

PLANS SURVEY
UPPERAFTON ROAD

From Burn's Ave.

To East Co. Line

CO. PROJ. N^o 24-56

RD^o/_c N^o 70

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 2-21-24

File No. 11

Project 24-56

Upper Afton Road

Transit Notes

Sta 0+00 - 98+86.9

6 - Pages.

R. B. Austin

W. H. Keoghan

W. Maloney

M. Galvin

} Party

Nov-1923

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed **2-21-24**

File No. **"11"**

**Upper Afton Road
From City Limits West
Co. Proj. 24-56**

West

13+092 Mont 1/4 1/4 cor.

7+33.85 P.O.T.

West

0+00 Mont. City limits

7. P. 5/35
40.35 @ 16"

43.58
6"
42.42 @ Maple 30"
Ment Down 3'
42.25 @ 6" Film.

E
Ang. ht. Ang. Rt.

35+97.45 P.O.T.

N63°26'W

33+42.47 ✓ F.C.

31+56.3 P.I.

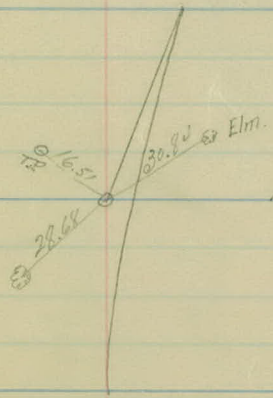
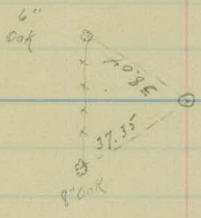
26°34'

29+62.95 B.C. ✓

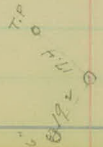
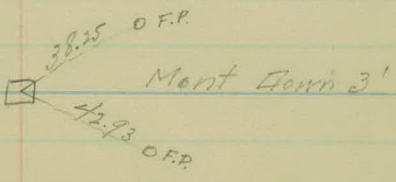
West

26+19.40 Mont. Cen. Sec. 2.

21+00 P.O.T.



7° Curve R.H.
 $\Delta = 26^{\circ} 34'$
 $T = 193.35$ ✓
 $Length = 319.52$ ✓



Ang. ht ⁴ Ang. Pt.

S89°23'W.

54+10.02 ✓ F.C.

51+13.16 P.I 30°26'

48+00.3 = 48+01.36 ✓ B.C. Equation Short Sta.

47+18.90 P.O.T.

N60°11'W.

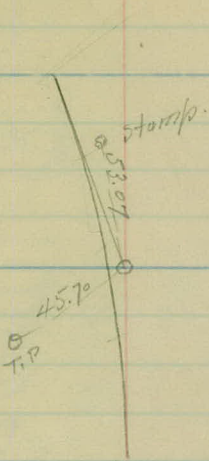
44+06.24 ✓ F.C.

43+25° P.I

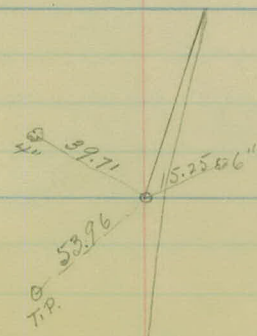
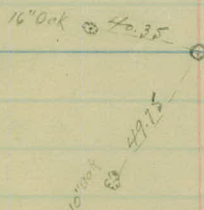
30°15'

42+43.74 ✓ B.C.

Sta. Elev.
 48+01.36-0000'
 49+00-2028'
 +50-3043'⊙
 50+00-4058'
 51+00-7028'⊙
 52+00-9058'
 53+00-12028'
 54+00-14058'
 +10.02-15013'



5° Curve Rt.
 $\Delta = 30^{\circ}26'$
 $T = 311.80$ ✓
 length 608.66 ✓



2° Curve Rt.
 $\Delta = 3^{\circ}15'$
 $T = 81.26$ ✓
 length 162.50 ✓

Anght. Anght.

N63°43'W

77+78.84 ✓ F.C.

76+84.68 P.I. 19°02'

75+88.51 ✓ B.C.

70+144.38 P.O.T

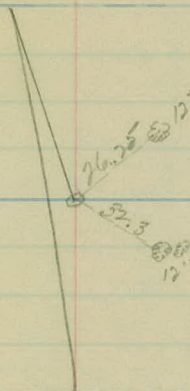
N.44°41'W.

68+116.24 ✓ F.C.

62+75.07 P.I

45°56'

56+67.91 ✓ B.C.

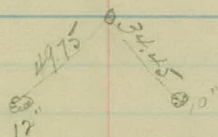


10° Curve Lt.

$\Delta = 19002$

$T = 96.17$ ✓

length = 190.33 ✓



B.C. 56+67.91 - 0°00'

59+25 - 5°06½'

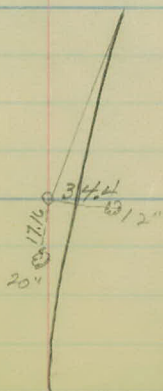
+75 - 6°08½'

62+00 - 10°38½'

+85 - 12°20½'

64+50 - 15°38½'

F.S. 68+16.24 - 22°58'



4° Curve Rt.

$\Delta = 45056$

$T = 607.16$ ✓

length = 1148.33 ✓

Height. ~~E~~ Ang. Pt.

N83°43'W

91+19.71 [✓] E.C.

90+13.25 P.I. 15°00'

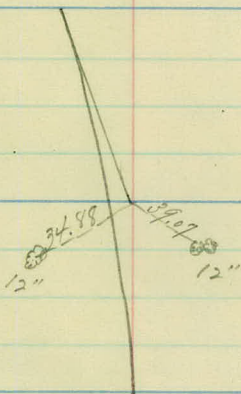
89+105.43 [✓] B.C.

N68°43'W.

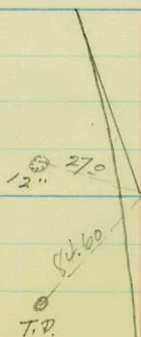
84+96.29 [✓] E.C.

84+13.02 P.I. 5°00'

83+29.63 [✓] B.C.



7° Curve ht.
 $\Delta = 15^{\circ}00'$
Tang = 107.82 ✓
Length = 214.28 ✓



3° Curve ht.
 $\Delta = 5^{\circ}00'$
Tang 83.39 ✓
Length 166.66 ✓

Flag. ht. Flag. Rt.

98+869 ✓ E.C.

S. 89° 35' W.

98+114.4 P.I. 45° 00'

97+31.7 ✓ B.C.

96+62.39 P.I.

83° 20'

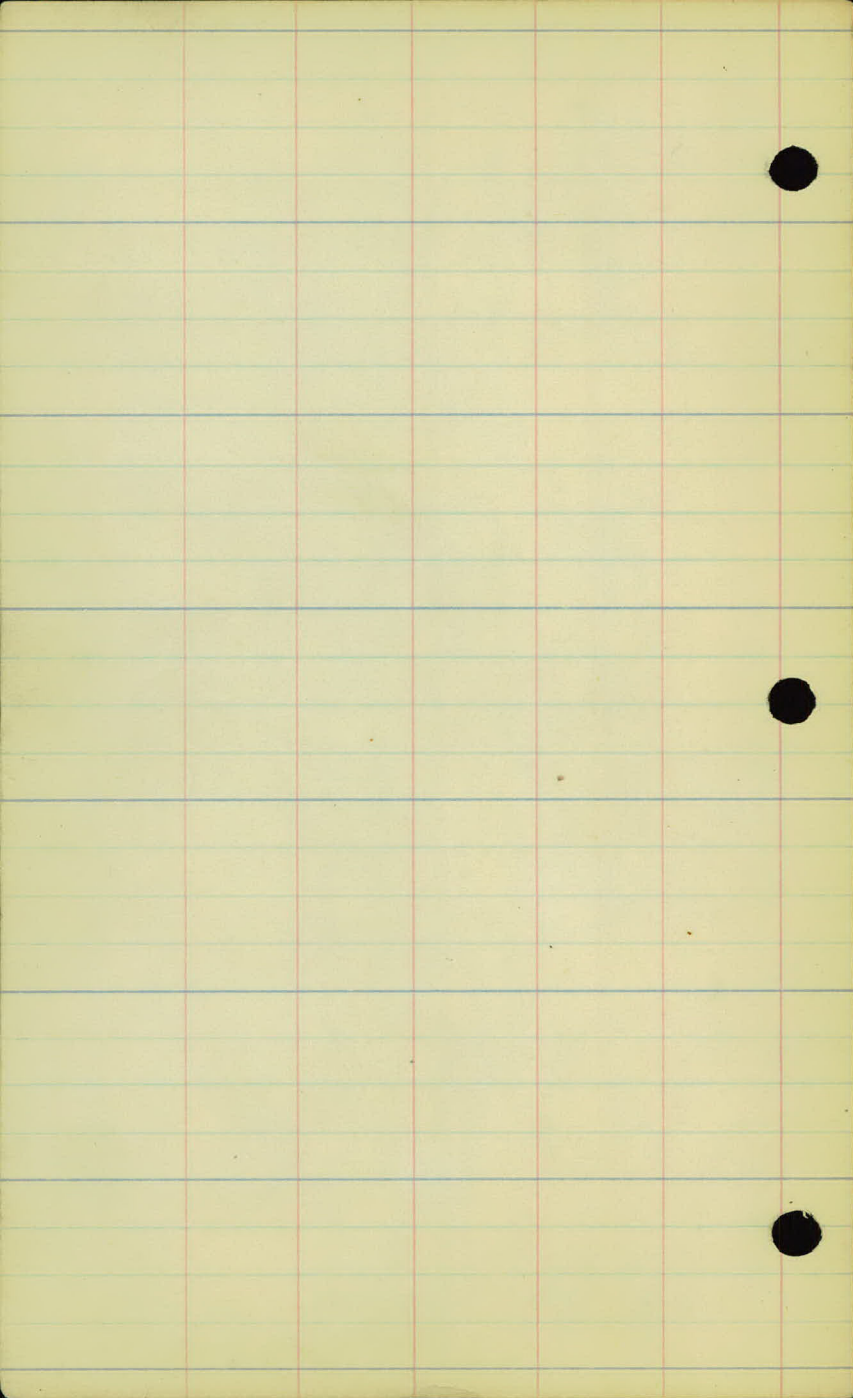
N. 75° 25' W.

95+99.6 ✓ E.C.

94+68.5 P.I.

38° 18'

93+26.2 ✓ B.C.



Project

Upper Afton Road.

Line change Sta. 56+84.9 to 68+64=

Transit Notes

1-Page.

11-23-23

R. E. Austin }
L. N. S. Keoghan } Party
W. Maloney }
M. Galvin }

±
Ang. ht. Ang. Ft.

68+64.5 ✓ E.C. = 68+82.9 on City's line

67+41.7 P.I. 19°52'

66+16.17 ✓ B.C.

65+00.35 P.O.T.

N64°34'W.

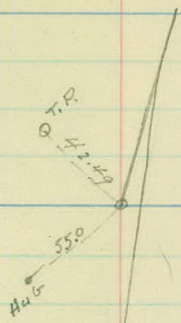
62+63.1 P.O.T.

60+10.5 ↓ E.C.

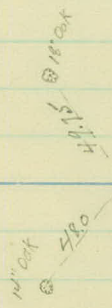
58+50.70 P.I. 26°03'

56+84.9 ↓ B.C.

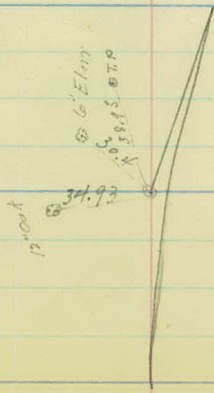
Sta. - Elev.
 66+16.17 - 0°00'
 +50 - 10°21'
 67+00 - 3°21'
 +50 - 5°21'
 68+00 - 7°21'
 +64.5 - 9°56'



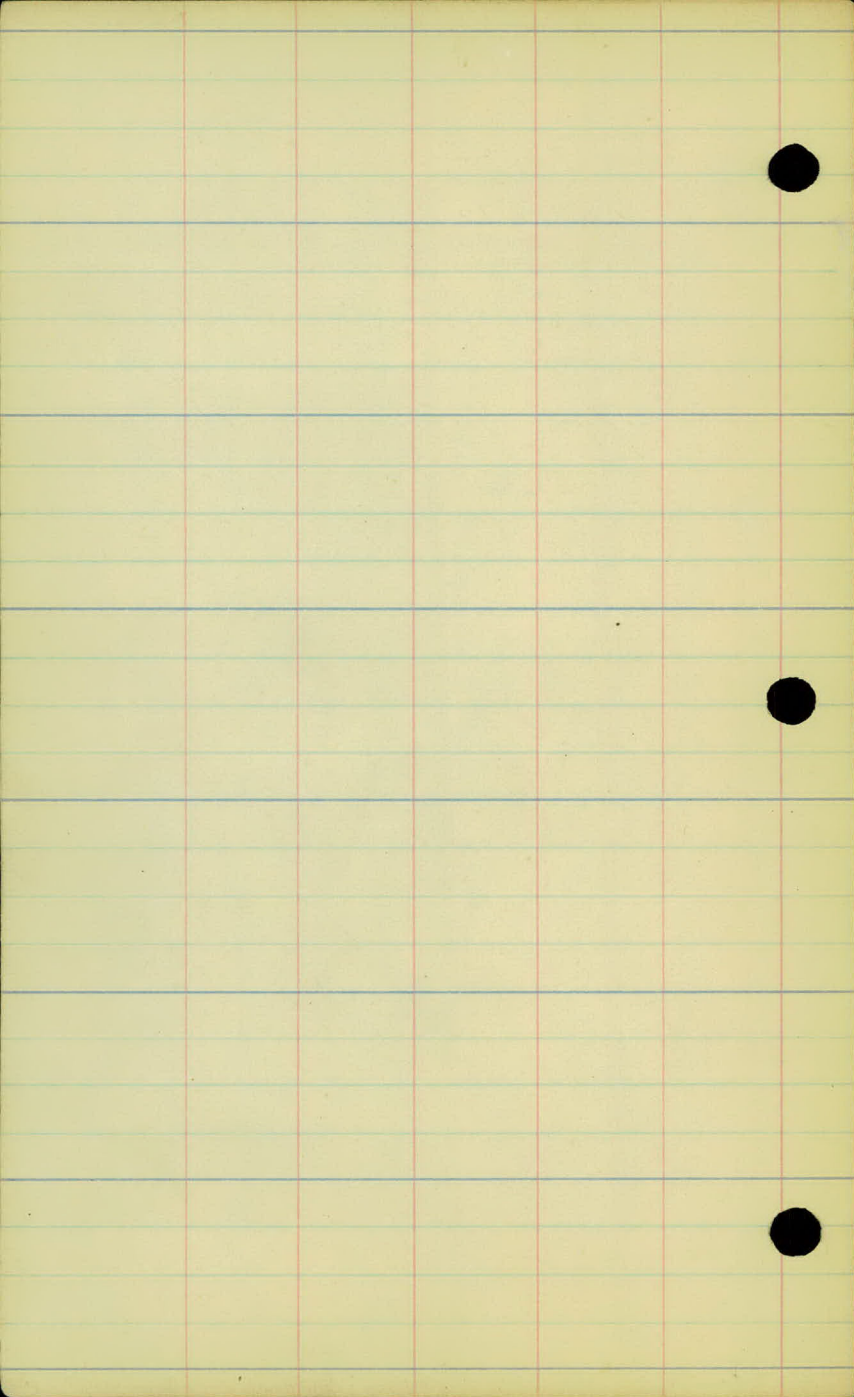
80 Curve RT.
 $\Delta = 19°52'$
 S.T. = 125.53 ✓
 B.C. = 66+16.17
 length = 248.33 ✓
 E.C. 68+64.5



Sta - Elev.
 56+84.9 - 0°00'
 57+00 - 0°36'
 +50 - 2°36'
 58+00 - 4°36'
 +50 - 6°36'
 59+00 - 8°36'
 +50 - 10°36'
 60+00 - 12°36'
 +10.5 - 13°01 1/2'



80 Curve RT.
 $\Delta = 26°03'$
 S.T. = 165.81 ✓
 B.C. = 56+84.9
 length = 325.6 ✓
 E.C. = 60+10.5



Project 24-56

= Topography. =

Sta. 0+00 - 98+86.9

16 Pages.

11-26-23

Cloudy - cold,

0+00 - 69+00

{ Corley
Maloney
Skogglan
Galvin,

69+00 - 98+86.9

{ Austin
Skogglan
Maloney
Galvin.

12-7-23

Sta

old rd.
RT

old rd
LT

5

E

4

E

3

02'

2

03'

1

04'

0+00

0.0

L+ E RT

5+89 2 small trees
32'

5+27-P.R. 27'

Fence 39'

4+55-P.P. 15'

Fence 38'

3+94 Group small trees

3+79 P.R. -23'

3+56 tree -37'

3+47 tree -36'

3+28 6" tree -29'

3+10 fence -32'

2+92 -P.R. 16'

2+90 -1 tree 34'

1 tree 29'

2+45-P.R. -28'

2+24 -12" tree 24'

Fence 31'

1+64-P.R. -16'

1+07-P.P. 28'

0+98-12" tree 17'

0+43-P.P. 16'

0+23 fence cot.
29' H

0+00

Intersection
Private road

Fence 38'

4+18-6" oak -32'

Fence 34'

3+93-10" tree 38'

3+87 tree 31'

3+45-6" tree 26'

3+33-6" tree 27'

3+09-4" tree -27'

3+10 fence -35'

3+02-8" tree -27'

3+00-36" tree 16'

2+81-6" tree 27'

2+66-6" tree 27'

2+27-6" tree 27'

End of row of trees

2+31-32' H

Fence 30'

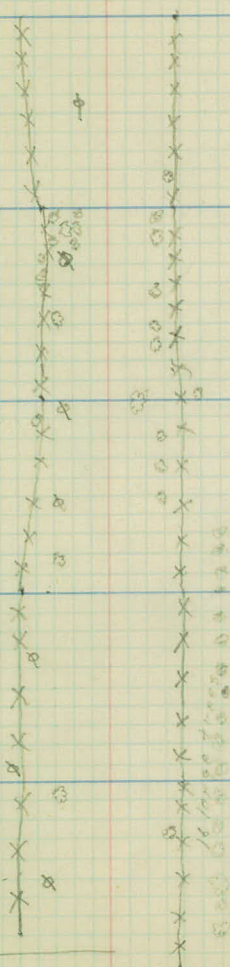
0+75-8" tree 25'

Fence 32' RT

0+21 begins

row of trees

37' RT



sta

old rd.
RT

old rd.
LT

11

05'

10

02

9

£

8

£

7

£

6

£

Lt ~~±~~ Rt

Fence 26'

10+66-T.P. 26'
10+65-P.P. 12'

Fence 25'

9+20-T.P. 26'
9+12-P.P. 12'
Fence 26'

Fence 27'

7+84-T.P. 27'
7+61-P.P. 13'

Fence 28'

6+53 bop. fence 28'
6+50 38' RT
End of fence
Large tree.
6+08, P.P. - 14'
Fence - 37'

Light clearing
10
11
12
13
14
15
16
17
18
19
20

Fence 31'
10+95 Twin 20 K
24" - 22'

10+11-24" + 105 32'
Fence 34'

Fence 31'

Fence 31'

Fence 31'

Fence - 34'

Woods large trees



5th

old wd.
RT

old
wd LT

17

10'

16

08'

15

06'

14

04'

13

E

12

02'

LT Rt

17+52-T.P.-26'

x



17+08 field ent
fence 35'

Fence - 24'

16+85-36" oak-20'

16+57-T.P.-11'
16+56 T.P.-26'

Brush
Brush



Fence 26'

Fence 24'

15+04-P.P.-12'
Fence 27'

15+47-24" oak 24'

Fence 24'

14+79-T.P.-26'

Brush

Fence 25'

Fence - 34'

13+54-P.P.-11'

13+40-T.P.-25'

B

fence 27'

Fence 34'

12+15-P.P. 12'

12+11-Fence cor
T.P.-12+07-26'



Brush

Woods

11+92 private
ent

Ent fence 11+75



sta

old-d.
Rt

old-d.
Lt

23

03'

22

09'

21

07'

20

09'

19

10'

18

09'

LT # RT

Fence 25'

22+95 T.P. - 26'
22+69 P.P. - 12'

22+19-5" tree 07'
22+14-7" tree 07'
Fence 23'

21+74-3-6" trees 30'
21+61-T.P. 24'
21+56-10" tree 20'

21+33-tree
21+13-P.P. 12'
21+05-6" tree 20'
Fence - 22'

20+87-6" tree 16'
20+82-7" tree 05'
20+61-10" tree 21'
20+55-Twin tree 23'
20+47-10" tree 24'
20+38-10" tree 23'
20+28-10" tree 22'
20+25-T.P. 26'

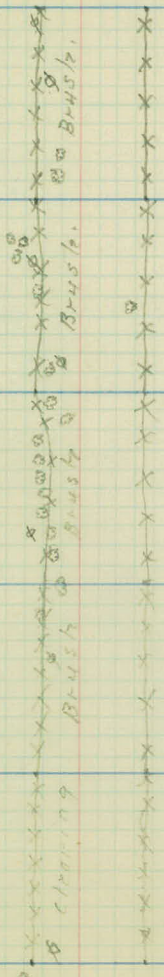
20+13-12" oak 14'
Fence 21'
20+00-12" oak 14'
19+86-12" tree 20'

19+60-P.P. 12'

Fence 22'

18+08-P.P. 11'
Fence 23'
18+00-7" tree 17'

17+90 T.P. 32'



Fence 35'

21+47-Tree-21'

Fence - 35'

Fence 35'

Fence 30'

Fence 35'

Sta

old rd.
R+

old rd.
L+

29

04'

28

07'

27

11'

26

09'

25

06'

24

02'

Lt E Rt

29+83 T.P. 26' x

Fence 26

Fence 34'

28+69 R.P. -11

28+44 T.P. 26'

Fence 26'

28+69 X Fence

Fence 34'

27+90 Branch of tree 24'

Farm Yard

27+17 R.P. -11'

27+07 T.P. 27'

Fence 26

27+15 Box fence 35'

27+07 priv. east fence

26+54 Farm east

XXXXX

26+51 priv. east

End fence 26+36 -35'

Fence 27

Fence 34'

25+73 T.P. -26'

25+65 R.P. -12'

25+27 Field east

Fence 28'

XXXXX

Fence 34'

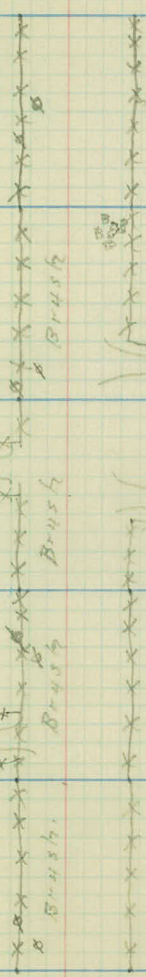
24+27 R.P. -26'

24+13 R.P. -11

Fence 27'

Fence 34'

23+97 -16" tree 22'



5th

old rd.
R+

old rd.
L+

35

05'

34

02'

33

02'

32

12'

31

10'

30

01'

Lt E Pt

Fence 27'

34+64 P.P. 11'
34+52 T.P. 33'

Fence 26'

33+21 Fence 26'
33+06 Cattle drive

31+61 P.P. 31'

31+50 fence 49'

30+02 T.P. 31'
30+99 tree 36'

30+50 fence 30'

30+21 P.P. 14'
Fence 26'



34+62 Priv. Drive
34+40 End fence 19'

Fence 22'

33+71 Cattle drive

33+24 8" tree 18'
33+21 6" tree 16'
33+17 8" tree 16'
Fence 18'

32+73 8" tree 13'

32+50 fence 12"

32+31 7" tree 07'

Fence 05'

31+71 10" tree 02'
31+61 fence 03'
31+50 fence 8'

Fence 19'

30+50 fence 22'

Fence 30'

540

old and old and
R+ H

41

±

40

03'

39

06'

38

08'

Sta 35+75 To sta

Rubble stone ditch 3' wide

37

10'

36

10'

L+ E R+

41+37 P.P. 13'

41+47 25 small trees 19'

Fence 44'

40+89 End fence 55'
40+85-8" tree 21'

Fence - 37'
39+98 P.P. - 13'
39+94-8" tree 25'

40+39 13-9 fence 58'

39+56 10" tree 28'

Fence 33'

39+88 Triple oak - 39'
39+00 End clearing

38+68 P.P. - 09'
38+51-8" tree 30'
38+17 Bay clearing 25' tree
Fence 34'

37+32 P.P. - 03'

37+57 Bay high clearing

Fence = 36'

36+00 A.P. - 03'
Fence 25'
35+96-8" tree 15'

35+72-8" tree 27'

39+00
39+05
39+10
39+15
39+20
39+25
39+30
39+35
39+40
39+45
39+50
39+55
39+60
39+65
39+70
39+75
39+80
39+85
39+90
39+95
40+00



Sta

old rd
R⁺

old rd
L⁺

47

35'

46

16'

45

04'

44

14'

43

10'

42

04'

|||

LT R

47+60 - P.P. - 27'

Fence ends +03
Fence -05

46+79 fence X lime

46+43 P.P. - 12'

End G.R. - 45+10
Guard rail 9'

44+84 - 8' tree 25'

44+13 - 18' tree 10'
Guard rail 15'

43+70 - Box G.P.P.

Fence 113'

42+67 wood culvert
8x6"

41+90 T.P. - 18'

41+60 priv. ent

46+63 - 8" oak 07'
46+55 -

46+29 - 14" oak 21'

46+00 bog fence 16'

45+93 - Clearing 08'

45+51 Clearing - 19'

45+23 - P.P. - 12'
End Guard 45+10
Guard rail 16'

44+79 - 8" tree 25'

44+12 - P.P. 28'
Guard Rail 25'

43+82 Bog G.P.P. 24'

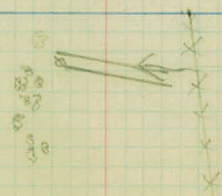
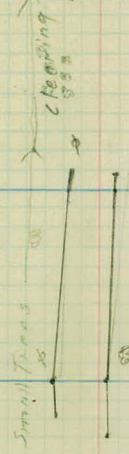
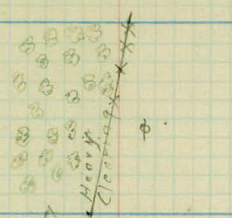
42+80 - 10" tree
42+76 - P.P. 21'
42+62 - 8" tree 30'

42+45 - 10" tree 38'

42+25 - 3" tree 22'

41+65 - 10" tree 22'

41+60 priv. ent



sta

Lt

Rt

53

03'

52

08'

51

109'

50

109'

49

48

53+74 - P.P. 17'

53+00 Beg Light
clearing bench on
Rt out 20' - 15' wide

52+45 P.P. - 09'

51+65 - 4s. Tr. 00520

51+12 - P.P. - 05'

50+79 - 10' willow 12'
50+71 - 6" tree 16'

End Fence 11'

49+83 - 24" oak 05'
49+76 - 12" oak 11'
49+62 - 14" oak 09'

49+33 - 14" oak 10'

49+11 - Reg fence 10'

49+89 - P.P. E

49+47 Fannert.

48+78 P.P. - 12'
48+75 End G.R. 14'

Stone Box Culvert 48+11

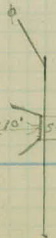
47+64 Beg G.R. 30'



Light 14K1



Deep Trench
120' x 120'



55

old rd
L+

old rd
R+

59

35'

+30

22'

58

11'

57

±

56

±

55

±

54

±

H # RL

Fence 06'
58+83 - P.P. 43'
Fence X line + 84

58+81.7" tree + 1
+ 50 Fence 06'

58+38.12" tree - 09'
58+02.7" tree 13
Fence 13'

57+70.14" tree 31'
57+65 - P.P. 20

57+92.2" tree - 19'
57+83.9" tree - 17'
57+69.12" tree 16'

57+31.12" tree 31
Fence 33'

57+32.26" tree 26'
57+27.14" tree 27
57+18.14" tree 27
Fence 23'

56+50 Bag clearing brush
17' x 14' 10" wide
56+29 - P.P. - 12'
56+04.9" tree 29'
Fence 34'

56+51.6" oak 24'
56+34.12" oak 25'
Fence 28'

55+04 - P.P. - 13'
Fence 32'

55+52.12" tree 28'

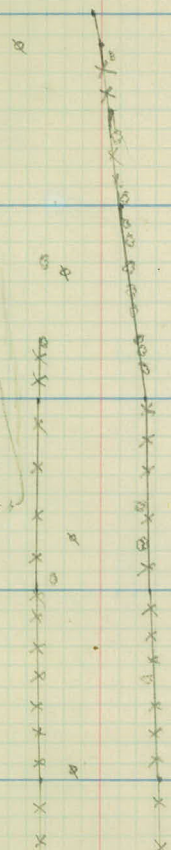
Fence 32'

54+51 - Fence 32'
54+41 - Tree

X X X X X

54+51 - Fence for 32

End of brush



Sta.

old rd
E

old rd.
R

65

54'

64

10'

63

38'

62

60'

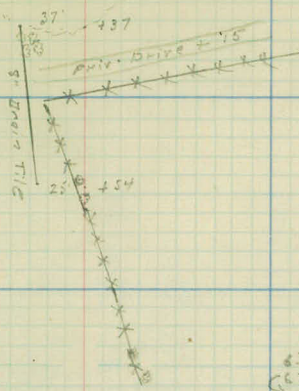
61

E

60

52'

24
Swamp



65+25 3 trees 24'
 Fence X Line +07
 64+98 Fence Cor
 64+56-6" tree 4'
 64+42-6" tree 4'
 Fence X line +91

Fence 17'

63+63-12" tree 28'
 63+57-8" tree 33'
 Fence 33'

63+33-9" tree 33'
 63+16-12" tree 32'
 63+06-12" tree 25'

62+87-12" tree 04'
 62+72-12" tree 30'
 62+62-14" tree 13'
 62+53-22" tree 26'
 62+39-6" tree 24'
 62+28-10" tree 16'
 62+14-8" tree 15'

62+97-PP. 09

62+65-14" tree 06'

61+98-2 trees 20-30'
 61+78-15" tree 27'
 61+55 Fence X line

61+25 Div. Drive
 61+08-PP-12'
 Fence 26'

Fence 41'

Fence X Line +33

Fence 14'

59+83-12" tree 01'
 59+71-8" tree 10'
 59+71 Fence 19'

60+66-6" tree 18'
 60+57-12" tree 16'
 60+53-14" tree 20'
 60+30-14" tree 28'
 60+20-8" tree 05'
 59+97-12" tree 30'
 59+93-12" tree 24'
 59+87-12" tree 23'

59+43 twin oak 18'

59+19-12" tree 09'



370

old rd
4'

old
rd off

71

±

70

±

69

7'

$69 + 64.5 = 68 + 92.9$

68

18'

67

48'

66

77'

+92 Trace 40'
+72 Trace 34'
+56 Trace 83'
+44 Trace 87'
+11 T.P. 25' L

+71 E.P. 19' A

+92 T.P. 82' L

+52 E Drive
+41 End Fence
+26 E.P. 21' L

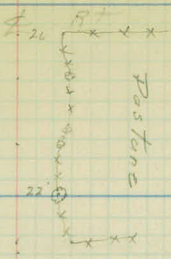
- 68+29-T.P. -37'

Fence X line +23
Fence 89'

66+50 Start Fence
26'

Cult. Field

Drive



+32 Drive

59' 100

43'

37'

46

124

+67 Trace 28'

+85 Trace 27'
+55 Trace 24'

+00 Trace Fence 71400

+77 Beg. Fence

+17 Trace 21' R
+14 Trace 31' R

70400

+86 Trace 20' R
+83 Trace 19' R

+67 Trace 15' R

+49 Trace 19' R

+25 Trace 19' R

69400

Fence 18'

67+50 Fence 08'

Ob. Rd & Oh. Rd.

left. Right.

78

L

77

76

L

75

L

74

L

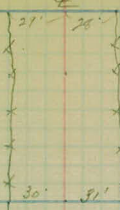
73

L

72

L

+69 Tree 27' R



78+00

+95 T.P. 28' L
+80 E.P. 19' L

+95 Tree 31'

Meadow



77+00

+66 T.P. 22'
+48 E.P. 13' L

+04 Drive

+80 Tree 24'

+69 Tree 38'



76+00

+35 1x1x1 Box, Coker
+27 T.P. 22'
+00 E.P. 16' L

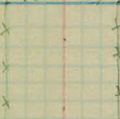
Meadow hand



Pasture

+84 Tree 23'

+47 T.P. 30' R

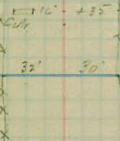


75+00

+59
+42 Road

+158

+60 T.P. 39'



74+00

+113 T.P. 24' L

+85 T.P. 24' R

+54 E.P. 10' L



+23 T.P. 35' L

+03 H6 Tree 32'

+15 Private Drive ?

73+00

+90 T.P. 31'

Pasture

+52 T.P. 25' L

+19 T.P. 30' L

+14 T.P. 38' L

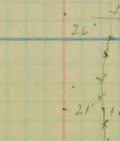
+11 E.P. 11' L



+21 +157

Calif. Field

72+00



85+00

±

84+00

±

83+00

±

82+00

±

81+00

±

80+00

±

79+00

±

Old Road
Left

Old Road
Right

92+00

4

91+00

±

90+00

±

89+00

±

88+00

±

87+00

±

86+00

±

+171 E.P. 18' L
+51 Tree 17' L

92+00

Field

Postage

91+00

+35 E.P. 13' L

+128 End Fence

24' - 19'

+40 Tree 19' R

+27 Beg. Fence

90+00

+99 Tree 25'

+75 Tr. 26' L

+57 Tr. 28' L

Field

+92 Tree 35' R

+82 Tree 34'

+59 Tree 30' R

+51 Tree 26' R

89+00

+15 Tree 26' L

+96 E.P. 14' L

+83 Tree 27' L

29'

+65 Tree 26' R

+41 Tree 29' L

Field

+34 L +10 End. Fence

88+00

+52 E.P. 15' L
+45 Tree 24' L

31' +62 End Fence

+38 Drive

+19 End Fence

23'

87+00

+19 Tree 25' L
+60 Tree 23'

Cult. Field

+72 Tree 26' L
+60 Tr. 27'
+51 Tr. 27'
+39 Tr. 27'
+29 Tr. 27'
+18 Tree 27' L
+13 E.P. 15' R
+09 Tr. 27'

24'

30'

86+00

old Rd $\frac{1}{2}$ old Rd
left. Right

+869 57nd. Project
99+00

+25

$\frac{1}{2}$

+50

75'

+37

78'

96+00

88'

+50

72'

95+00

43

+50

20'

94+00

9'

93+00

3'

92+00

+78 E.P. 21' R

+05 T.P. 7' L

98+00

+75 So. Line Burns Hk

45+75
15' x 15' x 74' Box Cdv
18' x 18' x 74' Box Cdv

+31 E.P. 25' L

+32 50' +29 Fence Cdn 213' R

91+00

+97 Fence Xing +95 To 114' R
+82 To 38' R

+69 To 18' R

+38 To 32' R

+37 E.P. 98' L

52 +50
55 +37

96+00

+09 Tacc 2' L

65'

+59 Tacc 39' L

46'

+57 Tacc 22' L
+50 E.P. 87' L

95+00

+14 Tacc 4' L

22'

+90 Tacc 37' R

+45 E.P. 32' L

+50'

Fence Xing

94+00

+14 E.P. 13' L

20'
20'
20'

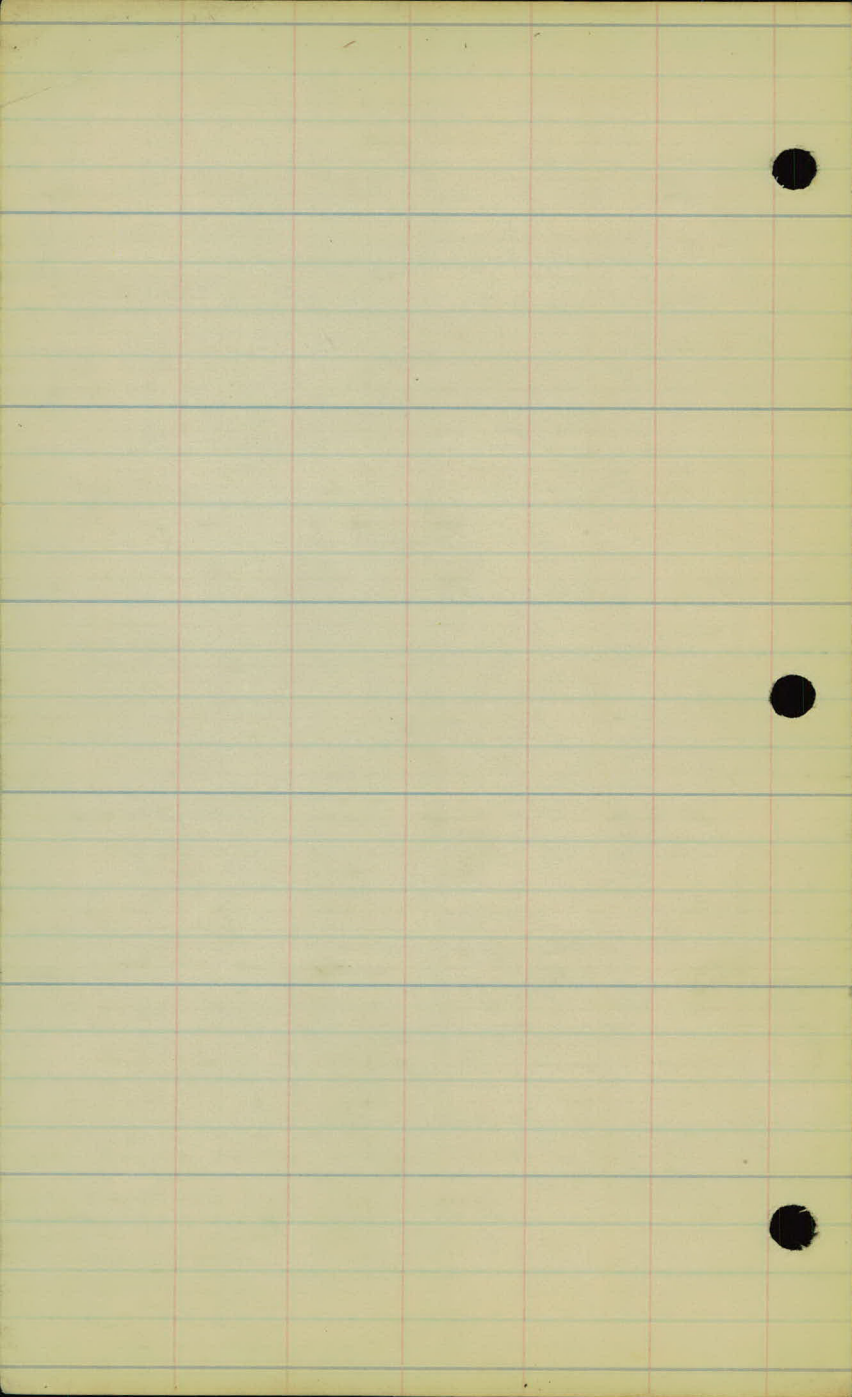
Post Fence

93+00

Field

92+00

20'



Project 24-56

Upper Atton Road.

Levels Sta. 0+00 - 50+00.

B. M. Check levels 50+00 - 98+86.9

11 - Pages

R. E. Austin }
D. N. S. Keoghan } Party
W. Maloney }
M. Galvin }

①

Station.	+	H.I	-	Red.	Elev.
B.M.	10.02	227.49			217.47
0 + 00				7.4	220.1
+ 50				7.1	220.4
1 + 00				6.0	221.5
+ 50				4.4	223.1
2 + 00				2.8	224.7
+ 50				0.2	227.3
T.P.	11.35	238.71	0.13	227.36	
3 + 00				9.4	229.3
+ 50				7.0	231.7
4 + 00				4.2	234.5
+ 50				1.6	237.1
T.P.	10.92	249.13	0.50	239.21	
5 + 00				9.2	239.9
+ 50				6.3	242.8
6 + 00				4.6	244.5

11-20-23.

① of 11

49.17
2.97
\$52.14

Spike 36" Maple. 30 Rt. Sta 0420

Station	+	HI 249.13	-	Rod.	Elev.
6	+50			3.1	246.0
7	+00			3.2	245.9
	+50			3.9	245.2
8	+00			5.0	244.1
	+50			6.0	243.0
9	+00			6.8	242.3
	T.P.	4.07	246.34	6.96	242.27
	+50			4.8	241.5
10	+00			5.7	240.6
	+50			6.0	240.3
11	+00			6.0	240.3
	+50			5.2	241.1
12	+00			4.7	241.6
	+50			4.5	241.8
13	+00			4.6	241.7

Station	+	H.I.	-	Rod.	Elev.
		246.34			
B.M.				4.31	242.03
13 + 50				4.8	241.5
14 + 00				5.5	240.8
+ 50				5.9	240.4
15 + 00				6.5	239.8
+ 50				6.9	239.4
T.P.	5.42	245.09	6.67	239.67	
16 + 00				5.8	239.3
+ 50				5.9	239.2
17 + 00				5.9	239.2
+ 50				5.9	239.2
18 + 00				5.6	239.5
+ 50				5.2	239.9
19 + 00				4.9	240.2
+ 50				4.8	240.3

45.09
530
3975

1/4 Con Mont. 13+09.7

Station	+	H.I.	-	Rod.	Elev.
		245.09			
20+00				5.1	240.0
+50				5.5	239.6
21+00				6.7	238.4
+50				8.7	236.4
22+00				10.8	234.3
T.P.	0.42	234.76	10.75	234.34	
+50				3.8	231.0
23+00				7.5	227.3
+50				11.7	223.1
T.P.	0.35	223.02	12.09	222.67	
24+00				3.7	219.3
+50				7.3	215.7
25+00				10.9	212.1
T.P.	1.04	211.71	12.35	210.67	
+40				2.3	209.4
+50				2.8	209.9

Station	+	H.I.	-	Rod.	Elev.
		211.71			
26 + 00				5.4	206.3
+ 50				8.6	203.1
27 + 00				10.7	201.0
B.M.	0.07	202.67	9.11	202.60	
+ 50				3.1	199.6
28 + 00				4.0	198.7
+ 50				5.1	197.6
29 + 00				5.8	196.9
+ 62.95	B.C.			6.5	196.2
30 + 57.83				6.9	195.8
31 + 52.71				7.5	195.2
T.P.	8.87	205.09	6.45	196.22	
32 + 47.59				7.5	197.6
33 + 42.47	E.C.			5.2	199.9
34 + 00				4.2	200.9
+ 50				3.1	202.0

T.P. left sta 27+15

Station	+	H.I.	-	Rod.	5/er.
35 + 00		205.09		2.2	202.9
+ 50				2.4	202.7
36 + 00				3.2	201.9
+ 50				5.4	199.7
T.P.	0.41	200.10	5.40		199.69
37 + 00				3.1	197.0
B.M.				2.41	197.69
+ 50				6.2	193.9
38 + 00				9.9	190.2
T.P.	0.31	187.91	12.50		187.60
+ 50				1.6	186.3
39 + 00				5.6	182.3
+ 50				9.7	178.2
B.M.				10.37	177.54
T.P.	0.22	175.77	12.36		175.55
40 + 00				1.5	174.3
+ 50				5.6	170.2

Nail in T.P. left Sta. 37+30

Station	+	H.I	-	Rod	Elev.
		175.77			
41+00				9.5	166.3
T.P.	1.09	163.97	12.89	162.88	
+50				1.9	162.1
42+00				5.7	158.3
43+74	B.C.			9.2	154.8
+95.0				13.0	151.0
T.P.	0.13	151.63	12.47	151.50	
43+26.12				3.3	148.3
+50				5.1	146.5
+75				6.9	144.7
44+06.24	E.C.			9.1	142.5
+30				10.5	141.1
+47				11.0	140.6
+62				11.3	140.3
+78				11.8	139.8

On sidewalk

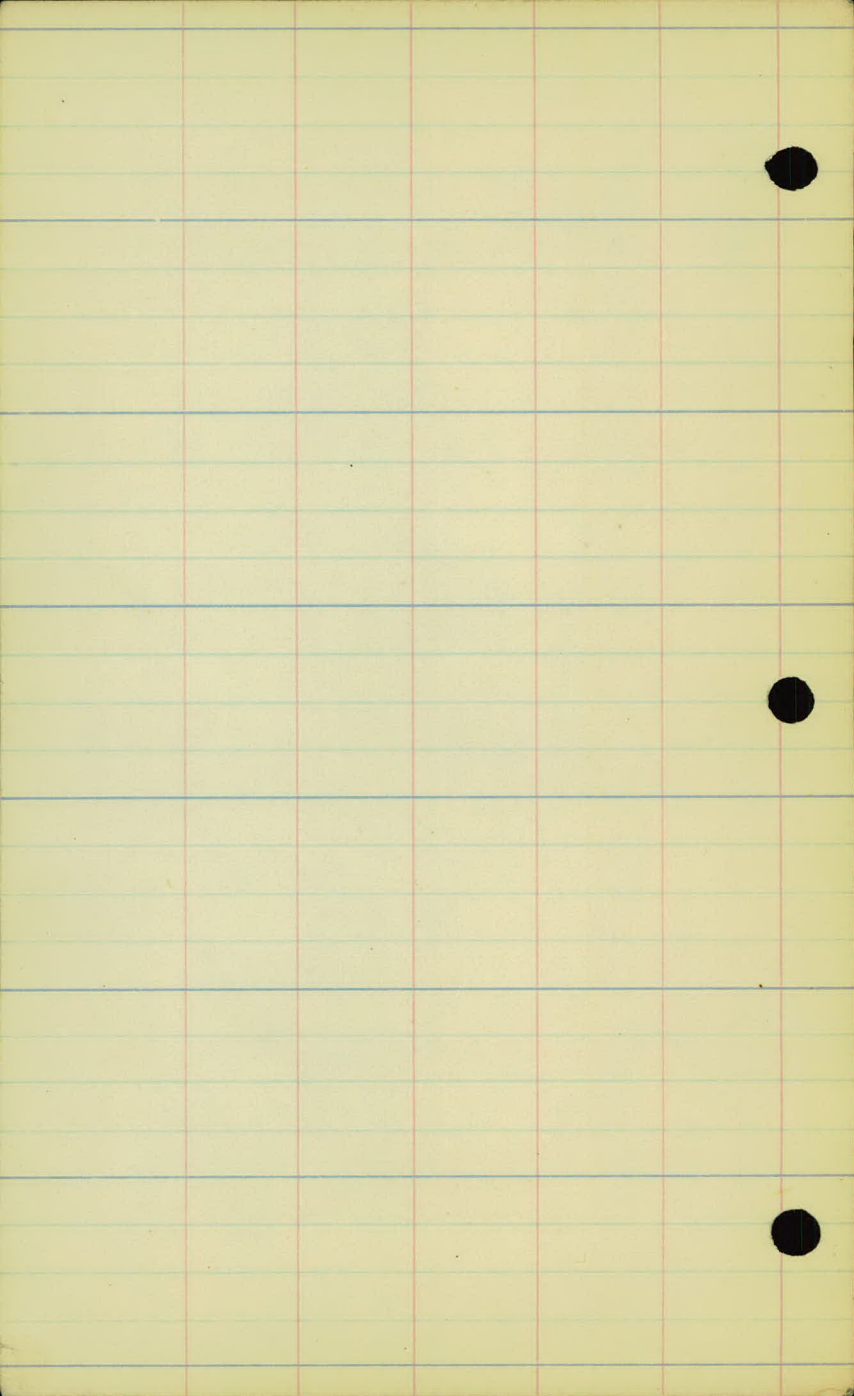
on sidewalk

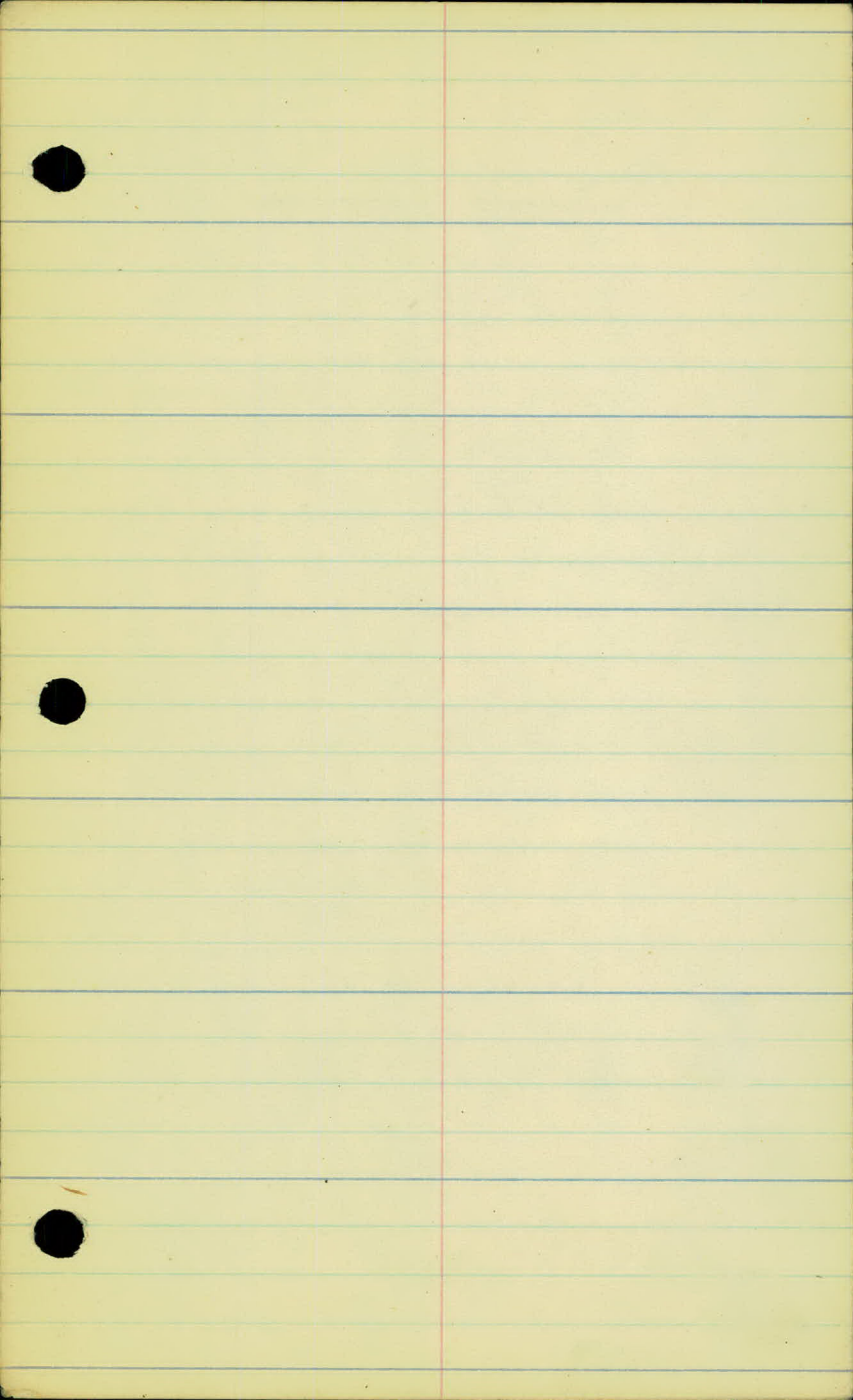
Station	+	H.I.	-	Rod.	Elev.
		151.63			
45+20				12.1	139.5
+70				11.9	139.7
B.M.	6.59	147.27	10.95	<u>140.68</u>	
46+00				7.9	139.4
+50				8.3	142.0
47+00				4.1	143.2
+35				1.9	145.4
+65				4.1	143.2
+85				10.7	136.6
T.P.	4.95	141.44	10.78	136.49	
48+01.36				12.5	128.9
+20				12.5	128.9
+35				13.1	128.3
+50				2.5	138.9
T.P.	12.78	154.01	2.21	139.23	
+80				9.9	142.1

Nail in T.P. lett. 579. 45-120

Station	+	H.I.	-	Rod.	Elev.
		152.01			
49+00				6.0	146.0
+50				3.1	148.9
T.P.			2.00	150.01	
B.M.					
50+00					
+50					
51+00					
+50					
52+00					
+50					
53+00					
+50					
54+10.02					E.C.
+60					
55+00					

Nail in Stump. RR. Sta 49+75





B.M. check 4 = 213 549.50 to 90

Station	+	H. I	-	Red	Elev.
T.P.	11.89	161.90			150.01
B.M.				6.98	152.92
T.P.	11.37	172.92	0.35	161.55	
T.P.	11.64	164.98	0.21	172.64	
B.M.				3.97	180.29
T.P.	10.34	194.49	0.13	184.15	
B.M.				2.13	192.36
T.P.	12.06	207.23	0.12	194.37	
B.M.				4.55	202.69
T.P.	11.77	218.88	0.12	207.11	
T.P.	11.71	230.40	0.19	218.69	
T.P.	11.60	241.87	0.13	230.27	
T.P.	2.04	240.69	3.22	238.65	
B.M.				1.16	239.53
B.M.	1.31	240.84		239.53	
B.M.	2.23	234.06	9.01	231.83	✓
B.M.	1.13	229.14	6.05	229.01	✓
T.P.	0.56	217.14	12.56	216.58	
B.M.				2.97	214.17
T.P.	0.65	206.51	11.28	205.86	
T.P.	0.95	194.59	12.87	193.64	
B.M.	1.15	191.42		4.32	190.29
T.P.	0.92	180.05	12.16	179.26	
T.P.	0.74	169.69	11.13	168.95	
B.M.	1.32	162.40	8.61	161.08	

Nail in Turnpike Rt Sta 49+75
T.P. height Sta. 50+00

Nail in T.P. height Sta 55+00

Nail in T.P. height Sta 58+50

Old B.M. 18" Oak height ✓

Nail in T.P. height Sta 69+25

vv vv vv 69+25

vv vv vv 73+55

Nail in T.P. height Sta 77+80

Nail in T.P., Left Sta 80+65

Nail in T.P. Left Sta 86+00

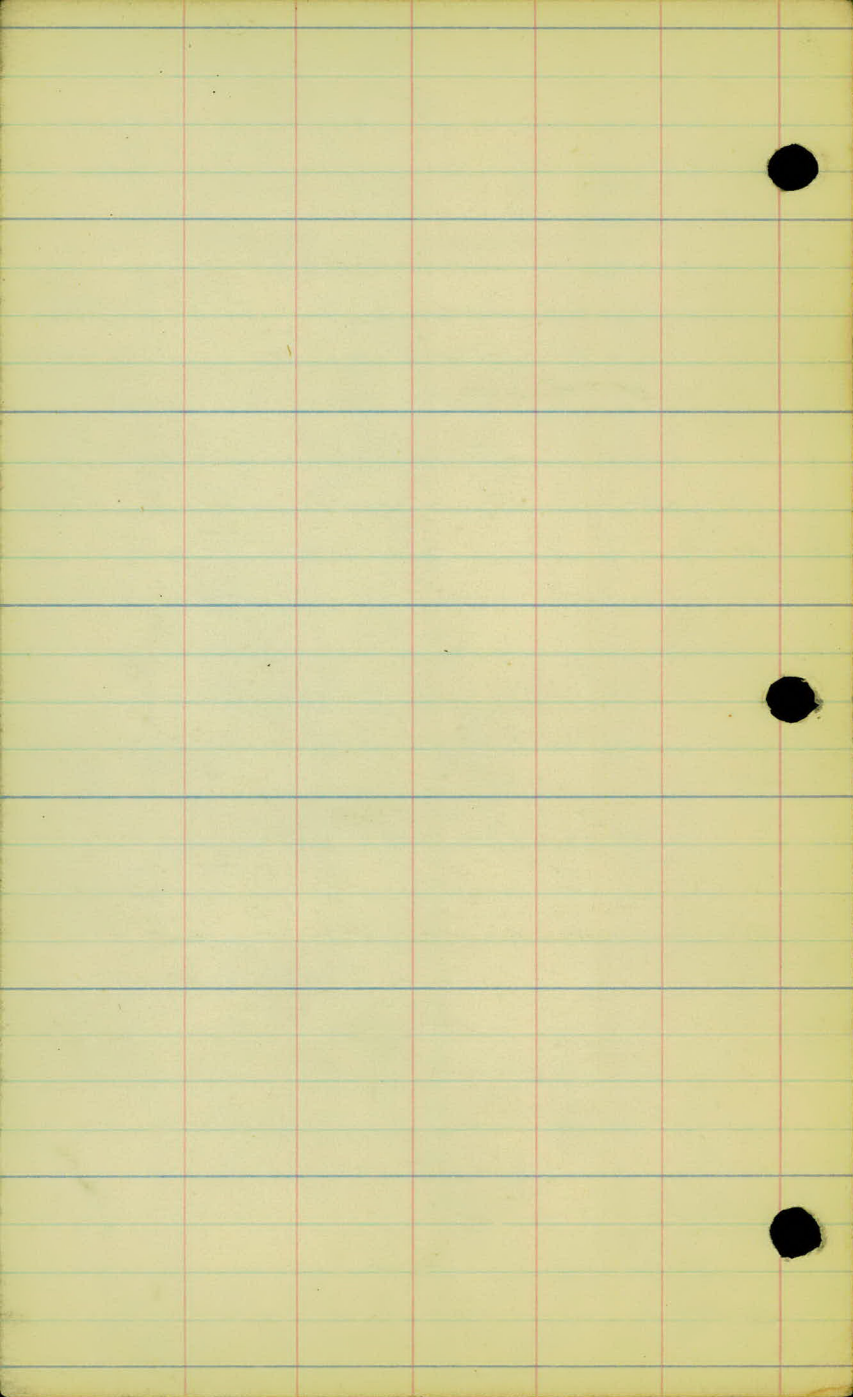
Nail in T.P. height. Sta 95+35

162.40

T. R. 1.56 153.78 10.18 152.22

B. M. 3.76 150.02

Top Hyd. N.E. Cor. Bunn + Hhon. Rd. ✓



Project 24-56

Calvents

Station

- 10+85 Recommend Culvert.
If new road grade follows
close to present Road grade.
- 29+88 12" C.M.P.
Extends 23' RA + 17.5 ft.
Intake Elev. = 193.76
Invert $rr = 193.27$ - Drains RA.
- 42+67 6" x 6" Box Culv.
Indications of a spring under Road.
- 65+90 Recommend 15" C.M.P.

~~301 — 24" P3~~

19+80 F.E.R.

No Culv. Road ✓

Change 25' C.M.s to 24' ✓

↓ 10+80 F.E.R. Pl. 12" x 24' C.M. ✓

↓ 0+00 Road Int. R. ✓

P 18" x 36' C.M. Culv. ✓

3+00 City - 30" Oak C/4Gr ✓

11+00 " - double 20" Oak C/ ✓

↓ 17+10 F.E.R. Pl. 12" x 24' C.M. ✓

19+00 — 20+50

C/ Brush - 16' wide ✓

✓ 25+20 F.E.L. Pl. 15" x 24' ✓

↓ 26+40 F.E.L. Pl. 15" x 24' ✓

✓ 26+30 F.E.R. Pl. 15" x 24' ✓

✓ 27+10 F.E.R. Pl. 15" x 24' ✓

Watch - real estate - Pioneer Bldg
Sweetzer

W. W. Trust Co.

24-56

W. L. Kidder

1959 Upper Afton Rd

✓ 33+10 F.E.L.
Pl. 12" x 24' ✓

✓ 33+70 F.E.R.
Pl. 12" x 24' ✓

36+00 — 38+00
Gravel Pit. on S. Side Road

41+70 F.E.R. & L
P2. 24" x 24' C.M. ✓
Use P2. Headwalk

36+00 — 43+00
Rubble gutter imp - both sides
Include Rubble ditch lining
for standard ditch ✓

✓ 47+00 F.E.R.
Pl. 12" x 24' C.M. ✓

✓ 65+18 F.E.R.
Pl. 12" x 24' ✓

✓ 67+00 F.E.L.
P. 12" x 24' ✓

74+44 Road Int. L.
No curb req.
No ent. on right ✓

79+60 x 79+80
Pl. 12" Pipes ✓

81+10 Pl. 12" Pipe ✓

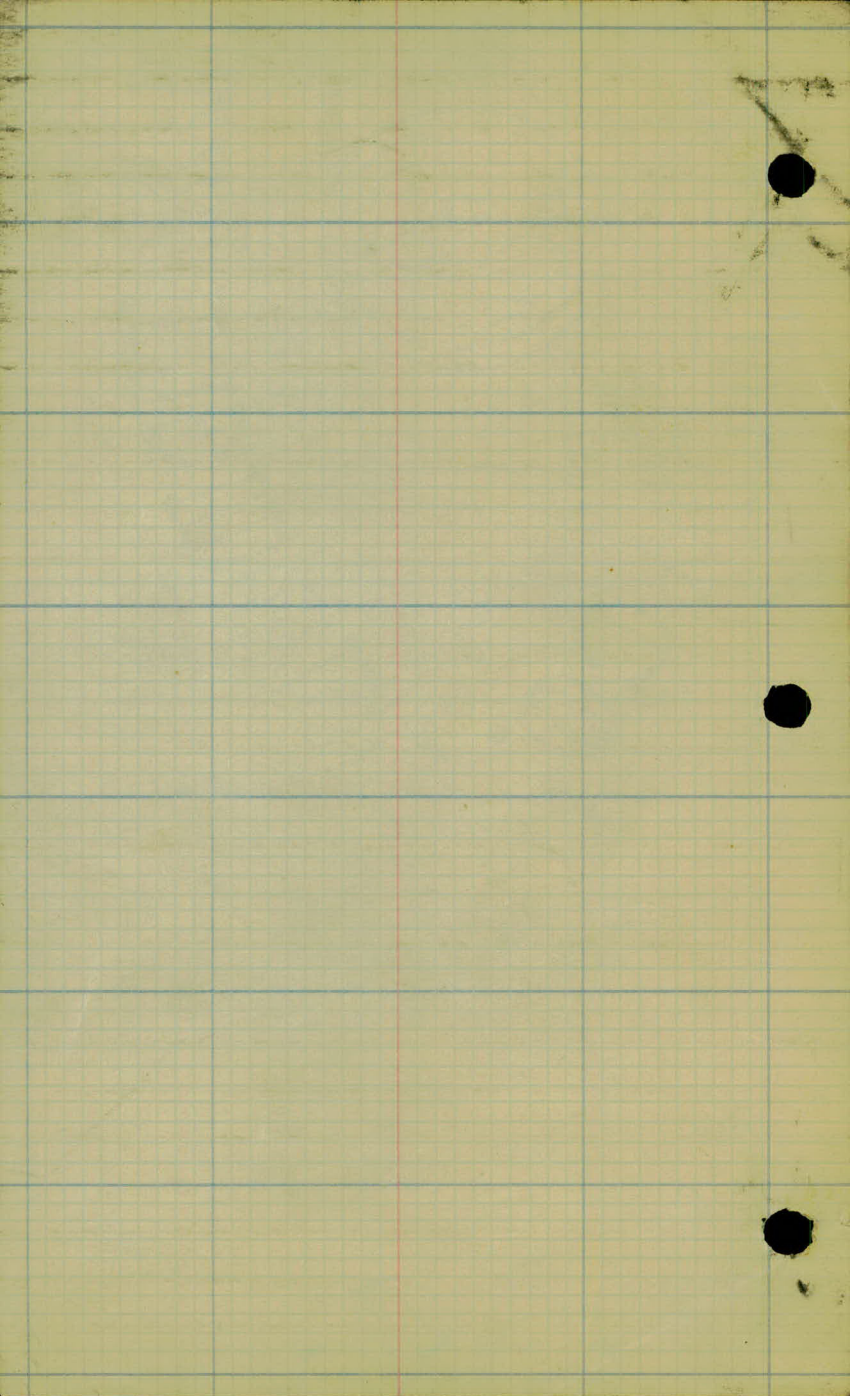
82+40 Pl. 12" Pipe ✓

85+30 Pl. 12" x 24' ✓

87+30 Pl. 12" x 24' ✓

97+75 Pl. 72'-30" P. 3 ✓

24-56



Project 24-56

Levels + X-sections
Sta. 56-69 line change
4 Pages.

E. levels + X sections

line change Sta. 56-69

Station	+	H.I.	—	Rod.	Elev.
B.M.	10.36	190.65			180.29
56+84.9	130.			5.3	185.4 ✓
57+00.				4.9	185.8 ✓
+50				3.4	187.3 ✓
58+00				1.9	188.8 ✓
T.P.	12.49	202.04 ✓	1.10		189.55 ✓
+50				11.4	190.6 ✓
59+00				3.7	198.3 ✓
T.P.	12.61	213.40 ✓	1.25		200.79 ✓
+50				4.9	208.5 ✓
T.P.	6.57	218. ³⁵ ₃₉₁ ✓	1.62		211.78 ✓
+65				7.5	210.9 ✓
+85				4.9	218.6 ✓
60+00				3.8	214.6 ✓
+15				3.3	215.1 ✓
+40				4.6	213.8 ✓

H E H

Nail in T.P. $\frac{1}{2}$ ft 500

-17	-13	-18	-22	-23	-24	-23	-12	-31	-25
50.0	32.0	18.0	15.0	10.0	7.0	4.0	18.0	25.0	50.0

-2.5	-2.2	-3.5	-2.7	0.0	-0.2	-0.2	-1.3	-2.1	-2.0
50.0	32.0	17.0	13.0	9.0	7.0	10.0	14.0	24.0	50.0

-7.7	-7.0	-5.0	0.0	0.0	-0.5	-1.7	-1.3	-2.4
50.0	35.0	22.0	12.0	6.0	10.0	14.0	24.0	50.0

-6.2	-6.7	-5.0	-8.5	-4.0	10.8	-0.3	-0.9	-2.0	-1.5
50.0	43.0	36.0	28.0	20.0	11.0	9.0	25.0	40.0	50.0

-1.5	-2.5	0.0	10.8	11.5	-0.1	+1.5	+3.0
50.0	40.0	38.0	22.0	15.0	7.0	26.0	50.0

-4.5	-5.0	-5.0	-5.0	-3.8	0.0	+1.4	+1.5	+2.0
50.0	37.0	28.0	22.0	17.0	15.0	20.0	37.0	50.0

-11.9	-12.4	-12.7	-5.0	-2.7	-0.9	+1.4	+1.1	+0.5
50.0	43.0	38.0	30.0	26.0	15.0	14.0	32.0	50.0

-13.6	-14.3	-14.2	-12.5	-8.0	-2.3	-1.1	+1.0	+1.0	+0.4
50.0	45.0	41.0	38.0	31.0	30.0	19.0	14.0	25.0	50.0

-14.5	-15.0	-15.0	-11.7	-5.0	-2.5	-1.6	+0.9	+0.9	-0.1
50.0	46.0	42.0	36.0	30.0	29.0	17.0	20.0	43.0	50.0

-14.4	-15.2	-14.1	-11.2	-3.3	-1.1	+1.6	+1.3	+0.7
50.0	41	37	31	27	18.0	18.0	36.0	50.0

-3.1	-14.0	-14.0	-15.3	-11.8	-8.0	-5.0	-1.7	+1.5	+1.8	+1.0
50.0	43	36	33	27	23	18	15	15	27	50

-11.4	-11.1	-12.3	-10.0	-8.5	-6.3	-5.0	-3.0	+3.2	+3.8
37.0	37.0	29.0	16.0	13.0	10.0	6.0	3.0	25.0	50.0

-11.5	-12.5	-11.6
46.0	48.0	50.0

Station + H.I. - Rod. Elev

218.38

60 +42 6.7 211.7

+60 11.9 206.5

T.P. 8.25 215.23 11.47 206.71

+62 10.2 205.0

+74 12.3 202.9
+78 203.0

+93 10.7 204.6

61 +00 L.Rd. 9.6 205.6

+60 10.0 205.2

62 +00 8.9 206.3

+05 8.6 206.6

+40 0.1 215.1

T.P. 11.02 225.86 0.39 214.87

+65 7.7 218.2

+85 7.7 218.2

63 +00 5.6 220.3

$$\begin{array}{r} -4.0 \\ 50.0 \end{array} \quad \begin{array}{r} -3.0 \\ 37.0 \end{array} \quad \begin{array}{r} -3.9 \\ 35.0 \end{array} \quad \begin{array}{r} -3.4 \\ 32.0 \end{array} \quad \begin{array}{r} -3.0 \\ 22.0 \end{array} \quad \begin{array}{r} -3.1 \\ 15.0 \end{array} \quad \begin{array}{r} -4.3 \\ 8.0 \end{array} \quad \begin{array}{r} -1.9 \\ 8.0 \end{array} \quad \begin{array}{r} +1.1 \\ 5.0 \end{array} \quad \begin{array}{r} +3.4 \\ 12.0 \end{array} \quad \begin{array}{r} +5.0 \\ 12.0 \end{array} \quad \begin{array}{r} +6.5 \\ 13.0 \end{array} \quad \begin{array}{r} +8.0 \\ 21.0 \end{array} \quad \begin{array}{r} +1.0 \\ 42.0 \end{array} \quad \begin{array}{r} +1.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 50.0 \end{array} \quad \begin{array}{r} +0.5 \\ 33.0 \end{array} \quad \begin{array}{r} 0.0 \\ 27.0 \end{array} \quad \begin{array}{r} +0.7 \\ 26.0 \end{array} \quad \begin{array}{r} +1.5 \\ 12.0 \end{array} \quad \begin{array}{r} +1.3 \\ 7.0 \end{array} \quad \begin{array}{r} +1.5 \\ 4.0 \end{array} \quad \begin{array}{r} +4.4 \\ 8.0 \end{array} \quad \begin{array}{r} +5.0 \\ 10.0 \end{array} \quad \begin{array}{r} +5.5 \\ 15.0 \end{array} \quad \begin{array}{r} +12.0 \\ 21.0 \end{array} \quad \begin{array}{r} +13.6 \\ 44.0 \end{array} \quad \begin{array}{r} +14.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} -3.0 \\ 50.0 \end{array} \quad \begin{array}{r} -2.1 \\ 26.0 \end{array} \quad \begin{array}{r} -1.1 \\ 13.0 \end{array} \quad \begin{array}{r} -0.5 \\ 7.0 \end{array} \quad \begin{array}{r} -0.1 \\ 12.0 \end{array} \quad \begin{array}{r} -0.6 \\ 16.0 \end{array} \quad \begin{array}{r} -0.5 \\ 20.0 \end{array} \quad \begin{array}{r} +2.0 \\ 22.0 \end{array} \quad \begin{array}{r} +5.0 \\ 28.0 \end{array} \quad \begin{array}{r} +7.9 \\ 40.0 \end{array} \quad \begin{array}{r} +7.1 \\ 50.0 \end{array}$$

$$\begin{array}{r} +2.5 \\ 50.0 \end{array} \quad \begin{array}{r} +0.5 \\ 40.0 \end{array} \quad \begin{array}{r} -1.1 \\ 25.0 \end{array} \quad \begin{array}{r} +1.1 \\ 13.0 \end{array} \quad \begin{array}{r} +3.5 \\ 27.0 \end{array} \quad \begin{array}{r} +1.7 \\ 30.0 \end{array} \quad \begin{array}{r} +3.0 \\ 46.0 \end{array} \quad \begin{array}{r} +4.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} +9.9 \\ 50.0 \end{array} \quad \begin{array}{r} +5.0 \\ 35.0 \end{array} \quad \begin{array}{r} +4.0 \\ 32.0 \end{array} \quad \begin{array}{r} +1.3 \\ 17.0 \end{array} \quad \begin{array}{r} +0.2 \\ 9.0 \end{array} \quad \begin{array}{r} +1.0 \\ 11.0 \end{array} \quad \begin{array}{r} +2.9 \\ 17.0 \end{array} \quad \begin{array}{r} +5.0 \\ 26.0 \end{array} \quad \begin{array}{r} +6.0 \\ 30.0 \end{array} \quad \begin{array}{r} +6.3 \\ 36.0 \end{array} \quad \begin{array}{r} +4.5 \\ 42.0 \end{array} \quad \begin{array}{r} +2.5 \\ 48.0 \end{array} \quad \begin{array}{r} +3.7 \\ 50.0 \end{array}$$

$$\begin{array}{r} +9.0 \\ 50.0 \end{array} \quad \begin{array}{r} +5.0 \\ 32.0 \end{array} \quad \begin{array}{r} +1.7 \\ 17.0 \end{array} \quad \begin{array}{r} -0.6 \\ 11.0 \end{array} \quad \begin{array}{r} +2.1 \\ 24.0 \end{array} \quad \begin{array}{r} +2.0 \\ 31.0 \end{array} \quad \begin{array}{r} -2.5 \\ 42.0 \end{array} \quad \begin{array}{r} -4.5 \\ 47.0 \end{array} \quad \begin{array}{r} -3.5 \\ 50.0 \end{array}$$

$$\begin{array}{r} +7.2 \\ 50.0 \end{array} \quad \begin{array}{r} +5.0 \\ 35.0 \end{array} \quad \begin{array}{r} +1.5 \\ 14.0 \end{array} \quad \begin{array}{r} -0.2 \\ 7.0 \end{array} \quad \begin{array}{r} +0.7 \\ 13.0 \end{array} \quad \begin{array}{r} +0.3 \\ 20.0 \end{array} \quad \begin{array}{r} -1.7 \\ 27.0 \end{array} \quad \begin{array}{r} -2.2 \\ 35.0 \end{array} \quad \begin{array}{r} -5.0 \\ 41.0 \end{array} \quad \begin{array}{r} -5.0 \\ 44.0 \end{array} \quad \begin{array}{r} -4.4 \\ 50.0 \end{array}$$

$$\begin{array}{r} +6.2 \\ 50 \end{array} \quad \begin{array}{r} +5.0 \\ 43 \end{array} \quad \begin{array}{r} +2.2 \\ 2.8 \end{array} \quad \begin{array}{r} +0.8 \\ 11 \end{array} \quad \begin{array}{r} +1.0 \\ 0.4 \end{array} \quad \begin{array}{r} +1.5 \\ 10 \end{array} \quad \begin{array}{r} -0.4 \\ 24 \end{array} \quad \begin{array}{r} -2.0 \\ 30 \end{array} \quad \begin{array}{r} -5.0 \\ 33 \end{array} \quad \begin{array}{r} -3.5 \\ 36 \end{array} \quad \begin{array}{r} -3.0 \\ 44 \end{array} \quad \begin{array}{r} -3.5 \\ 47 \end{array} \quad \begin{array}{r} -5.0 \\ 50 \end{array}$$

$$\begin{array}{r} +2.7 \\ 50 \end{array} \quad \begin{array}{r} +1.5 \\ 39 \end{array} \quad \begin{array}{r} +1.2 \\ 14 \end{array} \quad \begin{array}{r} -1.8 \\ 6 \end{array} \quad \begin{array}{r} +1.5 \\ 4 \end{array} \quad \begin{array}{r} -0.6 \\ 10 \end{array} \quad \begin{array}{r} -1.9 \\ 17 \end{array} \quad \begin{array}{r} -2.7 \\ 22 \end{array} \quad \begin{array}{r} -5.0 \\ 27 \end{array} \quad \begin{array}{r} -4.0 \\ 37 \end{array} \quad \begin{array}{r} -5.0 \\ 47 \end{array} \quad \begin{array}{r} -5.0 \\ 47 \end{array} \quad \begin{array}{r} -5.0 \\ 50 \end{array}$$

Station	+	H.I.	-	Rod	Elev.
		225.89			
63 + 50				6.4	219.5 ✓
+ 60				6.7	219.2 ✓
+ 80	2. Rd			5.2	220.7 ✓
64 + 00				5.1	220.8 ✓
+ 20				2.2	223.7 ✓
T.P.	2.81	235.50	0.17	225.69	
+ 34				4.7	227.8 ✓
+ 50				5.9	229.6 ✓
+ 75				3.4	232.1 ✓
65 + 00				3.9	231.7 ✓
+ 25				5.2	230.3 ✓
+ 37				8.4	227.1 ✓
+ 50				9.2	226.3 ✓
66 + 00				10.3	225.2 ✓

H.

L

3 of 4
A.
$$\begin{array}{r} 4.1 \\ 50.0 \end{array} \quad \begin{array}{r} +0.0 \\ 38.0 \end{array} \quad \begin{array}{r} 15.6 \\ 41.0 \end{array} \quad \begin{array}{r} +5.7 \\ 2.0 \end{array}$$

$$\begin{array}{r} -1.3 \\ 41.0 \end{array} \quad \begin{array}{r} -0.6 \\ 6.0 \end{array} \quad \begin{array}{r} -0.3 \\ 15.0 \end{array} \quad \begin{array}{r} -1.0 \\ 26.0 \end{array} \quad \begin{array}{r} -0.8 \\ 32.0 \end{array} \quad \begin{array}{r} +1.0 \\ 58.0 \end{array} \quad \begin{array}{r} +2.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} -17.7 \\ 50.0 \end{array} \quad \begin{array}{r} +16.6 \\ 36.0 \end{array} \quad \begin{array}{r} 15.0 \\ 32.0 \end{array} \quad \begin{array}{r} -13.0 \\ 27.0 \end{array} \quad \begin{array}{r} +10.6 \\ 22.0 \end{array} \quad \begin{array}{r} +11.2 \\ 10.0 \end{array} \quad \begin{array}{r} +0.7 \\ 3.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 4.0 \end{array} \quad \begin{array}{r} +1.2 \\ 11.0 \end{array} \quad \begin{array}{r} +1.1 \\ 22.0 \end{array} \quad \begin{array}{r} +0.5 \\ 37.0 \end{array} \quad \begin{array}{r} +1.5 \\ 50.0 \end{array}$$

$$\begin{array}{r} +5.0 \\ 45.0 \end{array} \quad \begin{array}{r} +2.5 \\ 40.0 \end{array} \quad \begin{array}{r} +2.5 \\ 37.0 \end{array} \quad \begin{array}{r} -0.5 \\ 38.0 \end{array} \quad \begin{array}{r} -0.4 \\ 20.0 \end{array} \quad \begin{array}{r} -1.0 \\ 12.0 \end{array} \quad \begin{array}{r} -2.0 \\ 10.0 \end{array} \quad \begin{array}{r} -2.0 \\ 7.0 \end{array}$$

$$\begin{array}{r} +1.7 \\ 3.0 \end{array} \quad \begin{array}{r} +0.9 \\ 15.0 \end{array} \quad \begin{array}{r} -0.6 \\ 34.0 \end{array} \quad \begin{array}{r} -1.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} 0.0 \\ 46.0 \end{array} \quad \begin{array}{r} -3.3 \\ 42.0 \end{array} \quad \begin{array}{r} -1.0 \\ 38.0 \end{array} \quad \begin{array}{r} -3.0 \\ 26.0 \end{array} \quad \begin{array}{r} -4.1 \\ 18.0 \end{array} \quad \begin{array}{r} -5.0 \\ 15.0 \end{array} \quad \begin{array}{r} -2.5 \\ 5.0 \end{array} \quad \begin{array}{r} 0.0 \\ 2.0 \end{array}$$

$$\begin{array}{r} -0.3 \\ 11.0 \end{array} \quad \begin{array}{r} -1.8 \\ 25.0 \end{array} \quad \begin{array}{r} -3.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} -5.1 \\ 50.0 \end{array} \quad \begin{array}{r} 5.0 \\ 47.0 \end{array} \quad \begin{array}{r} -5.9 \\ 39.0 \end{array} \quad \begin{array}{r} -5.0 \\ 31.0 \end{array} \quad \begin{array}{r} -4.0 \\ 29.0 \end{array} \quad \begin{array}{r} -1.3 \\ 22.0 \end{array}$$

$$\begin{array}{r} 10.0 \\ 14.0 \end{array} \quad \begin{array}{r} +0.5 \\ 32.0 \end{array} \quad \begin{array}{r} +0.2 \\ 50.0 \end{array}$$

$$\begin{array}{r} -0.4 \\ 50.0 \end{array} \quad \begin{array}{r} +0.7 \\ 45.0 \end{array} \quad \begin{array}{r} -1.2 \\ 35.0 \end{array} \quad \begin{array}{r} -3.0 \\ 29.0 \end{array} \quad \begin{array}{r} -3.0 \\ 14.0 \end{array} \quad \begin{array}{r} -0.2 \\ 4.0 \end{array}$$

$$\begin{array}{r} -0.2 \\ 5.0 \end{array} \quad \begin{array}{r} +1.7 \\ 14.0 \end{array} \quad \begin{array}{r} +3.7 \\ 33.0 \end{array} \quad \begin{array}{r} +5.0 \\ 40.0 \end{array} \quad \begin{array}{r} +5.6 \\ 50.0 \end{array}$$

$$\begin{array}{r} +2.5 \\ 50.0 \end{array} \quad \begin{array}{r} -0.4 \\ 46.0 \end{array} \quad \begin{array}{r} -1.3 \\ 32.0 \end{array} \quad \begin{array}{r} -0.5 \\ 7.0 \end{array}$$

$$\begin{array}{r} +2.3 \\ 10.0 \end{array} \quad \begin{array}{r} +5.0 \\ 24.0 \end{array} \quad \begin{array}{r} +8.0 \\ 50.0 \end{array}$$

$$\begin{array}{r} +5.0 \\ 50.0 \end{array} \quad \begin{array}{r} -13.0 \\ 44.0 \end{array} \quad \begin{array}{r} +11.7 \\ 37.0 \end{array} \quad \begin{array}{r} +0.9 \\ 20.0 \end{array}$$

$$\begin{array}{r} +0.3 \\ 15.0 \end{array} \quad \begin{array}{r} +1.0 \\ 34.0 \end{array} \quad \begin{array}{r} +2.5 \\ 50.0 \end{array}$$

Station	+	H.I.	-	Rod	Elev.
		235.53			
66 + 16.7	130			9.9	225.6 ✓
+ 50				7.3	228.2 ✓
T.T.	8.76	241.24 ²¹	0.05	235.41 ⁴⁵	
67 + 00				8.5	235.7 ✓
+ 50				4.9	239.3 ✓
+ 83				2.7	241.5 ✓
68 + 00				8.6	240.6 ✓
+ 30				4.9	239.3 ✓
+ 64.5	E.C.			5.3	238.9 ✓
B.M.				4.66	239.58 ⁵⁵ 6912.5

A

E

Dof 4

R.

$$\begin{array}{r} +5.0 \quad +2.2 \quad +1.0 \quad 0.0 \quad +0.8 \quad +1.8 \\ \hline 50.0 \quad 35.0 \quad 20.0 \quad 23.0 \quad 40.0 \quad 50.0 \end{array}$$

$$\begin{array}{r} +7.3 \quad +6.7 \quad +5.0 \quad +3.1 \quad -2.6 \quad -1.6 \quad -2.4 \\ \hline 50.0 \quad 44.0 \quad 30.0 \quad 15.0 \quad 6.0 \quad 30.0 \quad 50.0 \end{array}$$

$$\begin{array}{r} \text{d.R.} \\ +1.5 \quad +1.0 \quad +2.7 \quad +2.2 \quad -1.9 \quad -5.0 \quad -6.8 \\ \hline 50.0 \quad 32.0 \quad 25.0 \quad 19.0 \quad 17.0 \quad 25.0 \quad 50.0 \end{array}$$

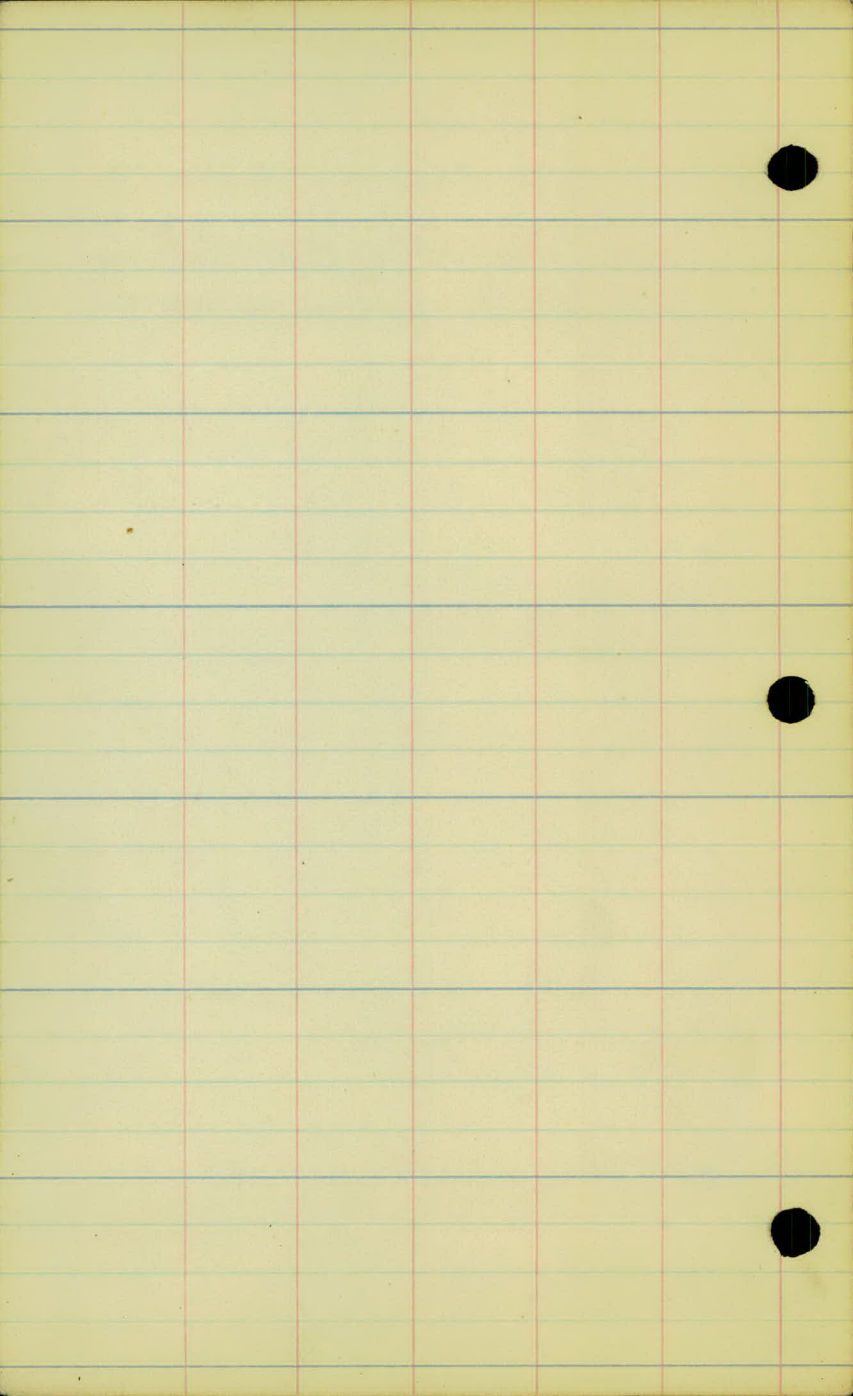
$$\begin{array}{r} \text{d.R.} \\ +1.5 \quad +1.5 \quad -1.1 \quad -0.5 \quad -1.2 \quad +0.9 \quad -1.1 \quad -3.1 \quad -5.0 \quad -7.2 \\ \hline 50.0 \quad 48.0 \quad 42.0 \quad 26.0 \quad 13.0 \quad 9.0 \quad 18.0 \quad 31.0 \quad 41.0 \quad 50.0 \end{array}$$

$$\begin{array}{r} \text{d.R.} \\ +1.0 \quad +1.3 \quad -2.9 \quad -2.4 \quad -2.6 \quad -0.7 \quad -5.0 \quad -7.1 \\ \hline 50.0 \quad 40.0 \quad 33.0 \quad 17.0 \quad 6.0 \quad 13.0 \quad 40.0 \quad 50.0 \end{array}$$

$$\begin{array}{r} +3.0 \quad +3.7 \quad +0.6 \quad -1.6 \quad -1.4 \quad -1.6 \quad +2.2 \quad +1.3 \quad -0.7 \quad -4.7 \\ \hline 50.0 \quad 39.0 \quad 35.0 \quad 30.0 \quad 17.0 \quad 3.0 \quad 4.0 \quad 15.0 \quad 33.0 \quad 50.0 \end{array}$$

$$\begin{array}{r} \text{d.R.} \\ +6.4 \quad +6.7 \quad +5.0 \quad 0.0 \quad +0.3 \quad +1.5 \quad +4.5 \quad +2.3 \quad -1.5 \\ \hline 50.0 \quad 35.0 \quad 22.0 \quad 24.0 \quad 12.0 \quad 4.0 \quad 9.0 \quad 23.0 \quad 20.0 \end{array}$$

$$\begin{array}{r} \text{d.R.} \\ +6.4 \quad +6.2 \quad +5.7 \quad +5.0 \quad +2.4 \quad 0.0 \quad +0.4 \quad +0.2 \quad +4.5 \quad +1.6 \quad +0.3 \\ \hline 50.0 \quad 45.0 \quad 35.0 \quad 30.0 \quad 26.0 \quad 22.0 \quad 8.0 \quad 2.0 \quad 10.0 \quad 21.0 \quad 50.0 \end{array}$$



Project 24-56

Upper. Afton Road.

Levels + X-sections

Sta. 93+26 - 98+86.9

2 Pages.

Station	+	HI	-	Rod	Elev.
B.M.	5.85	167.03 ✓			161.18 ✓
see city book - Page (27)					
93 + 26	B.C.			0.1	166.9 ✓
	+ 50			0.5	166.2 ✓
94 + 00				2.1	164.9 ✓
	+ 50			4.1	162.9 ✓
95 + 00				5.6	161.4 ✓
	+ 28			5.8	161.2 ✓
	+ 50			4.8	162.2 ✓
	+ 60			4.7	162.3 ✓
96 + 00				7.3	159.7 ✓
	+ 50			9.1	157.9 ✓
	+ 56			9.4	157.6 ✓
	+ 80			9.7	157.3 ✓
T.P.	147	155.72 ✓	12.80	154.23 ✓	

Te. Pole. List 95485

$$\frac{+1.0}{50.0} \quad \frac{+0.2}{19.0} \quad \frac{+0.3}{11.0}$$

$$\frac{+0.2}{12.0} \quad \frac{-0.7}{18.0} \quad \frac{-1.4}{29.0} \quad \frac{-3.5}{50.0}$$

$$\frac{+1.6}{50.0} \quad \frac{+0.6}{23.0} \quad \frac{+0.3}{12.0}$$

$$\frac{+0.2}{12.0} \quad \frac{-0.4}{15.0} \quad \frac{-0.9}{22.0} \quad \frac{-2.0}{26.0} \quad \frac{-3.7}{50.0}$$

$$\frac{+1.5}{50.0} \quad \frac{+1.1}{33.0} \quad \frac{+0.1}{20.0} \quad \frac{+0.5}{6.0} \quad \text{E.P.}$$

$$\frac{+0.3}{2.0} \quad \frac{-0.6}{12.0} \quad \frac{-1.5}{27.0} \quad \frac{-3.5}{50.0}$$

$$\frac{+0.0}{50.0} \quad \frac{+0.9}{27.0} \quad \frac{+1.0}{14.0}$$

$$\frac{-0.2}{11.0} \quad \frac{-0.7}{29.0} \quad \frac{-2.0}{50.0}$$

E.P.

$$\frac{+1.0}{50.0} \quad \frac{+0.9}{24.0} \quad \frac{+0.5}{22.0}$$

$$\frac{0.0}{19.0} \quad \frac{-0.2}{34.0} \quad \frac{-0.7}{50.0}$$

$$\frac{+0.3}{50.0} \quad \frac{+0.2}{40.0} \quad \frac{+0.3}{36.0} \quad \frac{+0.6}{26.0}$$

$$\frac{+0.4}{14.0} \quad \frac{+1.1}{48.0} \quad \frac{0.0}{50.0}$$

$$\frac{+0.2}{50.0} \quad \frac{+0.3}{30.0} \quad \frac{+0.6}{17.0}$$

$$\frac{+0.4}{17.0} \quad \frac{+0.7}{31.0} \quad \frac{-0.3}{35.0} \quad \frac{0.0}{42.0} \quad \frac{+1.2}{47.0} \quad \frac{+1.7}{50.0}$$

$$\frac{0.0}{50.0} \quad \frac{0.0}{17.0}$$

$$\frac{+1.0}{6.0} \quad \frac{+2.4}{27.0} \quad \frac{+2.5}{50.0}$$

$$\frac{-2.1}{50.0} \quad \frac{-0.8}{37.0} \quad \frac{+1.0}{33.0} \quad \frac{0.0}{12.0}$$

$$\frac{+1.6}{16.0} \quad \frac{+2.4}{33.0} \quad \frac{+2.1}{50.0}$$

$$\frac{-5.0}{50.0} \quad \frac{-6.5}{39.0} \quad \frac{-6.3}{24.0} \quad \frac{-6.3}{15.0} \quad \frac{-5.0}{10.0}$$

$$\frac{+0.6}{14.0} \quad \frac{+1.5}{31.0} \quad \frac{+1.6}{50.0}$$

Station	+	H.I	-	Rod. Elev.
		155.72		
96 + 90				4.9 150.8 ✓
97 + 00				7.4 148.3 ✓
+ 40				9.1 146.6 ✓
+ 65				10.2 145.5 ✓
B.M.				5.57 150.13 ✓
T.P.	1.77	145.17 ✓	12.32	143.40 ✓
+ 75				3.8 141.4 ✓
+ 90				6.4 138.8 ✓
98 + 00				3.5 141.7 142.7
+ 50				5.3 139.9 ✓
+ 86.9	E.C.			7.0 138.2 ✓

ht.

L

TR

20 of 2

$\frac{+0.8}{50.0}$	$\frac{-0.7}{30.0}$	$\frac{-1.3}{15.0}$	$\frac{-0.8}{10.0}$	$\frac{+1.7}{8.0}$	$\frac{+4.2}{19.0}$	$\frac{-15.0}{24.0}$	$\frac{+6.8}{33.0}$	$\frac{+6.8}{50.0}$
---------------------	---------------------	---------------------	---------------------	--------------------	---------------------	----------------------	---------------------	---------------------

$\frac{+2.6}{50.0}$	$\frac{+3.1}{47.0}$	$\frac{+2.1}{32.0}$	$\frac{+1.1}{18.0}$	$\frac{+0.8}{9.0}$	$\frac{+0.9}{7.0}$	$\frac{+1.5}{18.0}$	$\frac{+3.0}{36.0}$	$\frac{+4.0}{50.0}$
---------------------	---------------------	---------------------	---------------------	--------------------	--------------------	---------------------	---------------------	---------------------

$\frac{-5.0}{50.0}$	$\frac{+1.0}{42.0}$	$\frac{+2.1}{33.0}$	$\frac{+2.4}{27.0}$	$\frac{+0.8}{16.0}$	$\frac{+0.7}{9.0}$	$\frac{-0.4}{10.0}$	$\frac{-0.2}{21.0}$	$\frac{+0.1}{38.0}$	$\frac{-0.4}{50.0}$
---------------------	---------------------	---------------------	---------------------	---------------------	--------------------	---------------------	---------------------	---------------------	---------------------

$\frac{-7.0}{50.0}$	$\frac{-7.7}{40.0}$	$\frac{-7.0}{39.0}$	$\frac{-5.2}{23.0}$	$\frac{-5.0}{9.0}$	$\frac{-3.7}{10.0}$	$\frac{-0.3}{9.0}$	$\frac{-1.2}{14.0}$	$\frac{-1.1}{20.0}$	$\frac{0.0}{30.0}$	$\frac{+0.3}{50.0}$
---------------------	---------------------	---------------------	---------------------	--------------------	---------------------	--------------------	---------------------	---------------------	--------------------	---------------------

Top. Hyd. Burns Ave + Atten Rd.

$\frac{+1.0}{50.0}$	$\frac{-3.5}{41.0}$	$\frac{-3.4}{23.0}$	$\frac{-1.5}{4.0}$	$\frac{+3.4}{7.0}$	$\frac{+3.6}{12.0}$	$\frac{+2.3}{17.0}$	$\frac{+3.4}{30.0}$	$\frac{+3.8}{50.0}$
---------------------	---------------------	---------------------	--------------------	--------------------	---------------------	---------------------	---------------------	---------------------

$\frac{+5.0}{50.0}$	$\frac{+0.7}{42.0}$	$\frac{-1.5}{31.0}$	$\frac{-1.1}{20.0}$	$\frac{0.0}{7.0}$	$\frac{+4.2}{6.0}$	$\frac{+4.6}{11.0}$	$\frac{+3.9}{16.0}$	$\frac{+5.0}{25.0}$	$\frac{+5.5}{46.0}$	$\frac{+2.9}{50.0}$
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$\frac{+2.5}{50.0}$	$\frac{-3.2}{42.0}$	$\frac{-4.8}{35.0}$	$\frac{-4.1}{14.0}$	$\frac{-0.2}{7.0}$	$\frac{+0.8}{4.0}$	$\frac{+0.3}{11.0}$	$\frac{+1.5}{25.0}$	$\frac{+1.5}{36.0}$	$\frac{-1.4}{46.0}$	$\frac{-1.3}{50.0}$
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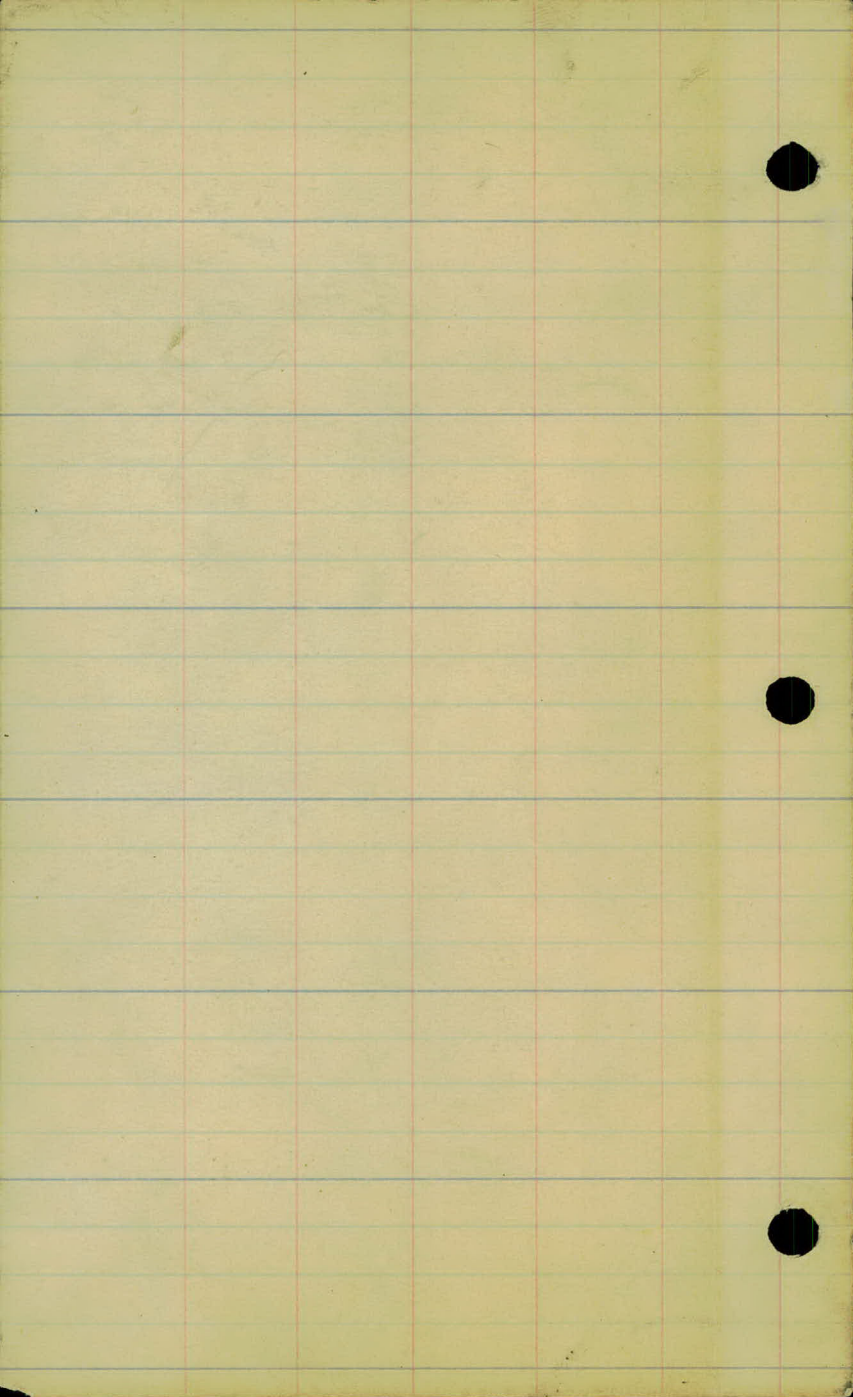
+ $\frac{9.0}{55.0}$

$\frac{+5.0}{50.0}$	$\frac{+0.8}{44.0}$	$\frac{-5.0}{38.0}$	$\frac{-6.0}{30.0}$	$\frac{-5.0}{25.0}$	$\frac{-1.5}{18.0}$	$\frac{0.0}{14.0}$
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$\frac{+0.2}{12.0}$	$\frac{+0.7}{19.0}$	$\frac{-2.1}{26.0}$	$\frac{-2.0}{31.0}$	$\frac{+1.1}{38.0}$	$\frac{+3.1}{50.0}$
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$\frac{+6.0}{50.0}$	$\frac{0.0}{44.0}$	$\frac{-5.0}{36.0}$	$\frac{-6.0}{33.0}$	$\frac{-5.0}{28.0}$	$\frac{-1.8}{23.0}$	$\frac{-0.2}{20.0}$	$\frac{0.0}{10.0}$
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$\frac{+0.2}{6.0}$	$\frac{+0.2}{15.0}$	$\frac{-0.5}{19.0}$	$\frac{-3.0}{21.0}$	$\frac{-2.8}{27.0}$	$\frac{+1.4}{34.0}$	$\frac{+4.5}{43.0}$	$\frac{+4.0}{50.0}$
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UZ469