

PLANS SURVEY  
RICE STREET

From Larpenteur Ave.

To County Road "A"

RD. 1/2 N<sup>o</sup> 1

PROJ. N<sup>o</sup> 26-02

Office of Ramsey Co. Engineer  
ST. PAUL, MINN.

Filed 11-25-25

File No.

7

Proj. # 26-02

Art. Topog. from  
Sta. 0100 to Sta. 26732.

Wichtig  
Pavement

Lt. & H.

2+00

12<sup>1</sup>

11<sup>2</sup>

1+00

12<sup>2</sup>

12<sup>2</sup>

0+00

12<sup>2</sup> - 12<sup>2</sup>

0-1+00

11/30/25

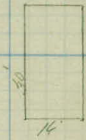
100 T.P. 21 R.

+63<sup>E</sup> S/100 ft 52 L.

+50 P.P. 19 L.

+42 P.P. 19 L.

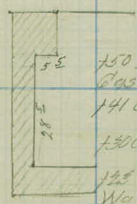
+33<sup>E</sup> Spore N. 30 L.



Porew Pit.

one Course Conc. 24 Wide

+95 T.P. 21<sup>5</sup> R.  
+70 Conc. Wall 26<sup>5</sup> R.  
+70 Conc. Blk 59 R.



+50 Intake Valve for  
Gas Tank 16 R.  
+41 Gasoline Pump 28 R.  
+30 Conc. Blk 55 R.  
+25<sup>E</sup> Cor of Side  
Wall R. 27 R.

+30 P.P. 20 L.

+25 Co. Rd. Sign 21 L.

+99<sup>E</sup> End of City  
Pave. 126.8 12 R.  
+84<sup>E</sup> End of Muffler  
Gutter 15 X 6 X 14

3' X 10' X 31'  
WOODEN  
HEADER

5' X 10' X 32'  
WOODEN  
HEADER

0700 & Loop. Rvc  
+71 Rubble Stone Gutter  
4 X 10  
+67<sup>E</sup> End of 24 R.  
+59<sup>E</sup> End of City P. 25 R.  
+59<sup>E</sup> Wall 140 5 R.  
+58<sup>E</sup> C.B. 25 R.

+69<sup>E</sup> Pave. 15 L.  
+69<sup>E</sup> End of Conc 23 L.  
+61 C.B. 25 L.  
+51<sup>E</sup> Pave. 4<sup>2</sup> L.  
+46 Pave. 10 L.  
+45 Hyd. 24 L.

+51<sup>E</sup> Pave. 4<sup>2</sup>  
+46 Pave 10 L.  
+45 P.P. 26 R.

+11 P.P. 24 L.  
5' X 8' Curp 25 L. R.R.  
Edge of Pvc. 23.7 25 R.  
" " " 10.7 25 R.



11.

11.

5700

12<sup>2</sup>

11<sup>8</sup>

4700

12<sup>0</sup>

12<sup>0</sup>

3700

12<sup>1</sup>

11<sup>2</sup>

2700

11/20/25

F. 36 L.

155 F. 35 E

130 F. 38 E L

181 P.P. 18 E L

172 P.P. 18 E L

169 P.P. 18 E L



Pasture



Timber

124 T.P. 21 R

104 T.P. 21 R

Lt. Pt.

8100

11<sup>75</sup>

12<sup>25</sup>

7100

11<sup>2</sup>

12<sup>2</sup>

6100

12<sup>0</sup>

12<sup>0</sup>

5100

11/20/25

107 P.P. 18<sup>5</sup> L.  
(Fro. light)

136 M. Carrans  
Lake Blvd. So.  
130 F. 57 L.

119 F. 37 L.

107 F. 28 L.

100 F. 28 L.

138 P.P. 18<sup>5</sup> L.

100 F. 33<sup>5</sup>

114-4-15" Willows 30 L.

109 P.P. 18<sup>5</sup>

Pasture

SWAMP  
175 T.P. 21<sup>5</sup> P.  
164 Mail Box 22 R.

131 Co. Rd. 500 18 R.



189 Chicken Shack  
35<sup>5</sup> R.

156 T.P. 21<sup>5</sup> R.

SWAMP

174 Pri. Ent.

161 T.P. 21 R.

144 Mail Box 20 R.



11700

11<sup>8</sup> . 12<sup>35</sup>

10700

11<sup>45</sup> . 12<sup>52</sup>

9700

11<sup>65</sup> . 12<sup>35</sup>



f.  
i.

9700

11/20/25

11  
10  
9  
8  
7  
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5  
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3  
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11

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0  
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7  
8  
9  
10  
11

155 End of Willows SW

112 T.P. 22R

SWAMP

SWAMP



112 P.P. 19L

192 P.P. 18L

193 T.P. 22R

150 Beginning of Willows 29L

164 Willows SW

14700

10<sup>25</sup>

13<sup>05</sup>

13700

11<sup>0</sup>

13<sup>0</sup>

12700

11<sup>4</sup>

12<sup>4</sup>

11700

11/20/25

T

+88 End of WW Pipe  
30' L.

+72 P.P. & Arc  
Light. Pole 10' L.

+15 F. Cor. 42' L.

+51 P.P. 20' L.

+74 - 18" Water Main  
55' L. and W. W.

+60 - 36" Water Main  
55' L.

+34 Cross Drain  
5x3' x 41' Conc. Box  
With Wing Walk  
Filled With Water  
Same type as at  
Sta. 17+55.

+31 P.P. 19' L.

+60 - 6" T. - 28' R.

+52 - 12" T. - 25' R.

+24 T.P. 20' R.

+42 Mail Box 26

+37 Mail Box 26

+36 - 12" T. - 31' R.

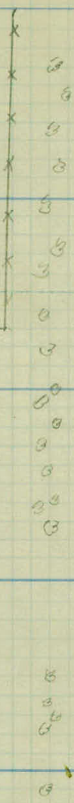
+21 @ Road 17'

+63 Cross Drain  
36" x 64' C.I.P.  
Extends 30 R. & 34 L.

Extends 29 L. & 32 R.

SWAMP

SWAMP



17+00

12<sup>95</sup>

11<sup>05</sup>

16+00

10<sup>25</sup>

13<sup>25</sup>

15+00

10<sup>8</sup>

13<sup>2</sup>

14+00

712 P.P. 17<sup>5</sup> L.

787 F. Cor. 40<sup>1</sup>.

777 F. Cor. 40<sup>5</sup> L.

720 M<sup>2</sup> Carross  
halle 5<sup>1</sup>/<sub>4</sub> 18<sup>1</sup>.

700 F. 29<sup>5</sup>

792 P.P. 17<sup>5</sup> L.

+ 47-6"-T.-24<sup>2</sup>  
+ 45-6"-T.-25<sup>2</sup>

763 Bldg. 36<sup>1</sup> R.



E. P. 20' 717 Bldg 36<sup>1</sup> R.  
716 T.P. 20<sup>1</sup> R.

766 30"-T.-36<sup>1</sup> R.

777-6"-T.-22  
771-6"-T.-22

759 T.P. 20<sup>1</sup> R.

Harj Neelson

20

11 <sup>40</sup>

12 <sup>75</sup>

19

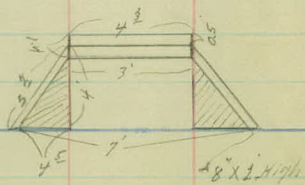
11 <sup>15</sup>

12 <sup>25</sup>

18

11 <sup>35</sup>

12 <sup>25</sup>



17

11/21/25

184 Surface  
Drain 15' W.  
19' 48' C. M.  
1900' Cont.  
171 P.P. 19 L.  
Arc. 240'

196 Side Drain 34' W

Hay Meadow

145 Foot of Willow  
30' R.

144 Surface Drain  
12' 48' W.  
12' 5' x 9' 5' C.M.  
15' 5' Foot Bank  
117 Footing of  
Willows 27' R.

183 F. C. 36'

189 T.P. 21 1/2

154 P.P. 19 1/2 L.

Ditch

Hay Meadow

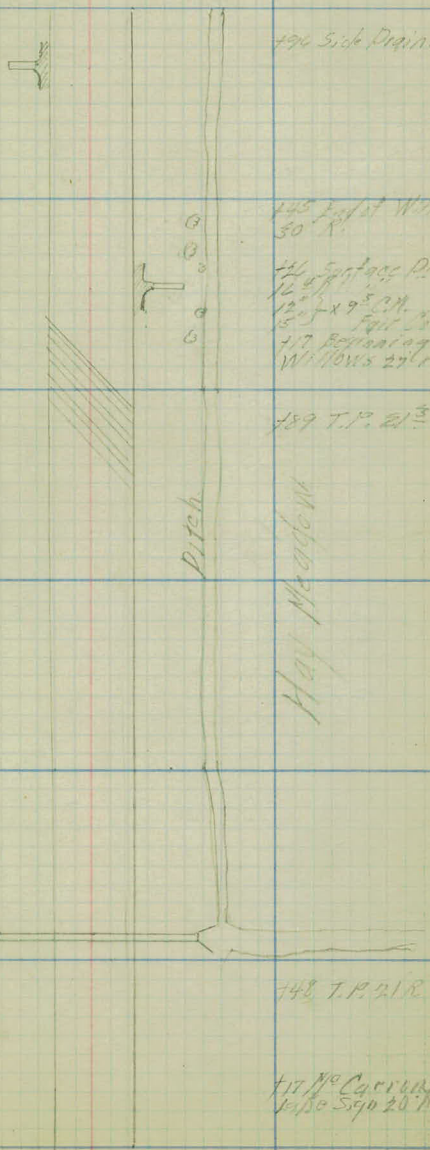
100 F. 37'

155 Cross Drain  
5' x 5' x 5' C. M. Box  
Extend 28' R. & 20'  
With Wing Walls

148 T.P. 21 R

152 P.P. 19 1/2 L.

117 No Curves  
14' 10' Sign 20' R.



23700

10<sup>45</sup>

13<sup>55</sup>

22700

10<sup>55</sup>

13<sup>45</sup>

21700

11<sup>0</sup>

13<sup>0</sup>

20700



26+00

12<sup>e</sup>

12<sup>e</sup>

25+00

11<sup>e</sup>

12<sup>4</sup>

24+00

11<sup>e</sup>

12<sup>2</sup>

23+00

11/21/20

+791 P.P. 18<sup>e</sup>

+400 P.P. 22<sup>e</sup>

+795 T.P. 20<sup>e</sup>

+752 F. 41<sup>e</sup> P.

Timber

P.W. 1/2

+794 F. 37<sup>e</sup> R.

+69 F. 30<sup>e</sup> P.

+61 T.P. 25<sup>e</sup> R.

+754 P.P. 18<sup>e</sup>

H.W.

+32 Farm Ent.

+20 F. Cor. 29<sup>e</sup> R.

+99 30<sup>e</sup> T. - 24<sup>e</sup> R.

+89 Side Drain 16<sup>e</sup> L.  
15' x 40' C.M. New

+81 Willows 31<sup>e</sup> R.

+69 Road to  
L. 9<sup>e</sup> R.

+47 Side Drain 15<sup>e</sup> L.

+34 P.P. 17<sup>e</sup> L.

+25 T.P. 21<sup>e</sup> R.



4  
B  
B  
B  
B  
B

48100

47100

12<sup>0</sup>

12<sup>0</sup>

452

12<sup>0</sup>

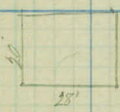
12<sup>0</sup>

46100

11/21/20

+59 Side Drain 25'  
8" x 7' Vitr.

+11 C.P. 18'



146' Culv.



+91 T.P. 19' K

+56 Co. Rd Sign 28'

+50 Side Drain 25'  
15" x 40" Cono. Culv.  
Very Good Cond.

+32 Co. Rd Sign

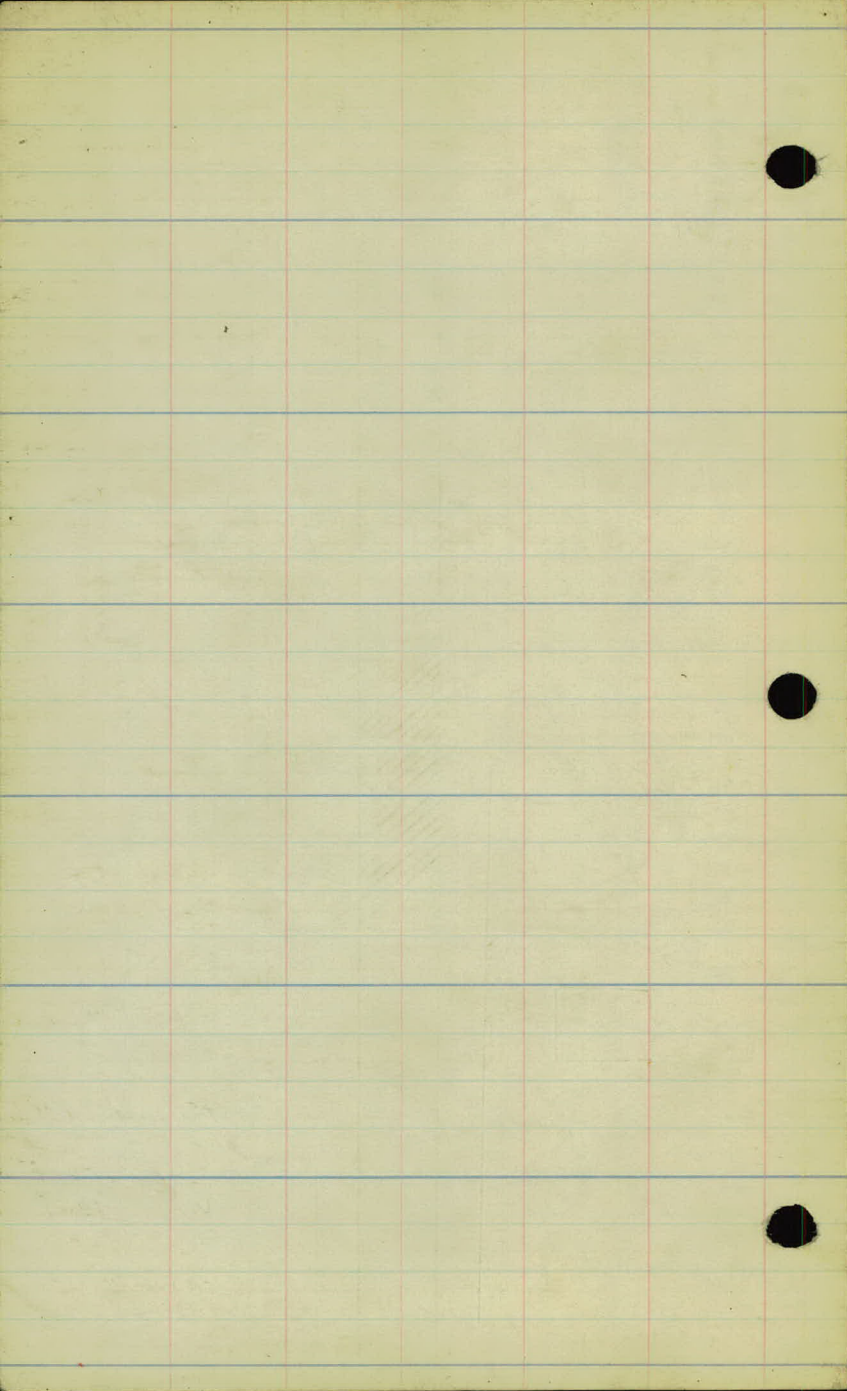
+10 Side Drain 23'

+77 Filling Station 45'

+46 Ref.

+24 Ref.

+11 Side Drain 14'  
15" x ? Cono. Culv.



Proj. # 26-02.

Alignment from  
Laipenteur to Co. Rd. A<sup>22</sup>.

Rice St.-

26-02

Office of Ramsey Co. Engineer  
ST. PAUL, MINN.

Date Filed 11-25-25

File No. ....

*Crane*

*Beethiaume*

*Franks.*

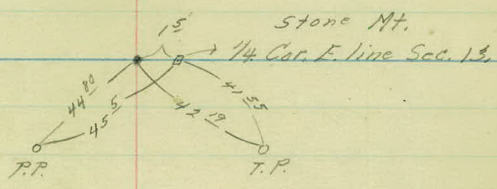
Stg. Point Lt. Mt.

26+32° P.O.T.

100°-00'E

0+00

Co. Rd. A<sup>2</sup>



T.P.  
O



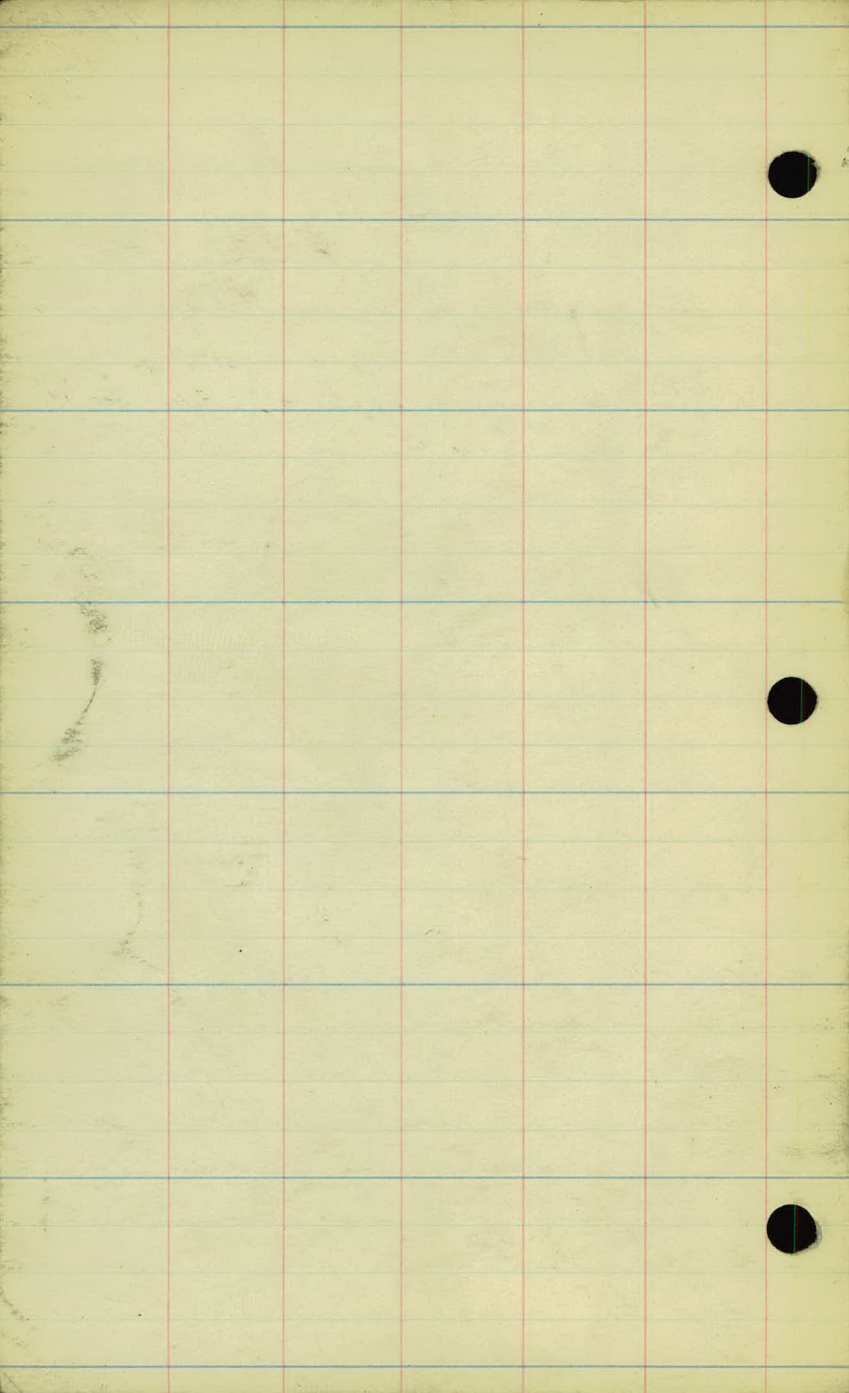
47.95

51  
44

Larpenteur Ave.



S.E. Cor. of Sec. 13.  
Stone Mt.



Proj # 26-07

Center line Levels &  
X Sections from Sta. 0+00-26+52.

Sta.	+	H. I.	-	Rod	Elev.
B.M.	5.54	870.77		865.23	
-2+00				1.00	869.77
-1+50				2.13	68.44
-1+00				3.28	67.49
-0+48 <sup>E</sup>				4.58	66.19
-0+30 <sup>E</sup>				5.06	65.71
0+00				5.78	64.99
1+00				7.94	62.53 62.93
+45				7.04	61.71
T.P.			1.24	869.53	
2+00				10.16	60.61
T.P.	2.83	863.34	10.24	860.53	
+60				3.94	59.40
3+00				4.74	58.60
+28				5.42	57.94
+48				5.85	57.51
+84				6.68	56.68

Lt.

Rt.

Sph. in Arc Light Pole Int. of Larp. & Rice. #1 B3.

41	48	5.52	5.10	5.16	5.42	4.76	4.8
33	23	23	9.4	5.06	9.5	29	23

Top of Carb

5.9	5.7	6.4	6.4	5.5	5.79	5.88	5.4	5.4	5.7
33	23	217	206	19	12	5.78	12	18	53

5.18 865.59 = Flex. Conc. Side Wall Lt.

5.15	865.52	"	"	"	"	"	"	"	"
		9.1	8.03	8.06	8.0	4.7	4.4		
		33	12	7.94	12	23	33	40	

8.8	8.9	9.10	9.12	9.2	9.7	9.0	1.3
312	30	12	9.06	12	19	25	58

Tip of Staffe.

9.7	10.3	11.4	10.4	10.27	10.50	10.4	10.6	10.6	10.0
50	33	27	20	12	10.16	12	19	21	24

2.8	4.9	5.5	4.0	4.00	4.12	4.6	4.2	4.6	4.2
32	27	24	18	12	3.94	12	12	17	22

5.5	6.1	5.0	4.83	4.89	5.3	5.1	5.5	4.4
26	32	12	12	4.74	12	12	16	26.7

4.5	7.1	7.1	5.9	5.51	5.54	5.8	5.5	6.4	6.4	5.2
31	24	19	15	12	5.42	12	12	17	14	27

6.1	7.7	7.7	6.2	5.97	5.92	6.3	6.0	6.9	6.8	5.9
33	27	14.6	17	12	5.85	12	12	17	14	28

8.4	8.0	6.9	6.77	6.80	7.2	6.7	6.8	7.5	7.3	4.1	3.3
31	21	17	12	6.68	12	12	16.8	25	28	32	36.40

Sta.	T	H.I.	-	Rod	Elev.
		863.34			
4+00				6.94	856.40
	425			7.44	55.90
T.P.			6.94	856.40	
T.P.	12.02	881.55		869.53	
T.P.	12.29	892.83	101	880.54	
T.P.	11.49	903.85	0.47	892.34	
2+60					
3+00					
3+28					
3+48					
T.P.	0.42	892.47	11.80	892.05	
3+84					
1+45					
1+00					
2+60					

Lt.

Rt.

<u>0.3</u>	<u>8.4</u>	<u>8.5</u>	<u>7.2</u>	<u>7.02</u>		<u>7.05</u>	<u>7.5</u>	<u>7.1</u>	<u>7.7</u>	<u>2.2</u>
40	32	25	18	12	6.94	12	12	17	30	40

<u>1.9</u>	<u>3.7</u>	<u>8.1</u>	<u>8.9</u>	<u>9.0</u>	<u>7.7</u>	<u>7.51</u>		<u>7.66</u>	<u>8.0</u>	<u>7.7</u>	<u>7.6</u>	<u>8.5</u>	<u>8.4</u>	<u>11.4</u>	<u>12.5</u>
37	36	31	28	23	17	12	7.44	12	12	17	21	24	27	36	44

Nail in T.P.

Top of stake.

<u>6.5</u>	<u>6.6</u>	<u>10.8</u>
100	83	80

<u>1.0</u>	<u>1.5</u>	<u>5.9</u>
100	83	75

<u>2.0</u>	<u>2.7</u>
100	80

<u>5.2</u>	<u>5.1</u>
100	86

<u>4.4</u>	<u>6.5</u>
100	73

<u>9.2</u>	<u>11.3</u>
62	75

<u>10.3</u>	<u>12.4</u>
52	65

<u>10.8</u>	<u>10.3</u>
49	65

Sta.	+	H.I.	-	Rod	Elev.
		872.47			
3+00					
3+28					
3+48					
T.P.	1.74	882.12	12.09	880.38	
3+84					
4+00					
T.P.	0.44	870.54	12.02	870.10	
4+25					
T.P.	0.62	858.66	12.50	858.04	
T.P.	2.24	858.66	1.24	856.40	
4+55				3.45	855.21
5+00				4.55	54.11
+50				5.72	52.94 53.94
+74	Pri. Ent. Pt.			6.24	52.40
6+00				6.75	51.91
T.P.	3.23	853.34	8.55	850.11	
+65				2.53	50.81

Lt.

Rt.

$\frac{10.6}{55}$      $\frac{9.5}{65}$

$\frac{9.4}{55}$      $\frac{9.2}{65}$

$\frac{11.0}{52}$      $\frac{10.9}{65}$

$\frac{13.0}{42}$      $\frac{14.0}{50}$

$\frac{1.8}{83}$      $\frac{3.9}{62}$

$\frac{5.1}{50}$      $\frac{6.2}{73}$

Nail in T.P.

$\frac{3.7}{50}$   $\frac{5.1}{38}$   $\frac{4.9}{32}$   $\frac{4.8}{22}$   $\frac{3.9}{18}$   $\frac{3.48}{12}$   $\frac{3.60}{12}$   $\frac{4.0}{22}$   $\frac{8.7}{296}$   $\frac{9.4}{33}$

$\frac{6.0}{33}$   $\frac{6.1}{23}$   $\frac{4.7}{19}$   $\frac{4.6}{12.2}$   $\frac{4.55}{4.55}$   $\frac{4.63}{11.8}$   $\frac{4.6}{18}$   $\frac{6.0}{23}$   $\frac{11.1}{33}$

$\frac{7.7}{33}$   $\frac{7.1}{23}$   $\frac{5.8}{20}$   $\frac{5.83}{12.2}$   $\frac{5.74}{5.74}$   $\frac{5.87}{11.8}$   $\frac{4.2}{19}$   $\frac{10.6}{33}$

$\frac{6.39}{6.24}$   $\frac{4.7}{12}$   $\frac{8.3}{17}$   $\frac{10.8}{24}$   $\frac{15.3}{38}$   $\frac{15.3}{64}$

$\frac{9.5}{33}$   $\frac{8.6}{25}$   $\frac{7.0}{18}$   $\frac{6.84}{12.1}$   $\frac{6.75}{6.75}$   $\frac{6.88}{11.9}$   $\frac{7.2}{20}$   $\frac{13.1}{30}$   $\frac{13.8}{33}$

$\frac{5.3}{33}$   $\frac{4.4}{33}$   $\frac{3.1}{20}$   $\frac{3.57}{12}$   $\frac{2.53}{2.53}$   $\frac{2.67}{12}$   $\frac{2.6}{19}$   $\frac{11.2}{34}$

Sta.	+	H.I.	-	Rod	Elev.
		853.34			
778				1.75	850.59
7+00				3.14	50.20
713				3.40	49.94
+20				3.50	49.84
734	Side Road Lt.			3.74	49.60
+64				4.25	49.09
774				4.52	48.82
8+00				4.92	48.42
+50				5.93	47.41
T.P.	1.32	847.67	6.99	846.35	
9+00					46.21
+50				2.11	45.56
10+00				2.92	44.75
+50				3.57	44.96
11+00				4.32	44.10
					43.35
734	Cross Drain				
+50				4.84	42.81
+60				5.03	42.64



Sta.	+	H.I.	-	Rod	Elev.
		847.67			
	+63	Cross Drain			
	+79			5.75	841.92
	+92			5.72	41.95
12	+00			5.31	42.36
11	+74	Water Main			
11	+74	" "			
12	+21	Adj. to Filtration Plant		4.77	42.90
12	+35			4.72	42.95
	T.P.	5.83 847.84	5.64	842.01	
	+79			4.10	43.04
13	+00				42.87
	+50			5.00	42.84
14	+00			4.82	43.02
	+50			4.64	43.18
15	+00				43.30
	+40			4.57	43.47
	+50			4.21	43.54
16	+00			4.00	43.84
	B.M.	3.78 848.07	3.55	844.29	844.30
	+50			3.99	44.08
17	+00			3.88	44.19

Lt.

Rt.

13.14  
34

13.27  
30

Invert Rt.

Top of pavement

12.2	12.0	6.4	5.4	6.51		5.75	5.4	6.1
33	29	18	12	11.4	5.31	12.6	18	33

9.5  
32  
10.0  
32

Top of 30" Water Main. Lt.

" " 18" " " Lt.

7.1  
200

						5.20	5.2	6.7	7.3	7.0	7.3
4.77						12.4	18	50	75	100	150

13.8	12.6	6.1	5.1	5.84		5.06	6.0	6.1
33	29	18	12	11.4	4.72	12.6	24	33

13.2	12.3	6.2	5.2	5.95		5.08	5.6	9.4	9.6	11.1
33	28	17	12	11.4	4.80	12.6	25	31	33	50

12.9	12.3	6.0	5.56			5.21	5.2	10.6	11.4	11.4
33	30	17	11.1	4.97		12.7	18	28	34	39

11.5	10.9	5.8	5.04			4.96	5.2	6.2	10.9	11.3	11.4
33	24	18	10.9	4.82		13.1	17	21	29	33	39

7.0	7.0	5.7	4.4	4.57		4.74	4.7	5.4	5.9	6.3
35	33	24	18	10.8	4.54	13.2	16	23	25	33

4.0	4.5	6.0	4.6	4.6	4.45		4.50	4.6	4.4	4.9
34	33	30	24	18	10.8	4.57	13.2	21	27	33

3.4	5.7	5.6	4.5	4.2	4.14		4.01	3.8	3.8
39	32	31	28	14	10.8	4.00	13.2	31	33

Spk in P.P. W. Side of Rice St., directly E. of M<sup>c</sup>Carsons Lake

Spk. in P.P. Lt. 37 or 16 + 12

34	5.0	5.1	4.5	4.1	4.08		3.93	3.8	3.4	4.0
36	29	24	22	14	11	3.88	13	18	21	33

Sta.	+	H.I	-	Rod	Elev.
		848.07			
147				3.95	844.12
155 <sup>s</sup>	Cross	Prin			
167				4.10	43.97
18+00				4.28	43.79
150				1.52	43.55 43.52
19+00				4.67	43.40
150				4.63	43.44
20+00				4.40	43.67
150				4.50	43.57
21+00				3.67	44.40
150				3.12	45.05
22+00				2.01	46.09
T.P.	8.35	865.48	0.24	847.13	
150				4.69	47.79
23+00				5.70	49.78
142				4.06	51.42
153				3.62	51.84
169	side	Road		3.10	52.38
180				2.74	52.74

LT

RT

72 63 60 46 42 411  
40 39 25 22 14 11

409 40 4.1 7.2 8.2 88  
13 17 22 27 33 40

106

264 837477-Invert

113

286 83677-Invert

87 86 103 104 51 44 424  
10 4 34 32 23 14 11 4.10

425 41 4.3 118 8.6 8.6  
129 14 21 30 35 37

93 92 102 71 51 46 445  
40 38 36 34 23 14 112 4.28

435 4.4 5.1 9.6 114 5.5 9.7  
128 14 32 30 32 36 41

104 94 55 42 476  
41 38 21 15 112 4.67

5.0 5.0 8.5 8.4 8.8 110 112 9.5  
128 14 21 24 30 31 33 34

112 110 103 98 56 52 53 457  
37 35 32 24 18 14 104 5 4.40

450 45 4.2 7.9 115 115 105 100  
128 17 21 30 33 35 38 42

102 104 95 43 41 416  
41 34 38 30 15 11 3.67

3.75 4.0 4.4 8.7 9.1 102 110 9.5  
13 17 21 27 33 38 42 47

85 82 74 65 12 197  
40 31 24 20 14 105 2.01

2.32 2.4 2.4 9.6 105 9.5 9.5  
13.5 17 31 41 43 45 50

104 104 60 558  
33 27 18 105 5.70

6.3 6.9 15.3 15.7  
135 21 34 40

81 77 67 72 41 480  
40 34 28 24 20 118 4.14

4.22 4.8 12.5 13.3  
122 17 28 40

42 37 3.77  
40 30 109 3.62

3.76 4.2 11.8 12.6  
13.1 20 32 40

28 38 37 30 3.77  
100 45 50 14 116 3.10

38 37 2.7 2.74  
40 33 74 11 2.74

1.80 2.9 8.5 8.8  
13 18 24 33

Sta.		H.I.	-	Rod.	Elev.
		855.48			
+91				2.32	853.14
24+00				2.00	53.48
+20				1.24	54.24
T.P.	12.92	848.17	0.93	855.25	
+43				13.11	55.04
25+00				1.04	57.13
+53				2.97	59.20 60.20
26+00				7.05	61.12
+09				6.67	61.50
+14				6.51	61.64
+19				6.32	61.85
+32	Co. Rd A <sup>2</sup>			5.71	62.24
+44				5.44	62.73
27+00				3.62	64.55

11

57

<u>22</u>	<u>28</u>	<u>47</u>	<u>47</u>	<u>30</u>	<u>2.51</u>	<u>2.40</u>	<u>2.5</u>	<u>6.8</u>	<u>7.0</u>	
50	42	39	25	21	111	2.52	12.9	19	26	34

<u>01</u>	<u>26</u>	<u>26</u>	<u>3.5</u>	<u>44</u>	<u>7.4</u>	<u>21</u>	<u>2.10</u>	<u>2.08</u>	<u>2.0</u>	<u>5.4</u>	<u>6.3</u>	
50	58	34	33	27	23	17	112	2.00	12.8	21	24	33

Above H.I.

<u>1.20</u>	<u>0.0</u>	<u>21</u>	<u>1.3</u>	<u>1.32</u>	<u>1.40</u>	<u>1.5</u>	<u>4.5</u>	<u>2.4</u>	<u>3.8</u>	<u>5.5</u>	
50	33	25	14	11.3	1.24	12.7	18	2.5	26	53	40

<u>08</u>	<u>14</u>	<u>5.8</u>	<u>11.9</u>	<u>13.8</u>	<u>13.9</u>	<u>13.3</u>	<u>13.17</u>	<u>12.27</u>	<u>13.5</u>	<u>14.4</u>	<u>14.4</u>	<u>13.5</u>	<u>14.4</u>	<u>15.4</u>	
57	50	40	25.5	23.4	22	20	11.4	13.11	12.4	18	21	22.6	24	33	40

Above H.I.

<u>1.65</u>	<u>11.00</u>	<u>86</u>	<u>7.7</u>	<u>11.5</u>	<u>12.4</u>	<u>12.1</u>	<u>11.3</u>	<u>11.16</u>	<u>11.20</u>	<u>11.1</u>	<u>12.7</u>	<u>12.8</u>	<u>0.1</u>	<u>0.1</u>	
66	53	39	25	24	21	20	18	11.4	11.04	12.4	19	20.7	25	37	40

Above H.I.

Above H.I.

<u>1.66</u>	<u>1.65</u>	<u>6.4</u>	<u>7.9</u>	<u>10.3</u>	<u>10.1</u>	<u>9.3</u>	<u>9.03</u>	<u>9.07</u>	<u>9.2</u>	<u>11.4</u>	<u>11.0</u>	<u>1.26</u>	<u>1.15</u>	
55	47	31	24	23	20	18.5	11.8	8.97	12.2	17	22.5	25	37	44

Above H.I.

Above H.I. + 24  
75

<u>1.20</u>	<u>1.21</u>	<u>7.4</u>	<u>9.2</u>	<u>7.1</u>	<u>7.2</u>	<u>7.12</u>	<u>7.12</u>	<u>7.12</u>	<u>7.12</u>	<u>6.8</u>	<u>9.3</u>	<u>7.2</u>	<u>4.9</u>	<u>5.2</u>	<u>3.5</u>	<u>7.2</u>
45	38.4	26	24	21	17	12	7.05	12	17	23	25	28	45	63	70	

Above H.I.

<u>1.26</u>	<u>1.06</u>	<u>5.4</u>	<u>7.6</u>	<u>7.0</u>	<u>9.0</u>	<u>6.9</u>	<u>6.78</u>	<u>6.92</u>	<u>6.5</u>	<u>9.2</u>	<u>9.0</u>	<u>5.0</u>	<u>5.1</u>	
45	40	31	25	22	22	18	12	6.67	12	21	23	29	33	50

<u>1.8</u>	<u>3.4</u>	<u>5.7</u>	<u>6.0</u>	<u>6.5</u>	<u>6.54</u>	<u>6.67</u>	<u>6.2</u>	<u>6.2</u>	<u>7.7</u>	<u>8.3</u>	<u>7.8</u>	
45	35	28	21	16	12	6.51	12	18	26	32	38	50

<u>3.0</u>	<u>3.6</u>	<u>5.4</u>	<u>6.41</u>	<u>6.50</u>	<u>6.0</u>	<u>6.0</u>	
45	37	25	12	6.32	12	20	50

<u>4.6</u>	<u>5.0</u>	<u>5.8</u>	<u>6.00</u>	<u>5.98</u>	<u>5.8</u>	<u>5.6</u>	<u>5.2</u>	
50	30	21	12	5.91	12	27	50	100

<u>4.6</u>	<u>4.9</u>	<u>5.54</u>	<u>5.51</u>	<u>5.4</u>	<u>6.0</u>	<u>6.0</u>	
45	29	13	5.44	12	30	37	50

Sta.	+	H.I.	-	Rod	Elev.
		868.17			
+50				2.12	866.05
28 + 00				0.62	865.43
B.M.			6.37	861.78	

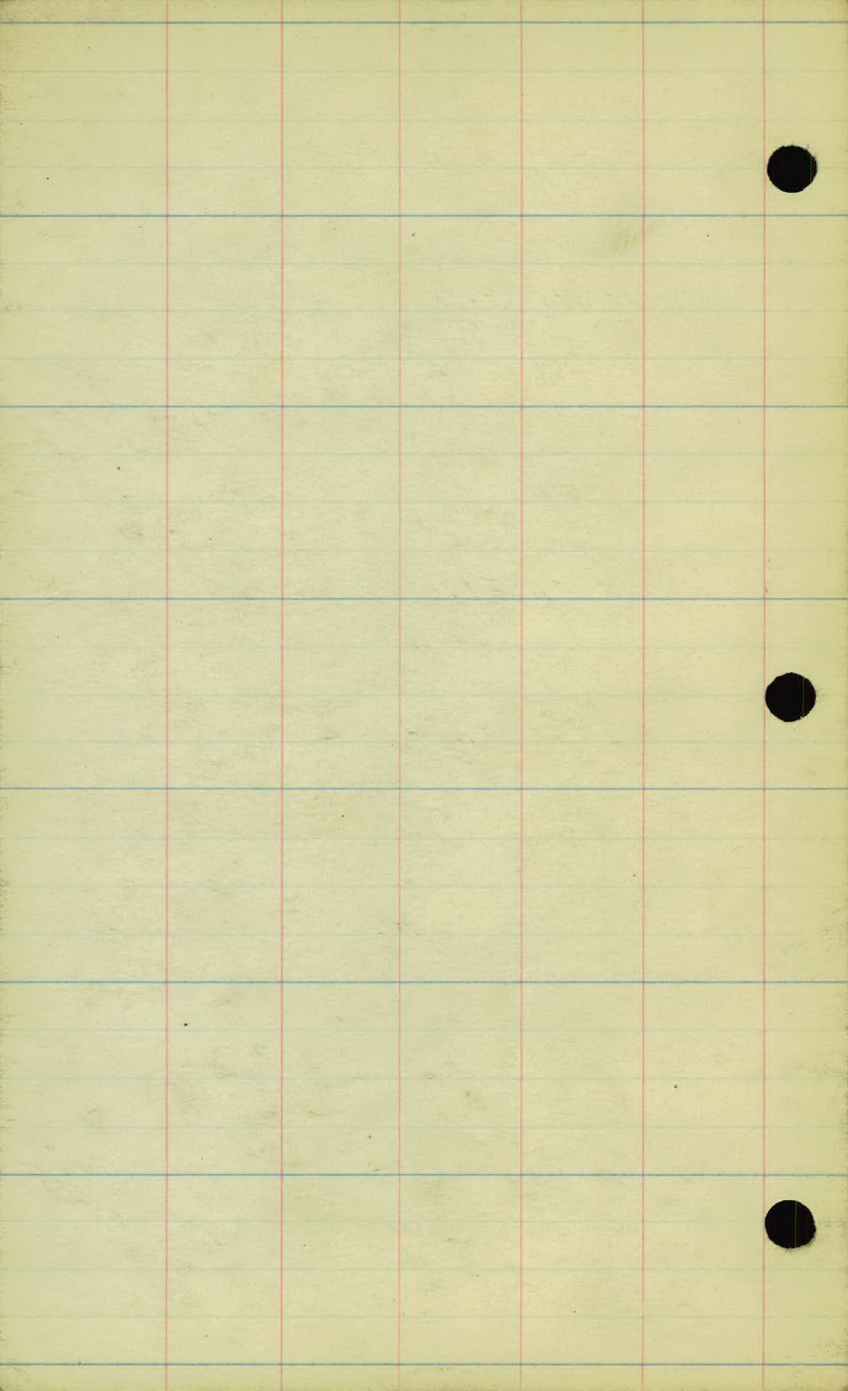
check levels from  
Sta. 25 + 91 to Sta. 16 + 12.

B.M.	0.07	861.85		861.78	
T.P.	0.41	850.95	11.31	850.54	
T.P.	4.80	848.24	7.51	843.44	
B.M.			3.96	844.28	844.27

SpK in P.P. Lt. Sta. 25+91.

SpK in P.P. Lt. Sta. 25+91

SpK in P.P. Lt. Sta. 16+12.



Rice Street

Proj. 26-02

Top Pavement X-Sec.

station	+	H.I.	-	E/ev.
B.M.	1.43	866.66		865.23
-0+30.5				65.72 ✓
-0+01.	= construction joint.			64.98 ✓
0+00				64.98 ✓
+25				64.52 ✓
+50				63.96 ✓
+75				63.34 ✓
1+00				62.86 ✓
+25				62.27 ✓
+50				61.75 ✓
+75				61.06 ✓
2+00				60.69 ✓
+25				60.09 ✓
+50				59.72 ✓

Lt.

±

Rt.

2

Spike in Arc. Lt. Pole (Larp &amp; Rice St.) H. Sta. 2430

Note: Readings to hundredths,  
are top of Pavement  
: Dist. to tenths are edge  
of Pavement.

0.94

W.H.C.  
A.L.P.  
M.G.  
H.B. } 3-3026

$$\frac{1.70}{12.0}$$

$$\frac{1.68}{12.0}$$

$$\frac{1.75}{12.0}$$

$$\frac{1.3}{18}$$

$$\frac{1.70}{12.0}$$

$$1.68$$

$$\frac{1.75}{12.0}$$

$$\frac{1.2}{18}$$

$$\frac{1.9}{18}$$

$$\frac{2.22}{11.9}$$

$$\frac{2.4}{12.0}$$

$$\frac{2.30}{12.0}$$

$$\frac{2.2}{19}$$

$$\frac{2.9}{18}$$

$$\frac{2.73}{11.9}$$

$$\frac{2.70}{12.0}$$

$$\frac{2.80}{11.9}$$

$$\frac{2.4}{18}$$

$$\frac{3.5}{18}$$

$$\frac{3.39}{11.9}$$

$$\frac{3.32}{12.0}$$

$$\frac{3.40}{11.9}$$

$$\frac{3.1}{18}$$

$$\frac{4.3}{18}$$

$$\frac{4.4}{12} \quad \frac{3.9}{11.8}$$

$$\frac{3.80}{12.0}$$

$$\frac{3.90}{11.9}$$

$$\frac{3.9}{17}$$

$$\frac{4.6}{18}$$

$$\frac{4.8}{12.5} \quad \frac{4.43}{11.9}$$

$$\frac{4.39}{12.0}$$

$$\frac{4.53}{12.0}$$

$$\frac{4.6}{17}$$

$$\frac{5.0}{17}$$

$$\frac{4.98}{12.0}$$

$$\frac{4.91}{12.0}$$

$$\frac{5.04}{11.9}$$

$$\frac{5.1}{17}$$

$$\frac{5.7}{18}$$

$$\frac{5.64}{12.0}$$

$$\frac{5.60}{12.0}$$

$$\frac{5.67}{12}$$

$$\frac{5.6}{17}$$

$$\frac{6.2}{17}$$

$$\frac{6.14}{12.0}$$

$$\frac{5.97}{12.0}$$

$$\frac{6.08}{11.9}$$

$$\frac{6.3}{16}$$

$$\frac{6.8}{17}$$

$$\frac{6.65}{12}$$

$$\frac{6.57}{12.0}$$

$$\frac{6.67}{11.9}$$

$$\frac{7.0}{13}$$

$$\frac{7.1}{17}$$

$$\frac{6.97}{12.0}$$

$$\frac{6.94}{12.0}$$

$$\frac{7.02}{11.9}$$

$$\frac{7.3}{12} \quad \frac{7.2}{16}$$

Station	+	H.I	-	Elev.
		866.66		
2+75				59.17 ✓
3+00				58.74 ✓
+25				58.07 ✓
+50				57.47 ✓
+75				58.93 ✓ 56.93
4+00				56.37 ✓
+25				55.95 ✓
T.P.	0.87	856.32 ✓	11.21	855.45 ✓
+50				55.34 ✓
+75				54.78 ✓
5+00				54.13 ✓
+25				52.50 ✓ 53.50
+50				52.97 ✓
+75				52.40 ✓

Lt.

L

Rt.

3

$$\frac{7.7}{17} \quad \frac{7.51}{12.0} \quad 7.49 \quad \frac{7.6}{11.9} \quad \frac{7.8}{12} \quad \frac{7.6}{17}$$

$$\frac{8.2}{17} \quad \frac{8.09}{12.1} \quad 7.92 \quad \frac{8.00}{11.9} \quad \frac{8.4}{12} \quad \frac{8.2}{17}$$

$$\frac{9.0}{15} \quad \frac{8.65}{12.0} \quad 8.59 \quad \frac{8.80}{12.0} \quad \frac{8.9}{16}$$

$$\frac{9.5}{17} \quad \frac{9.32}{12} \quad 9.19 \quad \frac{9.20}{12.0} \quad \frac{9.2}{17}$$

$$\frac{9.9}{17} \quad \frac{9.86}{11.9} \quad 9.73 \quad \frac{9.87}{12.2} \quad \frac{9.9}{17}$$

$$\frac{10.5}{17} \quad \frac{10.30}{11.9} \quad 10.29 \quad \frac{10.26}{12.0} \quad \frac{10.8}{12} \quad \frac{10.4}{18}$$

$$\frac{10.9}{17} \quad \frac{10.76}{12.0} \quad 10.71 \quad \frac{10.92}{12.0} \quad \frac{11.2}{12} \quad \frac{11.0}{17}$$

$$\frac{1.3}{17} \quad \frac{1.00}{12} \quad 0.98 \quad \frac{1.15}{11.9} \quad \frac{1.2}{17}$$

$$\frac{1.8}{16} \quad \frac{1.64}{12.2} \quad 1.54 \quad \frac{1.69}{11.9} \quad \frac{1.7}{12}$$

$$\frac{2.3}{16} \quad \frac{2.31}{12.1} \quad 2.19 \quad \frac{2.27}{11.8} \quad \frac{2.27}{17}$$

$$\frac{3.0}{16} \quad \frac{2.94}{12.0} \quad 2.82 \quad \frac{2.90}{11.9} \quad \frac{2.8}{17}$$

$$\frac{3.4}{16} \quad \frac{3.47}{12.0} \quad 3.35 \quad \frac{3.47}{11.9} \quad \frac{3.4}{17}$$

$$\frac{4.1}{18} \quad \frac{4.01}{12.0} \quad 3.92 \quad \frac{4.04}{12.0} \quad \frac{4.3}{16}$$

Station + H.I. - Elev.

856.32 ✓

6+00 51.93 ✓

+25 51.51 ✓

+50 51.11 ✓

+75 50.67 ✓

7+00 50.23 ✓

+25 49.81 ✓

+50 49.39 ✓

+75 48.86 ✓

8+00 48.45 ✓

+25 47.96 ✓

+50 47.42 ✓

+75 46.80 ✓

Lt.

Z

Rt.

4

$$\frac{4.6}{17} \quad \frac{4.48}{12.0} \quad 4.39 \quad \frac{4.53}{11.9} \quad \frac{4.4}{17}$$

$$\frac{4.9}{17} \quad \frac{4.87}{11.9} \quad \frac{4.81}{11.9} \quad \frac{4.25}{12.1} \quad \frac{4.8}{18}$$

$$\frac{5.3}{19} \quad \frac{5.25}{11.9} \quad \frac{5.21}{11.9} \quad \frac{5.37}{12.1} \quad \frac{5.3}{17}$$

$$\frac{6.3}{17} \quad \frac{5.72}{11.7} \quad \frac{5.65}{11.7} \quad \frac{5.84}{12.2} \quad \frac{5.7}{18}$$

$$\frac{6.2}{18} \quad \frac{6.05}{11.7} \quad \frac{6.09}{11.7} \quad \frac{6.25}{12.3} \quad \frac{6.0}{17}$$

$$\frac{6.7}{17} \quad \frac{6.60}{11.6} \quad \frac{6.51}{11.6} \quad \frac{6.70}{12.2} \quad \frac{6.5}{16}$$

$$\frac{7.2}{18} \quad \frac{7.01}{11.8} \quad \frac{6.93}{11.8} \quad \frac{7.04}{12.2} \quad \frac{7.0}{17}$$

$$\frac{7.6}{17} \quad \frac{7.53}{11.6} \quad \frac{7.46}{11.6} \quad \frac{7.55}{12.4} \quad \frac{7.5}{17}$$

$$\frac{8.2}{16} \quad \frac{7.93}{11.6} \quad \frac{7.87}{11.6} \quad \frac{8.05}{12.4} \quad \frac{8.0}{17}$$

$$\frac{8.8}{16} \quad \frac{8.51}{11.6} \quad \frac{8.36}{11.6} \quad \frac{8.49}{12.4} \quad \frac{8.5}{17}$$

$$\frac{9.4}{16} \quad \frac{9.21}{11.6} \quad \frac{8.90}{11.6} \quad \frac{8.97}{12.3} \quad \frac{9.2}{17}$$

$$\frac{10.0}{17} \quad \frac{9.89}{11.6} \quad \frac{9.52}{11.6} \quad \frac{9.61}{12.4} \quad \frac{9.8}{17}$$

Station	+	H.I	-	Elev.
		856.32 ✓		
9+00				46.27 ✓
+25				45.91 ✓
+50				45.62 ✓
T.P.	1.94	847.03 ✓	11.18	845.14 ✓
+75				45.20 ✓
10+00				44.79 ✓
+25				44.35 ✓
+50				44.14 ✓
+75				43.78 ✓
11+00				43.40 ✓
+25				43.04 ✓
+50				42.86 ✓
+70				42.31 ✓

Lt.

L

Rt.

5

$$\frac{10.4}{15}$$

$$\frac{10.28}{11.6}$$

$$10.05$$

$$\frac{10.25}{12.4}$$

$$\frac{10.2}{17}$$

$$\frac{10.8}{17}$$

$$\frac{10.59}{11.4}$$

$$\frac{10.41}{-}$$

$$\frac{10.66}{12.4}$$

$$\frac{10.7}{16}$$

$$\frac{11.0}{16}$$

$$\frac{10.84}{11.4}$$

$$10.70$$

$$\frac{10.92}{12.5}$$

$$\frac{11.1}{17}$$

$$\frac{2.4}{16}$$

$$\frac{2.06}{11.5}$$

$$1.88$$

$$\frac{2.00}{12.4}$$

$$\frac{2.4}{18}$$

$$\frac{2.9}{17}$$

$$\frac{2.58}{11.4}$$

$$2.19$$

$$\frac{2.40}{12.6}$$

$$\frac{2.7}{17}$$

$$\frac{3.5}{17}$$

$$\frac{3.24}{11.4}$$

$$\frac{2.73}{-}$$

$$\frac{2.88}{12.5}$$

$$\frac{2.9}{18}$$

$$\frac{3.9}{17}$$

$$\frac{3.72}{11.7}$$

$$2.94$$

$$\frac{3.19}{12.5}$$

$$\frac{3.6}{18}$$

$$\frac{4.4}{17}$$

$$\frac{4.22}{11.7}$$

$$\frac{3.47}{6.3}$$

$$\frac{3.30}{-}$$

$$\frac{3.57}{12.4}$$

$$\frac{3.9}{18}$$

$$\frac{4.8}{16}$$

$$\frac{4.92}{11.7}$$

$$3.68$$

$$\frac{4.31}{12.5}$$

$$\frac{4.3}{19}$$

$$\frac{4.9}{16}$$

$$\frac{4.9}{11.7}$$

$$4.04$$

$$\frac{4.75}{12.3}$$

$$\frac{4.8}{19}$$

$$\frac{5.5}{18}$$

$$\frac{5.3}{11.8}$$

$$4.22$$

$$\frac{4.27}{5}$$

$$\frac{4.93}{12.5}$$

$$\frac{4.7}{17}$$

$$\frac{5.5}{20}$$

Pave  
broken  
away

$$\frac{5.20}{6}$$

$$4.77$$

$$\frac{4.97}{12.5}$$

$$\frac{4.8}{20}$$

station	+	H.I	-	Elev.
		847.08 ✓		
11+85				41.98 ✓
12+00				42.40 ✓
12+25				42.97 ✓
+50				43.10 ✓
+75				43.10 ✓
13+00				42.93 ✓
+25				42.89 ✓
+50				42.91 ✓
+75				42.97 ✓
14+00				43.11 ✓
T.P.	6.05	848.99 ✓	4.14	842.94 ✓
+25				43.28 ✓
+50				43.31 ✓

$\frac{5.7}{18}$	$\frac{4.9}{12}$	Pave Broken Runway	$\frac{5.10}{-}$	$\frac{5.25}{12.6}$	$\frac{5.1}{21}$
------------------	------------------	--------------------------	------------------	---------------------	------------------

$\frac{5.6}{17}$	$\frac{4.7}{10}$	↓	$\frac{4.68}{-}$	$\frac{5.11}{13}$	$\frac{5.1}{22}$
------------------	------------------	---	------------------	-------------------	------------------

$\frac{5.1}{15}$	$\frac{4.72}{27}$	$\frac{4.23}{4.5}$	$\frac{4.11}{-}$	$\frac{4.51}{12.9}$	$\frac{4.8}{13}$
------------------	-------------------	--------------------	------------------	---------------------	------------------

$\frac{5.4}{16}$	↓	$\frac{4.15}{6.8}$	$\frac{3.98}{-}$	$\frac{4.27}{13.0}$	$\frac{4.4}{20}$ ✓
------------------	---	--------------------	------------------	---------------------	--------------------

$\frac{5.3}{18}$	↓	$\frac{4.2}{7.0}$	$\frac{3.98}{-}$	$\frac{4.24}{13}$	$\frac{4.4}{18}$
------------------	---	-------------------	------------------	-------------------	------------------

$\frac{5.1}{16}$	$\frac{4.90}{11}$		$\frac{4.15}{-}$	$\frac{4.40}{13.1}$	$\frac{4.0}{18}$
------------------	-------------------	--	------------------	---------------------	------------------

$\frac{4.7}{16}$	$\frac{4.90}{11}$		$\frac{4.19}{-}$	$\frac{4.24}{13}$	$\frac{4.60}{19}$
------------------	-------------------	--	------------------	-------------------	-------------------

$\frac{5.1}{16}$	$\frac{4.97}{10.9}$		$\frac{4.17}{-}$	$\frac{4.26}{13.2}$	$\frac{4.5}{19}$
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$\frac{5.0}{16}$	$\frac{4.54}{10.7}$		$\frac{4.11}{-}$	$\frac{4.26}{13.4}$	$\frac{4.4}{17}$
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$\frac{4.6}{16}$	$\frac{4.21}{10.8}$		$\frac{3.97}{-}$	$\frac{4.12}{13.2}$	$\frac{4.5}{18}$
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Nail in Arc Lt. Pole #2 Lt. Sta. 13+72

$\frac{6.2}{17}$	$\frac{5.90}{10.8}$		$\frac{5.71}{-}$	$\frac{5.75}{12.8}$	$\frac{6.2}{18}$
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$\frac{6.0}{18}$	$\frac{5.82}{11}$		$\frac{5.68}{-}$	$\frac{5.80}{13.1}$	$\frac{5.8}{19}$
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Station + H.I. - Elev.

848.99

14+75 43.40 ✓

15+00 43.39 ✓

+25 43.49 ✓

+50 43.62 ✓

+75 43.75 ✓

16+00 43.99 43.90

B.M. 4.65 848.99 4.65 844.34 ✓

+25 44.05 ✓

+50 44.14 ✓

+75 44.18 ✓

17+00 44.25 ✓

+25 44.24 ✓

+50 44.16 ✓

+75 44.02 ✓

Lt.

Q

Rt.

7

$\frac{5.9}{17}$	$\frac{5.75}{10.9}$	5.59	$\frac{5.81}{13.1}$	$\frac{6.0}{17}$
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$\frac{5.5}{17}$	$\frac{5.65}{10.7}$	5.60	$\frac{5.79}{13.2}$	$\frac{6.1}{16}$
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$\frac{5.7}{17}$	$\frac{5.58}{10.6}$	5.50	$\frac{5.65}{13.3}$	$\frac{5.70}{20}$
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$\frac{5.6}{17}$	$\frac{5.48}{10.5}$	5.37	$\frac{5.48}{13.3}$	$\frac{5.5}{19}$
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$\frac{5.4}{17}$	$\frac{5.25}{10.6}$	5.24	$\frac{5.34}{13.3}$	$\frac{5.4}{21}$
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$\frac{5.3}{17}$	$\frac{5.24}{10.8}$	5.09	$\frac{5.09}{13.2}$	$\frac{5.0}{19}$
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Spike in R.P. Lt. Sta. 16+12

$\frac{5.2}{17}$	$\frac{5.20}{10.7}$	4.94	$\frac{4.88}{13.1}$	$\frac{4.9}{20}$
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$\frac{5.3}{17}$	$\frac{5.13}{10.8}$	4.85	$\frac{4.79}{13.0}$	$\frac{4.8}{18}$
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$\frac{5.3}{18}$	$\frac{5.04}{10.9}$	4.81	$\frac{4.78}{13.0}$	$\frac{4.8}{20}$
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$\frac{5.1}{17}$	$\frac{4.94}{11.0}$	4.74	$\frac{4.78}{13.0}$	$\frac{4.5}{19}$
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$\frac{4.9}{17}$	$\frac{4.86}{11.0}$	4.75	$\frac{4.84}{13.0}$	$\frac{4.7}{18}$
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$\frac{5.2}{18}$	$\frac{4.98}{11.0}$	4.83	$\frac{4.95}{12.9}$	$\frac{5.0}{19}$
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$\frac{5.3}{18}$	$\frac{5.11}{11.2}$	4.97	$\frac{5.00}{12.9}$	$\frac{5.2}{18}$
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station	+	H.I	-	Elev.
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848.99

18	+			43.88 ✓
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	+			43.78 ✓
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	+			43.68 ✓
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	+			43.56 ✓
--	---	--	--	---------

19	+			43.49 ✓
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	+			43.45 ✓
--	---	--	--	---------

	+			43.53 ✓
--	---	--	--	---------

	+			43.74 ✓
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20	+			43.74 ✓
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	+			43.45 ✓
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	+			43.59 ✓
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	+			44.20 ✓
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Lt.

C

Rt.

8

$$\frac{5.6}{19} \quad \frac{5.30}{11.2} \quad \frac{5.11}{-} \quad \frac{5.20}{12.9} \quad \frac{5.2}{19}$$

$$\frac{6.0}{18} \quad \frac{5.43}{11} \quad \frac{5.21}{-} \quad \frac{5.34}{13.0} \quad \frac{5.6}{18}$$

$$\frac{5.7}{17} \quad \frac{5.85}{11.0} \quad \frac{5.31}{-} \quad \frac{5.44}{13.0} \quad \frac{5.7}{19}$$

$$\frac{5.7}{18} \quad \frac{5.64}{11.2} \quad \frac{5.43}{-} \quad \frac{5.66}{13} \quad \frac{5.9}{19}$$

$$\frac{6.0}{17} \quad \frac{5.60}{11.0} \quad \frac{5.50}{-} \quad \frac{5.85}{13} \quad \frac{6.1}{19}$$

$$\frac{6.1}{17} \quad \frac{5.60}{11.0} \quad \frac{5.54}{-} \quad \frac{5.95}{13} \quad \frac{5.9}{20}$$

$$\frac{6.2}{17} \quad \frac{6.00}{11.0} \quad \frac{5.44}{6.0} \quad \frac{5.46}{-} \quad \frac{5.85}{13.0} \quad \frac{5.9}{18}$$

$$\frac{5.9}{17} \quad \frac{6.30}{11.0} \quad \frac{5.42}{6.0} \quad \frac{5.25}{-} \quad \frac{5.61}{13.0} \quad \frac{5.8}{17}$$

$$\frac{6.4}{18} \quad \frac{6.30}{11.0} \quad \frac{5.46}{4.5} \quad \frac{5.25}{-} \quad \frac{5.35}{12.8} \quad \frac{5.4}{19}$$

$$\frac{6.4}{16} \quad \frac{6.20}{11} \quad \frac{5.54}{-} \quad \frac{5.30}{12.9} \quad \frac{5.50}{19}$$

$$\frac{6.2}{17} \quad \frac{6.04}{11.3} \quad \frac{5.40}{-} \quad \frac{5.05}{12.8} \quad \frac{5.3}{19}$$

$$\frac{5.8}{17} \quad \frac{5.50}{11.0} \quad \frac{4.79}{-} \quad \frac{4.80}{13.0} \quad \frac{5.1}{19}$$

station	+	H.I	-	Elev.
21+00		84899		44.45 ✓
+25				44.85 ✓
T.P.	13.22	858.31 ✓	3.90	845.09 ✓
+50				45.09 ✓
+75				45.42 ✓
22+00				46.07 ✓
+25				46.89 ✓
+50				47.85 ✓
+75				48.90 ✓
23+00				49.85 ✓
+25				50.81 ✓
+50				(51.66) 51.81
+75				52.64 ✓

Lt.

L

Rt.

9

$\frac{5.2}{17}$	$\frac{5.07}{11.0}$	$\frac{4.54}{13.2}$	$\frac{4.84}{13}$	$\frac{4.9}{18}$
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$\frac{4.6}{17}$	$\frac{4.55}{11.0}$	$\frac{4.4}{13.2}$	$\frac{4.67}{13.2}$	$\frac{4.7}{18}$
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$\frac{13.4}{18}$	$\frac{13.33}{10.7}$	$\frac{13.22}{13.4}$	$\frac{13.72}{13.4}$	$\frac{13.4}{18}$
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$\frac{13.0}{17}$	$\frac{12.85}{10.7}$	$\frac{12.89}{13.26}$	$\frac{13.26}{13.3}$	$\frac{13.3}{18}$
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$\frac{12.4}{17}$	$\frac{12.22}{10.6}$	$\frac{12.24}{13.4}$	$\frac{12.55}{13.4}$	$\frac{12.6}{19}$
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$\frac{11.22}{17}$	$\frac{11.31}{10.7}$	$\frac{11.42}{13.6}$	$\frac{11.90}{13.6}$	$\frac{12.0}{18}$
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$\frac{10.5}{17}$	$\frac{10.27}{10.5}$	$\frac{10.46}{13.6}$	$\frac{11.09}{13.6}$	$\frac{11.2}{18}$
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$\frac{10.0}{17}$	$\frac{9.25}{10.5}$	$\frac{9.41}{13.6}$	$\frac{10.05}{13.6}$	$\frac{10.2}{18}$
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$\frac{8.7}{17}$	$\frac{8.37}{10.6}$	$\frac{8.46}{13.5}$	$\frac{8.90}{13.5}$	$\frac{9.4}{19}$
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$\frac{7.5}{17}$	$\frac{7.45}{10.8}$	$\frac{7.50}{13.3}$	$\frac{7.79}{13.3}$	$\frac{8.0}{18}$
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$\frac{6.8}{19}$	$\frac{6.62}{11.0}$	$\frac{6.50}{13.2}$	$\frac{6.65}{13.2}$	$\frac{6.9}{18}$
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$\frac{5.7}{18}$	$\frac{5.83}{11.1}$	$\frac{5.67}{12.9}$	$\frac{5.74}{12.9}$	$\frac{5.8}{17}$
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station	+	H.I	-	Elev.
24+00		858.31		53.56 ✓
+25				54.49 ✓
+50				55.41 ✓
+75				56.32 ✓
25+00				57.20 ✓
	10.75	868.24 ✓	0.82	857.49 ✓
+25				58.13 ✓
+50				59.18 ✓
+70				60.24 ✓
26+00				61.20 ✓
+20				61.96 ✓
+32				62.36 ✓
+50	= construction joint			63.04 ✓
B.M			640	861.84 = 617.8

check levels next page.

Lt.

Q

Rt.

10

$\frac{5.1}{17}$	$\frac{4.91}{11.2}$	$\frac{4.75}{}$	$\frac{4.84}{13.0}$	$\frac{4.7}{19}$
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$\frac{3.9}{18}$	$\frac{3.88}{11}$	$\frac{3.82}{}$	$\frac{3.97}{12.9}$	$\frac{4.0}{17}$
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$\frac{3.1}{19}$	$\frac{2.95}{11.5}$	$\frac{2.90}{}$	$\frac{3.05}{12.7}$	$\frac{3.1}{18}$
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$\frac{2.1}{18}$	$\frac{2.09}{11.5}$	$\frac{1.99}{}$	$\frac{2.05}{12.6}$	$\frac{2.1}{18}$
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$\frac{1.0}{17}$	$\frac{1.22}{11.5}$	$\frac{1.11}{}$	$\frac{1.25}{12.3}$	$\frac{1.2}{18}$
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$\frac{10.4}{17}$	$\frac{10.18}{11.6}$	$\frac{10.11}{}$	$\frac{10.25}{12.6}$	$\frac{10.2}{20}$
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$\frac{9.4}{17}$	$\frac{9.18}{11.7}$	$\frac{9.06}{}$	$\frac{9.15}{12.4}$	$\frac{9.2}{18}$
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$\frac{8.3}{17}$	$\frac{8.08}{11.8}$	$\frac{8.00}{}$	$\frac{8.16}{12.4}$	$\frac{7.9}{18}$
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$\frac{7.2}{16}$	$\frac{7.10}{12.0}$	$\frac{7.04}{}$	$\frac{7.24}{12.1}$	$\frac{6.9}{19}$
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$\frac{6.0}{19}$	$\frac{6.35}{12.0}$	$\frac{6.28}{}$	$\frac{6.30}{12.2}$	$\frac{6.1}{20}$
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$\frac{5.6}{21}$	$\frac{6.01}{12}$	$\frac{5.88}{}$	$\frac{5.95}{12.0}$	$\frac{5.8}{22}$
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5.20

R.R. Exp. to Acc. Lt. Pole Lt. Sta 25+91

	+	H.I.	-	Elev.
B.M.	6.40	868.24		861.84
T.P.	0.54	858.03	10.75	857.49
✓	3.87	848.96	12.94	845.09
B.M.	4.62	848.96	4.62	844.34
T.P.	6.69	849.62	6.03	842.93
✓	9.69	858.32	0.99	848.63
✓	9.20	866.90	0.62	857.70
B.M.			1.65	865.25 = 65.23

R.R. Spike in Arc. Lt. Pole Lt. Sta. 25791

Spike in P.P. Lt. Sta. 16712

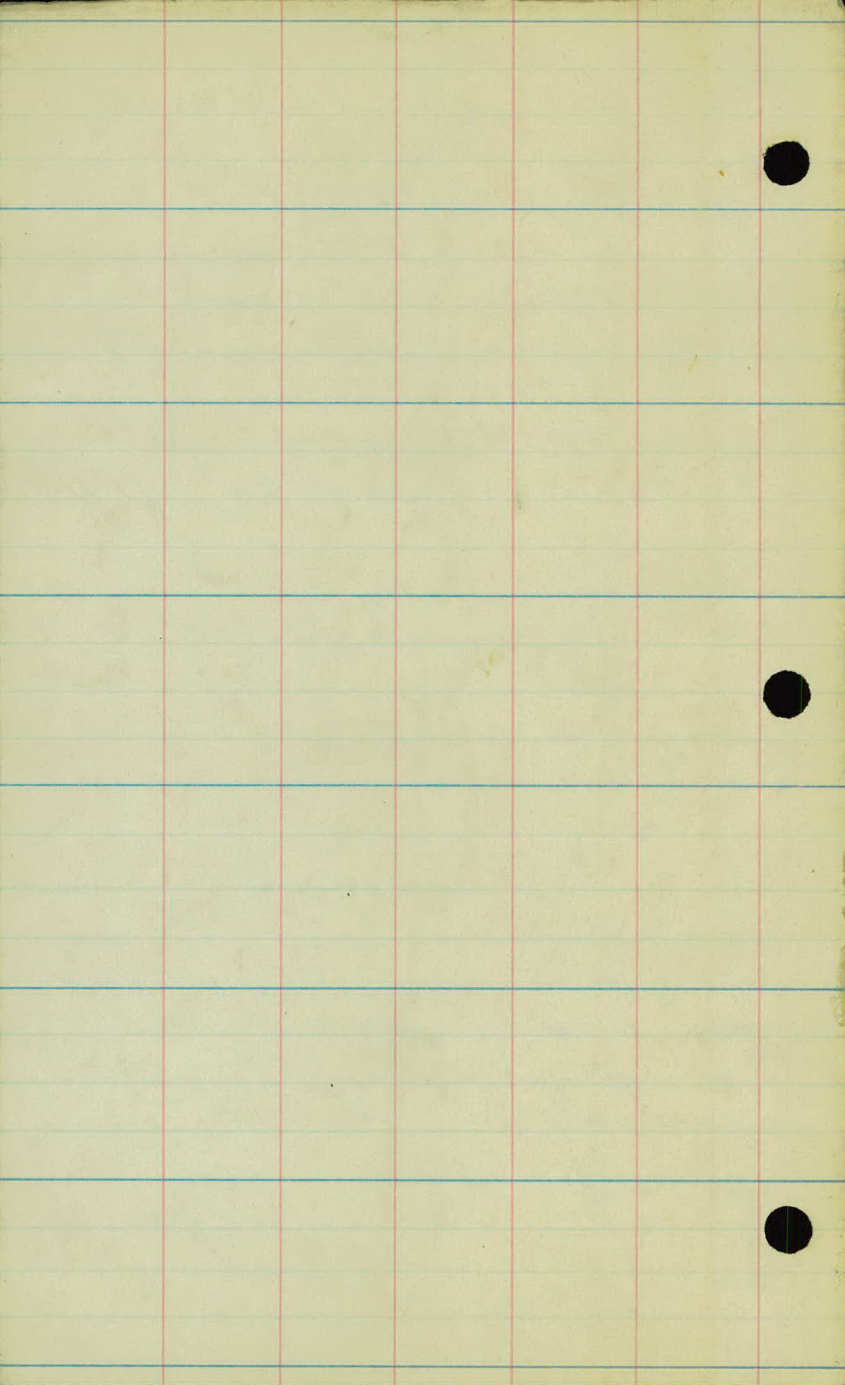
Spike Arc. Lt. Pole (Larp + Rice St) Lt. Sta. 0730

W.H.C.

A.L.P.

M. G. 3-30-26

H. B.



1 /

U2484