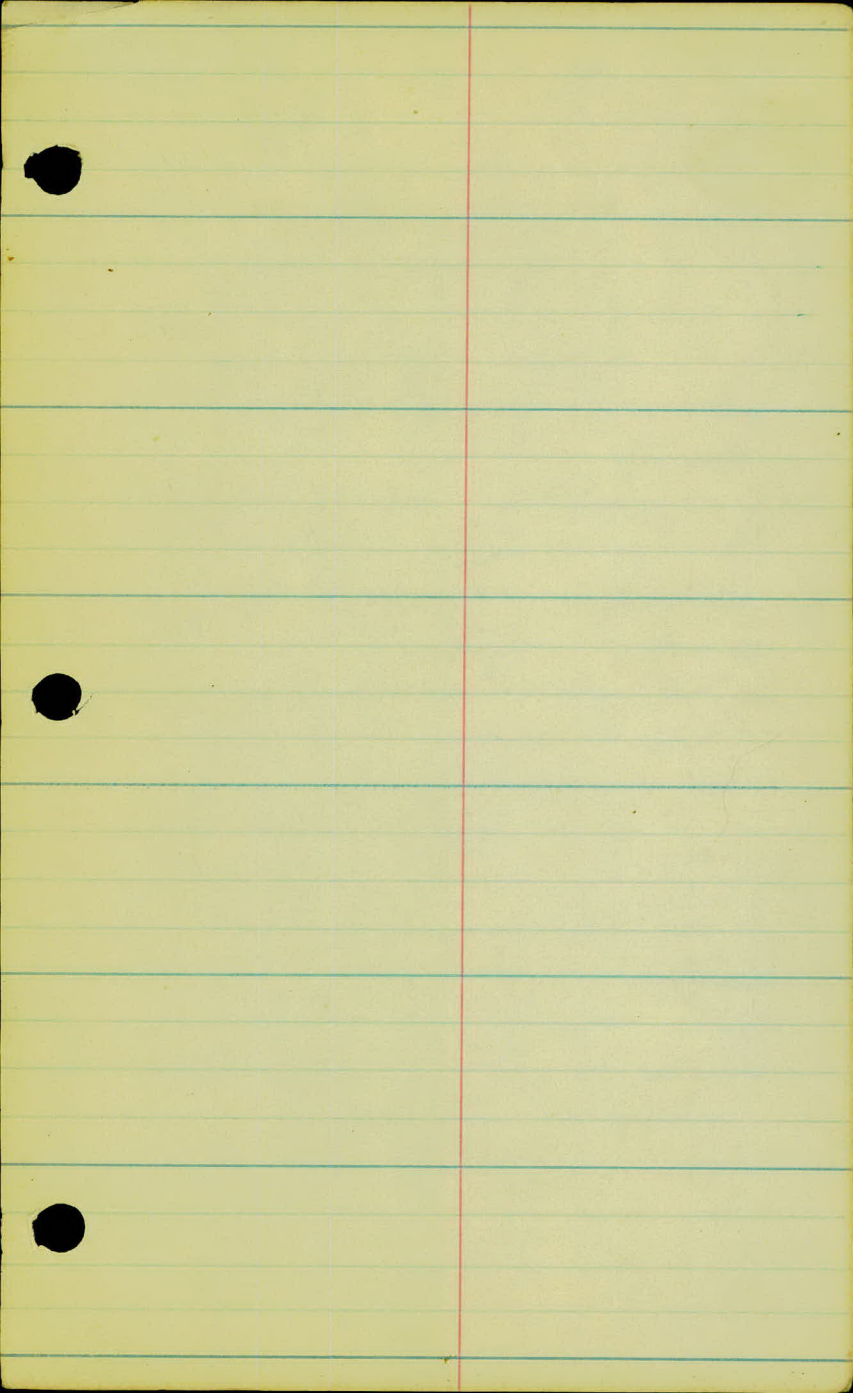
Sta 1+57 to 20+50

Carrens Lake TB line

Station	+	H.I.	-	Rod.	Elev.
B.M.	5.37	905.37			900.00
H57				8.8	96.6
2+00				8.6	96.8
+50				9.6	96.8
3+00				10.1	95.3
T.P.	0.22	894.39	11.20	894.17	
+50				3.0	91.4
+75				4.7	89.7
4+00				5.0	89.4
+50				5.6	88.8
5+00				6.3	88.1
+15				5.2	89.2
6+00				6.5	87.9
7+00				5.3	89.1
7+50				2.0	92.4
T.P.	4.29	897.36	1.32	893.07	
8+00				3.2	94.2
+50				3.0	94.4
+85				4.0	93.4
9+00				5.5	91.9
+20				7.1	90.3
10+00				8.2	89.2
+50				8.0	89.4
11+00				3.8	95.6
T.P.	2.49	898.27	1.58	895.78	

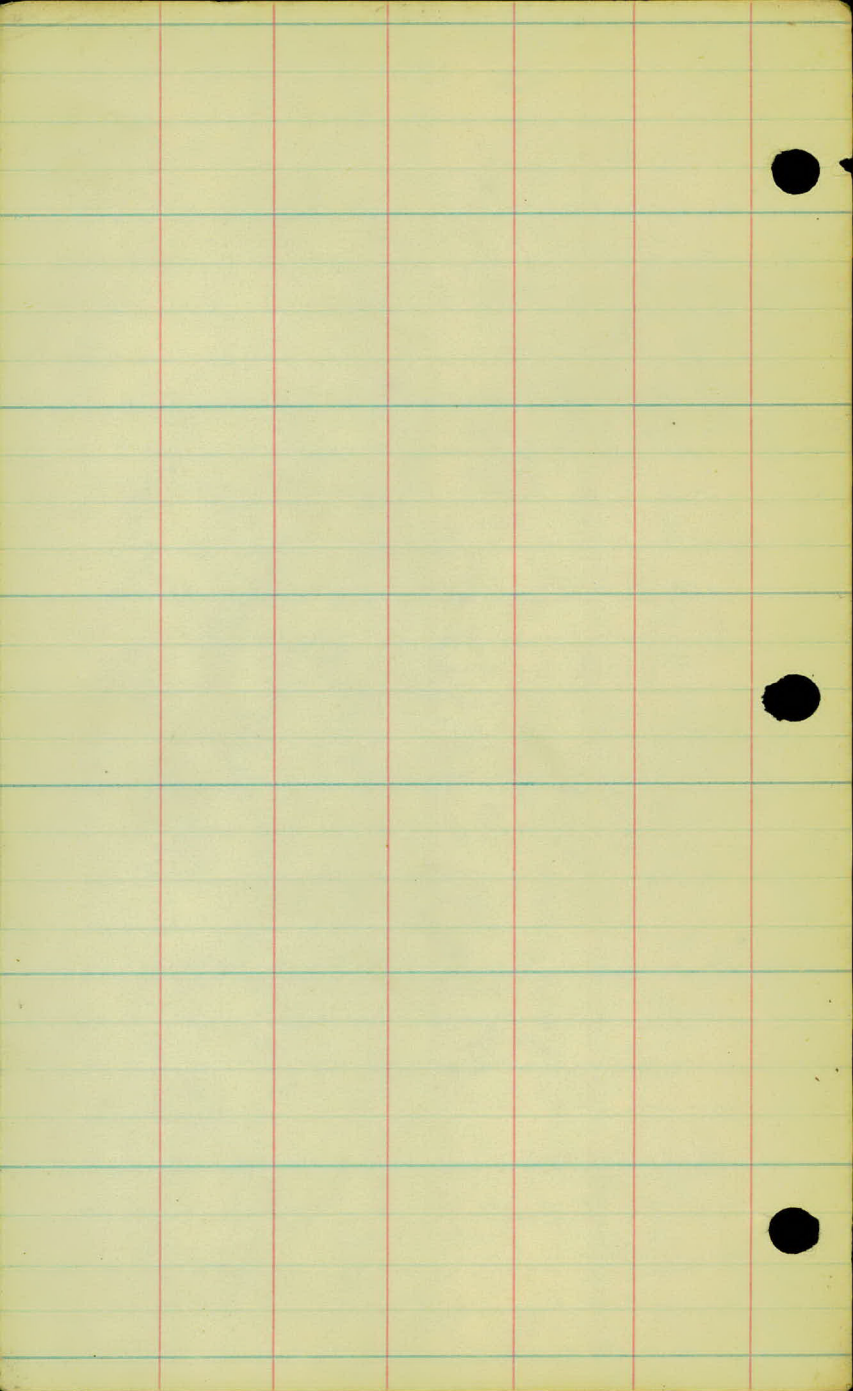
Sp. in P.P. 25' ht. Sta 0-28

Station	+	H.I.	-	Red.	Elev.
		498.27			
11+25				3.2	895.1
+50				2.1	96.2
+75				4.1	94.2
12+00				6.7	91.6
+15				9.0	89.3
+50				12.0	86.3
T.P.	0.12	886.89	11.50	886.77	
+59				1.7	85.2
+64				3.7	83.2
+80				5.6	81.3
13+00				6.3	80.6
+10				8.3	78.6
+20				8.2	78.7
T.P.	2.76	881.47	8.18	878.71	
+50				5.0	76.5
14+00				7.0	74.5
+25				8.2	73.3
+50				7.0	74.5
+80				7.4	74.1
15+00				7.0	74.5
+35				6.7	75.4
+50				4.1	77.4
+79				4.0	77.5
16+00				3.7	77.8
+30				5.1	76.4
T.P.	4.58	880.99	5.06	876.41	



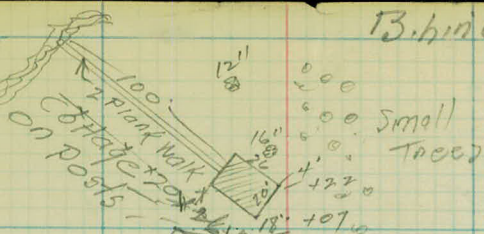
Station	+	H.I.	-	ROD,	Elev.
		880.99			
16+60				5.8	875.2
17+00				6.6	74.4
+30				5.0	76.0
+50				3.2	77.8
+75				1.6	79.4
T.P.	5.35	882.05	4.29	876.70	
18+00				3.0	79.1
+30				5.1	77.0
+50				6.1	76.0
+75				5.8	76.3
19+00				6.4	75.7
+15				6.5	75.6
+30				5.1	77.0
+60				6.9	75.2
T.P.	2.01	877.28	6.78	875.27	
20+00				3.2	74.1
+30				4.5	72.8
+50				3.5	73.8
B.M.			2.28	875.00	

Sp. in 12" Tree 15' Rt sta. 20-60



B.hine 14+00

lake



13+00



+54.5 Fence. Xing

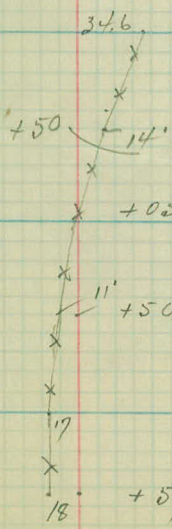
12+04.7 59'

12+00

11+00

4+00

Pasture



+05 Fence. Xing 3+00

+50

2+00

+57

1+00

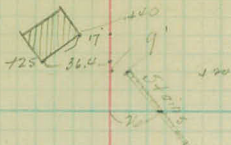
10.75  
1.25  
13.75  
1.80  
15.55

950.3  
1.05  
951.35

"B" line

21+00

12.5 x 24  
Bath. Ho



20+00

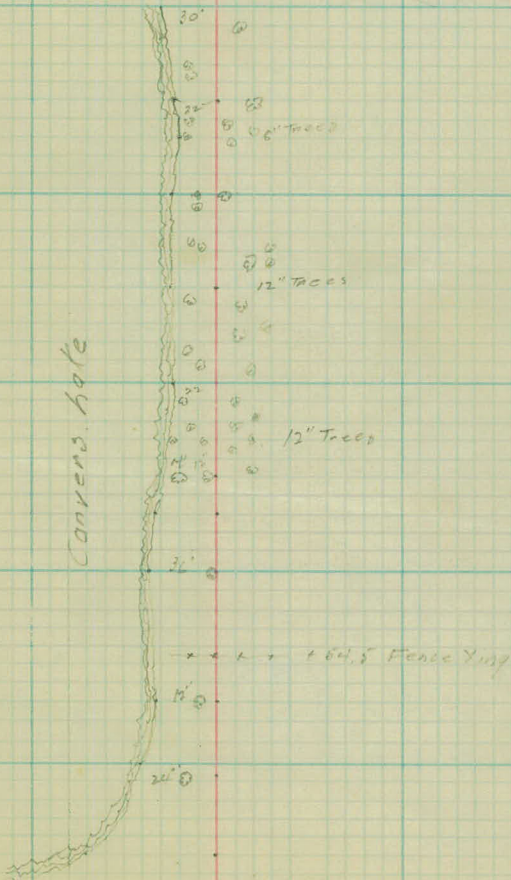
19+42 "B" line = }  
17+79.5 Sec. line }

Deep  
Wash. cut

19+42 Sec. line  
= 17+79.5

19+00

Canverson hole



18+00

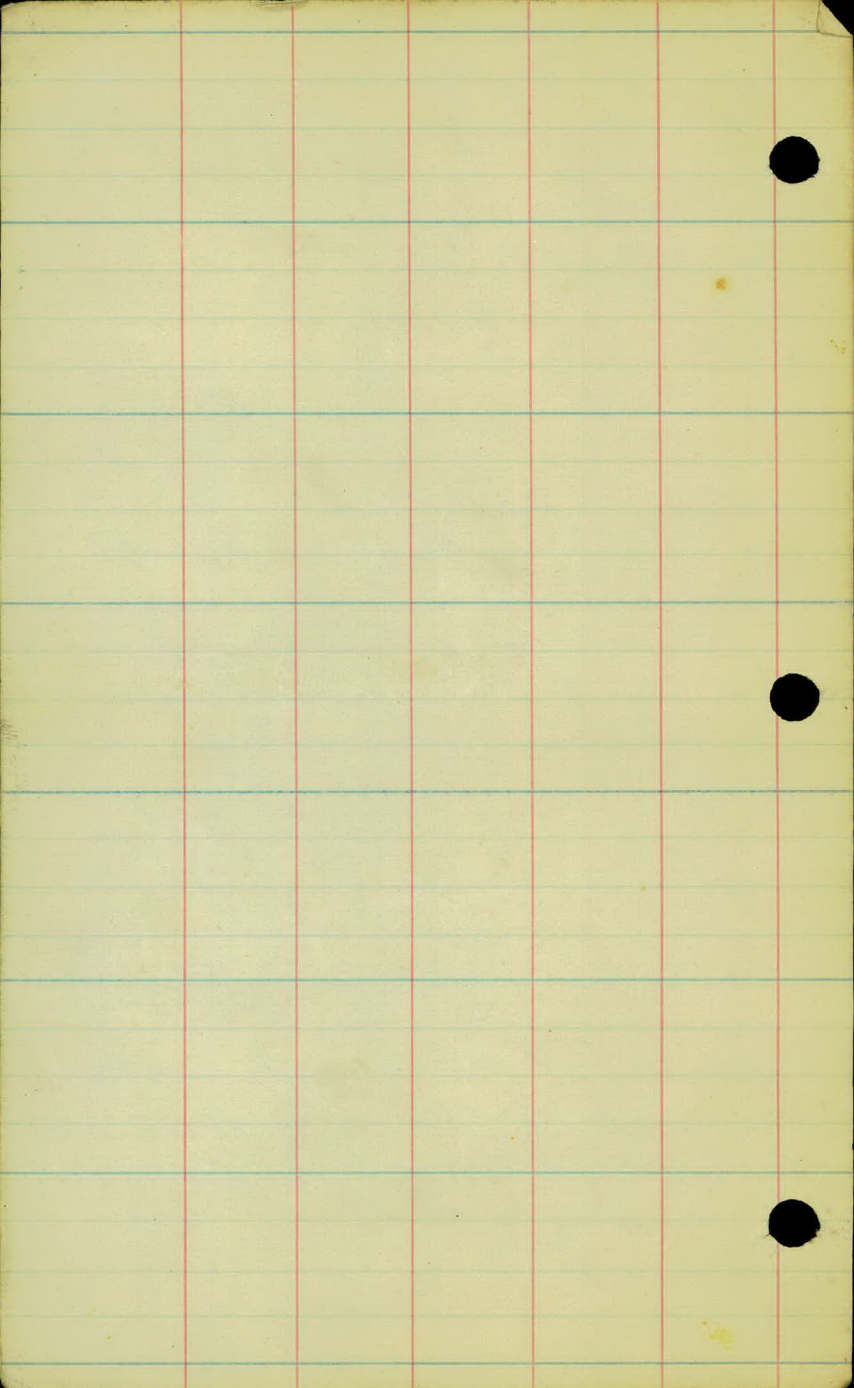
17+00

16+00

15+00

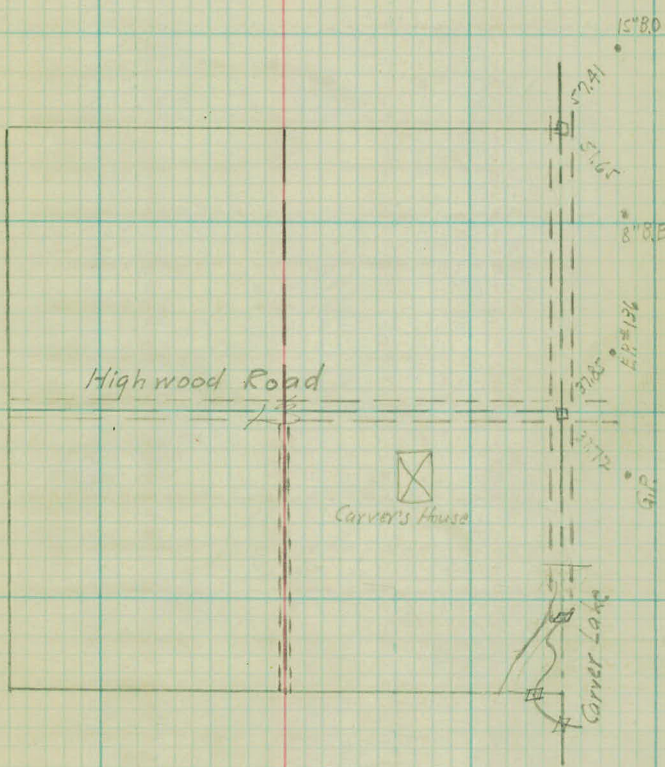
14+00

164.5 Fence Line

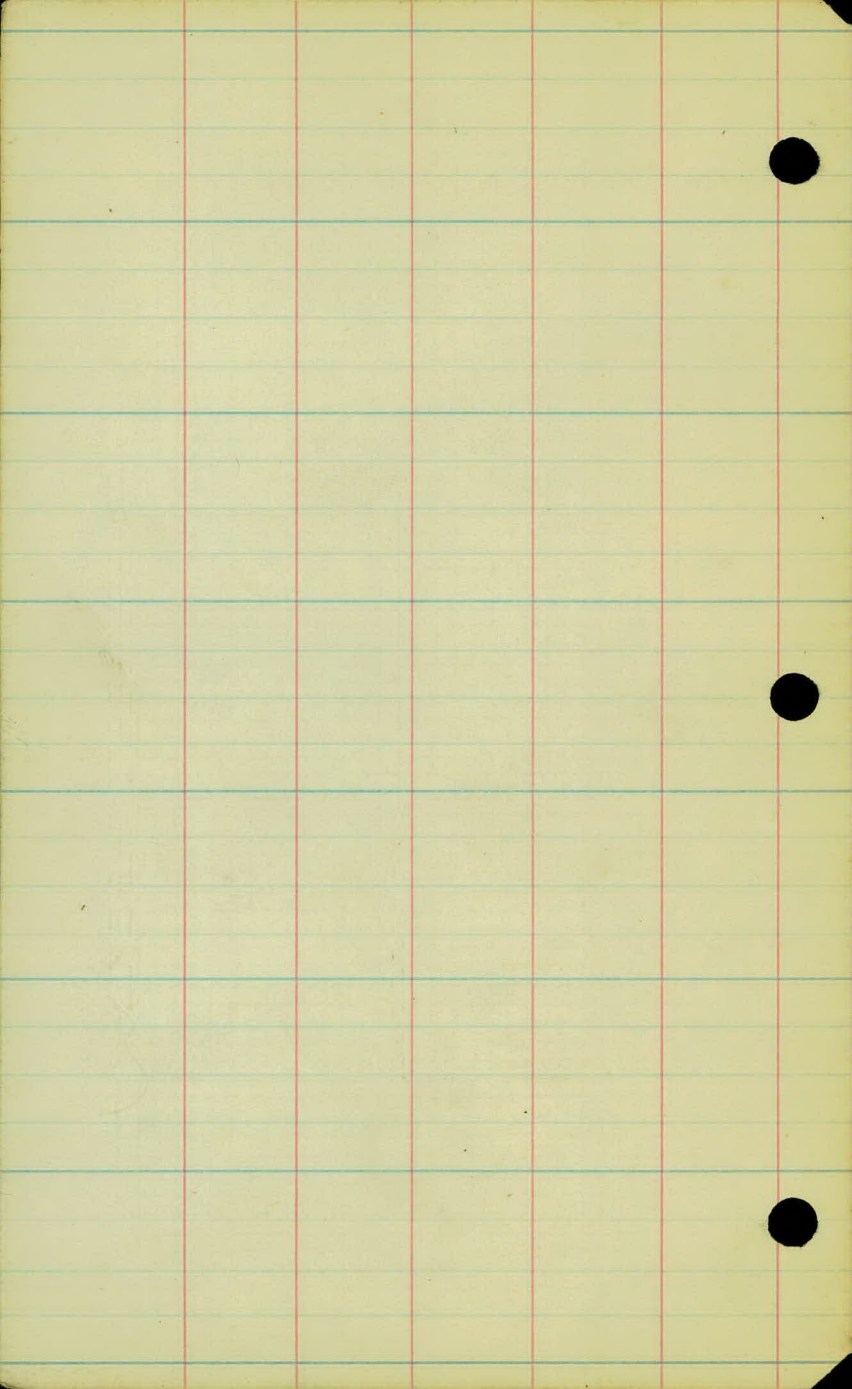


SEC. 13 - T28N - R22W

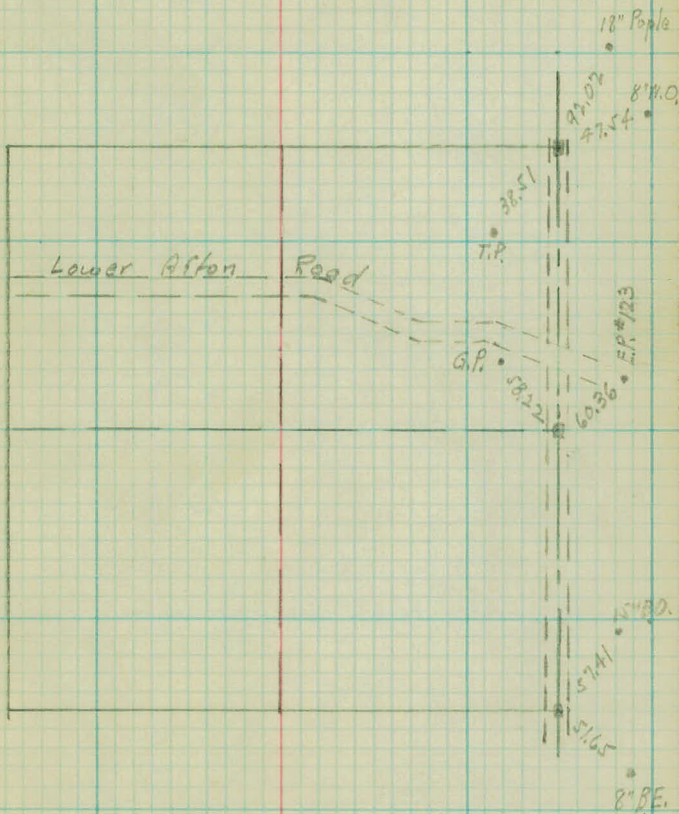
$\frac{42}{7}$   $\frac{8.2}{9}$   $\frac{7.2}{5}$

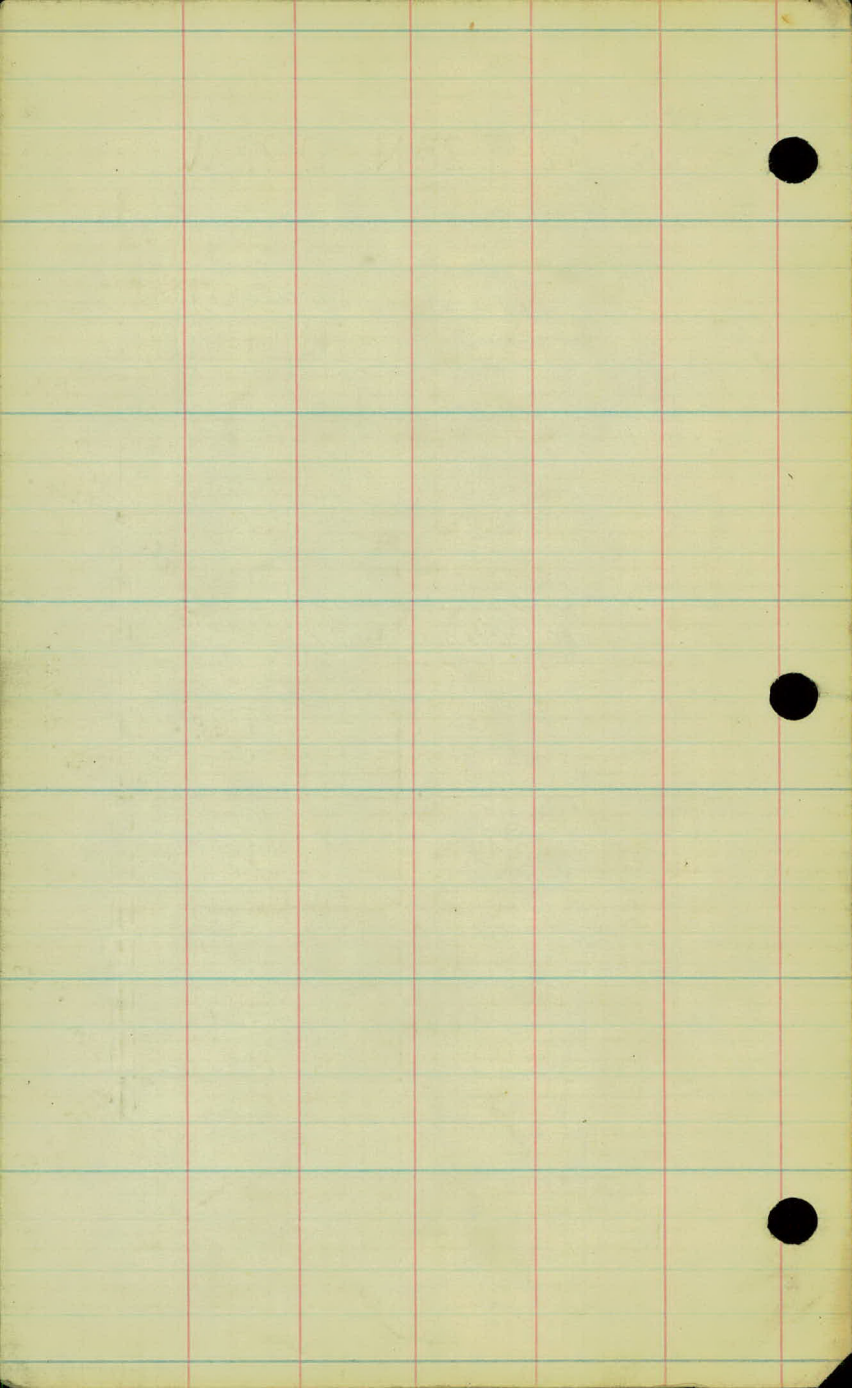


Ask Mr. Carver about M.C. of Lake.  
P.R.B. says Carver pointed one out to him.



SEC. 12-T. 28N. - R 22W:





Carvens Lake.  
"A" line.

Station	+	H.I.	-	Rod	Filev
B.M.	7.03	928.93 <sup>✓</sup>			931.90 <sup>✓</sup>
9+53 <sup>25</sup>				12.7	926.2
+62				11.9	27.0
+74				6.6	32.3
+85				3.0	35.9
10+00				5.3	33.6
+25				6.1	32.8
+50				5.3	33.6
+80				4.0	34.9
11+00				5.1	33.8
T.P.	2.41	929.28 <sup>✓</sup>	12.06	926.87 <sup>✓</sup>	
+50					26.8
+75					22.3
12+00					19.7
T.P.	1.29	918.94 <sup>✓</sup>	11.63	917.65 <sup>✓</sup>	

ht.

h

Rt.

6-5-25

Spike in Tree 50' ht 5 to 10 + 25

$\frac{14.8}{33.0}$	$\frac{14.0}{29.7}$	$\frac{15.5}{23.6}$	$\frac{13.4}{13.6}$	$\frac{13.3}{7.8}$	12.7	$\frac{12.6}{4.7}$	$\frac{10.4}{6.5}$	$\frac{9.5}{13.5}$	$\frac{6.4}{26.0}$	$\frac{0.4}{36.7}$
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$\frac{13.7}{33.0}$	$\frac{14.7}{24.0}$	$\frac{12.6}{15.2}$	$\frac{12.6}{8.5}$	11.9	$\frac{10.3}{6.0}$	$\frac{7.6}{7.2}$	$\frac{6.2}{19.0}$	$\frac{1.2}{29.5}$	$\frac{0.4}{33.0}$
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$\frac{3.9}{37.0}$	$\frac{6.1}{36.0}$	$\frac{12.5}{24.8}$	$\frac{11.6}{20.3}$	$\frac{11.4}{7.0}$	6.6	$\frac{1.2}{7.7}$	$\frac{1.5}{23.0}$	$\frac{2.7}{33.0}$
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$\frac{3.9}{33.0}$	$\frac{4.0}{31.0}$	$\frac{11.3}{20.5}$	$\frac{10.2}{17.6}$	$\frac{10.3}{9.0}$	3.0	$\frac{3.7}{18.0}$	$\frac{5.3}{33.0}$
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$\frac{5.7}{33.0}$	$\frac{5.4}{21.4}$	$\frac{4.0}{26.5}$	$\frac{9.2}{21.3}$	$\frac{8.6}{14.1}$	$\frac{8.8}{8.4}$	$\frac{5.4}{4.8}$	5.3	$\frac{5.1}{16.0}$	$\frac{5.6}{20.4}$	$\frac{5.3}{31.8}$	$\frac{5.4}{33.0}$
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$\frac{7.5}{33.0}$	$\frac{7.8}{28.0}$	$\frac{7.4}{14.4}$	$\frac{6.8}{11.4}$	6.1	$\frac{7.0}{15.0}$	$\frac{7.7}{33.0}$
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$\frac{7.3}{33.0}$	$\frac{6.6}{17.6}$	$\frac{5.5}{13.6}$	5.3	$\frac{5.2}{11.3}$	$\frac{6.0}{25.0}$	$\frac{6.4}{33.0}$
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$\frac{6.1}{33.0}$	$\frac{4.6}{22.1}$	$\frac{4.7}{16.4}$	4.0	$\frac{4.0}{7.8}$	$\frac{5.2}{21.5}$	$\frac{6.5}{33.0}$
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$\frac{5.9}{33.0}$	$\frac{5.0}{30.7}$	$\frac{5.0}{24.0}$	$\frac{4.6}{10.7}$	5.1	$\frac{6.1}{19.6}$	$\frac{7.8}{33.0}$
--------------------	--------------------	--------------------	--------------------	-----	--------------------	--------------------

$\frac{1.4}{33.0}$	$\frac{2.2}{15.0}$	2.5	$\frac{3.0}{13.0}$	$\frac{4.5}{33.0}$
--------------------	--------------------	-----	--------------------	--------------------

$\frac{5.1}{33.0}$	$\frac{6.4}{14.5}$	7.0	$\frac{7.2}{19.0}$	$\frac{7.0}{33.0}$
--------------------	--------------------	-----	--------------------	--------------------

$\frac{7.5}{33.0}$	$\frac{8.5}{16.0}$	9.6	$\frac{10.1}{17.0}$	$\frac{10.1}{33.0}$
--------------------	--------------------	-----	---------------------	---------------------

918.94

12 + 50					15.7
+ 75					12.6
13 + 00					11.2
+ 50					08.5
14 + 00					10.7
+ 50					13.8
15 + 00					14.4
+ 25					14.1
+ 50					10.8
T.P.	2.00	913.20	7.74	911.20	
+ 80					05.1
16 + 00					03.9
+ 18					01.7
+ 83					900.0

H.                       $\frac{1}{2}$                       R.

$\frac{2.0}{33.0}$      $\frac{3.0}{17.0}$     3.2     $\frac{3.5}{19.0}$      $\frac{2.7}{33.0}$

$\frac{5.7}{33.0}$      $\frac{6.2}{21.0}$     6.3     $\frac{5.5}{13.0}$      $\frac{4.0}{33.0}$

$\frac{9.6}{33.0}$      $\frac{9.7}{23.0}$     7.7     $\frac{6.2}{22.0}$      $\frac{5.7}{33.0}$

$\frac{11.6}{33.0}$      $\frac{11.2}{19.5}$     10.4     $\frac{9.2}{14.5}$      $\frac{7.2}{33.0}$

$\frac{11.2}{33.0}$      $\frac{11.2}{28.0}$      $\frac{10.6}{18.0}$     8.2     $\frac{6.2}{16.0}$      $\frac{4.1}{33.0}$

$\frac{8.6}{33.0}$      $\frac{7.1}{19.0}$     5.1     $\frac{3.3}{18.0}$      $\frac{1.7}{33.0}$

$\frac{6.4}{33.0}$      $\frac{5.8}{18.5}$     4.5     $\frac{3.8}{11.0}$      $\frac{1.6}{33.0}$

$\frac{5.5}{33.0}$      $\frac{5.0}{17.5}$     4.8     $\frac{4.3}{18.0}$      $\frac{4.2}{33.0}$

$\frac{5.0}{33.0}$      $\frac{6.5}{25.0}$     8.1     $\frac{8.1}{19.5}$      $\frac{7.7}{33.0}$

$\frac{0.8}{33.0}$      $\frac{6.4}{9.8}$     8.1     $\frac{8.7}{11.0}$      $\frac{9.0}{24.0}$      $\frac{8.7}{33.0}$

$\frac{2.0}{33.0}$      $\frac{6.6}{14.5}$     9.3     $\frac{10.7}{11.0}$      $\frac{11.9}{33.0}$

$\frac{2.7}{33.0}$      $\frac{6.0}{18.7}$      $\frac{6.3}{13.5}$      $\frac{10.0}{6.6}$     11.5     $\frac{14.7}{14.5}$      $\frac{19.5}{23.0}$      $\frac{21.0}{28.5}$      $\frac{19.5}{33.0}$

$\frac{3.3}{33.0}$      $\frac{5.0}{32.0}$      $\frac{6.4}{27.6}$      $\frac{8.0}{14.0}$      $\frac{10.6}{7.0}$     13.2     $\frac{17.1}{11.0}$      $\frac{19.5}{20.5}$      $\frac{21.0}{27.0}$      $\frac{22.5}{30.3}$      $\frac{27.6}{30.7}$      $\frac{29.3}{35.0}$   
27.5 293  
22.4 38.5

913.20

16 + 50

898.2

T.P. 1.27 906.40 8.07 905.13

+ 76

93.1

T.P. 2.03 897.20 11.23 895.17

17 + 00

89.5

+ 22

89.2

B.M.

3.72 893.48

+ 50

84.8

T.P. 1.22 888.30 10.12 887.08

18 + 00

78.0

+ 50

76.0

T.P. 10.22 876.48 12.04 876.26

19 + 00

75.3

B.M.

11.40 875.08 <sup>875.08</sup>

+ 50

73.8

T.P. 10.26 884.72 12.02 874.46

20 + 00

72.7

+ 50

72.5

21 + 00

72.6

+ 50

72.6

B.M.

9.64 875.08

ht. ft. ft.

3.2	6.0	9.0	9.7	16.0	16.6	21.3	23.0	26.5	32.5
38.5	31.5	25.5	11.4	15.0	25.5	15.0	19.5	34.8	37.8
								28.3	32.0
								73.6	65.0

906.6	0.3	2.5	6.2	8.2	9.7	13.3	15.7	22.0	22.6	26.5	26.5	28.5
33.0	31.4	30.3	23.2	16.4	5.5	13.3	5.5	21.0	23.8	30.0	41.0	44.5

903.8	902.1	0.7	1.7	3.3	7.7	12.0	13.7	14.0	17.5	17.3	15.7	14.5
33.0	29.4	26.0	15.5	6.3	7.7	10.0	13.0	15.8	16.7	30.0	35.5	30.0

x 15.5	16.0	18.2	15.0	14.8	14.3	11.0	6.2	4.7	897.6	902.8	x
47.6	33.6	30.5	19.2	15.3	12.5	2.0	9.0	70.5	79.0	33.0	

Nail in 6" Oak 75' Rt. sta 17+22

895.2	2.8	7.6	9.6	11.0	11.8	14.0	11.6.0	16.8	17.8	19.2	19.0
33.0	24.0	12.3	11.4	8.7	5.2	12.4	70.5	13.8	20.0	27.8	29.0
										16.7	12.1

890.3	0.0	3.7	7.0	10.5	10.3	10.5	11.7	11.7	9.7	6.3
33.0	28.5	20.7	12.7	2.0	10.3	7.0	13.7	17.2	21.0	25.3
										33.0

6.6	12.3	12.8	12.3	12.6	12.6	3.7
33.0	17.5	13.0	12.3	10.6	11.8	15.5
						33.0

11.4	11.6	11.3	11.2	11.6	11.6	9.9	2.0
33.0	26.0	13.5	11.2	12.3	14.1	17.0	18.7
							33.0

Sp. in 12" Tree 40' ht. sta 19+10

12.3	12.3	12.7	12.3	12.7	12.7	11.5	4.5
33.0	22.0	6.0	12.7	11.7	13.0	16.7	17.9
							33.0

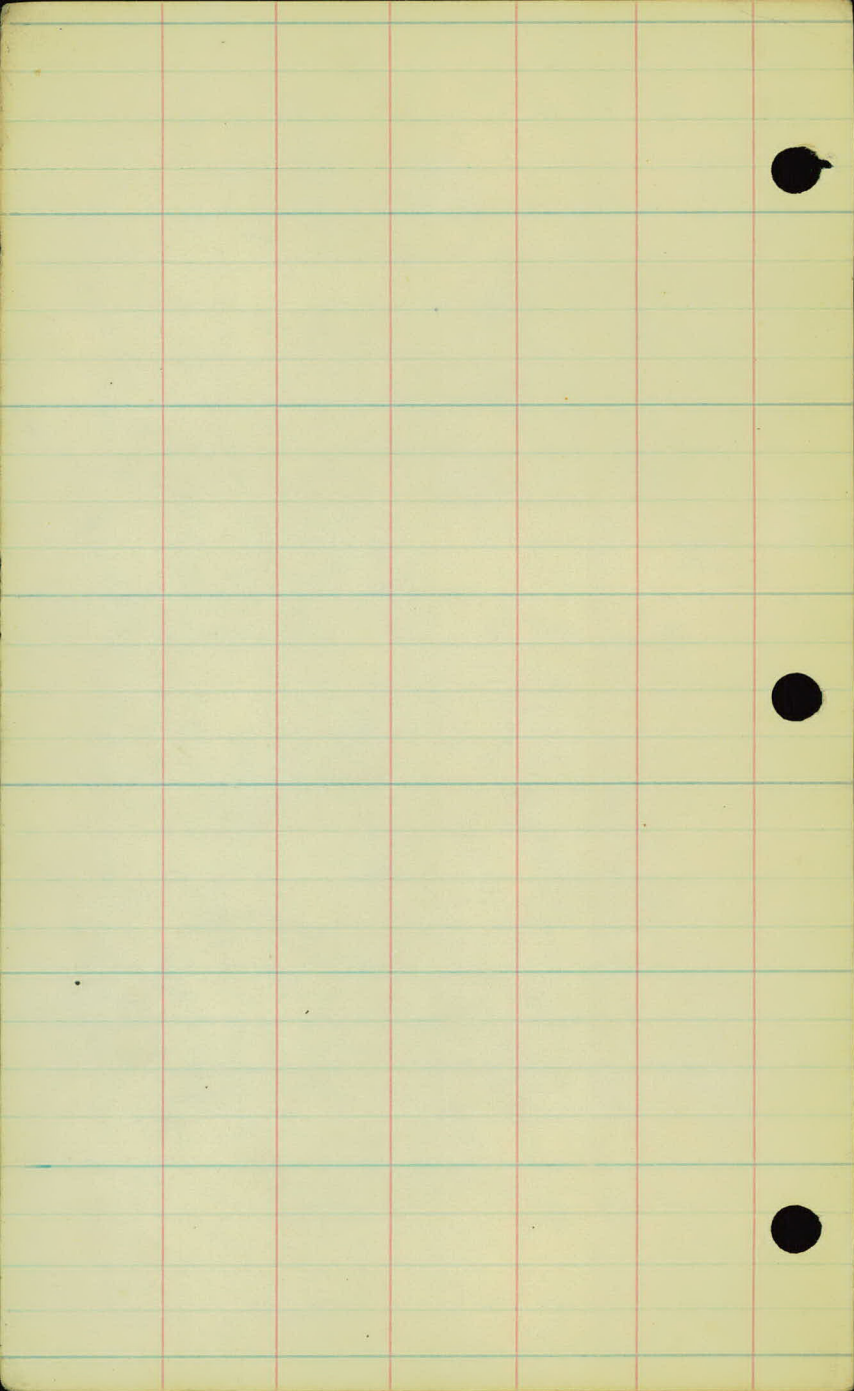
12.0	12.2	12.0	12.0	11.1	8.0	4.0	0.0	886.2
33.0	27.3	14.6	12.0	1.6	2.7	8.3	17.0	29.0
								33.0

13.2	13.0	12.7	12.0	5.5	2.5	0.0	857.9
33.0	23.0	3.7	12.2	4.0	12.6	18.5	24.5
							33.0

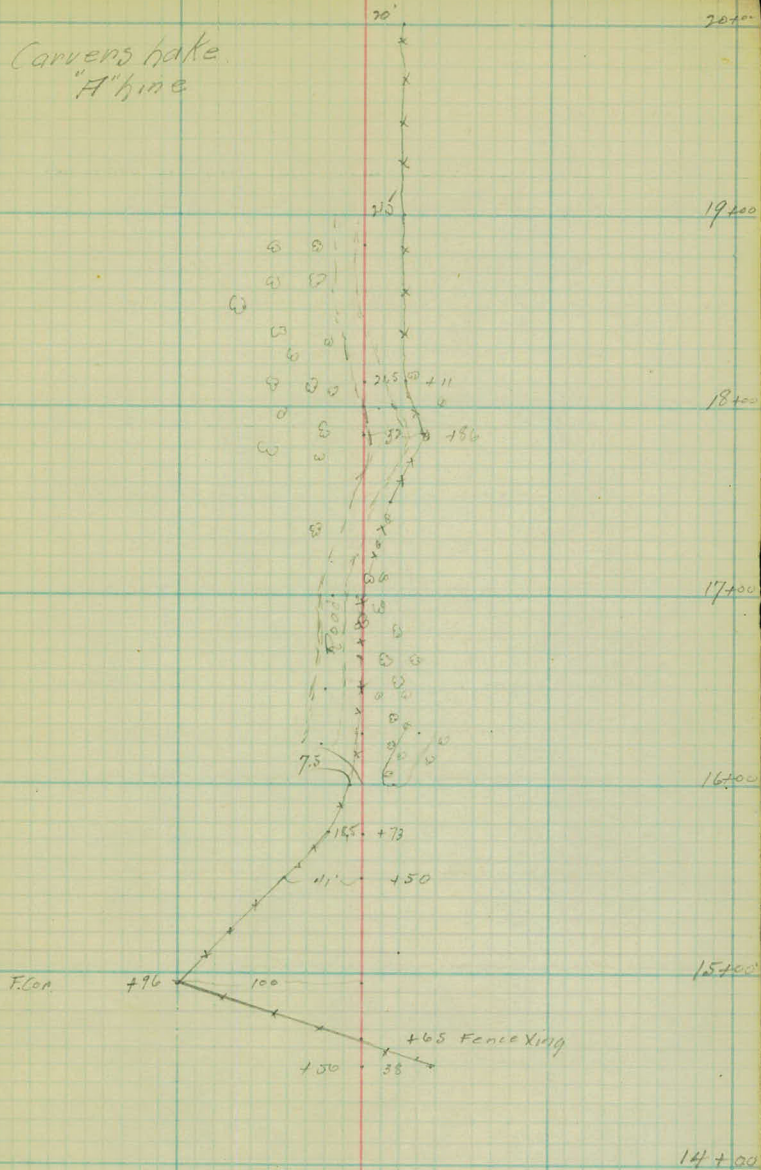
14.3	14.4	13.8	11.3	6.4	1.0	888.4
33.0	14.5	9.5	12.1	4.0	11.1	21.0
						33.0

15.8	15.0	10.6	5.2	1.4	887.7	870.5
33.0	17.0	12.1	4.9	12.5	16.5	24.0
						33.0

Sp. in 12" Tree 40' ht. sta 19+10



Carvers Lake  
"A" line



2010

19100

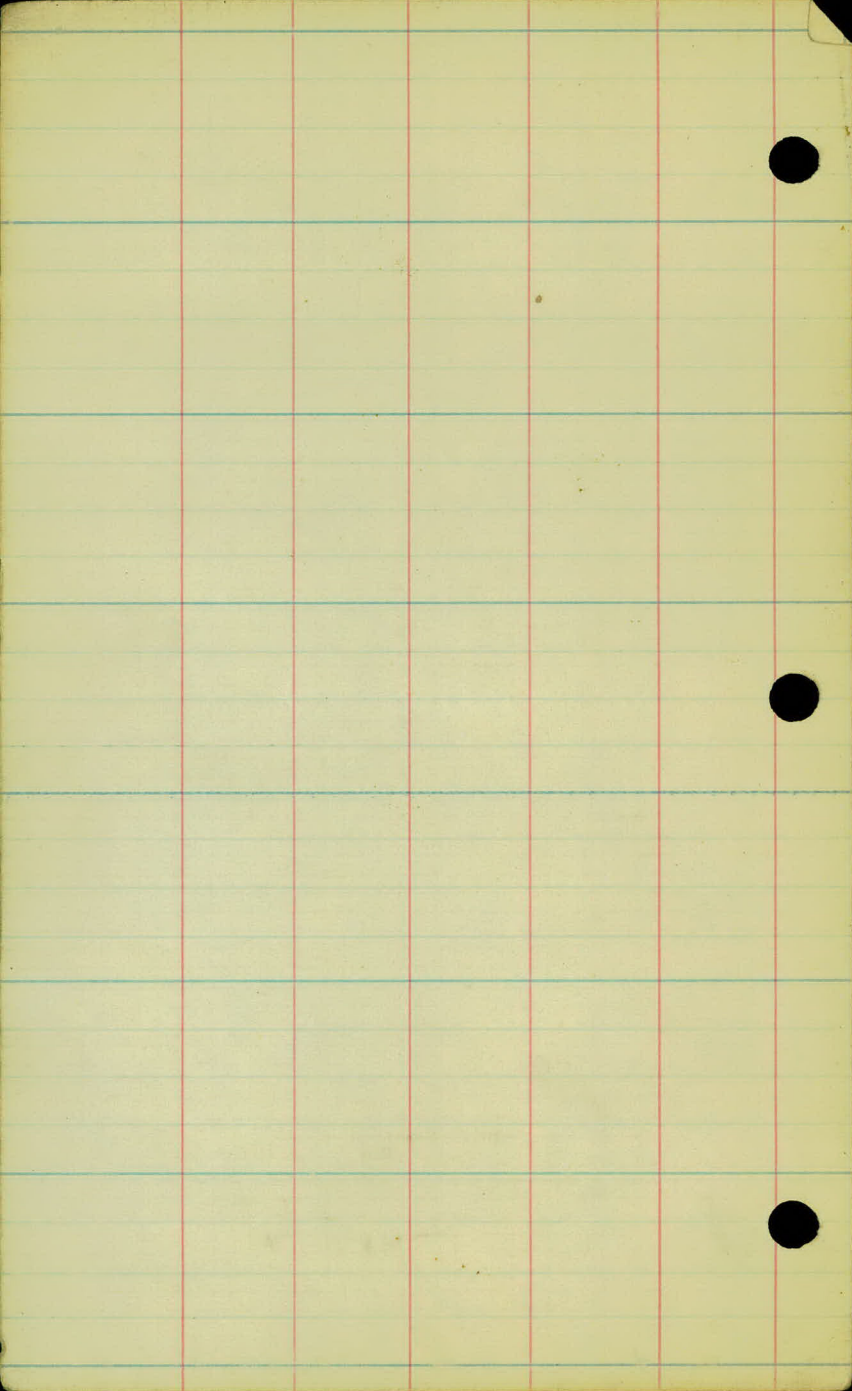
18100

17100

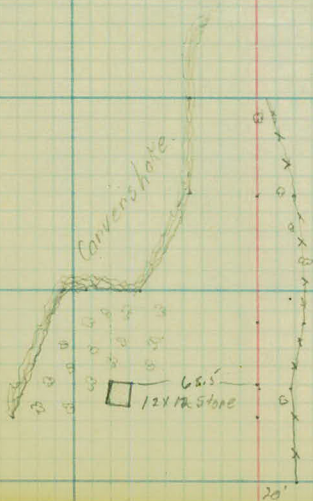
16100

15100

14100



"A" line

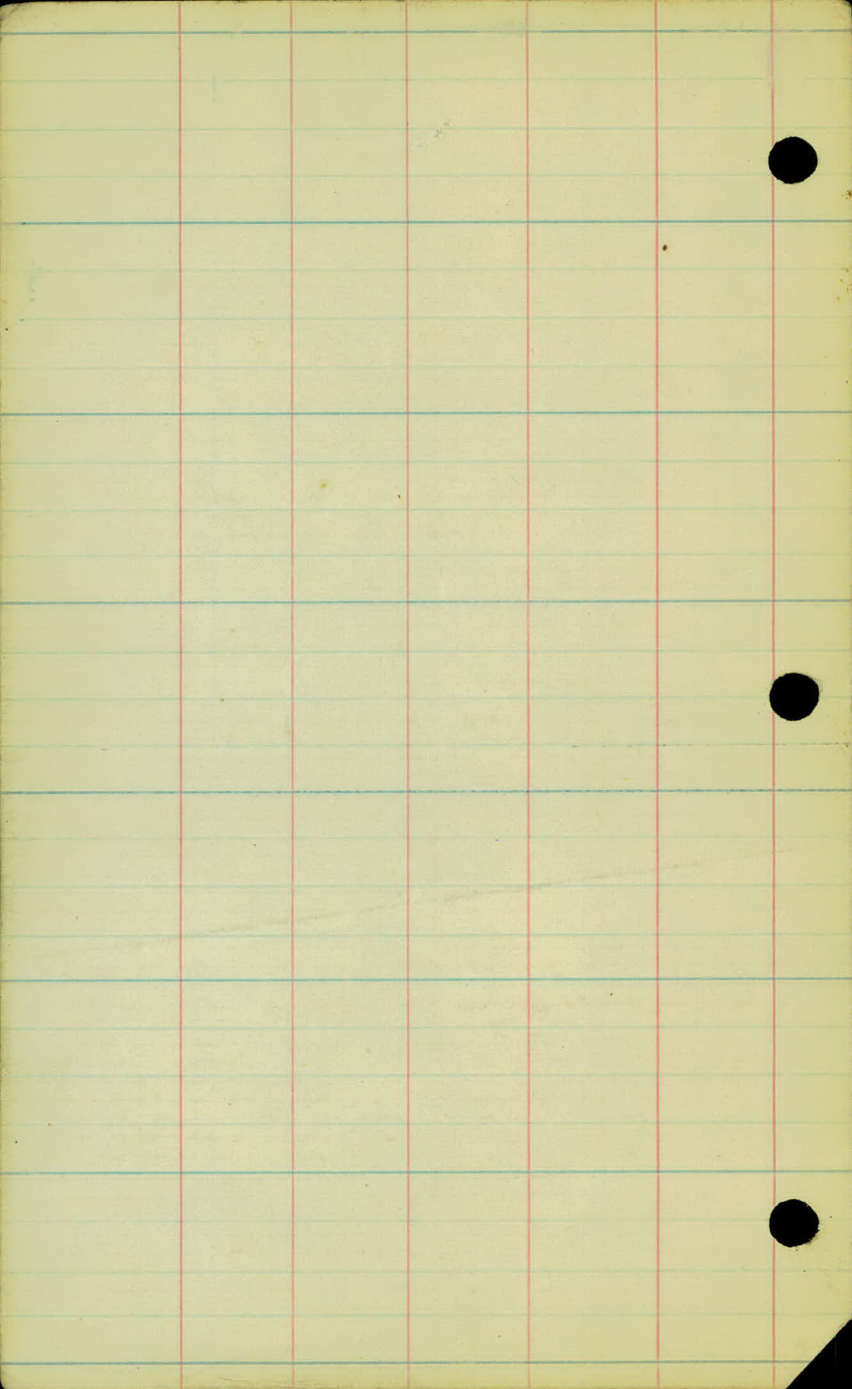


22.500

21.500

20.500

20'



Convens lake. "A" line

Sta 9+53.95 to 22+53.9

Station

Ang. ht. <sup>4</sup> Ang. R. BEAR.

56.23  
3-25  
22

S 23° 20' E

17+56<sup>48</sup> ✓ P.T.

16+81.7 P.I. 46° 40'

15+95.56 P.C. ✓

S 66° 40' W.

15+274 P.O.T.

12+45<sup>62</sup> P.T. ✓

11+01<sup>25</sup> P.I.

23° 20'

9+53<sup>25</sup> P.C. ✓

S 00° 00' W.

1770 60  
 360 40  
 33° 20'

15+95.56 - 0°00'  
 16+00 - 0°39'  
 +50 - 7°54'  
 17+00 - 15°09'  
 +56.46 - 23°20'

29° Curve ht.

$\Delta = 46°40'$

Rad = 199.70

Tang = 86.14 ✓

length = 160.92 ✓

49.77  
 18°  
 41.25  
 12°

Sta. - Def

9+53.95 - 0°00'  
 10+00 - 1°50½' ⊙  
 +50 - 3°50½'  
 11+00 - 5°50½' ⊙  
 +50 - 7°50½'  
 12+00 - 9°50½'  
 +45.63 - 11°40'

8° Curve Rt.

$\Delta = 23°20'$

Rad = 716.78

Tang = 148.00 ✓

length = 291.67 ✓

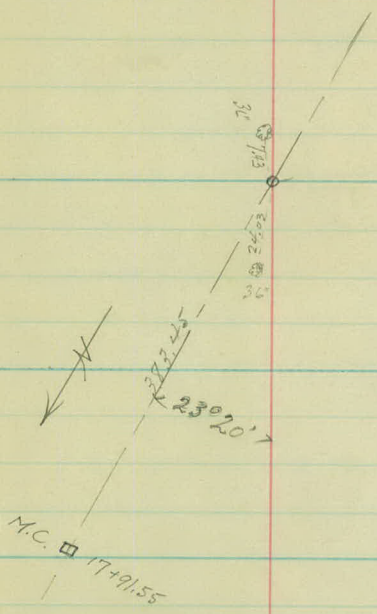
F.P.  
 35.26  
 30.2  
 F.P.

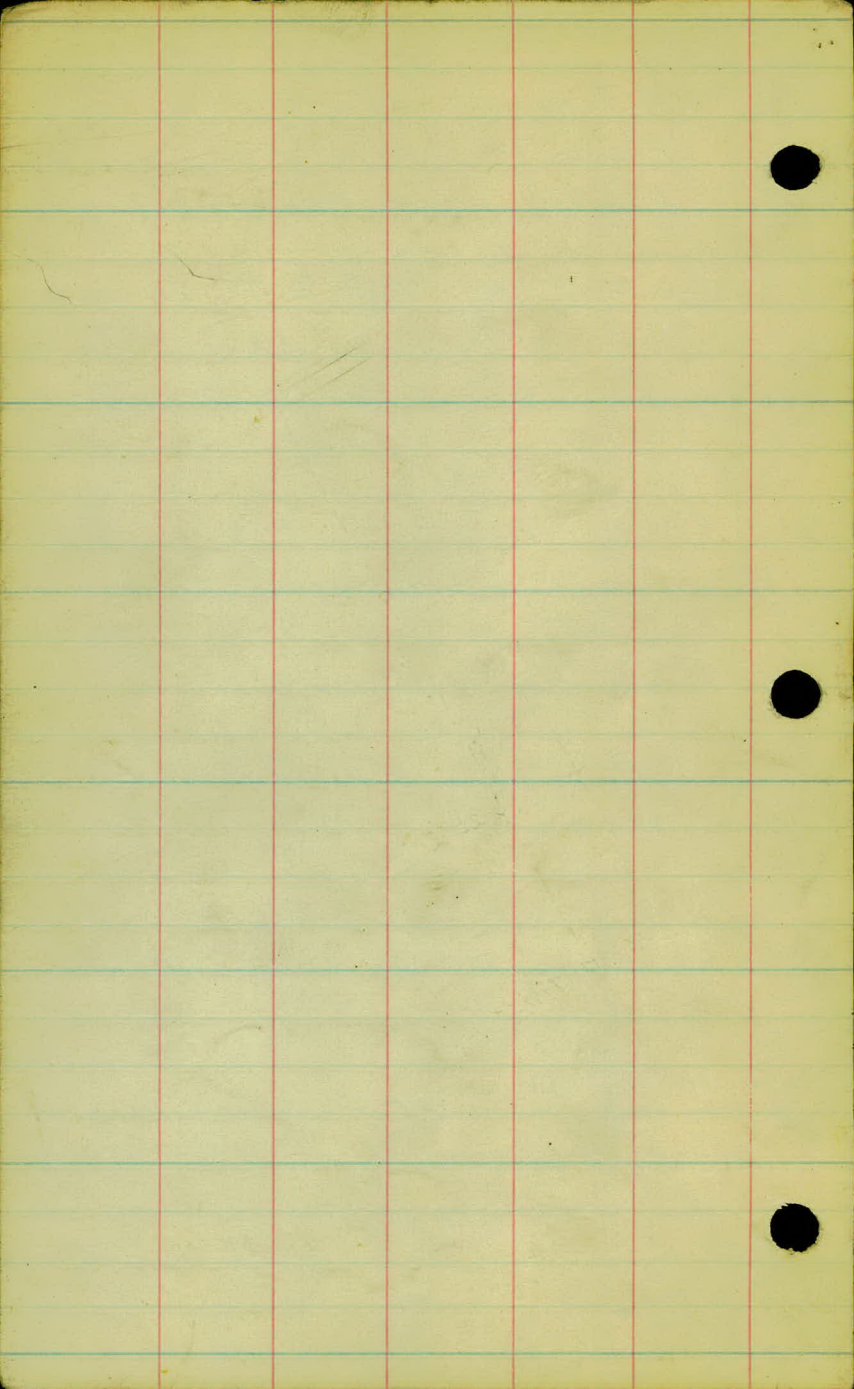
22+52.9 P.O.T = 21+75.0 sec. hind

S 23° 20' E.

22+05.95 P.O.T

21+00 P.O.T.





Proj. # 26-06

Carvers Lake.

Alignment on the "A" line  
from Sta. 21+64<sup>35</sup> to Sta.

Sta. Point Lt. Rt.

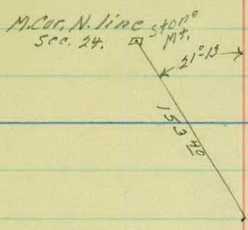
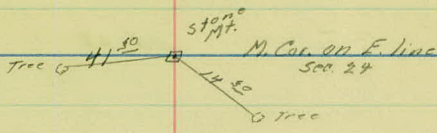
30741<sup>20</sup> P.I. 31°-08'

24714<sup>20</sup> P.I. 58°-10'

21799<sup>62</sup> P.O.T.

21764<sup>35</sup> P.I. 50°-15'

6/1/25



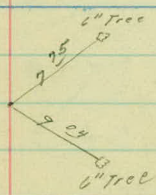
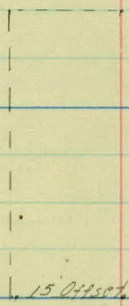
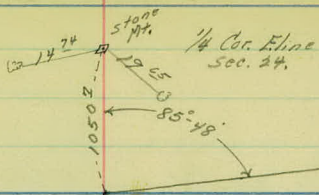
Sta. Point Lt. Ft.

43+68<sup>14</sup> P.I. 85°-48

40+94<sup>62</sup> P.O.T.

36+90<sup>68</sup> P.O.T.

34+40<sup>80</sup> P.O.T.



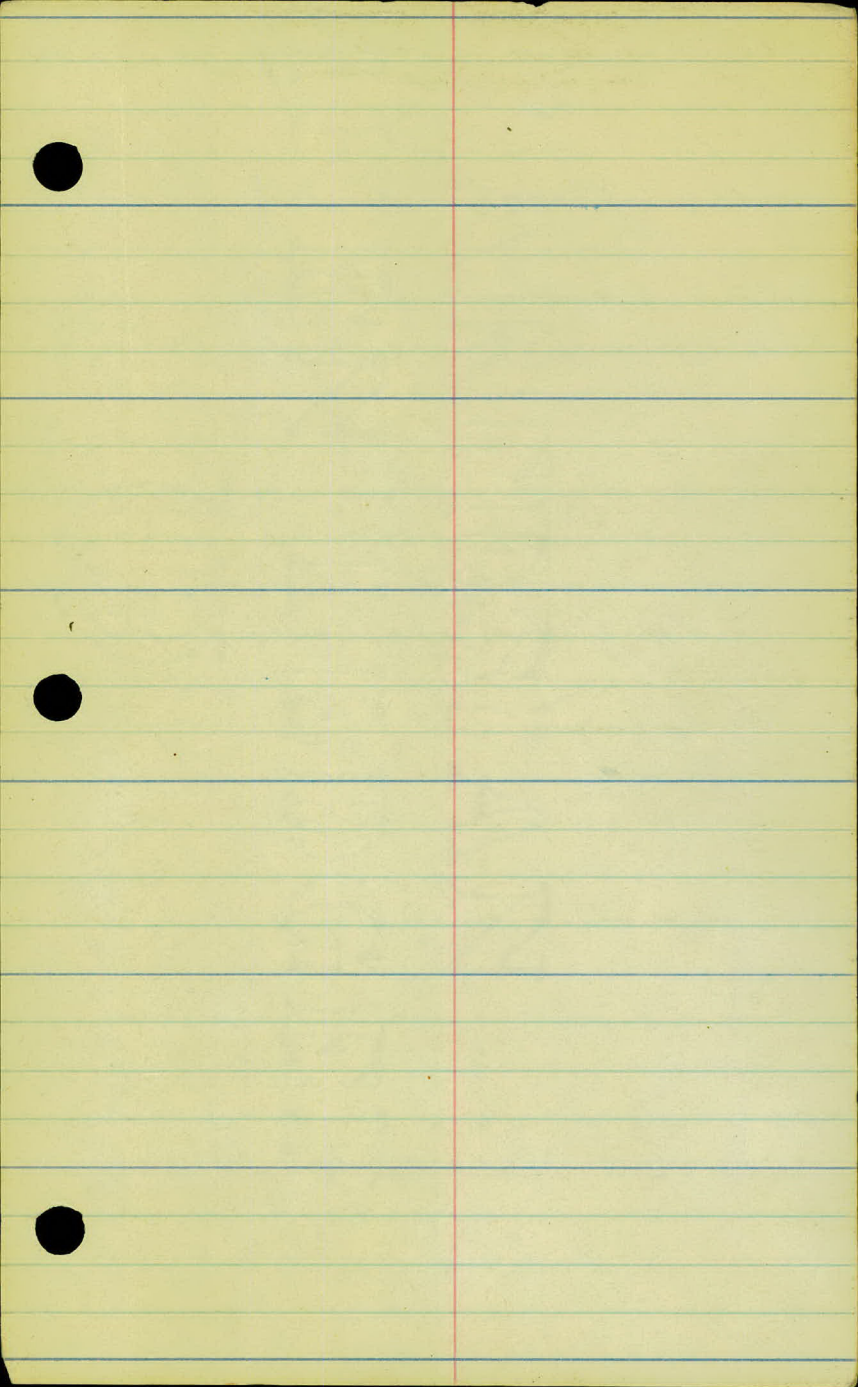
Sta. Point Lt. Rt.

54752 <sup>54</sup> P.I. 3°-00'

53752 <sup>54</sup> P.I. 5°-00'

50796 <sup>84</sup> P.I. 60°-00'

44796 <sup>84</sup> P.I. 16°-00'



Spt in 16" O. NE of Mont-35' 1028.66  
Linnwood and E. Carline

02988