

BRIDGE APPROACH
RICE CREEK BRIDGE

From sta 116+04⁶³

To sta 120+77.²⁶

CO. PROJ. N° 26-04

ROAD ½ N° 12

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 3-12-26

File No. "6")

Proj. # 26-04.

Line Revision from Sta. 116+04⁰⁰
to Sta. 120+77²⁶

Office of Railway Cor. Engineer
ST. PAUL, MINN.

Date Filed 12-11-25

File No. "14"

Sta. Point Lt. Pt.

119+44⁶³ P.T.

N 9°-21' E

118+04⁶³ P.T. 2°-48'

116+44⁶³ P.C.
116+64.63 PC

N-12°-09' E

111+74¹² P.T.

111+08¹⁸ P.T.

32°-52' Alignment
File # 16
For preceding
see No. 9/c # 12

110+37²⁵ P.C.

N 20°-43' W

116 + 64⁶³

117 - 0°-10^E

118 - 0°-40^E

119 - 1°-10^E

+44⁶³ - 1°-24[']

3 35 51
3 23 34

A - 2°-48[']

D - 1°-14[']

T - 140⁰

L - 280⁰⁰

R - 5729⁶⁵

110 + 37²⁵

+50 - 1°-32[']

111 - 7°-32[']

+50 - 13°-32[']

+74¹⁹ - 16°-26[']

Q Rice Creek Rd

0 12 23
T.P.
35 25
88°-57

P.P.
56 20 0

A - 32°-52[']

D - 24° 74

T - 70⁹³

L - 136⁹⁴

R - 240⁴⁹

semi Tang.

Sta. Point. Lt. Rt.

$126 + 46 \overset{80}{\rule{0.5em}{0.4pt}}$ P.I.

N-81°-57' E

Eq. 45
 $120 + 80 \overset{45}{\rule{0.5em}{0.4pt}}$ P.I. = $120 + 77.94$

3.57

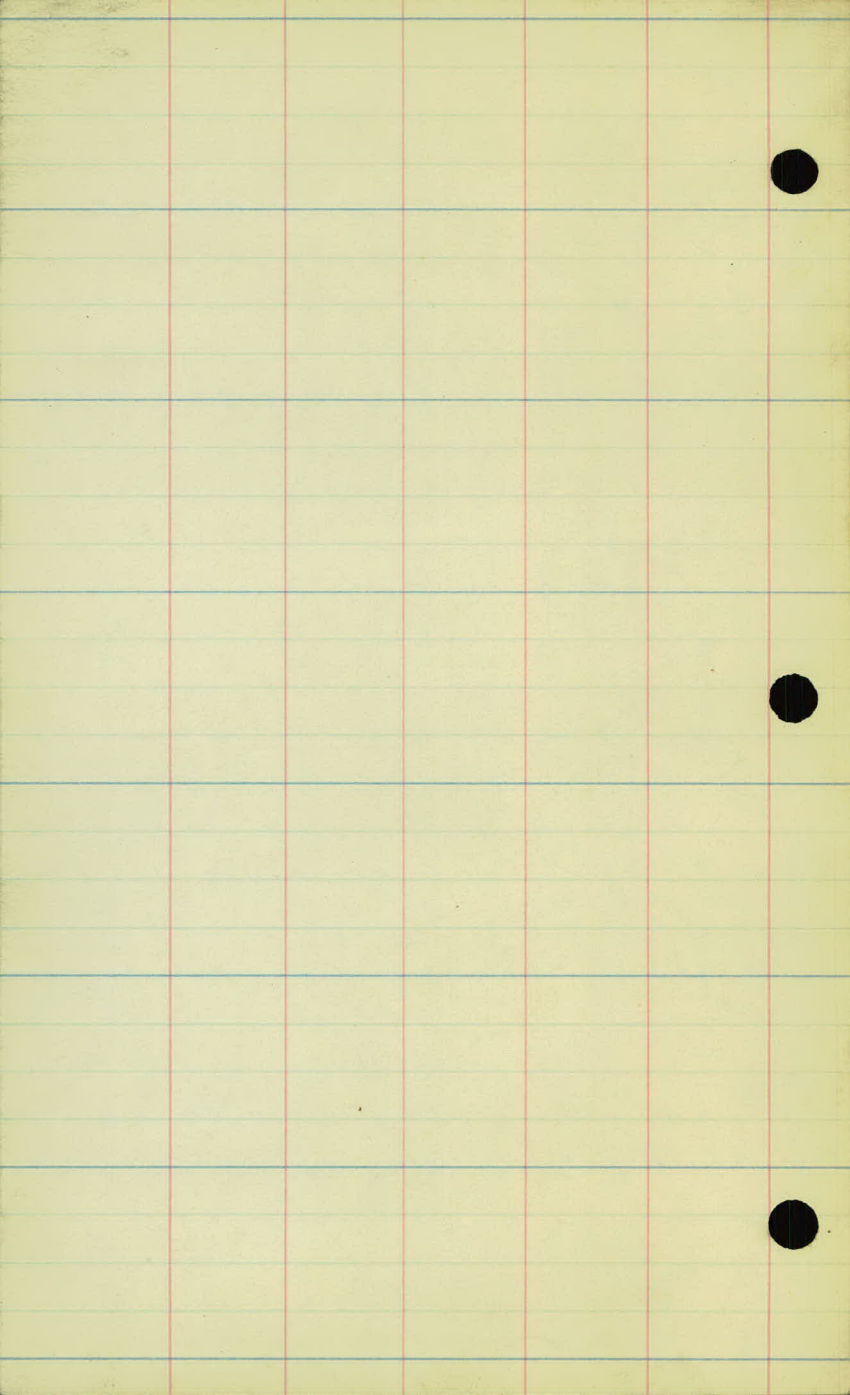
$120 + 48 \overset{35}{\rule{0.5em}{0.4pt}}$ P.I. 79°-36

$120 + 00 \overset{25}{\rule{0.5em}{0.4pt}}$

Guy Pole
0
243

0.37 42
T.P.

A - 79° - 36'
D - 120° - 17'
T - 48 ¹⁰
L - 80 ²⁰
R - 57 ²³



Proj # 26-04

Art. Topog. from
Sta. 104+00 to Sta. 119+00

109

108

107

106

105

104

12/9/25

S.L. 10 h.

+87 - T.P. 21 R

S.L. 10

+63 - T.P. 19 L

+27 Side Drain 28 h

+95 Rice Creek Rd
+65 T.P. 51 h.
+64 Side Drain 21 h
15' x 6' P.M.
800' Cor'd
+36 T.P. 25 h.

S.L. 13 h.

+77 T.P. 26 L

S.L. 11 h.

+59 T.P. 24 h.

S.L. 11 h.

Cultivated Field

Cultivated Field

S.L. 9

+26 P.P. 23 R

S.L. 10

+48 Cross Drain
15' x 27' C.M. Cor'd Pipe
Extends 1742 22 h.

+20 - P.P. 26 R

S.L. 8 R

+66 Guy Pole 13 R

+12 P.M. 17 R
S.L. - 9 R

S.L. 8 R

+74 - P.P. 18 R

S.L. 8 R

115

114

113

112

111

110

109

S.L. - 7' L.
+66 T.P. 24' R.

+31⁵ End of Bridge
S.L. 8' 10" R.

+81 Brick Abut.
10' L. & 10' R.

+84³ Beginning
of Bridge

+26 - T.P. 24' L.
S.L. - 10' L.

S.L. - 13' L.

+97 T.P. 24' L.

+50 S.L. 12' L.

+42 Guy 10' 10" 25' R.

+07 T.P. 24' L.

S.L. 11' L.

+19 - T.P. 17' L.

S.L. 9' L.

3
0
0

S.L. - 11' P.
+61 Beginning of
Row Trees 37' R.
+58 P.P. 18' R.
+43 - 12' T. - 17' R.

+55 End of M. post.
7' 5" L. & 15' R.

+86³ Edge of
bridge 6' L. & 9' R.

S.L. - 8' R.

+93 T.P. 21' R.

S.L. 7' R.

+56 S.L. - 9' R.

+53 P.P. 22' R.

S.L. - 10' R.

S.L. 9'

+81 P.P. 35' R.

Rice Creek

Long Lake

Cultivated field

Cultivated field

Hay field

118

117

116

115

S.L. 9' 1/2

+45 T.P. 24' 1/2

+15 End of Trees 10'

S.L. 10'

+89 Wall Box 12'

+69 Farm Est.

+60 Side Walk 13'

12" x 20" C.M.

+17 T.P. 26'

S.L. 9'

+47 Beginning of
Row of Trees 11 1/2'

S.L. 9'

+76 T.P. 25' 1/2

Cultivated Field

Farm
Yard

Cultivated Field

Cultivated Field

S.L. 9' 1/2

+79 P.P. 15' 1/2

S.L. 10' 1/2

+53 P.P. 14' 1/2

+88 End of T. 21'

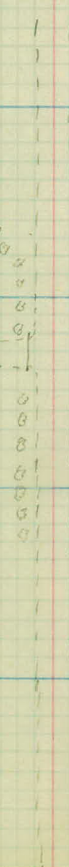
S.L. 9' 1/2

+05 P.P. 17' 1/2

S.L. 11'

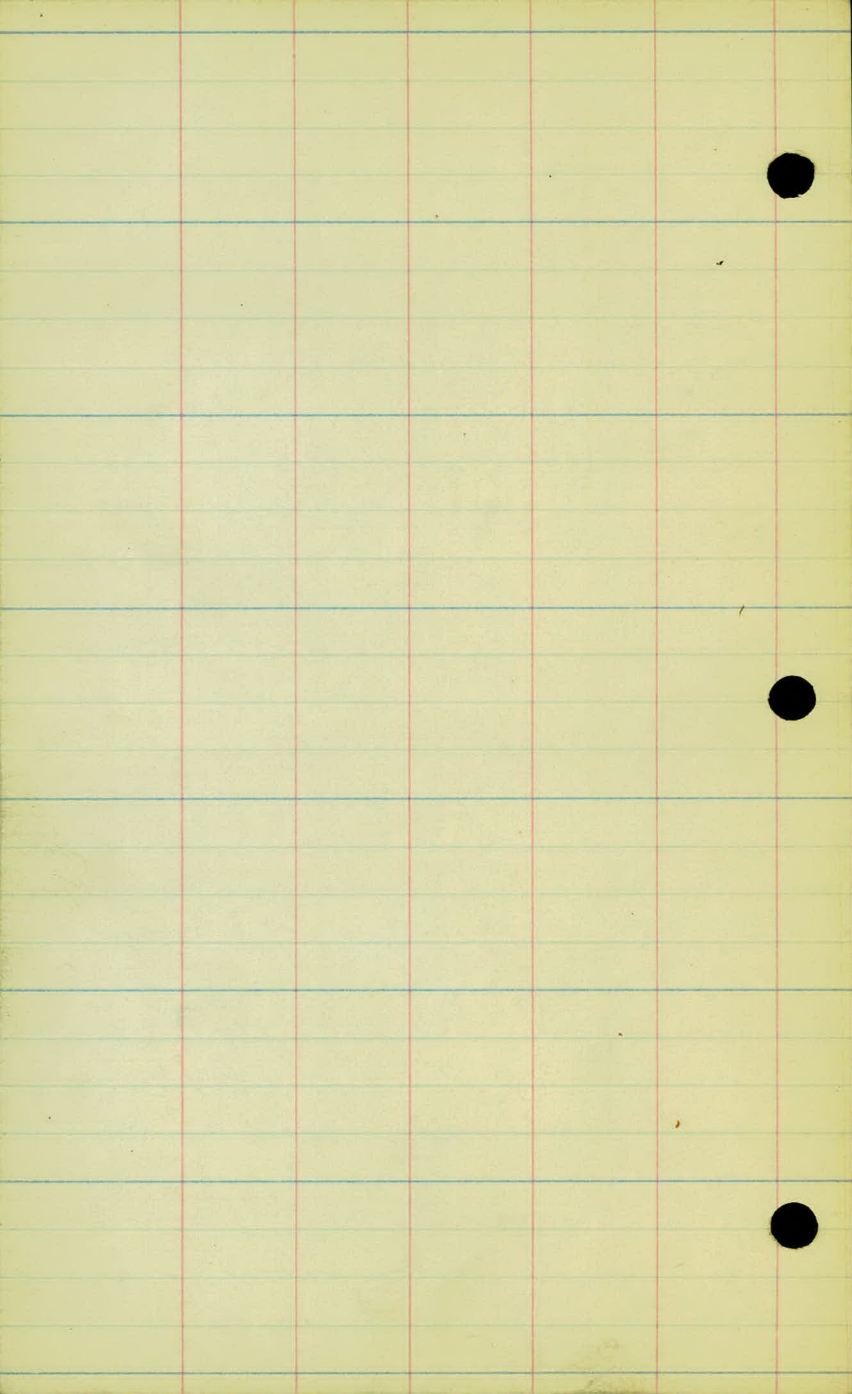
+73 Farm Est.

+67 Side Drain 22'
12" x 20" C.M.
Sand 2007



Farm
Yard

Cultivated
Field



Proj. # 26-04

Levels from New Brighton
to Rice Creek.

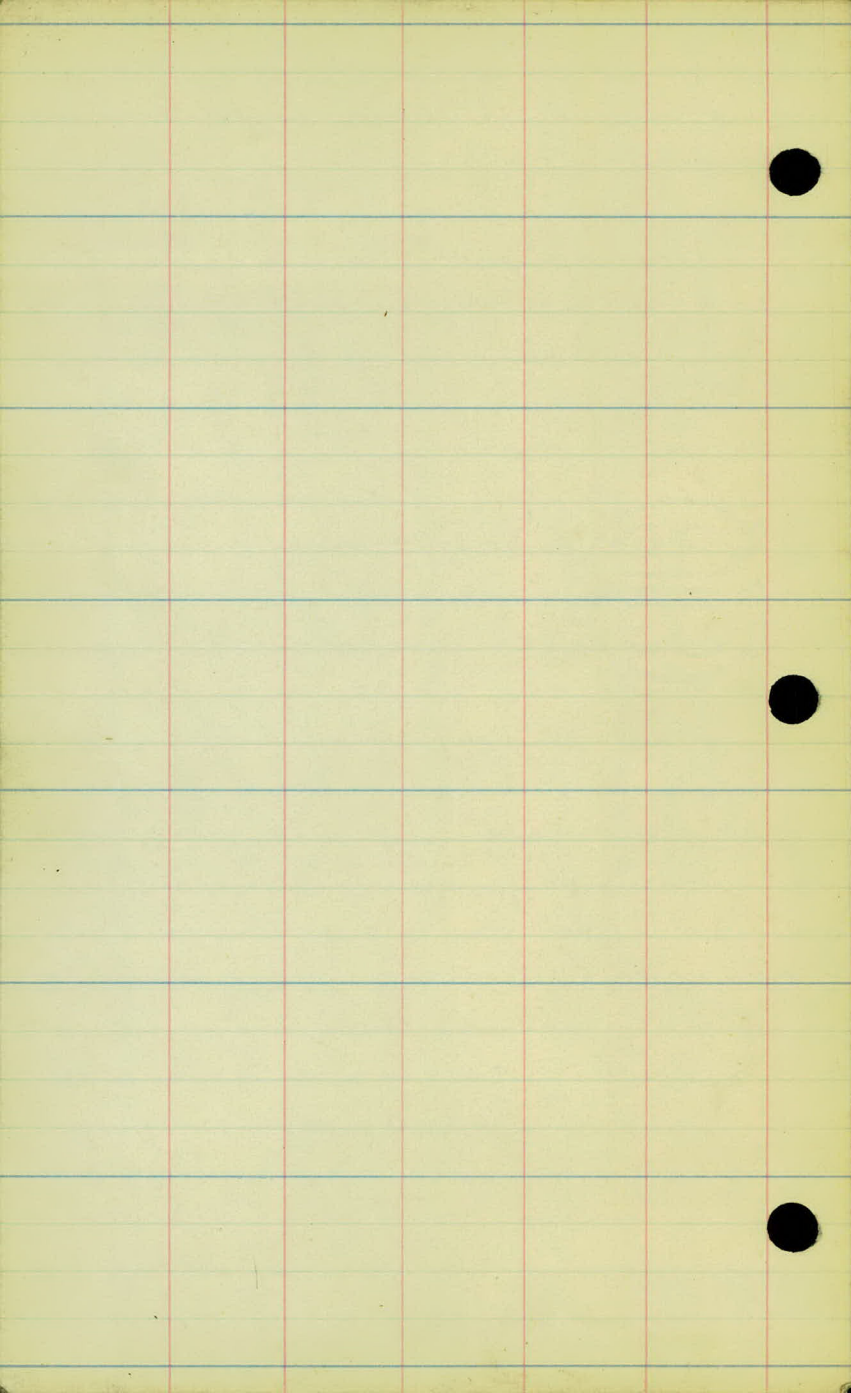
Sta.	T	H.I.	-	Elev.
B.M.	5.15	888.14		882.99
	4.56	891.54	3.14	885.00
	5.52	891.97	5.11	886.45
	1.34	889.35	3.98	887.99
	12.73	896.46	5.62	883.73
	7.91	905.98	0.39	896.07
	0.57	904.05	2.50	903.48
	0.07	894.40	9.72	894.33
	0.97	887.71	7.44	886.74
	3.48	878.87	12.32	875.39
	3.45	876.06	4.24	872.61
B.M.	10.32	881.81	4.57	871.49
	11.55	892.92	0.44	881.37
	6.23	898.45	0.90	892.22
	7.74	898.08	5.11	891.34
	7.48	903.46	2.10	895.98
	4.15	907.44	0.15	903.31
	0.13	896.31	11.28	896.10
B.M.	0.54	890.45	6.40	889.91
	1.74	883.73	8.48	881.97
	2.64	875.59	10.78	872.95
B.M.			6.48	868.91

12/2/20

Spk. in T.P. at N.W. Cor. of int. of 2 main streets
in New Brighton. # 54.

Spk. P.P. Rt. Sta. 109+34.

Spk. 12" C&K. 40 ft. Sta. 119+95.



Proj. # 26-04

Center line levels and
X sections from Sta. 102+00
to Sta. 118+00.

Sta.	+ B.M.	H.I.	-	Rod	Elev.
102	6.84	896.75		3.9	892.9.
103				6.5	90.3.
+24				7.1	89.7.
104				8.8	88.0.
T.P.	2.84	891.24	8.57	888.30.	
+55				4.0	87.2.
105				4.8	86.4.
+60				5.3	85.9.
104				5.9	85.3.
+52				6.5	84.7.
+68				6.4	84.6.
+77				6.8	84.4.
+90				7.1	84.1.
+95	Profile of Rice Creek Rd.			7.2	84.0.

11.

11.

$\frac{2.3}{53}$	$\frac{1.6}{22}$	$\frac{4.1}{17}$	$\frac{4.2}{13}$	$\frac{4.5}{10}$	$\frac{4.4}{14}$	$\frac{2.0}{20}$	$\frac{1.2}{24}$	$\frac{1.9}{33}$
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$\frac{8.5}{53}$	$\frac{4.7}{24}$	$\frac{7.5}{20}$	$\frac{7.1}{17}$	$\frac{6.7}{12}$	$\frac{6.5}{9}$	$\frac{7.0}{14}$	$\frac{5.7}{23}$	$\frac{6.2}{33}$
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$\frac{9.1}{33}$	$\frac{7.7}{15}$	$\frac{7.3}{11}$	$\frac{7.1}{7}$	$\frac{7.4}{9}$	$\frac{7.3}{11}$	$\frac{8.5}{23}$	$\frac{7.9}{26}$	$\frac{8.1}{33}$
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$\frac{14.3}{33}$	$\frac{13.5}{30}$	$\frac{11.0}{23}$	$\frac{10.4}{18}$	$\frac{9.1}{15}$	$\frac{8.9}{11}$	$\frac{8.8}{8}$	$\frac{9.3}{9}$	$\frac{9.7}{11}$	$\frac{10.7}{17}$	$\frac{10.2}{21}$	$\frac{10.5}{25}$	$\frac{12.7}{33}$
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$\frac{7.0}{33}$	$\frac{8.6}{27}$	$\frac{5.2}{15}$	$\frac{4.3}{11}$	$\frac{4.0}{4}$	$\frac{4.3}{7}$	$\frac{5.9}{13}$	$\frac{7.7}{17}$	$\frac{7.4}{25}$	$\frac{7.8}{33}$
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$\frac{5.3}{118}$	$\frac{5.7}{87}$	$\frac{7.3}{50}$	$\frac{7.3}{67}$	$\frac{6.8}{50}$	$\frac{7.0}{33}$	$\frac{6.7}{22}$	$\frac{5.5}{17}$	$\frac{5.4}{13}$	$\frac{4.9}{11}$	$\frac{4.9}{4.8}$	$\frac{5.4}{11}$	$\frac{6.3}{14}$	$\frac{8.0}{24}$	$\frac{8.7}{33}$
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$\frac{6.6}{25}$	$\frac{8.1}{85}$	$\frac{7.2}{100}$	$\frac{6.4}{109}$	$\frac{5.5}{110}$	$\frac{4.3}{135}$	$\frac{3.1}{150}$
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$\frac{6.0}{55}$	$\frac{5.3}{50}$	$\frac{4.7}{40}$	$\frac{4.4}{47}$	$\frac{4.6}{23}$	$\frac{6.0}{19}$	$\frac{6.0}{14}$	$\frac{5.6}{12}$	$\frac{6.1}{5.3}$	$\frac{6.2}{11}$	$\frac{5.4}{15}$	$\frac{5.2}{18}$	$\frac{5.7}{24}$	$\frac{5.7}{33}$
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$\frac{2.7}{180}$
 $\frac{1.3}{200}$

$\frac{4.1}{150}$	$\frac{5.2}{117}$	$\frac{5.9}{100}$	$\frac{4.5}{62}$	$\frac{3.8}{47}$	$\frac{3.7}{31}$	$\frac{3.7}{24}$	$\frac{4.5}{20}$	$\frac{4.2}{14}$	$\frac{4.4}{13}$	$\frac{6.1}{5.9}$	$\frac{6.3}{10}$	$\frac{8.1}{14}$	$\frac{7.3}{19}$	$\frac{5.1}{23}$	$\frac{5.7}{33}$
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$\frac{4.6}{200}$

$\frac{5.1}{150}$	$\frac{5.0}{132}$	$\frac{4.3}{119}$	$\frac{4.3}{100}$	$\frac{3.7}{82}$	$\frac{2.4}{50}$	$\frac{2.5}{41}$	$\frac{3.1}{30}$	$\frac{5.5}{19}$	$\frac{7.0}{14}$	$\frac{7.0}{6.5}$	$\frac{6.0}{9}$	$\frac{7.0}{15}$	$\frac{8.1}{23}$	$\frac{8.1}{33}$
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$\frac{5.4}{200}$

$\frac{5.1}{150}$	$\frac{5.1}{124}$	$\frac{4.1}{100}$	$\frac{3.5}{83}$	$\frac{2.5}{51}$	$\frac{4.6}{43}$	$\frac{7.0}{39}$	$\frac{7.7}{35}$	$\frac{7.1}{29}$	$\frac{6.5}{14}$	$\frac{6.5}{6.6}$	$\frac{7.3}{11}$	$\frac{6.7}{14}$	$\frac{7.6}{22}$	$\frac{8.2}{26}$	$\frac{9.0}{33}$
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$\frac{5.5}{200}$	$\frac{5.7}{150}$	$\frac{5.1}{121}$	$\frac{4.0}{100}$	$\frac{6.7}{65}$	$\frac{7.4}{55}$	$\frac{7.1}{43}$	$\frac{6.5}{21}$	$\frac{6.5}{6.8}$	$\frac{7.4}{8}$	$\frac{6.7}{13}$	$\frac{8.4}{23}$	$\frac{9.3}{33}$
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12

$\frac{5.9}{200}$	$\frac{5.9}{188}$	$\frac{7.1}{150}$	$\frac{7.4}{119}$	$\frac{6.5}{93}$	$\frac{6.7}{50}$	$\frac{6.7}{20}$	$\frac{7.1}{7.1}$	$\frac{7.2}{10}$	$\frac{7.9}{18}$	$\frac{8.8}{33}$
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$\frac{3.7}{250}$	$\frac{5.0}{200}$	$\frac{5.6}{150}$	$\frac{6.3}{100}$	$\frac{6.5}{50}$	$\frac{7.2}{7.2}$
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Sta.	+	H.I.	-	Ref	Elev.
107		891.22		7.3	883.9
+20				7.7	83.5
+30				7.9	83.3
+35				8.0	83.2
+50				8.5	82.7
108				9.0	82.2
+50				9.5	81.7
T.P.	2.49	884.67	9.04	882.18	
109				3.2	81.5
+50				3.7	81.0
110				4.5	80.2
+50				5.3	79.4
111				6.3	78.4
+50				7.7	77.0

6.3 6.4 5.7 6.4 6.6 7.5 7.2 8.4 9.8
200 181 150 100 50 7.3 8 10 17 33

5.0
200

5.7 6.2 6.9 7.7 8.1 8.2 7.7 8.1 7.6 7.9 7.3 8.7 8.9 10.0
150 115 100 74 50 45 30 22 13 7.7 8 10 18 25 33

5.3 5.7 7.1 7.2 1.5 2.6 7.7 8.6 8.1 8.4 8.5 8.0 8.9 9.4 9.9
200 168 137 111 50 33 27 25 19 12 7.9 10 12 12 31 33

6.2 6.7 6.8 2.5 1.8 3.1 8.7 8.4 8.4 8.6 8.1 9.4 9.4 9.9
200 184 150 90 50 24 12 14 10 8.0 11 13 23 31 33

7.1 4.2 2.9 2.4 3.6 8.2 8.9 8.3 8.8 8.8 8.8 10.7
200 150 100 50 25 18 15 13 9 8.5 12 33

4.1 4.0 3.7 4.8 7.3 8.4 8.8 9.6 9.5 7.3 9.2 11.8
200 150 100 50 19 15 11 9 7.0 13 15 20 33

3.6 5.4 6.4 7.8 8.4 9.1 7.9 10.1 9.5 9.6 11.4
200 150 100 50 21 11 9 7.5 11 12 19 33

0.0 2.6 3.1 2.9 3.3 3.7 3.8 3.9 3.0 3.8
150 100 50 37 22 15 11 3.2 7.0 12 33

6.6 6.9 5.7 4.4 4.1 4.5 4.3 3.4 3.6
100 74 50 25 14 12 3.7 7.0 13 33

6.6 5.0 4.5 5.0 5.0 5.1 3.9 4.6
50 31 17 14 11 4.5 7.0 14 33

5.0 4.7 4.9 5.1 6.0 5.8 4.9 5.6
33 31 15 10 9 5.3 7.2 18 33

6.2 5.7 6.6 7.0 6.1 6.7
33 13 11 6.3 7.0 14 33

4.3 9.6 7.6 6.8 7.8 6.2 7.7 7.3 7.8
33 24 18 15 12 7.7 8 10 14 33

Sta.	T	H.I.	-	Prof	Elev
		884.67			
112				9.3	875.4
+50				11.0	73.7
T.P.	2.41	875.34	11.74	872.93	
113				2.9	72.4
+30				3.4	71.7
+54				4.2	71.1
+80				4.9	70.4
+52				5.0	70.3
				10.1	65.2
114				4.7	70.6
				11.0	69.3
				11.4	63.7
				4.5	70.8
				11.0	64.3
				11.4	63.7
				4.6	70.7
				10.2	65.1
+31					
+93 ⁵				4.5	70.8
+42				3.8	71.5
					71.8
115				3.0	72.3

11.

17.

<u>40</u>	<u>45</u>	<u>104</u>	<u>89</u>	<u>94</u>		<u>97</u>	<u>91</u>	<u>105</u>
33	36	50	15	19	7.3	10	18	33

<u>81</u>	<u>82</u>	<u>95</u>	<u>120</u>	<u>114</u>	<u>114</u>	<u>115</u>	<u>111</u>	<u>109</u>	<u>124</u>	
33	39	32	18	14	12	11.0	8	10	14	33

<u>09</u>	<u>21</u>	<u>38</u>	<u>41</u>	<u>34</u>		<u>33</u>	<u>37</u>	<u>47</u>	<u>56</u>	<u>30</u>	<u>41</u>
33	22	17	13	10	2.9	8	11	13	18	23	33

<u>21</u>	<u>22</u>	<u>48</u>	<u>55</u>	<u>57</u>	<u>43</u>	<u>42</u>	<u>66</u>	<u>76</u>	<u>78</u>	<u>61</u>	<u>66</u>	<u>66</u>	<u>78</u>	
33	30	24	20	17	12	3.6	9	15	18	24	26	38	55	70

<u>32</u>	<u>37</u>	<u>51</u>	<u>73</u>	<u>74</u>	<u>45</u>	<u>45</u>	<u>57</u>	<u>97</u>	<u>90</u>	<u>97</u>	<u>103</u>	
40	34	24	19	17	9	4.2	10	15	24	32	36	50

top of ice

<u>59</u>	<u>74</u>	<u>77</u>	<u>102</u>	<u>92</u>	<u>78</u>	<u>72</u>	<u>46</u>	<u>50</u>	<u>95</u>	<u>104</u>	<u>108</u>	
48	33	25	22	15	12	10	4	7.9	10	16	22	31

<u>75</u>	<u>104</u>	<u>99</u>	<u>81</u>	<u>96</u>	<u>46</u>	<u>50</u>	<u>41</u>	<u>101</u>	<u>100</u>	<u>108</u>
50	26	17	11	6	6	10.1	10	10	18	28

Ground water table in large water table, ground table

<u>116</u>	<u>110</u>	<u>48</u>	<u>47</u>	<u>45</u>	<u>110</u>	<u>115</u>	
6	6	6	11.0	11.6	10	10	10

<u>116</u>	<u>110</u>	<u>46</u>	<u>45</u>	<u>40</u>	<u>110</u>	<u>115</u>	
6	6	6	11.0	11.6	10	10	10

Top of ice

<u>109</u>	<u>102</u>	<u>102</u>	<u>47</u>	<u>46</u>	<u>43</u>	<u>102</u>	<u>98</u>	<u>102</u>	<u>98</u>	<u>105</u>
19	14	4	6	102	10	10	17	27	38	50

Top of ice

<u>109</u>	<u>98</u>	<u>81</u>	<u>46</u>	<u>64</u>	<u>86</u>	<u>95</u>	<u>102</u>	<u>98</u>	<u>105</u>	
20	14	10	6	4.5	10	16	18	27	38	50

<u>85</u>	<u>80</u>	<u>62</u>	<u>41</u>	<u>40</u>	<u>52</u>	<u>76</u>	<u>91</u>	<u>91</u>	<u>63</u>	<u>61</u>	
50	18	10	5	3.8	10.5	15	21	26	31	36	50

<u>74</u>	<u>67</u>	<u>56</u>	<u>47</u>	<u>33</u>	<u>32</u>	<u>43</u>	<u>71</u>	<u>71</u>	<u>48</u>	<u>33</u>	
50	33	17	10	4	3.0	11	15	22	27	32	50

Sta.	+	H.I.	-	Rod	Elev.
		875.94			
B.M.	8.07	876.98	6.40	848.94	868.91
+35				3.4	873.6
+75	Farm Ent. Pt.			1.7	75.3
114				0.5	74.5
	11.51	888.27	0.22	876.74	
+50				7.4	78.9
117				6.8	81.5
+50				4.5	83.8
118				2.9	86.3
T.P.	0.51	877.48	11.30	876.97	
B.M.			8.57	868.91	868.91

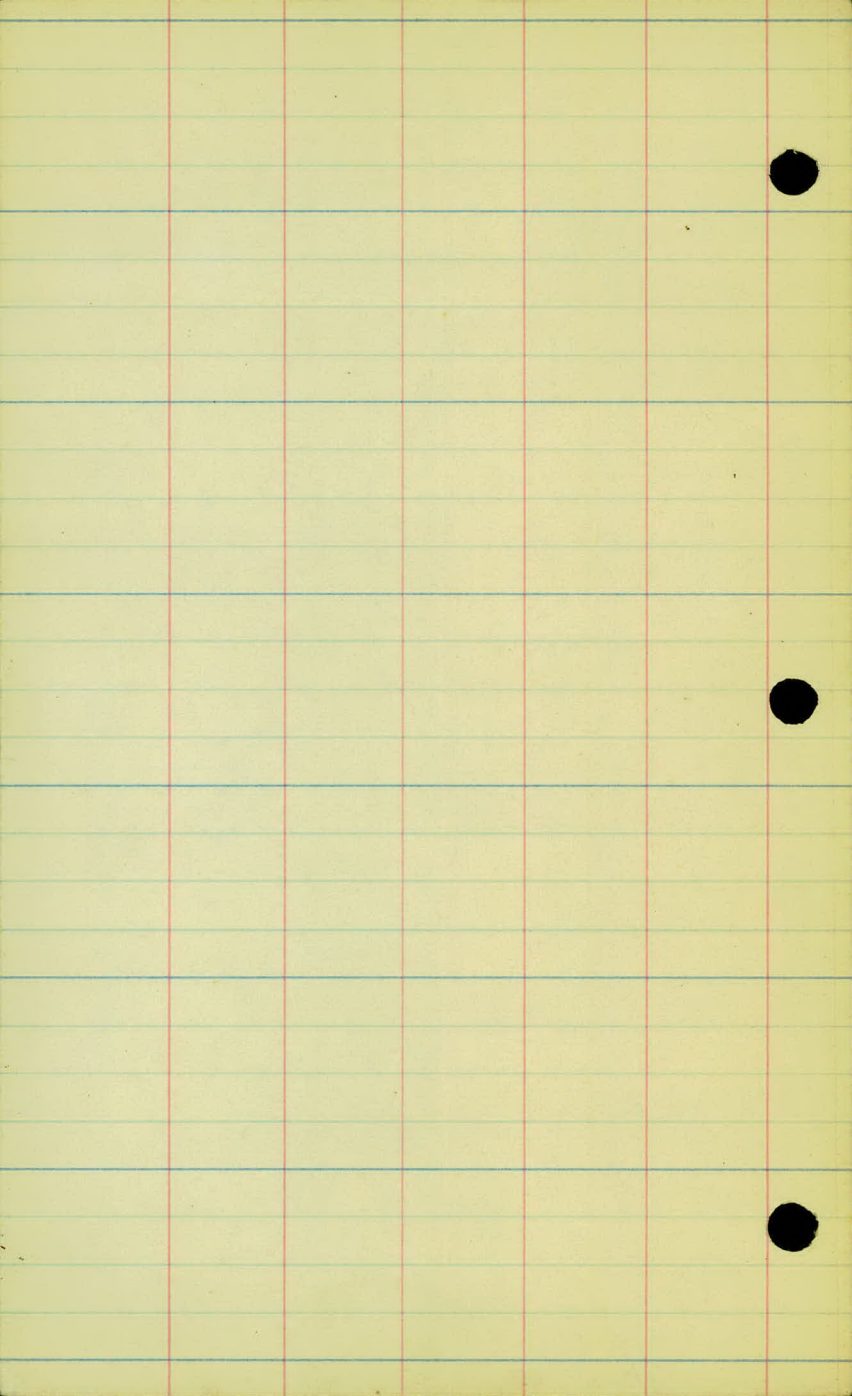
$\frac{74}{33}$	$\frac{5.6}{14}$	$\frac{4.8}{10}$	$\frac{3.9}{8}$	5.4	$\frac{3.7}{13}$	$\frac{5.8}{19}$	$\frac{6.1}{33}$	$\frac{4.9}{15}$	$\frac{3.9}{35}$
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1.7 $\frac{1.7}{25}$ $\frac{0.9}{50}$

$\frac{3.1}{33}$	$\frac{2.3}{20}$	$\frac{1.8}{10}$	0.5	$\frac{0.8}{14}$	$\frac{1.3}{30}$	$\frac{0.0}{38}$
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$\frac{90}{33}$	$\frac{7.7}{14}$	$\frac{8.3}{12}$	$\frac{7.5}{10}$	6.8	$\frac{7.1}{9}$	$\frac{6.4}{15}$	$\frac{6.4}{33}$
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$\frac{3.5}{33}$	$\frac{3.3}{13}$	$\frac{2.5}{10}$	2.0	$\frac{2.3}{12}$	$\frac{2.0}{19}$	$\frac{1.5}{33}$
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Proj. # 26-04

Profile of the ground
20' Rt. of Q from Sta. 111+00
to Sta. 117+00.

S + a.	f	H. I.	-	Roof	20' Right. Elev.
B.M.	11.20	880.11		848.91	
111				1.5	878.6
	+50			3.1	77.0
112				4.7	75.4
	+50			4.7	73.4
	+86			7.0	73.1
113				9.0	71.1
T.P.	2.41	875.31	7.21	872.90	
	+03			4.7	70.6
	+09			6.7	68.6
	+18			6.9	68.4
	+42			8.3	67.0
	+55			7.5	67.8
	+82			9.9	65.6
	+90			11.0	64.3
114				11.0	64.3
114				11.6	63.7
	+11			11.0	64.3
	+27			10.2	65.1
	+35			9.3	64.0
	+45			7.9	67.4
	+65			7.0	68.3
115				6.6	68.7
T.P.	9.49	882.40	2.40	872.91	
	+32			11.6	70.8
	+47			10.5	71.9

12/9/25

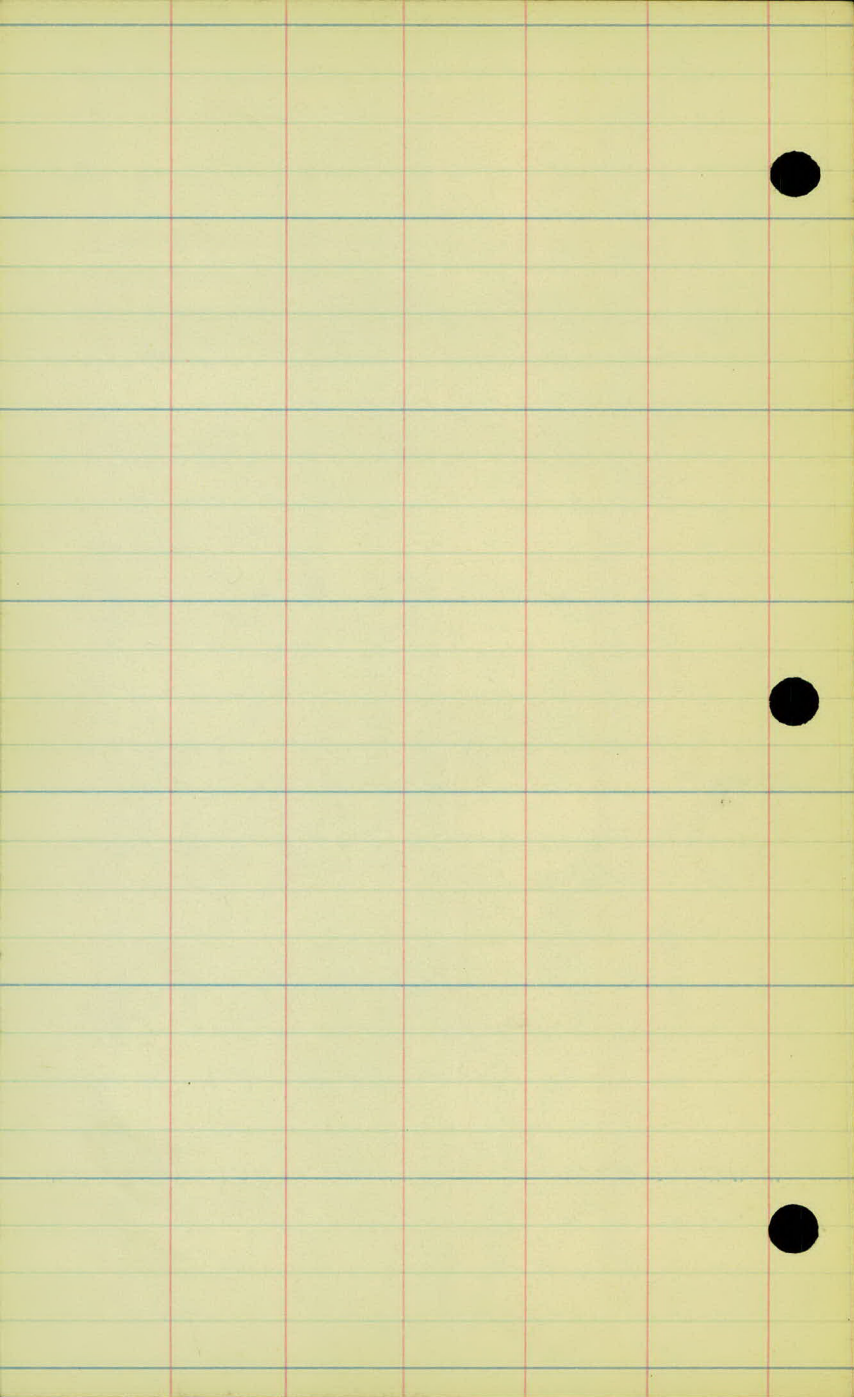
SpK in 12" Oak. 40' H. Sta. 113775.

Edge of Creek
top of Water
Bottom of Creek
Edge of Creek.

Sta.	+	H. I.	-	Rod	^{20' Right.} Elev.
		882.40			
	+49			95	872.9
	+67			83	74.1
	+71			74	75.0
	+89			4.8	75.6
	+90			7.8	74.6
	114			4.7	75.7
	+50			3.4	79.0
	117			1.4	82.0
T.P.	2.40	875.51	9.49	872.91	
B.M.			4.60	868.91	

12/9/25

SpK in 12" Oak 40' Lt. Stg. 113+75.



Proj # 26-04

Profile of the Ground
20' Left of \mathcal{Q} from Sta. 111+00
to Sta. 117+00.

Sta.	T	H.I.	-	R	20' Left. Elev.
B.M.	11.20	880.11		848.91	
111				1.5	878.6
+08				2.7	77.4
+30				2.6	77.5
+55				3.5	76.6
+85				4.7	75.4
112				6.0	74.1
+30				6.3	76.8
+48				5.2	74.9
+64				6.3	73.8
+86				7.1	73.0
113				7.7	72.4
T.P.	2.41	875.31	7.21	872.90	
+20				4.9	70.4
+70				8.4	66.9
+84				10.2	65.1
+91				11.0	64.3
114				11.0	64.3
114				11.6	63.7
+35				11.0	64.3
+53				8.9	66.4
+72				6.5	68.8
115				5.5	69.8
T.P.	7.49	882.40	2.40	872.91	
+50				10.7	71.7

12/9/25

LT.

Spk. in 12" Oak. 40 ft. Sta. 113+75.

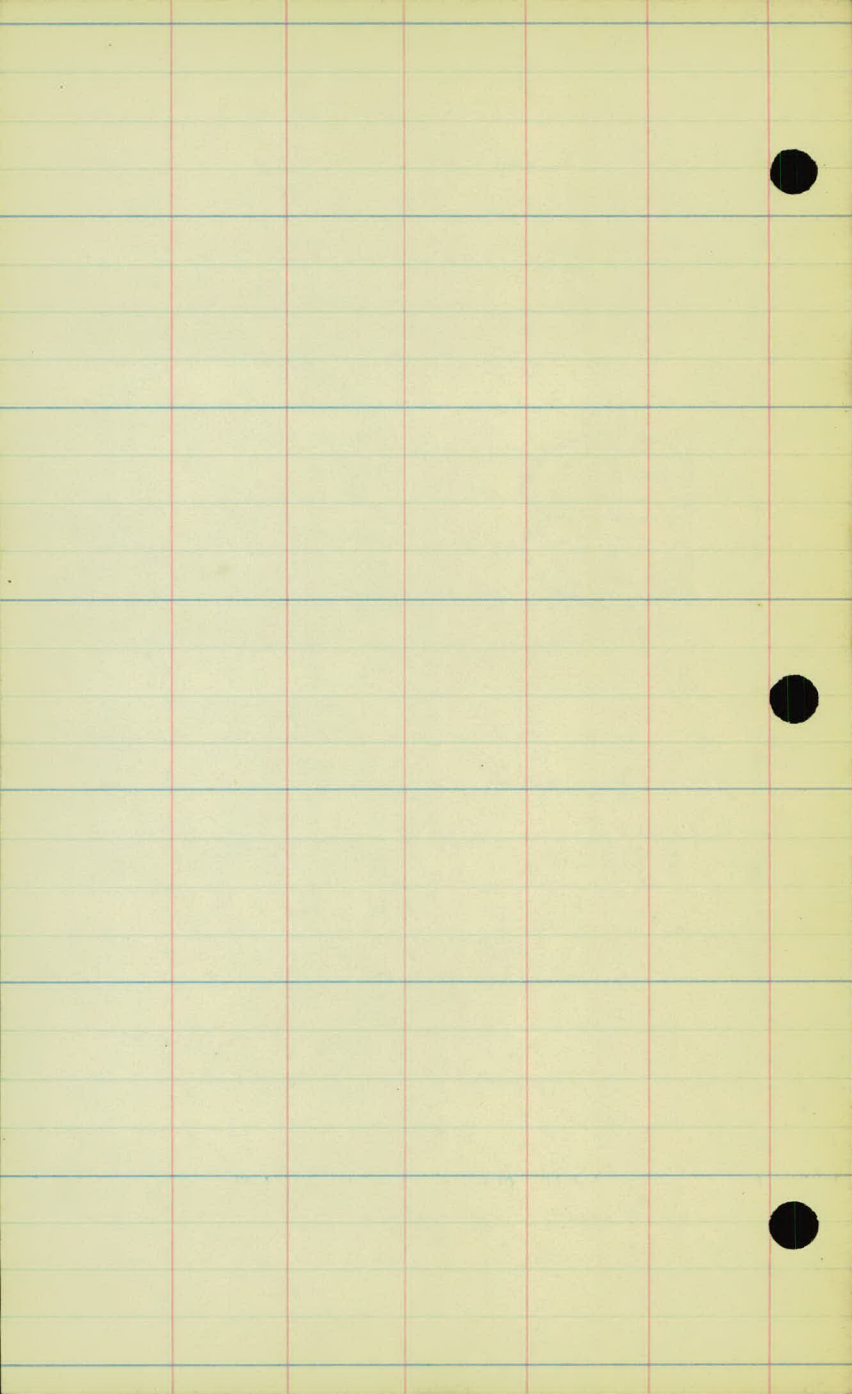
Edge of Creek.
Top of Water.
Bottom of Creek
Edge of Creek.

Sta.	+	H. I.	-	Red	20' Left. Elev
		882.40			
116				7.4	874.8
	+50			5.2	77.2
117				2.2	80.2
T. P.	2.40	875.51	9.49	872.91	
B. M.			6.40	868.91	

12/9/25

lett

Sp. K. in 12" Oak 40' lt. Sta. 113+75.



Proj. # 26-04

Soundings & Creek Elev.

Sta.	f	H.I.	-	Red	Elev.
B.M.	6.44	875.35		868.91	

Sounding # 1				10.8	864.6	=
18' Rt. Sta. 113+87				13.7	61.7	
				22.4	53.0	

Sounding # 2				11.0	864.4	=
12' Rt. Sta. 114+04				11.3	64.1	=
				12.5	62.9	=
				18.8	56.4	

Sounding # 3				10.5	864.9	
14' Rt. Sta. 114+24				13.1	62.3	
				19.1	56.3	

114+07 Readings in Bottom of Creek Lt. & Rt.

	8.7	866.7
	11.0	864.4
	11.5	843.9

Elev. of Ground.

Weight of one man

Driven With 5 lb mallet

0.05 = Penetration With 5 lb mallet.

Elev. of Water

" " Ground.

Weight of one man

Driven With 5 lb mallet

0.04 = Penetration With 5 lb mallet.

= Elev of Ground

Weight of one man

Driven With 5 lb mallet

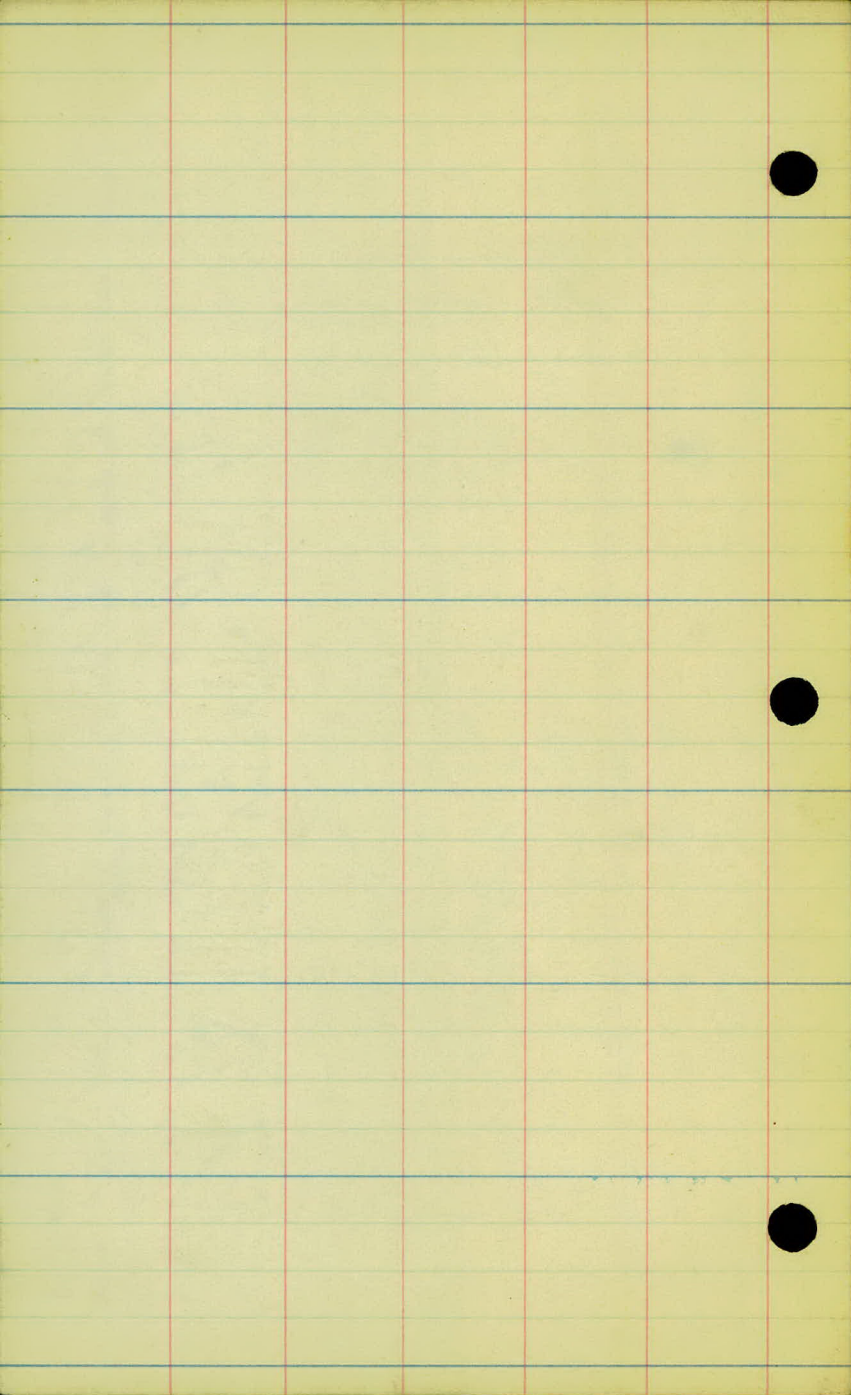
0.05 = Penetration With 5 lb mallet.

$\frac{13.2}{250}$	$\frac{12.2}{300}$	$\frac{11.6}{150}$	$\frac{11.4}{100}$	$\frac{11.6}{50}$	$\frac{12.6}{50}$	$\frac{13.2}{100}$	$\frac{13.7}{150}$	$\frac{13.7}{300}$	$\frac{13.8}{250}$
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High Water Mark.

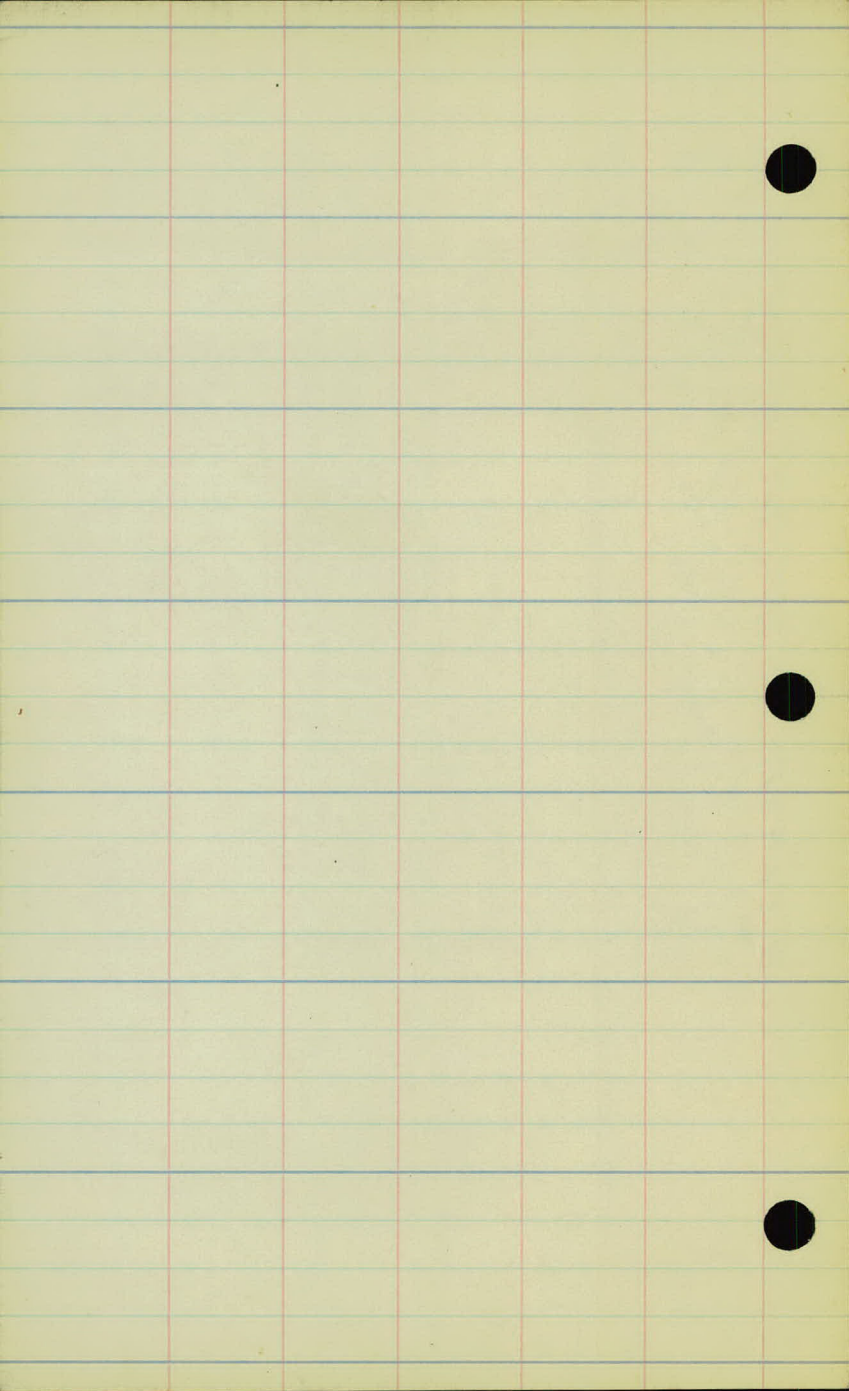
Present Water Elev.

Wing Wall footing.



Proj. # 26-04

Rice Creek Location.

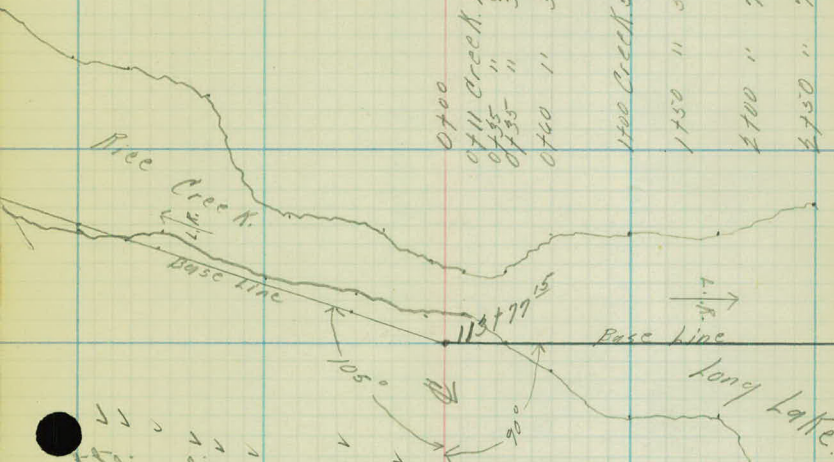


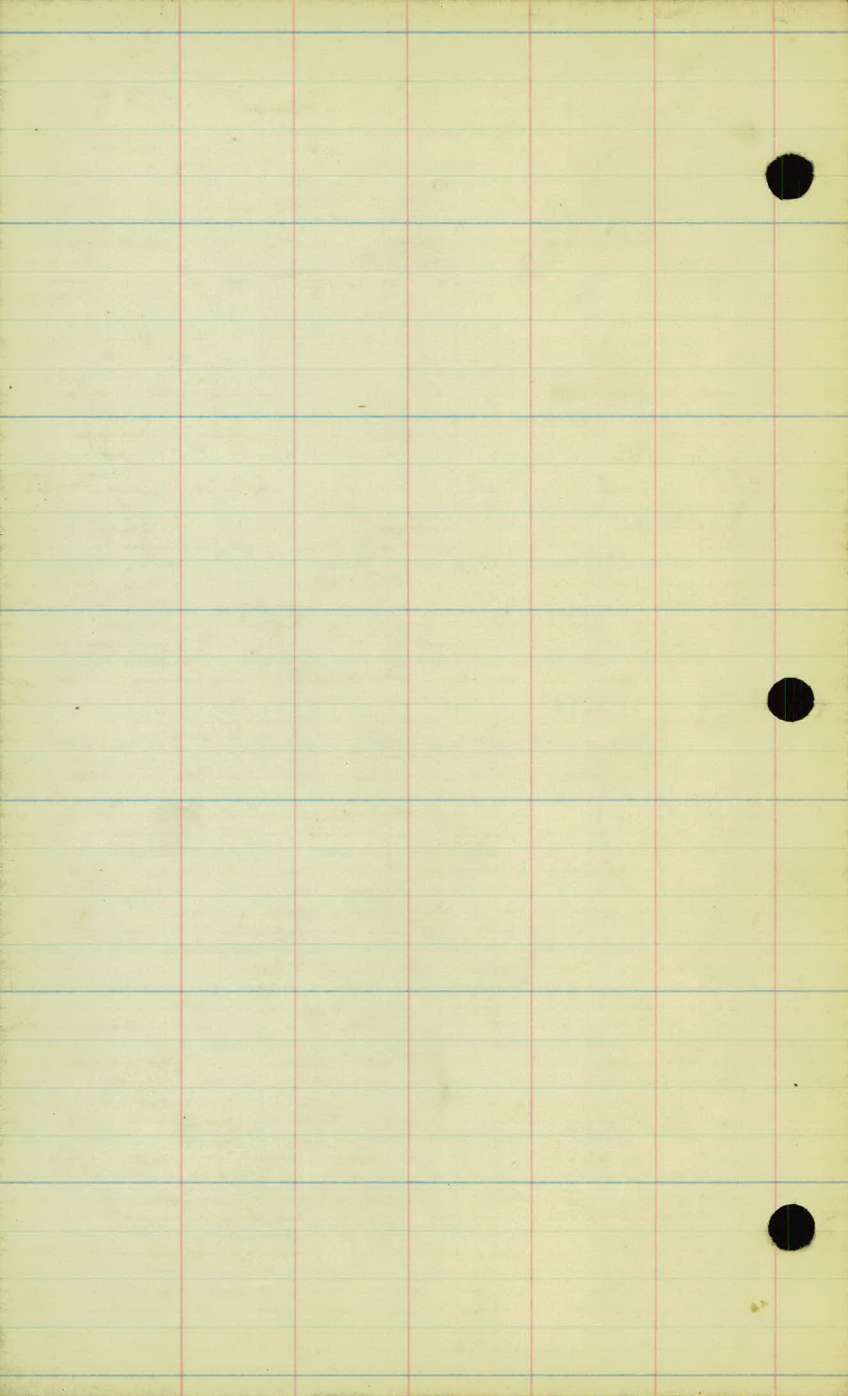
1750 Creek 5' L. 880' R. ✓
 1725 " 3' L. 870' R. ✓
 1700 " 2' L. 860' R. ✓
 1775 " " ✓
 1760 " C.R. 83' R. ✓
 1752 " C.R. 72' R. ✓
 1700 " 2' R. 38' R. ✓

0750 " 5' R. 848' R. ✓
 0710 " 11' R. 841' R. ✓
 0700 "

0760 Creek 15' R.
 1700 Creek 40' R.
 1750 " 75' R.
 2100 " 100' R.
 2750 " 95' R.

0700
 0711 Creek 11' L. 837' L.
 0755 " " 37' L.
 0735 " " 37' L.
 0740 " 1' 54' L.
 1700 Creek 54' L.
 1750 " 56' L.
 2100 " 72' L.
 2750 " 77' L.



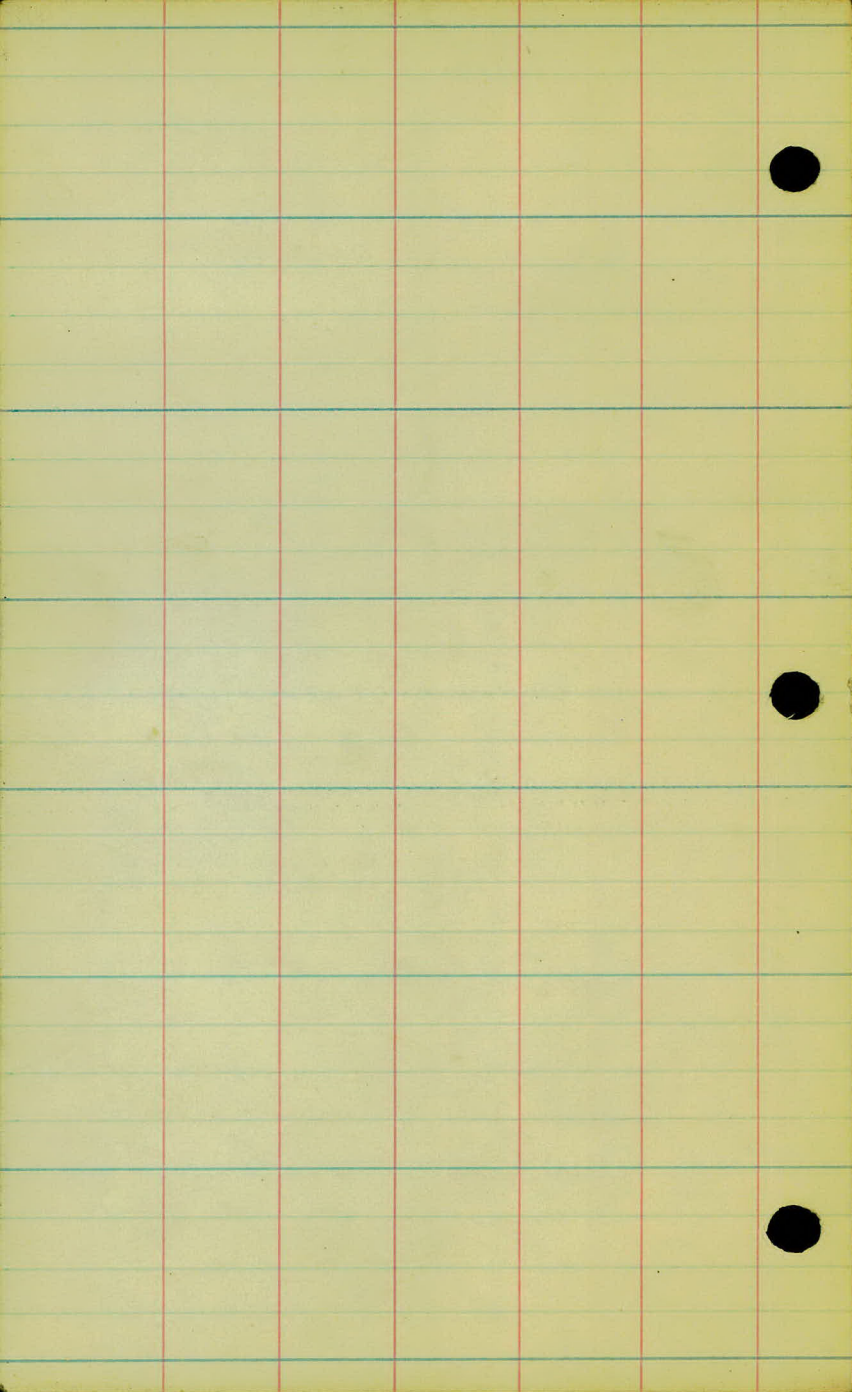


Proj # 26-04.

Check Levels from Rice Creek.
to New Brighton.

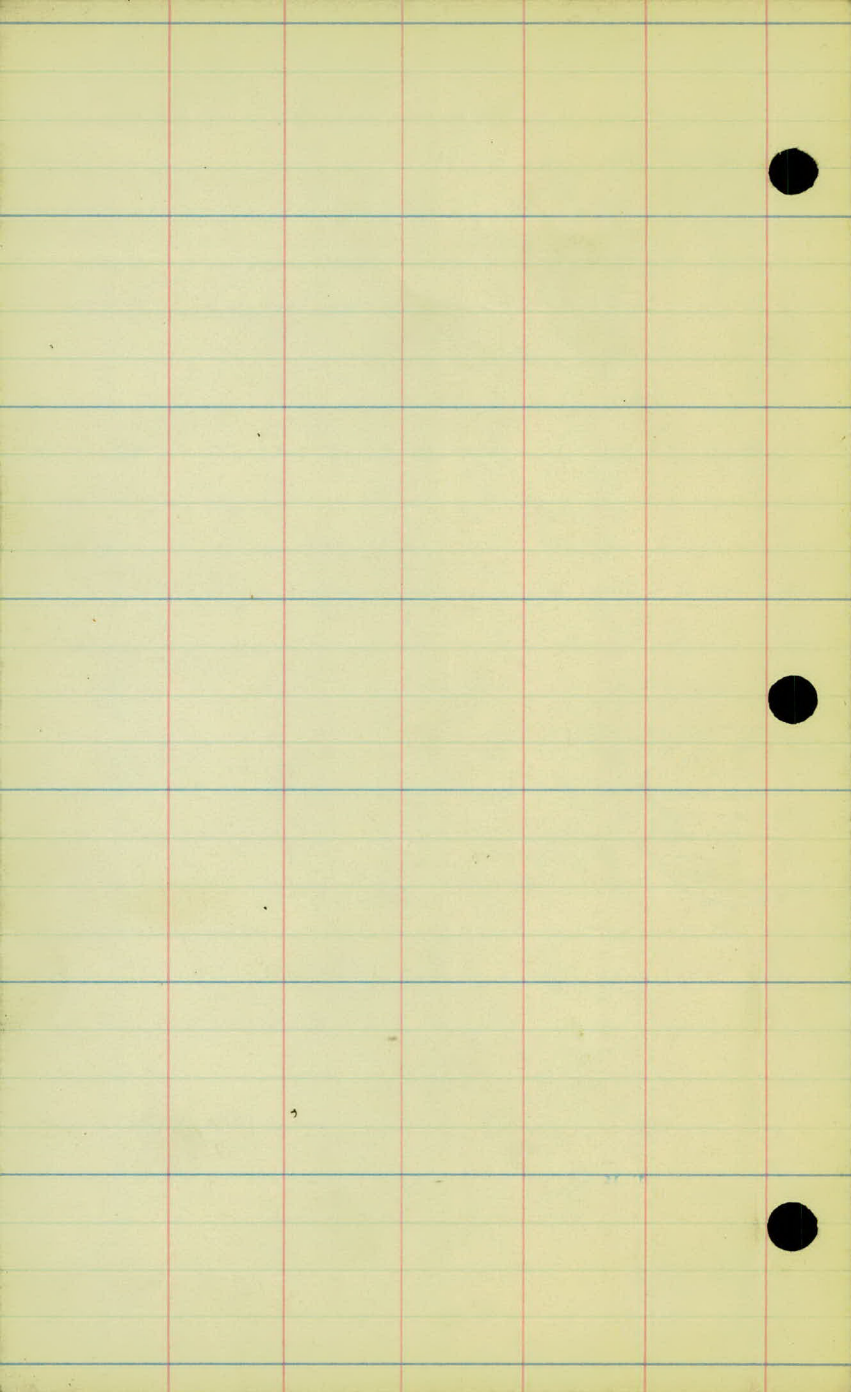
Sta.	+	H.I.	-	Elev.
B.M.	6.48	875.59		868.91
	9.33	885.90	1.02	874.57
	7.87	890.30	1.47	882.43
B.M.	7.84	897.75	0.39	889.91
	10.20	907.82	0.13	897.62
	0.67	903.80	4.49	903.13
	4.54	898.02	10.34	893.44
	4.33	898.04	4.29	893.73
	1.09	893.23	5.92	892.14
	1.36	881.52	13.07	880.16
B.M.	4.83	876.34	7.99	871.53 871.49
	5.73	880.57	1.52	874.84
	7.80	890.25	0.12	880.45
	8.95	896.31	2.87	887.34
	7.87	905.84	1.34	895.95
	2.84	905.79	2.87	902.93
	0.80	897.01	7.58	896.21
	2.90	888.50	11.41	885.60
	4.34	892.44	2.42	886.08
	3.42	891.17	4.49	887.75
	3.93	889.35	5.75	885.94
B.M.			6.35	883.00 882.99

12/7/25

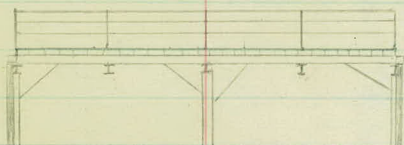


Proj. # 26-04

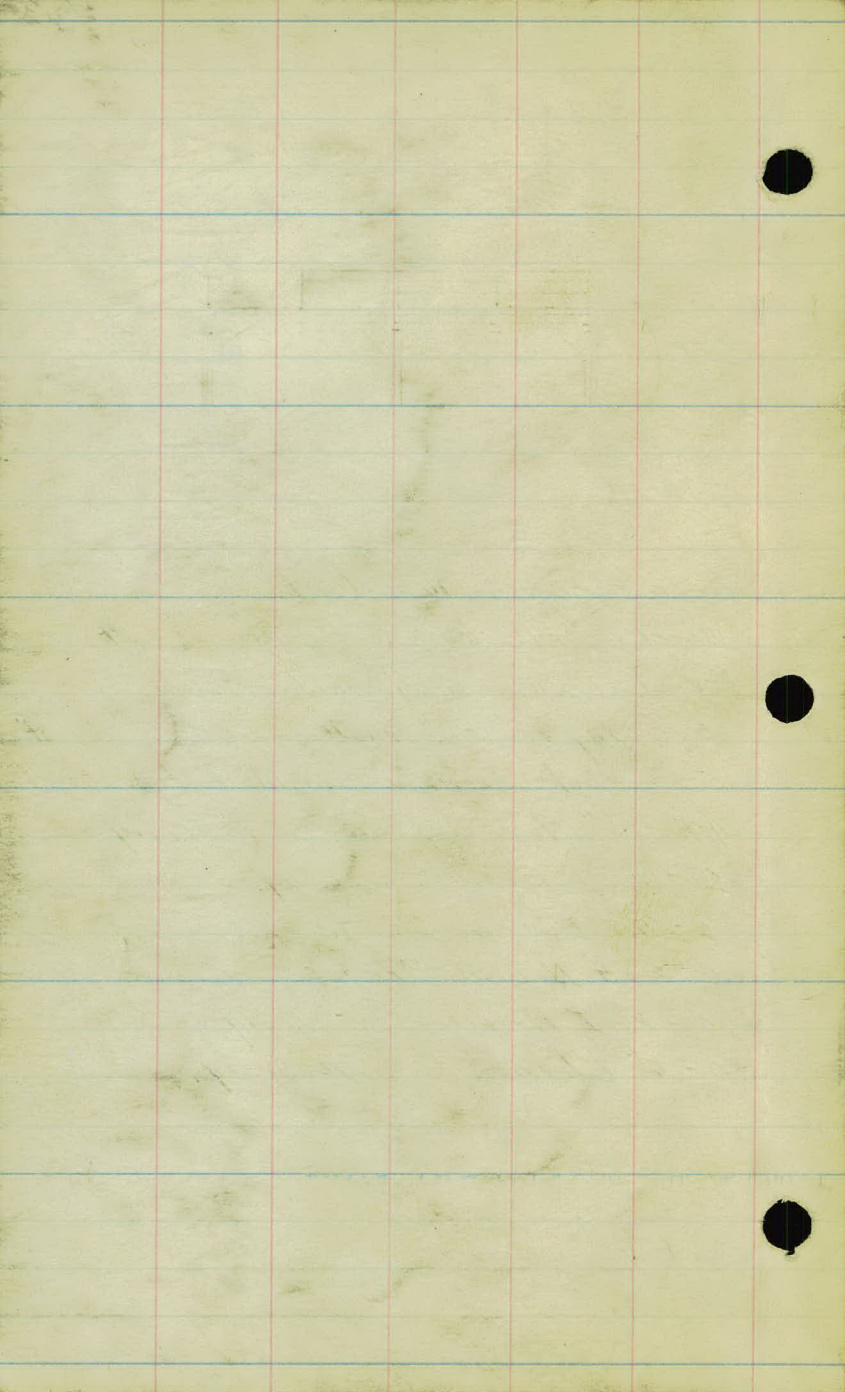
Rice Creek Bridge.



12/9/25



- ✓ For 50 - 3" x 12" x 16' Planks.
- ✓ Wheel Guards 50' of 4" x 6" Timbers Lt. & Rt.
- ✓ 50' of Iron Guard Rail Lt. & Rt.
Consisting of 3 - 2" Angle Iron Rails Lt. & Rt.
- ✓ 5 - 2" Angle Irons Up Rights 4' High Lt. & Rt.
- 4 - 8" Channel Iron 25' Lt. Long
- ✓ 2 - 6" I. Beams 16' Long.
- ✓ 2 - 7" I. Beam Post.
- 8 - 3" x 4" Δ Iron Braces.
- ✓ 10 - 8" I. Beams 25' Long.
- ✓ 6 - 6" Channel Iron 16' Long.



Plans in-hand Insp.-

3-2-26

Rice Creek Rd.-

Proj. 26-04

P.R.B.
H.D.V.K.

104+36. Insp. old 15" X 30" \checkmark too short
Rem. and Pl. 24" P₃ - Drains Rt.

105 to 106+95 Special Ditch Gr. Lt
to Drain Back. \checkmark Towards 104+36-

106+95 Lt. Rem. Culv. \checkmark none necessary

107+43. Rem. 15" X 39" C.M. \checkmark Good Cond. -
P. ~~24"~~ 18" P₃ - Drains Rt.

113+00 to Bridge G.R. on \checkmark Rt & Lt. -

Bridge to 115+60. G.R. on Rt \checkmark & Lt. -

115+73 Rt. 12" X 20" C.M. Rem. \checkmark F.F.
Pl. - 15" X 24" C.M.

115+50 to 117+00 - Cl. & Br. 7 trees Rt. \checkmark
Move Lilac bushes up to farmer

116+50 to 118+25 - Lt. Cl. \checkmark & Gr. 11 trees.

117+69 - Lt. - Imp 12" X 20' G.M. Perm. ✓
Pl. 15" X 24' G.M. F.E. ✓

Note on Plans - 110 to End ✓
Power poles on Rt. to be inserted

End.

U 2486